

WILLIAM T FUJIOKA Chief Executive Officer

## County of Los Angeles CHIEF EXECUTIVE OFFICE

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http://ceo.lacounty.gov
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October 08, 2013

The Honorable Board of Supervisors County of Los Angeles
383 Kenneth Hahn Hall of Administration
500 West Temple Street
Los Angeles, California 90012
Dear Supervisors:

ADOPIED
BOARD OF SUPERVISORS COUNTY OF LOS ANGELES
\#56
October 8, 2013


SET: November 26, 2013 @ 9:30 a.m.

> DEPARTMENT OF PUBLIC WORKS:
> EAST ANTELOPE VALLEY ANIMAL CARE CENTER PROJECT ADOPT MITIGATED NEGATIVE DECLARATION AND MITIGATION MONITORING AND REPORTING PROGRAM APPROVE PROJECT AND BUDGET AWARD DESIGN-BUILD CONTRACT AUTHORIZE LOCAL WORKER HIRING PROGRAM APPROVE AND ORDER PUBLICATION OF NOTICE OF INTENTION TO PURCHASE REAL PROPERTY AND APPROVE RELATED ACTIONS SPECS. 7003; CAPITAL PROJECT NO. 69570 (FIFTH DISTRICT)
> (3 VOTES)

## SUBJECT

Approval of the recommended actions will adopt the Mitigated Negative Declaration and Mitigation Monitoring and Reporting Program; approve the Project and budget; award the design-build contract; authorize a Local Worker Hiring Program; and authorize the acquisition of land for the implementation of the East Antelope Valley Animal Care Center Project in the City of Palmdale.

## IT IS RECOMMENDED THAT THE BOARD:

1. Consider the Mitigated Negative Declaration for the County of Los Angeles Animal Care Center Project, Palmdale, California (subsequently the East Antelope Valley Animal Care Center), together with any comments received during the public review period; find that the Mitigated Negative Declaration reflects the independent judgment and analysis of the Board; adopt the Mitigation Monitoring and Reporting Program, finding that the Mitigation Monitoring and Reporting Program is

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adequately designed to ensure compliance with the mitigation measures during Project implementation, and find on the basis of the whole record before the Board that there is no substantial evidence the Project will have a significant effect on the environment; and adopt the Mitigated Negative Declaration.
2. Approve the East Antelope Valley Animal Care Center Project (also known as East Antelope Valley Animal Shelter), Capital Project No. 69570, with a total budget of $\$ 20,100,000$.
3. Find that KPRS Construction Services, Inc., is the Responsive and Responsible bidder that submitted the most advantageous and best value proposal for the East Antelope Valley Animal Care Center Project, and award a design-build contract to KPRS Construction Services, Inc., for a contract sum of $\$ 14,874,000$, contingent upon submission of acceptable performance and payment bonds, and evidence of required insurance filed by KPRS Construction Services, Inc.
4. Authorize the implementation of a Local Worker Hiring Program for the East Antelope Valley Animal Care Center Project and find that the program furthers a legitimate governmental interest for the reasons stated in this letter and in the Project files.
5. Approve the Notice of Intention to acquire a 5.94 acre parcel of unimproved real property from the City of Palmdale located on the east side of the 38500 block of Sierra Highway in the City of Palmdale for the monetary consideration of $\$ 20,125$ to implement the East Antelope Valley Animal Care Center Project.
6. Instruct the Executive Officer of the Board of Supervisors to publish the Notice of Intention in accordance with Government Code Section 6063.
7. Find that the property described in the Notice of Intention is needed for a public purpose and set the date for a Public Hearing to receive comments and consummate the proposed transaction.

## IT IS FURTHER RECOMMENDED THAT, AT THE TIME OF CONSUMMATION, THE BOARD:

8. Order the purchase consummated in accordance with Government Code Section 25350. Approve and instruct the Chair of the Board to sign the Agreement for Purchase and Sale of Real Property together with the easements (Exhibit D - Common Driveway Easement and Exhibit F - Access Easement, respectively) with the seller, City of Palmdale, to acquire the subject property.
9. Authorize the Chief Executive Office to open and manage escrow, execute any required documentation necessary to complete the transfer of title to the County of Los Angeles, and accept the easements and deed conveying title to the County of Los Angeles.
10. Authorize the Auditor-Controller to issue a warrant to cover the purchase price of $\$ 20,125$ for the real property and any other required transactional costs or escrow fees, which are estimated not-toexceed \$5,000.
11. Authorize the Chief Executive Office to dedicate a portion of the acquired property to the City of Palmdale for road right-of-way purposes to create a new public sidewalk and right turn lane along Sierra Highway in connection with the development of the East Antelope Valley Animal Care Center Project.

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The purpose of the recommended actions will allow the County of Los Angeles (County) Department of Public Works (Public Works) to implement the new East Antelope Valley Animal Care Center (Project) in the City of Palmdale.

## Project Background and Description

The existing Lancaster Animal Care Center is experiencing high service demands due to the increasing animal population in the north County area. Over the past several years, the Department of Animal Care and Control (Department) has been looking for possible sites on the east side of the Antelope Valley to address the increased services required by the north County communities.

The Department, Chief Executive Office (CEO), and the City of Palmdale (City) have been working to identify possible real properties for the development of a new animal care center. The City has identified City-owned property located just south of the County Palmdale Sheriff Station to develop and implement a new animal care center. The City has agreed to sell to the County approximately 5.94 acres of undeveloped property located on the east side of the 38500 block of Sierra Highway, north of Avenue Q-6.

The proposed Project will consist of approximately 25,500 square feet indoor facility, including a public entry lobby; public adoption; space for animal relinquishment, control, quarantine, and euthanasia; a veterinary and spay/neuter clinic; and staff and administration areas.

The proposed Project will also include associated site improvements, including underground utility connections to serve the facility, separate staff and public parking areas, outdoor fenced exercise yard areas for the animals; walkways; security lighting; and drought-tolerant landscape. In addition, the Project will include offsite improvements, including a new landscaped parkway and dedicated right turn lane along Sierra Highway to serve the proposed new animal care center.

## Design-Build Contract Award

On August 23, 2012, Public Works issued a Request for Proposals (RFP) for design-build services for the proposed Project. The initial total project cost prior to the release of the RFP was estimated at $\$ 18,000,000$, which included a design-build contract cost estimate of $\$ 13,500,000$. A total of five firms submitted prequalification questionnaires in response to the RFP, and the three highest scoring prequalified proposers were invited to participate in the second part of the RFP for submission of technical and cost proposals. Based on the criteria stated in the RFP, KPRS Construction Services, Inc. (KPRS), submitted the most advantageous and best value proposal for design and construction of the proposed Project.

KPRS's base price proposal of $\$ 14,874,000$ was $\$ 1,374,000$ higher than the amount of $\$ 13,500,000$ estimated for the design-build contract amount, which includes furniture, fixtures, equipment, and low-voltage/telecommunication systems. This base price proposal is within 10 percent of the estimated design-build contract amount, and we consider it to be reasonable for the proposed Project scope of work. Based on the current market conditions, we do not anticipate receiving more favorable price proposals by readvertising the proposed Project.

As part of subsequent negotiations with KPRS, a Local Worker Hiring Program (LWHP) was added to the Project at the request of the County, which resulted in no net change to the base price proposal of $\$ 14,874,000$. Therefore, we recommend awarding the design-build contract for a contract sum of $\$ 14,874,000$ to KPRS.

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## Land Acquisition

The County and the City cooperatively evaluated potential sites in the Palmdale area and selected the proposed site owned by the City for the new animal care center location. The proposed site is located on the east side of the 38500 block of Sierra Highway, north of Avenue Q-6, in the City of Palmdale, and consists of approximately 5.94 acres of unimproved land. The proposed site is adequate in size and shape to accommodate the proposed improvements, compatible with the existing surrounding land uses, and directly accessible from Sierra Highway.

The County, in coordination with the City, has completed all of the necessary due diligence activities for the property, including environmental site assessments, geotechnical studies, and title review. In addition, the County has completed the Final Mitigated Negative Declaration (MND) for the proposed Project.

The parties have agreed that consideration for this transaction shall be a one-time only cash payment of $\$ 20,125$ to the City for the County's proportional share to contribute to the City's maintenance and repair in perpetuity for use of the City's existing driveway area pursuant to the Common Driveway Easement granted by the City to the County (Exhibit D of Attachment D), which will serve as the primary public access for the new animal care center.

The City Council is scheduled to approve and execute the Agreement for Purchase and Sale of Real Property (Agreement) (Attachment D) on November 6, 2013, after the County adopts the Final MND for the proposed Project.

## Local Worker Hiring Program

According to the Factual Predicate Study prepared in 2010, the proposed Project's location is surrounded by zip codes with unemployment rates in excess of 150 percent of the average County unemployment rate. Within a five-mile radius of the proposed Project, four of the six zip codes ( $93534,93536,93550$, and 93552 ) have an unemployment rate in excess of 150 percent of the average unemployment rate for the County. Beyond the five-mile radius, there are an additional 148 zip codes that have an unemployment rate in excess of 150 percent of the unemployment rate for the County.

Therefore, it is recommended that a LWHP be implemented for the proposed Project in the City of Palmdale with the following key elements:

- The design-builder is required to make a good-faith effort to employ qualified local workers to perform at least 30 percent of the total California craft worker hours.
- "Local residency" is defined with a two-tier system - first preference will be given to qualified workers residing within the County in zip codes within a five-mile radius of the proposed Project in the City of Palmdale; and second preference given to qualified workers residing within the County in any zip code having an unemployment rate in excess of 150 percent of unemployment rate for the County as a whole or a Bank Enterprise Award Distressed Community.


## Green Building/Sustainable Design Program

The proposed Project will comply with the County's Energy and Environmental Policy by achieving the United States Green Building Council Leadership in Energy and Environmental Design Silver

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level certification by incorporating sustainable design features to optimize energy and water use efficiency, enhance the sustainability of the site, improve indoor environmental quality, and maximize the use and reuse of sustainable and local resources.

## Implementation of Strategic Plan Goals

The Countywide Strategic Plan directs the provision of Operational Effectiveness (Goal 1) and Integrated Services Delivery (Goal 3), by investing in public infrastructure that will provide improved animal care and control services for County residents.

## FISCAL IMPACT/FINANCING

The total proposed Project cost, including land acquisition, scoping documents, consultant services, plan check, construction, furniture and equipment, civic art, telecommunications, miscellaneous expenditures, and County services, is currently estimated at $\$ 20,100,000$. Prior to the release of the RFP, the total Project cost was estimated at $\$ 18,000,000$, which included a design-build contract cost estimate of $\$ 13,500,000$. The bid of $\$ 14,874,000$, proposed by KPRS increased the estimated total Project cost by $\$ 2,100,000$ due to an increase in the Civic Arts allocation, the change order contingency, utilities, etc.

The construction cost of \$16,916,000 includes the recommended design-build contract with KPRS for $\$ 14,874,000$, a change order contingency fund of $\$ 1,487,400$, and $\$ 554,600$ for other construction items, such as civic art, telecommunication equipment, and other fees. The monetary compensation for the unimproved land is $\$ 20,125$, and approximately $\$ 5,000$ for the related title, escrow, and other related transactional costs necessary to consummate the transaction. Sufficient appropriation and financing will be included in Fiscal Year (FY) 201314 Supplemental Resolution. The Project Schedule and Budget Summary are detailed in Attachment A.

The proposed Project will be funded by $\$ 1,090,000$ Vehicle License Fees and $\$ 19,010,000$ taxexempt commercial paper, which will be ultimately financed through the issuance of long-term bonds. The par amount of each bond type to be issued will be based on market conditions and discussions with the Treasurer and Tax Collector and presented to the Board for approval prior to implementation of the financing.

In order for the Department to retain the current scope of the proposed Project, the Department's Operating Budget will contribute 10 percent per year towards the annual payment of the long-term bonds, not to exceed $\$ 336,000$ per year, due to the savings from the Department's completion of the repayment of Asset Development Improvement Fund loan in FY 2014-15.

## Operating Budget

Following completion of the proposed Project, the Department will work with the CEO to determine the appropriate level of associated maintenance and operational costs for the new indoor animal care center and will request funding as required.

## FACTS AND PROVISIONS/LEGAL REQUIREMENTS

Pursuant to the Board's Civic Art Policy adopted on December 7, 2004, and amended on December 15, 2009, the proposed Project budget includes one percent of design and construction costs to be allocated to the Civic Art Fund.

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Carde Ten Architects was contracted by the County to provide programming services, preparation of scoping documents, and design-build support services for the proposed Project. As part of the design-build support services, Carde Ten Architects assisted the County in the evaluation of the technical and cost proposals submitted by the prospective design-build firms, and will assist the County in reviewing the selected design builder's design and construction documents for conformance with the scoping documents.

Pursuant to Government Code Section 25350, the Notice of Intention (Attachment C) will be published in accordance with Government Code Section 6063 for the intended action to purchase real property, and a Public Hearing will be held for the Board to receive comments prior to consummating the acquisition.

Public Works, in accordance with Title 7, Division 1, Chapter 3, Article 7, Section 65402(b) of the Government Code; and notice under Title 22, Section 22.36.10 of the Los Angeles County Code as required for public agencies when acquiring real property interests for public purposes, has provided notification to the City's Planning Commission of the County's intent to acquire the real property. The City acknowledged that the subject parcel would be considered within public facility land use designation and in conformance with the City's General Plan.

A preliminary title report has been issued and reveals no claims or encumbrances, which would significantly affect or impair the subject property's title. Additionally, as required by Government Code Section 65402, the proposed acquisition was submitted to the City's Planning Commission for review and they have determined that the proposed Project is in accordance with the adopted land uses and design parameters permitted by the City. County Counsel has reviewed the Notice of Intention (Attachment C) and Purchase and Sale Agreement (Attachment D) in connection with this transaction and has approved them as to form.

The Agreement includes a clause that both the City and County agree to dedicate portions of their respective properties for road right-of-way purposes in order to create a new public sidewalk and right turn lane along Sierra Highway in connection with the County's development of the new animal care center.

## ENVIRONMENTAL DOCUMENTATION

An Initial Study for the County of Los Angeles Animal Care Center, Palmdale, CA Project (subsequently East Antelope Valley Animal Shelter) was prepared in compliance with the California Environmental Quality Act (CEQA). The Initial Study identified potentially significant effects of the proposed Project on cultural resources; geology and soils; and hazards and hazardous materials. However, prior to the release of the proposed MND and Initial Study for public review, revisions to the proposed Project were made or agreed to, which would avoid these effects or mitigate them to a point where clearly no significant effects would occur as follows:

- Cultural Resources: In the event that archeological materials or subsurface deposits are exposed during ground disturbance, findings shall be evaluated by a qualified archaeologist in accordance with existing law and appropriate treatment measures implemented; and in the event that human remains are encountered during Project construction, the Department of Medical Examiner-Coroner shall be immediately contacted to determine whether or not investigation of the cause of death is required and to determine procedures for handling of remains in accordance with existing law.

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- Geology and Soils: Design and construct the proposed Project in accordance with the Projectspecific geotechnical requirements and recommendations included in the Final MND.
- Hazards and Hazardous Materials: In the event that soil contamination is encountered during earthwork activities, all contaminated soil handling and removal will be required to adhere to a soil management plan prepared and approved by the County. The soil management plan will specify procedures for the proper handling and disposal of contaminated soil in accordance with all applicable local and State regulations.

The Initial Study and proposed Project revisions showed that there is no substantial evidence, in light of the whole record before the County, that the proposed Project as revised may have a significant effect on the environment. Based on the Initial Study and proposed Project revisions, an MND was prepared for the proposed Project. The proposed Mitigation Monitoring and Reporting Program (Section 6 of Attachment B) was prepared to ensure compliance with the environmental mitigation measures included as part of the final MND (Attachment B) relative to these areas during Project implementation. There has been no substantial revision of the MND since public circulation that would result in a new avoidable significant effect and previously proposed mitigation measures and Project revisions will ensure that all significant environmental effects are reduced to below the level of significance.

Public Notice was published in the Antelope Valley Press on April 25, 2013, pursuant to Public Resources Code Section 21092 and posted pursuant to Section 21092.3. During the 30-day comment period, which started on April 25, 2013, and ended on May 24, 2013, no comments were received from members of the public. Comment letters were received from the following three public agencies: Antelope Valley Air Quality Management District; the City of Palmdale; and the State of California, Governor's Office of Planning and Research. All comments received, as well as responses to the comments, are contained in the final MND (Section 7 of Attachment B) and have been sent to the commenting public agencies pursuant to Section 21092.5 of the Public Resources Code.

The location of the documents and other materials constituting the record of the proceedings upon, which the Board's decision is based in this manner is the County Public Works, Project Management Division I, 900 South Fremont Avenue, 5th Floor, Alhambra, California 91803. The custodian of such documents and materials is Jason Kim, Project Manager, Public Works.

The proposed Project is not exempt from payment of a fee to the California Department of Fish and Wildlife pursuant to Section 711.4 of the Fish and Game Code to defray the costs of fish and wildlife protection and management incurred by the California Department of Fish and Wildlife. Upon the Board's adoption of the MND, Public Works will file a Notice of Determination in accordance with Section $21152(\mathrm{a})$ of the California Public Resources Code and pay the required filing and processing fees with the Registrar-Recorder/County Clerk in the amount of $\$ 2,231.25$.

## CONTRACTING PROCESS

On August 23, 2012, Public Works issued the RFP for design-build services, including the standardized prequalification questionnaire, while the scoping documents were being prepared. This contract opportunity was listed in the County's "Doing Business with Us" website. The first part of the RFP required prospective design-build firms to submit responses to the standardized prequalification questionnaire. On October 4, 2012, five firms submitted prequalification questionnaires. Additionally, the RFP specified that the three highest scoring prequalified proposers

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would be short-listed and invited to participate in the second part of the RFP for submission of technical and cost proposals. The three short-listed firms were KPRS, Mallcraft, Inc., and Sinanian Development, Inc.

On March 14, 2013, Public Works requested technical and cost proposals from the three short-listed prequalified firms and on May 23, 2013, technical and cost proposals were received. On June 18, 2013, the proposals were evaluated and ranked based on technical design and construction expertise, design-build team personnel and organization, proposed delivery plan and schedule, price, life cycle costs, skilled labor force availability, and acceptable safety record. The evaluation was completed without regard to race, creed, color, or gender. The KPRS proposal received the highest score and was determined to be the best value in accordance with the provisions of the RFP. A scoring summary of the proposals is included in Attachment E .

A standard design-build contract, in a form previously approved by County Counsel, will be used. The contract will contain terms and conditions supporting the Board's ordinances, policies, and programs, including, but not limited to, County's Greater Avenues for Independence (GAIN) and General Relief Opportunities for Work (GROW) Programs, Board Policy No. 5.050; Contract Language to Assist in Placement of Displaced County Workers, Board Policy No. 5.110; Reporting of Improper Solicitations, Board Policy No. 5.060; Notice to Contract Employees of Newborn Abandonment Law (Safely Surrendered Baby Law), Board Policy No. 5.135; Contractor Employee Jury Service Program, Los Angeles County Code, Chapter 2.203; Notice to Employees regarding the Federal Income Credit (Federal Income Tax Law, Internal Revenue Service Notice 1015); Contractor Responsibility and Debarment, Los Angeles County Code, Chapter 2.202; the Los Angeles County's Child Support Compliance Program, Los Angeles County Code, Chapter 2.200; and the standard Board-directed clauses that provide for contract termination and renegotiation.

## IMPACT ON CURRENT SERVICES (OR PROJECTS)

Approval of the recommended actions will have no impact on current animal care and control services. The residents of the Antelope Valley will continue to be served by the existing Lancaster Animal Care Center during design and construction of the proposed Project.

## CONCLUSION

Please return all three submitted original copies of the signed Agreement for forwarding to the City for its signature and one adopted copy of this Board letter to the Chief Executive Office, Facilities and Asset Management Division. Also, please forward additional adopted copies of the Board letter to the Department of Animal Care and Control and the Department of Public Works, Project Management Division I. Once the City's signature has been obtained, a fully executed original copy of the Agreement will be returned to your office.

The Honorable Board of Supervisors
10/8/2013
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Respectfully submitted,


## WILLIAM T FUJIOKA

Chief Executive Officer

WTF:SHK:DJT
DKM:CF:zu

Enclosures
c: Executive Office, Board of Supervisors
County Counsel
Animal Care and Control
Arts Commission
Public Works

## ATTACHMENT A

DEPARTMENT OF PUBLIC WORKS:
EAST ANTELOPE VALLEY ANIMAL CARE CENTER PROJECT ADOPT MITIGATED NEGATIVE DECLARATION AND MITIGATION MONITORING AND REPORTING PROGRAM

## APPROVE PROJECT AND BUDGET

AWARD DESIGN-BUILD CONTRACT
AUTHORIZE LOCAL WORKER HIRING PROGRAM
APPROVE AND ORDER PUBLICATION OF NOTICE OF INTENTION TO PURCHASE REAL PROPERTY AND APPROVE RELATED ACTIONS SPECS. 7003; CAPITAL PROJECT NO. 69570
I. PROJECT SCHEDULE

| Project Activity | Scheduled <br> Completion Date |
| :--- | :---: |
| Scoping Document Contract Award | $05 / 23 / 2011^{*}$ |
| Prequalify Design-Builders | $03 / 14 / 2013^{*}$ |
| Award Design-Build Contract | $10 / 08 / 2013$ |
| Construction Documents | $07 / 17 / 2014$ |
| Jurisdictional Approvals | $10 / 15 / 2014$ |
| Construction Start | $10 / 20 / 2014$ |
| Substantial Completion | $04 / 07 / 2016$ |
| Final Acceptance | $06 / 06 / 2016$ |
| Grand Opening | $07 / 07 / 2016$ |

* Actual completion date.

Attachment A
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## II. PROJECT BUDGET SUMMARY



[^0]DEPARTMENT OF PUBLIC WORKS:
EAST ANTELOPE VALLEY ANIMAL CARE CENTER PROJECT ADOPT MITIGATED NEGATIVE DECLARATION AND MITIGATION MONITORING AND REPORTING PROGRAM

APPROVE PROJECT AND BUDGET
AWARD DESIGN-BUILD CONTRACT
AUTHORIZE LOCAL WORKER HIRING PROGRAM
APPROVE AND ORDER PUBLICATION OF NOTICE OF INTENTION TO PURCHASE REAL PROPERTY AND APPROVE RELATED ACTIONS

SPECS. 7003; CAPITAL PROJECT NO. 69570
MITIGATED NEGATIVE DECLARATION
(SEE ATTACHMENT)

Final Mitigated Negative Declaration

# County of Los Angeles Animal Care Center Project Palmdale, CA 

Prepared for<br>County of Los Angeles Department of Public Works

Irvine, California 92617

# COUNTY OF LOS ANGELES ANIMAL CARE CENTER PROJECT PALMDALE, CALIFORNIA 

## FINAL MITIGATED NEGATIVE DECLARATION

The Initial Study/Proposed Mitigated Negative Declaration (Draft IS/MND) for the County of Los Angeles Animal Care Center Project, Palmdale, California (project) was circulated for a 30-day public review period, beginning on April 25, 2013 and ending on May 24, 2013. The public review period, during which interested agencies, organizations, and members of the public were invited to submit written comments, was noticed and conducted in compliance with CEQA Section 21091 and State CEQA Guidelines 15105. During the 30-day public review period, three comment letters were received. The comments on the Draft IS/MND and responses to comments have been incorporated into this Final MND. The comments received did not result in changes to the Draft IS/MND text, analysis or mitigation.

Since circulation of the Draft IS/MND, minor corrections, additions and refinements have been made that update, clarify, amplify or represent insignificant modifications. Changes to the Draft IS/MND include:

- Minor editorial and grammatical corrections have been made to Section 6, Mitigation Monitoring and Reporting Program, to provide improved readability;
- Revision to mitigation measure MM HAZ-1 throughout the document to provide improved readability and amplify the intent of the measure;
- The addition as appendices of two geotechnical reports referenced within the Draft IS/MND; and,
- The addition of one new added section, Section 7, Response to Comments, which includes copies of the three comment letters associated with public review of the Draft IS/MND and corresponding responses.

The changes noted above do not result in any new significant impacts or an increase in the severity of any previously identified impacts. The revised mitigation measure (MM HAZ-1) is essentially the same measure and provides the same level of mitigation. The addition of
the two geotechnical reports that were previously referenced in the Draft IS/MND and part of the administrative record are being included as appendices because they are projectspecific studies that are noted in, and provide details associated with, mitigation measures MM SOILS-1 and MM SOILS-2.

This Final MND consists of the Draft IS/MND, including all technical appendices, this introduction, the revisions and clarifications section to the Draft IS/MND, as well as incorporation of those revisions and clarifications. The County of Los Angeles Board of Supervisors (Board) will use the Final MND for all environmental decisions related to the project. Prior to approving the project, the Board will consider the project in conjunction with comments received during the public review period. A project will only be approved when the Board "finds that there is no substantial evidence that the project will have a significant effect on the environment and that the [IS/MND] reflects the lead agency's independent judgment and analysis." When adopting a Final MND, a mitigation monitoring and reporting program (MMRP) must also be adopted to ensure implementation of mitigation measures required as a condition of approval. The MMRP is included in Section 6 of the Final MND.

# Revisions and Clarifications 

# County of Los Angeles Animal Care Center Project Palmdale, CA 

Final Mitigated Negative Declaration

## Revisions and Clarifications

The Initial Study/Proposed Mitigated Negative Declaration (Draft IS/MND) for the County of Los Angeles Animal Care Center Project, Palmdale, California (project) was circulated for a 30-day public review period, beginning on April 25, 2013 and ending on May 24, 2013. During the 30-day public review period, three comment letters were received. The comments on the Draft IS/MND and responses to comments have been incorporated into this Final MND. The comments received did not result in changes to the Draft IS/MND text, analysis or mitigation; however, minor revisions to the Draft IS/MND have been made to make minor corrections and additions that update, clarify, amplify or represent insignificant modifications.

Pursuant to Section 15073.5 of the State CEQA Guidelines, recirculation of a negative declaration is required when a document must be substantially revised after public notice has been given. A "substantial revision" is defined under this section to mean:
a) A new, avoidable significant effects have been identified and mitigation measures or project revisions must be added in order to reduce the effect to insignificance, or
b) The Lead Agency determines that the proposed mitigation measures or project revisions will not reduce potential effects to less than significant and new measures or revisions must be required.

Minor editorial revisions and grammatical modifications, not necessarily noted in this summary, have been incorporated. Editorial and grammatical corrections were limited to those that would not change the project scope or any findings and conclusions as presented in the original document; therefore, no recirculation of the MND is required. Revisions and additions have been incorporated and are prepresented in "revision-mode" (i.e., deletions are shown with strikethrough and additions are shown with underline) to reflect clarifications to the project and are limited to the respective sections of the Final MND listed below.

## Table of Contents

The Table of Contents has been updated to reflect changes related to addition of a new section (Section 7, Response to Comments), relabeling of the appendices heading to reflect the inclusion of the Draft IS/MND in the Final MND, and the addition to the appendices of the two project-specific geotechnical reports referenced within the Draft IS/MND reports.

## Section 3.8 Hazards and Hazardous Materials

Revision to mitigation measure MM HAZ-1 has been incorporated to provide improved readability and amplify the intent of the measure. On page $3-40$, the mitigation measure has been revised as follows:

> MM HAZ-1. Although contaminated soil is not anticipated to be encountered, All soil removal will be required to adhere to the provisons of a soil management plan that will include procedures and recommentand to follow in the event soil contamination is encountered during earthwork activities, all contaminated soil handling and removal will be required to adhere to a soil management plan prepared and approved by the County. The soil management plan will specify procedures for the proper handling and disposal of contaminated soil, which will be performed in accordance with all applicable local and state regulations.

## Section 6. Mitigation Monitoring and Reporting Program

Minor grammatical modifications (not noted in this summary) have been incorporated into Section 6. Throughout Section 6, as appropriate, the term "Lead Agency" has been replaced with LACDPW. The remaining minor editorial revisions and clarifications in this section are noted below with deletions shown with strikethrough.

On page 6-1, revise the two paragraphs under "Responsible Party" heading, as follows:
The County of Los Angeles Department of Public Works (hereafter referred to as LACDPW) will be responsible for implementing and reporting mitigation measures in this program. The LACDPW will have responsibility for ensuring that mitigation measures are accomplished in an environmentally responsible manner. The LACDPW will be responsible for ensuring that the status of mitigation measures is reported in accordance with this program. The LACDPW will be responsible for ensuring that the cost of mitigation is included in the project budget, as appropriate.

The LACDPW will be responsible for program oversight and ensure that applicable mitigation measures are carried forward in construction and operational and maintenance procedures. Mitigation measures will be included in applicable request for proposals, specifications and procedures issued for construction of the pool eomplex within the seope of this-project. Other mitigation measures implemented by the Design Builder will be subject to oversight by the LACDPW. In addition, the LACDPW will be responsible for ensuring that mitigation measures are properly carried out by designated and qualified personnel, which may include specialty contractors.

On page 6-2, revise the last two sentences of paragraph under "Schedule and Reporting Frequency" heading, as follows:

The monitoring table below describes the mitigation measure, organization responsible for implementing the measure, organization responsible for monitoring the measure, and timing of verification for each measure. A column is provided for the monitoring party to sign-off on the implementation of each mitigation measure. Due to possible funding conditions and other external factors, facility construction and operation could be delayed. These delays may also affect the start and eompletion of mitigation measures.

As revised within Section 3.8, mitigation measure MM HAZ-1, under the Mitigation Measure column on page 6-5 has been revised as follows:

> Although contaminated soil is not anticipated to be encountered, All soil removal will be required to adhere to the provisions of a seil management plan that will include procedures and recommendations to follow-in the event soil contamination is encountered during earthwork activities all contaminated soil handling and removal will be required to adhere to a soil management plan approved by the County. The soil management plan will specify procedures for the proper handling and disposal of contaminated soil, which will be performed in accordance with all applicable local and state regulations.

The last column within the table (on pages 6-4 through 6-5), Verification of Completion, has been deemed unnescesary and has therefore been deleted.

## Section 7. Response to Comments

This section is new and has been added to include copies of the three comment letters received during the public review of the Draft IS/MND and responses to those comments. In addition, the end of this section includes a copy of the Notice of Intent to Adopt a Mitigated Negative Declaration filed with the Los Angeles County Clerk, the proof copy of the publication of a notice in a newspaper of general circulation in the affected area (i.e., Antelope Valley Press), and the Notice of Completion submitted to the State of California, Governor's Office of Planning and Research, State Clearinghouse and Planning Unit (State Clearinghouse) for state agency review.

## Appendices

The Draft IS/MND appendices have been included as appendices to this Final MND. In addition, the following project-specific techncial reports have been added to the appendices:

Appendix D - Geotechnical Study Report, East Antelope Valley Animal Shelter" ${ }^{1}$ by Converse Consultants (April 19, 2012)

Appendix E - Subsurface Slab Assessment and Geotechnical Recommendations for Subsurface Slab Abandonment, Proposed East Antelope Valley Animal Shelter ${ }^{2}$ by Converse Consultants (October 10, 2012)

[^1]
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[^2]
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## Acronyms and Abbreviations

| AB | Assembly Bill |
| :--- | :--- |
| ACO | animal control officers |
| ADT | average daily traffic |
| AF | acre-feet |
| AQMP | Air Quality Management Plan |
| AVAQMD | Antelope Valley Air Quality Management District |
| AVTA | Antelope Valley Transit Authority |
| BEP | business emergency plans |
| bgs | below ground surface |
| BLM | Bureau of Land Management |
| BMPs | Best Management Practices |
| CAAQS | California Ambient Air Quality Standards |
| CARB | California Air Resources Board |
| CDFW | California Department of Fish and Wildlife |
| CBC | California Environmental Quality Act |
| CEQA | methane |
| CH | Congestion Management Program |
| CMP | California Natural Diversity Database |
| CNDDB | community equivalent noise level |
| CNEL | California Native Plant Society |
| CNPS | carbon monoxide |
| CO | carbon dioxide |
| CO | Carbon dioxide equivalent |
| CO | California Office of Noise Control Unified Program Agencies |
| CONC | CUPAs |


| dBA | decibels A-weighted |
| :---: | :---: |
| dbh | diameter at breast height |
| DTSC | California Department of Toxic Substances Control |
| ESA | Endangered Species Act |
| ESA | Environmental Site Assessment (Phase I or Phase II) |
| GHG | greenhouse gas |
| gpd | gallons per day |
| GWP | Global Warming Potential |
| HMBP | Hazardous Materials Business Plan |
| in/sec | inches per second |
| ITE | Institute of Transportation Engineers |
| LACDPW | Los Angeles County Department of Public Works |
| LACSD | Sanitation Districts of Los Angeles County |
| lb | pound |
| LEED | Leadership in Energy and Environmental Design |
| Leq | equivalent noise level |
| LID | low impact development |
| MBTA | Migratory Bird Treaty Act |
| MDAB | Mojave Desert Air Basin |
| mgd | million gallons per day |
| MRZ | Mineral Resource Zone |
| MS4 | municipal separate storm sewer system |
| $\mathrm{MTCO}_{2} \mathrm{e}$ | metric tons of carbon dioxide equivalents |
| $\mathrm{N}_{2} \mathrm{O}$ | nitrous oxide |
| NAAQS | National Ambient Air Quality Standards |
| NOx | nitrogen oxides |
| NPDES | National Pollutant Discharge Elimination System |
| $\mathrm{O}_{3}$ | ozone |
| OSHA | Occupational Safety and Health Administration |
| PCE | tetrachlorothene |
| PF | Public Facilities |
| PHS | Burlingame Peninsula Humane Society |
| PM | particulate matter |


| PM $_{2.5}$ | PM less than 2.5 microns in aerodynamic diameter |
| :--- | :--- |
| PM $_{10}$ | PM less than 10 microns in aerodynamic diameter |
| PRC | Public Resources Code |
| RCP | Regional Comprehensive Plan |
| RHNA | Regional Housing Needs Assessment |
| RWQCB | Regional Water Quality Control Board |
| SCAG | Southern California Association of Governments |
| SEA | Significant Ecological Area |
| SO $_{2}$ | sulfur dioxide |
| SO $_{x}$ | sulfur oxides |
| SR | State Route |
| SUSMP | Standard Urban Storm Water Mitigation Plan |
| SWPPP | Storm Water Pollution Prevention Plan |
| SWRCB | State Water Resources Control Board |
| TPH | total petroleum hydrocarbons |
| USEPA | United States Environmental Protection Agency |
| USFWS | U.S. Fish and Wildlife Service |
| USGS | U.S. Geological Survey |
| UWMP | urban water management plan |
| V/C | volume-to-capacity |
| VOC | volatile organic compound |
| WDR | Waste Discharge Requirements |
| WRP | Water Reclamation Plant |

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SECTION 1

## Background Information

### 1.2 Project Title

County of Los Angeles Animal Care Center Project, Palmdale, CA

### 1.3 Lead Agency Name and Address

County of Los Angeles
By Department of Public Works
900 S. Fremont Avenue
Alhambra, California 91803

### 1.4 Lead Agency Contact Person and Phone Number

Jason Kim, Capital Projects Manager
County of Los Angeles Department of Public Works (626) 300-2326

Email: jikim@dpw.lacounty.gov

### 1.5 Project Location

38532, 38560, 38600 and 38624 Sierra Highway
Palmdale, California 93550

### 1.6 Project Sponsor's Name and Address

Built/Managed By:
Same as Lead Agency above.
Operated by:
County of Los Angeles
Department of Animal Care and Control

### 1.7 General Plan Designation/Zoning

Public Facilities (PF)

### 1.8 Description of the Project

### 1.8.1 Project Overview

The County of Los Angeles Animal Care Center Project, Palmdale, CA (the "proposed project") is a proposed new County of Los Angeles animal care facility ("proposed project") that will service the needs of communities in the eastern portion of Antelope Valley, in northern Los Angeles County. The proposed facility will be on a 5.8 -acre site to be acquired from the City of Palmdale by Los Angeles County for the construction and operation of a one-story approximately 25,500 square foot indoor animal care center, as well as maintaining a portion of the site to remain fenced, vacant, and for possible future animal care center expansion. The proposed facility will have an average peak day capacity of approximately 361 animals of which approximately 35 percent (approximately 128) are anticipated to be dogs, 64 percent (approximately 229) are cats, and one percent (approximately 4) are wildlife (non-domesticated animals). No livestock will be housed at the proposed facility and no animals will be housed outdoors. The proposed facility will alleviate the high volume of animal control services at the existing Lancaster Animal Care Center and eliminate the need to continue to rent kennels (currently 32 kennels are rented by the County's Department of Animal Care and Control) at the Pet Stop in Lancaster, a privately owned facility used for the private boarding of animals/pets.

The project site is owned by the City of Palmdale. The proposed project includes acquisition of the project site by the County of Los Angeles from the City of Palmdale for the specific construction and operation of an animal care center. The County of Los Angeles will construct the proposed project and the County's Department of Animal Care and Control (DACC) will operate the facility. Therefore, the County of Los Angeles is the lead agency under California Environmental Quality Act (CEQA). The project will be implemented through the Los Angeles County Department of Public Works (LACDPW).

### 1.8.2 Project Site

The 5.8 -acre project site is located approximately a quarter of a mile north of the Palmdale Boulevard and Sierra Highway intersection in the eastern part of the Antelope Valley. The regional location is depicted on Figure 1. The project site is currently a vacant area immediately west of (adjacent to) residential uses, northwest of the Richard B. Hammack Community Activity Center (Hammack Activity Center), north of the South Valley WorkSource Center (WorkSource Center), ${ }^{5}$ east of Sierra Highway, and south of the Los Angeles County Sheriff's Department Palmdale Station. The residential uses to the east and the Sheriff's station to the north are separated from the project site by a block wall (estimated to be approximately eight-feet high). Since the paved portion of the project site is open, it is possible for the Hammack Activity Center and WorkSource Center to use that portion of the site for parking. The site is zoned as Public Facilities (PF). The project site and surrounding uses are shown on Figure 2.The project site is vacant and open (not fenced). The northern portion of the site is bare soil and gravel, while the remainder of the site is paved with asphalt. The site is relatively flat. The vegetation within the project site is

[^3]

Source: US Census Bureau, Geography Division, 2010

Figure 1
Regional Location

(ruderal (i.e., weeds). According to historical information, it appears that the project site had been undeveloped in 1917. By 1928, the northern portion of the project site was agricultural land orchard or groves), surrounded by undeveloped land with light industrial, commercial and residential properties interspersed. By 1948, several residential and light industrial/commercial structures were developed on the project site. The greater surrounding area appeared to be moderately populated with a mix of residential, commercial and light industrial properties, as well as some agricultural and undeveloped land. Building records issued as early as the 1950s indicated the use of the project site was for retail, including restaurants/lounge, salons, stores, and a church. Several commercial properties within the project site had been redeveloped by $1968 ;{ }^{6}$ however, the northeastern corner of the project site remained undeveloped. By 2002, the project site had been cleared of previous building development and was left vacant as it appears today (LACDPW, 2011).

### 1.8.3 Project Elements

The proposed one-story animal care facility will be situated within the central portion of the project site. The closest portion of the proposed facility (a DACC car wash area and emergency generator) is approximately 94 feet from the nearest sensitive receptor (residence at 38575 Friendly Avenue, immediately east of the project site). The proposed building is approximately 100 feet from the nearest sensitive receptor. As noted above, the residential uses to the east are separated from the project site by an approximate eight-foot tall block wall. The nearest recreational use (outdoor roller hockey rink), southeast of the project site, is approximately 128 feet from the proposed building and 230 feet from the nearest noise source (i.e., emergency generator). The proposed facility will be approximately 25,500 square feet with the roof line having varying heights (maximum assumed height of 30 feet) which will enhance scale and look of the exterior of the building while providing opportunities for vaulted ceilings and natural light within portions of the interior of the building.

The proposed facility includes various indoor spaces for public adoption, relinquishment, animal control, quarantine, euthanasia, veterinary and spay neuter clinic, and administration areas associated with the animal care facility and DACC operations. The proposed facility also includes outdoor spaces (i.e., fenced exercise yards) between the staff parking to the north and the new animal care center, and an ample open and grass area between the facility and the residential area to the east that will serve as a retention area to percolate stormwater runoff on-site. Court yard areas are proposed within the building footprint and are surrounded by all four sides by building walls, as well as landscaping. No animals will be housed outdoors.

As part of DACC and animal care center operations, a trash receptacle, small storage area, car wash (for use by DACC officers on department vehicles only), covered parking (i.e., carport), and sally port (i.e., loading and unloading area) are proposed at the northeast area of the facility. This area of the proposed facility also includes an emergency generator that will be exercised as part of monthly maintenance for a minimum of 30 minutes. The trash receptacle, storage area, car wash, sally port and emergency generator areas will be

[^4]separated from the residential area to the east by the existing block wall, as well as an additional/new eight-foot high concrete screen wall as part of the facility. Refer to Figure 3 for a conceptual schematic site plan.

In addition to the carport for DACC vehicles, two separate parking lots (one each for public and staff parking) are proposed at the north and south sides of the proposed facility. The proposed staff parking area will consist of approximately 32 spaces. The proposed public parking area will consist of the development of 71 parking spaces. Of the 71 public parking spaces being developed as part of the proposed project, approximately six are handicap spaces adjacent to the roller hockey rink associated with the Hammack Activity Center (east/southeast of the project site). There will be 65 spaces for use by the proposed facility. A conceptual schematic site plan delineating parking is shown on Figure 3.

The proposed facility will be accessed by the public from an existing driveway (just north of the WorkSource Center) on Sierra Highway. Staff and service vehicles associated with the facility will access the proposed facility from a new gated-entry and access driveway at the northern portion of the proposed facility on Sierra Highway. Landscaping and hardscaping will be installed all around the building.

As required by the City of Palmdale, a new turn lane/deceleration lane along Sierra Highway will be constructed within the existing right-of-way of Sierra Highway to provide access to the staff parking lot. There is an existing turn lane/deceleration lane at the public entrance to the south of the project site (near the WorkSource Center).

The proposed facility will be designed and built in a manner consistent with the adjacent facilities. The proposed facility will be surrounded by fencing, with the exception of the public entrances at the southern portion of the site. The project will introduce lighting that will be developed to be compatible with existing lighting. The exterior of the animal care facility, parking lots, and pedestrian walkways will be illuminated by lighting fixtures at a level adequate to ensure safety of visitors and staff. Security lighting will be low-lighting, pedestrian-scaled and will be directed downward and towards the interior of the animal care facility, or shielded, to ensure lighting does not spill over onto adjacent properties.

The northern portion of the project site will remain vacant. This area will be enclosed by wrought iron fencing and it will be reserved for future expansion of the shelter, should expansion be warranted in the future. ${ }^{7}$ No public access will occur within the area designated for possible future expansion.

[^5]

The facility will comply with the County's adopted Energy and Environmental Policy, which is part of the County's effort to help conserve natural resources and protect the environment. The goal of the policy is to provide guidelines for the development, implementation, and enhancement of energy conservation and environmental programs. In order to meet the goals of the policy, the County has implemented energy efficient projects in County facilities, specifically retrofitting or replacing building lighting systems and air conditioning equipment, or as is the case of the proposed project, the certification of new development under the United States Green Building Council's Leadership in Energy and Environmental Design (LEED) or equivalent standards, and implementation of County sponsored recycling programs, and the incorporation of Low Impact Design Standards and drought tolerant landscaping, as applicable. As such, the building will be designed and constructed to achieve (at a minimum) the LEED Silver level certification by incorporating sustainable design features to optimize energy and water use, enhance the sustainability of the site, improve indoor environmental quality, and maximize the use and reuse of sustainable and local resources.

### 1.8.4 Construction

Proposed project construction activities will include construction and installation of the proposed facilities described above within the project site boundaries. Construction activities include removal of existing pavement, site preparation, grading (excavated to a depth of at least three feet from the existing grade), construction of the building and infrastructure connections, painting, and installation of lighting, parking lot paving and striping, and landscaping and irrigation. An eight-foot high concrete screen wall will be constructed at the trash receptacle, storage area, car wash and adjacent planter area to screen views to the loading zone from the residential lot. A turn lane/deceleration lane along Sierra Highway will also be constructed to provide access to the staff parking lot.

Construction is expected to begin in the summer of 2014 and last for approximately 16-18 months. Anticipated duration for each construction phase is summarized in Table 1.7-1. Construction of the proposed project will require temporary staging and storage areas for materials and equipment and a maximum of 33 workers at any one time. The materials staging and storage will be located within the project site, primarily in the area designated for possible future expansion. Upon the completion of construction activities, the area designated for possible future expansion will subsequently be graded and fully fenced. All materials for project construction will be delivered by truck on existing roadways. Up to 14 construction delivery trips, 33 construction worker trips, and 17 haul truck trips ${ }^{8}$ are anticipated to occur to and from the project site per day during construction.

Construction will be scheduled for eight-hours per day between the hours of 7:00 a.m. and 5:00 p.m., Monday through Friday, and no holidays. If additional hours are necessary to make up schedule deficiencies or to complete critical construction activities, approval from the City of Palmdale and County will be obtained.

[^6]Table 1.7-1
Anticipated Construction Phases and Approximate Duration

| Construction Phase | Duration |
| :---: | :---: |
| Demolition (paved area and subsurface <br> slab/basement) | 1 month |
| Site Preparation and Grading | 1 to 2 weeks |
| Building Construction | 13 to 15 months* |
| Paving | 2 weeks |
| Architectural Coating | 3 weeks |

* For purposes of the air quality analysis a nine month duration was assumed for building construction, which represents a worst case (conservative) scenario.


### 1.8.5 Operation

The new animal care center is expected to be operational in the fall of 2015. The facility will be staffed by approximately 30 full-time County Animal Control Officers (ACOs) and approximately 20 part-time volunteers. It is anticipated that the facility will serve approximately 70 visitors per day and will be open to the public from noon to 7:00 p.m. from Monday through Thursday, and 10:00 a.m. to 5:00 p.m. from Friday through Sunday, and closed or special hours on selected holidays. The facility will always have staff on-site (24-hours per day, seven days per week) though there will be limited staff at the facility during hours the shelter is closed to the public. There may be other events or training that occurs on-site such as dog obedience classes. These activities will typically occur during normal public hours of operation. Business hours are subject to change based upon operational needs. Programs conducted at the proposed facility include:

- Rescue of, and shelter for, unwanted and sick or injured animals
- Capture of stray animals
- Reuniting lost pets with their owners
- Adoption of homeless animals
- Low-cost vaccinations and spay/neuter services
- Temporary impoundment and quarantine services (including certain species of wildlife)
- Licensing and enforcement
- Euthanasia services
- Emergency response to disasters

The proposed facility will have an average peak day capacity of approximately 361 animals of which approximately 35 percent (approximately 128) are anticipated to be dogs, 64 percent (approximately 229 ) are cats, and one percent (approximately 4 ) is allocated for
wildlife (which is managed per the DACC administrative policy - Policy No. LW140, Wild Animals). The interior of the proposed facility will contain several kennel areas to house the dogs and cats, as well as wildlife. In addition, the facility will have several holding areas to receive and temporarily house the animals.

It is estimated that the outdoor exercise yards will be used between the hours of 10:00 a.m. to 7:00 p.m. Monday through Thursday, and 10:00 a.m. to 5:00 p.m. Friday through Sunday under staff supervision. Animals dropped off the by the public will be delivered to staff or to indoor cages, and animal deliveries by field staff will occur behind screened fencing at the sally port to the rear of the facility.

The DACC will contract with a licensed disposal services for the regular pickup and disposal of wastes. The pickup schedules will be developed based on storage capacity and use. Delivery of supplies will occur on an irregular schedule based on frequency of orders. For the purpose of the analysis, the number of delivery/disposal trucks is conservatively estimated at three per day.

For the following analysis, unless otherwise stated, the proposed project will be operated in accordance with all the latest and applicable DACC administrative policies and procedures.

### 1.9 Project Actions and Approvals

The environmental document (i.e., this Initial Study/Proposed Mitigated Negative Declaration), proposed project, and land acquisition will require approval by the County of Los Angeles Board of Supervisors. Additional anticipated approval/ permit for the proposed project includes, but is not limited, to the following:

- Los Angeles County Department of Public Works Building and Safety Division approval of the building plans (including review and approval associated with the proposed site utilities) and issue building permits.
- City of Palmdale - agreement with Los Angeles County for land acquisition, review and approval of new access driveway and proposed dedicated right-turn lane (both along Sierra Highway), review and issuance of permit to connect to the existing sanitary sewer system, payment of required City fees (Traffic, Drainage, Fire Facility and Public Facility) if required, as well as review and approval for off-site site infrastructure improvements, as applicable.
- Palmdale Water District and Los Angeles County Fire Department - review and approval on-site fire hydrant.

The analysis in this document assumes that, unless otherwise stated, the proposed project will be designed, constructed and operated following all applicable laws, regulations, ordinances and formally adopted County of Los Angeles standards (e.g., Los Angeles County Code), and that all applicable permits will be obtained. Construction will also follow, as applicable, the uniform practices established by the Southern California Chapter of the American Public Works Association (e.g., Standard Specifications for Public Works Construction and the Work Area Traffic Control Handbook).

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## Environmental Determination

### 2.1 Environmental Factors Potentially Affected

The environmental factors checked below would be potentially affected by this project, i.e. involve at least one impact that is a "Potentially Significant Impact" as indicated by the checklist on the following pages.


| Agriculture/Forest Resources | $\square$ | Air Quality |
| :--- | :--- | :--- |
| Cultural Resources | $\square$ | Geology/Soils |
| Hazards \& Hazardous | $\square$ | Hydrology/Water |
| Materials | $\square$ | Quality |
| Mineral Resources | $\square$ | Recreation |
| Public Services | $\square$ | Mandatory Findings of <br> Significance |
| Utilities/Service Systems |  |  |

### 2.2 Determination

Determination: (To be completed by the Lead Agency)
On the basis of this initial evaluation:


I find that the proposed project COULD NOT have a significant effect on the environment, and a NEGATIVE DECLARATION will be prepared.


I find that although the proposed project could have a significant effect on the environment, there will not be a significant effect in this case because revisions in the project have been made by or agreed to by the project proponent. A MITIGATED NEGATIVE DECLARATION will be prepared.
$\square$ I find that the proposed project MAY have a significant effect on the environment, and an ENVIRONMENTAL IMPACT REPORT is required.


I find that the proposed project MAY have a "potentially significant impact" or "potentially significant unless mitigated" impact on the environment, but at least one effect 1) has been adequately analyzed in an earlier document pursuant to applicable legal standards, and 2) has been addressed by mitigation measures based on the earlier analysis as described on attached sheets. An ENVIRONMENTAL IMPACT REPORT is required, but it must analyze only the effects that remain to be addressed.
$\square$ I find that although the proposed project could have a significant effect on the environment, because all potentially significant effects (a) have been analyzed adequately in an earlier ENVIRONMENTAL IMPACT REPORT or NEGATIVE DECLARATION pursuant to applicable standards, and (b) have been avoided or mitigated pursuant to that earlier ENVIRONMENTAL IMPACT REPORT or NEGATIVE DECLARATION, including revisions or mitigation measures that are imposed upon the proposed


PROJECT MANAGER


Date
COUNTY OF LOS ANGELES DEPT OF PUBLIC WORKS
Title
Agency:

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## SECTION 3

## Evaluation of Environmental Impacts

### 3.1 Aesthetics

Aesthetics Checklist

| Would the project: | Potentially Significant Impact | Less Than Significant with Mitigation Incorporation | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
| a. Have a substantial adverse effect on a scenic vista? |  |  | $\pm$ |  |
| b. Substantially damage scenic resources, including, but not limited to, trees, rock outcroppings, and historic buildings within a state scenic highway? | $\square$ |  | $\square$ | $\searrow$ |
| c. Substantially degrade the existing visual character or quality of the site and its surroundings? |  |  | $\triangle$ |  |
| d. Create a new source of substantial light or glare which would adversely affect day or nighttime views in the area? |  |  | $\otimes$ |  |

### 3.1.1 Setting

The project site is currently a vacant lot located two blocks north of the intersection of Sierra Highway and Palmdale Boulevard. Single-family residences are located immediately east of the project site, blocked by a concrete fence. The Los Angeles County Sheriff's Department Palmdale Station, which includes a helicopter landing pad, is located north of the project site, adjacent to the area designated for possible future expansion. Two outdoor hockey rinks of the Hammack Activity Center are located adjacent to the project site to the southeast. The WorkSource Center is also located adjacent to the project site, on the northeast corner of the Sierra Highway and Avenue Q-6 intersection. The Dr. Robert C Saint Clair Parkway is located to the west of the project site, across Sierra Highway. Sycamore trees line the sidewalks of Sierra Highway. These trees and landscaping associated with the Dr. Robert C Saint Clair Parkway provide a visual break to the urban landscape.

The project site and surrounding area are predominantly flat, which provide distant vistas of the San Gabriel Mountains to the south. The Sierra Nevada Mountains are visible to some extent to the north. Although the mountain ranges create a dramatic backdrop and aesthetically pleasing viewshed, views of the mountain ranges are obscured by existing utilities and development. Views of the project site are primarily along Sierra Highway and Dr. Robert C Saint Clair Parkway. There are no outstanding focal points on the project site.

As mentioned before, the existing project site is vacant; thus, the site does not contain any lighting. The surrounding area is characterized by typical urban sources of light and glare,
such as street, parking, and commercial lighting. The residential area east of the project site is considered a light-sensitive land use. The Hammack Activity Center has lighting for its outdoor hockey rinks. This lighting does not carry over onto the project site because fixtures are directed inward onto the hockey rinks.

## Regulatory Setting

Federal. None
State. None

## Local.

Title 22 (Planning and Zoning) of the Los Angeles County Code requires general design standards, which limit the type and intensity of uses consistent with the General Plan and local plans. In addition, the City of Palmdale Zoning Ordinance (1994) also includes property development standards and design guidelines including allowable land uses, setback and height requirements, landscaping, lighting, screening, walls, signs, parking requirements, and trash and recycling storage.

The City of Palmdale General Plan includes a Community Design Element which has policies and objectives, including site design for the comfort and safety of users; community character through distinctive design and quality workmanship; human-scale developments; parking lot design and orientation to function well for site users and present an attractive appearance to enhance business environment; and community design to provide a visually interesting and stimulating setting by using varied physical forms and details which contribute to Palmdale's sense of place.

Under the Conservation and Open Space Element of the Draft Los Angeles County General Plan, goals and policies for scenic resources include protecting the County's ridgelines from incompatible development that diminished their scenic value; reducing light trespass and light pollution; requiring development to be designed to create a consistent visual relationship with the natural terrain and vegetation; and, prohibit outdoor advertising and billboards along scenic routes, corridors, and other scenic areas.

Although the project site is within the boundary of the City of Palmdale, as part of the project the site will become County property; therefore, the County's goals and policies are the governing regulation. However, the project is also consistent with the City of Palmdale's regulations.

### 3.1.2 Impacts Analysis

a. Would the project have a substantial adverse effect on a scenic vista?

LESS THAN SIGNIFICANT IMPACT. The nearest scenic resources to the project site are the San Gabriel Mountains to the south, which serve as the visual backdrop to the urban setting of the project. The project will include a one-story building with varying roof lines (approximately 30 feet high), which will be consistent in size with the adjacent buildings. The project will not introduce incompatible visual elements within the viewshed of the mountains or substantially alter the views of the mountains. The existing scenic view of the San Gabriel Mountains will continue to be fully visible from

Sierra Highway and the project area. Therefore, the project will have a less than significant impact on a scenic vista and no mitigation is required.
b. Would the project substantially damage scenic resources, including, but not limited to, trees, rock outcroppings, and historic buildings within a state scenic highway?

NO IMPACT. The project site is vacant. The northern portion of the site is bare soil and gravel, while the remainder of the site is paved with asphalt. Scenic resources such as trees, rock outcroppings, or historic buildings are not present on the project site. There is no official state or county scenic highways in the project area. The Angeles Crest Highway (Route 2) from the La Canada/Angeles National Forest boundary to the San Bernardino County line is the nearest officially designated scenic highway to the project site (Caltrans, 2012). The 55-mile segment of the state scenic highway is approximately 21 miles south, and not visible from, the project site. Therefore, the project will have no impact on scenic resources, including within a state scenic highway.
c. Would the project substantially degrade the existing visual character or quality of the site and its surroundings?

LESS THAN SIGNIFICANT IMPACT. The scenic vistas of the San Gabriel Mountains to the south of the project site are the primary contributors to the visual character and quality of the area, as discussed above. The project site is currently vacant and construction activities associated with the project will temporarily change the visual character of the site. Construction activities will vary throughout the 16-18 month construction period. Although the visual character of the site will change because of and during construction, the change will not substantially degrade the existing visual character or quality of the site. Elements of the project include a one-story building (potentially 30 feet in height), visitor and employee parking lots, and outdoor open spaces. The proposed structures will be similar in appearance and character to adjacent facilities (i.e., Hammack Activity Center, WorkSource Center, and the Los Angeles County Sheriff's Department Palmdale Station), while being sensitive to the immediate neighbors. The architectural design will be coordinated with the City of Palmdale to address regional and environmental appropriateness. Additionally, the proposed project will include civic art either inside and/or outside of the building, which will also add to the enhanced visual character of the site.

The project will be visible by viewers from the immediate surrounding area. The backyards of the single-family homes to the east of the project are separated from the site with an existing block wall. Similar to the existing block wall, an additional eightfoot high concrete screen wall will be constructed that will preclude direct views of the trash receptacle, car wash, emergency generator, and loading zone from the abutting residential lots. The new wall in the area of these portions of the facility will be approximately 94 feet from the abutting residential lots and the eastern most portion of the proposed building will be approximately 145 feet from these residences. As shown in Figure 3, landscaping (i.e., grass) is proposed in the open area between the proposed facility and abutting residences, as well as other landscaping (i.e., bushes and/or trees) along the eastern building facade. Therefore, the area to the east of the proposed building will remain undeveloped as a buffer zone between the animal facility and the residential neighbors.

The landscaping associated with the project will enhance the overall aesthetics of the site, which is currently paved with asphalt and contains bare soil and gravel, and surrounding area and will provide additional visual relief in conjunction with the existing sycamore trees along Sierra Highway.

Therefore, the project will not degrade the existing visual character or quality of the site, and the impact will be less than significant and no mitigation is required.
d. Would the project create a new source of substantial light or glare which would adversely affect day or nighttime views in the area?

LESS THAN SIGNIFICANT IMPACT. Construction activities for the project will occur during daylight hours; therefore, no new sources of artificial lighting will be necessary. Upon completion of construction activities, the project will introduce a new source of nighttime light and glare into the area. The exterior of the animal care facility, parking lots, and pedestrian walkways will be illuminated by lighting fixtures at a level adequate to ensure safety of visitors and staff. Security lighting will be low-lighting, pedestrian-scaled and will be directed downward and towards the interior of the animal care facility, or shielded, to ensure lighting does not spill over onto adjacent properties.

There is existing lighting (street, parking lot, and security lighting) adjacent and along all four areas of the site. With the new lighting sources, lighting levels at the project site will increase slightly from existing conditions. Spill of light onto adjacent residential neighborhood will be reduced and controlled by using shields/hoods and other design features on light fixtures to confine lighting within the site boundaries, as required by regulation. Therefore, lighting associated with the project will not affect the overall ambient lighting levels; a less than significant impact will occur and no mitigation is required.

### 3.2 Agriculture and Forest Resources

## Agriculture and Forest Resources Checklist

Would the project:
d. Result in the loss of forest land or conversion of forest land to non-forest use?

e. Involve other changes in the existing environment which, due to their location or nature, could result in
 conversion of Farmland, to non-agricultural use or conversion of forest land to non-forest use?

### 3.2.1 Setting

Although the greater Antelope Valley contains the majority of Los Angeles County's active agricultural land uses, the project is not located on or near land designated for agricultural use as defined by the Farmland Mapping and Monitoring Program or the Williamson Act, nor is there designated forest land at or near the site. The current land use of the project is designated as PF under the City of Palmdale General Plan.

## Regulatory Setting

Federal. None
State.
California Land Conservation Act. Under the provisions of the Williamson Act (California Land Conservation Act 1965, Section 51200), landowners enter into a contract to maintain agricultural or open space use of their lands in return for reduced property tax assessment.

Farmland Mapping and Monitoring Program. The California Department of Conservation, Division of Land Resource Protection Farmland Mapping and Monitoring Program monitors the conversion of the state's farmland to and from agricultural use. The map identifies eight classifications and uses a minimum mapping unit size of 10 acres. Four classifications of farmland: Prime Farmland, Farmland of Statewide Importance, Unique Farmland, and Farmland of Local Importance, are considered valuable.

Local. The proposed policies of the Draft Los Angeles County General Plan protects Agricultural Resource Areas from encroaching development and discourages incompatible adjacent land uses. However, the project site is not located within or adjacent to an Agricultural Resource Area.

The City of Palmdale General Plan also includes goals and objectives that address the premature conversion of agricultural lands to urban uses by aiming to encourage the preservation of agricultural lands in non-urban areas and as an interim use where urban development is not anticipated for several years.

Although the project site is within the boundary of the City of Palmdale, as part of the project the site will become County property; therefore, the County's proposed policies and goals within the Draft General Plan are the governing regulation. However, the project is also consistent with the City of Palmdale General Plan.

### 3.2.2 Impacts Analysis

a. Would the project convert Prime Farmland, Unique Farmland, or Farmland of Statewide Importance, as shown on the maps prepared pursuant to the Farmland Mapping and Monitoring Program of the California Resources Agency, to nonagricultural use?

NO IMPACT. The proposed project will not be located on agricultural land nor will it convert prime agricultural lands to non-agricultural use. The project site is not currently used for agricultural uses. The northern portion of the site is bare soil and gravel, while the remainder of the site is paved with asphalt. Therefore, there will be no impact to designated farmland.
b. Would the project conflict with existing zoning for agricultural use, or a Williamson Act contract?

NO IMPACT. The project site is currently zoned as PF. The proposed project is not located on or near land zoned for agriculture use or under a Williamson Act contract. Therefore, the proposed project will not have an impact on agricultural zoning or a Williamson Act contract.
c. Would the project conflict with existing zoning for, or cause rezoning of, forest land (as defined in PRC section 1220(g)) or timberland (as defined in PRC section 4526)?

NO IMPACT. There is no state or federally designated forests or timberland zoning in close proximity to the project site or in the project vicinity. Therefore, the proposed project will have no impact on land zoned for forest land.
d. Would the project result in the loss of forest land or conversion of forest land to non-forest use?

NO IMPACT. The project site is currently zoned as PF. The northern portion of the site is bare soil and gravel, while the remainder of the site is paved with asphalt. No forest land is present at the project site or in the project vicinity. Therefore, the proposed project will have no impact on forest land.
e. Would the project involve other changes in the existing environment which, due to their location or nature, could result in the conversion of Farmland, to nonagricultural use?

NO IMPACT. As described above, there is no farmland located on the project site or in the project vicinity and the project will not involve any changes that could result in the conversion of forest resources or farmland to non-agricultural use. Therefore, the proposed project will have no impact on agricultural uses or activities.

### 3.3 Air Quality

## Air Quality Checklist

Would the project:

### 3.3.1 Setting

## Regulatory Setting

The Clean Air Act as amended in 1990 is the federal law that governs air quality. Its counterpart in California is the California Clean Air Act of 1988. These laws set standards for the quantity of pollutants that can be in the air. At the federal level, these standards are called National Ambient Air Quality Standards (NAAQS) and at the state level, these standards are called California Ambient Air Quality Standards (CAAQS). Standards have been established for the following criteria pollutants that have been linked to potential health concerns: carbon monoxide (CO), nitrogen dioxide, ozone $\left(\mathrm{O}_{3}\right)$, inhalable particulate matter $\left(\mathrm{PM}_{10}\right)$, fine particulate matter $\left(\mathrm{PM}_{2.5}\right)$, lead, and sulfur dioxide $\left(\mathrm{SO}_{2}\right)$; and in addition visibility reducing particles, sulfates, hydrogen sulfide, and vinyl chloride in California.

The proposed project is located within the Antelope Valley Air Quality Management District (AVAQMD) in the Mojave Desert Air Basin (MDAB). The MDAB includes the desert portions of Kern, Los Angeles, San Bernardino, and Riverside counties and is adjacent to the South Coast Air Basin. The AVAQMD comprises 1,300 square miles and is bordered by Kern County to the north, the San Gabriel Mountains to the south, San Bernardino County to the east, and Ventura County to the west. The AVAQMD is responsible for developing and updating clean air plans to comply with federal and state air quality requirements including plans to correct levels of air pollutants to achieve or exceed air quality standards. Currently, the AVAQMD's jurisdiction meets federal and state standards for most criteria pollutants except $\mathrm{O}_{3}$ and $\mathrm{PM}_{10}$.

## AVAQMD CEQA and Federal Conformity Guidelines.

The AVAQMD CEQA and Federal Conformity Guidelines (2011), consider a project to have a significant effect on air quality if it does the following:

- Generates total emissions (direct and/or indirect) exceeding the thresholds given in the Guidelines;
- Generates a violation of any ambient air quality standard when added to the local background;
- Does not conform with the applicable attainment or maintenance plans; and/or,
- Exposes sensitive receptors to substantial pollutant concentrations, including those resulting in a cancer risk greater than or equal to 1 in one million and/or a Hazard Index (non-cancerous) greater than or equal to 0.1.

Table 3.3-1 below shows the AVAQMD significance thresholds for criteria pollutants.
Table 3.3-1
AVAQMD CEQA Significance Thresholds

| Pollutant | Daily Threshold <br> (lbs per day) | Annual Threshold <br> (tons per year) |
| :---: | :---: | :---: |
| Carbon Monoxide | 548 | 100 |
| Nitrogen Oxides | 137 | 25 |
| Volatile Organic Compounds | 137 | 25 |
| Inhalable Particulate Matter $\left(\mathrm{PM}_{10}\right)$ | 82 | 15 |
| Fine Particulate Matter $\left(\mathrm{PM}_{2.5}\right)$ | 82 | 15 |
| Sulfur Oxides | 137 | 25 |
| Lead | 3 | 10.6 |
| Hydrogen Sulfide | 54 | 100,000 |
| Greenhouse Gases | 548,000 |  |

Source: AVAQMD, 2011,
In general, project emissions that are lower than the threshold criteria is sufficient to demonstrate that a project will have less than significant impact on air quality. A project with a significant impact must incorporate mitigation sufficient to reduce its impact to a level that is not significant. A project that cannot be mitigated to a level that is not significant must incorporate all feasible mitigation measures. Federal and state attainment status designations assigned by the United States Environmental Protection Agency (USEPA) and California Air Resources Board (CARB) for the Antelope Valley are summarized below in Table 3.3-2. As can be seen, the Antelope Valley area is in attainment for all criteria pollutants except for $\mathrm{O}_{3}$ NAAQS and CAAQS and $\mathrm{PM}_{10}$ CAAQS.

Table 3.3-2
Attainment Designations of the Project Area

| Pollutant | State Designation | Federal Designation |
| :--- | :--- | :--- |
| Ozone (1-hour) | Extreme Nonattainment | NA |
| Ozone (8-hour) | Nonattainment | Severe Nonattainment |
| Inhalable Particulate <br> Matter (PM 10 | Nonattainment | Unclassifiable |
| Fine Particulate <br> Matter <br> (PM 2.5$)$ | Unclassified | Unclassifiable/Attainment |
| Carbon Monoxide | Attainment | Unclassifiable/Attainment |
| Nitrogen Dioxide | Attainment | Unclassifiable/Attainment |
| Sulfur Dioxide | Attainment | Unclassifiable |
| Lead | Attainment | NAclassifiable/Attainment |
| Sulfates | Unclassified | NA |
| Hydrogen Sulfide | Unclassified | NA |
| Visibility Reducing <br> Particles |  |  |

Sources: CARB, 2011. USEPA, 2012.

## AVAQMD Air Quality Management Plan

An air quality management plan (AQMP) or attainment plan is prepared by each air district that has not attained the NAAQS. The purpose of these plans is to describe how the district will achieve attainment. On May 20, 2008, AVAQMD adopted a federal 8-hour $\mathrm{O}_{3}$ attainment plan that forecasted attainment with $\mathrm{O}_{3}$ NAAQS by 2021.

## AVAQMD Rules

Air district rules are generally limited to regulating stationary sources while state and federal rules regulate both stationary and mobile sources. The following prohibitory rules will apply to the project during construction even though the project is well below AVAQMD's significance thresholds under CEQA, as discussed below. These rules further ensure that impacts are reduced to the maximum extent feasible.

Rule 401 - Visible Emissions. No emissions may exceed No. 1 on the Ringlemann Chart for a period or periods aggregating more than three minutes in any one hour.

Rule 402 - Nuisance. A person shall not discharge from any source whatsoever such quantities of air contaminants or other material which cause injury, detriment, nuisance, or annoyance to any considerable number of persons or the public, or which cause or have a natural tendency to cause injury or damage to business or property.

Rule 403 - Fugitive Dust. Visible dust is prohibited beyond the property line of an emission source. $\mathrm{PM}_{10}$ levels are prohibited from exceeding 50 micrograms per cubic meter when determined by simultaneous upwind and downwind sampling. Rule 403 contains a list of best applicable control measures to reduce fugitive dust impacts.

### 3.3.2 Impacts Analysis

The proposed project was evaluated for its potential to create a significant adverse air quality impact either during construction or operation.

## Construction Emissions

The California Emission Estimator Model (CalEEMod), Version 2011.1.1 was used to estimate emissions generated during construction of the proposed project. The following assumptions were input into the model for the most conservative analysis possible:

- CalEEMod defaults were used for the number and type of construction equipment, as summarized in Table 3.3-3, and number of workers necessary.
- Peak construction workers were assumed to be 33 .
- The AVAQMD was input as the appropriate air district.
- The acreage was 5-10 acres.
- The construction schedule was assumed 18 months.
- The VOC content of the paint was modified from CalEEMod to reflect the limits found in AVAQMD Rule 1113 - Architectural Coatings.
- Haul trip of removed pavement were assumed to be disposed of at the Antelope Valley Recycling and Disposal Facility in Palmdale, CA.

Table 3.3-3
Anticipated Construction Equipment

| Construction Phase | Equipment Type | Quantity |
| :---: | :---: | :---: |
| Demolition | Concrete Saw | 1 |
|  | Dozer |  |
| Loader/Backhoes | 1 |  |
| Site Preparation and Grading | Grader | 3 |
|  | Dozer | 1 |
|  | Loader/Backhoe | 1 |
|  | Crane | 1 |
| Parklift | 1 |  |
|  | Generator Set | 1 |
|  | Loader/Backhoe | 1 |
|  | Welders | 1 |
| Paving | Cement Mixer | 3 |
|  | 1 |  |
|  | Paving Equipment | 1 |
| Roller | 1 |  |
|  | Loader/Backhoe | 1 |

Table 3.3-4 presents the estimated maximum daily construction emissions anticipated to be generated by the proposed project.

Table 3.3-4
Summary of Estimated Maximum Daily Construction Emissions

|  | $\begin{gathered} \text { CO } \\ \text { (lb/day) } \end{gathered}$ | $\begin{aligned} & \text { NOx } \\ & \text { (Ib/day) } \end{aligned}$ | ROG (Ib/day) | $\begin{aligned} & \text { SOx } \\ & \text { (Ib/day) } \end{aligned}$ | $\mathrm{PM}_{10}$ (lb/day) | $\begin{gathered} \mathrm{PM}_{2.5} \\ \text { (Ib/day) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Demolition | 27 | 45 | 5 | <1 | 12 | 2 |
| Site Preparation | 18 | 30 | 4 | <1 | 4 | 3 |
| Grading | 15 | 25 | 3 | <1 | 4 | 2 |
| Building Construction | 19 | 24 | 5 | <1 | 2 | 2 |
| Paving | 13 | 16 | 3 | <1 | 2 | 1 |
| Architectural Coating | 2 | 3 | 66 | <1 | <1 | <1 |
| Maximum Daily Emissions from worstcase phase | 27 | 45 | 66 | <1 | 12 | 3 |
| AVAQMD CEQA Threshold | 548 | 137 | 137 | 137 | 82 | 82 |
| Emissions Exceed CEQA Threshold? | No | No | No | No | No | No |
| Notes: <br> AVAQMD = Antelope Valley Air Quality Management District, CEQA = California Environmental Quality Act, CO = carbon monoxide, lb/day = pounds per day, $\mathrm{NOx}=$ nitrogen oxides, $\mathrm{ROG}=$ reactive organic gases, $\mathrm{SOx}=$ sulfur oxides, $\mathrm{PM}_{10}=$ inhalable particulate matter, $\mathrm{PM}_{2.5}=$ fine particulate matter |  |  |  |  |  |  |

Table 3.3-5 presents the estimated annual construction emissions anticipated to be generated by the proposed project.

Table 3.3-5
Summary of Estimated Annual Construction Emissions

|  | CO <br> (ton/yr) | NOx <br> (ton/yr) | ROG <br> (ton/yr) | SOx <br> (ton/yr) | $\mathbf{P M}_{10}$ <br> (ton/yr) | PM <br> (ton/yr) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| 2014 | 2 | 3 | $<1$ | $<1$ | $<1$ | $<1$ |
| 2015 | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ |
| AVAQMD CEQA <br> Threshold | 100 | 25 | 25 | 25 | 15 | 15 |
| Emissions Exceed <br> CEQA Threshold? | No | No | No | No | No | No |

Notes:
AVAQMD = Antelope Valley Air Quality Management District, CEQA = California Environmental Quality Act, CO = carbon monoxide,
$\mathrm{NOx}=$ nitrogen oxides, $\mathrm{ROG}=$ reactive organic gases, $\mathrm{SOx}=$ sulfur oxides, $\mathrm{PM}_{10}=$ inhalable particulate matter, $\mathrm{PM}_{2.5}=$ fine particulate matter
2014 emissions include those from the demolition, site preparation, grading, and building construction (partial) phases. 2015 emissions include those from the building construction (partial), paving, and architectural coating phases.
Although construction is assumed to take 16 to 18 months, a construction period of 12 months was assumed as a worst case (conservative) scenario for purpose of the air quality construction analysis.

## Operational Emissions

The CalEEMod air quality modeling tool was also used to estimate emissions generated during operation of the proposed project. The following assumptions were input into the model for the most conservative analysis possible:

- Electricity and utility usage was assumed for a 25,500 square foot facility.
- Default assumptions were used for VOC-containing materials such as coatings and cleaning supplies.
- Vehicle trips were obtained from the project proponent and were no more than 30 employees; 20 volunteers; and up to 70 visitors per day. The analysis assumed that all of these trips will occur on a daily basis.

Tables 3.3-6 and 3.3-7 present the estimated maximum daily and annual emissions anticipated to be generated during operation of the proposed project, respectively. There will also be a diesel-powered emergency generator on-site that will be required as part of maintenance activities to be exercised for a minimum of 30 minutes a month, and will only be used during power outages; therefore, daily and annual emissions from the generator under normal conditions will be minimal. The appropriate permit will be obtained from AVAQMD prior to installation and operation of the emergency generator and the operator will follow required recordkeeping, reporting, and monitoring procedures.

Table 3.3-6
Summary of Estimated Maximum Daily Operational Emissions

|  | CO <br> (ton/yr) | NOx <br> (ton/yr) | ROG <br> (ton/yr) | SOx <br> (ton/yr) | $\mathbf{P M}_{10}$ <br> (ton/yr) | PM <br> (ton/5r) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Building Operations | $<1$ | $<1$ | 2 | $<1$ | $<1$ | $<1$ |
| Vehicle Travel | 146 | 38 | 19 | $<1$ | 23 | 2 |
| Total | 146 | 38 | 21 | $<1$ | 23 | 2 |
| AVAQMD CEQA <br> Threshold | 548 | 137 | 137 | 137 | 82 | 82 |
| Emissions Exceed <br> CEQA Threshold? | No | No | No | No | No | No |

Notes:
AVAQMD = Antelope Valley Air Quality Management District, CEQA = California Environmental Quality Act, CO = carbon monoxide, lb/day = pounds per day, $\mathrm{NOx}=$ nitrogen oxides, $\mathrm{ROG}=$ reactive organic gases, $\mathrm{SOx}=$ sulfur oxides, $\mathrm{PM}_{10}=$ inhalable particulate matter, $\mathrm{PM}_{2.5}=$ fine particulate matter

Table 3.3-7
Summary of Estimated Annual Operational Emissions

|  | CO <br> (Ib/day) | $\mathbf{N O}_{\mathbf{x}}$ <br> (Ib/day) | ROG <br> (Ib/day) | SOx <br> (Ib/day) | $\mathbf{P M}_{10}$ <br> (Ib/day) | $\mathbf{P M}_{\mathbf{2 . 5}}$ <br> (Ib/day) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Building Operations | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ | $<1$ |
| Vehicle Travel | 24 | 7 | 3 | $<1$ | 4 | $<1$ |
| Total | 24 | 7 | 3 | $<1$ | 4 | $<1$ |
| AVAQMD CEQA <br> Threshold | 100 | 25 | 25 | 25 | 15 | 15 |
| Emissions Exceed <br> CEQA Threshold? | No | No | No | No | No | No |

Notes:
AVAQMD = Antelope Valley Air Quality Management District, CEQA = California Environmental Quality Act, CO = carbon monoxide, $\mathrm{NOx}=$ nitrogen oxides, $\mathrm{ROG}=$ reactive organic gases, $\mathrm{SOx}=$ sulfur oxides, $\mathrm{PM}_{10}=$ inhalable particulate matter, $\mathrm{PM}_{2.5}=$ fine particulate matter
a. Would the project conflict with or obstruct implementation of the applicable air quality plan?

LESS THAN SIGNIFICANT IMPACT. As can be seen from the air quality analysis performed for both the construction and operation, emissions from the proposed project will be well below AVAQMD's significance thresholds for CEQA. Further, the emissions have no potential to jeopardize or obstruct any AVAQMD clean air plan. The region is in attainment for all pollutants with the exception of $\mathrm{O}_{3}$ and $\mathrm{PM}_{10}$. As presented in Tables 3.34 through 3.3-7 above, $\mathrm{PM}_{10}$ emissions are negligible as well as emissions of nitrogen oxides (NOx) and VOCs; which contribute to $\mathrm{O}_{3}$ formation. The proposed project will adhere to all AVAQMD rules and regulations; including those described above for $\mathrm{PM}_{10}$ emission control from construction operations. The proposed project will not conflict with or obstruct implementation of the air quality plan for the region. Therefore, impacts will be less than significant and no mitigation is required.
b. Would the project violate any air quality standard or contribute substantially to an existing or projected air quality violation?

LESS THAN SIGNIFICANT IMPACT. The air quality analysis performed for the construction and operation of the proposed project, as summarized in Tables 3.3-4 through 3.3-7, indicates that emissions will be well below AVAQMD's significance thresholds for CEQA with no potential to contribute to a violation of an air quality standard. In addition, the proposed project will comply with existing AVAQMD rules, as well as applicable state and federal regulations pertaining to construction equipment, to further reduce any potential impacts. Impacts are considered less than significant and no mitigation is required.
c. Would the project result in a cumulatively considerable net increase of any criteria pollutant for which the project region is non-attainment under an applicable federal or state ambient air quality standard (including releasing emissions which exceed quantitative thresholds for $\mathrm{O}_{3}$ precursors)?

LESS THAN SIGNIFICANT IMPACT. The proposed project will not result in a cumulatively considerable net increase of any criteria pollutant. As shown above in Tables 3.3-4 through 3.3-7, emissions from the proposed project are negligible and are far below AVAQMD's CEQA thresholds.

The region is in nonattainment for $\mathrm{O}_{3}$ and $\mathrm{PM}_{10}$. As discussed above, the proposed project will not considerably contribute to an increase in $\mathrm{O}_{3}$ precursors or $\mathrm{PM}_{10}$ in any way. Impacts in this area are considered less than significant and no mitigation is required.
d. Would the project expose sensitive receptors to substantial pollutant concentrations?

LESS THAN SIGNIFICANT IMPACT. The proposed project consists of a main building, two parking lots, as well as an exercise yards and open space. The proposed project is surrounded by a major roadway (Sierra Highway) to the west, the Los Angeles County Sheriff's Department Palmdale Station to the north, a residential area to the east, and a recreational and commercial use to the south.

Residences, schools, daycare centers, playgrounds and medical facilities are considered sensitive receptor land uses under the AVAQMD CEQA Handbook and Federal Conformity Guidelines (2011). The Handbook mandates that an analysis be conducted for specific project types located within 300-1000 feet of a residence (depending on project type). The proposed animal care facility does not fall under the specific types of projects requiring such an analysis per the Handbook. However, construction and operation emissions were evaluated for the proposed project as discussed above. The location of the new facility is roughly in the center of the site in order to allow for distance between the new facility and the nearest sensitive receptors (i.e., existing residences and outdoor roller hockey rink). Although the nearest sensitive receptor to the site is the adjacent residences along the eastern boundary of the project site, the closest active areas associated with the new facility (i.e., car wash and emergency generator) is approximately 100 feet from the nearest sensitive receptor (residence at 38575 Friendly Avenue), and the outdoor roller hockey rink is approximately 128 feet from the closest portion of the main building and approximately 230 feet from the emergency generator, which is the nearest potential emission source.

Due to the small construction crew, short-term schedule, and minimal trips upon project completion, no impacts have been identified to sensitive receptors as a result of the project. In addition, the proposed project will comply with existing AVAQMD rules, as well as applicable state and federal regulations pertaining to construction equipment, to further reduce any impacts. As shown above, emissions of criteria pollutants and any toxic pollutants contained in VOCs and PM emissions will be minimal. Impacts in this area are considered less than significant and no mitigation is required.
e. Would the project create objectionable odors affecting a substantial number of people?

LESS THAN SIGNIFICANT IMPACT. The proposed project will not create objectionable odors affecting a substantial number of people. The proposed project is an animal care facility with residences that border the site to the east. All animals will be kept indoors and enclosures will be cleaned regularly with the waste stored in sealed receptacles and contained on-site prior to their disposal. Animals will not be permitted in the open area along the eastern area of the proposed facility (which is closest to the abutting residences), but will only be permitted in the exercise yards located to the north of the facility (south of the staff parking area) during day time hours. The nearest exercise yard to the residences is approximately 233 feet. Animals will not be permitted in an exercise without constant supervision; therefore, the full staff or part-time volunteers will clean up any animal waste as soon as it occurs at an exercise yard. There will also be a diesel-powered emergency generator on-site that will be required as part of maintenance activities to be exercised for a minimum of 30 minutes a month, and will only be used during power outages. The appropriate permit will be obtained from AVAQMD prior to installation and operation of the emergency generator and the operator will follow required recordkeeping, reporting, and monitoring procedures. Therefore, potential for odors from the emergency generator are expected to be minimal. Impacts associated with objectionable odors will be less than significant and no mitigation is required.

### 3.4 Biological Resources

## Biological Resources Checklist

| Would the project: | Potentially Significant Impact | Less Than Significant with Mitigation Incorporation | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
| a. Have a substantial adverse effect, either directly or through habitat modifications, on any species identified as a candidate, sensitive, or special status species in local or regional plans, policies, or regulations, or by the California Department of Fish and Game or U.S. Fish and Wildlife Service? | $\square$ | $\square$ |  | $凶$ |
| b. Have a substantial adverse effect on any riparian habitat or other sensitive natural community identified in local or regional plans, policies, regulations or by the California Department of Fish and Game or U.S. Fish and Wildlife Service? | $\square$ | $\square$ | $\square$ | $\lesssim$ |
| c. Have a substantial adverse effect on federally protected wetlands as defined by Section 404 of the Clean Water Act (CWA) (including, but not limited to, marsh, vernal pool, coastal, etc.) through direct removal, filling, hydrological interruption, or other means? | $\square$ | $\square$ | $\square$ | $\searrow$ |
| d. Interfere substantially with the movement of any native resident or migratory fish or wildlife species or with established native resident or migratory wildlife corridors, or impede the use of native wildlife nursery sites? | $\square$ | $\square$ |  | $\pm$ |
| e. Conflict with any local policies or ordinances protecting biological resources, such as a tree preservation policy or ordinance? | $\square$ | $\square$ |  | $\pm$ |
| f. Conflict with the provisions of an adopted Habitat Conservation Plan, Natural Community Conservation Plan, or other approved local or regional habitat conservation plan? | $\square$ | $\square$ |  | $\searrow$ |

### 3.4.1 Setting

The project site consists of approximately 5.8 -acres of vacant land, the northern portion of which is bare soil with ruderal (weedy) vegetation while the southern portion is paved. Several mature trees, including California sycamores (Platanus racemosa) are located along Sierra Highway adjacent to the site. Adjacent land uses include light industrial, commercial, recreational, and residential.

The nearest open space to the project site is located at Ritter Ranch, approximately five miles southwest of the project site. Ritter Ranch provides habitat for wildlife and a corridor for wildlife movement to the adjacent Angeles National Forest.

A search of the California Natural Diversity Database (CNDDB) identified 12 special-status wildlife and plant species with potential to occur within the U.S. Geological Survey (USGS)

Palmdale Quadrangle, as presented in Table 3.4-1 (CDFG, 2012). Special-status species include those federally- and/or state-listed as threatened, endangered, and/ or candidate plant or wildlife species as well as those identified as species of concern by the California Department of Fish and Wildlife (CDFW) ${ }^{9}$ for wildlife, and as rare, threatened, or endangered by the California Native Plant Society (CNPS) for plants.

According to historical information, it appears that the project site had been undeveloped in 1917. By 1928, the northern portion of the project site was agricultural land (orchard or groves). Building records issued as early as the 1950s indicated the use of the project site was for retail, including restaurants/lounge, salons, stores, and a church. Several commercial properties within the project site had been redeveloped by 1968; however, the northeastern corner of the project site remained undeveloped. By 2002, the project site had been cleared of previous building development and was left vacant as it appears today (LACDPW, 2011). Given the disturbed nature of the site, and the lack of anything but ruderal vegetation (i.e., weeds) at the site, the urbanized surrounding area, and the lack of appropriate habitat, no species have the potential to be located at the project site. One bird species, the Cooper's hawk (Accipiter cooperii) could occur transiently in mature trees along Sierra Highway adjacent to the site. However, there is no habitat for foraging or nesting at the site or in the vicinity. Other migratory birds, which are protected under the Migratory Bird Treaty Act (MBTA) as described below, may utilize the mature trees along Sierra Highway for foraging during migration, but will be unlikely to nest there given the limited habitat and high level of human activity nearby.

## Regulatory Setting

## Federal.

Endangered Species Act. The Endangered Species Act (ESA) of 1973 (Public Law 93-205) and subsequent amendments provide for the conservation of endangered and threatened species and the ecosystems upon which they depend. Section 7 of the ESA requires Federal agencies to aid in the conservation of listed species, and to ensure that the activities of Federal agencies will not jeopardize the continued existence of listed species or adversely modify designated critical habitat. At the Federal level, the U.S. Fish and Wildlife Service (USFWS) and the National Marine Fisheries Service are responsible for administration of the ESA.

Migratory Bird Treaty Act. The MBTA of 1918 (16 USC $\S \S 703$ - 712) decrees that all migratory birds and their parts (including eggs, nests, and feathers) are fully protected. Under the MBTA, taking, killing, or possessing migratory birds is unlawful. Projects that are likely to result in the taking of birds protected under the MBTA will require the issuance of take permits from the USFWS. Activities that will require such a permit will include, but not be limited to, the destruction of migratory bird nesting habitat during the nesting season when eggs or young are likely to be present. In accordance with the MBTA, surveys are required to determine if nests will be disturbed and, if so, a buffer area with a specified radius around the nest will be established so that no disturbance or intrusion will be allowed until the young had fledged and left the nest. If not otherwise specified in the permit, the size of the buffer area will vary with species and local circumstances (e.g.

[^7]Table 3.4-1
Special-Status Species and Natural Communities Documented in the Palmdale Quadrangle

| Species | Status | Habitat Requirements | Likelihood of Occurrence |
| :---: | :---: | :---: | :---: |
| Reptiles |  |  |  |
| Silvery legless lizard Anniella pulchra pulchra | CSC | Sandy or loose loamy soils under sparse vegetation. Soil moisture is essential. | Unlikely to occur. No suitable habitat in the project area. |
| Coast horned lizard Phrynosoma blainvillii | CSC | Frequents a wide variety of habitats, most common in lowlands along sandy washes with scattered low bushes. Open areas for sunning, bushes for cover, patches of loose soil for burial, and abundant supply of ants and other insects. | Unlikely to occur. No suitable habitat in the project area. |
| Birds |  |  |  |
| Cooper's hawk Accipiter cooperii | None | Woodland, chiefly of open, interrupted or marginal type. Nest sites mainly in riparian growths of deciduous trees, as in canyon bottoms on river flood-plains and in live oaks. | May occur transiently; no suitable habitat in the project area for nesting. |
| Burrowing owl Athene cunicularia | CSC | Open, dry annual or perennial grasslands, deserts, and scrublands characterized by low-growing vegetation. Subterranean nester, dependent upon burrowing mammals, most notably, the California ground squirrel. | Unlikely to occur. No suitable habitat in the project area. |
| Loggerhead shrike Lanius ludovicianus | CSC | Broken woodlands, savannah, Pinyon-Juniper, Joshua Tree, and riparian woodlands, desert oases, scrub, and washes. Prefers open country for hunting, with perches for scanning, and fairly dense shrubs and brush for nesting. | Unlikely to occur. No suitable habitat in the project area. |
| Least Bell's vireo Vireo bellii pusillus | FE, SE | Summer resident of Southern California in low riparian in vicinity of water or in dry river bottoms below 2000 feet. Nests placed along margins of bushes or on twigs projecting into pathways, usually willow, Baccharis, mesquite. | Unlikely to occur. No suitable habitat in the project area. |
| LeConte's thrasher Toxostoma lecontei | CSC | Desert resident; primarily of open desert wash, desert scrub, alkali desert scrub, and desert succulent scrub habitats. Commonly nests in a dense, spiny shrub or densely branched cactus in desert wash habitat, usually 2-8 feet above ground. | Unlikely to occur. No suitable habitat in the project area. |
| Tricolored blackbird Agelaius tricolor | CSC | Highly colonial species, most numerous in Central Valley and vicinity. Largely endemic to California. Requires open water, protected nesting substrate, and foraging area with insect prey within a few kilometers of the colony. | Unlikely to occur. No suitable habitat in the project area. |
| Mammals |  |  |  |

## Table 3.4-1

Special-Status Species and Natural Communities Documented in the Palmdale Quadrangle

| Species | Status | Habitat Requirements | Likelihood of Occurrence |  |  |  |
| :--- | :--- | :--- | :--- | :---: | :---: | :---: |
| San Joaquin pocket mouse <br> Perognathus inornatus inornatus | None | Typically found in grasslands and blue oak savannas. Needs <br> friable soils. | Unlikely to occur. No suitable <br> habitat in the project area. |  |  |  |
| Mohave ground squirrel <br> Xerospermophilus mohavensis | ST | Open desert scrub, alkali scrub, and Joshua Tree woodland. <br> Also feeds in annual grasslands. Restricted to Mojave Desert. <br> Prefers sandy to gravelly soils, avoids rocky areas. Uses <br> burrows at base of shrubs for cover. Nests are in burrows. | Unlikely to occur. No suitable <br> habitat in the project area. |  |  |  |
| Plants |  |  |  |  |  |  |
| Sagebrush loeflingia <br> Loeflingia squarrosa var. artemisiarum | CNPS List <br> 2.2 | Great basin scrub, Sonoran Desert scrub, desert dunes. Sandy <br> flats and dunes. Sandy areas around clay slicks with Sarcobatus, <br> Atriplex, Tetradymia, etc. 700-1200m. | Unlikely to occur. No suitable <br> habitat in the project area. |  |  |  |
| Short-joint beavertail <br> Opuntia basilaris var. brachyclada | CNPS List <br> $1 B .2$ | Chaparral, Joshua Tree woodland, Mojavean Desert scrub, <br> Pinyon-Juniper woodland, riparian woodland. Sandy soil or <br> coarse, granitic loam. 425-1800m. | Unlikely to occur. No suitable <br> habitat in the project area. |  |  |  |

Source: CDFG, 2012 search of the Palmdale 7.5-minute USGS quadrangle (Note: As of January 1, 2013, the California Department of Fish and Game [CDFG] is now called the California Department of Fish and Wildlife [CDFW]).

CNPS (California Native Plant Society) List 1B. 2 - Plants rare, threatened, or endangered in California and elsewhere, fairly threatened in California
CNPS List 2.2 - Plants rare, threatened, or endangered in California, but more common elsewhere; fairly threatened in California
CSC - California Species of Concern
FE - Federal Endangered
None - No official federal or state listing but considered rare to varying extent
SE - State Endangered
ST - State Threatened
presence of busy roads), and will be based on the professional judgment of the monitoring biologist.

State.
California Fish and Game Code (Sections 3500 through 3705). Sections 3500 through 3705 of the California Fish and Game Code protect most migratory bird species and active nests from harm or destruction.

California Endangered Species Act of 1984 (California Fish and Game Code 2050-2116). The California Endangered Species Act of 1984 provides for the protection of rare, threatened, and endangered plants and animals, as recognized by CDFW, and prohibits the unauthorized taking of such species. As a responsible agency, the CDFW has regulatory authority over state-listed endangered and threatened species. State agencies are required to consult with CDFW on actions that may affect listed or candidate species.

California Fish and Game Code (Streambed Alteration Agreement). Under Chapter 6 of the California Fish and Game Code, CDFW is responsible for protecting and conserving the state's fish and wildlife resources. Sections 1600 et seq. of the Code define the responsibilities of CDFW, and the requirement for public and private applicants to obtain an agreement to:
... divert, obstruct, or change the natural flow or bed, channel, or bank of any river, stream, or lake designated by CDFG ${ }^{10}$ in which there is at any time an existing fish or wildlife resource or from which those resources derive benefit, or will use material from the streambeds designated by the department.

Local.
Los Angeles County Oak Tree Ordinance (\#22.56.2180). The ordinance protects any tree of the oak genus (Quercus) over eight inches in diameter at breast height (dbh), or 12 inches dbh combined for multiple trunks. Protected oak trees may not be damaged, removed, or encroached upon (within five feet of the drip line or 15 feet from the trunk) without an oak tree permit. The permit applicant may be required to replace oaks removed at a ratio of 2:1. When replacement or relocation of oak trees on the project site is inappropriate, the applicant may be required to pay into the oak forests special fund to plant new trees on public lands, maintain oaks on public lands, purchase prime oak woodlands, and purchase oaks of cultural significance. There are no oak trees at or adjacent to the project site.

Los Angeles County Tree Protection. Los Angeles County Code , Title 16 - Highways, Division 5 - Miscellaneous Provisions, Chapter 16.76, requires a permit to trim, prune, cut, break, deface, destroy, burn, or remove any shade or ornamental tree, hedge, plant, shrub, or flower growing on any public highway, public ground, or public property within the County of Los Angeles. The permit is issued either by the Department of Parks and Recreation for public property or public grounds, or by the LACDPW, Road Maintenance Division for public highways. The permit requires replacement of any removed tree with another tree of a type and quality to be determined by either the Director of Parks and Recreation or the Assistant Deputy Director of the Road Maintenance Division of the

[^8]LACDPW. There are no trees at the site but there are street trees in the public right-of -way along Sierra Highway (adjacent to the project site). As the proposed facility will be public property within the County, this code will apply during operation.

City of Palmdale Joshua Tree and Native Desert Vegetation Preservation. Under City of Palmdale Municipal Code, Chapter 14.04, all development proposal applications for sites containing native desert vegetation shall include a desert vegetation preservation plan and obtain a native desert vegetation removal permit from the City's Landscape Architect for removal of Joshua trees (Yuсса brevifolia), California juniper (Juniperus californica), or any other native desert vegetation identified pursuant to the California Desert Native Plants Act (Food and Agricultural Code Section 80001, et seq.) as protected or designated on any state or federal rare and endangered species list. There is no native desert vegetation at or adjacent to the project site.

In addition, although the project site is within the boundary of the City of Palmdale, as part of the project the site will become County property; therefore, the site is governed by the County's regulations. As there are no native desert vegetation at or adjacent to the project site, the project is also consistent with the City of Palmdale's regulations.

### 3.4.2 Impact Analysis

a. Would the project have a substantial adverse effect, either directly or through habitat modifications, on any species identified as candidate, sensitive, or special-status species in local or regional plans, policies, or regulations, or by the California Department of Fish and Game or U.S. Fish and Wildlife Service?

NO IMPACT. All construction and construction staging will occur within the project site footprint and the site will be accessed by existing roadways. The project site consists of bare soil and pavement in an urbanized area and does not provide habitat for any threatened, endangered, or rare animal species. Additionally, the nearest habitat for migratory birds consists of mature trees along Sierra Highway adjacent to the site, which do not provide suitable habitat for nesting. Thus, no impacts associated with disturbance of nesting migratory birds will occur. There will be no impacts to specialstatus species or habitat from the project.
b. Would the project have a substantial adverse effect on any riparian habitat or other sensitive natural community identified in local or regional plans, policies, or regulations, or by the California Department of Fish and Game or U.S. Fish and Wildlife Service?

NO IMPACT. The project site consists of bare soil and pavement and is located in an urbanized area. Adjacent land uses include light industrial, commercial, recreational, and residential. There is no riparian habitat, other sensitive natural community, or ecologically significant or critical areas located within or adjacent to the project site; therefore, no impact will occur.
c. Would the project have a substantial adverse effect on federally protected wetlands as defined by Section 404 of the CWA (including, but not limited to, marsh, vernal pool, coastal, etc.) through direct removal, filling, hydrological interruption, or other means?

NO IMPACT. As indicated above, the project site consists of bare soil and pavement and is located in an urbanized area. There are no jurisdictional wetlands or drainage features on or adjacent to the project site; therefore, no impact to wetlands will occur.
d. Would the project interfere substantially with the movement of any native resident or migratory fish or wildlife species or with established native resident or migratory wildlife corridors, or impede the use of native wildlife nursery sites?

NO IMPACT. The project site is located within an urban area surrounded by developed properties and does not provide habitat that will be utilized as a wildlife corridor. These conditions will not change with construction or operation of the proposed project. Therefore, no impacts associated with wildlife movement will occur.
e. Would the project conflict with any local policies or ordinances protecting biological resources, such as a tree preservation policy or ordinance?

NO IMPACT. As indicated above, a majority of the project site is paved and the portion of the site that is not paved is an area of bare soil and ruderal (weedy) vegetation; no trees are located on the project site. Further, construction and construction staging will occur on the project site and the project does not require the trimming, pruning, cutting, breaking, defacing, destroying, burning, or removal of any shade or ornamental tree, hedge, plant, shrub, or flower growing on any public highway, public ground, or public property within the County of Los Angeles (such as the street trees along Sierra Highway). As such, the proposed project will not conflict with any local policies or ordinances protecting biological resources, including protected trees or desert vegetation, and thus, no impact will occur.
f. Would the project conflict with the provisions of an adopted Habitat Conservation Plan, Natural Community Conservation Plan, or other approved local, regional, or state habitat conservation plan?

NO IMPACT. The project site is located within the planning area of the West Mojave Plan, a Habitat Conservation Plan that is being prepared by the Bureau of Land Management (BLM) in collaboration with the region's cities, counties, state and federal agencies (BLM, 2012). The purpose of the West Mojave Plan is to provide a regional strategy for conserving plant and animal species and their habitats and to define an efficient, equitable, and cost-effective process for complying with threatened and endangered species laws. The Plan will establish Desert Wildlife Management Areas that will be managed for the long-term survival and recovery of special-status species including the desert tortoise and Mohave ground squirrel.

The project site is located in an urban, developed area which does not provide habitat for special-status species and will not be designated as protected by the West Mojave Plan. Therefore, the proposed project will not conflict with the provisions of the West Mojave Plan and no impact will occur.

### 3.5 Cultural Resources

## Cultural Resources Checklist

| Would the project: | Potentially Significant Impact | Less Than Significant with Mitigation Incorporation | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
| a. Cause a substantial adverse change in the significance of a historical resource as defined in §15064.5? | $\square$ | $\square$ |  | $\searrow$ |
| b. Cause a substantial adverse change in the significance of an archaeological resource pursuant to §15064.5? | $\square$ | $X$ |  |  |
| c. Directly or indirectly destroy a unique paleontological resource or site or unique geologic feature? | $\square$ | $\square$ | $\square$ | $\triangle$ |
| d. Disturb any human remains, including those interred outside of formal cemeteries? | $\square$ | $\square$ | $\square$ | $\pm$ |

### 3.5.1 Setting

Past archaeological investigations point to a lengthy prehistoric tradition in the Antelope Valley. Archaeologists have learned that the Antelope Valley has been inhabited for the past 5,000 years, and may have been occupied many thousands of years before that (City of Palmdale, 1993). Cultural groups known to have occupied the Antelope Valley in late prehistoric and early historic times include the Kitanemuk, Kawaiisu, Tatavium, and Serrano/Vanyume. For the purposes of archaeological classification, Palmdale was divided into three primary physiographic environment types: the rift zone, the foothill areas, and the desert floor. The project site is located within the desert floor, which is moderately high probability of discovering prehistoric and historic sites (City of Palmdale, 1993).

According to a paleontological sensitivity study prepared in April 1990 by Robert E. Reynolds, the curator of Earth Sciences at the San Bernardino County Museum, Palmdale's low-lying areas consist of Quaternary alluvium which is known to contain numerous vertebrate fossils. Although Exhibit ER-8 in the Environmental Resources Element of the City of Palmdale General Plan shows the project site is located in an undetermined area of paleontological sensitivity, historical information shows that the project site was previously graded and developed. As discussed further in Section 3.6 Geology and Soils, the site soils include fill materials and alluvial soils, to a depth to 50 feet below ground surface (bgs). Fills up to a maximum observed depth of three feet were encountered in the borings; however, deeper artificial fill may exist at the site. The fill material was probably placed during original site grading.

According to historical information, it appears that the project site had been undeveloped in 1917, and consisted of agricultural land (orchard or groves) by 1928. By 1937, a structure was depicted on the southern portion of the project site. By 1948, several more structures were developed on the project site, and by 1968 had been redeveloped into several commercial properties. Building records dated as early as the 1950s indicated that the use of
these properties were for retail, including restaurants/lounge, salons, stores, and a church. The project site has been vacant since 2002 (LACDPW, 2011). Indications are that this development included a basement located at approximately 11 feet bgs and two feet thick (LACDPW, 2012a). Given the previous development that has occurred on-site, including the use of fill material, the likelihood of encountering intact paleontological and/or archaeological resources is low. Additionally, there is no indication that this development is associated with historical resources and the likelihood of any potentially historic artifact associated with the past uses being located on-site is extremely unlikely given site redevelopment and subsequent demolition and paving.

## Regulatory Setting

Federal. Section 106 of the National Historic Preservation Act requires that projects with federal agency involvement must take into account the effects of the project on historic properties and provide the Advisory Council on Historic Preservation a reasonable opportunity to comment. The Act defines historic properties as those included in the National Register of Historic Place or meet the criteria for the National Register. Additionally, in carrying out the requirements of Section 106, a federal agency must consult with any Native American tribe that identifies religious and/or cultural connections to historic properties that may be affected by the agency's undertakings.

State. The proposed project is subject to CEQA which requires public or private projects financed or approved by public agencies to assess their effects on historical resources. CEQA uses the term "historical resources" to include buildings, sites, structures, objects or districts, each of which may have historical, prehistoric, architectural, archaeological, cultural, or scientific importance. CEQA states that if implementation of a project results in significant effects on historical resources, then alternative plans or mitigation measures must be considered; however, only significant historical resources need to be addressed (California Code of Regulations 15064.5 and 15126.4).

Properties that area listed in or eligible for listing in the National Register of Historic Places are considered eligible for listing in the CRHR, and thus are significant historical resources for the purpose of CEQA (PRC Section 5024.1(d)(1)). However, the project site is not listed or eligible for listing in the National Register.

Local. Under the Conservation and Open Space Element of the Draft Los Angeles County General Plan, proposed policies for the protection of cultural heritage resources include mitigating all impacts from new development on or adjacent to historical a cultural heritage resources sites to the greatest extent feasible; support the preservation and rehabilitation of historic buildings; ensure proper notification procedures to Native American tribes in accordance with Senate Bill 18; and, ensure proper notification and recovery processes are carried out for development on or near historical and cultural heritage resource sites.

The Environmental Resources Element of City of Palmdale General Plan requires an evaluation to ascertain whether a proposed area contains historic or cultural resources of local or regional significance.

Although the project site is within the boundary of the City of Palmdale, as part of the project the site will become County property; therefore, the proposed goals and policies
within the County's Draft General Plan are the governing regulation. However, the project is also consistent with the City of Palmdale General Plan.

### 3.5.2 Impacts Analysis

a. Would the project cause a substantial adverse change in the significance of a historical resource as defined in $\S 15064.5$ ?

NO IMPACT. Although the project site has been previously disturbed and developed (previously used for agricultural and commercial uses), the site is currently vacant with no structures remaining. The possibility of any potentially historical artifact being located on-site associated with the past uses is extremely unlikely, given that the site is highly disturbed and been developed and redeveloped, with subsequent demolish of all structures. In addition, there are no known or documented national or State historic resources that have been designated as landmarks or points of interest on or in the immediate vicinity of the project. Therefore, the development of the project will not alter or destroy potentially historic resources; no impact is anticipated.
b. Would the project cause a substantial adverse change in the significance of an archaeological resource pursuant to $\$ 15064.5$ ?

LESS THAN SIGNIFICANT IMPACT WITH MITIGATION INCORPORATION. As discussed above and further in Section 3.6 Geology and Soils, fills up to a maximum observed depth of three feet were encountered in the borings; however, deeper artificial fill may exist at the site. Additionally, the previous development likely included a basement located at approximately 11 feet bgs and two feet thick (refer to Section 3.6, Geology and Soils, for details on the existence of a subsurface slab/basement) while the proposed project will not. Based on recommendations contained in the Geotechnical Study Report prepared from the proposed project (LACDPW, 2012a) the footprint of the building should be excavated to depth of three feet as measured from existing grades, or to a depth of at least two feet below the bottom of footings (recommended at 18 -inches bgs), or to the depth of undocumented fill, whichever is deeper. Pavement and hardscape areas beyond the footprint of the buildings should be excavated to a depth of two feet, as measured from existing grades. The depth to which soils have been disturbed is likely greater than will occur for the proposed project.

Although the potential of encountering intact archeological resources is unlikely given that the project site has been previously graded and developed, the proposed project involves grading which has a potential to encounter unknown subsurface archaeological material. To avoid potential impacts to unknown archaeological resources that may be buried beneath the project site, the County of Los Angeles Department of Public Works will ensure that the following mitigation measure is implemented:

MM CUL-1. In the event any archaeological materials or subsurface deposits are exposed during ground disturbance, the construction contractor will cease activity in the affected area (e.g., redirect activities into another area within the site) until the discovery can be evaluated by a qualified archaeologist or historic resources specialist, as required, and appropriate
treatment measures implemented. If the discovery proves to be significant pursuant to Section 15064.5(c) of CEQA Guidelines, additional work such as testing or data recovery will be conducted as warranted. Methods during monitoring and/or recovery of archaeological resources shall be documented in a report of findings.

With incorporation of this mitigation measure, impacts to archaeological resources are anticipated to be less than significant.

## c. Would the project directly or indirectly destroy a unique paleontological resource or site or unique geologic feature?

NO IMPACT. As described under Item b above, fills up to a maximum observed depth of three feet were encountered in the borings; however, deeper artificial fill may exist at the site. Additionally, the previous development likely included basements while the proposed project will not. In addition, the proposed project will not require deep construction or footings that could encounter paleontological resources. Therefore it is unlikely the project will encounter nor directly or indirectly destroy a unique paleontological resource or unique geologic features. Therefore, no impacts are anticipated regarding paleontological resources.
d. Would the project disturb any human remains, including those interred outside of formal cemeteries?

NO IMPACT. According to historical information, the project site has been disturbed and occupied since 1928 with various uses including agricultural, commercial, retail, and restaurant uses, until 2002 when the entire project site appeared to be vacant of development. The previous development included artificial fill and buildings likely included basements. Given the previous disturbance, it is extremely unlikely that human remains will be encountered at the site. To avoid potential impacts to unknown human remains that may be buried beneath the surface in the work area, the County of Los Angeles Department of Public Works will ensure that the following mitigation measure is implemented:

MM CUL-2. In the event human remains are encountered during project construction, the Los Angeles County Coroner shall be immediately contacted to determine whether or not investigation of the cause of death is required. The Coroner shall make a determination of origin and disposition pursuant to Public Resources Code Section 5097.98. The Coroner will be notified of the find immediately. In the event it is determined by the Coroner the remains are Native American in origin, the Native American Heritage Commission shall be contacted to determine necessary procedures for protection and preservation of remains, including reburial, as provided in the CEQA Guidelines, Section 15064.5(e).

With incorporation of this mitigation measure, impacts to unknown human remains are anticipated to be less than significant.

### 3.6 Geology and Soils

Geology and Soils Checklist
Would the project:

### 3.6.1 Setting

The project site is located approximately 2,650 feet above mean sea level with surface topography in the general vicinity sloping up towards the southwest (USGS Topographic Map, Palmdale, California, 1974, photo revised 1958). The project site is underlain by loamy sands of the Cajun series (Soil Conservation Service SSURGO Data, EDR Radius Map Report ordered April 2011). During soil vapor sampling in January 2012 and geotechnical investigations conducted in March 2012, site soils consisted of fills and alluvial deposits to the maximum explored depth of up to 50 feet bgs (LACDPW, 2012b). The fill encountered at a maximum depth of three feet consist primarily of silty sand and clayey silt. The fill material was probably placed during original site grading. Deeper artificial fill may exist at
the site. The alluvial deposits below the fill primarily consist of silty sands and sand with gravels.

Major topographical features consist of the San Gabriel Mountains and Sierra Nevada Mountains, located south and north of the project, respectively. The project site is located approximately two miles north of the San Andreas Fault, which is the dominant seismic feature traversing the southernmost portion of Palmdale. The San Andreas Fault extends over 600 miles from the Salton Sea, northwest toward the Pacific Ocean at Point Arena. Two of the three largest (8.0+ Richter) earthquakes in the state have occurred along the San Andreas Fault, two of which were the 1906 San Francisco earthquake which caused 21-foot offsets and the 1857 Fort Tejon earthquake.

The Safety Element of the City of Palmdale General Plan also identifies active fault traces crossing through the valley soils in Palmdale, including the Cemetery Fault, the Nadeau Fault, and the Littlerock Fault. All three faults are active splays of the San Andreas Fault. Thus, movement on the San Andreas Fault may activate one or all of these subsidiary faults. Other splays of the San Andreas Fault which are found in Palmdale are the Powerline Fault and the eastern end of the Clearwater Fault. A number of other faults located in the Southern California region could be responsible for earthquakes that would affect the Palmdale area.

A Geotechnical Study Report was prepared for the project site for Los Angeles County by Converse Consultants in April 2012 (LACDPW, 2012b). The impacts analysis is based on finding of that study. Recommendations contained in that study is incorporated into the proposed project as mitigation.

Regulatory Setting
Federal. None.

## State.

Alquist Priolo Earthquake Fault Act. The Alquist-Priolo Earthquake Fault Zone Act of 1972 (California PRC, Division 2, Chapter 7.5) established the Alquist-Priolo Earthquake Fault Zones to mitigate the hazard of surface faulting to structures for human occupancy. The primary purpose of the Act is to prevent the construction of buildings for human occupancy on the surface trace of active faults, to provide the citizens with increased safety, and to minimize loss of life during and immediately following earthquakes by facilitating seismic retrofitting to strengthen buildings against ground shaking. The State Geologist is required to establish regulatory zones, known as Earthquake Fault Zones, around the surface traces of active faults and to produce appropriate maps to assist cities and counties in planning, zoning, and building regulation functions. The maps define potential surface rupture or fault creep. New geologic and seismic data is continually reviewed by the State Geologist and revisions are made to existing zones when warranted by new information. Local agencies are required to enforce the Act in the development permit process, where applicable, and may impose greater restrictions than State law requires.

Seismic Hazards Mapping Act. The State of California Seismic Hazards Mapping Act of 1990 (PRC Section 2690-2699) addresses the effects of strong ground shaking, liquefaction, landslides, and other ground failures due to seismic events. Under this Act, the State Geologist is required to delineate seismic hazard zones. Cities and counties are required to
regulate certain development projects within the zones, investigate the geologic and soil conditions of the project, and incorporate appropriate mitigation measures, as appropriate, into development plans.

California Building Code. The California Building Code (CBC), which is based on the International Building Code, requires that project structures be designed with adequate strength to withstand the lateral dynamic displacements induced by the Design Basis Ground Motion, which the CBC defines as the earthquake ground motion that has two percent chance of being exceeded in 50 years.

Local. Under the Safety Element of the Draft Los Angeles County General Plan, proposed policies for an effective regulatory system that prevents or minimizes personal injury, loss of life and property damage due to seismic and geologic hazards and flood and inundation hazards include: discourage development in Seismic and Geologic Hazard Zones and Flood Hazard Zones; prohibit new developments within fault traces until a comprehensive geological study has been completed, as defined by the Alquist-Priolo Act; support the retrofitting of unreinforced masonry structures to help reduce the risk of structural and human loss due to seismic or geological hazards; and, discourage development from locating in dam and reservoir inundation routes.

Building and construction within the County is governed by the latest version of the Los Angeles County Building Code, which references the CBC.

Building and construction within the City of Palmdale are subject to the regulations of the City of Palmdale Municipal Code (Chapter 8.04.201) that adopts and incorporates the CBC by reference (Ordinance 1410 Section 2, 2010). The Municipal Code includes amendments and modifications to the CBC that are specific to the City of Palmdale. The CBC incorporates provisions of the International Building Code, which contains seismic design criteria and grading standards.

Although the project site is within the boundary of the City of Palmdale, as part of the project the site will become County property; therefore, the County's General Plan goals and policies are the governing regulation. However, as the County's policies include building and construction that incorporates the CBC, the project is also consistent with the City of Palmdale's regulations.

### 3.6.2 Impact Analysis

a. Would the project expose people or structures to potential substantial adverse effects, including the risk of loss, injury, or death involving:
i) Rupture of a known earthquake fault, as delineated on the most recent AlquistPriolo Earthquake Fault Zoning Map issued by the State Geologist for the area or based on other substantial evidence of a known fault? Refer to Division of Mines and Geology Special Publication 42.

LESS THAN SIGNIFICANT IMPACT. The project site is not located within the boundaries of an Alquist-Priolo Special Studies Zone. The project site is located in a seismically active area, as is most of southern California. The nearest active fault/special study zone is the San Andreas fault system approximately two miles south of the project site (LACDPW, 2012b; California Department of Conservation,
1979). However, no active faults are known to cross the project site. Nonetheless, the proposed project will be designed and constructed in conformance with building and seismic code requirements and industry standards, including the most recent edition of the CBC, which reduces potential impacts by ensuring that development is designed to withstand seismic or other geologic hazards. Such a design is considered to result in an acceptable level of risk for the Southern California region. As such, the construction and operation of the project will have a less than significant impact related to the potential rupture of a known earthquake fault and no mitigation is required.

## ii) Strong seismic ground shaking?

LESS THAN SIGNIFICANT IMPACT. Given the seismically active region of southern California, the project site is susceptible to ground shaking emanating from causative faults during an earthquake. As indicated above, the nearest active earthquake fault to the project site is the San Andreas Fault Zone, located approximately two miles south of the project site. Ground shaking from seismic activity along nearby regional faults could also affect the project site. The project includes the construction of a new animal care facility and eastern perimeter concrete screen wall which will be designed in accordance with the latest building and seismic code requirements, such as the CBC, which will reduce potential adverse effects associated with seismic ground shaking. Therefore, the potential impact from strong seismic ground shaking will be considered less than significant and no mitigation is required.

## iii) Seismic-related ground failure, including liquefaction?

LESS THAN SIGNIFICANT IMPACT. Liquefaction describes a phenomenon in which a saturated soil loses strength during an earthquake as a result of induced shearing strains. Lateral and vertical movement of the soil mass combined with loss of bearing usually results. Loose sand, high groundwater conditions (where the water table is within approximately 50 feet of the ground surface), higher intensity earthquakes, and particularly long duration of ground shaking are the requisite conditions for liquefaction. Exhibit S-10, Soil Expansion Potential, of the Safety Element in the City of Palmdale General Plan indicates that the project site is located within a low liquefaction area. Geotechnical site specific exploration did not encounter groundwater to a depth of 50.5 feet bgs. Absence of groundwater within 50 feet indicates liquefaction potential is very low and potential for seismicallyinduced settlement is negligible. Additionally, design and construction of the proposed project will comply with applicable building code requirements and industry standards. Therefore, the risks associated with seismic-related ground failure, including liquefaction will be less than significant and no mitigation is required.

## iv) Landslides?

LESS THAN SIGNIFICANT IMPACT. Landslides and mudflows are most likely in the foothill and mountain areas where fractured and steep slopes are present (as in the San Gabriel Mountains). The project site is located within a predominantly flat
area of the Antelope Valley and not within an area susceptible to, or affected by, landslides. Therefore, the potential risks associated with landslides are considered less than significant and no mitigation is required.
b. Would the project result in substantial soil erosion or the loss of topsoil?

LESS THAN SIGNIFICANT IMPACT. As shown in Exhibit S-11, Soil Erosion Potential, of the City of Palmdale General Plan, the project site is within an area of moderate soil erosion potential. Construction activities will include grading, excavation, trenching for utilities, temporary staging, and construction on flat terrain. These activities could result in the potential for erosion to occur at the project site, though soil exposure will be temporary and short-term in nature. Project implementation will increase storm water runoff from the project site and could result in additional water erosion. Construction projects resulting in the disturbance of one acre or more are required to obtain a National Pollutant Discharge Elimination System (NPDES) permit issued by the Regional Water Quality Control Board (RWQCB) to control soil erosion due to storm water. In addition, implementation of best management practices (BMPs) and a Storm Water Pollution Prevention Plan (SWPPP) will minimize the potential for soil erosion and sedimentation. After construction is completed, the project site will be covered by paving or landscaping and no large areas of exposed soil that will be exposed to erosion effects of wind or water will remain. As such, construction or operation of the project will have less than significant impacts related to erosion and loss of topsoil and no mitigation is required.
c. Would the project be located on a geologic unit or soils that is unstable, or that would become unstable as a result of the project, and potentially result in an on-site or offsite landslide, lateral spreading, subsidence, liquefaction, or collapse?

LESS THAN SIGNIFICANT IMPACT. The project will be constructed within an area of slow soil infiltration capacity (City of Palmdale, 1993). Soil borings, and vapor probes were installed at the project site as part of site investigations and did not encounter groundwater in any of the borings completed at depths up to 50.5 feet bgs. In addition, the Department of Water Resource data (2012) for Well 06N12W26Z003S (located underneath the project site) indicate the depth of groundwater was 262 feet in 1911. Due to the absence of shallow groundwater ( $>50$ feet), the risk for liquefaction at the site will be considered very low. As indicated above, the project site is located in a predominantly flat area of the Antelope Valley and not within an area susceptible to, or affected by, landslides. The soils under the project site will not become unstable or potentially result in off-site landslide, lateral spreading, subsidence, liquefactions or collapse. Additionally, design and construction of the project will comply with applicable building and safety requirements (such as the building standards contained in the most recent edition of the CBC). The proposed project will also comply with recommendations contained in the 2012 Geotechnical Study Report for the project site, including over-excavation and compaction of the existing site soils and undocumented fill material (LACDPW, 2012b). Therefore, the impact is considered less than significant and no mitigation is required.
d. Would the project be located on expansive soil, as defined in Table 18-1-B of the Uniform Building Code (1994), creating substantial risks to life or property?

LESS THAN SIGNIFICANT IMPACT WITH MITIGATION INCORPORATION.
Expansive soils are soils with a significant amount of clay. These soils have the ability to take on and absorb water. When this occurs, the soils swell and exert pressure on the loads imposed on them. As shown in Exhibit S-10, Soil Expansion Potential, of the City of Palmdale General Plan, soils at the project site have a low potential to be expansive. The subsurface soils at the project site consist of silty sands to sandy silts, which are materials that do not substantially expand or shrink with an increase in the moisture content. In addition, laboratory tests from the geotechnical investigation indicate the site soils have a low expansion potential. However, to further address the hazards associated with expansive soils, the following mitigation measures will be incorporated into project design/ specifications and followed during site construction:

MM SOILS-1. The proposed project will be designed and constructed in accordance with remedial grading and compaction requirements contained in the report entitled "Geotechnical Study Report, East Antelope Valley Animal Shelter"11 by Converse Consultants (April 19, 2012).

MM SOILS-2. The proposed project will follow site-specific geotechnical recommendations (e.g., drill drain holes and backfill, and excavate at least the upper two feet of soil for pavement) for the abandonment of the subsurface slab/basement, detailed in the correspondence from Converse Consultants dated October 10, 2012.

With incorporation of the above mitigation measures, the compacted fill soils are anticipated to have similar engineering characteristics with the underlying alluvial soils, and the placement of the new one-story building and associated hardscape improvements are not expected to result in collapse or soil settlement. Therefore, impacts from unstable/expansive soil conditions are anticipated to be less than significant.

Would the project have soils incapable of adequately supporting the use of septic tanks or alternative wastewater disposal systems where sewers are not available for the disposal of wastewater?

NO IMPACT. The proposed animal care facility will use the existing municipal sewer system and will therefore not require the use of septic tanks or alternative wastewater disposal systems. Therefore, no impact will occur.

[^9]
### 3.7 Greenhouse Gas Emissions

Greenhouse Gas Emissions Checklist

| Would the project: | Potentially Significant Impact | Less Than Significant with Mitigation Incorporation | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
| a. Generate greenhouse gas (GHG) emissions, either directly or indirectly, that may have a significant impact on the environment? | $\square$ |  | $\pm$ |  |
| b. Conflict with any applicable plan, policy, or regulation of an agency adopted for the purpose of reducing the emissions of GHGs? | $\square$ | $\square$ | $\triangle$ |  |

### 3.7.1 Setting

Various gases in the earth's atmosphere play an important role in moderating the earth's surface temperature. Solar radiation enters earth's atmosphere from space and a portion of the radiation is absorbed by the earth's surface. The earth emits this radiation back toward space, but the properties of the radiation change from high-frequency solar radiation to lower-frequency infrared radiation. Greenhouse gases (GHGs) are transparent to solar radiation, but are effective in absorbing infrared radiation. Consequently, radiation that will otherwise escape back into space is retained, resulting in a warming of the earth's atmosphere. This phenomenon is known as the greenhouse effect.

Scientific research to date indicates that some of the observed climate change is a result of increased GHG emissions associated with human activity. Among the GHGs contributing to the greenhouse effect are water vapor, carbon dioxide $\left(\mathrm{CO}_{2}\right)$, methane $\left(\mathrm{CH}_{4}\right)$, nitrous oxide ( $\mathrm{N}_{2} \mathrm{O}$ ), and chlorofluorocarbons. Human-caused emissions of these GHGs in excess of natural ambient concentrations are considered responsible for enhancing the greenhouse effect. GHG emissions contributing to global climate change are attributable, in large part, to human activities associated with the industrial/manufacturing, utility, transportation, residential, and agricultural sectors.

In 2008, California statewide GHG emissions were 474 million metric tons $\mathrm{CO}_{2}$-equivalent ( $\mathrm{MTCO}_{2} \mathrm{e}$ ) per year. Transportation contributes the most to the GHG emissions, followed by electric power generation (CARB, 2010).

## Regulatory Setting

Federal. None.
State. In 2006, the California State Legislature signed the Global Warming Solutions Act of 2006 or Assembly Bill (AB) 32, which provides the framework for regulating GHG emissions in California. This law requires CARB to design and implement emission limits, regulations, and other measures such that statewide GHG emissions are reduced in a technologically feasible and cost-effective manner to 1990 levels by 2020. The statewide 2020 emissions limit is 427 million MTCO $\mathrm{O}_{2}$ (CARB, 2006).

Local. Since the County of Los Angeles has not adopted thresholds of significance associated with GHG emissions for County projects, this analysis uses significance thresholds developed by the Antelope Valley AQMD. To provide guidance to local lead agencies on determining significance for GHG emissions in their CEQA documents, the Antelope Valley AQMD revised their CEQA and Federal Conformity guidelines in August 2011. This document includes a significance threshold of 100,000 tons per year and 548,000 pounds (lbs) per day of carbon dioxide equivalent $\left(\mathrm{CO}_{2} \mathrm{e}\right)$ that applies to all CEQA projects. $\mathrm{CO}_{2} \mathrm{e}$ is a measure used to compare the emissions from various GHGs based upon their global warming potential (GWP). $\mathrm{CO}_{2} \mathrm{e}$ are commonly expressed in terms of metric tons (i.e., $\mathrm{MTCO}_{2} \mathrm{e}$ ). The $\mathrm{CO}_{2}$ e for a gas is derived by multiplying the tons of the gas by its associated GWP. The GWP of a GHG, is also dependent on the lifetime, or persistence, of the gas molecule in the atmosphere. For example, $\mathrm{CH}_{4}$ is a much more potent GHG than $\mathrm{CO}_{2}$. Most mandatory and voluntary reporting registries require the use of the GWPs published in the Intergovernmental Panel on Climate Change's (IPCC's) Second Assessment Report (IPCC 1996); therefore, the GWPs from the Second Assessment Report were used to maintain consistency with the international standard. The Second Assessment Report describes that one ton of $\mathrm{CH}_{4}$ has the same contribution to the greenhouse effect as approximately 21 tons of $\mathrm{CO}_{2}$. Expressing GHG emissions in $\mathrm{CO}_{2} \mathrm{e}$ takes the contribution of all GHG emissions to the greenhouse effect and converts them to a single unit equivalent to the effect that will occur if only $\mathrm{CO}_{2}$ were being emitted.

Below is the formula for calculating the emissions:

$$
\mathrm{TCO}_{2} \mathrm{e}=(\text { tons of a gas }) *(\mathrm{GWP} \text { of the gas })
$$

On January 16, 2007, the County of Los Angeles adopted the Energy and Environmental Policy as part of the County's effort to help conserve natural resources and protect the environment. The goal of the policy is to provide guidelines for the development, implementation, and enhancement of energy conservation and environmental programs (e.g., energy and water efficiency, environmental stewardship, public outreach and education, and sustainable design). In order to meet the goals of the policy and ultimately AB 32, the County has implemented energy efficient projects in County facilities, specifically retrofitting or replacing building lighting systems and air conditioning equipment or as is the case of the proposed project, the certification of new development. The County has also developed/adopted tools and policies to support the reduction of GHG emissions that include but are not limited to: the "green building" ordinance, which will lead to all new private development within the unincorporated areas of the County being certified under the LEED or equivalent standards; County sponsored recycling programs; and the incorporation of Low Impact Design Standards and drought tolerant landscaping.

### 3.7.2 Impact Analysis

GHG emissions will be emitted as a result of the construction and operation of the proposed project. The majority of GHG emissions will be temporary and occur during the construction phase, which is expected to begin in summer of 2014 and last 16 to 18 months. These emissions will result from the use of on-road vehicles and diesel-fueled off-road equipment. Maximum daily and annual GHG emissions for construction phases are presented in Tables 3.7-1 and 3.72, respectively. Detailed assumptions and calculations for estimating purposes are included in Appendix A. Construction emissions were calculated using the CalEEMod program.

Table 3.7-1
Maximum Daily Project Construction GHG Emissions

| Construction Phase | $\mathbf{C O}_{\mathbf{2}} \mathbf{e}$ (Ib/day) |
| :--- | :--- |
| Demolition | 5,515 |
| Site Preparation | 3,343 |
| Grading | 2,778 |
| Building Construction | 3,291 |
| Paving | 1,848 |
| Architectural Coating | 352 |
| AVAQMD CEQA Threshold | 548,000 |
| Emissions Exceed CEQA <br> Threshold? | No |

Notes:
AVAQMD = Antelope Valley Air Quality Management District, CEQA = California Environmental Quality Act, $\mathrm{CO}_{2} \mathrm{e}=$ carbon dioxide equivalent, $\mathrm{GHG}=$ greenhouse gas, lb/day = pounds per day

Table 3.7-2
Annual Project Construction GHG Emissions (MTCO2e/year)

| Construction Phase | $\mathbf{2 0 1 4}$ | $\mathbf{2 0 1 5}$ |
| :--- | :---: | :---: |
| Demolition | 50 | - |
| Site Preparation | 3 | - |
| Grading | 5 | - |
| Building Construction | 263 | 31 |
| Paving | - | 8 |
| Architectural Coating | - | 2 |
| Annual Construction Emissions | $\mathbf{3 2 1}$ | $\mathbf{4 1}$ |
| Total Construction Emissions |  |  |

Notes:
GHG = greenhouse gas, $\mathrm{MTCO}_{2} \mathrm{e} /$ year $=$ metric tons carbon dioxide equivalent per year
Totals may not add up due to rounding. The construction emissions were calculated based on a 12 month construction schedule (which is a worst case scenario) at 5 days per week, 8 hours per day, assuming the maximum number of equipment on-site.

Once constructed, emissions associated with project operation will result primarily from employee, volunteer and visitor trips and from truck deliveries. There will also be a dieselpowered emergency generator on-site; however, the generator will be operated only periodically for testing (minimum of 30 minutes once a month) and will only be used during power outages. Therefore, daily and annual emissions from the generator under normal conditions will be minimal.

Indirect GHG emissions will occur from electricity use of the project. The new facility will be designed and constructed to achieve (at a minimum) LEED Silver level certification, which will incorporate sustainable design features to optimize energy use, enhance the sustainability of the site, reduce water use and maximize the use and reuse of sustainable and local resources. While not explicitly quantified because the exact amount of expected emissions reductions is not known, the incorporation of LEED design will serve to reduce GHG emissions associated with the proposed project. Daily and annual operation emissions are expected to be minimal and are presented in Tables 3.7-3 and 3.7-4, respectively. Maximum daily and total annual emissions
associated with the proposed project construction and operations compared with the AVAQMD thresholds are presented in Table 3.7-5. CEQA and Federal Conformity Guidelines (AVAQMD, 2011) does not specify that amortized construction emissions should be added to the operational emissions; therefore to be conservative, total construction emissions and annual operational emissions were compared against the thresholds. Appendix A contains the CalEEMod output showing GHG emissions during project operations.

Table 3.7-3
Maximum Daily Operational GHG Emissions (lb CO2e/day)

| Emissions Type | $\mathbf{2 0 1 5}$ and beyond |
| :---: | :---: |
| Energy Usage | 90 |
| Mobile Sources (vehicles) | 21,253 |
| Area Sources | $<1$ |
| Total | 21,343 |
| AVAQMD CEQA Threshold | 548,000 |
| Emissions Exceed CEQA Threshold? | No |

Note:
AVAQMD = Air Quality Management District, CEQA = California Environmental Quality Act, GHG = greenhouse gas, Ib $\mathrm{CO}_{2} \mathrm{e} / \mathrm{day}=$ pounds of carbon dioxide equivalent per day

Table 3.7-4
Annual Operational GHG Emissions (MTCO2elyear)

| Emissions Type |  |
| :---: | :---: |
| Energy Usage | $\mathbf{2 0 1 5}$ and beyond |
| Waste | 123 |
| Water | 125 |
| Mobile Sources (vehicles) | 17 |
| Area Sources | 3,141 |
| Total | 0 |

Note:
GHG = greenhouse gas, $\mathrm{MTCO}_{2} \mathrm{e} /$ year = metric tons carbon dioxide equivalent per year
Totals do not add up due to rounding. Emissions from "Water" includes energy used to supply, distribute, and treat water and wastewater associated with the proposed project.

Table 3.7-5
Total Proposed Project GHG Emissions Compared to AVAQMD Thresholds

| Emissions Type | Daily Emissions (lbs $\left.\mathbf{C O}_{2} \mathbf{e} / \mathrm{day}\right)$ | Annual Emissions (MTCO |
| :---: | :---: | :---: |
| $\mathbf{2} \mathbf{e}$ / year) |  |  |
| Total Construction Emissions ${ }^{1}$ | 5,515 | 363 |
| Total Operational Emissions | 21,343 | 3,406 |
| AVAQMD GHG Thresholds | 548,000 | $90,718^{2}$ |
| Exceeding Thresholds? | No | No |

Note:
AVAQMD = Antelope Valley Air Quality Management District, GHG = greenhouse gas, lbs $\mathrm{CO}_{2} \mathrm{e} /$ day $=$ pounds of carbon dioxide equivalent per day, $\mathrm{MTCO}_{2} \mathrm{e} /$ year = metric tons carbon dioxide equivalent per year
${ }^{1}$ Construction emissions presented for comparison with the annual threshold are the total construction emissions from all construction phases occurring in 2014 and 2015. Construction emissions during the individual years in 2014 and 2015 will be less than this amount.
${ }^{2}$ AVAQMD's annual GHG threshold was converted from short tons to metric tons.
a. Would the project generate GHG emissions, either directly or indirectly, that may have a significant impact on the environment?

LESS THAN SIGNIFICANT IMPACT. As shown in Tables 3.7-1 through 3.7-5 above, the proposed project will result in a short-term increase in GHG emissions during construction and minimal GHG emissions from its operation. The annual GHG emissions, which include the direct emissions from additional vehicle travel, the indirect emissions from electricity purchasing, and the construction emissions are substantially less than the AVAQMD GHG significance threshold of 100,000 short tons per year ( $90,718 \mathrm{MTCO}_{2} \mathrm{e} /$ year) and $548,000 \mathrm{lbs}$ per day of $\mathrm{CO}_{2} \mathrm{e}$. Therefore, the proposed project will result in a less than significant impact from GHG emissions and no mitigation is required.
b. Would the project conflict with any applicable plan, policy, or regulation of an agency adopted for the purpose of reducing the emissions of GHGs?

LESS THAN SIGNIFICANT IMPACT. The proposed project will not conflict with an applicable plan, policy, or regulation adopted to reduce GHG emissions. The short-term construction GHG emissions will not interfere with the AB 32 Scoping Plan and the long-term goal of AB 32 to reduce GHG emissions to 1990 levels by 2020. Operation of the proposed project will result in minor GHG emissions from vehicle travel and electricity use. However GHG emissions are negligible compared to the statewide GHG inventory. In addition, the new facility will be designed and operated under the LEED program, which confirms with the County's adopted Energy and Environmental Policy to enhance energy conservation. It is anticipated that the proposed project through design and operation will include energy-related conservation equipment and practices as part of compliance with both LEED certification and the County's adopted Energy and Environmental Policy. Incorporation of LEED design will serve to reduce GHG emissions associated with the proposed project. Therefore, the project will not conflict with plans, policies, or regulations intended to reduce GHGs and impacts will be less than significant and no mitigation is required.

### 3.8 Hazards and Hazardous Materials

Hazards and Hazardous Materials Checklist
Would the project:

a. | Create a significant hazard to the public or the |
| :--- |
| environment through the routine transport, use, or |
| disposal of hazardous materials? |
| Potentially |
| Significant |
| Impact |

| Cess Than |
| :--- |
| Significant with |
| Mitigation |
| Incorporation |


| Less Than |
| :--- |
| Significant |
| Impact |
| environment through reasonably foreseeable upset |
| and accident conditions involving the release of |
| hazardous materials into the environment? |

c. | Emit hazardous emissions or handle hazardous or |
| :---: |
| acutely hazardous materials, substances, or waste |
| within one-quarter mile of an existing or proposed |

school?
d. Be located on a site, which is included on a list of hazardous materials sites compiled pursuant to Government Code Section 65962.5 and, as a result, would it create a significant hazard to the public or the environment?
e. For a project located within an airport land use plan, or where such a plan has not been adopted, within two miles of a public airport or public use airport, would the project result in a safety hazard for people residing or working in the project area?
f. For a project within the vicinity of a private airstrip, would the project result in a safety hazard for people residing or working in the project area?
g. Impair implementation of or physically interfere with an adopted emergency response plan or emergency evacuation plan?
h. Expose people or structures to a significant risk of loss, injury, or death involving wildland fires, including where wildlands are adjacent to urbanized areas or where residences are intermixed with wildlands?

### 3.8.1 Setting

The project site consists of approximately 5.8 -acres of vacant land in which the northern portion is bare soil and the southern portion is covered by pavement. Adjacent land uses include light industrial, commercial, and residential. There are no schools located within one quarter mile of the project site, and the project site is not located in the vicinity of an airport or private airstrip. A helipad is located to the north at the Los Angeles County Sheriff's Department Palmdale Station.

A Phase I Environmental Site Assessment (Phase I ESA) was conducted for the site to identify potential environmental conditions, including the presence of hazardous materials, in connection with past uses of the site and past and current uses of nearby properties (LACDPW, 2011). The Phase I ESA included a search of regulatory databases, a reconnaissance survey, interviews with the property owner representatives and public agency personnel, and review of historical photos and maps. Based on information provided by the regulatory database search, the project site does not appear on any list of hazardous materials sites compiled pursuant to Government Code Section 65962.5.

The findings of the Phase I ESA indicated there was potential for the presence of hazardous materials from the historic use of the site for light industrial and agricultural purposes and the historic use of the adjacent properties for service stations and dry cleaners. The Phase I ESA concluded that a Phase II ESA, including soil and soil gas sampling, was warranted to evaluate the potential for subsurface contamination due to the historic light industrial use of the site and adjacent properties. Due to the time elapsed since last possible application of agricultural chemicals at the site (prior to 1950), sampling was not warranted for potential agricultural chemicals (LACDPW, 2011).

A Phase II ESA was subsequently conducted and included sampling of soil and soil gas at several locations at the project site (LACDPW, 2012a). Soil samples were analyzed for total
petroleum hydrocarbons (TPH) carbon chain analysis and gasoline, metals, VOCs, and semi-volatile organic compounds. Soil gas samples were analyzed for VOCs plus oxygenates and TPH-gasoline. Groundwater was not encountered in any of the borings completed to depths up to 50.5 feet bgs.

The findings of the Phase II ESA indicate that low concentrations of tetrachloroethene (PCE) were detected in the underlying soils in the southwestern portion of the site and appear to be associated with former dry cleaners west and south of site, which are the presumed sources. Based on the proposed animal care facility development plans, no structures are proposed to be constructed in the southwestern portion of the site over where the PCE was detected. Based on the concentrations and a human health risk evaluation, the Phase II ESA concluded that the site does not pose a health risk for the proposed commercial/industrial land use or for construction workers.

During previous investigative activities at the project site, a subsurface feature was encountered at approximately 11 feet bgs. The subsurface feature was determined to be a concrete slab about two feet thick that appears to have been the abandoned basement slab of the previous building. The subsurface slab will be drilled with drain holes and backfilled in place during construction of the proposed project. The area of the subsurface slab will be a paved surface parking lot (LACDPW, 2012c).

## Regulatory Setting

Federal. The USEPA is the lead federal agency responsible for enforcing federal regulations regarding hazardous materials. The project site is not a known superfund site or a site that has stored or generated hazardous waste; therefore, many of the federal regulations do not apply.

State. The California Department of Toxic Substances Control (DTSC) and the RWQCB are the state agencies primarily responsible for the regulation of hazardous materials in California. DTSC is responsible for the management of hazardous substances and oversees the investigation and remediation of contaminated sites. The Lahontan RWQCB is primarily responsible for the protection of groundwater and surface water resources from hazardous materials in the project area. The project site is not a known superfund site or a site that has stored or generated hazardous waste (DTSC, 2012); therefore, many of the state regulations do not apply.

State of California Occupational Safety and Health Act (Cal OSHA). Cal OSHA regulates worker safety similar to federal OSHA but also requires preparation of an Injury and Illness Prevention Program, an employee safety program of inspections, procedures to correct unsafe conditions, employee training, and occupational safety communication. In addition, Cal OSHA regulations indirectly protect the general public by requiring construction managers to post warnings signs, limit public access to construction areas, and obtain permits for work considered to present a significant risk of injury, such as excavations greater than five feet.

In addition, Cal OSHA requires the maintaining of Materials Safety Data Sheets (MSDSs) for hazardous materials present in DACC's operations which identify the types and handling requirements of hazardous materials used in given areas (such as the sanitation solutions and pharmaceuticals stored and used at an animal care center).

Unified Hazardous Waste and Hazardous Materials Management Regulatory Program. This program designates local agencies called Certified Unified Program Agencies (CUPAs). These local agencies have jurisdiction to manage hazardous substances with respect to hazardous waste generators and hazardous waste on-site treatment; underground storage tanks; aboveground storage tanks; and hazardous materials release response plans and inventories (business emergency plans [BEP]), including Unified Fire Code hazardous materials management plans and inventories; and risk management and accidental release prevention programs.

## Waters Bill of 1985 (Business Emergency Plan/Hazardous Materials Business Plan).

Administered by the CUPA, the Waters Bill requires facilities which meet minimum hazardous materials use/storage thresholds to file a BEP, or a Hazardous Materials Business Plan (HMBP), which includes a complete inventory of the hazardous materials being used and stored on a site. Employee training and emergency response plans and procedures for the accidental release of hazardous materials are also included in a BEP.

Antelope Valley Air Quality Management District Rule 403. Rule 403 requires actions to prevent, reduce or mitigate fugitive dust emissions from sources including, but not limited to, earth-moving activities, construction/demolition activities, disturbed surface area, or heavy- and light-duty vehicular movement.

Medical Waste Management Act (MWMA). MWMA (California Health and Safety Code, Sections 117600 -
118360) http://www.cdph.ca.gov/certlic/medicalwaste/Documents/MedicalWaste/2013/ MWMAfinal2013.doc governs the management of medical waste in all jurisdictions of the state. The Act identifies and regulates the type of medical waste generators, as well as regulates the containment and storage of medical waste, treatment of waste (including sharps waste and animal remains), haulers of waste, and enforcement.

Local. The owner or operator of any business or entity that handles a hazardous material above threshold quantities is required, by State and Federal laws, to submit a HMBP to the local CUPA. The CUPA with local jurisdiction over the proposed project area is the Los Angeles County Fire Department, Health Hazardous Materials Division.

In addition, DACC has policies and procedures, such as Policy No. OPG120, Controlled Substances, which details the storage, use and disposal of controlled substances (such as sodium pentobarbital, ketamine and diazepam) at an animal care facility.

### 3.8.2 Impacts Analysis

a. Would the project create a significant hazard to the public or the environment through the routine transport, use, or disposal of hazardous materials?

LESS THAN SIGNIFICANT IMPACT WITH MITIGATION INCORPORATION. Hazardous materials will be handled in compliance with applicable laws and regulations regarding transport, handling, disposal, and storage. Small quantities of hazardous materials will be used during project construction, such as gasoline, diesel fuel, motor oil, cleaning chemicals and detergents, lubrication oil, and oxygen and acetylene for any welding activities. Transport, handling, disposal, and storage of these materials to and from the project site would occur in compliance with applicable
regulations. Best management practices will be used during construction to prevent and control spills and leaks of these substances.

Based on the Phase II ESA (LACDPW, 2012a), soil and soil gas samples taken at the project site in May and July 2011 showed low human health risk levels of total petroleum hydrocarbons and volatile organic compounds, all of which were below regulatory and permissible exposure limits for residential and commercial/industrial land uses. Although no visible signs of contamination were observed during sampling, there is a potential to encounter unknown subsurface contamination during construction. For this reason, the following mitigation measure will be implemented:

MM HAZ-1. Although contaminated soil is not anticipated to be encountered, in the event soil contamination is encountered during earthwork activities, all contaminated soil handling and removal will be required to adhere to a soil management plan prepared and approved by the County. The soil management plan will specify procedures for the proper handling and disposal of contaminated soil in accordance with all applicable local and state regulations.

With implementation of this mitigation measure, potential impacts to the public, including construction workers, from unknown hazardous materials encountered during construction at the site and from the transport and disposal of any such hazardous materials are anticipated to be less than significant.

Operation of the proposed facility will require the use and storage of routine chemicals such as cleaning compounds. In addition, the proposed animal care facility includes an on-site clinic. The clinic includes the storage and use of pharmaceuticals (such as anesthetic, sedative and euthanasia solution) commonly utilized in the daily operations of the facility. All sanitation solution and pharmaceuticals will be stored in a manner specified in their applicable MSDS and DACC's policies and procedures. Medical waste (such as sharps and animal remains) will be stored and disposed of in accordance with the MWMA, which includes the pick-up and disposal of such waste by a licensed disposal services under contract with DACC. Therefore, with storage, handling, and transport of such materials in compliance with applicable regulations, the proposed project will not create a significant hazard to the public or the environment through the routine transport, use, or disposal of hazardous materials, and impacts are anticipated to be less than significant.
b. Would the project create a significant hazard to the public or the environment through reasonably foreseeable upset and accident conditions involving the release of hazardous materials into the environment?

LESS THAN SIGNIFICANT IMPACT. During construction, spill handling procedures will be implemented should a small fuel (gasoline, diesel, or oil) spill occur during onsite refueling. Any release of construction-related hazardous materials will be limited to small areas of contaminated soil, if spills occur during fueling or operation of construction equipment. No hazardous materials will be used during operation of the proposed facility other than cleaning chemicals. Therefore, the proposed project will not create a significant hazard to the public or the environment through an accidental release of hazardous materials. Impacts will be less than significant and no mitigation is required.
c. Would the project emit hazardous emissions or handle hazardous or acutely hazardous materials, substances, or waste within one-quarter mile of an existing or proposed school?

NO IMPACT. The nearest school, R. Rex Parris High School, is located approximately 0.28 mile ( 1,500 feet) northwest of the project site at 38801 Clock Tower Plaza Drive in Palmdale. Given the distance of the nearest school; there is no risk that the project will emit hazardous emissions or handle hazardous or acutely hazardous materials, substances or waste within 0.25 mile of an existing or proposed school, and no impact will result.
d. Would the project be located on a site which is included on a list of hazardous materials sites compiled pursuant to Government Code Section 65962.5 and, as a result, would it create a significant hazard to the public or the environment?

NO IMPACT. The proposed project is not located on a site that is included on a list of hazardous materials sites compiled pursuant to Government Code Section 65962.5, based on the findings of a Phase I ESA conducted for the site (LACDPW, 2011). Therefore, the proposed project will not result in an impact associated with being located on a site included on a list of hazardous materials site.
e. For a project located within an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, would the project result in a safety hazard for people residing or working in the project area?

NO IMPACT. The project site is not located within an airport land use plan or in the vicinity of a public airport or public use airport. The nearest airport is the Palmdale Regional Airport, located approximately two miles northeast of the project site. The proposed project will not result in any airport-related safety hazard for people working in the project area. Therefore, no impact will result.
f. For a project within the vicinity of a private airstrip, would the project result in a safety hazard for people residing or working in the project area?

NO IMPACT. There are no private airstrips located within the project vicinity. A helipad is located to the north at the Los Angeles County Sheriff's Department Palmdale Station. The helipad is located within a secure area for Los Angeles County Sheriff use. It will not result in an aviation safety hazard for people working in the project area. Therefore, no impact will result.
g. Would the project impair implementation of or physically interfere with an adopted emergency response plan or emergency evacuation plan?

LESS THAN SIGNIFICANT IMPACT. The proposed project will not impair implementation of or physically interfere with an adopted emergency response plan or emergency evacuation plan. Construction activities, including staging, will occur on-site and no road closures are anticipated. The project site shares an entrance with the WorkSource Center. Ingress and egress to the site will be maintained at all times. Impacts are anticipated to be less than significant no mitigation is required.
h. Would the project expose people or structures to a significant risk of loss, injury, or death involving wildland fires, including where wildlands are adjacent to urbanized areas or where residences are intermixed with wildlands?

NO IMPACT. The project site is in an urban area surrounded by developed lands. It is not within a high fire severity zone. Therefore, no impact will result.

### 3.9 Hydrology and Water Quality

Hydrology and Water Quality Checklist

| Would the project: | Potentially Significant Impact | Less Than <br> Significant with <br> Mitigation Incorporation | Less Than Significant Impact | No <br> Impact |
| :---: | :---: | :---: | :---: | :---: |
| a. Violate any water quality standards or waste discharge requirements (WDR)? |  | $\square$ | $\triangle$ |  |
| b. Substantially deplete groundwater supplies or interfere substantially with groundwater recharge such that there would be a net deficit in aquifer volume or a lowering of the local groundwater table level (e.g., the production rate of pre-existing nearby wells would drop to a level which would not support existing land uses or planned uses for which permits have been granted)? |  |  | $\triangle$ |  |
| c. Substantially alter the existing drainage pattern of the site or area, including through the alteration of the course of a stream or river, in a manner which would result in substantial erosion or siltation on-site or offsite? |  |  | $\triangle$ |  |
| d. Substantially alter the existing drainage pattern of the site or area, including through the alteration of the course of a stream or river, or substantially increase the rate or amount of surface runoff in a manner which would result in flooding on-site or off-site? |  |  | $\triangle$ |  |
| e. Create or contribute runoff water, which would exceed the capacity of existing or planned storm water drainage systems, or provide substantial additional sources of polluted runoff? |  | \| | $\triangle$ |  |
| f. Otherwise substantially degrade water quality? |  |  | $\triangle$ |  |
| g. Place housing within a 100-year flood hazard area as mapped on a federal Flood Hazard Boundary or Flood Insurance Rate Map or other flood hazard delineation map? |  |  |  | $\sum$ |
| h. Place within a 100-year flood hazard area structures, which would impede or redirect flood flows? |  |  |  | $\square$ |
| i. Expose people or structures to a significant risk of loss, injury, or death involving flooding, including flooding as a result of the failure of a levee or dam? |  |  |  | $\square$ |
| j. Inundation by seiche, tsunami, or mudflow? |  |  |  | $\square$ |

### 3.9.1 Setting

The project site is located in a high desert climate, characterized by hot dry summers and cool wet winters. Average annual precipitation in the project region is 7.9 inches which occur mostly during winter from December to March (Palmdale Water District, 2010). There is little precipitation during the summer from June to September.

The project area includes the Antelope Valley Groundwater Basin, which is comprised of an unconfined principal aquifer and a confined deep aquifer. They are important sources of local groundwater that meet 40 percent of the water demands in the region (Palmdale Water District, 2010). Natural ground water recharge in the area occurs from percolation of precipitation from the San Gabriel Mountains to the south. Human activities are responsible for other sources of recharge such as irrigation of agriculture and landscapes and wastewater effluent management practices.

The nearest well with recent groundwater data is Well No. 9974, located approximately 4.75 miles northeast of the project site. Depth to groundwater was reported to be 229 feet bgs. In addition, groundwater was not encountered in any of the drillings or borings completed to depths up to 50.5 feet bgs during soil vapor or geotechnical investigations. Based upon regional groundwater data included in the Seismic Hazard Evaluation Report for the Palmdale 7.5-minute Quadrangle (2003), historic high groundwater levels for the project site are reportedly greater than 40 feet bgs. The direction of regional groundwater is inferred to follow surface topography to the southwest.

No permanent surface water is present on or adjacent to the project site, a portion of which is vacant and paved. The historical drainage pattern at the site is generally south easterly to a discharge point via a wall opening to the adjacent cul-de-sac at Avenue Q-4 and Friendly Avenue (at the adjacent residential neighborhood), or runoff flows off-site at Sierra Highway and into the curb and gutter. There is no existing underground storm drainage infrastructure on the project site or in the surrounding streets.

## Regulatory Setting

Federal. In California, discharges of storm water are regulated by the State Water Resources Control Board (SWRCB) through each RWQCB pursuant to the federal CWA and the state Porter-Cologne Water Quality Control Act. Regulatory details are discussed below.

## State.

Construction Storm Water National Pollution Discharge Elimination System Permit. The federal CWA effectively prohibits discharges of storm water from construction sites unless the discharge is in compliance with a NPDES permit. The SWRCB is the permitting authority in California and has adopted a statewide General Permit for Storm Water Discharges Associated with Construction and Land Disturbance Activity (SWRCB Water Quality Order No. 2009-0009DWQ; SWRCB, 2009) that applies to projects resulting in one or more acres of soil disturbance (effective July 1, 2010). This permit requires development and implementation of a SWPPP.

## Local.

County of Los Angeles Condition Use Permit for Grading. Grading projects, off-site transport, require a grading permit as provided in Title 26 Building Code. Compliance shall be made
with all applicable requirements of other county departments and other governmental agencies. All hauling shall be restricted to a route approved by the road commissioner.

Municipal Storm Water Permitting Program. The Municipal Storm Water Permitting Program regulates storm water discharges from municipal separate storm sewer systems (MS4s). To implement the requirements of the NPDES permit, the Los Angeles County co-permittees have created development planning guidance and control measures that control and mitigate storm water quality and quantity impacts to receiving waters as a result of new development activity. The Los Angeles County co-permittees are also required to implement other municipal source detection and elimination programs and maintenance measures.

Low Impact Development (LID). Low Impact Development, or LID, is a design strategy using naturalistic, on-site BMPs to lessen the impacts of development on stormwater quality and quantity. As of January 1, 2009, the County of Los Angeles instituted LID requirements for development occurring within unincorporated portions of the County. The recently adopted MS4 Permit for Los Angeles County includes similar LID requirements for new development and significant redevelopment. LID BMPs control stormwater at or close to the source to reduce off-site runoff using facilities that infiltrate, evapotranspirate, or biotreat runoff. Other low impact development benefits include water conservation, groundwater recharge and greening communities. Specific requirements for the proposed project include the use of BMPs for a LID design water quality volume, which is equal to the runoff that would result from an 85th percentile storm ( $\sim 0.5$ inches) for the post development site condition. The selection of BMPs must be prioritized in the following order of preference:

- BMPs that promote infiltration.
- BMPs that store and beneficially use stormwater runoff.
- BMPs that utilize the runoff for other water conservation uses including, but not limited to, BMPs that incorporate vegetation to promote pollutant removal and runoff volume reduction and integrate multiple uses, and BMPs that percolate runoff through engineered soil and allow it to discharge downstream slowly.

To move from one BMP category to the next in the hierarchy, technical infeasibility must be demonstrated as specified in the LID Guidance Manual.

Standard Urban Stormwater Mitigation Plan (SUSMP). The SUSMP was approved by the Los Angeles RWQCB as part of the MS4 program to address storm water pollution from new construction throughout Los Angeles County. The SUSMP contains a list of minimum BMPs that must be employed to infiltrate or treat storm water runoff, control peak flow discharge, and reduce the post-development discharge of pollutants from storm water conveyance systems. The SUSMP defines, based upon land use type, the types of BMPs that must be included and issues appropriate to the development type and size that must be addressed. Compliance with SUSMP requirements is used as one method to evaluate the significance of project development impacts on surface water runoff.

City of Palmdale Excavation and Grading Regulations. Excavation, grading, and earthwork construction regulations are outlined in Section 8.04.265 Chapter 70 of the City of Palmdale Municipal Code. This chapter sets forth regulations for the control of excavation, grading, and earthwork construction, including fills or embankments, and for the control of grading site runoff, including erosion, sediments and construction related pollutants. These regulations establish minimum standards and are not intended to prevent the use of alternate materials, methods, or means of conforming to such standards, provided such alternate has been approved. Exceptions for a grading permit are listed in the code. The City of Palmdale regulations will apply to grading or excavation activities that occur, if any, within the City of Palmdale's jurisdiction.

Although the project site is within the boundary of the City of Palmdale, as part of the project the site will become County property; therefore, the project is governed by the County's regulations. However, the project is also consistent with the City of Palmdale's regulations.

### 3.9.2 Impact Analysis

## a. Would the project violate any water quality standards or Waste Discharge Requirements (WDR)?

LESS THAN SIGNIFICANT IMPACT. The project site is vacant and has relatively flat topography. The existing asphalt will be removed in order to construct the main building, outdoor spaces, and impervious surfaces such as walkways and parking lots. Soil exposure will occur during excavation and construction allowing for possible erosion and runoff into storm drains. During construction, the proposed project will be required to obtain coverage under the State's NPDES General Permit for Construction Activities and General Permit for Discharges of Stormwater Runoff Associated with Construction Activity.

The project site is currently undeveloped with the historical drainage pattern at the site generally flowing south easterly to a discharge point via a wall opening at the eastern boundary of the project site to the adjacent cul-de-sac at Avenue Q-4 and Friendly Avenue (at the adjacent residential neighborhood), or runoff flows off-site at Sierra Highway and into the curb and gutter. The proposed project will maintain the existing general drainage pattern currently at the site. In addition, the project includes two detention areas to capture a portion of the runoff. The open area to the north of the proposed facility (future expansion area) will remain undeveloped and may be used for stormwater retention. A detention basin (to be used as a SUSMP BMP) is proposed on the eastern area of the development, in the buffer zone between the facility and residential neighborhood, to capture by way of overland flow and underground storm drain piping a portion of runoff for on-site detention and treatment. Excess runoff will be conveyed to Friendly Street via the existing wall opening.

Further, project construction and operation will be required to comply with all County of Los Angeles (and City of Palmdale as applicable) ordinances and standard practices which assure proper grading and proper storm water drainage. The project will also comply with all local, state, and federal regulations, including requirements to prepare and implement a SWPPP to meet the requirements of the General Permit. The SWPPP
will include identification and implementation of BMPs to control erosion from disturbed areas and reduce runoff.

Based on the above, construction and operation will result in a less than significant impact on water quality standards or WDR. Therefore, impacts will be less than significant and no mitigation is required.
b. Would the project substantially deplete groundwater supplies or interfere substantially with groundwater recharge such that there would be a net deficit in aquifer volume or a lowering of the local groundwater table level (e.g., the production rate of pre-existing nearby wells would drop to a level which would not support existing land uses or planned uses for which permits have been granted?

LESS THAN SIGNIFICANT IMPACT. The proposed project will result in the demolition of the existing asphalt and result in an increase in pervious surfaces (i.e., exercise yard, acquaint yard/courtyard, landscaping/trees, etc.) on the site. An increase in pervious surfaces will allow more water to percolate into the soil; however, this will not affect potable groundwater supplies. In addition, the project area is not used for groundwater pumping. The proposed project will not result in substantial depletion of ground water supplies from the basin or interference with groundwater recharge because the proposed project does not include new wells or other means of extracting groundwater supplies. Therefore, impacts to groundwater supplies will be considered less than significant.
c. Would the project substantially alter the existing drainage pattern of the site or area, including through the alteration of the course of a stream or river, in a manner which would result in substantial erosion or siltation on-site or off-site?

LESS THAN SIGNIFICANT IMPACT. The project site is relatively flat and primarily paved. Construction activities include the replacement of impervious surfaces with a pervious landscaping and new parking lots at the project site that will have a positive effect on directing runoff from the existing vacant site. The proposed project will be designed to include on-site drainage and storm water flow systems (such as on-site detention and treatment) to accommodate the new facility and its parking lots. Under the proposed project, the amount of impervious surface area will decrease, given that areas currently paved will be replaced with turf and landscaping (i.e., exercise yard, courtyard/ acquaint yard, and landscaped setbacks). Additionally, the area designated for possible future expansion will be replaced with hard packed bare dirt with turf, which will increase the perviousness of the soil. Therefore, the amount of previous surfaces will be greater, which could reduce the amount of runoff that occurs from the site. Therefore, it is anticipated that the existing storm drain system will have sufficient capacity to accommodate the flows from the project site and no substantial increase in erosion or siltation will occur. No streams or rivers will be affected or altered as part of the project. The applicant will comply with all applicable requirements and conditions as for construction activities, including measures addressing drainage. Therefore, the proposed project will result in a less than significant impact relative to the existing drainage pattern of the site and no mitigation is required.
d. Would the project substantially alter the existing drainage pattern of the site or area, including through the alteration of the course of a stream or river, or substantially increase the rate or amount of surface runoff in a manner which would result in flooding on-site or off-site?

LESS THAN SIGNIGICANT IMPACT. As discussed for item c. above, the existing site is relatively flat and vacant. The new on-site drainage system of the proposed project will not substantially alter the existing drainage pattern of the site or area and the rate of runoff is expected to be less than existing conditions because of the increases in pervious landscaping (i.e., exercise yard, courtyard/acquaint yard, landscaped setbacks and turf on the possible future expansion area) in the area currently paved. The existing storm drain system has the capacity to accommodate the flows from the proposed project and will not result in flooding conditions on- or off-site. As such, impacts are considered to be less than significant and no mitigation is required.
e. Would the project create or contribute runoff water which would exceed the capacity of existing or planned storm water drainage systems or provide substantial additional sources of polluted runoff?

LESS THAN SIGNIFICANT IMPACT. The portion of the project site to be developed is currently paved, and thereby impervious. The proposed project will maintain impervious areas (i.e., main building, walkways, and parking lots) and add pervious surfaces (i.e., exercise yard, acquaint yard, and landscaping) to an area currently paved. The change in impervious surfaces and increase in pervious surfaces will not increase the volume of runoff to a level that will exceed the capacity of the storm drain system serving a project site. The existing storm drain system has sufficient capacity to accommodate the flows from the site.

Construction activities typically involve machines that have the potential to leak hazardous materials that may include oil and gasoline. It is expected that the construction contractor will use standard containment and handling protocols to ensure that these vehicles do not leak any material that may add sources of polluted runoff to the storm drain system.

Operation of the proposed project will not be a substantial source of polluted runoff. Animal wastes and medical wastes associated with the proposed project will be disposed of properly (i.e., animal wastes will be disposed of in the sanitary sewer or offsite and medical wastes will be removed by a licensed disposal services) and will not be allowed to enter the stormwater system.

In addition, as shown in Figure 3, within the project site, in the area between the main building and the existing block wall, a SUSMP BMP is proposed to infiltrate a LID design water quality volume of approximately 4,000 cubic feet (estimated using the Los Angeles County LID Volume Calculator - included as Appendix C). Additionally, the northern portion of the project site that will remain vacant for possible future expansion and unpaved may also function as a BMP for infiltration of surface water.

