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# ARGON-OXYGEN-NITROGEN THREE COMPONENT SYSTEM EXPERIMENTAL VAPOR-LIQUID EQUILIBRIUM DATA

TECHNICAL DOCUMENTARY REPORT NO. APL TDR 64-64  
APRIL 1964

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AF Aero Propulsion Laboratory  
Research and Technology Division  
Air Force Systems Command  
Wright-Patterson Air Force Base, Ohio

PROJECT NO. 3048, TASK NO. 30193

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(Prepared under Contract No. AF 33(657)-8742  
by Air Products and Chemicals, Inc., Research and  
Development Department, Allentown, Pa.; G. M. Wilson,  
P. M. Silverberg, and M. G. Zellner, authors)

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## FOREWORD

This report summarizes all work done under contract to the Air Force for the experimental determination of vapor-liquid equilibrium in argon, oxygen, and nitrogen mixtures from July 15, 1962 to April 8, 1964.

The following persons were contributing authors on this subject:

L. Israel - literature search and many useful computer programs.

A. Jambhekar - mixture virial coefficients.

C. J. Sterner - former director of the vapor-liquid laboratory.

P. Fennema - improved chromatographic analysis.

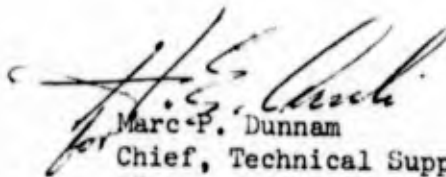
This report is dedicated to that hardy band of technicians who ran the equipment two shifts for a seemingly endless ten months. Our thanks go to E. Frederick, R. Gotthardt, J. Wallace, C. Worman, and especially to H. Donat whose perserverance, unfailing precision, and mechanical ability helped pull us over many rough spots.

ABSTRACT

This Final Technical Documentary Report presents the results from July 15, 1962 to April 15, 1964 as covered by the contract for the experimental determination of vapor-liquid equilibrium data in argon, oxygen, and nitrogen mixtures. The experimental apparatus and procedures are described. The experimental data at 26, 23, 20, 18, 16, 14, 12, 10, 8, 6, 4, 2 and 1 atmosphere levels are presented. A correlation of our experimental data is made. Plots and tables of equilibrium constants, relative volatilities and activity coefficients are presented. Experimental and calculated results are compared and a comparison of the data to the literature is made. Analytical enthalpy data is presented.

The correlation reproduces the experimental data with an error less than 2.5%; being worst at 20 atmospheres and best at 6 atmospheres.

This Technical Documentary Report has been reviewed and is approved.



Marc P. Dunnam  
Chief, Technical Support Division  
AF Aero-Propulsion Laboratory

## TABLE OF CONTENTS

	<u>Page</u>
I. INTRODUCTION . . . . .	1
II. LITERATURE SEARCH. . . . .	3
III. EXPERIMENTAL APPARATUS AND PROCEDURE . . . . .	5
A. Recirculation System . . . . .	5
B. Equilibrium Cell . . . . .	5
C. Constant-Temperature Bath. . . . .	9
D. Operating Procedure. . . . .	9
E. Sampling Systems . . . . .	11
F. Pressure Measurement . . . . .	12
G. Temperature Measurement. . . . .	12
H. Time of Equilibration. . . . .	15
IV. ANALYTICAL METHODS . . . . .	18
A. Analyses to Run 264. . . . .	18
B. Analyses After Run 264 . . . . .	18
V. EXPERIMENTAL DATA. . . . .	26
VI. CORRELATION OF EXPERIMENTAL DATA . . . . .	55
A. Thermodynamic Equations. . . . .	55
B. Liquid Molar Volume. . . . .	58
C. Vapor Pressure of Pure Components. . . . .	59
D. Fugacity Coefficient . . . . .	63
E. Activity Coefficient Equation. . . . .	72
VII. COMPARISON OF COPRELATION TO DATA. . . . .	77

TABLE OF CONTENTS (continued)

	<u>Page</u>
VIII. ENTHALPY CORRELATION . . . . .	140
A. Heat of Mixing . . . . .	140
B. Ideal Gas Heat Capacity 140-250°R. . . . .	141
C. Latent Heat. . . . .	141
D. Enthalpy of the Real Gas . . . . .	142
E. Saturated Pure Component Heat Capacity . . . . .	142
IX. REFERENCES . . . . .	146
X. APPENDIXES . . . . .	149

## ILLUSTRATIONS

<u>Figure</u>	<u>Page</u>
1 Vapor-Liquid Equilibrium Apparatus . . . . .	6
2 Front View of Equilibrium Apparatus . . . . .	7
3 Detail of Cell and Constant-Temperature Bath. . . . .	8
4 Close-up of the Equilibrium Cell and Constant Temperature Bath. . . . .	10
5 Dead Weight Test of 500 Psi Heise Gauge . . . . .	13
6 Dead Weight Test of 300 Psi Heise Gauge . . . . .	13
7 Thermocouple Calibration. . . . .	14
8 Equilibration Test Run on Vapor-Liquid Apparatus. . . . .	17
9 Sample Chromatogram . . . . .	20
10 Photograph of Gas Chromatograph . . . . .	22
11 Close-up of Electronic Components of the Chromatograph. .	23
12 Chromatograph Calibration Curves. . . . .	24
13 Deviation of APCI Nitrogen Vapor Pressure Data from Riedel Equation . . . . .	60
14. Deviation of APCI Argon Vapor Pressure Data from Riedel Equation . . . . .	61
15 Deviation of Literature Oxygen Vapor Pressure Data from Riedel Equation. . . . .	62
16 Deviation of Literature Vapor Pressure from APCI Correlation for Nitrogen. . . . .	64
17 Deviation of Literature Vapor Pressure from APCI Correlation for Argon . . . . .	65
18 Calculated Second and Third Virial Coefficients, B and C, for Nitrogen . . . . .	68



ILLUSTRATIONS (continued)

<u>Figure</u>	<u>Page</u>
19	Calculated Second and Third Virial Coefficients, B and C, for Argon . . . . . 69
20	Calculated Second and Third Virial Coefficients, B and C, for Oxygen. . . . . 70
21	Comparison of Calculated and Experimental Compressibility Data, Argon. . . . . 71
22	Comparison of Calculated and Experimental Compressibility Data, Oxygen . . . . . 71
23	Comparison of Calculated and Experimental Compressibility Data, Nitrogen . . . . . 73
24	Comparison of Calculated and Experimental Cross Coefficients . . . . . 73
25	Comparison of Calculated and Experimental Compressibility Data, Nitrogen-Oxygen Mixtures . . . . . 74
26	Comparison of Calculated and Experimental Compressibility Data, Air. . . . . 75
27	Summary of Bias of Points in Region I. . . . . 80
28	Summary of Bias of Points in Region II . . . . . 81
29	Summary of Bias of Points in Region III. . . . . 82
30	Summary of Bias of Points in Region IV . . . . . 83
31	Summary of Bias of Points in all Regions . . . . . 84
32	Activity Coefficients in the Nitrogen-Oxygen Binary System, Calculated Vs. Experimental. . . . . 85
33	Activity Coefficients in the Nitrogen-Oxygen Binary System, Calculated Vs. Experimental. . . . . 86
34	Activity Coefficients in the Nitrogen-Oxygen Binary System, Calculated Vs. Experimental. . . . . 87
35	Activity Coefficients in the Nitrogen-Oxygen Binary System, Calculated Vs. Experimental. . . . . 88

## ILLUSTRATIONS (continued)

<u>Figure</u>		<u>Page</u>
36	Activity Coefficients in the Nitrogen-Oxygen Binary System, Calculated Vs. Experimental. . . . .	89
37	Activity Coefficients in the Oxygen-Argon Binary System, Calculated Vs. Experimental. . . . .	90
38	Activity Coefficients in the Oxygen-Argon Binary System, Calculated Vs. Experimental. . . . .	91
39	Activity Coefficients in the Oxygen-Argon Binary System, Calculated Vs. Experimental. . . . .	92
40	Activity Coefficients in the Oxygen-Argon Binary System, Calculated Vs. Experimental. . . . .	93
41	Activity Coefficients in the Nitrogen-Argon Binary System, Calculated Vs. Experimental. . . . .	94
42	Activity Coefficients in the Nitrogen-Argon Binary System, Calculated Vs. Experimental. . . . .	95
43	Activity Coefficients in the Nitrogen-Argon Binary System, Calculated Vs. Experimental. . . . .	96
44	Activity Coefficients in the Nitrogen-Argon Binary System, Calculated Vs. Experimental. . . . .	97
45	Activity Coefficients in the Nitrogen-Argon Binary System, Calculated Vs. Experimental. . . . .	98
46	Comparison of Experimental Data and the Correlation, 1 Atmosphere . . . . .	100
47	Comparison of Experimental Data and the Correlation, 1 Atmosphere . . . . .	101
48	Comparison of Experimental Data and the Correlation, 1 Atmosphere . . . . .	102
49	Comparison of Experimental Data and the Correlation, 1 Atmosphere . . . . .	103
50	Comparison of Experimental Data and the Correlation, 2 Atmospheres. . . . .	104

ILLUSTRATIONS (continued)

<u>Figure</u>	<u>Page</u>
51 Comparison of Experimental Data and the Correlation, 2 Atmospheres. . . . .	105
52 Comparison of Experimental Data and the Correlation, 2 Atmospheres. . . . .	106
53 Comparison of Experimental Data and the Correlation, 2 Atmospheres. . . . .	107
54 Comparison of Experimental Data and the Correlation, 4 Atmospheres. . . . .	108
55 Comparison of Experimental Data and the Correlation, 4 Atmospheres. . . . .	109
56 Comparison of Experimental Data and the Correlation, 4 Atmospheres. . . . .	110
57 Comparison of Experimental Data and the Correlation, 6 Atmospheres. . . . .	111
58 Comparison of Experimental Data and the Correlation, 6 Atmospheres. . . . .	112
59 Comparison of Experimental Data and the Correlation, 6 Atmospheres. . . . .	113
60 Comparison of Experimental Data and the Correlation, 8 Atmospheres. . . . .	114
61 Comparison of Experimental Data and the Correlation, 8 Atmospheres. . . . .	115
62 Comparison of Experimental Data and the Correlation, 8 Atmospheres. . . . .	116
63 Comparison of Experimental Data and the Correlation, 10 Atmospheres . . . . .	117
64 Comparison of Experimental Data and the Correlation, 10 Atmospheres . . . . .	118
65 Comparison of Experimental Data and the Correlation, 10 Atmospheres . . . . .	119

## ILLUSTRATIONS (continued)

<u>Figure</u>		<u>Page</u>
66	Comparison of Experimental Data and the Correlation, 12 Atmospheres . . . . .	120
67	Comparison of Experimental Data and the Correlation, 12 Atmospheres . . . . .	121
68	Comparison of Experimental Data and the Correlation, 12 Atmospheres . . . . .	122
69	Comparison of Experimental Data and the Correlation, 14 Atmospheres . . . . .	123
70	Comparison of Experimental Data and the Correlation, 14 Atmospheres . . . . .	124
71	Comparison of Experimental Data and the Correlation, 14 Atmospheres . . . . .	125
72	Comparison of Experimental Data and the Correlation, 16 Atmospheres . . . . .	126
73	Comparison of Experimental Data and the Correlation, 16 Atmospheres . . . . .	127
74	Comparison of Experimental Data and the Correlation, 18 Atmospheres . . . . .	128
75	Comparison of Experimental Data and the Correlation, 18 Atmospheres . . . . .	129
76	Comparison of Experimental Data and the Correlation, 20 Atmospheres . . . . .	130
77	Comparison of Experimental Data and the Correlation, 20 Atmospheres . . . . .	131
78	Comparison of Experimental Data and the Correlation, 20 Atmospheres . . . . .	132
79	Comparison of Experimental Data and the Correlation, 23 Atmospheres . . . . .	133
80	Comparison of Experimental Data and the Correlation, 23 Atmospheres . . . . .	134

ILLUSTRATIONS (continued)

<u>Figure</u>	<u>Page</u>
81 Comparison of Experimental Data and the Correlation, 26 Atmospheres . . . . .	135
82 Comparison of Experimental Data and the Correlation, 26 Atmospheres . . . . .	136
83 Comparison of APCI Correlation to Latimer Correlation for Nitrogen-Oxygen System . . . . .	137
84 Comparison of APCI Correlation to Latimer Correlation for Argon-Nitrogen System. . . . .	138
85 Comparison of APCI Correlation to Latimer Correlation for Argon-Oxygen System. . . . .	139
86 K-Values of Nitrogen . . . . .	151
87 K-Values of Nitrogen . . . . .	152
88 K-Values of Nitrogen . . . . .	153
89 K-Values of Nitrogen . . . . .	154
90 K-Values of Nitrogen . . . . .	155
91 K-Values of Nitrogen . . . . .	156
92 K-Values of Nitrogen . . . . .	157
93 K-Values of Nitrogen . . . . .	158
94 K-Values of Argon. . . . .	159
95 K-Values of Argon. . . . .	160
96 K-Values of Argon. . . . .	161
97 K-Values of Argon. . . . .	162
98 K-Values of Argon. . . . .	163
99 K-Values of Argon. . . . .	164
100 K-Values of Argon. . . . .	165
101 K-Values of Oxygen . . . . .	166
102 K-Values of Oxygen . . . . .	167

## ILLUSTRATIONS (continued)

<u>Figure</u>		<u>Page</u>
103	K-Values of Oxygen . . . . .	168
104	K-Values of Oxygen . . . . .	169
105	K-Values of Oxygen . . . . .	170
106	K-Values of Oxygen . . . . .	171
107	K-Values of Oxygen . . . . .	172
108	K-Values of Oxygen . . . . .	173
109	K-Values of Oxygen . . . . .	174
110	K-Values of Oxygen . . . . .	175
111	Relative Volatility of Argon to Nitrogen . . . . .	177
112	Relative Volatility of Argon to Nitrogen . . . . .	178
113	Relative Volatility of Argon to Nitrogen . . . . .	179
114	Relative Volatility of Argon to Nitrogen . . . . .	180
115	Relative Volatility of Argon to Nitrogen . . . . .	181
116	Relative Volatility of Argon to Nitrogen . . . . .	182
117	Relative Volatility of Argon to Nitrogen . . . . .	183
118	Relative Volatility of Argon to Nitrogen . . . . .	184
119	Relative Volatility of Argon to Nitrogen . . . . .	185
120	Relative Volatility of Argon to Nitrogen . . . . .	186
121	Relative Volatility of Argon to Nitrogen . . . . .	187
122	Relative Volatility of Argon to Oxygen . . . . .	189
123	Relative Volatility of Argon to Oxygen . . . . .	190
124	Relative Volatility of Argon to Oxygen . . . . .	191
125	Relative Volatility of Argon to Oxygen . . . . .	192

ILLUSTRATIONS (continued)

<u>Figure</u>	<u>Page</u>
126	Relative Volatility of Argon to Oxygen . . . . . 193
127	Relative Volatility of Argon to Oxygen . . . . . 194
128	Relative Volatility of Argon to Oxygen . . . . . 195
129	Relative Volatility of Argon to Oxygen . . . . . 196
130	Relative Volatility of Argon to Oxygen . . . . . 197
131	Relative Volatility of Argon to Oxygen . . . . . 198
132	Relative Volatility of Argon to Oxygen . . . . . 199
133	Relative Volatility of Argon to Nitrogen with No Oxygen Present in the System . . . . . 201
134	Relative Volatility of Argon to Oxygen with No Nitrogen Present in the System . . . . . 203
135	Nitrogen Pressure Activity Coefficients, 1 Atmosphere . . . . . 205
136	Nitrogen Pressure Activity Coefficients, 2 Atmospheres. . . . . 206
137	Nitrogen Pressure Activity Coefficients, 4 Atmospheres. . . . . 207
138	Nitrogen Pressure Activity Coefficients, 6 Atmospheres. . . . . 208
139	Nitrogen Pressure Activity Coefficients, 8 Atmospheres. . . . . 209
140	Nitrogen Pressure Activity Coefficients, 10 Atmospheres . . . . . 210
141	Nitrogen Pressure Activity Coefficients, 12 Atmospheres . . . . . 211
142	Nitrogen Pressure Activity Coefficients, 14 Atmospheres . . . . . 212
143	Nitrogen Pressure Activity Coefficients, 16 Atmospheres . . . . . 213

## ILLUSTRATIONS (continued)

<u>Figure</u>		<u>Page</u>
144	Nitrogen Pressure Activity Coefficients, 18 Atmospheres . . . . .	214
145	Nitrogen Pressure Activity Coefficients, 20 Atmospheres . . . . .	215
146	Nitrogen Pressure Activity Coefficients, 23 Atmospheres . . . . .	216
147	Nitrogen Pressure Activity Coefficients, 26 Atmospheres . . . . .	217
148	Argon Pressure Activity Coefficients, 1 Atmosphere . . . .	218
149	Argon Pressure Activity Coefficients, 2 Atmospheres . . . .	219
150	Argon Pressure Activity Coefficients, 4 Atmospheres . . . .	220
151	Argon Pressure Activity Coefficients, 6 Atmospheres . . . .	221
152	Argon Pressure Activity Coefficients, 8 Atmospheres . . . .	222
153	Argon Pressure Activity Coefficients, 10 Atmospheres . . . .	223
154	Argon Pressure Activity Coefficients, 12 Atmospheres . . . .	224
155	Argon Pressure Activity Coefficients, 14 Atmospheres . . . .	225
156	Argon Pressure Activity Coefficients, 16 Atmospheres . . . .	226
157	Argon Pressure Activity Coefficients, 18 Atmospheres . . . .	227
158	Argon Pressure Activity Coefficients, 20 Atmospheres . . . .	228
159	Argon Pressure Activity Coefficients, 23 Atmospheres . . . .	229
160	Argon Pressure Activity Coefficients, 26 Atmospheres . . . .	230
161	Oxygen Pressure Activity Coefficients, 1 Atmosphere . . . .	231
162	Oxygen Pressure Activity Coefficients, 2 Atmospheres . . . .	232
163	Oxygen Pressure Activity Coefficients, 4 Atmospheres . . . .	233
164	Oxygen Pressure Activity Coefficients, 6 Atmospheres . . . .	234
165	Oxygen Pressure Activity Coefficients, 8 Atmospheres . . . .	235