Therefore, the proposed project will not contribute runoff water which will exceed the capacity of existing or planned storm water drainage systems or provide a substantial
additional source of polluted runoff, and impacts will be less than significant and no mitigation is required.
f. Would the project otherwise substantially degrade water quality?

LESS THAN SIGNIFICANT IMPACT. As described under item e. above, the proposed project will not result in any other effects that could substantially degrade water quality or substantially change the amount of polluted runoff from the project site. Further, as described under item a., the proposed project will not violate any water quality standards. The proposed project will comply with NPDES General Permit for Construction Activities and General Permit for Discharges of Stormwater Runoff Associated with Construction Activity and will be designed and constructed using BMPs to avoid impacts to water quality. Operation of the proposed project will not generate a substantial new source polluted runoff. Therefore, the proposed project will not result in a significant impact on water quality and no mitigation is required.
g. Would the project place housing within a 100 -year flood hazard area as mapped on a federal Flood Hazard Boundary or Flood Insurance Rate Map or other flood hazard delineation map?

NO IMPACT. The project site is located within an area that is determined to be outside the 100- and 500-year floodplains as mapped on the federal Flood Insurance Rate Map \# 06037C0700F (2008). In addition, no housing will be constructed as a part of the project. Therefore, proposed project will not result in flood hazard impacts to housing.
h. Would the project place within a 100-year flood hazard area structures which would impede or redirect flood flows?

NO IMPACT. As noted in item g. above, the project site is located outside of the 100and 500-year floodplain hazard areas. With incorporation of drainage features that increase infiltration and provide adequate site drainage, flood flows in the project area will not be impeded or redirected. As such, no impacts will occur.
i. Would the project expose people or structures to a significant risk of loss, injury, or death involving flooding, including flooding as a result of the failure of a levee or dam?

NO IMPACT. As indicated above, the project area is lies outside the 100- and 500-year flood plains. The project site is located approximately two miles and nine miles north of Lake Palmdale and Littlerock Reservoir/Dam, respectively. The proposed project will not result in the construction or operation of new structures that will be vulnerable to flooding or inundation as a result of dam failure. In addition, the project site is not located within an inundation area of a dam or levee as identified on the proposed Dam and Reservoir Inundation Routes Policy Map (Figure 9.4) of the Safety Element of the Draft Los Angeles County General Plan. Therefore, there will be no impact related to the exposure of people or structures to a significant risk of loss, injury or death involving flooding, including flooding as a result of the failure of a levee or dam.
j. Would the project result in inundation by seiche, tsunami, or mudflow?

NO IMPACT. The project site is located in the Antelope Valley of northern Los Angeles County, over 45 miles from the coast. The proposed project is not located in an influence area that is at risk for seiche, tsunami, or mud flow as identified on the Draft Los Angeles County General Plan proposed Plate 6 of the Safety Element, Flood and Inundation Hazards, and proposed Figure 9.3, Los Angeles County Tsunami Hazard Area. Therefore, people or structures will not be exposed to hazards associated with seiches, tsunamis, or mudflows and no impact will occur.

### 3.10 Land Use and Planning <br> Land Use and Planning Checklist

| Would the project: | Potentially Significant Impact | Less Than <br> Significant with <br> Mitigation Incorporation | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
| a. Physically divide an established community? | $\square$ |  | $\square$ | $\searrow$ |
| b. Conflict with any applicable land use plan, policy, or regulation of an agency with jurisdiction over the project (including, but not limited to the general plan, specific plan, local coastal program, or zoning ordinance) adopted for the purpose of avoiding or mitigating an environmental effect? |  |  | $\searrow$ |  |
| c. Conflict with any applicable habitat conservation plan or natural community conservation plan? |  |  | $\square$ | $\searrow$ |

### 3.10.1 Setting

The City of Palmdale manages land use through the Land Use Element of the City of Palmdale General Plan and the Palmdale Zoning Ordinance (Ordinance U-1060, dated December 14. 1994, and as amended). The general plan sets forth high-level goals, objectives, and policies and is used as a blueprint for future growth in the city. The zoning code regulates the location, height, bulk, and number of stories and size of buildings, structures; regulates land uses; establishes requirements for off-street parking and loading; established building setback lines; and other matters. The City of Palmdale General Plan designates the project site as PF. The northern portion of the project site is bare soil, while the remainder of the project site is paved land. Although the project site is vacant, the PF designation supports and allows for development.

The project site is in a general area of mixed uses including light industrial, commercial, recreational, and residential properties. Surrounding uses include the Dr. Robert C Saint Clair Parkway on the west side of Sierra Highway, the Hammack Activity Center immediately to the southeast, the WorkSource Center to the south, residences to the east, and the Los Angeles County Sheriff's Department Palmdale Station to the north.

## Regulatory Setting

Federal. None.
State. None.
Local. The project site is designated under the Public Facilities (PF) land use in the City of Palmdale General Plan. Applicable zoning regulations for the City of Palmdale are within the Palmdale Municipal Code (Chapter 17 - Zoning) and the Palmdale Zoning Ordinance. Applicable zoning regulations for the County are within Title 22 (Planning and Zoning) of the Los Angeles County Code. The PF zone is intended to provide for public and quasipublic uses, such as schools, government facilities, community facilities, libraries, police and fire stations, etc.

Although the project site is within the boundary of the City of Palmdale, as part of the project the site will become County property; therefore, the project is governed by the County's regulations. However, the project is also consistent with the City of Palmdale's regulations.

### 3.10.2 Impact Analysis

a. Would the project physically divide an established community?

NO IMPACT. The proposed project will consist of construction of a new animal care facility on vacant parcel. The proposed project will occur within the project site boundaries and neither construction nor operation will include features such as a highway, above-ground infrastructure, or an easement that will cause a permanent disruption to an established community or will otherwise create a physical barrier within an established community. Therefore, no impact will occur.
b. Would the project conflict with any applicable land use plan, policy, or regulation of an agency with jurisdiction over the project (including, but not limited to, the general plan, specific plan, local coastal program, or zoning ordinance) adopted for the purpose of avoiding or mitigating an environmental effect?

LESS THAN SIGNIFICANT IMPACT. The existing land use of the project site is PF. The City of Palmdale General Plan allows development on existing vacant land under PF land uses and the proposed use will be consistent with land uses allowed under the PF zoning. The proposed new animal care facility will not be incompatible with the existing light industrial, commercial, recreational, and residential land uses surrounding the site. Nor will it conflict with the goals, policies, and vision of the City of Palmdale General Plan. Therefore, the impact is considered less than significant and no mitigation is required.
c. Would the project conflict with any applicable habitat conservation plan or natural community conservation plan?

NO IMPACT. The project site is not located within or a near a habitat conservation plan or natural community conservation plan. The project site is also not located within any Los Angeles County Significant Ecological Area (SEA). The Antelope Valley SEA is located approximately eight miles east of the project site. Therefore, the proposed project will not conflict with such plans and no impact will occur.

### 3.11 Mineral Resources

Mineral Resources Checklist

| Would the project: | Potentially <br> Significant <br> Impact | Less Than <br> Significant <br> with <br> Mitigation <br> Incorporation | Less Than <br> Significant <br> Impact |
| :--- | :--- | :--- | :--- |
| a.Result in the loss of availability of a known mineral <br> resource that would be of value to the region and <br> the residents of the state? | $\square$ |  |  |
| b.Result in the loss of availability of a locally-important <br> mineral resource recovery site delineated on a local <br> general plan, specific plan or other land use plan? | $\square$ |  |  |

### 3.11.1 Setting

The project site is not located in an area of known mineral resources. As shown in the Draft Los Angeles County's General Plan, the project site is approximately 11 miles east to Little Rock Creek Fan, a designated Mineral Resource Zone (MRZ-2). Little Rock Creek MRZ-2 extends over 37 square miles and contains significant deposits (i.e., sand and gravel) that can provide for future needs through the year 2046.

### 3.11.2 Impact Analysis

a. Would the project result in the loss of availability of a known mineral resource that would be of value to the region and the residents of the state?

NO IMPACT. The project will not result in the loss of availability of a known mineral because there are no existing or proposed mineral resource recovery activities in or around the project site. The project will not impact or result in the loss of availability of any known mineral or other available resource; therefore, no impact will result from construction or operation of the project.
b. Would the project result in the loss of availability of a locally-important mineral resource recovery site delineated on a local general plan, specific plan, or other land use plan?

NO IMPACT. The project will not result in the loss of availability of a mineral resource recovery site as described under item a. above. The project site is not located within an established MRZ, the closest mineral zone is approximately 11 miles west of the project site, and no economically viable mineral deposits are known to be present. Therefore, no impact to the availability of a mineral resource will result from construction or operation of the project.

### 3.12 Noise <br> Noise Checklist

| Would the project: | Potentially Significant Impact | Less Than Significant with Mitigation Incorporation | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
| a. Exposure of persons to or generation of noise levels in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies? |  |  | $\pm$ |  |
| b. Exposure of persons to or generation of excessive groundborne vibration or groundborne noise levels? |  |  | $\searrow$ |  |
| c. A substantial permanent increase in ambient noise levels in the project vicinity above levels existing without the project? |  |  | $\measuredangle$ |  |
| d. A substantial temporary or periodic increase in ambient noise levels in the project vicinity above levels existing without the project? |  |  | $\measuredangle$ |  |
| e. For a project located within an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, would the project expose people residing or working in the project area to excessive noise levels? |  |  | $\measuredangle$ |  |
| f. For a project within the vicinity of a private airstrip, would the project expose people residing or working in the project area to excessive noise levels? | $\square$ | , | $\square$ | $\triangle$ |

### 3.12.1 Setting

## Basic Noise Concepts

Sound is mechanical energy characterized by the rate of oscillation of sound waves (frequency), the speed of propagation, and the pressure level (amplitude). The human ear experiences sound as pressure on the ear. The sound pressure level is the logarithmic ratio of that pressure to a reference pressure, and is expressed in decibels (dB). Approximately zero dB corresponds to the threshold of human hearing.

The A-scale simulates the frequency response of the human ear by giving more weight to the middle frequency sounds and less to the low and high frequency sounds. A-weighted sound levels are designated as dBA. Table 3.12-1, Typical Noise Levels, shows the range of sound levels of common indoor and outdoor activities, in dBA.

Table 3.12-1
Typical Noise Levels

| Common Outdoor Activities | Noise Level (dBA) | Common Indoor Activities |
| :---: | :---: | :---: |
|  | 110 | Rock band |
| Jet flyover at 1,000 feet |  |  |
|  | 100 |  |
| Gas lawnmower at 3 feet |  |  |
|  | 90 |  |
| Diesel truck at 50 feet at 50 mph |  | Food blender at 3 feet |
|  | 80 | Garbage disposal at 3 feet |
| Noisy urban area, daytime |  |  |
| Gas lawnmower, 100 feet | 70 | Vacuum cleaner at 10 feet |
| Commercial area |  | Normal speech at 3 feet |
| Heavy traffic at 300 feet | 60 |  |
|  |  | Large business office |
| Quiet urban daytime | 50 | Dishwater in next room |
|  |  |  |
| Quiet urban nighttime | 40 | Theater, large conference room (background) |
| Quiet suburban nighttime |  |  |
|  | 30 | Library |
| Quiet rural nighttime |  | Bedroom at night, concert hall (background) |
|  | 20 |  |
|  |  | Broadcast/recording studio |
|  | 10 |  |
|  |  |  |
|  | 0 |  |

Source: Caltrans, 2009.

Because sound levels in the environment usually vary with time, they cannot simply be described with a single number. One method used to describe variable sound is the equivalent noise level, which is derived from a large number of moment-to-moment Aweighted noise level measurements. The equivalent noise level (Leq) is the constant sound level that in a given period has the same sound energy level as the actual time-varying sound pressure level. Leq provides a methodology for combining noise from individual events and steady state sources into a measure of cumulative noise exposure.

In the State of California, the community equivalent noise level (CNEL) is widely used. The CNEL is a 24-hour cumulative noise descriptor that considers the sensitivity of humans to noise at night. The CNEL adds a 5 dBA penalty for evening hours between 7:00 p.m. and 10:00 p.m. For the nighttime hours between 10:00 p.m. and 7:00 a.m., a 10 dBA penalty is added for the CNEL.

Sound is based on a logarithmic scale; a doubling of a noise source results in an increase of 3 dB . Noise levels reduce with distance at a rate of 6 dB per doubling of distance from a point source, such as a stationary machine, and 3 to 4.5 dB per doubling of distance from a road.

A key concept in evaluating potential noise impacts is the perceived effect of incremental increases in existing noise levels. The effect of increasing noise levels is presented in Table 3.12-2. For example, the table shows that an increase of 3 dBA is barely perceptible, an increase of 5 dBA is noticeable, and that a 10 dBA increase will be perceived by someone to be a doubling of the loudness. In practice, the goal of a noise impact analysis is usually to show that the proposed project will result in no more than a 5 dBA increase in noise level (moderate impact). An increase of 5 to 10 dBA will tend to be noticeable to most but not substantial. An increase of 10 dBA or more will be perceived by most people as a substantial increase from existing noise levels.

Table 3.12-2
Decibel Changes, Loudness, and Energy Loss

| Sound Level Change (dBA) | Relative Loudness/ Impact | Acoustical Energy Gain (\%) |
| :--- | :--- | :--- |
| 0 | Reference | 0 |
| +3 | Barely Perceptible <br> Change/Slight | 50 |
| +5 | Noticeable Change/Moderate | 67 |
| +10 | Twice as Loud/Substantial | 90 |
| +20 | Four Times as Loud/Very <br> Substantial | 99 |

Source: Federal Highway Administration, 2011 (Modified).

## Existing Conditions and Sensitive Receptors

There are multiple noise sources that contribute to background noise in the project area. The project will be located approximately 2.5 miles southwest of Air Force Plant 42 and is within the low altitude overflight area as described in City of Palmdale General Plan. Directly to the west of the project site is Sierra Highway with approximately 17,000 average daily traffic (ADT) (2006 traffic count, Google Earth Pro) and the Metrolink/Union Pacific railroad.

The project is in an area of mixed uses including light industrial, commercial, recreational, and residential properties. Noise receptors include the residences located along Friendly Avenue to the east of the project site, the Hammack Activity Center southeast of the project site, and the Dr. Robert C Saint Clair Parkway between Sierra Highway and the railroad to the west of the project site. Based on the noise contours in the City of Palmdale General Plan and the types of noise sources in the project area, it was estimated that the project area has a CNEL of 60 dBA (i.e. daytime noise level is 60 dBA , evening noise level is 55 dBA , and night time noise level is 50 dBA ). The closest school, the R. Rex Parris High School, is approximately 1,500 feet to the north of the project site. There are two elementary schools and a daycare center located within 0.5 mile of the project site.

The location of the new facility is roughly in the center of the site in order to allow for the greatest distance possible between the new facility and the nearest sensitive receptors (i.e., existing residences and outdoor roller hockey rink). Although the nearest sensitive receptor to the site is the adjacent residences along the eastern boundary of the project site, the closest noise generating activity associated with the project (i.e., car wash) is approximately

90 feet from the nearest sensitive receptor (residence at 38575 Friendly Avenue), and the outdoor roller hockey rink is approximately 128 feet from the closest portion of the main building and approximately 230 feet from the emergency generator and car wash, which are the nearest noise source.

Regulatory Setting
Federal. None.
State. The California Office of Noise Control (CONC) was established under the California Noise Control Act of 1972. The CONC is a division of the California Department of Public Health Services who are responsible for developing model noise ordinances for urban, suburban, and rural environments, developing criteria, and guidelines for use in setting standards for human noise exposure and assisting local governments in developing and implementing noise abatement procedures (California Health and Safety Code Section 46002).

CONC has established guidelines for evaluating the compatibility of various land uses as a function of community noise exposure in the form of a land use/noise compatibility matrix. This matrix is presented in Table 3.12-3. Cities within the State have incorporated this compatibility matrix into their General Plan noise elements. These guidelines are meant to maintain acceptable noise levels in a community setting based on the type of land use. Noise compatibility by different types of land uses is a range from "Normally Acceptable" to "Clearly Unacceptable" levels. The guidelines are used by cities within the State to help determine the appropriate land uses that could be located within an existing or anticipated ambient noise level.

Table 3.12-3
Land Use Compatibility Community Equivalent Noise Levels in dBA)

| Land Use | Normally Acceptable | Conditionally Acceptable | Normally Unacceptable ${ }^{(c)}$ | Clearly Unacceptable |
| :---: | :---: | :---: | :---: | :---: |
| Single-family, Duplex, Mobile Homes | 50-60 | 55-70 | 70-75 | above 70 |
| Multi-Family Homes | 50-65 | 60-70 | 70-75 | above 70 |
| Schools, Libraries, Churches, Hospitals, Nursing Homes | 50-70 | 60-70 | 70-80 | above 80 |
| Transient Lodging Motels, Hotels | 50-65 | 60-70 | 70-80 | above 80 |
| Auditoriums, Concert Halls, Amphitheaters | --- | 50-70 | --- | above 65 |
| Sports Arena, Outdoor Spectator Sports | --- | 50-75 | --- | above 70 |
| Playgrounds, Neighborhood Parks | 50-70 | --- | 67-75 | above 72 |
| Golf Courses, Riding Stables, Water Recreation, Cemeteries | 50-75 | --- | 70-80 | above 80 |
| Office Buildings, Business and Professional Commercial | 50-70 | 67-77 | above 75 | --- |
| Industrial, Manufacturing, Utilities, Agriculture | 50-75 | 70-80 | above 75 | --- |

Table 3.12-3
Land Use Compatibility Community Equivalent Noise Levels in dBA)

| Land Use | Normally <br> Acceptable $^{\text {(a) }}$ | Conditionally <br> Acceptable $^{\text {(b) }}$ | Normally <br> Unacceptable | Clearly <br> Unacceptable |
| :--- | :--- | :--- | :--- | :--- |
| (a) Normally Acceptable: Specified land use is satisfactory, based upon the assumption that any buildings involved are <br> of normal conventional construction without any special noise insulation requirements. |  |  |  |  |
| (b) Conditionally Acceptable: New construction or development should be undertaken only after a detailed analysis of <br> the noise reduction requirements is made and needed noise insulation features included in the design. Conventional <br> construction, but with closed windows and fresh air supply systems or air conditioning will normally suffice. |  |  |  |  |
| (c) Normally Unacceptable: New construction or development should generally be discouraged. If new construction or <br> development does proceed, a detailed analysis of the noise reduction requirements must be made and needed noise <br> insulation features are included in project design. Conventional construction, but with closed windows and fresh air <br> supply systems or air conditioning normally will suffice. |  |  |  |  |
| (d) Insulation features included in the design. Clearly Unacceptable: New construction or development should generally <br> not be undertaken. |  |  |  |  |

Source: California Governor's Office of Planning and Research, 2003.

Local. The project has the potential to affect noise levels within the City of Palmdale. Noise within the City is regulated by noise ordinance in the City of Palmdale Municipal Code Sections 8.28 and 9.18. The noise ordinance prohibits intrusive noise and establishes hours of operation for certain activities (such as construction and trash collection). Construction activities are limited to between the hours of 6:30 a.m. and 8:00 p.m. on Mondays through Saturdays (City of Palmdale Municipal Code Section 8.28.030). Construction may not occur within 500 feet of any residence without written permission of the City Engineer (City of Palmdale Municipal Code Sections 8.28 .030 and 8.28.040). The City of Palmdale has no quantitative thresholds for construction or operational noise and vibration levels.

The City of Palmdale General Plan Noise Element provides noise management goals, objectives, policies, and programs for the City to achieve and incorporate the CONC noise compatibility matrix. This matrix is used to help the City determine the appropriate land use and mitigation measures based on the existing or anticipated ambient noise levels. The State recommended noise level guideline presented in Table 3.12-3 was adopted by the City. Per the General Plan Noise Element, the exterior noise levels are set at 65 dBA CNEL and acceptable interior noise levels are 45 dBA CNEL.

Chapter 12.08 (Noise Control) of the Los Angeles County Municipal Code establishes allowable construction noise levels. Specifically, Chapter 12.08 .440 prohibits construction between the hours of 7:00 p.m. and 7:00 a.m., and anytime on Sunday or holidays. The County also requires the use of suitable exhaust and air-intake silencers. Further, during the allowable hours, mobile equipment shall not exceed noise levels in excess of 75 dBA at single-family residential uses, 80 dBA at multi-family residential uses, and 85 dBA at commercial and semi (mixed)-residential uses.

The County prohibits generation of noise (excluding construction) exceeding 70 dBA outside at and 55 dBA inside of a residential receptor during the day for any period of time (County Code Sections 12.08 .390 and 12.08.40). Noise levels averaged of a longer period of time have lower thresholds.

Although the project site is within the boundary of the City of Palmdale, as part of the project the site will be County property; therefore, the County's noise ordinance is the governing regulation. Although the County's noise standards are the governing noise
regulations associated with the project site, the project will be consistent with the City of Palmdale's noise regulations.

### 3.12.2 Impact Analysis

a. Would the project result in exposure of persons to generation of noise levels in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies?

LESS THAN SIGNIFICANT IMPACT. A significant impact may occur if the proposed project were to expose persons to or generate noise levels in excess of standards established in the Los Angeles County Code, City of Palmdale General Plan or the City's Municipal Code. Construction of the proposed animal care facility is expected to occur between 7:00 a.m. and 5:00 p.m. on Mondays through Fridays, which will be consistent with the County and City Codes. Because there are residences adjacent to the project area, a written permission must be obtained from the City Engineer before construction.

Construction noise will be produced from mobile construction equipment (refer to Table 3.3-3 for a list of the estimated type and number of construction equipment); however, the mobile equipment thresholds established by the County is applicable to equipment operating for less than 10 days. Thresholds established for stationary equipment will be inappropriate for mobile equipment operating near single residential homes. The existing ambient noise level is approximately the same as the threshold for stationary equipment operating near single residential areas (i.e. no additional noise can be produced without violating the threshold). For the purposes of this analysis, the mobile equipment threshold for a single residential area (noise level exceeding 75 dBA ) was used to determine significance. It is estimated that the maximum hourly Leq experienced at the residences will be approximately 75 dBA , which does not exceed the County threshold. There are no quantitative construction noise limits established by the City.

Operation of the proposed animal care facility must not cause "loud, unnecessary, or unusual noise which unreasonably disturbs the peace and quiet of any neighborhood or which causes discomfort or annoyance to any reasonable person of normal sensitiveness residing in the area" (City of Palmdale Municipal Code Section 9.18.010). There are no quantitative operational noise limits established by the city. Assuming the kennel buildings have sufficient interior/exterior sound insulation and that the doors and windows will be kept closed, except as needed for entry, noise levels from inside the buildings are anticipated to be negligible at the nearest receptor. As shown in the conceptual site layout (Figure 3), the proposed facility has been planned to have minimal noise impacts on adjacent uses. The main building centered at the project site and is separated from the residences by an open area that is not expected to be used except as buffer area and a portion as a SUSMP BMP (a passive surface water infiltration area). Exercise yards, which will be used by dogs under supervision of staff during daytime hours, have been located away from the nearest residential uses, at the north and northwestern areas of the proposed building. The nearest outdoor exercise yard is located approximately 233 feet from the nearest residence to the east. The County prohibits generation of noise exceeding 70 dBA outside at and 55 dBA inside a residential receptor during the day for any period of time (County Code Sections
12.08 .390 and 12.08.40). Based on an assumption that a barking dog produces approximately 67 dBA of instantaneous noise at 55 feet (Sound Solutions, 2011), it was determined that the exterior threshold will not be violated unless more than 72 dogs barked simultaneously at approximately 233 feet from the residences. A building may provide 15-25 dBA reduction in noise levels in the interior of the residence; therefore the 55 dBA threshold will not be exceeded.

The emergency generator, which will be located approximately 100 feet from the nearest residence, will be behind an eight-foot high concrete screen wall and have sound attenuated weatherproof housing with a sound rating of 50 dBA at 50 feet. Therefore, during period testing and in the event of power outages, noise from the emergency generator is expected to be minimal. Adjacent to the emergency generator, and also behind an eight-foot high concrete screen wall, is the DACC car wash. This is an outdoor area that will be equipped with a high pressure sprayer and a central vacuum system to clean out the interiors of the vehicles. ACO's are required to wash each truck prior to leaving the site each day. As shown in Figure 3, there is parking (a carport for approximately eight trucks); therefore it is estimated that the car wash will be used six to eight time, of short duration, and during business hours. The noise from the emergency generator and use of the car wash is expected to be intermittent; therefore, noise from the emergency generator, high pressure sprayer, and central vacuum system is expected to be minimal. Therefore, operation of the proposed project will not violate the noise ordinance.

Local ordinances will not be violated by construction or operation of the project. Therefore, the project will not result in exposure of persons to generation of noise levels in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies and noise impacts will be less than significant and no mitigation is required.

## b. Would the project result in exposure of persons to or generation of excessive groundborne vibration or groundborne noise levels?

LESS THAN SIGNIFICANT IMPACT. Construction activities associated with the project could generate vibration. Construction equipment such as dozers and rollers will generate vibrations that could result in groundborne noise or vibration that may affect nearby structures or residents. Los Angeles County Code Section 12.08.560 states that the threshold of perception is a vibration level of 0.01 inch per second (in/sec). Vibration levels greater than 0.3 inches per second (in/sec) have potential to damage older residential structures and levels greater than $0.1 \mathrm{in} / \mathrm{sec}$ will be strongly perceptible and possibly annoying to a human (Caltrans, 2004). For the purpose of this analysis, vibration levels exceeding $0.1 \mathrm{in} / \mathrm{sec}$ will be considered significant. The maximum estimated vibration during construction will be $0.01 \mathrm{in} / \mathrm{sec}$ at the nearest residence, which is below the vibration that could have potential to damage older residential structures and the vibration level severely noticeable to a human (Federal Transit Administration, 2006). Excessive groundborne vibration and/or groundborne noise are not anticipated. Therefore, the proposed project will have a less than significant groundborne vibration and noise impact during project construction and no mitigation is required.

The proposed project involves operation of an animal care facility. Project operations will not involve equipment or activities that could generate vibration or groundborne noise, or otherwise expose persons to such impacts. Therefore, project operation will not result in a significant impact related to groundborne vibration or noise and no mitigation is required.
c. Would the project result in a substantial permanent increase in ambient noise levels in the project vicinity above levels existing without the project?

LESS THAN SIGNIFICANT IMPACT. Operations of the project could generate noise impacts from barking dogs. These noise impacts will be intermittent and will occur when dogs are present in the exercise yard. Dogs inside the kennel buildings and in the get-acquainted yard are not expected to produce noise levels that will impact the nearby residences given the attenuation of noise from the interior to the exterior of the kennel buildings and the distance and location of the get-acquaint yard (over 233 feet away from the residences and behind a portion of the main facility). Supervisors will be responsible for controlling barking behavior.

Because the County thresholds do not address long term, permanent increase in noise levels, a noise level increase of 10 dBA or above was considered a significant impact. A measured noise level of one barking dog at 55 feet of 60 dBA 1 -hour Leq was used to estimate potential noise levels from the exercise yard (Sound Solutions, 2011). The concrete screen wall will provide at least a 3 dBA reduction in noise. Based on noise modeling done for the proposed project, it was determined that if there were 128 dogs (peak average) barking simultaneously for seven hours a day in the nearest exercise yard will only result in a CNEL increase of 3 dBA , which would be barely perceptible, and would not cause the exterior noise levels in the adjacent residential area (to the east of the project) to exceed 65 dBA CNEL (per the City's General Plan Noise Element). It is unlikely for 128 dogs to be in the exercise yard at the same time; therefore, operation of the proposed project will not result in a 10 dBA increase in noise and the permanent increase in ambient noise levels in the project vicinity will be less than significant and no mitigation is required. As described above (under " $a$ "), the emergency generator, which will be located approximately 100 feet from the nearest residence, will have sound attenuated weatherproof housing with a sound rating of 50 dBA at 50 feet. Therefore, during period testing and in the event of power outages, noise from the emergency generator is expected to be minimal. Adjacent to the emergency generator, and also behind an eight-foot high concrete screen wall, is the DACC car wash, which will be equipped with a high pressure sprayer and a central vacuum system to clean out the interiors of the vehicles. It is estimated that the car wash will be used six to eight time, of short duration, and during business hours. The noise from the emergency generator and use of the car wash is expected to be intermittent; therefore, noise from the emergency generator, high pressure sprayer, and central vacuum system is expected to be minimal.

In addition, the increase in roadway noise on Sierra Highway due to the traffic generated by the project is anticipated to be negligible. It takes a doubling of the noise source, in this case traffic, to produce a 3 dB increase in noise, which is barely perceptible by the human ear. The ADT along Sierra Highway is 17,000 . Using a trip generation rate for a similar project (see Section 3.16, Transportation/Traffic), it is
estimated that the proposed project will generate approximately 240 daily trips, which will not result in a doubling of traffic along Sierra Highway. Therefore, roadway noise impacts associated with the proposed project will be less than significant and no mitigation is required.
d. Would the project result in a substantial temporary or periodic increase in ambient noise levels in the project vicinity above levels existing without the project?

LESS THAN SIGNIFICANT IMPACT. Using the Federal Highway Administration's Roadway Construction Noise Model and the equipment list identified in the air quality and GHG analyses, it was estimated that construction activities will produce an hourly Leq of 76 to 86 dBA at 50 feet depending on the construction phase (Appendix B). Construction equipment will be located at different distances from the residences located along Friendly Avenue. However on average, it is estimated that the maximum hourly Leq experienced at the residences will be approximately 75 dBA during debris removal and paving phases. As described earlier, the County's threshold for mobile construction equipment in single family residential area was used to determine significance for this analysis. The estimated maximum hourly Leq from construction will not exceed the significance threshold. It was assumed that all anticipated equipment for each construction phase will be operating at the same time. However actual levels will be lower during construction, given that not all equipment will be operating at the same time and will operate at all locations farther than the nearest property line. Therefore, construction noise levels will be less than significant and no mitigation is required.

Traffic on Sierra Highway from construction worker commute, deliveries, and hauling will not result in a doubling of traffic and traffic noise associated with construction vehicles is anticipated to be negligible and no mitigation is required.
e. For a project located within an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, would the project expose people residing or working in the project area to excessive noise levels?

LESS THAN SIGNIFICANT IMPACT. The project site is located approximately 2.5 miles southwest of Air Force Plant 42 and is beyond the 60 CNEL contour from activities at Air Force Plant 42. However, the project is within an area that is frequently overflown by aircraft at low altitudes. The General Plan Noise Element discourages high density residential, hospital, and school uses of this area. The proposed project does not propose any of these uses in the area. The project area is not considered to have excessive noise levels and is suitable for industrial, commercial, and low density residential land use. Therefore, exposure to aircraft noise will be less than significant and no mitigation is required.
f. For a project within the vicinity of a private airstrip, would the project expose people residing or working in the project area to excessive noise levels?

NO IMPACT. No private airstrips are located within the vicinity of the project area. The closest private airstrip is Bohunk's Airpark located approximately 12 miles northwest of the project site. The Los Angeles County Sherriff's Department Palmdale Station just
north of the project site has a heliport; however, the heliport is used infrequently and is not a source of consistent or excessive noise. Therefore, the project will not expose people residing or working in the project area to excessive noise levels and no impact will occur.

### 3.13 Population and Housing

## Population and Housing Checklist

| Would the project: | Potentially <br> Significant Impact | Less Than Significant with Mitigation Incorporation | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
| a. Induce substantial population growth in an area, either directly (for example, by proposing new homes and businesses) or indirectly (for example, through extension of roads or other infrastructure)? |  | $\square$ | $\square$ | $\triangle$ |
| b. Displace substantial numbers of existing housing, necessitating the construction of replacement housing elsewhere? |  |  |  | $\bigotimes$ |
| c. Displace substantial numbers of people, necessitating the construction of replacement housing elsewhere? |  |  |  | $\pm$ |

### 3.13.1 Setting

There are no housing units on the project site. The nearest residences are located immediately east of the project site. The residential lots are separated by a block walk from the existing vacant lot.

## Regulatory Setting

Federal. None.
State. California Planning and Zoning Law (Government Code Sections 65000 et seq.) requires that each city and county adopt a comprehensive, long-term plan for the physical development of the land within its planning area. The general plan must include a housing element that identifies the planning area's housing needs, the sites that can accommodate those needs, and the policies and programs to assure that the housing units can be provided. The Housing Element is required to be updated every five years.

Regional. Southern California Association of Governments' (SCAG's) Regional Housing Needs Assessment (RHNA) and Regional Comprehensive Plan (RCP) are tools for coordinating regional planning and housing development strategies in southern California.

State Housing Law mandates that local governments, through Councils of Governments, identify existing and future housing needs in a RHNA. The RHNA provides recommendations and guidelines to identify housing needs within cities for various income levels. It does not impose requirements as to housing development in cities. The RHNA Plan that covers the period from January 1, 2006 to June 30, 2014, identified the County of Los Angeles housing needs at 283,927 dwelling units.

The latest RCP, adopted in 2008, integrates the major elements of planning for the region, including: Air Quality; Economy; Energy; Finance; Land Use and Housing; Open Space and Habitat; Security and Emergency Preparedness; Solid Waste; Transportation; and Water (SCAG, 2008b). The 2008 RCP is built around the "Compass Growth Vision and 2\% Strategy" adopted by the Regional Council in April 2004, which is based on four key principles. These principles include mobility, getting where we want to go; livability, creating positive communities; prosperity, long-term health for the region; and sustainability, preserving natural surroundings. The Land Use and Housing chapter focuses on integrating land and transportation planning and achieving land use and housing sustainability.

County. Each county within California is also required to prepare and adopt a housing element. The housing element in the Los Angeles County General Plan outlines growth and development, addresses the housing needs of all income levels, and facilitates programs for a variety of housing types and affordability in the unincorporated areas of Los Angeles County. On August 5, 2008, the Los Angeles County 2008-2014 Housing Element was adopted by the Board of Supervisors and subsequently certified by the State Department of Housing and Community Development.

Local. As described under the state regulations above, each city in California is required to prepare a housing element as part of the general plan and update it every five years. The housing element in the City of Palmdale General Plan identifies the community's housing needs and provides a statement of goals, policies, quantified objectives, financial resources and scheduled programs for the preservation, improvement and development of housing.

### 3.13.2 Impact Analysis

a. Would the project induce substantial population growth in an area, either directly (for example, by proposing new homes and businesses) or indirectly (for example, through extension of roads or other infrastructure)?

NO IMPACT. The project does not propose new housing. The new animal care facility will house animals and serve an existing need and will not induce population growth in the area nor create new infrastructure that could be considered growth inducing. Therefore, no impact will occur.
b. Would the project displace substantial numbers of existing housing, necessitating the construction of replacement housing elsewhere?

NO IMPACT. The project is an animal care facility on a vacant site; therefore no displacement of existing housing will occur. Neither construction, nor operation, will result in the displacement of existing housing nor will it necessitate the construction of any replacement housing on the adjacent residential lot. Therefore, no impact will occur.
c. Would the project displace substantial numbers of people, necessitating the construction of replacement housing elsewhere?

NO IMPACT. The project site is currently vacant. Therefore, construction of the proposed project will not result in the displacement of any housing or businesses. Construction and operation of the proposed project will not result in the displacement of
people, nor will it necessitate the construction of replacement housing elsewhere. Therefore, no impact will occur.

### 3.14 Public Services

## Public Services Checklist

Would the project result in substantial adverse physical impacts associated with the provision of new or physically altered governmental facilities, need for new or physically altered governmental facilities, the construction of which could cause significant environmental impacts, in order to maintain acceptable service ratios, response times, or other performance objectives for any of the public services:

| Potentially | Less Than <br> Significant | Less Than |
| :---: | :---: | :---: |
| Significant | with Mitigation <br> Impact <br> Incorporation | Significant <br> Impact | No Impact



### 3.14.1 Setting

Public services and facilities are provided and maintained by local and county entities. The County of Los Angeles provides public services including fire and police. The City of Palmdale provides public services including public works and building and safety. There is currently no demand on these services from the existing project site because it is vacant land.

## Regulatory Setting

Federal. None.
State. The California Fire Code contains specialized regulations related to construction, maintenance, and use of buildings in relation to fire and safety. The extent of the code coverage pertains to fire department access, fire hydrants, automatic sprinkler systems, fire alarm systems, fire and explosion hazard safety, hazardous material storage and use, provisions to aid fire responders, industrial processes, and other fire-safety requirements for new and existing buildings.

California Health and Safety Code contains State fire regulations as set forth in Sections 13000 et seq. of the California Health and Safety Code, include regulations for building standards (as also set forth in the CBC), fire protection and notification systems, fire protection devices such as extinguishers and smoke alarms, high-rise building and childcare facility standards, and fire suppression training.

Local. Title 32 Los Angeles County Fire Code of the Los Angeles County Code establishes the minimum requirements consistent with nationally recognized good practices for providing a reasonable level of life safety and property protection from the hazards of fire, explosion, or dangerous conditions in new and existing building, structures, and premises, and to provide safety to fire fights and emergency responders during emergency operations. The City of Palmdale adopted the Los Angeles County Fire Code into the Palmdale Municipal Code.

### 3.14.2 Impact Analysis

Would the project result in substantial adverse physical impacts associated with the provision of new or physically altered governmental facilities, need for new or physically altered governmental facilities, the construction of which could cause significant environmental impacts, in order to maintain acceptable service ratios, response times, or other performance objectives for any of the public services:

## a. Fire protection?

LESS THAN SIGNIFICANT IMPACT. Fire protection services are provided by the Los Angeles County Fire Department. The proposed project includes a new on-site fire hydrant as required by the Fire Department. The nearest fire station to the project site and surrounding area is Fire Station 37 at $383189^{\text {th }}$ Street East, Palmdale approximately 0.3 mile southeast of the site. Construction activities and staging will occur on-site and thus no street closure or work in the public right-of-way is anticipated. Construction of the proposed project will also be temporary and not require the addition of a new fire station or the expansion, consolidation or relocation of an existing facility to maintain service. The proposed animal care facility will require fire protection services, but this will not result in a substantial increase in the demand for fire protection services or generate a need for new fire stations in the area because the site is already within an existing service area. The proposed project will comply with fire safety requirements of the CBC, and incorporate recommendations from the Los Angeles County Fire Department regarding fire safety into the project design as appropriate to minimize potential impacts. Therefore, impacts related to fire services are considered less than significant and no mitigation is required.
b. Police protection?

LESS THAN SIGNIFICANT IMPACT. Law enforcement services are provided, by contract, with the Los Angeles County Sheriff's Department. The Palmdale Sheriff Station is immediately north of the project; at 750 East Avenue Q, Palmdale. The operation of the proposed facility will require police protection services; however, the proximity of the project site to the sheriffs' station is conducive to meeting the necessary response time and will not result in a substantial increase in the demand for police protection services. Therefore, the existing police service will be adequate and impacts to police protection will be considered less than significant and no mitigation is required.

## c. Schools?

NO IMPACT. The project site is located approximately 0.28 mile from R. Rex Parris High School. The proposed project involves operation of an animal care facility, which will not generate additional population or student enrollment. Therefore, the proposed animal care facility will not utilize services of the local school district nor increase the demand for schools in the area. No impact will occur.
d. Parks?

NO IMPACT. As previously noted above, the proposed project is not growth-inducing, either directly or indirectly. Construction activities and staging will occur within the vacant land of the project site and thus no trail closures or other temporary disruption to recreation use is expected to occur. The proposed project will include exercise yards onsite for the animals and will not increase the use of the existing Dr. Robert C Saint Clair Parkway or the Hammack Activity Center. Therefore, the proposed project will not result in impacts to existing or planned parks in the region.

## e. Other public facilities?

NO IMPACT. The proposed project involves operation of an animal care facility, which will not result in an increase in population. In addition, the proposed project facilities will be operated and maintained by the County of Los Angeles. Therefore, the proposed project will not affect other government services or public facilities.

### 3.15 Recreation

## Recreation Checklist

|  | Potentially <br> Significant <br> Impact |
| :--- | :--- |
| Less Than <br> Significant <br> with <br> Mitigation <br> Incorporation | Less Than <br> Significant <br> Impact |
| Would the project increase the use of existing <br> neighborhood and regional parks or other <br> recreational facilities such that substantial physical <br> deterioration of the facility would occur or be <br> accelerated? |  |
| b.Does the project include recreational facilities or <br> require the construction or expansion of <br> recreational facilities which might have an adverse <br> physical effect on the environment? |  |

### 3.15.1 Setting

The Dr. Robert C Saint Clair Parkway, located to the west of the project site across the Sierra Highway, is less than three acres in size, and serves the residential and business areas within walking distance. Amenities for the park include passive features, such as a walking/running/ bicycle pathway. The path is approximately one mile long and 12 feet wide between Avenue Q and Avenue R.

The Hammack Activity Center is located immediately southeast of the project site. Two roller hockey rinks are located in the parking lot just west of the Center. The Boys \& Girls Club offers a variety of activities for children at the Hammack Activity Center.

## Regulatory Setting

Federal. None.
State. None.
Local. Both the County of Los Angeles and City of Palmdale have a Department of Parks and Recreation that manages the parks within their respective jurisdictional limits. Regulations related to parks are in Title 17 Parks, Beaches and Other Public Area of the Los Angeles County Code, and the Palmdale Municipal Code, Chapter 8.24 Park and Recreation Areas. Proposed related goals, objectives, and policies are set forth in the Parks and Recreation Element of the Draft Los Angeles County General Plan and the Parks, Recreation, and Trails Element of the City of Palmdale General Plan.

Although the project site is within the boundary of the City of Palmdale, as part of the project the site will become County property; therefore, the project is governed by the County's regulations. However, the project is also consistent with the City of Palmdale's goals and policies.

### 3.15.2 Impact Analysis

a. Would the project increase the use of existing neighborhood and regional parks or other recreational facilities such that substantial physical deterioration of the facility would occur or be accelerated?

NO IMPACT. The proposed project involves the construction and operation of an animal care facility and will not result in increased use of the Hammack Activity Center, Dr. Robert C Saint Clair Parkway, or other recreational facilities in the area and will not eliminate existing park space, nor result in substantial deterioration of other recreational facilities at a rate greater than normal use will cause. Therefore, no impact will occur.
b. Does the project include recreational facilities or require the construction or expansion of recreational facilities which might have an adverse physical effect on the environment?

NO IMPACT. The proposed project does not include recreational facilities. The proposed project involves the construction and operation of an animal care facility, which will not induce population growth, either directly or indirectly; therefore, the proposed project will not increase the demand for parks or other recreational facilities that might have an adverse physical effect on the environment. Therefore, no impact will occur.

### 3.16 Transportation/Traffic

## Transportation/Traffic Checklist

| Would the Project: | Potentially Significant Impact | Less Than <br> Significant with <br> Mitigation Incorporation | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
| a. Conflict with an applicable plan, ordinance or policy establishing measures of effectiveness for the performance of the circulation system, taking into account all modes of transportation including mass transit and non-motorized travel and relevant components of the circulation system, including but not limited to intersections, streets, highways and freeways, pedestrian and bicycle paths, and mass transit? |  |  | $צ$ |  |
| b. Conflict with an applicable congestion management program, including, but not limited to level of service standards and travel demand measures, or other standards established by the county congestion management agency for designated roads or highways? |  |  | $\square$ | $\square$ |
| c. Result in a change in air traffic patterns, including either an increase in traffic levels or a change in location that results in substantial safety risks? |  |  |  | $\square$ |
| d. Substantially increase hazards due to a design feature (e.g., sharp curves or dangerous intersections) or incompatible uses (e.g., farm equipment)? |  |  |  | $\square$ |
| e. Result in inadequate emergency access? |  |  | $\triangle$ |  |
| f. Conflict with adopted policies, plans, or programs regarding public transit, bicycle, or pedestrian facilities, or otherwise decrease the performance or safety of such facilities? |  | I | $\searrow$ |  |

### 3.16.1 Setting

The project site is located along northbound Sierra Highway about 350 feet north of East Avenue Q-6 in the City of Palmdale, California. It is generally bounded by residential property parcels and El Toreo Inc. offices to the east and northeast, the Hammack Activity Center to the southeast, the WorkSource Center to the south, and a County of Los Angeles Sheriff's Department Palmdale Station to the north. To the west of the project site is the east side of Sierra Highway, which will be the primarily access to the site. In the vicinity of the project site, Sierra Highway consists of five lanes, two travel lanes in each direction and a center two-way left-turn lane.

The proposed facility will be accessed from two driveways from Sierra Highway - one existing driveway currently serving the WorkSource Center and one new driveway proposed approximately 400 feet to the north of the existing driveway. At the existing
driveway, a short 150-foot deceleration turn lane from northbound Sierra Highway is currently provided. Similar deceleration lane is planned for the new driveway as well to assist northbound vehicles entering the project site.

## Regulatory Setting

Federal. None.
State. None.
Local. Los Angeles County maintains a list of principal arterials and freeways critical to the function and operation of local and regional travel throughout the county. This list is included in the 2010 Congestion Management Program (CMP) for Los Angeles County. In the vicinity of the project site, State Route 138 (SR-138) is located approximately 0.25 mile to the south of the site and runs along Palmdale Boulevard.

According to the 2010 CMP (Chapter 5), a traffic impact analysis is required if the proposed project adds 50 or more trips to any CMP arterial segment or intersection during the weekday AM or PM peak hours. Should CMP intersections and roadways be significantly affected by the proposed project as determined by the 2010 CMP guidelines, mitigation measures reducing the impact of the proposed project to a less than significant level are required. Per Appendix D of the 2010 CMP guidelines, a significant impact occurs under the following conditions:

- If the proposed project would cause a CMP facility to operate at LOS F by increasing its traffic demand by two percent of capacity, i.e., the volume-to-capacity ratio (V/C ratio) is increased at least by 0.02 ; or
- If the proposed project would increase traffic demand on a CMP facility already operating at LOS F by two percent of capacity, i.e., the V/C ratio is increased at least by 0.02 .


### 3.16.2 Impact Analysis

a. Conflict with an applicable plan, ordinance or policy establishing measures of effectiveness for the performance of the circulation system, taking into account all modes of transportation including mass transit and non-motorized travel and relevant components of the circulation system, including but not limited to intersections, streets, highways and freeways, pedestrian and bicycle paths, and mass transit?

LESS THAN SIGNIFICANT IMPACT. The proposed animal care facility project will primarily serve the eastern Antelope Valley area and provide additional space for animal control services. Operation of the animal care facility is estimated to result in a maximum of approximately 120 people on the site daily, based on Los Angeles County's DACC estimates. This is assumed to consist of a staff of 30 full-time ACOs to be at the site, 20 part-time volunteers, and up to 70 visitors a day during facility operating hours (Noon to 7:00 p.m. Monday through Thursday and 10:00 a.m. to 5:00 p.m. Friday through Sunday). The facility will house animals 24 hours a day, seven days a week, and will have limited staff always on-site; however, the majority of staff will work at the shelter during regular operating hours.

Generally, the latest version of the Institute of Transportation Engineers (ITE) Trip Generation Manual (8th Edition) is used to estimate project trip generation. However, an animal care facility land use is not available in the ITE Trip Generation Manual; the land use closest in activity to the proposed project available in the ITE Trip Generation Manual is an animal hospital. The nature of an animal care facility is different to that of an animal hospital; as such, the ITE Trip Generation Manual was not used to estimate project-related trips. Instead, a similar study conducted for a planned animal care facility in the City of Burlingame, California ([PHS/SPCA]) was used to estimate project trip generation (City of Burlingame, 2006). As part of this study, trip generation rates for an animal care facility were estimated by conducting trip generation observations at three similar facilities located in the San Francisco Bay Area. According to this report, the trip generation rate for an animal care facility was estimated to be 1.72 trips per 1,000 square feet during the PM peak hour ( 37 percent inbound and 63 percent outbound trips). Applying this trip generation rate, the proposed project is estimated to generate about 44 trips ( 16 inbound and 28 outbound) during the PM peak hour. During the AM peak hour no visitor activity is expected at the proposed animal care facility (since the facility will only typically be open to public from Noon to 7:00 p.m.); as such, it is expected that the number of AM peak hour trips will be less than those in the PM peak hour. Using the trip generation rate for the similar project, the proposed project is estimated to generate a maximum of 240 daily trips and 44 weekday AM/PM peak hour trips.

Since the proposed project is expected to generate only 44 trips during the weekday AM or PM peak hours (less than the 2010 CMP's 50 peak hour trip threshold), a less than significant impact on nearby transportation facilities is anticipated. Hence, per 2010 CMP guidelines, the proposed project will result in less than significant impact to traffic operations and no mitigation is required.

Parking Operations - The proposed staff parking area will consist of approximately 32 spaces. The proposed public parking area will consist of the development of 71 parking spaces. Of the 71 public parking spaces being developed as part of the proposed project, approximately six are handicap spaces adjacent to the roller hockey rink associated with the Hammack Activity Center (east/southeast of the project site). There will be 65 spaces for use by the proposed facility. A schematic site plan showing the proposed parking is shown on Figure 3.

The latest version of ITE Parking Generation Manual (4th Edition) is typically used to estimate project-related parking demand. However, similar to the ITE Trip Generation Manual, the ITE Parking Generation Manual does not include an animal care facility land use; therefore, the parking rates observed and estimated for an animal care facility in the Burlingame PHS/SPCA Transportation Impact Analysis Report, June 2006 were used to estimate the proposed project's parking demand. According to this report, the parking generation rate for an animal care facility was estimated to be 1.56 spaces per 1000 square feet during a weekday. Using this parking rate, the proposed project is estimated to generate a maximum parking demand of about 40 spaces during a typical weekday. Since the parking demand of 40 spaces will be lower than the parking supply of 65 spaces, the proposed project will result in less than significant impact to neighboring parking operations and no mitigation is required.

Transit Operations - At the project site, the following transit services are currently available:

- Local fixed-route service (within one-fourth-mile radius): Antelope Valley Transit Authority (AVTA) Route 1 (Lancaster/Palmdale), Route 2 (Palmdale Boulevard), Route 3 (Avenue R), and Route 10 (Palmdale/Lancaster);
- Express bus service (within two-mile radius): AVTA Route "Lake LA Express" and Santa Clarita Transit Route 795 (Palmdale/Lancaster); and
- Rail service (within two-mile radius): Metrolink Antelope Valley Line Palmdale Station

According to Appendix D of the 2010 CMP, project-related transit trips can be estimated based on project-related vehicle trips, primary nature of project (residential vs. commercial), type of transit service available in the vicinity of the project site (transit center vs. transit corridor), and the distance between the project site and neighboring transit service. Project-related transit trips estimated using the 2010 CMP methodology are shown in Table 3.16-1.

| Table 3.16-1 <br> Project-Related Transit Trips per 2010 CMP Methodology |  |
| :---: | :---: | :---: | :---: |
| Parameter | Conversion Factor |

Notes:
${ }^{1}$ Conversion factors were obtained from the 2010 CMP.
${ }^{2}$ A conservative 7 percent value was used to account for transit service operating along CMP roadways.

The nearest transit corridor, SR-138 is located less than 0.25 mile away from the project site. Therefore, a more conservative person trip-to-transit trip conversion factor of 7 percent, instead of the default 3.5 percent, was used to estimate transit trips. As shown in Table 3.16-1, the proposed project will generate a maximum of 23 daily and 4 peak hour transit trips. Given the amount of available transit services near the project site and the low anticipated project-related transit demand, the proposed project is expected to result in a less than significant impact to neighboring transit operations and no mitigation is required.

Bicycle Operations - In the vicinity of the project site, the Sierra Highway Bicycle Trail provides a bicycle path for recreational and commute travel between Palmdale and the City of Lancaster. A bicycle lane is also provided along Palmdale Boulevard. Bicycle activity along neighboring roadways, including Sierra Highway is low under existing conditions.

The majority of project-related trips are expected to be auto based, with only a few bicycle trips. Given the low bicycle demand in the neighborhood under existing conditions, the few bicycle trips anticipated to be generated by the proposed project will cause a less than significant impact to bicycle operations and no mitigation is required.

Pedestrian Operations - In the vicinity of the project site, sidewalks are provided along both sides of Sierra Highway. However, pedestrian activity is low in the neighborhood under existing conditions.

Similar to bicycle demand, pedestrian demand related to the proposed project is expected to be low, since the majority of project-related trips are expected to auto based. Given the low pedestrian demand in the neighborhood under existing conditions, the few pedestrian trips anticipated to be generated by the proposed project will cause a less than significant impact to pedestrian operations and no mitigation is required.

Construction Operations - Construction is anticipated to begin in the summer of 2014 and last around 16-18 months. Construction will be scheduled for eight hours a day between 7:00 a.m. and 5:00 p.m., Monday through Friday. During construction, it is estimated that a maximum of 33 workers and 14 trucks will access the project site daily. Assuming truck trips are equally distributed throughout the day, the construction of the proposed project will generate a maximum of 94 daily trips ( 66 construction worker trips and 28 truck trips) and 37 AM/PM peak hour trips ( 33 construction worker trips and 4 truck trips) during the AM and PM peak hours. Therefore, the maximum number of construction trips anticipated during the AM and PM peak hours is lower than the 2010 CMP's 50 peak hour trip threshold for conducting a traffic impact analysis. Also, construction staging will be located on the project site and are not anticipated to disrupt roadway operations or restrict pedestrian facilities. In addition, construction traffic is temporary in nature. Therefore, the construction of this project is expected to result in a less than significant impact to neighboring circulation network and no mitigation is required.
b. Conflict with an applicable congestion management program, including, but not limited to level of service standards and travel demand measures, or other standards established by the county congestion management agency for designated roads or highways?

LESS THAN SIGNIFICANT IMPACT. The 2010 CMP designates only Palmdale Boulevard (SR-138) as a CMP roadway in the proposed project's vicinity. The proposed project will entail a maximum of 37 construction-related and 44 operation-related trips during the weekday AM and PM peak hours, which are lower than the 2010 CMP's 50 peak hour trip threshold for conducting a traffic impact analysis. As such, the additional trips generated by the project could be accommodated by the neighboring CMP roadway without causing any significant impacts to its operations. Therefore, the proposed project will not conflict with the standards established by the Los Angeles CMP and the impact will be less than significant and no mitigation is required.
c. Result in a change in air traffic patterns, including either an increase in traffic levels or a change in location that results in substantial safety risks?

NO IMPACT. The proposed project involves operation of an animal care facility and will have no impact on air traffic patterns.
d. Substantially increase hazards due to a design feature (e.g., sharp curves or dangerous intersections) or incompatible uses (e.g., farm equipment)?

NO IMPACT. The proposed project will not substantially alter any nearby roadways and will not include dangerous design features or incompatible uses. The proposed project will include a deceleration lane for the new driveway to assist northbound vehicles entering the project site, which will increase the safety of drivers slowing to enter the site. As such, no impact will occur.

## e. Result in inadequate emergency access?

LESS THAN SIGNIFICANT IMPACT. Access to the project site during construction and operation will be directly to and from an existing driveway off of Sierra Highway. All construction and construction staging will take place within the project site. No temporary road closures are anticipated and access to and from the site, including for emergency vehicles, will be maintained at all times. All travel lanes along Sierra Highway will be maintained during the construction phase. Therefore, impacts related to emergency access are expected to be less than significant and no mitigation is required.
f. Conflict with adopted policies, plans, or programs regarding public transit, bicycle, or pedestrian facilities, or otherwise decrease the performance or safety of such facilities?

LESS THAN SIGNIFICANT IMPACT. The proposed project entails construction and operation of an animal care facility and will not affect use of an alternative transportation mode during its construction or operation. Therefore, the proposed project will not conflict with any adopted policies, plans, or programs regarding public transit, bicycle, or pedestrian facilities. All construction activities and staging will occur on-site and no temporary blockages or closures of adjacent circulation facilities are anticipated; therefore, the project will not have a significant impact on the performance or safety of such facilities. Therefore, impacts are expected to be less than significant and no mitigation is required.

As part of the proposed project, a new driveway will be provided along northbound Sierra Highway to provide additional access to the project site. This driveway could impact pedestrian safety by increasing the potential for vehicle-pedestrian conflicts between vehicles accessing the project site and pedestrians traveling along northbound Sierra Highway. However, since pedestrian activity is minimal near the project site and a maximum of 44 vehicle trips will access the project site per hour, the increase in vehicle-pedestrian conflicts is anticipated to be minimal. Therefore, the proposed project will cause less than significant impact to safety of neighboring circulation facilities and no mitigation is required.

### 3.17 Utilities and Service Systems

Utilities and Service Systems Checklist

| Would the Project: | Potentially Significant Impact | Less Than Significant with Mitigation Incorporation | Less Than Significant Impact | No Impact |
| :---: | :---: | :---: | :---: | :---: |
| a. Exceed wastewater treatment requirements of the applicable RWQCB? |  | $\square$ | $\triangle$ |  |
| b. Require or result in the construction of new water or wastewater treatment facilities or expansion of existing facilities, the construction of which could cause significant environmental effects? |  | $\square$ |  |  |
| c. Require or result in the construction of new storm water drainage facilities or expansion of existing facilities, the construction of which could cause significant environmental effects? |  |  | $\searrow$ |  |
| d. Have sufficient water supplies available to serve the project from existing entitlements and resources, or are new or expanded entitlements needed? |  |  | $\searrow$ |  |
| e. Result in a determination by the wastewater treatment provider which serves or may serve the project that it has adequate capacity to serve the project's projected demand in addition to the provider's existing commitments? |  |  | $\triangle$ |  |
| f. Be served by a landfill with sufficient permitted capacity to accommodate the project's solid waste disposal needs? |  |  | $\triangle$ |  |
| g. Comply with federal, state, and local statutes and regulations related to solid waste? | $\square$ |  | $\searrow$ |  |

### 3.17.1 Setting

Southern California Edison and Southern California Gas Company provide electricity and natural gas services, respectively, to the City of Palmdale. The Palmdale Water District provides potable water services. The water supply sources include groundwater drawn from the Antelope Valley Groundwater Basin and surface water from the California Aqueduct (imported) and Littlerock Dam (local). Approximately 40 to 50 percent of potable water supplies consist of groundwater and the balance is supplied from surface water.

In 2010, the District's water demand was 19,800 acre-feet (AF). Based on population growth projections, the Palmdale Urban Water Management Plan (UWMP) projects water demand to increase to $35,000 \mathrm{AF}$ in 2015 and 60,000 AF in 2035. However, due to the recent economic downturn, there has been lower-than-expected population growth in the district between 2009 and 2010. This will likely result in a decrease of water demand by
approximately $5,000 \mathrm{AF}$ (i.e., actual demand for 2015 will be closer to $30,000 \mathrm{AF}$ and actual demand for 2035 will be closer to 55,000 AF) (Palmdale Water District, 2011). The District is projected to meet its future water demand through 2035 by current water supplies (groundwater and surface water) and future water supplies (i.e., recycled water, groundwater banking and anticipated new supplies from transfers and exchanges [i.e., banking of imported water]) (Palmdale Water District, 2011).

The project site is within the jurisdictional boundary of the Antelope Valley Groundwater Adjudication. According to the 2010 Urban Water Management Plan for the Antelope Valley-East Kern Water Agency, the Agency is implementing a groundwater banking project that will improve the reliability of the Antelope Valley Region's water supplies through construction of the necessary infrastructure to store excess water during wet periods and recover water during dry and high demand periods. Probable supply totals for the year 2015 are based on the Agency receiving 62 percent of its delivery amount from the State Water Project, which is about 87,688 AF of water per year. Additional supply of 20,000 AF per year is projected to be available from water banking projects on a limited basis. The projected probable year supply and demand indicates that sufficient supplies are available to meet demand through 2030 in a normal year.

The City of Palmdale Utilities Division provides sanitary sewer collection service to its residents and businesses. Wastewater from Palmdale is treated at the Palmdale Water Reclamation Plant (WRP) which is operated by Sanitation Districts of Los Angeles County (LACSD). Treated effluent is reused for irrigation of trees and feed crops on adjacent land leased from the Los Angeles World Airports. The capacity of the Palmdale WRP is 15.0 million gallons per day (mgd). In 2007, the Palmdale WRP received an average of 9.5 mgd of inflow, leaving an excess capacity of 5.5 mgd . A Palmdale WRP 2025 Master Plan was developed in 2005 that included a planned set of improvements that will double capacity to 30.0 mgd (LACSD, 2005). However, since that time, plans have scaled back due to lower than projected development rates in Antelope Valley. Future capacity at Palmdale WRP will be expanded as needed as wastewater flows increase (Palmdale Water District, 2010). Residents and businesses in Palmdale receive a comprehensive range of refuse disposal and waste management planning services from Waste Management of Antelope Valley. Solid waste is sent to either the Antelope Valley Landfill or the Lancaster Landfill where it is process or recycled.

The proposed facility will be designed and constructed to achieve (at a minimum) LEED Silver level certification. The proposed project will incorporate sustainable design features to optimize energy and water use, enhance the sustainability of the site, improve indoor environmental quality, and maximize the use and reuse of sustainable and local resources.

## Regulatory Setting

Federal. None.
State. None.
Local. The Environmental Management Chapter 14.05 Title 14 of the Palmdale Municipal Code requires water efficient landscaping for all new construction and rehabilitated landscaping for public agency and private development projects requiring a permit, plan
check, or design review. This ordinance aims to promote the values and benefits of landscaping while recognizing the need to utilize water and other resources as efficiently as possible.

Under Public Services Element of the City of Palmdale General Plan, goals and policies are set forth to ensure that all development in Palmdale is serviced by adequate water distribution and sewage facilities. The policies also require that provision of streets, sewer, water, drainage, and other needed infrastructure be coordinate in a logical manner between adjacent developments, so as to reduce cost of design, construction and maintenance.

County's Adopted Energy and Environmental Policy (2006). This policy includes programs and elements, one of which is the Energy and Water Efficiency Program, which implements and monitoring energy and water conservation practices and efficiency projects, and enhances employee energy and water conservation awareness through education and promotions.

Ordinance No. 91-0046U, Title 11 - Health and Safety of the Los Angeles County Code. Part 4 of thie County Code, Water Conservation Requirements for Unincorporated Los Angeles County Area, includes prohibition and requirements associated with watering of lawns, landscaping, and washing vehicles.

Palmdale Water District Resolution 91-10. Resolution 91-10 becomes mandatory when a Stage 1 Water Shortage Emergency is declared and prohibits the watering of lawns, landscaping, and other turf areas at facilities such and public open space and landscaped areas more often than every third day and between the hours of 6:00 a.m. and 6:00 p.m during a declared water shortage.

City of Palmdale's Water Efficient Landscape Ordinance (2008). The landscape and irrigation engineering design standards of the ordinance reflects the changes mandated by AB 1881Model Water Efficient Landscape Ordinance that is coordinated through the California Department of Water Resources. Two of the state mandated changes are the required use of SMART controllers and the need to have a water budget for each project. For the efficient use of water, applicant shall submit landscape plan, landscape design plan, and irrigation design plan.

Although the project site is within the boundary of the City of Palmdale, as part of the project the site will become County property; therefore, the project is governed by the County's regulations. However, the project is also consistent with the City of Palmdale's goals and policies.

### 3.17.2 Impact Analysis

## a. Exceed wastewater treatment requirements of the applicable RWQCB?

LESS THAN SIGNIFICANT IMPACT. During construction, water will be required primarily for dust suppression, but will also be used for concrete washout and soil compaction. This water percolates into the ground after use, requiring no wastewater treatment. The new animal care facility will introduce wastewater discharge from daily operations (i.e., car wash, restroom use and maintenance activities [i.e., cleaning of animal enclosures and other facilities]) into the sanitary sewer system. The quality of wastewater generated by the proposed project will be similar to that generated by other
municipal uses. The wastewater will be transported to the Palmdale WRP where it will receive treatment. As described, below, there is adequate capacity available at the WRP to accept wastewater from the propose project. As such, the proposed project will not generate wastewater which will exceed the wastewater treatment requirements of the RWQCB. Therefore, impacts to WDR will be considered less than significant and no mitigation is required.
b. Require or result in the construction of new water or wastewater treatment facilities or expansion of existing facilities, the construction of which could cause significant environmental effects?

LESS THAN SIGNIFICANT IMPACT. During construction, water will be used for dust suppression during excavation, grading, and other construction-related activities such as mixing with concrete. In most cases, water trucks, which are filled off-site, are used during construction. No significant impact is anticipated to occur due to project construction activities because the water demands associated with such activities are short-term (temporary) and not anticipated to exceed available supplies or distribution infrastructure.

Operation of the proposed project will require an on-site fire hydrant, as well as water and wastewater infrastructure to connect to existing utilities within the adjacent Sierra Highway. During operations, water use and wastewater generation will be associated with activities such as drinking water, car wash, restroom use, landscaping, and maintenance of the facilities (i.e., cleaning animal cages). The DACC car wash is an outdoor area that will be equipped with a high pressure sprayer to clean each DACC truck prior to leaving the site each day. As shown in Figure 3, there is parking (a carport for approximately eight trucks); therefore it is estimated that the car wash will be used six to eight time, of short duration, and during business hours. The car wash will be equipped with a water clarifier and will use state-of-the art equipment that is energy and water efficient.

The proposed project also includes landscaping. As part of the County's adopted Energy and Environmental Policy, as well as LEED certification, there are requirements to optimize water use efficiency, such as water efficient equipment and landscaping, such as an automatic irrigation system and landscaping with drought-tolerant vegetation.

Based on the water duty factor of 750 gallons per day (gpd) for indoor uses and 304 gpd for outdoor uses for public facilities (Palmdale Water District, 2001), it is estimated that the proposed project will use approximately 2,035 gallons of water per day, which represents an increase in water demand compared to the existing vacant use on project site. Future water production can also be calculated as being 10 percent greater than wastewater demand to account for evaporation and lack of infiltration. Using this methodology, the water demand for the proposed project is estimated to be 2,750 gpd. The Palmdale Water District delivered 19,800 AF of water to its service area in 2010 and anticipates the demand to increase to $35,000 \mathrm{AF}$ in 2015, which is an increase of 15,200 AF. Using either the Palmdale Water District's water use factors or the 10 percent of wastewater generation method, the water demand of the proposed project will represent approximately 13 or 18 percent, respectively, of increased demand projected between

2010 and 2015 in the UWMP. Therefore, the proposed project will account for a small percentage of the overall increased demand for potable water within the Palmdale Water District. According to the UWMP, the increase in demand can be served by existing and planned water supplies. Therefore, the Palmdale Water District will be able to meet the water demand of the proposed project without the need for new or expanded facilities or resources, other than those already considered as part of the UWMP. Further, as described previously, the actual demand for water within the District is expected to be 5,000 AF less than projected in the UWMP given the slower than expected population growth rates, which further indicates that adequate water supply facilities will be available. Therefore, the proposed project will result in a less than significant impact to potable water supply facilities.

The 2009 City of Palmdale Sewer Master Plan estimates wastewater generation for nonresidential uses at a flow rate of 50 gpd per employee. This factor is equivalent to 1,000 to 1,200 gpd per net acre (City of Palmdale, 2009). Applying the employee wastewater generation rate factor to the proposed project, the operation of the new animal care facility will generate approximately 2,500 gallons of wastewater per day based on a total of 30 employees and 20 volunteers. As previously described, there is currently approximately 5.5 mgd of excess capacity at the Palmdale WRP. The proposed project represents approximately less than 0.05 percent of the excess capacity. Therefore, adequate treatment capacity is currently available and thus, no new treatment capacity will be required.

Further, the new facility will be built to achieve (at a minimum) LEED Silver Certification, which will require the incorporation of elements designed to reduce water use (which could also be associated with a reduction in wastewater generation) and wastewater generation such as use of low flow water fixtures, on-site wastewater treatment, and use of recycled water).

As described above, the proposed project will not require the construction of new or expanded water supply or wastewater treatment facilities. Therefore, impacts to water or wastewater treatment facilities from the proposed project will be considered less than significant and no mitigation is required.
c. Require or result in the construction of new storm water drainage facilities or expansion of existing facilities, the construction of which could cause significant environmental effects?

LESS THAN SIGNIFICANT IMPACT. The proposed project will include an on-site storm water drainage system to accommodate new impervious surface associated with two parking lots, walkways, and main building. These improvements will not result in need for new or expanded storm water drain facilities outside of the project site. As the project is largely vacant and paved, the amount of runoff will be less than existing conditions due to open spaces (i.e., exercise yard, courtyard/ acquaint yard, and shrubs and trees). Impacts from construction of the storm drainage system will be considered less than significant and no mitigation is required.
d. Have sufficient water supplies available to serve the project from existing entitlements and resources, or are new or expanded entitlements needed?

LESS THAN SIGNIFICANT IMPACT. During construction, water will be required primarily for dust suppression, and will also be used for concrete washout and soil compaction. Water required for construction will be obtained from the Palmdale Water District. Construction water volumes will be minimal and will not require new or expanded entitlements.

As discussed above, it is estimated that the proposed project will use approximately 2,035 to 2,750 gallons of water per day, which represents an increase in water demand compared to the existing vacant use on project site. Further, the new facility will be built to achieve (at a minimum) LEED Silver Certification and thus, will be required to incorporate elements designed to reduce water use such as use of low flow water fixtures, recycled water, and low water landscaping.

The Palmdale Water District delivered 19,800 AF of water to its service area in 2010. Using either the Palmdale Water District's water use factors or the 10 percent of wastewater generation method, the water demand of the proposed project will represent approximately 13 or 18 percent, respectively, of increased demand projected between 2010 and 2015 in the UWMP. According to the UWMP, the Palmdale Water District will be able to meet the water demand of the proposed project by existing and planned water supplies. Therefore, the project will result in a less than significant impact to potable water supply and no mitigation is required.
e. Result in a determination by the wastewater treatment provider which serves or may serve the project that it has adequate capacity to serve the project's projected demand in addition to the provider's existing commitments?

LESS THAN SIGNIFICANT IMPACT. As described in items a. and b. above, the proposed project will increase wastewater generation. The Palmdale WRP is anticipated to be to meet the wastewater needs of the proposed project without the need from new or expanded facilities or resources. The City of Palmdale Utilities Division will also have adequate capacity to serve the projected demand for this project in addition to its current commitments. Therefore, the proposed project will not require additional wastewater treatment capacity during project construction and operation resulting in a less than significant impact and no mitigation is required.
f. Be served by a landfill with sufficient permitted capacity to accommodate the project's solid waste disposal needs?

LESS THAN SIGNIFICANT IMPACT. Construction activities will generate solid waste; however, waste management during construction will include diversion of wastes from disposal through recycling and reuse. During project operation, the proposed project will generate a new source of solid waste, approximately 230.6 tons per year (considering 30 full-time employees, 20 part-time volunteers, and 70 daily visitors). All waste will be disposed of in accordance with federal, state, and local regulations.

The landfills serving the project area are the Antelope Valley Landfill, approximately two miles southwest of the project site (remaining capacity of 20,400,000 cy), and the

Lancaster Landfill, approximately 11 miles north of the project site (remaining capacity of $19,088,739 \mathrm{cy})$. Solid waste generation from the proposed project will represent 0.00012 percent and 0.00025 percent of the permitted throughput for the Antelope Valley Landfill and Lancaster Landfill, respectively. (CalRecycle, 2012) Both landfills have sufficient remaining capacity to accommodate the proposed project. The proposed project will not require the development of new landfills, nor will it require existing landfills to be expanded. Therefore, the proposed project will have a less than significant impact on landfills and no mitigation is required.
g. Comply with federal, state, and local statutes and regulations related to solid waste?

LESS THAN SIGNIFICANT IMPACT. All solid waste disposal will be managed in accordance with applicable federal, state and local statutes and regulations. Construction waste is accepted at local disposal facilities and recycling is encouraged. Impacts to solid waste will be considered less than significant and no mitigation is required.

### 3.18 Mandatory Findings of Significance

Mandatory Findings of Significance Checklist

a. Does the project have the potential to degrade the quality of the environment, substantially reduce the habitat of a fish or wildlife species, cause a fish or wildlife population to drop below self-sustaining levels, threaten to eliminate a plant or animal community, reduce the number or restrict the range of a rare or endangered plant or animal or eliminate important examples of the major periods of California history or prehistory?

LESS THAN SIGNIFICANT IMPACT. The proposed project will not be expected to substantially degrade fish, wildlife, and/or plant populations because there are no such populations on the site. Implementation of the proposed project will not impact a biological community. Additionally, there are no historical resources or expected archeological resources on-site. The proposed project will involve moderate amounts of grading and excavation and will not disturb native soils. The proposed site does not contain any important examples of the major periods of California history or prehistory. Therefore, the project will result in a less than significant impact on the quality of the environment and no mitigation is required.
b. Does the project have impacts that are individually limited, but cumulatively considerable? ("Cumulatively considerable" means that the incremental effects of a project are considerable when viewed in connection with the effects of past projects, the effects of other current projects, and the effects of probable future projects)

LESS THAN SIGNIFICANT IMPACT. As indicated throughout this Initial Study, impacts on all environmental resources were deemed to result in either "no impact" (agricultural resources, biological resource, mineral resources, population/housing, and recreation), "less than significant impact" (air quality, GHG, and utilities and service systems), or a combination of no impact/less than significant impact responses (aesthetics, geology/soils, hazards and hazardous materials, hydrology/water quality, land use, noise, transportation/traffic, and public services). By its very nature, climate change is a cumulative phenomenon and is not possible to link a single project to specific climatological changes; therefore the GHG emission analysis completed in Section 3.7, Greenhouse Gas Emissions, is a cumulative analysis.

To evaluate the proposed project's contribution to cumulative impacts, a list of past, approved, and pending projects within the project vicinity were identified (see Figure 4). The proposed project is the construction and operation of a new animal care facility. The cumulative analysis focuses on projects identified within a one mile radius of the project site. A one mile radius was deemed appropriate based on the project location in comparison with the proposed development projects on record with the City of Palmdale, as well as the potential for overlap of environmental resource impacts. Following is a list of the four related projects (nearest to furthest) within one mile of the proposed project (and their number as identified on Figure 4):
5. Religious Assembly Use: request to construct a 10,272 square foot building and two caretaker residences (each 1,746 square feet) at the southwest corner of $10^{\text {th }}$ Street East and Avenue Q-6 (located approximately 0.30 mile southeast from the project site)


Source: City of Palmdale, Planning Department, 2012.

1 Gold Buying at Keven Jewelers
2 Wireless Telecommunication Facility
3 Shopping Cart Control Plan
4 Intertex Companies Industrial Use
5 Religious Assembly Use
6 Commercial/Retail Center
7 Retail Center
8 Industrial Buildings
9 Commercial Buildings
10 Commercial Development
11 RY Properties

12 Subdivide 185.4 acres into 1 Public Facility Lot
13 Zoning Ord. Amendment to the Express Carwash Use
14 Time Extension to Mining Operation
15 Time Extension for Assisted Living Facility
16 Commercial Building w/ Alcohol \& Tobacco
17 Wireless Communication Facility
18 Alcoholic Beverage Establishment
19 PV Solar Facility
20 MW Photovoltaic Solar Facility
21 1.5-2 MW Solar PV Facility
22 4.0 MW Solar Facility

23 Commercial Express Carwash
24 Auto Parts Store
25 Subdivide Parcel
26 Commercial/Retail Building
27 Four Commercial/Retail Buildings
28 Global Premier Development
29 Public Service Building
30 Expansion of Existing Cable TV Equipment Room
31 Commercial Center w/ Supermarket
32 Construct a Drive Thru Restaurant
33 Construct Retail Building

18 Alcoholic Beverage Establishment: request to establish an incidental off-sale alcoholic beverage establishment at a discount retailer to be located at 244 East Palmdale Boulevard (located approximately 0.57 mile southwest from the project site)

24 Auto Part Store: request to construct an 8,241 square foot auto parts store at the intersection of $12^{\text {th }}$ Street East and Palmdale Boulevard (located approximately 0.60 mile southeast from the project site)
28. Global Premier Development: request to construct 16 single family homes on 6.22 acres behind the Desert Senior Apartments - located at 38780 Orchid View Place (located approximately 0.63 mile northeast from the project site)

There is no known construction dates associated with the related projects. The proposed expansion project will not result in any potentially significant impacts to the immediate areas surrounding the project site and no mitigation is required; therefore, no cumulative impact is anticipated. Following is an analysis of the resources associated with construction that have the potential to cause construction-related cumulative impacts:

## Air Quality

It is possible that construction of the proposed project could coincide with construction of the cumulative projects in the project area. Even if construction activities were concurrent, the proposed project's contribution to short-term, construction related air emissions will not be cumulatively considerable. The cumulative projects are subject to the same air quality thresholds and will be required to implement measures during construction, as required, to ensure that short-term air emissions will not be significant. As discussed in Section 3.3, Air Quality, air emissions generated during project construction and operation are below the air quality thresholds (refer to Table 3.3-3 and Table 3.3-4). The proposed project, therefore, will not result in a significant cumulative air quality impact and no mitigation is required.

## Noise

Project-level noise impacts will not be significant and have been evaluated in Section 3.12 above. Compliance with existing noise regulations of the City of Palmdale and County, as applicable, for all identified cumulative projects will minimize construction noise impacts. Vehicle volumes on roadways that might be generated by cumulative projects will have to double before it results in noise level increase perceptible to humans. Therefore, no perceptible increase in noise levels from traffic from cumulative projects is anticipated. The nearest cumulative project is the proposed Religious Assembly User (approximately 0.30 mile southeast from the project site). Being that a majority of the use of this type of project will be during evening and weekend hours, the ambient noise levels in the project area when combined with non-traffic operational noise generated by the proposed project will be minimal and will not substantially increase existing ambient noise levels in the project area. The cumulative project with the potential for the greatest generation of traffic is the Global Premier Development, which is a relatively small residential development approximately 0.63 mile from the project site. The ambient noise levels in the project area when combined with non-traffic
operational noise generated by the proposed project and the proposed residential development will be minimal and will not substantially increase existing ambient noise levels in the project area. Therefore, the proposed project will not contribute to cumulatively considerable noise impacts and no mitigation is required.

## Traffic

Project-level traffic impacts will not be significant and have been evaluated in Section 3.16 above. It is possible that a minor cumulative increase in traffic could occur with the construction of the proposed project and nearby projects. However, the City of Palmdale and surrounding area is relatively built-out and the cumulative projects identified will not likely lead to significant population or employment growth thereby creating a substantial increase in vehicle travel (commercial and industrial projects tend to be growth-inducing and generate many more vehicle trips than residential or institutional projects). With the exception of the Global Premier Development, which is a relatively small residential development approximately 0.63 mile from the project site, it is anticipated that vehicle trips from a majority of the cumulative projects are currently part of the daily volumes on area roadways. The proposed residential development is small (approximately 16 single family residences) and the furthest away from the project site. For these reasons, the proposed project will not contribute to cumulatively considerable traffic impacts and no mitigation is required.

As discussed in the respective issue areas, the proposed project will have no impact or a less than significant impact on environmental resources. Analysis of the proposed project did not discover any evidence that any impact of the proposed project could be significant in conjunction with related projects. Therefore, the proposed project will not result in any potentially significant impacts to the immediate areas surrounding the project site.
c. Does the project have environmental effects which will cause substantial adverse effects on human beings, either directly or indirectly?

LESS THAN SIGNIFICANT IMPACT. As indicated throughout this Initial Study, impacts on all environmental resources were deemed to result in either "no impact" or a "less than significant impact." These impacts are primarily construction-related (i.e., noise, dust and localized traffic increases) and are short-term effects to the environment. The proposed project will not have highly uncertain and potentially significant environmental effects or involve unique or unknown environmental risk, nor will it establish a precedent for future actions with potentially significant environmental effects. As a result, the proposed project will not create environmental effects that will cause substantial adverse effects on human beings, either directly or indirectly, and the preparation of an Environmental Impact Report is not required. Therefore, impacts from the proposed project on humans are considered less than significant and no mitigation is required.

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## SECTION 4

## List of Preparers

## Los Angeles County

Jason Kim - Capital Projects Manager

## CDM Smith

Dorothy Meyer - Project Manager, Principal Planner
Katie Owston - Environmental Planner
Lucy DeRosier - Environmental Planner
Juan Ramirez - Environmental Planner
Jennifer Jones - Environmental Scientist
Bhanu Kala - Traffic Engineer
Asami Tanimoto -Engineer

## Environmental Compliance Solutions, Inc.

Erin Sheehy - Air Quality Specialist

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## SECTION 5

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# Mitigation Monitoring and Reporting Program 

Section 21081.6 of the Public Resources Code (PRC), enacted by passage of AB 3180 (Cortese Bill), and CEQA Guidelines section 15097 require public agencies approving projects with significant environmental impacts to adopt a Mitigation Monitoring and Reporting Program (MMRP). The objective of this program is to ensure that mitigation measures adopted to avoid or mitigate potentially significant environmental impacts are implemented as part of the project. Section 21081.6 of the PRC requires all state and local agencies to establish monitoring and reporting programs whenever approval of a project relies upon a Mitigated Negative Declaration (MND) or an environmental impact report (EIR). In accordance with these requirements, this MMRP has been prepared to ensure that mitigation measures identified in the Initial Study (IS)/ MND for the proposed construction and operation of the County of Los Angeles Animal Care Center, Palmdale, CA (proposed project) are implemented in an effective and timely manner, and that identified impacts are avoided or mitigated to a level of insignificance. This plan identifies responsible parties for the mitigation program, and includes a detailed discussion of monitoring and reporting procedures for each mitigation measure.

## Responsible Party

The County of Los Angeles Department of Public Works (hereafter referred to as LACDPW) will be responsible for implementing and reporting mitigation measures in this program. The LACDPW will have responsibility for ensuring that mitigation measures are accomplished in an environmentally responsible manner. The LACDPW will be responsible for ensuring that the status of mitigation measures is reported in accordance with this program.

The LACDPW will be responsible for program oversight and ensure that applicable mitigation measures are carried forward in construction and operational and maintenance procedures. Mitigation measures will be included in applicable request for proposals, specifications and procedures issued for construction of the project. Other mitigation measures implemented by the Design Builder will be subject to oversight by the LACDPW. In addition, the LACDPW will be responsible for ensuring that mitigation measures are properly carried out by designated and qualified personnel.

## Mitigation Requirements

Based on the findings of the IS/MND, mitigation measures are not required for Aesthetics, Agriculture and Forest Resources, Air Quality, Biological Resources, Greenhouse Gas Emissions, Hydrology and Water Quality, Land Use and Planning, Mineral Resources, Noise, Population and Housing, Public Services, Recreation, Transportation/Traffic, and Utilities and Service Systems. Specific mitigation measures are required for Cultural Resources, Geology and Soils, and Hazards and Hazardous Materials. Potentially significant impacts in these environmental resource areas will be avoided or minimized with implementation of five (5) specific mitigation measures summarized on the monitoring table. The mitigation measures for
the project must be adopted by the Lead Agency (i.e. County of Los Angeles Board of Supervisors), in conjunction with adoption of the MND.

## Schedule and Reporting Frequency

The monitoring table below describes the mitigation measure, organization responsible for implementing the measure, organization responsible for monitoring the measure, and timing of verification for each measure. A column is provided for the monitoring party to sign-off on the implementation of each mitigation measure.

| Measure No. | Mitigation Measure | Responsible <br> Party | Monitoring Party | Timing of Verification |
| :--- | :--- | :--- | :--- | :--- |
| MM CUL-1 | In the event any archaeological materials or <br> subsurface deposits are exposed during ground <br> disturbance, the construction contractor will <br> cease activity in the affected area (e.g., redirect <br> activities into another area within the site) until <br> the discovery can be evaluated by a qualified <br> archaeologist or historic resources specialist, as <br> required, and appropriate treatment measures <br> implemented. If the discovery proves to be <br> significant pursuant to Section 15064.5(c) of <br> California Environmental Quality Act Guidelines, <br> additional work such as testing or data recovery <br> will be conducted as warranted. Methods during <br> monitoring and/or recovery of archaeological <br> resources shall be documented in a report of <br> findings. | Design Builder/ <br> Construction <br> Contractor | County of Los <br> Angeles <br> Department of <br> Public Works | During excavation and <br> grading |


| Measure No. | Mitigation Measure | Responsible <br> Party | Monitoring Party | Timing of Verification |
| :--- | :--- | :--- | :--- | :--- |
| MM CUL-2 | In the event human remains are encountered <br> during project construction, the Los Angeles <br> County Coroner shall be immediately contacted <br> to determine whether or not investigation of the <br> cause of death is required. The Cononer shall <br> make a determination of origin and disposition <br> pursuant to Public Resources Code Section <br> 5097.98. The Coroner will be notified of the find <br> immediately. In the event it is determined by the <br> Coroner the remains are Native American in <br> origin, the Native American Heritage <br> Commission shall be contacted to determine <br> necessary procedures for protection and <br> preservation of remains, including reburial, as <br> provided in the California Environmental Quality <br> Act Guidelines, Section 15064.5(e). | Design Builder/ <br> Construction <br> Contractor | Los Angeles <br> County <br> Department of <br> Public Works | During excavation and <br> grading |
| MM SOILS-1 | The proposed project will be designed and <br> constructed in accordance with remedial grading <br> and compaction requirements contained in the <br> report entitled "Geotechnical Study Report, East <br> Antelope Valley Animal Shelter"14 by Converse <br> Consultants (April 19, 2012). | Design Builder/ <br> Construction <br> Contractor | Los Angeles <br> County <br> Department of <br> Public Works | Prior to Final Design; During <br> Construction |

[^11]| Measure No. | Mitigation Measure | Responsible <br> Party | Monitoring Party | Timing of Verification |
| :--- | :--- | :--- | :--- | :--- |
| MM SOILS-2 | The proposed project will follow site-specific <br> geotechnical recommendations (e.g., drill drain <br> holes and backfill, and excavate at least the <br> upper two feet of soil for pavement) for the <br> abandonment of the subsurface slab/basement, <br> detailed in the correspondence from Converse <br> Consultants dated October 10, 2012. | Design Builder/ <br> Construction <br> Contractor | Los Angeles <br> County <br> Department of <br> Public Works | Prior to Final Design; During <br> Construction |
| MM HAZ-1 | Although contaminated soil is not anticipated to <br> be encountered, in the event soil contamination <br> is encountered during earthwork activities, all <br> contaminated soil handling and removal will be <br> required to adhere to a soil management plan <br> prepared and approved by the County. The soil <br> management plan will specify procedures for the <br> proper handling and disposal of contaminated <br> soil in accordance with all applicable local and <br> state regulations. | Design Builder/ <br> Construction <br> Contractor; Los <br> Angeles County <br> Department of <br> Public Works | Los Angeles <br> County <br> Department of <br> Public Works | During construction |

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## Section 7

## Response to Comments

The Draft IS/MND was circulated for a 30-day public review period, beginning on April 25, 2013 and ending on May 24, 2013. The public review period, during which interested agencies, organizations, and members of the public were invited to submit written comments, was noticed and conducted in compliance with CEQA Section 21091 and State CEQA Guidelines 15105. During the 30-day public review period, three comment letters were received. This section is organized in the following manner. Each letter received has been identified by a Comment Letter Number (No.). Comments requiring specific responses are bracketed and numbered (e.g., 1, 2, 3, etc.) and are referred to by Comment Letter No. and Response No. Copies of the written comment letters are provided before the response to comment. No changes have been made to the Draft IS/MND text.

The following is a list of the commenters on the Draft IS/MND:

| Comment Letter No. 1: | Antelope Valley Air Quality Management District <br> Bret Banks, Operations Manager <br> May 17, 2013 |
| :--- | :--- |
| Comment Letter No. 2: | City of Palmdale <br> Richard Kite, Planning Manager <br> May 22, 2013 |
| Comment Letter No. 3: | State of California, Governor's Office of Planning and Research, <br> State Clearinghouse and Planning Unit <br> Scott Morgan, Director <br> May 28, 2013 |

May 17, 2013


Eldon Heaston, Executive Director

In reply, please refer to AV0513/038

Mr. Jason Kim, Capitol Projects Manager
County of Los Angeles
Department of Public Works
Project Management Division I
900 South Fremont Avenue
Alhambra, CA 91803-1331

## RE: Initial Study/Proposed Mitigated Negative Declaration New County of Los Angeles Animal Care Facility

Mr. Kim:
The Antelope Valley Air Quality Management District (District) has received the request for comment on the proposed County of Los Angeles Animal Care Facility located at 38532,38560,38600 and 38624 Sierra Highway, Palmdale California.

The District requires compliance with District Rule 403, Fugitive Dust. One element of the rule is the submittal and approval of a Dust Control Plan prior to construction activities on a site that includes five acres or more of a Disturbed Surface Area for non-residential developments. The District will also require all applicable air quality permits.

Thank you for the opportunity to review this planning document. If you have any questions regarding this letter, please contact Bret Banks at (661) 723-8070 x2.

Sincerely,


Bret Banks
Operations Manager BB/bl

### 7.1 COMMENT LETTER NO. 1

## Antelope Valley Air Quality Management District

## Comment No. 1

The District requires compliance with District Rule 403, Fugitive Dust. One element of the rule is the submittal and approval of a Dust Control Plan prior to construction activities on a site that includes five acres or more of a Disturbed Surface Area for non-residential developments. The District will also require all applicable air quality permits.

## Response No. 1

Comment noted. As detailed in Section 3.3, Air Quality, of the Draft IS/MND (beginning on page 3-7), the project analysis addressed the District's Rule 403, Fugitive Dust, which includes the prohibition that visible dust will go beyond the property line of an emission source and contains a list of best applicable control measures to reduce fugitive dust impacts. The proposed project will adhere to all District rules and regulations; including those specific to $\mathrm{PM}_{10}$ emission control from construction operations (including a Dust Control Plan). In addition, as described on page 3-12 of the Draft IS/MND, the appropriate permit will be obtained from District prior to installation and operation of the emergency generator.

JAMES C. LEDFORD, JR. Mayor

TOM LACKEY Mayor Pro Tem

LAURA BETTENCOURT Councilmember

MIKE DISPENZA Councilmember

STEVEN D. HOFBAUER Councilmember

38300 Sierra Highway

Palmdale, CA 93550-4798

Tel: 661/267-5100

Fax: 661/267-5122

TDD: 661/267-5167

Auxiliary aids provided for
communication accessibility


May 22, 2013

Mr. Jason Kim, Capital Projecis Manager
County of Los Angeles
Department of Public Works
Project Management Division I
900 S. Fremont Avenue
Alhambra, CA 91803

## RE: Initial Study and Mitigated Negative Declaration for a New County of Los Angeles Animal Care Facility

Dear Mr. Kim:
Thank you for the opportunity to review the above referenced document. At this time, the City of Palmdale offers no comments.

If you have any questions, please do not hesitate to contact the Planning Department at (661) 267-5200.


Richard Kite Planning Manager

RK:KI

$$
w w w . c i t y o f p a l m d a l e . o r g
$$

### 7.2 COMMENT LETTER NO. 2

## City of Palmdale

## Comment No. 1

Thank you for the opportunity to review the above referenced document. At this time, the City of Palmdale offers no comments.

## Response No. 1

Thank you for your review of the document.


Ken Alex
DIRECTOR

May 28, 2013

Jason Kim
Los Angeles County
900 South Fremont Avenue
Alhambra, CA 91803-1331
Subject: Animal Care Center
SCH\#: 2013041077
Dear Jason Kim:
The State Clearinghouse submitted the above named Mitigated Negative Declaration to selected state agencies for review. The review period closed on May 24, 2013, and no state agencies submitted comments by that date. This letter acknowledges that you have complied with the State Clearinghouse review requirements for draft environmental documents, pursuant to the California Environmental Quality Act.

Please call the State Clearinghouse at (916) 445-0613 if you have any questions regarding the environmental review process. If you have a question about the above-named project, please refer to the ten-digit State Clearinghouse number when contacting this office.

Sincerely,


Director, State Clearinghouse

# Document Details Report <br> State Clearinghouse Data Base 



## Project Location

| County City | Los Angeles Palmdale |
| :---: | :---: |
| Region |  |
| Lat / Long | $34^{\circ} 35^{\prime} 1.7^{\prime \prime} \mathrm{N} / 118^{\circ} 6^{\prime} 58.7{ }^{\prime \prime} \mathrm{W}$ |
| Cross Streets | Sierra Highway and Avenue Q-6 East |
| Parcel No. | 3008-030-900 to -904 \& part of -905 |
| Township | Range Section Base |
| Proximity to: |  |
| Highways | Hwy 14 |
| Airports | Palmdale Regional |
| Railways | UP/Metrolink |
| Waterways |  |
| Schools | R. Rex Parris HS, Yucca ES, Guidance Charter School |
| Land Use | Public Facilities |
| Project Issues | Aesthetic/Visual; Agricultural Land; Air Quality; Archaeologic-Historic; Biological Resources; |
|  | Drainage/Absorption; Flood Plain/Flooding; Forest Land/Fire Hazard; Geologic/Seismic; Minerals; |
|  | Noise; Population/Housing Balance; Public Services; Recreation/Parks; Schools/Universities; Septic |
|  | System; Sewer Capacity; Soil Erosion/Compaction/Grading; Solid Waste; Toxic/Hazardous; |
|  | Traffic/Circulation; Vegetation; Water Quality; Water Supply; Wetland/Riparian; Landuse; Cumulative |
|  | Effects; Other Issues |

## Reviewing <br> Agencies

Resources Agency; Department of Fish and Wildlife, Region 5; Department of Parks and Recreation; Department of Water Resources; Resources, Recycling and Recovery; Caltrans, Division of Aeronautics; Caltrans, District 7; Regional Water Quality Control Bd., Region 6 (Victorville); Department of Toxic Substances Control; Native American Heritage Commission

### 7.3 COMMENT LETTER NO. 3

State of California Governor's Office of Planning and Research, State Clearinghouse and Planning Unit

## Comment No. 1

The State Clearinghouse submitted the above named Mitigated Negative Declaration to selected state agencies for review. The review period closed on May 24, 2013, and no state agencies submitted comments by that date. This letter acknowledges that you have complied with the State Clearinghouse review requirements for draft environmental documents, pursuant to the California Environmental Quality Act.

## Response No. 1

This is the transmittal letter from the State Clearinghouse that indicates the Lead Agency has complied with state requirements for distribution of the Initial Study and Mitigated Negative Declaration. No response is required.

# NOTICE OF INTENT TO ADOPT A MITIGATED NEGATIVE DECLARATION Project Titk: COUNTY OF LOS ANGELES ANIMAL CARE CENTER PROJECT, PALMDALE, CALIFORNIA 

Pursuant to the State of California Public Resources Code Article 7 of the California Environmental Quality Act (CEQA), as amended, the County of Los Angeles Department of Public Works has prepared an Initial Study for the project described below. Under CEQA, the County identified no significant impacts and proposes to adopt a Mitigated Negative Declaration

The County of Los Angeles proposes a new County of Los Angeles animal care facility (the County of Los Angeles Animal Care Center Project, Palmdale, CA, or "proposed project") that will alleviate the high volume of animal control services at the existing Lancaster Animal Care Center and further serve the needs of communities in the eastern portion of Antelope Valley, in northern Los Angeles County. The proposed facility will be on a 5.8 -acre site to be acquired from the City of Palmdale by Los Angeles County for the construction and operation of a one-story approximately 25,500 square foot indoor animal care center, as well as maintaining a portion of the site to remain fenced, vacant, and for possible future animal care center expansion. The proposed facility will have an average peak day capacity of approximately 361 animals of which approximately 35 percent (approximately 128) are anticipated to be dogs, 64 percent (approximately 229) are cats, and one percent (approximately four) are wildlife (nondomesticated animals). No livestock will be housed at the proposed facility and no animals will be housed outdoors.

An Initial Study and Mitigated Negative Declaration have been prepared pursuant to the requirements of the CEQA to assess the proposed project's potential impacts on the environment. Appropriate mitigation measures have been included in the proposed project in order to minimize any potential environmental impacts. Copies of the Initial Study and Mitigated Negative Declaration are available for public review at the following locations:

| County of Los Angeles | County of Los Angeles |  |
| :---: | :---: | :---: |
| Lake Los Angeles Library | Department of Public Works |  |
| 16921 E. Avenue O, \#A | Project Management Division I |  |
| Palmdale, CA 93591 | 900 South Fremont Avenue |  |
| M-T, 11:00 am to 7:00 pm | Alhambra, CA 91803 |  |
| W-Th-F, 10:00 am to 6:00 pm | M-Th, 6:45 am to 5:30 pm |  |
| Sat, 10:00 am to 5:00 pm |  |  |
| Palmdale City Hall | Palmdale City Library | Palmdale Planning Counter |
| 38300 N. Sierra Highway | 700 E. Palmdale Boulevard | 38250 N. Sierra Highway |
| Palmdale, CA 93550 | Palmdale, CA 93550 | Palmdale, CA 93550 |
| M-Th, 7:30 am to 6:00 pm | M-Th, 10:00 am to 8:00 pm F-Sat, 10:00 am to $5: 00 \mathrm{pm}$ Sun, 1:00 pm to $5: 00 \mathrm{pm}$ | M-Th, 7:30 am to 6:00 pm |

The 30-day review period will begin on April 25, 2013, and will end on May 24, 2013. Comments on the Initial Study and Mitigated Negative Declaration must be submitted in writing no later than May 24, 2013 at 5:30 pm. Please address all written comments to:

Mr. Jason Kim, Capital Projects Manager
County of Los Angeles
Department of Public Works
Project Management Division I
900 South Fremont Avenue
Alhambra, CA 91803-1331


THIS NOTICE WAS POSTED

Palmdale City Library
700 E. Palmdale Boulevard CA 93550 F-Sat, 10:00 am to 5:00 pm Sun, 1:00 pm to $5: 00 \mathrm{pm}$

Palmdale Planning Counter
N. Sierra Highway

Palmdale, CA 93550
M-Th, 7:30 am to 6:00 pm

Fax: (626) 979-5321
Email: jikim@dpw.lacounty.gov

Dean C. Logan, Registrar - Recorder/County Clerk
Electronically signed by TYFFANY YATES

REGISTRAR-RECORDER/COUNTY CLERK

The Final Mitigated Negative Declaration will incorporate responses to written comments received during the public review period and will be considered by the Board of Supervisors for approval of the project.

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|  |  |  |  | Hididide |  | COUNTY OF LOS ANGELESNOTICE OF INTENT TO ADOPT A MITIGATED NEGATIVE DECLARATIONCOUNTY OF LOS ANGELES ANIMAL CARE CENTER PROJECT， |  |  |
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## Notice of Completion \& Environmental Document Transmittal

Mail to: State Clearinghouse, P.O. Box 3044, Sacramento, CA 95812-3044 (916) 445-0613
For Hand Delivery/Street Address: 1400 Tenth Street, Sacramento, CA 95814

## SCH \#

Project Title: County of Los Angeles Animal Care Center, Palmdale, CA



Present Land Use/Zoning/General Plan Designation:
Public Facilities (PF)

The proposed project is a new approximately 25,500 square foot indoor County of Los Angeles animal care facility that will alleviate the high volume of animal control services at the existing Lancaster Animal Care Center and further serve the needs of communities in the eastern portion of Antelope Valley, in northern Los Angeles County. The facility is proposed on a 5.8-acre site to be acquired from the City of Palmdale by Los Angeles County for the construction/operation of the one-story facility, which includes visitor and employee parking. No livestock will be housed at the facility and no animals will be housed outdoors

## Reviewing Agencies Checklist

Lead Agencies may recommend State Clearinghouse distribution by marking agencies below with and "X". If you have already sent your document to the agency please denote that with an "S".

| X | Air Resources Board | X | Office of Historic Preservation |
| :---: | :---: | :---: | :---: |
|  | Boating \& Waterways, Department of |  | Office of Public School Construction |
|  | California Emergency Management Agency |  | Parks \& Recreation, Department of |
|  | California Highway Patrol |  | Pesticide Regulation, Department of |
| X | Caltrans District \# 5 |  | Public Utilities Commission |
|  | Caltrans Division of Aeronautics | X | Regional WQCB \# 6 |
|  | Caltrans Planning | $\bar{X}$ | Resources Agency |
|  | Central Valley Flood Protection Board |  | Resources Recycling and Recovery, Department of |
|  | Coachella Valley Mtns. Conservancy |  | S.F. Bay Conservation \& Development Comm. |
|  | Coastal Commission |  | San Gabriel \& Lower L.A. Rivers \& Mtns. Conservancy |
|  | Colorado River Board |  | San Joaquin River Conservancy |
|  | Conservation, Department of |  | Santa Monica Mtns. Conservancy |
|  | Corrections, Department of |  | State Lands Commission |
|  | Delta Protection Commission |  | SWRCB: Clean Water Grants |
|  | Education, Department of |  | SWRCB: Water Quality |
|  | Energy Commission |  | SWRCB: Water Rights |
| X | Fish \& Game Region \# 5 |  | Tahoe Regional Planning Agency |
|  | Food \& Agriculture, Department of | X | Toxic Substances Control, Department of |
|  | Forestry and Fire Protection, Department of | X | Water Resources, Department of |
|  | General Services, Department of |  |  |
|  | Health Services, Department of |  | Other: |
|  | Housing \& Community Development |  | Other: |
| X | Native American Heritage Commission |  |  |

## Local Public Review Period (to be filled in by lead agency)

Starting Date April 25, 2013 Ending Date May 24, 2013

## Lead Agency (Complete if applicable):

Consulting Firm: CDM Smith Applicant: County of Los Angeles Dept. of Public Works
Address: 111 Academy, Suite 150
City/State/Zip: Irvine, CA 92617
Contact: Dorothy Meyer
Address: 900 South Fremont Avenue
City/State/Zip: Alhambra, CA 91803-1331
Phone: (626) 300-2326
Phone: (949) 752-5452


Authority cited: Section 21083, Public Resources Code. Reference: Section 21161, Public Resources Code.

Appendix A
CalEEMod Emissions Output

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# County of Los Angeles Animal Care Center, Palmdale, CA 

Antelope Valley APCD Air District, Annual

### 1.0 Project Characteristics

### 1.1 Land Usage

| Land Uses | Size | Metric |
| :---: | :---: | :---: |
| Medical Office Building | 25.5 | 1000sqft |
| Parking Lot | 60 | 1000sqft |

### 1.2 Other Project Characteristics

| Urbanization | Urban | Wind Speed (m/s) | $2.2 \quad$ Utility Company |
| :--- | :--- | :--- | :--- |

Climate Zone
9
Precipitation Freq (Days) 33

### 1.3 User Entered Comments

Project Characteristics -
Land Use - Site acreage is 6.02 acres per project description (includes main building, parking lots, outdoor lot areas, courtyard, loading zone, etc)
Construction Phase - Architectural coating: assumes 15 days (default is 10 days).
Trips and VMT - Demolition hauling trips assume 20 tons of material per load, 5 mile trip length to landfill (model default is 20 miles)
Demolition $-\sim 3,500$ tons of debris estimated for removal of $\sim 2$ acres of existing pavement and miscellaneous debris.
Architectural Coating - Assume average interior/exterior VOC content is $125 \mathrm{~g} / \mathrm{L}$, which is $50 \%$ of default value (default = $250 \mathrm{~g} / \mathrm{L}$ ).

Vehicle Trips - Trip rate = 134 trips/day, 7 days/week ( 30 workers, 20 volunteers, 70 visitors, 14 deliveries). This trip rate is higher than model default trip rates for weekdays, Saturdays, and Sundays.
Area Coating -
Landscape Equipment -
Construction Off-road Equipment Mitigation - Fugitive dust mitigation assumes watering exposed areas 2 times per day, with $55 \%$ PM10 reduction and 55\% PM2.5 reduction (defaults).

### 2.0 Emissions Summary

### 2.1 Overall Construction

Unmitigated Construction

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| 2014 | 0.47 | 2.67 | 2.00 | 0.00 | 0.17 | 0.16 | 0.34 | 0.01 | 0.16 | 0.18 | 0.00 | 320.45 | 320.45 | 0.04 | 0.00 | 321.23 |
| 2015 | 0.56 | 0.33 | 0.27 | 0.00 | 0.01 | 0.02 | 0.03 | 0.00 | 0.02 | 0.02 | 0.00 | 41.36 | 41.36 | 0.00 | 0.00 | 41.46 |
| Total | 1.03 | 3.00 | 2.27 | 0.00 | 0.18 | 0.18 | 0.37 | 0.01 | 0.18 | 0.20 | 0.00 | 361.81 | 361.81 | 0.04 | 0.00 | 362.69 |

### 2.1 Overall Construction

Mitigated Construction

|  | ROG | NOx | co | SO2 | Fugitive PM10 | Exhaust <br> PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
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| Year | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| 2014 | 0.47 | 2.67 | 2.00 | 0.00 | 0.14 | 0.16 | 0.31 | 0.01 | 0.16 | 0.17 | 0.00 | 320.45 | 320.45 | 0.04 | 0.00 | 321.23 |
| 2015 | 0.56 | 0.33 | 0.27 | 0.00 | 0.01 | 0.02 | 0.03 | 0.00 | 0.02 | 0.02 | 0.00 | 41.36 | 41.36 | 0.00 | 0.00 | 41.46 |
| Total | 1.03 | 3.00 | 2.27 | 0.00 | 0.15 | 0.18 | 0.34 | 0.01 | 0.18 | 0.19 | 0.00 | 361.81 | 361.81 | 0.04 | 0.00 | 362.69 |

### 2.2 Overall Operational

Unmitigated Operational

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Total | Bio- CO2 | NBioCO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Area | 0.43 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Energy | 0.00 | 0.01 | 0.01 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 122.65 | 122.65 | 0.01 | 0.00 | 123.41 |
| Mobile | 2.79 | 6.51 | 24.26 | 0.03 | 3.61 | 0.22 | 3.83 | 0.06 | 0.21 | 0.27 | 0.00 | 3,137.39 | 3,137.39 | 0.15 | 0.00 | 3,140.60 |
| Waste |  |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 55.90 | 0.00 | 55.90 | 3.30 | 0.00 | -725.28 |
| Water |  |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 14.12 | 14.12 | 0.10 | 0.00 | 17.01 |
| Total | 3.22 | 6.52 | 24.27 | 0.03 | 3.61 | 0.22 | 3.83 | 0.06 | 0.21 | 0.27 | 55.90 | 3,274.16 | 3,330.06 | 3.56 | 0.00 | 3,406.30 |

### 2.2 Overall Operational

Mitigated Operational

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Area | 0.43 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Energy | 0.00 | 0.01 | 0.01 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 122.65 | 122.65 | 0.01 | 0.00 | 123.41 |
| Mobile | 2.79 | 6.51 | 24.26 | 0.03 | 3.61 | 0.22 | 3.83 | 0.06 | 0.21 | 0.27 | 0.00 | 3,137.39 | 3,137.39 | 0.15 | 0.00 | 3,140.60 |
| Waste |  |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 55.90 | 0.00 | 55.90 | 3.30 | 0.00 | 125.28 |
| Water |  |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 14.12 | 14.12 | 0.10 | 0.00 | 17.01 |
| Total | 3.22 | 6.52 | 24.27 | 0.03 | 3.61 | 0.22 | 3.83 | 0.06 | 0.21 | 0.27 | 55.90 | 3,274.16 | 3,330.06 | 3.56 | 0.00 | 3,406.30 |

### 3.0 Construction Detail

3.1 Mitigation Measures Construction

Water Exposed Area

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.04 | 0.00 | 0.04 | 0.01 | 0.00 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Off-Road | 0.05 | 0.36 | 0.23 | 0.00 |  | 0.02 | 0.02 |  | 0.02 | 0.02 | 0.00 | 35.79 | 35.79 | 0.00 | 0.00 | 35.87 |
| Total | 0.05 | 0.36 | 0.23 | 0.00 | 0.04 | 0.02 | 0.06 | 0.01 | 0.02 | 0.03 | 0.00 | 35.79 | 35.79 | 0.00 | 0.00 | 35.87 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.01 | 0.08 | 0.03 | 0.00 | 0.07 | 0.00 | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 12.89 | 12.89 | 0.00 | 0.00 | 12.89 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Worker | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.05 | 1.05 | 0.00 | 0.00 | 1.06 |
| Total | 0.01 | 0.08 | 0.04 | 0.00 | 0.07 | 0.00 | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 13.94 | 13.94 | 0.00 | 0.00 | 13.95 |

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.02 | 0.00 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Off-Road | 0.05 | 0.36 | 0.23 | 0.00 |  | 0.02 | 0.02 |  | 0.02 | 0.02 | 0.00 | 35.79 | 35.79 | 0.00 | 0.00 | 35.87 |
| Total | 0.05 | 0.36 | 0.23 | 0.00 | 0.02 | 0.02 | 0.04 | 0.00 | 0.02 | 0.02 | 0.00 | 35.79 | 35.79 | 0.00 | 0.00 | 35.87 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.01 | 0.08 | 0.03 | 0.00 | 0.07 | 0.00 | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 12.89 | 12.89 | 0.00 | 0.00 | 12.89 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Worker | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.05 | 1.05 | 0.00 | 0.00 | 1.06 |
| Total | 0.01 | 0.08 | 0.04 | 0.00 | 0.07 | 0.00 | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 | 13.94 | 13.94 | 0.00 | 0.00 | 13.95 |

### 3.3 Site Preparation - 2014

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.01 | 0.00 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Off-Road | 0.00 | 0.03 | 0.02 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 2.95 | 2.95 | 0.00 | 0.00 | 2.96 |
| Total | 0.00 | 0.03 | 0.02 | 0.00 | 0.01 | 0.00 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 2.95 | 2.95 | 0.00 | 0.00 | 2.96 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 | Bio- CO2 | NBio CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Worker | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.06 | 0.06 | 0.00 | 0.00 | 0.06 |
| Total | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.06 | 0.06 | 0.00 | 0.00 | 0.06 |

### 3.3 Site Preparation - 2014

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Off-Road | 0.00 | 0.03 | 0.02 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 2.95 | 2.95 | 0.00 | 0.00 | 2.96 |
| Total | 0.00 | 0.03 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.95 | 2.95 | 0.00 | 0.00 | 2.96 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{gathered} \hline \text { NBio- } \\ \text { CO2 } \end{gathered}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Worker | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.06 | 0.06 | 0.00 | 0.00 | 0.06 |
| Total | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.06 | 0.06 | 0.00 | 0.00 | 0.06 |

### 3.4 Grading - 2014

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.01 | 0.00 | 0.01 | 0.01 | 0.00 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Off-Road | 0.01 | 0.05 | 0.03 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 4.88 | 4.88 | 0.00 | 0.00 | 4.89 |
| Total | 0.01 | 0.05 | 0.03 | 0.00 | 0.01 | 0.00 | 0.01 | 0.01 | 0.00 | 0.01 | 0.00 | 4.88 | 4.88 | 0.00 | 0.00 | 4.89 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Worker | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.13 | 0.13 | 0.00 | 0.00 | 0.13 |
| Total | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.13 | 0.13 | 0.00 | 0.00 | 0.13 |

### 3.4 Grading - 2014

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Off-Road | 0.01 | 0.05 | 0.03 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 4.88 | 4.88 | 0.00 | 0.00 | 4.89 |
| Total | 0.01 | 0.05 | 0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.88 | 4.88 | 0.00 | 0.00 | 4.89 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Worker | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.13 | 0.13 | 0.00 | 0.00 | 0.13 |
| Total | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.13 | 0.13 | 0.00 | 0.00 | 0.13 |

### 3.5 Building Construction - 2014

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | 0.37 | 1.95 | 1.42 | 0.00 |  | 0.13 | 0.13 |  | 0.13 | 0.13 | 0.00 | 207.93 | 207.93 | 0.03 | 0.00 | 208.56 |
| Total | 0.37 | 1.95 | 1.42 | 0.00 |  | 0.13 | 0.13 |  | 0.13 | 0.13 | 0.00 | 207.93 | 207.93 | 0.03 | 0.00 | 208.56 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Vendor | 0.02 | 0.19 | 0.10 | 0.00 | 0.01 | ---01 | 0.02 | 0.00 | -0.01 | 0.01 | 0.00 | 30.82 | 30.82 | 0.00 | -0.00 | 30.83 |
| Worker | 0.02 | 0.02 | 0.16 | 0.00 | 0.03 | 0.00 | 0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 23.94 | 23.94 | 0.00 | 0.00 | 23.97 |
| Total | 0.04 | 0.21 | 0.26 | 0.00 | 0.04 | 0.01 | 0.06 | 0.00 | 0.01 | 0.01 | 0.00 | 54.76 | 54.76 | 0.00 | 0.00 | 54.80 |

### 3.5 Building Construction - 2014

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | 0.37 | 1.95 | 1.42 | 0.00 |  | 0.13 | 0.13 |  | 0.13 | 0.13 | 0.00 | 207.93 | 207.93 | 0.03 | 0.00 | 208.56 |
| Total | 0.37 | 1.95 | 1.42 | 0.00 |  | 0.13 | 0.13 |  | 0.13 | 0.13 | 0.00 | 207.93 | 207.93 | 0.03 | 0.00 | 208.56 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Vendor | 0.02 | 0.19 | 0.10 | 0.00 | 0.01 | 0.01 | 0.02 | 0.00 | 0.01 | 0.01 | 0.00 | 30.82 | 30.82 | 0.00 | 0.00 | 30.83 |
| Worker | 0.02 | 0.02 | 0.16 | 0.00 | 0.03 | 0.00 | 0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 23.94 | 23.94 | 0.00 | 0.00 | 23.97 |
| Total | 0.04 | 0.21 | 0.26 | 0.00 | 0.04 | 0.01 | 0.06 | 0.00 | 0.01 | 0.01 | 0.00 | 54.76 | 54.76 | 0.00 | 0.00 | 54.80 |

### 3.5 Building Construction - 2015

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | 0.04 | 0.21 | 0.16 | 0.00 |  | 0.01 | 0.01 |  | 0.01 | 0.01 | 0.00 | 24.39 | 24.39 | 0.00 | 0.00 | 24.46 |
| Total | 0.04 | 0.21 | 0.16 | 0.00 |  | 0.01 | 0.01 |  | 0.01 | 0.01 | 0.00 | 24.39 | 24.39 | 0.00 | 0.00 | 24.46 |

## Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Vendor | 0.00 | 0.02 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.62 | 3.62 | 0.00 | 0.00 | 3.62 |
| Worker | 0.00 | 0.00 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.74 | 2.74 | 0.00 | 0.00 | 2.74 |
| Total | 0.00 | 0.02 | 0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 6.36 | 6.36 | 0.00 | 0.00 | 6.36 |

### 3.5 Building Construction - 2015

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | 0.04 | 0.21 | 0.16 | 0.00 |  | 0.01 | 0.01 |  | 0.01 | 0.01 | 0.00 | 24.39 | 24.39 | 0.00 | 0.00 | 24.46 |
| Total | 0.04 | 0.21 | 0.16 | 0.00 |  | 0.01 | 0.01 |  | 0.01 | 0.01 | 0.00 | 24.39 | 24.39 | 0.00 | 0.00 | 24.46 |

Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Vendor | 0.00 | 0.02 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.62 | 3.62 | 0.00 | 0.00 | 3.62 |
| Worker | 0.00 | 0.00 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.74 | 2.74 | 0.00 | 0.00 | 2.74 |
| Total | 0.00 | 0.02 | 0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 6.36 | 6.36 | 0.00 | 0.00 | 6.36 |

3.6 Paving - 2015

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | 0.01 | 0.08 | 0.06 | 0.00 |  | 0.01 | 0.01 |  | 0.01 | 0.01 | 0.00 | 7.77 | 7.77 | 0.00 | 0.00 | 7.79 |
| Paving | 0.00 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Total | 0.01 | 0.08 | 0.06 | 0.00 |  | 0.01 | 0.01 |  | 0.01 | 0.01 | 0.00 | 7.77 | 7.77 | 0.00 | 0.00 | 7.79 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Worker | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.51 | 0.51 | 0.00 | 0.00 | 0.51 |
| Total | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.51 | 0.51 | 0.00 | 0.00 | 0.51 |

3.6 Paving - 2015

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Off-Road | 0.01 | 0.08 | 0.06 | 0.00 |  | 0.01 | 0.01 |  | 0.01 | 0.01 | 0.00 | 7.77 | 7.77 | 0.00 | 0.00 | 7.79 |
| Paving | 0.00 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Total | 0.01 | 0.08 | 0.06 | 0.00 |  | 0.01 | 0.01 |  | 0.01 | 0.01 | 0.00 | 7.77 | 7.77 | 0.00 | 0.00 | 7.79 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Worker | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.51 | 0.51 | 0.00 | 0.00 | 0.51 |
| Total | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.51 | 0.51 | 0.00 | 0.00 | 0.51 |

### 3.7 Architectural Coating - 2015

Unmitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Archit. Coating | 0.49 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Off-Road | 0.00 | 0.02 | 0.01 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 1.91 | 1.91 | 0.00 | 0.00 | 1.92 |
| Total | 0.49 | 0.02 | 0.01 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 1.91 | 1.91 | 0.00 | 0.00 | 1.92 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 | Bio- CO2 | NBio CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Worker | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.41 | 0.41 | 0.00 | 0.00 | 0.42 |
| Total | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.41 | 0.41 | 0.00 | 0.00 | 0.42 |

### 3.7 Architectural Coating - 2015

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Archit. Coating | 0.49 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Off-Road | 0.00 | 0.02 | 0.01 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 1.91 | 1.91 | 0.00 | 0.00 | 1.92 |
| Total | 0.49 | 0.02 | 0.01 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 1.91 | 1.91 | 0.00 | 0.00 | 1.92 |

Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Worker | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.41 | 0.41 | 0.00 | 0.00 | 0.42 |
| Total | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.41 | 0.41 | 0.00 | 0.00 | 0.42 |

### 4.0 Mobile Detail

4.1 Mitigation Measures Mobile

|  | ROG | NOX | co | SO2 | $\begin{gathered} \text { Fugitive } \\ \text { PM10 } \end{gathered}$ | Exhaust <br> PM10 | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Mitigated | 2.79 | 6.51 | 24.26 | 0.03 | 3.61 | 0.22 | 3.83 | 0.06 | 0.21 | 0.27 | 0.00 | 3,137.39 | : 3,137.39 | 0.15 | 0.00 | 3,140.60 |
| Unmitigated | 2.79 | 6.51 | 24.26 | 0.03 | 3.61 | 0.22 | 3.83 | 0.06 | 0.21 | 0.27 | 0.00 | 3,137.39 | 3,137.39 | 0.15 | 0.00 | 3,140.60 |
| Total | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |

### 4.2 Trip Summary Information

|  | Average Daily Trip Rate |  |  | Unmitigated | Mitigated |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Weekday | Saturday | Sunday | Annual VMT | Annual VMT |
| Medical Office Building | 3,417.00 | 3,417.00 | 3417.00 | 6,687,923 | 6,687,923 |
| Parking Lot | 0.00 | 0.00 | 0.00 |  |  |
| Total | 3,417.00 | 3,417.00 | 3,417.00 | 6,687,923 | 6,687,923 |

### 4.3 Trip Type Information

|  | Miles |  |  | Trip \% |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | H-W or C-W | $\mathrm{H}-\mathrm{S}$ or $\mathrm{C}-\mathrm{C}$ | H-O or C-NW | H-W or C-W | H-S or C-C | H-O or C-NW |
| Medical Office Building | 9.50 | 7.30 | 7.30 | 29.60 | 51.40 | 19.00 |
| Parking Lot | 9.50 | 7.30 | 7.30 | 0.00 | 0.00 | 0.00 |

### 5.0 Energy Detail

5.1 Mitigation Measures Energy

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Electricity Mitigated |  |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 107.77 | 107.77 | 0.00 | 0.00 | 108.45 |
| Electricity Unmitigated |  |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 107.77 | 107.77 | 0.00 | 0.00 | 108.45 |
| NaturalGas Mitigated | 0.00 | 0.01 | 0.01 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 14.87 | 14.87 | 0.00 | 0.00 | 14.96 |
| NaturalGas Unmitigated | 0.00 | 0.01 | 0.01 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 14.87 | 14.87 | 0.00 | 0.00 | 14.96 |
| Total | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |

### 5.2 Energy by Land Use - NaturalGas

Unmitigated

|  | NaturalGas Use | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kBTU | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Medical Office Building | 278715 | 0.00 | 0.01 | 0.01 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 14.87 | 14.87 | 0.00 | 0.00 | 14.96 |
| Parking Lot | 0 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Total |  | 0.00 | 0.01 | 0.01 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 14.87 | 14.87 | 0.00 | 0.00 | 14.96 |

## Mitigated

|  | NaturalGas Use | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kBTU | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Medical Office Building | 278715 | 0.00 | 0.01 | 0.01 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 14.87 | 14.87 | 0.00 | 0.00 | 14.96 |
| Parking Lot | 0 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Total |  | 0.00 | 0.01 | 0.01 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 14.87 | 14.87 | 0.00 | 0.00 | 14.96 |

### 5.3 Energy by Land Use - Electricity

Unmitigated

|  | Electricity Use | ROG | NOx | CO | SO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kWh | tons/yr |  |  |  | MT/yr |  |  |  |
| Medical Office Building | 370515 |  |  |  |  | 107.77 | 0.00 | 0.00 | 108.45 |
| Parking Lot | 0 |  |  |  |  | 0.00 | 0.00 | 0.00 | 0.00 |
| Total |  |  |  |  |  | 107.77 | 0.00 | 0.00 | 108.45 |

Mitigated

|  | Electricity Use | ROG | NOx | CO | SO2 | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kWh | tons/yr |  |  |  | MT/yr |  |  |  |
| Medical Office Building | 370515 |  |  |  |  | 107.77 | 0.00 | 0.00 | 108.45 |
| Parking Lot | 0 |  |  |  |  | 0.00 | 0.00 | 0.00 | 0.00 |
| Total |  |  |  |  |  | 107.77 | 0.00 | 0.00 | 108.45 |

### 6.0 Area Detail

6.1 Mitigation Measures Area

|  | ROG | NOX | co | SO2 | Fugitive PM10 | Exhaust <br> PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \hline \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Mitigated | 0.43 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Unmitigated | 0.43 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Total | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |

### 6.2 Area by SubCategory

## Unmitigated

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SubCategory | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Architectural Coating | 0.10 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Consumer Products | 0.33 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Landscaping | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Total | 0.43 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

### 6.2 Area by SubCategory

Mitigated

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \hline \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SubCategory | tons/yr |  |  |  |  |  |  |  |  |  | MT/yr |  |  |  |  |  |
| Architectural Coating | 0.10 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Consumer Products | 0.33 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Landscaping | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Total | 0.43 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

7.0 Water Detail
7.1 Mitigation Measures Water

|  | ROG | NOx | CO | SO2 | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | tons/yr |  |  |  | MT/yr |  |  |  |
| Mitigated |  |  |  |  | 14.12 | 0.10 | 0.00 | 17.01 |
| Unmitigated |  |  |  |  | 14.12 | 0.10 | 0.00 | 17.01 |
| Total | NA | NA | NA | NA | NA | NA | NA | NA |

### 7.2 Water by Land Use

Unmitigated

|  | Indoor/Outdoor Use | ROG | NOx | CO | SO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Mgal | tons/yr |  |  |  | MT/yr |  |  |  |
| Medical Office Building | $\begin{aligned} & 3.19975 / \\ & 0.609477 \end{aligned}$ |  |  |  |  | 14.12 | 0.10 | 0.00 | 17.01 |
| Parking Lot | $0 / 0$ |  |  |  |  | 0.00 | 0.00 | 0.00 | 0.00 |
| Total |  |  |  |  |  | 14.12 | 0.10 | 0.00 | 17.01 |

### 7.2 Water by Land Use

Mitigated

|  | $\begin{aligned} & \text { Indoor/Outdoor } \\ & \text { Use } \end{aligned}$ | ROG | NOx | co | SO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Mgal | tons/yr |  |  |  | MT/yr |  |  |  |
| Medical Office Building | $\begin{aligned} & 3.19975 / \\ & 0.609477 \end{aligned}$ |  |  |  |  | 14.12 | 0.10 | 0.00 | 17.01 |
| Parking Lot | $0 / 0$ |  |  |  |  | 0.00 | 0.00 | 0.00 | 0.00 |
| Total |  |  |  |  |  | 14.12 | 0.10 | 0.00 | 17.01 |

### 8.0 Waste Detail

### 8.1 Mitigation Measures Waste

Category/Year

|  | ROG | NOx | CO | SO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |

### 8.2 Waste by Land Use

Unmitigated

|  | Waste Disposed | ROG | NOx | CO | SO2 | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | tons | tons/yr |  |  |  | MT/yr |  |  |  |
| Medical Office Building | 275.4 |  |  |  |  | 55.90 | 3.30 | 0.00 | 125.28 |
| Parking Lot | 0 |  |  |  |  | 0.00 | 0.00 | 0.00 | 0.00 |
| Total |  |  |  |  |  | 55.90 | 3.30 | 0.00 | 125.28 |

Mitigated

|  | Waste Disposed | ROG | NOx | CO | SO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | tons | tons/yr |  |  |  | MT/yr |  |  |  |
| Medical Office Building | 275.4 |  |  |  |  | 55.90 | 3.30 | 0.00 | 125.28 |
| Parking Lot | 0 |  |  |  |  | 0.00 | 0.00 | 0.00 | 0.00 |
| Total |  |  |  |  |  | 55.90 | 3.30 | 0.00 | 125.28 |

# County of Los Angeles Animal Care Center, Palmdale, CA 

Antelope Valley APCD Air District, Summer

### 1.0 Project Characteristics

### 1.1 Land Usage

| Land Uses | Size | Metric |
| :---: | :---: | :---: |
| Medical Office Building | 25.5 | 1000sqft |
| Parking Lot | 60 | 1000sqft |

### 1.2 Other Project Characteristics

Urbanization Urban $\quad$ Wind Speed (m/s) $2.2 \quad$ Utility Company Southern California Edison
Climate Zone
9
Precipitation Freq (Days) 33

### 1.3 User Entered Comments

Project Characteristics -
Land Use - Site acreage is 6.02 acres per project description (includes main building, parking lots, outdoor lot areas, courtyard, loading zone, etc)
Construction Phase - Architectural coating: assumes 15 days (default is 10 days).
Trips and VMT - Demolition hauling trips assume 20 tons of material per load, 5 mile trip length to landfill (model default is 20 miles)
Demolition $-\sim 3,500$ tons of debris estimated for removal of $\sim 2$ acres of existing pavement and miscellaneous debris.
Architectural Coating - Assume average interior/exterior VOC content is $125 \mathrm{~g} / \mathrm{L}$, which is $50 \%$ of default value (default = $250 \mathrm{~g} / \mathrm{L}$ ).

Vehicle Trips - Trip rate = 134 trips/day, 7 days/week ( 30 workers, 20 volunteers, 70 visitors, 14 deliveries). This trip rate is higher than model default trip rates for weekdays, Saturdays, and Sundays.
Area Coating -
Landscape Equipment -
Construction Off-road Equipment Mitigation - Fugitive dust mitigation assumes watering exposed areas 2 times per day, with $55 \%$ PM10 reduction and 55\% PM2.5 reduction (defaults).

### 2.0 Emissions Summary

### 2.1 Overall Construction (Maximum Daily Emission)

Unmitigated Construction

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| 2014 | 5.48 | 44.29 | 26.98 | 0.05 | 12.01 | 2.39 | 14.40 | 2.90 | 2.36 | 4.37 | 0.00 | 5,504.94 | 0.00 | 0.46 | 0.00 | 5,514.66 |
| 2015 | 66.44 | 22.23 | 18.45 | 0.04 | 0.56 | 1.38 | 1.94 | 0.01 | 1.37 | 1.38 | 0.00 | 3,274.43 | 0.00 | 0.36 | 0.00 | 3,282.04 |
| Total | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |

### 2.1 Overall Construction (Maximum Daily Emission)

Mitigated Construction

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | NBioCO 2 | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| 2014 | 5.48 | 44.29 | 26.98 | 0.05 | 9.95 | 2.39 | 12.34 | 1.30 | 2.36 | 2.77 | 0.00 | 5,504.94 | 0.00 | 0.46 | 0.00 | 5,514.66 |
| 2015 | 66.44 | 22.23 | 18.45 | 0.04 | 0.56 | 1.38 | 1.94 | 0.01 | 1.37 | 1.38 | 0.00 | 3,274.43 | 0.00 | 0.36 | 0.00 | 3,282.04 |
| Total | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |

### 2.2 Overall Operational

Unmitigated Operational

|  | ROG | NOx | CO | SO2 | Fugitive | Exhaust | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive | Exhaust PM2.5 | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \mathrm{CO2} \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Area | 2.37 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Energy | 0.01 | 0.07 | 0.06 | 0.00 |  | 0.00 | 0.01 |  | 0.00 | 0.01 |  | 89.84 |  | 0.00 | 0.00 | 90.38 |
| Mobile | 18.77 | 36.53 | 146.43 | 0.21 | 22.15 | 1.23 | 23.37 | 0.31 | 1.16 | 1.47 |  | 21,233.92 |  | 0.90 |  | 21,252.76 |
| Total | 21.15 | 36.60 | 146.49 | 0.21 | 22.15 | 1.23 | 23.38 | 0.31 | 1.16 | 1.48 |  | 21,323.76 |  | 0.90 | 0.00 | 21,343.14 |

Mitigated Operational

|  | ROG | NOx | co | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | 1b/day |  |  |  |  |  |
| Area | 2.37 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Energy | 0.01 | 0.07 | 0.06 | 0.00 |  | 0.00 | 0.01 |  | 0.00 | 0.01 |  | 89.84 |  | 0.00 | 0.00 | 90.38 |
| Mobile | 18.77 | 36.53 | 146.43 | 0.21 | 22.15 | 1.23 | 23.37 | 0.31 | 1.16 | 1.47 |  | 21,233.92 |  | 0.90 |  | 21,252.76 |
| Total | 21.15 | 36.60 | 146.49 | 0.21 | 22.15 | 1.23 | 23.38 | 0.31 | 1.16 | 1.48 |  | 21,323.76 |  | 0.90 | 0.00 | 21,343.14 |

### 3.1 Mitigation Measures Construction

Water Exposed Area

### 3.2 Demolition - 2014

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 3.74 | 0.00 | 3.74 | 0.00 | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Off-Road | 4.75 | 35.99 | 22.84 | 0.04 |  | 2.08 | 2.08 |  | 2.08 | 2.08 |  | 3,946.47 |  | 0.42 |  | 3,955.39 |
| Total | 4.75 | 35.99 | 22.84 | 0.04 | 3.74 | 2.08 | 5.82 | 0.00 | 2.08 | 2.08 |  | 3,946.47 |  | 0.42 |  | 3,955.39 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.64 | 8.22 | 3.29 | 0.01 | 8.10 | 0.30 | 8.40 | 0.02 | 0.28 | 0.30 |  | 1,424.55 |  | 0.03 |  | 1,425.20 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.09 | 0.07 | 0.85 | 0.00 | 0.17 | 0.00 | 0.17 | 0.00 | 0.00 | 0.01 |  | 133.92 |  | 0.01 |  | 134.07 |
| Total | 0.73 | 8.29 | 4.14 | 0.01 | 8.27 | 0.30 | 8.57 | 0.02 | 0.28 | 0.31 |  | 1,558.47 |  | 0.04 |  | 1,559.27 |

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 1.69 | 0.00 | 1.69 | 0.00 | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Off-Road | 4.75 | 35.99 | 22.84 | 0.04 |  | 2.08 | 2.08 |  | 2.08 | 2.08 | 0.00 | 3,946.47 |  | 0.42 |  | 3,955.39 |
| Total | 4.75 | 35.99 | 22.84 | 0.04 | 1.69 | 2.08 | 3.77 | 0.00 | 2.08 | 2.08 | 0.00 | 3,946.47 |  | 0.42 |  | 3,955.39 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.64 | 8.22 | 3.29 | 0.01 | 8.10 | 0.30 | 8.40 | 0.02 | 0.28 | 0.30 |  | 1,424.55 |  | 0.03 |  | 1,425.20 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.09 | 0.07 | 0.85 | 0.00 | 0.17 | 0.00 | 0.17 | 0.00 | 0.00 | 0.01 |  | 133.92 |  | 0.01 |  | 134.07 |
| Total | 0.73 | 8.29 | 4.14 | 0.01 | 8.27 | 0.30 | 8.57 | 0.02 | 0.28 | 0.31 |  | 1,558.47 |  | 0.04 |  | 1,559.27 |

### 3.3 Site Preparation - 2014

Unmitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive | Exhaust PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \hline \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio-CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 5.80 | 0.00 | 5.80 | 2.90 | 0.00 | 2.90 |  |  |  |  |  | 0.00 |
| Off-Road | 3.75 | 29.67 | 17.95 | 0.03 |  | 1.47 | 1.47 |  | 1.47 | 1.47 |  | 3,253.39 |  | 0.34 |  | 3,260.45 |
| Total | 3.75 | 29.67 | 17.95 | 0.03 | 5.80 | 1.47 | 7.27 | 2.90 | 1.47 | 4.37 |  | 3,253.39 |  | 0.34 |  | 3,260.45 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.05 | 0.04 | 0.52 | 0.00 | 0.10 | 0.00 | 0.11 | 0.00 | 0.00 | 0.00 |  | 82.41 |  | 0.00 |  | 82.51 |
| Total | 0.05 | 0.04 | 0.52 | 0.00 | 0.10 | 0.00 | 0.11 | 0.00 | 0.00 | 0.00 |  | 82.41 |  | 0.00 |  | 82.51 |

### 3.3 Site Preparation - 2014

Mitigated Construction On-Site

|  | ROG | NOX | co | SO2 | Fugitive PM10 | Exhaust <br> PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \hline \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | co2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 2.61 | 0.00 | 2.61 | 1.30 | 0.00 | 1.30 |  |  |  |  |  | 0.00 |
| Off-Road | 3.75 | 29.67 | 17.95 | 0.03 |  | 1.47 | 1.47 |  | 1.47 | 1.47 | 0.00 | 3,253.39 |  | 0.34 |  | 3,260.45 |
| Total | 3.75 | 29.67 | 17.95 | 0.03 | 2.61 | 1.47 | 4.08 | 1.30 | 1.47 | 2.77 | 0.00 | 3,253.39 |  | 0.34 |  | 3,260.45 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{gathered} \hline \text { NBio- } \\ \text { CO2 } \end{gathered}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.05 | 0.04 | 0.52 | 0.00 | 0.10 | 0.00 | 0.11 | 0.00 | 0.00 | 0.00 |  | 82.41 |  | 0.00 |  | 82.51 |
| Total | 0.05 | 0.04 | 0.52 | 0.00 | 0.10 | 0.00 | 0.11 | 0.00 | 0.00 | 0.00 |  | 82.41 |  | 0.00 |  | 82.51 |

### 3.4 Grading - 2014

Unmitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 4.91 | 0.00 | 4.91 | 2.48 | 0.00 | 2.48 |  |  |  |  |  | 0.00 |
| Off-Road | 3.11 | 24.59 | 14.80 | 0.03 |  | 1.21 | 1.21 |  | 1.21 | 1.21 |  | 2,689.9 |  | 0.28 |  | 2,695.82 |
| Total | 3.11 | 24.59 | 14.80 | 0.03 | 4.91 | 1.21 | 6.12 | 2.48 | 1.21 | 3.69 |  | 2,689.97 |  | 0.28 |  | 2,695.82 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.05 | 0.04 | 0.52 | 0.00 | 0.10 | 0.00 | 0.11 | 0.00 | 0.00 | 0.00 |  | 82.41 |  | 0.00 |  | 82.51 |
| Total | 0.05 | 0.04 | 0.52 | 0.00 | 0.10 | 0.00 | 0.11 | 0.00 | 0.00 | 0.00 |  | 82.41 |  | 0.00 |  | 82.51 |

### 3.4 Grading - 2014

Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive | Exhaust PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \hline \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 2.21 | 0.00 | 2.21 | 1.12 | 0.00 | 1.12 |  |  |  |  |  | 0.00 |
| Off-Road | 3.11 | 24.59 | 14.80 | 0.03 |  | 1.21 | 1.21 |  | 1.21 | 1.21 | 0.00 | 2,689.97 |  | 0.28 |  | 2,695.82 |
| Total | 3.11 | 24.59 | 14.80 | 0.03 | 2.21 | 1.21 | 3.42 | 1.12 | 1.21 | 2.33 | 0.00 | 2,689.97 |  | 0.28 |  | 2,695.82 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.05 | 0.04 | 0.52 | 0.00 | 0.10 | 0.00 | 0.11 | 0.00 | 0.00 | 0.00 |  | 82.41 |  | 0.00 |  | 82.51 |
| Total | 0.05 | 0.04 | 0.52 | 0.00 | 0.10 | 0.00 | 0.11 | 0.00 | 0.00 | 0.00 |  | 82.41 |  | 0.00 |  | 82.51 |

### 3.5 Building Construction - 2014

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | NBioCO 2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 4.15 | 21.74 | 15.92 | 0.03 |  | 1.46 | 1.46 |  | 1.46 | 1.46 |  | 2,561.58 |  | 0.37 |  | 2,569.39 |
| Total | 4.15 | 21.74 | 15.92 | 0.03 |  | 1.46 | 1.46 |  | 1.46 | 1.46 |  | 2,561.58 |  | 0.37 |  | 2,569.39 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.16 | 2.10 | 0.98 | 0.00 | --13 | -0.06 | --19 | 0.00 | -0.06 | 0.06 |  | 381.14 |  | 0.01 |  | 381.31 |
| Worker | 0.22 | 0.19 | 2.17 | 0.00 | 0.43 | 0.01 | 0.44 | 0.01 | 0.01 | 0.02 |  | 339.96 |  | 0.02 |  | 340.34 |
| Total | 0.38 | 2.29 | 3.15 | 0.00 | 0.56 | 0.07 | 0.63 | 0.01 | 0.07 | 0.08 |  | 721.10 |  | 0.03 |  | 721.65 |

### 3.5 Building Construction - 2014

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{gathered} \text { NBio- } \\ \mathrm{CO} 2 \end{gathered}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 4.15 | 21.74 | 15.92 | 0.03 |  | 1.46 | 1.46 |  | 1.46 | 1.46 | 0.00 | 2,561.58 | ' | 0.37 |  | 2,569.39 |
| Total | 4.15 | 21.74 | 15.92 | 0.03 |  | 1.46 | 1.46 |  | 1.46 | 1.46 | 0.00 | 2,561.58 |  | 0.37 |  | 2,569.39 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.16 | 2.10 | 0.98 | 0.00 | --13 | -0.06 | --19 | 0.00 | -0.06 | 0.06 |  | 381.14 |  | 0.01 |  | 381.31 |
| Worker | 0.22 | 0.19 | 2.17 | 0.00 | 0.43 | 0.01 | 0.44 | 0.01 | 0.01 | 0.02 |  | 339.96 |  | 0.02 |  | 340.34 |
| Total | 0.38 | 2.29 | 3.15 | 0.00 | 0.56 | 0.07 | 0.63 | 0.01 | 0.07 | 0.08 |  | 721.10 |  | 0.03 |  | 721.65 |

### 3.5 Building Construction - 2015

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBioCO 2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 3.78 | 20.14 | 15.61 | 0.03 |  | 1.31 | 1.31 |  | 1.31 | 1.31 |  | 2,561.58 |  | 0.34 |  | 2,568.69 |
| Total | 3.78 | 20.14 | 15.61 | 0.03 |  | 1.31 | 1.31 |  | 1.31 | 1.31 |  | 2,561.58 |  | 0.34 |  | 2,568.69 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.15 | 1.93 | 0.91 | 0.00 | --13 | -0.06 | --19 | 0.00 | --05 | 0.06 |  | -381.30 |  | 0.01 |  | 381.45 |
| Worker | 0.20 | 0.16 | 1.93 | 0.00 | 0.43 | 0.01 | 0.44 | 0.01 | 0.01 | 0.02 |  | 331.55 |  | 0.02 |  | 331.90 |
| Total | 0.35 | 2.09 | 2.84 | 0.00 | 0.56 | 0.07 | 0.63 | 0.01 | 0.06 | 0.08 |  | 712.85 |  | 0.03 |  | 713.35 |

### 3.5 Building Construction - 2015

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{gathered} \text { NBio- } \\ \mathrm{CO} 2 \end{gathered}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 3.78 | 20.14 | 15.61 | 0.03 |  | 1.31 | 1.31 |  | 1.31 | 1.31 | 0.00 | 2,561.58 | ' | 0.34 |  | 2,568.69 |
| Total | 3.78 | 20.14 | 15.61 | 0.03 |  | 1.31 | 1.31 |  | 1.31 | 1.31 | 0.00 | 2,561.58 |  | 0.34 |  | 2,568.69 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.15 | 1.93 | 0.91 | 0.00 | --13 | -0.06 | --19 | 0.00 | --05 | 0.06 |  | -381.30 |  | 0.01 |  | 381.45 |
| Worker | 0.20 | 0.16 | 1.93 | 0.00 | 0.43 | 0.01 | 0.44 | 0.01 | 0.01 | 0.02 |  | 331.55 |  | 0.02 |  | 331.90 |
| Total | 0.35 | 2.09 | 2.84 | 0.00 | 0.56 | 0.07 | 0.63 | 0.01 | 0.06 | 0.08 |  | 712.85 |  | 0.03 |  | 713.35 |

3.6 Paving - 2015

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 2.62 | 16.38 | 11.89 | 0.02 |  | 1.34 | 1.34 |  | 1.34 | 1.34 |  | 1,712.73 |  | 0.24 |  | 1,717.66 |
| Paving | 0.36 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Total | 2.98 | 16.38 | 11.89 | 0.02 |  | 1.34 | 1.34 |  | 1.34 | 1.34 |  | 1,712.73 |  | 0.24 |  | 1,717.66 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.08 | 0.06 | 0.76 | 0.00 | 0.17 | 0.00 | 0.17 | 0.00 | 0.00 | 0.01 |  | 130.61 |  | 0.01 |  | 130.75 |
| Total | 0.08 | 0.06 | 0.76 | 0.00 | 0.17 | 0.00 | 0.17 | 0.00 | 0.00 | 0.01 |  | 130.61 |  | 0.01 |  | 130.75 |

3.6 Paving - 2015

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 2.62 | 16.38 | 11.89 | 0.02 |  | 1.34 | 1.34 |  | 1.34 | 1.34 | 0.00 | 1,712.73 |  | 0.24 |  | 1,717.66 |
| Paving | 0.36 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Total | 2.98 | 16.38 | 11.89 | 0.02 |  | 1.34 | 1.34 |  | 1.34 | 1.34 | 0.00 | 1,712.73 |  | 0.24 |  | 1,717.66 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.08 | 0.06 | 0.76 | 0.00 | 0.17 | 0.00 | 0.17 | 0.00 | 0.00 | 0.01 |  | 130.61 |  | 0.01 |  | 130.75 |
| Total | 0.08 | 0.06 | 0.76 | 0.00 | 0.17 | 0.00 | 0.17 | 0.00 | 0.00 | 0.01 |  | 130.61 |  | 0.01 |  | 130.75 |

### 3.7 Architectural Coating - 2015

Unmitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive | Exhaust PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \hline \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio-CO2 | $\begin{gathered} \text { NBio- } \\ \text { CO2 } \end{gathered}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Archit. Coating | 65.99 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Off-Road | 0.41 | 2.57 | 1.90 | 0.00 |  | 0.22 | 0.22 |  | 0.22 | 0.22 |  | 281.19 |  | 0.04 |  | 281.96 |
| Total | 66.40 | 2.57 | 1.90 | 0.00 |  | 0.22 | 0.22 |  | 0.22 | 0.22 |  | 281.19 |  | 0.04 |  | 281.96 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 | Bio- CO2 | NBioCO 2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.04 | 0.03 | 0.41 | 0.00 | 0.09 | 0.00 | 0.09 | 0.00 | 0.00 | 0.00 |  | 70.33 |  | 0.00 |  | 70.40 |
| Total | 0.04 | 0.03 | 0.41 | 0.00 | 0.09 | 0.00 | 0.09 | 0.00 | 0.00 | 0.00 |  | 70.33 |  | 0.00 |  | 70.40 |

### 3.7 Architectural Coating - 2015

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Archit. Coating | 65.99 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Off-Road | 0.41 | 2.57 | 1.90 | 0.00 |  | 0.22 | 0.22 |  | 0.22 | 0.22 | 0.00 | 281.19 |  | 0.04 |  | 281.96 |
| Total | 66.40 | 2.57 | 1.90 | 0.00 |  | 0.22 | 0.22 |  | 0.22 | 0.22 | 0.00 | 281.19 |  | 0.04 |  | 281.96 |

Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.04 | 0.03 | 0.41 | 0.00 | 0.09 | 0.00 | 0.09 | 0.00 | 0.00 | 0.00 |  | 70.33 |  | 0.00 |  | 70.40 |
| Total | 0.04 | 0.03 | 0.41 | 0.00 | 0.09 | 0.00 | 0.09 | 0.00 | 0.00 | 0.00 |  | 70.33 |  | 0.00 |  | 70.40 |

### 4.0 Mobile Detail

4.1 Mitigation Measures Mobile

|  | ROG | NOX | co | SO2 | $\begin{gathered} \text { Fugitive } \\ \text { PM10 } \end{gathered}$ | Exhaust <br> PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | Ib/day |  |  |  |  |  |
| Mitigated | 18.77 | 36.53 | 146.43 | 0.21 | 22.15 | 1.23 | 23.37 | 0.31 | 1.16 | 1.47 |  | 1,233.9 |  | 0.90 |  | 21,252.76 |
| Unmitigated | 18.77 | 36.53 | 146.43 | 0.21 | 22.15 | 1.23 | 23.37 | 0.31 | 1.16 | 1.47 |  | 1,233.9 |  | 0.90 |  | 21,252.76 |
| Total | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |

### 4.2 Trip Summary Information

|  | Average Daily Trip Rate |  |  | Unmitigated | Mitigated |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Weekday | Saturday | Sunday | Annual VMT | Annual VMT |
| Medical Office Building | 3,417.00 | 3,417.00 | 3417.00 | 6,687,923 | 6,687,923 |
| Parking Lot | 0.00 | 0.00 | 0.00 |  |  |
| Total | 3,417.00 | 3,417.00 | 3,417.00 | 6,687,923 | 6,687,923 |

### 4.3 Trip Type Information

|  | Miles |  |  | Trip \% |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | H-W or C-W | H-S or C-C | H-O or C-NW | H-W or C-W | H-S or C-C | H-O or C-NW |
| Medical Office Building | 9.50 | 7.30 | 7.30 | 29.60 | 51.40 | 19.00 |
| Parking Lot | 9.50 | 7.30 | 7.30 | 0.00 | 0.00 | 0.00 |

### 5.0 Energy Detail

5.1 Mitigation Measures Energy

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive | Exhaust PM2.5 | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | Ib/day |  |  |  |  |  |  |  |  |  | Ib/day |  |  |  |  |  |
| NaturalGas Mitigated | 0.01 | 0.07 | 0.06 | 0.00 |  | 0.00 | 0.01 |  | 0.00 | 0.01 |  | 89.84 |  | 0.00 | 0.00 | 90.38 |
| NaturalGas Unmitigated | 0.01 | 0.07 | 0.06 | 0.00 |  | 0.00 | 0.01 |  | 0.00 | 0.01 |  | 89.84 |  | 0.00 | 0.00 | 90.38 |
| Total | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |

### 5.2 Energy by Land Use - NaturaIGas

Unmitigated

|  | NaturalGas Use | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kBTU | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Medical Office Building | 763.603 | 0.01 | 0.07 | 0.06 | 0.00 |  | 0.00 | 0.01 |  | 0.00 | 0.01 |  | 89.84 |  | 0.00 | 0.00 | 90.38 |
| Parking Lot | 0 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 | 0.00 | 0.00 |
| Total |  | 0.01 | 0.07 | 0.06 | 0.00 |  | 0.00 | 0.01 |  | 0.00 | 0.01 |  | 89.84 |  | 0.00 | 0.00 | 90.38 |

### 5.2 Energy by Land Use - NaturalGas

Mitigated

|  | NaturalGas Use | ROG | NOx | co | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \hline \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kBTU | lb/day |  |  |  |  |  |  |  |  |  | Ib/day |  |  |  |  |  |
| Medical Office Building | 0.763603 | 0.01 | 0.07 | 0.06 | 0.00 |  | 0.00 | 0.01 |  | 0.00 | 0.01 |  | 89.84 |  | 0.00 | 0.00 | 90.38 |
| Parking Lot | 0 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 | 0.00 | 0.00 |
| Total |  | 0.01 | 0.07 | 0.06 | 0.00 |  | 0.00 | 0.01 |  | 0.00 | 0.01 |  | 89.84 |  | 0.00 | 0.00 | 90.38 |

### 6.0 Area Detail

### 6.1 Mitigation Measures Area

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Mitigated | 2.37 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Unmitigated | 2.37 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Total | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |

### 6.2 Area by SubCategory

## Unmitigated

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SubCategory | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Architectural Coating | 0.54 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Consumer Products | 1.83 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Landscaping | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Total | 2.37 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |

## Mitigated

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SubCategory | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Architectural Coating | 0.54 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Consumer Products | 1.83 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Landscaping | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Total | 2.37 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |

7.1 Mitigation Measures Water
8.0 Waste Detail
8.1 Mitigation Measures Waste
9.0 Vegetation

# County of Los Angeles Animal Care Center, Palmdale, CA 

## Antelope Valley APCD Air District, Winter

### 1.0 Project Characteristics

### 1.1 Land Usage

| Land Uses | Size | Metric |
| :---: | :---: | :---: |
| Medical Office Building | 25.5 | 1000sqft |
| Parking Lot | 60 | 1000sqft |

### 1.2 Other Project Characteristics

| Urbanization | Urban | Wind Speed (m/s) | $2.2 \quad$ Utility Company |
| :--- | :--- | :--- | :--- |

Climate Zone
9
Precipitation Freq (Days) 33

### 1.3 User Entered Comments

Project Characteristics -
Land Use - Site acreage is 6.02 acres per project description (includes main building, parking lots, outdoor lot areas, courtyard, loading zone, etc)
Construction Phase - Architectural coating: assumes 15 days (default is 10 days).
Trips and VMT - Demolition hauling trips assume 20 tons of material per load, 5 mile trip length to landfill (model default is 20 miles)
Demolition $-\sim 3,500$ tons of debris estimated for removal of $\sim 2$ acres of existing pavement and miscellaneous debris.
Architectural Coating - Assume average interior/exterior VOC content is $125 \mathrm{~g} / \mathrm{L}$, which is $50 \%$ of default value (default = $250 \mathrm{~g} / \mathrm{L}$ ).

Vehicle Trips - Trip rate = 134 trips/day, 7 days/week ( 30 workers, 20 volunteers, 70 visitors, 14 deliveries). This trip rate is higher than model default trip rates for weekdays, Saturdays, and Sundays.
Area Coating -
Landscape Equipment -
Construction Off-road Equipment Mitigation - Fugitive dust mitigation assumes watering exposed areas 2 times per day, with $55 \%$ PM10 reduction and 55\% PM2.5 reduction (defaults).

### 2.0 Emissions Summary

### 2.1 Overall Construction (Maximum Daily Emission)

Unmitigated Construction

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| 2014 | 5.49 | 44.57 | 27.20 | 0.05 | 12.01 | 2.39 | 14.41 | 2.90 | 2.37 | 4.37 | 0.00 | 5,475.35 | 0.00 | 0.46 | 0.00 | 5,485.07 |
| 2015 | 66.44 | 22.28 | 18.26 | 0.03 | 0.56 | 1.38 | 1.94 | 0.01 | 1.37 | 1.38 | 0.00 | 3,219.83 | 0.00 | 0.36 | 0.00 | 3,227.41 |
| Total | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |

### 2.1 Overall Construction (Maximum Daily Emission)

Mitigated Construction

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \hline \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| 2014 | 5.49 | 44.57 | 27.20 | 0.05 | 9.95 | 2.39 | 12.35 | 1.30 | 2.37 | 2.77 | 0.00 | 5,475.35 | 0.00 | 0.46 | 0.00 | 5,485.07 |
| 2015 | 66.44 | 22.28 | 18.26 | 0.03 | 0.56 | 1.38 | 1.94 | 0.01 | 1.37 | 1.38 | 0.00 | 3,219.83 | 0.00 | 0.36 | 0.00 | 3,227.41 |
| Total | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |

### 2.2 Overall Operational

Unmitigated Operational

|  | ROG | NOx | co | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | Ib/day |  |  |  |  |  |
| Area | 2.37 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Energy | 0.01 | 0.07 | 0.06 | 0.00 |  | 0.00 | 0.01 |  | 0.00 | 0.01 |  | 89.84 |  | 0.00 | 0.00 | 90.38 |
| Mobile | 16.60 | 37.68 | 133.59 | 0.18 | 22.15 | 1.25 | 23.40 | 0.31 | 1.18 | 1.50 |  | 18,635.29 |  | 0.88 |  | 18,653.83 |
| Total | 18.98 | 37.75 | 133.65 | 0.18 | 22.15 | 1.25 | 23.41 | 0.31 | 1.18 | 1.51 |  | 18,725.13 |  | 0.88 | 0.00 | 18,744.21 |

Mitigated Operational

|  | ROG | NOx | co | SO2 | Fugitive | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Area | 2.37 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Energy | 0.01 | 0.07 | 0.06 | 0.00 |  | 0.00 | 0.01 |  | 0.00 | 0.01 |  | 89.84 |  | 0.00 | 0.00 | 90.38 |
| Mobile | 16.60 | 37.68 | 133.59 | 0.18 | 22.15 | 1.25 | 23.40 | 0.31 | 1.18 | 1.50 |  | 18,635.29 |  | 0.88 |  | 18,653.83 |
| Total | 18.98 | 37.75 | 133.65 | 0.18 | 22.15 | 1.25 | 23.41 | 0.31 | 1.18 | 1.51 |  | 18,725.13 |  | 0.88 | 0.00 | 18,744.21 |

### 3.1 Mitigation Measures Construction

Water Exposed Area

### 3.2 Demolition - 2014

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 3.74 | 0.00 | 3.74 | 0.00 | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Off-Road | 4.75 | 35.99 | 22.84 | 0.04 |  | 2.08 | 2.08 |  | 2.08 | 2.08 |  | 3,946.47 |  | 0.42 |  | 3,955.39 |
| Total | 4.75 | 35.99 | 22.84 | 0.04 | 3.74 | 2.08 | 5.82 | 0.00 | 2.08 | 2.08 |  | 3,946.47 |  | 0.42 |  | 3,955.39 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.66 | 8.50 | 3.66 | 0.01 | 8.10 | 0.31 | 8.41 | 0.02 | 0.28 | 0.30 |  | 1,415.43 |  | 0.03 |  | 1,416.10 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.08 | 0.08 | 0.70 | 0.00 | 0.17 | 0.00 | 0.17 | 0.00 | 0.00 | 0.01 |  | 113.45 |  | 0.01 |  | 113.58 |
| Total | 0.74 | 8.58 | 4.36 | 0.01 | 8.27 | 0.31 | 8.58 | 0.02 | 0.28 | 0.31 |  | 1,528.88 |  | 0.04 |  | 1,529.68 |

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 1.69 | 0.00 | 1.69 | 0.00 | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Off-Road | 4.75 | 35.99 | 22.84 | 0.04 |  | 2.08 | 2.08 |  | 2.08 | 2.08 | 0.00 | 3,946.47 |  | 0.42 |  | 3,955.39 |
| Total | 4.75 | 35.99 | 22.84 | 0.04 | 1.69 | 2.08 | 3.77 | 0.00 | 2.08 | 2.08 | 0.00 | 3,946.47 |  | 0.42 |  | 3,955.39 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.66 | 8.50 | 3.66 | 0.01 | 8.10 | 0.31 | 8.41 | 0.02 | 0.28 | 0.30 |  | 1,415.43 |  | 0.03 |  | 1,416.10 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.08 | 0.08 | 0.70 | 0.00 | 0.17 | 0.00 | 0.17 | 0.00 | 0.00 | 0.01 |  | 113.45 |  | 0.01 |  | 113.58 |
| Total | 0.74 | 8.58 | 4.36 | 0.01 | 8.27 | 0.31 | 8.58 | 0.02 | 0.28 | 0.31 |  | 1,528.88 |  | 0.04 |  | 1,529.68 |

### 3.3 Site Preparation - 2014

Unmitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \mathrm{CO2} \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 5.80 | 0.00 | 5.80 | 2.90 | 0.00 | 2.90 |  |  |  |  |  | 0.00 |
| Off-Road | 3.75 | 29.67 | 17.95 | 0.03 |  | 1.47 | 1.47 |  | 1.47 | 1.47 |  | 3,253.39 |  | 0.34 |  | 3,260.45; |
| Total | 3.75 | 29.67 | 17.95 | 0.03 | 5.80 | 1.47 | 7.27 | 2.90 | 1.47 | 4.37 |  | 3,253.39 |  | 0.34 |  | 3,260.45 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.05 | 0.05 | 0.43 | 0.00 | 0.10 | 0.00 | 0.11 | 0.00 | 0.00 | 0.00 |  | 69.81 |  | 0.00 |  | 69.90 |
| Total | 0.05 | 0.05 | 0.43 | 0.00 | 0.10 | 0.00 | 0.11 | 0.00 | 0.00 | 0.00 |  | 69.81 |  | 0.00 |  | 69.90 |

### 3.3 Site Preparation - 2014

Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \mathrm{CO2} \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 2.61 | 0.00 | 2.61 | 1.30 | 0.00 | 1.30 |  |  |  |  |  | 0.00 |
| Off-Road | 3.75 | 29.67 | 17.95 | 0.03 |  | 1.47 | 1.47 |  | 1.47 | 1.47 | 0.00 | 3,253.39 |  | 0.34 |  | 3,260.45; |
| Total | 3.75 | 29.67 | 17.95 | 0.03 | 2.61 | 1.47 | 4.08 | 1.30 | 1.47 | 2.77 | 0.00 | 3,253.39 |  | 0.34 |  | 3,260.45 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{gathered} \hline \text { NBio- } \\ \text { CO2 } \end{gathered}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.05 | 0.05 | 0.43 | 0.00 | 0.10 | 0.00 | 0.11 | 0.00 | 0.00 | 0.00 |  | 69.81 |  | 0.00 |  | 69.90 |
| Total | 0.05 | 0.05 | 0.43 | 0.00 | 0.10 | 0.00 | 0.11 | 0.00 | 0.00 | 0.00 |  | 69.81 |  | 0.00 |  | 69.90 |

### 3.4 Grading - 2014

Unmitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 4.91 | 0.00 | 4.91 | 2.48 | 0.00 | 2.48 |  |  |  |  |  | 0.00 |
| Off-Road | 3.11 | 24.59 | 14.80 | 0.03 |  | 1.21 | 1.21 |  | 1.21 | 1.21 |  | 2,689.9 |  | 0.28 |  | 2,695.82 |
| Total | 3.11 | 24.59 | 14.80 | 0.03 | 4.91 | 1.21 | 6.12 | 2.48 | 1.21 | 3.69 |  | 2,689.97 |  | 0.28 |  | 2,695.82 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.05 | 0.05 | 0.43 | 0.00 | 0.10 | 0.00 | 0.11 | 0.00 | 0.00 | 0.00 |  | 69.81 |  | 0.00 |  | 69.90 |
| Total | 0.05 | 0.05 | 0.43 | 0.00 | 0.10 | 0.00 | 0.11 | 0.00 | 0.00 | 0.00 |  | 69.81 |  | 0.00 |  | 69.90 |

### 3.4 Grading - 2014

Mitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive | Exhaust PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \hline \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Fugitive Dust |  |  |  |  | 2.21 | 0.00 | 2.21 | 1.12 | 0.00 | 1.12 |  |  |  |  |  | 0.00 |
| Off-Road | 3.11 | 24.59 | 14.80 | 0.03 |  | 1.21 | 1.21 |  | 1.21 | 1.21 | 0.00 | 2,689.97 |  | 0.28 |  | 2,695.82 |
| Total | 3.11 | 24.59 | 14.80 | 0.03 | 2.21 | 1.21 | 3.42 | 1.12 | 1.21 | 2.33 | 0.00 | 2,689.97 |  | 0.28 |  | 2,695.82 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.05 | 0.05 | 0.43 | 0.00 | 0.10 | 0.00 | 0.11 | 0.00 | 0.00 | 0.00 |  | 69.81 |  | 0.00 |  | 69.90 |
| Total | 0.05 | 0.05 | 0.43 | 0.00 | 0.10 | 0.00 | 0.11 | 0.00 | 0.00 | 0.00 |  | 69.81 |  | 0.00 |  | 69.90 |

### 3.5 Building Construction - 2014

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | NBioCO 2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 4.15 | 21.74 | 15.92 | 0.03 |  | 1.46 | 1.46 |  | 1.46 | 1.46 |  | 2,561.58 |  | 0.37 |  | 2,569.39 |
| Total | 4.15 | 21.74 | 15.92 | 0.03 |  | 1.46 | 1.46 |  | 1.46 | 1.46 |  | 2,561.58 |  | 0.37 |  | 2,569.39 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.17 | 2.15 | 1.15 | 0.00 | --13 | -0.07 | --19 | 0.00 | -0.06 | 0.06 |  | -377.45 |  | 0.01 |  | -377.63 |
| Worker | 0.20 | 0.20 | 1.77 | 0.00 | 0.43 | 0.01 | 0.44 | 0.01 | 0.01 | 0.02 |  | 287.98 |  | 0.02 |  | 288.32 |
| Total | 0.37 | 2.35 | 2.92 | 0.00 | 0.56 | 0.08 | 0.63 | 0.01 | 0.07 | 0.08 |  | 665.43 |  | 0.03 |  | 665.95 |

### 3.5 Building Construction - 2014

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{gathered} \text { NBio- } \\ \mathrm{CO} 2 \end{gathered}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 4.15 | 21.74 | 15.92 | 0.03 |  | 1.46 | 1.46 |  | 1.46 | 1.46 | 0.00 | 2,561.58 | ' | 0.37 |  | 2,569.39 |
| Total | 4.15 | 21.74 | 15.92 | 0.03 |  | 1.46 | 1.46 |  | 1.46 | 1.46 | 0.00 | 2,561.58 |  | 0.37 |  | 2,569.39 |

Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.17 | 2.15 | 1.15 | 0.00 | 0.13 | -0.07 | -7.19 | 0.00 | 0.06 | 0.06 |  | 377.45 |  | 0.01 |  | 377.63 |
| Worker | 0.20 | 0.20 | 1.77 | 0.00 | 0.43 | 0.01 | 0.44 | 0.01 | 0.01 | 0.02 |  | 287.98 |  | 0.02 |  | 288.32 |
| Total | 0.37 | 2.35 | 2.92 | 0.00 | 0.56 | 0.08 | 0.63 | 0.01 | 0.07 | 0.08 |  | 665.43 |  | 0.03 |  | 665.95 |

### 3.5 Building Construction - 2015

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 3.78 | 20.14 | 15.61 | 0.03 |  | 1.31 | 1.31 |  | 1.31 | 1.31 |  | 2,561.58 |  | 0.34 |  | 2,568.69 |
| Total | 3.78 | 20.14 | 15.61 | 0.03 |  | 1.31 | 1.31 |  | 1.31 | 1.31 |  | 2,561.58 |  | 0.34 |  | 2,568.69 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.16 | 1.97 | 1.07 | 0.00 | --13 | -0.06 | --19 | 0.00 | --05 | 0.06 |  | 377.58 |  | 0.01 |  | -377.74 |
| Worker | 0.19 | 0.18 | 1.57 | 0.00 | 0.43 | 0.01 | 0.44 | 0.01 | 0.01 | 0.02 |  | 280.67 |  | 0.01 |  | 280.98 |
| Total | 0.35 | 2.15 | 2.64 | 0.00 | 0.56 | 0.07 | 0.63 | 0.01 | 0.06 | 0.08 |  | 658.25 |  | 0.02 |  | 658.72 |

### 3.5 Building Construction - 2015

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{aligned} & \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{gathered} \text { NBio- } \\ \mathrm{CO} 2 \end{gathered}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 3.78 | 20.14 | 15.61 | 0.03 |  | 1.31 | 1.31 |  | 1.31 | 1.31 | 0.00 | 2,561.58 | ' | 0.34 |  | 2,568.69 |
| Total | 3.78 | 20.14 | 15.61 | 0.03 |  | 1.31 | 1.31 |  | 1.31 | 1.31 | 0.00 | 2,561.58 |  | 0.34 |  | 2,568.69 |

Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.16 | 1.97 | 1.07 | 0.00 | --13 | -0.06 | --19 | 0.00 | --05 | 0.06 |  | 377.58 |  | 0.01 |  | -377.74 |
| Worker | 0.19 | 0.18 | 1.57 | 0.00 | 0.43 | 0.01 | 0.44 | 0.01 | 0.01 | 0.02 |  | 280.67 |  | 0.01 |  | 280.98 |
| Total | 0.35 | 2.15 | 2.64 | 0.00 | 0.56 | 0.07 | 0.63 | 0.01 | 0.06 | 0.08 |  | 658.25 |  | 0.02 |  | 658.72 |

3.6 Paving - 2015

Unmitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 2.62 | 16.38 | 11.89 | 0.02 |  | 1.34 | 1.34 |  | 1.34 | 1.34 |  | 1,712.73 |  | 0.24 |  | 1,717.66 |
| Paving | 0.36 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Total | 2.98 | 16.38 | 11.89 | 0.02 |  | 1.34 | 1.34 |  | 1.34 | 1.34 |  | 1,712.73 |  | 0.24 |  | 1,717.66 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.07 | 0.07 | 0.62 | 0.00 | 0.17 | 0.00 | 0.17 | 0.00 | 0.00 | 0.01 |  | 110.57 |  | 0.01 |  | 110.69 |
| Total | 0.07 | 0.07 | 0.62 | 0.00 | 0.17 | 0.00 | 0.17 | 0.00 | 0.00 | 0.01 |  | 110.57 |  | 0.01 |  | 110.69 |

3.6 Paving - 2015

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 <br> Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH 4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Off-Road | 2.62 | 16.38 | 11.89 | 0.02 |  | 1.34 | 1.34 |  | 1.34 | 1.34 | 0.00 | 1,712.73 |  | 0.24 |  | 1,717.66 |
| Paving | 0.36 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Total | 2.98 | 16.38 | 11.89 | 0.02 |  | 1.34 | 1.34 |  | 1.34 | 1.34 | 0.00 | 1,712.73 |  | 0.24 |  | 1,717.66 |

## Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \hline \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.07 | 0.07 | 0.62 | 0.00 | 0.17 | 0.00 | 0.17 | 0.00 | 0.00 | 0.01 |  | 110.57 |  | 0.01 |  | 110.69 |
| Total | 0.07 | 0.07 | 0.62 | 0.00 | 0.17 | 0.00 | 0.17 | 0.00 | 0.00 | 0.01 |  | 110.57 |  | 0.01 |  | 110.69 |

### 3.7 Architectural Coating - 2015

Unmitigated Construction On-Site

|  | ROG | NOx | co | SO2 | Fugitive | Exhaust PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \hline \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio-CO2 | $\begin{gathered} \text { NBio- } \\ \text { CO2 } \end{gathered}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Archit. Coating | 65.99 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Off-Road | 0.41 | 2.57 | 1.90 | 0.00 |  | 0.22 | 0.22 |  | 0.22 | 0.22 |  | 281.19 |  | 0.04 |  | 281.96 |
| Total | 66.40 | 2.57 | 1.90 | 0.00 |  | 0.22 | 0.22 |  | 0.22 | 0.22 |  | 281.19 |  | 0.04 |  | 281.96 |

Unmitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | $\begin{gathered} \text { PM10 } \\ \text { Total } \end{gathered}$ | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.04 | 0.04 | 0.33 | 0.00 | 0.09 | 0.00 | 0.09 | 0.00 | 0.00 | 0.00 |  | 59.54 |  | 0.00 |  | 59.60 |
| Total | 0.04 | 0.04 | 0.33 | 0.00 | 0.09 | 0.00 | 0.09 | 0.00 | 0.00 | 0.00 |  | 59.54 |  | 0.00 |  | 59.60 |

### 3.7 Architectural Coating - 2015

Mitigated Construction On-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Archit. Coating | 65.99 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Off-Road | 0.41 | 2.57 | 1.90 | 0.00 |  | 0.22 | 0.22 |  | 0.22 | 0.22 | 0.00 | 281.19 |  | 0.04 |  | 281.96 |
| Total | 66.40 | 2.57 | 1.90 | 0.00 |  | 0.22 | 0.22 |  | 0.22 | 0.22 | 0.00 | 281.19 |  | 0.04 |  | 281.96 |

Mitigated Construction Off-Site

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Hauling | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Vendor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Worker | 0.04 | 0.04 | 0.33 | 0.00 | 0.09 | 0.00 | 0.09 | 0.00 | 0.00 | 0.00 |  | 59.54 |  | 0.00 |  | 59.60 |
| Total | 0.04 | 0.04 | 0.33 | 0.00 | 0.09 | 0.00 | 0.09 | 0.00 | 0.00 | 0.00 |  | 59.54 |  | 0.00 |  | 59.60 |

### 4.0 Mobile Detail

4.1 Mitigation Measures Mobile

|  | ROG | NOX | co | SO2 | $\begin{gathered} \text { Fugitive } \\ \text { PM10 } \end{gathered}$ | Exhaust <br> PM10 | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | 1b/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Mitigated | 16.60 | 37.68 | 133.59 | 0.18 | 22.15 | 1.25 | 23.40 | 0.31 | 1.18 | 1.50 |  | 18,635.2 |  | 0.88 |  | 8,653.83 |
| Unmitigated | 16.60 | 37.68 | 133.59 | 0.18 | 22.15 | 1.25 | 23.40 | 0.31 | 1.18 | 1.50 |  | 18,635.2 |  | 0.88 |  | 8,653.83 |
| Total | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |

### 4.2 Trip Summary Information

|  | Average Daily Trip Rate |  |  | Unmitigated | Mitigated |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Weekday | Saturday | Sunday | Annual VMT | Annual VMT |
| Medical Office Building | 3,417.00 | 3,417.00 | 3417.00 | 6,687,923 | 6,687,923 |
| Parking Lot | 0.00 | 0.00 | 0.00 |  |  |
| Total | 3,417.00 | 3,417.00 | 3,417.00 | 6,687,923 | 6,687,923 |

### 4.3 Trip Type Information

|  | Miles |  |  | Trip \% |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | H-W or C-W | $\mathrm{H}-\mathrm{S}$ or $\mathrm{C}-\mathrm{C}$ | H-O or C-NW | H-W or C-W | H-S or C-C | H-O or C-NW |
| Medical Office Building | 9.50 | 7.30 | 7.30 | 29.60 | 51.40 | 19.00 |
| Parking Lot | 9.50 | 7.30 | 7.30 | 0.00 | 0.00 | 0.00 |

### 5.0 Energy Detail

5.1 Mitigation Measures Energy

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive | Exhaust PM2.5 | $\begin{aligned} & \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | Ib/day |  |  |  |  |  |  |  |  |  | Ib/day |  |  |  |  |  |
| NaturalGas Mitigated | 0.01 | 0.07 | 0.06 | 0.00 |  | 0.00 | 0.01 |  | 0.00 | 0.01 |  | 89.84 |  | 0.00 | 0.00 | 90.38 |
| NaturalGas Unmitigated | 0.01 | 0.07 | 0.06 | 0.00 |  | 0.00 | 0.01 |  | 0.00 | 0.01 |  | 89.84 |  | 0.00 | 0.00 | 90.38 |
| Total | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |

### 5.2 Energy by Land Use - NaturaIGas

Unmitigated

|  | NaturalGas Use | ROG | NOx | CO | SO2 | Fugitive PM10 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM10 } \end{aligned}$ | PM10 Total | Fugitive PM2.5 | $\begin{aligned} & \text { Exhaust } \\ & \text { PM2.5 } \end{aligned}$ | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kBTU | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Medical Office Building | 763.603 | 0.01 | 0.07 | 0.06 | 0.00 |  | 0.00 | 0.01 |  | 0.00 | 0.01 |  | 89.84 |  | 0.00 | 0.00 | 90.38 |
| Parking Lot | 0 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 | 0.00 | 0.00 |
| Total |  | 0.01 | 0.07 | 0.06 | 0.00 |  | 0.00 | 0.01 |  | 0.00 | 0.01 |  | 89.84 |  | 0.00 | 0.00 | 90.38 |

### 5.2 Energy by Land Use - NaturalGas

Mitigated

|  | NaturalGas Use | ROG | NOx | co | SO2 | Fugitive PM10 | $\begin{gathered} \text { Exhaust } \\ \text { PM10 } \end{gathered}$ | $\begin{aligned} & \hline \text { PM10 } \\ & \text { Total } \end{aligned}$ | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{aligned} & \hline \text { PM2.5 } \\ & \text { Total } \end{aligned}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | kBTU | lb/day |  |  |  |  |  |  |  |  |  | Ib/day |  |  |  |  |  |
| Medical Office Building | 0.763603 | 0.01 | 0.07 | 0.06 | 0.00 |  | 0.00 | 0.01 |  | 0.00 | 0.01 |  | 89.84 |  | 0.00 | 0.00 | 90.38 |
| Parking Lot | 0 | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 | 0.00 | 0.00 |
| Total |  | 0.01 | 0.07 | 0.06 | 0.00 |  | 0.00 | 0.01 |  | 0.00 | 0.01 |  | 89.84 |  | 0.00 | 0.00 | 90.38 |

### 6.0 Area Detail

### 6.1 Mitigation Measures Area

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Category | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Mitigated | 2.37 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Unmitigated | 2.37 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Total | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |

### 6.2 Area by SubCategory

## Unmitigated

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 <br> Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SubCategory | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Architectural Coating | 0.54 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Consumer Products | 1.83 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Landscaping | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Total | 2.37 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |

## Mitigated

|  | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | $\begin{gathered} \text { PM2.5 } \\ \text { Total } \end{gathered}$ | Bio- CO2 | $\begin{aligned} & \text { NBio- } \\ & \text { CO2 } \end{aligned}$ | Total CO2 | CH4 | N2O | CO2e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SubCategory | lb/day |  |  |  |  |  |  |  |  |  | lb/day |  |  |  |  |  |
| Architectural Coating | 0.54 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Consumer Products | 1.83 |  |  |  |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  |  |  |  |  | 0.00 |
| Landscaping | 0.00 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |
| Total | 2.37 | 0.00 | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 | 0.00 |  | 0.00 |  | 0.00 |  | 0.00 |

7.1 Mitigation Measures Water
8.0 Waste Detail
8.1 Mitigation Measures Waste
9.0 Vegetation

# Appendix B <br> Noise Worksheets 

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County of Los Angeles Animal Care Center, Palmdale, CA
Initial Study

## Construction Noise

## Construction Schedule

Mon-Fri
8 -hours per day between 7am and 5pm
3/20/2014-3/6/2015
Phases do not overlap

| Phase | Equipment Description | Usage Factor | Equipment <br> Lmax @ 50' | Equipment <br> Leq @ 50' | Number of Equipment | Add to Single Source Level (dBA) | Total Lmax <br> @ 50' | Total Leq <br> @ 50' |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Debris Removal | Concrete/Industrial Saws | 20\% | 90 | 83 | 1 | 0 | 90 | 83 |
|  | Rubber Tired Dozers | 40\% | 85 | 81 | 1 | 0 | 85 | 81 |
|  | Tractors/Loaders/Backhoes | 40\% | 80 | 76 | 3 | 5 | 85 | 81 |
| Debris Removal Total |  |  |  |  |  |  | 92 | 86 |
| Site Preparation | Graders | 40\% | 85 | 81 | 1 | 0 | 85 | 81 |
|  | Rubber Tired Dozers | 40\% | 85 | 81 | 1 | 0 | 85 | 81 |
|  | Tractors/Loaders/Backhoes | 40\% | 80 | 76 | 1 | 0 | 80 | 76 |
| Site Preparation Total |  |  |  |  |  |  | 89 | 85 |
| Grading | Graders | 40\% | 85 | 81 | 1 | 0 | 85 | 81 |
|  | Rubber Tired Dozers | 40\% | 85 | 81 | 1 | 0 | 85 | 81 |
|  | Tractors/Loaders/Backhoes | 40\% | 80 | 76 | 1 | 0 | 80 | 76 |
| Grading Total |  |  |  |  |  |  | 89 | 85 |
| Building Construction | Cranes | 16\% | 85 | 77 | 1 | 0 | 85 | 77 |
|  | Forklifts | 20\% | 85 | 78 | 1 | 0 | 85 | 78 |
|  | Generator Sets | 50\% | 82 | 79 | 1 | 0 | 82 | 79 |
|  | Tractors/Loaders/Backhoes | 40\% | 80 | 76 | 1 | 0 | 80 | 76 |
|  | Welders | 40\% | 73 | 69 | 3 | 5 | 78 | 74 |
| Building Construction Total |  |  |  |  |  |  | 90 | 84 |
| Paving | Cement and Mortar Mixers | 20\% | 80 | 73 | 1 | 0 | 80 | 73 |
|  | Pavers | 50\% | 85 | 82 | 1 | 0 | 85 | 82 |
|  | Paving Equipment | 50\% | 85 | 82 | 1 | 0 | 85 | 82 |
|  | Rollers | 20\% | 85 | 78 | 1 | 0 | 85 | 78 |
|  | Tractors/Loaders/Backhoes | 40\% | 80 | 76 | 1 | 0 | 80 | 76 |
| Paving Total |  |  |  |  |  |  | 91 | 86 |
| Architectural Coating | Air Compressors | 40\% | 80 | 76 | 1 | 0 | 80 | 76 |

Assume all equipment operates at the same time during each phase.
Calculations based on FHWA. 2006. Roadway Construction Noise Model. January.

## County of Los Angeles Animal Care Center, Palmdale, CA

## Initial Study

## Construction Noise

| Impacts to Residential_Area on Friendly Avenue |  |  | Google Earth |
| :---: | :---: | :---: | :---: |
| Distance from the Center of the Construction Area (ft) |  | 200 |  |
| Maximum Construction Noise Level @ 50 ft (dBA) |  | 86 |  |
| Distance Divergence (dBA) |  | 12.0 |  |
| Atmospheric_Attenuation (dBA) |  | 0.08 |  |
| Construction Noise Levelat the_Receptor (dBA) 74 |  |  |  |
| Hour | Background w/ CNEL penalty | Construction | Total |
|  | (dBA) | (dBA) | (dBA) |
| $0 \cdot 00$ | 60 | 0 | 60 |
| 1:00 | 60 | 0 | 60 |
| 2:00 | 60 | 0 | 60 |
| 3:00 | 60 | 0 | 60 |
| 4:00 | 60 | 0 | 60 |
| 5:00 | 60 | 0 | 60 |
| 6:00 | 60 | 0 | 60 |
| 7:00 | 60 | 74 | 75 |
| 8:00 | 60 | 74 | 75 |
| 9:00 | 60 | 74 | 75 |
| 10:00 | 60 | 74 | 75 |
| 11:00 | 60 | 0 | 60 |
| 12:00 | 60 | 0 | 60 |
| 13:00 | 60 | 74 | 75 |
| 14:00 | 60 | 74 | 75 |
| 15:00 | 60 | 74 | 75 |
| 16:00 | 60 | 74 | 75 |
| 17:00 | 60 | 0 | 60 |
| 18:00 | 60 | 0 | 60 |
| 19:00 | 60 | 0 | 60 |
| 20:00 | 60 | 0 | 60 |
| 21:00 | 60 | 0 | 60 |
| 22:00 | 60 | 0 | 60 |
| 23:00 | 60 | 0 | 60 |
|  |  | CNEL | 70 |
|  |  | rease in CNEL | 10 |

## County of Los Angeles Animal Care Center, Palmdale, CA Initial Study <br> Construction Noise

## Construction Vehicles

9 haul trips (heavy trucks)
3 vendor trips (medium trucks)
33 construction workers (auto)
Equivalent Vehicle ( 55 mph )
4.1 auto per medium truck
10.4 auto per heavy truck

Speed limit on Sierra Highway obtained from Google Maps Street View
Caltrans. 2009. Technical Supplement to the Noise Protocol.
Total Equivalent Vehicles per Hour
139 per hour (assuming all operating at the same time)

Sierra Highway ADT
Estimated peak traffic

17,000
1,700 Assumes $10 \%$ of ADT is peak hour traffic.

Doubling of the noise source produces only a 3 dB increase, which is barely perceptible by the human ear.
No audible change in traffic noise as traffic will not double as a result of this project
FHWA. 2011. Highway Traffic Noise: Analysis and Abatement Guidance.

## County of Los Angeles Animal Care Center, Palmdale, CA

Initial Study
Construction Vibration

|  |  |  |
| :--- | :---: | :---: |
| Distance (ft) | 25 | 200 |
| PPV (in/sec) |  |  |
| Large Bulldozer |  | 0.089 |
| Vibratory Roller |  | 0.21 |

FTA. 2006. Transit Noise and Vibration Impact Assessment.

## County of Los Angeles Animal Care Center Project <br> Initial Study <br> Operational Noise

Settings
660 ft from metrolink/Union Pacific railroad
2.5 mi NE $=$ Air Force Plant 42

400 ft from Sierra Highway
17,000 ADT

## Operations - Animal Noise

Monday-Thursday noon-19:00; Friday-Saturday 10-17:00
Peak shelter animal population 128 dogs
229 cats
"Get Acquainted Yard" is surrounded by buildings and has minimal noise impact.
Exercise Yard is approximately 233 ft from residences on Friendly Ave.
There is a 8 ft wall at the property boundary, along residences.
Exercise yard will be used during hours that are open to the public (i.e. no nighttime noise).
Instantaneous (dBA)
1 dog barking @ 55' 72
Number of dogs barking 20
Multiple dogs barking @ 55' 85
Multiple dogs barking @ 233' 73
$\begin{array}{ll}\text { Noise reduction by wall } & -3 \\ \text { Noise level with wall } & 70\end{array}$

1-hour Leq (dBA)
1 dog barking @ 55' 60
Number of dogs barking 128
Multiple dogs barking @ 55' 81
Multiple dogs barking @ 233' 69
Barking + existing @ 233' 69

Noise reduction by wall -3
Noise level with wall 66

| Hour | Background w/ <br> CNEL penalty <br> (dBA) | Operation <br> (dBA) | Total <br> (dBA) |
| :---: | :---: | :---: | :---: |
| $0: 00$ | 60 | 0 | 60 |
| $1: 00$ | 60 | 0 | 60 |
| $2: 00$ | 60 | 0 | 60 |
| $3: 00$ | 60 | 0 | 60 |
| $4: 00$ | 60 | 0 | 60 |
| $5: 00$ | 60 | 0 | 60 |
| $6: 00$ | 60 | 0 | 60 |
| $7: 00$ | 60 | 0 | 60 |
| $8: 00$ | 60 | 0 | 60 |
| $9: 00$ | 60 | 0 | 60 |
| $10: 00$ | 60 | 0 | 60 |
| $11: 00$ | 60 | 0 | 60 |
| $12: 00$ | 60 | 66 | 67 |
| $13: 00$ | 60 | 66 | 67 |
| $14: 00$ | 60 | 66 | 67 |
| $15: 00$ | 60 | 66 | 67 |
| $16: 00$ | 60 | 66 | 67 |
| $17: 00$ | 60 | 66 | 67 |
| $18: 00$ | 60 | 66 | 67 |
| $19: 00$ | 60 | 0 | 60 |
| $20: 00$ | 60 | 0 | 60 |
| $21: 00$ | 60 | 0 | 60 |
| $22: 00$ | 60 | 0 | 60 |
| $23: 00$ | 60 | 0 | 60 |
|  |  | CNEL | 63 |
|  |  | 3 |  |

## Reference:

Measurement of 1 dog barking at 55' from Sound Solutions. Noise Impacts and Mitigation in Connection with the Proposed Meadows Kennel, 6445 Highway 12, Sonoma County, California. August 2011

## County of Los Angeles Animal Care Center, Palmdale, CA Initial Study

 Operational NoiseOperations - Traffic Noise
30 full time, 20 part time, 70 visitors
120 auto
3 vendor trips per day
3 medium trucks
Equivalent Vehicle (55 mph)
4.1 auto per medium truck

Speed limit on Sierra Highway obtained from Google Maps Street View
Caltrans. 2009. Technical Supplement to the Noise Protocol.
Total Equivalent Vehicles per Hour
132 per hour (assuming all operating at the same time)
Sierra Highway ADT 17,000
Estimated peak traffic 1,700 Assumes $10 \%$ of ADT is peak hour traffic.

Doubling of the noise source produces only a 3 dB increase, which is barely perceptible by the human ear. No audible change in traffic noise as traffic will not double as a result of this project FHWA. 2011. Highway Traffic Noise: Analysis and Abatement Guidance.

Noise contours in the general plan noise element show that the project area falls below the 60 dB contour line from transportation noise. The project site is within the low altitude overflight area.

Appendix C
Los Angeles County LID Volume Calculator

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Hydrograph





[^12]| Soil Type: |  |  |  |  | soil type: | 2 | I : | 0.1 | C: | 0.100 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | C | 0.00 | I |  |  |  |  |  |  |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.12 | 0.10 | 0.37 | 0.12 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.23 | 0.37 | 0.52 | 0.23 |  |  |  |  |  |  | 0.12 | 0.1 |
|  | 0.4 | 0.52 | 0.69 | 0.4 |  |  |  |  |  |  |  |  |
|  | 0.8 | 0.69 | 0.78 | 0.8 |  |  |  |  |  |  |  |  |
|  | 1.3 | 0.78 | 0.84 | 1.3 |  |  |  |  |  |  |  |  |
|  | 2 | 0.84 | 0.88 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.88 | 0.91 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.91 | 0.94 | 4 |  |  |  |  |  |  |  |  |
|  | 7 | 0.94 | 0.96 | 7 |  |  |  |  |  |  |  |  |
|  | 13 | 0.96 | 0.97 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0.97 | 0.97 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0.97 | 0.98 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.98 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 3 | I | C | 0.00 | I | soil type: | 3 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.86 | 0.10 | 0.20 | 0.86 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.3 | 0.20 | 0.28 | 1.3 |  |  |  |  |  |  | 0.86 | 0.1 |
|  | 1.7 | 0.28 | 0.40 | 1.7 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.40 | 0.50 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.50 | 0.58 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.58 | 0.63 | 4.5 |  |  |  |  |  |  |  |  |
|  | 5.5 | 0.63 | 0.69 | 5.5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.69 | 0.74 | 7 |  |  |  |  |  |  |  |  |
|  | 9 | 0.74 | 0.76 | 9 |  |  |  |  |  |  |  |  |
|  | 10 | 0.76 | 0.81 | 10 |  |  |  |  |  |  |  |  |
|  | 13.75 | 0.81 | 0.85 | 13.75 |  |  |  |  |  |  |  |  |
|  | 20 | 0.85 | 0.87 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.87 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 4 | 1 | C | 0.00 | I | soil type: | 4 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.44 | 0.10 | 0.21 | 0.44 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.21 | 0.40 | 0.5 |  |  |  |  |  |  | 0.44 | 0.1 |
|  | 0.75 | 0.40 | 0.49 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1 | 0.49 | 0.60 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.60 | 0.67 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.67 | 0.71 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.71 | 0.76 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.76 | 0.80 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.80 | 0.84 | 5 |  |  |  |  |  |  |  |  |
|  | 8 | 0.84 | 0.86 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.86 | 0.89 | 10 |  |  |  |  |  |  |  |  |
|  | 20 | 0.89 | 0.89 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.89 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 5 | I | C | 0.00 | I | soil type: | 5 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.5 | 0.10 | 0.35 | 0.5 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.35 | 0.46 | 0.75 |  |  |  |  |  |  | 0.5 | 0.1 |
|  | 1 | 0.46 | 0.59 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.59 | 0.67 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.67 | 0.73 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.73 | 0.80 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.80 | 0.86 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.86 | 0.91 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.91 | 0.95 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.95 | 0.98 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.98 | 0.99 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 6 | I | C | 0.00 | I | soil type: | 6 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |


|  | 0.37 | 0.10 | 0.32 | 0.37 |  |  |  |  |  |  | Upper I | Upper C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.5 | 0.32 | 0.50 | 0.5 |  |  |  |  |  |  | 0.37 | 0.1 |
|  | 0.75 | 0.50 | 0.59 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1 | 0.59 | 0.68 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.68 | 0.79 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.79 | 0.86 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.86 | 0.91 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.91 | 0.95 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.95 | 0.97 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.97 | 0.98 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.98 | 0.99 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 0.99 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.99 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 7 | I | C | 0.00 | I | soil type: | 7 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.73 | 0.10 | 0.27 | 0.73 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.27 | 0.44 | 1 |  |  |  |  |  |  | 0.73 | 0.1 |
|  | 1.5 | 0.44 | 0.54 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.54 | 0.61 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.61 | 0.66 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.66 | 0.75 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.75 | 0.80 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.80 | 0.87 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.87 | 0.92 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.92 | 0.95 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.95 | 0.96 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.96 | 0.97 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.97 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 8 | I | C | 0.00 | I | soil type: | 8 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.2 | 0.10 | 0.44 | 0.2 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.3 | 0.44 | 0.63 | 0.3 |  |  |  |  |  |  | 0.2 | 0.1 |
|  | 0.5 | 0.63 | 0.76 | 0.5 |  |  |  |  |  |  |  |  |
|  | 0.8 | 0.76 | 0.80 | 0.8 |  |  |  |  |  |  |  |  |
|  | 1 | 0.80 | 0.87 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.87 | 0.90 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.90 | 0.93 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.93 | 0.95 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.95 | 0.96 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.96 | 0.99 | 5 |  |  |  |  |  |  |  |  |
|  | 10 | 0.99 | 1.00 | 10 |  |  |  |  |  |  |  |  |
|  | 20 | 1.00 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 9 | I | C | 0.00 | I | soil type: | 9 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.3 | 0.10 | 0.27 | 0.3 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.27 | 0.43 | 0.5 |  |  |  |  |  |  | 0.3 | 0.1 |
|  | 0.8 | 0.43 | 0.61 | 0.8 |  |  |  |  |  |  |  |  |
|  | 1.25 | 0.61 | 0.73 | 1.25 |  |  |  |  |  |  |  |  |
|  | 1.75 | 0.73 | 0.84 | 1.75 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.84 | 0.88 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.88 | 0.93 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.93 | 0.97 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.97 | 0.99 | 6 |  |  |  |  |  |  |  |  |
|  | 10 | 0.99 | 0.99 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.99 | 1.00 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 1.00 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 10 | I | C | 0.00 | I | soil type: | 10 | l : | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.82 | 0.10 | 0.29 | 0.82 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.5 | 0.29 | 0.48 | 1.5 |  |  |  |  |  |  | 0.82 | 0.1 |
|  | 2.5 | 0.48 | 0.62 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.62 | 0.71 | 3.5 |  |  |  |  |  |  |  |  |


|  | 4.5 | 0.71 | 0.78 | 4.5 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 5.5 | 0.78 | 0.83 | 5.5 |  |  |  |  |  |  |  |  |
|  | 6.5 | 0.83 | 0.86 | 6.5 |  |  |  |  |  |  |  |  |
|  | 7.5 | 0.86 | 0.90 | 7.5 |  |  |  |  |  |  |  |  |
|  | 9 | 0.90 | 0.94 | 9 |  |  |  |  |  |  |  |  |
|  | 12 | 0.94 | 0.96 | 12 |  |  |  |  |  |  |  |  |
|  | 15 | 0.96 | 0.97 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.97 | 0.98 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.98 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 11 | 1 | C | 0.00 | 1 | soil type: | 11 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.25 | 0.10 | 0.39 | 0.25 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.39 | 0.51 | 0.5 |  |  |  |  |  |  | 0.25 | 0.1 |
|  | 0.75 | 0.51 | 0.59 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1 | 0.59 | 0.68 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.68 | 0.73 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.73 | 0.80 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.80 | 0.83 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.83 | 0.87 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.87 | 0.89 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.89 | 0.93 | 8 |  |  |  |  |  |  |  |  |
|  | 15 | 0.93 | 0.94 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.94 | 0.94 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.94 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 12 | I | C | 0.00 | I | soil type: | 12 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.2 | 0.10 | 0.57 | 0.2 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.25 | 0.57 | 0.74 | 0.25 |  |  |  |  |  |  | 0.2 | 0.1 |
|  | 0.5 | 0.74 | 0.80 | 0.5 |  |  |  |  |  |  |  |  |
|  | 0.75 | 0.80 | 0.84 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1 | 0.84 | 0.89 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.89 | 0.92 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.92 | 0.96 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.96 | 0.98 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.98 | 0.99 | 4 |  |  |  |  |  |  |  |  |
|  | 7 | 0.99 | 0.99 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.99 | 0.99 | 10 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 0.99 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.99 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 13 | 1 | C | 0.00 | 1 | soil type: | 13 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.6 | 0.10 | 0.32 | 0.6 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.32 | 0.46 | 0.75 |  |  |  |  |  |  | 0.6 | 0.1 |
|  | 1 | 0.46 | 0.70 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.70 | 0.83 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.83 | 0.89 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.89 | 0.93 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.93 | 0.95 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.95 | 0.98 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.98 | 0.99 | 5 |  |  |  |  |  |  |  |  |
|  | 8 | 0.99 | 0.99 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.99 | 0.99 | 10 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 14 | I | C | 0.00 | 1 | soil type: | 14 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.9 | 0.10 | 0.25 | 0.9 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.25 | 0.51 | 1 |  |  |  |  |  |  | 0.9 | 0.1 |
|  | 1.5 | 0.51 | 0.63 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.63 | 0.70 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.70 | 0.78 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.78 | 0.83 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.83 | 0.87 | 4.5 |  |  |  |  |  |  |  |  |
|  | 5.5 | 0.87 | 0.90 | 5.5 |  |  |  |  |  |  |  |  |


|  | 7 | 0.90 | 0.94 | 7 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 0.94 | 0.97 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.97 | 0.98 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.98 | 0.99 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.99 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 15 | 1 | C | 0.00 | 1 | soil type: | 15 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1.02 | 0.10 | 0.22 | 1.02 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.5 | 0.22 | 0.29 | 1.5 |  |  |  |  |  |  | 1.02 | 0.1 |
|  | 2 | 0.29 | 0.41 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.41 | 0.51 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.51 | 0.58 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.58 | 0.67 | 5 |  |  |  |  |  |  |  |  |
|  | 6.5 | 0.67 | 0.76 | 6.5 |  |  |  |  |  |  |  |  |
|  | 8.5 | 0.76 | 0.82 | 8.5 |  |  |  |  |  |  |  |  |
|  | 10.5 | 0.82 | 0.88 | 10.5 |  |  |  |  |  |  |  |  |
|  | 13 | 0.88 | 0.93 | 13 |  |  |  |  |  |  |  |  |
|  | 16 | 0.93 | 0.98 | 16 |  |  |  |  |  |  |  |  |
|  | 20 | 0.98 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 16 |  | C | 0.00 | I | soil type: | 16 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.4 | 0.10 | 0.42 | 0.4 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.42 | 0.54 | 0.75 |  |  |  |  |  |  | 0.4 | 0.1 |
|  | 1 | 0.54 | 0.68 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.68 | 0.76 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.76 | 0.81 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.81 | 0.85 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.85 | 0.90 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.90 | 0.93 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.93 | 0.96 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.96 | 0.98 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.98 | 1.00 | 10 |  |  |  |  |  |  |  |  |
|  | 20 | 1.00 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 17 | 1 | C | 0.00 | 1 | soil type: | 17 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.3 | 0.10 | 0.46 | 0.3 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.46 | 0.62 | 0.5 |  |  |  |  |  |  | 0.3 | 0.1 |
|  | 0.75 | 0.62 | 0.70 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1 | 0.70 | 0.79 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.79 | 0.84 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.84 | 0.87 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.87 | 0.91 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.91 | 0.94 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.94 | 0.96 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.96 | 0.98 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.98 | 1.00 | 10 |  |  |  |  |  |  |  |  |
|  | 20 | 1.00 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 18 | 1 | C | 0.00 | 1 | soil type: | 18 | I : | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 2.8 | 0.10 | 0.14 | 2.8 |  |  |  |  |  |  | Upper I | Upper C |
|  | 3 | 0.14 | 0.30 | 3 |  |  |  |  |  |  | 2.8 | 0.1 |
|  | 4 | 0.30 | 0.41 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.41 | 0.49 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.49 | 0.55 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.55 | 0.61 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.61 | 0.65 | 8 |  |  |  |  |  |  |  |  |
|  | 9 | 0.65 | 0.73 | 9 |  |  |  |  |  |  |  |  |
|  | 11.5 | 0.73 | 0.78 | 11.5 |  |  |  |  |  |  |  |  |
|  | 14 | 0.78 | 0.81 | 14 |  |  |  |  |  |  |  |  |
|  | 16 | 0.81 | 0.84 | 16 |  |  |  |  |  |  |  |  |
|  | 20 | 0.84 | 0.88 | 20 |  |  |  |  |  |  |  |  |


|  | 25 | 0.88 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 19 | 1 | C | 0.00 | 1 | soil type: | 19 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1 | 0.10 | 0.37 | 1 |  |  |  |  |  |  | Upper I | Upper C |
|  | 2.5 | 0.37 | 0.57 | 2.5 |  |  |  |  |  |  | 1 | 0.1 |
|  | 4 | 0.57 | 0.66 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.66 | 0.72 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.72 | 0.76 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.76 | 0.79 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.79 | 0.81 | 8 |  |  |  |  |  |  |  |  |
|  | 9 | 0.81 | 0.82 | 9 |  |  |  |  |  |  |  |  |
|  | 10 | 0.82 | 0.84 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.84 | 0.86 | 12 |  |  |  |  |  |  |  |  |
|  | 14 | 0.86 | 0.90 | 14 |  |  |  |  |  |  |  |  |
|  | 20 | 0.90 | 0.91 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.91 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 20 | I | C | 0.00 | I | soil type: | 20 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.3 | 0.10 | 0.19 | 0.3 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.19 | 0.35 | 0.5 |  |  |  |  |  |  | 0.3 | 0.1 |
|  | 1 | 0.35 | 0.45 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.45 | 0.52 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.52 | 0.61 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.61 | 0.66 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.66 | 0.73 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.73 | 0.76 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.76 | 0.78 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.78 | 0.82 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.82 | 0.83 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.83 | 0.84 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.84 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 21 | I | C | 0.00 | I | soil type: | 21 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.75 | 0.10 | 0.17 | 0.75 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.17 | 0.29 | 1 |  |  |  |  |  |  | 0.75 | 0.1 |
|  | 1.5 | 0.29 | 0.38 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.38 | 0.51 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.51 | 0.59 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.59 | 0.66 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.66 | 0.70 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.70 | 0.76 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.76 | 0.82 | 8 |  |  |  |  |  |  |  |  |
|  | 11 | 0.82 | 0.86 | 11 |  |  |  |  |  |  |  |  |
|  | 15 | 0.86 | 0.89 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.89 | 0.91 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.91 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 22 | I | C | 0.00 | I | soil type: | 22 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.4 | 0.10 | 0.37 | 0.4 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.37 | 0.45 | 0.75 |  |  |  |  |  |  | 0.4 | 0.1 |
|  | 1 | 0.45 | 0.55 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.55 | 0.62 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.62 | 0.66 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.66 | 0.70 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.70 | 0.74 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.74 | 0.79 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.79 | 0.82 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.82 | 0.85 | 8 |  |  |  |  |  |  |  |  |
|  | 12 | 0.85 | 0.88 | 12 |  |  |  |  |  |  |  |  |
|  | 20 | 0.88 | 0.89 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.89 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 23 | I | C | 0.00 | 1 | soil type: | 23 | l | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |


|  | 0.4 | 0.10 | 0.30 | 0.4 |  |  |  |  |  |  | Upper I | Upper C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.75 | 0.30 | 0.40 | 0.75 |  |  |  |  |  |  | 0.4 | 0.1 |
|  | 1 | 0.40 | 0.53 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.53 | 0.62 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.62 | 0.68 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.68 | 0.72 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.72 | 0.78 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.78 | 0.84 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.84 | 0.88 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.88 | 0.91 | 8 |  |  |  |  |  |  |  |  |
|  | 12 | 0.91 | 0.94 | 12 |  |  |  |  |  |  |  |  |
|  | 20 | 0.94 | 0.95 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.95 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 24 | I | C | 0.00 | I | soil type: | 24 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1.4 | 0.10 | 0.17 | 1.4 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.7 | 0.17 | 0.22 | 1.7 |  |  |  |  |  |  | 1.4 | 0.1 |
|  | 1.9 | 0.22 | 0.29 | 1.9 |  |  |  |  |  |  |  |  |
|  | 2.2 | 0.29 | 0.35 | 2.2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.35 | 0.43 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.43 | 0.51 | 3 |  |  |  |  |  |  |  |  |
|  | 3.9 | 0.51 | 0.58 | 3.9 |  |  |  |  |  |  |  |  |
|  | 5 | 0.58 | 0.64 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.64 | 0.69 | 7 |  |  |  |  |  |  |  |  |
|  | 9.8 | 0.69 | 0.72 | 9.8 |  |  |  |  |  |  |  |  |
|  | 13.75 | 0.72 | 0.75 | 13.75 |  |  |  |  |  |  |  |  |
|  | 20 | 0.75 | 0.76 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.76 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 25 | 1 | C | 0.00 | 1 | soil type: | 25 |  | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.17 | 0.10 | 0.19 | 0.17 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.18 | 0.19 | 0.54 | 0.18 |  |  |  |  |  |  | 0.17 | 0.1 |
|  | 0.3 | 0.54 | 0.62 | 0.3 |  |  |  |  |  |  |  |  |
|  | 0.6 | 0.62 | 0.67 | 0.6 |  |  |  |  |  |  |  |  |
|  | 1 | 0.67 | 0.74 | 1 |  |  |  |  |  |  |  |  |
|  | 2 | 0.74 | 0.80 | 2 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.80 | 0.86 | 3.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.86 | 0.90 | 6 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0.90 | 0.93 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0.93 | 0.95 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0.95 | 0.95 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0.95 | 0.96 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.96 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 26 | 1 | C | 0.00 | I | soil type: | 26 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 4 | 0.10 | 0.14 | 4 |  |  |  |  |  |  | Upper I | Upper C |
|  | 4.5 | 0.14 | 0.17 | 4.5 |  |  |  |  |  |  | 4 | 0.1 |
|  | 5 | 0.17 | 0.21 | 5 |  |  |  |  |  |  |  |  |
|  | 5.5 | 0.21 | 0.23 | 5.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.23 | 0.26 | 6 |  |  |  |  |  |  |  |  |
|  | 6.5 | 0.26 | 0.28 | 6.5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.28 | 0.31 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.31 | 0.36 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.36 | 0.39 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.39 | 0.43 | 12 |  |  |  |  |  |  |  |  |
|  | 16 | 0.43 | 0.45 | 16 |  |  |  |  |  |  |  |  |
|  | 20 | 0.45 | 0.47 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.47 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 27 | 1 | C | 0.00 | 1 | soil type: | 27 | l : | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.71 | 0.10 | 0.35 | 0.71 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.7 | 0.35 | 0.48 | 1.7 |  |  |  |  |  |  | 0.71 | 0.1 |
|  | 2.5 | 0.48 | 0.58 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.58 | 0.64 | 3.5 |  |  |  |  |  |  |  |  |


|  | 4.25 | 0.64 | 0.68 | 4.25 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 5 | 0.68 | 0.74 | 5 |  |  |  |  |  |  |  |  |
|  | 6.5 | 0.74 | 0.78 | 6.5 |  |  |  |  |  |  |  |  |
|  | 8 | 0.78 | 0.82 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.82 | 0.85 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.85 | 0.87 | 12 |  |  |  |  |  |  |  |  |
|  | 14 | 0.87 | 0.90 | 14 |  |  |  |  |  |  |  |  |
|  | 20 | 0.90 | 0.92 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.92 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 28 | I | C | 0.00 | I | soil type: | 28 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.54 | 0.10 | 0.26 | 0.54 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.26 | 0.44 | 1 |  |  |  |  |  |  | 0.54 | 0.1 |
|  | 1.75 | 0.44 | 0.56 | 1.75 |  |  |  |  |  |  |  |  |
|  | 2.6 | 0.56 | 0.64 | 2.6 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.64 | 0.70 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.70 | 0.75 | 4.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.75 | 0.78 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.78 | 0.80 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.80 | 0.81 | 10 |  |  |  |  |  |  |  |  |
|  | 13 | 0.81 | 0.82 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0.82 | 0.82 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0.82 | 0.83 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.83 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 29 | I | C | 0.00 | I | soil type: | 29 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.18 | 0.10 | 0.20 | 0.18 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.2 | 0.20 | 0.56 | 0.2 |  |  |  |  |  |  | 0.18 | 0.1 |
|  | 0.5 | 0.56 | 0.71 | 0.5 |  |  |  |  |  |  |  |  |
|  | 0.9 | 0.71 | 0.80 | 0.9 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.80 | 0.87 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.87 | 0.90 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.90 | 0.93 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5.5 | 0.93 | 0.96 | 5.5 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0.96 | 0.96 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0.96 | 0.97 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0.97 | 0.97 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0.97 | 0.98 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.98 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 30 | 1 | C | 0.00 | 1 | soil type: | 30 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.8 | 0.10 | 0.21 | 0.8 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.21 | 0.35 | 1 |  |  |  |  |  |  | 0.8 | 0.1 |
|  | 1.5 | 0.35 | 0.43 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.43 | 0.49 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.49 | 0.53 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.53 | 0.59 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.59 | 0.64 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.64 | 0.70 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.70 | 0.75 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.75 | 0.79 | 10 |  |  |  |  |  |  |  |  |
|  | 14 | 0.79 | 0.82 | 14 |  |  |  |  |  |  |  |  |
|  | 20 | 0.82 | 0.84 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.84 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 31 | I | C | 0.00 | I | soil type: | 31 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1 | 0.10 | 0.26 | 1 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.25 | 0.26 | 0.40 | 1.25 |  |  |  |  |  |  | 1 | 0.1 |
|  | 1.6 | 0.40 | 0.52 | 1.6 |  |  |  |  |  |  |  |  |
|  | 2.25 | 0.52 | 0.60 | 2.25 |  |  |  |  |  |  |  |  |
|  | 3 | 0.60 | 0.67 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.67 | 0.71 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.71 | 0.73 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.73 | 0.77 | 6 |  |  |  |  |  |  |  |  |


|  | 8 | 0.77 | 0.79 | 8 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 0.79 | 0.82 | 10 |  |  |  |  |  |  |  |  |
|  | 14 | 0.82 | 0.84 | 14 |  |  |  |  |  |  |  |  |
|  | 20 | 0.84 | 0.84 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.84 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 32 | 1 | C | 0.00 | 1 | soil type: | 32 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.2 | 0.10 | 0.31 | 0.2 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.31 | 0.52 | 0.5 |  |  |  |  |  |  | 0.2 | 0.1 |
|  | 1 | 0.52 | 0.63 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.63 | 0.71 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.71 | 0.79 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.79 | 0.83 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.83 | 0.88 | 4 |  |  |  |  |  |  |  |  |
|  | 7 | 0.88 | 0.91 | 7 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0.91 | 0.93 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0.93 | 0.95 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0.95 | 0.96 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0.96 | 0.97 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.97 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 33 | I | C | 0.00 | I | soil type: | 33 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.6 | 0.10 | 0.20 | 0.6 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.7 | 0.20 | 0.32 | 0.7 |  |  |  |  |  |  | 0.6 | 0.1 |
|  | 0.9 | 0.32 | 0.43 | 0.9 |  |  |  |  |  |  |  |  |
|  | 1.25 | 0.43 | 0.55 | 1.25 |  |  |  |  |  |  |  |  |
|  | 2 | 0.55 | 0.65 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.65 | 0.71 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.71 | 0.77 | 4 |  |  |  |  |  |  |  |  |
|  | 5.5 | 0.77 | 0.83 | 5.5 |  |  |  |  |  |  |  |  |
|  | 8 | 0.83 | 0.86 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.86 | 0.91 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.91 | 0.94 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.94 | 0.96 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.96 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 34 | I | C | 0.00 | I | soil type: | 34 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.2 | 0.10 | 0.43 | 0.2 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.43 | 0.65 | 0.5 |  |  |  |  |  |  | 0.2 | 0.1 |
|  | 1 | 0.65 | 0.74 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.74 | 0.79 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.79 | 0.84 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.84 | 0.88 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.88 | 0.91 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.91 | 0.95 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.95 | 0.97 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.97 | 0.99 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.99 | 0.99 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 0.99 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.99 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 35 | 1 | C | 0.00 | 1 | soil type: | 35 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | $0.1$ |
|  | 1.67 | 0.10 | 0.20 | 1.67 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.8 | 0.20 | 0.30 | 1.8 |  |  |  |  |  |  | 1.67 | 0.1 |
|  | 2 | 0.30 | 0.44 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.44 | 0.51 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.51 | 0.56 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.56 | 0.59 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4 | 0.59 | 0.63 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.63 | 0.68 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.68 | 0.73 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.73 | 0.78 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.78 | 0.82 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.82 | 0.85 | 20 |  |  |  |  |  |  |  |  |


| 25 | 0.85 | 0.00 | 25 |
| :---: | :---: | :---: | :---: |
| I | C | 0.00 | 1 |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |
| 0.2 | 0.10 | 0.44 | 0.2 |
| 0.45 | 0.44 | 0.65 | 0.45 |
| 1 | 0.65 | 0.74 | 1 |
| 1.5 | 0.74 | 0.79 | 1.5 |
| 2 | 0.79 | 0.83 | 2 |
| 2.5 | 0.83 | 0.89 | 2.5 |
| 3.5 | 0.89 | 0.92 | 3.5 |
| 4.5 | 0.92 | 0.95 | 4.5 |
| 6 | 0.95 | 0.97 | 6 |
| 8 | 0.97 | 0.99 | 8 |
| 12 | 0.99 | 1.00 | 12 |
| 20 | 1.00 | 1.00 | 20 |
| 25 | 1.00 | 0.00 | 25 |
| I | C | 0.00 | I |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |
| 0.78 | 0.10 | 0.25 | 0.78 |
| 1 | 0.25 | 0.40 | 1 |
| 1.5 | 0.40 | 0.49 | 1.5 |
| 2 | 0.49 | 0.60 | 2 |
| 3 | 0.60 | 0.66 | 3 |
| 4 | 0.66 | 0.71 | 4 |
| 5 | 0.71 | 0.75 | 5 |
| 6 | 0.75 | 0.80 | 6 |
| 8 | 0.80 | 0.83 | 8 |
| 10 | 0.83 | 0.88 | 10 |
| 15 | 0.88 | 0.90 | 15 |
| 20 | 0.90 | 0.92 | 20 |
| 25 | 0.92 | 0.00 | 25 |
| I | C | 0.00 | I |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |
| 0.56 | 0.10 | 0.29 | 0.56 |
| 0.75 | 0.29 | 0.40 | 0.75 |
| 1 | 0.40 | 0.54 | 1 |
| 1.5 | 0.54 | 0.61 | 1.5 |
| 2 | 0.61 | 0.71 | 2 |
| 3 | 0.71 | 0.76 | 3 |
| 4 | 0.76 | 0.82 | 4 |
| 6 | 0.82 | 0.85 | 6 |
| 8 | 0.85 | 0.87 | 8 |
| 10 | 0.87 | 0.90 | 10 |
| 15 | 0.90 | 0.92 | 15 |
| 20 | 0.92 | 0.93 | 20 |
| 25 | 0.93 | 0.00 | 25 |
| 1 | C | 0.00 | 1 |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |
| 0.24 | 0.10 | 0.46 | 0.24 |
| 0.5 | 0.46 | 0.58 | 0.5 |
| 0.75 | 0.58 | 0.66 | 0.75 |
| 1 | 0.66 | 0.75 | 1 |
| 1.5 | 0.75 | 0.80 | 1.5 |
| 2 | 0.80 | 0.85 | 2 |
| 3 | 0.85 | 0.88 | 3 |
| 4 | 0.88 | 0.92 | 4 |
| 6 | 0.92 | 0.95 | 6 |
| 10 | 0.95 | 0.96 | 10 |
| 15 | 0.96 | 0.97 | 15 |
| 20 | 0.97 | 0.97 | 20 |
| 25 | 0.97 | 0.00 | 25 |
| I | C | 0.00 | 1 |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |


| soil type: | 36 | I: | 0.1 | C: | 0.100 | Lower I <br> 0 <br> Upper I <br> 0.2 | Lower C $0.1$ <br> Upper C 0.1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| soil type: | 37 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | Lower I <br> 0 <br> Upper I <br> 0.78 | Lower C $0.1$ <br> Upper C 0.1 |
| soil type: | 38 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | $\begin{gathered} \text { Lower I } \\ 0 \\ \text { Upper I } \\ 0.56 \end{gathered}$ | Lower C <br> 0.1 <br> Upper C 0.1 |
| soil type: | 39 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | $\begin{gathered} \text { Lower I } \\ 0 \\ \text { Upper I } \\ 0.24 \end{gathered}$ | Lower C <br> 0.1 <br> Upper C 0.1 |
| soil type: | 40 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | $\begin{gathered} \text { Lower I } \\ 0 \end{gathered}$ | $\begin{gathered} \text { Lower C } \\ 0.1 \end{gathered}$ |


| 0.26 | 0.10 | 0.36 | 0.26 |
| :---: | :---: | :---: | :---: |
| 0.4 | 0.36 | 0.51 | 0.4 |
| 0.6 | 0.51 | 0.66 | 0.6 |
| 1 | 0.66 | 0.74 | 1 |
| 1.5 | 0.74 | 0.79 | 1.5 |
| 2 | 0.79 | 0.84 | 2 |
| 2.75 | 0.84 | 0.88 | 2.75 |
| 4 | 0.88 | 0.91 | 4 |
| 6 | 0.91 | 0.94 | 6 |
| 10 | 0.94 | 0.96 | 10 |
| 15 | 0.96 | 0.96 | 15 |
| 20 | 0.96 | 0.97 | 20 |
| 25 | 0.97 | 0.00 | 25 |
| I | C | 0.00 | I |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |
| 2.56 | 0.10 | 0.23 | 2.56 |
| 3 | 0.23 | 0.35 | 3 |
| 3.5 | 0.35 | 0.43 | 3.5 |
| 4 | 0.43 | 0.48 | 4 |
| 4.5 | 0.48 | 0.52 | 4.5 |
| 5 | 0.52 | 0.55 | 5 |
| 5.5 | 0.55 | 0.60 | 5.5 |
| 6.5 | 0.60 | 0.63 | 6.5 |
| 8 | 0.63 | 0.68 | 8 |
| 11 | 0.68 | 0.70 | 11 |
| 15 | 0.70 | 0.72 | 15 |
| 20 | 0.72 | 0.73 | 20 |
| 25 | 0.73 | 0.00 | 25 |
| I | C | 0.00 | 1 |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |
| 0.285 | 0.10 | 0.34 | 0.285 |
| 0.5 | 0.34 | 0.46 | 0.5 |
| 0.75 | 0.46 | 0.59 | 0.75 |
| 1.25 | 0.59 | 0.69 | 1.25 |
| 2 | 0.69 | 0.75 | 2 |
| 2.75 | 0.75 | 0.80 | 2.75 |
| 3.75 | 0.80 | 0.83 | 3.75 |
| 5 | 0.83 | 0.87 | 5 |
| 7 | 0.87 | 0.90 | 7 |
| 10 | 0.90 | 0.92 | 10 |
| 15 | 0.92 | 0.93 | 15 |
| 20 | 0.93 | 0.94 | 20 |
| 25 | 0.94 | 0.00 | 25 |
| 1 | C | 0.00 | 1 |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |
| 0.58 | 0.10 | 0.21 | 0.58 |
| 1 | 0.21 | 0.31 | 1 |
| 1.5 | 0.31 | 0.40 | 1.5 |
| 2 | 0.40 | 0.46 | 2 |
| 2.5 | 0.46 | 0.56 | 2.5 |
| 3.5 | 0.56 | 0.64 | 3.5 |
| 4.5 | 0.64 | 0.71 | 4.5 |
| 6 | 0.71 | 0.77 | 6 |
| 8 | 0.77 | 0.83 | 8 |
| 11 | 0.83 | 0.88 | 11 |
| 15 | 0.88 | 0.91 | 15 |
| 20 | 0.91 | 0.93 | 20 |
| 25 | 0.93 | 0.00 | 25 |
| I | C | 0.00 | 1 |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |
| 0.14 | 0.10 | 0.45 | 0.14 |
| 0.3 | 0.45 | 0.70 | 0.3 |
| 0.75 | 0.70 | 0.80 | 0.75 |
| 1.25 | 0.80 | 0.85 | 1.25 |


| soil type: | 41 | I: | 0.1 | C: | 0.100 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | $\begin{gathered} \text { Lower I } \\ 0 \\ \text { Upper I } \\ 2.56 \end{gathered}$ | Lower C 0.1 Upper C 0.1 |
| soil type: | 42 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | $\begin{gathered} \text { Lower I } \\ 0 \\ \text { Upper I } \\ 0.285 \end{gathered}$ | Lower C 0.1 Upper C 0.1 |
| soil type: | 43 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | $\begin{gathered} \text { Lower I } \\ 0 \\ \text { Upper I } \\ 0.58 \end{gathered}$ | Lower C 0.1 Upper C 0.1 |
| soil type: | 44 | I : | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | Lower I 0 <br> Upper I 0.14 | Lower C 0.1 Upper C 0.1 |


|  | 1.75 | 0.85 | 0.90 | 1.75 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2.5 | 0.90 | 0.91 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.91 | 0.94 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.94 | 0.96 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.96 | 0.98 | 6 |  |  |  |  |  |  |  |  |
|  | 10 | 0.98 | 0.99 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.99 | 1.00 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 1.00 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 45 | 1 | C | 0.00 | I | soil type: | 45 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 2 | 0.10 | 0.21 | 2 |  |  |  |  |  |  | Upper I | Upper C |
|  | 2.25 | 0.21 | 0.27 | 2.25 |  |  |  |  |  |  | 2 | 0.1 |
|  | 2.5 | 0.27 | 0.39 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.25 | 0.39 | 0.46 | 3.25 |  |  |  |  |  |  |  |  |
|  | 4 | 0.46 | 0.49 | 4 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.49 | 0.52 | 4.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.52 | 0.56 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.56 | 0.61 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.61 | 0.66 | 8 |  |  |  |  |  |  |  |  |
|  | 11 | 0.66 | 0.70 | 11 |  |  |  |  |  |  |  |  |
|  | 15 | 0.70 | 0.72 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.72 | 0.74 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.74 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 46 | I | C | 0.00 | 1 | soil type: | 46 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1.6 | 0.10 | 0.14 | 1.6 |  |  |  |  |  |  | Upper I | Upper C |
|  | 2 | 0.14 | 0.23 | 2 |  |  |  |  |  |  | 1.6 | 0.1 |
|  | 3 | 0.23 | 0.30 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.30 | 0.34 | 4 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.34 | 0.37 | 4.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.37 | 0.42 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.42 | 0.50 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.50 | 0.55 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.55 | 0.60 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.60 | 0.65 | 12 |  |  |  |  |  |  |  |  |
|  | 15 | 0.65 | 0.70 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.70 | 0.73 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.73 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 47 | I | C | 0.00 | I | soil type: | 47 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.33 | 0.10 | 0.24 | 0.33 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.24 | 0.46 | 0.5 |  |  |  |  |  |  | 0.33 | 0.1 |
|  | 1 | 0.46 | 0.59 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.59 | 0.71 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2.25 | 0.71 | 0.78 | 2.25 |  |  |  |  |  |  |  |  |
|  | 3 | 0.78 | 0.84 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.84 | 0.88 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.88 | 0.90 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.90 | 0.93 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.93 | 0.95 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.95 | 0.96 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.96 | 0.97 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.97 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 48 | I | C | 0.00 | 1 | soil type: | 48 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.7 | 0.10 | 0.29 | 0.7 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.29 | 0.43 | 1 |  |  |  |  |  |  | 0.7 | 0.1 |
|  | 1.5 | 0.43 | 0.52 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.52 | 0.59 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.59 | 0.64 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.64 | 0.71 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.71 | 0.76 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.76 | 0.83 | 5 |  |  |  |  |  |  |  |  |


|  | 7 | 0.83 | 0.89 | 7 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 0.89 | 0.94 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.94 | 0.97 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.97 | 0.99 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.99 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 49 | I | C | 0.00 | 1 | soil type: | 49 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.25 | 0.10 | 0.35 | 0.25 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.35 | 0.55 | 0.5 |  |  |  |  |  |  | 0.25 | 0.1 |
|  | 1 | 0.55 | 0.65 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.65 | 0.71 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.71 | 0.76 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.76 | 0.82 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.82 | 0.87 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.87 | 0.91 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.91 | 0.95 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.95 | 0.98 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.98 | 0.99 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 50 | I | C | 0.00 | I | soil type: | 50 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.17 | 0.10 | 0.48 | 0.17 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.48 | 0.60 | 0.5 |  |  |  |  |  |  | 0.17 | 0.1 |
|  | 0.75 | 0.60 | 0.68 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1 | 0.68 | 0.77 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.77 | 0.85 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2.25 | 0.85 | 0.89 | 2.25 |  |  |  |  |  |  |  |  |
|  | 3 | 0.89 | 0.93 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.93 | 0.96 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.96 | 0.98 | 6 |  |  |  |  |  |  |  |  |
|  | 10 | 0.98 | 0.99 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.99 | 0.99 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 0.99 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.99 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 51 | I | C | 0.00 | I | soil type: | 51 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.48 | 0.10 | 0.32 | 0.48 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.32 | 0.42 | 0.75 |  |  |  |  |  |  | 0.48 | 0.1 |
|  | 1 | 0.42 | 0.54 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.54 | 0.61 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.61 | 0.66 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.66 | 0.70 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.70 | 0.75 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.75 | 0.81 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.81 | 0.84 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.84 | 0.88 | 8 |  |  |  |  |  |  |  |  |
|  | 12 | 0.88 | 0.91 | 12 |  |  |  |  |  |  |  |  |
|  | 20 | 0.91 | 0.92 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.92 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 52 | 1 | C | 0.00 | 1 | soil type: | 52 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 4.22 | 0.10 | 0.13 | 4.22 |  |  |  |  |  |  | Upper I | Upper C |
|  | 4.5 | 0.13 | 0.19 | 4.5 |  |  |  |  |  |  | 4.22 | 0.1 |
|  | 5 | 0.19 | 0.28 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.28 | 0.35 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.35 | 0.41 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.41 | 0.45 | 8 |  |  |  |  |  |  |  |  |
|  | 9 | 0.45 | 0.48 | 9 |  |  |  |  |  |  |  |  |
|  | 10 | 0.48 | 0.53 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.53 | 0.57 | 12 |  |  |  |  |  |  |  |  |
|  | 14 | 0.57 | 0.59 | 14 |  |  |  |  |  |  |  |  |
|  | 16 | 0.59 | 0.63 | 16 |  |  |  |  |  |  |  |  |
|  | 20 | 0.63 | 0.66 | 20 |  |  |  |  |  |  |  |  |


|  | 25 | 0.66 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 53 | 1 | C | 0.00 | 1 | soil type: | 53 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.6 | 0.10 | 0.18 | 0.6 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.18 | 0.31 | 0.75 |  |  |  |  |  |  | 0.6 | 0.1 |
|  | 1.25 | 0.31 | 0.42 | 1.25 |  |  |  |  |  |  |  |  |
|  | 2 | 0.42 | 0.47 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.47 | 0.51 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.51 | 0.58 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.58 | 0.62 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.62 | 0.69 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.69 | 0.76 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.76 | 0.82 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.82 | 0.86 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.86 | 0.88 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.88 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 54 | I | C | 0.00 | I | soil type: | 54 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.465 | 0.10 | 0.33 | 0.465 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.33 | 0.50 | 0.75 |  |  |  |  |  |  | 0.465 | 0.1 |
|  | 1.25 | 0.50 | 0.63 | 1.25 |  |  |  |  |  |  |  |  |
|  | 2 | 0.63 | 0.69 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.69 | 0.73 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.73 | 0.76 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.76 | 0.83 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.83 | 0.88 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.88 | 0.92 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.92 | 0.96 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.96 | 0.98 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.98 | 0.99 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.99 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 55 | I | C | 0.00 | 1 | soil type: | 55 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.455 | 0.10 | 0.48 | 0.455 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.5 | 0.48 | 0.58 | 1.5 |  |  |  |  |  |  | 0.455 | 0.1 |
|  | 2 | 0.58 | 0.64 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.64 | 0.69 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.69 | 0.73 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.73 | 0.79 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.79 | 0.85 | 4.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.85 | 0.89 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.89 | 0.94 | 8 |  |  |  |  |  |  |  |  |
|  | 12 | 0.94 | 0.96 | 12 |  |  |  |  |  |  |  |  |
|  | 15 | 0.96 | 0.98 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.98 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 56 | I | C | 0.00 | I | soil type: | 56 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.26 | 0.10 | 0.31 | 0.26 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.31 | 0.47 | 0.5 |  |  |  |  |  |  | 0.26 | 0.1 |
|  | 0.75 | 0.47 | 0.65 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1.25 | 0.65 | 0.74 | 1.25 |  |  |  |  |  |  |  |  |
|  | 1.75 | 0.74 | 0.79 | 1.75 |  |  |  |  |  |  |  |  |
|  | 2.25 | 0.79 | 0.83 | 2.25 |  |  |  |  |  |  |  |  |
|  | 3 | 0.83 | 0.86 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.86 | 0.89 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.89 | 0.91 | 6 |  |  |  |  |  |  |  |  |
|  | 10 | 0.91 | 0.92 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.92 | 0.93 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.93 | 0.93 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.93 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 57 | 1 | C | 0.00 | 1 | soil type: | 57 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |


|  | 1.25 | 0.10 | 0.23 | 1.25 |  |  |  |  |  |  | Upper I | Upper C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1.75 | 0.23 | 0.39 | 1.75 |  |  |  |  |  |  | 1.25 | 0.1 |
|  | 2.5 | 0.39 | 0.47 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.47 | 0.53 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.53 | 0.58 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4 | 0.58 | 0.65 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.65 | 0.69 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.69 | 0.75 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.75 | 0.82 | 8 |  |  |  |  |  |  |  |  |
|  | 11 | 0.82 | 0.86 | 11 |  |  |  |  |  |  |  |  |
|  | 15 | 0.86 | 0.90 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.90 | 0.92 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.92 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 58 | I | C | 0.00 | I | soil type: | 58 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.52 | 0.10 | 0.21 | 0.52 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.63 | 0.21 | 0.29 | 0.63 |  |  |  |  |  |  | 0.52 | 0.1 |
|  | 0.79 | 0.29 | 0.44 | 0.79 |  |  |  |  |  |  |  |  |
|  | 1.25 | 0.44 | 0.53 | 1.25 |  |  |  |  |  |  |  |  |
|  | 1.75 | 0.53 | 0.63 | 1.75 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.63 | 0.70 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.70 | 0.77 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.77 | 0.83 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.83 | 0.88 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.88 | 0.92 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.92 | 0.94 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.94 | 0.96 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.96 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 59 | 1 | C | 0.00 | 1 | soil type: | 59 | I : | 0.1 | C : | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.33 | 0.10 | 0.34 | 0.33 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.34 | 0.49 | 0.5 |  |  |  |  |  |  | 0.33 | 0.1 |
|  | 0.75 | 0.49 | 0.64 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1.25 | 0.64 | 0.75 | 1.25 |  |  |  |  |  |  |  |  |
|  | 2 | 0.75 | 0.83 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.83 | 0.87 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.87 | 0.90 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.90 | 0.93 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.93 | 0.96 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.96 | 0.98 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.98 | 0.99 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 60 | I | C | 0.00 | I | soil type: | 60 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1 | 0.10 | 0.25 | 1 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.5 | 0.25 | 0.34 | 1.5 |  |  |  |  |  |  | 1 | 0.1 |
|  | 2 | 0.34 | 0.40 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.40 | 0.44 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.44 | 0.47 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.47 | 0.49 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4 | 0.49 | 0.52 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.52 | 0.55 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.55 | 0.58 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.58 | 0.60 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.60 | 0.61 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.61 | 0.61 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.61 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 61 | I | C | 0.00 | 1 | soil type: | 61 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 4.1 | 0.10 | 0.15 | 4.1 |  |  |  |  |  |  | Upper I | Upper C |
|  | 4.25 | 0.15 | 0.21 | 4.25 |  |  |  |  |  |  | 4.1 | 0.1 |
|  | 4.5 | 0.21 | 0.29 | 4.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.29 | 0.35 | 5 |  |  |  |  |  |  |  |  |


|  | 5.5 | 0.35 | 0.39 | 5.5 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 6 | 0.39 | 0.45 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.45 | 0.49 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.49 | 0.53 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.53 | 0.56 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.56 | 0.58 | 12 |  |  |  |  |  |  |  |  |
|  | 15 | 0.58 | 0.60 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.60 | 0.62 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.62 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 62 | I | C | 0.00 | I | soil type: | 62 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.73 | 0.10 | 0.28 | 0.73 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.28 | 0.43 | 1 |  |  |  |  |  |  | 0.73 | 0.1 |
|  | 1.5 | 0.43 | 0.53 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.53 | 0.59 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.59 | 0.64 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.64 | 0.72 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.72 | 0.79 | 4 |  |  |  |  |  |  |  |  |
|  | 5.5 | 0.79 | 0.85 | 5.5 |  |  |  |  |  |  |  |  |
|  | 7.5 | 0.85 | 0.89 | 7.5 |  |  |  |  |  |  |  |  |
|  | 10 | 0.89 | 0.95 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.95 | 0.98 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.98 | 0.99 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.99 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 63 | I | C | 0.00 | I | soil type: | 63 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.47 | 0.10 | 0.31 | 0.47 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.31 | 0.40 | 0.75 |  |  |  |  |  |  | 0.47 | 0.1 |
|  | 1 | 0.40 | 0.52 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.52 | 0.59 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.59 | 0.69 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.69 | 0.75 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.75 | 0.79 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.79 | 0.85 | 5 |  |  |  |  |  |  |  |  |
|  | 7.5 | 0.85 | 0.88 | 7.5 |  |  |  |  |  |  |  |  |
|  | 10 | 0.88 | 0.92 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.92 | 0.94 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.94 | 0.95 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.95 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 64 | I | C | 0.00 | I | soil type: | 64 | $\mathrm{I}:$ | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.21 | 0.10 | 0.36 | 0.21 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.36 | 0.57 | 0.5 |  |  |  |  |  |  | 0.21 | 0.1 |
|  | 1 | 0.57 | 0.67 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.67 | 0.73 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.73 | 0.80 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.80 | 0.84 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.84 | 0.87 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.87 | 0.88 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.88 | 0.92 | 6 |  |  |  |  |  |  |  |  |
|  | 10 | 0.92 | 0.94 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.94 | 0.95 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.95 | 0.95 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.95 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 65 | 1 | C | 0.00 | I | soil type: | 65 | $\mathrm{I}:$ | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.13 | 0.10 | 0.38 | 0.13 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.25 | 0.38 | 0.62 | 0.25 |  |  |  |  |  |  | 0.13 | 0.1 |
|  | 0.6 | 0.62 | 0.74 | 0.6 |  |  |  |  |  |  |  |  |
|  | 1 | 0.74 | 0.81 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.81 | 0.87 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2.25 | 0.87 | 0.90 | 2.25 |  |  |  |  |  |  |  |  |
|  | 3 | 0.90 | 0.92 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.92 | 0.95 | 4 |  |  |  |  |  |  |  |  |


|  | 6 | 0.95 | 0.97 | 6 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 0.97 | 0.98 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.98 | 0.99 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 0.99 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.99 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 66 | 1 | C | 0.00 | I | soil type: | 66 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.32 | 0.10 | 0.15 | 0.32 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.4 | 0.15 | 0.38 | 0.4 |  |  |  |  |  |  | 0.32 | 0.1 |
|  | 0.7 | 0.38 | 0.48 | 0.7 |  |  |  |  |  |  |  |  |
|  | 1 | 0.48 | 0.58 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.58 | 0.64 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.64 | 0.71 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.71 | 0.76 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.76 | 0.80 | 4 |  |  |  |  |  |  |  |  |
|  | 5.5 | 0.80 | 0.85 | 5.5 |  |  |  |  |  |  |  |  |
|  | 8 | 0.85 | 0.89 | 8 |  |  |  |  |  |  |  |  |
|  | 12 | 0.89 | 0.93 | 12 |  |  |  |  |  |  |  |  |
|  | 20 | 0.93 | 0.95 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.95 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 67 | I | C | 0.00 | I | soil type: | 67 | I : | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.7 | 0.10 | 0.26 | 0.7 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.26 | 0.39 | 1 |  |  |  |  |  |  | 0.7 | 0.1 |
|  | 1.5 | 0.39 | 0.47 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.47 | 0.52 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.52 | 0.56 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.56 | 0.61 | 3 |  |  |  |  |  |  |  |  |
|  | 3.75 | 0.61 | 0.66 | 3.75 |  |  |  |  |  |  |  |  |
|  | 5 | 0.66 | 0.72 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.72 | 0.76 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.76 | 0.80 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.80 | 0.82 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.82 | 0.84 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.84 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 68 | 1 | C | 0.00 | 1 | soil type: | 68 | I : | 0.1 | C : | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.33 | 0.10 | 0.29 | 0.33 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.29 | 0.50 | 0.75 |  |  |  |  |  |  | 0.33 | 0.1 |
|  | 1.5 | 0.50 | 0.58 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.58 | 0.68 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.68 | 0.71 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.71 | 0.76 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.76 | 0.81 | 4.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.81 | 0.85 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.85 | 0.87 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.87 | 0.90 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.90 | 0.92 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.92 | 0.93 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.93 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 69 | I | C | 0.00 | I | soil type: | 69 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.23 | 0.10 | 0.30 | 0.23 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.30 | 0.40 | 1 |  |  |  |  |  |  | 0.23 | 0.1 |
|  | 1.5 | 0.40 | 0.47 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.47 | 0.52 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.52 | 0.56 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.56 | 0.63 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.63 | 0.67 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.67 | 0.73 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.73 | 0.77 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.77 | 0.82 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.82 | 0.84 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.84 | 0.85 | 20 |  |  |  |  |  |  |  |  |

70
$\stackrel{H}{\lambda}$

N

73

74

| 25 | 0.85 | 0.00 | 25 |
| :---: | :---: | :---: | :---: |
| 1 | C | 0.00 | 1 |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |
| 0.32 | 0.10 | 0.34 | 0.32 |
| 0.5 | 0.34 | 0.47 | 0.5 |
| 0.75 | 0.47 | 0.54 | 0.75 |
| 1 | 0.54 | 0.63 | 1 |
| 1.5 | 0.63 | 0.67 | 1.5 |
| 2 | 0.67 | 0.70 | 2 |
| 2.5 | 0.70 | 0.75 | 2.5 |
| 4 | 0.75 | 0.78 | 4 |
| 6 | 0.78 | 0.80 | 6 |
| 10 | 0.80 | 0.82 | 10 |
| 15 | 0.82 | 0.82 | 15 |
| 20 | 0.82 | 0.83 | 20 |
| 25 | 0.83 | 0.00 | 25 |
| I | C | 0.00 | 1 |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |
| 0.24 | 0.10 | 0.46 | 0.24 |
| 0.5 | 0.46 | 0.58 | 0.5 |
| 0.75 | 0.58 | 0.65 | 0.75 |
| 1 | 0.65 | 0.74 | 1 |
| 1.5 | 0.74 | 0.79 | 1.5 |
| 2 | 0.79 | 0.85 | 2 |
| 3 | 0.85 | 0.88 | 3 |
| 4 | 0.88 | 0.92 | 4 |
| 6 | 0.92 | 0.94 | 6 |
| 10 | 0.94 | 0.96 | 10 |
| 15 | 0.96 | 0.97 | 15 |
| 20 | 0.97 | 0.97 | 20 |
| 25 | 0.97 | 0.00 | 25 |
| I | C | 0.00 | 1 |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |
| 0.46 | 0.10 | 0.31 | 0.46 |
| 0.75 | 0.31 | 0.43 | 0.75 |
| 1 | 0.43 | 0.59 | 1 |
| 1.5 | 0.59 | 0.68 | 1.5 |
| 2 | 0.68 | 0.74 | 2 |
| 2.5 | 0.74 | 0.81 | 2.5 |
| 3.5 | 0.81 | 0.86 | 3.5 |
| 5 | 0.86 | 0.90 | 5 |
| 7 | 0.90 | 0.93 | 7 |
| 10 | 0.93 | 0.96 | 10 |
| 15 | 0.96 | 0.97 | 15 |
| 20 | 0.97 | 0.98 | 20 |
| 25 | 0.98 | 0.00 | 25 |
| I | C | 0.00 | 1 |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |
| 0.77 | 0.10 | 0.41 | 0.77 |
| 1.5 | 0.41 | 0.54 | 1.5 |
| 2 | 0.54 | 0.62 | 2 |
| 2.5 | 0.62 | 0.68 | 2.5 |
| 3 | 0.68 | 0.72 | 3 |
| 3.5 | 0.72 | 0.78 | 3.5 |
| 4.5 | 0.78 | 0.83 | 4.5 |
| 6 | 0.83 | 0.87 | 6 |
| 8 | 0.87 | 0.89 | 8 |
| 10 | 0.89 | 0.93 | 10 |
| 15 | 0.93 | 0.94 | 15 |
| 20 | 0.94 | 0.95 | 20 |
| 25 | 0.95 | 0.00 | 25 |
| I | C | 0.00 | 1 |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |


| soil type: | 70 | I: | 0.1 | C: | 0.100 | Lower I <br> 0 <br> Upper I $0.32$ | Lower C $0.1$ <br> Upper C 0.1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| soil type: | 71 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | Lower I <br> 0 <br> Upper I <br> 0.24 | Lower C $0.1$ <br> Upper C 0.1 |
| soil type: | 72 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | Lower I 0 <br> Upper I 0.46 | Lower C 0.1 Upper C 0.1 |
| soil type: | 73 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | $\begin{gathered} \text { Lower I } \\ 0 \\ \text { Upper I } \\ 0.77 \end{gathered}$ | Lower C 0.1 <br> Upper C 0.1 |
| soil type: | 74 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | $\begin{gathered} \text { Lower I } \\ 0 \end{gathered}$ | $\begin{gathered} \text { Lower C } \\ 0.1 \end{gathered}$ |


|  | 0.47 | 0.10 | 0.20 | 0.47 |  |  |  |  |  |  | Upper I | Upper C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.75 | 0.20 | 0.39 | 0.75 |  |  |  |  |  |  | 0.47 | 0.1 |
|  | 1.5 | 0.39 | 0.49 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.49 | 0.56 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.56 | 0.64 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.25 | 0.64 | 0.70 | 3.25 |  |  |  |  |  |  |  |  |
|  | 4 | 0.70 | 0.75 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.75 | 0.78 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.78 | 0.84 | 6 |  |  |  |  |  |  |  |  |
|  | 10 | 0.84 | 0.89 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.89 | 0.91 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.91 | 0.93 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.93 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 75 | 1 | C | 0.00 | 1 | soil type: | 75 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.83 | 0.10 | 0.29 | 0.83 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.5 | 0.29 | 0.39 | 1.5 |  |  |  |  |  |  | 0.83 | 0.1 |
|  | 2 | 0.39 | 0.47 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.47 | 0.53 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.53 | 0.58 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.58 | 0.65 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.65 | 0.73 | 4.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.73 | 0.79 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.79 | 0.83 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.83 | 0.89 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.89 | 0.92 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.92 | 0.93 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.93 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 76 | 1 | C | 0.00 | 1 | soil type: | 76 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.55 | 0.10 | 0.25 | 0.55 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.25 | 0.33 | 1 |  |  |  |  |  |  | 0.55 | 0.1 |
|  | 1.5 | 0.33 | 0.39 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.39 | 0.44 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.44 | 0.48 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.48 | 0.54 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.54 | 0.58 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.58 | 0.65 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.65 | 0.71 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.71 | 0.77 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.77 | 0.81 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.81 | 0.83 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.83 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 77 | I | C | 0.00 | I | soil type: | 77 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.37 | 0.10 | 0.33 | 0.37 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.33 | 0.59 | 0.5 |  |  |  |  |  |  | 0.37 | 0.1 |
|  | 1 | 0.59 | 0.70 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.70 | 0.76 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.76 | 0.80 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.80 | 0.83 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.83 | 0.87 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.87 | 0.91 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.91 | 0.94 | 6 |  |  |  |  |  |  |  |  |
|  | 10 | 0.94 | 0.96 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.96 | 0.97 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.97 | 0.97 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.97 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 78 | 1 | C | 0.00 | 1 | soil type: | 78 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.575 | 0.10 | 0.29 | 0.575 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.9 | 0.29 | 0.44 | 0.9 |  |  |  |  |  |  | 0.575 | 0.1 |
|  | 1.5 | 0.44 | 0.51 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.51 | 0.57 | 2 |  |  |  |  |  |  |  |  |


|  | 2.5 | 0.57 | 0.61 | 2.5 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3 | 0.61 | 0.68 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.68 | 0.73 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.73 | 0.79 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.79 | 0.84 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.84 | 0.89 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.89 | 0.92 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.92 | 0.94 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.94 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 79 | 1 | C | 0.00 | 1 | soil type: | 79 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.38 | 0.10 | 0.26 | 0.38 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.26 | 0.51 | 0.5 |  |  |  |  |  |  | 0.38 | 0.1 |
|  | 1 | 0.51 | 0.62 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.62 | 0.69 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.69 | 0.77 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.77 | 0.82 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.82 | 0.87 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.87 | 0.90 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.90 | 0.92 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.92 | 0.95 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.95 | 0.96 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.96 | 0.97 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.97 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 80 | 1 | C | 0.00 | 1 | soil type: | 80 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.425 | 0.10 | 0.24 | 0.425 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.6 | 0.24 | 0.33 | 0.6 |  |  |  |  |  |  | 0.425 | 0.1 |
|  | 0.8 | 0.33 | 0.40 | 0.8 |  |  |  |  |  |  |  |  |
|  | 1 | 0.40 | 0.51 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.51 | 0.61 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2.25 | 0.61 | 0.67 | 2.25 |  |  |  |  |  |  |  |  |
|  | 3 | 0.67 | 0.73 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.73 | 0.80 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.80 | 0.86 | 6 |  |  |  |  |  |  |  |  |
|  | 9 | 0.86 | 0.89 | 9 |  |  |  |  |  |  |  |  |
|  | 12 | 0.89 | 0.94 | 12 |  |  |  |  |  |  |  |  |
|  | 20 | 0.94 | 0.95 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.95 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 81 | 1 | C | 0.00 | 1 | soil type: | 81 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.285 | 0.10 | 0.35 | 0.285 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.35 | 0.58 | 0.5 |  |  |  |  |  |  | 0.285 | 0.1 |
|  | 1 | 0.58 | 0.69 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.69 | 0.75 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.75 | 0.79 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.79 | 0.83 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.83 | 0.87 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.87 | 0.91 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.91 | 0.95 | 6 |  |  |  |  |  |  |  |  |
|  | 10 | 0.95 | 0.97 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.97 | 0.99 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 0.99 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.99 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 82 | I | C | 0.00 | I | soil type: | 82 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.445 | 0.10 | 0.35 | 0.445 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.35 | 0.49 | 1 |  |  |  |  |  |  | 0.445 | 0.1 |
|  | 1.5 | 0.49 | 0.61 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2.25 | 0.61 | 0.68 | 2.25 |  |  |  |  |  |  |  |  |
|  | 3 | 0.68 | 0.72 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.72 | 0.77 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.77 | 0.81 | 4.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.81 | 0.85 | 6 |  |  |  |  |  |  |  |  |


|  | 8 | 0.85 | 0.87 | 8 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 0.87 | 0.90 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.90 | 0.92 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.92 | 0.93 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.93 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 84 | 1 | C | 0.00 | I | soil type: | 84 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.63 | 0.10 | 0.22 | 0.63 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.22 | 0.35 | 1 |  |  |  |  |  |  | 0.63 | 0.1 |
|  | 1.5 | 0.35 | 0.45 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.45 | 0.52 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.52 | 0.63 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.63 | 0.70 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.70 | 0.77 | 4.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.77 | 0.84 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.84 | 0.88 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.88 | 0.93 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.93 | 0.96 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.96 | 0.98 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.98 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 85 | I | C | 0.00 | I | soil type: | 85 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1.22 | 0.10 | 0.22 | 1.22 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.5 | 0.22 | 0.34 | 1.5 |  |  |  |  |  |  | 1.22 | 0.1 |
|  | 2 | 0.34 | 0.42 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.42 | 0.48 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.48 | 0.53 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.53 | 0.60 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.60 | 0.68 | 4.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.68 | 0.74 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.74 | 0.79 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.79 | 0.86 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.86 | 0.90 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.90 | 0.93 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.93 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 86 | I | C | 0.00 | I | soil type: | 86 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1.48 | 0.10 | 0.20 | 1.48 |  |  |  |  |  |  | Upper I | Upper C |
|  | 2 | 0.20 | 0.30 | 2 |  |  |  |  |  |  | 1.48 | 0.1 |
|  | 2.5 | 0.30 | 0.44 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.44 | 0.52 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.52 | 0.58 | 4.5 |  |  |  |  |  |  |  |  |
|  | 5.5 | 0.58 | 0.63 | 5.5 |  |  |  |  |  |  |  |  |
|  | 6.5 | 0.63 | 0.69 | 6.5 |  |  |  |  |  |  |  |  |
|  | 8 | 0.69 | 0.74 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.74 | 0.78 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.78 | 0.82 | 12 |  |  |  |  |  |  |  |  |
|  | 15 | 0.82 | 0.86 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.86 | 0.89 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.89 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 87 | 1 | C | 0.00 | I | soil type: | 87 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.73 | 0.10 | 0.22 | 0.73 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.22 | 0.35 | 1 |  |  |  |  |  |  | 0.73 | 0.1 |
|  | 1.5 | 0.35 | 0.45 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.45 | 0.57 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.57 | 0.65 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.65 | 0.70 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.70 | 0.74 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.74 | 0.79 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.79 | 0.82 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.82 | 0.86 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.86 | 0.89 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.89 | 0.90 | 20 |  |  |  |  |  |  |  |  |


|  | 25 | 0.90 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 88 | 1 | C | 0.00 | 1 | soil type: | 88 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.69 | 0.10 | 0.23 | 0.69 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.23 | 0.38 | 1 |  |  |  |  |  |  | 0.69 | 0.1 |
|  | 1.5 | 0.38 | 0.49 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.49 | 0.65 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.65 | 0.70 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.70 | 0.78 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.78 | 0.85 | 4.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.85 | 0.87 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.87 | 0.92 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.92 | 0.94 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.94 | 0.95 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.95 | 0.95 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.95 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 89 | I | C | 0.00 | I | soil type: | 89 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.33 | 0.10 | 0.29 | 0.33 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.29 | 0.49 | 0.5 |  |  |  |  |  |  | 0.33 | 0.1 |
|  | 1 | 0.49 | 0.58 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.58 | 0.64 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.64 | 0.68 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.68 | 0.71 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.71 | 0.73 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.73 | 0.77 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.77 | 0.81 | 5 |  |  |  |  |  |  |  |  |
|  | 8 | 0.81 | 0.84 | 8 |  |  |  |  |  |  |  |  |
|  | 15 | 0.84 | 0.86 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.86 | 0.86 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.86 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 90 | , | C | 0.00 | , | soil type: | 90 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.16 | 0.10 | 0.43 | 0.16 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.4 | 0.43 | 0.59 | 0.4 |  |  |  |  |  |  | 0.16 | 0.1 |
|  | 0.75 | 0.59 | 0.66 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1 | 0.66 | 0.74 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.74 | 0.78 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.78 | 0.82 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.82 | 0.85 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.85 | 0.88 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.88 | 0.90 | 4.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.90 | 0.93 | 6 |  |  |  |  |  |  |  |  |
|  | 10 | 0.93 | 0.95 | 10 |  |  |  |  |  |  |  |  |
|  | 20 | 0.95 | 0.96 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.96 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 91 | I | C | 0.00 | I | soil type: | 91 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.18 | 0.10 | 0.26 | 0.18 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.25 | 0.26 | 0.47 | 0.25 |  |  |  |  |  |  | 0.18 | 0.1 |
|  | 0.5 | 0.47 | 0.57 | 0.5 |  |  |  |  |  |  |  |  |
|  | 0.75 | 0.57 | 0.63 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1 | 0.63 | 0.70 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.70 | 0.74 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.74 | 0.79 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.79 | 0.83 | 3 |  |  |  |  |  |  |  |  |
|  | 5 | 0.83 | 0.87 | 5 |  |  |  |  |  |  |  |  |
|  | 10 | 0.87 | 0.88 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.88 | 0.89 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.89 | 0.89 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.89 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 92 | 1 | C | 0.00 | 1 | soil type: | 92 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |


| 0.18 | 0.10 | 0.36 | 0.18 |
| :---: | :---: | :---: | :---: |
| 0.3 | 0.36 | 0.52 | 0.3 |
| 0.5 | 0.52 | 0.62 | 0.5 |
| 0.75 | 0.62 | 0.68 | 0.75 |
| 1 | 0.68 | 0.74 | 1 |
| 1.5 | 0.74 | 0.78 | 1.5 |
| 2 | 0.78 | 0.82 | 2 |
| 3 | 0.82 | 0.85 | 3 |
| 4 | 0.85 | 0.88 | 4 |
| 7 | 0.88 | 0.89 | 7 |
| 10 | 0.89 | 0.91 | 10 |
| 20 | 0.91 | 0.91 | 20 |
| 25 | 0.91 | 0.00 | 25 |
| I | C | 0.00 | I |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |
| 0.29 | 0.10 | 0.25 | 0.29 |
| 0.5 | 0.25 | 0.36 | 0.5 |
| 0.75 | 0.36 | 0.45 | 0.75 |
| 1 | 0.45 | 0.56 | 1 |
| 1.5 | 0.56 | 0.63 | 1.5 |
| 2 | 0.63 | 0.68 | 2 |
| 2.5 | 0.68 | 0.75 | 2.5 |
| 3.5 | 0.75 | 0.80 | 3.5 |
| 5 | 0.80 | 0.84 | 5 |
| 7 | 0.84 | 0.88 | 7 |
| 12 | 0.88 | 0.91 | 12 |
| 20 | 0.91 | 0.91 | 20 |
| 25 | 0.91 | 0.00 | 25 |
| I | C | 0.00 | I |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |
| 0.2 | 0.10 | 0.29 | 0.2 |
| 0.25 | 0.29 | 0.57 | 0.25 |
| 0.5 | 0.57 | 0.68 | 0.5 |
| 0.75 | 0.68 | 0.74 | 0.75 |
| 1 | 0.74 | 0.81 | 1 |
| 1.5 | 0.81 | 0.85 | 1.5 |
| 2 | 0.85 | 0.88 | 2 |
| 3 | 0.88 | 0.90 | 3 |
| 4 | 0.90 | 0.93 | 4 |
| 7 | 0.93 | 0.95 | 7 |
| 12 | 0.95 | 0.95 | 12 |
| 20 | 0.95 | 0.96 | 20 |
| 25 | 0.96 | 0.00 | 25 |
| I | C | 0.00 | I |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |
| 0.22 | 0.10 | 0.41 | 0.22 |
| 0.4 | 0.41 | 0.59 | 0.4 |
| 0.75 | 0.59 | 0.66 | 0.75 |
| 1 | 0.66 | 0.73 | 1 |
| 1.5 | 0.73 | 0.77 | 1.5 |
| 2 | 0.77 | 0.80 | 2 |
| 2.5 | 0.80 | 0.83 | 2.5 |
| 3.5 | 0.83 | 0.86 | 3.5 |
| 5 | 0.86 | 0.88 | 5 |
| 7 | 0.88 | 0.90 | 7 |
| 12 | 0.90 | 0.91 | 12 |
| 20 | 0.91 | 0.92 | 20 |
| 25 | 0.92 | 0.00 | 25 |
| I | C | 0.00 | 1 |
| 0 | 0.00 | 0.10 | 0 |
| 0 | 0.10 | 0.10 | 0 |
| 1.74 | 0.10 | 0.18 | 1.74 |
| 2 | 0.18 | 0.30 | 2 |
| 2.5 | 0.30 | 0.39 | 2.5 |
| 3 | 0.39 | 0.46 | 3 |


| soil type: | 93 | I: | 0.1 | C: | 0.100 | Lower I <br> 0 <br> Upper I <br> 0.29 | Lower C 0.1 <br> Upper C 0.1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| soil type: | 94 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | Lower I <br> 0 <br> Upper I $0.2$ | Lower C 0.1 <br> Upper C 0.1 |
| soil type: | 95 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | Lower I <br> 0 <br> Upper I <br> 0.22 | Lower C 0.1 <br> Upper C 0.1 |
| soil type: | 96 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | Lower I <br> 0 <br> Upper I <br> 1.74 | Lower C $0.1$ <br> Upper C 0.1 |


|  | 3.5 | 0.46 | 0.51 | 3.5 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | 0.51 | 0.58 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.58 | 0.64 | 5 |  |  |  |  |  |  |  |  |
|  | 6.5 | 0.64 | 0.70 | 6.5 |  |  |  |  |  |  |  |  |
|  | 9 | 0.70 | 0.74 | 9 |  |  |  |  |  |  |  |  |
|  | 12 | 0.74 | 0.77 | 12 |  |  |  |  |  |  |  |  |
|  | 15 | 0.77 | 0.79 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.79 | 0.81 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.81 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 97 | I | C | 0.00 | 1 | soil type: | 97 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.32 | 0.10 | 0.31 | 0.32 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.31 | 0.44 | 0.5 |  |  |  |  |  |  | 0.32 | 0.1 |
|  | 0.75 | 0.44 | 0.52 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1 | 0.52 | 0.61 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.61 | 0.67 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.67 | 0.71 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.71 | 0.75 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.75 | 0.78 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.78 | 0.82 | 4.5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.82 | 0.84 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.84 | 0.87 | 10 |  |  |  |  |  |  |  |  |
|  | 20 | 0.87 | 0.88 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.88 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 98 | 1 | C | 0.00 | 1 | soil type: | 98 | I : | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.25 | 0.10 | 0.44 | 0.25 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.44 | 0.59 | 0.5 |  |  |  |  |  |  | 0.25 | 0.1 |
|  | 0.75 | 0.59 | 0.67 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1 | 0.67 | 0.76 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.76 | 0.80 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.80 | 0.82 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.82 | 0.86 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.86 | 0.88 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.88 | 0.90 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.90 | 0.92 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.92 | 0.95 | 10 |  |  |  |  |  |  |  |  |
|  | 20 | 0.95 | 0.97 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.97 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 99 | I | C | 0.00 | 1 | soil type: | 99 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.28 | 0.10 | 0.43 | 0.28 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.43 | 0.57 | 0.5 |  |  |  |  |  |  | 0.28 | 0.1 |
|  | 0.75 | 0.57 | 0.64 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1 | 0.64 | 0.73 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.73 | 0.78 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.78 | 0.81 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.81 | 0.85 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.85 | 0.88 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.88 | 0.90 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.90 | 0.92 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.92 | 0.94 | 10 |  |  |  |  |  |  |  |  |
|  | 20 | 0.94 | 0.94 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.94 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 100 | I | C | 0.00 | I | soil type: | 100 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.66 | 0.10 | 0.30 | 0.66 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.30 | 0.44 | 1 |  |  |  |  |  |  | 0.66 | 0.1 |
|  | 1.5 | 0.44 | 0.52 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.52 | 0.58 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.58 | 0.66 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.66 | 0.71 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.71 | 0.76 | 4.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.76 | 0.80 | 6 |  |  |  |  |  |  |  |  |


|  | 8 | 0.80 | 0.83 | 8 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 0.83 | 0.87 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.87 | 0.89 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.89 | 0.90 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.90 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 101 | I | C | 0.00 | I | soil type: | 101 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.63 | 0.10 | 0.28 | 0.63 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.28 | 0.39 | 1 |  |  |  |  |  |  | 0.63 | 0.1 |
|  | 1.5 | 0.39 | 0.45 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.45 | 0.50 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.50 | 0.53 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.53 | 0.58 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.58 | 0.63 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.63 | 0.66 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.66 | 0.68 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.68 | 0.71 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.71 | 0.72 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.72 | 0.73 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.73 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 102 | I | C | 0.00 | 1 | soil type: | 102 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.3 | 0.10 | 0.40 | 0.3 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.40 | 0.62 | 0.5 |  |  |  |  |  |  | 0.3 | 0.1 |
|  | 1 | 0.62 | 0.71 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.71 | 0.76 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.76 | 0.79 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.79 | 0.82 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.82 | 0.86 | 3 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.86 | 0.89 | 4.5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.89 | 0.91 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.91 | 0.92 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.92 | 0.93 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.93 | 0.94 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.94 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 103 | I | C | 0.10 | I | soil type: | 103 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.29 | 0.10 | 0.31 | 0.29 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.31 | 0.43 | 0.5 |  |  |  |  |  |  | 0.29 | 0.1 |
|  | 0.75 | 0.43 | 0.51 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1 | 0.51 | 0.61 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.61 | 0.67 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.67 | 0.75 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.75 | 0.81 | 3 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.81 | 0.86 | 4.5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.86 | 0.89 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.89 | 0.92 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.92 | 0.93 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.93 | 0.94 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.94 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 104 | 1 | C | 0.00 | 1 | soil type: | 104 | I : | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.725 | 0.10 | 0.27 | 0.725 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.27 | 0.42 | 1 |  |  |  |  |  |  | 0.725 | 0.1 |
|  | 1.5 | 0.42 | 0.51 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.51 | 0.57 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.57 | 0.62 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.62 | 0.69 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.69 | 0.77 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.77 | 0.81 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.81 | 0.84 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.84 | 0.89 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.89 | 0.91 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.91 | 0.93 | 20 |  |  |  |  |  |  |  |  |


| 25 | 0.93 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I | C | 0.00 | , | soil type: | 105 | I : | 0.1 | C: | 0.100 |  |  |
| 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
| 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
| 0.33 | 0.10 | 0.28 | 0.33 |  |  |  |  |  |  | Upper I | Upper C |
| 0.75 | 0.28 | 0.46 | 0.75 |  |  |  |  |  |  | 0.33 | 0.1 |
| 1.5 | 0.46 | 0.54 | 1.5 |  |  |  |  |  |  |  |  |
| 2 | 0.54 | 0.59 | 2 |  |  |  |  |  |  |  |  |
| 2.5 | 0.59 | 0.63 | 2.5 |  |  |  |  |  |  |  |  |
| 3 | 0.63 | 0.70 | 3 |  |  |  |  |  |  |  |  |
| 4 | 0.70 | 0.74 | 4 |  |  |  |  |  |  |  |  |
| 5 | 0.74 | 0.81 | 5 |  |  |  |  |  |  |  |  |
| 7 | 0.81 | 0.88 | 7 |  |  |  |  |  |  |  |  |
| 10 | 0.88 | 0.94 | 10 |  |  |  |  |  |  |  |  |
| 15 | 0.94 | 0.99 | 15 |  |  |  |  |  |  |  |  |
| 20 | 0.99 | 1.00 | 20 |  |  |  |  |  |  |  |  |
| 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| I | C | 0.00 | I | soil type: | 106 | I : | 0.1 | C: | 0.100 |  |  |
| 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
| 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
| 1.665 | 0.10 | 0.15 | 1.665 |  |  |  |  |  |  | Upper I | Upper C |
| 2 | 0.15 | 0.21 | 2 |  |  |  |  |  |  | 1.665 | 0.1 |
| 2.5 | 0.21 | 0.25 | 2.5 |  |  |  |  |  |  |  |  |
| 3 | 0.25 | 0.31 | 3 |  |  |  |  |  |  |  |  |
| 4 | 0.31 | 0.35 | 4 |  |  |  |  |  |  |  |  |
| 5 | 0.35 | 0.39 | 5 |  |  |  |  |  |  |  |  |
| 6 | 0.39 | 0.41 | 6 |  |  |  |  |  |  |  |  |
| 7 | 0.41 | 0.44 | 7 |  |  |  |  |  |  |  |  |
| 8 | 0.44 | 0.48 | 8 |  |  |  |  |  |  |  |  |
| 10 | 0.48 | 0.54 | 10 |  |  |  |  |  |  |  |  |
| 15 | 0.54 | 0.58 | 15 |  |  |  |  |  |  |  |  |
| 20 | 0.58 | 0.61 | 20 |  |  |  |  |  |  |  |  |
| 25 | 0.61 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| I | C | 0.00 | I | soil type: | 107 | I | 0.1 | C: | 0.100 |  |  |
| 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
| 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
| 0.23 | 0.10 | 0.42 | 0.23 |  |  |  |  |  |  | Upper I | Upper C |
| 0.5 | 0.42 | 0.53 | 0.5 |  |  |  |  |  |  | 0.23 | 0.1 |
| 0.75 | 0.53 | 0.60 | 0.75 |  |  |  |  |  |  |  |  |
| 1 | 0.60 | 0.68 | 1 |  |  |  |  |  |  |  |  |
| 1.5 | 0.68 | 0.73 | 1.5 |  |  |  |  |  |  |  |  |
| 2 | 0.73 | 0.79 | 2 |  |  |  |  |  |  |  |  |
| 3 | 0.79 | 0.82 | 3 |  |  |  |  |  |  |  |  |
| 4 | 0.82 | 0.86 | 4 |  |  |  |  |  |  |  |  |
| 6 | 0.86 | 0.89 | 6 |  |  |  |  |  |  |  |  |
| 10 | 0.89 | 0.91 | 10 |  |  |  |  |  |  |  |  |
| 15 | 0.91 | 0.92 | 15 |  |  |  |  |  |  |  |  |
| 20 | 0.92 | 0.92 | 20 |  |  |  |  |  |  |  |  |
| 25 | 0.92 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| I | C | 0.00 | I | soil type: | 108 | I: | 0.1 | C: | 0.100 |  |  |
| 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
| 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0.1 | 0.1 |
| 0.1 | 0.10 | 0.49 | 0.1 |  |  |  |  |  |  | Upper I | Upper C |
| 0.25 | 0.49 | 0.61 | 0.25 |  |  |  |  |  |  | 0.25 | 0.48964 |
| 0.5 | 0.61 | 0.70 | 0.5 |  |  |  |  |  |  |  |  |
| 1 | 0.70 | 0.75 | 1 |  |  |  |  |  |  |  |  |
| 1.5 | 0.75 | 0.78 | 1.5 |  |  |  |  |  |  |  |  |
| 2 | 0.78 | 0.82 | 2 |  |  |  |  |  |  |  |  |
| 3 | 0.82 | 0.87 | 3 |  |  |  |  |  |  |  |  |
| 5 | 0.87 | 0.89 | 5 |  |  |  |  |  |  |  |  |
| 7 | 0.89 | 0.92 | 7 |  |  |  |  |  |  |  |  |
| 10 | 0.92 | 0.94 | 10 |  |  |  |  |  |  |  |  |
| 15 | 0.94 | 0.95 | 15 |  |  |  |  |  |  |  |  |
| 20 | 0.95 | 0.95 | 20 |  |  |  |  |  |  |  |  |
| 25 | 0.95 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 1 | C | 0.00 | 1 | soil type: | 109 | I: | 0.1 | C: | 0.100 |  |  |
| 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
| 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |


|  | 0.3 | 0.10 | 0.35 | 0.3 |  |  |  |  |  |  | Upper I | Upper C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.5 | 0.35 | 0.56 | 0.5 |  |  |  |  |  |  | 0.3 | 0.1 |
|  | 1 | 0.56 | 0.65 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.65 | 0.70 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.70 | 0.73 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.73 | 0.77 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.77 | 0.81 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.81 | 0.83 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.83 | 0.85 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.85 | 0.87 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.87 | 0.88 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.88 | 0.88 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.88 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 110 | I | C | 0.00 | 1 | soil type: | 110 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0.1 | 0.1 |
|  | 0.1 | 0.10 | 0.46 | 0.1 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.25 | 0.46 | 0.66 | 0.25 |  |  |  |  |  |  | 0.25 | 0.456878 |
|  | 0.6 | 0.66 | 0.75 | 0.6 |  |  |  |  |  |  |  |  |
|  | 1 | 0.75 | 0.80 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.80 | 0.82 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.82 | 0.84 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.84 | 0.87 | 2.5 |  |  |  |  |  |  |  |  |
|  | 4 | 0.87 | 0.88 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.88 | 0.90 | 5 |  |  |  |  |  |  |  |  |
|  | 10 | 0.90 | 0.90 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.90 | 0.91 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.91 | 0.91 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.91 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 111 | I | C | 0.00 | 1 | soil type: | 111 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.385 | 0.10 | 0.39 | 0.385 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.39 | 0.48 | 0.75 |  |  |  |  |  |  | 0.385 | 0.1 |
|  | 1 | 0.48 | 0.58 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.58 | 0.64 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.64 | 0.72 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.72 | 0.76 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.76 | 0.81 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.81 | 0.83 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.83 | 0.85 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.85 | 0.87 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.87 | 0.88 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.88 | 0.89 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.89 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 112 | I | C | 0.00 | I | soil type: | 112 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.28 | 0.10 | 0.42 | 0.28 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.42 | 0.63 | 0.5 |  |  |  |  |  |  | 0.28 | 0.1 |
|  | 1 | 0.63 | 0.71 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.71 | 0.76 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.76 | 0.82 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.82 | 0.84 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.84 | 0.86 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.86 | 0.88 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.88 | 0.90 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.90 | 0.92 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.92 | 0.92 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.92 | 0.93 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.93 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 113 | I | C | 0.00 | I | soil type: | 113 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.25 | 0.10 | 0.34 | 0.25 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.34 | 0.52 | 0.5 |  |  |  |  |  |  | 0.25 | 0.1 |
|  | 1 | 0.52 | 0.62 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.62 | 0.68 | 1.5 |  |  |  |  |  |  |  |  |


|  | 2 | 0.68 | 0.76 | 2 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3 | 0.76 | 0.80 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.80 | 0.84 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.84 | 0.88 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.88 | 0.91 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.91 | 0.94 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.94 | 0.95 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.95 | 0.96 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.96 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 114 | 1 | C | 0.00 | I | soil type: | 114 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.35 | 0.10 | 0.29 | 0.35 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.29 | 0.36 | 0.75 |  |  |  |  |  |  | 0.35 | 0.1 |
|  | 1 | 0.36 | 0.46 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.46 | 0.53 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.53 | 0.63 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.63 | 0.69 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.69 | 0.75 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.75 | 0.82 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.82 | 0.89 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.89 | 0.95 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.95 | 0.99 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 115 | I | C | 0.00 | I | soil type: | 115 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.22 | 0.10 | 0.42 | 0.22 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.42 | 0.53 | 0.5 |  |  |  |  |  |  | 0.22 | 0.1 |
|  | 0.75 | 0.53 | 0.59 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1 | 0.59 | 0.68 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.68 | 0.77 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.77 | 0.81 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.81 | 0.85 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.85 | 0.88 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.88 | 0.90 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.90 | 0.92 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.92 | 0.92 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.92 | 0.93 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.93 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 116 | I | C | 0.00 | 1 | soil type: | 116 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.72 | 0.10 | 0.29 | 0.72 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.29 | 0.44 | 1 |  |  |  |  |  |  | 0.72 | 0.1 |
|  | 1.5 | 0.44 | 0.52 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.52 | 0.57 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.57 | 0.61 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.61 | 0.66 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.66 | 0.72 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.72 | 0.76 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.76 | 0.78 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.78 | 0.81 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.81 | 0.82 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.82 | 0.83 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.83 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 117 | I | C | 0.00 | I | soil type: | 117 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0.1 | 0.1 |
|  | 0.1 | 0.10 | 0.52 | 0.1 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.3 | 0.52 | 0.68 | 0.3 |  |  |  |  |  |  | 0.3 | 0.524112 |
|  | 0.6 | 0.68 | 0.77 | 0.6 |  |  |  |  |  |  |  |  |
|  | 1 | 0.77 | 0.82 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.82 | 0.85 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.85 | 0.87 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.87 | 0.89 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.89 | 0.91 | 3.5 |  |  |  |  |  |  |  |  |


|  | 5 | 0.91 | 0.93 | 5 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 0.93 | 0.93 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.93 | 0.94 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.94 | 0.94 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.94 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 118 | 1 | C | 0.00 | 1 | soil type: | 118 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.58 | 0.10 | 0.39 | 0.58 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.39 | 0.52 | 1 |  |  |  |  |  |  | 0.58 | 0.1 |
|  | 1.5 | 0.52 | 0.60 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.60 | 0.66 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.66 | 0.70 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.70 | 0.76 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.76 | 0.79 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.79 | 0.84 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.84 | 0.88 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.88 | 0.91 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.91 | 0.93 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.93 | 0.94 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.94 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 119 | I | C | 0.00 | I | soil type: | 119 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.77 | 0.10 | 0.31 | 0.77 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.5 | 0.31 | 0.42 | 1.5 |  |  |  |  |  |  | 0.77 | 0.1 |
|  | 2 | 0.42 | 0.50 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.50 | 0.56 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.56 | 0.64 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.64 | 0.70 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.70 | 0.74 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.74 | 0.79 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.79 | 0.82 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.82 | 0.87 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.87 | 0.90 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.90 | 0.91 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.91 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 120 | 1 | C | 0.00 | 1 | soil type: | 120 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.65 | 0.10 | 0.32 | 0.65 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.32 | 0.46 | 1 |  |  |  |  |  |  | 0.65 | 0.1 |
|  | 1.5 | 0.46 | 0.55 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.55 | 0.60 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.60 | 0.68 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.68 | 0.74 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.74 | 0.79 | 4.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.79 | 0.83 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.83 | 0.86 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.86 | 0.90 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.90 | 0.92 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.92 | 0.94 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.94 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 121 | I | C | 0.00 | I | soil type: | 121 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 3.7 | 0.10 | 0.17 | 3.7 |  |  |  |  |  |  | Upper I | Upper C |
|  | 4 | 0.17 | 0.29 | 4 |  |  |  |  |  |  | 3.7 | 0.1 |
|  | 5 | 0.29 | 0.38 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.38 | 0.46 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.46 | 0.52 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.52 | 0.57 | 8 |  |  |  |  |  |  |  |  |
|  | 9 | 0.57 | 0.61 | 9 |  |  |  |  |  |  |  |  |
|  | 10 | 0.61 | 0.67 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.67 | 0.71 | 12 |  |  |  |  |  |  |  |  |
|  | 14 | 0.71 | 0.75 | 14 |  |  |  |  |  |  |  |  |
|  | 16 | 0.75 | 0.80 | 16 |  |  |  |  |  |  |  |  |
|  | 20 | 0.80 | 0.94 | 20 |  |  |  |  |  |  |  |  |


|  | 25 | 0.94 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 122 | 1 | C | 0.00 | 1 | soil type: | 122 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.82 | 0.10 | 0.29 | 0.82 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.5 | 0.29 | 0.39 | 1.5 |  |  |  |  |  |  | 0.82 | 0.1 |
|  | 2 | 0.39 | 0.47 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.47 | 0.53 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.53 | 0.61 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.61 | 0.67 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.67 | 0.71 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.71 | 0.77 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.77 | 0.81 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.81 | 0.86 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.86 | 0.89 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.89 | 0.91 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.91 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 123 | I | C | 0.00 | I | soil type: | 123 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.12 | 0.10 | 0.48 | 0.12 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.48 | 0.63 | 0.5 |  |  |  |  |  |  | 0.12 | 0.1 |
|  | 1 | 0.63 | 0.71 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.71 | 0.76 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.76 | 0.79 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.79 | 0.85 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.75 | 0.85 | 0.87 | 3.75 |  |  |  |  |  |  |  |  |
|  | 5 | 0.87 | 0.89 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.89 | 0.92 | 6 |  |  |  |  |  |  |  |  |
|  | 10 | 0.92 | 0.94 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.94 | 0.95 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.95 | 0.96 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.96 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 124 | I | C | 0.00 | I | soil type: | 124 | I : | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1.4 | 0.10 | 0.21 | 1.4 |  |  |  |  |  |  | Upper I | Upper C |
|  | 2 | 0.21 | 0.29 | 2 |  |  |  |  |  |  | 1.4 | 0.1 |
|  | 2.5 | 0.29 | 0.36 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.36 | 0.47 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.47 | 0.56 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.56 | 0.62 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.62 | 0.67 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.67 | 0.71 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.71 | 0.77 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.77 | 0.83 | 10 |  |  |  |  |  |  |  |  |
|  | 13 | 0.83 | 0.91 | 13 |  |  |  |  |  |  |  |  |
|  | 20 | 0.91 | 0.94 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.94 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 125 | 1 | C | 0.00 | 1 | soil type: | 125 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 2.82 | 0.10 | 0.22 | 2.82 |  |  |  |  |  |  | Upper I | Upper C |
|  | 3.5 | 0.22 | 0.37 | 3.5 |  |  |  |  |  |  | 2.82 | 0.1 |
|  | 4.5 | 0.37 | 0.42 | 4.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.42 | 0.51 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.51 | 0.58 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.58 | 0.63 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.63 | 0.67 | 8 |  |  |  |  |  |  |  |  |
|  | 9 | 0.67 | 0.70 | 9 |  |  |  |  |  |  |  |  |
|  | 10 | 0.70 | 0.75 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.75 | 0.80 | 12 |  |  |  |  |  |  |  |  |
|  | 15 | 0.80 | 0.85 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.85 | 0.88 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.88 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 126 | 1 | C | 0.00 | 1 | soil type: | 126 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |


|  | 0.68 | 0.10 | 0.27 | 0.68 |  |  |  |  |  |  | Upper I | Upper C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 0.27 | 0.41 | 1 |  |  |  |  |  |  | 0.68 | 0.1 |
|  | 1.5 | 0.41 | 0.49 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.49 | 0.56 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.56 | 0.61 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.61 | 0.68 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.68 | 0.74 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.74 | 0.82 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.82 | 0.89 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.89 | 0.95 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.95 | 0.99 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 127 | 1 | C | 0.00 | 1 | soil type: | 127 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1.42 | 0.10 | 0.23 | 1.42 |  |  |  |  |  |  | Upper I | Upper C |
|  | 2 | 0.23 | 0.38 | 2 |  |  |  |  |  |  | 1.42 | 0.1 |
|  | 3 | 0.38 | 0.49 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.49 | 0.57 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.57 | 0.62 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.62 | 0.67 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.67 | 0.70 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.70 | 0.75 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.75 | 0.79 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.79 | 0.83 | 12 |  |  |  |  |  |  |  |  |
|  | 15 | 0.83 | 0.87 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.87 | 0.90 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.90 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 128 | I | C | 0.00 | 1 | soil type: | 128 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1.52 | 0.10 | 0.24 | 1.52 |  |  |  |  |  |  | Upper I | Upper C |
|  | 2 | 0.24 | 0.39 | 2 |  |  |  |  |  |  | 1.52 | 0.1 |
|  | 3 | 0.39 | 0.49 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.49 | 0.56 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.56 | 0.62 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.62 | 0.67 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.67 | 0.71 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.71 | 0.78 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.78 | 0.84 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.84 | 0.93 | 12 |  |  |  |  |  |  |  |  |
|  | 16 | 0.93 | 0.99 | 16 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 129 | I | C | 0.00 | I | soil type: | 129 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1.02 | 0.10 | 0.20 | 1.02 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.5 | 0.20 | 0.29 | 1.5 |  |  |  |  |  |  | 1.02 | 0.1 |
|  | 2 | 0.29 | 0.37 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.37 | 0.44 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.44 | 0.54 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.54 | 0.62 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.62 | 0.68 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.68 | 0.76 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.76 | 0.82 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.82 | 0.89 | 10 |  |  |  |  |  |  |  |  |
|  | 14 | 0.89 | 0.95 | 14 |  |  |  |  |  |  |  |  |
|  | 20 | 0.95 | 0.98 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.98 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 130 | I | C | 0.00 | 1 | soil type: | 130 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 2.06 | 0.10 | 0.17 | 2.06 |  |  |  |  |  |  | Upper I | Upper C |
|  | 2.5 | 0.17 | 0.23 | 2.5 |  |  |  |  |  |  | 2.06 | 0.1 |
|  | 3 | 0.23 | 0.27 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.27 | 0.31 | 3.5 |  |  |  |  |  |  |  |  |


|  | 4 | 0.31 | 0.36 | 4 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 5 | 0.36 | 0.40 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.40 | 0.43 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.43 | 0.45 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.45 | 0.48 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.48 | 0.52 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.52 | 0.54 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.54 | 0.55 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.55 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 131 | 1 | C | 0.00 | I | soil type: | 131 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 3.27 | 0.10 | 0.19 | 3.27 |  |  |  |  |  |  | Upper I | Upper C |
|  | 4 | 0.19 | 0.31 | 4 |  |  |  |  |  |  | 3.27 | 0.1 |
|  | 5 | 0.31 | 0.41 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.41 | 0.48 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.48 | 0.54 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.54 | 0.59 | 8 |  |  |  |  |  |  |  |  |
|  | 9 | 0.59 | 0.63 | 9 |  |  |  |  |  |  |  |  |
|  | 10 | 0.63 | 0.69 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.69 | 0.73 | 12 |  |  |  |  |  |  |  |  |
|  | 14 | 0.73 | 0.77 | 14 |  |  |  |  |  |  |  |  |
|  | 16 | 0.77 | 0.82 | 16 |  |  |  |  |  |  |  |  |
|  | 20 | 0.82 | 0.86 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.86 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 132 | I | C | 0.00 | I | soil type: | 132 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 4 | 0.10 | 0.15 | 4 |  |  |  |  |  |  | Upper I | Upper C |
|  | 4.5 | 0.15 | 0.27 | 4.5 |  |  |  |  |  |  | 4 | 0.1 |
|  | 5.5 | 0.27 | 0.31 | 5.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.31 | 0.35 | 6 |  |  |  |  |  |  |  |  |
|  | 6.5 | 0.35 | 0.38 | 6.5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.38 | 0.40 | 7 |  |  |  |  |  |  |  |  |
|  | 7.5 | 0.40 | 0.43 | 7.5 |  |  |  |  |  |  |  |  |
|  | 8.5 | 0.43 | 0.45 | 8.5 |  |  |  |  |  |  |  |  |
|  | 10 | 0.45 | 0.46 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.46 | 0.47 | 12 |  |  |  |  |  |  |  |  |
|  | 14 | 0.47 | 0.48 | 14 |  |  |  |  |  |  |  |  |
|  | 20 | 0.48 | 0.48 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.48 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 133 | I | C | 0.00 | 1 | soil type: | 133 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.28 | 0.10 | 0.46 | 0.28 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.46 | 0.55 | 0.75 |  |  |  |  |  |  | 0.28 | 0.1 |
|  | 1 | 0.55 | 0.66 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.66 | 0.72 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.72 | 0.76 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.76 | 0.79 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.79 | 0.83 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.83 | 0.85 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.85 | 0.86 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.86 | 0.89 | 6 |  |  |  |  |  |  |  |  |
|  | 10 | 0.89 | 0.92 | 10 |  |  |  |  |  |  |  |  |
|  | 20 | 0.92 | 0.92 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.92 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 134 | I | C | 0.00 | I | soil type: | 134 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1.2 | 0.10 | 0.26 | 1.2 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.75 | 0.26 | 0.39 | 1.75 |  |  |  |  |  |  | 1.2 | 0.1 |
|  | 2.5 | 0.39 | 0.45 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.45 | 0.50 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.50 | 0.54 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4 | 0.54 | 0.61 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.61 | 0.66 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.66 | 0.75 | 6 |  |  |  |  |  |  |  |  |


|  | 8 | 0.75 | 0.81 | 8 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 0.81 | 0.88 | 10 |  |  |  |  |  |  |  |  |
|  | 13 | 0.88 | 0.99 | 13 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 135 | I | C | 0.00 | I | soil type: | 135 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.37 | 0.10 | 0.33 | 0.37 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.33 | 0.59 | 0.5 |  |  |  |  |  |  | 0.37 | 0.1 |
|  | 1 | 0.59 | 0.69 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.69 | 0.74 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.74 | 0.81 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.81 | 0.84 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.84 | 0.88 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.88 | 0.89 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.89 | 0.91 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.91 | 0.92 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.92 | 0.93 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.93 | 0.93 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.93 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 136 | I | C | 0.00 | I | soil type: | 136 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 2.2 | 0.10 | 0.20 | 2.2 |  |  |  |  |  |  | Upper I | Upper C |
|  | 2.5 | 0.20 | 0.30 | 2.5 |  |  |  |  |  |  | 2.2 | 0.1 |
|  | 3 | 0.30 | 0.36 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.36 | 0.41 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4 | 0.41 | 0.45 | 4 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.45 | 0.51 | 4.5 |  |  |  |  |  |  |  |  |
|  | 5.5 | 0.51 | 0.58 | 5.5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.58 | 0.64 | 7 |  |  |  |  |  |  |  |  |
|  | 9 | 0.64 | 0.70 | 9 |  |  |  |  |  |  |  |  |
|  | 12 | 0.70 | 0.74 | 12 |  |  |  |  |  |  |  |  |
|  | 15 | 0.74 | 0.78 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.78 | 0.81 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.81 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 137 | 1 | C | 0.00 | 1 | soil type: | 137 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.3 | 0.10 | 0.37 | 0.3 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.37 | 0.47 | 0.75 |  |  |  |  |  |  | 0.3 | 0.1 |
|  | 1 | 0.47 | 0.59 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.59 | 0.66 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.66 | 0.70 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.70 | 0.74 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.74 | 0.80 | 3 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.80 | 0.84 | 4.5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.84 | 0.86 | 7 |  |  |  |  |  |  |  |  |
|  | 9 | 0.86 | 0.89 | 9 |  |  |  |  |  |  |  |  |
|  | 15 | 0.89 | 0.90 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.90 | 0.90 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.90 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 138 | I | C | 0.00 | 1 | soil type: | 138 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.97 | 0.10 | 0.35 | 0.97 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.5 | 0.35 | 0.48 | 1.5 |  |  |  |  |  |  | 0.97 | 0.1 |
|  | 2 | 0.48 | 0.55 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.55 | 0.60 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.60 | 0.67 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.67 | 0.71 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.71 | 0.75 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.75 | 0.76 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.76 | 0.78 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.78 | 0.81 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.81 | 0.82 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.82 | 0.83 | 20 |  |  |  |  |  |  |  |  |


|  | 25 | 0.83 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 139 | 1 | C | 0.00 | I | soil type: | 139 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.13 | 0.10 | 0.48 | 0.13 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.48 | 0.64 | 0.5 |  |  |  |  |  |  | 0.13 | 0.1 |
|  | 1 | 0.64 | 0.73 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.73 | 0.78 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.78 | 0.84 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.84 | 0.88 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.88 | 0.92 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.92 | 0.95 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.95 | 0.96 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.96 | 0.98 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.98 | 0.99 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 140 | I | C | 0.00 | 1 | soil type: | 140 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.73 | 0.10 | 0.33 | 0.73 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.33 | 0.53 | 1 |  |  |  |  |  |  | 0.73 | 0.1 |
|  | 1.5 | 0.53 | 0.63 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.63 | 0.69 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.69 | 0.73 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.73 | 0.78 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.78 | 0.82 | 4 |  |  |  |  |  |  |  |  |
|  | 5.5 | 0.82 | 0.85 | 5.5 |  |  |  |  |  |  |  |  |
|  | 7.5 | 0.85 | 0.87 | 7.5 |  |  |  |  |  |  |  |  |
|  | 10 | 0.87 | 0.88 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.88 | 0.89 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.89 | 0.90 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.90 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 141 | I | C | 0.00 | I | soil type: | 141 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.52 | 0.10 | 0.39 | 0.52 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.39 | 0.55 | 1 |  |  |  |  |  |  | 0.52 | 0.1 |
|  | 1.5 | 0.55 | 0.63 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.63 | 0.68 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.68 | 0.72 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.72 | 0.76 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.76 | 0.80 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.80 | 0.82 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.82 | 0.84 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.84 | 0.85 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.85 | 0.86 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.86 | 0.87 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.87 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 142 | I | C | 0.00 | I | soil type: | 142 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.53 | 0.10 | 0.34 | 0.53 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.34 | 0.46 | 0.75 |  |  |  |  |  |  | 0.53 | 0.1 |
|  | 1 | 0.46 | 0.59 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.59 | 0.67 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.67 | 0.72 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.72 | 0.78 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.78 | 0.84 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.84 | 0.88 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.88 | 0.91 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.91 | 0.94 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.94 | 0.95 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.95 | 0.96 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.96 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 143 | I | C | 0.00 | I | soil type: | 143 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |


|  | 1.5 | 0.10 | 0.27 | 1.5 |
| :---: | :---: | :---: | :---: | :---: |
|  | 2 | 0.27 | 0.37 | 2 |
|  | 2.5 | 0.37 | 0.44 | 2.5 |
|  | 3 | 0.44 | 0.49 | 3 |
|  | 3.5 | 0.49 | 0.53 | 3.5 |
|  | 4 | 0.53 | 0.58 | 4 |
|  | 5 | 0.58 | 0.62 | 5 |
|  | 6 | 0.62 | 0.66 | 6 |
|  | 8 | 0.66 | 0.69 | 8 |
|  | 10 | 0.69 | 0.70 | 10 |
|  | 12 | 0.70 | 0.74 | 12 |
|  | 20 | 0.74 | 0.75 | 20 |
|  | 25 | 0.75 | 0.00 | 25 |
| 144 | I | C | 0.00 | 1 |
|  | 0 | 0.00 | 0.10 | 0 |
|  | 0 | 0.10 | 0.10 | 0 |
|  | 1.17 | 0.10 | 0.26 | 1.17 |
|  | 1.5 | 0.26 | 0.41 | 1.5 |
|  | 2 | 0.41 | 0.50 | 2 |
|  | 2.5 | 0.50 | 0.57 | 2.5 |
|  | 3 | 0.57 | 0.64 | 3 |
|  | 4 | 0.64 | 0.69 | 4 |
|  | 5 | 0.69 | 0.72 | 5 |
|  | 6 | 0.72 | 0.76 | 6 |
|  | 8 | 0.76 | 0.78 | 8 |
|  | 10 | 0.78 | 0.81 | 10 |
|  | 15 | 0.81 | 0.83 | 15 |
|  | 20 | 0.83 | 0.84 | 20 |
|  | 25 | 0.84 | 0.00 | 25 |
| 145 | 1 | C | 0.00 | 1 |
|  | 0 | 0.00 | 0.10 | 0 |
|  | 0 | 0.10 | 0.10 | 0 |
|  | 2.69 | 0.10 | 0.16 | 2.69 |
|  | 3 | 0.16 | 0.23 | 3 |
|  | 3.5 | 0.23 | 0.28 | 3.5 |
|  | 4 | 0.28 | 0.35 | 4 |
|  | 5 | 0.35 | 0.41 | 5 |
|  | 6 | 0.41 | 0.45 | 6 |
|  | 7 | 0.45 | 0.48 | 7 |
|  | 8 | 0.48 | 0.54 | 8 |
|  | 10 | 0.54 | 0.58 | 10 |
|  | 12 | 0.58 | 0.63 | 12 |
|  | 15 | 0.63 | 0.68 | 15 |
|  | 20 | 0.68 | 0.72 | 20 |
|  | 25 | 0.72 | 0.00 | 25 |
| 146 | I | C | 0.00 | I |
|  | 0 | 0.00 | 0.10 | 0 |
|  | 0 | 0.10 | 0.10 | 0 |
|  | 0.7 | 0.10 | 0.32 | 0.7 |
|  | 1 | 0.32 | 0.49 | 1 |
|  | 1.5 | 0.49 | 0.59 | 1.5 |
|  | 2 | 0.59 | 0.64 | 2 |
|  | 2.5 | 0.64 | 0.70 | 2.5 |
|  | 3.5 | 0.70 | 0.74 | 3.5 |
|  | 4.5 | 0.74 | 0.76 | 4.5 |
|  | 6 | 0.76 | 0.79 | 6 |
|  | 8 | 0.79 | 0.80 | 8 |
|  | 10 | 0.80 | 0.82 | 10 |
|  | 15 | 0.82 | 0.83 | 15 |
|  | 20 | 0.83 | 0.83 | 20 |
|  | 25 | 0.83 | 0.00 | 25 |
| 147 | I | C | 0.00 | I |
|  | 0 | 0.00 | 0.10 | 0 |
|  | 0 | 0.10 | 0.10 | 0 |
|  | 0.8 | 0.10 | 0.24 | 0.8 |
|  | 1 | 0.24 | 0.47 | 1 |
|  | 1.5 | 0.47 | 0.59 | 1.5 |
|  | 2 | 0.59 | 0.66 | 2 |



|  | 2.5 | 0.66 | 0.73 | 2.5 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3.25 | 0.73 | 0.79 | 3.25 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.79 | 0.84 | 4.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.84 | 0.87 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.87 | 0.88 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.88 | 0.91 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.91 | 0.92 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.92 | 0.93 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.93 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 148 | I | C | 0.00 | I | soil type: | 148 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.8 | 0.10 | 0.23 | 0.8 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.23 | 0.41 | 1 |  |  |  |  |  |  | 0.8 | 0.1 |
|  | 1.5 | 0.41 | 0.51 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.51 | 0.57 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.57 | 0.63 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.25 | 0.63 | 0.68 | 3.25 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.68 | 0.71 | 4.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.71 | 0.74 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.74 | 0.75 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.75 | 0.77 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.77 | 0.78 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.78 | 0.79 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.79 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 149 | I | C | 0.00 | 1 | soil type: | 149 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1.62 | 0.10 | 0.26 | 1.62 |  |  |  |  |  |  | Upper I | Upper C |
|  | 2 | 0.26 | 0.36 | 2 |  |  |  |  |  |  | 1.62 | 0.1 |
|  | 2.5 | 0.36 | 0.43 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.43 | 0.48 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.48 | 0.52 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4 | 0.52 | 0.58 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.58 | 0.62 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.62 | 0.68 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.68 | 0.72 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.72 | 0.77 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.77 | 0.80 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.80 | 0.82 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.82 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 150 | I | C | 0.00 | 1 | soil type: | 150 | l | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1.72 | 0.10 | 0.21 | 1.72 |  |  |  |  |  |  | Upper I | Upper C |
|  | 2 | 0.21 | 0.35 | 2 |  |  |  |  |  |  | 1.72 | 0.1 |
|  | 2.5 | 0.35 | 0.44 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.44 | 0.50 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.50 | 0.55 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4 | 0.55 | 0.61 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.61 | 0.65 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.65 | 0.70 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.70 | 0.74 | 8 |  |  |  |  |  |  |  |  |
|  | 11 | 0.74 | 0.77 | 11 |  |  |  |  |  |  |  |  |
|  | 15 | 0.77 | 0.79 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.79 | 0.91 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.91 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 151 | I | C | 0.00 | 1 | soil type: | 151 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.27 | 0.10 | 0.42 | 0.27 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.42 | 0.59 | 0.5 |  |  |  |  |  |  | 0.27 | 0.1 |
|  | 0.75 | 0.59 | 0.67 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1 | 0.67 | 0.76 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.76 | 0.80 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.80 | 0.84 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.84 | 0.86 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.86 | 0.88 | 4 |  |  |  |  |  |  |  |  |


|  | 6 | 0.88 | 0.89 | 6 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 0.89 | 0.90 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.90 | 0.91 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.91 | 0.91 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.91 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 152 | I | C | 0.00 | 1 | soil type: | 152 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.43 | 0.10 | 0.45 | 0.43 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.45 | 0.58 | 0.75 |  |  |  |  |  |  | 0.43 | 0.1 |
|  | 1 | 0.58 | 0.71 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.71 | 0.77 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.77 | 0.84 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.84 | 0.87 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.87 | 0.90 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.90 | 0.91 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.91 | 0.92 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.92 | 0.93 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.93 | 0.94 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.94 | 0.94 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.94 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 153 | I | C | 0.00 | I | soil type: | 153 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1.9 | 0.10 | 0.18 | 1.9 |  |  |  |  |  |  | Upper I | Upper C |
|  | 2 | 0.18 | 0.40 | 2 |  |  |  |  |  |  | 1.9 | 0.1 |
|  | 2.5 | 0.40 | 0.51 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.51 | 0.59 | 3 |  |  |  |  |  |  |  |  |
|  | 3.75 | 0.59 | 0.66 | 3.75 |  |  |  |  |  |  |  |  |
|  | 5 | 0.66 | 0.69 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.69 | 0.71 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.71 | 0.72 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.72 | 0.74 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.74 | 0.76 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.76 | 0.77 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.77 | 0.77 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.77 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 154 | 1 | C | 0.00 | 1 | soil type: | 154 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.38 | 0.10 | 0.32 | 0.38 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.32 | 0.49 | 0.5 |  |  |  |  |  |  | 0.38 | 0.1 |
|  | 0.75 | 0.49 | 0.58 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1 | 0.58 | 0.67 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.67 | 0.73 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.73 | 0.79 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.79 | 0.84 | 3 |  |  |  |  |  |  |  |  |
|  | 5 | 0.84 | 0.86 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.86 | 0.88 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.88 | 0.90 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.90 | 0.90 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.90 | 0.91 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.91 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 155 | I | C | 0.00 | 1 | soil type: | 155 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.3 | 0.10 | 0.26 | 0.3 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.26 | 0.33 | 0.75 |  |  |  |  |  |  | 0.3 | 0.1 |
|  | 1 | 0.33 | 0.53 | 1 |  |  |  |  |  |  |  |  |
|  | 2 | 0.53 | 0.65 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.65 | 0.73 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.73 | 0.78 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.78 | 0.82 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.82 | 0.88 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.88 | 0.91 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.91 | 0.96 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.96 | 0.99 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 1.00 | 20 |  |  |  |  |  |  |  |  |


|  | 25 | 1.00 | 0.00 | 25 |
| :---: | :---: | :---: | :---: | :---: |
| 156 | 1 | C | 0.00 | I |
|  | 0 | 0.00 | 0.10 | 0 |
|  | 0 | 0.10 | 0.10 | 0 |
|  | 0.45 | 0.10 | 0.28 | 0.45 |
|  | 1 | 0.28 | 0.54 | 1 |
|  | 2 | 0.54 | 0.70 | 2 |
|  | 3 | 0.70 | 0.75 | 3 |
|  | 3.5 | 0.75 | 0.79 | 3.5 |
|  | 4 | 0.79 | 0.81 | 4 |
|  | 4.5 | 0.81 | 0.84 | 4.5 |
|  | 5.5 | 0.84 | 0.86 | 5.5 |
|  | 7 | 0.86 | 0.88 | 7 |
|  | 10 | 0.88 | 0.90 | 10 |
|  | 15 | 0.90 | 0.92 | 15 |
|  | 20 | 0.92 | 0.93 | 20 |
|  | 25 | 0.93 | 0.00 | 25 |
| 157 | I | C | 0.00 | I |
|  | 0 | 0.00 | 0.10 | 0 |
|  | 0 | 0.10 | 0.10 | 0 |
|  | 1.5 | 0.10 | 0.30 | 1.5 |
|  | 2 | 0.30 | 0.41 | 2 |
|  | 2.5 | 0.41 | 0.47 | 2.5 |
|  | 3 | 0.47 | 0.51 | 3 |
|  | 3.5 | 0.51 | 0.54 | 3.5 |
|  | 4 | 0.54 | 0.56 | 4 |
|  | 4.5 | 0.56 | 0.60 | 4.5 |
|  | 6 | 0.60 | 0.63 | 6 |
|  | 8 | 0.63 | 0.64 | 8 |
|  | 10 | 0.64 | 0.66 | 10 |
|  | 15 | 0.66 | 0.67 | 15 |
|  | 20 | 0.67 | 0.68 | 20 |
|  | 25 | 0.68 | 0.00 | 25 |
| 158 | I | C | 0.00 | 1 |
|  | 0 | 0.00 | 0.10 | 0 |
|  | 0 | 0.10 | 0.10 | 0 |
|  | 0.55 | 0.10 | 0.30 | 0.55 |
|  | 1 | 0.30 | 0.42 | 1 |
|  | 1.5 | 0.42 | 0.49 | 1.5 |
|  | 2 | 0.49 | 0.55 | 2 |
|  | 2.5 | 0.55 | 0.63 | 2.5 |
|  | 3.5 | 0.63 | 0.69 | 3.5 |
|  | 4.5 | 0.69 | 0.75 | 4.5 |
|  | 6 | 0.75 | 0.80 | 6 |
|  | 8 | 0.80 | 0.87 | 8 |
|  | 12 | 0.87 | 0.90 | 12 |
|  | 15 | 0.90 | 0.93 | 15 |
|  | 20 | 0.93 | 0.95 | 20 |
|  | 25 | 0.95 | 0.00 | 25 |
| 159 | 1 | C | 0.00 | I |
|  | 0 | 0.00 | 0.10 | 0 |
|  | 0 | 0.10 | 0.10 | 0 |
|  | 0.5 | 0.10 | 0.31 | 0.5 |
|  | 1 | 0.31 | 0.45 | 1 |
|  | 1.5 | 0.45 | 0.54 | 1.5 |
|  | 2 | 0.54 | 0.61 | 2 |
|  | 2.5 | 0.61 | 0.67 | 2.5 |
|  | 3 | 0.67 | 0.73 | 3 |
|  | 4 | 0.73 | 0.77 | 4 |
|  | 5 | 0.77 | 0.80 | 5 |
|  | 7 | 0.80 | 0.83 | 7 |
|  | 10 | 0.83 | 0.84 | 10 |
|  | 15 | 0.84 | 0.84 | 15 |
|  | 20 | 0.84 | 0.85 | 20 |
|  | 25 | 0.85 | 0.00 | 25 |
| 160 | 1 | C | 0.00 | I |
|  | 0 | 0.00 | 0.10 | 0 |
|  | 0 | 0.10 | 0.10 | 0 |


| soil type: | 156 | I: | 0.1 | C: | 0.100 | Lower I <br> 0 <br> Upper I <br> 0.45 | Lower C $0.1$ <br> Upper C 0.1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| soil type: | 157 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | Lower I <br> 0 <br> Upper I $1.5$ | Lower C 0.1 <br> Upper C 0.1 |
| soil type: | 158 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | Lower I <br> 0 <br> Upper I 0.55 | Lower C 0.1 Upper C 0.1 |
| soil type: | 159 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | Lower I <br> 0 <br> Upper I $0.5$ | Lower C $0.1$ <br> Upper C 0.1 |
| soil type: | 160 | I: | 0.1 | C: | 0.100 |  |  |
|  |  |  |  |  |  | Lower I 0 | $\begin{gathered} \text { Lower C } \\ 0.1 \end{gathered}$ |


|  | 1.72 | 0.10 | 0.14 | 1.72 |  |  |  |  |  |  | Upper I | Upper C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2 | 0.14 | 0.30 | 2 |  |  |  |  |  |  | 1.72 | 0.1 |
|  | 3 | 0.30 | 0.42 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.42 | 0.51 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.51 | 0.58 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.58 | 0.64 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.64 | 0.69 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.69 | 0.76 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.76 | 0.81 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.81 | 0.87 | 12 |  |  |  |  |  |  |  |  |
|  | 15 | 0.87 | 0.93 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.93 | 0.97 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.97 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 161 | 1 | C | 0.00 | 1 | soil type: | 161 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1 | 0.10 | 0.22 | 1 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.5 | 0.22 | 0.39 | 1.5 |  |  |  |  |  |  | 1 | 0.1 |
|  | 2.5 | 0.39 | 0.46 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.46 | 0.57 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.57 | 0.66 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.66 | 0.72 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.72 | 0.81 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.81 | 0.86 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.86 | 0.90 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.90 | 0.93 | 12 |  |  |  |  |  |  |  |  |
|  | 15 | 0.93 | 0.95 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.95 | 0.96 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.96 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 162 | I | C | 0.00 | I | soil type: | 162 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.34 | 0.10 | 0.29 | 0.34 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.29 | 0.53 | 0.5 |  |  |  |  |  |  | 0.34 | 0.1 |
|  | 1 | 0.53 | 0.65 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.65 | 0.73 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.73 | 0.78 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.78 | 0.84 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.84 | 0.89 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.89 | 0.93 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.93 | 0.96 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.96 | 0.98 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.98 | 0.99 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 163 | I | C | 0.00 | I | soil type: | 163 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.13 | 0.10 | 0.39 | 0.13 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.25 | 0.39 | 0.58 | 0.25 |  |  |  |  |  |  | 0.13 | 0.1 |
|  | 0.5 | 0.58 | 0.73 | 0.5 |  |  |  |  |  |  |  |  |
|  | 1 | 0.73 | 0.79 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.79 | 0.83 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.83 | 0.86 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.86 | 0.89 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.89 | 0.91 | 4 |  |  |  |  |  |  |  |  |
|  | 7 | 0.91 | 0.93 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.93 | 0.94 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.94 | 0.94 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.94 | 0.94 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.94 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 164 | I | C | 0.00 | 1 | soil type: | 164 | l : | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.38 | 0.10 | 0.35 | 0.38 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.35 | 0.43 | 0.75 |  |  |  |  |  |  | 0.38 | 0.1 |
|  | 1 | 0.43 | 0.53 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.53 | 0.60 | 1.5 |  |  |  |  |  |  |  |  |


|  | 2 | 0.60 | 0.64 | 2 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2.5 | 0.64 | 0.70 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.70 | 0.76 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.76 | 0.80 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.80 | 0.83 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.83 | 0.86 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.86 | 0.88 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.88 | 0.89 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.89 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 165 | I | C | 0.00 | I | soil type: | 165 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.42 | 0.10 | 0.36 | 0.42 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.36 | 0.45 | 0.75 |  |  |  |  |  |  | 0.42 | 0.1 |
|  | 1 | 0.45 | 0.56 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.56 | 0.63 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.63 | 0.73 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.73 | 0.78 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.78 | 0.85 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.85 | 0.88 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.88 | 0.91 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.91 | 0.94 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.94 | 0.96 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.96 | 0.97 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.97 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 166 | I | C | 0.00 | 1 | soil type: | 166 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 4.83 | 0.10 | 0.11 | 4.83 |  |  |  |  |  |  | Upper I | Upper C |
|  | 5 | 0.11 | 0.15 | 5 |  |  |  |  |  |  | 4.83 | 0.1 |
|  | 6 | 0.15 | 0.19 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.19 | 0.23 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.23 | 0.27 | 8 |  |  |  |  |  |  |  |  |
|  | 9 | 0.27 | 0.30 | 9 |  |  |  |  |  |  |  |  |
|  | 10 | 0.30 | 0.37 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.37 | 0.42 | 12 |  |  |  |  |  |  |  |  |
|  | 14 | 0.42 | 0.47 | 14 |  |  |  |  |  |  |  |  |
|  | 16 | 0.47 | 0.51 | 16 |  |  |  |  |  |  |  |  |
|  | 18 | 0.51 | 0.54 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0.54 | 0.61 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.61 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 167 | I | C | 0.00 | I | soil type: | 167 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.17 | 0.10 | 0.22 | 0.17 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.25 | 0.22 | 0.43 | 0.25 |  |  |  |  |  |  | 0.17 | 0.1 |
|  | 0.5 | 0.43 | 0.64 | 0.5 |  |  |  |  |  |  |  |  |
|  | 1 | 0.64 | 0.74 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.74 | 0.80 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.80 | 0.86 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.86 | 0.90 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.90 | 0.94 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.94 | 0.97 | 6 |  |  |  |  |  |  |  |  |
|  | 10 | 0.97 | 0.98 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.98 | 0.99 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 168 | I | C | 0.00 | I | soil type: | 168 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 3.78 | 0.10 | 0.11 | 3.78 |  |  |  |  |  |  | Upper I | Upper C |
|  | 4 | 0.11 | 0.17 | 4 |  |  |  |  |  |  | 3.78 | 0.1 |
|  | 5 | 0.17 | 0.25 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.25 | 0.31 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.31 | 0.36 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.36 | 0.40 | 8 |  |  |  |  |  |  |  |  |
|  | 9 | 0.40 | 0.42 | 9 |  |  |  |  |  |  |  |  |
|  | 10 | 0.42 | 0.47 | 10 |  |  |  |  |  |  |  |  |


|  | 12 | 0.47 | 0.50 | 12 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 14 | 0.50 | 0.52 | 14 |  |  |  |  |  |  |  |  |
|  | 16 | 0.52 | 0.55 | 16 |  |  |  |  |  |  |  |  |
|  | 20 | 0.55 | 0.57 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.57 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 169 | I | C | 0.00 | I | soil type: | 169 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.27 | 0.10 | 0.31 | 0.27 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.31 | 0.37 | 0.5 |  |  |  |  |  |  | 0.27 | 0.1 |
|  | 0.75 | 0.37 | 0.40 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1 | 0.40 | 0.44 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.44 | 0.46 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.46 | 0.48 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.48 | 0.50 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.50 | 0.59 | 4 |  |  |  |  |  |  |  |  |
|  | 6.5 | 0.59 | 0.66 | 6.5 |  |  |  |  |  |  |  |  |
|  | 9 | 0.66 | 0.73 | 9 |  |  |  |  |  |  |  |  |
|  | 13 | 0.73 | 0.81 | 13 |  |  |  |  |  |  |  |  |
|  | 20 | 0.81 | 0.85 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.85 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 170 | I | C | 0.00 | I | soil type: | 170 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 3.53 | 0.10 | 0.14 | 3.53 |  |  |  |  |  |  | Upper I | Upper C |
|  | 4 | 0.14 | 0.19 | 4 |  |  |  |  |  |  | 3.53 | 0.1 |
|  | 5 | 0.19 | 0.22 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.22 | 0.24 | 6 |  |  |  |  |  |  |  |  |
|  | 7 | 0.24 | 0.26 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.26 | 0.28 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.28 | 0.30 | 10 |  |  |  |  |  |  |  |  |
|  | 12 | 0.30 | 0.31 | 12 |  |  |  |  |  |  |  |  |
|  | 14 | 0.31 | 0.32 | 14 |  |  |  |  |  |  |  |  |
|  | 16 | 0.32 | 0.32 | 16 |  |  |  |  |  |  |  |  |
|  | 18 | 0.32 | 0.33 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0.33 | 0.34 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.34 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 171 | I | C | 0.00 | I | soil type: | 171 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.37 | 0.10 | 0.25 | 0.37 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.25 | 0.43 | 0.75 |  |  |  |  |  |  | 0.37 | 0.1 |
|  | 1.5 | 0.43 | 0.50 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.50 | 0.60 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.60 | 0.66 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.66 | 0.70 | 4 |  |  |  |  |  |  |  |  |
|  | 5 | 0.70 | 0.72 | 5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.72 | 0.76 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.76 | 0.79 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.79 | 0.82 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.82 | 0.84 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.84 | 0.85 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.85 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 172 | I | C | 0.00 | 1 | soil type: | 172 | I : | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.75 | 0.10 | 0.14 | 0.75 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1 | 0.14 | 0.34 | 1 |  |  |  |  |  |  | 0.75 | 0.1 |
|  | 2 | 0.34 | 0.49 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.49 | 0.59 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.59 | 0.63 | 4 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.63 | 0.70 | 4.5 |  |  |  |  |  |  |  |  |
|  | 5.5 | 0.70 | 0.77 | 5.5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.77 | 0.84 | 7 |  |  |  |  |  |  |  |  |
|  | 9 | 0.84 | 0.90 | 9 |  |  |  |  |  |  |  |  |
|  | 12 | 0.90 | 0.94 | 12 |  |  |  |  |  |  |  |  |
|  | 15 | 0.94 | 0.99 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.99 | 1.00 | 20 |  |  |  |  |  |  |  |  |


|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 173 | 1 | C | 0.00 | I | soil type: | 173 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 2.1 | 0.10 | 0.29 | 2.1 |  |  |  |  |  |  | Upper I | Upper C |
|  | 2.3 | 0.29 | 0.42 | 2.3 |  |  |  |  |  |  | 2.1 | 0.1 |
|  | 2.7 | 0.42 | 0.47 | 2.7 |  |  |  |  |  |  |  |  |
|  | 3 | 0.47 | 0.52 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.52 | 0.55 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4 | 0.55 | 0.57 | 4 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.57 | 0.60 | 4.5 |  |  |  |  |  |  |  |  |
|  | 5.5 | 0.60 | 0.62 | 5.5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.62 | 0.64 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.64 | 0.66 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.66 | 0.66 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.66 | 0.67 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.67 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 174 | I | C | 0.00 | I | soil type: | 174 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.10 | 0.10 | 0.005 |  |  |  |  |  |  | 0.005 | 0.1 |
|  | 0.6 | 0.10 | 0.23 | 0.6 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.8 | 0.23 | 0.48 | 0.8 |  |  |  |  |  |  | 0.6 | 0.1 |
|  | 1.5 | 0.48 | 0.58 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.58 | 0.65 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.65 | 0.70 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.70 | 0.74 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.74 | 0.78 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.78 | 0.81 | 4.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.81 | 0.83 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.83 | 0.85 | 8 |  |  |  |  |  |  |  |  |
|  | 12 | 0.85 | 0.86 | 12 |  |  |  |  |  |  |  |  |
|  | 20 | 0.86 | 0.86 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.86 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 175 | I | C | 0.00 | I | soil type: | 175 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 1 | 0.10 | 0.24 | 1 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.1 | 0.24 | 0.44 | 1.1 |  |  |  |  |  |  | 1 | 0.1 |
|  | 1.5 | 0.44 | 0.56 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.56 | 0.63 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.63 | 0.67 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.67 | 0.73 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.73 | 0.78 | 4 |  |  |  |  |  |  |  |  |
|  | 5.5 | 0.78 | 0.83 | 5.5 |  |  |  |  |  |  |  |  |
|  | 8 | 0.83 | 0.86 | 8 |  |  |  |  |  |  |  |  |
|  | 12 | 0.86 | 0.87 | 12 |  |  |  |  |  |  |  |  |
|  | 16 | 0.87 | 0.88 | 16 |  |  |  |  |  |  |  |  |
|  | 20 | 0.88 | 0.89 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.89 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 176 | I | C | 0.00 | I | soil type: | 176 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |
|  | 0.25 | 0.10 | 0.38 | 0.25 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.5 | 0.38 | 0.50 | 0.5 |  |  |  |  |  |  | 0.25 | 0.1 |
|  | 0.75 | 0.50 | 0.63 | 0.75 |  |  |  |  |  |  |  |  |
|  | 1.25 | 0.63 | 0.74 | 1.25 |  |  |  |  |  |  |  |  |
|  | 2 | 0.74 | 0.82 | 2 |  |  |  |  |  |  |  |  |
|  | 3 | 0.82 | 0.86 | 3 |  |  |  |  |  |  |  |  |
|  | 4 | 0.86 | 0.91 | 4 |  |  |  |  |  |  |  |  |
|  | 6 | 0.91 | 0.94 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.94 | 0.97 | 8 |  |  |  |  |  |  |  |  |
|  | 12 | 0.97 | 0.99 | 12 |  |  |  |  |  |  |  |  |
|  | 16 | 0.99 | 1.00 | 16 |  |  |  |  |  |  |  |  |
|  | 20 | 1.00 | 1.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 1.00 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 177 | I | C | 0.00 | I | soil type: | 177 | I | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0 | 0.10 | 0.10 | 0 |  |  |  |  |  |  | 0 | 0.1 |


|  | 0.315 | 0.10 | 0.26 | 0.315 |  |  |  |  |  |  | Upper I | Upper C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.4 | 0.26 | 0.43 | 0.4 |  |  |  |  |  |  | 0.315 | 0.1 |
|  | 0.6 | 0.43 | 0.58 | 0.6 |  |  |  |  |  |  |  |  |
|  | 1 | 0.58 | 0.68 | 1 |  |  |  |  |  |  |  |  |
|  | 1.5 | 0.68 | 0.75 | 1.5 |  |  |  |  |  |  |  |  |
|  | 2 | 0.75 | 0.79 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.79 | 0.84 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.84 | 0.88 | 3.5 |  |  |  |  |  |  |  |  |
|  | 5 | 0.88 | 0.91 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.91 | 0.94 | 7 |  |  |  |  |  |  |  |  |
|  | 11 | 0.94 | 0.97 | 11 |  |  |  |  |  |  |  |  |
|  | 20 | 0.97 | 0.97 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.97 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 178 | 1 | C | 0.00 | 1 | soil type: | 178 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.10 | 0.10 | 0.005 |  |  |  |  |  |  | 0.005 | 0.1 |
|  | 2.1 | 0.10 | 0.24 | 2.1 |  |  |  |  |  |  | Upper I | Upper C |
|  | 2.25 | 0.24 | 0.35 | 2.25 |  |  |  |  |  |  | 2.1 | 0.1 |
|  | 2.5 | 0.35 | 0.49 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.49 | 0.58 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.58 | 0.70 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.70 | 0.76 | 4.5 |  |  |  |  |  |  |  |  |
|  | 5.5 | 0.76 | 0.83 | 5.5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.83 | 0.85 | 7 |  |  |  |  |  |  |  |  |
|  | 8 | 0.85 | 0.89 | 8 |  |  |  |  |  |  |  |  |
|  | 11 | 0.89 | 0.91 | 11 |  |  |  |  |  |  |  |  |
|  | 15 | 0.91 | 0.93 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.93 | 0.93 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.93 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 179 | I | C | 0.00 | I | soil type: | 179 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.10 | 0.10 | 0.005 |  |  |  |  |  |  | 0.005 | 0.1 |
|  | 1.55 | 0.10 | 0.25 | 1.55 |  |  |  |  |  |  | Upper I | Upper C |
|  | 1.75 | 0.25 | 0.35 | 1.75 |  |  |  |  |  |  | 1.55 | 0.1 |
|  | 2 | 0.35 | 0.47 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.47 | 0.56 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3 | 0.56 | 0.62 | 3 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.62 | 0.66 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4 | 0.66 | 0.69 | 4 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.69 | 0.73 | 4.5 |  |  |  |  |  |  |  |  |
|  | 5.5 | 0.73 | 0.75 | 5.5 |  |  |  |  |  |  |  |  |
|  | 7 | 0.75 | 0.77 | 7 |  |  |  |  |  |  |  |  |
|  | 10 | 0.77 | 0.77 | 10 |  |  |  |  |  |  |  |  |
|  | 20 | 0.77 | 0.77 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.77 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 180 | I | C | 0.00 | I | soil type: | 180 | I: | 0.1 | C: | 0.100 |  |  |
|  | 0 | 0.00 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.10 | 0.10 | 0.005 |  |  |  |  |  |  | 0.005 | 0.1 |
|  | 0.5 | 0.10 | 0.35 | 0.5 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0.75 | 0.35 | 0.44 | 0.75 |  |  |  |  |  |  | 0.5 | 0.1 |
|  | 1 | 0.44 | 0.65 | 1 |  |  |  |  |  |  |  |  |
|  | 2 | 0.65 | 0.72 | 2 |  |  |  |  |  |  |  |  |
|  | 2.5 | 0.72 | 0.80 | 2.5 |  |  |  |  |  |  |  |  |
|  | 3.5 | 0.80 | 0.85 | 3.5 |  |  |  |  |  |  |  |  |
|  | 4.5 | 0.85 | 0.88 | 4.5 |  |  |  |  |  |  |  |  |
|  | 6 | 0.88 | 0.90 | 6 |  |  |  |  |  |  |  |  |
|  | 8 | 0.90 | 0.91 | 8 |  |  |  |  |  |  |  |  |
|  | 10 | 0.91 | 0.93 | 10 |  |  |  |  |  |  |  |  |
|  | 15 | 0.93 | 0.93 | 15 |  |  |  |  |  |  |  |  |
|  | 20 | 0.93 | 0.93 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0.93 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 181 | I | C | 0.00 | 1 | soil type: | 181 | I: | 0.1 | C: | 0.000 |  |  |
|  | 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
|  | 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |


| 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
| 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
| 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
| 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
| 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
| 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
| 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
| 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 1 | C | 0.00 | 1 | soil type: | 182 | I: | 0.1 | C: | 0.000 |  |  |
| 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
| 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
| 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
| 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
| 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
| 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
| 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
| 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
| 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
| 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
| 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
| 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
| 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
| 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
| 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 1 | c | 0.00 | , | soil type: | 183 | I: | 0.1 | C: | 0.000 |  |  |
| 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
| 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
| 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
| 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
| 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
| 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
| 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
| 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
| 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
| 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
| 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
| 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
| 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
| 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
| 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 1 | c | 0.00 | 1 | soil type: | 184 | I: | 0.1 | C: | 0.000 |  |  |
| 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
| 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
| 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
| 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
| 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
| 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
| 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
| 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
| 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
| 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
| 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
| 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
| 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
| 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
| 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 1 | c | 0.00 | 1 | soil type: | 185 | I: | 0.1 | C: | 0.000 |  |  |
| 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
| 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
| 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
| 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
| 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
| 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
| 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
| 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
| 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
| 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |


|  | 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 186 | I | C | 0.00 | I | soil type: | 186 | I: | 0.1 | C: | 0.000 |  |  |
|  | 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
|  | 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
|  | 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
|  | 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
|  | 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 187 | I | C | 0.00 | 1 | soil type: | 187 | I: | 0.1 | C: | 0.000 |  |  |
|  | 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
|  | 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
|  | 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
|  | 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
|  | 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 188 | 1 | C | 0.00 | 1 | soil type: | 188 | I: | 0.1 | C: | 0.000 |  |  |
|  | 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
|  | 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
|  | 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
|  | 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
|  | 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 189 | I | C | 0.00 | 1 | soil type: | 189 | $\mathrm{I}:$ | 0.1 | C: | 0.000 |  |  |
|  | 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
|  | 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
|  | 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
|  | 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
|  | 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |


|  | 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 190 | I | C | 0.00 | I | soil type: | 190 | I | 0.1 | C: | 0.000 |  |  |
|  | 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
|  | 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
|  | 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
|  | 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
|  | 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 191 | I | C | 0.00 | I | soil type: | 191 | I | 0.1 | C: | 0.000 |  |  |
|  | 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
|  | 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
|  | 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
|  | 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
|  | 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 192 | I | C | 0.00 | I | soil type: | 192 | I | 0.1 | C: | 0.000 |  |  |
|  | 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
|  | 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
|  | 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
|  | 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
|  | 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 193 | I | C | 0.00 | I | soil type: | 193 | I | 0.1 | C: | 0.000 |  |  |
|  | 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
|  | 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
|  | 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
|  | 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
|  | 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 194 | I | C | 0.00 | 1 | soil type: | 194 | I: | 0.1 | C: | 0.000 |  |  |
|  | 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |


|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
|  | 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
|  | 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
|  | 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
|  | 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 195 | I | C | 0.00 | I | soil type: | 195 | I | 0.1 | C: | 0.000 |  |  |
|  | 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
|  | 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
|  | 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
|  | 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
|  | 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 196 | I | C | 0.00 | I | soil type: | 196 | I | 0.1 | C: | 0.000 |  |  |
|  | 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
|  | 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
|  | 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
|  | 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
|  | 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 197 | 1 | C | 0.00 | 1 | soil type: | 197 | I | 0.1 | C: | 0.000 |  |  |
|  | 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
|  | 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
|  | 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
|  | 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
|  | 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 198 | 1 | C | 0.00 | 1 | soil type: | 198 | I | 0.1 | C: | 0.000 |  |  |
|  | 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
|  | 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |


|  | 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
|  | 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |
| 199 | 1 | c | 0.00 | 1 | soil type: | 199 | l | 0.1 | C: | 0.000 |  |  |
|  | 0 | 0 | 0.10 | 0 |  |  |  |  |  |  | Lower I | Lower C |
|  | 0.005 | 0.1 | 0.00 | 0.005 |  |  |  |  |  |  | 0 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | Upper I | Upper C |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  | 25 | 0 |
|  | 0 | 0 | 0.00 | 0 |  |  |  |  |  |  |  |  |
|  | 1 | 0 | 0.00 | 1 |  |  |  |  |  |  |  |  |
|  | 2 | 0 | 0.00 | 2 |  |  |  |  |  |  |  |  |
|  | 3.4 | 0 | 0.00 | 3.4 |  |  |  |  |  |  |  |  |
|  | 5 | 0 | 0.00 | 5 |  |  |  |  |  |  |  |  |
|  | 7 | 0 | 0.00 | 7 |  |  |  |  |  |  |  |  |
|  | 9.6 | 0 | 0.00 | 9.6 |  |  |  |  |  |  |  |  |
|  | 13 | 0 | 0.00 | 13 |  |  |  |  |  |  |  |  |
|  | 18 | 0 | 0.00 | 18 |  |  |  |  |  |  |  |  |
|  | 20 | 0 | 0.00 | 20 |  |  |  |  |  |  |  |  |
|  | 25 | 0 | 0.00 | 25 |  |  |  |  |  |  |  |  |

## DESIGN STORM

This design storm is generated using the intensity-duration relationship and with the inflection point at $80 \%$.