## ILLUSTRATIONS (continued)

<u>Figure</u>		<u>Page</u>
166	Oxygen Pressure Activity Coefficient, 10 Atmospheres. . .	236
167	Oxygen Pressure Activity Coefficient, 12 Atmospheres. . .	237
168	Oxygen Pressure Activity Coefficient, 14 Atmospheres. . .	238
169	Oxygen Pressure Activity Coefficient, 16 Atmospheres. . .	239
170	Oxygen Pressure Activity Coefficient, 18 Atmospheres. . .	240
171	Oxygen Pressure Activity Coefficient, 20 Atmospheres. . .	241
172	Oxygen Pressure Activity Coefficient, 23 Atmospheres. . .	242
173	Oxygen Pressure Activity Coefficient, 26 Atmospheres. . .	243
174	Vapor Pressure of Specific Mixtures of $N_2$ -Ar- $O_2$ . . . . .	245
175	Vapor Pressure of Specific Mixtures of $N_2$ -Ar- $O_2$ . . . . .	246
176	Vapor Pressure of Specific Mixtures of $N_2$ -Ar- $O_2$ . . . . .	247
177	Vapor Pressure of Specific Mixtures of $N_2$ -Ar- $O_2$ . . . . .	248
178	Vapor Pressure of Specific Mixtures of $N_2$ -Ar- $O_2$ . . . . .	249
179	Vapor Pressure of Specific Mixtures of $N_2$ -Ar- $O_2$ . . . . .	250
180	Vapor Pressure of Specific Mixtures of $N_2$ -Ar- $O_2$ . . . . .	251
181	Vapor Pressure of Specific Mixtures of $N_2$ -Ar- $O_2$ . . . . .	252
182	Vapor Pressure of Specific Mixtures of $N_2$ -Ar- $O_2$ . . . . .	253
183	Vapor Pressure of Specific Mixtures of $N_2$ -Ar- $O_2$ . . . . .	254
184	Vapor Pressure of Specific Mixtures of $N_2$ -Ar- $O_2$ . . . . .	255
185	Vapor Pressure of Specific Mixtures of $N_2$ -Ar- $O_2$ . . . . .	256
186	Vapor Pressure of Specific Mixtures of $N_2$ -Ar- $O_2$ . . . . .	257
187	Vapor Pressure of Specific Mixtures of $N_2$ -Ar- $O_2$ . . . . .	258
188	Vapor Pressure of Specific Mixtures of $N_2$ -Ar- $O_2$ . . . . .	259

TABLES

<u>Table</u>	<u>Page</u>
1 Equilibration Test Results . . . . .	16
2 Sample Long-Term Analyses. . . . .	25
3 Experimental Data at 1 Atm . . . . .	28
4 Experimental Data at 2 Atm . . . . .	30
5 Experimental Data at 4 Atm . . . . .	32
6 Experimental Data at 6 Atm . . . . .	34
7 Experimental Data at 8 Atm . . . . .	36
8 Experimental Data at 10 Atm. . . . .	38
9 Experimental Data at 12 Atm. . . . .	40
10 Experimental Data at 14 Atm. . . . .	42
11 Experimental Data at 16 Atm. . . . .	44
12 Experimental Data at 18 Atm. . . . .	46
13 Experimental Data at 20 Atm. . . . .	48
14 Experimental Data at 23 Atm. . . . .	50
15 Experimental Data at 26 Atm. . . . .	52
16 Experimental Data at Mixed Pressure Levels . . . . .	54
17 Liquid Molar Volume Correlation Constants. . . . .	58
18 Constants for Pure Component Vapor Pressures . . . . .	59
19 Second Virial Coefficients Used in Calculations. . . . .	66
20 Third Virial Coefficients Used in Calculations . . . . .	67
21 Van Laar Constants for Nitrogen-Argon-Oxygen Activity Coefficients in the Liquid Phase. . . . .	76

TABLES (continued)

<u>Table</u>		<u>Page</u>
22	Constants and Root Mean Square Error of Various Curve Fits . . . . .	78
23	Summary of Positive and Negative Deviations of Experimental Points from Correlation . . . . .	79
24	Comparison of Calculated and Experimental Saturated Liquid Heat Capacities, BTU/lb-Mole °R . . . . .	145
25	Isobaric Calculated Values . . . . .	261
26	Isothermal Calculated Values . . . . .	275

## I. INTRODUCTION

This project, under contract with the U. S. Air Force, was undertaken to measure and correlate vapor-liquid equilibrium data in binary and ternary mixtures of oxygen, nitrogen, and argon. This project was undertaken because much of the existing data are reported only for low pressures and few data have been obtained in the ternary system. The measurements of this project establish the vapor-liquid equilibrium properties of the oxygen-nitrogen-argon system over a wide range of pressures and over the entire range of binary and ternary compositions. One thousand nine hundred and sixty two data points were measured and this system may well be one of the most thoroughly studied ternary systems to date.

The project effort was divided into three parts as follows:

1. A literature search for existing data.
2. The measurement of vapor-liquid equilibrium data at the following combinations of pressures and compositions. The actual compositions measured are in only approximate agreement with the listed compositions and, therefore, more than one run was sometimes made in a given concentration region.

<u>Pressure, Atm</u>	<u>Mole Ratio</u>	
	$\frac{N_2}{(N_2+O_2)}$	<u>Mole Fraction Argon</u>
1	0	0
2	0.10	0.01
4	0.20	0.02
6	0.40	0.03
8	0.60	0.04
10	0.80	0.05
12	0.90	0.07
14	0.97	0.10
16	1.00	0.20
18	----	0.40
20	----	0.60
23	----	0.80
26	----	0.90

3. The thermodynamic correlation of the equilibrium data and the analytical determination of enthalpy data.

---

Manuscript released by authors April 1964 for publication as an RTD Technical Documentary Report.

This report summarizes:

1. The results of the literature search.
2. A bibliography of existing vapor-liquid equilibrium, enthalpy, and related data of the oxygen-nitrogen-argon system.
3. A description of the experimental apparatus.
4. Tables of the experimental data.
5. A thermodynamic correlation of the data.
6. Tables and figures of derived vapor-liquid equilibrium and enthalpy data.

The experimental data are accurate to within + 0.5% in the pressure and + 1% in the relative volatility. By smoothing the data it is possible to obtain equilibria accurate to + 0.5% in the relative volatility. The thermodynamic correlation of the data is not quite as accurate as the experimental data due to a weakness in the correlation method at temperatures above the critical temperature of nitrogen and at pressures near the critical point of a mixture. The largest difference between the correlation and the experimental data appears to be at 20 atmospheres where the calculated pressure and relative volatilities deviate 2.5% from the experimental data. This accuracy is satisfactory for most process design calculations, but it may be desirable on occasion to interpolate directly from the experimental data.

## II. LITERATURE SEARCH

A literature search was made to obtain all existing data relating to vapor-liquid equilibrium and enthalpy of the oxygen-nitrogen-argon system. The search included the following sources of information.

1. Chemical Abstracts (January 1957 - December 1962).
2. Chemical Titles (January 1961 - May 1963).
3. Armed Services Technical Information Agency (ASTIA) - A complete search of the ASTIA collection was obtained (to September 1963).
4. Cryogenic Data Center - NBS Cryogenic Engineering Laboratory, Boulder, Colorado - Two searches to January 1963 and to October 1963.
5. Existing bibliographies on the subject:
  - a. "The Compendium", Johnson, V. J. (ed.), WADD Tech. Rept. 60-56, (1961).
  - b. E. F. Yendall and Olzewski, W. J., "Saturation Properties of Oxygen-Nitrogen Mixtures", ASD Technical Rept. 61-536, Sept. 1961.
  - c. Ju Chin Chu, et al, Vapor Liquid Equilibrium Data, J. W. Edwards Co., Ann Arbor, Michigan, 1956.
  - d. E. Hala, et al, Vapor-Liquid Equilibrium, Pergamon, New York, 1958.
  - e. G. A. Cook, ed., Argon, Helium, and the Rare Gases, Vol. II, Interscience, New York, 1961.
  - f. J. Timmermans, Physico-Chemical Constants of Binary Systems, Interscience, New York, 1960.

A bibliography of the data is given in the Appendix according to the following categories:

- A. Vapor-Liquid Equilibrium Data Nitrogen-Oxygen System
- B. Vapor-Liquid Equilibrium Data Nitrogen-Argon System
- C. Vapor-Liquid Equilibrium Data Argon-Oxygen System

- D. Vapor-Liquid Equilibrium Data Nitrogen-Oxygen-Argon Ternary System
- E. Enthalpy Data
- F. Pressure-Volume-Temperature Data for Gaseous Mixtures of  $N_2$ - $O_2$ -Ar (including air) used in checking the virial coefficients
- G. Vapor Pressure Data
- H. Miscellaneous References

From this search it is concluded that few vapor-liquid equilibrium data exist in three principal areas, namely:

1. Few data exist for the nitrogen-argon binary system.
2. Few data exist above pressures of 5 to 10 atmospheres.
3. Few data exist for the argon-oxygen-nitrogen ternary system.

From the search for enthalpy data it is concluded that:

1. Heat of mixing data for the binaries of the oxygen-nitrogen-argon system are reported only at low temperatures.
2. Latent heat data are reported in terms of correlations based principally on vapor pressure data. Except for argon the data appear to be satisfactory, but in the case of argon there appears to be little experimental data to back up the correlated data.

### III. EXPERIMENTAL APPARATUS AND PROCEDURE

#### A. Recirculation System

A schematic flow diagram of the equilibrium apparatus<sup>(1)</sup> is presented in Figure 1. The elements which make up the complete apparatus consist of: equilibrium cell, recirculation pump, closed recirculation loop, constant-temperature bath, system pressure gauge, cell thermocouple, liquid sampling line, gas sampling coil, system volume regulator, charging manifold, vacuum pump and numerous subsidiary equipment such as valves, gauges, etc. A photograph of the apparatus is presented in Figure 2 showing the cell barricade, pressure gauges, volume regulator and temperature controller.

The recirculation method is one of the standard laboratory techniques for obtaining accurate vapor-liquid equilibrium data at temperatures below ambient. With this method, a cell partly full of liquid and of appreciable volume is maintained at a constant operating temperature. The vapor inside the cell is drawn out of the top of the cell, warmed to ambient temperature, passed through a pump which increases the pressure of the vapor slightly, cooled back to the cell temperature and introduced to the bottom of the cell. The recirculated vapor bubbles through the liquid to the vapor space and continues the cycle through the system. As the vapor bubbles through the liquid, the liquid is agitated and the liquid and vapor approach equilibrium. When equilibrium is achieved, portions of the vapor and of the liquid are withdrawn from the system and analyzed for chemical compositions.

In this apparatus, the vapors warm to ambient temperature in exposed tubing, recirculate by use of an electromagnetic pump<sup>(2)</sup> and cool to cell temperature in a coil of tubing which is immersed in the constant-temperature bath.

#### B. Equilibrium Cell

A schematic diagram of the equilibrium cell is shown on Figure 3. The equilibrium cell is a vertical cylindrical tube made of laminated glass which is sealed at both ends by Teflon gaskets supported by end flanges. The end flanges are connected to each other by tie-rods outside of the cell. The glass tube, which is usable at pressures up to 800 psia and temperatures to  $-340^{\circ}\text{F}$ , is  $3/8$  in. ID,  $11/16$  in. OD and  $3-1/2$  in. long with squared-off ends ground flat and fire-polished. The liquid sampling line and the three-element thermocouple both enter the equilibrium cell at the top through the  $1/4$  in. OD vapor outlet line. The recirculated vapor enters the cell through small holes in a distributor plate which caps the inlet line. Inside the cell the flow of bubbles from the vapor inlet is broken up by a series of horizontal screens. Near the top of the cell, a plug of fiberglass prevents carryover of entrained liquid.



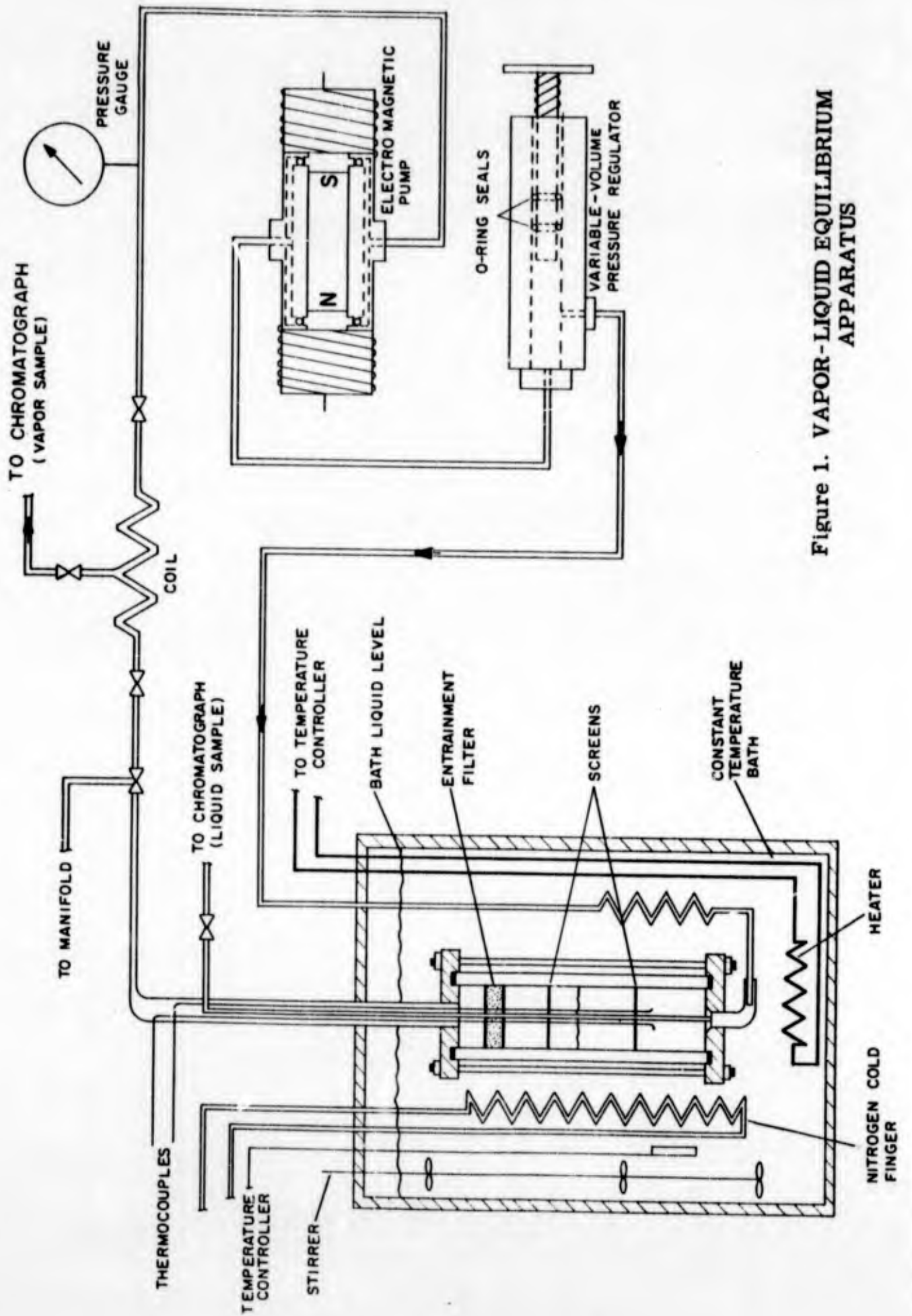


Figure 1. VAPOR-LIQUID EQUILIBRIUM APPARATUS

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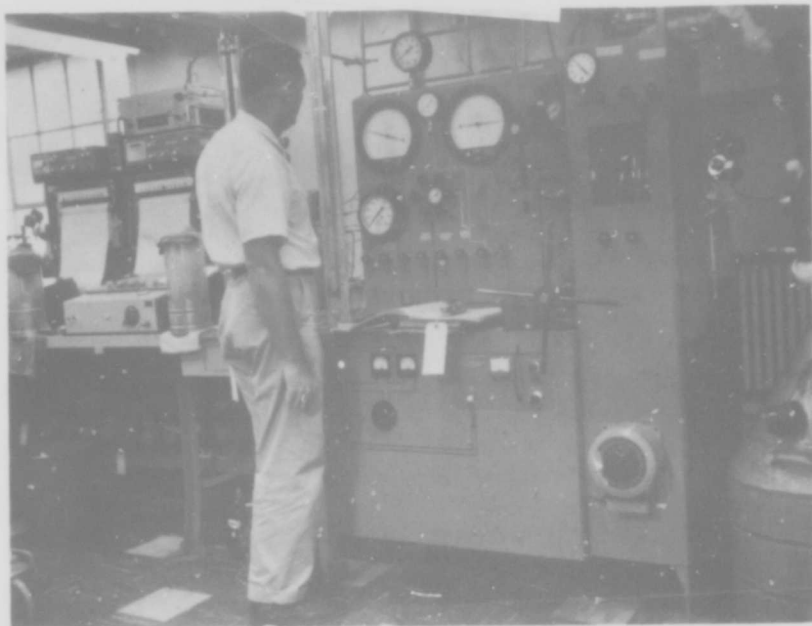