| $t$ (min.) | Dt/D24 | $\mathrm{t}^{*} 20 \%$ | 0.8+(Dt/D24)*. 2 | t*80\% | 0.8-(Dt/D24)*. 8 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0.000 | 0.00 | 0.80000000 | 0.0 | 0.8000000 |
| 0.25 | 0.010 | 0.05 | 0.80203239 | 0.2 | 0.79187046 |
| 0.5 | 0.015 | 0.10 | 0.80293462 | 0.4 | 0.78826152 |
| 0.75 | 0.018 | 0.15 | 0.80363815 | 0.6 | 0.78544741 |
| 1 | 0.021 | 0.20 | 0.80423738 | 0.8 | 0.78305046 |
| 1.25 | 0.024 | 0.25 | 0.80476936 | 1.0 | 0.78092256 |
| 1.5 | 0.026 | 0.30 | 0.80525323 | 1.2 | 0.77898709 |
| 1.75 | 0.029 | 0.35 | 0.80570044 | 1.4 | 0.77719826 |
| 2 | 0.031 | 0.40 | 0.80611848 | 1.6 | 0.77552607 |
| 2.25 | 0.033 | 0.45 | 0.80651260 | 1.8 | 0.77394959 |
| 2.5 | 0.034 | 0.50 | 0.80688662 | 2.0 | 0.77245352 |
| 2.75 | 0.036 | 0.55 | 0.80724343 | 2.2 | 0.77102628 |
| 3 | 0.038 | 0.60 | 0.80758529 | 2.4 | 0.76965884 |
| 3.25 | 0.040 | 0.65 | 0.80791400 | 2.6 | 0.76834400 |
| 3.5 | 0.041 | 0.70 | 0.80823103 | 2.8 | 0.76707590 |
| 3.75 | 0.043 | 0.75 | 0.80853757 | 3.0 | 0.76584971 |
| 4 | 0.044 | 0.80 | 0.80883466 | 3.2 | 0.76466137 |
| 4.25 | 0.046 | 0.85 | 0.80912313 | 3.4 | 0.76350747 |
| 4.5 | 0.047 | 0.90 | 0.80940374 | 3.6 | 0.76238505 |
| 4.75 | 0.048 | 0.95 | 0.80967711 | 3.8 | 0.76129158 |
| 5 | 0.050 | 1.00 | 0.80994379 | 4.0 | 0.76022484 |
| 5.25 | 0.051 | 1.05 | 0.81020428 | 4.2 | 0.75918289 |
| 5.5 | 0.052 | 1.10 | 0.81045900 | 4.4 | 0.75816401 |
| 5.75 | 0.054 | 1.15 | 0.81070833 | 4.6 | 0.75716667 |
| 6 | 0.055 | 1.20 | 0.81095262 | 4.8 | 0.75618952 |
| 6.25 | 0.056 | 1.25 | 0.81119217 | 5.0 | 0.75523132 |
| 6.5 | 0.057 | 1.30 | 0.81142726 | 5.2 | 0.75429098 |
| 6.75 | 0.058 | 1.35 | 0.81165813 | 5.4 | 0.75336748 |
| 7 | 0.059 | 1.40 | 0.81188502 | 5.6 | 0.75245993 |
| 7.25 | 0.061 | 1.45 | 0.81210813 | 5.8 | 0.75156749 |
| 7.5 | 0.062 | 1.50 | 0.81232765 | 6.0 | 0.75068939 |
| 7.75 | 0.063 | 1.55 | 0.81254376 | 6.2 | 0.74982496 |
| 8 | 0.064 | 1.60 | 0.81275662 | 6.4 | 0.74897353 |
| 8.25 | 0.065 | 1.65 | 0.81296637 | 6.6 | 0.74813451 |
| 8.5 | 0.066 | 1.70 | 0.81317316 | 6.8 | 0.74730737 |
| 8.75 | 0.067 | 1.75 | 0.81337711 | 7.0 | 0.74649158 |
| 9 | 0.068 | 1.80 | 0.81357833 | 7.2 | 0.74568667 |
| 9.25 | 0.069 | 1.85 | 0.81377695 | 7.4 | 0.74489221 |
| 9.5 | 0.070 | 1.90 | 0.81397306 | 7.6 | 0.74410778 |
| 9.75 | 0.071 | 1.95 | 0.81416675 | 7.8 | 0.74333299 |
| 10 | 0.072 | 2.00 | 0.81435813 | 8.0 | 0.74256748 |
| 10.25 | 0.073 | 2.05 | 0.81454727 | 8.2 | 0.74181092 |
| 10.5 | 0.074 | 2.10 | 0.81473426 | 8.4 | 0.74106298 |
| 10.75 | 0.075 | 2.15 | 0.81491916 | 8.6 | 0.74032336 |
| 11 | 0.076 | 2.20 | 0.81510205 | 8.8 | 0.73959179 |
| 11.25 | 0.076 | 2.25 | 0.81528300 | 9.0 | 0.73886799 |
| 11.5 | 0.077 | 2.30 | 0.81546207 | 9.2 | 0.73815171 |
| 11.75 | 0.078 | 2.35 | 0.81563932 | 9.4 | 0.73744271 |
| 12 | 0.079 | 2.40 | 0.81581481 | 9.6 | 0.73674077 |
| 12.25 | 0.080 | 2.45 | 0.81598858 | 9.8 | 0.73604566 |
| 12.5 | 0.081 | 2.50 | 0.81616070 | 10.0 | 0.73535720 |
| 12.75 | 0.082 | 2.55 | 0.81633121 | 10.2 | 0.73467517 |
| 13 | 0.083 | 2.60 | 0.81650015 | 10.4 | 0.73399941 |
| 13.25 | 0.083 | 2.65 | 0.81666757 | 10.6 | 0.73332972 |
| 13.5 | 0.084 | 2.70 | 0.81683351 | 10.8 | 0.73266595 |
| 13.75 | 0.085 | 2.75 | 0.81699802 | 11.0 | 0.73200792 |
| 14 | 0.086 | 2.80 | 0.81716112 | 11.2 | 0.73135550 |
| 14.25 | 0.087 | 2.85 | 0.81732287 | 11.4 | 0.73070853 |
| 14.5 | 0.087 | 2.90 | 0.81748328 | 11.6 | 0.73006688 |
| 14.75 | 0.088 | 2.95 | 0.81764240 | 11.8 | 0.72943040 |
| 15 | 0.089 | 3.00 | 0.81780026 | 12.0 | 0.72879898 |
| 15.25 | 0.090 | 3.05 | 0.81795688 | 12.2 | 0.72817248 |
| 15.5 | 0.091 | 3.10 | 0.81811230 | 12.4 | 0.72755079 |
| 15.75 | 0.091 | 3.15 | 0.81826655 | 12.6 | 0.72693379 |

## 1-minute mass curve DEPTH = 0.500 in

|  | time (min. | total | depth |
| :---: | :---: | :---: | :---: |
| 1152 | 0 | 0.00000 | 0.0000 |
| 1151 | 1 | 0.00037 | 0.0002 |
| 1150 | 2 | 0.00074 | 0.0004 |
| 1149 | 3 | 0.00110 | 0.0006 |
| 1148 | 4 | 0.00147 | 0.0007 |
| 1147 | 5 | 0.00184 | 0.0009 |
| 1146 | 6 | 0.00221 | 0.0011 |
| 1145 | 7 | 0.00258 | 0.0013 |
| 1144 | 8 | 0.00295 | 0.0015 |
| 1143 | 9 | 0.00332 | 0.0017 |
| 1142 | 10 | 0.00369 | 0.0018 |
| 1141 | 11 | 0.00406 | 0.0020 |
| 1140 | 12 | 0.00443 | 0.0022 |
| 1139 | 13 | 0.00480 | 0.0024 |
| 1138 | 14 | 0.00517 | 0.0026 |
| 1137 | 15 | 0.00554 | 0.0028 |
| 1136 | 16 | 0.00591 | 0.0030 |
| 1135 | 17 | 0.00628 | 0.0031 |
| 1134 | 18 | 0.00665 | 0.0033 |
| 1133 | 19 | 0.00702 | 0.0035 |
| 1132 | 20 | 0.00739 | 0.0037 |
| 1131 | 21 | 0.00776 | 0.0039 |
| 1130 | 22 | 0.00813 | 0.0041 |
| 1129 | 23 | 0.00851 | 0.0043 |
| 1128 | 24 | 0.00888 | 0.0044 |
| 1127 | 25 | 0.00925 | 0.0046 |
| 1126 | 26 | 0.00962 | 0.0048 |
| 1125 | 27 | 0.00999 | 0.0050 |
| 1124 | 28 | 0.01037 | 0.0052 |
| 1123 | 29 | 0.01074 | 0.0054 |
| 1122 | 30 | 0.01111 | 0.0056 |
| 1121 | 31 | 0.01148 | 0.0057 |
| 1120 | 32 | 0.01186 | 0.0059 |
| 1119 | 33 | 0.01223 | 0.0061 |
| 1118 | 34 | 0.01260 | 0.0063 |
| 1117 | 35 | 0.01298 | 0.0065 |
| 1116 | 36 | 0.01335 | 0.0067 |
| 1115 | 37 | 0.01372 | 0.0069 |
| 1114 | 38 | 0.01410 | 0.0070 |
| 1113 | 39 | 0.01447 | 0.0072 |
| 1112 | 40 | 0.01484 | 0.0074 |
| 1111 | 41 | 0.01522 | 0.0076 |
| 1110 | 42 | 0.01559 | 0.0078 |
| 1109 | 43 | 0.01597 | 0.0080 |
| 1108 | 44 | 0.01634 | 0.0082 |
| 1107 | 45 | 0.01672 | 0.0084 |
| 1106 | 46 | 0.01709 | 0.0085 |
| 1105 | 47 | 0.01747 | 0.0087 |
| 1104 | 48 | 0.01784 | 0.0089 |
| 1103 | 49 | 0.01822 | 0.0091 |
| 1102 | 50 | 0.01859 | 0.0093 |
| 1101 | 51 | 0.01897 | 0.0095 |
| 1100 | 52 | 0.01935 | 0.0097 |
| 1099 | 53 | 0.01972 | 0.0099 |
| 1098 | 54 | 0.02010 | 0.0100 |
| 1097 | 55 | 0.02048 | 0.0102 |
| 1096 | 56 | 0.02085 | 0.0104 |
| 1095 | 57 | 0.02123 | 0.0106 |
| 1094 | 58 | 0.02161 | 0.0108 |
| 1093 | 59 | 0.02198 | 0.0110 |
| 1092 | 60 | 0.02236 | 0.0112 |
| 1091 | 61 | 0.02274 | 0.0114 |
| 1090 | 62 | 0.02312 | 0.0116 |
| 1089 | 63 | 0.02349 | 0.0117 |


| 16 | 0.092 | 3.20 | 0.81841965 | 12.8 | 0.72632138 | 1088 | 64 | 0.02387 | 0.0119 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16.25 | 0.093 | 3.25 | 0.81857164 | 13.0 | 0.72571346 | 1087 | 65 | 0.02425 | 0.0121 |
| 16.5 | 0.094 | 3.30 | 0.81872252 | 13.2 | 0.72510991 | 1086 | 66 | 0.02463 | 0.0123 |
| 16.75 | 0.094 | 3.35 | 0.81887234 | 13.4 | 0.72451064 | 1085 | 67 | 0.02501 | 0.0125 |
| 17 | 0.095 | 3.40 | 0.81902111 | 13.6 | 0.72391557 | 1084 | 68 | 0.02539 | 0.0127 |
| 17.25 | 0.096 | 3.45 | 0.81916885 | 13.8 | 0.72332459 | 1083 | 69 | 0.02576 | 0.0129 |
| 17.5 | 0.097 | 3.50 | 0.81931559 | 14.0 | 0.72273763 | 1082 | 70 | 0.02614 | 0.0131 |
| 17.75 | 0.097 | 3.55 | 0.81946135 | 14.2 | 0.72215459 | 1081 | 71 | 0.02652 | 0.0133 |
| 18 | 0.098 | 3.60 | 0.81960615 | 14.4 | 0.72157540 | 1080 | 72 | 0.02690 | 0.0135 |
| 18.25 | 0.099 | 3.65 | 0.81975000 | 14.6 | 0.72099998 | 1079 | 73 | 0.02728 | 0.0136 |
| 18.5 | 0.099 | 3.70 | 0.81989294 | 14.8 | 0.72042825 | 1078 | 74 | 0.02766 | 0.0138 |
| 18.75 | 0.100 | 3.75 | 0.82003496 | 15.0 | 0.71986015 | 1077 | 75 | 0.02804 | 0.0140 |
| 19 | 0.101 | 3.80 | 0.82017610 | 15.2 | 0.71929559 | 1076 | 76 | 0.02842 | 0.0142 |
| 19.25 | 0.102 | 3.85 | 0.82031637 | 15.4 | 0.71873451 | 1075 | 77 | 0.02880 | 0.0144 |
| 19.5 | 0.102 | 3.90 | 0.82045579 | 15.6 | 0.71817685 | 1074 | 78 | 0.02918 | 0.0146 |
| 19.75 | 0.103 | 3.95 | 0.82059437 | 15.8 | 0.71762253 | 1073 | 79 | 0.02956 | 0.0148 |
| 20 | 0.104 | 4.00 | 0.82073212 | 16.0 | 0.71707151 | 1072 | 80 | 0.02994 | 0.0150 |
| 20.25 | 0.104 | 4.05 | 0.82086907 | 16.2 | 0.71652371 | 1071 | 81 | 0.03032 | 0.0152 |
| 20.5 | 0.105 | 4.10 | 0.82100523 | 16.4 | 0.71597908 | 1070 | 82 | 0.03070 | 0.0154 |
| 20.75 | 0.106 | 4.15 | 0.82114061 | 16.6 | 0.71543757 | 1069 | 83 | 0.03108 | 0.0155 |
| 21 | 0.106 | 4.20 | 0.82127522 | 16.8 | 0.71489911 | 1068 | 84 | 0.03147 | 0.0157 |
| 21.25 | 0.107 | 4.25 | 0.82140909 | 17.0 | 0.71436366 | 1067 | 85 | 0.03185 | 0.0159 |
| 21.5 | 0.108 | 4.30 | 0.82154221 | 17.2 | 0.71383116 | 1066 | 86 | 0.03223 | 0.0161 |
| 21.75 | 0.108 | 4.35 | 0.82167461 | 17.4 | 0.71330156 | 1065 | 87 | 0.03261 | 0.0163 |
| 22 | 0.109 | 4.40 | 0.82180630 | 17.6 | 0.71277482 | 1064 | 88 | 0.03299 | 0.0165 |
| 22.25 | 0.110 | 4.45 | 0.82193728 | 17.8 | 0.71225088 | 1063 | 89 | 0.03338 | 0.0167 |
| 22.5 | 0.110 | 4.50 | 0.82206757 | 18.0 | 0.71172970 | 1062 | 90 | 0.03376 | 0.0169 |
| 22.75 | 0.111 | 4.55 | 0.82219719 | 18.2 | 0.71121124 | 1061 | 91 | 0.03414 | 0.0171 |
| 23 | 0.112 | 4.60 | 0.82232614 | 18.4 | 0.71069544 | 1060 | 92 | 0.03452 | 0.0173 |
| 23.25 | 0.112 | 4.65 | 0.82245443 | 18.6 | 0.71018228 | 1059 | 93 | 0.03491 | 0.0175 |
| 23.5 | 0.113 | 4.70 | 0.82258207 | 18.8 | 0.70967170 | 1058 | 94 | 0.03529 | 0.0176 |
| 23.75 | 0.114 | 4.75 | 0.82270908 | 19.0 | 0.70916367 | 1057 | 95 | 0.03567 | 0.0178 |
| 24 | 0.114 | 4.80 | 0.82283546 | 19.2 | 0.70865815 | 1056 | 96 | 0.03606 | 0.0180 |
| 24.25 | 0.115 | 4.85 | 0.82296123 | 19.4 | 0.70815509 | 1055 | 97 | 0.03644 | 0.0182 |
| 24.5 | 0.115 | 4.90 | 0.82308638 | 19.6 | 0.70765447 | 1054 | 98 | 0.03682 | 0.0184 |
| 24.75 | 0.116 | 4.95 | 0.82321094 | 19.8 | 0.70715624 | 1053 | 99 | 0.03721 | 0.0186 |
| 25 | 0.117 | 5.00 | 0.82333491 | 20.0 | 0.70666037 | 1052 | 100 | 0.03759 | 0.0188 |
| 25.25 | 0.117 | 5.05 | 0.82345829 | 20.2 | 0.70616683 | 1051 | 101 | 0.03797 | 0.0190 |
| 25.5 | 0.118 | 5.10 | 0.82358111 | 20.4 | 0.70567558 | 1050 | 102 | 0.03836 | 0.0192 |
| 25.75 | 0.119 | 5.15 | 0.82370335 | 20.6 | 0.70518658 | 1049 | 103 | 0.03874 | 0.0194 |
| 26 | 0.119 | 5.20 | 0.82382505 | 20.8 | 0.70469982 | 1048 | 104 | 0.03913 | 0.0196 |
| 26.25 | 0.120 | 5.25 | 0.82394619 | 21.0 | 0.70421524 | 1047 | 105 | 0.03951 | 0.0198 |
| 26.5 | 0.120 | 5.30 | 0.82406679 | 21.2 | 0.70373284 | 1046 | 106 | 0.03990 | 0.0199 |
| 26.75 | 0.121 | 5.35 | 0.82418686 | 21.4 | 0.70325256 | 1045 | 107 | 0.04028 | 0.0201 |
| 27 | 0.122 | 5.40 | 0.82430640 | 21.6 | 0.70277439 | 1044 | 108 | 0.04067 | 0.0203 |
| 27.25 | 0.122 | 5.45 | 0.82442542 | 21.8 | 0.70229830 | 1043 | 109 | 0.04105 | 0.0205 |
| 27.5 | 0.123 | 5.50 | 0.82454394 | 22.0 | 0.70182426 | 1042 | 110 | 0.04144 | 0.0207 |
| 27.75 | 0.123 | 5.55 | 0.82466194 | 22.2 | 0.70135224 | 1041 | 111 | 0.04183 | 0.0209 |
| 28 | 0.124 | 5.60 | 0.82477945 | 22.4 | 0.70088221 | 1040 | 112 | 0.04221 | 0.0211 |
| 28.25 | 0.124 | 5.65 | 0.82489646 | 22.6 | 0.70041415 | 1039 | 113 | 0.04260 | 0.0213 |
| 28.5 | 0.125 | 5.70 | 0.82501299 | 22.8 | 0.69994803 | 1038 | 114 | 0.04298 | 0.0215 |
| 28.75 | 0.126 | 5.75 | 0.82512904 | 23.0 | 0.69948383 | 1037 | 115 | 0.04337 | 0.0217 |
| 29 | 0.126 | 5.80 | 0.82524462 | 23.2 | 0.69902153 | 1036 | 116 | 0.04376 | 0.0219 |
| 29.25 | 0.127 | 5.85 | 0.82535973 | 23.4 | 0.69856109 | 1035 | 117 | 0.04414 | 0.0221 |
| 29.5 | 0.127 | 5.90 | 0.82547438 | 23.6 | 0.69810250 | 1034 | 118 | 0.04453 | 0.0223 |
| 29.75 | 0.128 | 5.95 | 0.82558857 | 23.8 | 0.69764573 | 1033 | 119 | 0.04492 | 0.0225 |
| 30 | 0.129 | 6.00 | 0.82570231 | 24.0 | 0.69719076 | 1032 | 120 | 0.04531 | 0.0227 |
| 30.25 | 0.129 | 6.05 | 0.82581561 | 24.2 | 0.69673758 | 1031 | 121 | 0.04569 | 0.0228 |
| 30.5 | 0.130 | 6.10 | 0.82592846 | 24.4 | 0.69628614 | 1030 | 122 | 0.04608 | 0.0230 |
| 30.75 | 0.130 | 6.15 | 0.82604089 | 24.6 | 0.69583645 | 1029 | 123 | 0.04647 | 0.0232 |
| 31 | 0.131 | 6.20 | 0.82615288 | 24.8 | 0.69538847 | 1028 | 124 | 0.04686 | 0.0234 |
| 31.25 | 0.131 | 6.25 | 0.82626445 | 25.0 | 0.69494218 | 1027 | 125 | 0.04725 | 0.0236 |
| 31.5 | 0.132 | 6.30 | 0.82637561 | 25.2 | 0.69449757 | 1026 | 126 | 0.04764 | 0.0238 |
| 31.75 | 0.132 | 6.35 | 0.82648635 | 25.4 | 0.69405462 | 1025 | 127 | 0.04802 | 0.0240 |
| 32 | 0.133 | 6.40 | 0.82659668 | 25.6 | 0.69361330 | 1024 | 128 | 0.04841 | 0.0242 |
| 32.25 | 0.134 | 6.45 | 0.82670660 | 25.8 | 0.69317359 | 1023 | 129 | 0.04880 | 0.0244 |
| 32.5 | 0.134 | 6.50 | 0.82681613 | 26.0 | 0.69273549 | 1022 | 130 | 0.04919 | 0.0246 |
| 32.75 | 0.135 | 6.55 | 0.82692526 | 26.2 | 0.69229897 | 1021 | 131 | 0.04958 | 0.0248 |
| 33 | 0.135 | 6.60 | 0.82703400 | 26.4 | 0.69186401 | 1020 | 132 | 0.04997 | 0.0250 |
| 33.25 | 0.136 | 6.65 | 0.82714235 | 26.6 | 0.69143060 | 1019 | 133 | 0.05036 | 0.0252 |
| 33.5 | 0.136 | 6.70 | 0.82725032 | 26.8 | 0.69099872 | 1018 | 134 | 0.05075 | 0.0254 |


| 33.75 | 0.137 | 6.75 | 0.82735791 | 27.0 | 0.69056834 | 1017 | 135 | 0.05114 | 0.0256 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 34 | 0.137 | 6.80 | 0.82746513 | 27.2 | 0.69013947 | 1016 | 136 | 0.05153 | 0.0258 |
| 34.25 | 0.138 | 6.85 | 0.82757198 | 27.4 | 0.68971207 | 1015 | 137 | 0.05192 | 0.0260 |
| 34.5 | 0.138 | 6.90 | 0.82767846 | 27.6 | 0.68928614 | 1014 | 138 | 0.05231 | 0.0262 |
| 34.75 | 0.139 | 6.95 | 0.82778459 | 27.8 | 0.68886166 | 1013 | 139 | 0.05270 | 0.0264 |
| 35 | 0.139 | 7.00 | 0.82789035 | 28.0 | 0.68843861 | 1012 | 140 | 0.05309 | 0.0265 |
| 35.25 | 0.140 | 7.05 | 0.82799576 | 28.2 | 0.68801697 | 1011 | 141 | 0.05349 | 0.0267 |
| 35.5 | 0.141 | 7.10 | 0.82810081 | 28.4 | 0.68759674 | 1010 | 142 | 0.05388 | 0.0269 |
| 35.75 | 0.141 | 7.15 | 0.82820552 | 28.6 | 0.68717790 | 1009 | 143 | 0.05427 | 0.0271 |
| 36 | 0.142 | 7.20 | 0.82830989 | 28.8 | 0.68676044 | 1008 | 144 | 0.05466 | 0.0273 |
| 36.25 | 0.142 | 7.25 | 0.82841392 | 29.0 | 0.68634433 | 1007 | 145 | 0.05505 | 0.0275 |
| 36.5 | 0.143 | 7.30 | 0.82851761 | 29.2 | 0.68592957 | 1006 | 146 | 0.05544 | 0.0277 |
| 36.75 | 0.143 | 7.35 | 0.82862096 | 29.4 | 0.68551614 | 1005 | 147 | 0.05584 | 0.0279 |
| 37 | 0.144 | 7.40 | 0.82872399 | 29.6 | 0.68510403 | 1004 | 148 | 0.05623 | 0.0281 |
| 37.25 | 0.144 | 7.45 | 0.82882669 | 29.8 | 0.68469323 | 1003 | 149 | 0.05662 | 0.0283 |
| 37.5 | 0.145 | 7.50 | 0.82892907 | 30.0 | 0.68428373 | 1002 | 150 | 0.05701 | 0.0285 |
| 37.75 | 0.145 | 7.55 | 0.82903112 | 30.2 | 0.68387550 | 1001 | 151 | 0.05741 | 0.0287 |
| 38 | 0.146 | 7.60 | 0.82913286 | 30.4 | 0.68346854 | 1000 | 152 | 0.05780 | 0.0289 |
| 38.25 | 0.146 | 7.65 | 0.82923429 | 30.6 | 0.68306284 | 999 | 153 | 0.05819 | 0.0291 |
| 38.5 | 0.147 | 7.70 | 0.82933540 | 30.8 | 0.68265839 | 998 | 154 | 0.05859 | 0.0293 |
| 38.75 | 0.147 | 7.75 | 0.82943621 | 31.0 | 0.68225516 | 997 | 155 | 0.05898 | 0.0295 |
| 39 | 0.148 | 7.80 | 0.82953671 | 31.2 | 0.68185316 | 996 | 156 | 0.05938 | 0.0297 |
| 39.25 | 0.148 | 7.85 | 0.82963691 | 31.4 | 0.68145237 | 995 | 157 | 0.05977 | 0.0299 |
| 39.5 | 0.149 | 7.90 | 0.82973681 | 31.6 | 0.68105277 | 994 | 158 | 0.06016 | 0.0301 |
| 39.75 | 0.149 | 7.95 | 0.82983641 | 31.8 | 0.68065436 | 993 | 159 | 0.06056 | 0.0303 |
| 40 | 0.150 | 8.00 | 0.82993572 | 32.0 | 0.68025713 | 992 | 160 | 0.06095 | 0.0305 |
| 40.25 | 0.150 | 8.05 | 0.83003473 | 32.2 | 0.67986106 | 991 | 161 | 0.06135 | 0.0307 |
| 40.5 | 0.151 | 8.10 | 0.83013346 | 32.4 | 0.67946615 | 990 | 162 | 0.06174 | 0.0309 |
| 40.75 | 0.151 | 8.15 | 0.83023190 | 32.6 | 0.67907238 | 989 | 163 | 0.06214 | 0.0311 |
| 41 | 0.152 | 8.20 | 0.83033006 | 32.8 | 0.67867975 | 988 | 164 | 0.06254 | 0.0313 |
| 41.25 | 0.152 | 8.25 | 0.83042794 | 33.0 | 0.67828823 | 987 | 165 | 0.06293 | 0.0315 |
| 41.5 | 0.153 | 8.30 | 0.83052554 | 33.2 | 0.67789784 | 986 | 166 | 0.06333 | 0.0317 |
| 41.75 | 0.153 | 8.35 | 0.83062286 | 33.4 | 0.67750854 | 985 | 167 | 0.06372 | 0.0319 |
| 42 | 0.154 | 8.40 | 0.83071991 | 33.6 | 0.67712034 | 984 | 168 | 0.06412 | 0.0321 |
| 42.25 | 0.154 | 8.45 | 0.83081669 | 33.8 | 0.67673323 | 983 | 169 | 0.06452 | 0.0323 |
| 42.5 | 0.155 | 8.50 | 0.83091320 | 34.0 | 0.67634719 | 982 | 170 | 0.06491 | 0.0325 |
| 42.75 | 0.155 | 8.55 | 0.83100945 | 34.2 | 0.67596221 | 981 | 171 | 0.06531 | 0.0327 |
| 43 | 0.156 | 8.60 | 0.83110543 | 34.4 | 0.67557830 | 980 | 172 | 0.06571 | 0.0329 |
| 43.25 | 0.156 | 8.65 | 0.83120114 | 34.6 | 0.67519543 | 979 | 173 | 0.06610 | 0.0331 |
| 43.5 | 0.156 | 8.70 | 0.83129660 | 34.8 | 0.67481359 | 978 | 174 | 0.06650 | 0.0333 |
| 43.75 | 0.157 | 8.75 | 0.83139180 | 35.0 | 0.67443279 | 977 | 175 | 0.06690 | 0.0334 |
| 44 | 0.157 | 8.80 | 0.83148675 | 35.2 | 0.67405301 | 976 | 176 | 0.06730 | 0.0336 |
| 44.25 | 0.158 | 8.85 | 0.83158144 | 35.4 | 0.67367425 | 975 | 177 | 0.06769 | 0.0338 |
| 44.5 | 0.158 | 8.90 | 0.83167588 | 35.6 | 0.67329648 | 974 | 178 | 0.06809 | 0.0340 |
| 44.75 | 0.159 | 8.95 | 0.83177007 | 35.8 | 0.67291972 | 973 | 179 | 0.06849 | 0.0342 |
| 45 | 0.159 | 9.00 | 0.83186402 | 36.0 | 0.67254394 | 972 | 180 | 0.06889 | 0.0344 |
| 45.25 | 0.160 | 9.05 | 0.83195772 | 36.2 | 0.67216914 | 971 | 181 | 0.06929 | 0.0346 |
| 45.5 | 0.160 | 9.10 | 0.83205117 | 36.4 | 0.67179531 | 970 | 182 | 0.06969 | 0.0348 |
| 45.75 | 0.161 | 9.15 | 0.83214439 | 36.6 | 0.67142245 | 969 | 183 | 0.07009 | 0.0350 |
| 46 | 0.161 | 9.20 | 0.83223736 | 36.8 | 0.67105054 | 968 | 184 | 0.07049 | 0.0352 |
| 46.25 | 0.162 | 9.25 | 0.83233010 | 37.0 | 0.67067959 | 967 | 185 | 0.07088 | 0.0354 |
| 46.5 | 0.162 | 9.30 | 0.83242261 | 37.2 | 0.67030957 | 966 | 186 | 0.07128 | 0.0356 |
| 46.75 | 0.163 | 9.35 | 0.83251488 | 37.4 | 0.66994049 | 965 | 187 | 0.07168 | 0.0358 |
| 47 | 0.163 | 9.40 | 0.83260692 | 37.6 | 0.66957233 | 964 | 188 | 0.07208 | 0.0360 |
| 47.25 | 0.163 | 9.45 | 0.83269873 | 37.8 | 0.66920509 | 963 | 189 | 0.07248 | 0.0362 |
| 47.5 | 0.164 | 9.50 | 0.83279031 | 38.0 | 0.66883877 | 962 | 190 | 0.07289 | 0.0364 |
| 47.75 | 0.164 | 9.55 | 0.83288166 | 38.2 | 0.66847335 | 961 | 191 | 0.07329 | 0.0366 |
| 48 | 0.165 | 9.60 | 0.83297279 | 38.4 | 0.66810883 | 960 | 192 | 0.07369 | 0.0368 |
| 48.25 | 0.165 | 9.65 | 0.83306370 | 38.6 | 0.66774520 | 959 | 193 | 0.07409 | 0.0370 |
| 48.5 | 0.166 | 9.70 | 0.83315439 | 38.8 | 0.66738245 | 958 | 194 | 0.07449 | 0.0372 |
| 48.75 | 0.166 | 9.75 | 0.83324485 | 39.0 | 0.66702059 | 957 | 195 | 0.07489 | 0.0374 |
| 49 | 0.167 | 9.80 | 0.83333510 | 39.2 | 0.66665959 | 956 | 196 | 0.07529 | 0.0376 |
| 49.25 | 0.167 | 9.85 | 0.83342514 | 39.4 | 0.66629946 | 955 | 197 | 0.07569 | 0.0378 |
| 49.5 | 0.168 | 9.90 | 0.83351495 | 39.6 | 0.66594018 | 954 | 198 | 0.07610 | 0.0380 |
| 49.75 | 0.168 | 9.95 | 0.83360456 | 39.8 | 0.66558176 | 953 | 199 | 0.07650 | 0.0382 |
| 50 | 0.168 | 10.00 | 0.83369395 | 40.0 | 0.66522418 | 952 | 200 | 0.07690 | 0.0385 |
| 50.25 | 0.169 | 10.05 | 0.83378314 | 40.2 | 0.66486745 | 951 | 201 | 0.07730 | 0.0387 |
| 50.5 | 0.169 | 10.10 | 0.83387211 | 40.4 | 0.66451154 | 950 | 202 | 0.07771 | 0.0389 |
| 50.75 | 0.170 | 10.15 | 0.83396088 | 40.6 | 0.66415647 | 949 | 203 | 0.07811 | 0.0391 |
| 51 | 0.170 | 10.20 | 0.83404945 | 40.8 | 0.66380221 | 948 | 204 | 0.07851 | 0.0393 |
| 51.25 | 0.171 | 10.25 | 0.83413781 | 41.0 | 0.66344877 | 947 | 205 | 0.07892 | 0.0395 |


| 51.5 | 0.171 | 10.30 | 0.83422597 | 41.2 | 0.66309614 | 946 | 206 | 0.07932 | 0.0397 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 51.75 | 0.172 | 10.35 | 0.83431392 | 41.4 | 0.66274431 | 945 | 207 | 0.07972 | 0.0399 |
| 52 | 0.172 | 10.40 | 0.83440168 | 41.6 | 0.66239328 | 944 | 208 | 0.08013 | 0.0401 |
| 52.25 | 0.172 | 10.45 | 0.83448924 | 41.8 | 0.66204304 | 943 | 209 | 0.08053 | 0.0403 |
| 52.5 | 0.173 | 10.50 | 0.83457660 | 42.0 | 0.66169359 | 942 | 210 | 0.08094 | 0.0405 |
| 52.75 | 0.173 | 10.55 | 0.83466377 | 42.2 | 0.66134492 | 941 | 211 | 0.08134 | 0.0407 |
| 53 | 0.174 | 10.60 | 0.83475074 | 42.4 | 0.66099703 | 940 | 212 | 0.08175 | 0.0409 |
| 53.25 | 0.174 | 10.65 | 0.83483752 | 42.6 | 0.66064991 | 939 | 213 | 0.08215 | 0.0411 |
| 53.5 | 0.175 | 10.70 | 0.83492411 | 42.8 | 0.66030355 | 938 | 214 | 0.08256 | 0.0413 |
| 53.75 | 0.175 | 10.75 | 0.83501051 | 43.0 | 0.65995795 | 937 | 215 | 0.08296 | 0.0415 |
| 54 | 0.175 | 10.80 | 0.83509672 | 43.2 | 0.65961311 | 936 | 216 | 0.08337 | 0.0417 |
| 54.25 | 0.176 | 10.85 | 0.83518275 | 43.4 | 0.65926901 | 935 | 217 | 0.08377 | 0.0419 |
| 54.5 | 0.176 | 10.90 | 0.83526858 | 43.6 | 0.65892566 | 934 | 218 | 0.08418 | 0.0421 |
| 54.75 | 0.177 | 10.95 | 0.83535424 | 43.8 | 0.65858305 | 933 | 219 | 0.08459 | 0.0423 |
| 55 | 0.177 | 11.00 | 0.83543971 | 44.0 | 0.65824118 | 932 | 220 | 0.08499 | 0.0425 |
| 55.25 | 0.178 | 11.05 | 0.83552499 | 44.2 | 0.65790003 | 931 | 221 | 0.08540 | 0.0427 |
| 55.5 | 0.178 | 11.10 | 0.83561010 | 44.4 | 0.65755961 | 930 | 222 | 0.08581 | 0.0429 |
| 55.75 | 0.178 | 11.15 | 0.83569502 | 44.6 | 0.65721991 | 929 | 223 | 0.08621 | 0.0431 |
| 56 | 0.179 | 11.20 | 0.83577977 | 44.8 | 0.65688093 | 928 | 224 | 0.08662 | 0.0433 |
| 56.25 | 0.179 | 11.25 | 0.83586434 | 45.0 | 0.65654265 | 927 | 225 | 0.08703 | 0.0435 |
| 56.5 | 0.180 | 11.30 | 0.83594873 | 45.2 | 0.65620508 | 926 | 226 | 0.08744 | 0.0437 |
| 56.75 | 0.180 | 11.35 | 0.83603295 | 45.4 | 0.65586821 | 925 | 227 | 0.08784 | 0.0439 |
| 57 | 0.181 | 11.40 | 0.83611699 | 45.6 | 0.65553204 | 924 | 228 | 0.08825 | 0.0441 |
| 57.25 | 0.181 | 11.45 | 0.83620086 | 45.8 | 0.65519656 | 923 | 229 | 0.08866 | 0.0443 |
| 57.5 | 0.181 | 11.50 | 0.83628456 | 46.0 | 0.65486177 | 922 | 230 | 0.08907 | 0.0445 |
| 57.75 | 0.182 | 11.55 | 0.83636808 | 46.2 | 0.65452766 | 921 | 231 | 0.08948 | 0.0447 |
| 58 | 0.182 | 11.60 | 0.83645144 | 46.4 | 0.65419423 | 920 | 232 | 0.08989 | 0.0449 |
| 58.25 | 0.183 | 11.65 | 0.83653463 | 46.6 | 0.65386148 | 919 | 233 | 0.09030 | 0.0451 |
| 58.5 | 0.183 | 11.70 | 0.83661765 | 46.8 | 0.65352940 | 918 | 234 | 0.09071 | 0.0454 |
| 58.75 | 0.184 | 11.75 | 0.83670051 | 47.0 | 0.65319798 | 917 | 235 | 0.09111 | 0.0456 |
| 59 | 0.184 | 11.80 | 0.83678319 | 47.2 | 0.65286722 | 916 | 236 | 0.09152 | 0.0458 |
| 59.25 | 0.184 | 11.85 | 0.83686572 | 47.4 | 0.65253713 | 915 | 237 | 0.09193 | 0.0460 |
| 59.5 | 0.185 | 11.90 | 0.83694808 | 47.6 | 0.65220768 | 914 | 238 | 0.09234 | 0.0462 |
| 59.75 | 0.185 | 11.95 | 0.83703028 | 47.8 | 0.65187889 | 913 | 239 | 0.09276 | 0.0464 |
| 60 | 0.186 | 12.00 | 0.83711231 | 48.0 | 0.65155074 | 912 | 240 | 0.09317 | 0.0466 |
| 60.25 | 0.186 | 12.05 | 0.83719419 | 48.2 | 0.65122324 | 911 | 241 | 0.09358 | 0.0468 |
| 60.5 | 0.186 | 12.10 | 0.83727591 | 48.4 | 0.65089637 | 910 | 242 | 0.09399 | 0.0470 |
| 60.75 | 0.187 | 12.15 | 0.83735747 | 48.6 | 0.65057014 | 909 | 243 | 0.09440 | 0.0472 |
| 61 | 0.187 | 12.20 | 0.83743887 | 48.8 | 0.65024454 | 908 | 244 | 0.09481 | 0.0474 |
| 61.25 | 0.188 | 12.25 | 0.83752011 | 49.0 | 0.64991956 | 907 | 245 | 0.09522 | 0.0476 |
| 61.5 | 0.188 | 12.30 | 0.83760120 | 49.2 | 0.64959521 | 906 | 246 | 0.09563 | 0.0478 |
| 61.75 | 0.188 | 12.35 | 0.83768213 | 49.4 | 0.64927147 | 905 | 247 | 0.09605 | 0.0480 |
| 62 | 0.189 | 12.40 | 0.83776291 | 49.6 | 0.64894835 | 904 | 248 | 0.09646 | 0.0482 |
| 62.25 | 0.189 | 12.45 | 0.83784354 | 49.8 | 0.64862585 | 903 | 249 | 0.09687 | 0.0484 |
| 62.5 | 0.190 | 12.50 | 0.83792401 | 50.0 | 0.64830395 | 902 | 250 | 0.09728 | 0.0486 |
| 62.75 | 0.190 | 12.55 | 0.83800434 | 50.2 | 0.64798266 | 901 | 251 | 0.09770 | 0.0488 |
| 63 | 0.190 | 12.60 | 0.83808451 | 50.4 | 0.64766196 | 900 | 252 | 0.09811 | 0.0491 |
| 63.25 | 0.191 | 12.65 | 0.83816453 | 50.6 | 0.64734187 | 899 | 253 | 0.09852 | 0.0493 |
| 63.5 | 0.191 | 12.70 | 0.83824441 | 50.8 | 0.64702237 | 898 | 254 | 0.09894 | 0.0495 |
| 63.75 | 0.192 | 12.75 | 0.83832414 | 51.0 | 0.64670346 | 897 | 255 | 0.09935 | 0.0497 |
| 64 | 0.192 | 12.80 | 0.83840372 | 51.2 | 0.64638513 | 896 | 256 | 0.09977 | 0.0499 |
| 64.25 | 0.192 | 12.85 | 0.83848315 | 51.4 | 0.64606739 | 895 | 257 | 0.10018 | 0.0501 |
| 64.5 | 0.193 | 12.90 | 0.83856244 | 51.6 | 0.64575023 | 894 | 258 | 0.10059 | 0.0503 |
| 64.75 | 0.193 | 12.95 | 0.83864159 | 51.8 | 0.64543365 | 893 | 259 | 0.10101 | 0.0505 |
| 65 | 0.194 | 13.00 | 0.83872059 | 52.0 | 0.64511764 | 892 | 260 | 0.10142 | 0.0507 |
| 65.25 | 0.194 | 13.05 | 0.83879945 | 52.2 | 0.64480221 | 891 | 261 | 0.10184 | 0.0509 |
| 65.5 | 0.194 | 13.10 | 0.83887817 | 52.4 | 0.64448734 | 890 | 262 | 0.10225 | 0.0511 |
| 65.75 | 0.195 | 13.15 | 0.83895674 | 52.6 | 0.64417303 | 889 | 263 | 0.10267 | 0.0513 |
| 66 | 0.195 | 13.20 | 0.83903518 | 52.8 | 0.64385929 | 888 | 264 | 0.10309 | 0.0515 |
| 66.25 | 0.196 | 13.25 | 0.83911347 | 53.0 | 0.64354610 | 887 | 265 | 0.10350 | 0.0518 |
| 66.5 | 0.196 | 13.30 | 0.83919163 | 53.2 | 0.64323347 | 886 | 266 | 0.10392 | 0.0520 |
| 66.75 | 0.196 | 13.35 | 0.83926965 | 53.4 | 0.64292139 | 885 | 267 | 0.10434 | 0.0522 |
| 67 | 0.197 | 13.40 | 0.83934753 | 53.6 | 0.64260986 | 884 | 268 | 0.10475 | 0.0524 |
| 67.25 | 0.197 | 13.45 | 0.83942528 | 53.8 | 0.64229888 | 883 | 269 | 0.10517 | 0.0526 |
| 67.5 | 0.198 | 13.50 | 0.83950289 | 54.0 | 0.64198844 | 882 | 270 | 0.10559 | 0.0528 |
| 67.75 | 0.198 | 13.55 | 0.83958037 | 54.2 | 0.64167854 | 881 | 271 | 0.10600 | 0.0530 |
| 68 | 0.198 | 13.60 | 0.83965771 | 54.4 | 0.64136917 | 880 | 272 | 0.10642 | 0.0532 |
| 68.25 | 0.199 | 13.65 | 0.83973491 | 54.6 | 0.64106034 | 879 | 273 | 0.10684 | 0.0534 |
| 68.5 | 0.199 | 13.70 | 0.83981199 | 54.8 | 0.64075204 | 878 | 274 | 0.10726 | 0.0536 |
| 68.75 | 0.199 | 13.75 | 0.83988893 | 55.0 | 0.64044427 | 877 | 275 | 0.10768 | 0.0538 |
| 69 | 0.200 | 13.80 | 0.83996574 | 55.2 | 0.64013703 | 876 | 276 | 0.10809 | 0.0540 |


| 69.25 | 0.200 | 13.85 | 0.84004242 | 55.4 | 0.63983031 | 875 | 277 | 0.10851 | 0.0543 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 69.5 | 0.201 | 13.90 | 0.84011897 | 55.6 | 0.63952410 | 874 | 278 | 0.10893 | 0.0545 |
| 69.75 | 0.201 | 13.95 | 0.84019540 | 55.8 | 0.63921842 | 873 | 279 | 0.10935 | 0.0547 |
| 70 | 0.201 | 14.00 | 0.84027169 | 56.0 | 0.63891325 | 872 | 280 | 0.10977 | 0.0549 |
| 70.25 | 0.202 | 14.05 | 0.84034785 | 56.2 | 0.63860859 | 871 | 281 | 0.11019 | 0.0551 |
| 70.5 | 0.202 | 14.10 | 0.84042389 | 56.4 | 0.63830444 | 870 | 282 | 0.11061 | 0.0553 |
| 70.75 | 0.202 | 14.15 | 0.84049980 | 56.6 | 0.63800080 | 869 | 283 | 0.11103 | 0.0555 |
| 71 | 0.203 | 14.20 | 0.84057559 | 56.8 | 0.63769766 | 868 | 284 | 0.11145 | 0.0557 |
| 71.25 | 0.203 | 14.25 | 0.84065125 | 57.0 | 0.63739502 | 867 | 285 | 0.11187 | 0.0559 |
| 71.5 | 0.204 | 14.30 | 0.84072678 | 57.2 | 0.63709288 | 866 | 286 | 0.11229 | 0.0561 |
| 71.75 | 0.204 | 14.35 | 0.84080219 | 57.4 | 0.63679124 | 865 | 287 | 0.11271 | 0.0564 |
| 72 | 0.204 | 14.40 | 0.84087748 | 57.6 | 0.63649009 | 864 | 288 | 0.11313 | 0.0566 |
| 72.25 | 0.205 | 14.45 | 0.84095264 | 57.8 | 0.63618943 | 863 | 289 | 0.11355 | 0.0568 |
| 72.5 | 0.205 | 14.50 | 0.84102769 | 58.0 | 0.63588926 | 862 | 290 | 0.11398 | 0.0570 |
| 72.75 | 0.206 | 14.55 | 0.84110261 | 58.2 | 0.63558957 | 861 | 291 | 0.11440 | 0.0572 |
| 73 | 0.206 | 14.60 | 0.84117741 | 58.4 | 0.63529037 | 860 | 292 | 0.11482 | 0.0574 |
| 73.25 | 0.206 | 14.65 | 0.84125209 | 58.6 | 0.63499165 | 859 | 293 | 0.11524 | 0.0576 |
| 73.5 | 0.207 | 14.70 | 0.84132665 | 58.8 | 0.63469341 | 858 | 294 | 0.11567 | 0.0578 |
| 73.75 | 0.207 | 14.75 | 0.84140109 | 59.0 | 0.63439565 | 857 | 295 | 0.11609 | 0.0580 |
| 74 | 0.207 | 14.80 | 0.84147541 | 59.2 | 0.63409836 | 856 | 296 | 0.11651 | 0.0583 |
| 74.25 | 0.208 | 14.85 | 0.84154961 | 59.4 | 0.63380154 | 855 | 297 | 0.11693 | 0.0585 |
| 74.5 | 0.208 | 14.90 | 0.84162370 | 59.6 | 0.63350519 | 854 | 298 | 0.11736 | 0.0587 |
| 74.75 | 0.208 | 14.95 | 0.84169767 | 59.8 | 0.63320931 | 853 | 299 | 0.11778 | 0.0589 |
| 75 | 0.209 | 15.00 | 0.84177153 | 60.0 | 0.63291389 | 852 | 300 | 0.11821 | 0.0591 |
| 75.25 | 0.209 | 15.05 | 0.84184526 | 60.2 | 0.63261894 | 851 | 301 | 0.11863 | 0.0593 |
| 75.5 | 0.210 | 15.10 | 0.84191889 | 60.4 | 0.63232445 | 850 | 302 | 0.11905 | 0.0595 |
| 75.75 | 0.210 | 15.15 | 0.84199240 | 60.6 | 0.63203041 | 849 | 303 | 0.11948 | 0.0597 |
| 76 | 0.210 | 15.20 | 0.84206579 | 60.8 | 0.63173683 | 848 | 304 | 0.11990 | 0.0600 |
| 76.25 | 0.211 | 15.25 | 0.84213907 | 61.0 | 0.63144370 | 847 | 305 | 0.12033 | 0.0602 |
| 76.5 | 0.211 | 15.30 | 0.84221224 | 61.2 | 0.63115103 | 846 | 306 | 0.12075 | 0.0604 |
| 76.75 | 0.211 | 15.35 | 0.84228530 | 61.4 | 0.63085880 | 845 | 307 | 0.12118 | 0.0606 |
| 77 | 0.212 | 15.40 | 0.84235825 | 61.6 | 0.63056702 | 844 | 308 | 0.12161 | 0.0608 |
| 77.25 | 0.212 | 15.45 | 0.84243108 | 61.8 | 0.63027568 | 843 | 309 | 0.12203 | 0.0610 |
| 77.5 | 0.213 | 15.50 | 0.84250380 | 62.0 | 0.62998479 | 842 | 310 | 0.12246 | 0.0612 |
| 77.75 | 0.213 | 15.55 | 0.84257641 | 62.2 | 0.62969434 | 841 | 311 | 0.12289 | 0.0614 |
| 78 | 0.213 | 15.60 | 0.84264892 | 62.4 | 0.62940433 | 840 | 312 | 0.12331 | 0.0617 |
| 78.25 | 0.214 | 15.65 | 0.84272131 | 62.6 | 0.62911475 | 839 | 313 | 0.12374 | 0.0619 |
| 78.5 | 0.214 | 15.70 | 0.84279360 | 62.8 | 0.62882561 | 838 | 314 | 0.12417 | 0.0621 |
| 78.75 | 0.214 | 15.75 | 0.84286577 | 63.0 | 0.62853690 | 837 | 315 | 0.12459 | 0.0623 |
| 79 | 0.215 | 15.80 | 0.84293784 | 63.2 | 0.62824862 | 836 | 316 | 0.12502 | 0.0625 |
| 79.25 | 0.215 | 15.85 | 0.84300981 | 63.4 | 0.62796077 | 835 | 317 | 0.12545 | 0.0627 |
| 79.5 | 0.215 | 15.90 | 0.84308166 | 63.6 | 0.62767335 | 834 | 318 | 0.12588 | 0.0629 |
| 79.75 | 0.216 | 15.95 | 0.84315341 | 63.8 | 0.62738635 | 833 | 319 | 0.12631 | 0.0632 |
| 80 | 0.216 | 16.00 | 0.84322506 | 64.0 | 0.62709977 | 832 | 320 | 0.12674 | 0.0634 |
| 80.25 | 0.216 | 16.05 | 0.84329660 | 64.2 | 0.62681362 | 831 | 321 | 0.12716 | 0.0636 |
| 80.5 | 0.217 | 16.10 | 0.84336803 | 64.4 | 0.62652788 | 830 | 322 | 0.12759 | 0.0638 |
| 80.75 | 0.217 | 16.15 | 0.84343936 | 64.6 | 0.62624256 | 829 | 323 | 0.12802 | 0.0640 |
| 81 | 0.218 | 16.20 | 0.84351059 | 64.8 | 0.62595766 | 828 | 324 | 0.12845 | 0.0642 |
| 81.25 | 0.218 | 16.25 | 0.84358171 | 65.0 | 0.62567316 | 827 | 325 | 0.12888 | 0.0644 |
| 81.5 | 0.218 | 16.30 | 0.84365273 | 65.2 | 0.62538908 | 826 | 326 | 0.12931 | 0.0647 |
| 81.75 | 0.219 | 16.35 | 0.84372365 | 65.4 | 0.62510541 | 825 | 327 | 0.12974 | 0.0649 |
| 82 | 0.219 | 16.40 | 0.84379446 | 65.6 | 0.62482214 | 824 | 328 | 0.13017 | 0.0651 |
| 82.25 | 0.219 | 16.45 | 0.84386518 | 65.8 | 0.62453928 | 823 | 329 | 0.13061 | 0.0653 |
| 82.5 | 0.220 | 16.50 | 0.84393579 | 66.0 | 0.62425683 | 822 | 330 | 0.13104 | 0.0655 |
| 82.75 | 0.220 | 16.55 | 0.84400631 | 66.2 | 0.62397478 | 821 | 331 | 0.13147 | 0.0657 |
| 83 | 0.220 | 16.60 | 0.84407672 | 66.4 | 0.62369312 | 820 | 332 | 0.13190 | 0.0659 |
| 83.25 | 0.221 | 16.65 | 0.84414703 | 66.6 | 0.62341187 | 819 | 333 | 0.13233 | 0.0662 |
| 83.5 | 0.221 | 16.70 | 0.84421725 | 66.8 | 0.62313101 | 818 | 334 | 0.13276 | 0.0664 |
| 83.75 | 0.221 | 16.75 | 0.84428736 | 67.0 | 0.62285055 | 817 | 335 | 0.13320 | 0.0666 |
| 84 | 0.222 | 16.80 | 0.84435738 | 67.2 | 0.62257048 | 816 | 336 | 0.13363 | 0.0668 |
| 84.25 | 0.222 | 16.85 | 0.84442730 | 67.4 | 0.62229080 | 815 | 337 | 0.13406 | 0.0670 |
| 84.5 | 0.222 | 16.90 | 0.84449712 | 67.6 | 0.62201151 | 814 | 338 | 0.13450 | 0.0672 |
| 84.75 | 0.223 | 16.95 | 0.84456685 | 67.8 | 0.62173261 | 813 | 339 | 0.13493 | 0.0675 |
| 85 | 0.223 | 17.00 | 0.84463648 | 68.0 | 0.62145409 | 812 | 340 | 0.13536 | 0.0677 |
| 85.25 | 0.224 | 17.05 | 0.84470601 | 68.2 | 0.62117596 | 811 | 341 | 0.13580 | 0.0679 |
| 85.5 | 0.224 | 17.10 | 0.84477545 | 68.4 | 0.62089822 | 810 | 342 | 0.13623 | 0.0681 |
| 85.75 | 0.224 | 17.15 | 0.84484479 | 68.6 | 0.62062085 | 809 | 343 | 0.13667 | 0.0683 |
| 86 | 0.225 | 17.20 | 0.84491403 | 68.8 | 0.62034387 | 808 | 344 | 0.13710 | 0.0685 |
| 86.25 | 0.225 | 17.25 | 0.84498318 | 69.0 | 0.62006726 | 807 | 345 | 0.13753 | 0.0688 |
| 86.5 | 0.225 | 17.30 | 0.84505224 | 69.2 | 0.61979103 | 806 | 346 | 0.13797 | 0.0690 |
| 86.75 | 0.226 | 17.35 | 0.84512121 | 69.4 | 0.61951518 | 805 | 347 | 0.13841 | 0.0692 |


| 87 | 0.226 | 17.40 | 0.84519008 | 69.6 | 0.61923969 | 804 | 348 | 0.13884 | 0.0694 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 87.25 | 0.226 | 17.45 | 0.84525885 | 69.8 | 0.61896458 | 803 | 349 | 0.13928 | 0.0696 |
| 87.5 | 0.227 | 17.50 | 0.84532754 | 70.0 | 0.61868984 | 802 | 350 | 0.13971 | 0.0699 |
| 87.75 | 0.227 | 17.55 | 0.84539613 | 70.2 | 0.61841547 | 801 | 351 | 0.14015 | 0.0701 |
| 88 | 0.227 | 17.60 | 0.84546463 | 70.4 | 0.61814147 | 800 | 352 | 0.14059 | 0.0703 |
| 88.25 | 0.228 | 17.65 | 0.84553304 | 70.6 | 0.61786783 | 799 | 353 | 0.14102 | 0.0705 |
| 88.5 | 0.228 | 17.70 | 0.84560136 | 70.8 | 0.61759455 | 798 | 354 | 0.14146 | 0.0707 |
| 88.75 | 0.228 | 17.75 | 0.84566959 | 71.0 | 0.61732164 | 797 | 355 | 0.14190 | 0.0709 |
| 89 | 0.229 | 17.80 | 0.84573773 | 71.2 | 0.61704909 | 796 | 356 | 0.14234 | 0.0712 |
| 89.25 | 0.229 | 17.85 | 0.84580577 | 71.4 | 0.61677690 | 795 | 357 | 0.14277 | 0.0714 |
| 89.5 | 0.229 | 17.90 | 0.84587373 | 71.6 | 0.61650507 | 794 | 358 | 0.14321 | 0.0716 |
| 89.75 | 0.230 | 17.95 | 0.84594160 | 71.8 | 0.61623359 | 793 | 359 | 0.14365 | 0.0718 |
| 90 | 0.230 | 18.00 | 0.84600938 | 72.0 | 0.61596247 | 792 | 360 | 0.14409 | 0.0720 |
| 90.25 | 0.230 | 18.05 | 0.84607707 | 72.2 | 0.61569170 | 791 | 361 | 0.14453 | 0.0723 |
| 90.5 | 0.231 | 18.10 | 0.84614468 | 72.4 | 0.61542129 | 790 | 362 | 0.14497 | 0.0725 |
| 90.75 | 0.231 | 18.15 | 0.84621219 | 72.6 | 0.61515122 | 789 | 363 | 0.14541 | 0.0727 |
| 91 | 0.231 | 18.20 | 0.84627962 | 72.8 | 0.61488151 | 788 | 364 | 0.14585 | 0.0729 |
| 91.25 | 0.232 | 18.25 | 0.84634696 | 73.0 | 0.61461214 | 787 | 365 | 0.14629 | 0.0731 |
| 91.5 | 0.232 | 18.30 | 0.84641422 | 73.2 | 0.61434312 | 786 | 366 | 0.14673 | 0.0734 |
| 91.75 | 0.232 | 18.35 | 0.84648139 | 73.4 | 0.61407445 | 785 | 367 | 0.14717 | 0.0736 |
| 92 | 0.233 | 18.40 | 0.84654847 | 73.6 | 0.61380611 | 784 | 368 | 0.14761 | 0.0738 |
| 92.25 | 0.233 | 18.45 | 0.84661547 | 73.8 | 0.61353813 | 783 | 369 | 0.14805 | 0.0740 |
| 92.5 | 0.233 | 18.50 | 0.84668238 | 74.0 | 0.61327048 | 782 | 370 | 0.14849 | 0.0742 |
| 92.75 | 0.234 | 18.55 | 0.84674921 | 74.2 | 0.61300317 | 781 | 371 | 0.14893 | 0.0745 |
| 93 | 0.234 | 18.60 | 0.84681595 | 74.4 | 0.61273620 | 780 | 372 | 0.14938 | 0.0747 |
| 93.25 | 0.234 | 18.65 | 0.84688261 | 74.6 | 0.61246957 | 779 | 373 | 0.14982 | 0.0749 |
| 93.5 | 0.235 | 18.70 | 0.84694918 | 74.8 | 0.61220327 | 778 | 374 | 0.15026 | 0.0751 |
| 93.75 | 0.235 | 18.75 | 0.84701567 | 75.0 | 0.61193731 | 777 | 375 | 0.15070 | 0.0754 |
| 94 | 0.235 | 18.80 | 0.84708208 | 75.2 | 0.61167168 | 776 | 376 | 0.15115 | 0.0756 |
| 94.25 | 0.236 | 18.85 | 0.84714840 | 75.4 | 0.61140638 | 775 | 377 | 0.15159 | 0.0758 |
| 94.5 | 0.236 | 18.90 | 0.84721465 | 75.6 | 0.61114142 | 774 | 378 | 0.15203 | 0.0760 |
| 94.75 | 0.236 | 18.95 | 0.84728080 | 75.8 | 0.61087678 | 773 | 379 | 0.15248 | 0.0762 |
| 95 | 0.237 | 19.00 | 0.84734688 | 76.0 | 0.61061247 | 772 | 380 | 0.15292 | 0.0765 |
| 95.25 | 0.237 | 19.05 | 0.84741288 | 76.2 | 0.61034849 | 771 | 381 | 0.15337 | 0.0767 |
| 95.5 | 0.237 | 19.10 | 0.84747879 | 76.4 | 0.61008483 | 770 | 382 | 0.15381 | 0.0769 |
| 95.75 | 0.238 | 19.15 | 0.84754463 | 76.6 | 0.60982150 | 769 | 383 | 0.15425 | 0.0771 |
| 96 | 0.238 | 19.20 | 0.84761038 | 76.8 | 0.60955849 | 768 | 384 | 0.15470 | 0.0774 |
| 96.25 | 0.238 | 19.25 | 0.84767605 | 77.0 | 0.60929580 | 767 | 385 | 0.15515 | 0.0776 |
| 96.5 | 0.239 | 19.30 | 0.84774164 | 77.2 | 0.60903343 | 766 | 386 | 0.15559 | 0.0778 |
| 96.75 | 0.239 | 19.35 | 0.84780715 | 77.4 | 0.60877138 | 765 | 387 | 0.15604 | 0.0780 |
| 97 | 0.239 | 19.40 | 0.84787259 | 77.6 | 0.60850965 | 764 | 388 | 0.15648 | 0.0782 |
| 97.25 | 0.240 | 19.45 | 0.84793794 | 77.8 | 0.60824824 | 763 | 389 | 0.15693 | 0.0785 |
| 97.5 | 0.240 | 19.50 | 0.84800321 | 78.0 | 0.60798714 | 762 | 390 | 0.15738 | 0.0787 |
| 97.75 | 0.240 | 19.55 | 0.84806841 | 78.2 | 0.60772636 | 761 | 391 | 0.15782 | 0.0789 |
| 98 | 0.241 | 19.60 | 0.84813353 | 78.4 | 0.60746589 | 760 | 392 | 0.15827 | 0.0791 |
| 98.25 | 0.241 | 19.65 | 0.84819857 | 78.6 | 0.60720573 | 759 | 393 | 0.15872 | 0.0794 |
| 98.5 | 0.241 | 19.70 | 0.84826353 | 78.8 | 0.60694588 | 758 | 394 | 0.15917 | 0.0796 |
| 98.75 | 0.242 | 19.75 | 0.84832841 | 79.0 | 0.60668635 | 757 | 395 | 0.15962 | 0.0798 |
| 99 | 0.242 | 19.80 | 0.84839322 | 79.2 | 0.60642712 | 756 | 396 | 0.16006 | 0.0800 |
| 99.25 | 0.242 | 19.85 | 0.84845795 | 79.4 | 0.60616820 | 755 | 397 | 0.16051 | 0.0803 |
| 99.5 | 0.243 | 19.90 | 0.84852260 | 79.6 | 0.60590958 | 754 | 398 | 0.16096 | 0.0805 |
| 99.75 | 0.243 | 19.95 | 0.84858718 | 79.8 | 0.60565127 | 753 | 399 | 0.16141 | 0.0807 |
| 100 | 0.243 | 20.00 | 0.84865168 | 80.0 | 0.60539327 | 752 | 400 | 0.16186 | 0.0809 |
| 100.25 | 0.244 | 20.05 | 0.84871611 | 80.2 | 0.60513556 | 751 | 401 | 0.16231 | 0.0812 |
| 100.5 | 0.244 | 20.10 | 0.84878046 | 80.4 | 0.60487816 | 750 | 402 | 0.16276 | 0.0814 |
| 100.75 | 0.244 | 20.15 | 0.84884473 | 80.6 | 0.60462106 | 749 | 403 | 0.16321 | 0.0816 |
| 101 | 0.245 | 20.20 | 0.84890893 | 80.8 | 0.60436426 | 748 | 404 | 0.16366 | 0.0818 |
| 101.25 | 0.245 | 20.25 | 0.84897306 | 81.0 | 0.60410776 | 747 | 405 | 0.16411 | 0.0821 |
| 101.5 | 0.245 | 20.30 | 0.84903711 | 81.2 | 0.60385156 | 746 | 406 | 0.16456 | 0.0823 |
| 101.75 | 0.246 | 20.35 | 0.84910109 | 81.4 | 0.60359565 | 745 | 407 | 0.16502 | 0.0825 |
| 102 | 0.246 | 20.40 | 0.84916499 | 81.6 | 0.60334004 | 744 | 408 | 0.16547 | 0.0827 |
| 102.25 | 0.246 | 20.45 | 0.84922882 | 81.8 | 0.60308472 | 743 | 409 | 0.16592 | 0.0830 |
| 102.5 | 0.246 | 20.50 | 0.84929258 | 82.0 | 0.60282969 | 742 | 410 | 0.16637 | 0.0832 |
| 102.75 | 0.247 | 20.55 | 0.84935626 | 82.2 | 0.60257496 | 741 | 411 | 0.16682 | 0.0834 |
| 103 | 0.247 | 20.60 | 0.84941987 | 82.4 | 0.60232052 | 740 | 412 | 0.16728 | 0.0836 |
| 103.25 | 0.247 | 20.65 | 0.84948341 | 82.6 | 0.60206637 | 739 | 413 | 0.16773 | 0.0839 |
| 103.5 | 0.248 | 20.70 | 0.84954687 | 82.8 | 0.60181250 | 738 | 414 | 0.16818 | 0.0841 |
| 103.75 | 0.248 | 20.75 | 0.84961027 | 83.0 | 0.60155893 | 737 | 415 | 0.16864 | 0.0843 |
| 104 | 0.248 | 20.80 | 0.84967359 | 83.2 | 0.60130564 | 736 | 416 | 0.16909 | 0.0845 |
| 104.25 | 0.249 | 20.85 | 0.84973684 | 83.4 | 0.60105264 | 735 | 417 | 0.16955 | 0.0848 |
| 104.5 | 0.249 | 20.90 | 0.84980002 | 83.6 | 0.60079992 | 734 | 418 | 0.17000 | 0.0850 |


| 104.75 | 0.249 | 20.95 | 0.84986313 | 83.8 | 0.60054749 | 733 | 419 | 0.17046 | 0.0852 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 105 | 0.250 | 21.00 | 0.84992616 | 84.0 | 0.60029534 | 732 | 420 | 0.17091 | 0.0855 |
| 105.25 | 0.250 | 21.05 | 0.84998913 | 84.2 | 0.60004347 | 731 | 421 | 0.17137 | 0.0857 |
| 105.5 | 0.250 | 21.10 | 0.85005203 | 84.4 | 0.59979189 | 730 | 422 | 0.17182 | 0.0859 |
| 105.75 | 0.251 | 21.15 | 0.85011485 | 84.6 | 0.59954058 | 729 | 423 | 0.17228 | 0.0861 |
| 106 | 0.251 | 21.20 | 0.85017761 | 84.8 | 0.59928955 | 728 | 424 | 0.17274 | 0.0864 |
| 106.25 | 0.251 | 21.25 | 0.85024030 | 85.0 | 0.59903881 | 727 | 425 | 0.17319 | 0.0866 |
| 106.5 | 0.252 | 21.30 | 0.85030292 | 85.2 | 0.59878833 | 726 | 426 | 0.17365 | 0.0868 |
| 106.75 | 0.252 | 21.35 | 0.85036547 | 85.4 | 0.59853814 | 725 | 427 | 0.17411 | 0.0871 |
| 107 | 0.252 | 21.40 | 0.85042795 | 85.6 | 0.59828822 | 724 | 428 | 0.17457 | 0.0873 |
| 107.25 | 0.252 | 21.45 | 0.85049036 | 85.8 | 0.59803857 | 723 | 429 | 0.17502 | 0.0875 |
| 107.5 | 0.253 | 21.50 | 0.85055270 | 86.0 | 0.59778920 | 722 | 430 | 0.17548 | 0.0877 |
| 107.75 | 0.253 | 21.55 | 0.85061498 | 86.2 | 0.59754010 | 721 | 431 | 0.17594 | 0.0880 |
| 108 | 0.253 | 21.60 | 0.85067718 | 86.4 | 0.59729127 | 720 | 432 | 0.17640 | 0.0882 |
| 108.25 | 0.254 | 21.65 | 0.85073932 | 86.6 | 0.59704271 | 719 | 433 | 0.17686 | 0.0884 |
| 108.5 | 0.254 | 21.70 | 0.85080139 | 86.8 | 0.59679442 | 718 | 434 | 0.17732 | 0.0887 |
| 108.75 | 0.254 | 21.75 | 0.85086340 | 87.0 | 0.59654640 | 717 | 435 | 0.17778 | 0.0889 |
| 109 | 0.255 | 21.80 | 0.85092534 | 87.2 | 0.59629865 | 716 | 436 | 0.17824 | 0.0891 |
| 109.25 | 0.255 | 21.85 | 0.85098721 | 87.4 | 0.59605116 | 715 | 437 | 0.17870 | 0.0893 |
| 109.5 | 0.255 | 21.90 | 0.85104901 | 87.6 | 0.59580394 | 714 | 438 | 0.17916 | 0.0896 |
| 109.75 | 0.256 | 21.95 | 0.85111075 | 87.8 | 0.59555699 | 713 | 439 | 0.17962 | 0.0898 |
| 110 | 0.256 | 22.00 | 0.85117242 | 88.0 | 0.59531030 | 712 | 440 | 0.18008 | 0.0900 |
| 110.25 | 0.256 | 22.05 | 0.85123403 | 88.2 | 0.59506387 | 711 | 441 | 0.18054 | 0.0903 |
| 110.5 | 0.256 | 22.10 | 0.85129557 | 88.4 | 0.59481771 | 710 | 442 | 0.18101 | 0.0905 |
| 110.75 | 0.257 | 22.15 | 0.85135705 | 88.6 | 0.59457181 | 709 | 443 | 0.18147 | 0.0907 |
| 111 | 0.257 | 22.20 | 0.85141846 | 88.8 | 0.59432617 | 708 | 444 | 0.18193 | 0.0910 |
| 111.25 | 0.257 | 22.25 | 0.85147980 | 89.0 | 0.59408078 | 707 | 445 | 0.18239 | 0.0912 |
| 111.5 | 0.258 | 22.30 | 0.85154108 | 89.2 | 0.59383566 | 706 | 446 | 0.18286 | 0.0914 |
| 111.75 | 0.258 | 22.35 | 0.85160230 | 89.4 | 0.59359080 | 705 | 447 | 0.18332 | 0.0917 |
| 112 | 0.258 | 22.40 | 0.85166345 | 89.6 | 0.59334619 | 704 | 448 | 0.18378 | 0.0919 |
| 112.25 | 0.259 | 22.45 | 0.85172454 | 89.8 | 0.59310184 | 703 | 449 | 0.18425 | 0.0921 |
| 112.5 | 0.259 | 22.50 | 0.85178556 | 90.0 | 0.59285774 | 702 | 450 | 0.18471 | 0.0924 |
| 112.75 | 0.259 | 22.55 | 0.85184652 | 90.2 | 0.59261390 | 701 | 451 | 0.18518 | 0.0926 |
| 113 | 0.260 | 22.60 | 0.85190742 | 90.4 | 0.59237032 | 700 | 452 | 0.18564 | 0.0928 |
| 113.25 | 0.260 | 22.65 | 0.85196825 | 90.6 | 0.59212698 | 699 | 453 | 0.18611 | 0.0931 |
| 113.5 | 0.260 | 22.70 | 0.85202902 | 90.8 | 0.59188390 | 698 | 454 | 0.18657 | 0.0933 |
| 113.75 | 0.260 | 22.75 | 0.85208973 | 91.0 | 0.59164107 | 697 | 455 | 0.18704 | 0.0935 |
| 114 | 0.261 | 22.80 | 0.85215038 | 91.2 | 0.59139850 | 696 | 456 | 0.18750 | 0.0938 |
| 114.25 | 0.261 | 22.85 | 0.85221096 | 91.4 | 0.59115617 | 695 | 457 | 0.18797 | 0.0940 |
| 114.5 | 0.261 | 22.90 | 0.85227148 | 91.6 | 0.59091409 | 694 | 458 | 0.18844 | 0.0942 |
| 114.75 | 0.262 | 22.95 | 0.85233194 | 91.8 | 0.59067226 | 693 | 459 | 0.18890 | 0.0945 |
| 115 | 0.262 | 23.00 | 0.85239233 | 92.0 | 0.59043067 | 692 | 460 | 0.18937 | 0.0947 |
| 115.25 | 0.262 | 23.05 | 0.85245267 | 92.2 | 0.59018933 | 691 | 461 | 0.18984 | 0.0949 |
| 115.5 | 0.263 | 23.10 | 0.85251294 | 92.4 | 0.58994824 | 690 | 462 | 0.19031 | 0.0952 |
| 115.75 | 0.263 | 23.15 | 0.85257315 | 92.6 | 0.58970740 | 689 | 463 | 0.19078 | 0.0954 |
| 116 | 0.263 | 23.20 | 0.85263330 | 92.8 | 0.58946680 | 688 | 464 | 0.19125 | 0.0956 |
| 116.25 | 0.263 | 23.25 | 0.85269339 | 93.0 | 0.58922644 | 687 | 465 | 0.19171 | 0.0959 |
| 116.5 | 0.264 | 23.30 | 0.85275342 | 93.2 | 0.58898632 | 686 | 466 | 0.19218 | 0.0961 |
| 116.75 | 0.264 | 23.35 | 0.85281339 | 93.4 | 0.58874645 | 685 | 467 | 0.19265 | 0.0963 |
| 117 | 0.264 | 23.40 | 0.85287330 | 93.6 | 0.58850682 | 684 | 468 | 0.19312 | 0.0966 |
| 117.25 | 0.265 | 23.45 | 0.85293314 | 93.8 | 0.58826743 | 683 | 469 | 0.19359 | 0.0968 |
| 117.5 | 0.265 | 23.50 | 0.85299293 | 94.0 | 0.58802827 | 682 | 470 | 0.19407 | 0.0970 |
| 117.75 | 0.265 | 23.55 | 0.85305266 | 94.2 | 0.58778936 | 681 | 471 | 0.19454 | 0.0973 |
| 118 | 0.266 | 23.60 | 0.85311233 | 94.4 | 0.58755069 | 680 | 472 | 0.19501 | 0.0975 |
| 118.25 | 0.266 | 23.65 | 0.85317194 | 94.6 | 0.58731225 | 679 | 473 | 0.19548 | 0.0977 |
| 118.5 | 0.266 | 23.70 | 0.85323149 | 94.8 | 0.58707405 | 678 | 474 | 0.19595 | 0.0980 |
| 118.75 | 0.266 | 23.75 | 0.85329098 | 95.0 | 0.58683609 | 677 | 475 | 0.19642 | 0.0982 |
| 119 | 0.267 | 23.80 | 0.85335041 | 95.2 | 0.58659836 | 676 | 476 | 0.19690 | 0.0984 |
| 119.25 | 0.267 | 23.85 | 0.85340978 | 95.4 | 0.58636086 | 675 | 477 | 0.19737 | 0.0987 |
| 119.5 | 0.267 | 23.90 | 0.85346910 | 95.6 | 0.58612360 | 674 | 478 | 0.19784 | 0.0989 |
| 119.75 | 0.268 | 23.95 | 0.85352836 | 95.8 | 0.58588658 | 673 | 479 | 0.19832 | 0.0992 |
| 120 | 0.268 | 24.00 | 0.85358755 | 96.0 | 0.58564978 | 672 | 480 | 0.19879 | 0.0994 |
| 120.25 | 0.268 | 24.05 | 0.85364669 | 96.2 | 0.58541322 | 671 | 481 | 0.19926 | 0.0996 |
| 120.5 | 0.269 | 24.10 | 0.85370578 | 96.4 | 0.58517689 | 670 | 482 | 0.19974 | 0.0999 |
| 120.75 | 0.269 | 24.15 | 0.85376480 | 96.6 | 0.58494079 | 669 | 483 | 0.20021 | 0.1001 |
| 121 | 0.269 | 24.20 | 0.85382377 | 96.8 | 0.58470492 | 668 | 484 | 0.20069 | 0.1003 |
| 121.25 | 0.269 | 24.25 | 0.85388268 | 97.0 | 0.58446927 | 667 | 485 | 0.20117 | 0.1006 |
| 121.5 | 0.270 | 24.30 | 0.85394154 | 97.2 | 0.58423386 | 666 | 486 | 0.20164 | 0.1008 |
| 121.75 | 0.270 | 24.35 | 0.85400033 | 97.4 | 0.58399867 | 665 | 487 | 0.20212 | 0.1011 |
| 122 | 0.270 | 24.40 | 0.85405907 | 97.6 | 0.58376371 | 664 | 488 | 0.20259 | 0.1013 |
| 122.25 | 0.271 | 24.45 | 0.85411776 | 97.8 | 0.58352898 | 663 | 489 | 0.20307 | 0.1015 |


| 122.5 | 0.271 | 24.50 | 0.85417638 | 98.0 | 0.58329447 | 662 | 490 | 0.20355 | 0.1018 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 122.75 | 0.271 | 24.55 | 0.85423495 | 98.2 | 0.58306019 | 661 | 491 | 0.20403 | 0.1020 |
| 123 | 0.271 | 24.60 | 0.85429347 | 98.4 | 0.58282613 | 660 | 492 | 0.20450 | 0.1023 |
| 123.25 | 0.272 | 24.65 | 0.85435193 | 98.6 | 0.58259229 | 659 | 493 | 0.20498 | 0.1025 |
| 123.5 | 0.272 | 24.70 | 0.85441033 | 98.8 | 0.58235868 | 658 | 494 | 0.20546 | 0.1027 |
| 123.75 | 0.272 | 24.75 | 0.85446868 | 99.0 | 0.58212529 | 657 | 495 | 0.20594 | 0.1030 |
| 124 | 0.273 | 24.80 | 0.85452697 | 99.2 | 0.58189212 | 656 | 496 | 0.20642 | 0.1032 |
| 124.25 | 0.273 | 24.85 | 0.85458521 | 99.4 | 0.58165917 | 655 | 497 | 0.20690 | 0.1034 |
| 124.5 | 0.273 | 24.90 | 0.85464339 | 99.6 | 0.58142644 | 654 | 498 | 0.20738 | 0.1037 |
| 124.75 | 0.274 | 24.95 | 0.85470152 | 99.8 | 0.58119393 | 653 | 499 | 0.20786 | 0.1039 |
| 125 | 0.274 | 25.00 | 0.85475959 | 100.0 | 0.58096164 | 652 | 500 | 0.20834 | 0.1042 |
| 125.25 | 0.274 | 25.05 | 0.85481761 | 100.2 | 0.58072957 | 651 | 501 | 0.20882 | 0.1044 |
| 125.5 | 0.274 | 25.10 | 0.85487557 | 100.4 | 0.58049772 | 650 | 502 | 0.20930 | 0.1047 |
| 125.75 | 0.275 | 25.15 | 0.85493348 | 100.6 | 0.58026608 | 649 | 503 | 0.20979 | 0.1049 |
| 126 | 0.275 | 25.20 | 0.85499134 | 100.8 | 0.58003466 | 648 | 504 | 0.21027 | 0.1051 |
| 126.25 | 0.275 | 25.25 | 0.85504914 | 101.0 | 0.57980345 | 647 | 505 | 0.21075 | 0.1054 |
| 126.5 | 0.276 | 25.30 | 0.85510688 | 101.2 | 0.57957246 | 646 | 506 | 0.21123 | 0.1056 |
| 126.75 | 0.276 | 25.35 | 0.85516458 | 101.4 | 0.57934169 | 645 | 507 | 0.21172 | 0.1059 |
| 127 | 0.276 | 25.40 | 0.85522222 | 101.6 | 0.57911113 | 644 | 508 | 0.21220 | 0.1061 |
| 127.25 | 0.276 | 25.45 | 0.85527981 | 101.8 | 0.57888078 | 643 | 509 | 0.21268 | 0.1063 |
| 127.5 | 0.277 | 25.50 | 0.85533734 | 102.0 | 0.57865064 | 642 | 510 | 0.21317 | 0.1066 |
| 127.75 | 0.277 | 25.55 | 0.85539482 | 102.2 | 0.57842072 | 641 | 511 | 0.21365 | 0.1068 |
| 128 | 0.277 | 25.60 | 0.85545225 | 102.4 | 0.57819101 | 640 | 512 | 0.21414 | 0.1071 |
| 128.25 | 0.278 | 25.65 | 0.85550962 | 102.6 | 0.57796151 | 639 | 513 | 0.21462 | 0.1073 |
| 128.5 | 0.278 | 25.70 | 0.85556695 | 102.8 | 0.57773221 | 638 | 514 | 0.21511 | 0.1076 |
| 128.75 | 0.278 | 25.75 | 0.85562422 | 103.0 | 0.57750313 | 637 | 515 | 0.21559 | 0.1078 |
| 129 | 0.278 | 25.80 | 0.85568144 | 103.2 | 0.57727426 | 636 | 516 | 0.21608 | 0.1080 |
| 129.25 | 0.279 | 25.85 | 0.85573860 | 103.4 | 0.57704559 | 635 | 517 | 0.21657 | 0.1083 |
| 129.5 | 0.279 | 25.90 | 0.85579572 | 103.6 | 0.57681714 | 634 | 518 | 0.21706 | 0.1085 |
| 129.75 | 0.279 | 25.95 | 0.85585278 | 103.8 | 0.57658889 | 633 | 519 | 0.21754 | 0.1088 |
| 130 | 0.280 | 26.00 | 0.85590979 | 104.0 | 0.57636084 | 632 | 520 | 0.21803 | 0.1090 |
| 130.25 | 0.280 | 26.05 | 0.85596675 | 104.2 | 0.57613301 | 631 | 521 | 0.21852 | 0.1093 |
| 130.5 | 0.280 | 26.10 | 0.85602366 | 104.4 | 0.57590538 | 630 | 522 | 0.21901 | 0.1095 |
| 130.75 | 0.280 | 26.15 | 0.85608051 | 104.6 | 0.57567795 | 629 | 523 | 0.21950 | 0.1097 |
| 131 | 0.281 | 26.20 | 0.85613732 | 104.8 | 0.57545073 | 628 | 524 | 0.21999 | 0.1100 |
| 131.25 | 0.281 | 26.25 | 0.85619407 | 105.0 | 0.57522371 | 627 | 525 | 0.22048 | 0.1102 |
| 131.5 | 0.281 | 26.30 | 0.85625078 | 105.2 | 0.57499689 | 626 | 526 | 0.22097 | 0.1105 |
| 131.75 | 0.282 | 26.35 | 0.85630743 | 105.4 | 0.57477028 | 625 | 527 | 0.22146 | 0.1107 |
| 132 | 0.282 | 26.40 | 0.85636403 | 105.6 | 0.57454387 | 624 | 528 | 0.22195 | 0.1110 |
| 132.25 | 0.282 | 26.45 | 0.85642059 | 105.8 | 0.57431766 | 623 | 529 | 0.22244 | 0.1112 |
| 132.5 | 0.282 | 26.50 | 0.85647709 | 106.0 | 0.57409165 | 622 | 530 | 0.22293 | 0.1115 |
| 132.75 | 0.283 | 26.55 | 0.85653354 | 106.2 | 0.57386584 | 621 | 531 | 0.22342 | 0.1117 |
| 133 | 0.283 | 26.60 | 0.85658994 | 106.4 | 0.57364023 | 620 | 532 | 0.22391 | 0.1120 |
| 133.25 | 0.283 | 26.65 | 0.85664629 | 106.6 | 0.57341482 | 619 | 533 | 0.22441 | 0.1122 |
| 133.5 | 0.284 | 26.70 | 0.85670260 | 106.8 | 0.57318961 | 618 | 534 | 0.22490 | 0.1124 |
| 133.75 | 0.284 | 26.75 | 0.85675885 | 107.0 | 0.57296460 | 617 | 535 | 0.22539 | 0.1127 |
| 134 | 0.284 | 26.80 | 0.85681505 | 107.2 | 0.57273979 | 616 | 536 | 0.22589 | 0.1129 |
| 134.25 | 0.284 | 26.85 | 0.85687121 | 107.4 | 0.57251517 | 615 | 537 | 0.22638 | 0.1132 |
| 134.5 | 0.285 | 26.90 | 0.85692731 | 107.6 | 0.57229075 | 614 | 538 | 0.22687 | 0.1134 |
| 134.75 | 0.285 | 26.95 | 0.85698337 | 107.8 | 0.57206652 | 613 | 539 | 0.22737 | 0.1137 |
| 135 | 0.285 | 27.00 | 0.85703938 | 108.0 | 0.57184249 | 612 | 540 | 0.22787 | 0.1139 |
| 135.25 | 0.285 | 27.05 | 0.85709534 | 108.2 | 0.57161866 | 611 | 541 | 0.22836 | 0.1142 |
| 135.5 | 0.286 | 27.10 | 0.85715125 | 108.4 | 0.57139502 | 610 | 542 | 0.22886 | 0.1144 |
| 135.75 | 0.286 | 27.15 | 0.85720711 | 108.6 | 0.57117157 | 609 | 543 | 0.22935 | 0.1147 |
| 136 | 0.286 | 27.20 | 0.85726292 | 108.8 | 0.57094832 | 608 | 544 | 0.22985 | 0.1149 |
| 136.25 | 0.287 | 27.25 | 0.85731869 | 109.0 | 0.57072526 | 607 | 545 | 0.23035 | 0.1152 |
| 136.5 | 0.287 | 27.30 | 0.85737440 | 109.2 | 0.57050239 | 606 | 546 | 0.23084 | 0.1154 |
| 136.75 | 0.287 | 27.35 | 0.85743007 | 109.4 | 0.57027971 | 605 | 547 | 0.23134 | 0.1157 |
| 137 | 0.287 | 27.40 | 0.85748569 | 109.6 | 0.57005723 | 604 | 548 | 0.23184 | 0.1159 |
| 137.25 | 0.288 | 27.45 | 0.85754127 | 109.8 | 0.56983493 | 603 | 549 | 0.23234 | 0.1162 |
| 137.5 | 0.288 | 27.50 | 0.85759679 | 110.0 | 0.56961283 | 602 | 550 | 0.23284 | 0.1164 |
| 137.75 | 0.288 | 27.55 | 0.85765227 | 110.2 | 0.56939091 | 601 | 551 | 0.23334 | 0.1167 |
| 138 | 0.289 | 27.60 | 0.85770770 | 110.4 | 0.56916919 | 600 | 552 | 0.23384 | 0.1169 |
| 138.25 | 0.289 | 27.65 | 0.85776309 | 110.6 | 0.56894765 | 599 | 553 | 0.23434 | 0.1172 |
| 138.5 | 0.289 | 27.70 | 0.85781842 | 110.8 | 0.56872630 | 598 | 554 | 0.23484 | 0.1174 |
| 138.75 | 0.289 | 27.75 | 0.85787371 | 111.0 | 0.56850514 | 597 | 555 | 0.23534 | 0.1177 |
| 139 | 0.290 | 27.80 | 0.85792896 | 111.2 | 0.56828417 | 596 | 556 | 0.23584 | 0.1179 |
| 139.25 | 0.290 | 27.85 | 0.85798416 | 111.4 | 0.56806338 | 595 | 557 | 0.23634 | 0.1182 |
| 139.5 | 0.290 | 27.90 | 0.85803931 | 111.6 | 0.56784278 | 594 | 558 | 0.23685 | 0.1184 |
| 139.75 | 0.290 | 27.95 | 0.85809441 | 111.8 | 0.56762236 | 593 | 559 | 0.23735 | 0.1187 |
| 140 | 0.291 | 28.00 | 0.85814947 | 112.0 | 0.56740213 | 592 | 560 | 0.23785 | 0.1189 |


| 140.25 | 0.291 | 28.05 | 0.85820448 | 112.2 | 0.56718209 | 591 | 561 | 0.23836 | 0.1192 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 140.5 | 0.291 | 28.10 | 0.85825944 | 112.4 | 0.56696223 | 590 | 562 | 0.23886 | 0.1194 |
| 140.75 | 0.292 | 28.15 | 0.85831436 | 112.6 | 0.56674255 | 589 | 563 | 0.23936 | 0.1197 |
| 141 | 0.292 | 28.20 | 0.85836924 | 112.8 | 0.56652306 | 588 | 564 | 0.23987 | 0.1199 |
| 141.25 | 0.292 | 28.25 | 0.85842406 | 113.0 | 0.56630375 | 587 | 565 | 0.24037 | 0.1202 |
| 141.5 | 0.292 | 28.30 | 0.85847885 | 113.2 | 0.56608462 | 586 | 566 | 0.24088 | 0.1204 |
| 141.75 | 0.293 | 28.35 | 0.85853358 | 113.4 | 0.56586567 | 585 | 567 | 0.24138 | 0.1207 |
| 142 | 0.293 | 28.40 | 0.85858827 | 113.6 | 0.56564691 | 584 | 568 | 0.24189 | 0.1209 |
| 142.25 | 0.293 | 28.45 | 0.85864292 | 113.8 | 0.56542832 | 583 | 569 | 0.24240 | 0.1212 |
| 142.5 | 0.293 | 28.50 | 0.85869752 | 114.0 | 0.56520992 | 582 | 570 | 0.24290 | 0.1215 |
| 142.75 | 0.294 | 28.55 | 0.85875208 | 114.2 | 0.56499170 | 581 | 571 | 0.24341 | 0.1217 |
| 143 | 0.294 | 28.60 | 0.85880659 | 114.4 | 0.56477365 | 580 | 572 | 0.24392 | 0.1220 |
| 143.25 | 0.294 | 28.65 | 0.85886105 | 114.6 | 0.56455579 | 579 | 573 | 0.24443 | 0.1222 |
| 143.5 | 0.295 | 28.70 | 0.85891547 | 114.8 | 0.56433810 | 578 | 574 | 0.24494 | 0.1225 |
| 143.75 | 0.295 | 28.75 | 0.85896985 | 115.0 | 0.56412059 | 577 | 575 | 0.24545 | 0.1227 |
| 144 | 0.295 | 28.80 | 0.85902418 | 115.2 | 0.56390326 | 576 | 576 | 0.24596 | 0.1230 |
| 144.25 | 0.295 | 28.85 | 0.85907847 | 115.4 | 0.56368611 | 575 | 577 | 0.24647 | 0.1232 |
| 144.5 | 0.296 | 28.90 | 0.85913272 | 115.6 | 0.56346913 | 574 | 578 | 0.24698 | 0.1235 |
| 144.75 | 0.296 | 28.95 | 0.85918692 | 115.8 | 0.56325233 | 573 | 579 | 0.24749 | 0.1237 |
| 145 | 0.296 | 29.00 | 0.85924107 | 116.0 | 0.56303571 | 572 | 580 | 0.24800 | 0.1240 |
| 145.25 | 0.296 | 29.05 | 0.85929519 | 116.2 | 0.56281926 | 571 | 581 | 0.24851 | 0.1243 |
| 145.5 | 0.297 | 29.10 | 0.85934925 | 116.4 | 0.56260299 | 570 | 582 | 0.24902 | 0.1245 |
| 145.75 | 0.297 | 29.15 | 0.85940328 | 116.6 | 0.56238689 | 569 | 583 | 0.24954 | 0.1248 |
| 146 | 0.297 | 29.20 | 0.85945726 | 116.8 | 0.56217096 | 568 | 584 | 0.25005 | 0.1250 |
| 146.25 | 0.298 | 29.25 | 0.85951120 | 117.0 | 0.56195521 | 567 | 585 | 0.25056 | 0.1253 |
| 146.5 | 0.298 | 29.30 | 0.85956509 | 117.2 | 0.56173963 | 566 | 586 | 0.25108 | 0.1255 |
| 146.75 | 0.298 | 29.35 | 0.85961894 | 117.4 | 0.56152423 | 565 | 587 | 0.25159 | 0.1258 |
| 147 | 0.298 | 29.40 | 0.85967275 | 117.6 | 0.56130899 | 564 | 588 | 0.25210 | 0.1261 |
| 147.25 | 0.299 | 29.45 | 0.85972652 | 117.8 | 0.56109393 | 563 | 589 | 0.25262 | 0.1263 |
| 147.5 | 0.299 | 29.50 | 0.85978024 | 118.0 | 0.56087904 | 562 | 590 | 0.25313 | 0.1266 |
| 147.75 | 0.299 | 29.55 | 0.85983392 | 118.2 | 0.56066433 | 561 | 591 | 0.25365 | 0.1268 |
| 148 | 0.299 | 29.60 | 0.85988756 | 118.4 | 0.56044978 | 560 | 592 | 0.25417 | 0.1271 |
| 148.25 | 0.300 | 29.65 | 0.85994115 | 118.6 | 0.56023540 | 559 | 593 | 0.25468 | 0.1273 |
| 148.5 | 0.300 | 29.70 | 0.85999470 | 118.8 | 0.56002119 | 558 | 594 | 0.25520 | 0.1276 |
| 148.75 | 0.300 | 29.75 | 0.86004821 | 119.0 | 0.55980716 | 557 | 595 | 0.25572 | 0.1279 |
| 149 | 0.301 | 29.80 | 0.86010168 | 119.2 | 0.55959329 | 556 | 596 | 0.25624 | 0.1281 |
| 149.25 | 0.301 | 29.85 | 0.86015510 | 119.4 | 0.55937959 | 555 | 597 | 0.25676 | 0.1284 |
| 149.5 | 0.301 | 29.90 | 0.86020849 | 119.6 | 0.55916606 | 554 | 598 | 0.25727 | 0.1286 |
| 149.75 | 0.301 | 29.95 | 0.86026183 | 119.8 | 0.55895269 | 553 | 599 | 0.25779 | 0.1289 |
| 150 | 0.302 | 30.00 | 0.86031513 | 120.0 | 0.55873949 | 552 | 600 | 0.25831 | 0.1292 |
| 150.25 | 0.302 | 30.05 | 0.86036838 | 120.2 | 0.55852646 | 551 | 601 | 0.25883 | 0.1294 |
| 150.5 | 0.302 | 30.10 | 0.86042160 | 120.4 | 0.55831360 | 550 | 602 | 0.25935 | 0.1297 |
| 150.75 | 0.302 | 30.15 | 0.86047477 | 120.6 | 0.55810090 | 549 | 603 | 0.25988 | 0.1299 |
| 151 | 0.303 | 30.20 | 0.86052791 | 120.8 | 0.55788837 | 548 | 604 | 0.26040 | 0.1302 |
| 151.25 | 0.303 | 30.25 | 0.86058100 | 121.0 | 0.55767601 | 547 | 605 | 0.26092 | 0.1305 |
| 151.5 | 0.303 | 30.30 | 0.86063405 | 121.2 | 0.55746380 | 546 | 606 | 0.26144 | 0.1307 |
| 151.75 | 0.303 | 30.35 | 0.86068706 | 121.4 | 0.55725177 | 545 | 607 | 0.26197 | 0.1310 |
| 152 | 0.304 | 30.40 | 0.86074003 | 121.6 | 0.55703989 | 544 | 608 | 0.26249 | 0.1312 |
| 152.25 | 0.304 | 30.45 | 0.86079295 | 121.8 | 0.55682819 | 543 | 609 | 0.26301 | 0.1315 |
| 152.5 | 0.304 | 30.50 | 0.86084584 | 122.0 | 0.55661664 | 542 | 610 | 0.26354 | 0.1318 |
| 152.75 | 0.304 | 30.55 | 0.86089869 | 122.2 | 0.55640526 | 541 | 611 | 0.26406 | 0.1320 |
| 153 | 0.305 | 30.60 | 0.86095149 | 122.4 | 0.55619404 | 540 | 612 | 0.26459 | 0.1323 |
| 153.25 | 0.305 | 30.65 | 0.86100426 | 122.6 | 0.55598298 | 539 | 613 | 0.26511 | 0.1326 |
| 153.5 | 0.305 | 30.70 | 0.86105698 | 122.8 | 0.55577208 | 538 | 614 | 0.26564 | 0.1328 |
| 153.75 | 0.306 | 30.75 | 0.86110966 | 123.0 | 0.55556135 | 537 | 615 | 0.26617 | 0.1331 |
| 154 | 0.306 | 30.80 | 0.86116231 | 123.2 | 0.55535077 | 536 | 616 | 0.26669 | 0.1333 |
| 154.25 | 0.306 | 30.85 | 0.86121491 | 123.4 | 0.55514036 | 535 | 617 | 0.26722 | 0.1336 |
| 154.5 | 0.306 | 30.90 | 0.86126747 | 123.6 | 0.55493011 | 534 | 618 | 0.26775 | 0.1339 |
| 154.75 | 0.307 | 30.95 | 0.86132000 | 123.8 | 0.55472001 | 533 | 619 | 0.26828 | 0.1341 |
| 155 | 0.307 | 31.00 | 0.86137248 | 124.0 | 0.55451008 | 532 | 620 | 0.26881 | 0.1344 |
| 155.25 | 0.307 | 31.05 | 0.86142492 | 124.2 | 0.55430030 | 531 | 621 | 0.26934 | 0.1347 |
| 155.5 | 0.307 | 31.10 | 0.86147733 | 124.4 | 0.55409069 | 530 | 622 | 0.26987 | 0.1349 |
| 155.75 | 0.308 | 31.15 | 0.86152969 | 124.6 | 0.55388123 | 529 | 623 | 0.27040 | 0.1352 |
| 156 | 0.308 | 31.20 | 0.86158202 | 124.8 | 0.55367193 | 528 | 624 | 0.27093 | 0.1355 |
| 156.25 | 0.308 | 31.25 | 0.86163430 | 125.0 | 0.55346279 | 527 | 625 | 0.27146 | 0.1357 |
| 156.5 | 0.308 | 31.30 | 0.86168655 | 125.2 | 0.55325380 | 526 | 626 | 0.27199 | 0.1360 |
| 156.75 | 0.309 | 31.35 | 0.86173876 | 125.4 | 0.55304498 | 525 | 627 | 0.27252 | 0.1363 |
| 157 | 0.309 | 31.40 | 0.86179092 | 125.6 | 0.55283630 | 524 | 628 | 0.27305 | 0.1365 |
| 157.25 | 0.309 | 31.45 | 0.86184305 | 125.8 | 0.55262779 | 523 | 629 | 0.27359 | 0.1368 |
| 157.5 | 0.309 | 31.50 | 0.86189514 | 126.0 | 0.55241943 | 522 | 630 | 0.27412 | 0.1371 |
| 157.75 | 0.310 | 31.55 | 0.86194719 | 126.2 | 0.55221122 | 521 | 631 | 0.27466 | 0.1373 |


| 158 | 0.310 | 31.60 | 0.86199921 | 126.4 | 0.55200317 | 520 | 632 | 0.27519 | 0.1376 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 158.25 | 0.310 | 31.65 | 0.86205118 | 126.6 | 0.55179528 | 519 | 633 | 0.27573 | 0.1379 |
| 158.5 | 0.311 | 31.70 | 0.86210312 | 126.8 | 0.55158754 | 518 | 634 | 0.27626 | 0.1381 |
| 158.75 | 0.311 | 31.75 | 0.86215501 | 127.0 | 0.55137995 | 517 | 635 | 0.27680 | 0.1384 |
| 159 | 0.311 | 31.80 | 0.86220687 | 127.2 | 0.55117252 | 516 | 636 | 0.27733 | 0.1387 |
| 159.25 | 0.311 | 31.85 | 0.86225869 | 127.4 | 0.55096524 | 515 | 637 | 0.27787 | 0.1389 |
| 159.5 | 0.312 | 31.90 | 0.86231047 | 127.6 | 0.55075811 | 514 | 638 | 0.27841 | 0.1392 |
| 159.75 | 0.312 | 31.95 | 0.86236222 | 127.8 | 0.55055114 | 513 | 639 | 0.27895 | 0.1395 |
| 160 | 0.312 | 32.00 | 0.86241392 | 128.0 | 0.55034432 | 512 | 640 | 0.27948 | 0.1397 |
| 160.25 | 0.312 | 32.05 | 0.86246559 | 128.2 | 0.55013765 | 511 | 641 | 0.28002 | 0.1400 |
| 160.5 | 0.313 | 32.10 | 0.86251722 | 128.4 | 0.54993113 | 510 | 642 | 0.28056 | 0.1403 |
| 160.75 | 0.313 | 32.15 | 0.86256881 | 128.6 | 0.54972476 | 509 | 643 | 0.28110 | 0.1406 |
| 161 | 0.313 | 32.20 | 0.86262036 | 128.8 | 0.54951854 | 508 | 644 | 0.28164 | 0.1408 |
| 161.25 | 0.313 | 32.25 | 0.86267188 | 129.0 | 0.54931248 | 507 | 645 | 0.28219 | 0.1411 |
| 161.5 | 0.314 | 32.30 | 0.86272336 | 129.2 | 0.54910656 | 506 | 646 | 0.28273 | 0.1414 |
| 161.75 | 0.314 | 32.35 | 0.86277480 | 129.4 | 0.54890079 | 505 | 647 | 0.28327 | 0.1416 |
| 162 | 0.314 | 32.40 | 0.86282621 | 129.6 | 0.54869518 | 504 | 648 | 0.28381 | 0.1419 |
| 162.25 | 0.314 | 32.45 | 0.86287757 | 129.8 | 0.54848971 | 503 | 649 | 0.28435 | 0.1422 |
| 162.5 | 0.315 | 32.50 | 0.86292890 | 130.0 | 0.54828439 | 502 | 650 | 0.28490 | 0.1424 |
| 162.75 | 0.315 | 32.55 | 0.86298020 | 130.2 | 0.54807922 | 501 | 651 | 0.28544 | 0.1427 |
| 163 | 0.315 | 32.60 | 0.86303145 | 130.4 | 0.54787420 | 500 | 652 | 0.28599 | 0.1430 |
| 163.25 | 0.315 | 32.65 | 0.86308267 | 130.6 | 0.54766932 | 499 | 653 | 0.28653 | 0.1433 |
| 163.5 | 0.316 | 32.70 | 0.86313385 | 130.8 | 0.54746459 | 498 | 654 | 0.28708 | 0.1435 |
| 163.75 | 0.316 | 32.75 | 0.86318500 | 131.0 | 0.54726001 | 497 | 655 | 0.28762 | 0.1438 |
| 164 | 0.316 | 32.80 | 0.86323611 | 131.2 | 0.54705558 | 496 | 656 | 0.28817 | 0.1441 |
| 164.25 | 0.316 | 32.85 | 0.86328718 | 131.4 | 0.54685129 | 495 | 657 | 0.28872 | 0.1444 |
| 164.5 | 0.317 | 32.90 | 0.86333821 | 131.6 | 0.54664715 | 494 | 658 | 0.28927 | 0.1446 |
| 164.75 | 0.317 | 32.95 | 0.86338921 | 131.8 | 0.54644315 | 493 | 659 | 0.28981 | 0.1449 |
| 165 | 0.317 | 33.00 | 0.86344017 | 132.0 | 0.54623930 | 492 | 660 | 0.29036 | 0.1452 |
| 165.25 | 0.317 | 33.05 | 0.86349110 | 132.2 | 0.54603560 | 491 | 661 | 0.29091 | 0.1455 |
| 165.5 | 0.318 | 33.10 | 0.86354199 | 132.4 | 0.54583204 | 490 | 662 | 0.29146 | 0.1457 |
| 165.75 | 0.318 | 33.15 | 0.86359284 | 132.6 | 0.54562862 | 489 | 663 | 0.29201 | 0.1460 |
| 166 | 0.318 | 33.20 | 0.86364366 | 132.8 | 0.54542535 | 488 | 664 | 0.29256 | 0.1463 |
| 166.25 | 0.318 | 33.25 | 0.86369444 | 133.0 | 0.54522222 | 487 | 665 | 0.29311 | 0.1466 |
| 166.5 | 0.319 | 33.30 | 0.86374519 | 133.2 | 0.54501924 | 486 | 666 | 0.29367 | 0.1468 |
| 166.75 | 0.319 | 33.35 | 0.86379590 | 133.4 | 0.54481640 | 485 | 667 | 0.29422 | 0.1471 |
| 167 | 0.319 | 33.40 | 0.86384657 | 133.6 | 0.54461370 | 484 | 668 | 0.29477 | 0.1474 |
| 167.25 | 0.319 | 33.45 | 0.86389721 | 133.8 | 0.54441114 | 483 | 669 | 0.29532 | 0.1477 |
| 167.5 | 0.320 | 33.50 | 0.86394782 | 134.0 | 0.54420873 | 482 | 670 | 0.29588 | 0.1479 |
| 167.75 | 0.320 | 33.55 | 0.86399839 | 134.2 | 0.54400646 | 481 | 671 | 0.29643 | 0.1482 |
| 168 | 0.320 | 33.60 | 0.86404892 | 134.4 | 0.54380433 | 480 | 672 | 0.29699 | 0.1485 |
| 168.25 | 0.320 | 33.65 | 0.86409941 | 134.6 | 0.54360234 | 479 | 673 | 0.29754 | 0.1488 |
| 168.5 | 0.321 | 33.70 | 0.86414988 | 134.8 | 0.54340049 | 478 | 674 | 0.29810 | 0.1491 |
| 168.75 | 0.321 | 33.75 | 0.86420030 | 135.0 | 0.54319879 | 477 | 675 | 0.29866 | 0.1493 |
| 169 | 0.321 | 33.80 | 0.86425069 | 135.2 | 0.54299722 | 476 | 676 | 0.29921 | 0.1496 |
| 169.25 | 0.322 | 33.85 | 0.86430105 | 135.4 | 0.54279579 | 475 | 677 | 0.29977 | 0.1499 |
| 169.5 | 0.322 | 33.90 | 0.86435137 | 135.6 | 0.54259451 | 474 | 678 | 0.30033 | 0.1502 |
| 169.75 | 0.322 | 33.95 | 0.86440166 | 135.8 | 0.54239336 | 473 | 679 | 0.30089 | 0.1504 |
| 170 | 0.322 | 34.00 | 0.86445191 | 136.0 | 0.54219235 | 472 | 680 | 0.30145 | 0.1507 |
| 170.25 | 0.323 | 34.05 | 0.86450213 | 136.2 | 0.54199148 | 471 | 681 | 0.30201 | 0.1510 |
| 170.5 | 0.323 | 34.10 | 0.86455231 | 136.4 | 0.54179075 | 470 | 682 | 0.30257 | 0.1513 |
| 170.75 | 0.323 | 34.15 | 0.86460246 | 136.6 | 0.54159016 | 469 | 683 | 0.30313 | 0.1516 |
| 171 | 0.323 | 34.20 | 0.86465257 | 136.8 | 0.54138971 | 468 | 684 | 0.30369 | 0.1518 |
| 171.25 | 0.324 | 34.25 | 0.86470265 | 137.0 | 0.54118939 | 467 | 685 | 0.30426 | 0.1521 |
| 171.5 | 0.324 | 34.30 | 0.86475270 | 137.2 | 0.54098921 | 466 | 686 | 0.30482 | 0.1524 |
| 171.75 | 0.324 | 34.35 | 0.86480271 | 137.4 | 0.54078917 | 465 | 687 | 0.30538 | 0.1527 |
| 172 | 0.324 | 34.40 | 0.86485268 | 137.6 | 0.54058927 | 464 | 688 | 0.30595 | 0.1530 |
| 172.25 | 0.325 | 34.45 | 0.86490263 | 137.8 | 0.54038950 | 463 | 689 | 0.30651 | 0.1533 |
| 172.5 | 0.325 | 34.50 | 0.86495253 | 138.0 | 0.54018986 | 462 | 690 | 0.30708 | 0.1535 |
| 172.75 | 0.325 | 34.55 | 0.86500241 | 138.2 | 0.53999037 | 461 | 691 | 0.30764 | 0.1538 |
| 173 | 0.325 | 34.60 | 0.86505225 | 138.4 | 0.53979101 | 460 | 692 | 0.30821 | 0.1541 |
| 173.25 | 0.326 | 34.65 | 0.86510205 | 138.6 | 0.53959178 | 459 | 693 | 0.30877 | 0.1544 |
| 173.5 | 0.326 | 34.70 | 0.86515183 | 138.8 | 0.53939269 | 458 | 694 | 0.30934 | 0.1547 |
| 173.75 | 0.326 | 34.75 | 0.86520157 | 139.0 | 0.53919374 | 457 | 695 | 0.30991 | 0.1550 |
| 174 | 0.326 | 34.80 | 0.86525127 | 139.2 | 0.53899492 | 456 | 696 | 0.31048 | 0.1552 |
| 174.25 | 0.327 | 34.85 | 0.86530094 | 139.4 | 0.53879623 | 455 | 697 | 0.31105 | 0.1555 |
| 174.5 | 0.327 | 34.90 | 0.86535058 | 139.6 | 0.53859768 | 454 | 698 | 0.31162 | 0.1558 |
| 174.75 | 0.327 | 34.95 | 0.86540019 | 139.8 | 0.53839926 | 453 | 699 | 0.31219 | 0.1561 |
| 175 | 0.327 | 35.00 | 0.86544976 | 140.0 | 0.53820097 | 452 | 700 | 0.31276 | 0.1564 |
| 175.25 | 0.327 | 35.05 | 0.86549930 | 140.2 | 0.53800282 | 451 | 701 | 0.31333 | 0.1567 |
| 175.5 | 0.328 | 35.10 | 0.86554880 | 140.4 | 0.53780480 | 450 | 702 | 0.31390 | 0.1570 |


| 175.75 | 0.328 | 35.15 | 0.86559827 | 140.6 | 0.53760691 | 449 | 703 | 0.31448 | 0.1572 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 176 | 0.328 | 35.20 | 0.86564771 | 140.8 | 0.53740916 | 448 | 704 | 0.31505 | 0.1575 |
| 176.25 | 0.328 | 35.25 | 0.86569712 | 141.0 | 0.53721153 | 447 | 705 | 0.31562 | 0.1578 |
| 176.5 | 0.329 | 35.30 | 0.86574649 | 141.2 | 0.53701404 | 446 | 706 | 0.31620 | 0.1581 |
| 176.75 | 0.329 | 35.35 | 0.86579583 | 141.4 | 0.53681668 | 445 | 707 | 0.31677 | 0.1584 |
| 177 | 0.329 | 35.40 | 0.86584514 | 141.6 | 0.53661945 | 444 | 708 | 0.31735 | 0.1587 |
| 177.25 | 0.329 | 35.45 | 0.86589441 | 141.8 | 0.53642235 | 443 | 709 | 0.31793 | 0.1590 |
| 177.5 | 0.330 | 35.50 | 0.86594365 | 142.0 | 0.53622539 | 442 | 710 | 0.31850 | 0.1593 |
| 177.75 | 0.330 | 35.55 | 0.86599286 | 142.2 | 0.53602855 | 441 | 711 | 0.31908 | 0.1595 |
| 178 | 0.330 | 35.60 | 0.86604204 | 142.4 | 0.53583184 | 440 | 712 | 0.31966 | 0.1598 |
| 178.25 | 0.330 | 35.65 | 0.86609118 | 142.6 | 0.53563527 | 439 | 713 | 0.32024 | 0.1601 |
| 178.5 | 0.331 | 35.70 | 0.86614030 | 142.8 | 0.53543882 | 438 | 714 | 0.32082 | 0.1604 |
| 178.75 | 0.331 | 35.75 | 0.86618938 | 143.0 | 0.53524250 | 437 | 715 | 0.32140 | 0.1607 |
| 179 | 0.331 | 35.80 | 0.86623842 | 143.2 | 0.53504631 | 436 | 716 | 0.32198 | 0.1610 |
| 179.25 | 0.331 | 35.85 | 0.86628744 | 143.4 | 0.53485025 | 435 | 717 | 0.32256 | 0.1613 |
| 179.5 | 0.332 | 35.90 | 0.86633642 | 143.6 | 0.53465432 | 434 | 718 | 0.32314 | 0.1616 |
| 179.75 | 0.332 | 35.95 | 0.86638537 | 143.8 | 0.53445851 | 433 | 719 | 0.32372 | 0.1619 |
| 180 | 0.332 | 36.00 | 0.86643429 | 144.0 | 0.53426284 | 432 | 720 | 0.32431 | 0.1622 |
| 180.25 | 0.332 | 36.05 | 0.86648318 | 144.2 | 0.53406729 | 431 | 721 | 0.32489 | 0.1624 |
| 180.5 | 0.333 | 36.10 | 0.86653203 | 144.4 | 0.53387187 | 430 | 722 | 0.32548 | 0.1627 |
| 180.75 | 0.333 | 36.15 | 0.86658086 | 144.6 | 0.53367657 | 429 | 723 | 0.32606 | 0.1630 |
| 181 | 0.333 | 36.20 | 0.86662965 | 144.8 | 0.53348141 | 428 | 724 | 0.32665 | 0.1633 |
| 181.25 | 0.333 | 36.25 | 0.86667841 | 145.0 | 0.53328637 | 427 | 725 | 0.32723 | 0.1636 |
| 181.5 | 0.334 | 36.30 | 0.86672714 | 145.2 | 0.53309145 | 426 | 726 | 0.32782 | 0.1639 |
| 181.75 | 0.334 | 36.35 | 0.86677583 | 145.4 | 0.53289667 | 425 | 727 | 0.32841 | 0.1642 |
| 182 | 0.334 | 36.40 | 0.86682450 | 145.6 | 0.53270200 | 424 | 728 | 0.32900 | 0.1645 |
| 182.25 | 0.334 | 36.45 | 0.86687313 | 145.8 | 0.53250747 | 423 | 729 | 0.32959 | 0.1648 |
| 182.5 | 0.335 | 36.50 | 0.86692174 | 146.0 | 0.53231306 | 422 | 730 | 0.33018 | 0.1651 |
| 182.75 | 0.335 | 36.55 | 0.86697031 | 146.2 | 0.53211877 | 421 | 731 | 0.33077 | 0.1654 |
| 183 | 0.335 | 36.60 | 0.86701885 | 146.4 | 0.53192461 | 420 | 732 | 0.33136 | 0.1657 |
| 183.25 | 0.335 | 36.65 | 0.86706736 | 146.6 | 0.53173058 | 419 | 733 | 0.33195 | 0.1660 |
| 183.5 | 0.336 | 36.70 | 0.86711583 | 146.8 | 0.53153666 | 418 | 734 | 0.33254 | 0.1663 |
| 183.75 | 0.336 | 36.75 | 0.86716428 | 147.0 | 0.53134288 | 417 | 735 | 0.33313 | 0.1666 |
| 184 | 0.336 | 36.80 | 0.86721270 | 147.2 | 0.53114921 | 416 | 736 | 0.33373 | 0.1669 |
| 184.25 | 0.336 | 36.85 | 0.86726108 | 147.4 | 0.53095567 | 415 | 737 | 0.33432 | 0.1672 |
| 184.5 | 0.337 | 36.90 | 0.86730944 | 147.6 | 0.53076226 | 414 | 738 | 0.33492 | 0.1675 |
| 184.75 | 0.337 | 36.95 | 0.86735776 | 147.8 | 0.53056896 | 413 | 739 | 0.33551 | 0.1678 |
| 185 | 0.337 | 37.00 | 0.86740605 | 148.0 | 0.53037579 | 412 | 740 | 0.33611 | 0.1681 |
| 185.25 | 0.337 | 37.05 | 0.86745431 | 148.2 | 0.53018274 | 411 | 741 | 0.33671 | 0.1684 |
| 185.5 | 0.338 | 37.10 | 0.86750255 | 148.4 | 0.52998982 | 410 | 742 | 0.33730 | 0.1687 |
| 185.75 | 0.338 | 37.15 | 0.86755075 | 148.6 | 0.52979702 | 409 | 743 | 0.33790 | 0.1690 |
| 186 | 0.338 | 37.20 | 0.86759892 | 148.8 | 0.52960433 | 408 | 744 | 0.33850 | 0.1693 |
| 186.25 | 0.338 | 37.25 | 0.86764706 | 149.0 | 0.52941177 | 407 | 745 | 0.33910 | 0.1696 |
| 186.5 | 0.338 | 37.30 | 0.86769517 | 149.2 | 0.52921934 | 406 | 746 | 0.33970 | 0.1699 |
| 186.75 | 0.339 | 37.35 | 0.86774325 | 149.4 | 0.52902702 | 405 | 747 | 0.34030 | 0.1702 |
| 187 | 0.339 | 37.40 | 0.86779129 | 149.6 | 0.52883482 | 404 | 748 | 0.34091 | 0.1705 |
| 187.25 | 0.339 | 37.45 | 0.86783931 | 149.8 | 0.52864275 | 403 | 749 | 0.34151 | 0.1708 |
| 187.5 | 0.339 | 37.50 | 0.86788730 | 150.0 | 0.52845079 | 402 | 750 | 0.34211 | 0.1711 |
| 187.75 | 0.340 | 37.55 | 0.86793526 | 150.2 | 0.52825896 | 401 | 751 | 0.34272 | 0.1714 |
| 188 | 0.340 | 37.60 | 0.86798319 | 150.4 | 0.52806724 | 400 | 752 | 0.34332 | 0.1717 |
| 188.25 | 0.340 | 37.65 | 0.86803109 | 150.6 | 0.52787565 | 399 | 753 | 0.34393 | 0.1720 |
| 188.5 | 0.340 | 37.70 | 0.86807896 | 150.8 | 0.52768417 | 398 | 754 | 0.34453 | 0.1723 |
| 188.75 | 0.341 | 37.75 | 0.86812680 | 151.0 | 0.52749282 | 397 | 755 | 0.34514 | 0.1726 |
| 189 | 0.341 | 37.80 | 0.86817461 | 151.2 | 0.52730158 | 396 | 756 | 0.34575 | 0.1729 |
| 189.25 | 0.341 | 37.85 | 0.86822238 | 151.4 | 0.52711046 | 395 | 757 | 0.34635 | 0.1732 |
| 189.5 | 0.341 | 37.90 | 0.86827013 | 151.6 | 0.52691946 | 394 | 758 | 0.34696 | 0.1735 |
| 189.75 | 0.342 | 37.95 | 0.86831785 | 151.8 | 0.52672858 | 393 | 759 | 0.34757 | 0.1738 |
| 190 | 0.342 | 38.00 | 0.86836555 | 152.0 | 0.52653782 | 392 | 760 | 0.34818 | 0.1741 |
| 190.25 | 0.342 | 38.05 | 0.86841321 | 152.2 | 0.52634717 | 391 | 761 | 0.34880 | 0.1744 |
| 190.5 | 0.342 | 38.10 | 0.86846084 | 152.4 | 0.52615665 | 390 | 762 | 0.34941 | 0.1747 |
| 190.75 | 0.343 | 38.15 | 0.86850844 | 152.6 | 0.52596624 | 389 | 763 | 0.35002 | 0.1750 |
| 191 | 0.343 | 38.20 | 0.86855601 | 152.8 | 0.52577594 | 388 | 764 | 0.35063 | 0.1753 |
| 191.25 | 0.343 | 38.25 | 0.86860356 | 153.0 | 0.52558577 | 387 | 765 | 0.35125 | 0.1756 |
| 191.5 | 0.343 | 38.30 | 0.86865107 | 153.2 | 0.52539571 | 386 | 766 | 0.35186 | 0.1759 |
| 191.75 | 0.343 | 38.35 | 0.86869856 | 153.4 | 0.52520577 | 385 | 767 | 0.35248 | 0.1762 |
| 192 | 0.344 | 38.40 | 0.86874601 | 153.6 | 0.52501594 | 384 | 768 | 0.35309 | 0.1765 |
| 192.25 | 0.344 | 38.45 | 0.86879344 | 153.8 | 0.52482623 | 383 | 769 | 0.35371 | 0.1769 |
| 192.5 | 0.344 | 38.50 | 0.86884084 | 154.0 | 0.52463664 | 382 | 770 | 0.35433 | 0.1772 |
| 192.75 | 0.344 | 38.55 | 0.86888821 | 154.2 | 0.52444716 | 381 | 771 | 0.35495 | 0.1775 |
| 193 | 0.345 | 38.60 | 0.86893555 | 154.4 | 0.52425780 | 380 | 772 | 0.35557 | 0.1778 |
| 193.25 | 0.345 | 38.65 | 0.86898286 | 154.6 | 0.52406855 | 379 | 773 | 0.35619 | 0.1781 |


| 193.5 | 0.345 | 38.70 | 0.86903015 | 154.8 | 0.52387942 | 378 | 774 | 0.35681 | 0.1784 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 193.75 | 0.345 | 38.75 | 0.86907740 | 155.0 | 0.52369040 | 377 | 775 | 0.35743 | 0.1787 |
| 194 | 0.346 | 38.80 | 0.86912463 | 155.2 | 0.52350150 | 376 | 776 | 0.35805 | 0.1790 |
| 194.25 | 0.346 | 38.85 | 0.86917182 | 155.4 | 0.52331271 | 375 | 777 | 0.35868 | 0.1793 |
| 194.5 | 0.346 | 38.90 | 0.86921899 | 155.6 | 0.52312404 | 374 | 778 | 0.35930 | 0.1797 |
| 194.75 | 0.346 | 38.95 | 0.86926613 | 155.8 | 0.52293547 | 373 | 779 | 0.35993 | 0.1800 |
| 195 | 0.347 | 39.00 | 0.86931324 | 156.0 | 0.52274703 | 372 | 780 | 0.36055 | 0.1803 |
| 195.25 | 0.347 | 39.05 | 0.86936033 | 156.2 | 0.52255869 | 371 | 781 | 0.36118 | 0.1806 |
| 195.5 | 0.347 | 39.10 | 0.86940738 | 156.4 | 0.52237048 | 370 | 782 | 0.36181 | 0.1809 |
| 195.75 | 0.347 | 39.15 | 0.86945441 | 156.6 | 0.52218237 | 369 | 783 | 0.36243 | 0.1812 |
| 196 | 0.348 | 39.20 | 0.86950141 | 156.8 | 0.52199437 | 368 | 784 | 0.36306 | 0.1815 |
| 196.25 | 0.348 | 39.25 | 0.86954838 | 157.0 | 0.52180649 | 367 | 785 | 0.36369 | 0.1818 |
| 196.5 | 0.348 | 39.30 | 0.86959532 | 157.2 | 0.52161872 | 366 | 786 | 0.36432 | 0.1822 |
| 196.75 | 0.348 | 39.35 | 0.86964223 | 157.4 | 0.52143107 | 365 | 787 | 0.36495 | 0.1825 |
| 197 | 0.348 | 39.40 | 0.86968912 | 157.6 | 0.52124352 | 364 | 788 | 0.36559 | 0.1828 |
| 197.25 | 0.349 | 39.45 | 0.86973598 | 157.8 | 0.52105609 | 363 | 789 | 0.36622 | 0.1831 |
| 197.5 | 0.349 | 39.50 | 0.86978281 | 158.0 | 0.52086877 | 362 | 790 | 0.36685 | 0.1834 |
| 197.75 | 0.349 | 39.55 | 0.86982961 | 158.2 | 0.52068156 | 361 | 791 | 0.36749 | 0.1837 |
| 198 | 0.349 | 39.60 | 0.86987638 | 158.4 | 0.52049446 | 360 | 792 | 0.36812 | 0.1841 |
| 198.25 | 0.350 | 39.65 | 0.86992313 | 158.6 | 0.52030747 | 359 | 793 | 0.36876 | 0.1844 |
| 198.5 | 0.350 | 39.70 | 0.86996985 | 158.8 | 0.52012060 | 358 | 794 | 0.36940 | 0.1847 |
| 198.75 | 0.350 | 39.75 | 0.87001654 | 159.0 | 0.51993383 | 357 | 795 | 0.37003 | 0.1850 |
| 199 | 0.350 | 39.80 | 0.87006321 | 159.2 | 0.51974718 | 356 | 796 | 0.37067 | 0.1853 |
| 199.25 | 0.351 | 39.85 | 0.87010984 | 159.4 | 0.51956063 | 355 | 797 | 0.37131 | 0.1857 |
| 199.5 | 0.351 | 39.90 | 0.87015645 | 159.6 | 0.51937420 | 354 | 798 | 0.37195 | 0.1860 |
| 199.75 | 0.351 | 39.95 | 0.87020303 | 159.8 | 0.51918787 | 353 | 799 | 0.37259 | 0.1863 |
| 200 | 0.351 | 40.00 | 0.87024959 | 160.0 | 0.51900165 | 352 | 800 | 0.37324 | 0.1866 |
| 200.25 | 0.351 | 40.05 | 0.87029611 | 160.2 | 0.51881555 | 351 | 801 | 0.37388 | 0.1869 |
| 200.5 | 0.352 | 40.10 | 0.87034261 | 160.4 | 0.51862955 | 350 | 802 | 0.37452 | 0.1873 |
| 200.75 | 0.352 | 40.15 | 0.87038908 | 160.6 | 0.51844366 | 349 | 803 | 0.37517 | 0.1876 |
| 201 | 0.352 | 40.20 | 0.87043553 | 160.8 | 0.51825788 | 348 | 804 | 0.37581 | 0.1879 |
| 201.25 | 0.352 | 40.25 | 0.87048195 | 161.0 | 0.51807221 | 347 | 805 | 0.37646 | 0.1882 |
| 201.5 | 0.353 | 40.30 | 0.87052834 | 161.2 | 0.51788665 | 346 | 806 | 0.37711 | 0.1886 |
| 201.75 | 0.353 | 40.35 | 0.87057470 | 161.4 | 0.51770119 | 345 | 807 | 0.37776 | 0.1889 |
| 202 | 0.353 | 40.40 | 0.87062104 | 161.6 | 0.51751585 | 344 | 808 | 0.37840 | 0.1892 |
| 202.25 | 0.353 | 40.45 | 0.87066735 | 161.8 | 0.51733061 | 343 | 809 | 0.37905 | 0.1895 |
| 202.5 | 0.354 | 40.50 | 0.87071363 | 162.0 | 0.51714548 | 342 | 810 | 0.37971 | 0.1899 |
| 202.75 | 0.354 | 40.55 | 0.87075989 | 162.2 | 0.51696045 | 341 | 811 | 0.38036 | 0.1902 |
| 203 | 0.354 | 40.60 | 0.87080612 | 162.4 | 0.51677553 | 340 | 812 | 0.38101 | 0.1905 |
| 203.25 | 0.354 | 40.65 | 0.87085232 | 162.6 | 0.51659072 | 339 | 813 | 0.38166 | 0.1908 |
| 203.5 | 0.354 | 40.70 | 0.87089849 | 162.8 | 0.51640602 | 338 | 814 | 0.38232 | 0.1912 |
| 203.75 | 0.355 | 40.75 | 0.87094464 | 163.0 | 0.51622143 | 337 | 815 | 0.38297 | 0.1915 |
| 204 | 0.355 | 40.80 | 0.87099077 | 163.2 | 0.51603694 | 336 | 816 | 0.38363 | 0.1918 |
| 204.25 | 0.355 | 40.85 | 0.87103686 | 163.4 | 0.51585255 | 335 | 817 | 0.38429 | 0.1921 |
| 204.5 | 0.355 | 40.90 | 0.87108293 | 163.6 | 0.51566827 | 334 | 818 | 0.38494 | 0.1925 |
| 204.75 | 0.356 | 40.95 | 0.87112897 | 163.8 | 0.51548410 | 333 | 819 | 0.38560 | 0.1928 |
| 205 | 0.356 | 41.00 | 0.87117499 | 164.0 | 0.51530004 | 332 | 820 | 0.38626 | 0.1931 |
| 205.25 | 0.356 | 41.05 | 0.87122098 | 164.2 | 0.51511608 | 331 | 821 | 0.38692 | 0.1935 |
| 205.5 | 0.356 | 41.10 | 0.87126695 | 164.4 | 0.51493222 | 330 | 822 | 0.38759 | 0.1938 |
| 205.75 | 0.357 | 41.15 | 0.87131288 | 164.6 | 0.51474847 | 329 | 823 | 0.38825 | 0.1941 |
| 206 | 0.357 | 41.20 | 0.87135879 | 164.8 | 0.51456482 | 328 | 824 | 0.38891 | 0.1945 |
| 206.25 | 0.357 | 41.25 | 0.87140468 | 165.0 | 0.51438128 | 327 | 825 | 0.38958 | 0.1948 |
| 206.5 | 0.357 | 41.30 | 0.87145054 | 165.2 | 0.51419785 | 326 | 826 | 0.39024 | 0.1951 |
| 206.75 | 0.357 | 41.35 | 0.87149637 | 165.4 | 0.51401452 | 325 | 827 | 0.39091 | 0.1955 |
| 207 | 0.358 | 41.40 | 0.87154218 | 165.6 | 0.51383129 | 324 | 828 | 0.39158 | 0.1958 |
| 207.25 | 0.358 | 41.45 | 0.87158796 | 165.8 | 0.51364816 | 323 | 829 | 0.39225 | 0.1961 |
| 207.5 | 0.358 | 41.50 | 0.87163371 | 166.0 | 0.51346514 | 322 | 830 | 0.39292 | 0.1965 |
| 207.75 | 0.358 | 41.55 | 0.87167944 | 166.2 | 0.51328223 | 321 | 831 | 0.39359 | 0.1968 |
| 208 | 0.359 | 41.60 | 0.87172515 | 166.4 | 0.51309942 | 320 | 832 | 0.39426 | 0.1971 |
| 208.25 | 0.359 | 41.65 | 0.87177082 | 166.6 | 0.51291671 | 319 | 833 | 0.39493 | 0.1975 |
| 208.5 | 0.359 | 41.70 | 0.87181648 | 166.8 | 0.51273410 | 318 | 834 | 0.39560 | 0.1978 |
| 208.75 | 0.359 | 41.75 | 0.87186210 | 167.0 | 0.51255160 | 317 | 835 | 0.39628 | 0.1981 |
| 209 | 0.360 | 41.80 | 0.87190770 | 167.2 | 0.51236919 | 316 | 836 | 0.39695 | 0.1985 |
| 209.25 | 0.360 | 41.85 | 0.87195328 | 167.4 | 0.51218690 | 315 | 837 | 0.39763 | 0.1988 |
| 209.5 | 0.360 | 41.90 | 0.87199883 | 167.6 | 0.51200470 | 314 | 838 | 0.39831 | 0.1992 |
| 209.75 | 0.360 | 41.95 | 0.87204435 | 167.8 | 0.51182261 | 313 | 839 | 0.39899 | 0.1995 |
| 210 | 0.360 | 42.00 | 0.87208985 | 168.0 | 0.51164061 | 312 | 840 | 0.39967 | 0.1998 |
| 210.25 | 0.361 | 42.05 | 0.87213532 | 168.2 | 0.51145872 | 311 | 841 | 0.40035 | 0.2002 |
| 210.5 | 0.361 | 42.10 | 0.87218077 | 168.4 | 0.51127694 | 310 | 842 | 0.40103 | 0.2005 |
| 210.75 | 0.361 | 42.15 | 0.87222619 | 168.6 | 0.51109525 | 309 | 843 | 0.40171 | 0.2009 |
| 211 | 0.361 | 42.20 | 0.87227158 | 168.8 | 0.51091366 | 308 | 844 | 0.40239 | 0.2012 |


| 211.25 | 0.362 | 42.25 | 0.87231696 | 169.0 | 0.51073218 | 307 | 845 | 0.40308 | 0.2015 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 211.5 | 0.362 | 42.30 | 0.87236230 | 169.2 | 0.51055079 | 306 | 846 | 0.40377 | 0.2019 |
| 211.75 | 0.362 | 42.35 | 0.87240762 | 169.4 | 0.51036951 | 305 | 847 | 0.40445 | 0.2022 |
| 212 | 0.362 | 42.40 | 0.87245292 | 169.6 | 0.51018833 | 304 | 848 | 0.40514 | 0.2026 |
| 212.25 | 0.362 | 42.45 | 0.87249819 | 169.8 | 0.51000725 | 303 | 849 | 0.40583 | 0.2029 |
| 212.5 | 0.363 | 42.50 | 0.87254343 | 170.0 | 0.50982626 | 302 | 850 | 0.40652 | 0.2033 |
| 212.75 | 0.363 | 42.55 | 0.87258865 | 170.2 | 0.50964538 | 301 | 851 | 0.40721 | 0.2036 |
| 213 | 0.363 | 42.60 | 0.87263385 | 170.4 | 0.50946460 | 300 | 852 | 0.40790 | 0.2040 |
| 213.25 | 0.363 | 42.65 | 0.87267902 | 170.6 | 0.50928392 | 299 | 853 | 0.40860 | 0.2043 |
| 213.5 | 0.364 | 42.70 | 0.87272417 | 170.8 | 0.50910334 | 298 | 854 | 0.40929 | 0.2046 |
| 213.75 | 0.364 | 42.75 | 0.87276929 | 171.0 | 0.50892285 | 297 | 855 | 0.40999 | 0.2050 |
| 214 | 0.364 | 42.80 | 0.87281438 | 171.2 | 0.50874247 | 296 | 856 | 0.41068 | 0.2053 |
| 214.25 | 0.364 | 42.85 | 0.87285945 | 171.4 | 0.50856218 | 295 | 857 | 0.41138 | 0.2057 |
| 214.5 | 0.365 | 42.90 | 0.87290450 | 171.6 | 0.50838200 | 294 | 858 | 0.41208 | 0.2060 |
| 214.75 | 0.365 | 42.95 | 0.87294952 | 171.8 | 0.50820191 | 293 | 859 | 0.41278 | 0.2064 |
| 215 | 0.365 | 43.00 | 0.87299452 | 172.0 | 0.50802192 | 292 | 860 | 0.41348 | 0.2067 |
| 215.25 | 0.365 | 43.05 | 0.87303949 | 172.2 | 0.50784203 | 291 | 861 | 0.41418 | 0.2071 |
| 215.5 | 0.365 | 43.10 | 0.87308444 | 172.4 | 0.50766224 | 290 | 862 | 0.41488 | 0.2074 |
| 215.75 | 0.366 | 43.15 | 0.87312936 | 172.6 | 0.50748254 | 289 | 863 | 0.41559 | 0.2078 |
| 216 | 0.366 | 43.20 | 0.87317426 | 172.8 | 0.50730294 | 288 | 864 | 0.41629 | 0.2081 |
| 216.25 | 0.366 | 43.25 | 0.87321914 | 173.0 | 0.50712344 | 287 | 865 | 0.41700 | 0.2085 |
| 216.5 | 0.366 | 43.30 | 0.87326399 | 173.2 | 0.50694404 | 286 | 866 | 0.41771 | 0.2089 |
| 216.75 | 0.367 | 43.35 | 0.87330882 | 173.4 | 0.50676474 | 285 | 867 | 0.41842 | 0.2092 |
| 217 | 0.367 | 43.40 | 0.87335362 | 173.6 | 0.50658553 | 284 | 868 | 0.41913 | 0.2096 |
| 217.25 | 0.367 | 43.45 | 0.87339839 | 173.8 | 0.50640642 | 283 | 869 | 0.41984 | 0.2099 |
| 217.5 | 0.367 | 43.50 | 0.87344315 | 174.0 | 0.50622741 | 282 | 870 | 0.42055 | 0.2103 |
| 217.75 | 0.367 | 43.55 | 0.87348788 | 174.2 | 0.50604849 | 281 | 871 | 0.42127 | 0.2106 |
| 218 | 0.368 | 43.60 | 0.87353258 | 174.4 | 0.50586967 | 280 | 872 | 0.42198 | 0.2110 |
| 218.25 | 0.368 | 43.65 | 0.87357726 | 174.6 | 0.50569095 | 279 | 873 | 0.42270 | 0.2113 |
| 218.5 | 0.368 | 43.70 | 0.87362192 | 174.8 | 0.50551232 | 278 | 874 | 0.42341 | 0.2117 |
| 218.75 | 0.368 | 43.75 | 0.87366655 | 175.0 | 0.50533379 | 277 | 875 | 0.42413 | 0.2121 |
| 219 | 0.369 | 43.80 | 0.87371116 | 175.2 | 0.50515535 | 276 | 876 | 0.42485 | 0.2124 |
| 219.25 | 0.369 | 43.85 | 0.87375575 | 175.4 | 0.50497701 | 275 | 877 | 0.42557 | 0.2128 |
| 219.5 | 0.369 | 43.90 | 0.87380031 | 175.6 | 0.50479877 | 274 | 878 | 0.42630 | 0.2131 |
| 219.75 | 0.369 | 43.95 | 0.87384484 | 175.8 | 0.50462062 | 273 | 879 | 0.42702 | 0.2135 |
| 220 | 0.369 | 44.00 | 0.87388936 | 176.0 | 0.50444257 | 272 | 880 | 0.42774 | 0.2139 |
| 220.25 | 0.370 | 44.05 | 0.87393385 | 176.2 | 0.50426461 | 271 | 881 | 0.42847 | 0.2142 |
| 220.5 | 0.370 | 44.10 | 0.87397831 | 176.4 | 0.50408674 | 270 | 882 | 0.42920 | 0.2146 |
| 220.75 | 0.370 | 44.15 | 0.87402276 | 176.6 | 0.50390897 | 269 | 883 | 0.42993 | 0.2150 |
| 221 | 0.370 | 44.20 | 0.87406717 | 176.8 | 0.50373130 | 268 | 884 | 0.43066 | 0.2153 |
| 221.25 | 0.371 | 44.25 | 0.87411157 | 177.0 | 0.50355372 | 267 | 885 | 0.43139 | 0.2157 |
| 221.5 | 0.371 | 44.30 | 0.87415594 | 177.2 | 0.50337623 | 266 | 886 | 0.43212 | 0.2161 |
| 221.75 | 0.371 | 44.35 | 0.87420029 | 177.4 | 0.50319884 | 265 | 887 | 0.43285 | 0.2164 |
| 222 | 0.371 | 44.40 | 0.87424461 | 177.6 | 0.50302155 | 264 | 888 | 0.43359 | 0.2168 |
| 222.25 | 0.371 | 44.45 | 0.87428891 | 177.8 | 0.50284434 | 263 | 889 | 0.43432 | 0.2172 |
| 222.5 | 0.372 | 44.50 | 0.87433319 | 178.0 | 0.50266723 | 262 | 890 | 0.43506 | 0.2175 |
| 222.75 | 0.372 | 44.55 | 0.87437745 | 178.2 | 0.50249022 | 261 | 891 | 0.43580 | 0.2179 |
| 223 | 0.372 | 44.60 | 0.87442168 | 178.4 | 0.50231329 | 260 | 892 | 0.43654 | 0.2183 |
| 223.25 | 0.372 | 44.65 | 0.87446588 | 178.6 | 0.50213646 | 259 | 893 | 0.43728 | 0.2186 |
| 223.5 | 0.373 | 44.70 | 0.87451007 | 178.8 | 0.50195972 | 258 | 894 | 0.43802 | 0.2190 |
| 223.75 | 0.373 | 44.75 | 0.87455423 | 179.0 | 0.50178308 | 257 | 895 | 0.43877 | 0.2194 |
| 224 | 0.373 | 44.80 | 0.87459837 | 179.2 | 0.50160653 | 256 | 896 | 0.43951 | 0.2198 |
| 224.25 | 0.373 | 44.85 | 0.87464248 | 179.4 | 0.50143007 | 255 | 897 | 0.44026 | 0.2201 |
| 224.5 | 0.373 | 44.90 | 0.87468657 | 179.6 | 0.50125370 | 254 | 898 | 0.44101 | 0.2205 |
| 224.75 | 0.374 | 44.95 | 0.87473064 | 179.8 | 0.50107743 | 253 | 899 | 0.44176 | 0.2209 |
| 225 | 0.374 | 45.00 | 0.87477469 | 180.0 | 0.50090125 | 252 | 900 | 0.44251 | 0.2213 |
| 225.25 | 0.374 | 45.05 | 0.87481871 | 180.2 | 0.50072516 | 251 | 901 | 0.44326 | 0.2216 |
| 225.5 | 0.374 | 45.10 | 0.87486271 | 180.4 | 0.50054916 | 250 | 902 | 0.44402 | 0.2220 |
| 225.75 | 0.375 | 45.15 | 0.87490669 | 180.6 | 0.50037325 | 249 | 903 | 0.44477 | 0.2224 |
| 226 | 0.375 | 45.20 | 0.87495064 | 180.8 | 0.50019744 | 248 | 904 | 0.44553 | 0.2228 |
| 226.25 | 0.375 | 45.25 | 0.87499457 | 181.0 | 0.50002172 | 247 | 905 | 0.44629 | 0.2231 |
| 226.5 | 0.375 | 45.30 | 0.87503848 | 181.2 | 0.49984608 | 246 | 906 | 0.44705 | 0.2235 |
| 226.75 | 0.375 | 45.35 | 0.87508236 | 181.4 | 0.49967054 | 245 | 907 | 0.44781 | 0.2239 |
| 227 | 0.376 | 45.40 | 0.87512623 | 181.6 | 0.49949509 | 244 | 908 | 0.44857 | 0.2243 |
| 227.25 | 0.376 | 45.45 | 0.87517007 | 181.8 | 0.49931973 | 243 | 909 | 0.44934 | 0.2247 |
| 227.5 | 0.376 | 45.50 | 0.87521388 | 182.0 | 0.49914446 | 242 | 910 | 0.45010 | 0.2251 |
| 227.75 | 0.376 | 45.55 | 0.87525768 | 182.2 | 0.49896928 | 241 | 911 | 0.45087 | 0.2254 |
| 228 | 0.377 | 45.60 | 0.87530145 | 182.4 | 0.49879420 | 240 | 912 | 0.45164 | 0.2258 |
| 228.25 | 0.377 | 45.65 | 0.87534520 | 182.6 | 0.49861920 | 239 | 913 | 0.45241 | 0.2262 |
| 228.5 | 0.377 | 45.70 | 0.87538893 | 182.8 | 0.49844429 | 238 | 914 | 0.45318 | 0.2266 |
| 228.75 | 0.377 | 45.75 | 0.87543263 | 183.0 | 0.49826947 | 237 | 915 | 0.45395 | 0.2270 |


| 229 | 0.377 | 45.80 | 0.87547631 | 183.2 | 0.49809475 | 236 | 916 | 0.45473 | 0.2274 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 229.25 | 0.378 | 45.85 | 0.87551997 | 183.4 | 0.49792011 | 235 | 917 | 0.45550 | 0.2278 |
| 229.5 | 0.378 | 45.90 | 0.87556361 | 183.6 | 0.49774556 | 234 | 918 | 0.45628 | 0.2281 |
| 229.75 | 0.378 | 45.95 | 0.87560723 | 183.8 | 0.49757110 | 233 | 919 | 0.45706 | 0.2285 |
| 230 | 0.378 | 46.00 | 0.87565082 | 184.0 | 0.49739673 | 232 | 920 | 0.45784 | 0.2289 |
| 230.25 | 0.378 | 46.05 | 0.87569439 | 184.2 | 0.49722245 | 231 | 921 | 0.45862 | 0.2293 |
| 230.5 | 0.379 | 46.10 | 0.87573794 | 184.4 | 0.49704825 | 230 | 922 | 0.45941 | 0.2297 |
| 230.75 | 0.379 | 46.15 | 0.87578146 | 184.6 | 0.49687415 | 229 | 923 | 0.46019 | 0.2301 |
| 231 | 0.379 | 46.20 | 0.87582497 | 184.8 | 0.49670014 | 228 | 924 | 0.46098 | 0.2305 |
| 231.25 | 0.379 | 46.25 | 0.87586845 | 185.0 | 0.49652621 | 227 | 925 | 0.46177 | 0.2309 |
| 231.5 | 0.380 | 46.30 | 0.87591191 | 185.2 | 0.49635237 | 226 | 926 | 0.46256 | 0.2313 |
| 231.75 | 0.380 | 46.35 | 0.87595534 | 185.4 | 0.49617862 | 225 | 927 | 0.46335 | 0.2317 |
| 232 | 0.380 | 46.40 | 0.87599876 | 185.6 | 0.49600496 | 224 | 928 | 0.46415 | 0.2321 |
| 232.25 | 0.380 | 46.45 | 0.87604215 | 185.8 | 0.49583139 | 223 | 929 | 0.46494 | 0.2325 |
| 232.5 | 0.380 | 46.50 | 0.87608553 | 186.0 | 0.49565790 | 222 | 930 | 0.46574 | 0.2329 |
| 232.75 | 0.381 | 46.55 | 0.87612887 | 186.2 | 0.49548450 | 221 | 931 | 0.46654 | 0.2333 |
| 233 | 0.381 | 46.60 | 0.87617220 | 186.4 | 0.49531119 | 220 | 932 | 0.46734 | 0.2337 |
| 233.25 | 0.381 | 46.65 | 0.87621551 | 186.6 | 0.49513797 | 219 | 933 | 0.46814 | 0.2341 |
| 233.5 | 0.381 | 46.70 | 0.87625879 | 186.8 | 0.49496483 | 218 | 934 | 0.46894 | 0.2345 |
| 233.75 | 0.382 | 46.75 | 0.87630205 | 187.0 | 0.49479178 | 217 | 935 | 0.46975 | 0.2349 |
| 234 | 0.382 | 46.80 | 0.87634530 | 187.2 | 0.49461882 | 216 | 936 | 0.47056 | 0.2353 |
| 234.25 | 0.382 | 46.85 | 0.87638851 | 187.4 | 0.49444594 | 215 | 937 | 0.47137 | 0.2357 |
| 234.5 | 0.382 | 46.90 | 0.87643171 | 187.6 | 0.49427315 | 214 | 938 | 0.47218 | 0.2361 |
| 234.75 | 0.382 | 46.95 | 0.87647489 | 187.8 | 0.49410045 | 213 | 939 | 0.47299 | 0.2365 |
| 235 | 0.383 | 47.00 | 0.87651804 | 188.0 | 0.49392784 | 212 | 940 | 0.47380 | 0.2369 |
| 235.25 | 0.383 | 47.05 | 0.87656117 | 188.2 | 0.49375531 | 211 | 941 | 0.47462 | 0.2373 |
| 235.5 | 0.383 | 47.10 | 0.87660428 | 188.4 | 0.49358286 | 210 | 942 | 0.47544 | 0.2377 |
| 235.75 | 0.383 | 47.15 | 0.87664737 | 188.6 | 0.49341051 | 209 | 943 | 0.47626 | 0.2381 |
| 236 | 0.383 | 47.20 | 0.87669044 | 188.8 | 0.49323824 | 208 | 944 | 0.47708 | 0.2385 |
| 236.25 | 0.384 | 47.25 | 0.87673349 | 189.0 | 0.49306605 | 207 | 945 | 0.47790 | 0.2390 |
| 236.5 | 0.384 | 47.30 | 0.87677651 | 189.2 | 0.49289395 | 206 | 946 | 0.47873 | 0.2394 |
| 236.75 | 0.384 | 47.35 | 0.87681952 | 189.4 | 0.49272193 | 205 | 947 | 0.47956 | 0.2398 |
| 237 | 0.384 | 47.40 | 0.87686250 | 189.6 | 0.49255001 | 204 | 948 | 0.48039 | 0.2402 |
| 237.25 | 0.385 | 47.45 | 0.87690546 | 189.8 | 0.49237816 | 203 | 949 | 0.48122 | 0.2406 |
| 237.5 | 0.385 | 47.50 | 0.87694840 | 190.0 | 0.49220640 | 202 | 950 | 0.48205 | 0.2410 |
| 237.75 | 0.385 | 47.55 | 0.87699132 | 190.2 | 0.49203473 | 201 | 951 | 0.48289 | 0.2414 |
| 238 | 0.385 | 47.60 | 0.87703422 | 190.4 | 0.49186314 | 200 | 952 | 0.48372 | 0.2419 |
| 238.25 | 0.385 | 47.65 | 0.87707709 | 190.6 | 0.49169164 | 199 | 953 | 0.48456 | 0.2423 |
| 238.5 | 0.386 | 47.70 | 0.87711995 | 190.8 | 0.49152022 | 198 | 954 | 0.48540 | 0.2427 |
| 238.75 | 0.386 | 47.75 | 0.87716278 | 191.0 | 0.49134888 | 197 | 955 | 0.48625 | 0.2431 |
| 239 | 0.386 | 47.80 | 0.87720559 | 191.2 | 0.49117763 | 196 | 956 | 0.48709 | 0.2435 |
| 239.25 | 0.386 | 47.85 | 0.87724838 | 191.4 | 0.49100646 | 195 | 957 | 0.48794 | 0.2440 |
| 239.5 | 0.386 | 47.90 | 0.87729116 | 191.6 | 0.49083538 | 194 | 958 | 0.48879 | 0.2444 |
| 239.75 | 0.387 | 47.95 | 0.87733391 | 191.8 | 0.49066438 | 193 | 959 | 0.48964 | 0.2448 |
| 240 | 0.387 | 48.00 | 0.87737663 | 192.0 | 0.49049346 | 192 | 960 | 0.49049 | 0.2452 |
| 240.25 | 0.387 | 48.05 | 0.87741934 | 192.2 | 0.49032263 | 191 | 961 | 0.49135 | 0.2457 |
| 240.5 | 0.387 | 48.10 | 0.87746203 | 192.4 | 0.49015188 | 190 | 962 | 0.49221 | 0.2461 |
| 240.75 | 0.388 | 48.15 | 0.87750470 | 192.6 | 0.48998122 | 189 | 963 | 0.49307 | 0.2465 |
| 241 | 0.388 | 48.20 | 0.87754734 | 192.8 | 0.48981064 | 188 | 964 | 0.49393 | 0.2470 |
| 241.25 | 0.388 | 48.25 | 0.87758996 | 193.0 | 0.48964014 | 187 | 965 | 0.49479 | 0.2474 |
| 241.5 | 0.388 | 48.30 | 0.87763257 | 193.2 | 0.48946973 | 186 | 966 | 0.49566 | 0.2478 |
| 241.75 | 0.388 | 48.35 | 0.87767515 | 193.4 | 0.48929939 | 185 | 967 | 0.49653 | 0.2483 |
| 242 | 0.389 | 48.40 | 0.87771771 | 193.6 | 0.48912914 | 184 | 968 | 0.49740 | 0.2487 |
| 242.25 | 0.389 | 48.45 | 0.87776026 | 193.8 | 0.48895898 | 183 | 969 | 0.49827 | 0.2491 |
| 242.5 | 0.389 | 48.50 | 0.87780278 | 194.0 | 0.48878889 | 182 | 970 | 0.49914 | 0.2496 |
| 242.75 | 0.389 | 48.55 | 0.87784528 | 194.2 | 0.48861889 | 181 | 971 | 0.50002 | 0.2500 |
| 243 | 0.389 | 48.60 | 0.87788776 | 194.4 | 0.48844897 | 180 | 972 | 0.50090 | 0.2505 |
| 243.25 | 0.390 | 48.65 | 0.87793022 | 194.6 | 0.48827913 | 179 | 973 | 0.50178 | 0.2509 |
| 243.5 | 0.390 | 48.70 | 0.87797266 | 194.8 | 0.48810938 | 178 | 974 | 0.50267 | 0.2513 |
| 243.75 | 0.390 | 48.75 | 0.87801507 | 195.0 | 0.48793970 | 177 | 975 | 0.50355 | 0.2518 |
| 244 | 0.390 | 48.80 | 0.87805747 | 195.2 | 0.48777011 | 176 | 976 | 0.50444 | 0.2522 |
| 244.25 | 0.390 | 48.85 | 0.87809985 | 195.4 | 0.48760060 | 175 | 977 | 0.50533 | 0.2527 |
| 244.5 | 0.391 | 48.90 | 0.87814221 | 195.6 | 0.48743117 | 174 | 978 | 0.50623 | 0.2531 |
| 244.75 | 0.391 | 48.95 | 0.87818454 | 195.8 | 0.48726183 | 173 | 979 | 0.50712 | 0.2536 |
| 245 | 0.391 | 49.00 | 0.87822686 | 196.0 | 0.48709256 | 172 | 980 | 0.50802 | 0.2540 |
| 245.25 | 0.391 | 49.05 | 0.87826916 | 196.2 | 0.48692337 | 171 | 981 | 0.50892 | 0.2545 |
| 245.5 | 0.392 | 49.10 | 0.87831143 | 196.4 | 0.48675427 | 170 | 982 | 0.50983 | 0.2549 |
| 245.75 | 0.392 | 49.15 | 0.87835369 | 196.6 | 0.48658525 | 169 | 983 | 0.51073 | 0.2554 |
| 246 | 0.392 | 49.20 | 0.87839592 | 196.8 | 0.48641631 | 168 | 984 | 0.51164 | 0.2558 |
| 246.25 | 0.392 | 49.25 | 0.87843814 | 197.0 | 0.48624744 | 167 | 985 | 0.51255 | 0.2563 |
| 246.5 | 0.392 | 49.30 | 0.87848033 | 197.2 | 0.48607866 | 166 | 986 | 0.51347 | 0.2567 |


| 246.75 | 0.393 | 49.35 | 0.87852251 | 197.4 | 0.48590996 | 165 | 987 | 0.51438 | 0.2572 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 247 | 0.393 | 49.40 | 0.87856466 | 197.6 | 0.48574134 | 164 | 988 | 0.51530 | 0.2577 |
| 247.25 | 0.393 | 49.45 | 0.87860680 | 197.8 | 0.48557280 | 163 | 989 | 0.51622 | 0.2581 |
| 247.5 | 0.393 | 49.50 | 0.87864891 | 198.0 | 0.48540434 | 162 | 990 | 0.51715 | 0.2586 |
| 247.75 | 0.393 | 49.55 | 0.87869101 | 198.2 | 0.48523596 | 161 | 991 | 0.51807 | 0.2590 |
| 248 | 0.394 | 49.60 | 0.87873308 | 198.4 | 0.48506766 | 160 | 992 | 0.51900 | 0.2595 |
| 248.25 | 0.394 | 49.65 | 0.87877514 | 198.6 | 0.48489944 | 159 | 993 | 0.51993 | 0.2600 |
| 248.5 | 0.394 | 49.70 | 0.87881717 | 198.8 | 0.48473130 | 158 | 994 | 0.52087 | 0.2604 |
| 248.75 | 0.394 | 49.75 | 0.87885919 | 199.0 | 0.48456324 | 157 | 995 | 0.52181 | 0.2609 |
| 249 | 0.395 | 49.80 | 0.87890119 | 199.2 | 0.48439526 | 156 | 996 | 0.52275 | 0.2614 |
| 249.25 | 0.395 | 49.85 | 0.87894316 | 199.4 | 0.48422736 | 155 | 997 | 0.52369 | 0.2618 |
| 249.5 | 0.395 | 49.90 | 0.87898512 | 199.6 | 0.48405953 | 154 | 998 | 0.52464 | 0.2623 |
| 249.75 | 0.395 | 49.95 | 0.87902705 | 199.8 | 0.48389179 | 153 | 999 | 0.52559 | 0.2628 |
| 250 | 0.395 | 50.00 | 0.87906897 | 200.0 | 0.48372412 | 152 | 1000 | 0.52654 | 0.2633 |
| 250.25 | 0.396 | 50.05 | 0.87911087 | 200.2 | 0.48355653 | 151 | 1001 | 0.52749 | 0.2637 |
| 250.5 | 0.396 | 50.10 | 0.87915274 | 200.4 | 0.48338903 | 150 | 1002 | 0.52845 | 0.2642 |
| 250.75 | 0.396 | 50.15 | 0.87919460 | 200.6 | 0.48322160 | 149 | 1003 | 0.52941 | 0.2647 |
| 251 | 0.396 | 50.20 | 0.87923644 | 200.8 | 0.48305425 | 148 | 1004 | 0.53038 | 0.2652 |
| 251.25 | 0.396 | 50.25 | 0.87927826 | 201.0 | 0.48288697 | 147 | 1005 | 0.53134 | 0.2657 |
| 251.5 | 0.397 | 50.30 | 0.87932006 | 201.2 | 0.48271978 | 146 | 1006 | 0.53231 | 0.2662 |
| 251.75 | 0.397 | 50.35 | 0.87936183 | 201.4 | 0.48255266 | 145 | 1007 | 0.53329 | 0.2666 |
| 252 | 0.397 | 50.40 | 0.87940359 | 201.6 | 0.48238562 | 144 | 1008 | 0.53426 | 0.2671 |
| 252.25 | 0.397 | 50.45 | 0.87944533 | 201.8 | 0.48221866 | 143 | 1009 | 0.53524 | 0.2676 |
| 252.5 | 0.397 | 50.50 | 0.87948706 | 202.0 | 0.48205178 | 142 | 1010 | 0.53623 | 0.2681 |
| 252.75 | 0.398 | 50.55 | 0.87952876 | 202.2 | 0.48188497 | 141 | 1011 | 0.53721 | 0.2686 |
| 253 | 0.398 | 50.60 | 0.87957044 | 202.4 | 0.48171825 | 140 | 1012 | 0.53820 | 0.2691 |
| 253.25 | 0.398 | 50.65 | 0.87961210 | 202.6 | 0.48155160 | 139 | 1013 | 0.53919 | 0.2696 |
| 253.5 | 0.398 | 50.70 | 0.87965374 | 202.8 | 0.48138502 | 138 | 1014 | 0.54019 | 0.2701 |
| 253.75 | 0.398 | 50.75 | 0.87969537 | 203.0 | 0.48121853 | 137 | 1015 | 0.54119 | 0.2706 |
| 254 | 0.399 | 50.80 | 0.87973697 | 203.2 | 0.48105211 | 136 | 1016 | 0.54219 | 0.2711 |
| 254.25 | 0.399 | 50.85 | 0.87977856 | 203.4 | 0.48088577 | 135 | 1017 | 0.54320 | 0.2716 |
| 254.5 | 0.399 | 50.90 | 0.87982012 | 203.6 | 0.48071950 | 134 | 1018 | 0.54421 | 0.2721 |
| 254.75 | 0.399 | 50.95 | 0.87986167 | 203.8 | 0.48055331 | 133 | 1019 | 0.54522 | 0.2726 |
| 255 | 0.400 | 51.00 | 0.87990320 | 204.0 | 0.48038720 | 132 | 1020 | 0.54624 | 0.2731 |
| 255.25 | 0.400 | 51.05 | 0.87994471 | 204.2 | 0.48022117 | 131 | 1021 | 0.54726 | 0.2736 |
| 255.5 | 0.400 | 51.10 | 0.87998620 | 204.4 | 0.48005521 | 130 | 1022 | 0.54828 | 0.2741 |
| 255.75 | 0.400 | 51.15 | 0.88002767 | 204.6 | 0.47988933 | 129 | 1023 | 0.54931 | 0.2747 |
| 256 | 0.400 | 51.20 | 0.88006912 | 204.8 | 0.47972352 | 128 | 1024 | 0.55034 | 0.2752 |
| 256.25 | 0.401 | 51.25 | 0.88011055 | 205.0 | 0.47955779 | 127 | 1025 | 0.55138 | 0.2757 |
| 256.5 | 0.401 | 51.30 | 0.88015197 | 205.2 | 0.47939214 | 126 | 1026 | 0.55242 | 0.2762 |
| 256.75 | 0.401 | 51.35 | 0.88019336 | 205.4 | 0.47922656 | 125 | 1027 | 0.55346 | 0.2767 |
| 257 | 0.401 | 51.40 | 0.88023474 | 205.6 | 0.47906105 | 124 | 1028 | 0.55451 | 0.2773 |
| 257.25 | 0.401 | 51.45 | 0.88027609 | 205.8 | 0.47889563 | 123 | 1029 | 0.55556 | 0.2778 |
| 257.5 | 0.402 | 51.50 | 0.88031743 | 206.0 | 0.47873028 | 122 | 1030 | 0.55662 | 0.2783 |
| 257.75 | 0.402 | 51.55 | 0.88035875 | 206.2 | 0.47856500 | 121 | 1031 | 0.55768 | 0.2788 |
| 258 | 0.402 | 51.60 | 0.88040005 | 206.4 | 0.47839980 | 120 | 1032 | 0.55874 | 0.2794 |
| 258.25 | 0.402 | 51.65 | 0.88044133 | 206.6 | 0.47823467 | 119 | 1033 | 0.55981 | 0.2799 |
| 258.5 | 0.402 | 51.70 | 0.88048259 | 206.8 | 0.47806962 | 118 | 1034 | 0.56088 | 0.2804 |
| 258.75 | 0.403 | 51.75 | 0.88052384 | 207.0 | 0.47790465 | 117 | 1035 | 0.56196 | 0.2810 |
| 259 | 0.403 | 51.80 | 0.88056506 | 207.2 | 0.47773975 | 116 | 1036 | 0.56304 | 0.2815 |
| 259.25 | 0.403 | 51.85 | 0.88060627 | 207.4 | 0.47757492 | 115 | 1037 | 0.56412 | 0.2821 |
| 259.5 | 0.403 | 51.90 | 0.88064746 | 207.6 | 0.47741017 | 114 | 1038 | 0.56521 | 0.2826 |
| 259.75 | 0.403 | 51.95 | 0.88068863 | 207.8 | 0.47724550 | 113 | 1039 | 0.56630 | 0.2832 |
| 260 | 0.404 | 52.00 | 0.88072978 | 208.0 | 0.47708089 | 112 | 1040 | 0.56740 | 0.2837 |
| 260.25 | 0.404 | 52.05 | 0.88077091 | 208.2 | 0.47691637 | 111 | 1041 | 0.56851 | 0.2843 |
| 260.5 | 0.404 | 52.10 | 0.88081202 | 208.4 | 0.47675191 | 110 | 1042 | 0.56961 | 0.2848 |
| 260.75 | 0.404 | 52.15 | 0.88085312 | 208.6 | 0.47658754 | 109 | 1043 | 0.57073 | 0.2854 |
| 261 | 0.404 | 52.20 | 0.88089419 | 208.8 | 0.47642323 | 108 | 1044 | 0.57184 | 0.2859 |
| 261.25 | 0.405 | 52.25 | 0.88093525 | 209.0 | 0.47625900 | 107 | 1045 | 0.57296 | 0.2865 |
| 261.5 | 0.405 | 52.30 | 0.88097629 | 209.2 | 0.47609484 | 106 | 1046 | 0.57409 | 0.2870 |
| 261.75 | 0.405 | 52.35 | 0.88101731 | 209.4 | 0.47593076 | 105 | 1047 | 0.57522 | 0.2876 |
| 262 | 0.405 | 52.40 | 0.88105831 | 209.6 | 0.47576675 | 104 | 1048 | 0.57636 | 0.2882 |
| 262.25 | 0.405 | 52.45 | 0.88109930 | 209.8 | 0.47560281 | 103 | 1049 | 0.57750 | 0.2888 |
| 262.5 | 0.406 | 52.50 | 0.88114026 | 210.0 | 0.47543895 | 102 | 1050 | 0.57865 | 0.2893 |
| 262.75 | 0.406 | 52.55 | 0.88118121 | 210.2 | 0.47527516 | 101 | 1051 | 0.57980 | 0.2899 |
| 263 | 0.406 | 52.60 | 0.88122214 | 210.4 | 0.47511144 | 100 | 1052 | 0.58096 | 0.2905 |
| 263.25 | 0.406 | 52.65 | 0.88126305 | 210.6 | 0.47494780 | 99 | 1053 | 0.58213 | 0.2911 |
| 263.5 | 0.407 | 52.70 | 0.88130394 | 210.8 | 0.47478423 | 98 | 1054 | 0.58329 | 0.2916 |
| 263.75 | 0.407 | 52.75 | 0.88134482 | 211.0 | 0.47462073 | 97 | 1055 | 0.58447 | 0.2922 |
| 264 | 0.407 | 52.80 | 0.88138567 | 211.2 | 0.47445731 | 96 | 1056 | 0.58565 | 0.2928 |
| 264.25 | 0.407 | 52.85 | 0.88142651 | 211.4 | 0.47429396 | 95 | 1057 | 0.58684 | 0.2934 |