FIGURE 2. FRONT VIEW OF EQUILIBRIUM APPARATUS

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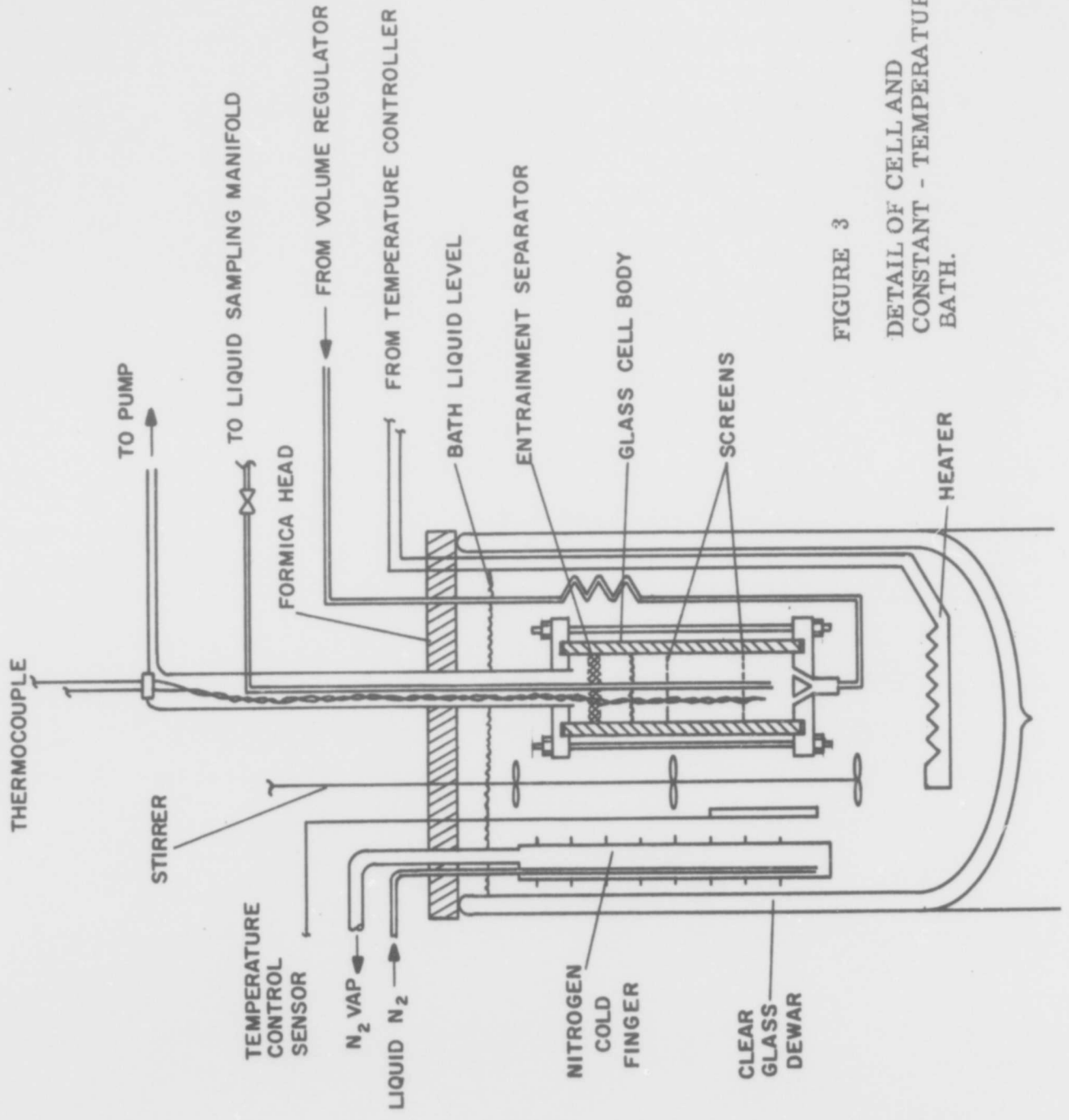


FIGURE 3  
 DETAIL OF CELL AND  
 CONSTANT - TEMPERATURE  
 BATH.

The equilibrium cell is immersed in a constant-temperature liquid bath which is contained in a clear glass dewar vessel. The dewar is supported on a pedestal within a steel barricade which is open top and bottom. The equilibrium cell is illuminated and may be viewed while operating through the clear dewar and a safety glass window in the barricade. A photograph of the cell and bath are shown in Figure 4.

C. Constant-Temperature Bath

The constant-temperature bath in which the equilibrium cell is immersed may be any of one of several fluids, depending on the operating temperature. From the highest temperature covered down to  $-301^{\circ}\text{F}$ , Freon-13\* was used. Liquid argon was used down to  $-308^{\circ}\text{F}$ . Liquid nitrogen was used down to  $-320^{\circ}\text{F}$ .

The temperature of the bath liquid is controlled to within  $+ 0.01^{\circ}\text{F}$  by use of a proportional electronic controller. The bath is cooled by liquid nitrogen which flows into a "cold finger" at a constant rate and evaporates. The temperature of the bath is adjusted to operating conditions by passing an electrical current through a resistance heating element immersed in the bath. The heating current is regulated by the controller which receives temperature information from a platinum resistance thermometer which is immersed in the bath. The bath liquid is kept agitated by a motor-driven stirrer. Two additional thermocouples in the bath are used to determine the bath temperature and to check on the controller action.

D. Operating Procedure

Routine operation of the equilibrium apparatus begins with the cell at room temperature and the entire system under vacuum. Precooled bath liquid is added to the dewar vessel and the cell is cooled down to the operating temperature. Measured quantities of the component gases are introduced to the system, one component at a time, generally starting with nitrogen. The quantities of gas added are calculated beforehand and measured by pressure changes in a volume-calibrated manifold. Before any component is allowed to enter the manifold, the manifold is evacuated and purged with the appropriate gas. The recirculation pump is turned on while the components are being introduced and continues to operate until it is time to sample. When all components have been added to the system, slight adjustments of the pressure and liquid volume are made by adding small additional quantities of the appropriate component. After the desired liquid volume has formed and the pressure is established at the proper level, the apparatus is permitted to operate at constant temperature and pressure for approximately one half hour before taking samples. The sampling procedures are described under "E. Sampling Systems".

\*E.I. Dupont de Nemours Inc. registered trademark.

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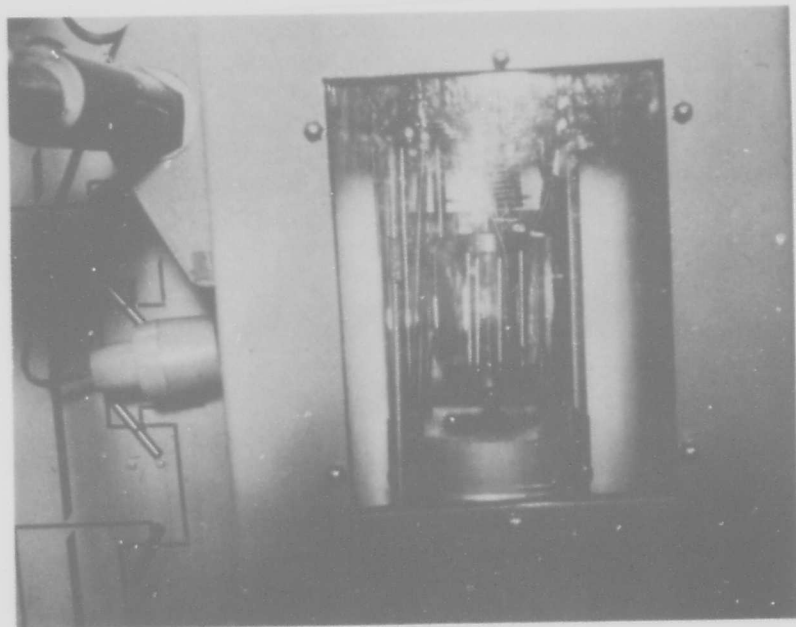


FIGURE 4. CLOSE-UP OF THE EQUILIBRIUM CELL AND  
CONSTANT TEMPERATURE BATH.

The cell is the long cylinder upright in the center of the dewar.

Normally, after the samples have been taken, the pressure is released from the system, the bath liquid is recovered from dewar and the cell is allowed to warm to room temperature. The system is then evacuated and allowed to remain under vacuum overnight to be ready for operation the next day. Since more than one run is made per day, it was not necessary to allow the cell to warm up between runs on a particular day, but only at the last run.

#### E. Sampling Systems

After one-half hour of operation, the recirculating pump is stopped and the system pressure is recorded. At this time, a large proportion of the vapor in the system remains in the vapor sampling coil which is part of the recirculation loop. Valves at the end of this sampling coil are closed to isolate the coil from the rest of the system. When these valves are closed, gas samples can be removed at anytime from the coil through the gas sampling valve without being affected by the liquid sampling procedure.

After the vapor sample has been trapped in the vapor coil, the liquid in the cell is sampled by withdrawing a portion of it through the liquid sampling line. The liquid sampling line extends into the equilibrium cell through the vapor outlet to a point just above the vapor distributor plate. The holes in the distributor plate are so arranged that the bubbles of vapor rise clear of the end of the sampling line as they pass up through the liquid. The liquid sampling line, which is a 1/16 in. OD tube with the dead volume reduced to capillary dimensions by insertion of a 20 ga. wire, leads to the liquid sampling valve, which in turn leads to the liquid sampling manifold.

The procedure for taking liquid samples is quite critical and has a considerable effect on the accuracy of the final data. As the liquid sample passes up through the sampling line to the sampling valve, it is warmed from its saturation temperature to a temperature well in the superheat region. The liquid totally vaporizes in a short section of the sampling line, resulting in a fractionation effect in that section of the line. As liquid continues to flow, the fractionation region of the sampling line tends to accumulate the less volatile components, finally reaching approximate equilibrium with the flowing sample stream. It is necessary to throw away the first portion of sample which passes through the sampling valve and to make sure that the flow rate of sample is maintained constant during the sample period. The flow rate is maintained constant by making only one setting of the sampling valve and allowing the vapor to expand through the valve to a pressure which is less than half of the system pressure. Also, while the liquid sample is being withdrawn from the cell, the pressure in the system is maintained by screwing in on the system volume regulator.

Both liquid and vapor samples are finally collected in 75 cc. sample cylinders which are equipped with a pressure gauge at one end and a shut-off valve at the other end. Sample cylinders and manifold are normally purged with sample gas and then evacuated before being filled with the sample.

#### F. Pressure Measurement

The pressure in the equilibrium system is measured by a temperature-compensated Bourdon-tube gauge which has been calibrated by the manufacturer (Heise) and checked with a dead-weight gauge. The low-pressure gauge which was used for measuring pressures at 20 atmospheres and below can be read directly to the nearest 0.1 psi with a hysteresis error of + 0.005 psi. The high-pressure gauge which was used for pressures above 20 atmospheres can be read directly to the nearest 0.3 psi with a hysteresis error of + 0.1 psi.

The pressure gauges used in this experimental program have been tested with an Ashcroft Portable Dead-Weight Tester. The results of this calibration are shown in Figures 5 and 6. As can be seen on the graphs, the 500 psia gauge, Heise H16100, shows no deviation up to 220 psia and deviates only 0.1 psi above 220 psia. The 300 psia gauge, Heise H31596, shows a slight drift with increasing pressure, but the error is never larger than 0.1%. This gauge is considered satisfactory without a correction to the readings.

#### G. Temperature Measurement

The temperature of the equilibrium liquid is measured by a three-element copper-constantan thermocouple which is immersed in the liquid inside the cell. Melting ice is used as the warm end reference junction. Seven separate calibrations have been made of the thermocouple by measurement of the vapor pressure of oxygen. We initially calibrated against the vapor pressures of argon, oxygen and nitrogen but systematic deviations became evident. Oxygen was used as the standard because its normal boiling point is an International Standard Temperature and in this way our calibration was guaranteed to pass through this point.

All seven calibrations covered the temperature range  $-220^{\circ}\text{F}$  to  $-300^{\circ}\text{F}$ . One calibration extended warmer and one calibration extended colder. The data for all seven calibrations was fitted by least squares to a polynomial of millivolts vs. temperature. Figure 7 shows the deviation of the measured versus calculated millivolts with a dashed line drawn to indicate the millivolt deviation equivalent to  $0.1^{\circ}\text{F}$ . As can be seen, almost all points are within  $0.1^{\circ}\text{F}$  of the calibration equation.

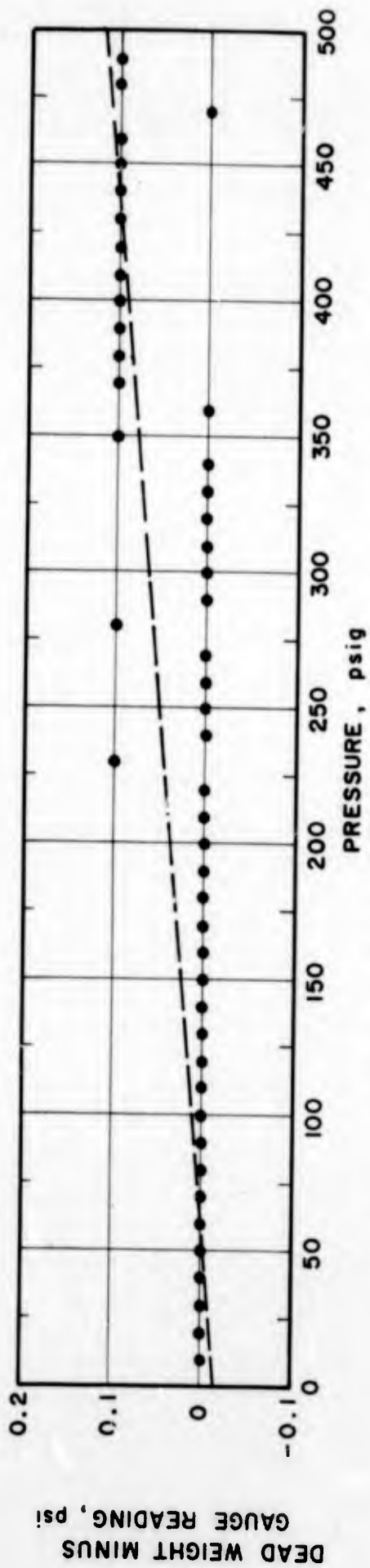


Figure 5. Dead Weight Test of 500 psi Heise Gauge.

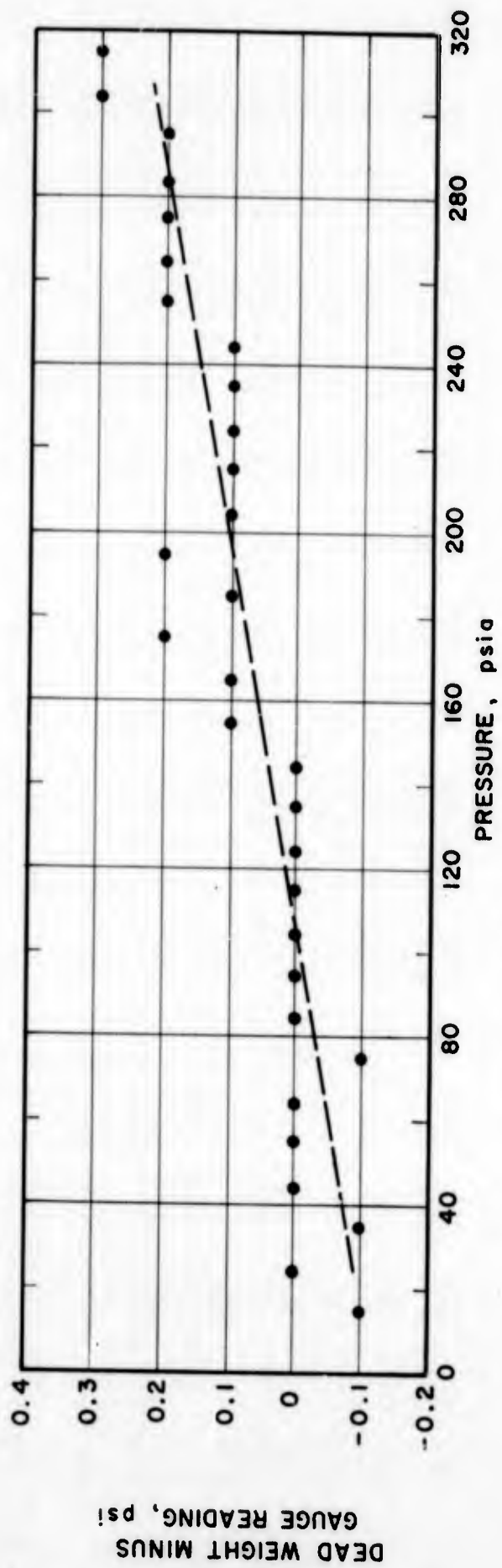


Figure 6. Dead Weight Test of 300 psi Heise Gauge.



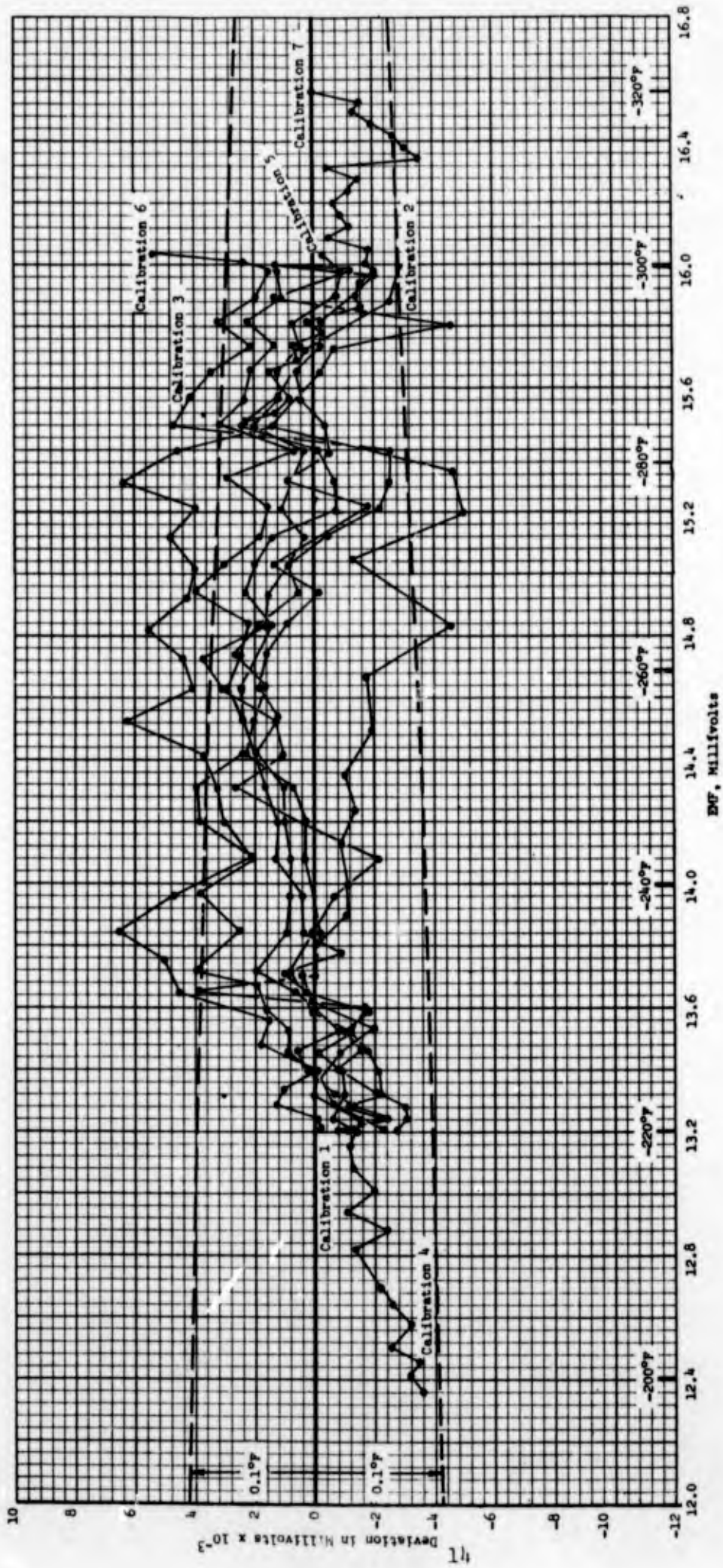


Figure 7. Thermocouple Calibration.

## H. Time of Equilibration

Five runs were made to determine equilibration time of the experimental apparatus with mixtures of nitrogen and argon in the cell. Measurements were made of the following variables after adding an incremental sample of either argon or nitrogen:

1. Temperature - every five seconds
2. Pressure - every five seconds
3. Liquid level - every second on movie film
4. Composition - continuously by means of a Gow-Mac Thermal Conductivity Cell installed in parallel to the vapor recirculation line.

The conditions of the runs are given in Table 1 and the results of Run A, which can be considered typical, are shown in Figure 8. This figure indicates that all the properties change at the same time and the same way. In this case, there was a sharp rise right after the argon was added, a rapid fall-off, a slow recovery with overshoot and a settling to steady-state values. By the time six minutes had elapsed, the transient had settled out. In the measurement of vapor-liquid equilibria, thirty minutes were allowed for equilibration, so equilibrium errors are negligible and contribute a smaller error than reading the pressure and temperature.

TABLE 1  
EQUILIBRATION TEST RESULTS

<u>Run</u>	<u>Temperature of</u>	<u>Initial Pressure Psia</u>	<u>Final Pressure Psia</u>	<u>Time to Equilibrate</u>	<u>% N<sub>2</sub> in Vapor</u>	<u>% Ar in Vapor</u>	<u>Material Added</u>
A	-255	175.6	174.0	4-1/2 min.	51.04	48.96	Argon
B	-247	293.8	290.3	4-1/2 min.	83.73	16.27	Argon
C	-228	294.1	293.7	4-1/2 min.	10.40	89.60	Argon
D	-279	58.8	60.8	5 min.	34.02	65.98	Nitrogen
E	-294	58.8	57.5	4 min.	94.21	5.79	Argon

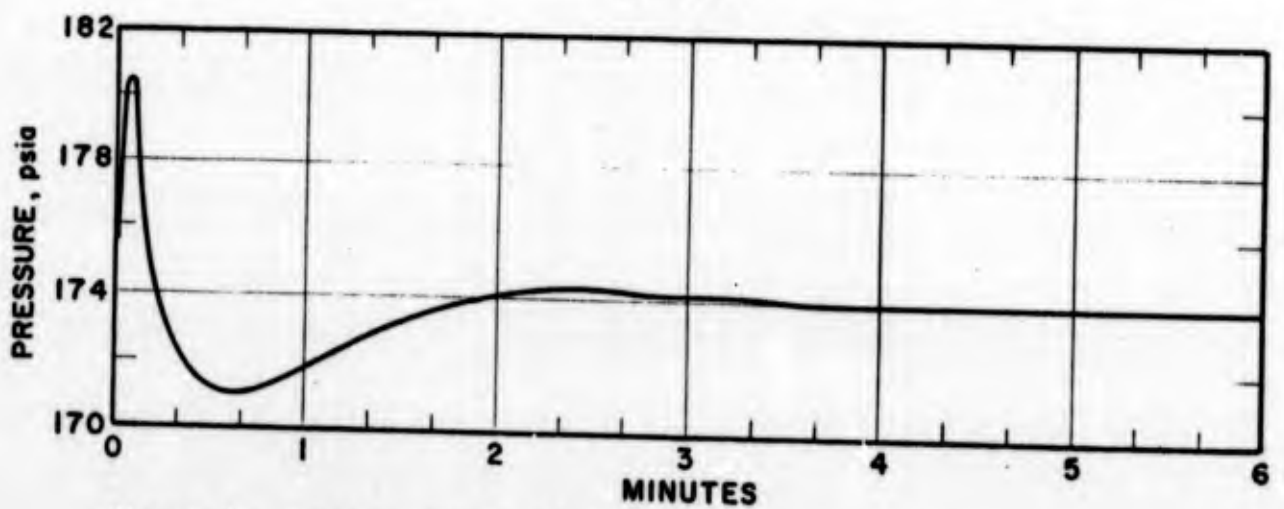
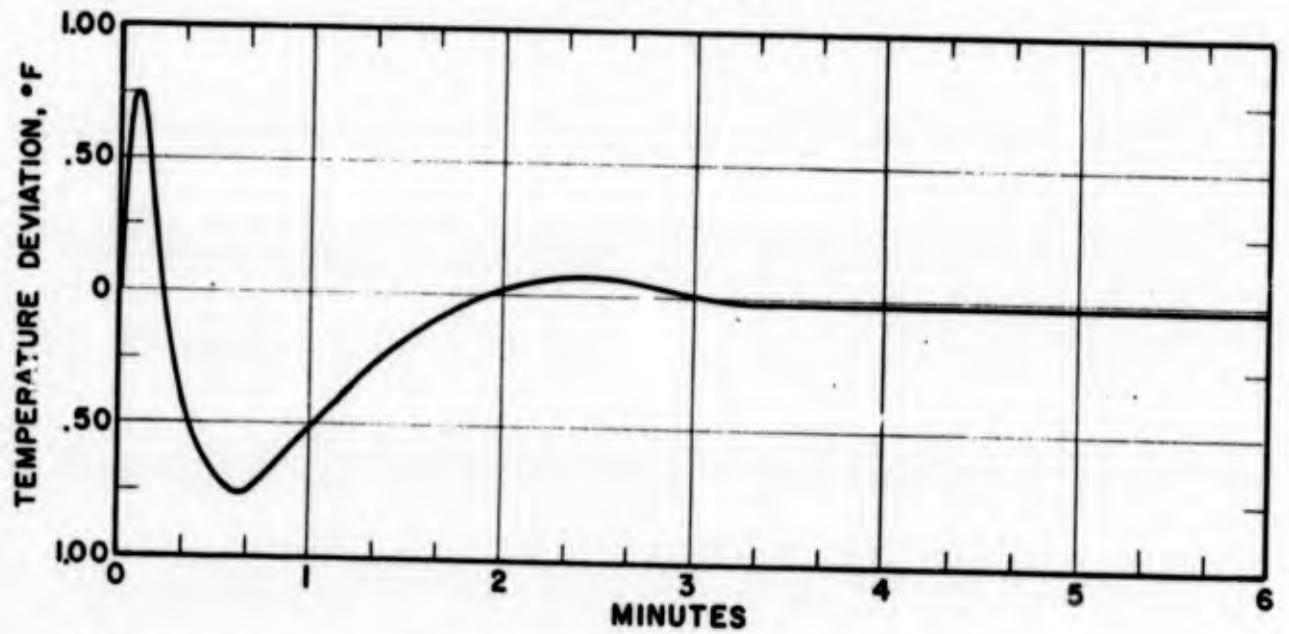
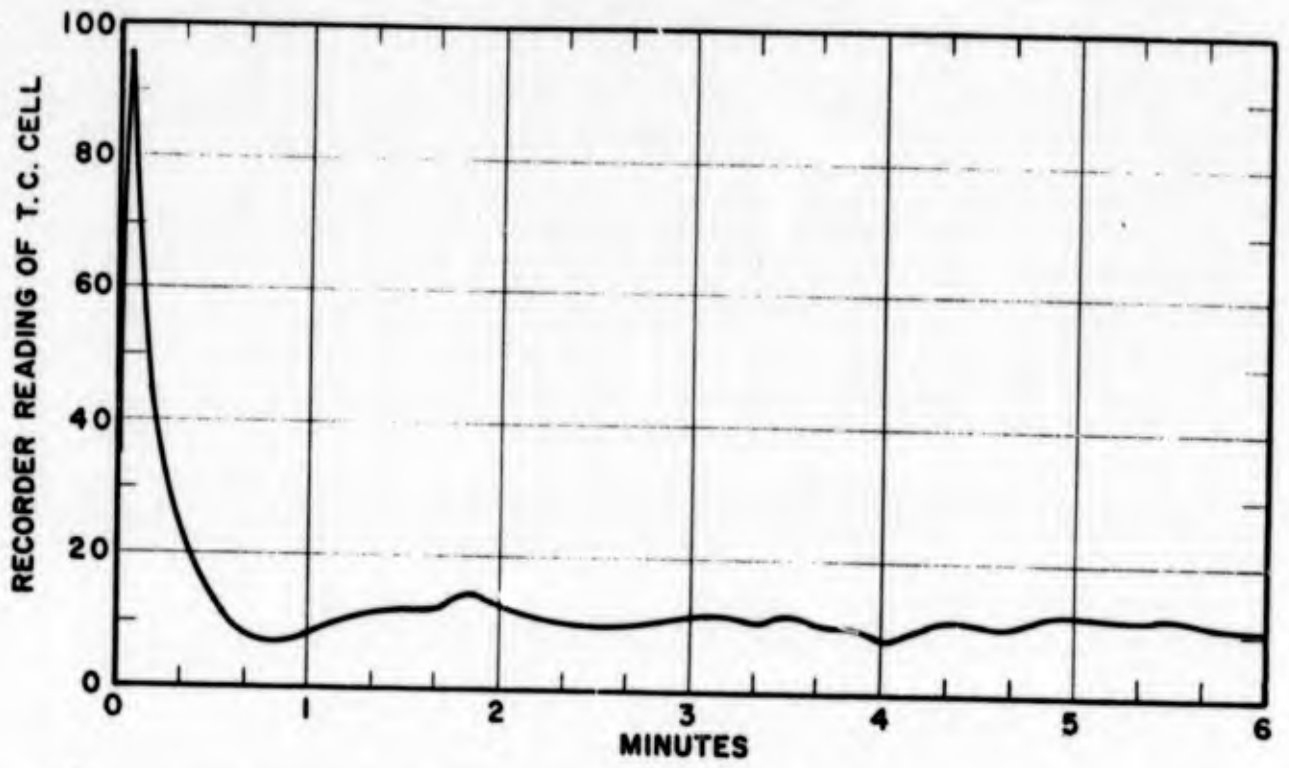


Figure 8. Equilibration Test Run on Vapor-Liquid Apparatus.

#### IV. ANALYTICAL METHODS

The best analytical method for analyzing the argon-oxygen-nitrogen mixtures was judged to be gas chromatography. Other techniques which were considered included: paramagnetic and electrolytic methods for oxygen, titanium sponge technique for argon, and mass spectrometry for argon, oxygen and nitrogen. These techniques were found to have limitations of accuracy and speed which make them inferior to gas chromatography.

##### A. Analyses to Run 264

For the first 150 experimental points a technique was used described in the first quarterly report (3). With this technique, the flow of carrier gas and sample was split, passed through two separate columns and recombined to pass through the same detector. One column was a five-foot length of 28-32 mesh molecular sieve 5A at 105°F and the other column was a six-foot length of 30-70 mesh molecular sieve 5A at -110°F. The first column was used to separate the nitrogen from the argon plus oxygen and the second column was used to separate the oxygen from the argon. In order to get proper separation of the argon it was necessary to provide a retention time of about 12.5 minutes for the oxygen. The maximum deviation with any particular sample was about 1.5% of the resulting analysis.

Between runs 150 and 264 a dual-chromatograph system was used for analysis. One chromatograph determined oxygen and nitrogen and the other chromatograph determined argon. The columns in each chromatograph were identical (6 ft 5A molecular sieves at 30°C), but one chromatograph used argon as the carrier gas and the other used oxygen as the carrier. In this way, the only separation required in either column was between the nitrogen and the other two gases. The chromatograph using argon carrier gas would only register the oxygen part of the argon + oxygen peak and in the chromatograph using oxygen carrier gas, only the argon part of the argon + oxygen peak would register. Frequent calibration standards were required to assure internal consistency of the data. There was an improvement in accuracy over the preceding method.

##### B. Analyses After Run 264

Beginning with run 264 a new method was adopted whereby all three components of an oxygen-nitrogen-argon mixture can be separated on a single chromatographic column. By this method it is possible to calculate the relative proportions of each component from the relative peak size. This has several advantages over the previous methods where a knowledge of the absolute peak size was required. This new method is less sensitive to drift in operating detector current and column

variations since it is only the variation during the period of elution of the peaks which affect the analysis. With the absolute method, any variation in current or column conditions from the time a standard calibration is run until the unknown sample is run will affect the analysis.

By this new method, the components are separated at liquid oxygen temperature on a chromatographic column containing tetrafluoromethane (Freon 14)\* as a solvent on firebrick. The separation is made in the order of the boiling points of the gases with nitrogen emerging first from the column. A sample chromatogram of a mixture containing 77.40% nitrogen, 10.13% argon and 12.47% oxygen is shown in Figure 9. Each of the component peaks is clearly separated from the other peaks. It is possible to obtain duplicate analyses of a mixture which agree within 0.3%. Tests with a standard blend, however, show variations of as much as 1% between analyses on separate days. This presumably is due to some interference between the peaks.

The separation is performed on a 15' x 1/4" column with a flow rate of approximately 230 cc/minute of helium. The ratio of Freon 14 to firebrick is about 1 to 3 by weight. The column is made up by first packing the column with the firebrick, then charging the column with a mixture of Freon 14 and helium at room temperature to a pressure high enough to put the required amount of Freon 14 in the column. This usually requires charging to a pressure between 900 and 1100 psig. Subsequent to pressurization with the Freon 14-helium mixture the column is submerged in boiling liquid oxygen whereupon the Freon 14 condenses as the immobile chromatographic solvent on the firebrick. This column is then used in the conventional manner to separate the components of the oxygen-nitrogen-argon mixtures. The sample size is 5 cc fed in at either 760 or 900 mm Hg (10 cc flooded the column). A sample normally fully separates in fourteen minutes.

Starting with run 1530, the method was modified. It was discovered that a mixture of 30% ethane, 60% tetrafluoromethane, and 10% helium solved the problem of the tailing of nitrogen into the argon peak. The argon retention time increased slightly bringing it closer to the oxygen peak. The charging pressure of the column was reduced to between 500 and 700 psig and the flow rate increased to 300 cc/minute. Analysis time was reduced by this improvement to nine minutes.

A specially built electronic integrator records the response of the thermal conductivity cell. The basic chromatograph is a Beckman GC-2 with two 5 cc sample loops. The column described above is external to the chromatograph box in a dewar of liquid oxygen. The integrator has

\*E. I. Dupont de Nemours Inc. registered trademark.