| 264.5 | 0.407 | 52.90 | 0.88146733 | 211.6 | 0.47413068 | 94 | 1058 | 0.58803 | 0.2940 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 264.75 | 0.408 | 52.95 | 0.88150813 | 211.8 | 0.47396747 | 93 | 1059 | 0.58923 | 0.2946 |
| 265 | 0.408 | 53.00 | 0.88154892 | 212.0 | 0.47380434 | 92 | 1060 | 0.59043 | 0.2952 |
| 265.25 | 0.408 | 53.05 | 0.88158968 | 212.2 | 0.47364128 | 91 | 1061 | 0.59164 | 0.2958 |
| 265.5 | 0.408 | 53.10 | 0.88163043 | 212.4 | 0.47347829 | 90 | 1062 | 0.59286 | 0.2964 |
| 265.75 | 0.408 | 53.15 | 0.88167116 | 212.6 | 0.47331537 | 89 | 1063 | 0.59408 | 0.2970 |
| 266 | 0.409 | 53.20 | 0.88171187 | 212.8 | 0.47315253 | 88 | 1064 | 0.59531 | 0.2977 |
| 266.25 | 0.409 | 53.25 | 0.88175256 | 213.0 | 0.47298975 | 87 | 1065 | 0.59655 | 0.2983 |
| 266.5 | 0.409 | 53.30 | 0.88179324 | 213.2 | 0.47282705 | 86 | 1066 | 0.59779 | 0.2989 |
| 266.75 | 0.409 | 53.35 | 0.88183389 | 213.4 | 0.47266442 | 85 | 1067 | 0.59904 | 0.2995 |
| 267 | 0.409 | 53.40 | 0.88187453 | 213.6 | 0.47250186 | 84 | 1068 | 0.60030 | 0.3001 |
| 267.25 | 0.410 | 53.45 | 0.88191516 | 213.8 | 0.47233938 | 83 | 1069 | 0.60156 | 0.3008 |
| 267.5 | 0.410 | 53.50 | 0.88195576 | 214.0 | 0.47217696 | 82 | 1070 | 0.60283 | 0.3014 |
| 267.75 | 0.410 | 53.55 | 0.88199635 | 214.2 | 0.47201462 | 81 | 1071 | 0.60411 | 0.3021 |
| 268 | 0.410 | 53.60 | 0.88203691 | 214.4 | 0.47185234 | 80 | 1072 | 0.60539 | 0.3027 |
| 268.25 | 0.410 | 53.65 | 0.88207746 | 214.6 | 0.47169014 | 79 | 1073 | 0.60669 | 0.3033 |
| 268.5 | 0.411 | 53.70 | 0.88211800 | 214.8 | 0.47152801 | 78 | 1074 | 0.60799 | 0.3040 |
| 268.75 | 0.411 | 53.75 | 0.88215851 | 215.0 | 0.47136595 | 77 | 1075 | 0.60930 | 0.3046 |
| 269 | 0.411 | 53.80 | 0.88219901 | 215.2 | 0.47120396 | 76 | 1076 | 0.61061 | 0.3053 |
| 269.25 | 0.411 | 53.85 | 0.88223949 | 215.4 | 0.47104204 | 75 | 1077 | 0.61194 | 0.3060 |
| 269.5 | 0.411 | 53.90 | 0.88227995 | 215.6 | 0.47088020 | 74 | 1078 | 0.61327 | 0.3066 |
| 269.75 | 0.412 | 53.95 | 0.88232039 | 215.8 | 0.47071842 | 73 | 1079 | 0.61461 | 0.3073 |
| 270 | 0.412 | 54.00 | 0.88236082 | 216.0 | 0.47055671 | 72 | 1080 | 0.61596 | 0.3080 |
| 270.25 | 0.412 | 54.05 | 0.88240123 | 216.2 | 0.47039508 | 71 | 1081 | 0.61732 | 0.3087 |
| 270.5 | 0.412 | 54.10 | 0.88244162 | 216.4 | 0.47023351 | 70 | 1082 | 0.61869 | 0.3093 |
| 270.75 | 0.412 | 54.15 | 0.88248200 | 216.6 | 0.47007202 | 69 | 1083 | 0.62007 | 0.3100 |
| 271 | 0.413 | 54.20 | 0.88252235 | 216.8 | 0.46991059 | 68 | 1084 | 0.62145 | 0.3107 |
| 271.25 | 0.413 | 54.25 | 0.88256269 | 217.0 | 0.46974924 | 67 | 1085 | 0.62285 | 0.3114 |
| 271.5 | 0.413 | 54.30 | 0.88260301 | 217.2 | 0.46958795 | 66 | 1086 | 0.62426 | 0.3121 |
| 271.75 | 0.413 | 54.35 | 0.88264332 | 217.4 | 0.46942673 | 65 | 1087 | 0.62567 | 0.3128 |
| 272 | 0.413 | 54.40 | 0.88268360 | 217.6 | 0.46926559 | 64 | 1088 | 0.62710 | 0.3135 |
| 272.25 | 0.414 | 54.45 | 0.88272387 | 217.8 | 0.46910451 | 63 | 1089 | 0.62854 | 0.3143 |
| 272.5 | 0.414 | 54.50 | 0.88276412 | 218.0 | 0.46894350 | 62 | 1090 | 0.62998 | 0.3150 |
| 272.75 | 0.414 | 54.55 | 0.88280436 | 218.2 | 0.46878257 | 61 | 1091 | 0.63144 | 0.3157 |
| 273 | 0.414 | 54.60 | 0.88284458 | 218.4 | 0.46862170 | 60 | 1092 | 0.63291 | 0.3165 |
| 273.25 | 0.414 | 54.65 | 0.88288478 | 218.6 | 0.46846090 | 59 | 1093 | 0.63440 | 0.3172 |
| 273.5 | 0.415 | 54.70 | 0.88292496 | 218.8 | 0.46830017 | 58 | 1094 | 0.63589 | 0.3179 |
| 273.75 | 0.415 | 54.75 | 0.88296512 | 219.0 | 0.46813951 | 57 | 1095 | 0.63740 | 0.3187 |
| 274 | 0.415 | 54.80 | 0.88300527 | 219.2 | 0.46797891 | 56 | 1096 | 0.63891 | 0.3195 |
| 274.25 | 0.415 | 54.85 | 0.88304540 | 219.4 | 0.46781839 | 55 | 1097 | 0.64044 | 0.3202 |
| 274.5 | 0.415 | 54.90 | 0.88308552 | 219.6 | 0.46765794 | 54 | 1098 | 0.64199 | 0.3210 |
| 274.75 | 0.416 | 54.95 | 0.88312561 | 219.8 | 0.46749755 | 53 | 1099 | 0.64355 | 0.3218 |
| 275 | 0.416 | 55.00 | 0.88316569 | 220.0 | 0.46733723 | 52 | 1100 | 0.64512 | 0.3226 |
| 275.25 | 0.416 | 55.05 | 0.88320575 | 220.2 | 0.46717699 | 51 | 1101 | 0.64670 | 0.3234 |
| 275.5 | 0.416 | 55.10 | 0.88324580 | 220.4 | 0.46701681 | 50 | 1102 | 0.64830 | 0.3242 |
| 275.75 | 0.416 | 55.15 | 0.88328583 | 220.6 | 0.46685669 | 49 | 1103 | 0.64992 | 0.3250 |
| 276 | 0.417 | 55.20 | 0.88332584 | 220.8 | 0.46669665 | 48 | 1104 | 0.65155 | 0.3258 |
| 276.25 | 0.417 | 55.25 | 0.88336583 | 221.0 | 0.46653667 | 47 | 1105 | 0.65320 | 0.3266 |
| 276.5 | 0.417 | 55.30 | 0.88340581 | 221.2 | 0.46637677 | 46 | 1106 | 0.65486 | 0.3274 |
| 276.75 | 0.417 | 55.35 | 0.88344577 | 221.4 | 0.46621693 | 45 | 1107 | 0.65654 | 0.3283 |
| 277 | 0.417 | 55.40 | 0.88348571 | 221.6 | 0.46605715 | 44 | 1108 | 0.65824 | 0.3291 |
| 277.25 | 0.418 | 55.45 | 0.88352564 | 221.8 | 0.46589745 | 43 | 1109 | 0.65996 | 0.3300 |
| 277.5 | 0.418 | 55.50 | 0.88356555 | 222.0 | 0.46573781 | 42 | 1110 | 0.66169 | 0.3308 |
| 277.75 | 0.418 | 55.55 | 0.88360544 | 222.2 | 0.46557824 | 41 | 1111 | 0.66345 | 0.3317 |
| 278 | 0.418 | 55.60 | 0.88364531 | 222.4 | 0.46541874 | 40 | 1112 | 0.66522 | 0.3326 |
| 278.25 | 0.418 | 55.65 | 0.88368517 | 222.6 | 0.46525931 | 39 | 1113 | 0.66702 | 0.3335 |
| 278.5 | 0.419 | 55.70 | 0.88372501 | 222.8 | 0.46509994 | 38 | 1114 | 0.66884 | 0.3344 |
| 278.75 | 0.419 | 55.75 | 0.88376484 | 223.0 | 0.46494064 | 37 | 1115 | 0.67068 | 0.3353 |
| 279 | 0.419 | 55.80 | 0.88380465 | 223.2 | 0.46478141 | 36 | 1116 | 0.67254 | 0.3363 |
| 279.25 | 0.419 | 55.85 | 0.88384444 | 223.4 | 0.46462225 | 35 | 1117 | 0.67443 | 0.3372 |
| 279.5 | 0.419 | 55.90 | 0.88388421 | 223.6 | 0.46446315 | 34 | 1118 | 0.67635 | 0.3382 |
| 279.75 | 0.420 | 55.95 | 0.88392397 | 223.8 | 0.46430412 | 33 | 1119 | 0.67829 | 0.3391 |
| 280 | 0.420 | 56.00 | 0.88396371 | 224.0 | 0.46414515 | 32 | 1120 | 0.68026 | 0.3401 |
| 280.25 | 0.420 | 56.05 | 0.88400344 | 224.2 | 0.46398625 | 31 | 1121 | 0.68226 | 0.3411 |
| 280.5 | 0.420 | 56.10 | 0.88404314 | 224.4 | 0.46382742 | 30 | 1122 | 0.68428 | 0.3421 |
| 280.75 | 0.420 | 56.15 | 0.88408284 | 224.6 | 0.46366866 | 29 | 1123 | 0.68634 | 0.3432 |
| 281 | 0.421 | 56.20 | 0.88412251 | 224.8 | 0.46350996 | 28 | 1124 | 0.68844 | 0.3442 |
| 281.25 | 0.421 | 56.25 | 0.88416217 | 225.0 | 0.46335133 | 27 | 1125 | 0.69057 | 0.3453 |
| 281.5 | 0.421 | 56.30 | 0.88420181 | 225.2 | 0.46319276 | 26 | 1126 | 0.69274 | 0.3464 |
| 281.75 | 0.421 | 56.35 | 0.88424143 | 225.4 | 0.46303426 | 25 | 1127 | 0.69494 | 0.3475 |
| 282 | 0.421 | 56.40 | 0.88428104 | 225.6 | 0.46287583 | 24 | 1128 | 0.69719 | 0.3486 |


| 282.25 | 0.422 | 56.45 | 0.88432064 | 225.8 | 0.46271746 | 23 | 1129 | 0.69948 | 0.3497 |
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| 282.5 | 0.422 | 56.50 | 0.88436021 | 226.0 | 0.46255916 | 22 | 1130 | 0.70182 | 0.3509 |
| 282.75 | 0.422 | 56.55 | 0.88439977 | 226.2 | 0.46240092 | 21 | 1131 | 0.70422 | 0.3521 |
| 283 | 0.422 | 56.60 | 0.88443931 | 226.4 | 0.46224275 | 20 | 1132 | 0.70666 | 0.3533 |
| 283.25 | 0.422 | 56.65 | 0.88447884 | 226.6 | 0.46208465 | 19 | 1133 | 0.70916 | 0.3546 |
| 283.5 | 0.423 | 56.70 | 0.88451835 | 226.8 | 0.46192661 | 18 | 1134 | 0.71173 | 0.3559 |
| 283.75 | 0.423 | 56.75 | 0.88455784 | 227.0 | 0.46176864 | 17 | 1135 | 0.71436 | 0.3572 |
| 284 | 0.423 | 56.80 | 0.88459732 | 227.2 | 0.46161073 | 16 | 1136 | 0.71707 | 0.3585 |
| 284.25 | 0.423 | 56.85 | 0.88463678 | 227.4 | 0.46145289 | 15 | 1137 | 0.71986 | 0.3599 |
| 284.5 | 0.423 | 56.90 | 0.88467622 | 227.6 | 0.46129511 | 14 | 1138 | 0.72274 | 0.3614 |
| 284.75 | 0.424 | 56.95 | 0.88471565 | 227.8 | 0.46113740 | 13 | 1139 | 0.72571 | 0.3629 |
| 285 | 0.424 | 57.00 | 0.88475506 | 228.0 | 0.46097975 | 12 | 1140 | 0.72880 | 0.3644 |
| 285.25 | 0.424 | 57.05 | 0.88479446 | 228.2 | 0.46082217 | 11 | 1141 | 0.73201 | 0.3660 |
| 285.5 | 0.424 | 57.10 | 0.88483384 | 228.4 | 0.46066465 | 10 | 1142 | 0.73536 | 0.3677 |
| 285.75 | 0.424 | 57.15 | 0.88487320 | 228.6 | 0.46050720 | 9 | 1143 | 0.73887 | 0.3694 |
| 286 | 0.425 | 57.20 | 0.88491255 | 228.8 | 0.46034981 | 8 | 1144 | 0.74257 | 0.3713 |
| 286.25 | 0.425 | 57.25 | 0.88495188 | 229.0 | 0.46019249 | 7 | 1145 | 0.74649 | 0.3732 |
| 286.5 | 0.425 | 57.30 | 0.88499119 | 229.2 | 0.46003523 | 6 | 1146 | 0.75069 | 0.3753 |
| 286.75 | 0.425 | 57.35 | 0.88503049 | 229.4 | 0.45987803 | 5 | 1147 | 0.75523 | 0.3776 |
| 287 | 0.425 | 57.40 | 0.88506977 | 229.6 | 0.45972090 | 4 | 1148 | 0.76022 | 0.3801 |
| 287.25 | 0.426 | 57.45 | 0.88510904 | 229.8 | 0.45956384 | 3 | 1149 | 0.76585 | 0.3829 |
| 287.5 | 0.426 | 57.50 | 0.88514829 | 230.0 | 0.45940684 | 2 | 1150 | 0.77245 | 0.3862 |
| 287.75 | 0.426 | 57.55 | 0.88518753 | 230.2 | 0.45924990 | 1 | 1151 | 0.78092 | 0.3905 |
| 288 | 0.426 | 57.60 | 0.88522674 | 230.4 | 0.45909303 | 0 | 1152 | 0.80000 | 0.4000 |
| 288.25 | 0.426 | 57.65 | 0.88526595 | 230.6 | 0.45893622 | 1 | 1153 | 0.80994 | 0.4050 |
| 288.5 | 0.427 | 57.70 | 0.88530513 | 230.8 | 0.45877947 | 2 | 1154 | 0.81436 | 0.4072 |
| 288.75 | 0.427 | 57.75 | 0.88534430 | 231.0 | 0.45862279 | 3 | 1155 | 0.81780 | 0.4089 |
| 289 | 0.427 | 57.80 | 0.88538346 | 231.2 | 0.45846617 | 4 | 1156 | 0.82073 | 0.4104 |
| 289.25 | 0.427 | 57.85 | 0.88542259 | 231.4 | 0.45830962 | 5 | 1157 | 0.82333 | 0.4117 |
| 289.5 | 0.427 | 57.90 | 0.88546172 | 231.6 | 0.45815313 | 6 | 1158 | 0.82570 | 0.4129 |
| 289.75 | 0.428 | 57.95 | 0.88550082 | 231.8 | 0.45799670 | 7 | 1159 | 0.82789 | 0.4139 |
| 290 | 0.428 | 58.00 | 0.88553991 | 232.0 | 0.45784034 | 8 | 1160 | 0.82994 | 0.4150 |
| 290.25 | 0.428 | 58.05 | 0.88557899 | 232.2 | 0.45768404 | 9 | 1161 | 0.83186 | 0.4159 |
| 290.5 | 0.428 | 58.10 | 0.88561805 | 232.4 | 0.45752780 | 10 | 1162 | 0.83369 | 0.4168 |
| 290.75 | 0.428 | 58.15 | 0.88565709 | 232.6 | 0.45737163 | 11 | 1163 | 0.83544 | 0.4177 |
| 291 | 0.428 | 58.20 | 0.88569612 | 232.8 | 0.45721552 | 12 | 1164 | 0.83711 | 0.4186 |
| 291.25 | 0.429 | 58.25 | 0.88573513 | 233.0 | 0.45705947 | 13 | 1165 | 0.83872 | 0.4194 |
| 291.5 | 0.429 | 58.30 | 0.88577413 | 233.2 | 0.45690349 | 14 | 1166 | 0.84027 | 0.4201 |
| 291.75 | 0.429 | 58.35 | 0.88581311 | 233.4 | 0.45674757 | 15 | 1167 | 0.84177 | 0.4209 |
| 292 | 0.429 | 58.40 | 0.88585207 | 233.6 | 0.45659171 | 16 | 1168 | 0.84323 | 0.4216 |
| 292.25 | 0.429 | 58.45 | 0.88589102 | 233.8 | 0.45643591 | 17 | 1169 | 0.84464 | 0.4223 |
| 292.5 | 0.430 | 58.50 | 0.88592996 | 234.0 | 0.45628018 | 18 | 1170 | 0.84601 | 0.4230 |
| 292.75 | 0.430 | 58.55 | 0.88596887 | 234.2 | 0.45612451 | 19 | 1171 | 0.84735 | 0.4237 |
| 293 | 0.430 | 58.60 | 0.88600778 | 234.4 | 0.45596890 | 20 | 1172 | 0.84865 | 0.4243 |
| 293.25 | 0.430 | 58.65 | 0.88604666 | 234.6 | 0.45581335 | 21 | 1173 | 0.84993 | 0.4250 |
| 293.5 | 0.430 | 58.70 | 0.88608553 | 234.8 | 0.45565787 | 22 | 1174 | 0.85117 | 0.4256 |
| 293.75 | 0.431 | 58.75 | 0.88612439 | 235.0 | 0.45550245 | 23 | 1175 | 0.85239 | 0.4262 |
| 294 | 0.431 | 58.80 | 0.88616323 | 235.2 | 0.45534709 | 24 | 1176 | 0.85359 | 0.4268 |
| 294.25 | 0.431 | 58.85 | 0.88620205 | 235.4 | 0.45519179 | 25 | 1177 | 0.85476 | 0.4274 |
| 294.5 | 0.431 | 58.90 | 0.88624086 | 235.6 | 0.45503656 | 26 | 1178 | 0.85591 | 0.4280 |
| 294.75 | 0.431 | 58.95 | 0.88627965 | 235.8 | 0.45488138 | 27 | 1179 | 0.85704 | 0.4285 |
| 295 | 0.432 | 59.00 | 0.88631843 | 236.0 | 0.45472627 | 28 | 1180 | 0.85815 | 0.4291 |
| 295.25 | 0.432 | 59.05 | 0.88635719 | 236.2 | 0.45457122 | 29 | 1181 | 0.85924 | 0.4296 |
| 295.5 | 0.432 | 59.10 | 0.88639594 | 236.4 | 0.45441623 | 30 | 1182 | 0.86032 | 0.4302 |
| 295.75 | 0.432 | 59.15 | 0.88643467 | 236.6 | 0.45426131 | 31 | 1183 | 0.86137 | 0.4307 |
| 296 | 0.432 | 59.20 | 0.88647339 | 236.8 | 0.45410644 | 32 | 1184 | 0.86241 | 0.4312 |
| 296.25 | 0.433 | 59.25 | 0.88651209 | 237.0 | 0.45395164 | 33 | 1185 | 0.86344 | 0.4317 |
| 296.5 | 0.433 | 59.30 | 0.88655078 | 237.2 | 0.45379690 | 34 | 1186 | 0.86445 | 0.4322 |
| 296.75 | 0.433 | 59.35 | 0.88658945 | 237.4 | 0.45364222 | 35 | 1187 | 0.86545 | 0.4327 |
| 297 | 0.433 | 59.40 | 0.88662810 | 237.6 | 0.45348760 | 36 | 1188 | 0.86643 | 0.4332 |
| 297.25 | 0.433 | 59.45 | 0.88666674 | 237.8 | 0.45333304 | 37 | 1189 | 0.86741 | 0.4337 |
| 297.5 | 0.434 | 59.50 | 0.88670536 | 238.0 | 0.45317854 | 38 | 1190 | 0.86837 | 0.4342 |
| 297.75 | 0.434 | 59.55 | 0.88674397 | 238.2 | 0.45302411 | 39 | 1191 | 0.86931 | 0.4347 |
| 298 | 0.434 | 59.60 | 0.88678257 | 238.4 | 0.45286973 | 40 | 1192 | 0.87025 | 0.4351 |
| 298.25 | 0.434 | 59.65 | 0.88682115 | 238.6 | 0.45271542 | 41 | 1193 | 0.87117 | 0.4356 |
| 298.5 | 0.434 | 59.70 | 0.88685971 | 238.8 | 0.45256116 | 42 | 1194 | 0.87209 | 0.4360 |
| 298.75 | 0.434 | 59.75 | 0.88689826 | 239.0 | 0.45240697 | 43 | 1195 | 0.87299 | 0.4365 |
| 299 | 0.435 | 59.80 | 0.88693679 | 239.2 | 0.45225284 | 44 | 1196 | 0.87389 | 0.4369 |
| 299.25 | 0.435 | 59.85 | 0.88697531 | 239.4 | 0.45209876 | 45 | 1197 | 0.87477 | 0.4374 |
| 299.5 | 0.435 | 59.90 | 0.88701381 | 239.6 | 0.45194475 | 46 | 1198 | 0.87565 | 0.4378 |
| 299.75 | 0.435 | 59.95 | 0.88705230 | 239.8 | 0.45179080 | 47 | 1199 | 0.87652 | 0.4383 |


| 300 | 0.435 | 60.00 | 0.88709077 | 240.0 | 0.45163691 | 48 | 1200 | 0.87738 | 0.4387 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 300.25 | 0.436 | 60.05 | 0.88712923 | 240.2 | 0.45148308 | 49 | 1201 | 0.87823 | 0.4391 |
| 300.5 | 0.436 | 60.10 | 0.88716767 | 240.4 | 0.45132931 | 50 | 1202 | 0.87907 | 0.4395 |
| 300.75 | 0.436 | 60.15 | 0.88720610 | 240.6 | 0.45117560 | 51 | 1203 | 0.87990 | 0.4400 |
| 301 | 0.436 | 60.20 | 0.88724451 | 240.8 | 0.45102195 | 52 | 1204 | 0.88073 | 0.4404 |
| 301.25 | 0.436 | 60.25 | 0.88728291 | 241.0 | 0.45086836 | 53 | 1205 | 0.88155 | 0.4408 |
| 301.5 | 0.437 | 60.30 | 0.88732129 | 241.2 | 0.45071483 | 54 | 1206 | 0.88236 | 0.4412 |
| 301.75 | 0.437 | 60.35 | 0.88735966 | 241.4 | 0.45056136 | 55 | 1207 | 0.88317 | 0.4416 |
| 302 | 0.437 | 60.40 | 0.88739801 | 241.6 | 0.45040795 | 56 | 1208 | 0.88396 | 0.4420 |
| 302.25 | 0.437 | 60.45 | 0.88743635 | 241.8 | 0.45025460 | 57 | 1209 | 0.88476 | 0.4424 |
| 302.5 | 0.437 | 60.50 | 0.88747467 | 242.0 | 0.45010131 | 58 | 1210 | 0.88554 | 0.4428 |
| 302.75 | 0.438 | 60.55 | 0.88751298 | 242.2 | 0.44994808 | 59 | 1211 | 0.88632 | 0.4432 |
| 303 | 0.438 | 60.60 | 0.88755127 | 242.4 | 0.44979491 | 60 | 1212 | 0.88709 | 0.4435 |
| 303.25 | 0.438 | 60.65 | 0.88758955 | 242.6 | 0.44964179 | 61 | 1213 | 0.88786 | 0.4439 |
| 303.5 | 0.438 | 60.70 | 0.88762782 | 242.8 | 0.44948874 | 62 | 1214 | 0.88862 | 0.4443 |
| 303.75 | 0.438 | 60.75 | 0.88766606 | 243.0 | 0.44933575 | 63 | 1215 | 0.88937 | 0.4447 |
| 304 | 0.439 | 60.80 | 0.88770430 | 243.2 | 0.44918281 | 64 | 1216 | 0.89012 | 0.4451 |
| 304.25 | 0.439 | 60.85 | 0.88774252 | 243.4 | 0.44902993 | 65 | 1217 | 0.89086 | 0.4454 |
| 304.5 | 0.439 | 60.90 | 0.88778072 | 243.6 | 0.44887712 | 66 | 1218 | 0.89160 | 0.4458 |
| 304.75 | 0.439 | 60.95 | 0.88781891 | 243.8 | 0.44872436 | 67 | 1219 | 0.89234 | 0.4462 |
| 305 | 0.439 | 61.00 | 0.88785708 | 244.0 | 0.44857166 | 68 | 1220 | 0.89306 | 0.4465 |
| 305.25 | 0.439 | 61.05 | 0.88789525 | 244.2 | 0.44841902 | 69 | 1221 | 0.89379 | 0.4469 |
| 305.5 | 0.440 | 61.10 | 0.88793339 | 244.4 | 0.44826644 | 70 | 1222 | 0.89450 | 0.4473 |
| 305.75 | 0.440 | 61.15 | 0.88797152 | 244.6 | 0.44811392 | 71 | 1223 | 0.89522 | 0.4476 |
| 306 | 0.440 | 61.20 | 0.88800964 | 244.8 | 0.44796145 | 72 | 1224 | 0.89593 | 0.4480 |
| 306.25 | 0.440 | 61.25 | 0.88804774 | 245.0 | 0.44780905 | 73 | 1225 | 0.89663 | 0.4483 |
| 306.5 | 0.440 | 61.30 | 0.88808583 | 245.2 | 0.44765670 | 74 | 1226 | 0.89733 | 0.4487 |
| 306.75 | 0.441 | 61.35 | 0.88812390 | 245.4 | 0.44750441 | 75 | 1227 | 0.89802 | 0.4490 |
| 307 | 0.441 | 61.40 | 0.88816196 | 245.6 | 0.44735218 | 76 | 1228 | 0.89872 | 0.4494 |
| 307.25 | 0.441 | 61.45 | 0.88820000 | 245.8 | 0.44720001 | 77 | 1229 | 0.89940 | 0.4497 |
| 307.5 | 0.441 | 61.50 | 0.88823803 | 246.0 | 0.44704789 | 78 | 1230 | 0.90008 | 0.4500 |
| 307.75 | 0.441 | 61.55 | 0.88827604 | 246.2 | 0.44689584 | 79 | 1231 | 0.90076 | 0.4504 |
| 308 | 0.442 | 61.60 | 0.88831404 | 246.4 | 0.44674384 | 80 | 1232 | 0.90144 | 0.4507 |
| 308.25 | 0.442 | 61.65 | 0.88835203 | 246.6 | 0.44659190 | 81 | 1233 | 0.90211 | 0.4511 |
| 308.5 | 0.442 | 61.70 | 0.88839000 | 246.8 | 0.44644002 | 82 | 1234 | 0.90277 | 0.4514 |
| 308.75 | 0.442 | 61.75 | 0.88842795 | 247.0 | 0.44628819 | 83 | 1235 | 0.90343 | 0.4517 |
| 309 | 0.442 | 61.80 | 0.88846589 | 247.2 | 0.44613643 | 84 | 1236 | 0.90409 | 0.4520 |
| 309.25 | 0.443 | 61.85 | 0.88850382 | 247.4 | 0.44598472 | 85 | 1237 | 0.90475 | 0.4524 |
| 309.5 | 0.443 | 61.90 | 0.88854173 | 247.6 | 0.44583307 | 86 | 1238 | 0.90540 | 0.4527 |
| 309.75 | 0.443 | 61.95 | 0.88857963 | 247.8 | 0.44568147 | 87 | 1239 | 0.90605 | 0.4530 |
| 310 | 0.443 | 62.00 | 0.88861752 | 248.0 | 0.44552994 | 88 | 1240 | 0.90669 | 0.4533 |
| 310.25 | 0.443 | 62.05 | 0.88865539 | 248.2 | 0.44537846 | 89 | 1241 | 0.90733 | 0.4537 |
| 310.5 | 0.443 | 62.10 | 0.88869324 | 248.4 | 0.44522704 | 90 | 1242 | 0.90797 | 0.4540 |
| 310.75 | 0.444 | 62.15 | 0.88873108 | 248.6 | 0.44507567 | 91 | 1243 | 0.90860 | 0.4543 |
| 311 | 0.444 | 62.20 | 0.88876891 | 248.8 | 0.44492437 | 92 | 1244 | 0.90923 | 0.4546 |
| 311.25 | 0.444 | 62.25 | 0.88880672 | 249.0 | 0.44477312 | 93 | 1245 | 0.90986 | 0.4549 |
| 311.5 | 0.444 | 62.30 | 0.88884452 | 249.2 | 0.44462192 | 94 | 1246 | 0.91049 | 0.4552 |
| 311.75 | 0.444 | 62.35 | 0.88888230 | 249.4 | 0.44447079 | 95 | 1247 | 0.91111 | 0.4556 |
| 312 | 0.445 | 62.40 | 0.88892007 | 249.6 | 0.44431971 | 96 | 1248 | 0.91173 | 0.4559 |
| 312.25 | 0.445 | 62.45 | 0.88895783 | 249.8 | 0.44416869 | 97 | 1249 | 0.91234 | 0.4562 |
| 312.5 | 0.445 | 62.50 | 0.88899557 | 250.0 | 0.44401772 | 98 | 1250 | 0.91295 | 0.4565 |
| 312.75 | 0.445 | 62.55 | 0.88903330 | 250.2 | 0.44386681 | 99 | 1251 | 0.91356 | 0.4568 |
| 313 | 0.445 | 62.60 | 0.88907101 | 250.4 | 0.44371596 | 100 | 1252 | 0.91417 | 0.4571 |
| 313.25 | 0.446 | 62.65 | 0.88910871 | 250.6 | 0.44356517 | 101 | 1253 | 0.91477 | 0.4574 |
| 313.5 | 0.446 | 62.70 | 0.88914639 | 250.8 | 0.44341443 | 102 | 1254 | 0.91537 | 0.4577 |
| 313.75 | 0.446 | 62.75 | 0.88918406 | 251.0 | 0.44326375 | 103 | 1255 | 0.91597 | 0.4580 |
| 314 | 0.446 | 62.80 | 0.88922172 | 251.2 | 0.44311312 | 104 | 1256 | 0.91657 | 0.4583 |
| 314.25 | 0.446 | 62.85 | 0.88925936 | 251.4 | 0.44296255 | 105 | 1257 | 0.91716 | 0.4586 |
| 314.5 | 0.446 | 62.90 | 0.88929699 | 251.6 | 0.44281204 | 106 | 1258 | 0.91775 | 0.4589 |
| 314.75 | 0.447 | 62.95 | 0.88933460 | 251.8 | 0.44266158 | 107 | 1259 | 0.91834 | 0.4592 |
| 315 | 0.447 | 63.00 | 0.88937220 | 252.0 | 0.44251118 | 108 | 1260 | 0.91892 | 0.4595 |
| 315.25 | 0.447 | 63.05 | 0.88940979 | 252.2 | 0.44236084 | 109 | 1261 | 0.91951 | 0.4598 |
| 315.5 | 0.447 | 63.10 | 0.88944736 | 252.4 | 0.44221055 | 110 | 1262 | 0.92009 | 0.4600 |
| 315.75 | 0.447 | 63.15 | 0.88948492 | 252.6 | 0.44206032 | 111 | 1263 | 0.92066 | 0.4603 |
| 316 | 0.448 | 63.20 | 0.88952246 | 252.8 | 0.44191014 | 112 | 1264 | 0.92124 | 0.4606 |
| 316.25 | 0.448 | 63.25 | 0.88955999 | 253.0 | 0.44176002 | 113 | 1265 | 0.92181 | 0.4609 |
| 316.5 | 0.448 | 63.30 | 0.88959751 | 253.2 | 0.44160996 | 114 | 1266 | 0.92238 | 0.4612 |
| 316.75 | 0.448 | 63.35 | 0.88963501 | 253.4 | 0.44145995 | 115 | 1267 | 0.92295 | 0.4615 |
| 317 | 0.448 | 63.40 | 0.88967250 | 253.6 | 0.44130999 | 116 | 1268 | 0.92351 | 0.4618 |
| 317.25 | 0.449 | 63.45 | 0.88970998 | 253.8 | 0.44116010 | 117 | 1269 | 0.92408 | 0.4620 |
| 317.5 | 0.449 | 63.50 | 0.88974744 | 254.0 | 0.44101025 | 118 | 1270 | 0.92464 | 0.4623 |


| 317.75 | 0.449 | 63.55 | 0.88978488 | 254.2 | 0.44086047 | 119 | 1271 | 0.92520 | 0.4626 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 318 | 0.449 | 63.60 | 0.88982232 | 254.4 | 0.44071074 | 120 | 1272 | 0.92575 | 0.4629 |
| 318.25 | 0.449 | 63.65 | 0.88985973 | 254.6 | 0.44056106 | 121 | 1273 | 0.92631 | 0.4632 |
| 318.5 | 0.449 | 63.70 | 0.88989714 | 254.8 | 0.44041144 | 122 | 1274 | 0.92686 | 0.4634 |
| 318.75 | 0.450 | 63.75 | 0.88993453 | 255.0 | 0.44026187 | 123 | 1275 | 0.92741 | 0.4637 |
| 319 | 0.450 | 63.80 | 0.88997191 | 255.2 | 0.44011236 | 124 | 1276 | 0.92796 | 0.4640 |
| 319.25 | 0.450 | 63.85 | 0.89000927 | 255.4 | 0.43996291 | 125 | 1277 | 0.92850 | 0.4643 |
| 319.5 | 0.450 | 63.90 | 0.89004662 | 255.6 | 0.43981351 | 126 | 1278 | 0.92905 | 0.4645 |
| 319.75 | 0.450 | 63.95 | 0.89008396 | 255.8 | 0.43966416 | 127 | 1279 | 0.92959 | 0.4648 |
| 320 | 0.451 | 64.00 | 0.89012128 | 256.0 | 0.43951487 | 128 | 1280 | 0.93013 | 0.4651 |
| 320.25 | 0.451 | 64.05 | 0.89015859 | 256.2 | 0.43936563 | 129 | 1281 | 0.93067 | 0.4653 |
| 320.5 | 0.451 | 64.10 | 0.89019589 | 256.4 | 0.43921645 | 130 | 1282 | 0.93120 | 0.4656 |
| 320.75 | 0.451 | 64.15 | 0.89023317 | 256.6 | 0.43906733 | 131 | 1283 | 0.93174 | 0.4659 |
| 321 | 0.451 | 64.20 | 0.89027044 | 256.8 | 0.43891825 | 132 | 1284 | 0.93227 | 0.4661 |
| 321.25 | 0.452 | 64.25 | 0.89030769 | 257.0 | 0.43876924 | 133 | 1285 | 0.93280 | 0.4664 |
| 321.5 | 0.452 | 64.30 | 0.89034493 | 257.2 | 0.43862027 | 134 | 1286 | 0.93333 | 0.4667 |
| 321.75 | 0.452 | 64.35 | 0.89038216 | 257.4 | 0.43847137 | 135 | 1287 | 0.93385 | 0.4669 |
| 322 | 0.452 | 64.40 | 0.89041937 | 257.6 | 0.43832251 | 136 | 1288 | 0.93438 | 0.4672 |
| 322.25 | 0.452 | 64.45 | 0.89045657 | 257.8 | 0.43817371 | 137 | 1289 | 0.93490 | 0.4675 |
| 322.5 | 0.452 | 64.50 | 0.89049376 | 258.0 | 0.43802497 | 138 | 1290 | 0.93542 | 0.4677 |
| 322.75 | 0.453 | 64.55 | 0.89053093 | 258.2 | 0.43787627 | 139 | 1291 | 0.93594 | 0.4680 |
| 323 | 0.453 | 64.60 | 0.89056809 | 258.4 | 0.43772764 | 140 | 1292 | 0.93646 | 0.4682 |
| 323.25 | 0.453 | 64.65 | 0.89060524 | 258.6 | 0.43757905 | 141 | 1293 | 0.93697 | 0.4685 |
| 323.5 | 0.453 | 64.70 | 0.89064237 | 258.8 | 0.43743053 | 142 | 1294 | 0.93749 | 0.4687 |
| 323.75 | 0.453 | 64.75 | 0.89067949 | 259.0 | 0.43728205 | 143 | 1295 | 0.93800 | 0.4690 |
| 324 | 0.454 | 64.80 | 0.89071659 | 259.2 | 0.43713363 | 144 | 1296 | 0.93851 | 0.4693 |
| 324.25 | 0.454 | 64.85 | 0.89075368 | 259.4 | 0.43698526 | 145 | 1297 | 0.93902 | 0.4695 |
| 324.5 | 0.454 | 64.90 | 0.89079076 | 259.6 | 0.43683695 | 146 | 1298 | 0.93953 | 0.4698 |
| 324.75 | 0.454 | 64.95 | 0.89082783 | 259.8 | 0.43668869 | 147 | 1299 | 0.94003 | 0.4700 |
| 325 | 0.454 | 65.00 | 0.89086488 | 260.0 | 0.43654048 | 148 | 1300 | 0.94054 | 0.4703 |
| 325.25 | 0.455 | 65.05 | 0.89090192 | 260.2 | 0.43639233 | 149 | 1301 | 0.94104 | 0.4705 |
| 325.5 | 0.455 | 65.10 | 0.89093894 | 260.4 | 0.43624423 | 150 | 1302 | 0.94154 | 0.4708 |
| 325.75 | 0.455 | 65.15 | 0.89097595 | 260.6 | 0.43609618 | 151 | 1303 | 0.94204 | 0.4710 |
| 326 | 0.455 | 65.20 | 0.89101295 | 260.8 | 0.43594819 | 152 | 1304 | 0.94254 | 0.4713 |
| 326.25 | 0.455 | 65.25 | 0.89104994 | 261.0 | 0.43580025 | 153 | 1305 | 0.94303 | 0.4715 |
| 326.5 | 0.455 | 65.30 | 0.89108691 | 261.2 | 0.43565237 | 154 | 1306 | 0.94353 | 0.4718 |
| 326.75 | 0.456 | 65.35 | 0.89112387 | 261.4 | 0.43550453 | 155 | 1307 | 0.94402 | 0.4720 |
| 327 | 0.456 | 65.40 | 0.89116081 | 261.6 | 0.43535675 | 156 | 1308 | 0.94451 | 0.4723 |
| 327.25 | 0.456 | 65.45 | 0.89119774 | 261.8 | 0.43520903 | 157 | 1309 | 0.94500 | 0.4725 |
| 327.5 | 0.456 | 65.50 | 0.89123466 | 262.0 | 0.43506135 | 158 | 1310 | 0.94549 | 0.4727 |
| 327.75 | 0.456 | 65.55 | 0.89127157 | 262.2 | 0.43491373 | 159 | 1311 | 0.94598 | 0.4730 |
| 328 | 0.457 | 65.60 | 0.89130846 | 262.4 | 0.43476617 | 160 | 1312 | 0.94647 | 0.4732 |
| 328.25 | 0.457 | 65.65 | 0.89134534 | 262.6 | 0.43461865 | 161 | 1313 | 0.94695 | 0.4735 |
| 328.5 | 0.457 | 65.70 | 0.89138220 | 262.8 | 0.43447119 | 162 | 1314 | 0.94743 | 0.4737 |
| 328.75 | 0.457 | 65.75 | 0.89141906 | 263.0 | 0.43432378 | 163 | 1315 | 0.94791 | 0.4740 |
| 329 | 0.457 | 65.80 | 0.89145589 | 263.2 | 0.43417642 | 164 | 1316 | 0.94839 | 0.4742 |
| 329.25 | 0.457 | 65.85 | 0.89149272 | 263.4 | 0.43402912 | 165 | 1317 | 0.94887 | 0.4744 |
| 329.5 | 0.458 | 65.90 | 0.89152953 | 263.6 | 0.43388187 | 166 | 1318 | 0.94935 | 0.4747 |
| 329.75 | 0.458 | 65.95 | 0.89156633 | 263.8 | 0.43373467 | 167 | 1319 | 0.94983 | 0.4749 |
| 330 | 0.458 | 66.00 | 0.89160312 | 264.0 | 0.43358752 | 168 | 1320 | 0.95030 | 0.4752 |
| 330.25 | 0.458 | 66.05 | 0.89163989 | 264.2 | 0.43344043 | 169 | 1321 | 0.95078 | 0.4754 |
| 330.5 | 0.458 | 66.10 | 0.89167665 | 264.4 | 0.43329339 | 170 | 1322 | 0.95125 | 0.4756 |
| 330.75 | 0.459 | 66.15 | 0.89171340 | 264.6 | 0.43314640 | 171 | 1323 | 0.95172 | 0.4759 |
| 331 | 0.459 | 66.20 | 0.89175013 | 264.8 | 0.43299946 | 172 | 1324 | 0.95219 | 0.4761 |
| 331.25 | 0.459 | 66.25 | 0.89178686 | 265.0 | 0.43285258 | 173 | 1325 | 0.95266 | 0.4763 |
| 331.5 | 0.459 | 66.30 | 0.89182356 | 265.2 | 0.43270574 | 174 | 1326 | 0.95312 | 0.4766 |
| 331.75 | 0.459 | 66.35 | 0.89186026 | 265.4 | 0.43255896 | 175 | 1327 | 0.95359 | 0.4768 |
| 332 | 0.459 | 66.40 | 0.89189694 | 265.6 | 0.43241223 | 176 | 1328 | 0.95405 | 0.4770 |
| 332.25 | 0.460 | 66.45 | 0.89193361 | 265.8 | 0.43226556 | 177 | 1329 | 0.95452 | 0.4773 |
| 332.5 | 0.460 | 66.50 | 0.89197027 | 266.0 | 0.43211893 | 178 | 1330 | 0.95498 | 0.4775 |
| 332.75 | 0.460 | 66.55 | 0.89200691 | 266.2 | 0.43197236 | 179 | 1331 | 0.95544 | 0.4777 |
| 333 | 0.460 | 66.60 | 0.89204354 | 266.4 | 0.43182584 | 180 | 1332 | 0.95590 | 0.4780 |
| 333.25 | 0.460 | 66.65 | 0.89208016 | 266.6 | 0.43167937 | 181 | 1333 | 0.95636 | 0.4782 |
| 333.5 | 0.461 | 66.70 | 0.89211676 | 266.8 | 0.43153295 | 182 | 1334 | 0.95682 | 0.4784 |
| 333.75 | 0.461 | 66.75 | 0.89215335 | 267.0 | 0.43138658 | 183 | 1335 | 0.95727 | 0.4786 |
| 334 | 0.461 | 66.80 | 0.89218993 | 267.2 | 0.43124027 | 184 | 1336 | 0.95773 | 0.4789 |
| 334.25 | 0.461 | 66.85 | 0.89222650 | 267.4 | 0.43109400 | 185 | 1337 | 0.95818 | 0.4791 |
| 334.5 | 0.461 | 66.90 | 0.89226305 | 267.6 | 0.43094779 | 186 | 1338 | 0.95863 | 0.4793 |
| 334.75 | 0.461 | 66.95 | 0.89229959 | 267.8 | 0.43080163 | 187 | 1339 | 0.95908 | 0.4795 |
| 335 | 0.462 | 67.00 | 0.89233612 | 268.0 | 0.43065552 | 188 | 1340 | 0.95953 | 0.4798 |
| 335.25 | 0.462 | 67.05 | 0.89237263 | 268.2 | 0.43050946 | 189 | 1341 | 0.95998 | 0.4800 |


| 335.5 | 0.462 | 67.10 | 0.89240914 | 268.4 | 0.43036345 | 190 | 1342 | 0.96043 | 0.4802 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 335.75 | 0.462 | 67.15 | 0.89244563 | 268.6 | 0.43021750 | 191 | 1343 | 0.96088 | 0.4804 |
| 336 | 0.462 | 67.20 | 0.89248210 | 268.8 | 0.43007159 | 192 | 1344 | 0.96132 | 0.4807 |
| 336.25 | 0.463 | 67.25 | 0.89251857 | 269.0 | 0.42992574 | 193 | 1345 | 0.96177 | 0.4809 |
| 336.5 | 0.463 | 67.30 | 0.89255502 | 269.2 | 0.42977994 | 194 | 1346 | 0.96221 | 0.4811 |
| 336.75 | 0.463 | 67.35 | 0.89259145 | 269.4 | 0.42963418 | 195 | 1347 | 0.96266 | 0.4813 |
| 337 | 0.463 | 67.40 | 0.89262788 | 269.6 | 0.42948848 | 196 | 1348 | 0.96310 | 0.4815 |
| 337.25 | 0.463 | 67.45 | 0.89266429 | 269.8 | 0.42934283 | 197 | 1349 | 0.96354 | 0.4818 |
| 337.5 | 0.464 | 67.50 | 0.89270069 | 270.0 | 0.42919723 | 198 | 1350 | 0.96398 | 0.4820 |
| 337.75 | 0.464 | 67.55 | 0.89273708 | 270.2 | 0.42905168 | 199 | 1351 | 0.96442 | 0.4822 |
| 338 | 0.464 | 67.60 | 0.89277345 | 270.4 | 0.42890618 | 200 | 1352 | 0.96485 | 0.4824 |
| 338.25 | 0.464 | 67.65 | 0.89280982 | 270.6 | 0.42876074 | 201 | 1353 | 0.96529 | 0.4826 |
| 338.5 | 0.464 | 67.70 | 0.89284617 | 270.8 | 0.42861534 | 202 | 1354 | 0.96573 | 0.4829 |
| 338.75 | 0.464 | 67.75 | 0.89288250 | 271.0 | 0.42846999 | 203 | 1355 | 0.96616 | 0.4831 |
| 339 | 0.465 | 67.80 | 0.89291883 | 271.2 | 0.42832470 | 204 | 1356 | 0.96659 | 0.4833 |
| 339.25 | 0.465 | 67.85 | 0.89295514 | 271.4 | 0.42817945 | 205 | 1357 | 0.96703 | 0.4835 |
| 339.5 | 0.465 | 67.90 | 0.89299144 | 271.6 | 0.42803425 | 206 | 1358 | 0.96746 | 0.4837 |
| 339.75 | 0.465 | 67.95 | 0.89302772 | 271.8 | 0.42788911 | 207 | 1359 | 0.96789 | 0.4839 |
| 340 | 0.465 | 68.00 | 0.89306400 | 272.0 | 0.42774401 | 208 | 1360 | 0.96832 | 0.4842 |
| 340.25 | 0.466 | 68.05 | 0.89310026 | 272.2 | 0.42759897 | 209 | 1361 | 0.96874 | 0.4844 |
| 340.5 | 0.466 | 68.10 | 0.89313651 | 272.4 | 0.42745397 | 210 | 1362 | 0.96917 | 0.4846 |
| 340.75 | 0.466 | 68.15 | 0.89317274 | 272.6 | 0.42730903 | 211 | 1363 | 0.96960 | 0.4848 |
| 341 | 0.466 | 68.20 | 0.89320897 | 272.8 | 0.42716413 | 212 | 1364 | 0.97002 | 0.4850 |
| 341.25 | 0.466 | 68.25 | 0.89324518 | 273.0 | 0.42701929 | 213 | 1365 | 0.97045 | 0.4852 |
| 341.5 | 0.466 | 68.30 | 0.89328138 | 273.2 | 0.42687449 | 214 | 1366 | 0.97087 | 0.4854 |
| 341.75 | 0.467 | 68.35 | 0.89331756 | 273.4 | 0.42672974 | 215 | 1367 | 0.97129 | 0.4856 |
| 342 | 0.467 | 68.40 | 0.89335374 | 273.6 | 0.42658505 | 216 | 1368 | 0.97172 | 0.4859 |
| 342.25 | 0.467 | 68.45 | 0.89338990 | 273.8 | 0.42644040 | 217 | 1369 | 0.97214 | 0.4861 |
| 342.5 | 0.467 | 68.50 | 0.89342605 | 274.0 | 0.42629581 | 218 | 1370 | 0.97256 | 0.4863 |
| 342.75 | 0.467 | 68.55 | 0.89346219 | 274.2 | 0.42615126 | 219 | 1371 | 0.97298 | 0.4865 |
| 343 | 0.467 | 68.60 | 0.89349831 | 274.4 | 0.42600676 | 220 | 1372 | 0.97339 | 0.4867 |
| 343.25 | 0.468 | 68.65 | 0.89353442 | 274.6 | 0.42586231 | 221 | 1373 | 0.97381 | 0.4869 |
| 343.5 | 0.468 | 68.70 | 0.89357052 | 274.8 | 0.42571792 | 222 | 1374 | 0.97423 | 0.4871 |
| 343.75 | 0.468 | 68.75 | 0.89360661 | 275.0 | 0.42557357 | 223 | 1375 | 0.97464 | 0.4873 |
| 344 | 0.468 | 68.80 | 0.89364268 | 275.2 | 0.42542927 | 224 | 1376 | 0.97506 | 0.4875 |
| 344.25 | 0.468 | 68.85 | 0.89367875 | 275.4 | 0.42528502 | 225 | 1377 | 0.97547 | 0.4877 |
| 344.5 | 0.469 | 68.90 | 0.89371480 | 275.6 | 0.42514082 | 226 | 1378 | 0.97589 | 0.4879 |
| 344.75 | 0.469 | 68.95 | 0.89375083 | 275.8 | 0.42499666 | 227 | 1379 | 0.97630 | 0.4881 |
| 345 | 0.469 | 69.00 | 0.89378686 | 276.0 | 0.42485256 | 228 | 1380 | 0.97671 | 0.4884 |
| 345.25 | 0.469 | 69.05 | 0.89382287 | 276.2 | 0.42470851 | 229 | 1381 | 0.97712 | 0.4886 |
| 345.5 | 0.469 | 69.10 | 0.89385887 | 276.4 | 0.42456450 | 230 | 1382 | 0.97753 | 0.4888 |
| 345.75 | 0.469 | 69.15 | 0.89389486 | 276.6 | 0.42442055 | 231 | 1383 | 0.97794 | 0.4890 |
| 346 | 0.470 | 69.20 | 0.89393084 | 276.8 | 0.42427664 | 232 | 1384 | 0.97834 | 0.4892 |
| 346.25 | 0.470 | 69.25 | 0.89396680 | 277.0 | 0.42413278 | 233 | 1385 | 0.97875 | 0.4894 |
| 346.5 | 0.470 | 69.30 | 0.89400276 | 277.2 | 0.42398897 | 234 | 1386 | 0.97916 | 0.4896 |
| 346.75 | 0.470 | 69.35 | 0.89403870 | 277.4 | 0.42384521 | 235 | 1387 | 0.97956 | 0.4898 |
| 347 | 0.470 | 69.40 | 0.89407463 | 277.6 | 0.42370150 | 236 | 1388 | 0.97997 | 0.4900 |
| 347.25 | 0.471 | 69.45 | 0.89411054 | 277.8 | 0.42355784 | 237 | 1389 | 0.98037 | 0.4902 |
| 347.5 | 0.471 | 69.50 | 0.89414644 | 278.0 | 0.42341422 | 238 | 1390 | 0.98077 | 0.4904 |
| 347.75 | 0.471 | 69.55 | 0.89418234 | 278.2 | 0.42327066 | 239 | 1391 | 0.98118 | 0.4906 |
| 348 | 0.471 | 69.60 | 0.89421822 | 278.4 | 0.42312714 | 240 | 1392 | 0.98158 | 0.4908 |
| 348.25 | 0.471 | 69.65 | 0.89425408 | 278.6 | 0.42298367 | 241 | 1393 | 0.98198 | 0.4910 |
| 348.5 | 0.471 | 69.70 | 0.89428994 | 278.8 | 0.42284025 | 242 | 1394 | 0.98238 | 0.4912 |
| 348.75 | 0.472 | 69.75 | 0.89432578 | 279.0 | 0.42269688 | 243 | 1395 | 0.98278 | 0.4914 |
| 349 | 0.472 | 69.80 | 0.89436161 | 279.2 | 0.42255355 | 244 | 1396 | 0.98318 | 0.4916 |
| 349.25 | 0.472 | 69.85 | 0.89439743 | 279.4 | 0.42241028 | 245 | 1397 | 0.98357 | 0.4918 |
| 349.5 | 0.472 | 69.90 | 0.89443324 | 279.6 | 0.42226705 | 246 | 1398 | 0.98397 | 0.4920 |
| 349.75 | 0.472 | 69.95 | 0.89446903 | 279.8 | 0.42212387 | 247 | 1399 | 0.98437 | 0.4922 |
| 350 | 0.473 | 70.00 | 0.89450482 | 280.0 | 0.42198074 | 248 | 1400 | 0.98476 | 0.4924 |
| 350.25 | 0.473 | 70.05 | 0.89454059 | 280.2 | 0.42183765 | 249 | 1401 | 0.98516 | 0.4926 |
| 350.5 | 0.473 | 70.10 | 0.89457635 | 280.4 | 0.42169462 | 250 | 1402 | 0.98555 | 0.4928 |
| 350.75 | 0.473 | 70.15 | 0.89461209 | 280.6 | 0.42155163 | 251 | 1403 | 0.98594 | 0.4930 |
| 351 | 0.473 | 70.20 | 0.89464783 | 280.8 | 0.42140869 | 252 | 1404 | 0.98633 | 0.4932 |
| 351.25 | 0.473 | 70.25 | 0.89468355 | 281.0 | 0.42126580 | 253 | 1405 | 0.98673 | 0.4934 |
| 351.5 | 0.474 | 70.30 | 0.89471926 | 281.2 | 0.42112296 | 254 | 1406 | 0.98712 | 0.4936 |
| 351.75 | 0.474 | 70.35 | 0.89475496 | 281.4 | 0.42098016 | 255 | 1407 | 0.98751 | 0.4938 |
| 352 | 0.474 | 70.40 | 0.89479065 | 281.6 | 0.42083741 | 256 | 1408 | 0.98790 | 0.4939 |
| 352.25 | 0.474 | 70.45 | 0.89482632 | 281.8 | 0.42069471 | 257 | 1409 | 0.98829 | 0.4941 |
| 352.5 | 0.474 | 70.50 | 0.89486199 | 282.0 | 0.42055206 | 258 | 1410 | 0.98867 | 0.4943 |
| 352.75 | 0.474 | 70.55 | 0.89489764 | 282.2 | 0.42040945 | 259 | 1411 | 0.98906 | 0.4945 |
| 353 | 0.475 | 70.60 | 0.89493328 | 282.4 | 0.42026690 | 260 | 1412 | 0.98945 | 0.4947 |


| 353.25 | 0.475 | 70.65 | 0.89496890 | 282.6 | 0.42012438 | 261 | 1413 | 0.98983 | 0.4949 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 353.5 | 0.475 | 70.70 | 0.89500452 | 282.8 | 0.41998192 | 262 | 1414 | 0.99022 | 0.4951 |
| 353.75 | 0.475 | 70.75 | 0.89504012 | 283.0 | 0.41983951 | 263 | 1415 | 0.99060 | 0.4953 |
| 354 | 0.475 | 70.80 | 0.89507572 | 283.2 | 0.41969714 | 264 | 1416 | 0.99099 | 0.4955 |
| 354.25 | 0.476 | 70.85 | 0.89511130 | 283.4 | 0.41955482 | 265 | 1417 | 0.99137 | 0.4957 |
| 354.5 | 0.476 | 70.90 | 0.89514686 | 283.6 | 0.41941254 | 266 | 1418 | 0.99175 | 0.4959 |
| 354.75 | 0.476 | 70.95 | 0.89518242 | 283.8 | 0.41927031 | 267 | 1419 | 0.99213 | 0.4961 |
| 355 | 0.476 | 71.00 | 0.89521797 | 284.0 | 0.41912813 | 268 | 1420 | 0.99251 | 0.4963 |
| 355.25 | 0.476 | 71.05 | 0.89525350 | 284.2 | 0.41898600 | 269 | 1421 | 0.99289 | 0.4964 |
| 355.5 | 0.476 | 71.10 | 0.89528902 | 284.4 | 0.41884392 | 270 | 1422 | 0.99327 | 0.4966 |
| 355.75 | 0.477 | 71.15 | 0.89532453 | 284.6 | 0.41870188 | 271 | 1423 | 0.99365 | 0.4968 |
| 356 | 0.477 | 71.20 | 0.89536003 | 284.8 | 0.41855988 | 272 | 1424 | 0.99403 | 0.4970 |
| 356.25 | 0.477 | 71.25 | 0.89539552 | 285.0 | 0.41841794 | 273 | 1425 | 0.99441 | 0.4972 |
| 356.5 | 0.477 | 71.30 | 0.89543099 | 285.2 | 0.41827604 | 274 | 1426 | 0.99479 | 0.4974 |
| 356.75 | 0.477 | 71.35 | 0.89546645 | 285.4 | 0.41813419 | 275 | 1427 | 0.99516 | 0.4976 |
| 357 | 0.478 | 71.40 | 0.89550190 | 285.6 | 0.41799238 | 276 | 1428 | 0.99554 | 0.4978 |
| 357.25 | 0.478 | 71.45 | 0.89553734 | 285.8 | 0.41785063 | 277 | 1429 | 0.99591 | 0.4980 |
| 357.5 | 0.478 | 71.50 | 0.89557277 | 286.0 | 0.41770891 | 278 | 1430 | 0.99629 | 0.4981 |
| 357.75 | 0.478 | 71.55 | 0.89560819 | 286.2 | 0.41756725 | 279 | 1431 | 0.99666 | 0.4983 |
| 358 | 0.478 | 71.60 | 0.89564359 | 286.4 | 0.41742563 | 280 | 1432 | 0.99704 | 0.4985 |
| 358.25 | 0.478 | 71.65 | 0.89567899 | 286.6 | 0.41728406 | 281 | 1433 | 0.99741 | 0.4987 |
| 358.5 | 0.479 | 71.70 | 0.89571437 | 286.8 | 0.41714253 | 282 | 1434 | 0.99778 | 0.4989 |
| 358.75 | 0.479 | 71.75 | 0.89574974 | 287.0 | 0.41700105 | 283 | 1435 | 0.99815 | 0.4991 |
| 359 | 0.479 | 71.80 | 0.89578509 | 287.2 | 0.41685962 | 284 | 1436 | 0.99852 | 0.4993 |
| 359.25 | 0.479 | 71.85 | 0.89582044 | 287.4 | 0.41671823 | 285 | 1437 | 0.99889 | 0.4994 |
| 359.5 | 0.479 | 71.90 | 0.89585578 | 287.6 | 0.41657689 | 286 | 1438 | 0.99926 | 0.4996 |
| 359.75 | 0.479 | 71.95 | 0.89589110 | 287.8 | 0.41643560 | 287 | 1439 | 0.99963 | 0.4998 |
| 360 | 0.480 | 72.00 | 0.89592641 | 288.0 | 0.41629435 | 288 | 1440 | 1.00000 | 0.5000 |
| 360.25 | 0.480 | 72.05 | 0.89596171 | 288.2 | 0.41615315 |  |  |  |  |
| 360.5 | 0.480 | 72.10 | 0.89599700 | 288.4 | 0.41601199 |  |  |  |  |
| 360.75 | 0.480 | 72.15 | 0.89603228 | 288.6 | 0.41587088 |  |  |  |  |
| 361 | 0.480 | 72.20 | 0.89606754 | 288.8 | 0.41572982 |  |  |  |  |
| 361.25 | 0.481 | 72.25 | 0.89610280 | 289.0 | 0.41558880 |  |  |  |  |
| 361.5 | 0.481 | 72.30 | 0.89613804 | 289.2 | 0.41544783 |  |  |  |  |
| 361.75 | 0.481 | 72.35 | 0.89617327 | 289.4 | 0.41530690 |  |  |  |  |
| 362 | 0.481 | 72.40 | 0.89620849 | 289.6 | 0.41516602 |  |  |  |  |
| 362.25 | 0.481 | 72.45 | 0.89624370 | 289.8 | 0.41502519 |  |  |  |  |
| 362.5 | 0.481 | 72.50 | 0.89627890 | 290.0 | 0.41488440 |  |  |  |  |
| 362.75 | 0.482 | 72.55 | 0.89631409 | 290.2 | 0.41474366 |  |  |  |  |
| 363 | 0.482 | 72.60 | 0.89634926 | 290.4 | 0.41460296 |  |  |  |  |
| 363.25 | 0.482 | 72.65 | 0.89638442 | 290.6 | 0.41446231 |  |  |  |  |
| 363.5 | 0.482 | 72.70 | 0.89641958 | 290.8 | 0.41432170 |  |  |  |  |
| 363.75 | 0.482 | 72.75 | 0.89645472 | 291.0 | 0.41418114 |  |  |  |  |
| 364 | 0.482 | 72.80 | 0.89648984 | 291.2 | 0.41404062 |  |  |  |  |
| 364.25 | 0.483 | 72.85 | 0.89652496 | 291.4 | 0.41390015 |  |  |  |  |
| 364.5 | 0.483 | 72.90 | 0.89656007 | 291.6 | 0.41375972 |  |  |  |  |
| 364.75 | 0.483 | 72.95 | 0.89659516 | 291.8 | 0.41361934 |  |  |  |  |
| 365 | 0.483 | 73.00 | 0.89663025 | 292.0 | 0.41347901 |  |  |  |  |
| 365.25 | 0.483 | 73.05 | 0.89666532 | 292.2 | 0.41333872 |  |  |  |  |
| 365.5 | 0.484 | 73.10 | 0.89670038 | 292.4 | 0.41319847 |  |  |  |  |
| 365.75 | 0.484 | 73.15 | 0.89673543 | 292.6 | 0.41305827 |  |  |  |  |
| 366 | 0.484 | 73.20 | 0.89677047 | 292.8 | 0.41291812 |  |  |  |  |
| 366.25 | 0.484 | 73.25 | 0.89680550 | 293.0 | 0.41277801 |  |  |  |  |
| 366.5 | 0.484 | 73.30 | 0.89684051 | 293.2 | 0.41263795 |  |  |  |  |
| 366.75 | 0.484 | 73.35 | 0.89687552 | 293.4 | 0.41249793 |  |  |  |  |
| 367 | 0.485 | 73.40 | 0.89691051 | 293.6 | 0.41235795 |  |  |  |  |
| 367.25 | 0.485 | 73.45 | 0.89694549 | 293.8 | 0.41221802 |  |  |  |  |
| 367.5 | 0.485 | 73.50 | 0.89698047 | 294.0 | 0.41207814 |  |  |  |  |
| 367.75 | 0.485 | 73.55 | 0.89701543 | 294.2 | 0.41193830 |  |  |  |  |
| 368 | 0.485 | 73.60 | 0.89705038 | 294.4 | 0.41179850 |  |  |  |  |
| 368.25 | 0.485 | 73.65 | 0.89708531 | 294.6 | 0.41165875 |  |  |  |  |
| 368.5 | 0.486 | 73.70 | 0.89712024 | 294.8 | 0.41151904 |  |  |  |  |
| 368.75 | 0.486 | 73.75 | 0.89715516 | 295.0 | 0.41137938 |  |  |  |  |
| 369 | 0.486 | 73.80 | 0.89719006 | 295.2 | 0.41123976 |  |  |  |  |
| 369.25 | 0.486 | 73.85 | 0.89722495 | 295.4 | 0.41110019 |  |  |  |  |
| 369.5 | 0.486 | 73.90 | 0.89725984 | 295.6 | 0.41096066 |  |  |  |  |
| 369.75 | 0.486 | 73.95 | 0.89729471 | 295.8 | 0.41082117 |  |  |  |  |
| 370 | 0.487 | 74.00 | 0.89732957 | 296.0 | 0.41068173 |  |  |  |  |
| 370.25 | 0.487 | 74.05 | 0.89736442 | 296.2 | 0.41054234 |  |  |  |  |
| 370.5 | 0.487 | 74.10 | 0.89739925 | 296.4 | 0.41040299 |  |  |  |  |
| 370.75 | 0.487 | 74.15 | 0.89743408 | 296.6 | 0.41026368 |  |  |  |  |


| 371 | 0.487 | 74.20 | 0.89746890 | 296.8 | 0.41012442 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 371.25 | 0.488 | 74.25 | 0.89750370 | 297.0 | 0.40998520 |
| 371.5 | 0.488 | 74.30 | 0.89753849 | 297.2 | 0.40984602 |
| 371.75 | 0.488 | 74.35 | 0.89757328 | 297.4 | 0.40970689 |
| 372 | 0.488 | 74.40 | 0.89760805 | 297.6 | 0.40956780 |
| 372.25 | 0.488 | 74.45 | 0.89764281 | 297.8 | 0.40942876 |
| 372.5 | 0.488 | 74.50 | 0.89767756 | 298.0 | 0.40928976 |
| 372.75 | 0.489 | 74.55 | 0.89771230 | 298.2 | 0.40915081 |
| 373 | 0.489 | 74.60 | 0.89774703 | 298.4 | 0.40901189 |
| 373.25 | 0.489 | 74.65 | 0.89778174 | 298.6 | 0.40887303 |
| 373.5 | 0.489 | 74.70 | 0.89781645 | 298.8 | 0.40873420 |
| 373.75 | 0.489 | 74.75 | 0.89785114 | 299.0 | 0.40859542 |
| 374 | 0.489 | 74.80 | 0.89788583 | 299.2 | 0.40845668 |
| 374.25 | 0.490 | 74.85 | 0.89792050 | 299.4 | 0.40831799 |
| 374.5 | 0.490 | 74.90 | 0.89795517 | 299.6 | 0.40817934 |
| 374.75 | 0.490 | 74.95 | 0.89798982 | 299.8 | 0.40804073 |
| 375 | 0.490 | 75.00 | 0.89802446 | 300.0 | 0.40790217 |
| 375.25 | 0.490 | 75.05 | 0.89805909 | 300.2 | 0.40776365 |
| 375.5 | 0.490 | 75.10 | 0.89809371 | 300.4 | 0.40762517 |
| 375.75 | 0.491 | 75.15 | 0.89812831 | 300.6 | 0.40748674 |
| 376 | 0.491 | 75.20 | 0.89816291 | 300.8 | 0.40734835 |
| 376.25 | 0.491 | 75.25 | 0.89819750 | 301.0 | 0.40721001 |
| 376.5 | 0.491 | 75.30 | 0.89823207 | 301.2 | 0.40707170 |
| 376.75 | 0.491 | 75.35 | 0.89826664 | 301.4 | 0.40693344 |
| 377 | 0.492 | 75.40 | 0.89830119 | 301.6 | 0.40679523 |
| 377.25 | 0.492 | 75.45 | 0.89833574 | 301.8 | 0.40665705 |
| 377.5 | 0.492 | 75.50 | 0.89837027 | 302.0 | 0.40651892 |
| 377.75 | 0.492 | 75.55 | 0.89840479 | 302.2 | 0.40638083 |
| 378 | 0.492 | 75.60 | 0.89843930 | 302.4 | 0.40624279 |
| 378.25 | 0.492 | 75.65 | 0.89847380 | 302.6 | 0.40610479 |
| 378.5 | 0.493 | 75.70 | 0.89850829 | 302.8 | 0.40596683 |
| 378.75 | 0.493 | 75.75 | 0.89854277 | 303.0 | 0.40582891 |
| 379 | 0.493 | 75.80 | 0.89857724 | 303.2 | 0.40569104 |
| 379.25 | 0.493 | 75.85 | 0.89861170 | 303.4 | 0.40555321 |
| 379.5 | 0.493 | 75.90 | 0.89864615 | 303.6 | 0.40541542 |
| 379.75 | 0.493 | 75.95 | 0.89868058 | 303.8 | 0.40527767 |
| 380 | 0.494 | 76.00 | 0.89871501 | 304.0 | 0.40513997 |
| 380.25 | 0.494 | 76.05 | 0.89874942 | 304.2 | 0.40500231 |
| 380.5 | 0.494 | 76.10 | 0.89878383 | 304.4 | 0.40486469 |
| 380.75 | 0.494 | 76.15 | 0.89881822 | 304.6 | 0.40472712 |
| 381 | 0.494 | 76.20 | 0.89885260 | 304.8 | 0.40458959 |
| 381.25 | 0.494 | 76.25 | 0.89888698 | 305.0 | 0.40445210 |
| 381.5 | 0.495 | 76.30 | 0.89892134 | 305.2 | 0.40431465 |
| 381.75 | 0.495 | 76.35 | 0.89895569 | 305.4 | 0.40417724 |
| 382 | 0.495 | 76.40 | 0.89899003 | 305.6 | 0.40403988 |
| 382.25 | 0.495 | 76.45 | 0.89902436 | 305.8 | 0.40390256 |
| 382.5 | 0.495 | 76.50 | 0.89905868 | 306.0 | 0.40376528 |
| 382.75 | 0.495 | 76.55 | 0.89909299 | 306.2 | 0.40362804 |
| 383 | 0.496 | 76.60 | 0.89912729 | 306.4 | 0.40349085 |
| 383.25 | 0.496 | 76.65 | 0.89916158 | 306.6 | 0.40335370 |
| 383.5 | 0.496 | 76.70 | 0.89919585 | 306.8 | 0.40321658 |
| 383.75 | 0.496 | 76.75 | 0.89923012 | 307.0 | 0.40307952 |
| 384 | 0.496 | 76.80 | 0.89926438 | 307.2 | 0.40294249 |
| 384.25 | 0.496 | 76.85 | 0.89929862 | 307.4 | 0.40280551 |
| 384.5 | 0.497 | 76.90 | 0.89933286 | 307.6 | 0.40266856 |
| 384.75 | 0.497 | 76.95 | 0.89936708 | 307.8 | 0.40253166 |
| 385 | 0.497 | 77.00 | 0.89940130 | 308.0 | 0.40239480 |
| 385.25 | 0.497 | 77.05 | 0.89943550 | 308.2 | 0.40225799 |
| 385.5 | 0.497 | 77.10 | 0.89946970 | 308.4 | 0.40212121 |
| 385.75 | 0.498 | 77.15 | 0.89950388 | 308.6 | 0.40198448 |
| 386 | 0.498 | 77.20 | 0.89953805 | 308.8 | 0.40184778 |
| 386.25 | 0.498 | 77.25 | 0.89957222 | 309.0 | 0.40171113 |
| 386.5 | 0.498 | 77.30 | 0.89960637 | 309.2 | 0.40157452 |
| 386.75 | 0.498 | 77.35 | 0.89964051 | 309.4 | 0.40143796 |
| 387 | 0.498 | 77.40 | 0.89967464 | 309.6 | 0.40130143 |
| 387.25 | 0.499 | 77.45 | 0.89970876 | 309.8 | 0.40116495 |
| 387.5 | 0.499 | 77.50 | 0.89974287 | 310.0 | 0.40102850 |
| 387.75 | 0.499 | 77.55 | 0.89977697 | 310.2 | 0.40089210 |
| 388 | 0.499 | 77.60 | 0.89981106 | 310.4 | 0.40075574 |
| 388.25 | 0.499 | 77.65 | 0.89984514 | 310.6 | 0.40061942 |
| 388.5 | 0.499 | 77.70 | 0.89987921 | 310.8 | 0.40048314 |


| 388.75 | 0.500 | 77.75 | 0.89991327 | 311.0 | 0.40034691 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 389 | 0.500 | 77.80 | 0.89994732 | 311.2 | 0.40021071 |
| 389.25 | 0.500 | 77.85 | 0.89998136 | 311.4 | 0.40007456 |
| 389.5 | 0.500 | 77.90 | 0.90001539 | 311.6 | 0.39993844 |
| 389.75 | 0.500 | 77.95 | 0.90004941 | 311.8 | 0.39980237 |
| 390 | 0.500 | 78.00 | 0.90008342 | 312.0 | 0.39966634 |
| 390.25 | 0.501 | 78.05 | 0.90011741 | 312.2 | 0.39953035 |
| 390.5 | 0.501 | 78.10 | 0.90015140 | 312.4 | 0.39939440 |
| 390.75 | 0.501 | 78.15 | 0.90018538 | 312.6 | 0.39925849 |
| 391 | 0.501 | 78.20 | 0.90021934 | 312.8 | 0.39912262 |
| 391.25 | 0.501 | 78.25 | 0.90025330 | 313.0 | 0.39898680 |
| 391.5 | 0.501 | 78.30 | 0.90028725 | 313.2 | 0.39885101 |
| 391.75 | 0.502 | 78.35 | 0.90032118 | 313.4 | 0.39871527 |
| 392 | 0.502 | 78.40 | 0.90035511 | 313.6 | 0.39857956 |
| 392.25 | 0.502 | 78.45 | 0.90038903 | 313.8 | 0.39844390 |
| 392.5 | 0.502 | 78.50 | 0.90042293 | 314.0 | 0.39830827 |
| 392.75 | 0.502 | 78.55 | 0.90045683 | 314.2 | 0.39817269 |
| 393 | 0.502 | 78.60 | 0.90049071 | 314.4 | 0.39803715 |
| 393.25 | 0.503 | 78.65 | 0.90052459 | 314.6 | 0.39790165 |
| 393.5 | 0.503 | 78.70 | 0.90055845 | 314.8 | 0.39776619 |
| 393.75 | 0.503 | 78.75 | 0.90059231 | 315.0 | 0.39763077 |
| 394 | 0.503 | 78.80 | 0.90062615 | 315.2 | 0.39749539 |
| 394.25 | 0.503 | 78.85 | 0.90065999 | 315.4 | 0.39736005 |
| 394.5 | 0.503 | 78.90 | 0.90069381 | 315.6 | 0.39722475 |
| 394.75 | 0.504 | 78.95 | 0.90072763 | 315.8 | 0.39708949 |
| 395 | 0.504 | 79.00 | 0.90076143 | 316.0 | 0.39695427 |
| 395.25 | 0.504 | 79.05 | 0.90079523 | 316.2 | 0.39681909 |
| 395.5 | 0.504 | 79.10 | 0.90082901 | 316.4 | 0.39668395 |
| 395.75 | 0.504 | 79.15 | 0.90086279 | 316.6 | 0.39654885 |
| 396 | 0.504 | 79.20 | 0.90089655 | 316.8 | 0.39641379 |
| 396.25 | 0.505 | 79.25 | 0.90093031 | 317.0 | 0.39627878 |
| 396.5 | 0.505 | 79.30 | 0.90096405 | 317.2 | 0.39614380 |
| 396.75 | 0.505 | 79.35 | 0.90099779 | 317.4 | 0.39600886 |
| 397 | 0.505 | 79.40 | 0.90103151 | 317.6 | 0.39587396 |
| 397.25 | 0.505 | 79.45 | 0.90106522 | 317.8 | 0.39573910 |
| 397.5 | 0.505 | 79.50 | 0.90109893 | 318.0 | 0.39560428 |
| 397.75 | 0.506 | 79.55 | 0.90113262 | 318.2 | 0.39546950 |
| 398 | 0.506 | 79.60 | 0.90116631 | 318.4 | 0.39533477 |
| 398.25 | 0.506 | 79.65 | 0.90119998 | 318.6 | 0.39520007 |
| 398.5 | 0.506 | 79.70 | 0.90123365 | 318.8 | 0.39506541 |
| 398.75 | 0.506 | 79.75 | 0.90126730 | 319.0 | 0.39493079 |
| 399 | 0.507 | 79.80 | 0.90130095 | 319.2 | 0.39479621 |
| 399.25 | 0.507 | 79.85 | 0.90133458 | 319.4 | 0.39466167 |
| 399.5 | 0.507 | 79.90 | 0.90136821 | 319.6 | 0.39452717 |
| 399.75 | 0.507 | 79.95 | 0.90140182 | 319.8 | 0.39439271 |
| 400 | 0.507 | 80.00 | 0.90143543 | 320.0 | 0.39425828 |
| 400.25 | 0.507 | 80.05 | 0.90146902 | 320.2 | 0.39412390 |
| 400.5 | 0.508 | 80.10 | 0.90150261 | 320.4 | 0.39398956 |
| 400.75 | 0.508 | 80.15 | 0.90153619 | 320.6 | 0.39385526 |
| 401 | 0.508 | 80.20 | 0.90156975 | 320.8 | 0.39372099 |
| 401.25 | 0.508 | 80.25 | 0.90160331 | 321.0 | 0.39358677 |
| 401.5 | 0.508 | 80.30 | 0.90163685 | 321.2 | 0.39345258 |
| 401.75 | 0.508 | 80.35 | 0.90167039 | 321.4 | 0.39331844 |
| 402 | 0.509 | 80.40 | 0.90170392 | 321.6 | 0.39318433 |
| 402.25 | 0.509 | 80.45 | 0.90173743 | 321.8 | 0.39305026 |
| 402.5 | 0.509 | 80.50 | 0.90177094 | 322.0 | 0.39291623 |
| 402.75 | 0.509 | 80.55 | 0.90180444 | 322.2 | 0.39278224 |
| 403 | 0.509 | 80.60 | 0.90183793 | 322.4 | 0.39264829 |
| 403.25 | 0.509 | 80.65 | 0.90187140 | 322.6 | 0.39251438 |
| 403.5 | 0.510 | 80.70 | 0.90190487 | 322.8 | 0.39238051 |
| 403.75 | 0.510 | 80.75 | 0.90193833 | 323.0 | 0.39224668 |
| 404 | 0.510 | 80.80 | 0.90197178 | 323.2 | 0.39211288 |
| 404.25 | 0.510 | 80.85 | 0.90200522 | 323.4 | 0.39197913 |
| 404.5 | 0.510 | 80.90 | 0.90203865 | 323.6 | 0.39184541 |
| 404.75 | 0.510 | 80.95 | 0.90207207 | 323.8 | 0.39171173 |
| 405 | 0.511 | 81.00 | 0.90210548 | 324.0 | 0.39157809 |
| 405.25 | 0.511 | 81.05 | 0.90213888 | 324.2 | 0.39144449 |
| 405.5 | 0.511 | 81.10 | 0.90217227 | 324.4 | 0.39131093 |
| 405.75 | 0.511 | 81.15 | 0.90220565 | 324.6 | 0.39117741 |
| 406 | 0.511 | 81.20 | 0.90223902 | 324.8 | 0.39104392 |
| 406.25 | 0.511 | 81.25 | 0.90227238 | 325.0 | 0.39091048 |


| 406.5 | 0.512 | 81.30 | 0.90230573 | 325.2 | 0.39077707 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 406.75 | 0.512 | 81.35 | 0.90233907 | 325.4 | 0.39064370 |
| 407 | 0.512 | 81.40 | 0.90237241 | 325.6 | 0.39051037 |
| 407.25 | 0.512 | 81.45 | 0.90240573 | 325.8 | 0.39037708 |
| 407.5 | 0.512 | 81.50 | 0.90243904 | 326.0 | 0.39024383 |
| 407.75 | 0.512 | 81.55 | 0.90247235 | 326.2 | 0.39011062 |
| 408 | 0.513 | 81.60 | 0.90250564 | 326.4 | 0.38997744 |
| 408.25 | 0.513 | 81.65 | 0.90253892 | 326.6 | 0.38984430 |
| 408.5 | 0.513 | 81.70 | 0.90257220 | 326.8 | 0.38971120 |
| 408.75 | 0.513 | 81.75 | 0.90260546 | 327.0 | 0.38957814 |
| 409 | 0.513 | 81.80 | 0.90263872 | 327.2 | 0.38944512 |
| 409.25 | 0.513 | 81.85 | 0.90267197 | 327.4 | 0.38931213 |
| 409.5 | 0.514 | 81.90 | 0.90270520 | 327.6 | 0.38917919 |
| 409.75 | 0.514 | 81.95 | 0.90273843 | 327.8 | 0.38904628 |
| 410 | 0.514 | 82.00 | 0.90277165 | 328.0 | 0.38891341 |
| 410.25 | 0.514 | 82.05 | 0.90280486 | 328.2 | 0.38878058 |
| 410.5 | 0.514 | 82.10 | 0.90283805 | 328.4 | 0.38864778 |
| 410.75 | 0.514 | 82.15 | 0.90287124 | 328.6 | 0.38851503 |
| 411 | 0.515 | 82.20 | 0.90290442 | 328.8 | 0.38838231 |
| 411.25 | 0.515 | 82.25 | 0.90293759 | 329.0 | 0.38824963 |
| 411.5 | 0.515 | 82.30 | 0.90297075 | 329.2 | 0.38811699 |
| 411.75 | 0.515 | 82.35 | 0.90300390 | 329.4 | 0.38798438 |
| 412 | 0.515 | 82.40 | 0.90303705 | 329.6 | 0.38785182 |
| 412.25 | 0.515 | 82.45 | 0.90307018 | 329.8 | 0.38771929 |
| 412.5 | 0.516 | 82.50 | 0.90310330 | 330.0 | 0.38758680 |
| 412.75 | 0.516 | 82.55 | 0.90313641 | 330.2 | 0.38745434 |
| 413 | 0.516 | 82.60 | 0.90316952 | 330.4 | 0.38732193 |
| 413.25 | 0.516 | 82.65 | 0.90320261 | 330.6 | 0.38718955 |
| 413.5 | 0.516 | 82.70 | 0.90323570 | 330.8 | 0.38705721 |
| 413.75 | 0.516 | 82.75 | 0.90326877 | 331.0 | 0.38692491 |
| 414 | 0.517 | 82.80 | 0.90330184 | 331.2 | 0.38679264 |
| 414.25 | 0.517 | 82.85 | 0.90333490 | 331.4 | 0.38666041 |
| 414.5 | 0.517 | 82.90 | 0.90336794 | 331.6 | 0.38652822 |
| 414.75 | 0.517 | 82.95 | 0.90340098 | 331.8 | 0.38639607 |
| 415 | 0.517 | 83.00 | 0.90343401 | 332.0 | 0.38626396 |
| 415.25 | 0.517 | 83.05 | 0.90346703 | 332.2 | 0.38613188 |
| 415.5 | 0.518 | 83.10 | 0.90350004 | 332.4 | 0.38599984 |
| 415.75 | 0.518 | 83.15 | 0.90353304 | 332.6 | 0.38586783 |
| 416 | 0.518 | 83.20 | 0.90356603 | 332.8 | 0.38573587 |
| 416.25 | 0.518 | 83.25 | 0.90359901 | 333.0 | 0.38560394 |
| 416.5 | 0.518 | 83.30 | 0.90363199 | 333.2 | 0.38547205 |
| 416.75 | 0.518 | 83.35 | 0.90366495 | 333.4 | 0.38534020 |
| 417 | 0.518 | 83.40 | 0.90369791 | 333.6 | 0.38520838 |
| 417.25 | 0.519 | 83.45 | 0.90373085 | 333.8 | 0.38507660 |
| 417.5 | 0.519 | 83.50 | 0.90376379 | 334.0 | 0.38494486 |
| 417.75 | 0.519 | 83.55 | 0.90379671 | 334.2 | 0.38481315 |
| 418 | 0.519 | 83.60 | 0.90382963 | 334.4 | 0.38468148 |
| 418.25 | 0.519 | 83.65 | 0.90386254 | 334.6 | 0.38454985 |
| 418.5 | 0.519 | 83.70 | 0.90389544 | 334.8 | 0.38441826 |
| 418.75 | 0.520 | 83.75 | 0.90392833 | 335.0 | 0.38428670 |
| 419 | 0.520 | 83.80 | 0.90396121 | 335.2 | 0.38415518 |
| 419.25 | 0.520 | 83.85 | 0.90399408 | 335.4 | 0.38402369 |
| 419.5 | 0.520 | 83.90 | 0.90402694 | 335.6 | 0.38389225 |
| 419.75 | 0.520 | 83.95 | 0.90405979 | 335.8 | 0.38376084 |
| 420 | 0.520 | 84.00 | 0.90409263 | 336.0 | 0.38362946 |
| 420.25 | 0.521 | 84.05 | 0.90412547 | 336.2 | 0.38349813 |
| 420.5 | 0.521 | 84.10 | 0.90415829 | 336.4 | 0.38336683 |
| 420.75 | 0.521 | 84.15 | 0.90419111 | 336.6 | 0.38323556 |
| 421 | 0.521 | 84.20 | 0.90422392 | 336.8 | 0.38310434 |
| 421.25 | 0.521 | 84.25 | 0.90425671 | 337.0 | 0.38297315 |
| 421.5 | 0.521 | 84.30 | 0.90428950 | 337.2 | 0.38284199 |
| 421.75 | 0.522 | 84.35 | 0.90432228 | 337.4 | 0.38271088 |
| 422 | 0.522 | 84.40 | 0.90435505 | 337.6 | 0.38257980 |
| 422.25 | 0.522 | 84.45 | 0.90438781 | 337.8 | 0.38244875 |
| 422.5 | 0.522 | 84.50 | 0.90442056 | 338.0 | 0.38231775 |
| 422.75 | 0.522 | 84.55 | 0.90445331 | 338.2 | 0.38218677 |
| 423 | 0.522 | 84.60 | 0.90448604 | 338.4 | 0.38205584 |
| 423.25 | 0.523 | 84.65 | 0.90451876 | 338.6 | 0.38192494 |
| 423.5 | 0.523 | 84.70 | 0.90455148 | 338.8 | 0.38179408 |
| 423.75 | 0.523 | 84.75 | 0.90458419 | 339.0 | 0.38166325 |
| 424 | 0.523 | 84.80 | 0.90461688 | 339.2 | 0.38153247 |


| 424.25 | 0.523 | 84.85 | 0.90464957 | 339.4 | 0.38140171 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 424.5 | 0.523 | 84.90 | 0.90468225 | 339.6 | 0.38127100 |
| 424.75 | 0.524 | 84.95 | 0.90471492 | 339.8 | 0.38114032 |
| 425 | 0.524 | 85.00 | 0.90474758 | 340.0 | 0.38100967 |
| 425.25 | 0.524 | 85.05 | 0.90478023 | 340.2 | 0.38087906 |
| 425.5 | 0.524 | 85.10 | 0.90481288 | 340.4 | 0.38074849 |
| 425.75 | 0.524 | 85.15 | 0.90484551 | 340.6 | 0.38061795 |
| 426 | 0.524 | 85.20 | 0.90487814 | 340.8 | 0.38048745 |
| 426.25 | 0.525 | 85.25 | 0.90491075 | 341.0 | 0.38035699 |
| 426.5 | 0.525 | 85.30 | 0.90494336 | 341.2 | 0.38022656 |
| 426.75 | 0.525 | 85.35 | 0.90497596 | 341.4 | 0.38009617 |
| 427 | 0.525 | 85.40 | 0.90500855 | 341.6 | 0.37996581 |
| 427.25 | 0.525 | 85.45 | 0.90504113 | 341.8 | 0.37983549 |
| 427.5 | 0.525 | 85.50 | 0.90507370 | 342.0 | 0.37970521 |
| 427.75 | 0.526 | 85.55 | 0.90510626 | 342.2 | 0.37957496 |
| 428 | 0.526 | 85.60 | 0.90513881 | 342.4 | 0.37944475 |
| 428.25 | 0.526 | 85.65 | 0.90517136 | 342.6 | 0.37931457 |
| 428.5 | 0.526 | 85.70 | 0.90520389 | 342.8 | 0.37918443 |
| 428.75 | 0.526 | 85.75 | 0.90523642 | 343.0 | 0.37905432 |
| 429 | 0.526 | 85.80 | 0.90526894 | 343.2 | 0.37892425 |
| 429.25 | 0.527 | 85.85 | 0.90530145 | 343.4 | 0.37879422 |
| 429.5 | 0.527 | 85.90 | 0.90533395 | 343.6 | 0.37866422 |
| 429.75 | 0.527 | 85.95 | 0.90536644 | 343.8 | 0.37853425 |
| 430 | 0.527 | 86.00 | 0.90539892 | 344.0 | 0.37840432 |
| 430.25 | 0.527 | 86.05 | 0.90543139 | 344.2 | 0.37827443 |
| 430.5 | 0.527 | 86.10 | 0.90546386 | 344.4 | 0.37814457 |
| 430.75 | 0.527 | 86.15 | 0.90549631 | 344.6 | 0.37801475 |
| 431 | 0.528 | 86.20 | 0.90552876 | 344.8 | 0.37788497 |
| 431.25 | 0.528 | 86.25 | 0.90556120 | 345.0 | 0.37775522 |
| 431.5 | 0.528 | 86.30 | 0.90559362 | 345.2 | 0.37762550 |
| 431.75 | 0.528 | 86.35 | 0.90562604 | 345.4 | 0.37749582 |
| 432 | 0.528 | 86.40 | 0.90565846 | 345.6 | 0.37736618 |
| 432.25 | 0.528 | 86.45 | 0.90569086 | 345.8 | 0.37723657 |
| 432.5 | 0.529 | 86.50 | 0.90572325 | 346.0 | 0.37710699 |
| 432.75 | 0.529 | 86.55 | 0.90575564 | 346.2 | 0.37697745 |
| 433 | 0.529 | 86.60 | 0.90578801 | 346.4 | 0.37684795 |
| 433.25 | 0.529 | 86.65 | 0.90582038 | 346.6 | 0.37671848 |
| 433.5 | 0.529 | 86.70 | 0.90585274 | 346.8 | 0.37658905 |
| 433.75 | 0.529 | 86.75 | 0.90588509 | 347.0 | 0.37645965 |
| 434 | 0.530 | 86.80 | 0.90591743 | 347.2 | 0.37633028 |
| 434.25 | 0.530 | 86.85 | 0.90594976 | 347.4 | 0.37620095 |
| 434.5 | 0.530 | 86.90 | 0.90598208 | 347.6 | 0.37607166 |
| 434.75 | 0.530 | 86.95 | 0.90601440 | 347.8 | 0.37594240 |
| 435 | 0.530 | 87.00 | 0.90604671 | 348.0 | 0.37581318 |
| 435.25 | 0.530 | 87.05 | 0.90607900 | 348.2 | 0.37568399 |
| 435.5 | 0.531 | 87.10 | 0.90611129 | 348.4 | 0.37555484 |
| 435.75 | 0.531 | 87.15 | 0.90614357 | 348.6 | 0.37542572 |
| 436 | 0.531 | 87.20 | 0.90617584 | 348.8 | 0.37529663 |
| 436.25 | 0.531 | 87.25 | 0.90620810 | 349.0 | 0.37516758 |
| 436.5 | 0.531 | 87.30 | 0.90624036 | 349.2 | 0.37503857 |
| 436.75 | 0.531 | 87.35 | 0.90627260 | 349.4 | 0.37490959 |
| 437 | 0.532 | 87.40 | 0.90630484 | 349.6 | 0.37478064 |
| 437.25 | 0.532 | 87.45 | 0.90633707 | 349.8 | 0.37465173 |
| 437.5 | 0.532 | 87.50 | 0.90636929 | 350.0 | 0.37452285 |
| 437.75 | 0.532 | 87.55 | 0.90640150 | 350.2 | 0.37439401 |
| 438 | 0.532 | 87.60 | 0.90643370 | 350.4 | 0.37426521 |
| 438.25 | 0.532 | 87.65 | 0.90646589 | 350.6 | 0.37413643 |
| 438.5 | 0.532 | 87.70 | 0.90649808 | 350.8 | 0.37400770 |
| 438.75 | 0.533 | 87.75 | 0.90653025 | 351.0 | 0.37387899 |
| 439 | 0.533 | 87.80 | 0.90656242 | 351.2 | 0.37375032 |
| 439.25 | 0.533 | 87.85 | 0.90659458 | 351.4 | 0.37362169 |
| 439.5 | 0.533 | 87.90 | 0.90662673 | 351.6 | 0.37349309 |
| 439.75 | 0.533 | 87.95 | 0.90665887 | 351.8 | 0.37336452 |
| 440 | 0.533 | 88.00 | 0.90669100 | 352.0 | 0.37323599 |
| 440.25 | 0.534 | 88.05 | 0.90672313 | 352.2 | 0.37310750 |
| 440.5 | 0.534 | 88.10 | 0.90675524 | 352.4 | 0.37297903 |
| 440.75 | 0.534 | 88.15 | 0.90678735 | 352.6 | 0.37285060 |
| 441 | 0.534 | 88.20 | 0.90681945 | 352.8 | 0.37272221 |
| 441.25 | 0.534 | 88.25 | 0.90685154 | 353.0 | 0.37259385 |
| 441.5 | 0.534 | 88.30 | 0.90688362 | 353.2 | 0.37246552 |
| 441.75 | 0.535 | 88.35 | 0.90691569 | 353.4 | 0.37233723 |


| 442 | 0.535 | 88.40 | 0.90694776 | 353.6 | 0.37220897 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 442.25 | 0.535 | 88.45 | 0.90697981 | 353.8 | 0.37208075 |
| 442.5 | 0.535 | 88.50 | 0.90701186 | 354.0 | 0.37195256 |
| 442.75 | 0.535 | 88.55 | 0.90704390 | 354.2 | 0.37182441 |
| 443 | 0.535 | 88.60 | 0.90707593 | 354.4 | 0.37169629 |
| 443.25 | 0.536 | 88.65 | 0.90710795 | 354.6 | 0.37156820 |
| 443.5 | 0.536 | 88.70 | 0.90713996 | 354.8 | 0.37144014 |
| 443.75 | 0.536 | 88.75 | 0.90717197 | 355.0 | 0.37131212 |
| 444 | 0.536 | 88.80 | 0.90720397 | 355.2 | 0.37118414 |
| 444.25 | 0.536 | 88.85 | 0.90723595 | 355.4 | 0.37105619 |
| 444.5 | 0.536 | 88.90 | 0.90726793 | 355.6 | 0.37092827 |
| 444.75 | 0.536 | 88.95 | 0.90729990 | 355.8 | 0.37080039 |
| 445 | 0.537 | 89.00 | 0.90733187 | 356.0 | 0.37067254 |
| 445.25 | 0.537 | 89.05 | 0.90736382 | 356.2 | 0.37054472 |
| 445.5 | 0.537 | 89.10 | 0.90739577 | 356.4 | 0.37041694 |
| 445.75 | 0.537 | 89.15 | 0.90742770 | 356.6 | 0.37028919 |
| 446 | 0.537 | 89.20 | 0.90745963 | 356.8 | 0.37016147 |
| 446.25 | 0.537 | 89.25 | 0.90749155 | 357.0 | 0.37003379 |
| 446.5 | 0.538 | 89.30 | 0.90752346 | 357.2 | 0.36990614 |
| 446.75 | 0.538 | 89.35 | 0.90755537 | 357.4 | 0.36977853 |
| 447 | 0.538 | 89.40 | 0.90758726 | 357.6 | 0.36965095 |
| 447.25 | 0.538 | 89.45 | 0.90761915 | 357.8 | 0.36952340 |
| 447.5 | 0.538 | 89.50 | 0.90765103 | 358.0 | 0.36939588 |
| 447.75 | 0.538 | 89.55 | 0.90768290 | 358.2 | 0.36926840 |
| 448 | 0.539 | 89.60 | 0.90771476 | 358.4 | 0.36914096 |
| 448.25 | 0.539 | 89.65 | 0.90774661 | 358.6 | 0.36901354 |
| 448.5 | 0.539 | 89.70 | 0.90777846 | 358.8 | 0.36888616 |
| 448.75 | 0.539 | 89.75 | 0.90781030 | 359.0 | 0.36875881 |
| 449 | 0.539 | 89.80 | 0.90784212 | 359.2 | 0.36863150 |
| 449.25 | 0.539 | 89.85 | 0.90787394 | 359.4 | 0.36850422 |
| 449.5 | 0.540 | 89.90 | 0.90790576 | 359.6 | 0.36837697 |
| 449.75 | 0.540 | 89.95 | 0.90793756 | 359.8 | 0.36824976 |
| 450 | 0.540 | 90.00 | 0.90796936 | 360.0 | 0.36812258 |
| 450.25 | 0.540 | 90.05 | 0.90800114 | 360.2 | 0.36799543 |
| 450.5 | 0.540 | 90.10 | 0.90803292 | 360.4 | 0.36786832 |
| 450.75 | 0.540 | 90.15 | 0.90806469 | 360.6 | 0.36774124 |
| 451 | 0.540 | 90.20 | 0.90809645 | 360.8 | 0.36761419 |
| 451.25 | 0.541 | 90.25 | 0.90812821 | 361.0 | 0.36748717 |
| 451.5 | 0.541 | 90.30 | 0.90815995 | 361.2 | 0.36736019 |
| 451.75 | 0.541 | 90.35 | 0.90819169 | 361.4 | 0.36723324 |
| 452 | 0.541 | 90.40 | 0.90822342 | 361.6 | 0.36710633 |
| 452.25 | 0.541 | 90.45 | 0.90825514 | 361.8 | 0.36697945 |
| 452.5 | 0.541 | 90.50 | 0.90828685 | 362.0 | 0.36685260 |
| 452.75 | 0.542 | 90.55 | 0.90831856 | 362.2 | 0.36672578 |
| 453 | 0.542 | 90.60 | 0.90835025 | 362.4 | 0.36659900 |
| 453.25 | 0.542 | 90.65 | 0.90838194 | 362.6 | 0.36647224 |
| 453.5 | 0.542 | 90.70 | 0.90841362 | 362.8 | 0.36634553 |
| 453.75 | 0.542 | 90.75 | 0.90844529 | 363.0 | 0.36621884 |
| 454 | 0.542 | 90.80 | 0.90847695 | 363.2 | 0.36609219 |
| 454.25 | 0.543 | 90.85 | 0.90850861 | 363.4 | 0.36596557 |
| 454.5 | 0.543 | 90.90 | 0.90854025 | 363.6 | 0.36583898 |
| 454.75 | 0.543 | 90.95 | 0.90857189 | 363.8 | 0.36571243 |
| 455 | 0.543 | 91.00 | 0.90860352 | 364.0 | 0.36558591 |
| 455.25 | 0.543 | 91.05 | 0.90863515 | 364.2 | 0.36545942 |
| 455.5 | 0.543 | 91.10 | 0.90866676 | 364.4 | 0.36533296 |
| 455.75 | 0.543 | 91.15 | 0.90869837 | 364.6 | 0.36520654 |
| 456 | 0.544 | 91.20 | 0.90872996 | 364.8 | 0.36508015 |
| 456.25 | 0.544 | 91.25 | 0.90876155 | 365.0 | 0.36495379 |
| 456.5 | 0.544 | 91.30 | 0.90879313 | 365.2 | 0.36482746 |
| 456.75 | 0.544 | 91.35 | 0.90882471 | 365.4 | 0.36470117 |
| 457 | 0.544 | 91.40 | 0.90885627 | 365.6 | 0.36457491 |
| 457.25 | 0.544 | 91.45 | 0.90888783 | 365.8 | 0.36444868 |
| 457.5 | 0.545 | 91.50 | 0.90891938 | 366.0 | 0.36432248 |
| 457.75 | 0.545 | 91.55 | 0.90895092 | 366.2 | 0.36419632 |
| 458 | 0.545 | 91.60 | 0.90898245 | 366.4 | 0.36407019 |
| 458.25 | 0.545 | 91.65 | 0.90901398 | 366.6 | 0.36394409 |
| 458.5 | 0.545 | 91.70 | 0.90904549 | 366.8 | 0.36381802 |
| 458.75 | 0.545 | 91.75 | 0.90907700 | 367.0 | 0.36369199 |
| 459 | 0.546 | 91.80 | 0.90910850 | 367.2 | 0.36356599 |
| 459.25 | 0.546 | 91.85 | 0.90914000 | 367.4 | 0.36344002 |
| 459.5 | 0.546 | 91.90 | 0.90917148 | 367.6 | 0.36331408 |


| 459.75 | 0.546 | 91.95 | 0.90920296 | 367.8 | 0.36318817 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 460 | 0.546 | 92.00 | 0.90923442 | 368.0 | 0.36306230 |
| 460.25 | 0.546 | 92.05 | 0.90926588 | 368.2 | 0.36293646 |
| 460.5 | 0.546 | 92.10 | 0.90929734 | 368.4 | 0.36281065 |
| 460.75 | 0.547 | 92.15 | 0.90932878 | 368.6 | 0.36268487 |
| 461 | 0.547 | 92.20 | 0.90936022 | 368.8 | 0.36255913 |
| 461.25 | 0.547 | 92.25 | 0.90939165 | 369.0 | 0.36243342 |
| 461.5 | 0.547 | 92.30 | 0.90942307 | 369.2 | 0.36230774 |
| 461.75 | 0.547 | 92.35 | 0.90945448 | 369.4 | 0.36218209 |
| 462 | 0.547 | 92.40 | 0.90948588 | 369.6 | 0.36205647 |
| 462.25 | 0.548 | 92.45 | 0.90951728 | 369.8 | 0.36193089 |
| 462.5 | 0.548 | 92.50 | 0.90954867 | 370.0 | 0.36180533 |
| 462.75 | 0.548 | 92.55 | 0.90958005 | 370.2 | 0.36167981 |
| 463 | 0.548 | 92.60 | 0.90961142 | 370.4 | 0.36155432 |
| 463.25 | 0.548 | 92.65 | 0.90964278 | 370.6 | 0.36142887 |
| 463.5 | 0.548 | 92.70 | 0.90967414 | 370.8 | 0.36130344 |
| 463.75 | 0.549 | 92.75 | 0.90970549 | 371.0 | 0.36117805 |
| 464 | 0.549 | 92.80 | 0.90973683 | 371.2 | 0.36105269 |
| 464.25 | 0.549 | 92.85 | 0.90976816 | 371.4 | 0.36092736 |
| 464.5 | 0.549 | 92.90 | 0.90979949 | 371.6 | 0.36080206 |
| 464.75 | 0.549 | 92.95 | 0.90983080 | 371.8 | 0.36067679 |
| 465 | 0.549 | 93.00 | 0.90986211 | 372.0 | 0.36055156 |
| 465.25 | 0.549 | 93.05 | 0.90989341 | 372.2 | 0.36042635 |
| 465.5 | 0.550 | 93.10 | 0.90992470 | 372.4 | 0.36030118 |
| 465.75 | 0.550 | 93.15 | 0.90995599 | 372.6 | 0.36017604 |
| 466 | 0.550 | 93.20 | 0.90998727 | 372.8 | 0.36005093 |
| 466.25 | 0.550 | 93.25 | 0.91001854 | 373.0 | 0.35992585 |
| 466.5 | 0.550 | 93.30 | 0.91004980 | 373.2 | 0.35980081 |
| 466.75 | 0.550 | 93.35 | 0.91008105 | 373.4 | 0.35967580 |
| 467 | 0.551 | 93.40 | 0.91011230 | 373.6 | 0.35955081 |
| 467.25 | 0.551 | 93.45 | 0.91014353 | 373.8 | 0.35942586 |
| 467.5 | 0.551 | 93.50 | 0.91017476 | 374.0 | 0.35930094 |
| 467.75 | 0.551 | 93.55 | 0.91020599 | 374.2 | 0.35917605 |
| 468 | 0.551 | 93.60 | 0.91023720 | 374.4 | 0.35905120 |
| 468.25 | 0.551 | 93.65 | 0.91026841 | 374.6 | 0.35892637 |
| 468.5 | 0.551 | 93.70 | 0.91029961 | 374.8 | 0.35880158 |
| 468.75 | 0.552 | 93.75 | 0.91033080 | 375.0 | 0.35867681 |
| 469 | 0.552 | 93.80 | 0.91036198 | 375.2 | 0.35855208 |
| 469.25 | 0.552 | 93.85 | 0.91039315 | 375.4 | 0.35842738 |
| 469.5 | 0.552 | 93.90 | 0.91042432 | 375.6 | 0.35830271 |
| 469.75 | 0.552 | 93.95 | 0.91045548 | 375.8 | 0.35817807 |
| 470 | 0.552 | 94.00 | 0.91048663 | 376.0 | 0.35805347 |
| 470.25 | 0.553 | 94.05 | 0.91051778 | 376.2 | 0.35792889 |
| 470.5 | 0.553 | 94.10 | 0.91054891 | 376.4 | 0.35780435 |
| 470.75 | 0.553 | 94.15 | 0.91058004 | 376.6 | 0.35767983 |
| 471 | 0.553 | 94.20 | 0.91061116 | 376.8 | 0.35755535 |
| 471.25 | 0.553 | 94.25 | 0.91064228 | 377.0 | 0.35743090 |
| 471.5 | 0.553 | 94.30 | 0.91067338 | 377.2 | 0.35730648 |
| 471.75 | 0.554 | 94.35 | 0.91070448 | 377.4 | 0.35718209 |
| 472 | 0.554 | 94.40 | 0.91073557 | 377.6 | 0.35705773 |
| 472.25 | 0.554 | 94.45 | 0.91076665 | 377.8 | 0.35693340 |
| 472.5 | 0.554 | 94.50 | 0.91079772 | 378.0 | 0.35680911 |
| 472.75 | 0.554 | 94.55 | 0.91082879 | 378.2 | 0.35668484 |
| 473 | 0.554 | 94.60 | 0.91085985 | 378.4 | 0.35656061 |
| 473.25 | 0.554 | 94.65 | 0.91089090 | 378.6 | 0.35643640 |
| 473.5 | 0.555 | 94.70 | 0.91092194 | 378.8 | 0.35631223 |
| 473.75 | 0.555 | 94.75 | 0.91095298 | 379.0 | 0.35618809 |
| 474 | 0.555 | 94.80 | 0.91098401 | 379.2 | 0.35606398 |
| 474.25 | 0.555 | 94.85 | 0.91101503 | 379.4 | 0.35593990 |
| 474.5 | 0.555 | 94.90 | 0.91104604 | 379.6 | 0.35581585 |
| 474.75 | 0.555 | 94.95 | 0.91107704 | 379.8 | 0.35569183 |
| 475 | 0.556 | 95.00 | 0.91110804 | 380.0 | 0.35556784 |
| 475.25 | 0.556 | 95.05 | 0.91113903 | 380.2 | 0.35544388 |
| 475.5 | 0.556 | 95.10 | 0.91117001 | 380.4 | 0.35531995 |
| 475.75 | 0.556 | 95.15 | 0.91120099 | 380.6 | 0.35519606 |
| 476 | 0.556 | 95.20 | 0.91123195 | 380.8 | 0.35507219 |
| 476.25 | 0.556 | 95.25 | 0.91126291 | 381.0 | 0.35494836 |
| 476.5 | 0.556 | 95.30 | 0.91129386 | 381.2 | 0.35482455 |
| 476.75 | 0.557 | 95.35 | 0.91132481 | 381.4 | 0.35470078 |
| 477 | 0.557 | 95.40 | 0.91135574 | 381.6 | 0.35457703 |
| 477.25 | 0.557 | 95.45 | 0.91138667 | 381.8 | 0.35445332 |


| 477.5 | 0.557 | 95.50 | 0.91141759 | 382.0 | 0.35432964 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 477.75 | 0.557 | 95.55 | 0.91144850 | 382.2 | 0.35420598 |
| 478 | 0.557 | 95.60 | 0.91147941 | 382.4 | 0.35408236 |
| 478.25 | 0.558 | 95.65 | 0.91151031 | 382.6 | 0.35395877 |
| 478.5 | 0.558 | 95.70 | 0.91154120 | 382.8 | 0.35383521 |
| 478.75 | 0.558 | 95.75 | 0.91157208 | 383.0 | 0.35371168 |
| 479 | 0.558 | 95.80 | 0.91160296 | 383.2 | 0.35358818 |
| 479.25 | 0.558 | 95.85 | 0.91163382 | 383.4 | 0.35346471 |
| 479.5 | 0.558 | 95.90 | 0.91166468 | 383.6 | 0.35334127 |
| 479.75 | 0.558 | 95.95 | 0.91169554 | 383.8 | 0.35321786 |
| 480 | 0.559 | 96.00 | 0.91172638 | 384.0 | 0.35309448 |
| 480.25 | 0.559 | 96.05 | 0.91175722 | 384.2 | 0.35297113 |
| 480.5 | 0.559 | 96.10 | 0.91178805 | 384.4 | 0.35284781 |
| 480.75 | 0.559 | 96.15 | 0.91181887 | 384.6 | 0.35272452 |
| 481 | 0.559 | 96.20 | 0.91184968 | 384.8 | 0.35260126 |
| 481.25 | 0.559 | 96.25 | 0.91188049 | 385.0 | 0.35247803 |
| 481.5 | 0.560 | 96.30 | 0.91191129 | 385.2 | 0.35235483 |
| 481.75 | 0.560 | 96.35 | 0.91194208 | 385.4 | 0.35223166 |
| 482 | 0.560 | 96.40 | 0.91197287 | 385.6 | 0.35210852 |
| 482.25 | 0.560 | 96.45 | 0.91200365 | 385.8 | 0.35198542 |
| 482.5 | 0.560 | 96.50 | 0.91203442 | 386.0 | 0.35186234 |
| 482.75 | 0.560 | 96.55 | 0.91206518 | 386.2 | 0.35173929 |
| 483 | 0.560 | 96.60 | 0.91209593 | 386.4 | 0.35161627 |
| 483.25 | 0.561 | 96.65 | 0.91212668 | 386.6 | 0.35149328 |
| 483.5 | 0.561 | 96.70 | 0.91215742 | 386.8 | 0.35137032 |
| 483.75 | 0.561 | 96.75 | 0.91218815 | 387.0 | 0.35124739 |
| 484 | 0.561 | 96.80 | 0.91221888 | 387.2 | 0.35112449 |
| 484.25 | 0.561 | 96.85 | 0.91224959 | 387.4 | 0.35100162 |
| 484.5 | 0.561 | 96.90 | 0.91228030 | 387.6 | 0.35087878 |
| 484.75 | 0.562 | 96.95 | 0.91231101 | 387.8 | 0.35075598 |
| 485 | 0.562 | 97.00 | 0.91234170 | 388.0 | 0.35063320 |
| 485.25 | 0.562 | 97.05 | 0.91237239 | 388.2 | 0.35051044 |
| 485.5 | 0.562 | 97.10 | 0.91240307 | 388.4 | 0.35038772 |
| 485.75 | 0.562 | 97.15 | 0.91243374 | 388.6 | 0.35026503 |
| 486 | 0.562 | 97.20 | 0.91246441 | 388.8 | 0.35014237 |
| 486.25 | 0.562 | 97.25 | 0.91249506 | 389.0 | 0.35001974 |
| 486.5 | 0.563 | 97.30 | 0.91252572 | 389.2 | 0.34989714 |
| 486.75 | 0.563 | 97.35 | 0.91255636 | 389.4 | 0.34977457 |
| 487 | 0.563 | 97.40 | 0.91258699 | 389.6 | 0.34965202 |
| 487.25 | 0.563 | 97.45 | 0.91261762 | 389.8 | 0.34952951 |
| 487.5 | 0.563 | 97.50 | 0.91264824 | 390.0 | 0.34940703 |
| 487.75 | 0.563 | 97.55 | 0.91267886 | 390.2 | 0.34928457 |
| 488 | 0.564 | 97.60 | 0.91270946 | 390.4 | 0.34916215 |
| 488.25 | 0.564 | 97.65 | 0.91274006 | 390.6 | 0.34903975 |
| 488.5 | 0.564 | 97.70 | 0.91277065 | 390.8 | 0.34891739 |
| 488.75 | 0.564 | 97.75 | 0.91280124 | 391.0 | 0.34879505 |
| 489 | 0.564 | 97.80 | 0.91283181 | 391.2 | 0.34867274 |
| 489.25 | 0.564 | 97.85 | 0.91286238 | 391.4 | 0.34855047 |
| 489.5 | 0.564 | 97.90 | 0.91289295 | 391.6 | 0.34842822 |
| 489.75 | 0.565 | 97.95 | 0.91292350 | 391.8 | 0.34830600 |
| 490 | 0.565 | 98.00 | 0.91295405 | 392.0 | 0.34818381 |
| 490.25 | 0.565 | 98.05 | 0.91298459 | 392.2 | 0.34806165 |
| 490.5 | 0.565 | 98.10 | 0.91301512 | 392.4 | 0.34793952 |
| 490.75 | 0.565 | 98.15 | 0.91304565 | 392.6 | 0.34781742 |
| 491 | 0.565 | 98.20 | 0.91307616 | 392.8 | 0.34769535 |
| 491.25 | 0.566 | 98.25 | 0.91310667 | 393.0 | 0.34757330 |
| 491.5 | 0.566 | 98.30 | 0.91313718 | 393.2 | 0.34745129 |
| 491.75 | 0.566 | 98.35 | 0.91316767 | 393.4 | 0.34732930 |
| 492 | 0.566 | 98.40 | 0.91319816 | 393.6 | 0.34720735 |
| 492.25 | 0.566 | 98.45 | 0.91322864 | 393.8 | 0.34708542 |
| 492.5 | 0.566 | 98.50 | 0.91325912 | 394.0 | 0.34696352 |
| 492.75 | 0.566 | 98.55 | 0.91328959 | 394.2 | 0.34684166 |
| 493 | 0.567 | 98.60 | 0.91332005 | 394.4 | 0.34671982 |
| 493.25 | 0.567 | 98.65 | 0.91335050 | 394.6 | 0.34659801 |
| 493.5 | 0.567 | 98.70 | 0.91338094 | 394.8 | 0.34647622 |
| 493.75 | 0.567 | 98.75 | 0.91341138 | 395.0 | 0.34635447 |
| 494 | 0.567 | 98.80 | 0.91344181 | 395.2 | 0.34623275 |
| 494.25 | 0.567 | 98.85 | 0.91347224 | 395.4 | 0.34611105 |
| 494.5 | 0.568 | 98.90 | 0.91350265 | 395.6 | 0.34598939 |
| 494.75 | 0.568 | 98.95 | 0.91353306 | 395.8 | 0.34586775 |
| 495 | 0.568 | 99.00 | 0.91356346 | 396.0 | 0.34574614 |


| 495.25 | 0.568 | 99.05 | 0.91359386 | 396.2 | 0.34562457 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 495.5 | 0.568 | 99.10 | 0.91362425 | 396.4 | 0.34550302 |
| 495.75 | 0.568 | 99.15 | 0.91365463 | 396.6 | 0.34538150 |
| 496 | 0.568 | 99.20 | 0.91368500 | 396.8 | 0.34526000 |
| 496.25 | 0.569 | 99.25 | 0.91371537 | 397.0 | 0.34513854 |
| 496.5 | 0.569 | 99.30 | 0.91374572 | 397.2 | 0.34501710 |
| 496.75 | 0.569 | 99.35 | 0.91377608 | 397.4 | 0.34489570 |
| 497 | 0.569 | 99.40 | 0.91380642 | 397.6 | 0.34477432 |
| 497.25 | 0.569 | 99.45 | 0.91383676 | 397.8 | 0.34465297 |
| 497.5 | 0.569 | 99.50 | 0.91386709 | 398.0 | 0.34453165 |
| 497.75 | 0.569 | 99.55 | 0.91389741 | 398.2 | 0.34441036 |
| 498 | 0.570 | 99.60 | 0.91392773 | 398.4 | 0.34428910 |
| 498.25 | 0.570 | 99.65 | 0.91395803 | 398.6 | 0.34416786 |
| 498.5 | 0.570 | 99.70 | 0.91398834 | 398.8 | 0.34404666 |
| 498.75 | 0.570 | 99.75 | 0.91401863 | 399.0 | 0.34392548 |
| 499 | 0.570 | 99.80 | 0.91404892 | 399.2 | 0.34380433 |
| 499.25 | 0.570 | 99.85 | 0.91407920 | 399.4 | 0.34368321 |
| 499.5 | 0.571 | 99.90 | 0.91410947 | 399.6 | 0.34356212 |
| 499.75 | 0.571 | 99.95 | 0.91413974 | 399.8 | 0.34344106 |
| 500 | 0.571 | 100.00 | 0.91416999 | 400.0 | 0.34332003 |
| 500.25 | 0.571 | 100.05 | 0.91420025 | 400.2 | 0.34319902 |
| 500.5 | 0.571 | 100.10 | 0.91423049 | 400.4 | 0.34307804 |
| 500.75 | 0.571 | 100.15 | 0.91426073 | 400.6 | 0.34295709 |
| 501 | 0.571 | 100.20 | 0.91429096 | 400.8 | 0.34283617 |
| 501.25 | 0.572 | 100.25 | 0.91432118 | 401.0 | 0.34271528 |
| 501.5 | 0.572 | 100.30 | 0.91435140 | 401.2 | 0.34259442 |
| 501.75 | 0.572 | 100.35 | 0.91438161 | 401.4 | 0.34247358 |
| 502 | 0.572 | 100.40 | 0.91441181 | 401.6 | 0.34235277 |
| 502.25 | 0.572 | 100.45 | 0.91444200 | 401.8 | 0.34223199 |
| 502.5 | 0.572 | 100.50 | 0.91447219 | 402.0 | 0.34211124 |
| 502.75 | 0.573 | 100.55 | 0.91450237 | 402.2 | 0.34199052 |
| 503 | 0.573 | 100.60 | 0.91453254 | 402.4 | 0.34186982 |
| 503.25 | 0.573 | 100.65 | 0.91456271 | 402.6 | 0.34174916 |
| 503.5 | 0.573 | 100.70 | 0.91459287 | 402.8 | 0.34162852 |
| 503.75 | 0.573 | 100.75 | 0.91462302 | 403.0 | 0.34150791 |
| 504 | 0.573 | 100.80 | 0.91465317 | 403.2 | 0.34138733 |
| 504.25 | 0.573 | 100.85 | 0.91468331 | 403.4 | 0.34126677 |
| 504.5 | 0.574 | 100.90 | 0.91471344 | 403.6 | 0.34114625 |
| 504.75 | 0.574 | 100.95 | 0.91474356 | 403.8 | 0.34102575 |
| 505 | 0.574 | 101.00 | 0.91477368 | 404.0 | 0.34090528 |
| 505.25 | 0.574 | 101.05 | 0.91480379 | 404.2 | 0.34078484 |
| 505.5 | 0.574 | 101.10 | 0.91483389 | 404.4 | 0.34066443 |
| 505.75 | 0.574 | 101.15 | 0.91486399 | 404.6 | 0.34054404 |
| 506 | 0.574 | 101.20 | 0.91489408 | 404.8 | 0.34042368 |
| 506.25 | 0.575 | 101.25 | 0.91492416 | 405.0 | 0.34030335 |
| 506.5 | 0.575 | 101.30 | 0.91495424 | 405.2 | 0.34018305 |
| 506.75 | 0.575 | 101.35 | 0.91498431 | 405.4 | 0.34006278 |
| 507 | 0.575 | 101.40 | 0.91501437 | 405.6 | 0.33994253 |
| 507.25 | 0.575 | 101.45 | 0.91504442 | 405.8 | 0.33982231 |
| 507.5 | 0.575 | 101.50 | 0.91507447 | 406.0 | 0.33970212 |
| 507.75 | 0.576 | 101.55 | 0.91510451 | 406.2 | 0.33958196 |
| 508 | 0.576 | 101.60 | 0.91513454 | 406.4 | 0.33946183 |
| 508.25 | 0.576 | 101.65 | 0.91516457 | 406.6 | 0.33934172 |
| 508.5 | 0.576 | 101.70 | 0.91519459 | 406.8 | 0.33922164 |
| 508.75 | 0.576 | 101.75 | 0.91522460 | 407.0 | 0.33910159 |
| 509 | 0.576 | 101.80 | 0.91525461 | 407.2 | 0.33898157 |
| 509.25 | 0.576 | 101.85 | 0.91528461 | 407.4 | 0.33886157 |
| 509.5 | 0.577 | 101.90 | 0.91531460 | 407.6 | 0.33874160 |
| 509.75 | 0.577 | 101.95 | 0.91534458 | 407.8 | 0.33862166 |
| 510 | 0.577 | 102.00 | 0.91537456 | 408.0 | 0.33850175 |
| 510.25 | 0.577 | 102.05 | 0.91540453 | 408.2 | 0.33838186 |
| 510.5 | 0.577 | 102.10 | 0.91543450 | 408.4 | 0.33826201 |
| 510.75 | 0.577 | 102.15 | 0.91546446 | 408.6 | 0.33814218 |
| 511 | 0.577 | 102.20 | 0.91549441 | 408.8 | 0.33802237 |
| 511.25 | 0.578 | 102.25 | 0.91552435 | 409.0 | 0.33790260 |
| 511.5 | 0.578 | 102.30 | 0.91555429 | 409.2 | 0.33778285 |
| 511.75 | 0.578 | 102.35 | 0.91558422 | 409.4 | 0.33766313 |
| 512 | 0.578 | 102.40 | 0.91561414 | 409.6 | 0.33754344 |
| 512.25 | 0.578 | 102.45 | 0.91564406 | 409.8 | 0.33742377 |
| 512.5 | 0.578 | 102.50 | 0.91567397 | 410.0 | 0.33730414 |
| 512.75 | 0.579 | 102.55 | 0.91570387 | 410.2 | 0.33718453 |


| 513 | 0.579 | 102.60 | 0.91573376 | 410.4 | 0.33706494 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 513.25 | 0.579 | 102.65 | 0.91576365 | 410.6 | 0.33694539 |
| 513.5 | 0.579 | 102.70 | 0.91579353 | 410.8 | 0.33682586 |
| 513.75 | 0.579 | 102.75 | 0.91582341 | 411.0 | 0.33670636 |
| 514 | 0.579 | 102.80 | 0.91585328 | 411.2 | 0.33658689 |
| 514.25 | 0.579 | 102.85 | 0.91588314 | 411.4 | 0.33646744 |
| 514.5 | 0.580 | 102.90 | 0.91591299 | 411.6 | 0.33634802 |
| 514.75 | 0.580 | 102.95 | 0.91594284 | 411.8 | 0.33622863 |
| 515 | 0.580 | 103.00 | 0.91597268 | 412.0 | 0.33610927 |
| 515.25 | 0.580 | 103.05 | 0.91600252 | 412.2 | 0.33598993 |
| 515.5 | 0.580 | 103.10 | 0.91603235 | 412.4 | 0.33587062 |
| 515.75 | 0.580 | 103.15 | 0.91606217 | 412.6 | 0.33575134 |
| 516 | 0.580 | 103.20 | 0.91609198 | 412.8 | 0.33563208 |
| 516.25 | 0.581 | 103.25 | 0.91612179 | 413.0 | 0.33551285 |
| 516.5 | 0.581 | 103.30 | 0.91615159 | 413.2 | 0.33539365 |
| 516.75 | 0.581 | 103.35 | 0.91618138 | 413.4 | 0.33527448 |
| 517 | 0.581 | 103.40 | 0.91621117 | 413.6 | 0.33515533 |
| 517.25 | 0.581 | 103.45 | 0.91624095 | 413.8 | 0.33503621 |
| 517.5 | 0.581 | 103.50 | 0.91627072 | 414.0 | 0.33491712 |
| 517.75 | 0.582 | 103.55 | 0.91630049 | 414.2 | 0.33479805 |
| 518 | 0.582 | 103.60 | 0.91633025 | 414.4 | 0.33467901 |
| 518.25 | 0.582 | 103.65 | 0.91636000 | 414.6 | 0.33456000 |
| 518.5 | 0.582 | 103.70 | 0.91638975 | 414.8 | 0.33444102 |
| 518.75 | 0.582 | 103.75 | 0.91641948 | 415.0 | 0.33432206 |
| 519 | 0.582 | 103.80 | 0.91644922 | 415.2 | 0.33420313 |
| 519.25 | 0.582 | 103.85 | 0.91647894 | 415.4 | 0.33408423 |
| 519.5 | 0.583 | 103.90 | 0.91650866 | 415.6 | 0.33396535 |
| 519.75 | 0.583 | 103.95 | 0.91653838 | 415.8 | 0.33384650 |
| 520 | 0.583 | 104.00 | 0.91656808 | 416.0 | 0.33372768 |
| 520.25 | 0.583 | 104.05 | 0.91659778 | 416.2 | 0.33360888 |
| 520.5 | 0.583 | 104.10 | 0.91662747 | 416.4 | 0.33349011 |
| 520.75 | 0.583 | 104.15 | 0.91665716 | 416.6 | 0.33337137 |
| 521 | 0.583 | 104.20 | 0.91668684 | 416.8 | 0.33325265 |
| 521.25 | 0.584 | 104.25 | 0.91671651 | 417.0 | 0.33313396 |
| 521.5 | 0.584 | 104.30 | 0.91674618 | 417.2 | 0.33301530 |
| 521.75 | 0.584 | 104.35 | 0.91677583 | 417.4 | 0.33289666 |
| 522 | 0.584 | 104.40 | 0.91680549 | 417.6 | 0.33277806 |
| 522.25 | 0.584 | 104.45 | 0.91683513 | 417.8 | 0.33265947 |
| 522.5 | 0.584 | 104.50 | 0.91686477 | 418.0 | 0.33254092 |
| 522.75 | 0.584 | 104.55 | 0.91689440 | 418.2 | 0.33242239 |
| 523 | 0.585 | 104.60 | 0.91692403 | 418.4 | 0.33230389 |
| 523.25 | 0.585 | 104.65 | 0.91695365 | 418.6 | 0.33218541 |
| 523.5 | 0.585 | 104.70 | 0.91698326 | 418.8 | 0.33206696 |
| 523.75 | 0.585 | 104.75 | 0.91701287 | 419.0 | 0.33194854 |
| 524 | 0.585 | 104.80 | 0.91704246 | 419.2 | 0.33183014 |
| 524.25 | 0.585 | 104.85 | 0.91707206 | 419.4 | 0.33171177 |
| 524.5 | 0.586 | 104.90 | 0.91710164 | 419.6 | 0.33159343 |
| 524.75 | 0.586 | 104.95 | 0.91713122 | 419.8 | 0.33147511 |
| 525 | 0.586 | 105.00 | 0.91716079 | 420.0 | 0.33135682 |
| 525.25 | 0.586 | 105.05 | 0.91719036 | 420.2 | 0.33123856 |
| 525.5 | 0.586 | 105.10 | 0.91721992 | 420.4 | 0.33112032 |
| 525.75 | 0.586 | 105.15 | 0.91724947 | 420.6 | 0.33100211 |
| 526 | 0.586 | 105.20 | 0.91727902 | 420.8 | 0.33088393 |
| 526.25 | 0.587 | 105.25 | 0.91730856 | 421.0 | 0.33076577 |
| 526.5 | 0.587 | 105.30 | 0.91733809 | 421.2 | 0.33064764 |
| 526.75 | 0.587 | 105.35 | 0.91736762 | 421.4 | 0.33052954 |
| 527 | 0.587 | 105.40 | 0.91739714 | 421.6 | 0.33041146 |
| 527.25 | 0.587 | 105.45 | 0.91742665 | 421.8 | 0.33029340 |
| 527.5 | 0.587 | 105.50 | 0.91745616 | 422.0 | 0.33017538 |
| 527.75 | 0.587 | 105.55 | 0.91748566 | 422.2 | 0.33005738 |
| 528 | 0.588 | 105.60 | 0.91751515 | 422.4 | 0.32993941 |
| 528.25 | 0.588 | 105.65 | 0.91754464 | 422.6 | 0.32982146 |
| 528.5 | 0.588 | 105.70 | 0.91757412 | 422.8 | 0.32970354 |
| 528.75 | 0.588 | 105.75 | 0.91760359 | 423.0 | 0.32958564 |
| 529 | 0.588 | 105.80 | 0.91763306 | 423.2 | 0.32946777 |
| 529.25 | 0.588 | 105.85 | 0.91766252 | 423.4 | 0.32934993 |
| 529.5 | 0.588 | 105.90 | 0.91769197 | 423.6 | 0.32923212 |
| 529.75 | 0.589 | 105.95 | 0.91772142 | 423.8 | 0.32911433 |
| 530 | 0.589 | 106.00 | 0.91775086 | 424.0 | 0.32899656 |
| 530.25 | 0.589 | 106.05 | 0.91778029 | 424.2 | 0.32887882 |
| 530.5 | 0.589 | 106.10 | 0.91780972 | 424.4 | 0.32876111 |


| 530.75 | 0.589 | 106.15 | 0.91783914 | 424.6 | 0.32864343 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 531 | 0.589 | 106.20 | 0.91786856 | 424.8 | 0.32852577 |
| 531.25 | 0.589 | 106.25 | 0.91789797 | 425.0 | 0.32840813 |
| 531.5 | 0.590 | 106.30 | 0.91792737 | 425.2 | 0.32829053 |
| 531.75 | 0.590 | 106.35 | 0.91795676 | 425.4 | 0.32817294 |
| 532 | 0.590 | 106.40 | 0.91798615 | 425.6 | 0.32805539 |
| 532.25 | 0.590 | 106.45 | 0.91801554 | 425.8 | 0.32793786 |
| 532.5 | 0.590 | 106.50 | 0.91804491 | 426.0 | 0.32782036 |
| 532.75 | 0.590 | 106.55 | 0.91807428 | 426.2 | 0.32770288 |
| 533 | 0.591 | 106.60 | 0.91810364 | 426.4 | 0.32758543 |
| 533.25 | 0.591 | 106.65 | 0.91813300 | 426.6 | 0.32746800 |
| 533.5 | 0.591 | 106.70 | 0.91816235 | 426.8 | 0.32735060 |
| 533.75 | 0.591 | 106.75 | 0.91819169 | 427.0 | 0.32723323 |
| 534 | 0.591 | 106.80 | 0.91822103 | 427.2 | 0.32711588 |
| 534.25 | 0.591 | 106.85 | 0.91825036 | 427.4 | 0.32699855 |
| 534.5 | 0.591 | 106.90 | 0.91827969 | 427.6 | 0.32688126 |
| 534.75 | 0.592 | 106.95 | 0.91830900 | 427.8 | 0.32676399 |
| 535 | 0.592 | 107.00 | 0.91833831 | 428.0 | 0.32664674 |
| 535.25 | 0.592 | 107.05 | 0.91836762 | 428.2 | 0.32652952 |
| 535.5 | 0.592 | 107.10 | 0.91839692 | 428.4 | 0.32641233 |
| 535.75 | 0.592 | 107.15 | 0.91842621 | 428.6 | 0.32629516 |
| 536 | 0.592 | 107.20 | 0.91845550 | 428.8 | 0.32617802 |
| 536.25 | 0.592 | 107.25 | 0.91848477 | 429.0 | 0.32606090 |
| 536.5 | 0.593 | 107.30 | 0.91851405 | 429.2 | 0.32594381 |
| 536.75 | 0.593 | 107.35 | 0.91854331 | 429.4 | 0.32582675 |
| 537 | 0.593 | 107.40 | 0.91857257 | 429.6 | 0.32570971 |
| 537.25 | 0.593 | 107.45 | 0.91860183 | 429.8 | 0.32559269 |
| 537.5 | 0.593 | 107.50 | 0.91863107 | 430.0 | 0.32547570 |
| 537.75 | 0.593 | 107.55 | 0.91866032 | 430.2 | 0.32535874 |
| 538 | 0.593 | 107.60 | 0.91868955 | 430.4 | 0.32524180 |
| 538.25 | 0.594 | 107.65 | 0.91871878 | 430.6 | 0.32512489 |
| 538.5 | 0.594 | 107.70 | 0.91874800 | 430.8 | 0.32500800 |
| 538.75 | 0.594 | 107.75 | 0.91877721 | 431.0 | 0.32489114 |
| 539 | 0.594 | 107.80 | 0.91880642 | 431.2 | 0.32477431 |
| 539.25 | 0.594 | 107.85 | 0.91883563 | 431.4 | 0.32465750 |
| 539.5 | 0.594 | 107.90 | 0.91886482 | 431.6 | 0.32454071 |
| 539.75 | 0.594 | 107.95 | 0.91889401 | 431.8 | 0.32442395 |
| 540 | 0.595 | 108.00 | 0.91892319 | 432.0 | 0.32430722 |
| 540.25 | 0.595 | 108.05 | 0.91895237 | 432.2 | 0.32419051 |
| 540.5 | 0.595 | 108.10 | 0.91898154 | 432.4 | 0.32407383 |
| 540.75 | 0.595 | 108.15 | 0.91901071 | 432.6 | 0.32395717 |
| 541 | 0.595 | 108.20 | 0.91903986 | 432.8 | 0.32384054 |
| 541.25 | 0.595 | 108.25 | 0.91906902 | 433.0 | 0.32372393 |
| 541.5 | 0.595 | 108.30 | 0.91909816 | 433.2 | 0.32360735 |
| 541.75 | 0.596 | 108.35 | 0.91912730 | 433.4 | 0.32349080 |
| 542 | 0.596 | 108.40 | 0.91915643 | 433.6 | 0.32337426 |
| 542.25 | 0.596 | 108.45 | 0.91918556 | 433.8 | 0.32325776 |
| 542.5 | 0.596 | 108.50 | 0.91921468 | 434.0 | 0.32314128 |
| 542.75 | 0.596 | 108.55 | 0.91924379 | 434.2 | 0.32302482 |
| 543 | 0.596 | 108.60 | 0.91927290 | 434.4 | 0.32290839 |
| 543.25 | 0.597 | 108.65 | 0.91930200 | 434.6 | 0.32279199 |
| 543.5 | 0.597 | 108.70 | 0.91933110 | 434.8 | 0.32267561 |
| 543.75 | 0.597 | 108.75 | 0.91936019 | 435.0 | 0.32255925 |
| 544 | 0.597 | 108.80 | 0.91938927 | 435.2 | 0.32244293 |
| 544.25 | 0.597 | 108.85 | 0.91941834 | 435.4 | 0.32232662 |
| 544.5 | 0.597 | 108.90 | 0.91944741 | 435.6 | 0.32221034 |
| 544.75 | 0.597 | 108.95 | 0.91947648 | 435.8 | 0.32209409 |
| 545 | 0.598 | 109.00 | 0.91950554 | 436.0 | 0.32197786 |
| 545.25 | 0.598 | 109.05 | 0.91953459 | 436.2 | 0.32186166 |
| 545.5 | 0.598 | 109.10 | 0.91956363 | 436.4 | 0.32174548 |
| 545.75 | 0.598 | 109.15 | 0.91959267 | 436.6 | 0.32162932 |
| 546 | 0.598 | 109.20 | 0.91962170 | 436.8 | 0.32151319 |
| 546.25 | 0.598 | 109.25 | 0.91965073 | 437.0 | 0.32139709 |
| 546.5 | 0.598 | 109.30 | 0.91967975 | 437.2 | 0.32128101 |
| 546.75 | 0.599 | 109.35 | 0.91970876 | 437.4 | 0.32116496 |
| 547 | 0.599 | 109.40 | 0.91973777 | 437.6 | 0.32104893 |
| 547.25 | 0.599 | 109.45 | 0.91976677 | 437.8 | 0.32093292 |
| 547.5 | 0.599 | 109.50 | 0.91979576 | 438.0 | 0.32081695 |
| 547.75 | 0.599 | 109.55 | 0.91982475 | 438.2 | 0.32070099 |
| 548 | 0.599 | 109.60 | 0.91985373 | 438.4 | 0.32058506 |
| 548.25 | 0.599 | 109.65 | 0.91988271 | 438.6 | 0.32046916 |


| 548.5 | 0.600 | 109.70 | 0.91991168 | 438.8 | 0.32035328 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 548.75 | 0.600 | 109.75 | 0.91994064 | 439.0 | 0.32023742 |
| 549 | 0.600 | 109.80 | 0.91996960 | 439.2 | 0.32012159 |
| 549.25 | 0.600 | 109.85 | 0.91999855 | 439.4 | 0.32000579 |
| 549.5 | 0.600 | 109.90 | 0.92002750 | 439.6 | 0.31989001 |
| 549.75 | 0.600 | 109.95 | 0.92005644 | 439.8 | 0.31977425 |
| 550 | 0.600 | 110.00 | 0.92008537 | 440.0 | 0.31965852 |
| 550.25 | 0.601 | 110.05 | 0.92011430 | 440.2 | 0.31954281 |
| 550.5 | 0.601 | 110.10 | 0.92014322 | 440.4 | 0.31942713 |
| 550.75 | 0.601 | 110.15 | 0.92017213 | 440.6 | 0.31931148 |
| 551 | 0.601 | 110.20 | 0.92020104 | 440.8 | 0.31919584 |
| 551.25 | 0.601 | 110.25 | 0.92022994 | 441.0 | 0.31908024 |
| 551.5 | 0.601 | 110.30 | 0.92025884 | 441.2 | 0.31896465 |
| 551.75 | 0.601 | 110.35 | 0.92028773 | 441.4 | 0.31884909 |
| 552 | 0.602 | 110.40 | 0.92031661 | 441.6 | 0.31873356 |
| 552.25 | 0.602 | 110.45 | 0.92034549 | 441.8 | 0.31861805 |
| 552.5 | 0.602 | 110.50 | 0.92037436 | 442.0 | 0.31850257 |
| 552.75 | 0.602 | 110.55 | 0.92040322 | 442.2 | 0.31838711 |
| 553 | 0.602 | 110.60 | 0.92043208 | 442.4 | 0.31827167 |
| 553.25 | 0.602 | 110.65 | 0.92046093 | 442.6 | 0.31815626 |
| 553.5 | 0.602 | 110.70 | 0.92048978 | 442.8 | 0.31804087 |
| 553.75 | 0.603 | 110.75 | 0.92051862 | 443.0 | 0.31792551 |
| 554 | 0.603 | 110.80 | 0.92054746 | 443.2 | 0.31781018 |
| 554.25 | 0.603 | 110.85 | 0.92057628 | 443.4 | 0.31769486 |
| 554.5 | 0.603 | 110.90 | 0.92060511 | 443.6 | 0.31757957 |
| 554.75 | 0.603 | 110.95 | 0.92063392 | 443.8 | 0.31746431 |
| 555 | 0.603 | 111.00 | 0.92066273 | 444.0 | 0.31734907 |
| 555.25 | 0.603 | 111.05 | 0.92069154 | 444.2 | 0.31723385 |
| 555.5 | 0.604 | 111.10 | 0.92072033 | 444.4 | 0.31711866 |
| 555.75 | 0.604 | 111.15 | 0.92074913 | 444.6 | 0.31700350 |
| 556 | 0.604 | 111.20 | 0.92077791 | 444.8 | 0.31688836 |
| 556.25 | 0.604 | 111.25 | 0.92080669 | 445.0 | 0.31677324 |
| 556.5 | 0.604 | 111.30 | 0.92083546 | 445.2 | 0.31665814 |
| 556.75 | 0.604 | 111.35 | 0.92086423 | 445.4 | 0.31654307 |
| 557 | 0.604 | 111.40 | 0.92089299 | 445.6 | 0.31642803 |
| 557.25 | 0.605 | 111.45 | 0.92092175 | 445.8 | 0.31631301 |
| 557.5 | 0.605 | 111.50 | 0.92095050 | 446.0 | 0.31619801 |
| 557.75 | 0.605 | 111.55 | 0.92097924 | 446.2 | 0.31608304 |
| 558 | 0.605 | 111.60 | 0.92100798 | 446.4 | 0.31596809 |
| 558.25 | 0.605 | 111.65 | 0.92103671 | 446.6 | 0.31585317 |
| 558.5 | 0.605 | 111.70 | 0.92106543 | 446.8 | 0.31573827 |
| 558.75 | 0.605 | 111.75 | 0.92109415 | 447.0 | 0.31562339 |
| 559 | 0.606 | 111.80 | 0.92112286 | 447.2 | 0.31550854 |
| 559.25 | 0.606 | 111.85 | 0.92115157 | 447.4 | 0.31539371 |
| 559.5 | 0.606 | 111.90 | 0.92118027 | 447.6 | 0.31527891 |
| 559.75 | 0.606 | 111.95 | 0.92120897 | 447.8 | 0.31516413 |
| 560 | 0.606 | 112.00 | 0.92123766 | 448.0 | 0.31504938 |
| 560.25 | 0.606 | 112.05 | 0.92126634 | 448.2 | 0.31493465 |
| 560.5 | 0.606 | 112.10 | 0.92129501 | 448.4 | 0.31481994 |
| 560.75 | 0.607 | 112.15 | 0.92132369 | 448.6 | 0.31470526 |
| 561 | 0.607 | 112.20 | 0.92135235 | 448.8 | 0.31459060 |
| 561.25 | 0.607 | 112.25 | 0.92138101 | 449.0 | 0.31447596 |
| 561.5 | 0.607 | 112.30 | 0.92140966 | 449.2 | 0.31436135 |
| 561.75 | 0.607 | 112.35 | 0.92143831 | 449.4 | 0.31424677 |
| 562 | 0.607 | 112.40 | 0.92146695 | 449.6 | 0.31413221 |
| 562.25 | 0.607 | 112.45 | 0.92149558 | 449.8 | 0.31401767 |
| 562.5 | 0.608 | 112.50 | 0.92152421 | 450.0 | 0.31390315 |
| 562.75 | 0.608 | 112.55 | 0.92155283 | 450.2 | 0.31378866 |
| 563 | 0.608 | 112.60 | 0.92158145 | 450.4 | 0.31367419 |
| 563.25 | 0.608 | 112.65 | 0.92161006 | 450.6 | 0.31355975 |
| 563.5 | 0.608 | 112.70 | 0.92163867 | 450.8 | 0.31344533 |
| 563.75 | 0.608 | 112.75 | 0.92166727 | 451.0 | 0.31333094 |
| 564 | 0.608 | 112.80 | 0.92169586 | 451.2 | 0.31321656 |
| 564.25 | 0.609 | 112.85 | 0.92172445 | 451.4 | 0.31310222 |
| 564.5 | 0.609 | 112.90 | 0.92175303 | 451.6 | 0.31298789 |
| 564.75 | 0.609 | 112.95 | 0.92178160 | 451.8 | 0.31287359 |
| 565 | 0.609 | 113.00 | 0.92181017 | 452.0 | 0.31275932 |
| 565.25 | 0.609 | 113.05 | 0.92183873 | 452.2 | 0.31264506 |
| 565.5 | 0.609 | 113.10 | 0.92186729 | 452.4 | 0.31253084 |
| 565.75 | 0.609 | 113.15 | 0.92189584 | 452.6 | 0.31241663 |
| 566 | 0.610 | 113.20 | 0.92192439 | 452.8 | 0.31230245 |


| 566.25 | 0.610 | 113.25 | 0.92195293 | 453.0 | 0.31218829 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 566.5 | 0.610 | 113.30 | 0.92198146 | 453.2 | 0.31207416 |
| 566.75 | 0.610 | 113.35 | 0.92200999 | 453.4 | 0.31196005 |
| 567 | 0.610 | 113.40 | 0.92203851 | 453.6 | 0.31184596 |
| 567.25 | 0.610 | 113.45 | 0.92206703 | 453.8 | 0.31173190 |
| 567.5 | 0.610 | 113.50 | 0.92209554 | 454.0 | 0.31161786 |
| 567.75 | 0.611 | 113.55 | 0.92212404 | 454.2 | 0.31150384 |
| 568 | 0.611 | 113.60 | 0.92215254 | 454.4 | 0.31138985 |
| 568.25 | 0.611 | 113.65 | 0.92218103 | 454.6 | 0.31127588 |
| 568.5 | 0.611 | 113.70 | 0.92220952 | 454.8 | 0.31116194 |
| 568.75 | 0.611 | 113.75 | 0.92223800 | 455.0 | 0.31104802 |
| 569 | 0.611 | 113.80 | 0.92226647 | 455.2 | 0.31093412 |
| 569.25 | 0.611 | 113.85 | 0.92229494 | 455.4 | 0.31082024 |
| 569.5 | 0.612 | 113.90 | 0.92232340 | 455.6 | 0.31070639 |
| 569.75 | 0.612 | 113.95 | 0.92235186 | 455.8 | 0.31059256 |
| 570 | 0.612 | 114.00 | 0.92238031 | 456.0 | 0.31047876 |
| 570.25 | 0.612 | 114.05 | 0.92240875 | 456.2 | 0.31036498 |
| 570.5 | 0.612 | 114.10 | 0.92243719 | 456.4 | 0.31025122 |
| 570.75 | 0.612 | 114.15 | 0.92246563 | 456.6 | 0.31013749 |
| 571 | 0.612 | 114.20 | 0.92249406 | 456.8 | 0.31002378 |
| 571.25 | 0.613 | 114.25 | 0.92252248 | 457.0 | 0.30991009 |
| 571.5 | 0.613 | 114.30 | 0.92255089 | 457.2 | 0.30979643 |
| 571.75 | 0.613 | 114.35 | 0.92257930 | 457.4 | 0.30968279 |
| 572 | 0.613 | 114.40 | 0.92260771 | 457.6 | 0.30956917 |
| 572.25 | 0.613 | 114.45 | 0.92263611 | 457.8 | 0.30945558 |
| 572.5 | 0.613 | 114.50 | 0.92266450 | 458.0 | 0.30934201 |
| 572.75 | 0.613 | 114.55 | 0.92269288 | 458.2 | 0.30922846 |
| 573 | 0.614 | 114.60 | 0.92272127 | 458.4 | 0.30911494 |
| 573.25 | 0.614 | 114.65 | 0.92274964 | 458.6 | 0.30900144 |
| 573.5 | 0.614 | 114.70 | 0.92277801 | 458.8 | 0.30888796 |
| 573.75 | 0.614 | 114.75 | 0.92280637 | 459.0 | 0.30877451 |
| 574 | 0.614 | 114.80 | 0.92283473 | 459.2 | 0.30866108 |
| 574.25 | 0.614 | 114.85 | 0.92286308 | 459.4 | 0.30854767 |
| 574.5 | 0.614 | 114.90 | 0.92289143 | 459.6 | 0.30843429 |
| 574.75 | 0.615 | 114.95 | 0.92291977 | 459.8 | 0.30832093 |
| 575 | 0.615 | 115.00 | 0.92294810 | 460.0 | 0.30820759 |
| 575.25 | 0.615 | 115.05 | 0.92297643 | 460.2 | 0.30809427 |
| 575.5 | 0.615 | 115.10 | 0.92300475 | 460.4 | 0.30798098 |
| 575.75 | 0.615 | 115.15 | 0.92303307 | 460.6 | 0.30786771 |
| 576 | 0.615 | 115.20 | 0.92306138 | 460.8 | 0.30775447 |
| 576.25 | 0.615 | 115.25 | 0.92308969 | 461.0 | 0.30764125 |
| 576.5 | 0.616 | 115.30 | 0.92311799 | 461.2 | 0.30752805 |
| 576.75 | 0.616 | 115.35 | 0.92314628 | 461.4 | 0.30741487 |
| 577 | 0.616 | 115.40 | 0.92317457 | 461.6 | 0.30730172 |
| 577.25 | 0.616 | 115.45 | 0.92320285 | 461.8 | 0.30718859 |
| 577.5 | 0.616 | 115.50 | 0.92323113 | 462.0 | 0.30707548 |
| 577.75 | 0.616 | 115.55 | 0.92325940 | 462.2 | 0.30696240 |
| 578 | 0.616 | 115.60 | 0.92328767 | 462.4 | 0.30684934 |
| 578.25 | 0.617 | 115.65 | 0.92331592 | 462.6 | 0.30673630 |
| 578.5 | 0.617 | 115.70 | 0.92334418 | 462.8 | 0.30662329 |
| 578.75 | 0.617 | 115.75 | 0.92337243 | 463.0 | 0.30651029 |
| 579 | 0.617 | 115.80 | 0.92340067 | 463.2 | 0.30639732 |
| 579.25 | 0.617 | 115.85 | 0.92342891 | 463.4 | 0.30628438 |
| 579.5 | 0.617 | 115.90 | 0.92345714 | 463.6 | 0.30617146 |
| 579.75 | 0.617 | 115.95 | 0.92348536 | 463.8 | 0.30605856 |
| 580 | 0.618 | 116.00 | 0.92351358 | 464.0 | 0.30594568 |
| 580.25 | 0.618 | 116.05 | 0.92354179 | 464.2 | 0.30583282 |
| 580.5 | 0.618 | 116.10 | 0.92357000 | 464.4 | 0.30571999 |
| 580.75 | 0.618 | 116.15 | 0.92359820 | 464.6 | 0.30560718 |
| 581 | 0.618 | 116.20 | 0.92362640 | 464.8 | 0.30549440 |
| 581.25 | 0.618 | 116.25 | 0.92365459 | 465.0 | 0.30538163 |
| 581.5 | 0.618 | 116.30 | 0.92368278 | 465.2 | 0.30526889 |
| 581.75 | 0.619 | 116.35 | 0.92371096 | 465.4 | 0.30515618 |
| 582 | 0.619 | 116.40 | 0.92373913 | 465.6 | 0.30504348 |
| 582.25 | 0.619 | 116.45 | 0.92376730 | 465.8 | 0.30493081 |
| 582.5 | 0.619 | 116.50 | 0.92379546 | 466.0 | 0.30481816 |
| 582.75 | 0.619 | 116.55 | 0.92382362 | 466.2 | 0.30470553 |
| 583 | 0.619 | 116.60 | 0.92385177 | 466.4 | 0.30459293 |
| 583.25 | 0.619 | 116.65 | 0.92387991 | 466.6 | 0.30448035 |
| 583.5 | 0.620 | 116.70 | 0.92390805 | 466.8 | 0.30436779 |
| 583.75 | 0.620 | 116.75 | 0.92393619 | 467.0 | 0.30425525 |


| 584 | 0.620 | 116.80 | 0.92396431 | 467.2 | 0.30414274 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 584.25 | 0.620 | 116.85 | 0.92399244 | 467.4 | 0.30403025 |
| 584.5 | 0.620 | 116.90 | 0.92402055 | 467.6 | 0.30391778 |
| 584.75 | 0.620 | 116.95 | 0.92404867 | 467.8 | 0.30380534 |
| 585 | 0.620 | 117.00 | 0.92407677 | 468.0 | 0.30369291 |
| 585.25 | 0.621 | 117.05 | 0.92410487 | 468.2 | 0.30358051 |
| 585.5 | 0.621 | 117.10 | 0.92413297 | 468.4 | 0.30346814 |
| 585.75 | 0.621 | 117.15 | 0.92416105 | 468.6 | 0.30335578 |
| 586 | 0.621 | 117.20 | 0.92418914 | 468.8 | 0.30324345 |
| 586.25 | 0.621 | 117.25 | 0.92421722 | 469.0 | 0.30313114 |
| 586.5 | 0.621 | 117.30 | 0.92424529 | 469.2 | 0.30301885 |
| 586.75 | 0.621 | 117.35 | 0.92427335 | 469.4 | 0.30290659 |
| 587 | 0.622 | 117.40 | 0.92430141 | 469.6 | 0.30279434 |
| 587.25 | 0.622 | 117.45 | 0.92432947 | 469.8 | 0.30268212 |
| 587.5 | 0.622 | 117.50 | 0.92435752 | 470.0 | 0.30256993 |
| 587.75 | 0.622 | 117.55 | 0.92438556 | 470.2 | 0.30245775 |
| 588 | 0.622 | 117.60 | 0.92441360 | 470.4 | 0.30234560 |
| 588.25 | 0.622 | 117.65 | 0.92444163 | 470.6 | 0.30223347 |
| 588.5 | 0.622 | 117.70 | 0.92446966 | 470.8 | 0.30212136 |
| 588.75 | 0.622 | 117.75 | 0.92449768 | 471.0 | 0.30200928 |
| 589 | 0.623 | 117.80 | 0.92452570 | 471.2 | 0.30189721 |
| 589.25 | 0.623 | 117.85 | 0.92455371 | 471.4 | 0.30178517 |
| 589.5 | 0.623 | 117.90 | 0.92458171 | 471.6 | 0.30167315 |
| 589.75 | 0.623 | 117.95 | 0.92460971 | 471.8 | 0.30156116 |
| 590 | 0.623 | 118.00 | 0.92463770 | 472.0 | 0.30144918 |
| 590.25 | 0.623 | 118.05 | 0.92466569 | 472.2 | 0.30133723 |
| 590.5 | 0.623 | 118.10 | 0.92469367 | 472.4 | 0.30122530 |
| 590.75 | 0.624 | 118.15 | 0.92472165 | 472.6 | 0.30111340 |
| 591 | 0.624 | 118.20 | 0.92474962 | 472.8 | 0.30100151 |
| 591.25 | 0.624 | 118.25 | 0.92477759 | 473.0 | 0.30088965 |
| 591.5 | 0.624 | 118.30 | 0.92480555 | 473.2 | 0.30077781 |
| 591.75 | 0.624 | 118.35 | 0.92483350 | 473.4 | 0.30066599 |
| 592 | 0.624 | 118.40 | 0.92486145 | 473.6 | 0.30055419 |
| 592.25 | 0.624 | 118.45 | 0.92488939 | 473.8 | 0.30044242 |
| 592.5 | 0.625 | 118.50 | 0.92491733 | 474.0 | 0.30033067 |
| 592.75 | 0.625 | 118.55 | 0.92494527 | 474.2 | 0.30021894 |
| 593 | 0.625 | 118.60 | 0.92497319 | 474.4 | 0.30010723 |
| 593.25 | 0.625 | 118.65 | 0.92500111 | 474.6 | 0.29999555 |
| 593.5 | 0.625 | 118.70 | 0.92502903 | 474.8 | 0.29988388 |
| 593.75 | 0.625 | 118.75 | 0.92505694 | 475.0 | 0.29977224 |
| 594 | 0.625 | 118.80 | 0.92508484 | 475.2 | 0.29966062 |
| 594.25 | 0.626 | 118.85 | 0.92511274 | 475.4 | 0.29954903 |
| 594.5 | 0.626 | 118.90 | 0.92514064 | 475.6 | 0.29943745 |
| 594.75 | 0.626 | 118.95 | 0.92516852 | 475.8 | 0.29932590 |
| 595 | 0.626 | 119.00 | 0.92519641 | 476.0 | 0.29921437 |
| 595.25 | 0.626 | 119.05 | 0.92522428 | 476.2 | 0.29910286 |
| 595.5 | 0.626 | 119.10 | 0.92525216 | 476.4 | 0.29899138 |
| 595.75 | 0.626 | 119.15 | 0.92528002 | 476.6 | 0.29887991 |
| 596 | 0.627 | 119.20 | 0.92530788 | 476.8 | 0.29876847 |
| 596.25 | 0.627 | 119.25 | 0.92533574 | 477.0 | 0.29865705 |
| 596.5 | 0.627 | 119.30 | 0.92536359 | 477.2 | 0.29854565 |
| 596.75 | 0.627 | 119.35 | 0.92539143 | 477.4 | 0.29843427 |
| 597 | 0.627 | 119.40 | 0.92541927 | 477.6 | 0.29832292 |
| 597.25 | 0.627 | 119.45 | 0.92544710 | 477.8 | 0.29821159 |
| 597.5 | 0.627 | 119.50 | 0.92547493 | 478.0 | 0.29810027 |
| 597.75 | 0.628 | 119.55 | 0.92550275 | 478.2 | 0.29798899 |
| 598 | 0.628 | 119.60 | 0.92553057 | 478.4 | 0.29787772 |
| 598.25 | 0.628 | 119.65 | 0.92555838 | 478.6 | 0.29776647 |
| 598.5 | 0.628 | 119.70 | 0.92558619 | 478.8 | 0.29765525 |
| 598.75 | 0.628 | 119.75 | 0.92561399 | 479.0 | 0.29754405 |
| 599 | 0.628 | 119.80 | 0.92564178 | 479.2 | 0.29743287 |
| 599.25 | 0.628 | 119.85 | 0.92566957 | 479.4 | 0.29732171 |
| 599.5 | 0.628 | 119.90 | 0.92569736 | 479.6 | 0.29721057 |
| 599.75 | 0.629 | 119.95 | 0.92572514 | 479.8 | 0.29709946 |
| 600 | 0.629 | 120.00 | 0.92575291 | 480.0 | 0.29698837 |
| 600.25 | 0.629 | 120.05 | 0.92578068 | 480.2 | 0.29687730 |
| 600.5 | 0.629 | 120.10 | 0.92580844 | 480.4 | 0.29676625 |
| 600.75 | 0.629 | 120.15 | 0.92583620 | 480.6 | 0.29665522 |
| 601 | 0.629 | 120.20 | 0.92586395 | 480.8 | 0.29654421 |
| 601.25 | 0.629 | 120.25 | 0.92589169 | 481.0 | 0.29643323 |
| 601.5 | 0.630 | 120.30 | 0.92591943 | 481.2 | 0.29632227 |


| 601.75 | 0.630 | 120.35 | 0.92594717 | 481.4 | 0.29621133 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 602 | 0.630 | 120.40 | 0.92597490 | 481.6 | 0.29610041 |
| 602.25 | 0.630 | 120.45 | 0.92600262 | 481.8 | 0.29598951 |
| 602.5 | 0.630 | 120.50 | 0.92603034 | 482.0 | 0.29587864 |
| 602.75 | 0.630 | 120.55 | 0.92605805 | 482.2 | 0.29576778 |
| 603 | 0.630 | 120.60 | 0.92608576 | 482.4 | 0.29565695 |
| 603.25 | 0.631 | 120.65 | 0.92611347 | 482.6 | 0.29554614 |
| 603.5 | 0.631 | 120.70 | 0.92614116 | 482.8 | 0.29543535 |
| 603.75 | 0.631 | 120.75 | 0.92616885 | 483.0 | 0.29532458 |
| 604 | 0.631 | 120.80 | 0.92619654 | 483.2 | 0.29521383 |
| 604.25 | 0.631 | 120.85 | 0.92622422 | 483.4 | 0.29510311 |
| 604.5 | 0.631 | 120.90 | 0.92625190 | 483.6 | 0.29499241 |
| 604.75 | 0.631 | 120.95 | 0.92627957 | 483.8 | 0.29488173 |
| 605 | 0.632 | 121.00 | 0.92630723 | 484.0 | 0.29477107 |
| 605.25 | 0.632 | 121.05 | 0.92633489 | 484.2 | 0.29466043 |
| 605.5 | 0.632 | 121.10 | 0.92636255 | 484.4 | 0.29454981 |
| 605.75 | 0.632 | 121.15 | 0.92639020 | 484.6 | 0.29443921 |
| 606 | 0.632 | 121.20 | 0.92641784 | 484.8 | 0.29432864 |
| 606.25 | 0.632 | 121.25 | 0.92644548 | 485.0 | 0.29421809 |
| 606.5 | 0.632 | 121.30 | 0.92647311 | 485.2 | 0.29410756 |
| 606.75 | 0.633 | 121.35 | 0.92650074 | 485.4 | 0.29399705 |
| 607 | 0.633 | 121.40 | 0.92652836 | 485.6 | 0.29388656 |
| 607.25 | 0.633 | 121.45 | 0.92655598 | 485.8 | 0.29377609 |
| 607.5 | 0.633 | 121.50 | 0.92658359 | 486.0 | 0.29366564 |
| 607.75 | 0.633 | 121.55 | 0.92661119 | 486.2 | 0.29355522 |
| 608 | 0.633 | 121.60 | 0.92663880 | 486.4 | 0.29344482 |
| 608.25 | 0.633 | 121.65 | 0.92666639 | 486.6 | 0.29333444 |
| 608.5 | 0.633 | 121.70 | 0.92669398 | 486.8 | 0.29322408 |
| 608.75 | 0.634 | 121.75 | 0.92672157 | 487.0 | 0.29311374 |
| 609 | 0.634 | 121.80 | 0.92674915 | 487.2 | 0.29300342 |
| 609.25 | 0.634 | 121.85 | 0.92677672 | 487.4 | 0.29289312 |
| 609.5 | 0.634 | 121.90 | 0.92680429 | 487.6 | 0.29278285 |
| 609.75 | 0.634 | 121.95 | 0.92683185 | 487.8 | 0.29267259 |
| 610 | 0.634 | 122.00 | 0.92685941 | 488.0 | 0.29256236 |
| 610.25 | 0.634 | 122.05 | 0.92688696 | 488.2 | 0.29245215 |
| 610.5 | 0.635 | 122.10 | 0.92691451 | 488.4 | 0.29234196 |
| 610.75 | 0.635 | 122.15 | 0.92694205 | 488.6 | 0.29223179 |
| 611 | 0.635 | 122.20 | 0.92696959 | 488.8 | 0.29212164 |
| 611.25 | 0.635 | 122.25 | 0.92699712 | 489.0 | 0.29201151 |
| 611.5 | 0.635 | 122.30 | 0.92702465 | 489.2 | 0.29190141 |
| 611.75 | 0.635 | 122.35 | 0.92705217 | 489.4 | 0.29179132 |
| 612 | 0.635 | 122.40 | 0.92707968 | 489.6 | 0.29168126 |
| 612.25 | 0.636 | 122.45 | 0.92710720 | 489.8 | 0.29157122 |
| 612.5 | 0.636 | 122.50 | 0.92713470 | 490.0 | 0.29146120 |
| 612.75 | 0.636 | 122.55 | 0.92716220 | 490.2 | 0.29135120 |
| 613 | 0.636 | 122.60 | 0.92718970 | 490.4 | 0.29124122 |
| 613.25 | 0.636 | 122.65 | 0.92721718 | 490.6 | 0.29113126 |
| 613.5 | 0.636 | 122.70 | 0.92724467 | 490.8 | 0.29102133 |
| 613.75 | 0.636 | 122.75 | 0.92727215 | 491.0 | 0.29091141 |
| 614 | 0.636 | 122.80 | 0.92729962 | 491.2 | 0.29080151 |
| 614.25 | 0.637 | 122.85 | 0.92732709 | 491.4 | 0.29069164 |
| 614.5 | 0.637 | 122.90 | 0.92735455 | 491.6 | 0.29058179 |
| 614.75 | 0.637 | 122.95 | 0.92738201 | 491.8 | 0.29047196 |
| 615 | 0.637 | 123.00 | 0.92740946 | 492.0 | 0.29036215 |
| 615.25 | 0.637 | 123.05 | 0.92743691 | 492.2 | 0.29025236 |
| 615.5 | 0.637 | 123.10 | 0.92746435 | 492.4 | 0.29014259 |
| 615.75 | 0.637 | 123.15 | 0.92749179 | 492.6 | 0.29003284 |
| 616 | 0.638 | 123.20 | 0.92751922 | 492.8 | 0.28992311 |
| 616.25 | 0.638 | 123.25 | 0.92754665 | 493.0 | 0.28981341 |
| 616.5 | 0.638 | 123.30 | 0.92757407 | 493.2 | 0.28970372 |
| 616.75 | 0.638 | 123.35 | 0.92760149 | 493.4 | 0.28959406 |
| 617 | 0.638 | 123.40 | 0.92762890 | 493.6 | 0.28948442 |
| 617.25 | 0.638 | 123.45 | 0.92765630 | 493.8 | 0.28937479 |
| 617.5 | 0.638 | 123.50 | 0.92768370 | 494.0 | 0.28926519 |
| 617.75 | 0.639 | 123.55 | 0.92771110 | 494.2 | 0.28915561 |
| 618 | 0.639 | 123.60 | 0.92773849 | 494.4 | 0.28904605 |
| 618.25 | 0.639 | 123.65 | 0.92776587 | 494.6 | 0.28893651 |
| 618.5 | 0.639 | 123.70 | 0.92779325 | 494.8 | 0.28882700 |
| 618.75 | 0.639 | 123.75 | 0.92782063 | 495.0 | 0.28871750 |
| 619 | 0.639 | 123.80 | 0.92784799 | 495.2 | 0.28860802 |
| 619.25 | 0.639 | 123.85 | 0.92787536 | 495.4 | 0.28849857 |