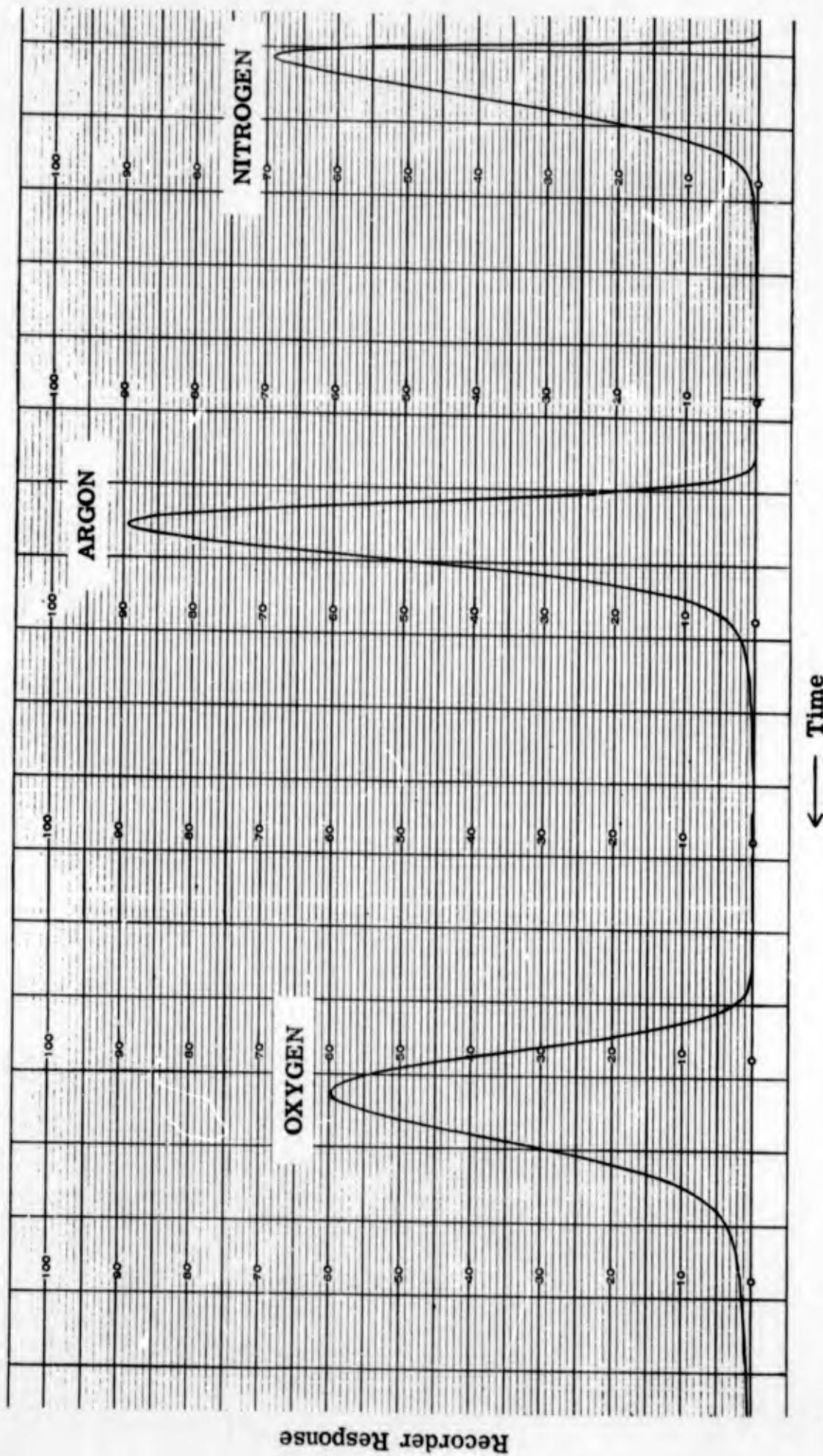


Figure 9. Sample Chromatogram.

four components:

- (1) Hewlett-Packard 5532A Electronic Counter for display
- (2) Dymec Model 2210 Voltage to Frequency Converter
- (3) Sola Type CVH-1 Harmonic-Neutralized Constant Voltage Transformer
- (4) Sanborn 860-1500-PA Amplifier

Also the output of the thermal conductivity cell is recorded as peaks by a Brown Elektronik Recorder with variable sensitivity and span. This recorder is electrically isolated from the integrator. Photographs of the chromatograph are shown in Figures 10 and 11.

The thermal conductivity detector was calibrated in December 1962 and November 1963 over a wide range of sample size and operating conditions to insure accurate analysis of the mixtures. It was found that a two-fold variation in flow rate affects the analysis only 0.3%. A change in the filament current to 2/3 the operating value only affected the analysis by 1%. During actual operation these variables would be expected to vary over only a fraction of these changes. In order to determine the effect of sample size, standard blends of oxygen, nitrogen, and argon were used to determine the response of the detector relative to a 2 cc sample of oxygen. The results of this calibration are shown in Figure 12, in which the relative response,  $q$ , is the inverse of the thermal conductivity cell response. The triangles represent points taken in 1963 and the circles represent the points taken in 1962. The lines drawn on the graph are the calibrations used in all calculations. It can be seen that for the two calibrations the response of oxygen and the response of nitrogen agree. The response of argon differs by 2% for small samples. This difference in the case of argon probably represents a variation in the standards rather than a variation in the cell response. This is indicated by the results in Table 2 which lists analyses of two mixtures which were routinely analyzed daily to determine whether the column was good or needed rebuilding. The special mix ran out at the end of August and synthetic air was first used on April 18, 1963. It is evident from examination of Table 2 that while there was scatter in the daily analyses, there was no systematic trend in the analyses with time.

Compositions were calculated using the relative responses lines shown in Figure 12. The mole fraction of a component is given in terms of peak area and relative response as

$$x_i = \frac{A_i q_i}{A_1 q_1 + A_2 q_2 + A_3 q_3} \quad (1)$$



NOT REPRODUCIBLE



Figure 10. Photograph of Gas Chromatograph.

The column is submerged in the steel dewar in the background. The Beckman GC2-A is shown in the near background. The sample bomb and sample feed system are above the operator's hand. The manometer is behind the recorder. On top of the recorder are the Electronic Counter and the Voltage to Frequency Converter. Not shown are the transformer and amplifier.

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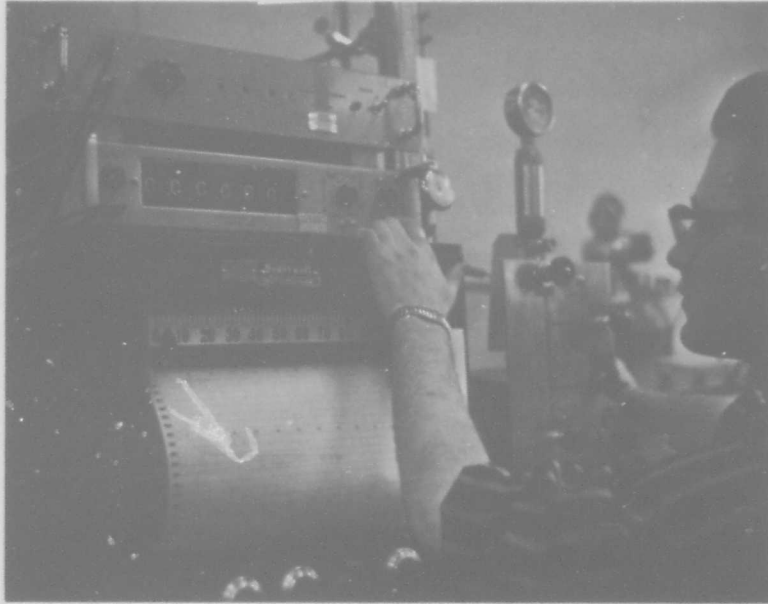


Figure 11. Close-up of Electronic Components of the Chromatograph.

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○ DEC., 1962

△ NOV., 1963

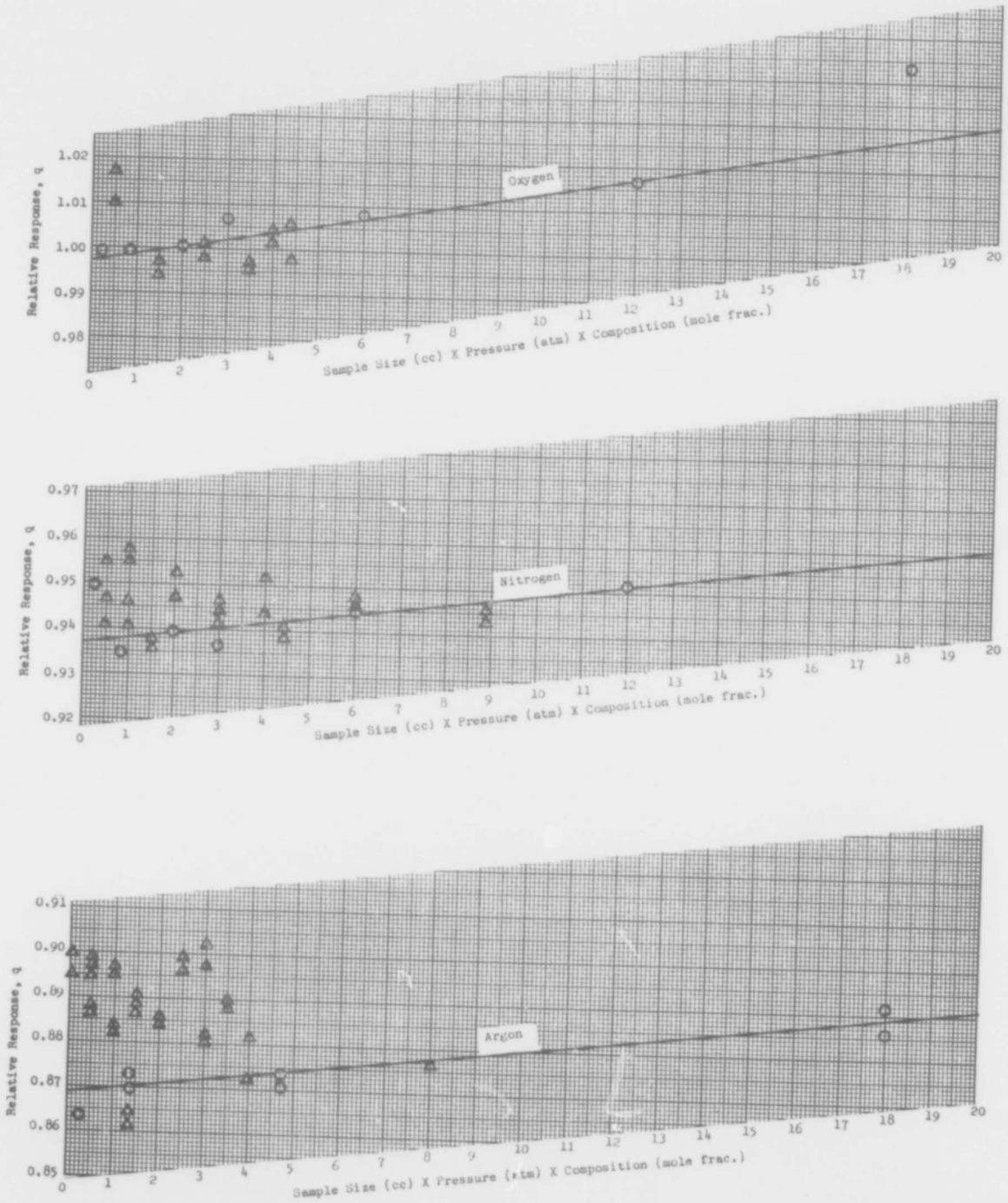


Figure 12. Chromatograph Calibration Curves.

TABLE 2

## SAMPLE LONG-TERM ANALYSES

Synthetic Air				Special Mix			
<u>Date</u>	<u>N<sub>2</sub></u>	<u>Ar</u>	<u>O<sub>2</sub></u>	<u>Date</u>	<u>N<sub>2</sub></u>	<u>Ar</u>	<u>O<sub>2</sub></u>
4-18-63	77.594	0.891	21.513	1-8-63	47.035	3.771	49.195
4-29-63	77.556	0.836	21.607	1-23-63	46.602	3.835	49.563
5-13-63	78.028	0.920	21.051	3-19-63	46.844	3.805	49.350
6-3-63	77.772	0.912	21.315	4-4-63	46.692	3.754	49.555
6-13-63	77.571	0.874	21.553	4-16-63	47.028	3.678	49.295
7-4-63	77.663	0.838	21.497	4-29-63	46.683	3.764	49.552
7-18-63	77.674	0.775	21.569	5-13-63	46.648	3.800	49.550
8-1-63	77.936	0.531	21.531	6-3-63	46.925	3.783	49.291
8-16-63	77.107	0.874	22.018	6-24-63	46.861	3.755	49.383
8-29-63	77.467	0.793	21.739	7-11-63	48.841	3.630	49.527
9-17-63	77.600	0.853	21.546	7-29-63	49.074	3.533	47.394
9-30-63	77.859	0.837	21.302	8-16-63	48.377	3.533	48.089
10-4-63	78.544	0.837	20.617	8-29-63	46.974	3.726	49.299
10-21-63	77.508	0.897	21.593				

## V. EXPERIMENTAL DATA

The tables to follow list the entire experimental data taken during this project. There are listed a total of 1962 points, although there are 1965 listed run numbers; the missing numbers are runs where a mishap such as a lost sample occurred. The data range from one to twenty-six atmospheres and from 139°R to 250°R. Tables 3 through 16 are arranged according to pressure level and the run numbers represent only the chronology of measurement. All runs have been included whether they were used in the correlation or discarded for badness of fit.

The component gases used for these measurements are APCI produced with typical analyses as follows:

Oxygen: 99.70% O<sub>2</sub>, 0.30% Ar

Nitrogen: 99.997% N<sub>2</sub>, 0.003% Ar

Argon: 99.996% Ar, 0.002% N<sub>2</sub>, 0.002% O<sub>2</sub>

A typical run had the following history. One hour elapsed from the time of introduction of the first gas into the equilibrium apparatus until the samples were taken. The samples were stored approximately six hours as analytical inventory and then one hour elapsed during analysis. The raw area data was sent to the computer the next morning and the calculated compositions returned in the afternoon one day later.

Modifications in procedure took place throughout the duration of the program. The first run was made Aug. 13, 1962 and the last run was made October 17, 1963. The following progressive modifications took place during the program.

Run 151: Changed to dual chromatograph system for analysis

Run 264: Changed to relative response, Freon column chromatograph for analysis

Run 609: Finished initial contract

Run 610: Started extension to contract. The 500 psia pressure gauge was installed on the equilibrium apparatus in place of the 300 psia gauge.

Run 936: The 500 psia pressure gauge was removed from the equilibrium apparatus and the 300 psia gauge re-installed.

Runs 1361-1683, 1689-1965: Detachable sample loops used on equilibrium apparatus. All other runs used sample bombs

Run 1530: Mixed solvent Freon-Ethane replaced Freon in the column of the chromatograph

Run 1965: Last run.

TABLE 3  
EXPERIMENTAL DATA AT 1 ATM.

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION	VAPOR MOL FRACTION	RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION	VAPOR MOL FRACTION	
		N2	AR					N2	AR			N2
1576	158.9	.0755	.....	.9245	.2524	1611	155.9	.0758	.5913	.2055	.5522	.2423
1577	155.9	.1554	.....	.8446	.4239	1612	155.9	.0653	.7274	.1825	.6592	.1583
1578	150.9	.3115	.....	.6885	.6571	1613	155.9	.0585	.8213	.1625	.7463	.0912
1579	155.9	.0462	.9538	.....	.1290	1614	152.9	.2371	.0361	.5597	.0316	.4087
1580	152.9	.1411	.8589	.....	.3381	1615	152.9	.2378	.0639	.5465	.0564	.3971
1581	162.4	.....	.0299	.9701	.....	1616	152.9	.2274	.0872	.5346	.0759	.3894
1582	162.2	.....	.0506	.9494	.....	1617	152.9	.2187	.1264	.5142	.1102	.3757
1583	162.1	.....	.0647	.9353	.....	1618	152.9	.2117	.2134	.4922	.1702	.3286
1584	161.8	.....	.0726	.9274	.....	1619	152.9	.1899	.3600	.4403	.2955	.2642
1585	161.5	.....	.0985	.9015	.....	1620	152.9	.1769	.4923	.4075	.3950	.1974
1584	161.2	.....	.1249	.8751	.....	1621	152.9	.1614	.6344	.3736	.4996	.1268
1587	160.4	.....	.2343	.7657	.....	1622	152.9	.1491	.7455	.3573	.5752	.0675
1588	158.9	.....	.5054	.4946	.....	1623	150.9	.3151	.0141	.6573	.0112	.3315
1589	158.4	.....	.6682	.3318	.....	1624	150.9	.3156	.0286	.6527	.0220	.3253
1590	157.9	.....	.8403	.1597	.....	1625	150.9	.3055	.0423	.6404	.0330	.3267
1591	157.4	.....	.9541	.0459	.....	1626	150.9	.3035	.0499	.6369	.0377	.3255
1592	158.9	.0743	.0197	.9156	.2341	1627	150.9	.3012	.0613	.6357	.0477	.3165
1593	158.9	.0629	.0231	.9140	.2175	1628	150.9	.3033	.0880	.6252	.0569	.3080
1594	158.9	.0629	.0335	.9036	.2116	1629	150.9	.3006	.1274	.6143	.0968	.2889
1595	158.9	.0604	.0448	.8948	.2045	1630	150.9	.2969	.2138	.6017	.1579	.2404
1596	158.9	.0591	.0559	.8850	.1977	1631	150.9	.2852	.3181	.5707	.2263	.2031
1597	158.9	.0549	.0812	.8639	.1821	1632	150.9	.2545	.4878	.5151	.3453	.1395
1598	158.9	.0574	.1087	.8339	.1621	1633	150.9	.2407	.6712	.4934	.4572	.0494
1599	158.9	.0411	.1632	.7957	.1310	1634	150.9	.3881	.0692	.7093	.0468	.2439
1600	158.9	.0239	.2824	.6937	.0792	1635	148.9	.3826	.1667	.6820	.1131	.2049
1601	155.9	.1496	.0165	.8339	.4169	1636	148.9	.3661	.2559	.6638	.1468	.1693
1602	155.9	.1451	.0266	.8242	.4091	1637	148.9	.3611	.3675	.6455	.2301	.1244
1603	155.9	.1475	.0347	.8178	.4075	1638	148.9	.3363	.5470	.6094	.3350	.0556
1604	155.9	.1432	.0478	.8090	.4024	1639	148.9	.3131	.6869	.5790	.4210	.....
1605	155.9	.1442	.0607	.7951	.4092	1640	145.0	.5523	.4477	.7838	.2162	.....
1606	155.9	.1381	.0846	.7773	.3871	1641	143.0	.8514	.1486	.8907	.1093	.....
1607	155.9	.1354	.1155	.7491	.3603	1642	143.0	.7307	.....	.9147	.....	.....
1608	155.9	.1249	.1894	.6857	.3331	1643	146.9	.4961	.....	.8050	.....	.....
1609	155.9	.1030	.3263	.5707	.2785	1644	141.5	.8710	.....	.9627	.....	.....
1610	155.9	.0883	.4522	.4595	.2397	1645	140.0	.9860	.....	.9962	.....	.....

TABLE 3  
EXPERIMENTAL DATA AT 1 ATM. (continued)

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION N2	LIQUID MOL FRACTION AR	LIQUID MOL FRACTION O2	VAPOR MOL FRACTION N2	VAPOR MOL FRACTION AR	VAPOR MOL FRACTION O2	RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION N2	LIQUID MOL FRACTION AR	LIQUID MOL FRACTION O2	VAPOR MOL FRACTION N2	VAPOR MOL FRACTION AR	VAPOR MOL FRACTION O2
1646	141.5	.8457	.1543	.....	.9363	.0637	.....	1682	140.0	.9766	.0102	.0132	.9917	.0025	.0057
1647	141.0	.8790	.1210	.....	.9506	.0494	.....	1683	140.0	.9779	.0162	.0059	.9892	.0096	.0012
1648	140.4	.9373	.0627	.....	.9749	.0251	.....	1923	162.5	.....	.0088	.9912	.....	.0142	.9858
1649	140.2	.9623	.0377	.....	.9843	.0157	.....	1924	160.4	.....	.2559	.7441	.....	.3327	.6673
1650	140.0	.9822	.0178	.....	.9938	.0062	.....	1925	158.9	.....	.0789	.9057	.....	.0191	.7250
1651	139.7	.9928	.0072	.....	.9973	.0027	.....	1926	158.9	.0543	.0154	.8317	.2559	.0191	.7250
1652	146.9	.4775	.0150	.5075	.7892	.0093	.2016	1927	157.4	.....	.9754	.0236	.1778	.1431	.6790
1653	146.9	.4825	.0217	.4958	.7883	.0145	.1972	1928	155.9	.1397	.0612	.7991	.....	.9783	.0217
1654	146.9	.4840	.0358	.4902	.7866	.0218	.1916	1929	155.9	.1297	.1193	.7509	.3901	.0641	.5458
1655	146.9	.4800	.0485	.4715	.7864	.0295	.1841	1930	155.9	.0578	.7335	.2087	.3595	.1244	.5160
1656	146.9	.4879	.0673	.4449	.7862	.0402	.1736	1931	155.9	.0432	.9005	.0563	.1596	.6820	.1584
1657	146.9	.4894	.0924	.4182	.7794	.0544	.1661	1942	150.9	.2924	.2203	.4874	.1187	.8395	.0418
1658	146.9	.4789	.1308	.3903	.7655	.0772	.1572	1943	146.9	.4958	.0207	.4835	.5925	.1610	.2465
1659	146.9	.4743	.2292	.2965	.7512	.1298	.1190	1944	146.9	.4529	.3779	.1693	.7978	.0124	.1898
1660	146.9	.4489	.3809	.1702	.7063	.2064	.0853	1945	145.0	.5769	.3597	.0634	.7196	.2104	.0699
1661	146.9	.4344	.5184	.0471	.6981	.2818	.0201	1946	145.0	.5936	.0404	.3660	.8015	.1750	.0235
1662	145.0	.6166	.0392	.3442	.8578	.0189	.1234	1947	145.0	.6075	.0895	.3030	.8474	.0215	.1304
1663	145.0	.6106	.0873	.3021	.8481	.0407	.1112	1948	145.0	.5867	.0956	.2177	.8474	.0461	.1065
1664	145.0	.5916	.1818	.2266	.8292	.0935	.0773	1949	143.0	.7464	.0102	.2435	.8223	.0992	.0785
1665	143.0	.5823	.2789	.1388	.8111	.1354	.0633	1950	143.0	.7571	.0275	.2153	.9182	.0048	.0770
1666	143.0	.7478	.0112	.2410	.9178	.0057	.0765	1951	143.0	.7150	.2431	.0419	.9193	.0124	.0683
1667	143.0	.7522	.0250	.2228	.9174	.0107	.0719	1952	143.0	.7077	.2923	.....	.8707	.1073	.0141
1668	143.0	.7584	.0337	.2080	.9197	.0150	.0633	1953	141.5	.9612	.0388	.....	.9851	.0149	.....
1669	143.0	.7524	.0502	.1975	.9150	.0228	.0621	1954	141.5	.8647	.....	.....	.9851	.0149	.....
1670	143.0	.7528	.0744	.1728	.9123	.0333	.0544	1955	141.5	.8504	.1496	.1353	.9606	.....	.0394
1671	143.0	.7464	.0921	.1615	.9078	.0414	.0508	1956	141.5	.8504	.1496	.....	.9387	.....	.....
1672	143.0	.7313	.1314	.1373	.8979	.0590	.0431	1957	141.5	.8664	.0095	.1239	.9581	.0613	.....
1673	143.0	.7203	.2422	.0375	.8922	.1064	.0114	1958	141.5	.8562	.1093	.0345	.9454	.0041	.0377
1674	141.5	.8569	.0280	.1351	.9545	.0048	.0407	1959	140.8	.9001	.0999	.....	.9454	.0449	.0097
1675	141.5	.8573	.0186	.1241	.9549	.0078	.0407	1959	140.1	.9622	.0378	.....	.9598	.0402	.....
1676	141.5	.8378	.0395	.1027	.9544	.0078	.0373	1960	140.2	.9549	.0451	.....	.9852	.0148	.....
1677	141.5	.8515	.0499	.0986	.9544	.0170	.0286	1961	140.3	.9523	.0477	.....	.9818	.0182	.....
1678	141.5	.8544	.0615	.0841	.9500	.0205	.0295	1962	129.9	.9845	.0155	.....	.9808	.0192	.....
1679	141.5	.8502	.0875	.0623	.9492	.0251	.0251	1963	140.0	.9838	.0043	.....	.9940	.0060	.....
1680	141.5	.8616	.1097	.0287	.9458	.0360	.0181	1964	140.0	.9844	.0098	.0119	.9953	.0016	.0030
1681	140.0	.9788	.0080	.0132	.9490	.0425	.0085	1965	140.0	.9778	.0151	.0058	.9948	.0038	.0014
					.9934	.0022	.0044						.9924	.0057	.0019



TABLE 4  
EXPERIMENTAL DATA AT 2 ATM.

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION N2	LIQUID MOL FRACTION AR	LIQUID MOL FRACTION O2	VAPOR MOL FRACTION N2	VAPOR MOL FRACTION AR	VAPOR MOL FRACTION O2	TEMP. DEG.R	LIQUID MOL FRACTION N2	LIQUID MOL FRACTION AR	LIQUID MOL FRACTION O2	VAPOR MOL FRACTION N2	VAPOR MOL FRACTION AR	VAPOR MOL FRACTION O2
1466	171.9	.0721	.....	.9279	.2160	.....	.7840	1500	168.9	.1258	.1657	.3082	.1703	.5215
1467	168.9	.1470	.....	.8530	.3769	.....	.6231	1501	168.9	.1058	.2999	.2589	.2997	.4414
1468	162.9	.3437	.....	.6563	.6407	.....	.3593	1502	168.9	.0845	.4310	.2239	.4141	.3620
1469	158.9	.5139	.....	.4861	.7823	.....	.2177	1503	168.9	.0725	.5494	.1775	.5296	.2928
1470	160.9	.3406	.6594	.....	.5779	.4221	.....	1504	168.9	.0623	.6623	.1506	.6330	.2164
1471	165.9	.1371	.8629	.....	.3001	.6999	.....	1505	168.9	.0484	.7692	.1205	.7307	.1487
1472	167.9	.0708	.9292	.....	.1762	.8238	.....	1506	165.9	.2297	.0280	.5029	.0258	.4713
1473	175.1	.....	.0464	.9536	.....	.0644	.9356	1507	165.9	.2228	.0672	.4845	.0616	.4538
1474	175.3	.....	.0195	.9805	.....	.0288	.9712	1508	165.9	.2160	.1350	.4619	.1202	.4179
1475	175.0	.....	.0524	.9476	.....	.0753	.9247	1509	165.9	.2012	.2539	.4280	.2190	.3531
1476	174.8	.....	.0690	.9310	.....	.0975	.9025	1510	165.9	.1812	.4112	.3848	.3475	.2677
1477	174.7	.....	.0808	.9192	.....	.1138	.8862	1511	165.9	.1646	.5671	.3518	.4692	.1790
1478	174.5	.....	.0962	.9038	.....	.1335	.8665	1512	165.9	.1461	.7326	.3194	.5955	.0851
1479	174.3	.....	.1160	.8820	.....	.1594	.8406	1513	165.9	.1390	.8357	.3044	.6784	.0173
1480	173.4	.....	.2357	.7643	.....	.2972	.7028	1514	162.9	.3364	.0131	.6306	.0129	.3565
1481	171.9	.....	.5050	.4941	.....	.5674	.4326	1515	162.9	.3317	.0286	.6273	.0225	.3502
1482	171.4	.....	.5902	.4098	.....	.6432	.3568	1516	162.9	.3331	.0402	.6282	.0315	.3403
1483	170.6	.....	.7881	.2119	.....	.8151	.1849	1517	162.9	.3288	.0531	.6228	.0411	.3361
1484	170.3	.....	.9722	.0278	.....	.9762	.0238	1518	162.9	.3324	.0666	.6225	.0515	.3260
1485	171.9	.0719	.0094	.9187	.2081	.0122	.7797	1519	162.9	.3240	.0965	.6245	.0701	.3054
1486	171.9	.0717	.0187	.9096	.2118	.0233	.7648	1520	162.9	.3220	.1370	.5970	.1048	.2982
1487	171.9	.0699	.0332	.8969	.2009	.0414	.7577	1521	162.9	.3146	.2092	.5787	.1577	.2636
1488	171.9	.0658	.0507	.8835	.1892	.0627	.7481	1522	162.9	.2930	.3768	.5382	.2757	.1861
1489	171.9	.0652	.0619	.8729	.1856	.0767	.7378	1523	162.9	.2740	.5469	.5058	.3903	.1039
1490	171.9	.0565	.0680	.8555	.1619	.1083	.7298	1524	162.9	.2601	.6540	.4860	.4610	.0530
1491	171.9	.0505	.1286	.8209	.1439	.1568	.6993	1525	160.9	.4083	.0573	.6986	.0388	.2626
1492	171.9	.0282	.2552	.7167	.0804	.3037	.6159	1526	160.9	.4062	.0949	.6882	.0653	.2465
1493	168.9	.1393	.0098	.8509	.3684	.0108	.6208	1527	160.9	.3932	.1777	.6643	.1206	.2150
1494	168.9	.1370	.0266	.8364	.3545	.0283	.6172	1528	160.9	.3766	.3155	.6311	.2144	.1545
1495	168.9	.1353	.0374	.8273	.3490	.0388	.6122	1529	160.9	.3595	.4856	.6029	.3140	.0831
1496	168.9	.1388	.0482	.8130	.3401	.0512	.6087	1530	158.9	.5052	.0127	.7761	.0178	.2161
1497	168.9	.1363	.0581	.8056	.3482	.0620	.5899	1531	158.9	.5088	.0255	.7757	.0132	.2081
1498	168.9	.1318	.0880	.7802	.3397	.0893	.5710	1532	158.9	.5039	.0404	.7711	.0256	.2033
1499	168.9	.1323	.1132	.7545	.3284	.1183	.5533	1533	158.9	.5052	.0595	.7653	.0382	.1966

TABLE 4  
EXPERIMENTAL DATA AT 2 ATM. (continued)

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION N2	VAPOR MOL FRACTION AR	VAPOR MOL FRACTION O2
		N2	AR			N2	AR			
1534	158.9	.5070	.0721	1569	151.5	.9719	.0281	.9880	.0120	.....
1535	158.9	.5024	.0979	1570	151.7	.9529	.0471	.9798	.0202	.....
1536	158.9	.4960	.1387	1571	151.8	.9410	.0590	.9738	.0262	.....
1537	158.9	.4978	.2360	1572	152.2	.9001	.0999	.9547	.0453	.....
1538	158.9	.4725	.3439	1573	152.9	.8450	.1550	.9283	.0717	.....
1539	158.9	.4560	.4730	1574	154.9	.6956	.3044	.8500	.1500	.....
1540	156.9	.6172	.9377	1575	157.9	.4978	.5022	.7189	.2811	.....
1541	156.9	.6072	.1204	1896	175.2	.....	.0274	.....	.0395	.9605
1542	156.9	.6061	.1386	1897	171.9	.....	.4999	.....	.5608	.4392
1543	156.9	.6027	.1926	1898	171.9	.....	.0750	.....	.0133	.7694
1544	156.9	.5723	.3893	1899	170.2	.....	.0105	.....	.2172	.....
1545	154.9	.7392	.0133	1900	168.9	.....	.9785	.....	.9799	.0201
1546	154.9	.7376	.0279	1901	168.9	.0417	.8890	.1059	.8364	.0577
1547	154.9	.7343	.0418	1902	168.3	.1417	.0402	.3576	.0434	.5990
1548	154.9	.7318	.0541	1903	168.3	.1349	.0919	.3357	.0976	.5668
1549	154.9	.7273	.0693	1904	168.3	.0834	.4342	.2050	.4284	.3666
1550	154.9	.7220	.0992	1905	167.9	.0586	.6829	.1456	.6495	.2049
1551	154.9	.7246	.1281	1906	165.9	.0670	.9330	.1654	.8346	.....
1552	154.9	.7038	.2521	1907	165.9	.2359	.....	.5189	.....	.4811
1553	152.9	.8681	.0164	1908	165.9	.1335	.8386	.2960	.....	.0202
1554	152.9	.8756	.0249	1909	162.9	.3365	.0150	.6354	.0119	.3527
1555	152.9	.8732	.0380	1910	162.9	.3271	.0952	.6103	.0743	.3152
1556	152.9	.8722	.0465	1911	160.9	.4144	.0331	.7069	.0238	.2693
1557	152.9	.8633	.0539	1912	160.9	.4192	.0539	.7036	.0373	.2591
1558	152.9	.8654	.0813	1913	158.9	.4848	.2341	.7284	.1428	.1289
1559	152.9	.8595	.0724	1932	158.9	.5032	.0524	.7685	.0341	.1974
1560	151.9	.9460	.0952	1933	156.9	.6123	.0688	.8304	.0385	.1311
1561	151.9	.9409	.0071	1934	156.9	.5909	.1957	.8013	.1091	.0896
1562	151.9	.7349	.0207	1935	152.9	.8464	.1261	.9320	.0580	.0101
1563	151.9	.9343	.0339	1936	152.9	.8576	.0244	.9511	.0117	.0372
1564	154.9	.7401	.0424	1937	152.9	.8636	.0449	.9476	.0208	.0316
1565	152.9	.8744	.....	1938	152.9	.8583	.0582	.9436	.0273	.0291
1566	151.9	.9449	.....	1939	151.9	.9330	.0343	.9737	.0153	.0110
1567	151.2	.9949	.0051	1940	151.9	.9277	.0634	.9691	.0281	.0028
1568	151.4	.9810	.....	1941	151.2	.9336	.0434	.9731	.0191	.0078
						.9930	.0070	.9972	.0028	.....

TABLE 5  
EXPERIMENTAL DATA AT 4 ATM.