| 619.5 | 0.640 | 123.90 | 0.92790272 | 495.6 | 0.28838913 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 619.75 | 0.640 | 123.95 | 0.92793007 | 495.8 | 0.28827972 |
| 620 | 0.640 | 124.00 | 0.92795742 | 496.0 | 0.28817033 |
| 620.25 | 0.640 | 124.05 | 0.92798476 | 496.2 | 0.28806095 |
| 620.5 | 0.640 | 124.10 | 0.92801210 | 496.4 | 0.28795160 |
| 620.75 | 0.640 | 124.15 | 0.92803943 | 496.6 | 0.28784227 |
| 621 | 0.640 | 124.20 | 0.92806676 | 496.8 | 0.28773296 |
| 621.25 | 0.640 | 124.25 | 0.92809408 | 497.0 | 0.28762367 |
| 621.5 | 0.641 | 124.30 | 0.92812140 | 497.2 | 0.28751440 |
| 621.75 | 0.641 | 124.35 | 0.92814871 | 497.4 | 0.28740515 |
| 622 | 0.641 | 124.40 | 0.92817602 | 497.6 | 0.28729592 |
| 622.25 | 0.641 | 124.45 | 0.92820332 | 497.8 | 0.28718672 |
| 622.5 | 0.641 | 124.50 | 0.92823062 | 498.0 | 0.28707753 |
| 622.75 | 0.641 | 124.55 | 0.92825791 | 498.2 | 0.28696836 |
| 623 | 0.641 | 124.60 | 0.92828520 | 498.4 | 0.28685922 |
| 623.25 | 0.642 | 124.65 | 0.92831248 | 498.6 | 0.28675009 |
| 623.5 | 0.642 | 124.70 | 0.92833975 | 498.8 | 0.28664099 |
| 623.75 | 0.642 | 124.75 | 0.92836702 | 499.0 | 0.28653191 |
| 624 | 0.642 | 124.80 | 0.92839429 | 499.2 | 0.28642284 |
| 624.25 | 0.642 | 124.85 | 0.92842155 | 499.4 | 0.28631380 |
| 624.5 | 0.642 | 124.90 | 0.92844881 | 499.6 | 0.28620478 |
| 624.75 | 0.642 | 124.95 | 0.92847606 | 499.8 | 0.28609578 |
| 625 | 0.643 | 125.00 | 0.92850330 | 500.0 | 0.28598680 |
| 625.25 | 0.643 | 125.05 | 0.92853054 | 500.2 | 0.28587784 |
| 625.5 | 0.643 | 125.10 | 0.92855778 | 500.4 | 0.28576890 |
| 625.75 | 0.643 | 125.15 | 0.92858501 | 500.6 | 0.28565998 |
| 626 | 0.643 | 125.20 | 0.92861223 | 500.8 | 0.28555108 |
| 626.25 | 0.643 | 125.25 | 0.92863945 | 501.0 | 0.28544220 |
| 626.5 | 0.643 | 125.30 | 0.92866667 | 501.2 | 0.28533334 |
| 626.75 | 0.643 | 125.35 | 0.92869387 | 501.4 | 0.28522450 |
| 627 | 0.644 | 125.40 | 0.92872108 | 501.6 | 0.28511568 |
| 627.25 | 0.644 | 125.45 | 0.92874828 | 501.8 | 0.28500689 |
| 627.5 | 0.644 | 125.50 | 0.92877547 | 502.0 | 0.28489811 |
| 627.75 | 0.644 | 125.55 | 0.92880266 | 502.2 | 0.28478935 |
| 628 | 0.644 | 125.60 | 0.92882985 | 502.4 | 0.28468062 |
| 628.25 | 0.644 | 125.65 | 0.92885702 | 502.6 | 0.28457190 |
| 628.5 | 0.644 | 125.70 | 0.92888420 | 502.8 | 0.28446321 |
| 628.75 | 0.645 | 125.75 | 0.92891137 | 503.0 | 0.28435453 |
| 629 | 0.645 | 125.80 | 0.92893853 | 503.2 | 0.28424588 |
| 629.25 | 0.645 | 125.85 | 0.92896569 | 503.4 | 0.28413724 |
| 629.5 | 0.645 | 125.90 | 0.92899284 | 503.6 | 0.28402863 |
| 629.75 | 0.645 | 125.95 | 0.92901999 | 503.8 | 0.28392003 |
| 630 | 0.645 | 126.00 | 0.92904713 | 504.0 | 0.28381146 |
| 630.25 | 0.645 | 126.05 | 0.92907427 | 504.2 | 0.28370291 |
| 630.5 | 0.646 | 126.10 | 0.92910141 | 504.4 | 0.28359437 |
| 630.75 | 0.646 | 126.15 | 0.92912853 | 504.6 | 0.28348586 |
| 631 | 0.646 | 126.20 | 0.92915566 | 504.8 | 0.28337737 |
| 631.25 | 0.646 | 126.25 | 0.92918278 | 505.0 | 0.28326890 |
| 631.5 | 0.646 | 126.30 | 0.92920989 | 505.2 | 0.28316044 |
| 631.75 | 0.646 | 126.35 | 0.92923700 | 505.4 | 0.28305201 |
| 632 | 0.646 | 126.40 | 0.92926410 | 505.6 | 0.28294360 |
| 632.25 | 0.646 | 126.45 | 0.92929120 | 505.8 | 0.28283521 |
| 632.5 | 0.647 | 126.50 | 0.92931829 | 506.0 | 0.28272684 |
| 632.75 | 0.647 | 126.55 | 0.92934538 | 506.2 | 0.28261849 |
| 633 | 0.647 | 126.60 | 0.92937246 | 506.4 | 0.28251015 |
| 633.25 | 0.647 | 126.65 | 0.92939954 | 506.6 | 0.28240184 |
| 633.5 | 0.647 | 126.70 | 0.92942661 | 506.8 | 0.28229355 |
| 633.75 | 0.647 | 126.75 | 0.92945368 | 507.0 | 0.28218528 |
| 634 | 0.647 | 126.80 | 0.92948074 | 507.2 | 0.28207703 |
| 634.25 | 0.648 | 126.85 | 0.92950780 | 507.4 | 0.28196880 |
| 634.5 | 0.648 | 126.90 | 0.92953485 | 507.6 | 0.28186059 |
| 634.75 | 0.648 | 126.95 | 0.92956190 | 507.8 | 0.28175240 |
| 635 | 0.648 | 127.00 | 0.92958894 | 508.0 | 0.28164423 |
| 635.25 | 0.648 | 127.05 | 0.92961598 | 508.2 | 0.28153608 |
| 635.5 | 0.648 | 127.10 | 0.92964301 | 508.4 | 0.28142794 |
| 635.75 | 0.648 | 127.15 | 0.92967004 | 508.6 | 0.28131983 |
| 636 | 0.648 | 127.20 | 0.92969706 | 508.8 | 0.28121174 |
| 636.25 | 0.649 | 127.25 | 0.92972408 | 509.0 | 0.28110367 |
| 636.5 | 0.649 | 127.30 | 0.92975109 | 509.2 | 0.28099562 |
| 636.75 | 0.649 | 127.35 | 0.92977810 | 509.4 | 0.28088759 |
| 637 | 0.649 | 127.40 | 0.92980511 | 509.6 | 0.28077958 |


| 637.25 | 0.649 | 127.45 | 0.92983210 | 509.8 | 0.28067159 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 637.5 | 0.649 | 127.50 | 0.92985910 | 510.0 | 0.28056362 |
| 637.75 | 0.649 | 127.55 | 0.92988608 | 510.2 | 0.28045566 |
| 638 | 0.650 | 127.60 | 0.92991307 | 510.4 | 0.28034773 |
| 638.25 | 0.650 | 127.65 | 0.92994004 | 510.6 | 0.28023982 |
| 638.5 | 0.650 | 127.70 | 0.92996702 | 510.8 | 0.28013193 |
| 638.75 | 0.650 | 127.75 | 0.92999399 | 511.0 | 0.28002406 |
| 639 | 0.650 | 127.80 | 0.93002095 | 511.2 | 0.27991621 |
| 639.25 | 0.650 | 127.85 | 0.93004791 | 511.4 | 0.27980837 |
| 639.5 | 0.650 | 127.90 | 0.93007486 | 511.6 | 0.27970056 |
| 639.75 | 0.651 | 127.95 | 0.93010181 | 511.8 | 0.27959277 |
| 640 | 0.651 | 128.00 | 0.93012875 | 512.0 | 0.27948500 |
| 640.25 | 0.651 | 128.05 | 0.93015569 | 512.2 | 0.27937724 |
| 640.5 | 0.651 | 128.10 | 0.93018262 | 512.4 | 0.27926951 |
| 640.75 | 0.651 | 128.15 | 0.93020955 | 512.6 | 0.27916180 |
| 641 | 0.651 | 128.20 | 0.93023647 | 512.8 | 0.27905410 |
| 641.25 | 0.651 | 128.25 | 0.93026339 | 513.0 | 0.27894643 |
| 641.5 | 0.651 | 128.30 | 0.93029031 | 513.2 | 0.27883877 |
| 641.75 | 0.652 | 128.35 | 0.93031721 | 513.4 | 0.27873114 |
| 642 | 0.652 | 128.40 | 0.93034412 | 513.6 | 0.27862353 |
| 642.25 | 0.652 | 128.45 | 0.93037102 | 513.8 | 0.27851593 |
| 642.5 | 0.652 | 128.50 | 0.93039791 | 514.0 | 0.27840835 |
| 642.75 | 0.652 | 128.55 | 0.93042480 | 514.2 | 0.27830080 |
| 643 | 0.652 | 128.60 | 0.93045168 | 514.4 | 0.27819326 |
| 643.25 | 0.652 | 128.65 | 0.93047856 | 514.6 | 0.27808575 |
| 643.5 | 0.653 | 128.70 | 0.93050544 | 514.8 | 0.27797825 |
| 643.75 | 0.653 | 128.75 | 0.93053231 | 515.0 | 0.27787077 |
| 644 | 0.653 | 128.80 | 0.93055917 | 515.2 | 0.27776332 |
| 644.25 | 0.653 | 128.85 | 0.93058603 | 515.4 | 0.27765588 |
| 644.5 | 0.653 | 128.90 | 0.93061289 | 515.6 | 0.27754846 |
| 644.75 | 0.653 | 128.95 | 0.93063974 | 515.8 | 0.27744106 |
| 645 | 0.653 | 129.00 | 0.93066658 | 516.0 | 0.27733368 |
| 645.25 | 0.653 | 129.05 | 0.93069342 | 516.2 | 0.27722632 |
| 645.5 | 0.654 | 129.10 | 0.93072025 | 516.4 | 0.27711898 |
| 645.75 | 0.654 | 129.15 | 0.93074708 | 516.6 | 0.27701166 |
| 646 | 0.654 | 129.20 | 0.93077391 | 516.8 | 0.27690436 |
| 646.25 | 0.654 | 129.25 | 0.93080073 | 517.0 | 0.27679708 |
| 646.5 | 0.654 | 129.30 | 0.93082755 | 517.2 | 0.27668982 |
| 646.75 | 0.654 | 129.35 | 0.93085436 | 517.4 | 0.27658257 |
| 647 | 0.654 | 129.40 | 0.93088116 | 517.6 | 0.27647535 |
| 647.25 | 0.655 | 129.45 | 0.93090796 | 517.8 | 0.27636815 |
| 647.5 | 0.655 | 129.50 | 0.93093476 | 518.0 | 0.27626096 |
| 647.75 | 0.655 | 129.55 | 0.93096155 | 518.2 | 0.27615380 |
| 648 | 0.655 | 129.60 | 0.93098834 | 518.4 | 0.27604665 |
| 648.25 | 0.655 | 129.65 | 0.93101512 | 518.6 | 0.27593953 |
| 648.5 | 0.655 | 129.70 | 0.93104189 | 518.8 | 0.27583242 |
| 648.75 | 0.655 | 129.75 | 0.93106867 | 519.0 | 0.27572533 |
| 649 | 0.655 | 129.80 | 0.93109543 | 519.2 | 0.27561827 |
| 649.25 | 0.656 | 129.85 | 0.93112220 | 519.4 | 0.27551122 |
| 649.5 | 0.656 | 129.90 | 0.93114895 | 519.6 | 0.27540419 |
| 649.75 | 0.656 | 129.95 | 0.93117571 | 519.8 | 0.27529718 |
| 650 | 0.656 | 130.00 | 0.93120245 | 520.0 | 0.27519019 |
| 650.25 | 0.656 | 130.05 | 0.93122920 | 520.2 | 0.27508322 |
| 650.5 | 0.656 | 130.10 | 0.93125593 | 520.4 | 0.27497627 |
| 650.75 | 0.656 | 130.15 | 0.93128267 | 520.6 | 0.27486933 |
| 651 | 0.657 | 130.20 | 0.93130939 | 520.8 | 0.27476242 |
| 651.25 | 0.657 | 130.25 | 0.93133612 | 521.0 | 0.27465553 |
| 651.5 | 0.657 | 130.30 | 0.93136284 | 521.2 | 0.27454865 |
| 651.75 | 0.657 | 130.35 | 0.93138955 | 521.4 | 0.27444180 |
| 652 | 0.657 | 130.40 | 0.93141626 | 521.6 | 0.27433496 |
| 652.25 | 0.657 | 130.45 | 0.93144296 | 521.8 | 0.27422815 |
| 652.5 | 0.657 | 130.50 | 0.93146966 | 522.0 | 0.27412135 |
| 652.75 | 0.657 | 130.55 | 0.93149636 | 522.2 | 0.27401457 |
| 653 | 0.658 | 130.60 | 0.93152305 | 522.4 | 0.27390781 |
| 653.25 | 0.658 | 130.65 | 0.93154973 | 522.6 | 0.27380107 |
| 653.5 | 0.658 | 130.70 | 0.93157641 | 522.8 | 0.27369435 |
| 653.75 | 0.658 | 130.75 | 0.93160309 | 523.0 | 0.27358765 |
| 654 | 0.658 | 130.80 | 0.93162976 | 523.2 | 0.27348097 |
| 654.25 | 0.658 | 130.85 | 0.93165642 | 523.4 | 0.27337431 |
| 654.5 | 0.658 | 130.90 | 0.93168308 | 523.6 | 0.27326766 |
| 654.75 | 0.659 | 130.95 | 0.93170974 | 523.8 | 0.27316104 |


| 655 | 0.659 | 131.00 | 0.93173639 | 524.0 | 0.27305443 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 655.25 | 0.659 | 131.05 | 0.93176304 | 524.2 | 0.27294785 |
| 655.5 | 0.659 | 131.10 | 0.93178968 | 524.4 | 0.27284128 |
| 655.75 | 0.659 | 131.15 | 0.93181632 | 524.6 | 0.27273473 |
| 656 | 0.659 | 131.20 | 0.93184295 | 524.8 | 0.27262820 |
| 656.25 | 0.659 | 131.25 | 0.93186958 | 525.0 | 0.27252169 |
| 656.5 | 0.659 | 131.30 | 0.93189620 | 525.2 | 0.27241520 |
| 656.75 | 0.660 | 131.35 | 0.93192282 | 525.4 | 0.27230873 |
| 657 | 0.660 | 131.40 | 0.93194943 | 525.6 | 0.27220228 |
| 657.25 | 0.660 | 131.45 | 0.93197604 | 525.8 | 0.27209584 |
| 657.5 | 0.660 | 131.50 | 0.93200264 | 526.0 | 0.27198943 |
| 657.75 | 0.660 | 131.55 | 0.93202924 | 526.2 | 0.27188303 |
| 658 | 0.660 | 131.60 | 0.93205584 | 526.4 | 0.27177666 |
| 658.25 | 0.660 | 131.65 | 0.93208243 | 526.6 | 0.27167030 |
| 658.5 | 0.661 | 131.70 | 0.93210901 | 526.8 | 0.27156396 |
| 658.75 | 0.661 | 131.75 | 0.93213559 | 527.0 | 0.27145764 |
| 659 | 0.661 | 131.80 | 0.93216217 | 527.2 | 0.27135134 |
| 659.25 | 0.661 | 131.85 | 0.93218874 | 527.4 | 0.27124506 |
| 659.5 | 0.661 | 131.90 | 0.93221530 | 527.6 | 0.27113880 |
| 659.75 | 0.661 | 131.95 | 0.93224186 | 527.8 | 0.27103255 |
| 660 | 0.661 | 132.00 | 0.93226842 | 528.0 | 0.27092633 |
| 660.25 | 0.661 | 132.05 | 0.93229497 | 528.2 | 0.27082012 |
| 660.5 | 0.662 | 132.10 | 0.93232152 | 528.4 | 0.27071393 |
| 660.75 | 0.662 | 132.15 | 0.93234806 | 528.6 | 0.27060776 |
| 661 | 0.662 | 132.20 | 0.93237460 | 528.8 | 0.27050162 |
| 661.25 | 0.662 | 132.25 | 0.93240113 | 529.0 | 0.27039548 |
| 661.5 | 0.662 | 132.30 | 0.93242766 | 529.2 | 0.27028937 |
| 661.75 | 0.662 | 132.35 | 0.93245418 | 529.4 | 0.27018328 |
| 662 | 0.662 | 132.40 | 0.93248070 | 529.6 | 0.27007721 |
| 662.25 | 0.663 | 132.45 | 0.93250721 | 529.8 | 0.26997115 |
| 662.5 | 0.663 | 132.50 | 0.93253372 | 530.0 | 0.26986511 |
| 662.75 | 0.663 | 132.55 | 0.93256023 | 530.2 | 0.26975910 |
| 663 | 0.663 | 132.60 | 0.93258673 | 530.4 | 0.26965310 |
| 663.25 | 0.663 | 132.65 | 0.93261322 | 530.6 | 0.26954712 |
| 663.5 | 0.663 | 132.70 | 0.93263971 | 530.8 | 0.26944116 |
| 663.75 | 0.663 | 132.75 | 0.93266620 | 531.0 | 0.26933521 |
| 664 | 0.663 | 132.80 | 0.93269268 | 531.2 | 0.26922929 |
| 664.25 | 0.664 | 132.85 | 0.93271915 | 531.4 | 0.26912339 |
| 664.5 | 0.664 | 132.90 | 0.93274563 | 531.6 | 0.26901750 |
| 664.75 | 0.664 | 132.95 | 0.93277209 | 531.8 | 0.26891163 |
| 665 | 0.664 | 133.00 | 0.93279855 | 532.0 | 0.26880578 |
| 665.25 | 0.664 | 133.05 | 0.93282501 | 532.2 | 0.26869995 |
| 665.5 | 0.664 | 133.10 | 0.93285146 | 532.4 | 0.26859414 |
| 665.75 | 0.664 | 133.15 | 0.93287791 | 532.6 | 0.26848835 |
| 666 | 0.665 | 133.20 | 0.93290436 | 532.8 | 0.26838257 |
| 666.25 | 0.665 | 133.25 | 0.93293080 | 533.0 | 0.26827682 |
| 666.5 | 0.665 | 133.30 | 0.93295723 | 533.2 | 0.26817108 |
| 666.75 | 0.665 | 133.35 | 0.93298366 | 533.4 | 0.26806536 |
| 667 | 0.665 | 133.40 | 0.93301008 | 533.6 | 0.26795967 |
| 667.25 | 0.665 | 133.45 | 0.93303650 | 533.8 | 0.26785398 |
| 667.5 | 0.665 | 133.50 | 0.93306292 | 534.0 | 0.26774832 |
| 667.75 | 0.665 | 133.55 | 0.93308933 | 534.2 | 0.26764268 |
| 668 | 0.666 | 133.60 | 0.93311574 | 534.4 | 0.26753705 |
| 668.25 | 0.666 | 133.65 | 0.93314214 | 534.6 | 0.26743145 |
| 668.5 | 0.666 | 133.70 | 0.93316854 | 534.8 | 0.26732586 |
| 668.75 | 0.666 | 133.75 | 0.93319493 | 535.0 | 0.26722029 |
| 669 | 0.666 | 133.80 | 0.93322132 | 535.2 | 0.26711474 |
| 669.25 | 0.666 | 133.85 | 0.93324770 | 535.4 | 0.26700921 |
| 669.5 | 0.666 | 133.90 | 0.93327408 | 535.6 | 0.26690369 |
| 669.75 | 0.667 | 133.95 | 0.93330045 | 535.8 | 0.26679820 |
| 670 | 0.667 | 134.00 | 0.93332682 | 536.0 | 0.26669272 |
| 670.25 | 0.667 | 134.05 | 0.93335318 | 536.2 | 0.26658726 |
| 670.5 | 0.667 | 134.10 | 0.93337954 | 536.4 | 0.26648182 |
| 670.75 | 0.667 | 134.15 | 0.93340590 | 536.6 | 0.26637640 |
| 671 | 0.667 | 134.20 | 0.93343225 | 536.8 | 0.26627100 |
| 671.25 | 0.667 | 134.25 | 0.93345860 | 537.0 | 0.26616561 |
| 671.5 | 0.667 | 134.30 | 0.93348494 | 537.2 | 0.26606025 |
| 671.75 | 0.668 | 134.35 | 0.93351127 | 537.4 | 0.26595490 |
| 672 | 0.668 | 134.40 | 0.93353761 | 537.6 | 0.26584957 |
| 672.25 | 0.668 | 134.45 | 0.93356393 | 537.8 | 0.26574426 |
| 672.5 | 0.668 | 134.50 | 0.93359026 | 538.0 | 0.26563897 |


| 672.75 | 0.668 | 134.55 | 0.93361658 | 538.2 | 0.26553370 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 673 | 0.668 | 134.60 | 0.93364289 | 538.4 | 0.26542844 |
| 673.25 | 0.668 | 134.65 | 0.93366920 | 538.6 | 0.26532320 |
| 673.5 | 0.668 | 134.70 | 0.93369550 | 538.8 | 0.26521798 |
| 673.75 | 0.669 | 134.75 | 0.93372180 | 539.0 | 0.26511278 |
| 674 | 0.669 | 134.80 | 0.93374810 | 539.2 | 0.26500760 |
| 674.25 | 0.669 | 134.85 | 0.93377439 | 539.4 | 0.26490244 |
| 674.5 | 0.669 | 134.90 | 0.93380068 | 539.6 | 0.26479729 |
| 674.75 | 0.669 | 134.95 | 0.93382696 | 539.8 | 0.26469217 |
| 675 | 0.669 | 135.00 | 0.93385324 | 540.0 | 0.26458706 |
| 675.25 | 0.669 | 135.05 | 0.93387951 | 540.2 | 0.26448197 |
| 675.5 | 0.670 | 135.10 | 0.93390578 | 540.4 | 0.26437689 |
| 675.75 | 0.670 | 135.15 | 0.93393204 | 540.6 | 0.26427184 |
| 676 | 0.670 | 135.20 | 0.93395830 | 540.8 | 0.26416680 |
| 676.25 | 0.670 | 135.25 | 0.93398455 | 541.0 | 0.26406179 |
| 676.5 | 0.670 | 135.30 | 0.93401080 | 541.2 | 0.26395679 |
| 676.75 | 0.670 | 135.35 | 0.93403705 | 541.4 | 0.26385181 |
| 677 | 0.670 | 135.40 | 0.93406329 | 541.6 | 0.26374684 |
| 677.25 | 0.670 | 135.45 | 0.93408952 | 541.8 | 0.26364190 |
| 677.5 | 0.671 | 135.50 | 0.93411576 | 542.0 | 0.26353697 |
| 677.75 | 0.671 | 135.55 | 0.93414198 | 542.2 | 0.26343207 |
| 678 | 0.671 | 135.60 | 0.93416821 | 542.4 | 0.26332718 |
| 678.25 | 0.671 | 135.65 | 0.93419442 | 542.6 | 0.26322230 |
| 678.5 | 0.671 | 135.70 | 0.93422064 | 542.8 | 0.26311745 |
| 678.75 | 0.671 | 135.75 | 0.93424685 | 543.0 | 0.26301262 |
| 679 | 0.671 | 135.80 | 0.93427305 | 543.2 | 0.26290780 |
| 679.25 | 0.671 | 135.85 | 0.93429925 | 543.4 | 0.26280300 |
| 679.5 | 0.672 | 135.90 | 0.93432545 | 543.6 | 0.26269822 |
| 679.75 | 0.672 | 135.95 | 0.93435164 | 543.8 | 0.26259346 |
| 680 | 0.672 | 136.00 | 0.93437782 | 544.0 | 0.26248871 |
| 680.25 | 0.672 | 136.05 | 0.93440400 | 544.2 | 0.26238398 |
| 680.5 | 0.672 | 136.10 | 0.93443018 | 544.4 | 0.26227928 |
| 680.75 | 0.672 | 136.15 | 0.93445635 | 544.6 | 0.26217459 |
| 681 | 0.672 | 136.20 | 0.93448252 | 544.8 | 0.26206991 |
| 681.25 | 0.673 | 136.25 | 0.93450869 | 545.0 | 0.26196526 |
| 681.5 | 0.673 | 136.30 | 0.93453484 | 545.2 | 0.26186062 |
| 681.75 | 0.673 | 136.35 | 0.93456100 | 545.4 | 0.26175600 |
| 682 | 0.673 | 136.40 | 0.93458715 | 545.6 | 0.26165140 |
| 682.25 | 0.673 | 136.45 | 0.93461329 | 545.8 | 0.26154682 |
| 682.5 | 0.673 | 136.50 | 0.93463944 | 546.0 | 0.26144226 |
| 682.75 | 0.673 | 136.55 | 0.93466557 | 546.2 | 0.26133771 |
| 683 | 0.673 | 136.60 | 0.93469170 | 546.4 | 0.26123318 |
| 683.25 | 0.674 | 136.65 | 0.93471783 | 546.6 | 0.26112867 |
| 683.5 | 0.674 | 136.70 | 0.93474395 | 546.8 | 0.26102418 |
| 683.75 | 0.674 | 136.75 | 0.93477007 | 547.0 | 0.26091971 |
| 684 | 0.674 | 136.80 | 0.93479619 | 547.2 | 0.26081525 |
| 684.25 | 0.674 | 136.85 | 0.93482230 | 547.4 | 0.26071081 |
| 684.5 | 0.674 | 136.90 | 0.93484840 | 547.6 | 0.26060639 |
| 684.75 | 0.674 | 136.95 | 0.93487450 | 547.8 | 0.26050199 |
| 685 | 0.675 | 137.00 | 0.93490060 | 548.0 | 0.26039760 |
| 685.25 | 0.675 | 137.05 | 0.93492669 | 548.2 | 0.26029324 |
| 685.5 | 0.675 | 137.10 | 0.93495278 | 548.4 | 0.26018889 |
| 685.75 | 0.675 | 137.15 | 0.93497886 | 548.6 | 0.26008456 |
| 686 | 0.675 | 137.20 | 0.93500494 | 548.8 | 0.25998024 |
| 686.25 | 0.675 | 137.25 | 0.93503101 | 549.0 | 0.25987595 |
| 686.5 | 0.675 | 137.30 | 0.93505708 | 549.2 | 0.25977167 |
| 686.75 | 0.675 | 137.35 | 0.93508315 | 549.4 | 0.25966741 |
| 687 | 0.676 | 137.40 | 0.93510921 | 549.6 | 0.25956317 |
| 687.25 | 0.676 | 137.45 | 0.93513526 | 549.8 | 0.25945895 |
| 687.5 | 0.676 | 137.50 | 0.93516131 | 550.0 | 0.25935474 |
| 687.75 | 0.676 | 137.55 | 0.93518736 | 550.2 | 0.25925055 |
| 688 | 0.676 | 137.60 | 0.93521340 | 550.4 | 0.25914638 |
| 688.25 | 0.676 | 137.65 | 0.93523944 | 550.6 | 0.25904223 |
| 688.5 | 0.676 | 137.70 | 0.93526548 | 550.8 | 0.25893810 |
| 688.75 | 0.676 | 137.75 | 0.93529151 | 551.0 | 0.25883398 |
| 689 | 0.677 | 137.80 | 0.93531753 | 551.2 | 0.25872988 |
| 689.25 | 0.677 | 137.85 | 0.93534355 | 551.4 | 0.25862580 |
| 689.5 | 0.677 | 137.90 | 0.93536957 | 551.6 | 0.25852173 |
| 689.75 | 0.677 | 137.95 | 0.93539558 | 551.8 | 0.25841769 |
| 690 | 0.677 | 138.00 | 0.93542159 | 552.0 | 0.25831366 |
| 690.25 | 0.677 | 138.05 | 0.93544759 | 552.2 | 0.25820965 |


| 690.5 | 0.677 | 138.10 | 0.93547359 | 552.4 | 0.25810566 |
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| 690.75 | 0.677 | 138.15 | 0.93549958 | 552.6 | 0.25800168 |
| 691 | 0.678 | 138.20 | 0.93552557 | 552.8 | 0.25789772 |
| 691.25 | 0.678 | 138.25 | 0.93555155 | 553.0 | 0.25779378 |
| 691.5 | 0.678 | 138.30 | 0.93557753 | 553.2 | 0.25768986 |
| 691.75 | 0.678 | 138.35 | 0.93560351 | 553.4 | 0.25758596 |
| 692 | 0.678 | 138.40 | 0.93562948 | 553.6 | 0.25748207 |
| 692.25 | 0.678 | 138.45 | 0.93565545 | 553.8 | 0.25737820 |
| 692.5 | 0.678 | 138.50 | 0.93568141 | 554.0 | 0.25727435 |
| 692.75 | 0.679 | 138.55 | 0.93570737 | 554.2 | 0.25717051 |
| 693 | 0.679 | 138.60 | 0.93573333 | 554.4 | 0.25706670 |
| 693.25 | 0.679 | 138.65 | 0.93575928 | 554.6 | 0.25696290 |
| 693.5 | 0.679 | 138.70 | 0.93578522 | 554.8 | 0.25685912 |
| 693.75 | 0.679 | 138.75 | 0.93581116 | 555.0 | 0.25675535 |
| 694 | 0.679 | 138.80 | 0.93583710 | 555.2 | 0.25665161 |
| 694.25 | 0.679 | 138.85 | 0.93586303 | 555.4 | 0.25654788 |
| 694.5 | 0.679 | 138.90 | 0.93588896 | 555.6 | 0.25644417 |
| 694.75 | 0.680 | 138.95 | 0.93591488 | 555.8 | 0.25634048 |
| 695 | 0.680 | 139.00 | 0.93594080 | 556.0 | 0.25623680 |
| 695.25 | 0.680 | 139.05 | 0.93596671 | 556.2 | 0.25613314 |
| 695.5 | 0.680 | 139.10 | 0.93599262 | 556.4 | 0.25602950 |
| 695.75 | 0.680 | 139.15 | 0.93601853 | 556.6 | 0.25592588 |
| 696 | 0.680 | 139.20 | 0.93604443 | 556.8 | 0.25582227 |
| 696.25 | 0.680 | 139.25 | 0.93607033 | 557.0 | 0.25571868 |
| 696.5 | 0.680 | 139.30 | 0.93609622 | 557.2 | 0.25561511 |
| 696.75 | 0.681 | 139.35 | 0.93612211 | 557.4 | 0.25551156 |
| 697 | 0.681 | 139.40 | 0.93614799 | 557.6 | 0.25540802 |
| 697.25 | 0.681 | 139.45 | 0.93617387 | 557.8 | 0.25530451 |
| 697.5 | 0.681 | 139.50 | 0.93619975 | 558.0 | 0.25520100 |
| 697.75 | 0.681 | 139.55 | 0.93622562 | 558.2 | 0.25509752 |
| 698 | 0.681 | 139.60 | 0.93625149 | 558.4 | 0.25499405 |
| 698.25 | 0.681 | 139.65 | 0.93627735 | 558.6 | 0.25489061 |
| 698.5 | 0.682 | 139.70 | 0.93630321 | 558.8 | 0.25478717 |
| 698.75 | 0.682 | 139.75 | 0.93632906 | 559.0 | 0.25468376 |
| 699 | 0.682 | 139.80 | 0.93635491 | 559.2 | 0.25458036 |
| 699.25 | 0.682 | 139.85 | 0.93638075 | 559.4 | 0.25447698 |
| 699.5 | 0.682 | 139.90 | 0.93640659 | 559.6 | 0.25437362 |
| 699.75 | 0.682 | 139.95 | 0.93643243 | 559.8 | 0.25427028 |
| 700 | 0.682 | 140.00 | 0.93645826 | 560.0 | 0.25416695 |
| 700.25 | 0.682 | 140.05 | 0.93648409 | 560.2 | 0.25406364 |
| 700.5 | 0.683 | 140.10 | 0.93650991 | 560.4 | 0.25396035 |
| 700.75 | 0.683 | 140.15 | 0.93653573 | 560.6 | 0.25385707 |
| 701 | 0.683 | 140.20 | 0.93656155 | 560.8 | 0.25375382 |
| 701.25 | 0.683 | 140.25 | 0.93658736 | 561.0 | 0.25365058 |
| 701.5 | 0.683 | 140.30 | 0.93661316 | 561.2 | 0.25354735 |
| 701.75 | 0.683 | 140.35 | 0.93663896 | 561.4 | 0.25344415 |
| 702 | 0.683 | 140.40 | 0.93666476 | 561.6 | 0.25334096 |
| 702.25 | 0.683 | 140.45 | 0.93669055 | 561.8 | 0.25323779 |
| 702.5 | 0.684 | 140.50 | 0.93671634 | 562.0 | 0.25313463 |
| 702.75 | 0.684 | 140.55 | 0.93674213 | 562.2 | 0.25303150 |
| 703 | 0.684 | 140.60 | 0.93676791 | 562.4 | 0.25292838 |
| 703.25 | 0.684 | 140.65 | 0.93679368 | 562.6 | 0.25282527 |
| 703.5 | 0.684 | 140.70 | 0.93681945 | 562.8 | 0.25272219 |
| 703.75 | 0.684 | 140.75 | 0.93684522 | 563.0 | 0.25261912 |
| 704 | 0.684 | 140.80 | 0.93687098 | 563.2 | 0.25251607 |
| 704.25 | 0.684 | 140.85 | 0.93689674 | 563.4 | 0.25241304 |
| 704.5 | 0.685 | 140.90 | 0.93692249 | 563.6 | 0.25231002 |
| 704.75 | 0.685 | 140.95 | 0.93694824 | 563.8 | 0.25220702 |
| 705 | 0.685 | 141.00 | 0.93697399 | 564.0 | 0.25210404 |
| 705.25 | 0.685 | 141.05 | 0.93699973 | 564.2 | 0.25200108 |
| 705.5 | 0.685 | 141.10 | 0.93702547 | 564.4 | 0.25189813 |
| 705.75 | 0.685 | 141.15 | 0.93705120 | 564.6 | 0.25179520 |
| 706 | 0.685 | 141.20 | 0.93707693 | 564.8 | 0.25169228 |
| 706.25 | 0.686 | 141.25 | 0.93710265 | 565.0 | 0.25158939 |
| 706.5 | 0.686 | 141.30 | 0.93712837 | 565.2 | 0.25148651 |
| 706.75 | 0.686 | 141.35 | 0.93715409 | 565.4 | 0.25138365 |
| 707 | 0.686 | 141.40 | 0.93717980 | 565.6 | 0.25128080 |
| 707.25 | 0.686 | 141.45 | 0.93720551 | 565.8 | 0.25117797 |
| 707.5 | 0.686 | 141.50 | 0.93723121 | 566.0 | 0.25107516 |
| 707.75 | 0.686 | 141.55 | 0.93725691 | 566.2 | 0.25097237 |
| 708 | 0.686 | 141.60 | 0.93728260 | 566.4 | 0.25086959 |


| 708.25 | 0.687 | 141.65 | 0.93730829 | 566.6 | 0.25076683 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 708.5 | 0.687 | 141.70 | 0.93733398 | 566.8 | 0.25066409 |
| 708.75 | 0.687 | 141.75 | 0.93735966 | 567.0 | 0.25056137 |
| 709 | 0.687 | 141.80 | 0.93738534 | 567.2 | 0.25045866 |
| 709.25 | 0.687 | 141.85 | 0.93741101 | 567.4 | 0.25035597 |
| 709.5 | 0.687 | 141.90 | 0.93743668 | 567.6 | 0.25025329 |
| 709.75 | 0.687 | 141.95 | 0.93746234 | 567.8 | 0.25015063 |
| 710 | 0.687 | 142.00 | 0.93748800 | 568.0 | 0.25004799 |
| 710.25 | 0.688 | 142.05 | 0.93751366 | 568.2 | 0.24994537 |
| 710.5 | 0.688 | 142.10 | 0.93753931 | 568.4 | 0.24984276 |
| 710.75 | 0.688 | 142.15 | 0.93756496 | 568.6 | 0.24974017 |
| 711 | 0.688 | 142.20 | 0.93759060 | 568.8 | 0.24963760 |
| 711.25 | 0.688 | 142.25 | 0.93761624 | 569.0 | 0.24953505 |
| 711.5 | 0.688 | 142.30 | 0.93764187 | 569.2 | 0.24943251 |
| 711.75 | 0.688 | 142.35 | 0.93766750 | 569.4 | 0.24932999 |
| 712 | 0.688 | 142.40 | 0.93769313 | 569.6 | 0.24922748 |
| 712.25 | 0.689 | 142.45 | 0.93771875 | 569.8 | 0.24912499 |
| 712.5 | 0.689 | 142.50 | 0.93774437 | 570.0 | 0.24902252 |
| 712.75 | 0.689 | 142.55 | 0.93776998 | 570.2 | 0.24892007 |
| 713 | 0.689 | 142.60 | 0.93779559 | 570.4 | 0.24881763 |
| 713.25 | 0.689 | 142.65 | 0.93782120 | 570.6 | 0.24871521 |
| 713.5 | 0.689 | 142.70 | 0.93784680 | 570.8 | 0.24861281 |
| 713.75 | 0.689 | 142.75 | 0.93787239 | 571.0 | 0.24851042 |
| 714 | 0.689 | 142.80 | 0.93789799 | 571.2 | 0.24840805 |
| 714.25 | 0.690 | 142.85 | 0.93792358 | 571.4 | 0.24830570 |
| 714.5 | 0.690 | 142.90 | 0.93794916 | 571.6 | 0.24820336 |
| 714.75 | 0.690 | 142.95 | 0.93797474 | 571.8 | 0.24810104 |
| 715 | 0.690 | 143.00 | 0.93800031 | 572.0 | 0.24799874 |
| 715.25 | 0.690 | 143.05 | 0.93802589 | 572.2 | 0.24789646 |
| 715.5 | 0.690 | 143.10 | 0.93805145 | 572.4 | 0.24779419 |
| 715.75 | 0.690 | 143.15 | 0.93807702 | 572.6 | 0.24769193 |
| 716 | 0.691 | 143.20 | 0.93810258 | 572.8 | 0.24758970 |
| 716.25 | 0.691 | 143.25 | 0.93812813 | 573.0 | 0.24748748 |
| 716.5 | 0.691 | 143.30 | 0.93815368 | 573.2 | 0.24738528 |
| 716.75 | 0.691 | 143.35 | 0.93817923 | 573.4 | 0.24728309 |
| 717 | 0.691 | 143.40 | 0.93820477 | 573.6 | 0.24718093 |
| 717.25 | 0.691 | 143.45 | 0.93823031 | 573.8 | 0.24707878 |
| 717.5 | 0.691 | 143.50 | 0.93825584 | 574.0 | 0.24697664 |
| 717.75 | 0.691 | 143.55 | 0.93828137 | 574.2 | 0.24687452 |
| 718 | 0.692 | 143.60 | 0.93830689 | 574.4 | 0.24677242 |
| 718.25 | 0.692 | 143.65 | 0.93833242 | 574.6 | 0.24667034 |
| 718.5 | 0.692 | 143.70 | 0.93835793 | 574.8 | 0.24656827 |
| 718.75 | 0.692 | 143.75 | 0.93838345 | 575.0 | 0.24646622 |
| 719 | 0.692 | 143.80 | 0.93840895 | 575.2 | 0.24636418 |
| 719.25 | 0.692 | 143.85 | 0.93843446 | 575.4 | 0.24626217 |
| 719.5 | 0.692 | 143.90 | 0.93845996 | 575.6 | 0.24616016 |
| 719.75 | 0.692 | 143.95 | 0.93848545 | 575.8 | 0.24605818 |
| 720 | 0.693 | 144.00 | 0.93851095 | 576.0 | 0.24595621 |
| 720.25 | 0.693 | 144.05 | 0.93853643 | 576.2 | 0.24585426 |
| 720.5 | 0.693 | 144.10 | 0.93856192 | 576.4 | 0.24575233 |
| 720.75 | 0.693 | 144.15 | 0.93858740 | 576.6 | 0.24565041 |
| 721 | 0.693 | 144.20 | 0.93861287 | 576.8 | 0.24554851 |
| 721.25 | 0.693 | 144.25 | 0.93863834 | 577.0 | 0.24544662 |
| 721.5 | 0.693 | 144.30 | 0.93866381 | 577.2 | 0.24534476 |
| 721.75 | 0.693 | 144.35 | 0.93868927 | 577.4 | 0.24524290 |
| 722 | 0.694 | 144.40 | 0.93871473 | 577.6 | 0.24514107 |
| 722.25 | 0.694 | 144.45 | 0.93874019 | 577.8 | 0.24503925 |
| 722.5 | 0.694 | 144.50 | 0.93876564 | 578.0 | 0.24493745 |
| 722.75 | 0.694 | 144.55 | 0.93879108 | 578.2 | 0.24483566 |
| 723 | 0.694 | 144.60 | 0.93881653 | 578.4 | 0.24473389 |
| 723.25 | 0.694 | 144.65 | 0.93884196 | 578.6 | 0.24463214 |
| 723.5 | 0.694 | 144.70 | 0.93886740 | 578.8 | 0.24453041 |
| 723.75 | 0.694 | 144.75 | 0.93889283 | 579.0 | 0.24442869 |
| 724 | 0.695 | 144.80 | 0.93891825 | 579.2 | 0.24432699 |
| 724.25 | 0.695 | 144.85 | 0.93894368 | 579.4 | 0.24422530 |
| 724.5 | 0.695 | 144.90 | 0.93896909 | 579.6 | 0.24412363 |
| 724.75 | 0.695 | 144.95 | 0.93899451 | 579.8 | 0.24402198 |
| 725 | 0.695 | 145.00 | 0.93901991 | 580.0 | 0.24392034 |
| 725.25 | 0.695 | 145.05 | 0.93904532 | 580.2 | 0.24381872 |
| 725.5 | 0.695 | 145.10 | 0.93907072 | 580.4 | 0.24371712 |
| 725.75 | 0.695 | 145.15 | 0.93909612 | 580.6 | 0.24361553 |


| 726 | 0.696 | 145.20 | 0.93912151 | 580.8 | 0.24351396 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 726.25 | 0.696 | 145.25 | 0.93914690 | 581.0 | 0.24341240 |
| 726.5 | 0.696 | 145.30 | 0.93917228 | 581.2 | 0.24331087 |
| 726.75 | 0.696 | 145.35 | 0.93919766 | 581.4 | 0.24320934 |
| 727 | 0.696 | 145.40 | 0.93922304 | 581.6 | 0.24310784 |
| 727.25 | 0.696 | 145.45 | 0.93924841 | 581.8 | 0.24300635 |
| 727.5 | 0.696 | 145.50 | 0.93927378 | 582.0 | 0.24290488 |
| 727.75 | 0.696 | 145.55 | 0.93929914 | 582.2 | 0.24280342 |
| 728 | 0.697 | 145.60 | 0.93932450 | 582.4 | 0.24270198 |
| 728.25 | 0.697 | 145.65 | 0.93934986 | 582.6 | 0.24260056 |
| 728.5 | 0.697 | 145.70 | 0.93937521 | 582.8 | 0.24249915 |
| 728.75 | 0.697 | 145.75 | 0.93940056 | 583.0 | 0.24239776 |
| 729 | 0.697 | 145.80 | 0.93942590 | 583.2 | 0.24229639 |
| 729.25 | 0.697 | 145.85 | 0.93945124 | 583.4 | 0.24219503 |
| 729.5 | 0.697 | 145.90 | 0.93947658 | 583.6 | 0.24209369 |
| 729.75 | 0.698 | 145.95 | 0.93950191 | 583.8 | 0.24199237 |
| 730 | 0.698 | 146.00 | 0.93952724 | 584.0 | 0.24189106 |
| 730.25 | 0.698 | 146.05 | 0.93955256 | 584.2 | 0.24178976 |
| 730.5 | 0.698 | 146.10 | 0.93957788 | 584.4 | 0.24168849 |
| 730.75 | 0.698 | 146.15 | 0.93960319 | 584.6 | 0.24158723 |
| 731 | 0.698 | 146.20 | 0.93962850 | 584.8 | 0.24148598 |
| 731.25 | 0.698 | 146.25 | 0.93965381 | 585.0 | 0.24138476 |
| 731.5 | 0.698 | 146.30 | 0.93967911 | 585.2 | 0.24128355 |
| 731.75 | 0.699 | 146.35 | 0.93970441 | 585.4 | 0.24118235 |
| 732 | 0.699 | 146.40 | 0.93972971 | 585.6 | 0.24108117 |
| 732.25 | 0.699 | 146.45 | 0.93975500 | 585.8 | 0.24098001 |
| 732.5 | 0.699 | 146.50 | 0.93978028 | 586.0 | 0.24087886 |
| 732.75 | 0.699 | 146.55 | 0.93980557 | 586.2 | 0.24077773 |
| 733 | 0.699 | 146.60 | 0.93983084 | 586.4 | 0.24067662 |
| 733.25 | 0.699 | 146.65 | 0.93985612 | 586.6 | 0.24057552 |
| 733.5 | 0.699 | 146.70 | 0.93988139 | 586.8 | 0.24047444 |
| 733.75 | 0.700 | 146.75 | 0.93990666 | 587.0 | 0.24037338 |
| 734 | 0.700 | 146.80 | 0.93993192 | 587.2 | 0.24027233 |
| 734.25 | 0.700 | 146.85 | 0.93995718 | 587.4 | 0.24017130 |
| 734.5 | 0.700 | 146.90 | 0.93998243 | 587.6 | 0.24007028 |
| 734.75 | 0.700 | 146.95 | 0.94000768 | 587.8 | 0.23996928 |
| 735 | 0.700 | 147.00 | 0.94003293 | 588.0 | 0.23986829 |
| 735.25 | 0.700 | 147.05 | 0.94005817 | 588.2 | 0.23976733 |
| 735.5 | 0.700 | 147.10 | 0.94008341 | 588.4 | 0.23966637 |
| 735.75 | 0.701 | 147.15 | 0.94010864 | 588.6 | 0.23956544 |
| 736 | 0.701 | 147.20 | 0.94013387 | 588.8 | 0.23946452 |
| 736.25 | 0.701 | 147.25 | 0.94015910 | 589.0 | 0.23936362 |
| 736.5 | 0.701 | 147.30 | 0.94018432 | 589.2 | 0.23926273 |
| 736.75 | 0.701 | 147.35 | 0.94020954 | 589.4 | 0.23916186 |
| 737 | 0.701 | 147.40 | 0.94023475 | 589.6 | 0.23906100 |
| 737.25 | 0.701 | 147.45 | 0.94025996 | 589.8 | 0.23896016 |
| 737.5 | 0.701 | 147.50 | 0.94028517 | 590.0 | 0.23885934 |
| 737.75 | 0.702 | 147.55 | 0.94031037 | 590.2 | 0.23875853 |
| 738 | 0.702 | 147.60 | 0.94033556 | 590.4 | 0.23865774 |
| 738.25 | 0.702 | 147.65 | 0.94036076 | 590.6 | 0.23855697 |
| 738.5 | 0.702 | 147.70 | 0.94038595 | 590.8 | 0.23845621 |
| 738.75 | 0.702 | 147.75 | 0.94041113 | 591.0 | 0.23835546 |
| 739 | 0.702 | 147.80 | 0.94043632 | 591.2 | 0.23825474 |
| 739.25 | 0.702 | 147.85 | 0.94046149 | 591.4 | 0.23815403 |
| 739.5 | 0.702 | 147.90 | 0.94048667 | 591.6 | 0.23805333 |
| 739.75 | 0.703 | 147.95 | 0.94051184 | 591.8 | 0.23795265 |
| 740 | 0.703 | 148.00 | 0.94053700 | 592.0 | 0.23785199 |
| 740.25 | 0.703 | 148.05 | 0.94056216 | 592.2 | 0.23775134 |
| 740.5 | 0.703 | 148.10 | 0.94058732 | 592.4 | 0.23765071 |
| 740.75 | 0.703 | 148.15 | 0.94061248 | 592.6 | 0.23755010 |
| 741 | 0.703 | 148.20 | 0.94063763 | 592.8 | 0.23744950 |
| 741.25 | 0.703 | 148.25 | 0.94066277 | 593.0 | 0.23734892 |
| 741.5 | 0.703 | 148.30 | 0.94068791 | 593.2 | 0.23724835 |
| 741.75 | 0.704 | 148.35 | 0.94071305 | 593.4 | 0.23714780 |
| 742 | 0.704 | 148.40 | 0.94073818 | 593.6 | 0.23704726 |
| 742.25 | 0.704 | 148.45 | 0.94076331 | 593.8 | 0.23694674 |
| 742.5 | 0.704 | 148.50 | 0.94078844 | 594.0 | 0.23684624 |
| 742.75 | 0.704 | 148.55 | 0.94081356 | 594.2 | 0.23674575 |
| 743 | 0.704 | 148.60 | 0.94083868 | 594.4 | 0.23664528 |
| 743.25 | 0.704 | 148.65 | 0.94086379 | 594.6 | 0.23654482 |
| 743.5 | 0.704 | 148.70 | 0.94088890 | 594.8 | 0.23644438 |


| 743.75 | 0.705 | 148.75 | 0.94091401 | 595.0 | 0.23634396 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 744 | 0.705 | 148.80 | 0.94093911 | 595.2 | 0.23624355 |
| 744.25 | 0.705 | 148.85 | 0.94096421 | 595.4 | 0.23614316 |
| 744.5 | 0.705 | 148.90 | 0.94098930 | 595.6 | 0.23604278 |
| 744.75 | 0.705 | 148.95 | 0.94101439 | 595.8 | 0.23594242 |
| 745 | 0.705 | 149.00 | 0.94103948 | 596.0 | 0.23584208 |
| 745.25 | 0.705 | 149.05 | 0.94106456 | 596.2 | 0.23574175 |
| 745.5 | 0.705 | 149.10 | 0.94108964 | 596.4 | 0.23564144 |
| 745.75 | 0.706 | 149.15 | 0.94111472 | 596.6 | 0.23554114 |
| 746 | 0.706 | 149.20 | 0.94113979 | 596.8 | 0.23544086 |
| 746.25 | 0.706 | 149.25 | 0.94116485 | 597.0 | 0.23534059 |
| 746.5 | 0.706 | 149.30 | 0.94118991 | 597.2 | 0.23524034 |
| 746.75 | 0.706 | 149.35 | 0.94121497 | 597.4 | 0.23514011 |
| 747 | 0.706 | 149.40 | 0.94124003 | 597.6 | 0.23503989 |
| 747.25 | 0.706 | 149.45 | 0.94126508 | 597.8 | 0.23493969 |
| 747.5 | 0.706 | 149.50 | 0.94129012 | 598.0 | 0.23483950 |
| 747.75 | 0.707 | 149.55 | 0.94131517 | 598.2 | 0.23473933 |
| 748 | 0.707 | 149.60 | 0.94134021 | 598.4 | 0.23463917 |
| 748.25 | 0.707 | 149.65 | 0.94136524 | 598.6 | 0.23453903 |
| 748.5 | 0.707 | 149.70 | 0.94139027 | 598.8 | 0.23443891 |
| 748.75 | 0.707 | 149.75 | 0.94141530 | 599.0 | 0.23433880 |
| 749 | 0.707 | 149.80 | 0.94144032 | 599.2 | 0.23423871 |
| 749.25 | 0.707 | 149.85 | 0.94146534 | 599.4 | 0.23413863 |
| 749.5 | 0.707 | 149.90 | 0.94149036 | 599.6 | 0.23403857 |
| 749.75 | 0.708 | 149.95 | 0.94151537 | 599.8 | 0.23393853 |
| 750 | 0.708 | 150.00 | 0.94154038 | 600.0 | 0.23383850 |
| 750.25 | 0.708 | 150.05 | 0.94156538 | 600.2 | 0.23373848 |
| 750.5 | 0.708 | 150.10 | 0.94159038 | 600.4 | 0.23363848 |
| 750.75 | 0.708 | 150.15 | 0.94161537 | 600.6 | 0.23353850 |
| 751 | 0.708 | 150.20 | 0.94164037 | 600.8 | 0.23343853 |
| 751.25 | 0.708 | 150.25 | 0.94166535 | 601.0 | 0.23333858 |
| 751.5 | 0.708 | 150.30 | 0.94169034 | 601.2 | 0.23323865 |
| 751.75 | 0.709 | 150.35 | 0.94171532 | 601.4 | 0.23313873 |
| 752 | 0.709 | 150.40 | 0.94174029 | 601.6 | 0.23303882 |
| 752.25 | 0.709 | 150.45 | 0.94176527 | 601.8 | 0.23293893 |
| 752.5 | 0.709 | 150.50 | 0.94179023 | 602.0 | 0.23283906 |
| 752.75 | 0.709 | 150.55 | 0.94181520 | 602.2 | 0.23273920 |
| 753 | 0.709 | 150.60 | 0.94184016 | 602.4 | 0.23263936 |
| 753.25 | 0.709 | 150.65 | 0.94186512 | 602.6 | 0.23253953 |
| 753.5 | 0.709 | 150.70 | 0.94189007 | 602.8 | 0.23243972 |
| 753.75 | 0.710 | 150.75 | 0.94191502 | 603.0 | 0.23233993 |
| 754 | 0.710 | 150.80 | 0.94193996 | 603.2 | 0.23224015 |
| 754.25 | 0.710 | 150.85 | 0.94196490 | 603.4 | 0.23214038 |
| 754.5 | 0.710 | 150.90 | 0.94198984 | 603.6 | 0.23204063 |
| 754.75 | 0.710 | 150.95 | 0.94201477 | 603.8 | 0.23194090 |
| 755 | 0.710 | 151.00 | 0.94203970 | 604.0 | 0.23184118 |
| 755.25 | 0.710 | 151.05 | 0.94206463 | 604.2 | 0.23174148 |
| 755.5 | 0.710 | 151.10 | 0.94208955 | 604.4 | 0.23164179 |
| 755.75 | 0.711 | 151.15 | 0.94211447 | 604.6 | 0.23154212 |
| 756 | 0.711 | 151.20 | 0.94213938 | 604.8 | 0.23144247 |
| 756.25 | 0.711 | 151.25 | 0.94216429 | 605.0 | 0.23134283 |
| 756.5 | 0.711 | 151.30 | 0.94218920 | 605.2 | 0.23124320 |
| 756.75 | 0.711 | 151.35 | 0.94221410 | 605.4 | 0.23114359 |
| 757 | 0.711 | 151.40 | 0.94223900 | 605.6 | 0.23104400 |
| 757.25 | 0.711 | 151.45 | 0.94226389 | 605.8 | 0.23094442 |
| 757.5 | 0.711 | 151.50 | 0.94228879 | 606.0 | 0.23084486 |
| 757.75 | 0.712 | 151.55 | 0.94231367 | 606.2 | 0.23074531 |
| 758 | 0.712 | 151.60 | 0.94233856 | 606.4 | 0.23064578 |
| 758.25 | 0.712 | 151.65 | 0.94236343 | 606.6 | 0.23054626 |
| 758.5 | 0.712 | 151.70 | 0.94238831 | 606.8 | 0.23044676 |
| 758.75 | 0.712 | 151.75 | 0.94241318 | 607.0 | 0.23034727 |
| 759 | 0.712 | 151.80 | 0.94243805 | 607.2 | 0.23024780 |
| 759.25 | 0.712 | 151.85 | 0.94246291 | 607.4 | 0.23014835 |
| 759.5 | 0.712 | 151.90 | 0.94248777 | 607.6 | 0.23004891 |
| 759.75 | 0.713 | 151.95 | 0.94251263 | 607.8 | 0.22994949 |
| 760 | 0.713 | 152.00 | 0.94253748 | 608.0 | 0.22985008 |
| 760.25 | 0.713 | 152.05 | 0.94256233 | 608.2 | 0.22975068 |
| 760.5 | 0.713 | 152.10 | 0.94258717 | 608.4 | 0.22965131 |
| 760.75 | 0.713 | 152.15 | 0.94261201 | 608.6 | 0.22955194 |
| 761 | 0.713 | 152.20 | 0.94263685 | 608.8 | 0.22945260 |
| 761.25 | 0.713 | 152.25 | 0.94266168 | 609.0 | 0.22935326 |


| 761.5 | 0.713 | 152.30 | 0.94268651 | 609.2 | 0.22925395 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 761.75 | 0.714 | 152.35 | 0.94271134 | 609.4 | 0.22915465 |
| 762 | 0.714 | 152.40 | 0.94273616 | 609.6 | 0.22905536 |
| 762.25 | 0.714 | 152.45 | 0.94276098 | 609.8 | 0.22895609 |
| 762.5 | 0.714 | 152.50 | 0.94278579 | 610.0 | 0.22885683 |
| 762.75 | 0.714 | 152.55 | 0.94281060 | 610.2 | 0.22875759 |
| 763 | 0.714 | 152.60 | 0.94283541 | 610.4 | 0.22865837 |
| 763.25 | 0.714 | 152.65 | 0.94286021 | 610.6 | 0.22855916 |
| 763.5 | 0.714 | 152.70 | 0.94288501 | 610.8 | 0.22845996 |
| 763.75 | 0.715 | 152.75 | 0.94290980 | 611.0 | 0.22836078 |
| 764 | 0.715 | 152.80 | 0.94293459 | 611.2 | 0.22826162 |
| 764.25 | 0.715 | 152.85 | 0.94295938 | 611.4 | 0.22816247 |
| 764.5 | 0.715 | 152.90 | 0.94298417 | 611.6 | 0.22806334 |
| 764.75 | 0.715 | 152.95 | 0.94300894 | 611.8 | 0.22796422 |
| 765 | 0.715 | 153.00 | 0.94303372 | 612.0 | 0.22786512 |
| 765.25 | 0.715 | 153.05 | 0.94305849 | 612.2 | 0.22776603 |
| 765.5 | 0.715 | 153.10 | 0.94308326 | 612.4 | 0.22766696 |
| 765.75 | 0.716 | 153.15 | 0.94310802 | 612.6 | 0.22756790 |
| 766 | 0.716 | 153.20 | 0.94313279 | 612.8 | 0.22746886 |
| 766.25 | 0.716 | 153.25 | 0.94315754 | 613.0 | 0.22736983 |
| 766.5 | 0.716 | 153.30 | 0.94318229 | 613.2 | 0.22727082 |
| 766.75 | 0.716 | 153.35 | 0.94320704 | 613.4 | 0.22717182 |
| 767 | 0.716 | 153.40 | 0.94323179 | 613.6 | 0.22707284 |
| 767.25 | 0.716 | 153.45 | 0.94325653 | 613.8 | 0.22697388 |
| 767.5 | 0.716 | 153.50 | 0.94328127 | 614.0 | 0.22687493 |
| 767.75 | 0.717 | 153.55 | 0.94330600 | 614.2 | 0.22677599 |
| 768 | 0.717 | 153.60 | 0.94333073 | 614.4 | 0.22667707 |
| 768.25 | 0.717 | 153.65 | 0.94335546 | 614.6 | 0.22657816 |
| 768.5 | 0.717 | 153.70 | 0.94338018 | 614.8 | 0.22647927 |
| 768.75 | 0.717 | 153.75 | 0.94340490 | 615.0 | 0.22638040 |
| 769 | 0.717 | 153.80 | 0.94342962 | 615.2 | 0.22628154 |
| 769.25 | 0.717 | 153.85 | 0.94345433 | 615.4 | 0.22618269 |
| 769.5 | 0.717 | 153.90 | 0.94347903 | 615.6 | 0.22608386 |
| 769.75 | 0.718 | 153.95 | 0.94350374 | 615.8 | 0.22598505 |
| 770 | 0.718 | 154.00 | 0.94352844 | 616.0 | 0.22588625 |
| 770.25 | 0.718 | 154.05 | 0.94355313 | 616.2 | 0.22578746 |
| 770.5 | 0.718 | 154.10 | 0.94357783 | 616.4 | 0.22568869 |
| 770.75 | 0.718 | 154.15 | 0.94360252 | 616.6 | 0.22558994 |
| 771 | 0.718 | 154.20 | 0.94362720 | 616.8 | 0.22549120 |
| 771.25 | 0.718 | 154.25 | 0.94365188 | 617.0 | 0.22539247 |
| 771.5 | 0.718 | 154.30 | 0.94367656 | 617.2 | 0.22529376 |
| 771.75 | 0.719 | 154.35 | 0.94370123 | 617.4 | 0.22519507 |
| 772 | 0.719 | 154.40 | 0.94372590 | 617.6 | 0.22509639 |
| 772.25 | 0.719 | 154.45 | 0.94375057 | 617.8 | 0.22499773 |
| 772.5 | 0.719 | 154.50 | 0.94377523 | 618.0 | 0.22489908 |
| 772.75 | 0.719 | 154.55 | 0.94379989 | 618.2 | 0.22480044 |
| 773 | 0.719 | 154.60 | 0.94382454 | 618.4 | 0.22470182 |
| 773.25 | 0.719 | 154.65 | 0.94384920 | 618.6 | 0.22460322 |
| 773.5 | 0.719 | 154.70 | 0.94387384 | 618.8 | 0.22450463 |
| 773.75 | 0.719 | 154.75 | 0.94389849 | 619.0 | 0.22440605 |
| 774 | 0.720 | 154.80 | 0.94392313 | 619.2 | 0.22430750 |
| 774.25 | 0.720 | 154.85 | 0.94394776 | 619.4 | 0.22420895 |
| 774.5 | 0.720 | 154.90 | 0.94397239 | 619.6 | 0.22411042 |
| 774.75 | 0.720 | 154.95 | 0.94399702 | 619.8 | 0.22401191 |
| 775 | 0.720 | 155.00 | 0.94402165 | 620.0 | 0.22391341 |
| 775.25 | 0.720 | 155.05 | 0.94404627 | 620.2 | 0.22381492 |
| 775.5 | 0.720 | 155.10 | 0.94407089 | 620.4 | 0.22371645 |
| 775.75 | 0.720 | 155.15 | 0.94409550 | 620.6 | 0.22361800 |
| 776 | 0.721 | 155.20 | 0.94412011 | 620.8 | 0.22351956 |
| 776.25 | 0.721 | 155.25 | 0.94414472 | 621.0 | 0.22342113 |
| 776.5 | 0.721 | 155.30 | 0.94416932 | 621.2 | 0.22332272 |
| 776.75 | 0.721 | 155.35 | 0.94419392 | 621.4 | 0.22322433 |
| 777 | 0.721 | 155.40 | 0.94421851 | 621.6 | 0.22312595 |
| 777.25 | 0.721 | 155.45 | 0.94424310 | 621.8 | 0.22302758 |
| 777.5 | 0.721 | 155.50 | 0.94426769 | 622.0 | 0.22292923 |
| 777.75 | 0.721 | 155.55 | 0.94429228 | 622.2 | 0.22283089 |
| 778 | 0.722 | 155.60 | 0.94431686 | 622.4 | 0.22273257 |
| 778.25 | 0.722 | 155.65 | 0.94434143 | 622.6 | 0.22263427 |
| 778.5 | 0.722 | 155.70 | 0.94436601 | 622.8 | 0.22253598 |
| 778.75 | 0.722 | 155.75 | 0.94439058 | 623.0 | 0.22243770 |
| 779 | 0.722 | 155.80 | 0.94441514 | 623.2 | 0.22233944 |


| 779.25 | 0.722 | 155.85 | 0.94443970 | 623.4 | 0.22224119 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 779.5 | 0.722 | 155.90 | 0.94446426 | 623.6 | 0.22214296 |
| 779.75 | 0.722 | 155.95 | 0.94448881 | 623.8 | 0.22204474 |
| 780 | 0.723 | 156.00 | 0.94451337 | 624.0 | 0.22194654 |
| 780.25 | 0.723 | 156.05 | 0.94453791 | 624.2 | 0.22184835 |
| 780.5 | 0.723 | 156.10 | 0.94456246 | 624.4 | 0.22175018 |
| 780.75 | 0.723 | 156.15 | 0.94458699 | 624.6 | 0.22165202 |
| 781 | 0.723 | 156.20 | 0.94461153 | 624.8 | 0.22155388 |
| 781.25 | 0.723 | 156.25 | 0.94463606 | 625.0 | 0.22145575 |
| 781.5 | 0.723 | 156.30 | 0.94466059 | 625.2 | 0.22135764 |
| 781.75 | 0.723 | 156.35 | 0.94468512 | 625.4 | 0.22125954 |
| 782 | 0.724 | 156.40 | 0.94470964 | 625.6 | 0.22116145 |
| 782.25 | 0.724 | 156.45 | 0.94473415 | 625.8 | 0.22106338 |
| 782.5 | 0.724 | 156.50 | 0.94475867 | 626.0 | 0.22096533 |
| 782.75 | 0.724 | 156.55 | 0.94478318 | 626.2 | 0.22086729 |
| 783 | 0.724 | 156.60 | 0.94480768 | 626.4 | 0.22076926 |
| 783.25 | 0.724 | 156.65 | 0.94483219 | 626.6 | 0.22067125 |
| 783.5 | 0.724 | 156.70 | 0.94485669 | 626.8 | 0.22057326 |
| 783.75 | 0.724 | 156.75 | 0.94488118 | 627.0 | 0.22047527 |
| 784 | 0.725 | 156.80 | 0.94490567 | 627.2 | 0.22037731 |
| 784.25 | 0.725 | 156.85 | 0.94493016 | 627.4 | 0.22027936 |
| 784.5 | 0.725 | 156.90 | 0.94495465 | 627.6 | 0.22018142 |
| 784.75 | 0.725 | 156.95 | 0.94497913 | 627.8 | 0.22008350 |
| 785 | 0.725 | 157.00 | 0.94500360 | 628.0 | 0.21998559 |
| 785.25 | 0.725 | 157.05 | 0.94502808 | 628.2 | 0.21988770 |
| 785.5 | 0.725 | 157.10 | 0.94505255 | 628.4 | 0.21978982 |
| 785.75 | 0.725 | 157.15 | 0.94507701 | 628.6 | 0.21969195 |
| 786 | 0.726 | 157.20 | 0.94510147 | 628.8 | 0.21959410 |
| 786.25 | 0.726 | 157.25 | 0.94512593 | 629.0 | 0.21949627 |
| 786.5 | 0.726 | 157.30 | 0.94515039 | 629.2 | 0.21939845 |
| 786.75 | 0.726 | 157.35 | 0.94517484 | 629.4 | 0.21930064 |
| 787 | 0.726 | 157.40 | 0.94519929 | 629.6 | 0.21920285 |
| 787.25 | 0.726 | 157.45 | 0.94522373 | 629.8 | 0.21910508 |
| 787.5 | 0.726 | 157.50 | 0.94524817 | 630.0 | 0.21900732 |
| 787.75 | 0.726 | 157.55 | 0.94527261 | 630.2 | 0.21890957 |
| 788 | 0.726 | 157.60 | 0.94529704 | 630.4 | 0.21881184 |
| 788.25 | 0.727 | 157.65 | 0.94532147 | 630.6 | 0.21871412 |
| 788.5 | 0.727 | 157.70 | 0.94534590 | 630.8 | 0.21861641 |
| 788.75 | 0.727 | 157.75 | 0.94537032 | 631.0 | 0.21851873 |
| 789 | 0.727 | 157.80 | 0.94539474 | 631.2 | 0.21842105 |
| 789.25 | 0.727 | 157.85 | 0.94541915 | 631.4 | 0.21832339 |
| 789.5 | 0.727 | 157.90 | 0.94544356 | 631.6 | 0.21822575 |
| 789.75 | 0.727 | 157.95 | 0.94546797 | 631.8 | 0.21812812 |
| 790 | 0.727 | 158.00 | 0.94549237 | 632.0 | 0.21803050 |
| 790.25 | 0.728 | 158.05 | 0.94551678 | 632.2 | 0.21793290 |
| 790.5 | 0.728 | 158.10 | 0.94554117 | 632.4 | 0.21783531 |
| 790.75 | 0.728 | 158.15 | 0.94556557 | 632.6 | 0.21773774 |
| 791 | 0.728 | 158.20 | 0.94558995 | 632.8 | 0.21764018 |
| 791.25 | 0.728 | 158.25 | 0.94561434 | 633.0 | 0.21754264 |
| 791.5 | 0.728 | 158.30 | 0.94563872 | 633.2 | 0.21744511 |
| 791.75 | 0.728 | 158.35 | 0.94566310 | 633.4 | 0.21734759 |
| 792 | 0.728 | 158.40 | 0.94568748 | 633.6 | 0.21725009 |
| 792.25 | 0.729 | 158.45 | 0.94571185 | 633.8 | 0.21715261 |
| 792.5 | 0.729 | 158.50 | 0.94573622 | 634.0 | 0.21705514 |
| 792.75 | 0.729 | 158.55 | 0.94576058 | 634.2 | 0.21695768 |
| 793 | 0.729 | 158.60 | 0.94578494 | 634.4 | 0.21686024 |
| 793.25 | 0.729 | 158.65 | 0.94580930 | 634.6 | 0.21676281 |
| 793.5 | 0.729 | 158.70 | 0.94583365 | 634.8 | 0.21666540 |
| 793.75 | 0.729 | 158.75 | 0.94585800 | 635.0 | 0.21656800 |
| 794 | 0.729 | 158.80 | 0.94588235 | 635.2 | 0.21647061 |
| 794.25 | 0.730 | 158.85 | 0.94590669 | 635.4 | 0.21637324 |
| 794.5 | 0.730 | 158.90 | 0.94593103 | 635.6 | 0.21627589 |
| 794.75 | 0.730 | 158.95 | 0.94595536 | 635.8 | 0.21617855 |
| 795 | 0.730 | 159.00 | 0.94597970 | 636.0 | 0.21608122 |
| 795.25 | 0.730 | 159.05 | 0.94600402 | 636.2 | 0.21598391 |
| 795.5 | 0.730 | 159.10 | 0.94602835 | 636.4 | 0.21588661 |
| 795.75 | 0.730 | 159.15 | 0.94605267 | 636.6 | 0.21578932 |
| 796 | 0.730 | 159.20 | 0.94607699 | 636.8 | 0.21569205 |
| 796.25 | 0.731 | 159.25 | 0.94610130 | 637.0 | 0.21559480 |
| 796.5 | 0.731 | 159.30 | 0.94612561 | 637.2 | 0.21549756 |
| 796.75 | 0.731 | 159.35 | 0.94614992 | 637.4 | 0.21540033 |


| 797 | 0.731 | 159.40 | 0.94617422 | 637.6 | 0.21530312 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 797.25 | 0.731 | 159.45 | 0.94619852 | 637.8 | 0.21520592 |
| 797.5 | 0.731 | 159.50 | 0.94622282 | 638.0 | 0.21510874 |
| 797.75 | 0.731 | 159.55 | 0.94624711 | 638.2 | 0.21501157 |
| 798 | 0.731 | 159.60 | 0.94627140 | 638.4 | 0.21491441 |
| 798.25 | 0.731 | 159.65 | 0.94629568 | 638.6 | 0.21481727 |
| 798.5 | 0.732 | 159.70 | 0.94631996 | 638.8 | 0.21472015 |
| 798.75 | 0.732 | 159.75 | 0.94634424 | 639.0 | 0.21462304 |
| 799 | 0.732 | 159.80 | 0.94636852 | 639.2 | 0.21452594 |
| 799.25 | 0.732 | 159.85 | 0.94639279 | 639.4 | 0.21442885 |
| 799.5 | 0.732 | 159.90 | 0.94641705 | 639.6 | 0.21433179 |
| 799.75 | 0.732 | 159.95 | 0.94644132 | 639.8 | 0.21423473 |
| 800 | 0.732 | 160.00 | 0.94646558 | 640.0 | 0.21413769 |
| 800.25 | 0.732 | 160.05 | 0.94648983 | 640.2 | 0.21404066 |
| 800.5 | 0.733 | 160.10 | 0.94651409 | 640.4 | 0.21394365 |
| 800.75 | 0.733 | 160.15 | 0.94653834 | 640.6 | 0.21384665 |
| 801 | 0.733 | 160.20 | 0.94656258 | 640.8 | 0.21374967 |
| 801.25 | 0.733 | 160.25 | 0.94658682 | 641.0 | 0.21365270 |
| 801.5 | 0.733 | 160.30 | 0.94661106 | 641.2 | 0.21355575 |
| 801.75 | 0.733 | 160.35 | 0.94663530 | 641.4 | 0.21345881 |
| 802 | 0.733 | 160.40 | 0.94665953 | 641.6 | 0.21336188 |
| 802.25 | 0.733 | 160.45 | 0.94668376 | 641.8 | 0.21326497 |
| 802.5 | 0.734 | 160.50 | 0.94670798 | 642.0 | 0.21316807 |
| 802.75 | 0.734 | 160.55 | 0.94673220 | 642.2 | 0.21307118 |
| 803 | 0.734 | 160.60 | 0.94675642 | 642.4 | 0.21297431 |
| 803.25 | 0.734 | 160.65 | 0.94678064 | 642.6 | 0.21287746 |
| 803.5 | 0.734 | 160.70 | 0.94680485 | 642.8 | 0.21278062 |
| 803.75 | 0.734 | 160.75 | 0.94682905 | 643.0 | 0.21268379 |
| 804 | 0.734 | 160.80 | 0.94685326 | 643.2 | 0.21258698 |
| 804.25 | 0.734 | 160.85 | 0.94687746 | 643.4 | 0.21249018 |
| 804.5 | 0.735 | 160.90 | 0.94690165 | 643.6 | 0.21239339 |
| 804.75 | 0.735 | 160.95 | 0.94692584 | 643.8 | 0.21229662 |
| 805 | 0.735 | 161.00 | 0.94695003 | 644.0 | 0.21219986 |
| 805.25 | 0.735 | 161.05 | 0.94697422 | 644.2 | 0.21210312 |
| 805.5 | 0.735 | 161.10 | 0.94699840 | 644.4 | 0.21200639 |
| 805.75 | 0.735 | 161.15 | 0.94702258 | 644.6 | 0.21190968 |
| 806 | 0.735 | 161.20 | 0.94704676 | 644.8 | 0.21181298 |
| 806.25 | 0.735 | 161.25 | 0.94707093 | 645.0 | 0.21171629 |
| 806.5 | 0.735 | 161.30 | 0.94709510 | 645.2 | 0.21161962 |
| 806.75 | 0.736 | 161.35 | 0.94711926 | 645.4 | 0.21152296 |
| 807 | 0.736 | 161.40 | 0.94714342 | 645.6 | 0.21142632 |
| 807.25 | 0.736 | 161.45 | 0.94716758 | 645.8 | 0.21132969 |
| 807.5 | 0.736 | 161.50 | 0.94719173 | 646.0 | 0.21123307 |
| 807.75 | 0.736 | 161.55 | 0.94721588 | 646.2 | 0.21113647 |
| 808 | 0.736 | 161.60 | 0.94724003 | 646.4 | 0.21103988 |
| 808.25 | 0.736 | 161.65 | 0.94726417 | 646.6 | 0.21094331 |
| 808.5 | 0.736 | 161.70 | 0.94728831 | 646.8 | 0.21084675 |
| 808.75 | 0.737 | 161.75 | 0.94731245 | 647.0 | 0.21075020 |
| 809 | 0.737 | 161.80 | 0.94733658 | 647.2 | 0.21065367 |
| 809.25 | 0.737 | 161.85 | 0.94736071 | 647.4 | 0.21055715 |
| 809.5 | 0.737 | 161.90 | 0.94738484 | 647.6 | 0.21046065 |
| 809.75 | 0.737 | 161.95 | 0.94740896 | 647.8 | 0.21036416 |
| 810 | 0.737 | 162.00 | 0.94743308 | 648.0 | 0.21026768 |
| 810.25 | 0.737 | 162.05 | 0.94745719 | 648.2 | 0.21017122 |
| 810.5 | 0.737 | 162.10 | 0.94748131 | 648.4 | 0.21007478 |
| 810.75 | 0.738 | 162.15 | 0.94750541 | 648.6 | 0.20997834 |
| 811 | 0.738 | 162.20 | 0.94752952 | 648.8 | 0.20988192 |
| 811.25 | 0.738 | 162.25 | 0.94755362 | 649.0 | 0.20978552 |
| 811.5 | 0.738 | 162.30 | 0.94757772 | 649.2 | 0.20968913 |
| 811.75 | 0.738 | 162.35 | 0.94760181 | 649.4 | 0.20959275 |
| 812 | 0.738 | 162.40 | 0.94762590 | 649.6 | 0.20949638 |
| 812.25 | 0.738 | 162.45 | 0.94764999 | 649.8 | 0.20940003 |
| 812.5 | 0.738 | 162.50 | 0.94767408 | 650.0 | 0.20930370 |
| 812.75 | 0.738 | 162.55 | 0.94769816 | 650.2 | 0.20920738 |
| 813 | 0.739 | 162.60 | 0.94772223 | 650.4 | 0.20911107 |
| 813.25 | 0.739 | 162.65 | 0.94774631 | 650.6 | 0.20901477 |
| 813.5 | 0.739 | 162.70 | 0.94777038 | 650.8 | 0.20891849 |
| 813.75 | 0.739 | 162.75 | 0.94779444 | 651.0 | 0.20882223 |
| 814 | 0.739 | 162.80 | 0.94781851 | 651.2 | 0.20872597 |
| 814.25 | 0.739 | 162.85 | 0.94784257 | 651.4 | 0.20862974 |
| 814.5 | 0.739 | 162.90 | 0.94786662 | 651.6 | 0.20853351 |


| 814.75 | 0.739 | 162.95 | 0.94789067 | 651.8 | 0.20843730 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 815 | 0.740 | 163.00 | 0.94791472 | 652.0 | 0.20834110 |
| 815.25 | 0.740 | 163.05 | 0.94793877 | 652.2 | 0.20824492 |
| 815.5 | 0.740 | 163.10 | 0.94796281 | 652.4 | 0.20814875 |
| 815.75 | 0.740 | 163.15 | 0.94798685 | 652.6 | 0.20805260 |
| 816 | 0.740 | 163.20 | 0.94801089 | 652.8 | 0.20795646 |
| 816.25 | 0.740 | 163.25 | 0.94803492 | 653.0 | 0.20786033 |
| 816.5 | 0.740 | 163.30 | 0.94805895 | 653.2 | 0.20776421 |
| 816.75 | 0.740 | 163.35 | 0.94808297 | 653.4 | 0.20766811 |
| 817 | 0.741 | 163.40 | 0.94810699 | 653.6 | 0.20757203 |
| 817.25 | 0.741 | 163.45 | 0.94813101 | 653.8 | 0.20747596 |
| 817.5 | 0.741 | 163.50 | 0.94815503 | 654.0 | 0.20737990 |
| 817.75 | 0.741 | 163.55 | 0.94817904 | 654.2 | 0.20728385 |
| 818 | 0.741 | 163.60 | 0.94820304 | 654.4 | 0.20718782 |
| 818.25 | 0.741 | 163.65 | 0.94822705 | 654.6 | 0.20709180 |
| 818.5 | 0.741 | 163.70 | 0.94825105 | 654.8 | 0.20699580 |
| 818.75 | 0.741 | 163.75 | 0.94827505 | 655.0 | 0.20689981 |
| 819 | 0.741 | 163.80 | 0.94829904 | 655.2 | 0.20680384 |
| 819.25 | 0.742 | 163.85 | 0.94832303 | 655.4 | 0.20670787 |
| 819.5 | 0.742 | 163.90 | 0.94834702 | 655.6 | 0.20661193 |
| 819.75 | 0.742 | 163.95 | 0.94837100 | 655.8 | 0.20651599 |
| 820 | 0.742 | 164.00 | 0.94839498 | 656.0 | 0.20642007 |
| 820.25 | 0.742 | 164.05 | 0.94841896 | 656.2 | 0.20632416 |
| 820.5 | 0.742 | 164.10 | 0.94844293 | 656.4 | 0.20622827 |
| 820.75 | 0.742 | 164.15 | 0.94846690 | 656.6 | 0.20613239 |
| 821 | 0.742 | 164.20 | 0.94849087 | 656.8 | 0.20603652 |
| 821.25 | 0.743 | 164.25 | 0.94851483 | 657.0 | 0.20594067 |
| 821.5 | 0.743 | 164.30 | 0.94853879 | 657.2 | 0.20584483 |
| 821.75 | 0.743 | 164.35 | 0.94856275 | 657.4 | 0.20574901 |
| 822 | 0.743 | 164.40 | 0.94858670 | 657.6 | 0.20565320 |
| 822.25 | 0.743 | 164.45 | 0.94861065 | 657.8 | 0.20555740 |
| 822.5 | 0.743 | 164.50 | 0.94863460 | 658.0 | 0.20546162 |
| 822.75 | 0.743 | 164.55 | 0.94865854 | 658.2 | 0.20536585 |
| 823 | 0.743 | 164.60 | 0.94868248 | 658.4 | 0.20527009 |
| 823.25 | 0.744 | 164.65 | 0.94870641 | 658.6 | 0.20517435 |
| 823.5 | 0.744 | 164.70 | 0.94873034 | 658.8 | 0.20507862 |
| 823.75 | 0.744 | 164.75 | 0.94875427 | 659.0 | 0.20498291 |
| 824 | 0.744 | 164.80 | 0.94877820 | 659.2 | 0.20488720 |
| 824.25 | 0.744 | 164.85 | 0.94880212 | 659.4 | 0.20479152 |
| 824.5 | 0.744 | 164.90 | 0.94882604 | 659.6 | 0.20469584 |
| 824.75 | 0.744 | 164.95 | 0.94884995 | 659.8 | 0.20460018 |
| 825 | 0.744 | 165.00 | 0.94887387 | 660.0 | 0.20450453 |
| 825.25 | 0.744 | 165.05 | 0.94889777 | 660.2 | 0.20440890 |
| 825.5 | 0.745 | 165.10 | 0.94892168 | 660.4 | 0.20431328 |
| 825.75 | 0.745 | 165.15 | 0.94894558 | 660.6 | 0.20421768 |
| 826 | 0.745 | 165.20 | 0.94896948 | 660.8 | 0.20412208 |
| 826.25 | 0.745 | 165.25 | 0.94899337 | 661.0 | 0.20402650 |
| 826.5 | 0.745 | 165.30 | 0.94901727 | 661.2 | 0.20393094 |
| 826.75 | 0.745 | 165.35 | 0.94904115 | 661.4 | 0.20383539 |
| 827 | 0.745 | 165.40 | 0.94906504 | 661.6 | 0.20373985 |
| 827.25 | 0.745 | 165.45 | 0.94908892 | 661.8 | 0.20364432 |
| 827.5 | 0.746 | 165.50 | 0.94911280 | 662.0 | 0.20354881 |
| 827.75 | 0.746 | 165.55 | 0.94913667 | 662.2 | 0.20345332 |
| 828 | 0.746 | 165.60 | 0.94916054 | 662.4 | 0.20335783 |
| 828.25 | 0.746 | 165.65 | 0.94918441 | 662.6 | 0.20326236 |
| 828.5 | 0.746 | 165.70 | 0.94920827 | 662.8 | 0.20316690 |
| 828.75 | 0.746 | 165.75 | 0.94923213 | 663.0 | 0.20307146 |
| 829 | 0.746 | 165.80 | 0.94925599 | 663.2 | 0.20297603 |
| 829.25 | 0.746 | 165.85 | 0.94927985 | 663.4 | 0.20288061 |
| 829.5 | 0.747 | 165.90 | 0.94930370 | 663.6 | 0.20278521 |
| 829.75 | 0.747 | 165.95 | 0.94932754 | 663.8 | 0.20268982 |
| 830 | 0.747 | 166.00 | 0.94935139 | 664.0 | 0.20259445 |
| 830.25 | 0.747 | 166.05 | 0.94937523 | 664.2 | 0.20249908 |
| 830.5 | 0.747 | 166.10 | 0.94939907 | 664.4 | 0.20240374 |
| 830.75 | 0.747 | 166.15 | 0.94942290 | 664.6 | 0.20230840 |
| 831 | 0.747 | 166.20 | 0.94944673 | 664.8 | 0.20221308 |
| 831.25 | 0.747 | 166.25 | 0.94947056 | 665.0 | 0.20211777 |
| 831.5 | 0.747 | 166.30 | 0.94949438 | 665.2 | 0.20202248 |
| 831.75 | 0.748 | 166.35 | 0.94951820 | 665.4 | 0.20192719 |
| 832 | 0.748 | 166.40 | 0.94954202 | 665.6 | 0.20183193 |
| 832.25 | 0.748 | 166.45 | 0.94956583 | 665.8 | 0.20173667 |


| 832.5 | 0.748 | 166.50 | 0.94958964 | 666.0 | 0.20164143 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 832.75 | 0.748 | 166.55 | 0.94961345 | 666.2 | 0.20154620 |
| 833 | 0.748 | 166.60 | 0.94963725 | 666.4 | 0.20145099 |
| 833.25 | 0.748 | 166.65 | 0.94966105 | 666.6 | 0.20135579 |
| 833.5 | 0.748 | 166.70 | 0.94968485 | 666.8 | 0.20126060 |
| 833.75 | 0.749 | 166.75 | 0.94970864 | 667.0 | 0.20116543 |
| 834 | 0.749 | 166.80 | 0.94973243 | 667.2 | 0.20107027 |
| 834.25 | 0.749 | 166.85 | 0.94975622 | 667.4 | 0.20097512 |
| 834.5 | 0.749 | 166.90 | 0.94978000 | 667.6 | 0.20087999 |
| 834.75 | 0.749 | 166.95 | 0.94980378 | 667.8 | 0.20078487 |
| 835 | 0.749 | 167.00 | 0.94982756 | 668.0 | 0.20068976 |
| 835.25 | 0.749 | 167.05 | 0.94985133 | 668.2 | 0.20059467 |
| 835.5 | 0.749 | 167.10 | 0.94987510 | 668.4 | 0.20049959 |
| 835.75 | 0.749 | 167.15 | 0.94989887 | 668.6 | 0.20040452 |
| 836 | 0.750 | 167.20 | 0.94992263 | 668.8 | 0.20030947 |
| 836.25 | 0.750 | 167.25 | 0.94994639 | 669.0 | 0.20021443 |
| 836.5 | 0.750 | 167.30 | 0.94997015 | 669.2 | 0.20011940 |
| 836.75 | 0.750 | 167.35 | 0.94999390 | 669.4 | 0.20002439 |
| 837 | 0.750 | 167.40 | 0.95001765 | 669.6 | 0.19992939 |
| 837.25 | 0.750 | 167.45 | 0.95004140 | 669.8 | 0.19983440 |
| 837.5 | 0.750 | 167.50 | 0.95006514 | 670.0 | 0.19973943 |
| 837.75 | 0.750 | 167.55 | 0.95008888 | 670.2 | 0.19964447 |
| 838 | 0.751 | 167.60 | 0.95011262 | 670.4 | 0.19954952 |
| 838.25 | 0.751 | 167.65 | 0.95013635 | 670.6 | 0.19945459 |
| 838.5 | 0.751 | 167.70 | 0.95016008 | 670.8 | 0.19935967 |
| 838.75 | 0.751 | 167.75 | 0.95018381 | 671.0 | 0.19926476 |
| 839 | 0.751 | 167.80 | 0.95020753 | 671.2 | 0.19916987 |
| 839.25 | 0.751 | 167.85 | 0.95023125 | 671.4 | 0.19907499 |
| 839.5 | 0.751 | 167.90 | 0.95025497 | 671.6 | 0.19898012 |
| 839.75 | 0.751 | 167.95 | 0.95027868 | 671.8 | 0.19888527 |
| 840 | 0.752 | 168.00 | 0.95030239 | 672.0 | 0.19879043 |
| 840.25 | 0.752 | 168.05 | 0.95032610 | 672.2 | 0.19869560 |
| 840.5 | 0.752 | 168.10 | 0.95034980 | 672.4 | 0.19860079 |
| 840.75 | 0.752 | 168.15 | 0.95037350 | 672.6 | 0.19850598 |
| 841 | 0.752 | 168.20 | 0.95039720 | 672.8 | 0.19841120 |
| 841.25 | 0.752 | 168.25 | 0.95042089 | 673.0 | 0.19831642 |
| 841.5 | 0.752 | 168.30 | 0.95044458 | 673.2 | 0.19822166 |
| 841.75 | 0.752 | 168.35 | 0.95046827 | 673.4 | 0.19812692 |
| 842 | 0.752 | 168.40 | 0.95049195 | 673.6 | 0.19803218 |
| 842.25 | 0.753 | 168.45 | 0.95051564 | 673.8 | 0.19793746 |
| 842.5 | 0.753 | 168.50 | 0.95053931 | 674.0 | 0.19784275 |
| 842.75 | 0.753 | 168.55 | 0.95056299 | 674.2 | 0.19774806 |
| 843 | 0.753 | 168.60 | 0.95058666 | 674.4 | 0.19765338 |
| 843.25 | 0.753 | 168.65 | 0.95061032 | 674.6 | 0.19755871 |
| 843.5 | 0.753 | 168.70 | 0.95063399 | 674.8 | 0.19746405 |
| 843.75 | 0.753 | 168.75 | 0.95065765 | 675.0 | 0.19736941 |
| 844 | 0.753 | 168.80 | 0.95068130 | 675.2 | 0.19727478 |
| 844.25 | 0.754 | 168.85 | 0.95070496 | 675.4 | 0.19718017 |
| 844.5 | 0.754 | 168.90 | 0.95072861 | 675.6 | 0.19708556 |
| 844.75 | 0.754 | 168.95 | 0.95075226 | 675.8 | 0.19699097 |
| 845 | 0.754 | 169.00 | 0.95077590 | 676.0 | 0.19689640 |
| 845.25 | 0.754 | 169.05 | 0.95079954 | 676.2 | 0.19680184 |
| 845.5 | 0.754 | 169.10 | 0.95082318 | 676.4 | 0.19670729 |
| 845.75 | 0.754 | 169.15 | 0.95084681 | 676.6 | 0.19661275 |
| 846 | 0.754 | 169.20 | 0.95087044 | 676.8 | 0.19651823 |
| 846.25 | 0.754 | 169.25 | 0.95089407 | 677.0 | 0.19642372 |
| 846.5 | 0.755 | 169.30 | 0.95091770 | 677.2 | 0.19632922 |
| 846.75 | 0.755 | 169.35 | 0.95094132 | 677.4 | 0.19623473 |
| 847 | 0.755 | 169.40 | 0.95096493 | 677.6 | 0.19614026 |
| 847.25 | 0.755 | 169.45 | 0.95098855 | 677.8 | 0.19604580 |
| 847.5 | 0.755 | 169.50 | 0.95101216 | 678.0 | 0.19595136 |
| 847.75 | 0.755 | 169.55 | 0.95103577 | 678.2 | 0.19585693 |
| 848 | 0.755 | 169.60 | 0.95105937 | 678.4 | 0.19576251 |
| 848.25 | 0.755 | 169.65 | 0.95108297 | 678.6 | 0.19566810 |
| 848.5 | 0.756 | 169.70 | 0.95110657 | 678.8 | 0.19557371 |
| 848.75 | 0.756 | 169.75 | 0.95113017 | 679.0 | 0.19547933 |
| 849 | 0.756 | 169.80 | 0.95115376 | 679.2 | 0.19538497 |
| 849.25 | 0.756 | 169.85 | 0.95117735 | 679.4 | 0.19529061 |
| 849.5 | 0.756 | 169.90 | 0.95120093 | 679.6 | 0.19519627 |
| 849.75 | 0.756 | 169.95 | 0.95122451 | 679.8 | 0.19510195 |
| 850 | 0.756 | 170.00 | 0.95124809 | 680.0 | 0.19500763 |


| 850.25 | 0.756 | 170.05 | 0.95127167 | 680.2 | 0.19491333 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 850.5 | 0.756 | 170.10 | 0.95129524 | 680.4 | 0.19481904 |
| 850.75 | 0.757 | 170.15 | 0.95131881 | 680.6 | 0.19472477 |
| 851 | 0.757 | 170.20 | 0.95134237 | 680.8 | 0.19463050 |
| 851.25 | 0.757 | 170.25 | 0.95136594 | 681.0 | 0.19453626 |
| 851.5 | 0.757 | 170.30 | 0.95138950 | 681.2 | 0.19444202 |
| 851.75 | 0.757 | 170.35 | 0.95141305 | 681.4 | 0.19434780 |
| 852 | 0.757 | 170.40 | 0.95143660 | 681.6 | 0.19425359 |
| 852.25 | 0.757 | 170.45 | 0.95146015 | 681.8 | 0.19415939 |
| 852.5 | 0.757 | 170.50 | 0.95148370 | 682.0 | 0.19406521 |
| 852.75 | 0.758 | 170.55 | 0.95150724 | 682.2 | 0.19397103 |
| 853 | 0.758 | 170.60 | 0.95153078 | 682.4 | 0.19387688 |
| 853.25 | 0.758 | 170.65 | 0.95155432 | 682.6 | 0.19378273 |
| 853.5 | 0.758 | 170.70 | 0.95157785 | 682.8 | 0.19368860 |
| 853.75 | 0.758 | 170.75 | 0.95160138 | 683.0 | 0.19359448 |
| 854 | 0.758 | 170.80 | 0.95162491 | 683.2 | 0.19350037 |
| 854.25 | 0.758 | 170.85 | 0.95164843 | 683.4 | 0.19340628 |
| 854.5 | 0.758 | 170.90 | 0.95167195 | 683.6 | 0.19331220 |
| 854.75 | 0.758 | 170.95 | 0.95169547 | 683.8 | 0.19321813 |
| 855 | 0.759 | 171.00 | 0.95171898 | 684.0 | 0.19312408 |
| 855.25 | 0.759 | 171.05 | 0.95174249 | 684.2 | 0.19303004 |
| 855.5 | 0.759 | 171.10 | 0.95176600 | 684.4 | 0.19293601 |
| 855.75 | 0.759 | 171.15 | 0.95178950 | 684.6 | 0.19284199 |
| 856 | 0.759 | 171.20 | 0.95181300 | 684.8 | 0.19274799 |
| 856.25 | 0.759 | 171.25 | 0.95183650 | 685.0 | 0.19265400 |
| 856.5 | 0.759 | 171.30 | 0.95185999 | 685.2 | 0.19256002 |
| 856.75 | 0.759 | 171.35 | 0.95188349 | 685.4 | 0.19246606 |
| 857 | 0.760 | 171.40 | 0.95190697 | 685.6 | 0.19237211 |
| 857.25 | 0.760 | 171.45 | 0.95193046 | 685.8 | 0.19227817 |
| 857.5 | 0.760 | 171.50 | 0.95195394 | 686.0 | 0.19218424 |
| 857.75 | 0.760 | 171.55 | 0.95197742 | 686.2 | 0.19209033 |
| 858 | 0.760 | 171.60 | 0.95200089 | 686.4 | 0.19199643 |
| 858.25 | 0.760 | 171.65 | 0.95202436 | 686.6 | 0.19190254 |
| 858.5 | 0.760 | 171.70 | 0.95204783 | 686.8 | 0.19180867 |
| 858.75 | 0.760 | 171.75 | 0.95207130 | 687.0 | 0.19171481 |
| 859 | 0.760 | 171.80 | 0.95209476 | 687.2 | 0.19162096 |
| 859.25 | 0.761 | 171.85 | 0.95211822 | 687.4 | 0.19152712 |
| 859.5 | 0.761 | 171.90 | 0.95214167 | 687.6 | 0.19143330 |
| 859.75 | 0.761 | 171.95 | 0.95216513 | 687.8 | 0.19133949 |
| 860 | 0.761 | 172.00 | 0.95218858 | 688.0 | 0.19124570 |
| 860.25 | 0.761 | 172.05 | 0.95221202 | 688.2 | 0.19115191 |
| 860.5 | 0.761 | 172.10 | 0.95223547 | 688.4 | 0.19105814 |
| 860.75 | 0.761 | 172.15 | 0.95225890 | 688.6 | 0.19096438 |
| 861 | 0.761 | 172.20 | 0.95228234 | 688.8 | 0.19087064 |
| 861.25 | 0.762 | 172.25 | 0.95230577 | 689.0 | 0.19077690 |
| 861.5 | 0.762 | 172.30 | 0.95232920 | 689.2 | 0.19068318 |
| 861.75 | 0.762 | 172.35 | 0.95235263 | 689.4 | 0.19058947 |
| 862 | 0.762 | 172.40 | 0.95237606 | 689.6 | 0.19049578 |
| 862.25 | 0.762 | 172.45 | 0.95239948 | 689.8 | 0.19040210 |
| 862.5 | 0.762 | 172.50 | 0.95242289 | 690.0 | 0.19030843 |
| 862.75 | 0.762 | 172.55 | 0.95244631 | 690.2 | 0.19021477 |
| 863 | 0.762 | 172.60 | 0.95246972 | 690.4 | 0.19012113 |
| 863.25 | 0.762 | 172.65 | 0.95249313 | 690.6 | 0.19002750 |
| 863.5 | 0.763 | 172.70 | 0.95251653 | 690.8 | 0.18993388 |
| 863.75 | 0.763 | 172.75 | 0.95253993 | 691.0 | 0.18984027 |
| 864 | 0.763 | 172.80 | 0.95256333 | 691.2 | 0.18974668 |
| 864.25 | 0.763 | 172.85 | 0.95258672 | 691.4 | 0.18965310 |
| 864.5 | 0.763 | 172.90 | 0.95261012 | 691.6 | 0.18955953 |
| 864.75 | 0.763 | 172.95 | 0.95263351 | 691.8 | 0.18946598 |
| 865 | 0.763 | 173.00 | 0.95265689 | 692.0 | 0.18937244 |
| 865.25 | 0.763 | 173.05 | 0.95268027 | 692.2 | 0.18927891 |
| 865.5 | 0.764 | 173.10 | 0.95270365 | 692.4 | 0.18918539 |
| 865.75 | 0.764 | 173.15 | 0.95272703 | 692.6 | 0.18909189 |
| 866 | 0.764 | 173.20 | 0.95275040 | 692.8 | 0.18899840 |
| 866.25 | 0.764 | 173.25 | 0.95277377 | 693.0 | 0.18890492 |
| 866.5 | 0.764 | 173.30 | 0.95279714 | 693.2 | 0.18881145 |
| 866.75 | 0.764 | 173.35 | 0.95282050 | 693.4 | 0.18871800 |
| 867 | 0.764 | 173.40 | 0.95284386 | 693.6 | 0.18862456 |
| 867.25 | 0.764 | 173.45 | 0.95286722 | 693.8 | 0.18853113 |
| 867.5 | 0.764 | 173.50 | 0.95289057 | 694.0 | 0.18843772 |
| 867.75 | 0.765 | 173.55 | 0.95291392 | 694.2 | 0.18834432 |


| 868 | 0.765 | 173.60 | 0.95293727 | 694.4 | 0.18825093 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 868.25 | 0.765 | 173.65 | 0.95296061 | 694.6 | 0.18815755 |
| 868.5 | 0.765 | 173.70 | 0.95298395 | 694.8 | 0.18806418 |
| 868.75 | 0.765 | 173.75 | 0.95300729 | 695.0 | 0.18797083 |
| 869 | 0.765 | 173.80 | 0.95303063 | 695.2 | 0.18787749 |
| 869.25 | 0.765 | 173.85 | 0.95305396 | 695.4 | 0.18778417 |
| 869.5 | 0.765 | 173.90 | 0.95307729 | 695.6 | 0.18769085 |
| 869.75 | 0.766 | 173.95 | 0.95310061 | 695.8 | 0.18759755 |
| 870 | 0.766 | 174.00 | 0.95312393 | 696.0 | 0.18750426 |
| 870.25 | 0.766 | 174.05 | 0.95314725 | 696.2 | 0.18741099 |
| 870.5 | 0.766 | 174.10 | 0.95317057 | 696.4 | 0.18731772 |
| 870.75 | 0.766 | 174.15 | 0.95319388 | 696.6 | 0.18722447 |
| 871 | 0.766 | 174.20 | 0.95321719 | 696.8 | 0.18713123 |
| 871.25 | 0.766 | 174.25 | 0.95324050 | 697.0 | 0.18703801 |
| 871.5 | 0.766 | 174.30 | 0.95326380 | 697.2 | 0.18694480 |
| 871.75 | 0.766 | 174.35 | 0.95328710 | 697.4 | 0.18685159 |
| 872 | 0.767 | 174.40 | 0.95331040 | 697.6 | 0.18675841 |
| 872.25 | 0.767 | 174.45 | 0.95333369 | 697.8 | 0.18666523 |
| 872.5 | 0.767 | 174.50 | 0.95335698 | 698.0 | 0.18657207 |
| 872.75 | 0.767 | 174.55 | 0.95338027 | 698.2 | 0.18647892 |
| 873 | 0.767 | 174.60 | 0.95340355 | 698.4 | 0.18638578 |
| 873.25 | 0.767 | 174.65 | 0.95342684 | 698.6 | 0.18629265 |
| 873.5 | 0.767 | 174.70 | 0.95345011 | 698.8 | 0.18619954 |
| 873.75 | 0.767 | 174.75 | 0.95347339 | 699.0 | 0.18610644 |
| 874 | 0.767 | 174.80 | 0.95349666 | 699.2 | 0.18601335 |
| 874.25 | 0.768 | 174.85 | 0.95351993 | 699.4 | 0.18592028 |
| 874.5 | 0.768 | 174.90 | 0.95354320 | 699.6 | 0.18582722 |
| 874.75 | 0.768 | 174.95 | 0.95356646 | 699.8 | 0.18573417 |
| 875 | 0.768 | 175.00 | 0.95358972 | 700.0 | 0.18564113 |
| 875.25 | 0.768 | 175.05 | 0.95361297 | 700.2 | 0.18554810 |
| 875.5 | 0.768 | 175.10 | 0.95363623 | 700.4 | 0.18545509 |
| 875.75 | 0.768 | 175.15 | 0.95365948 | 700.6 | 0.18536209 |
| 876 | 0.768 | 175.20 | 0.95368272 | 700.8 | 0.18526910 |
| 876.25 | 0.769 | 175.25 | 0.95370597 | 701.0 | 0.18517613 |
| 876.5 | 0.769 | 175.30 | 0.95372921 | 701.2 | 0.18508316 |
| 876.75 | 0.769 | 175.35 | 0.95375245 | 701.4 | 0.18499021 |
| 877 | 0.769 | 175.40 | 0.95377568 | 701.6 | 0.18489728 |
| 877.25 | 0.769 | 175.45 | 0.95379891 | 701.8 | 0.18480435 |
| 877.5 | 0.769 | 175.50 | 0.95382214 | 702.0 | 0.18471144 |
| 877.75 | 0.769 | 175.55 | 0.95384537 | 702.2 | 0.18461854 |
| 878 | 0.769 | 175.60 | 0.95386859 | 702.4 | 0.18452565 |
| 878.25 | 0.769 | 175.65 | 0.95389181 | 702.6 | 0.18443277 |
| 878.5 | 0.770 | 175.70 | 0.95391502 | 702.8 | 0.18433991 |
| 878.75 | 0.770 | 175.75 | 0.95393824 | 703.0 | 0.18424706 |
| 879 | 0.770 | 175.80 | 0.95396145 | 703.2 | 0.18415422 |
| 879.25 | 0.770 | 175.85 | 0.95398465 | 703.4 | 0.18406139 |
| 879.5 | 0.770 | 175.90 | 0.95400785 | 703.6 | 0.18396858 |
| 879.75 | 0.770 | 175.95 | 0.95403106 | 703.8 | 0.18387578 |
| 880 | 0.770 | 176.00 | 0.95405425 | 704.0 | 0.18378299 |
| 880.25 | 0.770 | 176.05 | 0.95407745 | 704.2 | 0.18369021 |
| 880.5 | 0.771 | 176.10 | 0.95410064 | 704.4 | 0.18359745 |
| 880.75 | 0.771 | 176.15 | 0.95412383 | 704.6 | 0.18350470 |
| 881 | 0.771 | 176.20 | 0.95414701 | 704.8 | 0.18341196 |
| 881.25 | 0.771 | 176.25 | 0.95417019 | 705.0 | 0.18331923 |
| 881.5 | 0.771 | 176.30 | 0.95419337 | 705.2 | 0.18322652 |
| 881.75 | 0.771 | 176.35 | 0.95421655 | 705.4 | 0.18313381 |
| 882 | 0.771 | 176.40 | 0.95423972 | 705.6 | 0.18304112 |
| 882.25 | 0.771 | 176.45 | 0.95426289 | 705.8 | 0.18294845 |
| 882.5 | 0.771 | 176.50 | 0.95428605 | 706.0 | 0.18285578 |
| 882.75 | 0.772 | 176.55 | 0.95430922 | 706.2 | 0.18276313 |
| 883 | 0.772 | 176.60 | 0.95433238 | 706.4 | 0.18267049 |
| 883.25 | 0.772 | 176.65 | 0.95435553 | 706.6 | 0.18257786 |
| 883.5 | 0.772 | 176.70 | 0.95437869 | 706.8 | 0.18248524 |
| 883.75 | 0.772 | 176.75 | 0.95440184 | 707.0 | 0.18239264 |
| 884 | 0.772 | 176.80 | 0.95442499 | 707.2 | 0.18230005 |
| 884.25 | 0.772 | 176.85 | 0.95444813 | 707.4 | 0.18220747 |
| 884.5 | 0.772 | 176.90 | 0.95447127 | 707.6 | 0.18211490 |
| 884.75 | 0.772 | 176.95 | 0.95449441 | 707.8 | 0.18202235 |
| 885 | 0.773 | 177.00 | 0.95451755 | 708.0 | 0.18192981 |
| 885.25 | 0.773 | 177.05 | 0.95454068 | 708.2 | 0.18183728 |
| 885.5 | 0.773 | 177.10 | 0.95456381 | 708.4 | 0.18174476 |


| 885.75 | 0.773 | 177.15 | 0.95458694 | 708.6 | 0.18165225 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 886 | 0.773 | 177.20 | 0.95461006 | 708.8 | 0.18155976 |
| 886.25 | 0.773 | 177.25 | 0.95463318 | 709.0 | 0.18146728 |
| 886.5 | 0.773 | 177.30 | 0.95465630 | 709.2 | 0.18137481 |
| 886.75 | 0.773 | 177.35 | 0.95467941 | 709.4 | 0.18128236 |
| 887 | 0.774 | 177.40 | 0.95470252 | 709.6 | 0.18118991 |
| 887.25 | 0.774 | 177.45 | 0.95472563 | 709.8 | 0.18109748 |
| 887.5 | 0.774 | 177.50 | 0.95474873 | 710.0 | 0.18100506 |
| 887.75 | 0.774 | 177.55 | 0.95477184 | 710.2 | 0.18091265 |
| 888 | 0.774 | 177.60 | 0.95479494 | 710.4 | 0.18082026 |
| 888.25 | 0.774 | 177.65 | 0.95481803 | 710.6 | 0.18072788 |
| 888.5 | 0.774 | 177.70 | 0.95484112 | 710.8 | 0.18063551 |
| 888.75 | 0.774 | 177.75 | 0.95486421 | 711.0 | 0.18054315 |
| 889 | 0.774 | 177.80 | 0.95488730 | 711.2 | 0.18045080 |
| 889.25 | 0.775 | 177.85 | 0.95491038 | 711.4 | 0.18035847 |
| 889.5 | 0.775 | 177.90 | 0.95493346 | 711.6 | 0.18026615 |
| 889.75 | 0.775 | 177.95 | 0.95495654 | 711.8 | 0.18017384 |
| 890 | 0.775 | 178.00 | 0.95497962 | 712.0 | 0.18008154 |
| 890.25 | 0.775 | 178.05 | 0.95500269 | 712.2 | 0.17998925 |
| 890.5 | 0.775 | 178.10 | 0.95502575 | 712.4 | 0.17989698 |
| 890.75 | 0.775 | 178.15 | 0.95504882 | 712.6 | 0.17980472 |
| 891 | 0.775 | 178.20 | 0.95507188 | 712.8 | 0.17971247 |
| 891.25 | 0.775 | 178.25 | 0.95509494 | 713.0 | 0.17962024 |
| 891.5 | 0.776 | 178.30 | 0.95511800 | 713.2 | 0.17952801 |
| 891.75 | 0.776 | 178.35 | 0.95514105 | 713.4 | 0.17943580 |
| 892 | 0.776 | 178.40 | 0.95516410 | 713.6 | 0.17934360 |
| 892.25 | 0.776 | 178.45 | 0.95518715 | 713.8 | 0.17925141 |
| 892.5 | 0.776 | 178.50 | 0.95521019 | 714.0 | 0.17915924 |
| 892.75 | 0.776 | 178.55 | 0.95523323 | 714.2 | 0.17906707 |
| 893 | 0.776 | 178.60 | 0.95525627 | 714.4 | 0.17897492 |
| 893.25 | 0.776 | 178.65 | 0.95527930 | 714.6 | 0.17888278 |
| 893.5 | 0.777 | 178.70 | 0.95530234 | 714.8 | 0.17879065 |
| 893.75 | 0.777 | 178.75 | 0.95532537 | 715.0 | 0.17869854 |
| 894 | 0.777 | 178.80 | 0.95534839 | 715.2 | 0.17860644 |
| 894.25 | 0.777 | 178.85 | 0.95537141 | 715.4 | 0.17851434 |
| 894.5 | 0.777 | 178.90 | 0.95539443 | 715.6 | 0.17842227 |
| 894.75 | 0.777 | 178.95 | 0.95541745 | 715.8 | 0.17833020 |
| 895 | 0.777 | 179.00 | 0.95544046 | 716.0 | 0.17823814 |
| 895.25 | 0.777 | 179.05 | 0.95546347 | 716.2 | 0.17814610 |
| 895.5 | 0.777 | 179.10 | 0.95548648 | 716.4 | 0.17805407 |
| 895.75 | 0.778 | 179.15 | 0.95550949 | 716.6 | 0.17796205 |
| 896 | 0.778 | 179.20 | 0.95553249 | 716.8 | 0.17787005 |
| 896.25 | 0.778 | 179.25 | 0.95555549 | 717.0 | 0.17777805 |
| 896.5 | 0.778 | 179.30 | 0.95557848 | 717.2 | 0.17768607 |
| 896.75 | 0.778 | 179.35 | 0.95560147 | 717.4 | 0.17759410 |
| 897 | 0.778 | 179.40 | 0.95562446 | 717.6 | 0.17750214 |
| 897.25 | 0.778 | 179.45 | 0.95564745 | 717.8 | 0.17741020 |
| 897.5 | 0.778 | 179.50 | 0.95567043 | 718.0 | 0.17731826 |
| 897.75 | 0.778 | 179.55 | 0.95569341 | 718.2 | 0.17722634 |
| 898 | 0.779 | 179.60 | 0.95571639 | 718.4 | 0.17713443 |
| 898.25 | 0.779 | 179.65 | 0.95573937 | 718.6 | 0.17704253 |
| 898.5 | 0.779 | 179.70 | 0.95576234 | 718.8 | 0.17695065 |
| 898.75 | 0.779 | 179.75 | 0.95578531 | 719.0 | 0.17685877 |
| 899 | 0.779 | 179.80 | 0.95580827 | 719.2 | 0.17676691 |
| 899.25 | 0.779 | 179.85 | 0.95583123 | 719.4 | 0.17667506 |
| 899.5 | 0.779 | 179.90 | 0.95585419 | 719.6 | 0.17658322 |
| 899.75 | 0.779 | 179.95 | 0.95587715 | 719.8 | 0.17649140 |
| 900 | 0.780 | 180.00 | 0.95590010 | 720.0 | 0.17639958 |
| 900.25 | 0.780 | 180.05 | 0.95592305 | 720.2 | 0.17630778 |
| 900.5 | 0.780 | 180.10 | 0.95594600 | 720.4 | 0.17621599 |
| 900.75 | 0.780 | 180.15 | 0.95596895 | 720.6 | 0.17612421 |
| 901 | 0.780 | 180.20 | 0.95599189 | 720.8 | 0.17603245 |
| 901.25 | 0.780 | 180.25 | 0.95601483 | 721.0 | 0.17594069 |
| 901.5 | 0.780 | 180.30 | 0.95603776 | 721.2 | 0.17584895 |
| 901.75 | 0.780 | 180.35 | 0.95606069 | 721.4 | 0.17575722 |
| 902 | 0.780 | 180.40 | 0.95608362 | 721.6 | 0.17566550 |
| 902.25 | 0.781 | 180.45 | 0.95610655 | 721.8 | 0.17557380 |
| 902.5 | 0.781 | 180.50 | 0.95612947 | 722.0 | 0.17548210 |
| 902.75 | 0.781 | 180.55 | 0.95615239 | 722.2 | 0.17539042 |
| 903 | 0.781 | 180.60 | 0.95617531 | 722.4 | 0.17529875 |
| 903.25 | 0.781 | 180.65 | 0.95619823 | 722.6 | 0.17520709 |


| 903.5 | 0.781 | 180.70 | 0.95622114 | 722.8 | 0.17511545 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 903.75 | 0.781 | 180.75 | 0.95624405 | 723.0 | 0.17502381 |
| 904 | 0.781 | 180.80 | 0.95626695 | 723.2 | 0.17493219 |
| 904.25 | 0.781 | 180.85 | 0.95628986 | 723.4 | 0.17484058 |
| 904.5 | 0.782 | 180.90 | 0.95631276 | 723.6 | 0.17474898 |
| 904.75 | 0.782 | 180.95 | 0.95633565 | 723.8 | 0.17465739 |
| 905 | 0.782 | 181.00 | 0.95635855 | 724.0 | 0.17456582 |
| 905.25 | 0.782 | 181.05 | 0.95638144 | 724.2 | 0.17447425 |
| 905.5 | 0.782 | 181.10 | 0.95640432 | 724.4 | 0.17438270 |
| 905.75 | 0.782 | 181.15 | 0.95642721 | 724.6 | 0.17429116 |
| 906 | 0.782 | 181.20 | 0.95645009 | 724.8 | 0.17419964 |
| 906.25 | 0.782 | 181.25 | 0.95647297 | 725.0 | 0.17410812 |
| 906.5 | 0.782 | 181.30 | 0.95649585 | 725.2 | 0.17401662 |
| 906.75 | 0.783 | 181.35 | 0.95651872 | 725.4 | 0.17392513 |
| 907 | 0.783 | 181.40 | 0.95654159 | 725.6 | 0.17383365 |
| 907.25 | 0.783 | 181.45 | 0.95656446 | 725.8 | 0.17374218 |
| 907.5 | 0.783 | 181.50 | 0.95658732 | 726.0 | 0.17365072 |
| 907.75 | 0.783 | 181.55 | 0.95661018 | 726.2 | 0.17355928 |
| 908 | 0.783 | 181.60 | 0.95663304 | 726.4 | 0.17346784 |
| 908.25 | 0.783 | 181.65 | 0.95665589 | 726.6 | 0.17337642 |
| 908.5 | 0.783 | 181.70 | 0.95667875 | 726.8 | 0.17328501 |
| 908.75 | 0.784 | 181.75 | 0.95670160 | 727.0 | 0.17319362 |
| 909 | 0.784 | 181.80 | 0.95672444 | 727.2 | 0.17310223 |
| 909.25 | 0.784 | 181.85 | 0.95674729 | 727.4 | 0.17301086 |
| 909.5 | 0.784 | 181.90 | 0.95677013 | 727.6 | 0.17291950 |
| 909.75 | 0.784 | 181.95 | 0.95679296 | 727.8 | 0.17282815 |
| 910 | 0.784 | 182.00 | 0.95681580 | 728.0 | 0.17273681 |
| 910.25 | 0.784 | 182.05 | 0.95683863 | 728.2 | 0.17264548 |
| 910.5 | 0.784 | 182.10 | 0.95686146 | 728.4 | 0.17255417 |
| 910.75 | 0.784 | 182.15 | 0.95688428 | 728.6 | 0.17246286 |
| 911 | 0.785 | 182.20 | 0.95690711 | 728.8 | 0.17237157 |
| 911.25 | 0.785 | 182.25 | 0.95692993 | 729.0 | 0.17228029 |
| 911.5 | 0.785 | 182.30 | 0.95695274 | 729.2 | 0.17218903 |
| 911.75 | 0.785 | 182.35 | 0.95697556 | 729.4 | 0.17209777 |
| 912 | 0.785 | 182.40 | 0.95699837 | 729.6 | 0.17200653 |
| 912.25 | 0.785 | 182.45 | 0.95702118 | 729.8 | 0.17191529 |
| 912.5 | 0.785 | 182.50 | 0.95704398 | 730.0 | 0.17182407 |
| 912.75 | 0.785 | 182.55 | 0.95706678 | 730.2 | 0.17173286 |
| 913 | 0.785 | 182.60 | 0.95708958 | 730.4 | 0.17164167 |
| 913.25 | 0.786 | 182.65 | 0.95711238 | 730.6 | 0.17155048 |
| 913.5 | 0.786 | 182.70 | 0.95713517 | 730.8 | 0.17145931 |
| 913.75 | 0.786 | 182.75 | 0.95715796 | 731.0 | 0.17136815 |
| 914 | 0.786 | 182.80 | 0.95718075 | 731.2 | 0.17127700 |
| 914.25 | 0.786 | 182.85 | 0.95720354 | 731.4 | 0.17118586 |
| 914.5 | 0.786 | 182.90 | 0.95722632 | 731.6 | 0.17109473 |
| 914.75 | 0.786 | 182.95 | 0.95724910 | 731.8 | 0.17100362 |
| 915 | 0.786 | 183.00 | 0.95727187 | 732.0 | 0.17091251 |
| 915.25 | 0.786 | 183.05 | 0.95729464 | 732.2 | 0.17082142 |
| 915.5 | 0.787 | 183.10 | 0.95731741 | 732.4 | 0.17073034 |
| 915.75 | 0.787 | 183.15 | 0.95734018 | 732.6 | 0.17063927 |
| 916 | 0.787 | 183.20 | 0.95736295 | 732.8 | 0.17054822 |
| 916.25 | 0.787 | 183.25 | 0.95738571 | 733.0 | 0.17045717 |
| 916.5 | 0.787 | 183.30 | 0.95740846 | 733.2 | 0.17036614 |
| 916.75 | 0.787 | 183.35 | 0.95743122 | 733.4 | 0.17027512 |
| 917 | 0.787 | 183.40 | 0.95745397 | 733.6 | 0.17018411 |
| 917.25 | 0.787 | 183.45 | 0.95747672 | 733.8 | 0.17009311 |
| 917.5 | 0.787 | 183.50 | 0.95749947 | 734.0 | 0.17000212 |
| 917.75 | 0.788 | 183.55 | 0.95752221 | 734.2 | 0.16991115 |
| 918 | 0.788 | 183.60 | 0.95754495 | 734.4 | 0.16982019 |
| 918.25 | 0.788 | 183.65 | 0.95756769 | 734.6 | 0.16972924 |
| 918.5 | 0.788 | 183.70 | 0.95759043 | 734.8 | 0.16963830 |
| 918.75 | 0.788 | 183.75 | 0.95761316 | 735.0 | 0.16954737 |
| 919 | 0.788 | 183.80 | 0.95763589 | 735.2 | 0.16945645 |
| 919.25 | 0.788 | 183.85 | 0.95765861 | 735.4 | 0.16936555 |
| 919.5 | 0.788 | 183.90 | 0.95768134 | 735.6 | 0.16927465 |
| 919.75 | 0.789 | 183.95 | 0.95770406 | 735.8 | 0.16918377 |
| 920 | 0.789 | 184.00 | 0.95772677 | 736.0 | 0.16909290 |
| 920.25 | 0.789 | 184.05 | 0.95774949 | 736.2 | 0.16900204 |
| 920.5 | 0.789 | 184.10 | 0.95777220 | 736.4 | 0.16891119 |
| 920.75 | 0.789 | 184.15 | 0.95779491 | 736.6 | 0.16882036 |
| 921 | 0.789 | 184.20 | 0.95781762 | 736.8 | 0.16872954 |


| 921.25 | 0.789 | 184.25 | 0.95784032 | 737.0 | 0.16863872 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 921.5 | 0.789 | 184.30 | 0.95786302 | 737.2 | 0.16854792 |
| 921.75 | 0.789 | 184.35 | 0.95788572 | 737.4 | 0.16845713 |
| 922 | 0.790 | 184.40 | 0.95790841 | 737.6 | 0.16836636 |
| 922.25 | 0.790 | 184.45 | 0.95793110 | 737.8 | 0.16827559 |
| 922.5 | 0.790 | 184.50 | 0.95795379 | 738.0 | 0.16818484 |
| 922.75 | 0.790 | 184.55 | 0.95797648 | 738.2 | 0.16809409 |
| 923 | 0.790 | 184.60 | 0.95799916 | 738.4 | 0.16800336 |
| 923.25 | 0.790 | 184.65 | 0.95802184 | 738.6 | 0.16791264 |
| 923.5 | 0.790 | 184.70 | 0.95804452 | 738.8 | 0.16782193 |
| 923.75 | 0.790 | 184.75 | 0.95806719 | 739.0 | 0.16773124 |
| 924 | 0.790 | 184.80 | 0.95808986 | 739.2 | 0.16764055 |
| 924.25 | 0.791 | 184.85 | 0.95811253 | 739.4 | 0.16754988 |
| 924.5 | 0.791 | 184.90 | 0.95813520 | 739.6 | 0.16745922 |
| 924.75 | 0.791 | 184.95 | 0.95815786 | 739.8 | 0.16736857 |
| 925 | 0.791 | 185.00 | 0.95818052 | 740.0 | 0.16727793 |
| 925.25 | 0.791 | 185.05 | 0.95820317 | 740.2 | 0.16718730 |
| 925.5 | 0.791 | 185.10 | 0.95822583 | 740.4 | 0.16709668 |
| 925.75 | 0.791 | 185.15 | 0.95824848 | 740.6 | 0.16700608 |
| 926 | 0.791 | 185.20 | 0.95827113 | 740.8 | 0.16691549 |
| 926.25 | 0.791 | 185.25 | 0.95829377 | 741.0 | 0.16682491 |
| 926.5 | 0.792 | 185.30 | 0.95831642 | 741.2 | 0.16673434 |
| 926.75 | 0.792 | 185.35 | 0.95833906 | 741.4 | 0.16664378 |
| 927 | 0.792 | 185.40 | 0.95836169 | 741.6 | 0.16655323 |
| 927.25 | 0.792 | 185.45 | 0.95838433 | 741.8 | 0.16646270 |
| 927.5 | 0.792 | 185.50 | 0.95840696 | 742.0 | 0.16637217 |
| 927.75 | 0.792 | 185.55 | 0.95842959 | 742.2 | 0.16628166 |
| 928 | 0.792 | 185.60 | 0.95845221 | 742.4 | 0.16619116 |
| 928.25 | 0.792 | 185.65 | 0.95847483 | 742.6 | 0.16610067 |
| 928.5 | 0.792 | 185.70 | 0.95849745 | 742.8 | 0.16601019 |
| 928.75 | 0.793 | 185.75 | 0.95852007 | 743.0 | 0.16591972 |
| 929 | 0.793 | 185.80 | 0.95854268 | 743.2 | 0.16582927 |
| 929.25 | 0.793 | 185.85 | 0.95856529 | 743.4 | 0.16573882 |
| 929.5 | 0.793 | 185.90 | 0.95858790 | 743.6 | 0.16564839 |
| 929.75 | 0.793 | 185.95 | 0.95861051 | 743.8 | 0.16555797 |
| 930 | 0.793 | 186.00 | 0.95863311 | 744.0 | 0.16546756 |
| 930.25 | 0.793 | 186.05 | 0.95865571 | 744.2 | 0.16537716 |
| 930.5 | 0.793 | 186.10 | 0.95867831 | 744.4 | 0.16528678 |
| 930.75 | 0.794 | 186.15 | 0.95870090 | 744.6 | 0.16519640 |
| 931 | 0.794 | 186.20 | 0.95872349 | 744.8 | 0.16510604 |
| 931.25 | 0.794 | 186.25 | 0.95874608 | 745.0 | 0.16501569 |
| 931.5 | 0.794 | 186.30 | 0.95876866 | 745.2 | 0.16492534 |
| 931.75 | 0.794 | 186.35 | 0.95879125 | 745.4 | 0.16483501 |
| 932 | 0.794 | 186.40 | 0.95881383 | 745.6 | 0.16474470 |
| 932.25 | 0.794 | 186.45 | 0.95883640 | 745.8 | 0.16465439 |
| 932.5 | 0.794 | 186.50 | 0.95885898 | 746.0 | 0.16456409 |
| 932.75 | 0.794 | 186.55 | 0.95888155 | 746.2 | 0.16447381 |
| 933 | 0.795 | 186.60 | 0.95890412 | 746.4 | 0.16438354 |
| 933.25 | 0.795 | 186.65 | 0.95892668 | 746.6 | 0.16429328 |
| 933.5 | 0.795 | 186.70 | 0.95894924 | 746.8 | 0.16420303 |
| 933.75 | 0.795 | 186.75 | 0.95897180 | 747.0 | 0.16411279 |
| 934 | 0.795 | 186.80 | 0.95899436 | 747.2 | 0.16402256 |
| 934.25 | 0.795 | 186.85 | 0.95901691 | 747.4 | 0.16393234 |
| 934.5 | 0.795 | 186.90 | 0.95903947 | 747.6 | 0.16384214 |
| 934.75 | 0.795 | 186.95 | 0.95906201 | 747.8 | 0.16375195 |
| 935 | 0.795 | 187.00 | 0.95908456 | 748.0 | 0.16366176 |
| 935.25 | 0.796 | 187.05 | 0.95910710 | 748.2 | 0.16357159 |
| 935.5 | 0.796 | 187.10 | 0.95912964 | 748.4 | 0.16348143 |
| 935.75 | 0.796 | 187.15 | 0.95915218 | 748.6 | 0.16339129 |
| 936 | 0.796 | 187.20 | 0.95917471 | 748.8 | 0.16330115 |
| 936.25 | 0.796 | 187.25 | 0.95919724 | 749.0 | 0.16321102 |
| 936.5 | 0.796 | 187.30 | 0.95921977 | 749.2 | 0.16312091 |
| 936.75 | 0.796 | 187.35 | 0.95924230 | 749.4 | 0.16303081 |
| 937 | 0.796 | 187.40 | 0.95926482 | 749.6 | 0.16294072 |
| 937.25 | 0.796 | 187.45 | 0.95928734 | 749.8 | 0.16285064 |
| 937.5 | 0.797 | 187.50 | 0.95930986 | 750.0 | 0.16276057 |
| 937.75 | 0.797 | 187.55 | 0.95933237 | 750.2 | 0.16267051 |
| 938 | 0.797 | 187.60 | 0.95935488 | 750.4 | 0.16258046 |
| 938.25 | 0.797 | 187.65 | 0.95937739 | 750.6 | 0.16249043 |
| 938.5 | 0.797 | 187.70 | 0.95939990 | 750.8 | 0.16240040 |
| 938.75 | 0.797 | 187.75 | 0.95942240 | 751.0 | 0.16231039 |


| 939 | 0.797 | 187.80 | 0.95944490 | 751.2 | 0.16222039 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 939.25 | 0.797 | 187.85 | 0.95946740 | 751.4 | 0.16213040 |
| 939.5 | 0.797 | 187.90 | 0.95948989 | 751.6 | 0.16204042 |
| 939.75 | 0.798 | 187.95 | 0.95951239 | 751.8 | 0.16195045 |
| 940 | 0.798 | 188.00 | 0.95953488 | 752.0 | 0.16186050 |
| 940.25 | 0.798 | 188.05 | 0.95955736 | 752.2 | 0.16177055 |
| 940.5 | 0.798 | 188.10 | 0.95957984 | 752.4 | 0.16168062 |
| 940.75 | 0.798 | 188.15 | 0.95960233 | 752.6 | 0.16159070 |
| 941 | 0.798 | 188.20 | 0.95962480 | 752.8 | 0.16150079 |
| 941.25 | 0.798 | 188.25 | 0.95964728 | 753.0 | 0.16141089 |
| 941.5 | 0.798 | 188.30 | 0.95966975 | 753.2 | 0.16132100 |
| 941.75 | 0.798 | 188.35 | 0.95969222 | 753.4 | 0.16123112 |
| 942 | 0.799 | 188.40 | 0.95971469 | 753.6 | 0.16114125 |
| 942.25 | 0.799 | 188.45 | 0.95973715 | 753.8 | 0.16105140 |
| 942.5 | 0.799 | 188.50 | 0.95975961 | 754.0 | 0.16096156 |
| 942.75 | 0.799 | 188.55 | 0.95978207 | 754.2 | 0.16087172 |
| 943 | 0.799 | 188.60 | 0.95980452 | 754.4 | 0.16078190 |
| 943.25 | 0.799 | 188.65 | 0.95982698 | 754.6 | 0.16069209 |
| 943.5 | 0.799 | 188.70 | 0.95984943 | 754.8 | 0.16060229 |
| 943.75 | 0.799 | 188.75 | 0.95987187 | 755.0 | 0.16051250 |
| 944 | 0.799 | 188.80 | 0.95989432 | 755.2 | 0.16042273 |
| 944.25 | 0.800 | 188.85 | 0.95991676 | 755.4 | 0.16033296 |
| 944.5 | 0.800 | 188.90 | 0.95993920 | 755.6 | 0.16024321 |
| 944.75 | 0.800 | 188.95 | 0.95996163 | 755.8 | 0.16015346 |
| 945 | 0.800 | 189.00 | 0.95998407 | 756.0 | 0.16006373 |
| 945.25 | 0.800 | 189.05 | 0.96000650 | 756.2 | 0.15997401 |
| 945.5 | 0.800 | 189.10 | 0.96002892 | 756.4 | 0.15988430 |
| 945.75 | 0.800 | 189.15 | 0.96005135 | 756.6 | 0.15979460 |
| 946 | 0.800 | 189.20 | 0.96007377 | 756.8 | 0.15970491 |
| 946.25 | 0.800 | 189.25 | 0.96009619 | 757.0 | 0.15961524 |
| 946.5 | 0.801 | 189.30 | 0.96011861 | 757.2 | 0.15952557 |
| 946.75 | 0.801 | 189.35 | 0.96014102 | 757.4 | 0.15943592 |
| 947 | 0.801 | 189.40 | 0.96016343 | 757.6 | 0.15934628 |
| 947.25 | 0.801 | 189.45 | 0.96018584 | 757.8 | 0.15925664 |
| 947.5 | 0.801 | 189.50 | 0.96020824 | 758.0 | 0.15916702 |
| 947.75 | 0.801 | 189.55 | 0.96023065 | 758.2 | 0.15907741 |
| 948 | 0.801 | 189.60 | 0.96025305 | 758.4 | 0.15898782 |
| 948.25 | 0.801 | 189.65 | 0.96027544 | 758.6 | 0.15889823 |
| 948.5 | 0.801 | 189.70 | 0.96029784 | 758.8 | 0.15880865 |
| 948.75 | 0.802 | 189.75 | 0.96032023 | 759.0 | 0.15871909 |
| 949 | 0.802 | 189.80 | 0.96034262 | 759.2 | 0.15862953 |
| 949.25 | 0.802 | 189.85 | 0.96036500 | 759.4 | 0.15853999 |
| 949.5 | 0.802 | 189.90 | 0.96038739 | 759.6 | 0.15845046 |
| 949.75 | 0.802 | 189.95 | 0.96040977 | 759.8 | 0.15836094 |
| 950 | 0.802 | 190.00 | 0.96043214 | 760.0 | 0.15827143 |
| 950.25 | 0.802 | 190.05 | 0.96045452 | 760.2 | 0.15818193 |
| 950.5 | 0.802 | 190.10 | 0.96047689 | 760.4 | 0.15809244 |
| 950.75 | 0.802 | 190.15 | 0.96049926 | 760.6 | 0.15800296 |
| 951 | 0.803 | 190.20 | 0.96052163 | 760.8 | 0.15791350 |
| 951.25 | 0.803 | 190.25 | 0.96054399 | 761.0 | 0.15782404 |
| 951.5 | 0.803 | 190.30 | 0.96056635 | 761.2 | 0.15773460 |
| 951.75 | 0.803 | 190.35 | 0.96058871 | 761.4 | 0.15764517 |
| 952 | 0.803 | 190.40 | 0.96061106 | 761.6 | 0.15755575 |
| 952.25 | 0.803 | 190.45 | 0.96063342 | 761.8 | 0.15746634 |
| 952.5 | 0.803 | 190.50 | 0.96065577 | 762.0 | 0.15737694 |
| 952.75 | 0.803 | 190.55 | 0.96067811 | 762.2 | 0.15728755 |
| 953 | 0.804 | 190.60 | 0.96070046 | 762.4 | 0.15719817 |
| 953.25 | 0.804 | 190.65 | 0.96072280 | 762.6 | 0.15710881 |
| 953.5 | 0.804 | 190.70 | 0.96074514 | 762.8 | 0.15701945 |
| 953.75 | 0.804 | 190.75 | 0.96076747 | 763.0 | 0.15693011 |
| 954 | 0.804 | 190.80 | 0.96078981 | 763.2 | 0.15684077 |
| 954.25 | 0.804 | 190.85 | 0.96081214 | 763.4 | 0.15675145 |
| 954.5 | 0.804 | 190.90 | 0.96083447 | 763.6 | 0.15666214 |
| 954.75 | 0.804 | 190.95 | 0.96085679 | 763.8 | 0.15657284 |
| 955 | 0.804 | 191.00 | 0.96087911 | 764.0 | 0.15648355 |
| 955.25 | 0.805 | 191.05 | 0.96090143 | 764.2 | 0.15639427 |
| 955.5 | 0.805 | 191.10 | 0.96092375 | 764.4 | 0.15630500 |
| 955.75 | 0.805 | 191.15 | 0.96094606 | 764.6 | 0.15621575 |
| 956 | 0.805 | 191.20 | 0.96096837 | 764.8 | 0.15612650 |
| 956.25 | 0.805 | 191.25 | 0.96099068 | 765.0 | 0.15603727 |
| 956.5 | 0.805 | 191.30 | 0.96101299 | 765.2 | 0.15594805 |


| 956.75 | 0.805 | 191.35 | 0.96103529 | 765.4 | 0.15585883 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 957 | 0.805 | 191.40 | 0.96105759 | 765.6 | 0.15576963 |
| 957.25 | 0.805 | 191.45 | 0.96107989 | 765.8 | 0.15568044 |
| 957.5 | 0.806 | 191.50 | 0.96110218 | 766.0 | 0.15559126 |
| 957.75 | 0.806 | 191.55 | 0.96112448 | 766.2 | 0.15550209 |
| 958 | 0.806 | 191.60 | 0.96114677 | 766.4 | 0.15541294 |
| 958.25 | 0.806 | 191.65 | 0.96116905 | 766.6 | 0.15532379 |
| 958.5 | 0.806 | 191.70 | 0.96119134 | 766.8 | 0.15523465 |
| 958.75 | 0.806 | 191.75 | 0.96121362 | 767.0 | 0.15514553 |
| 959 | 0.806 | 191.80 | 0.96123590 | 767.2 | 0.15505641 |
| 959.25 | 0.806 | 191.85 | 0.96125817 | 767.4 | 0.15496731 |
| 959.5 | 0.806 | 191.90 | 0.96128045 | 767.6 | 0.15487822 |
| 959.75 | 0.807 | 191.95 | 0.96130272 | 767.8 | 0.15478914 |
| 960 | 0.807 | 192.00 | 0.96132498 | 768.0 | 0.15470007 |
| 960.25 | 0.807 | 192.05 | 0.96134725 | 768.2 | 0.15461101 |
| 960.5 | 0.807 | 192.10 | 0.96136951 | 768.4 | 0.15452196 |
| 960.75 | 0.807 | 192.15 | 0.96139177 | 768.6 | 0.15443292 |
| 961 | 0.807 | 192.20 | 0.96141403 | 768.8 | 0.15434390 |
| 961.25 | 0.807 | 192.25 | 0.96143628 | 769.0 | 0.15425488 |
| 961.5 | 0.807 | 192.30 | 0.96145853 | 769.2 | 0.15416587 |
| 961.75 | 0.807 | 192.35 | 0.96148078 | 769.4 | 0.15407688 |
| 962 | 0.808 | 192.40 | 0.96150303 | 769.6 | 0.15398790 |
| 962.25 | 0.808 | 192.45 | 0.96152527 | 769.8 | 0.15389892 |
| 962.5 | 0.808 | 192.50 | 0.96154751 | 770.0 | 0.15380996 |
| 962.75 | 0.808 | 192.55 | 0.96156975 | 770.2 | 0.15372101 |
| 963 | 0.808 | 192.60 | 0.96159198 | 770.4 | 0.15363207 |
| 963.25 | 0.808 | 192.65 | 0.96161421 | 770.6 | 0.15354314 |
| 963.5 | 0.808 | 192.70 | 0.96163644 | 770.8 | 0.15345423 |
| 963.75 | 0.808 | 192.75 | 0.96165867 | 771.0 | 0.15336532 |
| 964 | 0.808 | 192.80 | 0.96168089 | 771.2 | 0.15327642 |
| 964.25 | 0.809 | 192.85 | 0.96170312 | 771.4 | 0.15318754 |
| 964.5 | 0.809 | 192.90 | 0.96172533 | 771.6 | 0.15309866 |
| 964.75 | 0.809 | 192.95 | 0.96174755 | 771.8 | 0.15300980 |
| 965 | 0.809 | 193.00 | 0.96176976 | 772.0 | 0.15292095 |
| 965.25 | 0.809 | 193.05 | 0.96179197 | 772.2 | 0.15283210 |
| 965.5 | 0.809 | 193.10 | 0.96181418 | 772.4 | 0.15274327 |
| 965.75 | 0.809 | 193.15 | 0.96183639 | 772.6 | 0.15265445 |
| 966 | 0.809 | 193.20 | 0.96185859 | 772.8 | 0.15256564 |
| 966.25 | 0.809 | 193.25 | 0.96188079 | 773.0 | 0.15247684 |
| 966.5 | 0.810 | 193.30 | 0.96190299 | 773.2 | 0.15238805 |
| 966.75 | 0.810 | 193.35 | 0.96192518 | 773.4 | 0.15229928 |
| 967 | 0.810 | 193.40 | 0.96194737 | 773.6 | 0.15221051 |
| 967.25 | 0.810 | 193.45 | 0.96196956 | 773.8 | 0.15212175 |
| 967.5 | 0.810 | 193.50 | 0.96199175 | 774.0 | 0.15203301 |
| 967.75 | 0.810 | 193.55 | 0.96201393 | 774.2 | 0.15194428 |
| 968 | 0.810 | 193.60 | 0.96203611 | 774.4 | 0.15185555 |
| 968.25 | 0.810 | 193.65 | 0.96205829 | 774.6 | 0.15176684 |
| 968.5 | 0.810 | 193.70 | 0.96208047 | 774.8 | 0.15167814 |
| 968.75 | 0.811 | 193.75 | 0.96210264 | 775.0 | 0.15158945 |
| 969 | 0.811 | 193.80 | 0.96212481 | 775.2 | 0.15150077 |
| 969.25 | 0.811 | 193.85 | 0.96214698 | 775.4 | 0.15141210 |
| 969.5 | 0.811 | 193.90 | 0.96216914 | 775.6 | 0.15132344 |
| 969.75 | 0.811 | 193.95 | 0.96219130 | 775.8 | 0.15123479 |
| 970 | 0.811 | 194.00 | 0.96221346 | 776.0 | 0.15114615 |
| 970.25 | 0.811 | 194.05 | 0.96223562 | 776.2 | 0.15105752 |
| 970.5 | 0.811 | 194.10 | 0.96225777 | 776.4 | 0.15096891 |
| 970.75 | 0.811 | 194.15 | 0.96227992 | 776.6 | 0.15088030 |
| 971 | 0.812 | 194.20 | 0.96230207 | 776.8 | 0.15079171 |
| 971.25 | 0.812 | 194.25 | 0.96232422 | 777.0 | 0.15070312 |
| 971.5 | 0.812 | 194.30 | 0.96234636 | 777.2 | 0.15061455 |
| 971.75 | 0.812 | 194.35 | 0.96236850 | 777.4 | 0.15052599 |
| 972 | 0.812 | 194.40 | 0.96239064 | 777.6 | 0.15043744 |
| 972.25 | 0.812 | 194.45 | 0.96241278 | 777.8 | 0.15034890 |
| 972.5 | 0.812 | 194.50 | 0.96243491 | 778.0 | 0.15026037 |
| 972.75 | 0.812 | 194.55 | 0.96245704 | 778.2 | 0.15017185 |
| 973 | 0.812 | 194.60 | 0.96247917 | 778.4 | 0.15008334 |
| 973.25 | 0.813 | 194.65 | 0.96250129 | 778.6 | 0.14999484 |
| 973.5 | 0.813 | 194.70 | 0.96252341 | 778.8 | 0.14990635 |
| 973.75 | 0.813 | 194.75 | 0.96254553 | 779.0 | 0.14981787 |
| 974 | 0.813 | 194.80 | 0.96256765 | 779.2 | 0.14972941 |
| 974.25 | 0.813 | 194.85 | 0.96258976 | 779.4 | 0.14964095 |


| 974.5 | 0.813 | 194.90 | 0.96261187 | 779.6 | 0.14955251 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 974.75 | 0.813 | 194.95 | 0.96263398 | 779.8 | 0.14946407 |
| 975 | 0.813 | 195.00 | 0.96265609 | 780.0 | 0.14937565 |
| 975.25 | 0.813 | 195.05 | 0.96267819 | 780.2 | 0.14928724 |
| 975.5 | 0.814 | 195.10 | 0.96270029 | 780.4 | 0.14919884 |
| 975.75 | 0.814 | 195.15 | 0.96272239 | 780.6 | 0.14911044 |
| 976 | 0.814 | 195.20 | 0.96274448 | 780.8 | 0.14902206 |
| 976.25 | 0.814 | 195.25 | 0.96276658 | 781.0 | 0.14893369 |
| 976.5 | 0.814 | 195.30 | 0.96278867 | 781.2 | 0.14884533 |
| 976.75 | 0.814 | 195.35 | 0.96281075 | 781.4 | 0.14875698 |
| 977 | 0.814 | 195.40 | 0.96283284 | 781.6 | 0.14866865 |
| 977.25 | 0.814 | 195.45 | 0.96285492 | 781.8 | 0.14858032 |
| 977.5 | 0.814 | 195.50 | 0.96287700 | 782.0 | 0.14849200 |
| 977.75 | 0.814 | 195.55 | 0.96289908 | 782.2 | 0.14840369 |
| 978 | 0.815 | 195.60 | 0.96292115 | 782.4 | 0.14831540 |
| 978.25 | 0.815 | 195.65 | 0.96294322 | 782.6 | 0.14822711 |
| 978.5 | 0.815 | 195.70 | 0.96296529 | 782.8 | 0.14813884 |
| 978.75 | 0.815 | 195.75 | 0.96298736 | 783.0 | 0.14805057 |
| 979 | 0.815 | 195.80 | 0.96300942 | 783.2 | 0.14796232 |
| 979.25 | 0.815 | 195.85 | 0.96303148 | 783.4 | 0.14787408 |
| 979.5 | 0.815 | 195.90 | 0.96305354 | 783.6 | 0.14778585 |
| 979.75 | 0.815 | 195.95 | 0.96307559 | 783.8 | 0.14769762 |
| 980 | 0.815 | 196.00 | 0.96309765 | 784.0 | 0.14760941 |
| 980.25 | 0.816 | 196.05 | 0.96311970 | 784.2 | 0.14752121 |
| 980.5 | 0.816 | 196.10 | 0.96314174 | 784.4 | 0.14743302 |
| 980.75 | 0.816 | 196.15 | 0.96316379 | 784.6 | 0.14734484 |
| 981 | 0.816 | 196.20 | 0.96318583 | 784.8 | 0.14725667 |
| 981.25 | 0.816 | 196.25 | 0.96320787 | 785.0 | 0.14716852 |
| 981.5 | 0.816 | 196.30 | 0.96322991 | 785.2 | 0.14708037 |
| 981.75 | 0.816 | 196.35 | 0.96325194 | 785.4 | 0.14699223 |
| 982 | 0.816 | 196.40 | 0.96327397 | 785.6 | 0.14690410 |
| 982.25 | 0.816 | 196.45 | 0.96329600 | 785.8 | 0.14681599 |
| 982.5 | 0.817 | 196.50 | 0.96331803 | 786.0 | 0.14672788 |
| 982.75 | 0.817 | 196.55 | 0.96334005 | 786.2 | 0.14663979 |
| 983 | 0.817 | 196.60 | 0.96336207 | 786.4 | 0.14655170 |
| 983.25 | 0.817 | 196.65 | 0.96338409 | 786.6 | 0.14646363 |
| 983.5 | 0.817 | 196.70 | 0.96340611 | 786.8 | 0.14637557 |
| 983.75 | 0.817 | 196.75 | 0.96342812 | 787.0 | 0.14628751 |
| 984 | 0.817 | 196.80 | 0.96345013 | 787.2 | 0.14619947 |
| 984.25 | 0.817 | 196.85 | 0.96347214 | 787.4 | 0.14611144 |
| 984.5 | 0.817 | 196.90 | 0.96349415 | 787.6 | 0.14602342 |
| 984.75 | 0.818 | 196.95 | 0.96351615 | 787.8 | 0.14593541 |
| 985 | 0.818 | 197.00 | 0.96353815 | 788.0 | 0.14584741 |
| 985.25 | 0.818 | 197.05 | 0.96356015 | 788.2 | 0.14575942 |
| 985.5 | 0.818 | 197.10 | 0.96358214 | 788.4 | 0.14567144 |
| 985.75 | 0.818 | 197.15 | 0.96360413 | 788.6 | 0.14558347 |
| 986 | 0.818 | 197.20 | 0.96362612 | 788.8 | 0.14549551 |
| 986.25 | 0.818 | 197.25 | 0.96364811 | 789.0 | 0.14540756 |
| 986.5 | 0.818 | 197.30 | 0.96367009 | 789.2 | 0.14531962 |
| 986.75 | 0.818 | 197.35 | 0.96369208 | 789.4 | 0.14523170 |
| 987 | 0.819 | 197.40 | 0.96371406 | 789.6 | 0.14514378 |
| 987.25 | 0.819 | 197.45 | 0.96373603 | 789.8 | 0.14505587 |
| 987.5 | 0.819 | 197.50 | 0.96375801 | 790.0 | 0.14496798 |
| 987.75 | 0.819 | 197.55 | 0.96377998 | 790.2 | 0.14488009 |
| 988 | 0.819 | 197.60 | 0.96380195 | 790.4 | 0.14479222 |
| 988.25 | 0.819 | 197.65 | 0.96382391 | 790.6 | 0.14470435 |
| 988.5 | 0.819 | 197.70 | 0.96384587 | 790.8 | 0.14461650 |
| 988.75 | 0.819 | 197.75 | 0.96386784 | 791.0 | 0.14452866 |
| 989 | 0.819 | 197.80 | 0.96388979 | 791.2 | 0.14444082 |
| 989.25 | 0.820 | 197.85 | 0.96391175 | 791.4 | 0.14435300 |
| 989.5 | 0.820 | 197.90 | 0.96393370 | 791.6 | 0.14426519 |
| 989.75 | 0.820 | 197.95 | 0.96395565 | 791.8 | 0.14417739 |
| 990 | 0.820 | 198.00 | 0.96397760 | 792.0 | 0.14408960 |
| 990.25 | 0.820 | 198.05 | 0.96399955 | 792.2 | 0.14400182 |
| 990.5 | 0.820 | 198.10 | 0.96402149 | 792.4 | 0.14391405 |
| 990.75 | 0.820 | 198.15 | 0.96404343 | 792.6 | 0.14382629 |
| 991 | 0.820 | 198.20 | 0.96406537 | 792.8 | 0.14373854 |
| 991.25 | 0.820 | 198.25 | 0.96408730 | 793.0 | 0.14365080 |
| 991.5 | 0.821 | 198.30 | 0.96410923 | 793.2 | 0.14356307 |
| 991.75 | 0.821 | 198.35 | 0.96413116 | 793.4 | 0.14347535 |
| 992 | 0.821 | 198.40 | 0.96415309 | 793.6 | 0.14338764 |


| 992.25 | 0.821 | 198.45 | 0.96417501 | 793.8 | 0.14329994 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 992.5 | 0.821 | 198.50 | 0.96419694 | 794.0 | 0.14321226 |
| 992.75 | 0.821 | 198.55 | 0.96421885 | 794.2 | 0.14312458 |
| 993 | 0.821 | 198.60 | 0.96424077 | 794.4 | 0.14303691 |
| 993.25 | 0.821 | 198.65 | 0.96426269 | 794.6 | 0.14294926 |
| 993.5 | 0.821 | 198.70 | 0.96428460 | 794.8 | 0.14286161 |
| 993.75 | 0.822 | 198.75 | 0.96430651 | 795.0 | 0.14277398 |
| 994 | 0.822 | 198.80 | 0.96432841 | 795.2 | 0.14268635 |
| 994.25 | 0.822 | 198.85 | 0.96435032 | 795.4 | 0.14259874 |
| 994.5 | 0.822 | 198.90 | 0.96437222 | 795.6 | 0.14251113 |
| 994.75 | 0.822 | 198.95 | 0.96439412 | 795.8 | 0.14242354 |
| 995 | 0.822 | 199.00 | 0.96441601 | 796.0 | 0.14233596 |
| 995.25 | 0.822 | 199.05 | 0.96443790 | 796.2 | 0.14224838 |
| 995.5 | 0.822 | 199.10 | 0.96445980 | 796.4 | 0.14216082 |
| 995.75 | 0.822 | 199.15 | 0.96448168 | 796.6 | 0.14207327 |
| 996 | 0.823 | 199.20 | 0.96450357 | 796.8 | 0.14198572 |
| 996.25 | 0.823 | 199.25 | 0.96452545 | 797.0 | 0.14189819 |
| 996.5 | 0.823 | 199.30 | 0.96454733 | 797.2 | 0.14181067 |
| 996.75 | 0.823 | 199.35 | 0.96456921 | 797.4 | 0.14172316 |
| 997 | 0.823 | 199.40 | 0.96459109 | 797.6 | 0.14163566 |
| 997.25 | 0.823 | 199.45 | 0.96461296 | 797.8 | 0.14154817 |
| 997.5 | 0.823 | 199.50 | 0.96463483 | 798.0 | 0.14146069 |
| 997.75 | 0.823 | 199.55 | 0.96465670 | 798.2 | 0.14137322 |
| 998 | 0.823 | 199.60 | 0.96467856 | 798.4 | 0.14128576 |
| 998.25 | 0.824 | 199.65 | 0.96470042 | 798.6 | 0.14119831 |
| 998.5 | 0.824 | 199.70 | 0.96472228 | 798.8 | 0.14111087 |
| 998.75 | 0.824 | 199.75 | 0.96474414 | 799.0 | 0.14102344 |
| 999 | 0.824 | 199.80 | 0.96476599 | 799.2 | 0.14093602 |
| 999.25 | 0.824 | 199.85 | 0.96478785 | 799.4 | 0.14084861 |
| 999.5 | 0.824 | 199.90 | 0.96480970 | 799.6 | 0.14076122 |
| 999.75 | 0.824 | 199.95 | 0.96483154 | 799.8 | 0.14067383 |
| 1000 | 0.824 | 200.00 | 0.96485339 | 800.0 | 0.14058645 |
| 1000.25 | 0.824 | 200.05 | 0.96487523 | 800.2 | 0.14049908 |
| 1000.5 | 0.824 | 200.10 | 0.96489707 | 800.4 | 0.14041173 |
| 1000.75 | 0.825 | 200.15 | 0.96491890 | 800.6 | 0.14032438 |
| 1001 | 0.825 | 200.20 | 0.96494074 | 800.8 | 0.14023704 |
| 1001.25 | 0.825 | 200.25 | 0.96496257 | 801.0 | 0.14014972 |
| 1001.5 | 0.825 | 200.30 | 0.96498440 | 801.2 | 0.14006240 |
| 1001.75 | 0.825 | 200.35 | 0.96500623 | 801.4 | 0.13997510 |
| 1002 | 0.825 | 200.40 | 0.96502805 | 801.6 | 0.13988780 |
| 1002.25 | 0.825 | 200.45 | 0.96504987 | 801.8 | 0.13980052 |
| 1002.5 | 0.825 | 200.50 | 0.96507169 | 802.0 | 0.13971324 |
| 1002.75 | 0.825 | 200.55 | 0.96509351 | 802.2 | 0.13962598 |
| 1003 | 0.826 | 200.60 | 0.96511532 | 802.4 | 0.13953872 |
| 1003.25 | 0.826 | 200.65 | 0.96513713 | 802.6 | 0.13945148 |
| 1003.5 | 0.826 | 200.70 | 0.96515894 | 802.8 | 0.13936424 |
| 1003.75 | 0.826 | 200.75 | 0.96518075 | 803.0 | 0.13927702 |
| 1004 | 0.826 | 200.80 | 0.96520255 | 803.2 | 0.13918981 |
| 1004.25 | 0.826 | 200.85 | 0.96522435 | 803.4 | 0.13910260 |
| 1004.5 | 0.826 | 200.90 | 0.96524615 | 803.6 | 0.13901541 |
| 1004.75 | 0.826 | 200.95 | 0.96526794 | 803.8 | 0.13892823 |
| 1005 | 0.826 | 201.00 | 0.96528974 | 804.0 | 0.13884105 |
| 1005.25 | 0.827 | 201.05 | 0.96531153 | 804.2 | 0.13875389 |
| 1005.5 | 0.827 | 201.10 | 0.96533332 | 804.4 | 0.13866674 |
| 1005.75 | 0.827 | 201.15 | 0.96535510 | 804.6 | 0.13857960 |
| 1006 | 0.827 | 201.20 | 0.96537688 | 804.8 | 0.13849246 |
| 1006.25 | 0.827 | 201.25 | 0.96539866 | 805.0 | 0.13840534 |
| 1006.5 | 0.827 | 201.30 | 0.96542044 | 805.2 | 0.13831823 |
| 1006.75 | 0.827 | 201.35 | 0.96544222 | 805.4 | 0.13823113 |
| 1007 | 0.827 | 201.40 | 0.96546399 | 805.6 | 0.13814404 |
| 1007.25 | 0.827 | 201.45 | 0.96548576 | 805.8 | 0.13805696 |
| 1007.5 | 0.828 | 201.50 | 0.96550753 | 806.0 | 0.13796989 |
| 1007.75 | 0.828 | 201.55 | 0.96552929 | 806.2 | 0.13788282 |
| 1008 | 0.828 | 201.60 | 0.96555106 | 806.4 | 0.13779577 |
| 1008.25 | 0.828 | 201.65 | 0.96557282 | 806.6 | 0.13770873 |
| 1008.5 | 0.828 | 201.70 | 0.96559457 | 806.8 | 0.13762170 |
| 1008.75 | 0.828 | 201.75 | 0.96561633 | 807.0 | 0.13753468 |
| 1009 | 0.828 | 201.80 | 0.96563808 | 807.2 | 0.13744767 |
| 1009.25 | 0.828 | 201.85 | 0.96565983 | 807.4 | 0.13736067 |
| 1009.5 | 0.828 | 201.90 | 0.96568158 | 807.6 | 0.13727368 |
| 1009.75 | 0.829 | 201.95 | 0.96570332 | 807.8 | 0.13718670 |


| 1010 | 0.829 | 202.00 | 0.96572507 | 808.0 | 0.13709973 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1010.25 | 0.829 | 202.05 | 0.96574681 | 808.2 | 0.13701277 |
| 1010.5 | 0.829 | 202.10 | 0.96576854 | 808.4 | 0.13692582 |
| 1010.75 | 0.829 | 202.15 | 0.96579028 | 808.6 | 0.13683888 |
| 1011 | 0.829 | 202.20 | 0.96581201 | 808.8 | 0.13675195 |
| 1011.25 | 0.829 | 202.25 | 0.96583374 | 809.0 | 0.13666504 |
| 1011.5 | 0.829 | 202.30 | 0.96585547 | 809.2 | 0.13657813 |
| 1011.75 | 0.829 | 202.35 | 0.96587719 | 809.4 | 0.13649123 |
| 1012 | 0.829 | 202.40 | 0.96589892 | 809.6 | 0.13640434 |
| 1012.25 | 0.830 | 202.45 | 0.96592063 | 809.8 | 0.13631746 |
| 1012.5 | 0.830 | 202.50 | 0.96594235 | 810.0 | 0.13623059 |
| 1012.75 | 0.830 | 202.55 | 0.96596407 | 810.2 | 0.13614373 |
| 1013 | 0.830 | 202.60 | 0.96598578 | 810.4 | 0.13605688 |
| 1013.25 | 0.830 | 202.65 | 0.96600749 | 810.6 | 0.13597005 |
| 1013.5 | 0.830 | 202.70 | 0.96602920 | 810.8 | 0.13588322 |
| 1013.75 | 0.830 | 202.75 | 0.96605090 | 811.0 | 0.13579640 |
| 1014 | 0.830 | 202.80 | 0.96607260 | 811.2 | 0.13570959 |
| 1014.25 | 0.830 | 202.85 | 0.96609430 | 811.4 | 0.13562279 |
| 1014.5 | 0.831 | 202.90 | 0.96611600 | 811.6 | 0.13553600 |
| 1014.75 | 0.831 | 202.95 | 0.96613769 | 811.8 | 0.13544923 |
| 1015 | 0.831 | 203.00 | 0.96615939 | 812.0 | 0.13536246 |
| 1015.25 | 0.831 | 203.05 | 0.96618107 | 812.2 | 0.13527570 |
| 1015.5 | 0.831 | 203.10 | 0.96620276 | 812.4 | 0.13518895 |
| 1015.75 | 0.831 | 203.15 | 0.96622445 | 812.6 | 0.13510221 |
| 1016 | 0.831 | 203.20 | 0.96624613 | 812.8 | 0.13501549 |
| 1016.25 | 0.831 | 203.25 | 0.96626781 | 813.0 | 0.13492877 |
| 1016.5 | 0.831 | 203.30 | 0.96628948 | 813.2 | 0.13484206 |
| 1016.75 | 0.832 | 203.35 | 0.96631116 | 813.4 | 0.13475536 |
| 1017 | 0.832 | 203.40 | 0.96633283 | 813.6 | 0.13466868 |
| 1017.25 | 0.832 | 203.45 | 0.96635450 | 813.8 | 0.13458200 |
| 1017.5 | 0.832 | 203.50 | 0.96637617 | 814.0 | 0.13449533 |
| 1017.75 | 0.832 | 203.55 | 0.96639783 | 814.2 | 0.13440867 |
| 1018 | 0.832 | 203.60 | 0.96641949 | 814.4 | 0.13432202 |
| 1018.25 | 0.832 | 203.65 | 0.96644115 | 814.6 | 0.13423539 |
| 1018.5 | 0.832 | 203.70 | 0.96646281 | 814.8 | 0.13414876 |
| 1018.75 | 0.832 | 203.75 | 0.96648446 | 815.0 | 0.13406214 |
| 1019 | 0.833 | 203.80 | 0.96650612 | 815.2 | 0.13397553 |
| 1019.25 | 0.833 | 203.85 | 0.96652777 | 815.4 | 0.13388894 |
| 1019.5 | 0.833 | 203.90 | 0.96654941 | 815.6 | 0.13380235 |
| 1019.75 | 0.833 | 203.95 | 0.96657106 | 815.8 | 0.13371577 |
| 1020 | 0.833 | 204.00 | 0.96659270 | 816.0 | 0.13362920 |
| 1020.25 | 0.833 | 204.05 | 0.96661434 | 816.2 | 0.13354264 |
| 1020.5 | 0.833 | 204.10 | 0.96663598 | 816.4 | 0.13345610 |
| 1020.75 | 0.833 | 204.15 | 0.96665761 | 816.6 | 0.13336956 |
| 1021 | 0.833 | 204.20 | 0.96667924 | 816.8 | 0.13328303 |
| 1021.25 | 0.834 | 204.25 | 0.96670087 | 817.0 | 0.13319651 |
| 1021.5 | 0.834 | 204.30 | 0.96672250 | 817.2 | 0.13311000 |
| 1021.75 | 0.834 | 204.35 | 0.96674412 | 817.4 | 0.13302351 |
| 1022 | 0.834 | 204.40 | 0.96676575 | 817.6 | 0.13293702 |
| 1022.25 | 0.834 | 204.45 | 0.96678737 | 817.8 | 0.13285054 |
| 1022.5 | 0.834 | 204.50 | 0.96680898 | 818.0 | 0.13276407 |
| 1022.75 | 0.834 | 204.55 | 0.96683060 | 818.2 | 0.13267761 |
| 1023 | 0.834 | 204.60 | 0.96685221 | 818.4 | 0.13259116 |
| 1023.25 | 0.834 | 204.65 | 0.96687382 | 818.6 | 0.13250473 |
| 1023.5 | 0.834 | 204.70 | 0.96689543 | 818.8 | 0.13241830 |
| 1023.75 | 0.835 | 204.75 | 0.96691703 | 819.0 | 0.13233188 |
| 1024 | 0.835 | 204.80 | 0.96693863 | 819.2 | 0.13224547 |
| 1024.25 | 0.835 | 204.85 | 0.96696023 | 819.4 | 0.13215907 |
| 1024.5 | 0.835 | 204.90 | 0.96698183 | 819.6 | 0.13207268 |
| 1024.75 | 0.835 | 204.95 | 0.96700342 | 819.8 | 0.13198630 |
| 1025 | 0.835 | 205.00 | 0.96702502 | 820.0 | 0.13189993 |
| 1025.25 | 0.835 | 205.05 | 0.96704661 | 820.2 | 0.13181357 |
| 1025.5 | 0.835 | 205.10 | 0.96706819 | 820.4 | 0.13172723 |
| 1025.75 | 0.835 | 205.15 | 0.96708978 | 820.6 | 0.13164089 |
| 1026 | 0.836 | 205.20 | 0.96711136 | 820.8 | 0.13155456 |
| 1026.25 | 0.836 | 205.25 | 0.96713294 | 821.0 | 0.13146824 |
| 1026.5 | 0.836 | 205.30 | 0.96715452 | 821.2 | 0.13138193 |
| 1026.75 | 0.836 | 205.35 | 0.96717609 | 821.4 | 0.13129563 |
| 1027 | 0.836 | 205.40 | 0.96719767 | 821.6 | 0.13120934 |
| 1027.25 | 0.836 | 205.45 | 0.96721924 | 821.8 | 0.13112306 |
| 1027.5 | 0.836 | 205.50 | 0.96724080 | 822.0 | 0.13103679 |