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION	
		N2	AR	N2	AR			N2	AR	N2	AR
1361	182.8	.0702	.9298	.0000	.8453	1394	186.8	.0717	.0609	.1783	.0721
1362	180.8	.1320	.8660	.0000	.7297	1395	186.8	.0679	.0781	.1672	.0905
1363	174.8	.3687	.6313	.0000	.4268	1396	186.8	.0639	.1128	.1543	.1302
1364	171.9	.5277	.4723	.0000	.2870	1397	186.8	.0547	.1363	.1360	.1598
1365	168.4	.7372	.2628	.0000	.1417	1398	186.8	.0474	.1859	.1162	.2150
1366	166.9	.8444	.1556	.0000	.0786	1399	186.8	.0252	.3400	.0615	.3913
1367	165.9	.9181	.0819	.0000	.0386	1400	183.8	.1581	.0139	.3473	.0148
1368	165.6	.9373	.0627	.0000	.0292	1401	183.8	.1524	.0274	.3422	.0296
1369	165.4	.9529	.0471	.0000	.0222	1402	183.8	.1490	.0435	.3320	.0454
1370	165.3	.9632	.0368	.0000	.0172	1403	183.8	.1492	.0589	.3286	.0510
1371	165.1	.9775	.0225	.0000	.0098	1404	183.8	.1444	.0767	.3186	.0903
1372	165.0	.9872	.0128	.0000	.0059	1405	183.8	.1403	.1073	.3108	.1133
1373	186.8	.0860	.0000	.9140	.0000	1406	183.8	.1315	.1320	.2935	.1379
1374	183.8	.1591	.0000	.8409	.0000	1407	183.8	.1243	.1982	.2683	.2019
1375	177.8	.3454	.0000	.6546	.0000	1408	183.8	.0937	.4243	.2014	.4176
1376	171.9	.5987	.0000	.4013	.0000	1409	183.8	.0738	.5904	.1592	.5689
1377	168.4	.7788	.0000	.2212	.0000	1410	183.8	.0552	.7561	.1207	.7216
1378	166.9	.8697	.0000	.1303	.0000	1411	183.8	.0454	.9092	.1007	.8608
1379	165.4	.9620	.0000	.0380	.0000	1412	180.8	.2469	.0276	.4821	.0255
1380	190.6	.0000	.0252	.9748	.0000	1413	180.8	.2334	.0689	.4625	.0633
1381	190.4	.0000	.0514	.9466	.0346	1414	180.8	.2262	.1275	.4410	.4742
1382	190.3	.0000	.0446	.9554	.0677	1415	180.8	.2021	.2884	.3889	.4407
1383	190.2	.0000	.0471	.9529	.0605	1416	180.8	.1738	.5136	.3345	.4451
1384	190.1	.0000	.0519	.9481	.0640	1417	180.8	.1579	.6464	.3087	.4517
1385	189.8	.0000	.0804	.9196	.1077	1418	180.8	.1447	.7674	.2880	.6488
1386	188.8	.0000	.1947	.8053	.2444	1419	180.8	.1415	.8257	.2784	.6971
1387	187.3	.0000	.4232	.5768	.4807	1420	177.8	.3435	.0091	.6006	.0245
1388	186.3	.0000	.6296	.3704	.6616	1421	177.8	.3423	.0211	.5966	.0074
1389	185.8	.0000	.7869	.2131	.8077	1422	177.8	.3407	.0387	.5906	.0167
1390	185.4	.0000	.9313	.0687	.9399	1423	177.8	.3380	.0472	.5906	.0315
1391	186.8	.0812	.0154	.9033	.0182	1424	177.8	.3305	.0867	.5889	.0384
1392	186.8	.0765	.0316	.8920	.0378	1425	177.8	.3200	.1328	.5729	.0709
1393	186.8	.0748	.0478	.8774	.0563	1426	177.8	.3152	.1763	.5560	.1071
										.5436	.1412
											.3152

TABLE 5  
EXPERIMENTAL DATA AT 4 ATM. (continued)

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION	
		N <sub>2</sub>	AR	N <sub>2</sub>	O <sub>2</sub>			N <sub>2</sub>	AR	N <sub>2</sub>	AR
1427	177.8	.3092	.2168	.4740	.2885	1460	166.9	.8683	.0650	.9408	.0324
1428	177.8	.2841	.4007	.3153	.1978	1461	166.9	.8583	.1006	.9340	.0505
1429	177.8	.3054	.5906	.1040	.0743	1462	166.9	.8557	.1279	.9290	.0650
1430	174.8	.4548	.0319	.5132	.2771	1463	165.4	.9614	.0120	.9847	.0053
1431	174.8	.4474	.0906	.4621	.2509	1464	165.4	.9625	.0228	.9836	.0107
1432	174.8	.4374	.1559	.4068	.2229	1465	165.4	.9634	.0187	.9843	.0086
1433	174.8	.4171	.2735	.3094	.1670	1869	190.6	.0000	.0110	.0000	.0148
1434	174.8	.3981	.4444	.1574	.0833	1870	190.4	.0000	.0291	.0000	.0401
1435	174.8	.3890	.5421	.0689	.0405	1871	190.1	.0000	.0558	.0000	.0759
1436	171.9	.5909	.0114	.3887	.1861	1872	189.3	.0000	.1417	.0000	.1928
1437	171.9	.5913	.0251	.3837	.1850	1873	185.4	.0000	.9506	.0000	.9552
1438	171.9	.5940	.0341	.3718	.1757	1874	183.8	.1527	.0399	.3369	.0422
1439	171.9	.5931	.0512	.3557	.1706	1875	180.8	.1991	.2954	.3831	.2630
1440	171.9	.5932	.0618	.3451	.1674	1876	180.8	.1445	.7618	.2849	.6459
1441	171.9	.5898	.0880	.3222	.1555	1877	177.8	.2448	.7552	.4251	.5749
1442	171.9	.5868	.1162	.2970	.1438	1878	177.8	.3354	.0739	.5785	.0602
1443	171.9	.5664	.2279	.2057	.1011	1879	176.8	.2571	.6278	.4479	.4771
1444	171.9	.5505	.3544	.0951	.0454	1880	176.8	.3830	.0000	.6380	.0000
1445	169.9	.6897	.0641	.2461	.1074	1881	174.8	.3849	.5483	.5908	.3705
1446	169.9	.6811	.1252	.1936	.0859	1882	171.9	.5931	.0120	.8019	.0076
1447	169.9	.6678	.2317	.1005	.0451	1883	171.9	.5895	.0243	.7980	.0153
1448	168.4	.7814	.0118	.2068	.0890	1884	171.9	.5410	.3648	.7306	.2215
1449	168.4	.7764	.0259	.1977	.0826	1885	169.9	.6860	.0675	.8502	.0392
1450	168.4	.7744	.0406	.1850	.0792	1886	168.4	.7741	.0273	.9005	.0148
1451	168.4	.7694	.0565	.1741	.0738	1887	168.4	.7714	.0427	.8981	.0233
1452	168.4	.7686	.0645	.1669	.0696	1888	166.9	.8638	.0168	.9443	.0084
1453	168.4	.7668	.0929	.1403	.0599	1889	166.9	.8492	.1004	.9279	.0519
1454	168.4	.7614	.1346	.1040	.0449	1890	166.9	.8456	.1359	.9226	.0698
1455	168.4	.7486	.2051	.0463	.0200	1891	165.4	.9552	.0175	.9613	.0081
1456	166.9	.8655	.0126	.1219	.0461	1892	165.4	.9547	.0270	.9790	.0132
1457	166.9	.8678	.0255	.1067	.0421	1893	165.4	.9535	.0215	.9799	.0104
1458	166.9	.8681	.0344	.0975	.0394	1894	165.4	.9528	.0347	.9780	.0047
1459	166.9	.8667	.0487	.0846	.0344	1895	165.1	.9737	.0263	.9872	.0128

TABLE 6  
EXPERIMENTAL DATA AT 6 ATM.

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION	
		N <sub>2</sub>	AR	N <sub>2</sub>	AR			N <sub>2</sub>	AR	N <sub>2</sub>	AR
453	197.8	.0721	.....	.9279	.1646	492	186.8	.3645	.1810	.5705	.1430
454	195.8	.1213	.....	.8787	.2595	493	182.8	.5443	.0363	.7464	.0253
455	191.8	.2285	.....	.7715	.4310	494	182.8	.5410	.0555	.7405	.0377
456	187.8	.3548	.....	.6452	.5440	495	182.8	.5387	.0725	.7410	.0484
457	183.8	.5069	.....	.4931	.7208	496	182.8	.5354	.0936	.7308	.0650
458	179.8	.6890	.....	.3110	.8468	497	182.8	.5276	.1321	.7362	.0930
459	176.8	.8413	.....	.1587	.9284	498	182.8	.5153	.1887	.7076	.1292
460	174.8	.9513	.....	.0487	.9794	499	179.8	.6730	.0355	.8351	.0222
461	200.8	.....	.0274	.9726	.....	500	179.8	.6730	.0574	.8296	.0358
462	200.5	.....	.0550	.9450	.....	501	179.8	.6710	.0755	.8398	.0433
463	200.2	.....	.0868	.9132	.....	502	179.8	.6679	.0953	.8236	.0591
464	199.9	.....	.1198	.8802	.....	503	179.8	.6630	.1332	.8149	.0831
465	174.8	.9373	.0627	.....	.6666	504	179.8	.6536	.1906	.8404	.0957
466	175.3	.9035	.0965	.....	.9474	505	177.8	.7714	.0625	.8849	.0367
467	175.8	.8728	.1272	.....	.9314	506	177.8	.7655	.1372	.8814	.0540
468	176.3	.8395	.1605	.....	.9107	507	177.8	.7566	.1975	.8750	.0797
469	198.8	.6441	.0307	.9252	.1037	508	177.8	.8903	.0240	.9500	.0125
470	198.8	.0408	.0474	.9116	.0966	509	175.8	.8651	.0459	.9377	.0455
471	198.8	.0261	.0623	.9116	.0879	510	175.8	.8511	.0511	.9466	.0274
472	198.8	.0354	.0794	.8852	.0819	511	175.8	.8228	.0670	.9407	.0358
473	198.8	.0247	.1000	.8714	.0666	512	175.8	.8228	.0800	.9377	.0455
474	198.8	.0190	.1561	.8249	.0441	513	175.8	.8228	.0972	.9377	.0527
475	194.8	.1400	.0319	.8261	.2413	514	174.8	.8228	.1140	.9325	.0175
476	194.8	.1371	.0486	.8142	.1941	515	174.8	.8228	.0383	.9760	.0175
477	194.8	.1334	.0676	.7990	.0714	516	174.8	.9428	.0074	.9748	.0039
478	194.8	.1317	.0814	.7864	.2769	517	174.8	.9428	.0191	.9748	.0039
479	194.8	.1242	.1130	.7628	.2707	518	198.8	.0440	.0191	.9748	.0039
480	194.8	.1154	.1685	.7161	.2552	519	198.8	.0366	.0636	.1039	.0234
481	190.8	.2531	.0327	.7142	.2392	520	194.8	.1436	.0191	.0875	.0769
482	190.8	.2483	.0529	.6988	.4605	521	190.8	.2565	.0193	.2946	.0201
483	190.8	.2477	.0683	.6841	.4519	522	186.8	.3669	.0200	.4623	.0142
484	190.8	.2441	.0834	.6724	.4485	523	186.8	.3786	.0509	.6130	.0161
485	190.8	.2388	.1232	.6379	.4436	524	186.8	.5444	.0182	.6046	.0410
486	190.8	.2294	.1742	.5963	.4303	525	182.8	.5335	.0760	.7475	.0128
487	186.8	.3858	.0344	.5796	.4126	526	182.8	.5268	.1323	.7214	.0513
488	186.8	.3641	.0522	.5636	.6105	527	179.8	.6769	.0136	.8395	.0909
489	186.8	.3826	.0684	.5489	.6893	528	179.8	.6685	.0731	.8395	.0909
490	186.8	.3773	.0899	.5328	.6016	529	179.8	.6516	.1921	.8257	.0450
491	186.8	.3725	.1243	.5032	.5953	530	177.8	.7764	.0179	.8038	.1181
					.5856	531	177.8	.7785	.0314	.8944	.0097
					.3158	532				.8934	.0175
					.3158						

TABLE 6  
EXPERIMENTAL DATA AT 6 ATM. (continued)

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION	
		N2	AR	N2	AR			N2	AR	N2	AR
1304	190.8	.1452	.0548	.0000	.0000	1343	184.8	.3940	.4997	.5819	.3544
1305	184.8	.3758	.6242	.0000	.0000	1344	182.8	.5392	.0093	.7502	.0067
1306	179.8	.6219	.3781	.0000	.0000	1345	182.8	.5397	.0301	.7436	.0210
1307	177.8	.7409	.2591	.0000	.0000	1346	182.8	.4958	.3724	.6788	.2482
1308	174.6	.9522	.0478	.0000	.0000	1347	182.8	.4823	.4513	.6649	.2986
1309	174.4	.9610	.0390	.0000	.0000	1348	179.8	.6843	.0171	.8404	.0101
1310	174.3	.9701	.0299	.0000	.0000	1349	179.8	.6809	.0317	.8365	.0198
1311	174.2	.9802	.0198	.0000	.0000	1350	179.8	.6735	.0423	.8315	.0255
1312	174.1	.9918	.0082	.0000	.0000	1351	179.8	.6454	.2702	.7922	.1647
1313	201.0	.0000	.0036	.9964	.0000	1352	177.8	.7869	.0095	.8998	.0057
1314	200.9	.0000	.0035	.9965	.9942	1353	177.8	.7800	.0233	.8953	.0135
1315	200.7	.0000	.0232	.9768	.9948	1354	177.8	.7785	.0440	.8928	.0253
1316	198.8	.0000	.2430	.7570	.9647	1355	177.8	.7675	.0545	.8892	.0302
1317	197.8	.0000	.3928	.6072	.7150	1356	175.8	.8920	.0132	.9517	.0076
1318	196.8	.0000	.5850	.4150	.5593	1357	175.8	.8864	.0442	.9459	.0237
1319	196.4	.0000	.6895	.3104	.3805	1358	174.8	.9488	.0118	.9767	.0057
1320	195.1	.0000	.7832	.2168	.2853	1359	174.8	.9488	.0241	.9773	.0119
1321	198.8	.0464	.0120	.9416	.2014	1360	174.8	.9488	.0358	.9741	.0187
1322	194.8	.1446	.0118	.8436	.8752	1361	201.0	.0000	.0073	.0000	.0095
1323	194.8	.1371	.0524	.8106	.6877	1362	200.7	.0000	.0344	.0000	.0196
1324	194.8	.1188	.1409	.7403	.6618	1363	195.8	.0000	.9390	.0000	.0461
1325	194.8	.0854	.3512	.5635	.6077	1364	194.8	.0275	.9265	.0580	.9458
1326	194.8	.0469	.5288	.4094	.4670	1365	193.8	.0523	.9477	.1079	.8921
1327	194.8	.0377	.7657	.1966	.3469	1366	190.8	.2100	.3220	.3751	.2863
1328	190.8	.2539	.0170	.7291	.2504	1367	190.8	.2571	.0136	.4675	.0126
1329	190.8	.2444	.0603	.6953	.1718	1368	190.8	.1535	.8028	.2801	.6968
1330	190.8	.1907	.4286	.3807	.4998	1369	190.8	.1497	.8332	.2757	.7114
1331	190.8	.1711	.6049	.2240	.2709	1370	186.8	.3922	.0123	.2757	.7114
1332	190.8	.1592	.7272	.1136	.1691	1371	186.8	.3922	.0123	.6193	.0101
1333	190.8	.2109	.7528	.0363	.0865	1372	186.8	.3872	.0404	.6134	.0326
1334	190.8	.1435	.8454	.0111	.0332	1373	184.8	.4579	.0795	.6707	.0587
1335	186.8	.3855	.0331	.5814	.0116	1374	179.8	.6835	.0236	.8409	.0147
1336	186.8	.3277	.4581	.2142	.3634	1375	177.8	.7831	.0180	.8964	.0103
1337	186.8	.3115	.5889	.0996	.1355	1376	177.8	.7787	.0539	.8891	.0314
1338	186.8	.2999	.6581	.0419	.0643	1377	175.8	.8935	.0175	.8918	.0314
1339	184.8	.4486	.0794	.4720	.0285	1378	174.8	.9493	.0145	.9773	.0092
1340	184.8	.4397	.1528	.4075	.2778	1379	174.8	.9483	.0284	.9773	.0075
1341	184.8	.4238	.2668	.3094	.2400	1380	174.2	.9821	.0179	.9753	.0146
1342	184.8	.4238	.2668	.3094	.1839	1381	174.1	.9884	.0116	.9908	.0092
						1382				.9942	.0058

TABLE 7  
EXPERIMENTAL DATA AT 8 ATM.