| 1027.75 | 0.836 | 205.55 | 0.96726237 | 822.2 | 0.13095053 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1028 | 0.836 | 205.60 | 0.96728393 | 822.4 | 0.13086428 |
| 1028.25 | 0.837 | 205.65 | 0.96730549 | 822.6 | 0.13077803 |
| 1028.5 | 0.837 | 205.70 | 0.96732705 | 822.8 | 0.13069180 |
| 1028.75 | 0.837 | 205.75 | 0.96734860 | 823.0 | 0.13060558 |
| 1029 | 0.837 | 205.80 | 0.96737016 | 823.2 | 0.13051937 |
| 1029.25 | 0.837 | 205.85 | 0.96739171 | 823.4 | 0.13043317 |
| 1029.5 | 0.837 | 205.90 | 0.96741326 | 823.6 | 0.13034698 |
| 1029.75 | 0.837 | 205.95 | 0.96743480 | 823.8 | 0.13026080 |
| 1030 | 0.837 | 206.00 | 0.96745634 | 824.0 | 0.13017463 |
| 1030.25 | 0.837 | 206.05 | 0.96747788 | 824.2 | 0.13008846 |
| 1030.5 | 0.837 | 206.10 | 0.96749942 | 824.4 | 0.13000231 |
| 1030.75 | 0.838 | 206.15 | 0.96752096 | 824.6 | 0.12991617 |
| 1031 | 0.838 | 206.20 | 0.96754249 | 824.8 | 0.12983004 |
| 1031.25 | 0.838 | 206.25 | 0.96756402 | 825.0 | 0.12974391 |
| 1031.5 | 0.838 | 206.30 | 0.96758555 | 825.2 | 0.12965780 |
| 1031.75 | 0.838 | 206.35 | 0.96760708 | 825.4 | 0.12957170 |
| 1032 | 0.838 | 206.40 | 0.96762860 | 825.6 | 0.12948561 |
| 1032.25 | 0.838 | 206.45 | 0.96765012 | 825.8 | 0.12939952 |
| 1032.5 | 0.838 | 206.50 | 0.96767164 | 826.0 | 0.12931345 |
| 1032.75 | 0.838 | 206.55 | 0.96769315 | 826.2 | 0.12922738 |
| 1033 | 0.839 | 206.60 | 0.96771467 | 826.4 | 0.12914133 |
| 1033.25 | 0.839 | 206.65 | 0.96773618 | 826.6 | 0.12905529 |
| 1033.5 | 0.839 | 206.70 | 0.96775769 | 826.8 | 0.12896925 |
| 1033.75 | 0.839 | 206.75 | 0.96777919 | 827.0 | 0.12888323 |
| 1034 | 0.839 | 206.80 | 0.96780070 | 827.2 | 0.12879721 |
| 1034.25 | 0.839 | 206.85 | 0.96782220 | 827.4 | 0.12871121 |
| 1034.5 | 0.839 | 206.90 | 0.96784370 | 827.6 | 0.12862521 |
| 1034.75 | 0.839 | 206.95 | 0.96786519 | 827.8 | 0.12853923 |
| 1035 | 0.839 | 207.00 | 0.96788669 | 828.0 | 0.12845325 |
| 1035.25 | 0.840 | 207.05 | 0.96790818 | 828.2 | 0.12836728 |
| 1035.5 | 0.840 | 207.10 | 0.96792967 | 828.4 | 0.12828133 |
| 1035.75 | 0.840 | 207.15 | 0.96795115 | 828.6 | 0.12819538 |
| 1036 | 0.840 | 207.20 | 0.96797264 | 828.8 | 0.12810944 |
| 1036.25 | 0.840 | 207.25 | 0.96799412 | 829.0 | 0.12802352 |
| 1036.5 | 0.840 | 207.30 | 0.96801560 | 829.2 | 0.12793760 |
| 1036.75 | 0.840 | 207.35 | 0.96803708 | 829.4 | 0.12785169 |
| 1037 | 0.840 | 207.40 | 0.96805855 | 829.6 | 0.12776579 |
| 1037.25 | 0.840 | 207.45 | 0.96808002 | 829.8 | 0.12767991 |
| 1037.5 | 0.841 | 207.50 | 0.96810149 | 830.0 | 0.12759403 |
| 1037.75 | 0.841 | 207.55 | 0.96812296 | 830.2 | 0.12750816 |
| 1038 | 0.841 | 207.60 | 0.96814442 | 830.4 | 0.12742230 |
| 1038.25 | 0.841 | 207.65 | 0.96816589 | 830.6 | 0.12733645 |
| 1038.5 | 0.841 | 207.70 | 0.96818735 | 830.8 | 0.12725061 |
| 1038.75 | 0.841 | 207.75 | 0.96820880 | 831.0 | 0.12716478 |
| 1039 | 0.841 | 207.80 | 0.96823026 | 831.2 | 0.12707896 |
| 1039.25 | 0.841 | 207.85 | 0.96825171 | 831.4 | 0.12699315 |
| 1039.5 | 0.841 | 207.90 | 0.96827316 | 831.6 | 0.12690735 |
| 1039.75 | 0.841 | 207.95 | 0.96829461 | 831.8 | 0.12682156 |
| 1040 | 0.842 | 208.00 | 0.96831606 | 832.0 | 0.12673578 |
| 1040.25 | 0.842 | 208.05 | 0.96833750 | 832.2 | 0.12665001 |
| 1040.5 | 0.842 | 208.10 | 0.96835894 | 832.4 | 0.12656424 |
| 1040.75 | 0.842 | 208.15 | 0.96838038 | 832.6 | 0.12647849 |
| 1041 | 0.842 | 208.20 | 0.96840181 | 832.8 | 0.12639275 |
| 1041.25 | 0.842 | 208.25 | 0.96842325 | 833.0 | 0.12630702 |
| 1041.5 | 0.842 | 208.30 | 0.96844468 | 833.2 | 0.12622129 |
| 1041.75 | 0.842 | 208.35 | 0.96846610 | 833.4 | 0.12613558 |
| 1042 | 0.842 | 208.40 | 0.96848753 | 833.6 | 0.12604988 |
| 1042.25 | 0.843 | 208.45 | 0.96850895 | 833.8 | 0.12596418 |
| 1042.5 | 0.843 | 208.50 | 0.96853038 | 834.0 | 0.12587850 |
| 1042.75 | 0.843 | 208.55 | 0.96855179 | 834.2 | 0.12579282 |
| 1043 | 0.843 | 208.60 | 0.96857321 | 834.4 | 0.12570716 |
| 1043.25 | 0.843 | 208.65 | 0.96859462 | 834.6 | 0.12562150 |
| 1043.5 | 0.843 | 208.70 | 0.96861604 | 834.8 | 0.12553586 |
| 1043.75 | 0.843 | 208.75 | 0.96863745 | 835.0 | 0.12545022 |
| 1044 | 0.843 | 208.80 | 0.96865885 | 835.2 | 0.12536459 |
| 1044.25 | 0.843 | 208.85 | 0.96868026 | 835.4 | 0.12527898 |
| 1044.5 | 0.844 | 208.90 | 0.96870166 | 835.6 | 0.12519337 |
| 1044.75 | 0.844 | 208.95 | 0.96872306 | 835.8 | 0.12510777 |
| 1045 | 0.844 | 209.00 | 0.96874445 | 836.0 | 0.12502218 |
| 1045.25 | 0.844 | 209.05 | 0.96876585 | 836.2 | 0.12493660 |


| 1045.5 | 0.844 | 209.10 | 0.96878724 | 836.4 | 0.12485104 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1045.75 | 0.844 | 209.15 | 0.96880863 | 836.6 | 0.12476548 |
| 1046 | 0.844 | 209.20 | 0.96883002 | 836.8 | 0.12467993 |
| 1046.25 | 0.844 | 209.25 | 0.96885140 | 837.0 | 0.12459439 |
| 1046.5 | 0.844 | 209.30 | 0.96887279 | 837.2 | 0.12450886 |
| 1046.75 | 0.844 | 209.35 | 0.96889417 | 837.4 | 0.12442334 |
| 1047 | 0.845 | 209.40 | 0.96891554 | 837.6 | 0.12433782 |
| 1047.25 | 0.845 | 209.45 | 0.96893692 | 837.8 | 0.12425232 |
| 1047.5 | 0.845 | 209.50 | 0.96895829 | 838.0 | 0.12416683 |
| 1047.75 | 0.845 | 209.55 | 0.96897966 | 838.2 | 0.12408135 |
| 1048 | 0.845 | 209.60 | 0.96900103 | 838.4 | 0.12399588 |
| 1048.25 | 0.845 | 209.65 | 0.96902240 | 838.6 | 0.12391041 |
| 1048.5 | 0.845 | 209.70 | 0.96904376 | 838.8 | 0.12382496 |
| 1048.75 | 0.845 | 209.75 | 0.96906512 | 839.0 | 0.12373951 |
| 1049 | 0.845 | 209.80 | 0.96908648 | 839.2 | 0.12365408 |
| 1049.25 | 0.846 | 209.85 | 0.96910784 | 839.4 | 0.12356865 |
| 1049.5 | 0.846 | 209.90 | 0.96912919 | 839.6 | 0.12348324 |
| 1049.75 | 0.846 | 209.95 | 0.96915054 | 839.8 | 0.12339783 |
| 1050 | 0.846 | 210.00 | 0.96917189 | 840.0 | 0.12331244 |
| 1050.25 | 0.846 | 210.05 | 0.96919324 | 840.2 | 0.12322705 |
| 1050.5 | 0.846 | 210.10 | 0.96921458 | 840.4 | 0.12314167 |
| 1050.75 | 0.846 | 210.15 | 0.96923592 | 840.6 | 0.12305631 |
| 1051 | 0.846 | 210.20 | 0.96925726 | 840.8 | 0.12297095 |
| 1051.25 | 0.846 | 210.25 | 0.96927860 | 841.0 | 0.12288560 |
| 1051.5 | 0.846 | 210.30 | 0.96929994 | 841.2 | 0.12280026 |
| 1051.75 | 0.847 | 210.35 | 0.96932127 | 841.4 | 0.12271493 |
| 1052 | 0.847 | 210.40 | 0.96934260 | 841.6 | 0.12262961 |
| 1052.25 | 0.847 | 210.45 | 0.96936393 | 841.8 | 0.12254430 |
| 1052.5 | 0.847 | 210.50 | 0.96938525 | 842.0 | 0.12245900 |
| 1052.75 | 0.847 | 210.55 | 0.96940657 | 842.2 | 0.12237371 |
| 1053 | 0.847 | 210.60 | 0.96942789 | 842.4 | 0.12228843 |
| 1053.25 | 0.847 | 210.65 | 0.96944921 | 842.6 | 0.12220315 |
| 1053.5 | 0.847 | 210.70 | 0.96947053 | 842.8 | 0.12211789 |
| 1053.75 | 0.847 | 210.75 | 0.96949184 | 843.0 | 0.12203264 |
| 1054 | 0.848 | 210.80 | 0.96951315 | 843.2 | 0.12194739 |
| 1054.25 | 0.848 | 210.85 | 0.96953446 | 843.4 | 0.12186216 |
| 1054.5 | 0.848 | 210.90 | 0.96955577 | 843.6 | 0.12177693 |
| 1054.75 | 0.848 | 210.95 | 0.96957707 | 843.8 | 0.12169172 |
| 1055 | 0.848 | 211.00 | 0.96959837 | 844.0 | 0.12160651 |
| 1055.25 | 0.848 | 211.05 | 0.96961967 | 844.2 | 0.12152132 |
| 1055.5 | 0.848 | 211.10 | 0.96964097 | 844.4 | 0.12143613 |
| 1055.75 | 0.848 | 211.15 | 0.96966226 | 844.6 | 0.12135095 |
| 1056 | 0.848 | 211.20 | 0.96968355 | 844.8 | 0.12126578 |
| 1056.25 | 0.849 | 211.25 | 0.96970484 | 845.0 | 0.12118063 |
| 1056.5 | 0.849 | 211.30 | 0.96972613 | 845.2 | 0.12109548 |
| 1056.75 | 0.849 | 211.35 | 0.96974742 | 845.4 | 0.12101034 |
| 1057 | 0.849 | 211.40 | 0.96976870 | 845.6 | 0.12092521 |
| 1057.25 | 0.849 | 211.45 | 0.96978998 | 845.8 | 0.12084009 |
| 1057.5 | 0.849 | 211.50 | 0.96981126 | 846.0 | 0.12075498 |
| 1057.75 | 0.849 | 211.55 | 0.96983253 | 846.2 | 0.12066987 |
| 1058 | 0.849 | 211.60 | 0.96985380 | 846.4 | 0.12058478 |
| 1058.25 | 0.849 | 211.65 | 0.96987508 | 846.6 | 0.12049970 |
| 1058.5 | 0.849 | 211.70 | 0.96989634 | 846.8 | 0.12041463 |
| 1058.75 | 0.850 | 211.75 | 0.96991761 | 847.0 | 0.12032956 |
| 1059 | 0.850 | 211.80 | 0.96993887 | 847.2 | 0.12024451 |
| 1059.25 | 0.850 | 211.85 | 0.96996013 | 847.4 | 0.12015946 |
| 1059.5 | 0.850 | 211.90 | 0.96998139 | 847.6 | 0.12007443 |
| 1059.75 | 0.850 | 211.95 | 0.97000265 | 847.8 | 0.11998940 |
| 1060 | 0.850 | 212.00 | 0.97002390 | 848.0 | 0.11990438 |
| 1060.25 | 0.850 | 212.05 | 0.97004516 | 848.2 | 0.11981938 |
| 1060.5 | 0.850 | 212.10 | 0.97006641 | 848.4 | 0.11973438 |
| 1060.75 | 0.850 | 212.15 | 0.97008765 | 848.6 | 0.11964939 |
| 1061 | 0.851 | 212.20 | 0.97010890 | 848.8 | 0.11956441 |
| 1061.25 | 0.851 | 212.25 | 0.97013014 | 849.0 | 0.11947944 |
| 1061.5 | 0.851 | 212.30 | 0.97015138 | 849.2 | 0.11939448 |
| 1061.75 | 0.851 | 212.35 | 0.97017262 | 849.4 | 0.11930953 |
| 1062 | 0.851 | 212.40 | 0.97019385 | 849.6 | 0.11922459 |
| 1062.25 | 0.851 | 212.45 | 0.97021509 | 849.8 | 0.11913966 |
| 1062.5 | 0.851 | 212.50 | 0.97023632 | 850.0 | 0.11905474 |
| 1062.75 | 0.851 | 212.55 | 0.97025754 | 850.2 | 0.11896982 |
| 1063 | 0.851 | 212.60 | 0.97027877 | 850.4 | 0.11888492 |


| 1063.25 | 0.851 | 212.65 | 0.97029999 | 850.6 | 0.11880002 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1063.5 | 0.852 | 212.70 | 0.97032122 | 850.8 | 0.11871514 |
| 1063.75 | 0.852 | 212.75 | 0.97034243 | 851.0 | 0.11863026 |
| 1064 | 0.852 | 212.80 | 0.97036365 | 851.2 | 0.11854540 |
| 1064.25 | 0.852 | 212.85 | 0.97038486 | 851.4 | 0.11846054 |
| 1064.5 | 0.852 | 212.90 | 0.97040608 | 851.6 | 0.11837569 |
| 1064.75 | 0.852 | 212.95 | 0.97042729 | 851.8 | 0.11829085 |
| 1065 | 0.852 | 213.00 | 0.97044849 | 852.0 | 0.11820603 |
| 1065.25 | 0.852 | 213.05 | 0.97046970 | 852.2 | 0.11812121 |
| 1065.5 | 0.852 | 213.10 | 0.97049090 | 852.4 | 0.11803640 |
| 1065.75 | 0.853 | 213.15 | 0.97051210 | 852.6 | 0.11795160 |
| 1066 | 0.853 | 213.20 | 0.97053330 | 852.8 | 0.11786680 |
| 1066.25 | 0.853 | 213.25 | 0.97055449 | 853.0 | 0.11778202 |
| 1066.5 | 0.853 | 213.30 | 0.97057569 | 853.2 | 0.11769725 |
| 1066.75 | 0.853 | 213.35 | 0.97059688 | 853.4 | 0.11761249 |
| 1067 | 0.853 | 213.40 | 0.97061807 | 853.6 | 0.11752773 |
| 1067.25 | 0.853 | 213.45 | 0.97063925 | 853.8 | 0.11744299 |
| 1067.5 | 0.853 | 213.50 | 0.97066044 | 854.0 | 0.11735825 |
| 1067.75 | 0.853 | 213.55 | 0.97068162 | 854.2 | 0.11727353 |
| 1068 | 0.854 | 213.60 | 0.97070280 | 854.4 | 0.11718881 |
| 1068.25 | 0.854 | 213.65 | 0.97072397 | 854.6 | 0.11710410 |
| 1068.5 | 0.854 | 213.70 | 0.97074515 | 854.8 | 0.11701940 |
| 1068.75 | 0.854 | 213.75 | 0.97076632 | 855.0 | 0.11693472 |
| 1069 | 0.854 | 213.80 | 0.97078749 | 855.2 | 0.11685004 |
| 1069.25 | 0.854 | 213.85 | 0.97080866 | 855.4 | 0.11676537 |
| 1069.5 | 0.854 | 213.90 | 0.97082982 | 855.6 | 0.11668070 |
| 1069.75 | 0.854 | 213.95 | 0.97085099 | 855.8 | 0.11659605 |
| 1070 | 0.854 | 214.00 | 0.97087215 | 856.0 | 0.11651141 |
| 1070.25 | 0.854 | 214.05 | 0.97089331 | 856.2 | 0.11642678 |
| 1070.5 | 0.855 | 214.10 | 0.97091446 | 856.4 | 0.11634215 |
| 1070.75 | 0.855 | 214.15 | 0.97093562 | 856.6 | 0.11625754 |
| 1071 | 0.855 | 214.20 | 0.97095677 | 856.8 | 0.11617293 |
| 1071.25 | 0.855 | 214.25 | 0.97097792 | 857.0 | 0.11608834 |
| 1071.5 | 0.855 | 214.30 | 0.97099906 | 857.2 | 0.11600375 |
| 1071.75 | 0.855 | 214.35 | 0.97102021 | 857.4 | 0.11591918 |
| 1072 | 0.855 | 214.40 | 0.97104135 | 857.6 | 0.11583461 |
| 1072.25 | 0.855 | 214.45 | 0.97106249 | 857.8 | 0.11575005 |
| 1072.5 | 0.855 | 214.50 | 0.97108363 | 858.0 | 0.11566550 |
| 1072.75 | 0.856 | 214.55 | 0.97110476 | 858.2 | 0.11558096 |
| 1073 | 0.856 | 214.60 | 0.97112589 | 858.4 | 0.11549643 |
| 1073.25 | 0.856 | 214.65 | 0.97114702 | 858.6 | 0.11541191 |
| 1073.5 | 0.856 | 214.70 | 0.97116815 | 858.8 | 0.11532739 |
| 1073.75 | 0.856 | 214.75 | 0.97118928 | 859.0 | 0.11524289 |
| 1074 | 0.856 | 214.80 | 0.97121040 | 859.2 | 0.11515840 |
| 1074.25 | 0.856 | 214.85 | 0.97123152 | 859.4 | 0.11507391 |
| 1074.5 | 0.856 | 214.90 | 0.97125264 | 859.6 | 0.11498944 |
| 1074.75 | 0.856 | 214.95 | 0.97127376 | 859.8 | 0.11490497 |
| 1075 | 0.856 | 215.00 | 0.97129487 | 860.0 | 0.11482051 |
| 1075.25 | 0.857 | 215.05 | 0.97131598 | 860.2 | 0.11473607 |
| 1075.5 | 0.857 | 215.10 | 0.97133709 | 860.4 | 0.11465163 |
| 1075.75 | 0.857 | 215.15 | 0.97135820 | 860.6 | 0.11456720 |
| 1076 | 0.857 | 215.20 | 0.97137931 | 860.8 | 0.11448278 |
| 1076.25 | 0.857 | 215.25 | 0.97140041 | 861.0 | 0.11439837 |
| 1076.5 | 0.857 | 215.30 | 0.97142151 | 861.2 | 0.11431397 |
| 1076.75 | 0.857 | 215.35 | 0.97144261 | 861.4 | 0.11422957 |
| 1077 | 0.857 | 215.40 | 0.97146370 | 861.6 | 0.11414519 |
| 1077.25 | 0.857 | 215.45 | 0.97148480 | 861.8 | 0.11406082 |
| 1077.5 | 0.858 | 215.50 | 0.97150589 | 862.0 | 0.11397645 |
| 1077.75 | 0.858 | 215.55 | 0.97152698 | 862.2 | 0.11389210 |
| 1078 | 0.858 | 215.60 | 0.97154806 | 862.4 | 0.11380775 |
| 1078.25 | 0.858 | 215.65 | 0.97156915 | 862.6 | 0.11372341 |
| 1078.5 | 0.858 | 215.70 | 0.97159023 | 862.8 | 0.11363908 |
| 1078.75 | 0.858 | 215.75 | 0.97161131 | 863.0 | 0.11355476 |
| 1079 | 0.858 | 215.80 | 0.97163239 | 863.2 | 0.11347046 |
| 1079.25 | 0.858 | 215.85 | 0.97165346 | 863.4 | 0.11338615 |
| 1079.5 | 0.858 | 215.90 | 0.97167453 | 863.6 | 0.11330186 |
| 1079.75 | 0.858 | 215.95 | 0.97169560 | 863.8 | 0.11321758 |
| 1080 | 0.859 | 216.00 | 0.97171667 | 864.0 | 0.11313331 |
| 1080.25 | 0.859 | 216.05 | 0.97173774 | 864.2 | 0.11304904 |
| 1080.5 | 0.859 | 216.10 | 0.97175880 | 864.4 | 0.11296479 |
| 1080.75 | 0.859 | 216.15 | 0.97177986 | 864.6 | 0.11288054 |


| 1081 | 0.859 | 216.20 | 0.97180092 | 864.8 | 0.11279631 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1081.25 | 0.859 | 216.25 | 0.97182198 | 865.0 | 0.11271208 |
| 1081.5 | 0.859 | 216.30 | 0.97184303 | 865.2 | 0.11262786 |
| 1081.75 | 0.859 | 216.35 | 0.97186409 | 865.4 | 0.11254365 |
| 1082 | 0.859 | 216.40 | 0.97188514 | 865.6 | 0.11245945 |
| 1082.25 | 0.860 | 216.45 | 0.97190618 | 865.8 | 0.11237526 |
| 1082.5 | 0.860 | 216.50 | 0.97192723 | 866.0 | 0.11229108 |
| 1082.75 | 0.860 | 216.55 | 0.97194827 | 866.2 | 0.11220691 |
| 1083 | 0.860 | 216.60 | 0.97196931 | 866.4 | 0.11212275 |
| 1083.25 | 0.860 | 216.65 | 0.97199035 | 866.6 | 0.11203859 |
| 1083.5 | 0.860 | 216.70 | 0.97201139 | 866.8 | 0.11195445 |
| 1083.75 | 0.860 | 216.75 | 0.97203242 | 867.0 | 0.11187031 |
| 1084 | 0.860 | 216.80 | 0.97205345 | 867.2 | 0.11178619 |
| 1084.25 | 0.860 | 216.85 | 0.97207448 | 867.4 | 0.11170207 |
| 1084.5 | 0.860 | 216.90 | 0.97209551 | 867.6 | 0.11161796 |
| 1084.75 | 0.861 | 216.95 | 0.97211653 | 867.8 | 0.11153386 |
| 1085 | 0.861 | 217.00 | 0.97213756 | 868.0 | 0.11144977 |
| 1085.25 | 0.861 | 217.05 | 0.97215858 | 868.2 | 0.11136569 |
| 1085.5 | 0.861 | 217.10 | 0.97217960 | 868.4 | 0.11128162 |
| 1085.75 | 0.861 | 217.15 | 0.97220061 | 868.6 | 0.11119755 |
| 1086 | 0.861 | 217.20 | 0.97222162 | 868.8 | 0.11111350 |
| 1086.25 | 0.861 | 217.25 | 0.97224264 | 869.0 | 0.11102946 |
| 1086.5 | 0.861 | 217.30 | 0.97226364 | 869.2 | 0.11094542 |
| 1086.75 | 0.861 | 217.35 | 0.97228465 | 869.4 | 0.11086139 |
| 1087 | 0.862 | 217.40 | 0.97230566 | 869.6 | 0.11077738 |
| 1087.25 | 0.862 | 217.45 | 0.97232666 | 869.8 | 0.11069337 |
| 1087.5 | 0.862 | 217.50 | 0.97234766 | 870.0 | 0.11060937 |
| 1087.75 | 0.862 | 217.55 | 0.97236866 | 870.2 | 0.11052538 |
| 1088 | 0.862 | 217.60 | 0.97238965 | 870.4 | 0.11044140 |
| 1088.25 | 0.862 | 217.65 | 0.97241064 | 870.6 | 0.11035743 |
| 1088.5 | 0.862 | 217.70 | 0.97243163 | 870.8 | 0.11027346 |
| 1088.75 | 0.862 | 217.75 | 0.97245262 | 871.0 | 0.11018951 |
| 1089 | 0.862 | 217.80 | 0.97247361 | 871.2 | 0.11010556 |
| 1089.25 | 0.862 | 217.85 | 0.97249459 | 871.4 | 0.11002163 |
| 1089.5 | 0.863 | 217.90 | 0.97251557 | 871.6 | 0.10993770 |
| 1089.75 | 0.863 | 217.95 | 0.97253655 | 871.8 | 0.10985378 |
| 1090 | 0.863 | 218.00 | 0.97255753 | 872.0 | 0.10976988 |
| 1090.25 | 0.863 | 218.05 | 0.97257851 | 872.2 | 0.10968598 |
| 1090.5 | 0.863 | 218.10 | 0.97259948 | 872.4 | 0.10960208 |
| 1090.75 | 0.863 | 218.15 | 0.97262045 | 872.6 | 0.10951820 |
| 1091 | 0.863 | 218.20 | 0.97264142 | 872.8 | 0.10943433 |
| 1091.25 | 0.863 | 218.25 | 0.97266238 | 873.0 | 0.10935047 |
| 1091.5 | 0.863 | 218.30 | 0.97268335 | 873.2 | 0.10926661 |
| 1091.75 | 0.864 | 218.35 | 0.97270431 | 873.4 | 0.10918277 |
| 1092 | 0.864 | 218.40 | 0.97272527 | 873.6 | 0.10909893 |
| 1092.25 | 0.864 | 218.45 | 0.97274622 | 873.8 | 0.10901510 |
| 1092.5 | 0.864 | 218.50 | 0.97276718 | 874.0 | 0.10893129 |
| 1092.75 | 0.864 | 218.55 | 0.97278813 | 874.2 | 0.10884748 |
| 1093 | 0.864 | 218.60 | 0.97280908 | 874.4 | 0.10876368 |
| 1093.25 | 0.864 | 218.65 | 0.97283003 | 874.6 | 0.10867988 |
| 1093.5 | 0.864 | 218.70 | 0.97285097 | 874.8 | 0.10859610 |
| 1093.75 | 0.864 | 218.75 | 0.97287192 | 875.0 | 0.10851233 |
| 1094 | 0.864 | 218.80 | 0.97289286 | 875.2 | 0.10842856 |
| 1094.25 | 0.865 | 218.85 | 0.97291380 | 875.4 | 0.10834481 |
| 1094.5 | 0.865 | 218.90 | 0.97293473 | 875.6 | 0.10826106 |
| 1094.75 | 0.865 | 218.95 | 0.97295567 | 875.8 | 0.10817733 |
| 1095 | 0.865 | 219.00 | 0.97297660 | 876.0 | 0.10809360 |
| 1095.25 | 0.865 | 219.05 | 0.97299753 | 876.2 | 0.10800988 |
| 1095.5 | 0.865 | 219.10 | 0.97301846 | 876.4 | 0.10792617 |
| 1095.75 | 0.865 | 219.15 | 0.97303938 | 876.6 | 0.10784247 |
| 1096 | 0.865 | 219.20 | 0.97306031 | 876.8 | 0.10775877 |
| 1096.25 | 0.865 | 219.25 | 0.97308123 | 877.0 | 0.10767509 |
| 1096.5 | 0.866 | 219.30 | 0.97310215 | 877.2 | 0.10759142 |
| 1096.75 | 0.866 | 219.35 | 0.97312306 | 877.4 | 0.10750775 |
| 1097 | 0.866 | 219.40 | 0.97314398 | 877.6 | 0.10742409 |
| 1097.25 | 0.866 | 219.45 | 0.97316489 | 877.8 | 0.10734045 |
| 1097.5 | 0.866 | 219.50 | 0.97318580 | 878.0 | 0.10725681 |
| 1097.75 | 0.866 | 219.55 | 0.97320671 | 878.2 | 0.10717318 |
| 1098 | 0.866 | 219.60 | 0.97322761 | 878.4 | 0.10708956 |
| 1098.25 | 0.866 | 219.65 | 0.97324851 | 878.6 | 0.10700595 |
| 1098.5 | 0.866 | 219.70 | 0.97326941 | 878.8 | 0.10692234 |


| 1098.75 | 0.866 | 219.75 | 0.97329031 | 879.0 | 0.10683875 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1099 | 0.867 | 219.80 | 0.97331121 | 879.2 | 0.10675516 |
| 1099.25 | 0.867 | 219.85 | 0.97333210 | 879.4 | 0.10667159 |
| 1099.5 | 0.867 | 219.90 | 0.97335299 | 879.6 | 0.10658802 |
| 1099.75 | 0.867 | 219.95 | 0.97337388 | 879.8 | 0.10650446 |
| 1100 | 0.867 | 220.00 | 0.97339477 | 880.0 | 0.10642091 |
| 1100.25 | 0.867 | 220.05 | 0.97341566 | 880.2 | 0.10633737 |
| 1100.5 | 0.867 | 220.10 | 0.97343654 | 880.4 | 0.10625384 |
| 1100.75 | 0.867 | 220.15 | 0.97345742 | 880.6 | 0.10617032 |
| 1101 | 0.867 | 220.20 | 0.97347830 | 880.8 | 0.10608681 |
| 1101.25 | 0.867 | 220.25 | 0.97349917 | 881.0 | 0.10600330 |
| 1101.5 | 0.868 | 220.30 | 0.97352005 | 881.2 | 0.10591981 |
| 1101.75 | 0.868 | 220.35 | 0.97354092 | 881.4 | 0.10583632 |
| 1102 | 0.868 | 220.40 | 0.97356179 | 881.6 | 0.10575284 |
| 1102.25 | 0.868 | 220.45 | 0.97358266 | 881.8 | 0.10566937 |
| 1102.5 | 0.868 | 220.50 | 0.97360352 | 882.0 | 0.10558591 |
| 1102.75 | 0.868 | 220.55 | 0.97362438 | 882.2 | 0.10550246 |
| 1103 | 0.868 | 220.60 | 0.97364525 | 882.4 | 0.10541902 |
| 1103.25 | 0.868 | 220.65 | 0.97366610 | 882.6 | 0.10533558 |
| 1103.5 | 0.868 | 220.70 | 0.97368696 | 882.8 | 0.10525216 |
| 1103.75 | 0.869 | 220.75 | 0.97370781 | 883.0 | 0.10516874 |
| 1104 | 0.869 | 220.80 | 0.97372867 | 883.2 | 0.10508534 |
| 1104.25 | 0.869 | 220.85 | 0.97374952 | 883.4 | 0.10500194 |
| 1104.5 | 0.869 | 220.90 | 0.97377036 | 883.6 | 0.10491855 |
| 1104.75 | 0.869 | 220.95 | 0.97379121 | 883.8 | 0.10483517 |
| 1105 | 0.869 | 221.00 | 0.97381205 | 884.0 | 0.10475180 |
| 1105.25 | 0.869 | 221.05 | 0.97383289 | 884.2 | 0.10466844 |
| 1105.5 | 0.869 | 221.10 | 0.97385373 | 884.4 | 0.10458508 |
| 1105.75 | 0.869 | 221.15 | 0.97387457 | 884.6 | 0.10450174 |
| 1106 | 0.869 | 221.20 | 0.97389540 | 884.8 | 0.10441840 |
| 1106.25 | 0.870 | 221.25 | 0.97391623 | 885.0 | 0.10433508 |
| 1106.5 | 0.870 | 221.30 | 0.97393706 | 885.2 | 0.10425176 |
| 1106.75 | 0.870 | 221.35 | 0.97395789 | 885.4 | 0.10416845 |
| 1107 | 0.870 | 221.40 | 0.97397871 | 885.6 | 0.10408515 |
| 1107.25 | 0.870 | 221.45 | 0.97399954 | 885.8 | 0.10400186 |
| 1107.5 | 0.870 | 221.50 | 0.97402036 | 886.0 | 0.10391857 |
| 1107.75 | 0.870 | 221.55 | 0.97404118 | 886.2 | 0.10383530 |
| 1108 | 0.870 | 221.60 | 0.97406199 | 886.4 | 0.10375203 |
| 1108.25 | 0.870 | 221.65 | 0.97408281 | 886.6 | 0.10366878 |
| 1108.5 | 0.871 | 221.70 | 0.97410362 | 886.8 | 0.10358553 |
| 1108.75 | 0.871 | 221.75 | 0.97412443 | 887.0 | 0.10350229 |
| 1109 | 0.871 | 221.80 | 0.97414523 | 887.2 | 0.10341906 |
| 1109.25 | 0.871 | 221.85 | 0.97416604 | 887.4 | 0.10333584 |
| 1109.5 | 0.871 | 221.90 | 0.97418684 | 887.6 | 0.10325263 |
| 1109.75 | 0.871 | 221.95 | 0.97420764 | 887.8 | 0.10316943 |
| 1110 | 0.871 | 222.00 | 0.97422844 | 888.0 | 0.10308623 |
| 1110.25 | 0.871 | 222.05 | 0.97424924 | 888.2 | 0.10300305 |
| 1110.5 | 0.871 | 222.10 | 0.97427003 | 888.4 | 0.10291987 |
| 1110.75 | 0.871 | 222.15 | 0.97429082 | 888.6 | 0.10283670 |
| 1111 | 0.872 | 222.20 | 0.97431161 | 888.8 | 0.10275354 |
| 1111.25 | 0.872 | 222.25 | 0.97433240 | 889.0 | 0.10267039 |
| 1111.5 | 0.872 | 222.30 | 0.97435319 | 889.2 | 0.10258725 |
| 1111.75 | 0.872 | 222.35 | 0.97437397 | 889.4 | 0.10250412 |
| 1112 | 0.872 | 222.40 | 0.97439475 | 889.6 | 0.10242099 |
| 1112.25 | 0.872 | 222.45 | 0.97441553 | 889.8 | 0.10233788 |
| 1112.5 | 0.872 | 222.50 | 0.97443631 | 890.0 | 0.10225477 |
| 1112.75 | 0.872 | 222.55 | 0.97445708 | 890.2 | 0.10217167 |
| 1113 | 0.872 | 222.60 | 0.97447785 | 890.4 | 0.10208858 |
| 1113.25 | 0.872 | 222.65 | 0.97449862 | 890.6 | 0.10200550 |
| 1113.5 | 0.873 | 222.70 | 0.97451939 | 890.8 | 0.10192243 |
| 1113.75 | 0.873 | 222.75 | 0.97454016 | 891.0 | 0.10183937 |
| 1114 | 0.873 | 222.80 | 0.97456092 | 891.2 | 0.10175631 |
| 1114.25 | 0.873 | 222.85 | 0.97458168 | 891.4 | 0.10167327 |
| 1114.5 | 0.873 | 222.90 | 0.97460244 | 891.6 | 0.10159023 |
| 1114.75 | 0.873 | 222.95 | 0.97462320 | 891.8 | 0.10150720 |
| 1115 | 0.873 | 223.00 | 0.97464395 | 892.0 | 0.10142419 |
| 1115.25 | 0.873 | 223.05 | 0.97466471 | 892.2 | 0.10134118 |
| 1115.5 | 0.873 | 223.10 | 0.97468546 | 892.4 | 0.10125817 |
| 1115.75 | 0.874 | 223.15 | 0.97470620 | 892.6 | 0.10117518 |
| 1116 | 0.874 | 223.20 | 0.97472695 | 892.8 | 0.10109220 |
| 1116.25 | 0.874 | 223.25 | 0.97474769 | 893.0 | 0.10100922 |


| 1116.5 | 0.874 | 223.30 | 0.97476844 | 893.2 | 0.10092625 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1116.75 | 0.874 | 223.35 | 0.97478918 | 893.4 | 0.10084330 |
| 1117 | 0.874 | 223.40 | 0.97480991 | 893.6 | 0.10076035 |
| 1117.25 | 0.874 | 223.45 | 0.97483065 | 893.8 | 0.10067741 |
| 1117.5 | 0.874 | 223.50 | 0.97485138 | 894.0 | 0.10059448 |
| 1117.75 | 0.874 | 223.55 | 0.97487211 | 894.2 | 0.10051155 |
| 1118 | 0.874 | 223.60 | 0.97489284 | 894.4 | 0.10042864 |
| 1118.25 | 0.875 | 223.65 | 0.97491357 | 894.6 | 0.10034573 |
| 1118.5 | 0.875 | 223.70 | 0.97493429 | 894.8 | 0.10026284 |
| 1118.75 | 0.875 | 223.75 | 0.97495501 | 895.0 | 0.10017995 |
| 1119 | 0.875 | 223.80 | 0.97497573 | 895.2 | 0.10009707 |
| 1119.25 | 0.875 | 223.85 | 0.97499645 | 895.4 | 0.10001420 |
| 1119.5 | 0.875 | 223.90 | 0.97501717 | 895.6 | 0.09993134 |
| 1119.75 | 0.875 | 223.95 | 0.97503788 | 895.8 | 0.09984848 |
| 1120 | 0.875 | 224.00 | 0.97505859 | 896.0 | 0.09976564 |
| 1120.25 | 0.875 | 224.05 | 0.97507930 | 896.2 | 0.09968280 |
| 1120.5 | 0.876 | 224.10 | 0.97510001 | 896.4 | 0.09959998 |
| 1120.75 | 0.876 | 224.15 | 0.97512071 | 896.6 | 0.09951716 |
| 1121 | 0.876 | 224.20 | 0.97514141 | 896.8 | 0.09943435 |
| 1121.25 | 0.876 | 224.25 | 0.97516211 | 897.0 | 0.09935155 |
| 1121.5 | 0.876 | 224.30 | 0.97518281 | 897.2 | 0.09926875 |
| 1121.75 | 0.876 | 224.35 | 0.97520351 | 897.4 | 0.09918597 |
| 1122 | 0.876 | 224.40 | 0.97522420 | 897.6 | 0.09910319 |
| 1122.25 | 0.876 | 224.45 | 0.97524489 | 897.8 | 0.09902043 |
| 1122.5 | 0.876 | 224.50 | 0.97526558 | 898.0 | 0.09893767 |
| 1122.75 | 0.876 | 224.55 | 0.97528627 | 898.2 | 0.09885492 |
| 1123 | 0.877 | 224.60 | 0.97530695 | 898.4 | 0.09877218 |
| 1123.25 | 0.877 | 224.65 | 0.97532764 | 898.6 | 0.09868945 |
| 1123.5 | 0.877 | 224.70 | 0.97534832 | 898.8 | 0.09860673 |
| 1123.75 | 0.877 | 224.75 | 0.97536900 | 899.0 | 0.09852401 |
| 1124 | 0.877 | 224.80 | 0.97538967 | 899.2 | 0.09844131 |
| 1124.25 | 0.877 | 224.85 | 0.97541035 | 899.4 | 0.09835861 |
| 1124.5 | 0.877 | 224.90 | 0.97543102 | 899.6 | 0.09827592 |
| 1124.75 | 0.877 | 224.95 | 0.97545169 | 899.8 | 0.09819324 |
| 1125 | 0.877 | 225.00 | 0.97547236 | 900.0 | 0.09811057 |
| 1125.25 | 0.877 | 225.05 | 0.97549302 | 900.2 | 0.09802791 |
| 1125.5 | 0.878 | 225.10 | 0.97551369 | 900.4 | 0.09794525 |
| 1125.75 | 0.878 | 225.15 | 0.97553435 | 900.6 | 0.09786261 |
| 1126 | 0.878 | 225.20 | 0.97555501 | 900.8 | 0.09777997 |
| 1126.25 | 0.878 | 225.25 | 0.97557566 | 901.0 | 0.09769734 |
| 1126.5 | 0.878 | 225.30 | 0.97559632 | 901.2 | 0.09761472 |
| 1126.75 | 0.878 | 225.35 | 0.97561697 | 901.4 | 0.09753211 |
| 1127 | 0.878 | 225.40 | 0.97563762 | 901.6 | 0.09744951 |
| 1127.25 | 0.878 | 225.45 | 0.97565827 | 901.8 | 0.09736692 |
| 1127.5 | 0.878 | 225.50 | 0.97567892 | 902.0 | 0.09728433 |
| 1127.75 | 0.878 | 225.55 | 0.97569956 | 902.2 | 0.09720175 |
| 1128 | 0.879 | 225.60 | 0.97572020 | 902.4 | 0.09711919 |
| 1128.25 | 0.879 | 225.65 | 0.97574084 | 902.6 | 0.09703663 |
| 1128.5 | 0.879 | 225.70 | 0.97576148 | 902.8 | 0.09695408 |
| 1128.75 | 0.879 | 225.75 | 0.97578212 | 903.0 | 0.09687153 |
| 1129 | 0.879 | 225.80 | 0.97580275 | 903.2 | 0.09678900 |
| 1129.25 | 0.879 | 225.85 | 0.97582338 | 903.4 | 0.09670648 |
| 1129.5 | 0.879 | 225.90 | 0.97584401 | 903.6 | 0.09662396 |
| 1129.75 | 0.879 | 225.95 | 0.97586464 | 903.8 | 0.09654145 |
| 1130 | 0.879 | 226.00 | 0.97588526 | 904.0 | 0.09645895 |
| 1130.25 | 0.880 | 226.05 | 0.97590588 | 904.2 | 0.09637646 |
| 1130.5 | 0.880 | 226.10 | 0.97592651 | 904.4 | 0.09629398 |
| 1130.75 | 0.880 | 226.15 | 0.97594712 | 904.6 | 0.09621151 |
| 1131 | 0.880 | 226.20 | 0.97596774 | 904.8 | 0.09612904 |
| 1131.25 | 0.880 | 226.25 | 0.97598835 | 905.0 | 0.09604659 |
| 1131.5 | 0.880 | 226.30 | 0.97600897 | 905.2 | 0.09596414 |
| 1131.75 | 0.880 | 226.35 | 0.97602958 | 905.4 | 0.09588170 |
| 1132 | 0.880 | 226.40 | 0.97605018 | 905.6 | 0.09579927 |
| 1132.25 | 0.880 | 226.45 | 0.97607079 | 905.8 | 0.09571685 |
| 1132.5 | 0.880 | 226.50 | 0.97609139 | 906.0 | 0.09563443 |
| 1132.75 | 0.881 | 226.55 | 0.97611199 | 906.2 | 0.09555203 |
| 1133 | 0.881 | 226.60 | 0.97613259 | 906.4 | 0.09546963 |
| 1133.25 | 0.881 | 226.65 | 0.97615319 | 906.6 | 0.09538724 |
| 1133.5 | 0.881 | 226.70 | 0.97617378 | 906.8 | 0.09530486 |
| 1133.75 | 0.881 | 226.75 | 0.97619438 | 907.0 | 0.09522249 |
| 1134 | 0.881 | 226.80 | 0.97621497 | 907.2 | 0.09514013 |


| 1134.25 | 0.881 | 226.85 | 0.97623556 | 907.4 | 0.09505778 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1134.5 | 0.881 | 226.90 | 0.97625614 | 907.6 | 0.09497543 |
| 1134.75 | 0.881 | 226.95 | 0.97627673 | 907.8 | 0.09489310 |
| 1135 | 0.881 | 227.00 | 0.97629731 | 908.0 | 0.09481077 |
| 1135.25 | 0.882 | 227.05 | 0.97631789 | 908.2 | 0.09472845 |
| 1135.5 | 0.882 | 227.10 | 0.97633847 | 908.4 | 0.09464614 |
| 1135.75 | 0.882 | 227.15 | 0.97635904 | 908.6 | 0.09456383 |
| 1136 | 0.882 | 227.20 | 0.97637962 | 908.8 | 0.09448154 |
| 1136.25 | 0.882 | 227.25 | 0.97640019 | 909.0 | 0.09439925 |
| 1136.5 | 0.882 | 227.30 | 0.97642076 | 909.2 | 0.09431698 |
| 1136.75 | 0.882 | 227.35 | 0.97644132 | 909.4 | 0.09423471 |
| 1137 | 0.882 | 227.40 | 0.97646189 | 909.6 | 0.09415245 |
| 1137.25 | 0.882 | 227.45 | 0.97648245 | 909.8 | 0.09407020 |
| 1137.5 | 0.883 | 227.50 | 0.97650301 | 910.0 | 0.09398795 |
| 1137.75 | 0.883 | 227.55 | 0.97652357 | 910.2 | 0.09390572 |
| 1138 | 0.883 | 227.60 | 0.97654413 | 910.4 | 0.09382349 |
| 1138.25 | 0.883 | 227.65 | 0.97656468 | 910.6 | 0.09374128 |
| 1138.5 | 0.883 | 227.70 | 0.97658523 | 910.8 | 0.09365907 |
| 1138.75 | 0.883 | 227.75 | 0.97660578 | 911.0 | 0.09357687 |
| 1139 | 0.883 | 227.80 | 0.97662633 | 911.2 | 0.09349467 |
| 1139.25 | 0.883 | 227.85 | 0.97664688 | 911.4 | 0.09341249 |
| 1139.5 | 0.883 | 227.90 | 0.97666742 | 911.6 | 0.09333032 |
| 1139.75 | 0.883 | 227.95 | 0.97668796 | 911.8 | 0.09324815 |
| 1140 | 0.884 | 228.00 | 0.97670850 | 912.0 | 0.09316599 |
| 1140.25 | 0.884 | 228.05 | 0.97672904 | 912.2 | 0.09308384 |
| 1140.5 | 0.884 | 228.10 | 0.97674958 | 912.4 | 0.09300170 |
| 1140.75 | 0.884 | 228.15 | 0.97677011 | 912.6 | 0.09291957 |
| 1141 | 0.884 | 228.20 | 0.97679064 | 912.8 | 0.09283744 |
| 1141.25 | 0.884 | 228.25 | 0.97681117 | 913.0 | 0.09275533 |
| 1141.5 | 0.884 | 228.30 | 0.97683170 | 913.2 | 0.09267322 |
| 1141.75 | 0.884 | 228.35 | 0.97685222 | 913.4 | 0.09259112 |
| 1142 | 0.884 | 228.40 | 0.97687274 | 913.6 | 0.09250903 |
| 1142.25 | 0.884 | 228.45 | 0.97689326 | 913.8 | 0.09242695 |
| 1142.5 | 0.885 | 228.50 | 0.97691378 | 914.0 | 0.09234487 |
| 1142.75 | 0.885 | 228.55 | 0.97693430 | 914.2 | 0.09226281 |
| 1143 | 0.885 | 228.60 | 0.97695481 | 914.4 | 0.09218075 |
| 1143.25 | 0.885 | 228.65 | 0.97697532 | 914.6 | 0.09209870 |
| 1143.5 | 0.885 | 228.70 | 0.97699583 | 914.8 | 0.09201666 |
| 1143.75 | 0.885 | 228.75 | 0.97701634 | 915.0 | 0.09193463 |
| 1144 | 0.885 | 228.80 | 0.97703685 | 915.2 | 0.09185261 |
| 1144.25 | 0.885 | 228.85 | 0.97705735 | 915.4 | 0.09177059 |
| 1144.5 | 0.885 | 228.90 | 0.97707785 | 915.6 | 0.09168859 |
| 1144.75 | 0.885 | 228.95 | 0.97709835 | 915.8 | 0.09160659 |
| 1145 | 0.886 | 229.00 | 0.97711885 | 916.0 | 0.09152460 |
| 1145.25 | 0.886 | 229.05 | 0.97713934 | 916.2 | 0.09144262 |
| 1145.5 | 0.886 | 229.10 | 0.97715984 | 916.4 | 0.09136065 |
| 1145.75 | 0.886 | 229.15 | 0.97718033 | 916.6 | 0.09127868 |
| 1146 | 0.886 | 229.20 | 0.97720082 | 916.8 | 0.09119673 |
| 1146.25 | 0.886 | 229.25 | 0.97722130 | 917.0 | 0.09111478 |
| 1146.5 | 0.886 | 229.30 | 0.97724179 | 917.2 | 0.09103284 |
| 1146.75 | 0.886 | 229.35 | 0.97726227 | 917.4 | 0.09095091 |
| 1147 | 0.886 | 229.40 | 0.97728275 | 917.6 | 0.09086899 |
| 1147.25 | 0.887 | 229.45 | 0.97730323 | 917.8 | 0.09078708 |
| 1147.5 | 0.887 | 229.50 | 0.97732371 | 918.0 | 0.09070517 |
| 1147.75 | 0.887 | 229.55 | 0.97734418 | 918.2 | 0.09062327 |
| 1148 | 0.887 | 229.60 | 0.97736465 | 918.4 | 0.09054138 |
| 1148.25 | 0.887 | 229.65 | 0.97738512 | 918.6 | 0.09045950 |
| 1148.5 | 0.887 | 229.70 | 0.97740559 | 918.8 | 0.09037763 |
| 1148.75 | 0.887 | 229.75 | 0.97742606 | 919.0 | 0.09029577 |
| 1149 | 0.887 | 229.80 | 0.97744652 | 919.2 | 0.09021391 |
| 1149.25 | 0.887 | 229.85 | 0.97746698 | 919.4 | 0.09013207 |
| 1149.5 | 0.887 | 229.90 | 0.97748744 | 919.6 | 0.09005023 |
| 1149.75 | 0.888 | 229.95 | 0.97750790 | 919.8 | 0.08996840 |
| 1150 | 0.888 | 230.00 | 0.97752836 | 920.0 | 0.08988658 |
| 1150.25 | 0.888 | 230.05 | 0.97754881 | 920.2 | 0.08980476 |
| 1150.5 | 0.888 | 230.10 | 0.97756926 | 920.4 | 0.08972296 |
| 1150.75 | 0.888 | 230.15 | 0.97758971 | 920.6 | 0.08964116 |
| 1151 | 0.888 | 230.20 | 0.97761016 | 920.8 | 0.08955937 |
| 1151.25 | 0.888 | 230.25 | 0.97763060 | 921.0 | 0.08947760 |
| 1151.5 | 0.888 | 230.30 | 0.97765104 | 921.2 | 0.08939582 |
| 1151.75 | 0.888 | 230.35 | 0.97767148 | 921.4 | 0.08931406 |


| 1152 | 0.888 | 230.40 | 0.97769192 | 921.6 | 0.08923231 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1152.25 | 0.889 | 230.45 | 0.97771236 | 921.8 | 0.08915056 |
| 1152.5 | 0.889 | 230.50 | 0.97773279 | 922.0 | 0.08906882 |
| 1152.75 | 0.889 | 230.55 | 0.97775323 | 922.2 | 0.08898709 |
| 1153 | 0.889 | 230.60 | 0.97777366 | 922.4 | 0.08890537 |
| 1153.25 | 0.889 | 230.65 | 0.97779409 | 922.6 | 0.08882366 |
| 1153.5 | 0.889 | 230.70 | 0.97781451 | 922.8 | 0.08874195 |
| 1153.75 | 0.889 | 230.75 | 0.97783494 | 923.0 | 0.08866026 |
| 1154 | 0.889 | 230.80 | 0.97785536 | 923.2 | 0.08857857 |
| 1154.25 | 0.889 | 230.85 | 0.97787578 | 923.4 | 0.08849689 |
| 1154.5 | 0.889 | 230.90 | 0.97789620 | 923.6 | 0.08841522 |
| 1154.75 | 0.890 | 230.95 | 0.97791661 | 923.8 | 0.08833355 |
| 1155 | 0.890 | 231.00 | 0.97793703 | 924.0 | 0.08825190 |
| 1155.25 | 0.890 | 231.05 | 0.97795744 | 924.2 | 0.08817025 |
| 1155.5 | 0.890 | 231.10 | 0.97797785 | 924.4 | 0.08808861 |
| 1155.75 | 0.890 | 231.15 | 0.97799825 | 924.6 | 0.08800698 |
| 1156 | 0.890 | 231.20 | 0.97801866 | 924.8 | 0.08792536 |
| 1156.25 | 0.890 | 231.25 | 0.97803906 | 925.0 | 0.08784375 |
| 1156.5 | 0.890 | 231.30 | 0.97805946 | 925.2 | 0.08776214 |
| 1156.75 | 0.890 | 231.35 | 0.97807986 | 925.4 | 0.08768055 |
| 1157 | 0.891 | 231.40 | 0.97810026 | 925.6 | 0.08759896 |
| 1157.25 | 0.891 | 231.45 | 0.97812066 | 925.8 | 0.08751738 |
| 1157.5 | 0.891 | 231.50 | 0.97814105 | 926.0 | 0.08743581 |
| 1157.75 | 0.891 | 231.55 | 0.97816144 | 926.2 | 0.08735424 |
| 1158 | 0.891 | 231.60 | 0.97818183 | 926.4 | 0.08727269 |
| 1158.25 | 0.891 | 231.65 | 0.97820222 | 926.6 | 0.08719114 |
| 1158.5 | 0.891 | 231.70 | 0.97822260 | 926.8 | 0.08710960 |
| 1158.75 | 0.891 | 231.75 | 0.97824298 | 927.0 | 0.08702807 |
| 1159 | 0.891 | 231.80 | 0.97826336 | 927.2 | 0.08694655 |
| 1159.25 | 0.891 | 231.85 | 0.97828374 | 927.4 | 0.08686503 |
| 1159.5 | 0.892 | 231.90 | 0.97830412 | 927.6 | 0.08678353 |
| 1159.75 | 0.892 | 231.95 | 0.97832449 | 927.8 | 0.08670203 |
| 1160 | 0.892 | 232.00 | 0.97834486 | 928.0 | 0.08662054 |
| 1160.25 | 0.892 | 232.05 | 0.97836524 | 928.2 | 0.08653906 |
| 1160.5 | 0.892 | 232.10 | 0.97838560 | 928.4 | 0.08645759 |
| 1160.75 | 0.892 | 232.15 | 0.97840597 | 928.6 | 0.08637612 |
| 1161 | 0.892 | 232.20 | 0.97842633 | 928.8 | 0.08629467 |
| 1161.25 | 0.892 | 232.25 | 0.97844670 | 929.0 | 0.08621322 |
| 1161.5 | 0.892 | 232.30 | 0.97846706 | 929.2 | 0.08613178 |
| 1161.75 | 0.892 | 232.35 | 0.97848741 | 929.4 | 0.08605035 |
| 1162 | 0.893 | 232.40 | 0.97850777 | 929.6 | 0.08596892 |
| 1162.25 | 0.893 | 232.45 | 0.97852812 | 929.8 | 0.08588751 |
| 1162.5 | 0.893 | 232.50 | 0.97854847 | 930.0 | 0.08580610 |
| 1162.75 | 0.893 | 232.55 | 0.97856882 | 930.2 | 0.08572470 |
| 1163 | 0.893 | 232.60 | 0.97858917 | 930.4 | 0.08564331 |
| 1163.25 | 0.893 | 232.65 | 0.97860952 | 930.6 | 0.08556193 |
| 1163.5 | 0.893 | 232.70 | 0.97862986 | 930.8 | 0.08548056 |
| 1163.75 | 0.893 | 232.75 | 0.97865020 | 931.0 | 0.08539919 |
| 1164 | 0.893 | 232.80 | 0.97867054 | 931.2 | 0.08531783 |
| 1164.25 | 0.893 | 232.85 | 0.97869088 | 931.4 | 0.08523648 |
| 1164.5 | 0.894 | 232.90 | 0.97871121 | 931.6 | 0.08515514 |
| 1164.75 | 0.894 | 232.95 | 0.97873155 | 931.8 | 0.08507381 |
| 1165 | 0.894 | 233.00 | 0.97875188 | 932.0 | 0.08499248 |
| 1165.25 | 0.894 | 233.05 | 0.97877221 | 932.2 | 0.08491117 |
| 1165.5 | 0.894 | 233.10 | 0.97879254 | 932.4 | 0.08482986 |
| 1165.75 | 0.894 | 233.15 | 0.97881286 | 932.6 | 0.08474856 |
| 1166 | 0.894 | 233.20 | 0.97883318 | 932.8 | 0.08466727 |
| 1166.25 | 0.894 | 233.25 | 0.97885350 | 933.0 | 0.08458598 |
| 1166.5 | 0.894 | 233.30 | 0.97887382 | 933.2 | 0.08450471 |
| 1166.75 | 0.894 | 233.35 | 0.97889414 | 933.4 | 0.08442344 |
| 1167 | 0.895 | 233.40 | 0.97891445 | 933.6 | 0.08434218 |
| 1167.25 | 0.895 | 233.45 | 0.97893477 | 933.8 | 0.08426093 |
| 1167.5 | 0.895 | 233.50 | 0.97895508 | 934.0 | 0.08417969 |
| 1167.75 | 0.895 | 233.55 | 0.97897539 | 934.2 | 0.08409845 |
| 1168 | 0.895 | 233.60 | 0.97899569 | 934.4 | 0.08401723 |
| 1168.25 | 0.895 | 233.65 | 0.97901600 | 934.6 | 0.08393601 |
| 1168.5 | 0.895 | 233.70 | 0.97903630 | 934.8 | 0.08385480 |
| 1168.75 | 0.895 | 233.75 | 0.97905660 | 935.0 | 0.08377360 |
| 1169 | 0.895 | 233.80 | 0.97907690 | 935.2 | 0.08369240 |
| 1169.25 | 0.895 | 233.85 | 0.97909720 | 935.4 | 0.08361122 |
| 1169.5 | 0.896 | 233.90 | 0.97911749 | 935.6 | 0.08353004 |


| 1169.75 | 0.896 | 233.95 | 0.97913778 | 935.8 | 0.08344887 |
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| 1170 | 0.896 | 234.00 | 0.97915807 | 936.0 | 0.08336771 |
| 1170.25 | 0.896 | 234.05 | 0.97917836 | 936.2 | 0.08328656 |
| 1170.5 | 0.896 | 234.10 | 0.97919865 | 936.4 | 0.08320541 |
| 1170.75 | 0.896 | 234.15 | 0.97921893 | 936.6 | 0.08312428 |
| 1171 | 0.896 | 234.20 | 0.97923921 | 936.8 | 0.08304315 |
| 1171.25 | 0.896 | 234.25 | 0.97925949 | 937.0 | 0.08296203 |
| 1171.5 | 0.896 | 234.30 | 0.97927977 | 937.2 | 0.08288091 |
| 1171.75 | 0.897 | 234.35 | 0.97930005 | 937.4 | 0.08279981 |
| 1172 | 0.897 | 234.40 | 0.97932032 | 937.6 | 0.08271871 |
| 1172.25 | 0.897 | 234.45 | 0.97934059 | 937.8 | 0.08263763 |
| 1172.5 | 0.897 | 234.50 | 0.97936086 | 938.0 | 0.08255655 |
| 1172.75 | 0.897 | 234.55 | 0.97938113 | 938.2 | 0.08247547 |
| 1173 | 0.897 | 234.60 | 0.97940140 | 938.4 | 0.08239441 |
| 1173.25 | 0.897 | 234.65 | 0.97942166 | 938.6 | 0.08231336 |
| 1173.5 | 0.897 | 234.70 | 0.97944192 | 938.8 | 0.08223231 |
| 1173.75 | 0.897 | 234.75 | 0.97946218 | 939.0 | 0.08215127 |
| 1174 | 0.897 | 234.80 | 0.97948244 | 939.2 | 0.08207024 |
| 1174.25 | 0.898 | 234.85 | 0.97950270 | 939.4 | 0.08198922 |
| 1174.5 | 0.898 | 234.90 | 0.97952295 | 939.6 | 0.08190820 |
| 1174.75 | 0.898 | 234.95 | 0.97954320 | 939.8 | 0.08182719 |
| 1175 | 0.898 | 235.00 | 0.97956345 | 940.0 | 0.08174619 |
| 1175.25 | 0.898 | 235.05 | 0.97958370 | 940.2 | 0.08166520 |
| 1175.5 | 0.898 | 235.10 | 0.97960394 | 940.4 | 0.08158422 |
| 1175.75 | 0.898 | 235.15 | 0.97962419 | 940.6 | 0.08150325 |
| 1176 | 0.898 | 235.20 | 0.97964443 | 940.8 | 0.08142228 |
| 1176.25 | 0.898 | 235.25 | 0.97966467 | 941.0 | 0.08134132 |
| 1176.5 | 0.898 | 235.30 | 0.97968491 | 941.2 | 0.08126037 |
| 1176.75 | 0.899 | 235.35 | 0.97970514 | 941.4 | 0.08117943 |
| 1177 | 0.899 | 235.40 | 0.97972538 | 941.6 | 0.08109850 |
| 1177.25 | 0.899 | 235.45 | 0.97974561 | 941.8 | 0.08101757 |
| 1177.5 | 0.899 | 235.50 | 0.97976584 | 942.0 | 0.08093665 |
| 1177.75 | 0.899 | 235.55 | 0.97978606 | 942.2 | 0.08085574 |
| 1178 | 0.899 | 235.60 | 0.97980629 | 942.4 | 0.08077484 |
| 1178.25 | 0.899 | 235.65 | 0.97982651 | 942.6 | 0.08069395 |
| 1178.5 | 0.899 | 235.70 | 0.97984673 | 942.8 | 0.08061306 |
| 1178.75 | 0.899 | 235.75 | 0.97986695 | 943.0 | 0.08053219 |
| 1179 | 0.899 | 235.80 | 0.97988717 | 943.2 | 0.08045132 |
| 1179.25 | 0.900 | 235.85 | 0.97990739 | 943.4 | 0.08037046 |
| 1179.5 | 0.900 | 235.90 | 0.97992760 | 943.6 | 0.08028960 |
| 1179.75 | 0.900 | 235.95 | 0.97994781 | 943.8 | 0.08020876 |
| 1180 | 0.900 | 236.00 | 0.97996802 | 944.0 | 0.08012792 |
| 1180.25 | 0.900 | 236.05 | 0.97998823 | 944.2 | 0.08004709 |
| 1180.5 | 0.900 | 236.10 | 0.98000843 | 944.4 | 0.07996627 |
| 1180.75 | 0.900 | 236.15 | 0.98002864 | 944.6 | 0.07988546 |
| 1181 | 0.900 | 236.20 | 0.98004884 | 944.8 | 0.07980465 |
| 1181.25 | 0.900 | 236.25 | 0.98006904 | 945.0 | 0.07972385 |
| 1181.5 | 0.900 | 236.30 | 0.98008923 | 945.2 | 0.07964307 |
| 1181.75 | 0.901 | 236.35 | 0.98010943 | 945.4 | 0.07956229 |
| 1182 | 0.901 | 236.40 | 0.98012962 | 945.6 | 0.07948151 |
| 1182.25 | 0.901 | 236.45 | 0.98014981 | 945.8 | 0.07940075 |
| 1182.5 | 0.901 | 236.50 | 0.98017000 | 946.0 | 0.07931999 |
| 1182.75 | 0.901 | 236.55 | 0.98019019 | 946.2 | 0.07923924 |
| 1183 | 0.901 | 236.60 | 0.98021037 | 946.4 | 0.07915850 |
| 1183.25 | 0.901 | 236.65 | 0.98023056 | 946.6 | 0.07907777 |
| 1183.5 | 0.901 | 236.70 | 0.98025074 | 946.8 | 0.07899704 |
| 1183.75 | 0.901 | 236.75 | 0.98027092 | 947.0 | 0.07891633 |
| 1184 | 0.901 | 236.80 | 0.98029110 | 947.2 | 0.07883562 |
| 1184.25 | 0.902 | 236.85 | 0.98031127 | 947.4 | 0.07875492 |
| 1184.5 | 0.902 | 236.90 | 0.98033144 | 947.6 | 0.07867423 |
| 1184.75 | 0.902 | 236.95 | 0.98035161 | 947.8 | 0.07859354 |
| 1185 | 0.902 | 237.00 | 0.98037178 | 948.0 | 0.07851286 |
| 1185.25 | 0.902 | 237.05 | 0.98039195 | 948.2 | 0.07843220 |
| 1185.5 | 0.902 | 237.10 | 0.98041212 | 948.4 | 0.07835154 |
| 1185.75 | 0.902 | 237.15 | 0.98043228 | 948.6 | 0.07827088 |
| 1186 | 0.902 | 237.20 | 0.98045244 | 948.8 | 0.07819024 |
| 1186.25 | 0.902 | 237.25 | 0.98047260 | 949.0 | 0.07810960 |
| 1186.5 | 0.902 | 237.30 | 0.98049276 | 949.2 | 0.07802897 |
| 1186.75 | 0.903 | 237.35 | 0.98051291 | 949.4 | 0.07794835 |
| 1187 | 0.903 | 237.40 | 0.98053307 | 949.6 | 0.07786774 |
| 1187.25 | 0.903 | 237.45 | 0.98055322 | 949.8 | 0.07778713 |


| 1187.5 | 0.903 | 237.50 | 0.98057337 | 950.0 | 0.07770654 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1187.75 | 0.903 | 237.55 | 0.98059351 | 950.2 | 0.07762595 |
| 1188 | 0.903 | 237.60 | 0.98061366 | 950.4 | 0.07754537 |
| 1188.25 | 0.903 | 237.65 | 0.98063380 | 950.6 | 0.07746480 |
| 1188.5 | 0.903 | 237.70 | 0.98065394 | 950.8 | 0.07738423 |
| 1188.75 | 0.903 | 237.75 | 0.98067408 | 951.0 | 0.07730367 |
| 1189 | 0.903 | 237.80 | 0.98069422 | 951.2 | 0.07722312 |
| 1189.25 | 0.904 | 237.85 | 0.98071435 | 951.4 | 0.07714258 |
| 1189.5 | 0.904 | 237.90 | 0.98073449 | 951.6 | 0.07706205 |
| 1189.75 | 0.904 | 237.95 | 0.98075462 | 951.8 | 0.07698153 |
| 1190 | 0.904 | 238.00 | 0.98077475 | 952.0 | 0.07690101 |
| 1190.25 | 0.904 | 238.05 | 0.98079488 | 952.2 | 0.07682050 |
| 1190.5 | 0.904 | 238.10 | 0.98081500 | 952.4 | 0.07674000 |
| 1190.75 | 0.904 | 238.15 | 0.98083512 | 952.6 | 0.07665951 |
| 1191 | 0.904 | 238.20 | 0.98085525 | 952.8 | 0.07657902 |
| 1191.25 | 0.904 | 238.25 | 0.98087536 | 953.0 | 0.07649854 |
| 1191.5 | 0.904 | 238.30 | 0.98089548 | 953.2 | 0.07641807 |
| 1191.75 | 0.905 | 238.35 | 0.98091560 | 953.4 | 0.07633761 |
| 1192 | 0.905 | 238.40 | 0.98093571 | 953.6 | 0.07625716 |
| 1192.25 | 0.905 | 238.45 | 0.98095582 | 953.8 | 0.07617671 |
| 1192.5 | 0.905 | 238.50 | 0.98097593 | 954.0 | 0.07609627 |
| 1192.75 | 0.905 | 238.55 | 0.98099604 | 954.2 | 0.07601584 |
| 1193 | 0.905 | 238.60 | 0.98101614 | 954.4 | 0.07593542 |
| 1193.25 | 0.905 | 238.65 | 0.98103625 | 954.6 | 0.07585501 |
| 1193.5 | 0.905 | 238.70 | 0.98105635 | 954.8 | 0.07577460 |
| 1193.75 | 0.905 | 238.75 | 0.98107645 | 955.0 | 0.07569420 |
| 1194 | 0.905 | 238.80 | 0.98109655 | 955.2 | 0.07561381 |
| 1194.25 | 0.906 | 238.85 | 0.98111664 | 955.4 | 0.07553343 |
| 1194.5 | 0.906 | 238.90 | 0.98113674 | 955.6 | 0.07545306 |
| 1194.75 | 0.906 | 238.95 | 0.98115683 | 955.8 | 0.07537269 |
| 1195 | 0.906 | 239.00 | 0.98117692 | 956.0 | 0.07529233 |
| 1195.25 | 0.906 | 239.05 | 0.98119700 | 956.2 | 0.07521198 |
| 1195.5 | 0.906 | 239.10 | 0.98121709 | 956.4 | 0.07513164 |
| 1195.75 | 0.906 | 239.15 | 0.98123717 | 956.6 | 0.07505130 |
| 1196 | 0.906 | 239.20 | 0.98125726 | 956.8 | 0.07497098 |
| 1196.25 | 0.906 | 239.25 | 0.98127734 | 957.0 | 0.07489066 |
| 1196.5 | 0.906 | 239.30 | 0.98129741 | 957.2 | 0.07481035 |
| 1196.75 | 0.907 | 239.35 | 0.98131749 | 957.4 | 0.07473004 |
| 1197 | 0.907 | 239.40 | 0.98133756 | 957.6 | 0.07464975 |
| 1197.25 | 0.907 | 239.45 | 0.98135763 | 957.8 | 0.07456946 |
| 1197.5 | 0.907 | 239.50 | 0.98137770 | 958.0 | 0.07448918 |
| 1197.75 | 0.907 | 239.55 | 0.98139777 | 958.2 | 0.07440891 |
| 1198 | 0.907 | 239.60 | 0.98141784 | 958.4 | 0.07432865 |
| 1198.25 | 0.907 | 239.65 | 0.98143790 | 958.6 | 0.07424839 |
| 1198.5 | 0.907 | 239.70 | 0.98145796 | 958.8 | 0.07416814 |
| 1198.75 | 0.907 | 239.75 | 0.98147802 | 959.0 | 0.07408790 |
| 1199 | 0.907 | 239.80 | 0.98149808 | 959.2 | 0.07400767 |
| 1199.25 | 0.908 | 239.85 | 0.98151814 | 959.4 | 0.07392744 |
| 1199.5 | 0.908 | 239.90 | 0.98153819 | 959.6 | 0.07384723 |
| 1199.75 | 0.908 | 239.95 | 0.98155825 | 959.8 | 0.07376702 |
| 1200 | 0.908 | 240.00 | 0.98157830 | 960.0 | 0.07368682 |
| 1200.25 | 0.908 | 240.05 | 0.98159834 | 960.2 | 0.07360662 |
| 1200.5 | 0.908 | 240.10 | 0.98161839 | 960.4 | 0.07352644 |
| 1200.75 | 0.908 | 240.15 | 0.98163843 | 960.6 | 0.07344626 |
| 1201 | 0.908 | 240.20 | 0.98165848 | 960.8 | 0.07336609 |
| 1201.25 | 0.908 | 240.25 | 0.98167852 | 961.0 | 0.07328593 |
| 1201.5 | 0.908 | 240.30 | 0.98169856 | 961.2 | 0.07320578 |
| 1201.75 | 0.909 | 240.35 | 0.98171859 | 961.4 | 0.07312563 |
| 1202 | 0.909 | 240.40 | 0.98173863 | 961.6 | 0.07304549 |
| 1202.25 | 0.909 | 240.45 | 0.98175866 | 961.8 | 0.07296536 |
| 1202.5 | 0.909 | 240.50 | 0.98177869 | 962.0 | 0.07288524 |
| 1202.75 | 0.909 | 240.55 | 0.98179872 | 962.2 | 0.07280512 |
| 1203 | 0.909 | 240.60 | 0.98181875 | 962.4 | 0.07272502 |
| 1203.25 | 0.909 | 240.65 | 0.98183877 | 962.6 | 0.07264492 |
| 1203.5 | 0.909 | 240.70 | 0.98185879 | 962.8 | 0.07256483 |
| 1203.75 | 0.909 | 240.75 | 0.98187881 | 963.0 | 0.07248474 |
| 1204 | 0.909 | 240.80 | 0.98189883 | 963.2 | 0.07240467 |
| 1204.25 | 0.910 | 240.85 | 0.98191885 | 963.4 | 0.07232460 |
| 1204.5 | 0.910 | 240.90 | 0.98193887 | 963.6 | 0.07224454 |
| 1204.75 | 0.910 | 240.95 | 0.98195888 | 963.8 | 0.07216449 |
| 1205 | 0.910 | 241.00 | 0.98197889 | 964.0 | 0.07208444 |


| 1205.25 | 0.910 | 241.05 | 0.98199890 | 964.2 | 0.07200441 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1205.5 | 0.910 | 241.10 | 0.98201891 | 964.4 | 0.07192438 |
| 1205.75 | 0.910 | 241.15 | 0.98203891 | 964.6 | 0.07184436 |
| 1206 | 0.910 | 241.20 | 0.98205891 | 964.8 | 0.07176434 |
| 1206.25 | 0.910 | 241.25 | 0.98207892 | 965.0 | 0.07168434 |
| 1206.5 | 0.910 | 241.30 | 0.98209891 | 965.2 | 0.07160434 |
| 1206.75 | 0.911 | 241.35 | 0.98211891 | 965.4 | 0.07152435 |
| 1207 | 0.911 | 241.40 | 0.98213891 | 965.6 | 0.07144437 |
| 1207.25 | 0.911 | 241.45 | 0.98215890 | 965.8 | 0.07136439 |
| 1207.5 | 0.911 | 241.50 | 0.98217889 | 966.0 | 0.07128443 |
| 1207.75 | 0.911 | 241.55 | 0.98219888 | 966.2 | 0.07120447 |
| 1208 | 0.911 | 241.60 | 0.98221887 | 966.4 | 0.07112452 |
| 1208.25 | 0.911 | 241.65 | 0.98223886 | 966.6 | 0.07104458 |
| 1208.5 | 0.911 | 241.70 | 0.98225884 | 966.8 | 0.07096464 |
| 1208.75 | 0.911 | 241.75 | 0.98227882 | 967.0 | 0.07088471 |
| 1209 | 0.911 | 241.80 | 0.98229880 | 967.2 | 0.07080479 |
| 1209.25 | 0.912 | 241.85 | 0.98231878 | 967.4 | 0.07072488 |
| 1209.5 | 0.912 | 241.90 | 0.98233876 | 967.6 | 0.07064498 |
| 1209.75 | 0.912 | 241.95 | 0.98235873 | 967.8 | 0.07056508 |
| 1210 | 0.912 | 242.00 | 0.98237870 | 968.0 | 0.07048519 |
| 1210.25 | 0.912 | 242.05 | 0.98239867 | 968.2 | 0.07040531 |
| 1210.5 | 0.912 | 242.10 | 0.98241864 | 968.4 | 0.07032544 |
| 1210.75 | 0.912 | 242.15 | 0.98243861 | 968.6 | 0.07024557 |
| 1211 | 0.912 | 242.20 | 0.98245857 | 968.8 | 0.07016571 |
| 1211.25 | 0.912 | 242.25 | 0.98247853 | 969.0 | 0.07008586 |
| 1211.5 | 0.912 | 242.30 | 0.98249849 | 969.2 | 0.07000602 |
| 1211.75 | 0.913 | 242.35 | 0.98251845 | 969.4 | 0.06992619 |
| 1212 | 0.913 | 242.40 | 0.98253841 | 969.6 | 0.06984636 |
| 1212.25 | 0.913 | 242.45 | 0.98255836 | 969.8 | 0.06976654 |
| 1212.5 | 0.913 | 242.50 | 0.98257832 | 970.0 | 0.06968673 |
| 1212.75 | 0.913 | 242.55 | 0.98259827 | 970.2 | 0.06960693 |
| 1213 | 0.913 | 242.60 | 0.98261822 | 970.4 | 0.06952713 |
| 1213.25 | 0.913 | 242.65 | 0.98263816 | 970.6 | 0.06944734 |
| 1213.5 | 0.913 | 242.70 | 0.98265811 | 970.8 | 0.06936756 |
| 1213.75 | 0.913 | 242.75 | 0.98267805 | 971.0 | 0.06928779 |
| 1214 | 0.913 | 242.80 | 0.98269799 | 971.2 | 0.06920802 |
| 1214.25 | 0.914 | 242.85 | 0.98271793 | 971.4 | 0.06912827 |
| 1214.5 | 0.914 | 242.90 | 0.98273787 | 971.6 | 0.06904852 |
| 1214.75 | 0.914 | 242.95 | 0.98275781 | 971.8 | 0.06896878 |
| 1215 | 0.914 | 243.00 | 0.98277774 | 972.0 | 0.06888904 |
| 1215.25 | 0.914 | 243.05 | 0.98279767 | 972.2 | 0.06880932 |
| 1215.5 | 0.914 | 243.10 | 0.98281760 | 972.4 | 0.06872960 |
| 1215.75 | 0.914 | 243.15 | 0.98283753 | 972.6 | 0.06864989 |
| 1216 | 0.914 | 243.20 | 0.98285745 | 972.8 | 0.06857018 |
| 1216.25 | 0.914 | 243.25 | 0.98287738 | 973.0 | 0.06849049 |
| 1216.5 | 0.914 | 243.30 | 0.98289730 | 973.2 | 0.06841080 |
| 1216.75 | 0.915 | 243.35 | 0.98291722 | 973.4 | 0.06833112 |
| 1217 | 0.915 | 243.40 | 0.98293714 | 973.6 | 0.06825145 |
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| 1217.5 | 0.915 | 243.50 | 0.98297697 | 974.0 | 0.06809212 |
| 1217.75 | 0.915 | 243.55 | 0.98299688 | 974.2 | 0.06801248 |
| 1218 | 0.915 | 243.60 | 0.98301679 | 974.4 | 0.06793283 |
| 1218.25 | 0.915 | 243.65 | 0.98303670 | 974.6 | 0.06785320 |
| 1218.5 | 0.915 | 243.70 | 0.98305661 | 974.8 | 0.06777357 |
| 1218.75 | 0.915 | 243.75 | 0.98307651 | 975.0 | 0.06769395 |
| 1219 | 0.915 | 243.80 | 0.98309641 | 975.2 | 0.06761434 |
| 1219.25 | 0.916 | 243.85 | 0.98311631 | 975.4 | 0.06753474 |
| 1219.5 | 0.916 | 243.90 | 0.98313621 | 975.6 | 0.06745514 |
| 1219.75 | 0.916 | 243.95 | 0.98315611 | 975.8 | 0.06737556 |
| 1220 | 0.916 | 244.00 | 0.98317601 | 976.0 | 0.06729598 |
| 1220.25 | 0.916 | 244.05 | 0.98319590 | 976.2 | 0.06721640 |
| 1220.5 | 0.916 | 244.10 | 0.98321579 | 976.4 | 0.06713684 |
| 1220.75 | 0.916 | 244.15 | 0.98323568 | 976.6 | 0.06705728 |
| 1221 | 0.916 | 244.20 | 0.98325557 | 976.8 | 0.06697773 |
| 1221.25 | 0.916 | 244.25 | 0.98327545 | 977.0 | 0.06689819 |
| 1221.5 | 0.916 | 244.30 | 0.98329534 | 977.2 | 0.06681866 |
| 1221.75 | 0.917 | 244.35 | 0.98331522 | 977.4 | 0.06673913 |
| 1222 | 0.917 | 244.40 | 0.98333510 | 977.6 | 0.06665961 |
| 1222.25 | 0.917 | 244.45 | 0.98335498 | 977.8 | 0.06658010 |
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| 1223 | 0.917 | 244.60 | 0.98341460 | 978.4 | 0.06634161 |
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| 1223.25 | 0.917 | 244.65 | 0.98343447 | 978.6 | 0.06626213 |
| 1223.5 | 0.917 | 244.70 | 0.98345434 | 978.8 | 0.06618266 |
| 1223.75 | 0.917 | 244.75 | 0.98347420 | 979.0 | 0.06610319 |
| 1224 | 0.917 | 244.80 | 0.98349407 | 979.2 | 0.06602373 |
| 1224.25 | 0.918 | 244.85 | 0.98351393 | 979.4 | 0.06594428 |
| 1224.5 | 0.918 | 244.90 | 0.98353379 | 979.6 | 0.06586484 |
| 1224.75 | 0.918 | 244.95 | 0.98355365 | 979.8 | 0.06578540 |
| 1225 | 0.918 | 245.00 | 0.98357351 | 980.0 | 0.06570598 |
| 1225.25 | 0.918 | 245.05 | 0.98359336 | 980.2 | 0.06562656 |
| 1225.5 | 0.918 | 245.10 | 0.98361321 | 980.4 | 0.06554714 |
| 1225.75 | 0.918 | 245.15 | 0.98363306 | 980.6 | 0.06546774 |
| 1226 | 0.918 | 245.20 | 0.98365291 | 980.8 | 0.06538834 |
| 1226.25 | 0.918 | 245.25 | 0.98367276 | 981.0 | 0.06530895 |
| 1226.5 | 0.918 | 245.30 | 0.98369261 | 981.2 | 0.06522957 |
| 1226.75 | 0.919 | 245.35 | 0.98371245 | 981.4 | 0.06515020 |
| 1227 | 0.919 | 245.40 | 0.98373229 | 981.6 | 0.06507083 |
| 1227.25 | 0.919 | 245.45 | 0.98375213 | 981.8 | 0.06499147 |
| 1227.5 | 0.919 | 245.50 | 0.98377197 | 982.0 | 0.06491212 |
| 1227.75 | 0.919 | 245.55 | 0.98379181 | 982.2 | 0.06483278 |
| 1228 | 0.919 | 245.60 | 0.98381164 | 982.4 | 0.06475344 |
| 1228.25 | 0.919 | 245.65 | 0.98383147 | 982.6 | 0.06467411 |
| 1228.5 | 0.919 | 245.70 | 0.98385130 | 982.8 | 0.06459479 |
| 1228.75 | 0.919 | 245.75 | 0.98387113 | 983.0 | 0.06451548 |
| 1229 | 0.919 | 245.80 | 0.98389096 | 983.2 | 0.06443617 |
| 1229.25 | 0.920 | 245.85 | 0.98391078 | 983.4 | 0.06435687 |
| 1229.5 | 0.920 | 245.90 | 0.98393060 | 983.6 | 0.06427758 |
| 1229.75 | 0.920 | 245.95 | 0.98395042 | 983.8 | 0.06419830 |
| 1230 | 0.920 | 246.00 | 0.98397024 | 984.0 | 0.06411902 |
| 1230.25 | 0.920 | 246.05 | 0.98399006 | 984.2 | 0.06403976 |
| 1230.5 | 0.920 | 246.10 | 0.98400988 | 984.4 | 0.06396050 |
| 1230.75 | 0.920 | 246.15 | 0.98402969 | 984.6 | 0.06388124 |
| 1231 | 0.920 | 246.20 | 0.98404950 | 984.8 | 0.06380200 |
| 1231.25 | 0.920 | 246.25 | 0.98406931 | 985.0 | 0.06372276 |
| 1231.5 | 0.920 | 246.30 | 0.98408912 | 985.2 | 0.06364353 |
| 1231.75 | 0.921 | 246.35 | 0.98410892 | 985.4 | 0.06356431 |
| 1232 | 0.921 | 246.40 | 0.98412873 | 985.6 | 0.06348509 |
| 1232.25 | 0.921 | 246.45 | 0.98414853 | 985.8 | 0.06340589 |
| 1232.5 | 0.921 | 246.50 | 0.98416833 | 986.0 | 0.06332669 |
| 1232.75 | 0.921 | 246.55 | 0.98418813 | 986.2 | 0.06324749 |
| 1233 | 0.921 | 246.60 | 0.98420792 | 986.4 | 0.06316831 |
| 1233.25 | 0.921 | 246.65 | 0.98422772 | 986.6 | 0.06308913 |
| 1233.5 | 0.921 | 246.70 | 0.98424751 | 986.8 | 0.06300996 |
| 1233.75 | 0.921 | 246.75 | 0.98426730 | 987.0 | 0.06293080 |
| 1234 | 0.921 | 246.80 | 0.98428709 | 987.2 | 0.06285164 |
| 1234.25 | 0.922 | 246.85 | 0.98430688 | 987.4 | 0.06277250 |
| 1234.5 | 0.922 | 246.90 | 0.98432666 | 987.6 | 0.06269336 |
| 1234.75 | 0.922 | 246.95 | 0.98434644 | 987.8 | 0.06261423 |
| 1235 | 0.922 | 247.00 | 0.98436622 | 988.0 | 0.06253510 |
| 1235.25 | 0.922 | 247.05 | 0.98438600 | 988.2 | 0.06245598 |
| 1235.5 | 0.922 | 247.10 | 0.98440578 | 988.4 | 0.06237688 |
| 1235.75 | 0.922 | 247.15 | 0.98442556 | 988.6 | 0.06229777 |
| 1236 | 0.922 | 247.20 | 0.98444533 | 988.8 | 0.06221868 |
| 1236.25 | 0.922 | 247.25 | 0.98446510 | 989.0 | 0.06213959 |
| 1236.5 | 0.922 | 247.30 | 0.98448487 | 989.2 | 0.06206051 |
| 1236.75 | 0.923 | 247.35 | 0.98450464 | 989.4 | 0.06198144 |
| 1237 | 0.923 | 247.40 | 0.98452441 | 989.6 | 0.06190238 |
| 1237.25 | 0.923 | 247.45 | 0.98454417 | 989.8 | 0.06182332 |
| 1237.5 | 0.923 | 247.50 | 0.98456393 | 990.0 | 0.06174427 |
| 1237.75 | 0.923 | 247.55 | 0.98458369 | 990.2 | 0.06166523 |
| 1238 | 0.923 | 247.60 | 0.98460345 | 990.4 | 0.06158619 |
| 1238.25 | 0.923 | 247.65 | 0.98462321 | 990.6 | 0.06150717 |
| 1238.5 | 0.923 | 247.70 | 0.98464296 | 990.8 | 0.06142815 |
| 1238.75 | 0.923 | 247.75 | 0.98466272 | 991.0 | 0.06134914 |
| 1239 | 0.923 | 247.80 | 0.98468247 | 991.2 | 0.06127013 |
| 1239.25 | 0.924 | 247.85 | 0.98470222 | 991.4 | 0.06119114 |
| 1239.5 | 0.924 | 247.90 | 0.98472196 | 991.6 | 0.06111215 |
| 1239.75 | 0.924 | 247.95 | 0.98474171 | 991.8 | 0.06103316 |
| 1240 | 0.924 | 248.00 | 0.98476145 | 992.0 | 0.06095419 |
| 1240.25 | 0.924 | 248.05 | 0.98478119 | 992.2 | 0.06087522 |
| 1240.5 | 0.924 | 248.10 | 0.98480093 | 992.4 | 0.06079626 |


| 1240.75 | 0.924 | 248.15 | 0.98482067 | 992.6 | 0.06071731 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1241 | 0.924 | 248.20 | 0.98484041 | 992.8 | 0.06063837 |
| 1241.25 | 0.924 | 248.25 | 0.98486014 | 993.0 | 0.06055943 |
| 1241.5 | 0.924 | 248.30 | 0.98487987 | 993.2 | 0.06048050 |
| 1241.75 | 0.924 | 248.35 | 0.98489961 | 993.4 | 0.06040158 |
| 1242 | 0.925 | 248.40 | 0.98491933 | 993.6 | 0.06032266 |
| 1242.25 | 0.925 | 248.45 | 0.98493906 | 993.8 | 0.06024376 |
| 1242.5 | 0.925 | 248.50 | 0.98495879 | 994.0 | 0.06016486 |
| 1242.75 | 0.925 | 248.55 | 0.98497851 | 994.2 | 0.06008597 |
| 1243 | 0.925 | 248.60 | 0.98499823 | 994.4 | 0.06000708 |
| 1243.25 | 0.925 | 248.65 | 0.98501795 | 994.6 | 0.05992820 |
| 1243.5 | 0.925 | 248.70 | 0.98503767 | 994.8 | 0.05984933 |
| 1243.75 | 0.925 | 248.75 | 0.98505738 | 995.0 | 0.05977047 |
| 1244 | 0.925 | 248.80 | 0.98507710 | 995.2 | 0.05969162 |
| 1244.25 | 0.925 | 248.85 | 0.98509681 | 995.4 | 0.05961277 |
| 1244.5 | 0.926 | 248.90 | 0.98511652 | 995.6 | 0.05953393 |
| 1244.75 | 0.926 | 248.95 | 0.98513623 | 995.8 | 0.05945510 |
| 1245 | 0.926 | 249.00 | 0.98515593 | 996.0 | 0.05937627 |
| 1245.25 | 0.926 | 249.05 | 0.98517564 | 996.2 | 0.05929745 |
| 1245.5 | 0.926 | 249.10 | 0.98519534 | 996.4 | 0.05921864 |
| 1245.75 | 0.926 | 249.15 | 0.98521504 | 996.6 | 0.05913984 |
| 1246 | 0.926 | 249.20 | 0.98523474 | 996.8 | 0.05906104 |
| 1246.25 | 0.926 | 249.25 | 0.98525444 | 997.0 | 0.05898226 |
| 1246.5 | 0.926 | 249.30 | 0.98527413 | 997.2 | 0.05890348 |
| 1246.75 | 0.926 | 249.35 | 0.98529382 | 997.4 | 0.05882470 |
| 1247 | 0.927 | 249.40 | 0.98531352 | 997.6 | 0.05874594 |
| 1247.25 | 0.927 | 249.45 | 0.98533321 | 997.8 | 0.05866718 |
| 1247.5 | 0.927 | 249.50 | 0.98535289 | 998.0 | 0.05858843 |
| 1247.75 | 0.927 | 249.55 | 0.98537258 | 998.2 | 0.05850969 |
| 1248 | 0.927 | 249.60 | 0.98539226 | 998.4 | 0.05843095 |
| 1248.25 | 0.927 | 249.65 | 0.98541194 | 998.6 | 0.05835222 |
| 1248.5 | 0.927 | 249.70 | 0.98543163 | 998.8 | 0.05827350 |
| 1248.75 | 0.927 | 249.75 | 0.98545130 | 999.0 | 0.05819479 |
| 1249 | 0.927 | 249.80 | 0.98547098 | 999.2 | 0.05811608 |
| 1249.25 | 0.927 | 249.85 | 0.98549065 | 999.4 | 0.05803738 |
| 1249.5 | 0.928 | 249.90 | 0.98551033 | 999.6 | 0.05795869 |
| 1249.75 | 0.928 | 249.95 | 0.98553000 | 999.8 | 0.05788000 |
| 1250 | 0.928 | 250.00 | 0.98554967 | 1000.0 | 0.05780133 |
| 1250.25 | 0.928 | 250.05 | 0.98556934 | 1000.2 | 0.05772266 |
| 1250.5 | 0.928 | 250.10 | 0.98558900 | 1000.4 | 0.05764400 |
| 1250.75 | 0.928 | 250.15 | 0.98560866 | 1000.6 | 0.05756534 |
| 1251 | 0.928 | 250.20 | 0.98562833 | 1000.8 | 0.05748669 |
| 1251.25 | 0.928 | 250.25 | 0.98564799 | 1001.0 | 0.05740805 |
| 1251.5 | 0.928 | 250.30 | 0.98566764 | 1001.2 | 0.05732942 |
| 1251.75 | 0.928 | 250.35 | 0.98568730 | 1001.4 | 0.05725080 |
| 1252 | 0.929 | 250.40 | 0.98570696 | 1001.6 | 0.05717218 |
| 1252.25 | 0.929 | 250.45 | 0.98572661 | 1001.8 | 0.05709357 |
| 1252.5 | 0.929 | 250.50 | 0.98574626 | 1002.0 | 0.05701497 |
| 1252.75 | 0.929 | 250.55 | 0.98576591 | 1002.2 | 0.05693637 |
| 1253 | 0.929 | 250.60 | 0.98578555 | 1002.4 | 0.05685778 |
| 1253.25 | 0.929 | 250.65 | 0.98580520 | 1002.6 | 0.05677920 |
| 1253.5 | 0.929 | 250.70 | 0.98582484 | 1002.8 | 0.05670063 |
| 1253.75 | 0.929 | 250.75 | 0.98584448 | 1003.0 | 0.05662206 |
| 1254 | 0.929 | 250.80 | 0.98586412 | 1003.2 | 0.05654350 |
| 1254.25 | 0.929 | 250.85 | 0.98588376 | 1003.4 | 0.05646495 |
| 1254.5 | 0.930 | 250.90 | 0.98590340 | 1003.6 | 0.05638641 |
| 1254.75 | 0.930 | 250.95 | 0.98592303 | 1003.8 | 0.05630787 |
| 1255 | 0.930 | 251.00 | 0.98594266 | 1004.0 | 0.05622934 |
| 1255.25 | 0.930 | 251.05 | 0.98596229 | 1004.2 | 0.05615082 |
| 1255.5 | 0.930 | 251.10 | 0.98598192 | 1004.4 | 0.05607231 |
| 1255.75 | 0.930 | 251.15 | 0.98600155 | 1004.6 | 0.05599380 |
| 1256 | 0.930 | 251.20 | 0.98602118 | 1004.8 | 0.05591530 |
| 1256.25 | 0.930 | 251.25 | 0.98604080 | 1005.0 | 0.05583681 |
| 1256.5 | 0.930 | 251.30 | 0.98606042 | 1005.2 | 0.05575832 |
| 1256.75 | 0.930 | 251.35 | 0.98608004 | 1005.4 | 0.05567984 |
| 1257 | 0.930 | 251.40 | 0.98609966 | 1005.6 | 0.05560137 |
| 1257.25 | 0.931 | 251.45 | 0.98611927 | 1005.8 | 0.05552291 |
| 1257.5 | 0.931 | 251.50 | 0.98613889 | 1006.0 | 0.05544445 |
| 1257.75 | 0.931 | 251.55 | 0.98615850 | 1006.2 | 0.05536601 |
| 1258 | 0.931 | 251.60 | 0.98617811 | 1006.4 | 0.05528756 |
| 1258.25 | 0.931 | 251.65 | 0.98619772 | 1006.6 | 0.05520913 |


| 1258.5 | 0.931 | 251.70 | 0.98621732 | 1006.8 | 0.05513070 |
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| 1258.75 | 0.931 | 251.75 | 0.98623693 | 1007.0 | 0.05505228 |
| 1259 | 0.931 | 251.80 | 0.98625653 | 1007.2 | 0.05497387 |
| 1259.25 | 0.931 | 251.85 | 0.98627613 | 1007.4 | 0.05489547 |
| 1259.5 | 0.931 | 251.90 | 0.98629573 | 1007.6 | 0.05481707 |
| 1259.75 | 0.932 | 251.95 | 0.98631533 | 1007.8 | 0.05473868 |
| 1260 | 0.932 | 252.00 | 0.98633493 | 1008.0 | 0.05466030 |
| 1260.25 | 0.932 | 252.05 | 0.98635452 | 1008.2 | 0.05458192 |
| 1260.5 | 0.932 | 252.10 | 0.98637411 | 1008.4 | 0.05450356 |
| 1260.75 | 0.932 | 252.15 | 0.98639370 | 1008.6 | 0.05442519 |
| 1261 | 0.932 | 252.20 | 0.98641329 | 1008.8 | 0.05434684 |
| 1261.25 | 0.932 | 252.25 | 0.98643288 | 1009.0 | 0.05426849 |
| 1261.5 | 0.932 | 252.30 | 0.98645246 | 1009.2 | 0.05419016 |
| 1261.75 | 0.932 | 252.35 | 0.98647204 | 1009.4 | 0.05411182 |
| 1262 | 0.932 | 252.40 | 0.98649162 | 1009.6 | 0.05403350 |
| 1262.25 | 0.933 | 252.45 | 0.98651120 | 1009.8 | 0.05395518 |
| 1262.5 | 0.933 | 252.50 | 0.98653078 | 1010.0 | 0.05387687 |
| 1262.75 | 0.933 | 252.55 | 0.98655036 | 1010.2 | 0.05379857 |
| 1263 | 0.933 | 252.60 | 0.98656993 | 1010.4 | 0.05372028 |
| 1263.25 | 0.933 | 252.65 | 0.98658950 | 1010.6 | 0.05364199 |
| 1263.5 | 0.933 | 252.70 | 0.98660907 | 1010.8 | 0.05356371 |
| 1263.75 | 0.933 | 252.75 | 0.98662864 | 1011.0 | 0.05348543 |
| 1264 | 0.933 | 252.80 | 0.98664821 | 1011.2 | 0.05340717 |
| 1264.25 | 0.933 | 252.85 | 0.98666777 | 1011.4 | 0.05332891 |
| 1264.5 | 0.933 | 252.90 | 0.98668734 | 1011.6 | 0.05325066 |
| 1264.75 | 0.934 | 252.95 | 0.98670690 | 1011.8 | 0.05317241 |
| 1265 | 0.934 | 253.00 | 0.98672646 | 1012.0 | 0.05309418 |
| 1265.25 | 0.934 | 253.05 | 0.98674601 | 1012.2 | 0.05301595 |
| 1265.5 | 0.934 | 253.10 | 0.98676557 | 1012.4 | 0.05293773 |
| 1265.75 | 0.934 | 253.15 | 0.98678512 | 1012.6 | 0.05285951 |
| 1266 | 0.934 | 253.20 | 0.98680467 | 1012.8 | 0.05278130 |
| 1266.25 | 0.934 | 253.25 | 0.98682422 | 1013.0 | 0.05270310 |
| 1266.5 | 0.934 | 253.30 | 0.98684377 | 1013.2 | 0.05262491 |
| 1266.75 | 0.934 | 253.35 | 0.98686332 | 1013.4 | 0.05254672 |
| 1267 | 0.934 | 253.40 | 0.98688286 | 1013.6 | 0.05246854 |
| 1267.25 | 0.935 | 253.45 | 0.98690241 | 1013.8 | 0.05239037 |
| 1267.5 | 0.935 | 253.50 | 0.98692195 | 1014.0 | 0.05231221 |
| 1267.75 | 0.935 | 253.55 | 0.98694149 | 1014.2 | 0.05223405 |
| 1268 | 0.935 | 253.60 | 0.98696102 | 1014.4 | 0.05215590 |
| 1268.25 | 0.935 | 253.65 | 0.98698056 | 1014.6 | 0.05207776 |
| 1268.5 | 0.935 | 253.70 | 0.98700009 | 1014.8 | 0.05199962 |
| 1268.75 | 0.935 | 253.75 | 0.98701963 | 1015.0 | 0.05192150 |
| 1269 | 0.935 | 253.80 | 0.98703916 | 1015.2 | 0.05184338 |
| 1269.25 | 0.935 | 253.85 | 0.98705868 | 1015.4 | 0.05176526 |
| 1269.5 | 0.935 | 253.90 | 0.98707821 | 1015.6 | 0.05168716 |
| 1269.75 | 0.935 | 253.95 | 0.98709774 | 1015.8 | 0.05160906 |
| 1270 | 0.936 | 254.00 | 0.98711726 | 1016.0 | 0.05153096 |
| 1270.25 | 0.936 | 254.05 | 0.98713678 | 1016.2 | 0.05145288 |
| 1270.5 | 0.936 | 254.10 | 0.98715630 | 1016.4 | 0.05137480 |
| 1270.75 | 0.936 | 254.15 | 0.98717582 | 1016.6 | 0.05129673 |
| 1271 | 0.936 | 254.20 | 0.98719533 | 1016.8 | 0.05121867 |
| 1271.25 | 0.936 | 254.25 | 0.98721485 | 1017.0 | 0.05114061 |
| 1271.5 | 0.936 | 254.30 | 0.98723436 | 1017.2 | 0.05106256 |
| 1271.75 | 0.936 | 254.35 | 0.98725387 | 1017.4 | 0.05098452 |
| 1272 | 0.936 | 254.40 | 0.98727338 | 1017.6 | 0.05090649 |
| 1272.25 | 0.936 | 254.45 | 0.98729288 | 1017.8 | 0.05082846 |
| 1272.5 | 0.937 | 254.50 | 0.98731239 | 1018.0 | 0.05075044 |
| 1272.75 | 0.937 | 254.55 | 0.98733189 | 1018.2 | 0.05067243 |
| 1273 | 0.937 | 254.60 | 0.98735139 | 1018.4 | 0.05059442 |
| 1273.25 | 0.937 | 254.65 | 0.98737089 | 1018.6 | 0.05051643 |
| 1273.5 | 0.937 | 254.70 | 0.98739039 | 1018.8 | 0.05043843 |
| 1273.75 | 0.937 | 254.75 | 0.98740989 | 1019.0 | 0.05036045 |
| 1274 | 0.937 | 254.80 | 0.98742938 | 1019.2 | 0.05028247 |
| 1274.25 | 0.937 | 254.85 | 0.98744887 | 1019.4 | 0.05020451 |
| 1274.5 | 0.937 | 254.90 | 0.98746836 | 1019.6 | 0.05012654 |
| 1274.75 | 0.937 | 254.95 | 0.98748785 | 1019.8 | 0.05004859 |
| 1275 | 0.938 | 255.00 | 0.98750734 | 1020.0 | 0.04997064 |
| 1275.25 | 0.938 | 255.05 | 0.98752683 | 1020.2 | 0.04989270 |
| 1275.5 | 0.938 | 255.10 | 0.98754631 | 1020.4 | 0.04981477 |
| 1275.75 | 0.938 | 255.15 | 0.98756579 | 1020.6 | 0.04973684 |
| 1276 | 0.938 | 255.20 | 0.98758527 | 1020.8 | 0.04965892 |


| 1276.25 | 0.938 | 255.25 | 0.98760475 | 1021.0 | 0.04958101 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1276.5 | 0.938 | 255.30 | 0.98762422 | 1021.2 | 0.04950310 |
| 1276.75 | 0.938 | 255.35 | 0.98764370 | 1021.4 | 0.04942521 |
| 1277 | 0.938 | 255.40 | 0.98766317 | 1021.6 | 0.04934732 |
| 1277.25 | 0.938 | 255.45 | 0.98768264 | 1021.8 | 0.04926943 |
| 1277.5 | 0.939 | 255.50 | 0.98770211 | 1022.0 | 0.04919156 |
| 1277.75 | 0.939 | 255.55 | 0.98772158 | 1022.2 | 0.04911369 |
| 1278 | 0.939 | 255.60 | 0.98774104 | 1022.4 | 0.04903583 |
| 1278.25 | 0.939 | 255.65 | 0.98776051 | 1022.6 | 0.04895797 |
| 1278.5 | 0.939 | 255.70 | 0.98777997 | 1022.8 | 0.04888012 |
| 1278.75 | 0.939 | 255.75 | 0.98779943 | 1023.0 | 0.04880228 |
| 1279 | 0.939 | 255.80 | 0.98781889 | 1023.2 | 0.04872445 |
| 1279.25 | 0.939 | 255.85 | 0.98783834 | 1023.4 | 0.04864662 |
| 1279.5 | 0.939 | 255.90 | 0.98785780 | 1023.6 | 0.04856881 |
| 1279.75 | 0.939 | 255.95 | 0.98787725 | 1023.8 | 0.04849099 |
| 1280 | 0.939 | 256.00 | 0.98789670 | 1024.0 | 0.04841319 |
| 1280.25 | 0.940 | 256.05 | 0.98791615 | 1024.2 | 0.04833539 |
| 1280.5 | 0.940 | 256.10 | 0.98793560 | 1024.4 | 0.04825760 |
| 1280.75 | 0.940 | 256.15 | 0.98795505 | 1024.6 | 0.04817982 |
| 1281 | 0.940 | 256.20 | 0.98797449 | 1024.8 | 0.04810204 |
| 1281.25 | 0.940 | 256.25 | 0.98799393 | 1025.0 | 0.04802427 |
| 1281.5 | 0.940 | 256.30 | 0.98801337 | 1025.2 | 0.04794651 |
| 1281.75 | 0.940 | 256.35 | 0.98803281 | 1025.4 | 0.04786876 |
| 1282 | 0.940 | 256.40 | 0.98805225 | 1025.6 | 0.04779101 |
| 1282.25 | 0.940 | 256.45 | 0.98807168 | 1025.8 | 0.04771327 |
| 1282.5 | 0.940 | 256.50 | 0.98809112 | 1026.0 | 0.04763554 |
| 1282.75 | 0.941 | 256.55 | 0.98811055 | 1026.2 | 0.04755781 |
| 1283 | 0.941 | 256.60 | 0.98812998 | 1026.4 | 0.04748009 |
| 1283.25 | 0.941 | 256.65 | 0.98814941 | 1026.6 | 0.04740238 |
| 1283.5 | 0.941 | 256.70 | 0.98816883 | 1026.8 | 0.04732467 |
| 1283.75 | 0.941 | 256.75 | 0.98818826 | 1027.0 | 0.04724698 |
| 1284 | 0.941 | 256.80 | 0.98820768 | 1027.2 | 0.04716929 |
| 1284.25 | 0.941 | 256.85 | 0.98822710 | 1027.4 | 0.04709160 |
| 1284.5 | 0.941 | 256.90 | 0.98824652 | 1027.6 | 0.04701393 |
| 1284.75 | 0.941 | 256.95 | 0.98826594 | 1027.8 | 0.04693626 |
| 1285 | 0.941 | 257.00 | 0.98828535 | 1028.0 | 0.04685860 |
| 1285.25 | 0.942 | 257.05 | 0.98830476 | 1028.2 | 0.04678094 |
| 1285.5 | 0.942 | 257.10 | 0.98832418 | 1028.4 | 0.04670329 |
| 1285.75 | 0.942 | 257.15 | 0.98834359 | 1028.6 | 0.04662565 |
| 1286 | 0.942 | 257.20 | 0.98836300 | 1028.8 | 0.04654802 |
| 1286.25 | 0.942 | 257.25 | 0.98838240 | 1029.0 | 0.04647039 |
| 1286.5 | 0.942 | 257.30 | 0.98840181 | 1029.2 | 0.04639277 |
| 1286.75 | 0.942 | 257.35 | 0.98842121 | 1029.4 | 0.04631516 |
| 1287 | 0.942 | 257.40 | 0.98844061 | 1029.6 | 0.04623755 |
| 1287.25 | 0.942 | 257.45 | 0.98846001 | 1029.8 | 0.04615996 |
| 1287.5 | 0.942 | 257.50 | 0.98847941 | 1030.0 | 0.04608236 |
| 1287.75 | 0.942 | 257.55 | 0.98849880 | 1030.2 | 0.04600478 |
| 1288 | 0.943 | 257.60 | 0.98851820 | 1030.4 | 0.04592720 |
| 1288.25 | 0.943 | 257.65 | 0.98853759 | 1030.6 | 0.04584963 |
| 1288.5 | 0.943 | 257.70 | 0.98855698 | 1030.8 | 0.04577207 |
| 1288.75 | 0.943 | 257.75 | 0.98857637 | 1031.0 | 0.04569452 |
| 1289 | 0.943 | 257.80 | 0.98859576 | 1031.2 | 0.04561697 |
| 1289.25 | 0.943 | 257.85 | 0.98861514 | 1031.4 | 0.04553942 |
| 1289.5 | 0.943 | 257.90 | 0.98863453 | 1031.6 | 0.04546189 |
| 1289.75 | 0.943 | 257.95 | 0.98865391 | 1031.8 | 0.04538436 |
| 1290 | 0.943 | 258.00 | 0.98867329 | 1032.0 | 0.04530684 |
| 1290.25 | 0.943 | 258.05 | 0.98869267 | 1032.2 | 0.04522933 |
| 1290.5 | 0.944 | 258.10 | 0.98871204 | 1032.4 | 0.04515182 |
| 1290.75 | 0.944 | 258.15 | 0.98873142 | 1032.6 | 0.04507432 |
| 1291 | 0.944 | 258.20 | 0.98875079 | 1032.8 | 0.04499683 |
| 1291.25 | 0.944 | 258.25 | 0.98877016 | 1033.0 | 0.04491935 |
| 1291.5 | 0.944 | 258.30 | 0.98878953 | 1033.2 | 0.04484187 |
| 1291.75 | 0.944 | 258.35 | 0.98880890 | 1033.4 | 0.04476440 |
| 1292 | 0.944 | 258.40 | 0.98882827 | 1033.6 | 0.04468693 |
| 1292.25 | 0.944 | 258.45 | 0.98884763 | 1033.8 | 0.04460948 |
| 1292.5 | 0.944 | 258.50 | 0.98886699 | 1034.0 | 0.04453203 |
| 1292.75 | 0.944 | 258.55 | 0.98888635 | 1034.2 | 0.04445458 |
| 1293 | 0.945 | 258.60 | 0.98890571 | 1034.4 | 0.04437715 |
| 1293.25 | 0.945 | 258.65 | 0.98892507 | 1034.6 | 0.04429972 |
| 1293.5 | 0.945 | 258.70 | 0.98894443 | 1034.8 | 0.04422230 |
| 1293.75 | 0.945 | 258.75 | 0.98896378 | 1035.0 | 0.04414488 |


| 1294 | 0.945 | 258.80 | 0.98898313 | 1035.2 | 0.04406747 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1294.25 | 0.945 | 258.85 | 0.98900248 | 1035.4 | 0.04399007 |
| 1294.5 | 0.945 | 258.90 | 0.98902183 | 1035.6 | 0.04391268 |
| 1294.75 | 0.945 | 258.95 | 0.98904118 | 1035.8 | 0.04383529 |
| 1295 | 0.945 | 259.00 | 0.98906052 | 1036.0 | 0.04375791 |
| 1295.25 | 0.945 | 259.05 | 0.98907986 | 1036.2 | 0.04368054 |
| 1295.5 | 0.945 | 259.10 | 0.98909921 | 1036.4 | 0.04360317 |
| 1295.75 | 0.946 | 259.15 | 0.98911855 | 1036.6 | 0.04352582 |
| 1296 | 0.946 | 259.20 | 0.98913788 | 1036.8 | 0.04344846 |
| 1296.25 | 0.946 | 259.25 | 0.98915722 | 1037.0 | 0.04337112 |
| 1296.5 | 0.946 | 259.30 | 0.98917655 | 1037.2 | 0.04329378 |
| 1296.75 | 0.946 | 259.35 | 0.98919589 | 1037.4 | 0.04321645 |
| 1297 | 0.946 | 259.40 | 0.98921522 | 1037.6 | 0.04313913 |
| 1297.25 | 0.946 | 259.45 | 0.98923455 | 1037.8 | 0.04306181 |
| 1297.5 | 0.946 | 259.50 | 0.98925387 | 1038.0 | 0.04298450 |
| 1297.75 | 0.946 | 259.55 | 0.98927320 | 1038.2 | 0.04290720 |
| 1298 | 0.946 | 259.60 | 0.98929252 | 1038.4 | 0.04282990 |
| 1298.25 | 0.947 | 259.65 | 0.98931185 | 1038.6 | 0.04275262 |
| 1298.5 | 0.947 | 259.70 | 0.98933117 | 1038.8 | 0.04267533 |
| 1298.75 | 0.947 | 259.75 | 0.98935049 | 1039.0 | 0.04259806 |
| 1299 | 0.947 | 259.80 | 0.98936980 | 1039.2 | 0.04252079 |
| 1299.25 | 0.947 | 259.85 | 0.98938912 | 1039.4 | 0.04244353 |
| 1299.5 | 0.947 | 259.90 | 0.98940843 | 1039.6 | 0.04236628 |
| 1299.75 | 0.947 | 259.95 | 0.98942774 | 1039.8 | 0.04228903 |
| 1300 | 0.947 | 260.00 | 0.98944705 | 1040.0 | 0.04221179 |
| 1300.25 | 0.947 | 260.05 | 0.98946636 | 1040.2 | 0.04213456 |
| 1300.5 | 0.947 | 260.10 | 0.98948567 | 1040.4 | 0.04205733 |
| 1300.75 | 0.948 | 260.15 | 0.98950497 | 1040.6 | 0.04198012 |
| 1301 | 0.948 | 260.20 | 0.98952427 | 1040.8 | 0.04190290 |
| 1301.25 | 0.948 | 260.25 | 0.98954358 | 1041.0 | 0.04182570 |
| 1301.5 | 0.948 | 260.30 | 0.98956287 | 1041.2 | 0.04174850 |
| 1301.75 | 0.948 | 260.35 | 0.98958217 | 1041.4 | 0.04167131 |
| 1302 | 0.948 | 260.40 | 0.98960147 | 1041.6 | 0.04159413 |
| 1302.25 | 0.948 | 260.45 | 0.98962076 | 1041.8 | 0.04151695 |
| 1302.5 | 0.948 | 260.50 | 0.98964006 | 1042.0 | 0.04143978 |
| 1302.75 | 0.948 | 260.55 | 0.98965935 | 1042.2 | 0.04136262 |
| 1303 | 0.948 | 260.60 | 0.98967863 | 1042.4 | 0.04128546 |
| 1303.25 | 0.948 | 260.65 | 0.98969792 | 1042.6 | 0.04120831 |
| 1303.5 | 0.949 | 260.70 | 0.98971721 | 1042.8 | 0.04113117 |
| 1303.75 | 0.949 | 260.75 | 0.98973649 | 1043.0 | 0.04105403 |
| 1304 | 0.949 | 260.80 | 0.98975577 | 1043.2 | 0.04097691 |
| 1304.25 | 0.949 | 260.85 | 0.98977505 | 1043.4 | 0.04089979 |
| 1304.5 | 0.949 | 260.90 | 0.98979433 | 1043.6 | 0.04082267 |
| 1304.75 | 0.949 | 260.95 | 0.98981361 | 1043.8 | 0.04074556 |
| 1305 | 0.949 | 261.00 | 0.98983288 | 1044.0 | 0.04066846 |
| 1305.25 | 0.949 | 261.05 | 0.98985216 | 1044.2 | 0.04059137 |
| 1305.5 | 0.949 | 261.10 | 0.98987143 | 1044.4 | 0.04051428 |
| 1305.75 | 0.949 | 261.15 | 0.98989070 | 1044.6 | 0.04043720 |
| 1306 | 0.950 | 261.20 | 0.98990997 | 1044.8 | 0.04036013 |
| 1306.25 | 0.950 | 261.25 | 0.98992923 | 1045.0 | 0.04028307 |
| 1306.5 | 0.950 | 261.30 | 0.98994850 | 1045.2 | 0.04020601 |
| 1306.75 | 0.950 | 261.35 | 0.98996776 | 1045.4 | 0.04012896 |
| 1307 | 0.950 | 261.40 | 0.98998702 | 1045.6 | 0.04005191 |
| 1307.25 | 0.950 | 261.45 | 0.99000628 | 1045.8 | 0.03997487 |
| 1307.5 | 0.950 | 261.50 | 0.99002554 | 1046.0 | 0.03989784 |
| 1307.75 | 0.950 | 261.55 | 0.99004480 | 1046.2 | 0.03982082 |
| 1308 | 0.950 | 261.60 | 0.99006405 | 1046.4 | 0.03974380 |
| 1308.25 | 0.950 | 261.65 | 0.99008330 | 1046.6 | 0.03966679 |
| 1308.5 | 0.951 | 261.70 | 0.99010255 | 1046.8 | 0.03958979 |
| 1308.75 | 0.951 | 261.75 | 0.99012180 | 1047.0 | 0.03951279 |
| 1309 | 0.951 | 261.80 | 0.99014105 | 1047.2 | 0.03943580 |
| 1309.25 | 0.951 | 261.85 | 0.99016030 | 1047.4 | 0.03935882 |
| 1309.5 | 0.951 | 261.90 | 0.99017954 | 1047.6 | 0.03928184 |
| 1309.75 | 0.951 | 261.95 | 0.99019878 | 1047.8 | 0.03920487 |
| 1310 | 0.951 | 262.00 | 0.99021802 | 1048.0 | 0.03912791 |
| 1310.25 | 0.951 | 262.05 | 0.99023726 | 1048.2 | 0.03905096 |
| 1310.5 | 0.951 | 262.10 | 0.99025650 | 1048.4 | 0.03897401 |
| 1310.75 | 0.951 | 262.15 | 0.99027573 | 1048.6 | 0.03889707 |
| 1311 | 0.951 | 262.20 | 0.99029497 | 1048.8 | 0.03882013 |
| 1311.25 | 0.952 | 262.25 | 0.99031420 | 1049.0 | 0.03874321 |
| 1311.5 | 0.952 | 262.30 | 0.99033343 | 1049.2 | 0.03866629 |


| 1311.75 | 0.952 | 262.35 | 0.99035266 | 1049.4 | 0.03858937 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1312 | 0.952 | 262.40 | 0.99037188 | 1049.6 | 0.03851246 |
| 1312.25 | 0.952 | 262.45 | 0.99039111 | 1049.8 | 0.03843556 |
| 1312.5 | 0.952 | 262.50 | 0.99041033 | 1050.0 | 0.03835867 |
| 1312.75 | 0.952 | 262.55 | 0.99042955 | 1050.2 | 0.03828179 |
| 1313 | 0.952 | 262.60 | 0.99044877 | 1050.4 | 0.03820491 |
| 1313.25 | 0.952 | 262.65 | 0.99046799 | 1050.6 | 0.03812803 |
| 1313.5 | 0.952 | 262.70 | 0.99048721 | 1050.8 | 0.03805117 |
| 1313.75 | 0.953 | 262.75 | 0.99050642 | 1051.0 | 0.03797431 |
| 1314 | 0.953 | 262.80 | 0.99052564 | 1051.2 | 0.03789746 |
| 1314.25 | 0.953 | 262.85 | 0.99054485 | 1051.4 | 0.03782061 |
| 1314.5 | 0.953 | 262.90 | 0.99056406 | 1051.6 | 0.03774378 |
| 1314.75 | 0.953 | 262.95 | 0.99058326 | 1051.8 | 0.03766695 |
| 1315 | 0.953 | 263.00 | 0.99060247 | 1052.0 | 0.03759012 |
| 1315.25 | 0.953 | 263.05 | 0.99062167 | 1052.2 | 0.03751330 |
| 1315.5 | 0.953 | 263.10 | 0.99064088 | 1052.4 | 0.03743649 |
| 1315.75 | 0.953 | 263.15 | 0.99066008 | 1052.6 | 0.03735969 |
| 1316 | 0.953 | 263.20 | 0.99067928 | 1052.8 | 0.03728289 |
| 1316.25 | 0.953 | 263.25 | 0.99069847 | 1053.0 | 0.03720610 |
| 1316.5 | 0.954 | 263.30 | 0.99071767 | 1053.2 | 0.03712932 |
| 1316.75 | 0.954 | 263.35 | 0.99073686 | 1053.4 | 0.03705254 |
| 1317 | 0.954 | 263.40 | 0.99075606 | 1053.6 | 0.03697577 |
| 1317.25 | 0.954 | 263.45 | 0.99077525 | 1053.8 | 0.03689901 |
| 1317.5 | 0.954 | 263.50 | 0.99079444 | 1054.0 | 0.03682226 |
| 1317.75 | 0.954 | 263.55 | 0.99081362 | 1054.2 | 0.03674551 |
| 1318 | 0.954 | 263.60 | 0.99083281 | 1054.4 | 0.03666877 |
| 1318.25 | 0.954 | 263.65 | 0.99085199 | 1054.6 | 0.03659203 |
| 1318.5 | 0.954 | 263.70 | 0.99087117 | 1054.8 | 0.03651530 |
| 1318.75 | 0.954 | 263.75 | 0.99089035 | 1055.0 | 0.03643858 |
| 1319 | 0.955 | 263.80 | 0.99090953 | 1055.2 | 0.03636187 |
| 1319.25 | 0.955 | 263.85 | 0.99092871 | 1055.4 | 0.03628516 |
| 1319.5 | 0.955 | 263.90 | 0.99094789 | 1055.6 | 0.03620846 |
| 1319.75 | 0.955 | 263.95 | 0.99096706 | 1055.8 | 0.03613176 |
| 1320 | 0.955 | 264.00 | 0.99098623 | 1056.0 | 0.03605508 |
| 1320.25 | 0.955 | 264.05 | 0.99100540 | 1056.2 | 0.03597840 |
| 1320.5 | 0.955 | 264.10 | 0.99102457 | 1056.4 | 0.03590172 |
| 1320.75 | 0.955 | 264.15 | 0.99104374 | 1056.6 | 0.03582505 |
| 1321 | 0.955 | 264.20 | 0.99106290 | 1056.8 | 0.03574839 |
| 1321.25 | 0.955 | 264.25 | 0.99108206 | 1057.0 | 0.03567174 |
| 1321.5 | 0.956 | 264.30 | 0.99110123 | 1057.2 | 0.03559510 |
| 1321.75 | 0.956 | 264.35 | 0.99112039 | 1057.4 | 0.03551846 |
| 1322 | 0.956 | 264.40 | 0.99113954 | 1057.6 | 0.03544182 |
| 1322.25 | 0.956 | 264.45 | 0.99115870 | 1057.8 | 0.03536520 |
| 1322.5 | 0.956 | 264.50 | 0.99117786 | 1058.0 | 0.03528858 |
| 1322.75 | 0.956 | 264.55 | 0.99119701 | 1058.2 | 0.03521197 |
| 1323 | 0.956 | 264.60 | 0.99121616 | 1058.4 | 0.03513536 |
| 1323.25 | 0.956 | 264.65 | 0.99123531 | 1058.6 | 0.03505876 |
| 1323.5 | 0.956 | 264.70 | 0.99125446 | 1058.8 | 0.03498217 |
| 1323.75 | 0.956 | 264.75 | 0.99127360 | 1059.0 | 0.03490558 |
| 1324 | 0.956 | 264.80 | 0.99129275 | 1059.2 | 0.03482901 |
| 1324.25 | 0.957 | 264.85 | 0.99131189 | 1059.4 | 0.03475243 |
| 1324.5 | 0.957 | 264.90 | 0.99133103 | 1059.6 | 0.03467587 |
| 1324.75 | 0.957 | 264.95 | 0.99135017 | 1059.8 | 0.03459931 |
| 1325 | 0.957 | 265.00 | 0.99136931 | 1060.0 | 0.03452276 |
| 1325.25 | 0.957 | 265.05 | 0.99138845 | 1060.2 | 0.03444622 |
| 1325.5 | 0.957 | 265.10 | 0.99140758 | 1060.4 | 0.03436968 |
| 1325.75 | 0.957 | 265.15 | 0.99142671 | 1060.6 | 0.03429315 |
| 1326 | 0.957 | 265.20 | 0.99144584 | 1060.8 | 0.03421662 |
| 1326.25 | 0.957 | 265.25 | 0.99146497 | 1061.0 | 0.03414011 |
| 1326.5 | 0.957 | 265.30 | 0.99148410 | 1061.2 | 0.03406360 |
| 1326.75 | 0.958 | 265.35 | 0.99150323 | 1061.4 | 0.03398709 |
| 1327 | 0.958 | 265.40 | 0.99152235 | 1061.6 | 0.03391060 |
| 1327.25 | 0.958 | 265.45 | 0.99154147 | 1061.8 | 0.03383411 |
| 1327.5 | 0.958 | 265.50 | 0.99156059 | 1062.0 | 0.03375762 |
| 1327.75 | 0.958 | 265.55 | 0.99157971 | 1062.2 | 0.03368115 |
| 1328 | 0.958 | 265.60 | 0.99159883 | 1062.4 | 0.03360468 |
| 1328.25 | 0.958 | 265.65 | 0.99161795 | 1062.6 | 0.03352821 |
| 1328.5 | 0.958 | 265.70 | 0.99163706 | 1062.8 | 0.03345176 |
| 1328.75 | 0.958 | 265.75 | 0.99165617 | 1063.0 | 0.03337531 |
| 1329 | 0.958 | 265.80 | 0.99167528 | 1063.2 | 0.03329887 |
| 1329.25 | 0.958 | 265.85 | 0.99169439 | 1063.4 | 0.03322243 |


| 1329.5 | 0.959 | 265.90 | 0.99171350 | 1063.6 | 0.03314600 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1329.75 | 0.959 | 265.95 | 0.99173261 | 1063.8 | 0.03306958 |
| 1330 | 0.959 | 266.00 | 0.99175171 | 1064.0 | 0.03299316 |
| 1330.25 | 0.959 | 266.05 | 0.99177081 | 1064.2 | 0.03291675 |
| 1330.5 | 0.959 | 266.10 | 0.99178991 | 1064.4 | 0.03284035 |
| 1330.75 | 0.959 | 266.15 | 0.99180901 | 1064.6 | 0.03276396 |
| 1331 | 0.959 | 266.20 | 0.99182811 | 1064.8 | 0.03268757 |
| 1331.25 | 0.959 | 266.25 | 0.99184720 | 1065.0 | 0.03261118 |
| 1331.5 | 0.959 | 266.30 | 0.99186630 | 1065.2 | 0.03253481 |
| 1331.75 | 0.959 | 266.35 | 0.99188539 | 1065.4 | 0.03245844 |
| 1332 | 0.960 | 266.40 | 0.99190448 | 1065.6 | 0.03238208 |
| 1332.25 | 0.960 | 266.45 | 0.99192357 | 1065.8 | 0.03230572 |
| 1332.5 | 0.960 | 266.50 | 0.99194266 | 1066.0 | 0.03222938 |
| 1332.75 | 0.960 | 266.55 | 0.99196174 | 1066.2 | 0.03215303 |
| 1333 | 0.960 | 266.60 | 0.99198083 | 1066.4 | 0.03207670 |
| 1333.25 | 0.960 | 266.65 | 0.99199991 | 1066.6 | 0.03200037 |
| 1333.5 | 0.960 | 266.70 | 0.99201899 | 1066.8 | 0.03192405 |
| 1333.75 | 0.960 | 266.75 | 0.99203807 | 1067.0 | 0.03184774 |
| 1334 | 0.960 | 266.80 | 0.99205714 | 1067.2 | 0.03177143 |
| 1334.25 | 0.960 | 266.85 | 0.99207622 | 1067.4 | 0.03169513 |
| 1334.5 | 0.960 | 266.90 | 0.99209529 | 1067.6 | 0.03161883 |
| 1334.75 | 0.961 | 266.95 | 0.99211436 | 1067.8 | 0.03154254 |
| 1335 | 0.961 | 267.00 | 0.99213343 | 1068.0 | 0.03146626 |
| 1335.25 | 0.961 | 267.05 | 0.99215250 | 1068.2 | 0.03138999 |
| 1335.5 | 0.961 | 267.10 | 0.99217157 | 1068.4 | 0.03131372 |
| 1335.75 | 0.961 | 267.15 | 0.99219064 | 1068.6 | 0.03123746 |
| 1336 | 0.961 | 267.20 | 0.99220970 | 1068.8 | 0.03116121 |
| 1336.25 | 0.961 | 267.25 | 0.99222876 | 1069.0 | 0.03108496 |
| 1336.5 | 0.961 | 267.30 | 0.99224782 | 1069.2 | 0.03100872 |
| 1336.75 | 0.961 | 267.35 | 0.99226688 | 1069.4 | 0.03093248 |
| 1337 | 0.961 | 267.40 | 0.99228594 | 1069.6 | 0.03085626 |
| 1337.25 | 0.962 | 267.45 | 0.99230499 | 1069.8 | 0.03078004 |
| 1337.5 | 0.962 | 267.50 | 0.99232404 | 1070.0 | 0.03070382 |
| 1337.75 | 0.962 | 267.55 | 0.99234310 | 1070.2 | 0.03062761 |
| 1338 | 0.962 | 267.60 | 0.99236215 | 1070.4 | 0.03055141 |
| 1338.25 | 0.962 | 267.65 | 0.99238120 | 1070.6 | 0.03047522 |
| 1338.5 | 0.962 | 267.70 | 0.99240024 | 1070.8 | 0.03039903 |
| 1338.75 | 0.962 | 267.75 | 0.99241929 | 1071.0 | 0.03032285 |
| 1339 | 0.962 | 267.80 | 0.99243833 | 1071.2 | 0.03024668 |
| 1339.25 | 0.962 | 267.85 | 0.99245737 | 1071.4 | 0.03017051 |
| 1339.5 | 0.962 | 267.90 | 0.99247641 | 1071.6 | 0.03009435 |
| 1339.75 | 0.962 | 267.95 | 0.99249545 | 1071.8 | 0.03001820 |
| 1340 | 0.963 | 268.00 | 0.99251449 | 1072.0 | 0.02994205 |
| 1340.25 | 0.963 | 268.05 | 0.99253352 | 1072.2 | 0.02986591 |
| 1340.5 | 0.963 | 268.10 | 0.99255256 | 1072.4 | 0.02978977 |
| 1340.75 | 0.963 | 268.15 | 0.99257159 | 1072.6 | 0.02971365 |
| 1341 | 0.963 | 268.20 | 0.99259062 | 1072.8 | 0.02963753 |
| 1341.25 | 0.963 | 268.25 | 0.99260965 | 1073.0 | 0.02956141 |
| 1341.5 | 0.963 | 268.30 | 0.99262867 | 1073.2 | 0.02948531 |
| 1341.75 | 0.963 | 268.35 | 0.99264770 | 1073.4 | 0.02940921 |
| 1342 | 0.963 | 268.40 | 0.99266672 | 1073.6 | 0.02933311 |
| 1342.25 | 0.963 | 268.45 | 0.99268574 | 1073.8 | 0.02925703 |
| 1342.5 | 0.964 | 268.50 | 0.99270476 | 1074.0 | 0.02918094 |
| 1342.75 | 0.964 | 268.55 | 0.99272378 | 1074.2 | 0.02910487 |
| 1343 | 0.964 | 268.60 | 0.99274280 | 1074.4 | 0.02902880 |
| 1343.25 | 0.964 | 268.65 | 0.99276181 | 1074.6 | 0.02895274 |
| 1343.5 | 0.964 | 268.70 | 0.99278083 | 1074.8 | 0.02887669 |
| 1343.75 | 0.964 | 268.75 | 0.99279984 | 1075.0 | 0.02880064 |
| 1344 | 0.964 | 268.80 | 0.99281885 | 1075.2 | 0.02872460 |
| 1344.25 | 0.964 | 268.85 | 0.99283786 | 1075.4 | 0.02864857 |
| 1344.5 | 0.964 | 268.90 | 0.99285686 | 1075.6 | 0.02857254 |
| 1344.75 | 0.964 | 268.95 | 0.99287587 | 1075.8 | 0.02849652 |
| 1345 | 0.964 | 269.00 | 0.99289487 | 1076.0 | 0.02842051 |
| 1345.25 | 0.965 | 269.05 | 0.99291388 | 1076.2 | 0.02834450 |
| 1345.5 | 0.965 | 269.10 | 0.99293288 | 1076.4 | 0.02826850 |
| 1345.75 | 0.965 | 269.15 | 0.99295187 | 1076.6 | 0.02819250 |
| 1346 | 0.965 | 269.20 | 0.99297087 | 1076.8 | 0.02811652 |
| 1346.25 | 0.965 | 269.25 | 0.99298987 | 1077.0 | 0.02804054 |
| 1346.5 | 0.965 | 269.30 | 0.99300886 | 1077.2 | 0.02796456 |
| 1346.75 | 0.965 | 269.35 | 0.99302785 | 1077.4 | 0.02788859 |
| 1347 | 0.965 | 269.40 | 0.99304684 | 1077.6 | 0.02781263 |


| 1347.25 | 0.965 | 269.45 | 0.99306583 | 1077.8 | 0.02773668 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1347.5 | 0.965 | 269.50 | 0.99308482 | 1078.0 | 0.02766073 |
| 1347.75 | 0.966 | 269.55 | 0.99310380 | 1078.2 | 0.02758479 |
| 1348 | 0.966 | 269.60 | 0.99312279 | 1078.4 | 0.02750886 |
| 1348.25 | 0.966 | 269.65 | 0.99314177 | 1078.6 | 0.02743293 |
| 1348.5 | 0.966 | 269.70 | 0.99316075 | 1078.8 | 0.02735701 |
| 1348.75 | 0.966 | 269.75 | 0.99317973 | 1079.0 | 0.02728109 |
| 1349 | 0.966 | 269.80 | 0.99319870 | 1079.2 | 0.02720519 |
| 1349.25 | 0.966 | 269.85 | 0.99321768 | 1079.4 | 0.02712928 |
| 1349.5 | 0.966 | 269.90 | 0.99323665 | 1079.6 | 0.02705339 |
| 1349.75 | 0.966 | 269.95 | 0.99325562 | 1079.8 | 0.02697750 |
| 1350 | 0.966 | 270.00 | 0.99327460 | 1080.0 | 0.02690162 |
| 1350.25 | 0.966 | 270.05 | 0.99329356 | 1080.2 | 0.02682574 |
| 1350.5 | 0.967 | 270.10 | 0.99331253 | 1080.4 | 0.02674988 |
| 1350.75 | 0.967 | 270.15 | 0.99333150 | 1080.6 | 0.02667401 |
| 1351 | 0.967 | 270.20 | 0.99335046 | 1080.8 | 0.02659816 |
| 1351.25 | 0.967 | 270.25 | 0.99336942 | 1081.0 | 0.02652231 |
| 1351.5 | 0.967 | 270.30 | 0.99338838 | 1081.2 | 0.02644647 |
| 1351.75 | 0.967 | 270.35 | 0.99340734 | 1081.4 | 0.02637063 |
| 1352 | 0.967 | 270.40 | 0.99342630 | 1081.6 | 0.02629481 |
| 1352.25 | 0.967 | 270.45 | 0.99344525 | 1081.8 | 0.02621898 |
| 1352.5 | 0.967 | 270.50 | 0.99346421 | 1082.0 | 0.02614317 |
| 1352.75 | 0.967 | 270.55 | 0.99348316 | 1082.2 | 0.02606736 |
| 1353 | 0.968 | 270.60 | 0.99350211 | 1082.4 | 0.02599156 |
| 1353.25 | 0.968 | 270.65 | 0.99352106 | 1082.6 | 0.02591576 |
| 1353.5 | 0.968 | 270.70 | 0.99354001 | 1082.8 | 0.02583997 |
| 1353.75 | 0.968 | 270.75 | 0.99355895 | 1083.0 | 0.02576419 |
| 1354 | 0.968 | 270.80 | 0.99357790 | 1083.2 | 0.02568841 |
| 1354.25 | 0.968 | 270.85 | 0.99359684 | 1083.4 | 0.02561264 |
| 1354.5 | 0.968 | 270.90 | 0.99361578 | 1083.6 | 0.02553688 |
| 1354.75 | 0.968 | 270.95 | 0.99363472 | 1083.8 | 0.02546112 |
| 1355 | 0.968 | 271.00 | 0.99365366 | 1084.0 | 0.02538537 |
| 1355.25 | 0.968 | 271.05 | 0.99367259 | 1084.2 | 0.02530963 |
| 1355.5 | 0.968 | 271.10 | 0.99369153 | 1084.4 | 0.02523389 |
| 1355.75 | 0.969 | 271.15 | 0.99371046 | 1084.6 | 0.02515816 |
| 1356 | 0.969 | 271.20 | 0.99372939 | 1084.8 | 0.02508244 |
| 1356.25 | 0.969 | 271.25 | 0.99374832 | 1085.0 | 0.02500672 |
| 1356.5 | 0.969 | 271.30 | 0.99376725 | 1085.2 | 0.02493101 |
| 1356.75 | 0.969 | 271.35 | 0.99378617 | 1085.4 | 0.02485531 |
| 1357 | 0.969 | 271.40 | 0.99380510 | 1085.6 | 0.02477961 |
| 1357.25 | 0.969 | 271.45 | 0.99382402 | 1085.8 | 0.02470392 |
| 1357.5 | 0.969 | 271.50 | 0.99384294 | 1086.0 | 0.02462824 |
| 1357.75 | 0.969 | 271.55 | 0.99386186 | 1086.2 | 0.02455256 |
| 1358 | 0.969 | 271.60 | 0.99388078 | 1086.4 | 0.02447689 |
| 1358.25 | 0.969 | 271.65 | 0.99389969 | 1086.6 | 0.02440123 |
| 1358.5 | 0.970 | 271.70 | 0.99391861 | 1086.8 | 0.02432557 |
| 1358.75 | 0.970 | 271.75 | 0.99393752 | 1087.0 | 0.02424992 |
| 1359 | 0.970 | 271.80 | 0.99395643 | 1087.2 | 0.02417427 |
| 1359.25 | 0.970 | 271.85 | 0.99397534 | 1087.4 | 0.02409863 |
| 1359.5 | 0.970 | 271.90 | 0.99399425 | 1087.6 | 0.02402300 |
| 1359.75 | 0.970 | 271.95 | 0.99401316 | 1087.8 | 0.02394738 |
| 1360 | 0.970 | 272.00 | 0.99403206 | 1088.0 | 0.02387176 |
| 1360.25 | 0.970 | 272.05 | 0.99405096 | 1088.2 | 0.02379614 |
| 1360.5 | 0.970 | 272.10 | 0.99406987 | 1088.4 | 0.02372054 |
| 1360.75 | 0.970 | 272.15 | 0.99408877 | 1088.6 | 0.02364494 |
| 1361 | 0.971 | 272.20 | 0.99410766 | 1088.8 | 0.02356935 |
| 1361.25 | 0.971 | 272.25 | 0.99412656 | 1089.0 | 0.02349376 |
| 1361.5 | 0.971 | 272.30 | 0.99414545 | 1089.2 | 0.02341818 |
| 1361.75 | 0.971 | 272.35 | 0.99416435 | 1089.4 | 0.02334261 |
| 1362 | 0.971 | 272.40 | 0.99418324 | 1089.6 | 0.02326704 |
| 1362.25 | 0.971 | 272.45 | 0.99420213 | 1089.8 | 0.02319148 |
| 1362.5 | 0.971 | 272.50 | 0.99422102 | 1090.0 | 0.02311593 |
| 1362.75 | 0.971 | 272.55 | 0.99423990 | 1090.2 | 0.02304038 |
| 1363 | 0.971 | 272.60 | 0.99425879 | 1090.4 | 0.02296484 |
| 1363.25 | 0.971 | 272.65 | 0.99427767 | 1090.6 | 0.02288931 |
| 1363.5 | 0.971 | 272.70 | 0.99429655 | 1090.8 | 0.02281378 |
| 1363.75 | 0.972 | 272.75 | 0.99431544 | 1091.0 | 0.02273826 |
| 1364 | 0.972 | 272.80 | 0.99433431 | 1091.2 | 0.02266274 |
| 1364.25 | 0.972 | 272.85 | 0.99435319 | 1091.4 | 0.02258724 |
| 1364.5 | 0.972 | 272.90 | 0.99437207 | 1091.6 | 0.02251174 |
| 1364.75 | 0.972 | 272.95 | 0.99439094 | 1091.8 | 0.02243624 |


| 1365 | 0.972 | 273.00 | 0.99440981 | 1092.0 | 0.02236075 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1365.25 | 0.972 | 273.05 | 0.99442868 | 1092.2 | 0.02228527 |
| 1365.5 | 0.972 | 273.10 | 0.99444755 | 1092.4 | 0.02220980 |
| 1365.75 | 0.972 | 273.15 | 0.99446642 | 1092.6 | 0.02213433 |
| 1366 | 0.972 | 273.20 | 0.99448528 | 1092.8 | 0.02205886 |
| 1366.25 | 0.973 | 273.25 | 0.99450415 | 1093.0 | 0.02198341 |
| 1366.5 | 0.973 | 273.30 | 0.99452301 | 1093.2 | 0.02190796 |
| 1366.75 | 0.973 | 273.35 | 0.99454187 | 1093.4 | 0.02183252 |
| 1367 | 0.973 | 273.40 | 0.99456073 | 1093.6 | 0.02175708 |
| 1367.25 | 0.973 | 273.45 | 0.99457959 | 1093.8 | 0.02168165 |
| 1367.5 | 0.973 | 273.50 | 0.99459844 | 1094.0 | 0.02160623 |
| 1367.75 | 0.973 | 273.55 | 0.99461730 | 1094.2 | 0.02153081 |
| 1368 | 0.973 | 273.60 | 0.99463615 | 1094.4 | 0.02145540 |
| 1368.25 | 0.973 | 273.65 | 0.99465500 | 1094.6 | 0.02137999 |
| 1368.5 | 0.973 | 273.70 | 0.99467385 | 1094.8 | 0.02130460 |
| 1368.75 | 0.973 | 273.75 | 0.99469270 | 1095.0 | 0.02122921 |
| 1369 | 0.974 | 273.80 | 0.99471154 | 1095.2 | 0.02115382 |
| 1369.25 | 0.974 | 273.85 | 0.99473039 | 1095.4 | 0.02107844 |
| 1369.5 | 0.974 | 273.90 | 0.99474923 | 1095.6 | 0.02100307 |
| 1369.75 | 0.974 | 273.95 | 0.99476807 | 1095.8 | 0.02092771 |
| 1370 | 0.974 | 274.00 | 0.99478691 | 1096.0 | 0.02085235 |
| 1370.25 | 0.974 | 274.05 | 0.99480575 | 1096.2 | 0.02077699 |
| 1370.5 | 0.974 | 274.10 | 0.99482459 | 1096.4 | 0.02070165 |
| 1370.75 | 0.974 | 274.15 | 0.99484342 | 1096.6 | 0.02062631 |
| 1371 | 0.974 | 274.20 | 0.99486226 | 1096.8 | 0.02055098 |
| 1371.25 | 0.974 | 274.25 | 0.99488109 | 1097.0 | 0.02047565 |
| 1371.5 | 0.974 | 274.30 | 0.99489992 | 1097.2 | 0.02040033 |
| 1371.75 | 0.975 | 274.35 | 0.99491875 | 1097.4 | 0.02032502 |
| 1372 | 0.975 | 274.40 | 0.99493757 | 1097.6 | 0.02024971 |
| 1372.25 | 0.975 | 274.45 | 0.99495640 | 1097.8 | 0.02017441 |
| 1372.5 | 0.975 | 274.50 | 0.99497522 | 1098.0 | 0.02009911 |
| 1372.75 | 0.975 | 274.55 | 0.99499404 | 1098.2 | 0.02002383 |
| 1373 | 0.975 | 274.60 | 0.99501286 | 1098.4 | 0.01994855 |
| 1373.25 | 0.975 | 274.65 | 0.99503168 | 1098.6 | 0.01987327 |
| 1373.5 | 0.975 | 274.70 | 0.99505050 | 1098.8 | 0.01979800 |
| 1373.75 | 0.975 | 274.75 | 0.99506931 | 1099.0 | 0.01972274 |
| 1374 | 0.975 | 274.80 | 0.99508813 | 1099.2 | 0.01964748 |
| 1374.25 | 0.976 | 274.85 | 0.99510694 | 1099.4 | 0.01957224 |
| 1374.5 | 0.976 | 274.90 | 0.99512575 | 1099.6 | 0.01949699 |
| 1374.75 | 0.976 | 274.95 | 0.99514456 | 1099.8 | 0.01942176 |
| 1375 | 0.976 | 275.00 | 0.99516337 | 1100.0 | 0.01934653 |
| 1375.25 | 0.976 | 275.05 | 0.99518217 | 1100.2 | 0.01927130 |
| 1375.5 | 0.976 | 275.10 | 0.99520098 | 1100.4 | 0.01919609 |
| 1375.75 | 0.976 | 275.15 | 0.99521978 | 1100.6 | 0.01912088 |
| 1376 | 0.976 | 275.20 | 0.99523858 | 1100.8 | 0.01904567 |
| 1376.25 | 0.976 | 275.25 | 0.99525738 | 1101.0 | 0.01897047 |
| 1376.5 | 0.976 | 275.30 | 0.99527618 | 1101.2 | 0.01889528 |
| 1376.75 | 0.976 | 275.35 | 0.99529498 | 1101.4 | 0.01882010 |
| 1377 | 0.977 | 275.40 | 0.99531377 | 1101.6 | 0.01874492 |
| 1377.25 | 0.977 | 275.45 | 0.99533256 | 1101.8 | 0.01866975 |
| 1377.5 | 0.977 | 275.50 | 0.99535135 | 1102.0 | 0.01859458 |
| 1377.75 | 0.977 | 275.55 | 0.99537014 | 1102.2 | 0.01851942 |
| 1378 | 0.977 | 275.60 | 0.99538893 | 1102.4 | 0.01844427 |
| 1378.25 | 0.977 | 275.65 | 0.99540772 | 1102.6 | 0.01836912 |
| 1378.5 | 0.977 | 275.70 | 0.99542650 | 1102.8 | 0.01829398 |
| 1378.75 | 0.977 | 275.75 | 0.99544529 | 1103.0 | 0.01821885 |
| 1379 | 0.977 | 275.80 | 0.99546407 | 1103.2 | 0.01814372 |
| 1379.25 | 0.977 | 275.85 | 0.99548285 | 1103.4 | 0.01806860 |
| 1379.5 | 0.978 | 275.90 | 0.99550163 | 1103.6 | 0.01799349 |
| 1379.75 | 0.978 | 275.95 | 0.99552041 | 1103.8 | 0.01791838 |
| 1380 | 0.978 | 276.00 | 0.99553918 | 1104.0 | 0.01784328 |
| 1380.25 | 0.978 | 276.05 | 0.99555795 | 1104.2 | 0.01776818 |
| 1380.5 | 0.978 | 276.10 | 0.99557673 | 1104.4 | 0.01769309 |
| 1380.75 | 0.978 | 276.15 | 0.99559550 | 1104.6 | 0.01761801 |
| 1381 | 0.978 | 276.20 | 0.99561427 | 1104.8 | 0.01754294 |
| 1381.25 | 0.978 | 276.25 | 0.99563303 | 1105.0 | 0.01746787 |
| 1381.5 | 0.978 | 276.30 | 0.99565180 | 1105.2 | 0.01739280 |
| 1381.75 | 0.978 | 276.35 | 0.99567056 | 1105.4 | 0.01731775 |
| 1382 | 0.978 | 276.40 | 0.99568933 | 1105.6 | 0.01724270 |
| 1382.25 | 0.979 | 276.45 | 0.99570809 | 1105.8 | 0.01716765 |
| 1382.5 | 0.979 | 276.50 | 0.99572685 | 1106.0 | 0.01709261 |


| 1382.75 | 0.979 | 276.55 | 0.99574560 | 1106.2 | 0.01701758 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1383 | 0.979 | 276.60 | 0.99576436 | 1106.4 | 0.01694256 |
| 1383.25 | 0.979 | 276.65 | 0.99578312 | 1106.6 | 0.01686754 |
| 1383.5 | 0.979 | 276.70 | 0.99580187 | 1106.8 | 0.01679253 |
| 1383.75 | 0.979 | 276.75 | 0.99582062 | 1107.0 | 0.01671752 |
| 1384 | 0.979 | 276.80 | 0.99583937 | 1107.2 | 0.01664252 |
| 1384.25 | 0.979 | 276.85 | 0.99585812 | 1107.4 | 0.01656753 |
| 1384.5 | 0.979 | 276.90 | 0.99587686 | 1107.6 | 0.01649254 |
| 1384.75 | 0.979 | 276.95 | 0.99589561 | 1107.8 | 0.01641756 |
| 1385 | 0.980 | 277.00 | 0.99591435 | 1108.0 | 0.01634259 |
| 1385.25 | 0.980 | 277.05 | 0.99593310 | 1108.2 | 0.01626762 |
| 1385.5 | 0.980 | 277.10 | 0.99595184 | 1108.4 | 0.01619266 |
| 1385.75 | 0.980 | 277.15 | 0.99597057 | 1108.6 | 0.01611770 |
| 1386 | 0.980 | 277.20 | 0.99598931 | 1108.8 | 0.01604275 |
| 1386.25 | 0.980 | 277.25 | 0.99600805 | 1109.0 | 0.01596781 |
| 1386.5 | 0.980 | 277.30 | 0.99602678 | 1109.2 | 0.01589288 |
| 1386.75 | 0.980 | 277.35 | 0.99604551 | 1109.4 | 0.01581795 |
| 1387 | 0.980 | 277.40 | 0.99606424 | 1109.6 | 0.01574302 |
| 1387.25 | 0.980 | 277.45 | 0.99608297 | 1109.8 | 0.01566811 |
| 1387.5 | 0.981 | 277.50 | 0.99610170 | 1110.0 | 0.01559320 |
| 1387.75 | 0.981 | 277.55 | 0.99612043 | 1110.2 | 0.01551829 |
| 1388 | 0.981 | 277.60 | 0.99613915 | 1110.4 | 0.01544339 |
| 1388.25 | 0.981 | 277.65 | 0.99615787 | 1110.6 | 0.01536850 |
| 1388.5 | 0.981 | 277.70 | 0.99617660 | 1110.8 | 0.01529362 |
| 1388.75 | 0.981 | 277.75 | 0.99619532 | 1111.0 | 0.01521874 |
| 1389 | 0.981 | 277.80 | 0.99621403 | 1111.2 | 0.01514387 |
| 1389.25 | 0.981 | 277.85 | 0.99623275 | 1111.4 | 0.01506900 |
| 1389.5 | 0.981 | 277.90 | 0.99625146 | 1111.6 | 0.01499414 |
| 1389.75 | 0.981 | 277.95 | 0.99627018 | 1111.8 | 0.01491929 |
| 1390 | 0.981 | 278.00 | 0.99628889 | 1112.0 | 0.01484444 |
| 1390.25 | 0.982 | 278.05 | 0.99630760 | 1112.2 | 0.01476960 |
| 1390.5 | 0.982 | 278.10 | 0.99632631 | 1112.4 | 0.01469476 |
| 1390.75 | 0.982 | 278.15 | 0.99634502 | 1112.6 | 0.01461994 |
| 1391 | 0.982 | 278.20 | 0.99636372 | 1112.8 | 0.01454511 |
| 1391.25 | 0.982 | 278.25 | 0.99638243 | 1113.0 | 0.01447030 |
| 1391.5 | 0.982 | 278.30 | 0.99640113 | 1113.2 | 0.01439549 |
| 1391.75 | 0.982 | 278.35 | 0.99641983 | 1113.4 | 0.01432069 |
| 1392 | 0.982 | 278.40 | 0.99643853 | 1113.6 | 0.01424589 |
| 1392.25 | 0.982 | 278.45 | 0.99645722 | 1113.8 | 0.01417110 |
| 1392.5 | 0.982 | 278.50 | 0.99647592 | 1114.0 | 0.01409632 |
| 1392.75 | 0.982 | 278.55 | 0.99649462 | 1114.2 | 0.01402154 |
| 1393 | 0.983 | 278.60 | 0.99651331 | 1114.4 | 0.01394677 |
| 1393.25 | 0.983 | 278.65 | 0.99653200 | 1114.6 | 0.01387200 |
| 1393.5 | 0.983 | 278.70 | 0.99655069 | 1114.8 | 0.01379724 |
| 1393.75 | 0.983 | 278.75 | 0.99656938 | 1115.0 | 0.01372249 |
| 1394 | 0.983 | 278.80 | 0.99658806 | 1115.2 | 0.01364775 |
| 1394.25 | 0.983 | 278.85 | 0.99660675 | 1115.4 | 0.01357301 |
| 1394.5 | 0.983 | 278.90 | 0.99662543 | 1115.6 | 0.01349827 |
| 1394.75 | 0.983 | 278.95 | 0.99664411 | 1115.8 | 0.01342354 |
| 1395 | 0.983 | 279.00 | 0.99666279 | 1116.0 | 0.01334882 |
| 1395.25 | 0.983 | 279.05 | 0.99668147 | 1116.2 | 0.01327411 |
| 1395.5 | 0.984 | 279.10 | 0.99670015 | 1116.4 | 0.01319940 |
| 1395.75 | 0.984 | 279.15 | 0.99671883 | 1116.6 | 0.01312470 |
| 1396 | 0.984 | 279.20 | 0.99673750 | 1116.8 | 0.01305000 |
| 1396.25 | 0.984 | 279.25 | 0.99675617 | 1117.0 | 0.01297531 |
| 1396.5 | 0.984 | 279.30 | 0.99677484 | 1117.2 | 0.01290063 |
| 1396.75 | 0.984 | 279.35 | 0.99679351 | 1117.4 | 0.01282595 |
| 1397 | 0.984 | 279.40 | 0.99681218 | 1117.6 | 0.01275128 |
| 1397.25 | 0.984 | 279.45 | 0.99683085 | 1117.8 | 0.01267662 |
| 1397.5 | 0.984 | 279.50 | 0.99684951 | 1118.0 | 0.01260196 |
| 1397.75 | 0.984 | 279.55 | 0.99686817 | 1118.2 | 0.01252731 |
| 1398 | 0.984 | 279.60 | 0.99688683 | 1118.4 | 0.01245266 |
| 1398.25 | 0.985 | 279.65 | 0.99690549 | 1118.6 | 0.01237802 |
| 1398.5 | 0.985 | 279.70 | 0.99692415 | 1118.8 | 0.01230339 |
| 1398.75 | 0.985 | 279.75 | 0.99694281 | 1119.0 | 0.01222876 |
| 1399 | 0.985 | 279.80 | 0.99696146 | 1119.2 | 0.01215414 |
| 1399.25 | 0.985 | 279.85 | 0.99698012 | 1119.4 | 0.01207953 |
| 1399.5 | 0.985 | 279.90 | 0.99699877 | 1119.6 | 0.01200492 |
| 1399.75 | 0.985 | 279.95 | 0.99701742 | 1119.8 | 0.01193032 |
| 1400 | 0.985 | 280.00 | 0.99703607 | 1120.0 | 0.01185573 |
| 1400.25 | 0.985 | 280.05 | 0.99705472 | 1120.2 | 0.01178114 |


| 1400.5 | 0.985 | 280.10 | 0.99707336 | 1120.4 | 0.01170655 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1400.75 | 0.985 | 280.15 | 0.99709201 | 1120.6 | 0.01163198 |
| 1401 | 0.986 | 280.20 | 0.99711065 | 1120.8 | 0.01155741 |
| 1401.25 | 0.986 | 280.25 | 0.99712929 | 1121.0 | 0.01148284 |
| 1401.5 | 0.986 | 280.30 | 0.99714793 | 1121.2 | 0.01140828 |
| 1401.75 | 0.986 | 280.35 | 0.99716657 | 1121.4 | 0.01133373 |
| 1402 | 0.986 | 280.40 | 0.99718520 | 1121.6 | 0.01125919 |
| 1402.25 | 0.986 | 280.45 | 0.99720384 | 1121.8 | 0.01118465 |
| 1402.5 | 0.986 | 280.50 | 0.99722247 | 1122.0 | 0.01111012 |
| 1402.75 | 0.986 | 280.55 | 0.99724110 | 1122.2 | 0.01103559 |
| 1403 | 0.986 | 280.60 | 0.99725973 | 1122.4 | 0.01096107 |
| 1403.25 | 0.986 | 280.65 | 0.99727836 | 1122.6 | 0.01088655 |
| 1403.5 | 0.986 | 280.70 | 0.99729699 | 1122.8 | 0.01081205 |
| 1403.75 | 0.987 | 280.75 | 0.99731561 | 1123.0 | 0.01073755 |
| 1404 | 0.987 | 280.80 | 0.99733424 | 1123.2 | 0.01066305 |
| 1404.25 | 0.987 | 280.85 | 0.99735286 | 1123.4 | 0.01058856 |
| 1404.5 | 0.987 | 280.90 | 0.99737148 | 1123.6 | 0.01051408 |
| 1404.75 | 0.987 | 280.95 | 0.99739010 | 1123.8 | 0.01043960 |
| 1405 | 0.987 | 281.00 | 0.99740872 | 1124.0 | 0.01036513 |
| 1405.25 | 0.987 | 281.05 | 0.99742733 | 1124.2 | 0.01029067 |
| 1405.5 | 0.987 | 281.10 | 0.99744595 | 1124.4 | 0.01021621 |
| 1405.75 | 0.987 | 281.15 | 0.99746456 | 1124.6 | 0.01014176 |
| 1406 | 0.987 | 281.20 | 0.99748317 | 1124.8 | 0.01006731 |
| 1406.25 | 0.988 | 281.25 | 0.99750178 | 1125.0 | 0.00999287 |
| 1406.5 | 0.988 | 281.30 | 0.99752039 | 1125.2 | 0.00991844 |
| 1406.75 | 0.988 | 281.35 | 0.99753900 | 1125.4 | 0.00984401 |
| 1407 | 0.988 | 281.40 | 0.99755760 | 1125.6 | 0.00976959 |
| 1407.25 | 0.988 | 281.45 | 0.99757621 | 1125.8 | 0.00969518 |
| 1407.5 | 0.988 | 281.50 | 0.99759481 | 1126.0 | 0.00962077 |
| 1407.75 | 0.988 | 281.55 | 0.99761341 | 1126.2 | 0.00954637 |
| 1408 | 0.988 | 281.60 | 0.99763201 | 1126.4 | 0.00947197 |
| 1408.25 | 0.988 | 281.65 | 0.99765060 | 1126.6 | 0.00939758 |
| 1408.5 | 0.988 | 281.70 | 0.99766920 | 1126.8 | 0.00932320 |
| 1408.75 | 0.988 | 281.75 | 0.99768779 | 1127.0 | 0.00924882 |
| 1409 | 0.989 | 281.80 | 0.99770639 | 1127.2 | 0.00917445 |
| 1409.25 | 0.989 | 281.85 | 0.99772498 | 1127.4 | 0.00910008 |
| 1409.5 | 0.989 | 281.90 | 0.99774357 | 1127.6 | 0.00902573 |
| 1409.75 | 0.989 | 281.95 | 0.99776216 | 1127.8 | 0.00895137 |
| 1410 | 0.989 | 282.00 | 0.99778074 | 1128.0 | 0.00887703 |
| 1410.25 | 0.989 | 282.05 | 0.99779933 | 1128.2 | 0.00880269 |
| 1410.5 | 0.989 | 282.10 | 0.99781791 | 1128.4 | 0.00872835 |
| 1410.75 | 0.989 | 282.15 | 0.99783649 | 1128.6 | 0.00865403 |
| 1411 | 0.989 | 282.20 | 0.99785507 | 1128.8 | 0.00857970 |
| 1411.25 | 0.989 | 282.25 | 0.99787365 | 1129.0 | 0.00850539 |
| 1411.5 | 0.989 | 282.30 | 0.99789223 | 1129.2 | 0.00843108 |
| 1411.75 | 0.990 | 282.35 | 0.99791081 | 1129.4 | 0.00835678 |
| 1412 | 0.990 | 282.40 | 0.99792938 | 1129.6 | 0.00828248 |
| 1412.25 | 0.990 | 282.45 | 0.99794795 | 1129.8 | 0.00820819 |
| 1412.5 | 0.990 | 282.50 | 0.99796652 | 1130.0 | 0.00813391 |
| 1412.75 | 0.990 | 282.55 | 0.99798509 | 1130.2 | 0.00805963 |
| 1413 | 0.990 | 282.60 | 0.99800366 | 1130.4 | 0.00798536 |
| 1413.25 | 0.990 | 282.65 | 0.99802223 | 1130.6 | 0.00791109 |
| 1413.5 | 0.990 | 282.70 | 0.99804079 | 1130.8 | 0.00783683 |
| 1413.75 | 0.990 | 282.75 | 0.99805936 | 1131.0 | 0.00776258 |
| 1414 | 0.990 | 282.80 | 0.99807792 | 1131.2 | 0.00768833 |
| 1414.25 | 0.990 | 282.85 | 0.99809648 | 1131.4 | 0.00761409 |
| 1414.5 | 0.991 | 282.90 | 0.99811504 | 1131.6 | 0.00753985 |
| 1414.75 | 0.991 | 282.95 | 0.99813359 | 1131.8 | 0.00746562 |
| 1415 | 0.991 | 283.00 | 0.99815215 | 1132.0 | 0.00739140 |
| 1415.25 | 0.991 | 283.05 | 0.99817070 | 1132.2 | 0.00731719 |
| 1415.5 | 0.991 | 283.10 | 0.99818926 | 1132.4 | 0.00724297 |
| 1415.75 | 0.991 | 283.15 | 0.99820781 | 1132.6 | 0.00716877 |
| 1416 | 0.991 | 283.20 | 0.99822636 | 1132.8 | 0.00709457 |
| 1416.25 | 0.991 | 283.25 | 0.99824490 | 1133.0 | 0.00702038 |
| 1416.5 | 0.991 | 283.30 | 0.99826345 | 1133.2 | 0.00694620 |
| 1416.75 | 0.991 | 283.35 | 0.99828200 | 1133.4 | 0.00687202 |
| 1417 | 0.992 | 283.40 | 0.99830054 | 1133.6 | 0.00679784 |
| 1417.25 | 0.992 | 283.45 | 0.99831908 | 1133.8 | 0.00672368 |
| 1417.5 | 0.992 | 283.50 | 0.99833762 | 1134.0 | 0.00664951 |
| 1417.75 | 0.992 | 283.55 | 0.99835616 | 1134.2 | 0.00657536 |
| 1418 | 0.992 | 283.60 | 0.99837470 | 1134.4 | 0.00650121 |


| 1418.25 | 0.992 | 283.65 | 0.99839323 | 1134.6 | 0.00642707 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1418.5 | 0.992 | 283.70 | 0.99841177 | 1134.8 | 0.00635293 |
| 1418.75 | 0.992 | 283.75 | 0.99843030 | 1135.0 | 0.00627880 |
| 1419 | 0.992 | 283.80 | 0.99844883 | 1135.2 | 0.00620468 |
| 1419.25 | 0.992 | 283.85 | 0.99846736 | 1135.4 | 0.00613056 |
| 1419.5 | 0.992 | 283.90 | 0.99848589 | 1135.6 | 0.00605645 |
| 1419.75 | 0.993 | 283.95 | 0.99850441 | 1135.8 | 0.00598234 |
| 1420 | 0.993 | 284.00 | 0.99852294 | 1136.0 | 0.00590824 |
| 1420.25 | 0.993 | 284.05 | 0.99854146 | 1136.2 | 0.00583415 |
| 1420.5 | 0.993 | 284.10 | 0.99855998 | 1136.4 | 0.00576006 |
| 1420.75 | 0.993 | 284.15 | 0.99857851 | 1136.6 | 0.00568598 |
| 1421 | 0.993 | 284.20 | 0.99859702 | 1136.8 | 0.00561190 |
| 1421.25 | 0.993 | 284.25 | 0.99861554 | 1137.0 | 0.00553784 |
| 1421.5 | 0.993 | 284.30 | 0.99863406 | 1137.2 | 0.00546377 |
| 1421.75 | 0.993 | 284.35 | 0.99865257 | 1137.4 | 0.00538972 |
| 1422 | 0.993 | 284.40 | 0.99867108 | 1137.6 | 0.00531566 |
| 1422.25 | 0.993 | 284.45 | 0.99868959 | 1137.8 | 0.00524162 |
| 1422.5 | 0.994 | 284.50 | 0.99870810 | 1138.0 | 0.00516758 |
| 1422.75 | 0.994 | 284.55 | 0.99872661 | 1138.2 | 0.00509355 |
| 1423 | 0.994 | 284.60 | 0.99874512 | 1138.4 | 0.00501952 |
| 1423.25 | 0.994 | 284.65 | 0.99876362 | 1138.6 | 0.00494550 |
| 1423.5 | 0.994 | 284.70 | 0.99878213 | 1138.8 | 0.00487149 |
| 1423.75 | 0.994 | 284.75 | 0.99880063 | 1139.0 | 0.00479748 |
| 1424 | 0.994 | 284.80 | 0.99881913 | 1139.2 | 0.00472348 |
| 1424.25 | 0.994 | 284.85 | 0.99883763 | 1139.4 | 0.00464948 |
| 1424.5 | 0.994 | 284.90 | 0.99885613 | 1139.6 | 0.00457549 |
| 1424.75 | 0.994 | 284.95 | 0.99887462 | 1139.8 | 0.00450151 |
| 1425 | 0.994 | 285.00 | 0.99889312 | 1140.0 | 0.00442753 |
| 1425.25 | 0.995 | 285.05 | 0.99891161 | 1140.2 | 0.00435356 |
| 1425.5 | 0.995 | 285.10 | 0.99893010 | 1140.4 | 0.00427960 |
| 1425.75 | 0.995 | 285.15 | 0.99894859 | 1140.6 | 0.00420564 |
| 1426 | 0.995 | 285.20 | 0.99896708 | 1140.8 | 0.00413169 |
| 1426.25 | 0.995 | 285.25 | 0.99898557 | 1141.0 | 0.00405774 |
| 1426.5 | 0.995 | 285.30 | 0.99900405 | 1141.2 | 0.00398380 |
| 1426.75 | 0.995 | 285.35 | 0.99902253 | 1141.4 | 0.00390986 |
| 1427 | 0.995 | 285.40 | 0.99904102 | 1141.6 | 0.00383593 |
| 1427.25 | 0.995 | 285.45 | 0.99905950 | 1141.8 | 0.00376201 |
| 1427.5 | 0.995 | 285.50 | 0.99907798 | 1142.0 | 0.00368810 |
| 1427.75 | 0.995 | 285.55 | 0.99909645 | 1142.2 | 0.00361419 |
| 1428 | 0.996 | 285.60 | 0.99911493 | 1142.4 | 0.00354028 |
| 1428.25 | 0.996 | 285.65 | 0.99913340 | 1142.6 | 0.00346638 |
| 1428.5 | 0.996 | 285.70 | 0.99915188 | 1142.8 | 0.00339249 |
| 1428.75 | 0.996 | 285.75 | 0.99917035 | 1143.0 | 0.00331860 |
| 1429 | 0.996 | 285.80 | 0.99918882 | 1143.2 | 0.00324473 |
| 1429.25 | 0.996 | 285.85 | 0.99920729 | 1143.4 | 0.00317085 |
| 1429.5 | 0.996 | 285.90 | 0.99922575 | 1143.6 | 0.00309698 |
| 1429.75 | 0.996 | 285.95 | 0.99924422 | 1143.8 | 0.00302312 |
| 1430 | 0.996 | 286.00 | 0.99926268 | 1144.0 | 0.00294927 |
| 1430.25 | 0.996 | 286.05 | 0.99928115 | 1144.2 | 0.00287542 |
| 1430.5 | 0.996 | 286.10 | 0.99929961 | 1144.4 | 0.00280157 |
| 1430.75 | 0.997 | 286.15 | 0.99931807 | 1144.6 | 0.00272774 |
| 1431 | 0.997 | 286.20 | 0.99933652 | 1144.8 | 0.00265390 |
| 1431.25 | 0.997 | 286.25 | 0.99935498 | 1145.0 | 0.00258008 |
| 1431.5 | 0.997 | 286.30 | 0.99937344 | 1145.2 | 0.00250626 |
| 1431.75 | 0.997 | 286.35 | 0.99939189 | 1145.4 | 0.00243245 |
| 1432 | 0.997 | 286.40 | 0.99941034 | 1145.6 | 0.00235864 |
| 1432.25 | 0.997 | 286.45 | 0.99942879 | 1145.8 | 0.00228484 |
| 1432.5 | 0.997 | 286.50 | 0.99944724 | 1146.0 | 0.00221104 |
| 1432.75 | 0.997 | 286.55 | 0.99946569 | 1146.2 | 0.00213725 |
| 1433 | 0.997 | 286.60 | 0.99948413 | 1146.4 | 0.00206347 |
| 1433.25 | 0.998 | 286.65 | 0.99950258 | 1146.6 | 0.00198969 |
| 1433.5 | 0.998 | 286.70 | 0.99952102 | 1146.8 | 0.00191592 |
| 1433.75 | 0.998 | 286.75 | 0.99953946 | 1147.0 | 0.00184216 |
| 1434 | 0.998 | 286.80 | 0.99955790 | 1147.2 | 0.00176840 |
| 1434.25 | 0.998 | 286.85 | 0.99957634 | 1147.4 | 0.00169465 |
| 1434.5 | 0.998 | 286.90 | 0.99959477 | 1147.6 | 0.00162090 |
| 1434.75 | 0.998 | 286.95 | 0.99961321 | 1147.8 | 0.00154716 |
| 1435 | 0.998 | 287.00 | 0.99963164 | 1148.0 | 0.00147343 |
| 1435.25 | 0.998 | 287.05 | 0.99965008 | 1148.2 | 0.00139970 |
| 1435.5 | 0.998 | 287.10 | 0.99966851 | 1148.4 | 0.00132597 |
| 1435.75 | 0.998 | 287.15 | 0.99968694 | 1148.6 | 0.00125226 |


| 1436 | 0.999 | 287.20 | 0.99970536 | 1148.8 | 0.00117855 |
| ---: | :--- | :--- | :--- | :--- | :--- |
| 1436.25 | 0.999 | 287.25 | 0.99972379 | 1149.0 | 0.00110484 |
| 1436.5 | 0.999 | 287.30 | 0.99974221 | 1149.2 | 0.00103114 |
| 1436.75 | 0.999 | 287.35 | 0.99976064 | 1149.4 | 0.00095745 |
| 1437 | 0.999 | 287.40 | 0.99977906 | 1149.6 | 0.00088377 |
| 1437.25 | 0.999 | 287.45 | 0.99979748 | 1149.8 | 0.00081009 |
| 1437.5 | 0.999 | 287.50 | 0.99981590 | 1150.0 | 0.00073641 |
| 1437.75 | 0.999 | 287.55 | 0.99983431 | 1150.2 | 0.00066274 |
| 1438 | 0.999 | 287.60 | 0.99985273 | 1150.4 | 0.00058908 |
| 1438.25 | 0.999 | 287.65 | 0.99987114 | 1150.6 | 0.00051543 |
| 1438.5 | 0.999 | 287.70 | 0.99988956 | 1150.8 | 0.00044177 |
| 1438.75 | 1.000 | 287.75 | 0.99990797 | 1151.0 | 0.00036813 |
| 1439 | 1.000 | 287.80 | 0.99992638 | 1151.2 | 0.00029449 |
| 1439.25 | 1.000 | 287.85 | 0.99994478 | 1151.4 | 0.00022086 |
| 1439.5 | 1.000 | 287.90 | 0.99996319 | 1151.6 | 0.00014723 |
| 1439.75 | 1.000 | 287.95 | 0.99998160 | 1151.8 | 0.00007361 |
| 1440 | 1.000 | 288.00 | 1.00000000 | 1152.0 | 0.00000000 |

## Rainfall total (in): 0 (inten




























| 0.015 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 0.015 0.015 |  |  |  |  |
| 0.015 | 0.10 | 0.37 | 0.03 | 10.13 |
| 0.015 |  |  |  |  |
| 0.015 |  |  |  |  |  |  |  |
| ${ }^{0.015}$ |  |  |  |  |
|  |  |  |  |  |  |  |  |
| 0.015 | 0.10 | 0.37 | 0.03 | 10.17 |
| 0.015 |  |  |  |  |
| 0.0160.016 |  |  |  |  |
|  |  |  |  |  |  |  |  |
| ${ }^{0.016}$ |  |  |  |  |
| $\begin{array}{lllll}0.016 & 0.10 & 0.37 & 0.03 & 10.21 \\ 0.016\end{array}$ |  |  |  |  |
|  |  |  |  |  |  |  |  |
| $\begin{aligned} & 0.016 \\ & 0.016 \end{aligned}$ |  |  |  |  |
|  |  |  |  |  |  |  |  |
| ${ }_{0}^{0.016}$ |  |  |  |  |
| ${ }^{0.016}$ | 0.10 | 0.37 | 0.03 | 10.26 |
| 0.016 |  |  |  |  |
| $\begin{aligned} & 0.016 \\ & 0.016 \end{aligned}$ |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |
| 0.016 |  |  |  |  |
|  |  |  |  |  |  |  |  |
| $\begin{aligned} & 0.016 \\ & 0.016 \end{aligned}$ |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |
| ${ }^{0.016}$ | 0.10 | 0.37 | 0.03 | 10.34 |
| 0.016 |  |  |  |  |
| $\begin{aligned} & 0.016 \\ & 0.016 \end{aligned}$ |  |  |  |  |
|  |  |  |  |  |  |  |  |
| 0.016 |  |  |  |  |
| $\begin{array}{lllll}0.016 & 0.10 & 0.37 & 0.03 & 10.39\end{array}$ |  |  |  |  |
| 0.016 |  |  |  |  |
| $0.016$$0.016$ |  |  |  |  |
|  |  |  |  |  |  |  |  |
| $\begin{array}{lllll}0.016 & 0.0\end{array}$ |  |  |  |  |
|  |  |  |  |  |  |  |  |
| $\begin{aligned} & 0.016 \\ & 0.016 \end{aligned}$ |  |  |  |  |
|  |  |  |  |  |  |  |  |
| $\begin{aligned} & 0.016 \\ & 0.016 \end{aligned}$ |  |  |  |  |
| $\begin{array}{lllll}0.0016 & 0.10 & 0.37 & 0.04 & 10.48 \\ 0.016\end{array}$ |  |  |  |  |
|  |  |  |  |  |  |  |  |
| 0.0160.016 |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |
| 0.016 | 0.10 | 0.37 | 0.0 | 10.53 |
| 0.016 |  |  |  |  |
| 0.016 <br> 0.016 |  |  |  |  |
|  |  |  |  |  |  |  |  |
| $\begin{aligned} & 0.016 \\ & 0.016 \end{aligned}$ |  |  |  |  |
| 0.016 | 0.10 | 0.37 | 0.04 | 10.58 |
| 0.016 |  |  |  |  |
|  |  |  |  |  |
| ${ }^{0.016}$ |  |  |  |  |
| 0.016 |  |  |  |  |
| ${ }_{0.016}^{0.00}$ |  |  |  |  |
|  |  |  |  |  |  |  |  |
| 0.016 |  |  |  |  |
| ${ }^{0.016}$ |  |  |  |  |
|  |  |  |  |  |  |  |  |
| 0.016 | 0.10 | 0.37 | 0.04 | 10.67 |
| 0.016 |  |  |  |  |
| 0.016 |  |  |  |  |
| ${ }^{0.016}$ |  |  |  |  |
|  |  |  |  |  |  |  |  |
| 0.016 | 0.10 | 0.37 | 0.04 | 10.72 |
| 0.016 |  |  |  |  |
| 0.016 |  |  |  |  |
| ${ }_{0}^{0.016}$ |  |  |  |  |
| 0.016 |  |  |  |  |
| ${ }^{0.016}$ | 0.10 | 0.37 | 0.04 | 10.77 |
| 0.016 |  |  |  |  |
| 0.016 |  |  |  |  |
| ${ }^{0.016}$ |  |  |  |  |
| ${ }^{0.016}$ |  |  |  |  |
| 0.016 |  |  |  |  |
| 0.017 |  |  |  |  |
| 0.017 |  |  |  |  |
| 0.017 |  |  |  |  |
| $\begin{array}{lllll}0.017 & 0.10 & 0.37 & 0.04 & 10.88\end{array}$ |  |  |  |  |
| 0.0170.017 |  |  |  |  |
|  |  |  |  |  |  |  |  |
| 0.017 |  |  |  |  |
| 0.017 | 0.10 | 0.37 | 0.04 | 10.93 |
| $\begin{array}{lllll}0.017 & 0.10 & 0.37 & 0.04 & 10.93\end{array}$ |  |  |  |  |
| 0.017 |  |  |  |  |
| ${ }^{0.017}$ |  |  |  |  |
| 0.017 0.017 | 0.10 | 0.37 | 0.04 | 10.98 |
| $\begin{array}{lllll}0.017 & 0.10 & 0.37 & 0.04 & 10.98\end{array}$ |  |  |  |  |
| 0.017 |  |  |  |  |
| 0.017 |  |  |  |  |
|  |  |  |  |  |  |  |  |
| 0.017 0.10 0.37 0.04 11.04 <br> .017     |  |  |  |  |
|  |  |  |  |  |  |  |  |
| . 017 |  |  |  |  |
|  |  |  |  |  |  |  |  |
| . 01017 |  |  |  |  |
| 0.017 0.00 |  |  |  |  |
|  |  |  |  |  |  |  |  |
| . 01017 |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |
| $\begin{array}{lllll}0.017 & 0.10 & 0.37 & 0.04 & \end{array}$ |  |  |  |  |
|  |  |  |  |  |  |  |  |
| . 017 |  |  |  |  |
|  |  |  |  |  |  |  |  |
| 0.017 |  |  |  |  |
| 0.017 | 0.10 | 0.37 | 0.04 | 11.20 |
| 0.01 0.01 | 017 |  |  |  |
| . 01017 |  |  |  |  |
| 0.017 |  |  |  |  |
|  |  |  |  |  |
| 0.017 0.017 | 0.10 | 0.37 | 0.04 | 11.26 |
| ${ }^{0.017}$ |  |  |  |  |
|  |  |  |  |  |





| 0.017 |  | 0.37 | 0.04 | 11.32 |
| :---: | :---: | :---: | :---: | :---: |
| 0.017 | 0.10 |  |  |  |
| 0.0170.017 |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| 0.017 |  |  |  |  |
| 0.017 |  |  |  |  |
| 0.017 | 0.10 | 0.37 | 0.04 | 11.38 |
| 0.017 |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |
| 0.017 | 0.10 | 0.37 | 0.04 | 11.44 |
| 0.017 |  |  |  |  |
| $0.017$ |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |
| 0.018 | 0.10 | 0.37 | 0.04 | 11.50 |
| 0.018 |  |  |  |  |
| $\begin{aligned} & 0.018 \\ & 0.018 \end{aligned}$ |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |
| 0.018 | 0.10 | 0.37 | 0.04 | 11.57 |
| 0.018 |  |  |  |  |
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# Appendix D Geotechnical Study Report, East Antelope Valley Animal Shelter" ${ }^{15}$ by Converse Consultants (April 9, 2012) 

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## Converse Consultants

# GEOTECHNICAL STUDY REPORT 

 East Antelope Valley Animal ShelterPalmdale, California

April 19, 2012

## PREPARED FOR

Los Angeles County Department of Public Works
900 South Fremont Avenue
Alhambra, CA 91803

## Converse Consultants

Geotechnical Engineering, Environmental \& Groundwater Science, Inspection \& Testing Services

April 19, 2012
Mr. Jason Kim
Capital Projects Manager
Los Angeles County Department of Public Works
900 South Fremont Avenue
Alhambra, CA 91803

## Subject: GEOTECHNICAL STUDY REPORT East Antelope Valley Animal Shelter Palmdale, California Converse Project No. 12-31-145-01

Dear Mr. Kim:
Converse Consultants (Converse) is pleased to present this Geotechnical Study Report for the proposed new East Antelope Valley Animal Shelter in Palmdale, California.

The purpose of the study was to generate a report for geotechnical design parameters, percolation test results and pavement design for the construction of a new animal shelter and associated parking lots in Palmdale, California. The proposed building is likely to be one-story and support with slab on grade and shallow footings. No basement is planned at this time.

Our services were performed in accordance with our revised proposal dated March 1, 2012.
Based on our field exploration, laboratory testing, geologic evaluation and geotechnical analysis, the site is suitable from a geotechnical standpoint for the proposed project, provided our conclusions and recommendations are implemented during design and construction.

We appreciate the opportunity to be of continued service to the Los Angeles County Department of Public Works. If you should have any questions, please do not hesitate to contact us at (626) 930-1200.

## CONVERSE CONSULTANTS



William H. Chu, P.E., G.E.
Senior Vice President/Principal Engineer
Dist: 6/Addressee
MNR/GDS/SCL/NHC/amm

## PROFESSIONAL CERTIFICATION

This report for the proposed construction of a new animal shelter and associated parking lots located at 38532, 38560, 38600 and 38624 Sierra Highway in Palmdale, California has been prepared by the staff of Converse under the professional supervision of the individuals whose seals and signatures appear hereon.

The findings, recommendations, specifications or professional opinions contained in this report were prepared in accordance with generally accepted professional engineering and engineering geologic principles and practice in this area of Southern California. There is no warranty, either expressed or implied.

In the event that changes to the property occur, or additionai, relevant information about the property is brought to our attention, the conclusions contained in this report may not be valid uniess these changes and additional relevant information are reviewed and the recommendations of this report are modified or verified in writing.


Sean C. Lin, P.E., G.E.
Senior Engineer


Geoffrey D. Stokes, P.G., C.E.G. Senior Geologist


William H. Chu, P.E., G.E.
Principal Engineer, Senior Vice President


## EXECUTIVE SUMMARY

The following is the summary of our geotechnical study, findings, conclusions, and recommendations, as presented in the body of this report. Please refer to the appropriate sections of the report for complete conclusions and recommendations. In the event of a conflict between this summary and the report, or an omission in the summary, the report shall prevail.

- The project site for East Antelope Valley Animal Shelter is collectively located at 38532, 38560, 38600 and 38624 Sierra Highway in Palmdale, California. The project site area is relatively flat, with a gentle slope in grade towards the north. The site is paved with asphalt on the southern two-thirds, with vacant land on the northern one-third of the site.
- The proposed animal shelter structure will be situated within the central portion of the site, with new parking pavement along the north and south sides of the facility. The building will likely be one-story and supported with slab on grade and shallow footings. No basement levels are planned at this time.
- Seven (7) exploratory borings (BH-1 through BH-7) were drilled within the project site on March 22, 2012. The borings were advanced using a truck mounted 8 -inch diameter hollow stem auger drill rig to depths ranging from 16.5 to 51.5 feet below the existing ground surface (bgs). Two of the borings ( $\mathrm{BH}-1$ and $\mathrm{BH}-2$ ) were utilized to perform percolation tests.
- The site soils consisted of fills and alluvial deposits to the maximum explored depth of 51.5 feet below existing ground surface (bgs). Fills up to a maximum observed depth of 3 feet were encountered in the borings. The fill material was probably placed during original site grading. Deeper artificial fill may exist at the site. The fill encountered consist primarily of silty sand and clayey silt. The alluvial deposits below the fill primarily consist of silty sands and sand with gravels.
- Groundwater was not encountered during drilling to the maximum exploratory depth of 51.5 feet. Based upon regional groundwater data included in the Seismic Hazard Evaluation Report for the Palmdale 7.5-minute Quadrangle (2003), historic high groundwater levels for the subject site are reportedly greater than 40 feet below the ground surface.
- The site is not located within a mapped Seismic Hazard Zone for liquefaction potential. Site specific exploration did not encounter groundwater to a depth of 51.5 feet bgs. Based on the results of our subsurface exploration, including the absence of groundwater within 50 feet, and our experience on similar projects we anticipate liquefaction potential to be very low and seismically-induced settlement to be negligible.
- Based on the percolation test results, the site soils are primarily silty sand with moderate infiltration rates. These soils are considered suitable for infiltration drainage systems. The project Civil Engineer should review the raw data of percolation test to determine specific soil layers and percolation rates for design of the proposed infiltration system.
- The results of Phase I and Phase II Environmental Site Assessments by Converse (2011 and 2012) indicate previous improvements at the site had basement levels. Areas of former basements will contain undocumented fill soils.
- Remedial grading will be needed for support of new buildings and new hardscape improvements. Such grading should include over-excavation and re-compaction to mitigate disturbed native soils from site demolition, undocumented fill soils and to provide a relatively uniform soil condition in the area of planned construction.
- The proposed structures may use conventional foundation systems (spread footings and isolated pads) with slab-on-grade, supported on compacted fill.
- Based on the soil corrosivity test results, the on-site soils are not considered to be corrosive to buried ferrous metals and concrete.
- Laboratory testing indicates the site soils have a low expansion potential. Mitigation measures for expansive soils are needed for compacted fill derived from site soils.

Results of our study indicate that the site is suitable from a geotechnical standpoint for the proposed development, provided that the recommendations contained in this report are incorporated into the design and construction of the project.

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### 1.0 INTRODUCTION

This report contains the findings and recommendations of our geotechnical study performed for the proposed construction of a new animal shelter and associated parking pavement at adjacent site addresses 38532, 38560, 38600 and 38624 Sierra Highway in Palmdale as shown on Drawing No. 1, Site Location Map. The purpose of this work was to evaluate the subsurface soil conditions and provide geotechnical recommendations, percolation test results and pavement design recommendations for the design and construction of the proposed project, including current standard of practice seismic and geotechnical engineering interpretations. The purpose of the percolation test results is to provide the percolation rate for design of an infiltration system at the project site.

This report for geologic and geotechnical design parameters for the project described herein and is intended for use solely by the Los Angeles County Department of Public Works and their design team. This report should not be used as a bidding document but may be made available to the potential contractors for information on factual data only. For bidding purposes, the contractors should be responsible for making their own interpretation of the data contained in this report.

### 2.0 SITE AND PROJECT DESCRIPTION

The project site for East Antelope Valley Animal Shelter is collectively located at 38532, 38560, 38600 and 38624 Sierra Highway in Palmdale, California. The site is bordered by Sierra Highway to the west, a parking lot to the south, a residential neighborhood to the east, and a public facility to the north. The project site area is relatively flat, with a gentle slope in grade towards the north. Existing conditions include asphalt pavement within the southern two-thirds of the site and undeveloped land within the northern onethird of the site.

Review of historic aerial photos and topographic maps indicate several large buildings were present on the southern portion of the site between 1959 to at least 1981. The results of a Phase I Environmental Site Assessment (Converse, 2011) and Phase II Environmental Site Assessment (Converse, 2012) indicate that previous improvements at the site had basement levels; areas of former basements anticipated below the area of the planned parking pavement south of the animal shelter will contain undocumented fill.

Review of the conceptual site diagram shows that the proposed animal shelter will consist of one-story structures located within the central portion of the site. The buildings will likely be supported with slab on grade and shallow footings. No basement levels are planned at this time. The northern one-third of the site will be left as undeveloped land for future expansion, and majority of the east side will be converted to an exercise yard. Two new


## SITE LOCATION MAP


parking lots will also be constructed along the north and south portions of animal shelter buildings. The planned site improvements are illustrated on the base map provided for Drawing No. 2, Site Plan and Boring Locations.

### 3.0 SCOPE OF WORK

The scope of our work included a site reconnaissance, subsurface exploration with soil sampling and percolation testing, laboratory testing, engineering analysis, and preparation of this report.

### 3.1 Site Reconnaissance

A site reconnaissance was performed by a member of the Converse staff on March 12, 2012. The purpose of the site reconnaissance was to observe surface conditions and to mark exploratory boring locations. Underground Service Alert (USA) of Southern California was notified of our proposed drilling locations 48 hours prior to initiation of the subsurface field work. The reference ticket number from USA is A20731244.

### 3.2 Subsurface Exploration and Percolation Testing

Seven (7) exploratory borings (BH-1 through $\mathrm{BH}-7$ ) were drilled within the project site on March 22, 2012. The borings were advanced using a truck mounted 8-inch diameter hollow stem auger drill rig to depths ranging from 16.5 to 51.5 feet below the existing ground surface (bgs). Two of the borings ( $\mathrm{BH}-1$ and $\mathrm{BH}-2$ ) were utilized to perform percolation tests. Each boring was visually logged by an engineer and sampled at regular intervals and at changes in subsurface soils. Both relatively undisturbed and bulk soil samples were obtained for laboratory testing. California Modified Sampler (Ring samples), Standard Penetration Test samples, and bulk soil samples were obtained for laboratory testing. Standard Penetration Tests (SPTs) were performed in selected borings at selected intervals using a standard (1.4 inches inside diameter and 2.0 inches outside diameter) split-barrel sampler. The bore holes were backfilled and compacted with soil cuttings by reverse spinning of the auger following the completion of drilling. Borings within paved areas were patched with asphalt cold-patch, with the patch thickness matching the surrounding pavement section.

The approximate locations of the exploratory borings are shown in Drawing No. 2, Site Plan and Boring Locations. For a description of the field exploration and sampling program see Appendix A, Field Exploration.

Borings $\mathrm{BH}-1$ and $\mathrm{BH}-2$ were used for percolation testing prior to backfill. Percolation test procedures and test results are further discussed in report section 7.0, Percolation Testing and Appendix C.

### 3.3 Laboratory Testing

Representative samples of the site soils were tested in the laboratory to aid in the classification and to evaluate relevant engineering properties. The tests performed included:

- In situ moisture contents and dry densities (ASTM Standard D2216)
- Expansion (ASTM D4829)
- Soil corrosivity tests (Caltrans 643, 422, 417 and 532)
- Passing Sieve No. 200 (ASTM D1140)
- R-Value (ASTM D2844)
- Maximum dry density and optimum-moisture content relationship (ASTM Standard D1557)
- Direct shear (ASTM Standard D3080)
- Consolidation (ASTM Standard D2435)


### 3.4 Analyses and Report

Data obtained from the exploratory fieldwork, percolation testing and laboratory-testing program were analyzed and evaluated with respect to the planned construction. This report was prepared to provide the findings, conclusions and recommendations developed during our study and evaluation.

### 4.0 GEOLOGIC CONDITIONS

### 4.1 Regional Geologic Setting

The project site is located within the Mojave Desert geomorphic province of Southern California; a broad interior region of mountains and intervening expanses of desert plains bound to the north by the Garlock fault and to the south by the San Andreas fault zone. The convergence of the Garlock and San Andreas faults form a wedged shaped alluvial plain within the western portion of the province, with which the subject site is located. Alluvial soils in the area of the subject site are derived from the elevated terrain to the south and generally consist of unconsolidated sediments of generally Holocene age (last 11,000 years). Drawing No. 3, Geologic Map of Site Vicinity, has been prepared to show the location of the project site with respect to local geologic exposures. The base map for Drawing No. 3 is from the Seismic Hazard Evaluation Report for the Palmdale 7.5-minute Quadrangle (2003). Map symbol Q6m corresponds to medium grained sandy alluvial sediments.


## GEOLOGIC MAP OF SITE VICINTY

### 4.2 Subsurface Profile

The site soils consisted of fills and alluvial deposits to the maximum explored depth of 51.5 feet below existing ground surface (bgs). Fills up to a maximum observed depth of 3 feet were encountered in the borings. The fill material was probably placed during original site grading. Review of historic aerial photos and topographic maps indicate several large buildings were present on the site between as early as 1959. Deeper artificial fill may exist at the site. The fill encountered consist primarily of silty sand and clayey silt. The alluvial deposits below the fill primarily consist of silty sands and sand with gravels.

For a detailed description of the materials encountered during our exploration, see Appendix A, Field Exploration.

### 4.3 Groundwater

During our exploration, groundwater was not encountered to the maximum exploratory depth of 51.5 feet. Based upon regional groundwater data compiled by the Seismic Hazard Evaluation Report for the Palmdale 7.5-minute Quadrangle (2003), historic high groundwater levels for the subject site are reportedly greater than 40 feet below the ground surface (see Drawing No. 4, Groundwater Contour Map).

In general, groundwater levels fluctuate with the seasons and local zones of perched groundwater may be present within the near-surface soils due to local conditions or during rainy seasons. Groundwater conditions below any given site vary depending on numerous factors including seasonal rainfall, local irrigation, and groundwater pumping, among other factors. The regional groundwater table is not expected to be encountered during the planned construction, and confining clay layers were not observed within the zone of construction. Although conditions for isolated areas of perched groundwater were not encountered during our subsurface work, the possibility cannot be completely precluded.

### 4.4 Subsurface Variations

Based on results of the subsurface exploration and our experience, some variations in the continuity and nature of subsurface conditions within the project site should be anticipated. Because of the uncertainties involved in the nature and depositional characteristics of earth material, care should be exercised in interpolating or extrapolating subsurface conditions between or beyond the boring locations. If, during construction, subsurface conditions different from those presented in this report are encountered, this office should be notified immediately so that recommendations can be modified, if necessary.


GROUNDWATER CONTOUR MAP

### 5.0 FAULTING AND SEISMIC HAZARDS

The subject site is situated within a seismically active region. As is the case for most areas of Southern California, ground-shaking resulting from earthquakes associated with nearby and more distant faults may occur at the project site. During the life of the project, seismic activity associated with active faults can be expected to generate moderate to strong ground shaking at the site.

### 5.1 Faulting

The project site is not located within a currently designated State of California Earthquake Fault Zone for surface fault rupture. There are no known active faults trending across the site. The closest known capable fault to the project site with mappable surface projection is the San Andreas Fault, located approximately 1 mile to the south.

### 5.2 Seismic Hazards

In addition to surface fault rupture, strong ground shaking from earthquakes can also produce other side effects that include soil liquefaction, lateral spreading, seismically induced settlement, ground lurching, landsliding, earthquake-induced flooding, seiches, and tsunamis. Drawing No. 5, Seismic Hazard Zones Map, has been prepared to show the mapped location of potential liquefaction and earthquake-induced landslide areas near the project site. The State of California Seismic Hazard Zone Map for the Palmdale Quadrangle (October 17, 2003) shows the project site is not located within an area of potential liquefaction. The project site is also not shown with any earthquakeinduced landslide areas due to the relatively flat condition of the site topography.

Results of a site-specific evaluation for each type of possible seismic hazard are explained below:

### 5.2.1 Surface Fault Rupture

The site is not located within a currently designated State of California Earthquake Fault Zone. Based on a review of existing geologic information, no known active faults cross or project toward the site. The potential for surface rupture resulting from the movement of the nearby major faults is considered remote.

### 5.2.2 Liquefaction and Seismically-Induced Settlement

Liquefaction is the sudden decrease in the strength of cohesionless soils due to dynamic or cyclic shaking. Saturated soils behave temporarily as a viscous fluid (liquefaction) and, consequently, lose their capacity to support the structures


SEISMIC HAZARD ZONES MAP
founded on them. The potential for liquefaction decreases with increasing clay and gravel content, but increases as the ground acceleration and duration of shaking increase. Liquefaction potential has been found to be the greatest where the groundwater level and loose sands occur within 50 feet of the ground surface.

The site is not located within a mapped Seismic Hazard Zone for liquefaction potential. Site specific exploration did not encounter groundwater to a depth of 51.5 feet bgs. Based on the results of our subsurface exploration, including the absence of groundwater within 50 feet, and our experience on similar projects we anticipate liquefaction potential to be very low and seismically-induced settlement to be negligible.

### 5.2.3 Lateral Spreading

Seismically induced lateral spreading involves primarily lateral movement of earth materials along embankments due to ground shaking. It differs from slope failure in that deep seated movement does not occur due to the relatively smaller gradient of the initial ground surface. Lateral spreading is demonstrated by near-vertical cracks with predominantly horizontal movement of the soil mass involved. The topography at the project site and in the immediate vicinity of the site is relatively flat, with no nearby slopes or embankments. Under these circumstances, the potential for lateral spreading at the subject site is considered negligible.

### 5.2.4 Seismically-Induced Slope Instability

Seismically induced landslides and other slope failures are common occurrences during or soon after earthquakes. The project site is essentially flat. In the absence of significant ground slopes, the potential for seismically induced landslides to affect the proposed site is considered to be nil.

### 5.2.5 Earthquake-Induced Flooding

This is flooding caused by failure of dams or other water-retaining structures as a result of earthquakes. The site is located within an area that has a potential $0.2 \%$ annual flood chance per FEMA (2008), but is not located within the inundation zone for Palmdale Lake reservoir per the Los Angeles County General Plan. The potential of earthquake induced flooding of the subject site is considered to be minimal.

### 5.2.6 Seiches

Seiches are large waves generated in enclosed bodies of water in response to ground shaking. The Lake Palmdale reservoir is approximately 2.5 miles away and is the closest enclosed body of water to the site, but is not considered to pose a hazard because the site is not located within the inundation zone per the Los Angeles County General Plan.

### 6.0 SEISMIC ANALYSIS

The project site is classified as Site Class D, based on the soil classification and field Standard Penetration Tests. Seismic design parameters based on CBC 2010, calculated using the site coordinates by Ground Motion Parameter Calculator developed by the United States Geological Survey are provided below.

Table No. 1, CBC Seismic Parameters

| Seismic Parameters |  |
| :--- | :---: |
| Latitude | N 34.5827 |
| Longitude | W 118.1160 |
| Site Class | D |
| Mapped Short period (0.2-sec) Spectral Response Acceleration, $\mathrm{S}_{\mathrm{S}}$ | 2.000 g |
| Mapped 1-second Spectral Response Acceleration, $\mathrm{S}_{1}$ | 1.033 g |
| Site Coefficient (from Table 1613.5.3(1)), Fa | 1.0 |
| Site Coefficient (from Table 1613.5.3(2)), Fv | 1.5 |
| MCE 0.2-sec period Spectral Response Acceleration, $\mathrm{S}_{\mathrm{MS}}$ | 2.000 g |
| MCE 1-second period Spectral Response Acceleration, $\mathrm{S}_{\mathrm{M} 1}$ | 1.549 g |
| Design Spectral Response Acceleration for short period, $\mathrm{S}_{\mathrm{DS}}$ | 1.333 g |
| Design Spectral Response Acceleration for 1-sec. period, $\mathrm{S}_{\mathrm{D} 1}$ | 1.033 g |
| Seismic Design Category | D |

### 7.0 PERCOLATION TESTS

Percolation testing was performed utilizing exploratory Borings $\mathrm{BH}-1$ and $\mathrm{BH}-2$ on March 22, 2011. Each boring was cased using two-inch diameter perforated casing surrounded by gravel. Water was added to the test hole until the water level was at the ground surface and allowed to presoak for at least 2 hours. After pre-soak, water was added to the test hole until the water level was near the ground surface. Tests were performed using the falling head test method in accordance with Los Angeles County "Low Impact Development (LID) Best Management Practice (BMP) Guideline for Design, Investigation, and Reporting" dated January 2011. The water level was measured to the nearest tenth of a foot, and converted to inches in the calculation. The
results of the percolation tests are tabulated below and in Appendix C, Percolation Testing.

Table No. 2, Percolation Test Results

| Boring <br> No. | Depth of Boring <br> (feet) | Predominant Soil Types (USCS) | Average Percolation Rate <br> (inches/hour) |
| :---: | :---: | :---: | :---: |
| BH-1 | 31.5 | Sand (SP), Sand with Silt (SP-SM) | 6.02 |
| BH-2 | 31.5 | Silty Sand (SM), Clayey Sand (SC) | 2.74 |

Based on the percolation test results, the site soils are primarily sandy with various amount of fines (silt and clay) content. Sandy soils with fines content (BH-2) exhibit relatively moderate infiltration rates, and sandy soils with less fines content (BH-1) provided test results with relatively high infiltration. The sandy site soils are considered suitable for infiltration drainage systems. The project Civil Engineer should review the raw data of percolation test to determine specific soil layers and percolation rates for design of the proposed infiltration system.

The proposed infiltration system must comply with the following setbacks in accordance with Los Angeles County guideline.

Table No. 3, Infiltration Facility Setback Requirements per Los Angeles County

| Setback from | Distance |
| :---: | :---: |
| Property lines and public right of way | 5 feet |
| Any foundation | 15 feet or within $1: 1$ plane drawn up from the <br> bottom of foundation, whichever greater |
| Face of any slope | $\mathrm{H} / 2,5$ feet minimum (H is height of slope) |
| Water wells used for drinking water | 100 feet |

### 8.0 LABORATORY TESTING

Representative samples of the site soils were tested in our laboratory to aid in the classification and to evaluate relevant engineering properties. Selected sub-samples were tested by Environmental Geotechnology Laboratory, Inc. of Arcadia to evaluate the soils for corrosion potential. Results of the various laboratory tests are summarized below. For a more detailed description of the laboratory test methods and test results, see Appendix B, Laboratory Testing Program.

- In-situ Moisture and Dry Density - Results of in-situ moisture and dry density tests are presented on the Log of Borings in Appendix A, Field Exploration.
- Expansion Index - One (1) representative sample from the upper five (5) feet bgs of the site soil was tested to evaluate Expansion Index (EI). The test results indicate that the site soils have a "low" expansion potential (EI = 29).
- Soil Corrosivity - One (1) representative sample of the site soils was tested to evaluate soil corrosivity with respect to common construction materials such as concrete and steel. The test results are presented in Appendix B, Laboratory Testing Program.
- Percent Passing No. 200 - Two (2) representative samples were tested to evaluate the fines content (percent passing no. 200). Results are presented in Appendix B, Laboratory Testing Program, and indicate the samples tested are predominately silty sand.
- R-value - Two (2) representative samples from the upper five (5) feet bgs of the site soils were tested to evaluate the resistance and potential soil strength value to aid in the design of pavement sections. The test results indicate relatively moderate resistance, as presented in Appendix B, Laboratory Testing Program.
- Maximum Dry Density and Optimum Moisture Content - The moisture-density relationship of one (1) representative near surface soil sample are presented in Appendix B, Laboratory Testing Program. The test result indicates that the laboratory maximum dry density for the sample is 130.5 pounds per cubic foot (pcf) at 11.5 percent moisture content.
- Direct Shear - Two (2) direct shear tests were performed; one on representative insitu samples and one on specimens remolded to 90 percent relative compaction. Results of the direct shear testing are presented in Appendix B, Laboratory Testing Program.
- Consolidation Test - Two (2) consolidation tests were performed on representative samples of the site soils encountered within the upper 10 feet. The results of the testing are presented in Appendix B, Laboratory Testing Program. Based on the results of the test, the potential compressibility of the site soils is considered only slight.
For additional information on the subsurface conditions, see the Logs of Borings in Appendix A, Field Exploration.


### 9.0 GEOTECHNICAL EVALUATION AND CONCLUSION

Based on the results of our background review, subsurface exploration, laboratory testing, geotechnical analyses, and understanding of the planned site improvements, it is our opinion that the proposed project is feasible from a geotechnical standpoint, provided the following conclusions and recommendations are incorporated into the project plans, specifications, and are followed during site construction.

Remedial grading is recommended for ground preparation to support the planned single-story buildings and any new hardscape improvements. Such grading should include over-excavation and re-compaction to mitigate disturbed soils from site demolition, to remove and recompact undocumented fill soils (including former basement areas), and to provide a relatively uniform soil condition for the areas of future construction. Following remedial grading, compacted fill soils are anticipated to have similar engineering characteristics with the underlying alluvial soils.

The proposed structures may use conventional foundation systems (spread footings and isolated pads) with slab-on-grade, supported on compacted fill.

### 10.0 EARTHWORK RECOMMENDATIONS

### 10.1 General

Based on our field exploration, laboratory testing, and analyses of subsurface conditions at the site, remedial over-excavation grading is recommended to provide a relatively uniform soil condition across the site for support of the single-story structures and new hardscape and pavement improvements. To help reduce the potential for differential settlement, variations in the soil type, degree of compaction, and thickness of the compacted fill placed underneath the footings and slab should be kept uniform. Site grading recommendations provided in this report are based on our experience with similar projects in the area and our site-specific geotechnical evaluation.

The existing soils removed during over-excavation may be placed as compacted fill in structural areas after proper processing (free of vegetation, shrubs, roots and debris). Based on our understanding of past site usage, we anticipate that the site soil materials will contain scattered demolition debris. Earthwork should be performed with suitable equipment and techniques to selectively screen/remove debris from soils placed as engineered fill.

### 10.2 Over-Excavation/Removal

Remedial grading is recommended to over-excavate and re-compact existing site soils and undocumented fills. Based on our review of the Environmental Site Assessment Report, approximate 11 feet of undocumented fills are anticipated at the planned parking pavement south of the animal shelter. The footprint of the single-story structure should be over-excavated to depth of at least three (3) feet as measured from existing grades, or to a depth of at least two (2) feet below the bottom of footings, or to the depth of undocumented fill, whichever is deeper. Localized deeper removal may be needed where firm native soils are not exposed on the excavation bottom. The exposed bottom of the over-excavation area should be scarified at least 6 inches, moisture conditioned
as needed to near-optimum moisture content, and compacted to 90 percent relative compaction (laboratory maximum density evaluated per ASTM D1577).

The lateral limits of the over-excavation should extend at least 5 feet beyond the planned building footings, where feasible. However, over-excavation should not undermine adjacent off-site improvements. Remedial grading should not extend within a projected 1:1 (horizontal to vertical) plane projected down from the outer edge of adjacent off-site improvements.

Pavement and hardscape areas beyond the footprint of the buildings should be overexcavated to a depth of at least 2 feet, as measured from existing grades. Deeper removal will be needed if firm soil conditions are not exposed on the excavation bottom. The lateral limits of the over-excavation should extend at least 2 feet beyond the pavement/hardscape areas, where feasible.

Soils containing organic materials should not be used as structural fill. The extent of overexcavation removal should be further evaluated by the geotechnical representative based on observations during grading.

### 10.3 Engineered Fill

The bottom of the over-excavations should be scarified to a depth of at least six (6) inches. The scarified soils should be moisture conditioned to near-optimum moisture content and compacted to at least 90 percent of the laboratory maximum dry density to produce a firm and unyielding surface. All engineered fill should be placed on competent, scarified and compacted native materials as evaluated by the geotechnical engineer and in accordance with the specifications presented in this section.

Excavated site soils, free of deleterious materials and rock particles larger than three (3) inches in the largest dimension, should be suitable for placement as compacted fill. Any proposed import fill should be evaluated and approved by Converse prior to import to the site. Import fill material should have an expansion index less than 20.

Prior to compaction, fill materials should be thoroughly mixed and moisture conditioned to within three (3) percent of the optimum moisture content. All fill, if not specified otherwise elsewhere in this report, should be compacted to at least 90 percent of the laboratory dry density in accordance with the ASTM Standard D1557 test method. The upper 12 inches of subgrade below parking pavement areas should be compacted to 95 percent relative compaction.

### 10.4 Excavatability

Based on our field exploration, the earth materials at the site may be excavated with conventional heavy-duty earth moving and trenching equipment. The onsite materials will contain occasional demolition debris and gravel and/or cobbles. Earthwork should be performed with suitable equipment and methods for removal of debris from the engineered fill.

### 10.5 Expansive Soil

Based on soil classifications and laboratory test results, the recommendations contained in this report are based upon anticipated low expansion soil conditions. Any proposed import fill should have an expansion index less than 20, and should be evaluated and approved by Converse prior to import to the site.

The soil materials with Expansion Index higher than 20 should be mitigated. There are several mitigation measures that can be utilized to improve expansive soils at the site. Some mitigation measures include:

- Pre-saturation of on-site compacted subgrade soils to at approximate three (3) percent above optimum moisture content, or
- Reinforce footing with grade beams and place thicker concrete slab with moisture barrier.

It is very important to keep the site soils moisture content around or under the edge of foundation, concrete slab, and asphalt concrete pavement at approximately the same moisture content before, during and after construction. This will reduce greatly the expansion potential of the site soils.

If traditional slabs are planned to be used, removal and replacement of upper two (2) feet of the underlying soils with on site or imported sandy compacted fill (Expansion Index less than 20) to avoid expansion/shrinkage cracks is recommended.

Any proposed import fill should have an expansion index less than 20, and should be evaluated and approved by Converse prior to import to the site.

### 10.6 Pipeline Backfill Recommendations

Any soft and/or unsuitable material encountered at the pipe invert should be removed and replaced with an adequate bedding material. The pipe subgrade should be level, firm, uniform, free of loose materials and properly graded to provide uniform bearing and support to the entire section of the pipe placed on bedding material. Protruding
oversize particles larger than two (2) inches in the largest dimension, if any, should be removed from the trench bottom and replaced with compacted materials. During the digging of depressions for proper sealing of the pipe joints, the pipe should rest on a prepared bottom for as near its full length as is practicable. The bedding zone is defined as that portion of the pipe trench from four inches below the pipe invert to one foot above the top of pipe, in accordance with Section 306-1.2.1 of the Latest Edition of the Standard Specifications for Public Works Construction (SSPWC) and Los Angeles County Department of Public Works Standard Plans, 3080-0, Case 3, Pipe Bedding in Trenches.

### 10.7 Trench Zone Backfill

The following specifications are recommended to provide a basis for quality control during the placement of trench backfill.

Trench excavations to receive backfill shall be free of trash, debris or other unsatisfactory materials at the time of backfill placement. Excavated on-site soils free of oversize particles, defined as larger than one (1) inch in maximum dimension in the upper 12 inches of subgrade soils and larger than three (3) inches in the largest dimension in the trench backfill below, and deleterious matter after proper processing may be used to backfill the trench zone. Imported trench backfill, if used, should be approved by the project soils consultant prior to delivery at the site. No more than 30 percent of the backfill volume should be larger than $3 / 4$ inch in the largest dimension.

Trench backfill shall be compacted to 90 percent of the laboratory maximum dry density as per ASTM Standard D1557 test method. At least the upper twelve (12) inches of trench underlying pavements should be compacted to at least 95 percent of the laboratory maximum dry density.

Trench backfill shall be compacted by mechanical methods, such as sheepsfoot, vibrating or pneumatic rollers, or mechanical tampers, to achieve the density specified herein. The backfill materials shall be brought to within two (2) percent of optimum moisture content and then placed in horizontal layers if the expansion index is less than or equal to 30. Should the expansion index be greater than 30, backfill materials shall be brought to approximately 2 percent above optimum moisture content. The thickness of uncompacted layers should not exceed eight (8) inches. Each layer shall be evenly spread, moistened or dried as necessary, and then tamped or rolled until the specified density has been achieved.

The contractor shall select the equipment and processes to be used to achieve the specified density without damage to adjacent ground and completed work. The field density of the compacted soil shall be measured by the ASTM Standard D1556 or ASTM Standard D2922 test methods or equivalent. Observation and field tests should
be performed by Converse during construction to confirm that the required degree of compaction has been obtained. Where compaction is less than that specified, additional compactive effort shall be made with adjustment of the moisture content as necessary, until the specified compaction is obtained. It should be the responsibility of the contractor to maintain safe conditions during cut and/or fill operations. Trench backfill shall not be placed, spread or rolled during unfavorable weather conditions. When the work is interrupted by heavy rain, fill operations shall not be resumed until field tests by the project's geotechnical consultant indicate that the moisture content and density of the fill are as previously specified.

Imported soils, if any, used as compacted trench backfill should be predominantly granular and meet the following criteria:

- Expansion Index less than 20
- Free of all deleterious materials
- Contain no particles larger than 3 inches in the largest dimension
- Contain less than 30 percent by weight retained on $3 / 4$-inch sieve
- Contain at least 15 percent fines (passing \#200 sieve)
- Have a Plasticity Index of 10 or less

Any import fill should be tested and approved by the geotechnical representative prior to delivery to the site.

### 10.8 Shrinkage and Subsidence

Soil shrinkage and/or bulking as a result of remedial grading depends on several factors including the depth of over-excavation, and the grading method and equipment utilized, and average relative compaction. For preliminary estimation, bulking and shrinkage factors for various units of earth material at the site may be taken as presented below:

- The approximate shrinkage factor for the undocumented fill soils is estimated to range from ten (10) to fifteen (15) percent.
- The approximate shrinkage factor for the native alluvial soils is estimated to range from five (5) to ten (10) percent.
- For estimation purposes, ground subsidence may be taken as 0.1 feet as a result of remedial grading.

Although these values are only approximate, they represent our best estimates of the factors to be used to calculate lost volume that may occur during grading. If more accurate shrinkage and subsidence factors are needed, it is recommended that field-testing using the actual equipment and grading techniques be conducted.

### 11.0 DESIGN RECOMMENDATIONS

The proposed single-story structures may be supported on spread footings extending into properly compacted fill. Hardscape and pavement improvements should be supported on properly compacted fill.

### 11.1 Shallow Foundations

The design recommendations provided in this section are based on the assumption that in preparing the site, earthwork and grading recommendations presented in Section 11 will be implemented. The proposed single-story structures and any site walls may be supported on shallow continuous and isolated spread foundations provided our recommendations are incorporated in the design and construction plans.

### 11.1.1 Vertical Capacity

Shallow pad footing should be at least 24 inches square, and continuous footings should be at least 12 inches wide. Footings should be embedded at least 18 inches below lowest adjacent grade into compacted fill soils. The footing reinforcement should be based on the structural design. Conventional spread footings founded on compacted fill soils may be designed for a net bearing pressure of 2,000 pounds per square foot (psf) for dead-plus-live-loads.

The net allowable bearing pressure can be increased by 400 psf for each additional foot of excavation depth and by 300 for each additional foot of excavation width up to a maximum value of $4,000 \mathrm{psf}$.

The net allowable bearing values indicated above are for the dead loads and frequently applied live loads and are obtained by applying a factor of safety of 3.0 to the net ultimate bearing capacity.

### 11.1.2 Lateral Capacity

Resistance to lateral loads can be assumed to be provided by friction acting at the base of foundations and by passive earth pressure. A coefficient of friction of 0.3 between concrete and soil may be used with the dead load forces. An allowable passive earth pressure of 300 psf per foot of depth may be used for resistance against compacted fill or native soils. A factor of safety of 1.5 was applied in calculating passive earth pressure. The maximum value of the passive earth pressure should be limited to 3,000 psf for compacted fill or native soils.

### 11.1.3 Dynamic Increases

Vertical and lateral bearing values indicated above are for the total dead loads and frequently applied live loads. If normal code requirements are applied for design, the above vertical bearing and lateral resistance values may be increased by 33 percent for short duration loading, which will include the effect of wind or seismic forces.

### 11.1.4 Settlement

The static settlement of structures supported on continuous and/or spread footings founded on compacted fill and/or dense native soils will depend on the actual footing dimensions and the imposed vertical loads. Based on the maximum allowable net bearing pressures presented above, static settlement is anticipated to be less than 0.5 inch, and the differential settlement may be taken as equal to about one half of the total settlement over a horizontal distance of 30 feet.

### 11.2 Modulus of Subgrade Reaction

For the subject project, design of the structures supported on compacted fill subgrade prepared in accordance with the recommendations provided in this report may be based on a soil modulus of subgrade reaction $\left(\mathrm{k}_{\mathrm{s}}\right)$ of 150 pounds per square inch per inch.

### 11.3 Slabs-on-grade

The design of the slab-on-grade will depend on, among other factors, the expansion potential of the pad soils. Based on the expansion index test performed during this evaluation, the expansion potential of the site soils at a shallow depth is low. Accordingly, slabs-on-grade for building pads may be of the conventional type as opposed to post-tensioned.

Slabs-on-grade should be supported on properly compacted fill or deeper undisturbed native soils. Compacted fill used to support slabs-on-grade should be placed and compacted in accordance with report Section 10.0, Earthwork Recommendations.

Slabs-on-grade should have a minimum thickness of four inches nominal for support of normal ground-floor live loads. Minimum reinforcement for slabs-on-grade should be No. 3 reinforcing bars, spaced at 18 inches on-center each way. The thickness and reinforcement of more heavily-loaded slabs will be dependent upon the anticipated loads and should be designed by a structural engineer. A static modulus of subgrade reaction equal to 150 pounds per square inch per inch may be used in structural design of concrete slabs-on-grade.

If approved by the owner, equivalent welded wire mesh may be used for reinforcement of concrete slabs-on-grade. However, to be effective, it is imperative that the reinforcement be located within the center third of the slab thickness. The commonly used procedure of "hooking" the reinforcement during concrete placement seldom, if ever, results in proper location of the slab reinforcing.

It is critical that the exposed subgrade soils should not be allowed to desiccate prior to the slab pour. Care should be taken during concrete placement to avoid slab curling. Slabs should be designed and constructed as promulgated by the ACl and Portland Cement Association (PCA). Prior to the slab pour, all utility trenches should be properly backfilled and compacted.

If moisture-sensitive floor coverings, such as vinyl tile, carpet, or wood floors, are used, slabs should be protected by a minimum 10-mil thick moisture retarder/barrier in conformance with ASTM E 1745 Class A requirements.

### 11.4 Hardscape

Hardscape walkways and patio slabs should have a minimum thickness of four inches nominal for support of normal pedestrian traffic. Minimum reinforcement for walkways and patio slabs should be No. 3 reinforcing bars, spaced at 18 inches on-center each way. Crack control joints should be provided.

Transverse construction joints should not be spaced more than 8 feet and should be cut to a depth of $1 / 4$ the thickness of the slab. Longitudinal joints should not be spaced more than 8 feet apart. A longitudinal joint is not necessary in the pavement adjacent to the curb and gutter section.

It is critical that the exposed subgrade soils should not be allowed to desiccate prior to the slab pour. Care should be taken during concrete placement to avoid slab curling. Slabs should be designed and constructed as promulgated by the ACl and Portland Cement Association (PCA). Prior to the slab pour, all utility trenches should be properly backfilled and compacted.

Positive drainage should be provided away for all hardscape areas to prevent seepage of surface and/or subsurface water into the subgrade adjacent to structures.

### 11.5 Flexible Pavement Recommendations

We have performed flexible pavement design analyses to provide pavement structural sections for new driveway and/or parking areas. An R-value of 31 was used for the sandy on-site soils for pavement design based on the result of laboratory testing and our experience with similar projects. Our recommendations are presented as the following:

The flexible pavement structural section design recommendations were performed in accordance with the method contained in the CALTRANS Highway Design Manual, Chapter 630 without the factor of safety. No specific traffic study was performed to determine the Traffic Index ( TI ) for the proposed project, therefore a wide range of TI values were evaluated. The recommended flexible pavement structural sections for various Tl conditions are presented in the following table:

Table No. 4, Flexible Pavement Structural Sections

| Design <br> R-value | Design TI | Asphalt Concrete (AC) Over Aggregate Base (AB) <br> Structural Sections | Full AC <br> Structural Section |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | AC (inches) | AB (inches) | AC (inches) |

Actual traffic index and traffic load should be determined by either Civil Engineer or Traffic Engineer. The above pavement sections are recommended as a guideline for basic usage of the indicated Tl values, and may not be sufficient for actual traffic loading.

Base material shall conform to requirements for a Class 2 Aggregate Base (AB) or equivalent (such as crushed miscellaneous base - CMB) and should be placed in accordance with the requirements of the Standard Specifications for Public Works Construction (SSPWC, latest Edition).

Asphaltic materials should conform to Section 203-1, "Paving Asphalt," and Section 302-5, "Asphalt Concrete Pavement," of the SSPWC, latest edition.

### 11.6 Rigid Pavement Design

The Portland Cement Association's (PCA's) Southwest Region Publication P-14, Portland Cement Concrete Pavement (PCCP) for Light, Medium, and Heavy Traffic, presents a "Portland Cement Concrete Pavement (PCCP) Design Nomograph for Cities and Counties Roads." The pavement section presented in Table No. 5, Rigid Pavement Structural Sections, is based on this nomograph. Pavement sections are provided for the Traffic

Indices (TIs) ranging from 4 to 9 . An R -value of 31 was used for pavement design based on our experiences with similar project conditions.

Table No. 5, Rigid Pavement Structural Sections

| Design R-Value | Design <br> Traffic Index (TI) | PCCP Pavement Section <br> (inches) |
| :---: | :---: | :---: |
| 31 | 4.0 | 6.25 |
|  | 5.0 | 6.50 |
|  | 6.0 | 6.75 |
|  | 7.0 | 7.00 |
|  | 8.0 | 7.25 |
|  | 9.0 | 7.50 |

Actual traffic index and traffic load should be determined by either Civil Engineer or Traffic Engineer. The above pavement section is recommended for basic usage as indicated in the table and may not be sufficient for actual traffic loading.

Prior to placement of base aggregate, at least the upper 12 inches of subgrade soils below rigid pavement sections should be scarified, moisture-conditioned, if necessary, and recompacted to at least 95 percent relative compaction as defined by the ASTM D 1557 standard (current edition) test method.

The pavement section presented in Table No. 5 is based on a minimum 28-day Modulus of Rupture (M-R) of 550 psi and a compressive strength of $3,000 \mathrm{psi}$. The third point method of testing beams should be used to evaluate modulus of rupture. The concrete mix design should contain a minimum cement content of 5.5 sacks per cubic yard. Recommended maximum and minimum values of slump for pavement concrete are three inches to one inch, respectively.

Transverse contraction joints should not be spaced more than 15 feet and should be cut to a depth of $1 / 4$ the thickness of the slab. Longitudinal joints should not be spaced more than 12 feet apart. A longitudinal joint is not necessary in the pavement adjacent to the curb and gutter section.

All outside edges should conform to Section 201 of the most recent Standard Specifications for Public Works Construction (SSPWC), and should be constructed in accordance with Section 302-6 of the SSPWC. Pavement subgrade should be prepared in accordance with Section 301 of the SSPWC. The upper 12 inches of subgrade should be compacted to a relative compaction of at least 95 percent as per the current ASTM D 1557 standard.

Positive drainage should be provided away from all pavement areas to prevent seepage of surface and/or subsurface water into the pavement base and/or subgrade.

### 11.7 Soil Corrosivity Evaluation

Converse utilized the Environmental Geotechnology Laboratory, Inc., located in Arcadia, California, to test one (1) bulk soil samples taken in the general area of the proposed structures. The tests included minimum resistivity, pH , soluble sulfates, and chloride content, with the results summarized on the following table:

Table No. 6, Soil Corrosivity Test Results

| Boring No. | Sample <br> Depth <br> (feet) | pH <br> (Caltrans 643) | Soluble <br> Chlorides <br> (Caltrans 422) <br> ppm | Soluble <br> Sulfate <br> (Caltrans 417) <br> ppm | Saturated <br> Resistivity <br> (Caltrans 643) <br> Ohm-cm |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{BH}-5$ | $0-5$ | 8.04 | 65 | 10 | 4100 |

According to the Los Angeles County Manual for Preparation of Geotechnical Report (2010), the pH is in "non-corrosive" range, the Chlorides content is in "non-corrosive" range, the Sulfate content is in "non-corrosive" range, and the resistivity is in "moderately corrosive" range.

A corrosion engineer may be consulted for appropriate mitigation procedures and construction design, if needed. Conventional corrosion mitigation measures may include the following:

- Steel and wire concrete reinforcement should have at least three inches of concrete cover where cast against soil, unformed.
- Below-grade ferrous metals should be given a high-quality protective coating, such as 18 -mil plastic tape, extruded polyethylene, coal-tar enamel, or Portland cement mortar.
- Below-grade metals should be electrically insulated (isolated) from above-grade metals by means of dielectric fittings in ferrous utilities and/or exposed metal structures breaking grade.


### 11.8 Site Drainage

Adequate positive drainage should be provided away from the structure foundations to prevent ponding and to reduce percolation of water into the foundation soils. We recommend that any landscape areas immediately adjacent to the foundation shall be designed sloped away from the foundation with a minimum $5 \%$ slope gradient for at least 10 feet measured perpendicular to the face of the foundation. Impervious surfaces within 10 feet of the structure foundation shall be sloped a minimum of 2 percent away from the structure per 2010 CBC.

### 12.0 CONSTRUCTION CONSIDERATIONS

### 12.1 General

Site soils should be excavatable using conventional heavy-duty excavating equipment. Temporary sloped excavation is feasible if performed in accordance with the slope ratios provided in Section 12.2, Temporary Excavations. Existing utilities should be accurately located and either protected or removed as required.

### 12.2 Temporary Excavations

Based on the materials encountered in the exploratory borings, sloped temporary excavations may be constructed according to the slope ratios presented in Table No. 7, Slope Ratios for Temporary Excavation. Any loose utility trench backfill or other fill encountered in excavations will be less stable than the native soils. Temporary cuts encountering loose fill or loose dry sand should be constructed at a flatter gradient than presented in the following table:

Table No. 7, Slope Ratios for Temporary Excavation

| Maximum Depth of Cut <br> (feet) | Maximum Slope Ratio* <br> (horizontal: vertical) |
| :---: | :---: |
| $0-4$ | vertical |
| $4-8$ | $1: 1$ |
| $8+$ | $1.5: 1$ |

*Slope ratio assumed to be uniform from top to toe of slope.
Surfaces exposed in slope excavations should be kept moist but not saturated to minimize raveling and sloughing during construction. Adequate provisions should be made to protect the slopes from erosion during periods of rainfall. Surcharge loads, including construction, should not be placed within five (5) feet of the unsupported trench edge. The above maximum slopes are based on a maximum height of six (6) feet of stockpiled soils placed at least five (5) feet from the trench edge.

All applicable requirements of the California Construction and General Industry Safety Orders, the Occupational Safety and Health Act of 1987 and current amendments, and the Construction Safety Act should be met. The soils exposed in cuts should be observed during excavation by the project's geotechnical consultant. If potentially unstable soil conditions are encountered, modifications of slope ratios for temporary cuts may be required.

### 12.3 Geotechnical Services During Construction

This report has been prepared to aid in the foundation plans and specifications, and to assist the architect, civil and structural engineers in the design of the proposed structures. It is recommended that this office be provided an opportunity to review final design drawings and specifications to verify that the recommendations of this report have been properly implemented.

Recommendations presented herein are based upon the assumption that adequate earthwork monitoring will be provided by Converse. Footing excavations should be observed by Converse prior to placement of steel and concrete so that footings are founded on satisfactory materials and excavations are free of loose and disturbed materials. Trench backfill should be placed and compacted with observation and field density testing provided by this office.

During construction, the geotechnical engineer and/or their authorized representatives should be present at the site to provide a source of advice to the client regarding the geotechnical aspects of the project and to observe and test the earthwork performed. Their presence should not be construed as an acceptance of responsibility for the performance of the completed work, since it is the sole responsibility of the contractor performing the work to ensure that it complies with all applicable plans, specifications, ordinances, etc.

This firm does not practice or consult in the field of safety engineering. We do not direct the contractor's operations, and cannot be responsible for other than our own personnel on the site; therefore, the safety of others is the responsibility of the contractor. The contractor should notify the owner if he considers any recommended actions presented herein to be unsafe.

### 13.0 SECTION 111 STATEMENT

The subject project site is not located within a mapped seismic hazard zone (CDMG 2003) and will not be subject to seismic hazards such as ground rupture, landslides, liquefaction settlement, and lateral spreading of the site soil. The recommended grading operations for the subject project will be safe from the adverse affects of landsliding, settlement, and slippage provided the site conditions are maintained. In addition, bordering offsite properties will not sustain adverse geotechnical effects resulting from the recommended grading earthwork. Our findings and professional opinion do not constitute a guarantee or warranty, expressed or implied.

### 14.0 CLOSURE

The findings and recommendations of this report were formulated in compliance with Section 111 of the County of Los Angeles Building Code. Our conclusions and recommendations are based on the results of the field and laboratory studies, combined with an interpolation and extrapolation of soil conditions between and beyond boring locations. If conditions encountered during construction appear to be different from those shown by the borings, this office should be notified.

Design recommendations given in this report are based on the assumption that the earthwork and site grading recommendations contained in this report are implemented. Additional consultation may be prudent to interpret Converse's findings for contractors, or to possibly refine these recommendations based upon the review of the final site grading and actual site conditions encountered during construction. If the scope of the project changes, if project completion is to be delayed, or if the report is to be used for another purpose, this office should be consulted.

This report was prepared for the Los Angeles County Department of Public Works, for the subject project described herein. We are not responsible for technical interpretations made by others of our exploratory information. Specific questions or interpretations concerning our findings and conclusions may require a written clarification to avoid future misunderstandings.

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## APPENDIX A

## FIELD EXPLORATION

## APPENDIX A

## FIELD EXPLORATION

Field exploration included a site reconnaissance and subsurface exploration program. During the site reconnaissance, the surface conditions were noted, and the approximate locations of the boring were determined. The exploratory borings were approximately located using existing boundary and other features as a guide and should be considered accurate only to the degree implied by the method used. The various field study methods performed are discussed below.

## Exploratory Borings

Seven (7) borings (BH-1 through BH-7) were drilled within the project site on March 22 2012. The borings were advanced using a truck mounted drill rig equipped with an eight inch diameter hollow-stem auger. The depths drilled range from 16.5 feet to 51.5 feet below ground surface (bgs). Encountered earth materials were continuously logged by a Converse professional and classified in the field by visual examination in accordance with the Unified Soil Classification System (USCS). Where appropriate, field descriptions and classifications have been modified to reflect laboratory test results.

Ring samples of the subsurface materials were obtained at frequent intervals in the exploratory borings using a drive sampler (2.4-inches inside diameter and 3.0-inches outside diameter) lined with sample rings. The steel ring sampler was driven into the bottom of the borehole with successive drops of a 140-pound driving weight falling 30 inches, using an automatic hammer. Samples are retained in brass rings (2.4-inches inside diameter and $1.0-\mathrm{inch}$ in height). The central portion of the sample was retained and carefully sealed in waterproof plastic containers for shipment to the Converse laboratory. Blow counts for each sample interval are presented on the logs of borings. Bulk samples of typical soil types were also obtained.

Standard Penetration Test (SPT) was also performed using a standard (1.4-inches inside diameter and 2.0-inches outside diameter) split-barrel sampler. The mechanically driven hammer for the SPT sampler was 140 pounds, failing 30 inches for each blow. The recorded blow counts for every six inches for a total of 1.5 feet of sampler penetration are shown on the Logs of Borings in the "BLOWS" column. The standard penetration test was performed in accordance with the ASTM Standard D1586 test method.

It should be noted that the exact depths at which material changes occur cannot always be established accurately. Changes in material conditions that occur between driven samples are indicated in the logs at the top of the next drive sample. A key to soil symbols and terms is presented as Drawing No. A-1, Soil Classification Chart. The log of the exploratory boring is presented in Drawing Nos. A-2 through A-8, Log of Borings.

## SOIL CLASSIFICATION CHART

| MAJOR DIVISIONS |  |  | SYMBOLS |  | $\begin{gathered} \text { TYPICAL } \\ \text { DESCRIPTIONS } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | GRAPH | LETTER |  |
| COARSE GRAINED SOILS | $\begin{aligned} & \text { GRAVEL } \\ & \text { AND } \\ & \text { GRAVELLY } \\ & \text { SOILS } \end{aligned}$ | CLEAN GRAVELS |  | GW | well-graded gravels. GRAVEL-SAND MLXTU LTTLE OR NO FINES |
|  |  | (LITLE OR Nofnes) | $\begin{array}{\|cc\|} \hline 0 & 00 \\ 0 & 0 \\ 0.0 & 0 \\ 0 & 0 \\ 0 & 0 \end{array}$ | GP | poorly-graded grivels, GRAVEL - SAMD MIXTURES, LTTLE ORNO FINES |
|  | MORE THAN 50\% OF COARSE FRACTION RETAINED ON NO. 4 sileve | GRAVELS WITH FINES |  | GM | sILTY GRAVELS, GRAVEL - SAND sIt Mixtures |
|  |  | $\begin{gathered} \text { FINES } \\ \substack{\text { APPRECLABLE AMOUNT } \\ \text { OF FiNESS }} \\ \hline \end{gathered}$ | $80 / 8 / \mathrm{c}$ | GC | CLAMEVGRAYELS, GRAVEL- SAND-CLAY MiXTUPES SAND - CLAYMIXTURES |
| MORE THAN 50\% O MATERIAL IS LARGER THAN NO. 200 SIEVE SIZE | SAND AND SANDY SOILS | CLEAN SANDS (LUTTLE OR NO FINES) |  | SW | WELL-GRADED SANDS, GRAVELLY SANDS, UTTLE OR NO FINES |
|  |  |  |  | SP | poorly-graded sands, GRAVELY SAND, LIITLE OR NO FNES |
|  | MORE THAN 50\% OF COARSE FRACTION PASSING ON NO. 4 sieve | SANDS WITH FINES |  | SM | GITTMANDS. SAND-SILT tixTURES |
|  |  | (APPRECMELE AMOUNT of Fints) |  | SC | CLAYEY SANDS, SAND - CLAY MIXTURES |
| FINE GRAINED SOILS | SILTS AND CLAYS | LIQUIDLIMIT Less THAN 50 |  | ML |  |
|  |  |  |  | CL |  |
|  |  |  | $=-=-$ | OL | organic sils and organic sitryclars of low FLASTICITY |
| MORE THAN 50\% OF MATERIAL IS Smaller than no. 200 SIEVE SIIE | SILTS AND CLAYS | LIQUID LIMIT GREATER THAN 50 |  | MH | NORGANIC SILTS, MICACEOUS OR DLATOMACEOUS FINE SAND OR SKLY SORS |
|  |  |  |  | CH | INORGANIC CLAYS Of HiGH PLASTICTY |
|  |  |  |  | OH | ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SLTS |
| HIGHLY ORGANIC SOILS |  |  |  | PT | PEAT, HUMUS, SWAMP SOILS $\because$ CON HIGH ORGANIC CONTENTS |

NOTE: DUAL SYMBOLS ARE USED TO INDICATE BORDERLINE SOIL CLASSIFICATIONS

## BORING LOG SYMBOLS



| LABORATORY TESTING ABBREVIATIONS |  |  |  |
| :---: | :---: | :---: | :---: |
| IEST TYPE <br> (Results shown in Appendix B) |  | STRENGTH |  |
|  |  | Pocket Penstrometer | p |
|  |  | Direcl Shear | ds |
|  |  | Direct Shear (single point) | ds* |
| CLASSIFICATION |  | Unconfined Compression | UC |
|  |  | Trlaxial Compression | tx |
| Plasticity | pi | Vane Shear | vs |
| Grain Size Analysis Passing No. 200 Sleve | ma | Consolidation | c |
| Passing No. 200 Sleve | we | Collapse Test | coll |
| Expansion Index | el | Resistance (R) Value | r |
| Compaction Curve | max | Chemical Analysis | ca |
| Hydrometer | h | Electrical Resistivily | er |

## UNIFIED SOIL CLASSIFICATION AND KEY TO BORING LOG SYMBOLS

Dates Drilled: $\qquad$ 3/22/2012

Logged by: $\qquad$ Checked By: $\qquad$ SCL

Equipment: $\qquad$ Driving Weight and Drop: $\quad 140 \mathrm{lbs} / 30$ in
Ground Surface Elevation (ft): $\qquad$ Depth to Water (ft): NOT ENCOUNTERED

$\qquad$
NR
Checked By: $\qquad$ SCL

Equipment: $\qquad$ Driving Weight and Drop: $\quad 140 \mathrm{lbs} / 30$ in
Ground Surface Elevation (ft): N/A
Depth to Water (ft): NOT ENCOUNTERED

Dates Drilled:

Logged by:
NR
Checked By: $\qquad$ SCL
Equipment: $\qquad$ Driving Weight and Drop: $140 \mathrm{lbs} / 30 \mathrm{in}$
Ground Surface Elevation (ft): $\qquad$ Depth to Water (ft): NOT ENCOUNTERED

$\qquad$ Logged by: $\qquad$ Checked By: $\qquad$ SCL

Equipment: $\qquad$ Driving Weight and Drop: $\quad 140 \mathrm{lbs} / 30 \mathrm{in}$
Ground Surface Elevation (ft): $\qquad$ Depth to Water ( ft ): $\quad$ NOT ENCOUNTERED

$\qquad$ 3/22/2012

Logged by: $\qquad$ Checked By: $\qquad$ SCL
Equipment: $\qquad$ 8" HOLLOW STEM AUGER

Driving Weight and Drop: $140 \mathrm{lbs} / 30$ in
Ground Surface Elevation (ft): $\qquad$ Depth to Water (ft): NOT ENCOUNTERED


Dates Drilled: $\qquad$ 3/22/2012

Logged by: $\qquad$ Checked By: SCL

Equipment: $\qquad$ Driving Weight and Drop: $\quad 140 \mathrm{lbs} / 30$ in
Depth to Water $(\mathrm{ft}): \quad$ NOT ENCOUNTERED

$\qquad$ Logged by: $\qquad$ Checked By: $\qquad$ SCL

Equipment: $\qquad$ 8" HOLLOW STEM AUGER Driving Weight and Drop: $\quad 140 \mathrm{lbs} / 30$ in

Ground Surface Elevation (ft): $\qquad$ Depth to Water ( ft ): NOT ENCOUNTERED


## Log of Boring No. BH-7

Dates Drilled: $\qquad$ 3/22/2012

Logged by: $\qquad$ Checked By: $\qquad$ SCL

Equipment: 8" HOLLOW STEM AUGER
Driving Weight and Drop: $\quad 140 \mathrm{lbs} / 30 \mathrm{in}$
Ground Surface Elevation (ft): $\qquad$ Depth to Water ( ft ): _ NOT ENCOUNTERED


## APPENDIX B

## LABORATORY TESTING PROGRAM

## APPENDIX B

## LABORATORY TESTING PROGRAM

Tests were conducted in our laboratory on representative soil samples for the purpose of classification and evaluation of their relevant physical characteristics and engineering properties. The amount and selection of tests were based on the geotechnical requirements of the project. Test results are presented herein and on the Logs of Borings in Appendix A, Field Exploration. The following is a summary of the laboratory tests conducted for this project.

## Moisture Content and Dry Density

Results of moisture content and dry density tests, performed on relatively undisturbed ring samples were used to aid in the classification of the soils and to provide quantitative measure of the in situ dry density. Data obtained from this test provides qualitative information on strength and compressibility characteristics of site soils. For test results, see the Logs of Borings in Appendix A, Field Exploration.

## Percent Passing No. 200

To assist in classification of soils, percent of fine-grained (passing no. 200 sieve) analyses were performed on two (2) selected samples. Testing was performed in general accordance with the ASTM Standard D1140 test method. The test results are shown on the Logs of Borings in Appendix A, Field Exploration.

## Maximum Dry Density Test

One (1) laboratory maximum dry density-moisture content relationship tests were performed on representative bulk samples of the upper 5 feet of soil material. The testing was conducted in accordance with ASTM Standard D1557 laboratory procedure. The test result is presented on Drawing No. B-1, Moisture-Density Relationship Results.

## Direct Shear

Direct shear test was performed on one (1) relatively undisturbed in-situ sample and one (1) sample remolded to $90 \%$ relative compaction. For each test, three brass sampler rings were placed, one at a time, directly into the test apparatus and subjected to a range of normal loads appropriate for the anticipated conditions. The sample was then sheared at a constant strain rate of $0.01 \mathrm{inch} /$ minute. Shear deformation was recorded until a maximum of about 0.25 -inch shear displacement was achieved. Ultimate strength was selected from the shear-stress deformation data and plotted to determine the shear strength parameters. For test data, including sample density and moisture content, see Drawing No. B-2a and B-2b, Direct Shear Test Results.

## Consolidation

Consolidation test was performed on two (2) relatively undisturbed in-situ samples. Data obtained from this test procedure was used to evaluate the settlement characteristics of the foundation soils under load. Preparation for this test involved trimming the sample and placing the one-inch high brass ring into the test apparatus, which contained porous stones, both top and bottom, to accommodate drainage during testing. Normal axial loads were applied to one end of the sample through the porous stones, and the resulting deflections were recorded at various time periods. The load was increased after the sample reached a reasonable state equilibrium. Normal loads were applied at a constant load-increment ratio, successive loads being generally twice the preceding load. The sample was tested at field and submerged conditions. The test results, including sample density and moisture content, are presented in Drawing Nos. B-3a and B-3b, Consolidation Test Results.

## Expansion Index

One (1) representative bulk sample was tested to evaluate the expansion potential of materials encountered at the site. Test results are presented in the following table:

Table No. B-1, Expansion Index Test Results

| Boring No. | Depth <br> (feet) | Soil Description | Expansion <br> Index | Expansion <br> Potential |
| :---: | :---: | :---: | :---: | :---: |
| BH-3 | $0-5$ | Silty Sand (SM) | 29 | Low |

## Soil Corrosivity

One (1) representative soil sample was tested to evaluate minimum electrical resistivity, pH , and chemical content, including soluble sulfate and chloride concentrations. The purpose of these tests is to determine the corrosion potential of site soils when placed in contact with common construction materials. These tests were performed by Environmental Geotechnology Laboratory, Inc. (EGL), located in Arcadia, California. The test results received from EGL are included in the following table:

Table No. B-2, Corrosivity Test Results

| Boring No. | Sample <br> Depth <br> (feet) | pH <br> (Caltrans 643) | Soluble <br> Chlorides <br> (Caltrans 422) <br> ppm | Soluble <br> Sulfate <br> (Caltrans 417) <br> ppm | Saturated <br> Resistivity <br> (Caltrans 643) <br> Ohm-cm |
| :---: | :---: | :---: | :---: | :---: | :---: |
| BH-5 | $0-5$ | 8.04 | 65 | 10 | 4100 |

## R-value

Two (2) representative bulk soil samples were tested for resistance value (R-value) in accordance with State of California Standard Method 301-G. This test is designed to provide a relative measure of soil strength for use in pavement design. The test result is shown in the following table:

Table No. B-3, R-value Test Result

| Boring <br> No. | Depth <br> (feet) | Soil Description | Measured <br> R-value |
| :---: | :---: | :---: | :---: |
| BH-6 | $0-5.0$ | Silty SAND (SM) | 31 |
| BH-7 | $0-5.0$ | Silty SAND (SM) | 34 |

## Sample Storage

Soil samples presently stored in our laboratory will be discarded 30 days after the date of this report, unless this office receives a specific request to retain the samples for a longer period.

\(\left.$$
\begin{array}{|c|c|c|l|c|c|c|}\hline \text { SYMBOL } & \text { BORING NO. } & \text { DEPTH (ft) } & \text { DESCRIPTION } & \begin{array}{c}\text { ASTM } \\
\text { TEST METHOD }\end{array} & \begin{array}{c}\text { OPTIMUM } \\
\text { WATER, \% }\end{array} & \begin{array}{c}\text { MAXIMUM DRY } \\
\text { DENSITY, pcf }\end{array}
$$ <br>

\hline- \& BH-3 \& 0-5 \& SILTY SAND (SM) \& \& D1557 Method A \& 11.5\end{array}\right]\)| 130.5 |
| :---: |
|  |

EAST ANTELOPE VALLEY ANIMAL SHELTER LOS ANGELES COUNTY DEPARTMENT OF PUBLIC WORKS PALMDALE, CALIFORNIA


| BORING NO. | BH-3 | DEPTH (ft) | 0-5 |
| :---: | :---: | :---: | :---: |
| DESCRIPTION | SILTY SAND (SM) |  |  |
| COHESION (psf) | 100 | FRICTION ANGLE (degrees): | 27 |
| MOISTURE CONTENT (\%) | 11.1 | DRY DENSITY (pcf) | 117.9 |

NOTE: Ulimate Strength. Remolded to $90 \%$ relative compaction.

## DIRECT SHEAR TEST RESULTS

Project Name
EAST ANTELOPE VALLEY ANJMAL SHELTER LOS ANGELES COUNTY DEPARTMENT OF PUBLIC WORKS PALMDALE, CALIFORNIA


| BORING NO. | $:$ | BH-5 | DEPTH (ft) |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| DESCRIPTION | $:$ | SAND (SP) |  |  |
| COHESION (psf) | $:$ | 50 |  | 34 |
| MOISTURE CONTENT (\%) | $:$ | 6.8 | FRICTION ANGLE (degrees): | 114.7 |

NOTE: Ultimate Strength.

## DIRECT SHEAR TEST RESULTS



NOTE: SOLID CIRCLES INDICATE READINGS AFTER ADDITION OF WATER
CONSOLIDATION TEST RESULTS


NOTE: SOLID CIRCLES INDICATE READINGS AFTER ADDITION OF WATER

## CONSOLIDATION TEST RESULTS

## APPENDIX C

## PERCOLATION TESTING

## APPENDIX C

Percolation testing was performed utilizing exploratory Borings $\mathrm{BH}-1$ and $\mathrm{BH}-2$ on March 22, 2011. Each boring was cased using two-inch diameter perforated casing and gravel. Water was added to the bore hole until the water level was at the ground surface and allowed to presoak for at least 2 hours. After pre-soak, water was added to the bore hole until the water level was near the ground surface. Tests were performed using the falling head test method in accordance with Los Angeles County "Low Impact Development Best Management Practice Guideline for Design, Investigation, and Reporting". The water level was measured to the nearest tenth of a foot, and calculated in inches per hour.

Table No. C-1, Percolation Test Results

| Boring <br> No. | Depth of <br> Boring <br> (feet) | Predominant Soil Types (USCS) | Average Percolation Rate <br> (inches/hour) |
| :---: | :---: | :---: | :---: |
| BH-1 | 30 | Sand (SP), Silty Sand (SM) | 6.02 |
| BH-2 | 30 | Silty Sand (SM), Clayey Silts (ML) | 2.74 |

Based on the test results, the site soils are primarily silty sand and sand with moderate to good infiltration rates. These soils are considered suitable for infiltration drainage systems. The project Civil Engineer should review the raw data of percolation test attached with this memorandum to determine specific soil layers and percolation rates for design of the proposed infiltration system.

[^14]

Percolation Testing
Job Name: East Antelope Valley Animal Shelter
Job No.: 12-31-145-01
Test Date: $\underline{03.22 .12}$
Bu:
Final Time
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Note: Reduction Factor, $\left.R_{f}=\left(2^{*} d_{i}-\Delta d\right)\right\rangle D+1$
Lowest Pericolaton Rate $=1.29 \quad$ inch/hr


APPENDIX D EARTHWORK SPECIFICATIONS

## APPENDIX D

## EARTHWORK SPECIFICATIONS

## D1.1 Scope of Work

The work includes all labor, supplies and construction equipment required to construct the building pads in a good, workmanlike manner, as shown on the drawings and herein specified. The major items of work covered in this section include the following:

- Site Inspection
- Authority of Geotechnical Engineer
- Site Clearing
- Excavations
- Preparation of Fill Areas
- Placement and Compaction of Fill
- Observation and Testing


## D1.2 Site Inspection

1. The Contractor shall carefully examine the site and make all inspections necessary, in order to determine the full extent of the work required to make the completed work conform to the drawings and specifications. The Contractor shall satisfy himself as to the nature and location of the work, ground surface and the characteristics of equipment and facilities needed prior to and during prosecution of the work. The Contractor shall satisfy himself as to the character, quality, and quantity of surface and subsurface materials or obstacles to be encountered. Any inaccuracies or discrepancies between the actual field conditions and the drawings, or between the drawings and specifications must be brought to the Owner's attention in order to clarify the exact nature of the work to be performed.
2. This Geotechnical Study Report by Converse Consultants may be used as a reference to the surface and subsurface conditions on this project. The information presented in this report is intended for use in design and is subject to confirmation of the conditions encountered during construction. The exploration logs and related information depict subsurface conditions only at the particular time and location designated on the boring logs. Subsurface conditions at other locations may differ from conditions encountered at the exploration locations. In addition, the passage of time may result in a change in subsurface conditions at
the exploration locations. Any review of this information shall not relieve the Contractor from performing such independent investigation and evaluation to satisfy himself as to the nature of the surface and subsurface conditions to be encountered and the procedures to be used in performing his work.

## D1.3 Authority of the Geotechnical Engineer

1. The Geotechnical Engineer will observe the placement of compacted fill and will take sufficient tests to evaluate the uniformity and degree of compaction of filled ground.
2. As the Owner's representative, the Geotechnical Engineer will (a) have the authority to cause the removal and replacement of loose, soft, disturbed and other unsatisfactory soils and uncontrolled fill; (b) have the authority to approve the preparation of native ground to receive fill material; and (c) have the authority to approve or reject soils proposed for use in building areas.
3. The Civil Engineer and/or Owner will decide all questions regarding (a) the interpretation of the drawings and specifications, (b) the acceptable fulfillment of the contract on the part of the Contractor and (c) the matters of compensation.

## D1.4 Site Clearing

1. Clearing and grubbing shall consist of the removal from building areas to be graded of all existing structures, pavement, utilities, and vegetation.
2. Organic and inorganic materials resulting from the clearing and grubbing operations shall be hauled away from the areas to be graded.

## D1.5 Excavations

1. Based on observations made during our field explorations, the surficial soils can be excavated with conventional earthwork equipment.

## D1.6 Preparation of Fill Areas

1. All organic material, organic soils, incompetent alluvium, undocumented fill soils and debris should be removed from the proposed building areas.
2. The upper three (3) feet of existing soils, or to a depth of at least two (2) feet below footings, or to the depth of undocumented fill, whichever is deeper, should be removed and replaced as compacted fill for foundation support. The excavation should be extended to five (5) feet beyond the building limits and appendages shall be removed. All loose, soft or disturbed earth materials extending below the recommended removal depth should also be removed from the bottom of excavations before placing structural fill. The actual depth of removal should be
determined based on observations made during grading. Thickness of compacted fill underneath the buildings should not vary. Pavement and hardscape areas beyond the footprint of new building structures should be over-excavated to a depth of at least two (2) feet, as measured from existing grades. After the required removals have been made, the exposed native earth materials shall be excavated to provide a zone of structural fill for the support of footings, slabs-ongrade, and exterior flatwork. The fill thickness under structures should not vary.
3. The subgrade in all areas to receive fill shall be scarified to a minimum depth of six (6) inches, the soil moisture adjusted between optimum and three percent above optimum, and then compacted to at least 90 percent of the laboratory maximum dry density as determined by ASTM Standard D1557 test method.
4. Compacted fill may be placed on native soils that have been properly scarified and recompacted as discussed above.
5. All areas to receive compacted fill will be observed and approved by the Geotechnical Engineer before the placement of fill.

## D1.7 Placement and Compaction of Fill

1. Compacted fill placed for the support of footings, slabs-on-grade, exterior concrete flatwork, and driveways will be considered structural fill. Structural fill may consist of approved on-site soils or imported fill that meets the criteria indicated below.
2. Fill consisting of selected on-site earth materials or imported soils approved by the Geotechnical Engineer shall be placed in layers on approved earth materials. Soils used as compacted structural fill shall have the following characteristics:
a. All fill soil particles shall not exceed three inches in nominal size, and shall be free of organic matter and miscellaneous inorganic debris and inert rubble.
b. Imported fill materials shall have an Expansion Index (EI) less than 20. All imported fill should be compacted to at least 90 percent of the laboratory maximum dry density (ASTM Standard D1557) at about to three percent above optimum moisture.
3. Fill soils shall be evenly spread in maximum 8-inch lifts, watered or dried as necessary, mixed and compacted to at least the density specified below. The fill shall be placed and compacted on a horizontal plane, unless otherwise approved by the Geotechnical Engineer.
4. All fill placed at the site shall be compacted to at least 90 percent of the laboratory maximum dry density as determined by ASTM Standard D1557 test method. The on-site soils shall be moisture conditioned between optimum and three percent above the optimum moisture content.
5. Representative samples of materials being used, as compacted fill will be analyzed in the laboratory by the Geotechnical Engineer to obtain information on their physical properties. Maximum laboratory density of each soil type used in the compacted fill will be determined by the ASTM Standard D1557 compaction method.
6. Fill materials shall not be placed, spread or compacted during unfavorable weather conditions. When site grading is interrupted by heavy rain, filling operations shall not resume until the Geotechnical Engineer approves the moisture and density conditions of the previously placed fill.
7. It shall be the Grading Contractor's obligation to take all measures deemed necessary during grading to provide erosion control devices in order to protect slope areas and adjacent properties from storm damage and flood hazard originating on this project. It shall be the contractor's responsibility to maintain slopes in their as-graded form until all slopes are in satisfactory compliance with job specifications, all berms have been properly constructed, and all associated drainage devices meet the requirements of the Civil Engineer.

## D1.8 Trench Backfill

The following specifications are recommended to provide a basis for quality control during the placement of trench backfill.

1. Trench excavations to receive backfill shall be free of trash, debris or other unsatisfactory materials at the time of backfill placement.
2. Trench backfill shall be compacted to a minimum relative compaction of 90 percent as per ASTM Standard D1557 test method.
3. Rocks larger than one inch should not be placed within 12 inches of the top of the pipeline or within the upper 12 inches of pavement or structure subgrade. No more than 30 percent of the backfill volume shall be larger than $3 / 4$-inch in largest dimension. Rocks shall be well mixed with finer soil.
4. The pipe design engineer should select bedding material for the pipe. Bedding materials generally should have a Sand Equivalent (SE) greater than or equal to 30, as determined by the ASTM Standard D2419 test method.
5. Trench backfill shall be compacted by mechanical methods, such as sheepsfoot, vibrating or pneumatic rollers, or mechanical tampers, to achieve the density specified herein. The backfill materials shall be brought to between optimum and three percent above optimum, then placed in horizontal layers. The thickness of uncompacted layers should not exceed eight inches. Each layer shall be evenly spread, moistened or dried as necessary, and then tamped or rolled until the specified density has been achieved.
6. The contractor shall select the equipment and processes to be used to achieve the specified density without damage to adjacent ground and completed work.
7. The field density of the compacted soil shall be measured by the ASTM Standard D1556 or ASTM Standard D2922 test methods or equivalent.
8. Observation and field tests should be performed by Converse during construction to confirm that the required degree of compaction has been obtained. Where compaction is less than that specified, additional compactive effort shall be made with adjustment of the moisture content as necessary, until the specified compaction is obtained.
9. It should be the responsibility of the Contractor to maintain safe conditions during cut and/or fill operations.
10. Trench backfill shall not be placed, spread or rolled during unfavorable weather conditions. When the work is interrupted by heavy rain, fill operations shall not be resumed until field tests by the project's geotechnical consultant indicate that the moisture content and density of the fill are as previously specified.

## D1.9 Observation and Testing

1. During the progress of grading, the Geotechnical Engineer will provide observation of the fill placement operations.
2. Field density tests will be made during grading to provide an opinion on the degree of compaction being obtained by the contractor. Where compaction of less than specified herein is indicated, additional compactive effort with adjustment of the moisture content shall be made as necessary, until the required degree of compaction is obtained.
3. A sufficient number of field density tests will be performed to provide an opinion to the degree of compaction achieved. In general, density tests will be performed on each one-foot lift of fill, but not less than one for each 500 cubic yards of fill placed.

# Appendix E Subsurface Slab Assessment and Geotechnical Recommendations for Subsurface Slab Abandonment, Proposed East Antelope Valley Animal Shelterıb by Converse Consultants (October 10, 2012) 

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## Converse Consultants

Over 50 Years of Dedication in Geotechnical Engineering and Environmental Sciences

October 10, 2012
Mr. Jason Kim
Capital Projects Manager
Los Angeles County Department of Public Works
900 N. Fremont Avenue
Alhambra, California 91803
Subject: Subsurface Slab Assessment
Contract No. PW 13460
Proposed East Antelope Valley Animal Shelter
38532, 38560, 38600 and 38624 Sierra Highway
APNs 3008-030-900 thru -905
Palmdale, California
Converse Project No. 11-41-140-02
Mr. Kim:
During previous investigative activities conducted by Converse Consultants (Converse) at the above referenced property (herein referred to as Site), refusal was encountered at boring location BH-13 at 11-feet below ground surface (bgs). Step-outs from location BH-13 were attempted several times, all of which also encountered refusal at 11 -feet bgs. On July 12, 2012, Converse Consultants excavated a trench to evaluate the subsurface feature causing the refusal. Converse excavated a trench approximately 30 -feet long by 3 -feet wide just north of location BH-13. A concrete slab was encountered in the excavation at the depth of 11 -feet bgs. Using a breaker, the slab was penetrated and found to be approximately 2 -feet in thickness with some wire reinforcing. Historical aerial photos show former structures in the location of the slab. On July 13, 2012, the trench was backfilled to grade using the removed material. The material was moisture conditioned and compacted to $90 \%$ maximum density using a sheep's foot wheel roller in accordance with the recommendations presented in Converse's Geotechnical Study Report, dated April 19, 2012. The backfill and compaction was observed and tested by Converse. A copy of the compaction test results is attached.

On July 16, 2012 Converse advanced 17 borings using a Geoprobe drill rig to delineate the extent of the slab. Borings were initially located midway between the trench and locations of previous borings that did not encounter refusal at 11-feet bgs (B-11, B-12, B-14, and B-16). Additional borings were then located between these borings until the extents of the slab had been determined to within a few feet between the trench location and those previous borings. The extents of the slab in other areas were inferred based on the extents of historic structures visible in the aerial photographs. It is noted that in the vicinity of previous location $\mathrm{BH}-11$, refusal was encountered at 4 -feet bgs, and it is suspected that a former wall may have been encountered. The probe holes were backfilled with hydrated bentonite and cold patched. It is noted that the excavation area is anticipated to be paved in the near future.

A figure showing the Site vicinity is attached as Figure 1. A figure indicating the approximate extents of the slab and trench, and previous boring locations is attached as Figure 2. In addition,
aerial photos showing the footprint of former structures with the approximate location of the slab superimposed are attached as Figures 3A and 3B.

Based on the above our geotechnical group reviewed the results and concluded that the slab should be perforated during construction. A copy of their letter report is attached.

## Closure

Thank you for this opportunity to be of service. Should you have questions regarding this report, please contact John Ziegler at (626) 930-1234, Michael Van Fleet at (626) 930-1267, or Norman Eke at (626) 930-1260.

Sincerely,



Michael Van Fleet, PG
Senior Geologist


Norman Eke
Managing Officer
Dist: 1/Addressee via Electronic Mail
Attch: Figures 1, 2, 3A and 3B
Compaction Test Results
Geotechnical Recommendations for Subsurface Slab Abandonment

## Figures



Map created with TOPO! © (92003 National Geographic (www.rationalgeographic.com'topo)

## SITE LOCATION MAP




## APPROXIMATE SLAB LOCATION



## FORMER SITE BUILDINGS

Converse Consultants

## Compaction Test Results

DAILY TIME SHEET AND FIELD REPORT NOTIFICATION OF HOURS I SERVICE DURING CONSTRUCTION


Project Name: $\qquad$
EST ANTELOPE VALLEY
Project No.:
Client: $\qquad$


Date:
 $\qquad$



$\qquad$






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Signature of Field Representative for Converse Consultants Full Name Printed NANCH R, Q=NルLK


| $\square$ Monrovia | TEL | $(626) 930-1200$ |
| :--- | :--- | :--- |
|  | FAX | $(626) 930-1212$ |
| $\square$ Redlands | TEL. | $(909) 796-0544$ |
|  | FAX | $(909) 796-7675$ |
| $\square$ Costa Mesa | TEL. | $(714) 444-9660$ |
|  | FAX | $(714) 444-9640$ |
| $\square$ Sacramento | TEL | $(916) 331-5444$ |
|  | FAX | $(916) 331-6444$ |

## FIELD DENSITY TEST RESULTS



*Sand Cone $=S \quad$ Nuclear Gauge $=N$
MAXIMUM DENSITY - OPTIMUM MOISTURE TESTS


## Geotechnical Recommendations for Subsurface Slab Abandonment

## Converse Consultants

Geotechnical Engineering, Environmental and Groundwater Science, Inspection and Testing Services
October 10, 2012

Mr. Jason Kim
Capital Projects Manager
Los Angeles County Department of Public Works
900 N. Fremont Avenue
Alhambra, California 91803

Subject: GEOTECHNICAL RECOMMENDATIONS FOR SUBSURFACE SLAB ABANDONMENT
Proposed East Antelope Valley Animal Shelter
38532, 38569, 38600 and 38624 Sierra Highway
APNs 3008-030-900 thru -905
Palmdale, California
Converse Project No. 11-41-140-02
Dear Mr. Kim:

Converse Consultants (Converse) has prepared this letter to present our geotechnical recommendations for abandonment of the subsurface slab encountered at the project site. In order to prepare this letter, Converse has reviewed the following documents:

- Subsurface Slab Assessment, Contract No. PW 13460, Proposed East Antelope Valley Animal Shelter, 38532, 38569, 38600 and 38624 Sierra Highway, APNs 3008-030-900 thru -905, Palmdale, California; by Converse, Project No. 11-41-140-02, dated July 18, 2012.
- Geotechnical Study Report, East Antelope Valley Animal Shelter, Palmdale, , California, by Converse, Project No. 12-31-145-01, dated April 19, 2012.

Based on our review of the above-listed reports, the subsurface concrete slab was about 2 feet thick situated at approximate 11 feet below ground surface. The inferred extents of the slab based on field exploration and historic aerial photograph were depicted on Figure No. 1. The existing subsurface concrete slab appears to be the abandoned basement slab of the previous building. Based on our review of researched building permits provided by LA County Public Works for the subject site, there are no grading/compaction records for the abandonment of this basement. Therefore, the following recommendations should be followed for basement abandonment:

1. We recommend drill or core 6-inch-diameter drain holes to penetrate the subsurface slab at 30 feet spacing. The drilled holes should be backfilled with $3 / 8$-inch pea gravel to about 2 feet above the subsurface concrete slab. The remaining drilled holes can be backfilled with the soil cuttings from drilling.
2. Since the extents of this abandoned subsurface slab is to be used as a surface paved parking lot and not intended for building structure, we recommend overexcavate at least the upper 2 feet of soil for pavement as recommended in our April 9, 2012 report. All compaction requirements presented in the April 92012 report should be followed.

We appreciate the opportunity to be of continued service to the Los Angeles County Department of Public Works. If you should have any questions, please do not hesitate to contact us at (626) 930-1200.

## CONVERSE CONSULTANTS



SCLIJZ

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> ATTACHMENT C
> DEPARTMENT OF PUBLIC WORKS:
> EAST ANTELOPE VALLEY ANIMAL CARE CENTER PROJECT ADOPT MITIGATED NEGATIVE DECLARATION AND MITIGATION MONITORING AND REPORTING PROGRAM
> APPROVE PROJECT AND BUDGET
> AWARD DESIGN-BUILD CONTRACT
> AUTHORIZE LOCAL WORKER HIRING PROGRAM
> APPROVE AND ORDER PUBLICATION OF NOTICE OF INTENTION TO PURCHASE REAL PROPERTY AND APPROVE RELATED ACTIONS
> SPECS. 7003; CAPITAL PROJECT NO. 69570
> NOTICE OF INTENTION TO PURCHASE REAL PROPERTY (SEE ATTACHMENT)

## NOTICE OF INTENTION

## TO PURCHASE REAL PROPERTY

NOTICE IS HEREBY GIVEN that it is the intention of the Board of Supervisors of the County of Los Angeles, State of California to purchase approximately 5.94 acres of undeveloped land (the "Real Property") located on the east side of the 38500 block of Sierra Highway, north of Avenue Q-6, in the City of Palmdale, County of Los Angeles, State of California for the sum of Twenty Thousand One Hundred Twenty Five Dollars $(\$ 20,125)$ from the fee simple owner, City of Palmdale (the "Seller"). It is the intent of the County to develop the Real Property with a new approximately 25,500 square feet indoor animal care center and associated site improvements to provide improved animal care and control services for the Antelope Valley. Due to space limitations in this notice, a complete legal description of the property being acquired by the County is available at the Chief Executive Office Real Estate Division at 222 S. Hill Street, 3rd Floor, Los Angeles, California, 90012.

NOTICE IS HEREBY GIVEN that the purchase of the Real Property will be consummated by the Board of Supervisors of the County of Los Angeles, State of California, on the $2\left(0^{\text {th }}\right.$ day of Mouember, 2013, at 9:30 a.m. in the Hearing Room of the Board of Supervisors, Room 381, Kenneth Hahn Hall of Administration, 500 West Temple Street, Los Angeles, California 90012. No obligation will arise against the County and in favor of the Seller with respect to the purchase of the Real Property described herein until the Board of Supervisors approves the purchase on the named consummation date.


SACHI A. HAMAI, Executive Officer Board of Supervisors, County of Los Angeles


APPROVED AS TO FORM:

## JOHN F. KRATTLI <br> County Counsel

By


## ATTACHMENT D

DEPARTMENT OF PUBLIC WORKS:
EAST ANTELOPE VALLEY ANIMAL CARE CENTER PROJECT ADOPT MITIGATED NEGATIVE DECLARATION AND MITIGATION MONITORING AND REPORTING PROGRAM

APPROVE PROJECT AND BUDGET
AWARD DESIGN-BUILD CONTRACT
AUTHORIZE LOCAL WORKER HIRING PROGRAM
APPROVE AND ORDER PUBLICATION OF NOTICE OF INTENTION TO PURCHASE REAL PROPERTY AND APPROVE RELATED ACTIONS SPECS. 7003; CAPITAL PROJECT NO. 69570

PURCHASE AND SALE AGREEMENT
(SEE ATTACHMENT)

THIS AGREEMENT FOR PURCHASE AND SALE OF REAL PROPERTY ("Agreement"), is made and entered into as of this 26th day of November , 2013, by and between Seller, CITY OF PALMDALE ("City"), and Buyer, COUNTY OF LOS ANGELES, a body politic and corporate ("County"), for acquisition by County of certain real property described below.

## RECITALS

A. City is the owner of certain real property located northeast of the junction of Sierra Highway and Avenue Q-6, on the east side of the 38500 block of Sierra Highway in the City of Palmdale, County of Los Angeles, State of California, as depicted in Exhibit A, site map, and described in Exhibit B, legal description, both attached hereto and incorporated herein by this reference ("Property").
B. The Property is comprised of approximately 5.94 acres of unimproved land, together with the existing appurtenant parking, all easements and interests appurtenant thereto, and all intangible property owned or held in connection with the Property, including without limitation, development rights, governmental approvals and land entitlements.
C. County desires to acquire the Property for the initial purpose of constructing an animal care facility and City desires to convey the Property in accordance with the terms and conditions contained herein.

## AGREEMENT

NOW THEREFORE, the parties hereto agree as follows:

1. Purchase and Sale. City agrees to sell to County, and County agrees to purchase from City, upon the terms and for the consideration set forth in this Agreement, the fee simple absolute interest in the Property.
2. Consideration. In consideration for City conveying the Property to County, County covenants to construct and operate an animal care facility within five (5) years from completion of the conveyance. As additional consideration, County shall make payment to City for the total sum of Twenty Thousand One Hundred Twenty-Five Dollars $(\$ 20,125.00)$ (Cash Payment). The Cash Payment shall be a one-time-only payment to the City as County's proportional share to contribute to City's maintenance and repair, in perpetuity, of the existing common driveway area that provides ingress and egress from Sierra Highway to the Property as indicated in the Common Driveway Easement (attached hereto as Exhibit D).

The consideration recited hereinabove shall constitute payment in full, and City hereby waives and releases County from any and all claims for further compensation, expenses and/or damages, arising from or connected with County's acquisition of the Property or its use, maintenance, and repair of the common driveway area.
3. Cash Payment. County shall pay the Cash Payment by delivering the Cash Payment into Escrow (as defined in Section 7) in immediately available funds prior to the Closing (as defined in Section 9), and as otherwise provided for in this Agreement.
4. Form of Grant Deed. Fee simple absolute title to the Property shall be conveyed by City to County as described in and by the grant deed attached hereto as Exhibit C ("Grant Deed"), duly executed and acknowledged by City, subject only to matters of record approved in writing by County pursuant to paragraph 5.02 below.
5. Contingencies. Completion of the transaction contemplated by this Agreement is contingent upon the following ("Contingencies"):

### 5.01 Approval of Purchase and Sale.

5.02.01 Approval of this Agreement by the County Board of Supervisors;
5.02.02 The County Board of Supervisors adopting a Notice of Intention to Purchase the Property; and
5.02.03 The County Board of Supervisors approving the purchase of the Property.
5.02 Condition of Title to Transfer Property. City shall cause the conveyance of title to the Property to County as evidenced by a C.L.T.A. Standard Policy of Title Insurance ("Title Policy"), to be purchased by County at its own cost and issued by Commonwealth Land Title Company (the "Title Company") insuring good and marketable title to the Property in County in an amount equal to the appraised value of the Property and subject only to matters approved in writing by County ("Approved Exceptions"). County may also, at its own cost, obtain extended title insurance coverage. The Title Policy shall show as exceptions only the Approved Exceptions. The exceptions to title shown on Schedule B of the issued Title Report and Title Company's standard printed exceptions shall be deemed to be the Approved Exceptions.
5.03 Refurbishment of City's ADA Parking Stalls. At County's sole cost and expense, County shall refurbish the ADA parking stalls, which are located outside the Property's southeast boundary and which service City's roller hockey rinks, to meet current building code requirements, including new asphalt paving, striping, signage, and wheel stops.
5.04 Dedication or Set-Aside for Road Right of Way. Both City and County agree to dedicate, or set aside to the other party as necessary, portions of their respective properties for road right-of-way purposes in order to create a new public sidewalk and right turn lane along Sierra Highway in connection with County's development project.
6. Non-Satisfaction of Contingencies. Upon non-satisfaction of any one of the above Contingencies, by mutual written agreement, the parties may extend the period within which a party is required to cure a non-satisfaction. Alternatively, either party may elect to terminate the transaction by providing termination notice to the other party. If the Agreement is terminated as set forth herein, neither of the parties shall have any liability to the other thereafter, except as expressly provided for in this Agreement.

## 7. Escrow.

7.01 Opening of Escrow. No later than ten (10) business days after the execution of this Agreement by all parties, the parties shall open an escrow ("Escrow") with Commonwealth Land Title Company, 888 S. Figueroa St., Suite 2100, Los Angeles, CA 90017 ("Escrow Holder"), as mutually selected by City and County for the purpose of consummating the purchase and sale of the Property. The parties shall execute and deliver to Escrow Holder, within ten (10) business days of receipt, such escrow instructions prepared by Escrow Holder as may be required to consummate the transaction contemplated by this Agreement. Any such instructions shall not conflict with, amend, or supersede any provisions of this Agreement. If there is any inconsistency between such instructions and this Agreement, this Agreement shall control unless the parties expressly agree otherwise in writing.
7.02 Escrow Authorization. Escrow Holder is authorized to:
7.02.01 Pay, and charge City, for any delinquent taxes, and penalties and interest thereon, and for any delinquent assessments or bonds against the Property,
7.02.02 County shall be responsible for title insurance costs, documentary transfer tax, and recording fees;
7.02.03 Pay, and charge County for the amount of all escrow fees;
7.02.04 When conditions of Escrow have been fulfilled by County and City: (1) record documents of conveyance; (2) disburse the Cash Payment to City, less proration and City's expenses; (3) deliver to County and City copies of the Escrow closing statements; and (4) deliver to County and City any items or documents given to Escrow Holder to hold for County and/or City.

## 8. Conditions to Closing.

8.01 County's Conditions. County's obligation to consummate the transaction contemplated by this Agreement is conditioned upon: (i) City's delivery of the Grant Deed to Escrow Holder and the recordation thereof in the County of Los Angeles Registrar-Recorder/County Clerk's official records; (ii) City's representations, warranties and covenants shall be true and correct as of Closing; and (iii) Title Company's irrevocable commitment to issue the Title Policy. Upon non-satisfaction of any one of the above conditions, County may either allow City an opportunity to cure or terminate the transaction by written notice to City of such termination. If this transaction is terminated as set forth herein, neither of the parties thereafter shall have any liability to the other except as expressly provided for in this Agreement. If County does not object to City's non-satisfaction of said conditions, they shall be deemed satisfied as of the Closing.
8.02 City's Conditions. City's obligation to consummate the transaction contemplated by this Agreement is conditioned upon: (i) County's deposit of the Cash Payment into Escrow no later than fifteen (15) business days before the closing of Escrow; (ii) that the Closing shall occur as set forth in Section 9. After non-satisfaction by County of one of the above conditions, City may either waive the time limitation set forth therein or terminate the transaction by written notice to County of such termination. If this transaction is terminated as set forth herein, neither of the parties thereafter shall have any liability to the other except as expressly provided for in this Agreement. If City does not object to County's non-satisfaction of said conditions, they shall be deemed satisfied as of the Closing.
9. Closing. For the purposes of this Agreement, the "Closing" or "Closing Date" shall be defined as the date on which the recordation of the Grant Deed in the Official Records occurs. The Closing shall occur no later than fifteen (15) business days after the date of the Board of Supervisors' order consummating the purchase contemplated hereby. The parties may agree in writing to extensions of the Closing if such extensions appear to either party to be necessary. If the Closing does not occur within a reasonable period of time or by any date agreed to by the parties in writing, either party, who is not then in default, may cancel this Agreement by delivering written notice of such cancellation to the other party and to Escrow Holder before Closing occurs.

If the Closing does not occur as indicated above, neither of the parties thereafter shall have any liability to the other except as expressly provided for in this Agreement.
10. Grant of Easements. The parties acknowledge and agree that title to the Property will be conveyed subject to the easements to be granted by the parties as described below.
10.01 Grant of Common Driveway Easement from City to County. City will grant to County, and County will accept, a common driveway easement as described and in the form of Exhibit D, attached hereto (Common Driveway Easement), duly executed and acknowledged by City, which shall be recorded upon consummation of the conveyance.
10.02 Grant of Landscape Easements from City to County. City will grant to County, and County will accept a landscape easement, as described and in the form of Exhibit E attached hereto (Landscape Easement), duly executed and acknowledged by City, both which shall be recorded upon consummation of the conveyance.
10.03 Grant of Access Easement from County to City. County will grant to City, and City will accept, an access easement as described and in the form of Exhibit F attached hereto (Access Easement), duly executed and acknowledged by County, which shall be recorded upon consummation of the conveyance.
11. Loss by Fire or Other Casualty. City shall maintain fire and casualty insurance on the Property in full force until the Closing Date. In the event that, prior to Closing, the Property or any part thereof, is destroyed or damaged, and the cost of repair or cure is $\$ 10,000$ or less, as reasonably determined by City, City shall repair or cure the loss to the reasonable satisfaction of County prior to Closing. If the cost of repair or cure is more than $\$ 10,000$, County shall have the right, exercisable by giving notice of such decision to City within fifteen (15) days after receiving written notice of such damage or destruction, to terminate this Agreement. If County elects to move forward with the sales transaction, said sales transaction shall close and any proceeds of insurance paid or payable to City by reason of such damage or destruction shall be paid or assigned to County.
12. Maintenance of the Property. During the period between the City's execution of this Agreement and the Closing, City shall maintain the Property as presently maintained.
13. Notices. All notices or other communications required or permitted hereunder shall be in writing, and shall be personally delivered or sent by registered or certified mail, postage prepaid, return receipt requested or by US Postal Service Express Mail or Federal Express to the following address:

To County:
County of Los Angeles
Chief Executive Office, Real Estate Division
222 South Hill Street, 3rd Floor
Los Angeles, California 90012
Attn: Christopher M. Montana Acting Director of Real Estate Division

To City:

City of Palmdale<br>38300 Sierra Highway, Ste. A<br>Palmdale, California 93550<br>Attn: Dave Childs, City Manager

Notice shall be deemed given on the day delivered by a carrier as specified above. Notice of change of address shall be given by written notice in the manner detailed in this Section.
14. Brokers. City represents and warrants to County, and County represents and warrants to City, that no broker or finder has been engaged by it in connection with the transaction contemplated by this Agreement. In the event of any claims for brokers' or finders' fees or commissions in connection with the negotiation, execution or consummation of this Agreement, County shall indemnify, hold harmless and defend City, from and against such claims if they are based upon or are alleged to be based upon any statement, representation or agreement by County, and City shall indemnify, hold harmless and defend County from and against such claims if they are based upon or are alleged to be based upon any statement, representation or agreement by City.
15. City's Representations and Warranties. In consideration of County entering into this Agreement and as an inducement to County to purchase the Property, City makes the following representations and warranties, each of which is material and is being relied upon by County, the truth and accuracy of which shall constitute a condition precedent to County's obligations hereunder. Each of the following representations and warranties shall be deemed to have been re-made as of the Closing.
15.01 Power. City has the legal power, right and authority to enter into this Agreement and the instruments referenced herein, and to consummate the transaction contemplated hereby.
15.02 Requisite Action. All requisite action has been taken by City in connection with entering into this Agreement and the instruments referenced herein, and, by the Closing, all such necessary action will have been taken to authorize the consummation of this transaction. By the Closing, no additional consent of any person or entity, judicial or administrative body, governmental authority or other party shall be required for City to consummate this transaction.
15.03 Individual Authority. The individuals executing this Agreement and the instruments referenced herein on behalf of City have the legal power, right and actual authority to bind City to the terms and conditions hereof and thereof.
15.04 Validity. This Agreement and all documents required hereby to be executed by City are and shall be valid, legally binding obligations of and enforceable against City in accordance with their terms, subject only to applicable bankruptcy, insolvency, reorganization, moratorium laws or similar laws or equitable principles affecting or limiting the right of contracting parties generally.
15.05 Violations. City has no present actual knowledge of any outstanding and uncured, written notice or citation from applicable governmental authorities of violation of any applicable codes, environmental zoning and land use laws, subdivision laws, and other applicable federal, state and local laws, regulations and ordinances, including, but not limited to, those relating to environmental conditions, hazardous materials or wastes, toxic materials or wastes or other similar materials or wastes regarding the Property.
15.06 Litigation. City has no present actual knowledge of any litigation pending or threatened against City on any basis therefor that arises out of the ownership of the Property or that might detrimentally affect the Property or adversely affect the ability of City to perform its obligations under this Agreement.
16. County's Representations and Warranties. In consideration of City entering into this Agreement and as an inducement to City to sell the Property, County makes the following representations and warranties, each of which is material and is being relied upon by City, the truth and accuracy of which shall constitute a condition precedent to City's obligations hereunder. Each of the following representations and warranties shall be deemed to have been re-made as of the Closing.
16.01 Power. County has the legal power, right and authority to enter into this Agreement and the instruments referenced herein, and to consummate the transaction contemplated hereby.
16.02 Requisite Action. All requisite action has been taken by County in connection with entering into this Agreement and the instruments referenced herein, and, by the Closing, all such necessary action will have been taken to authorize the consummation of this transaction. By the Closing, no additional consent of any person or entity, judicial or administrative body, governmental authority or other party shall be required for County to consummate this transaction.
16.03 Individual Authority. The individuals executing this Agreement and the instruments referenced herein on behalf of County have the legal power, right and actual authority to bind County to the terms and conditions hereof and thereof.
16.04 Validity. This Agreement and all documents required hereby to be executed by County are and shall be valid, legally binding obligations of and enforceable against County in accordance with their terms, subject only to applicable bankruptcy, insolvency, reorganization, moratorium laws or similar laws or equitable principles affecting or limiting the right of contracting parties generally.

## 17. Inspection of the Site.

17.01 Access. City agrees to provide County and/or County's employees, representatives and agents with access to the Property, upon reasonable notice, to conduct any inspections County deems appropriate at any time prior to the Closing.
17.02 Testing. County shall not engage in any destructive, intrusive, or invasive testing during any inspection of the Property, without the prior written consent of City, which consent shall not unreasonably be withheld.
18. Condition of Property. AS IS: (i) With the exception of Section 15 hereof, there are no representations or warranties of any kind whatsoever, express or implied, made by City in connection with this Agreement, the purchase of the Property by County, the physical condition of the Property or whether the Property complies with applicable laws or is appropriate for County's intended use; (ii) County has (or has chosen not to have) investigated the Property and all matters pertaining thereto including, without limitation, the environmental condition of the Property; (iii) County is not relying on any statement or representation of City, its agents or its representatives except for the express representations and warranties set forth in Section 15 hereof; (iv) County, in entering into this Agreement and in completing its purchase of the Property, is relying on its own investigation of the Property (except for the express representations and warranties set forth in Section 15 hereof) and based on its knowledge of real property in the areas where the Property is located; (v) County is aware of all zoning regulations, other governmental requirements, site and physical conditions, and other matters affecting the use and condition of the Property; (vi) County's decision to purchase the Property on the terms and conditions hereof is made solely and exclusively in reliance on County's own review, inspection and investigation of the Property except for the express representations and warranties set forth in Section 15 hereof; and (vii) County shall purchase the Property in its "as is" condition as of the date of the Closing Date.
19. Indemnity. City shall defend, indemnify, and hold County and its elected and appointed officers, agents and employees free and harmless from and against any and all liabilities, damages, claims, costs and expenses (including without limitation, attorneys' fees, legal expenses and consultants' fees) related to or arising in whole or in part from the removal, eviction, vacation, or relocation of any occupant(s) of the Property, residing on the Property at any time prior to the Closing.
20. Survival of Covenants. The covenants, indemnities, agreements, representations and warranties made herein are intended to survive, for a period of one year, the Closing and recordation and delivery of the Grant Deed conveying the Property to County.
21. Required Actions of County and City. County and City agree to execute all such instruments and documents, and to take all actions pursuant to the provisions hereof, in order to complete this transaction and shall use their best efforts to effect the Closing in accordance with the provisions hereof.
22. Entire Agreement. This Agreement contains the entire agreement between the parties hereto and no addition or modification of any term or provision shall be effective unless set forth in writing, signed by both City and County.
23. California Law. This Agreement shall be construed in accordance with the internal laws of the State of California.
24. Waivers. No waiver by either party of any provision hereof shall be deemed a waiver of any other provision hereof or of any subsequent breach by either party of the same or any other provision.
25. Captions. The captions and the section and subsection numbers appearing in this Agreement are inserted only as a matter of convenience and in no way define, limit, construe or describe the scope or intent of such sections of this Agreement nor in any way affect this Agreement.
26. Interpretation. Unless the context of this Agreement clearly requires otherwise, (i) the plural and singular numbers shall be deemed to include the other; (ii) the masculine, feminine and neuter genders shall be deemed to include the others;(iii) "or" is not exclusive; and (iv) "includes" and "including" are not limiting.
27. Severability. Any provision of this Agreement which shall prove to be invalid, void or illegal shall in no way affect, impair or invalidate any other provision hereof and such other provisions shall remain in full force and effect.
28. Delegation of Authority. The Los Angeles County Board of Supervisors on behalf of County hereby delegates to its Chief Executive Officer or his designee, the authority to issue any and all approvals required by this Agreement and to execute any and all instruments necessary to consummate or complete this transaction.
29. Binding Effect. The provisions of this Agreement shall be binding upon the parties hereto and their respective successors-in-interest.
30. No Presumption Re: Drafter. The parties acknowledge and agree that the terms and provisions of this Agreement have been negotiated and discussed between the parties and their attorneys, and this Agreement reflects their mutual agreement regarding the same. Because of the nature of such negotiations and discussions, it would be inappropriate to deem any party to be the drafter of this Agreement, and therefore, no presumption for or against validity or as to any interpretation hereof, based upon the identity of the drafter shall be applicable in interpreting or enforcing this Agreement.
31. Assistance of Counsel. Each party hereto either had the assistance of counsel or had counsel available to it, in the negotiation for, and the execution of, this Agreement, and all related documents.
l 1 / SIGNATURE PAGE FOLLOWS $/$ / 1

IN WITNESS WHEREOF, CITY OF PALMDALE has executed this Agreement or caused it to be duly executed and this Agreement has been executed by the Chairman of the Los Angeles County Board of Supervisors on the day, month, and year first above written.

CITY OF PALMDALE:

$B y:$

James C. Ledford, Jr., Mayor

ATTEST:


By:
Rebecca J. Smith, City Clerk

## APPROVED AS TO FORM:



By:
Wm. Matthew Ditzhazy
City Attorney

## COUNTY OF LOS ANGELES:

a body politic and corporate


By:- aChillesmithumar
DKPux

## APPROVED AS TO FORM:

JOHN F. KRATTLI
County Counsel
$B y$ :


I hereby certify that pursuant to
Section 25103 of the Government Code, deliver ........hen made

NOV 26 2ก13

$$
\begin{aligned}
& \text { Such U. Hamal } \\
& \text { SACHIA. HAMAS } \\
& \text { EXECUTIVE OFFICER }
\end{aligned}
$$

SAC
Executive Office:
Clerk of the Board of Supervisors


IN WITNESS WHEREOF, CITY OF PALMDALE has executed this Agreement or caused it to be duly executed and this Agreement has been executed by the Chairman of the Los Angeles County Board of Supervisors on the day, month, and year first above written.

CITY OF PALMDALE:


ATTEST:

By: Rovanne Faber D.C.C. GorRebecca J. Smith, Cíty Clerk

## APPROVED AS TO FORM:

By:


COUNTY OF LOS ANGELES: a body politic and corporate

By:
Chairman, Board of Supervisors

## ATTEST:

SACHI A. HAMAI, Executive Officer Board of Supervisors

By: $\qquad$

## APPROVED AS TO FORM:

JOHN F. KRATTLI
County Counsel
$B y:$
Deputy

## LIST OF EXHIBITS

A. SITE MAP
B. LEGAL DESCRIPTION FEE PARCEL
C. GRANT DEED
D. COMMON DRIVEWAY EASEMENT
E. LANDSCAPE EASEMENT
F. ACCESS EASEMENT

## EXHIBIT A

## SITE MAP



## EXHIBIT B

## LEGAL DESCRIPTION FEE PARCEL

## EXHIBIT A

Being all of Block 12 and a portion of Block 13 of the Town and Suburbs of Palmdale, in the City of Palmdale, County of Los Angeles, State of California, as per map recorded in Book 52, Pages 55 and 56 of Miscellaneous Records, in the Office of the County Recorder of said County described in its entirety as follows:

Beginning at the intersection of the Westerly line of said Block 13, with a line that is parallel with and distant Northerly at right angles, 309.50 feet, from the North line of Avenue Q-6, formerly Walnut Street, 80 feet wide, as shown on said map;

Thence North $89^{\circ} 21^{\prime} 59^{\prime \prime}$ East along said parallel line, a distance of 229.20 feet;

Thence North $0^{\circ} 02^{\prime} 59^{\prime \prime}$ West, a distance of 103.39 feet to the beginning of a tangent curve, concave easterly and having a radius of 18.00 feet;

Thence northerly along said curve, through a central angle of $28^{\circ} 52^{\prime} 29^{\prime \prime}$ an arc length of 9.07 feet;

Thence non-tangent to last said curve, North $89^{\circ} 55^{\prime} 36^{\prime \prime}$ East, a distance of 89.92 feet;

Thence North $0^{\circ} 53^{\prime} 15^{\prime \prime}$ West, a distance of 17.13 feet;
Thence North $89^{\circ} 21^{\prime} 59^{\prime \prime}$ East, a distance of 36.32 feet;
Thence North $0^{\circ} 53^{\prime} 15^{\prime \prime}$ West, a distance of 38.80 feet;
Thence North $89^{\circ} 06^{\prime} 45^{\prime \prime}$ East, a distance of 3.00 feet to the easterly line of said Block 13;

Thence North $0^{\circ} 53^{\prime} 15^{\prime \prime}$ West along said easterly line, and along the easterly line of said Block 12, a distance of 515.46 feet to the northeasterly corner of said Block 12;

Thence South $89^{\circ} 21^{\prime} 56^{\prime \prime}$ West along the northerly line thereof, a distance of 441.39 feet to the northwesterly corner of said Block 12;

Thence South $7^{\circ} 29^{\prime} 32^{\prime \prime}$ East along the westerly line of said Block 12 and the westerly line of said Block 13, a distance of 687.48 feet to the point of beginning.

Containing 5.940 acres, more or less.
Subject to easements, covenants, conditions, and restrictions of record, if any.

As shown on Exhibit A-1, attached hereto and by this reference made a part hereof.

Prepared by me or under my supervision.




North: 8452.5557 East: 10626.0588
Line Course: N 00-53-15 W Length: 515.46
North: 8967.9539 East: 10618.0748
Line Course: S 89-21-56 W Length: 441.39
North: 8963.0664 East : 10176.7118
Line Course: S 07-29-32 E Length: 687.48
North: 8281.4557 East : 10266.3534
Line Course: N 89-21-59 E Length: 229.20
North: 8283.9903 East: 10495.5394
Line Course: N 00-02-59 W Length: 103.39
North: 8387.3803 East: 10495.4497
Curve Length: 9.07 Radius: 18.00
Delta: 28-52-29 Tangent: 4.63
Chord: 8.98 Course: N 14-23-16E
Course In: N 89-57-01 E Course Out: N 61-10-30 W
RP North: 8387.3959 East : 10513.4497
End North: 8396.0743 East : 10497.6800
Line Course: N 89-55-36 E Length: 89.92
North: 8396.1894 East: 10587.5999
Line Course: N 00-53-15 W Length: 17.13
North: 8413.3174 East : 10587.3346
Line Course: N 89-21-59 E Length: 36.32
North: 8413.7190 East : 10623.6523
Line Course: N 00-53-15 W Length: 38.80
North: 8452.5143 East: 10623.0514
Line Course: N 89-06-45 E Length: 3.00
North: 8452.5608 East: 10626.0510
Perimeter: 2171.15 Area: 258,754 sq.ft. 5.94 acres
Mapcheck Closure - (Uses listed courses, radii, and deltas)
Error Closure: 0.0093 Course: N 56-53-36 W
Error North: 0.00510 East : -0.00782
Precision 1: 233,458.06

## EXHIBIT C

## GRANT DEED

## GRANT DEED

## RECORDING REQUESTED BY COUNTY OF LOS ANGELES

WHEN RECORDED MAIL TO:
County of Los Angeles
222 South Hill Street, 3rd Floor
Los Angeles, CA 90012
Attention: Christopher M. Montana

Space above this line for Recorders use

THIS DOCUMENT IS EXEMPT FROM DOCUMENTARY TRANSFER TAX PURSUANT TO SECTION 11922 OF THE REVENUE \& TAXATION CODE

THIS DOCUMENT IS EXEMPT FROM RECORDING FEES PURSUANT TO SECTION 27383 OF THE GOVERNMENT CODE

ASSESSOR'S IDENTIFICATION NUMBER 3008-030-900; 3008-030-901; 3008-030-902; 3008-030-903 (Portion); 3008-033-904; 3008-033-905 (Portion) and 3008-033-906

## GRANT DEED

FOR A VALUABLE CONSIDERATION, receipt of which is hereby acknowledged, the CITY OF PALMDALE (hereinafter called "CITY"), does hereby grant to the COUNTY OF LOS ANGELES COUNTY, a body politic and corporate, all of the CITY's rights, title and interests to that certain real property in the City of Palmdale, County of Los Angeles, State of California, legally described in Exhibit A and depicted in Exhibit A-1, attached hereto and incorporated herein by this reference.

## SUBJECT TO:

1. All taxes, penalties and assessments of record, if any.
2. Covenants, conditions, restrictions, reservations, easements, rights, and rights-ofway, if any.

Dated


CITY OF PALMDALE




Place Notary Seal Above
who proved to me on the basis of satisfactory evidence to be the persons) whose names) is/are subscribed to the within instrument and acknowledged to me that he/shefthey executed the same in his/hertheir authorized capacity(ies), and that by his/her/their signature (s) on the instrument the persons), or the entity upon behalf of which the person (s) acted, executed the instrument.

I certify under PENALTY OF PERJURY under the laws of the State of California that the foregoing paragraph is true and correct.

WITNESS my hand and official seal.

Signature:


OPTIONAL
Though the information below is not required by law, it may prove valuable to persons relying on the document and could prevent fraudulent removal and reattachment of this form to another document.

## Description of Attached Document

Title or Type of Document: $\qquad$
Document Date: $\qquad$ Number of Pages: $\qquad$
Signers) Other Than Named Above:

## Capacity(ies) Claimed by Signers)


-

## EXHIBIT A

Being all of Block 12 and a portion of Block 13 of the Town and Suburbs of Palmdale, in the City of Palmdale, County of Los Angeles, State of California, as per map recorded in Book 52, Pages 55 and 56 of Miscellaneous Records, in the Office of the County Recorder of said County described in its entirety as follows:

Beginning at the intersection of the Westerly line of said Block 13, with a line that is parallel with and distant Northerly at right angles, 309.50 feet, from the North line of Avenue Q-6, formerly Walnut Street, 80 feet wide, as shown on said map;

Thence North $89^{\circ} 21^{\prime} 59^{\prime \prime}$ East along said parallel line, a distance of 229.20 feet;

Thence North $0^{\circ} 02^{\prime} 59^{\prime \prime}$ West, a distance of 103.39 feet to the beginning of a tangent curve, concave easterly and having a radius of 18.00 feet;

Thence northerly along said curve, through a central angle of $28^{\circ} 52^{\prime} 29^{\prime \prime}$ an arc length of 9.07 feet;

Thence non-tangent to last said curve, North $89^{\circ} 55^{\prime} 36^{\prime \prime}$ East, a distance of 89.92 feet;

Thence North $0^{\circ} 53^{\prime} 15^{\prime \prime}$ West, a distance of 17.13 feet;
Thence North $89^{\circ} 21^{\prime} 59^{\prime \prime}$ East, a distance of 36.32 feet;
Thence North $0^{\circ} 53^{\prime} 15^{\prime \prime}$ West, a distance of 38.80 feet;
Thence North $89^{\circ} 06^{\prime} 45^{\prime \prime}$ East, a distance of 3.00 feet to the easterly line of said Block 13;

Thence North $0^{\circ} 53^{\prime} 15^{\prime \prime}$ West along said easterly line, and along the easterly line of said Block 12, a distance of 515.46 feet to the northeasterly corner of said Block 12;

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Thence South $7^{\circ} 29^{\prime} 32^{\prime \prime}$ East along the westerly line of said Block 12 and the westerly line of said Block 13, a distance of 687.48 feet to the point of beginning.

Containing 5.940 acres, more or less.
Subject to easements, covenants, conditions, and restrictions of record, if any.

As shown on Exhibit A-1, attached hereto and by this reference made a part hereof.

Prepared by me or under my supervision.




North: 8452.5557 East : 10626.0588
Line Course: N 00-53-15 W Length: 515.46
North: 8967.9539 East: 10618.0748
Line Course: S 89-21-56 W Length: 441.39
North: 8963.0664 East: 10176.7118
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Curve Length: 9.07 Radius: 18.00
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Chord: $8.98 \quad$ Course: N 14-23-16E
Course In: N 89-57-01 E Course Out: N 61-10-30 W
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Line Course: N 89-21-59 E Length: 36.32
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Line Course: N 00-53-15 W Length: 38.80
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Line Course: N 89-06-45 E Length: 3.00
North: 8452.5608 East: 10626.0510
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Error Closure: 0.0093 Course: N 56-53-36 W
Error North: 0.00510 East : -0.00782
Precision 1: 233,458.06

COMMON DRIVEWAY EASEMENT

# RECORDING REQUESTED BY COUNTY OF LOS ANGELES <br> WHEN RECORDED MAIL TO: 

County of Los Angeles
Real Estate Division
222 South Hill Street, 3rd Floor
Los Angeles, CA 90012
Attention: Director of Real Estate

Space above this line for Recorders use

THIS DOCUMENT IS EXEMPT FROM DOCUMENTARY TRANSFER TAX PURSUANT TO SECTION 11922 OF THE REVENUE \& TAXATION CODE

THIS DOCUMENT IS EXEMPT FROM RECORDING FEES PURSUANT TO SECTION 27383 OF THE GOVERNMENT CODE

ASSESSOR'S IDENTIFICATION NUMBER 3008-033-907 (Portion) 3008-033-906 (Portion) 3008-033-905 (Portion)

## COMMON DRIVEWAY EASEMENT

For and in consideration of the mutual promises contained herein and other good and valuable consideration, the receipt and sufficiency of which is hereby acknowledged by the parties, the parties agree as follows:

The CITY OF PALMDALE (CITY), does hereby grant and convey to the COUNTY OF LOS ANGELES (COUNTY), a body politic and corporate, a perpetual, non-exclusive, Common Driveway Easement for vehicular ingress and egress purposes, and those appurtenances and uses commonly associated therewith, on, over, upon, and across that certain portion of CITY's real property situated in the City of Palmdale, County of Los Angeles, State of California, legally described on Exhibit A and depicted on Exhibit A-1, attached hereto and made a part hereof by this reference (Easement Area).

CITY covenants and agrees, on behalf of itself and its successors in interest that CITY shall be the sole responsible party to maintain and to keep the Easement Area in good order and repair in perpetuity. For all purposes of this Easement, the terms maintain and repair shall mean, without limitation, applying a slurry coat seal to the surface on and around the Easement Area every five (5) years, and all other necessary work required to maintain the Easement Area in a condition that will allow for reasonable and safe vehicular access.

In the event that CITY fails in any material respect to perform its maintenance and repair obligations as stated herein with reasonable diligence, COUNTY shall have the right, if such failure has continued for period of thirty (30) days after written notice thereof to CITY, to enter on and around the Easement Area and perform such maintenance and repair.

All reasonable maintenance expenses incurred by COUNTY in connection with the performance of such maintenance and repair of the Easement Area shall be paid by CITY within thirty (30) days after presentation of a written invoice for such expenses by COUNTY.

COUNTY agrees to defend, indemnify and hold harmless CITY, its officers, agents and employees, from and against any and all actions, demands, claims, liabilities, damages, losses, costs and expenses of every kind, nature and character, including but not limited to reasonable attorneys' and experts' fees, that arise in whole or in part from, or out of or in connection with COUNTY's use of or presence on the Easement Area.

All of the terms, covenants, conditions, and obligations set forth in this Common Driveway Easement shall inure to the benefit of and bind CITY and COUNTY, and their respective representatives, heirs, successors, transferees and assigns, and shall continue as a servitude running in perpetuity with CITY's property.

Dated


## CITY OF PALMDALE



Dated
NOV 262013

ATTEST: SACHIA. HAMA
EXECUTIVE OFFICER
CLERK OF THE BOARD OF SUPERVISORS


COUNTY OF LOS ANGELES a body politic and corporate


Chairman, Board of Supervisors
Los Angeles County



Place Notary Seal Above
who proved to me on the basis of satisfactory evidence to be the person(s) whose name(s) is/are subscribed to the within instrument and acknowledged to me that he/she/they executed the same in his/hortheir authorized capacity(ies), and that by his/hertheir signature(s) on the instrument the person(s), or the entity upon behalf of which the person(s) acted, executed the instrument.

I certify under PENALTY OF PERJURY under the laws of the State of California that the foregoing paragraph is true and correct.

WITNESS my hand and official seal.

Signature:


OPTIONAL
Though the information below is not required by law, it may prove valuable to persons relying on the document and could prevent fraudulent removal and reattachment of this form to another document.

## Description of Attached Document

Title or Type of Document: $\qquad$
Document Date: $\qquad$ Number of Pages: $\qquad$
Signer(s) Other Than Named Above:
Capacity(ies) Claimed by Signer(s)

Signer's Name:

| $\square$ Individual | RIGHT THUMBPRINT OF SICNER |
| :---: | :---: |
| $\square$ Partner - $\square$ Limited $\square$ General | Top of thumb here |
| $\square$ Attorney in Fact |  |
| $\square$ Trustee |  |
| $\square$ Guardian or Conservator |  |
| $\square$ Other: |  |
| Signer Is Representing: |  |


| Signer's Name: |
| :--- |
| $\square$ Corporate Officer - Title(s):_ |
| $\square$ Individual |
| $\square$ Partner $-\square$ Limited $\square$ GeneralRIGFITHUMBPRINT <br> of SICNER |
| $\square$ Attorney in Fact |
| $\square$ Trustee |
| $\square$ Guardian or Conservator |
| $\square$ Other: |

[^16]
## EXHIBIT A

Being a portion of Block 13 of the Town and Suburbs of Palmdale, in the City of Palmdale, County of Los Angeles, State of California, as per map recorded in Book 52, Pages 55 and 56 of Miscellaneous Records, in the Office of the County Recorder of said County described in its entirety as follows:

Commencing at the intersection of the Westerly line of said Block 13, with a line that is parallel with and distant Northerly at right angles, 309.50 feet, from the North line of Avenue Q-6, formerly Walnut Street, 80 feet wide, as shown on said map;

Thence North $89^{\circ} 21^{\prime} 59^{\prime \prime}$ East along said parallel line, a distance of 59.36 feet to the True Point of Beginning;

Thence continuing North $89^{\circ} 21^{\prime \prime} 59^{\prime \prime}$ East along said parallel line, a distance of 169.84 feet;

Thence South $0^{\circ} 38^{\prime} 07^{\prime \prime}$ East, a distance of 58.00 feet;
Thence South $89^{\circ} 21^{\prime} 59^{\prime \prime}$ West, a distance of 165.34 feet;
Thence South $86^{\circ} 47^{\prime} 57^{\prime \prime}$ West, a distance of 35.08 feet to the beginning of a tangent curve, concave southeasterly and having a radius of 20.00 feet;

Thence southwesterly along said curve, through a central angle of $94^{\circ} 17^{\prime} 29^{\prime \prime}$ an arc length of 32.91 feet to the westerly line of said Block 13;

Thence North $7^{\circ} 29^{\prime} 32^{\prime \prime}$ West along said westerly line, a distance of 66.72 feet to a point in a non-tangent curve, concave northerly and having a radius of 20.36 feet, a radial line to said point bears South $38^{\circ} 02^{\prime} 25^{\prime \prime}$ West;

Thence easterly along said curve through a central angle of $37^{\circ} 43^{\prime} 48^{\prime \prime}$ an arc length of 13.41 feet;

Thence tangent to last said curve, South $89^{\circ} 41^{\prime} 22^{\prime \prime}$ East, a distance of 22.77 feet to the beginning of a tangent curve, concave northwesterly and having a radius of 22.00 feet;

Thence northeasterly along said curve, through a central angle of $87^{\circ} 08^{\prime} 03^{\prime \prime}$ an arc length of 33.46 feet to the True Point of Beginning.

Containing 12,200 square feet, more or less.
Subject to easements, covenants, conditions, and restrictions of record, if any.

As shown on Exhibit A-1, attached hereto and by this reference made a part hereof.

Prepared by me or under my supervision.



Parcel name: DW2 access esmt

North: 8224.1663 East: 10330.8551


Line Course: S 86-47-57 W Length: 35.08
North: 8222.2076 East : 10295.8298
Curve Length: 32.91
Radius: 20.00
Delta: 94-17-29
Tangent: 21.56
Chord: 29.32
Course: S 39-39-12 W
Course In: S 03-12-03 E Course Out: S 82-30-28 W
RP North: 8202.2388 East : 10296.9465
End North: 8199.6310 East: 10277.1173
Line Course: N 07-29-32 W Length: 66.72
North: 8265.7813 East : 10268.4176
Curve Length: 13.41 Radius: 20.36
Delta: 37-43-47 Tangent: 6.96
Chord: 13.17 Course: S 70-49-29 E
Course In: N 38-02-25 E Course Out: S 00-18-38 W
RP North: 8281.8164 East : 10280.9637
End North: 8261.4567 East: 10280.8533
Line Course: S 89-41-22 E Length: 22.77
North: 8261.3333 East: 10303.6230
Curve Length: 33.46 Radius: 22.00
Delta: 87-08-04 Tangent: 20.93
Chord: $30.32 \quad$ Course: N 46-44-36 E
Course In: N 00-18-38 E Course Out: S 86-49-26 E
RP North: 8283.3330 East : 10303.7423
End North: 8282.1141 East: 10325.7085
Line Course: N 89-21-59 E Length: 169.84
North: 8283.9922 East: 10495.5381
Line Course: S 00-38-07 E Length: 58.00
North: 8225.9958 East: 10496.1812
Line Course: S 89-21-59 W Length: 165.34
North: $8224.1674 \quad$ East: 10330.8513

Perimeter: 597.53 Area: 12,200 sq.ft. 0.28 acres

Mapcheck Closure - (Uses listed courses, radii, and deltas)
Error Closure: 0.0040 Course: N 74-16-30 W
Error North: 0.00108 East : -0.00383
Precision 1: 149,382.50

LANDSCAPE EASEMENT

# RECORDING REQUESTED BY COUNTY OF LOS ANGELES 

WHEN RECORDED MAIL TO:
County of Los Angeles
Real Estate Division
222 South Hill Street, 3rd Floor
Los Angeles, CA 90012
Attention: Director of Real Estate

Space above this line for Recorders use

THIS DOCUMENT IS EXEMPT FROM DOCUMENTARY TRANSFER TAX PURSUANT TO SECTION 11922 OF THE REVENUE \& TAXATION CODE

ASSESSOR'S IDENTIFICATION NUMBER 3008-033-907 (Portion)

THIS DOCUMENT IS EXEMPT FROM RECORDING FEES PURSUANT TO SECTION 27383 OF THE GOVERNMENT CODE

## LANDSCAPE EASEMENT

For and in consideration of the mutual promises contained herein and other good and valuable consideration, the receipt and sufficiency of which is hereby acknowledged by the parties, the parties agree as follows:

The CITY OF PALMDALE (CITY), does hereby grant and convey to the COUNTY OF LOS ANGELES (COUNTY), a body politic and corporate, a perpetual, non-exclusive, Landscape Easement to plant, maintain, replace, or remove landscaping and install irrigation-watering systems in, upon, over, under and across that certain portion of CITY's real property situated in the City of Palmdale, County of Los Angeles, State of California, legally described on Exhibit A and depicted on Exhibit A-1, attached hereto and made a part hereof by this reference (Easement Area).

Together with the right to enter upon and to pass and repass over and along the Easement Area to deposit tools, implements and other materials thereon by COUNTY, its officers, agents and employees and by any contractor, his agents and employees engaged by COUNTY, whenever and wherever necessary for the purposes set forth above.

All of the terms, covenants, conditions, and obligations set forth in this Landscape Easement shall inure to the benefit of and bind CITY and COUNTY, and their respective representatives, heirs, successors, transferees and assigns, and shall continue as a servitude running in perpetuity with CITY's property.

Dated



who proved to me on the basis of satisfactory evidence to be the person(s) whose name(s) is/are subscribed to the within instrument and acknowledged to me that he/she7they executed the same in his/her/their authorized capacity(ies), and that by his/hor Itheir signature(s) on the instrument the person(s), or the entity upon behalf of which the person(s) acted, executed the instrument.

I certify under PENALTY OF PERJURY under the laws of the State of California that the foregoing paragraph is true and correct.

WITNESS my hand and official seal.
Signature:


Though the information below is not required by law, it may prove valuable to persons relying on the document and could prevent fraudulent removal and reatlachment of this form to another document.
Description of Attached Document
Title or Type of Document: $\qquad$
Document Date: $\qquad$ Number of Pages: $\qquad$
Signer(s) Other Than Named Above: $\qquad$ Capacity(ies) Claimed by Signer(s)

Signer's Name:
$\square$ Corporate Officer - Title(s)
$\square$ Individual
$\square$ Partner - $\square$ Limited $\square$ General
$\square$ Attorney in Fact
$\square$ Trustee
$\square$ Guardian or Conservator
$\square$ Other: $\qquad$

Signer Is Representing: $\qquad$


Signer's Name:

| $\square$ Individual | RIGHT TFUMBPRINT OF SIGNER |
| :---: | :---: |
| $\square$ Partner - $\square$ Limited $\square$ General | Top of thumb here |
| $\square$ Attorney in Fact |  |
| [] Trustee |  |
| $\square$ Guardian or Conservator |  |
| [] Other: |  |
| Signer Is Representing: |  |

## EXHIBIT A

Being a portion of Block 13 of the Town and Suburbs of Palmdale, in the City of Palmdale, Country of Los Angeles, State of California, as per map recorded in Book 52, Pages 55 and 56 of Miscellaneous Records, in the Office of the County Recorder of said County described in its entirety as follows:

Beginning at the intersection of the Westerly line of said Block 13, with a line that is parallel with and distant Northerly at right angles, 309.50 feet, from the North line of Avenue Q-6, formerly Walnut Street, 80 feet wide, as shown on said map;

Thence North $89^{\circ} 21^{\prime} 59^{\prime \prime}$ East along said parallel line, a distance of 59.36 feet to the a point in a non-tangent curve, concave northwesterly and having a radius of 22.00 feet, a radial line to said point bears South $86^{\circ} 49^{\prime} 26^{\prime \prime}$ East;

Thence southwesterly along said curve through a central angle of $87^{\circ} 08^{\prime} 03^{\prime \prime}$ an arc length of 33.46 feet;

Thence tangent to last said curve North $89^{\circ} 41^{\prime} 22^{\prime \prime}$ West, a distance of 22.77 feet to the beginning of a tangent curve, concave northerly and having a radius of 20.36 feet;

Thence westerly along said curve through a central angle of $37^{\circ} 43^{\prime} 48^{\prime \prime}$ an arc length of 13.41 feet to the aforesaid westerly line of Block 13;

Thence North $7^{\circ} 29^{\prime} 32^{\prime \prime}$ West along said westerly line, a distance of 15.81 feet to the point of beginning.

Containing 1,065 square feet, more or less.
Subject to easements, covenants, conditions, and restrictions of record, if any.

As shown on Exhibit A-1, attached hereto and by this reference made a part hereof.

Prepared by me or under my supervision.
 Expiration 12-31-2014



Parcel name: LS esmt
North: 8261.3323
Curve Length: 33.46
Delta: 87-08-04
Chord: 30.32
East : 10303.6307
Radius: 22.00
Tangent: 20.93
Course: N 46-44-36 E
Course In: N 00-18-38 E Course Out: S 86-49-26 E
RP North: 8283.3320 East: 10303.7499
End North: 8282.1131 East: 10325.7161
Line Course: S 89-21-59 W Length: 59.36
North: 8281.4566 East: 10266.3598
Line Course: S 07-29-32 E Length: 15.81
North: 8265.7816 East: 10268.4213
Curve Length: 13.41 Radius: 20.36
Delta: 37-43-47 Tangent: 6.96
Chord: 13.17 Course: S 70-49-29 E
Course In: N 38-02-25 E Course Out: S 00-18-38 W
RP North: 8281.8167 East: 10280.9674
End North: 8261.4570 East: 10280.8570
Line Course: S 89-41-22 E Length: 22.77
North: 8261.3336 East: 10303.6267
Perimeter: 144.81 Area: 1,065 sq.ft. 0.02 acres
Mapcheck Closure - (Uses listed courses, radii, and deltas)
Error Closure: 0.0042 Course: N 72-10-10 W
Error North: 0.00128 East: -0.00397
Precision 1: 34,478.57

## EXHIBIT F

## ACCESS EASEMENT

# RECORDING REQUESTED BY COUNTY OF LOS ANGELES <br> WHEN RECORDED MAIL TO: 

County of Los Angeles
Real Estate Division
222 South Hill Street, 3rd Floor
Los Angeles, CA 90012
Attention: Director of Real Estate

Space above this line for Recorders use

THIS DOCUMENT IS EXEMPT FROM DOCUMENTARY TRANSFER TAX PURSUANT TO SECTION 11922 OF THE REVENUE \& TAXATION CODE

ASSESSOR'S IDENTIFICATION NUMBER 3008-033-901 (Portion)

THIS DOCUMENT IS EXEMPT FROM RECORDING FEES PURSUANT TO SECTION 27383 OF THE GOVERNMENT CODE

## ACCESS EASEMENT

For and in consideration of the mutual promises contained herein and other good and valuable consideration, the receipt and sufficiency of which is hereby acknowledged by the parties, the parties agree as follows:

The COUNTY OF LOS ANGELES (COUNTY), a body politic and corporate, does hereby grant and convey to the CITY OF PALMDALE (CITY), a perpetual, nonexclusive, Access Easement for pedestrian and vehicular ingress and egress purposes, and those appurtenances and uses commonly associated therewith, on, over, upon, and across that certain portion of COUNTY's real property situated in the City of Palmdale, County of Los Angeles, State of California, legally described on Exhibit A and depicted on Exhibit A-1, attached hereto and made a part hereof by this reference (Easement Area).

The parties acknowledge and agree that CITY shall have no obligation or responsibility for maintaining or repairing the Easement Area.

CITY agrees to defend, indemnify and hold harmless COUNTY, its officers, agents and employees, from and against any and all actions, demands, claims, liabilities, damages, losses, costs and expenses of every kind, nature and character, including but not limited to reasonable attorneys' and experts' fees, that arise in whole or in part from, or out of or in connection with CITY's use of or presence on the Easement Area. This indemnity shall continue so long as this Access Easement is in effect.

The rights granted to CITY herein under this Access Easement may not be assigned or delegated by CITY without the prior written consent of COUNTY. Any attempted assignment or delegation by CITY without the prior written consent of COUNTY shall be void.

Notwithstanding the foregoing, in the event CITY should sell its adjoining real property interest (Dominant Tenement), then this Access Easement shall automatically terminate and be of no further force or effect, and CITY shall promptly execute, acknowledge and deliver such instruments) for recordation as COUNTY may request to evidence such termination.

Dated $\qquad$
NOV 262013

ATTEST: SACHIA. HAMAL EXECUTIVE OFFICER EXECUTIVE OFFICER
CLERK MF THE BOARD OF SUPERVISORS

Allot


Dated $\qquad$

COUNTY OF LOS ANGELES a body politic and corporate


CITY OF PALMDALE


who proved to me on the basis of satisfactory evidence to
 be the person(s) whose name(s) is/are subscribed to the within instrument and acknowledged to me that he/she/they executed the same in his/her their authorized capacity(ies), and that by his/her/their signature(s) on the instrument the person(s), or the entity upon behalf of which the person(s) acted, executed the instrument.

I certify under PENALTY OF PERJURY under the laws of the State of California that the foregoing paragraph is true and correct.


## OPTIONAL

Though the information below is not required by law, it may prove valuable to persons relying on the document and could prevent fraudulent removal and reattachment of this form to another document.

## Description of Attached Document

Title or Type of Document: $\qquad$
Document Date: $\qquad$ Number of Pages: $\qquad$
Signer(s) Other Than Named Above:

## Capacity(ies) Claimed by Signer(s)

Signer's Name: $\qquad$ Signer's Name: $\qquad$
$\square$ Individual
$\square$ Corporate Officer - Title(s):
$\square$ Partner - $\square$ Limited $\square$ General
$\square$ Attorney in Fact
$\square$ Trustee
$\square$ Guardian or Conservator
$\square$ Other:
Signer Is Representing:
$\square$ Individual
$\square$ Corporate Officer - Title(s): $\qquad$
$\square$ Partner - $\square$ Limited $\square$ General
$\square$ Attorney in Fact
$\square$ Trustee
$\square$ Guardian or Conservator
[] Other:
Signer Is Representing: $\qquad$

[^17] © 2007 National Notary Association• 9350 De Soto Ave.. P.O. Box 2402 •Chatsworth, CA $91313-2402 \bullet$ www.NationalNotary.org Item \#5907 Reorder: Call Toll-Free 1-800-876-6827

## EXHIBIT A

Being a portion of Block 13 of the Town and Suburbs of Palmdale, in the City of Palmdale, County of Los Angeles, State of California, as per map recorded in Book 52, Pages 55 and 56 of Miscellaneous Records, in the Office of the County Recorder of said County described in its entirety as follows:

Commencing at the intersection of the Westerly line of said Block 13, with a line that is parallel with and distant Northerly at right angles, 309.50 feet, from the North line of Avenue Q-6, formerly Walnut Street, 80 feet wide, as shown on said map;

Thence North $89^{\circ} 21^{\prime} 59^{\prime \prime}$ East along said parallel line, a distance of 229.20 feet to the True Point of Beginning;

Thence North $0^{\circ} 02^{\prime} 59^{\prime \prime}$ West, a distance of 103.39 feet to the beginning of a tangent curve, concave easterly and having a radius of 18.00 feet;

Thence northerly along said curve, through a central angle of $41^{\circ} 54^{\prime} 41^{\prime \prime}$ an arc length of 13.17 feet;

Thence tangent to last said curve, North $41^{\circ} 51^{\prime} 42^{\prime \prime}$ East, a distance of 17.67 feet to the beginning of a tangent curve, concave southerly and having a radius of 18.00 feet;

Thence easterly along said curve, through a central angle of $48^{\circ} 03^{\prime} 54^{\prime \prime}$ an arc length of 15.10 feet;

Thence tangent to last said curve, North $89^{\circ} 55^{\prime} 36^{\prime \prime}$ East, a distance of 98.36 feet;

Thence North $0^{\circ} 53^{\prime} 15^{\prime \prime}$ West, a distance of 28.00 feet;
Thence South $89^{\circ} 55^{\prime} 36^{\prime \prime}$ West, a distance of 97.96 feet to the beginning of a curve, concave southerly and having a radius of 46.00 feet;

Thence westerly along said curve, through a central angle of $48^{\circ} 03^{\prime} 54^{\prime \prime}$ an arc length of 38.59 feet;

Thence tangent to last said curve, South $41^{\circ} 51^{\prime} 42^{\prime \prime}$ West, a distance of 17.67 feet to the beginning of a curve, concave easterly and having a radius of 46.00 feet;

Thence southerly along said curve, through a central angle of $41^{\circ} 54^{\prime} 41^{\prime \prime}$ an arc length of 33.65 feet;

Thence tangent to last said curve, South $0^{\circ} 02^{\prime} 59^{\prime \prime}$ East, a distance of 103.72 feet to the aforesaid parallel line distant Northerly at right angles, 309.50 feet, from the North line of Avenue Q-6;

Thence North $89^{\circ} 21^{\prime} 59^{\prime \prime}$ East along said parallel line, a distance of 28.00 feet to the True Point of Beginning.

Containing 7551 square feet, more or less.
Subject to easements, covenants, conditions, and restrictions of record, if any.

As shown on Exhibit A-1, attached hereto and by this reference made a part hereof.

Prepared by me or under my supervision.


Expiration 12-31-2014



North: 8283.6812
East : 10467.5423
Line Course: N 00-02-59 W Length: 103.72
North: 8387.4011 East: 10467.4523
Curve Length: 33.65
Delta: 41-54-41
Chord: 32.90
Radius: 46.00
Tangent: 17.62
Course: N 20-54-21 E
Course In: N 89-57-01 E Course Out: N 48-08-18 W
RP North: 8387.4411 East: 10513.4522
End North: 8418.1384 East: 10479.1934
Line Course: N 41-51-42 E Length: 17.67
North: 8431.2983 East: 10490.9852
Curve Length: 38.59 Radius: 46.00
Delta: 48-03-54 Tangent: 20.51
Chord: 37.47 Course: N 65-53-39 E
Course In: S 48-08-18 E Course Out: N 00-04-24 W
RP North: 8400.6009 East : 10525.2440
End North: 8446.6009 East: 10525.1852
Line Course: N 89-55-36 E Length: 97.96
North: 8446.7263 East: 10623.1451
Line Course: S 00-53-15 E Length: 28.00
North: 8418.7296 East: 10623.5788
Line Course: S 89-55-36 W Length: 98.36
North: 8418.6037 East: 10525.2189
Curve Length: 15.10 Radius: 18.00
Delta: 48-03-54 Tangent: 8.03
Chord: 14.66 Course: S 65-53-39 W
Course In: S 00-04-24 E Course Out: N 48-08-18 W
RP North: 8400.6038 East: 10525.2419
End North: 8412.6158 East: 10511.8363
Line Course: S 41-51-42 W Length: 17.67
North: 8399.4559 East: 10500.0445
Curve Length: 13.17 Radius: 18.00
Delta: 41-54-41 Tangent: 6.89
Chord: $12.88 \quad$ Course: S 20-54-21 W
Course In: S 48-08-18 E Course Out: S 89-57-01 W
RP North: 8387.4439 East: 10513.4501
End North: 8387.4283 East: 10495.4501
Line Course: S 00-02-59 E Length: 103.43
North: $8283.9983 \quad$ East: 10495.5399
Line Course: S 89-21-59 W Length: 28.00
North: 8283.6887 East:10467.5416

Perimeter: 595.33 Area: 7,551 sq.ft. 0.17 acres
Mapcheck Closure - (Uses listed courses, radii, and deltas)
Error Closure: 0.0075 Course: N 05-15-59 W
Error North: 0.00749 East: -0.00069
Precision 1: 79,376.00

## ATTACHMENT E

DEPARTMENT OF PUBLIC WORKS:
EAST ANTELOPE VALLEY ANIMAL CARE CENTER PROJECT ADOPT MITIGATED NEGATIVE DECLARATION AND MITIGATION MONITORING AND REPORTING PROGRAM

APPROVE PROJECT AND BUDGET
AWARD DESIGN-BUILD CONTRACT
AUTHORIZE LOCAL WORKER HIRING PROGRAM
APPROVE AND ORDER PUBLICATION OF NOTICE OF INTENTION TO PURCHASE REAL PROPERTY AND APPROVE RELATED ACTIONS

SPECS. 7003; CAPITAL PROJECT NO. 69570
DESIGN-BUILD PROPOSAL SUMMARY AND RANKING

| Proposer | Best Value Score <br> (Maximum. Score $=$ <br> $\mathbf{1 , 0 0 0}$ points) | Base Price <br> Proposal |
| :--- | :---: | :---: |
| KPRS Construction Services, Inc. | 742 | $\$ 14,874,000$ |
| Sinanian Development, Inc. | 736 | $\$ 15,704,000$ |
| Mallcraft, Inc. | 671 | $\$ 21,730,000$ |


[^0]:    * Included in the design-build contract

[^1]:    ${ }^{1}$ The proposed project was originally referred to as the "East Antelope Valley Animal Shelter." Based on coordination with the City of Palmdale and DACC, the project name was revised to its current title: "County of Los Angeles Animal Care Center Project, Palmdale CA."
    2 Ibid.

[^2]:    ${ }^{3}$ The proposed project was originally referred to as the "East Antelope Valley Animal Shelter." Based on coordination with the City of Palmdale and DACC, the project name was revised to its current title: "County of Los Angeles Animal Care Center Project, Palmdale CA."
    4 Ibid.

[^3]:    5 The WorkSource Center is a network of workforce experts that leverage funding and resources across the Los Angeles region to provide job seekers and businesses with no-cost, high value employment and training services. The City of Palmdale is a proud partner of the WorkSource program, which is an initiative of the Los Angeles County Workforce Investment Board.

[^4]:    ${ }^{6}$ As part of research regarding the historical uses at the project site, it was noted that the project site may have been occupied by a JC Penny retail store; however, no records have been found on county level to verify if a JC Penny's was ever at this location.

[^5]:    7 No plans for expansion are being considered at this time. Should expansion be proposed in the future, this will be analyzed under a separate CEQA action.

[^6]:    8 Haul trucks will be in operation for approximately 20 days during the construction period.

[^7]:    9 As of January 1, 2013, the California Department of Fish and Game (CDFG) is now called the California Department of Fish and Wildlife (CDFW).

[^8]:    10 As of January 1, 2013, the California Department of Fish and Game (CDFG) is now called the California Department of Fish and Wildlife (CDFW).

[^9]:    11 The proposed project was originally referred to as the "East Antelope Valley Animal Shelter." Based on coordination with the City of Palmdale and DACC, the project name was revised to its current title: "County of Los Angeles Animal Care Center Project, Palmdale CA."

[^10]:    12 The proposed project was originally referred to as the "East Antelope Valley Animal Shelter." Based on coordination with the City of Palmdale and DACC, the project name was revised to its current title: "County of Los Angeles Animal Care Center Project, Palmdale CA."
    13 Ibid.

[^11]:    14 The proposed project was originally referred to as the "East Antelope Valley Animal Shelter." Based on coordination with the City of Palmdale and DACC, the project name was revised to its current title: "County of Los Angeles Animal Care Center Project, Palmdale CA."

[^12]:    

[^13]:    15 The proposed project was originally referred to as the "East Antelope Valley Animal Shelter." Based on coordination with the City of Palmdale and DACC, the project name was revised to its current title: "County of Los Angeles Animal Care Center Project, Palmdale CA."

[^14]:    Job Name: East Antelope Valley Animal Shelter Job No.: 12-31-145-01 Location: BH-1

    Test Date: 03.22 .12

[^15]:    16 The proposed project was originally referred to as the "East Antelope Valley Animal Shelter." Based on coordination with the City of Palmdale and DACC, the project name was revised to its current title: "County of Los Angeles Animal Care Center Project, Palmdale CA."

[^16]:    

[^17]:    ㅈㅏㅄㅄ.