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION	
		N <sub>2</sub>	AR	N <sub>2</sub>	O <sub>2</sub>			N <sub>2</sub>	AR	N <sub>2</sub>	AR
389	206.8	.0512	.9488	.1127	.8873	425	195.8	.3450	.0669	.5881	.3963
390	202.8	.1495	.8505	.2931	.7069	426	195.8	.3412	.0872	.5717	.3879
391	197.8	.2940	.7060	.4939	.5061	427	195.8	.3368	.1212	.5420	.3690
392	193.8	.4290	.5710	.6371	.3629	428	195.8	.3265	.1740	.4995	.3408
393	189.8	.5830	.4170	.7638	.2362	429	191.8	.4940	.0352	.4708	.2848
394	186.8	.7138	.2862	.8507	.1493	430	191.8	.4900	.0590	.4510	.2725
395	184.8	.8085	.1915	.9051	.0949	431	191.8	.4926	.0714	.4360	.2633
396	182.8	.9125	.0875	.9586	.0414	432	191.8	.4878	.0915	.4208	.2542
397	209.0	.0000	.9884	.0000	.0151	433	191.8	.4815	.1308	.3877	.2341
398	208.7	.0000	.9619	.0000	.0493	434	191.8	.4714	.1979	.3307	.2015
399	208.4	.0000	.9327	.0000	.0854	435	187.8	.6665	.0382	.2953	.1590
400	208.1	.0000	.9015	.0000	.1231	436	187.8	.6616	.0552	.2832	.1530
401	181.8	.9620	.0380	.9790	.0210	437	187.8	.6600	.0770	.2630	.1416
402	182.3	.9306	.0694	.9606	.0394	438	187.8	.6551	.0967	.2482	.1347
403	182.8	.8985	.1015	.9425	.0575	439	187.8	.6507	.1344	.2149	.1165
404	183.3	.8647	.1353	.9218	.0782	440	187.8	.6408	.1928	.1664	.0909
405	205.8	.0690	.9316	.1456	.8160	441	185.8	.7532	.0597	.1871	.0959
406	205.8	.0657	.8877	.1385	.8071	442	185.8	.7446	.1011	.1542	.0792
407	205.8	.0625	.8739	.1318	.7938	443	185.8	.7415	.1363	.1222	.0722
408	205.8	.0592	.8644	.1236	.7869	444	185.8	.7317	.1950	.0733	.0628
409	205.8	.0525	.8404	.1105	.7655	445	183.8	.8567	.0327	.1106	.0375
410	205.8	.0444	.8021	.0933	.7308	446	183.8	.8552	.0484	.0964	.0544
411	201.8	.1699	.7972	.3202	.6454	447	183.8	.8513	.0749	.0737	.0475
412	201.8	.1678	.7838	.3166	.6330	448	183.8	.9487	.0992	.0521	.0357
413	201.8	.1636	.7687	.3068	.6242	449	183.8	.8451	.1211	.0338	.0256
414	201.8	.1606	.7560	.3015	.6130	450	183.8	.8425	.1410	.0166	.0157
415	201.8	.1545	.7295	.2898	.5920	451	182.8	.9107	.0323	.0570	.0081
416	201.8	.1461	.6866	.2734	.5555	452	182.8	.9027	.0711	.0263	.0278
417	197.8	.2870	.6795	.4816	.4880	584	205.8	.0700	.0189	.0263	.0126
418	197.8	.2853	.6616	.4779	.4733	585	201.8	.1714	.0192	.9110	.8294
419	197.8	.2829	.6468	.4728	.4651	586	197.8	.2901	.0201	.6898	.6545
420	197.8	.2797	.6345	.4672	.4543	587	195.8	.3550	.0180	.6270	.4961
421	197.8	.2749	.6037	.4572	.4337	588	191.8	.4968	.0181	.4851	.4237
422	197.8	.2650	.5583	.4402	.4020	589	191.8	.4889	.0710	.4401	.2920
423	195.8	.3509	.6148	.5541	.4163	590	187.8	.6647	.0212	.3142	.2656
424	195.8	.3487	.5999	.5504	.4067	591	185.8	.7562	.0203	.2235	.1694
											.1148

TABLE 7  
EXPERIMENTAL DATA AT 8 ATM. (continued)

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		
		N <sub>2</sub>	AR	N <sub>2</sub>	AR			N <sub>2</sub>	AR	N <sub>2</sub>	AR	
592	185.8	.7534	.0354	.2113	.1075	1279	195.8	.3411	.0417	.5485	.0347	.4168
593	183.8	.8564	.0207	.1229	.0604	1280	195.8	.3143	.2450	.4933	.2042	.3025
594	182.8	.9033	.0201	.0766	.0346	1281	195.8	.2997	.3660	.4710	.2978	.2312
595	182.8	.9044	.0457	.0499	.0239	1282	195.8	.2740	.5207	.4346	.4200	.1455
1246	181.8	.9645	.....	.0355	.0166	1283	195.8	.2585	.6835	.4130	.5460	.0410
1247	199.8	.1126	.8874	.....	.....	1284	191.8	.4970	.0086	.6947	.0065	.2988
1248	197.8	.1775	.8225	.....	.....	1285	191.8	.4926	.0517	.6850	.0384	.2766
1249	191.8	.4142	.5858	.....	.....	1286	191.8	.4462	.3391	.6202	.2462	.1336
1250	187.8	.6073	.3927	.....	.....	1287	191.8	.4224	.5123	.5912	.3688	.0400
1251	184.8	.7771	.2229	.....	.....	1288	189.8	.5739	.0373	.7521	.0264	.2215
1252	182.0	.9466	.0534	.....	.....	1289	189.8	.5669	.0828	.7357	.0599	.2044
1253	181.6	.9691	.0309	.....	.....	1290	189.8	.5621	.1163	.7340	.0819	.1841
1254	181.4	.9835	.0165	.....	.....	1291	189.8	.5426	.2457	.7074	.1695	.1230
1255	181.2	.9965	.0035	.....	.....	1292	189.8	.5223	.3915	.6826	.2669	.0505
1256	209.0	.....	.0088	.9912	.9894	1293	187.8	.6227	.3095	.7633	.1989	.0378
1257	208.8	.....	.0260	.9740	.9687	1294	187.8	.6094	.3581	.7529	.2294	.0177
1258	208.4	.....	.0709	.9291	.9123	1295	185.8	.7578	.0059	.8790	.0033	.1177
1259	207.3	.....	.2000	.8000	.7609	1296	185.8	.7597	.0266	.8743	.0160	.1097
1260	205.8	.....	.4186	.5814	.5372	1297	185.8	.7517	.0702	.8669	.0422	.0909
1261	204.8	.....	.6224	.3776	.3476	1298	185.8	.7256	.2362	.8368	.1435	.0197
1262	204.0	.....	.8511	.1489	.....	1299	182.8	.9085	.0139	.9588	.0062	.0350
1263	205.8	.0707	.0113	.9180	.8357	1300	182.8	.9042	.0596	.9497	.0335	.0168
1264	205.8	.0257	.2503	.7240	.6640	1301	181.8	.9644	.0080	.9835	.0040	.0125
1265	201.8	.1728	.0128	.8145	.6594	1302	181.8	.9609	.0170	.9810	.0090	.0100
1266	201.8	.1044	.4105	.4851	.4023	1303	181.8	.9582	.3317	.9785	.0172	.0043
1267	201.8	.0613	.5967	.3220	.2713	1827	209.0	.....	.0110	.....	.0148	.9852
1268	201.8	.0679	.7204	.2118	.1790	1928	208.8	.....	.0302	.....	.0398	.9602
1269	201.8	.0587	.8326	.1087	.0962	1829	197.8	.2801	.0685	.4706	.0621	.4673
1270	201.8	.0546	.8906	.0548	.0475	1830	195.8	.3500	.0454	.5525	.0383	.4092
1271	199.8	.1785	.3013	.5202	.4020	1831	203.8	.....	.9248	.....	.9294	.0706
1272	199.8	.1560	.4659	.3780	.2972	1832	185.8	.7611	.0118	.....	.0072	.1146
1273	199.8	.1362	.6018	.2619	.2093	1833	183.8	.8432	.1271	.8782	.0072	.1146
1274	199.8	.1215	.7635	.1151	.0940	1834	182.8	.9144	.0155	.9121	.0738	.0141
1275	197.8	.2154	.4646	.3200	.2378	1835	181.8	.9653	.0124	.9591	.0087	.0322
1276	197.8	.1972	.6106	.1923	.1466	1836	181.8	.9582	.0418	.9841	.0064	.0095
1277	197.8	.1641	.7776	.0382	.0295	1837	181.2	.9957	.0043	.9977	.0231	.....



TABLE 8  
EXPERIMENTAL DATA AT 10 ATM.

RUN NO.	TEMP. DEG. R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		RUN NO.	TEMP. DEG. R	LIQUID MOL FRACTION		VAPOR MOL FRACTION	
		N <sub>2</sub>	AR	N <sub>2</sub>	AR			N <sub>2</sub>	AR	N <sub>2</sub>	AR
325	212.8	.0706	.....	.9294	.1439	365	197.8	.5153	.0624	.4224	.6903
326	209.8	.1463	.....	.8537	.2719	366	197.8	.5171	.0566	.4263	.6927
327	205.8	.2587	.....	.7413	.4329	367	197.8	.5155	.0722	.4124	.6888
328	201.8	.3844	.....	.6156	.5767	368	197.8	.5117	.0890	.3993	.6850
329	197.8	.5284	.....	.4716	.7067	369	197.8	.5055	.1278	.3668	.6753
330	193.8	.6881	.....	.3119	.8249	370	197.8	.4974	.1829	.3198	.6644
331	190.8	.8243	.....	.1757	.9077	371	193.8	.6860	.0358	.2783	.8183
332	188.8	.9203	.....	.0797	.9606	372	193.8	.6813	.0565	.2622	.8137
333	215.8	.....	.0076	.9924	.....	373	193.8	.6607	.0741	.2453	.8121
334	215.5	.....	.0352	.9646	.....	374	193.8	.6752	.0950	.2298	.8076
335	215.2	.....	.0681	.9319	.....	375	193.8	.6680	.1326	.1994	.7968
336	214.9	.....	.1024	.8976	.....	376	193.8	.6624	.1813	.1563	.7901
337	187.7	.9666	.0334	.....	.9810	377	191.8	.7714	.0556	.1730	.8707
338	188.2	.9384	.0614	.....	.9640	378	191.8	.7636	.0948	.1417	.8625
339	188.8	.9090	.0910	.....	.9460	379	191.8	.7556	.1378	.1066	.8543
340	189.3	.8801	.1199	.....	.9282	380	191.8	.7474	.1895	.0631	.8461
341	212.8	.0652	.0278	.9070	.1306	381	189.8	.8714	.0228	.1057	.9314
342	212.8	.0611	.0453	.8936	.1218	382	189.8	.8689	.0300	.1011	.9289
343	212.8	.0567	.0594	.8836	.1154	383	189.8	.8663	.0502	.0835	.9257
344	212.8	.0536	.0779	.8686	.1079	384	189.8	.8628	.0717	.0654	.9220
345	212.8	.0470	.1085	.8446	.0947	385	189.8	.8578	.0996	.0426	.9168
346	212.8	.0395	.1524	.8081	.0791	386	188.8	.8518	.1285	.0197	.9109
347	208.8	.1662	.0330	.8009	.3027	387	188.8	.9208	.0285	.0508	.9553
348	208.8	.1621	.0496	.7883	.2971	388	188.8	.9126	.0616	.0258	.9507
349	208.8	.1592	.0653	.7755	.2992	571	188.8	.9184	.0283	.0534	.9574
350	208.8	.1566	.0814	.7620	.2847	572	188.8	.9203	.0097	.0700	.9600
351	208.8	.1524	.1131	.7346	.2741	573	191.8	.7752	.0174	.2074	.8715
352	208.8	.1430	.1481	.7090	.2580	574	191.8	.7683	.0396	.1921	.8726
353	204.8	.2805	.0320	.6876	.4575	575	193.8	.6833	.0188	.2979	.8203
354	204.8	.2797	.0493	.6711	.4575	576	197.8	.5209	.0117	.4674	.7018
355	204.8	.2768	.0635	.6597	.4496	577	197.8	.5195	.0317	.4488	.6955
356	204.8	.2714	.0816	.6471	.4419	578	200.8	.4110	.0170	.5720	.6008
357	204.8	.2698	.1141	.6161	.4355	579	204.8	.2810	.0176	.7014	.4571
358	204.8	.2595	.1655	.5760	.4173	580	204.8	.2705	.0483	.6812	.4458
359	200.8	.4122	.0375	.5503	.6006	581	208.8	.1676	.0171	.8154	.3039
360	200.8	.4086	.0535	.5379	.5960	582	208.8	.1569	.0667	.7764	.2841
361	200.8	.4056	.0703	.5241	.5864	583	190.8	.7971	.1572	.0457	.8774
362	200.8	.4002	.0881	.5117	.5328	1189	187.6	.9887	.....	.0113	.9944
363	200.8	.3935	.1234	.4831	.5741	1190	205.8	.1452	.8548	.....	.2469
364	200.8	.3857	.1770	.4373	.5611	1191	202.8	.2515	.7485	.....	.3883

TABLE 8  
EXPERIMENTAL DATA AT 10 ATM. (continued)

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		
		N2	AR	N2	AR			N2	AR	N2	AR	
1192	197.8	.4502	.5498	.5035	.3965	1233	195.8	.5945	.0607	.7537	.0434	
1193	193.8	.6400	.3600	.7632	.2368	1234	195.8	.5862	.1151	.7403	.0816	
1194	190.8	.8015	.1985	.8780	.1220	1235	195.8	.5754	.1983	.7288	.1377	
1195	188.2	.9529	.0471	.9728	.0272	1236	195.8	.5438	.3528	.6963	.2416	
1196	188.0	.9657	.0343	.9800	.0200	1237	193.8	.6847	.0094	.8209	.0075	
1197	187.5	.9948	.0052	.9983	.0017	1238	193.8	.6349	.3232	.7592	.2172	
1198	215.6	.0000	.0488	.0000	.0654	1239	191.8	.7736	.0123	.8738	.0078	
1199	215.4	.0000	.0683	.0000	.0855	1240	191.8	.7717	.0223	.8774	.0130	
1200	213.8	.0000	.0723	.0000	.0894	1241	191.8	.7705	.0372	.8737	.0228	
1201	213.8	.0000	.2500	.0000	.0894	1242	188.8	.9273	.0074	.9621	.0044	
1202	212.3	.0000	.4866	.0000	.2866	1243	188.8	.9286	.0202	.9626	.0116	
1203	211.3	.0000	.7066	.0000	.7254	1244	188.8	.9272	.0399	.9611	.0228	
1204	210.6	.0000	.9671	.0000	.9681	1245	188.8	.9242	.0463	.9589	.0264	
1205	212.8	.0297	.0130	.1394	.0133	1800	215.7	.0000	.0153	.0000	.0195	
1206	212.8	.0623	.0232	.1305	.0288	1801	215.6	.0000	.0279	.0000	.0350	
1207	212.8	.0179	.2537	.0363	.2861	1802	211.0	.0000	.7560	.0000	.7721	
1208	208.8	.1617	.0251	.3009	.6777	1803	210.6	.0000	.9094	.0000	.9143	
1209	208.8	.1574	.0409	.2884	.6723	1804	212.8	.0676	.0144	.1357	.0167	
1210	208.8	.1281	.1969	.2357	.6685	1805	212.8	.0643	.0286	.1292	.0327	
1211	208.8	.1058	.3809	.1885	.5663	1806	208.8	.1683	.0115	.3073	.0118	
1212	208.8	.0793	.5783	.1416	.4339	1807	208.8	.1659	.0253	.3013	.0255	
1213	208.8	.0625	.7524	.1128	.2949	1808	204.8	.2634	.1119	.4303	.1023	
1214	208.8	.0508	.9123	.0935	.1638	1809	212.8	.0672	.0100	.1355	.0113	
1215	204.8	.2811	.0274	.4585	.5161	1810	204.8	.1893	.6308	.3082	.5510	
1216	204.8	.2745	.0671	.4475	.4910	1811	200.8	.3992	.0743	.5841	.0619	
1217	204.8	.2430	.2485	.3938	.2236	1812	200.8	.3964	.0999	.5782	.0824	
1218	204.8	.2100	.4539	.3420	.4003	1813	197.8	.5210	.0104	.7001	.0078	
1219	204.8	.1939	.6274	.3089	.5503	1814	195.8	.5936	.0229	.7588	.0166	
1220	204.8	.1813	.7375	.2979	.6362	1815	195.8	.5691	.1958	.7189	.1384	
1221	202.8	.2963	.3051	.4520	.2627	1816	193.8	.6843	.0137	.8199	.0094	
1222	202.8	.2644	.5489	.4063	.4562	1817	193.8	.6382	.3279	.7645	.2166	
1223	202.8	.2468	.7069	.3825	.5829	1818	191.8	.7775	.0138	.8794	.0091	
1224	200.8	.4077	.0109	.5980	.0089	1819	191.8	.7757	.0264	.8770	.0167	
1225	200.8	.4020	.0353	.5899	.0290	1820	191.8	.7776	.0160	.8807	.0101	
1226	200.8	.3433	.4331	.5013	.3432	1821	191.8	.7735	.0374	.8758	.0238	
1227	200.8	.3267	.5761	.4790	.6693	1822	191.8	.7500	.1960	.8481	.1004	
1228	197.8	.5163	.0263	.6931	.0198	1823	190.8	.8212	.0000	.9078	.0000	
1229	197.8	.5092	.0500	.6860	.0375	1824	187.8	.9826	.0000	.9923	.0000	
1230	197.8	.4729	.3089	.6337	.2275	1825	187.5	.9839	.0161	.9917	.0083	
1231	197.8	.4624	.3994	.6188	.2918	1826	188.8	.9213	.0165	.9591	.0090	
					.0893				.0622		.0319	

TABLE 9  
EXPERIMENTAL DATA AT 12 ATM.

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION N2	LIQUID MOL FRACTION AR	LIQUID MOL FRACTION O2	VAPOR MOL FRACTION N2	VAPOR MOL FRACTION AR	VAPOR MOL FRACTION O2	RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION N2	LIQUID MOL FRACTION AR	LIQUID MOL FRACTION O2	VAPOR MOL FRACTION N2	VAPOR MOL FRACTION AR	VAPOR MOL FRACTION O2
258	216.7	.1193	.....	.8817	.2185	.....	.7815	295	206.8	.4015	.0376	.5610	.5758	.0319	.3923
259	212.8	.2247	.....	.7753	.3643	.....	.6357	296	206.8	.3987	.0571	.5442	.5739	.0479	.3783
260	208.8	.3421	.....	.6579	.5214	.....	.4786	297	206.8	.3965	.0748	.5287	.5670	.0637	.3693
261	204.8	.4602	.....	.5198	.6496	.....	.3504	298	206.8	.3926	.0923	.5151	.5615	.0776	.3609
262	200.8	.6261	.....	.3739	.7712	.....	.2288	299	206.8	.3843	.1320	.4837	.5514	.1104	.3382
263	197.8	.7524	.....	.2476	.8592	.....	.1408	300	206.8	.3749	.1886	.4365	.5374	.1558	.3068
264	195.8	.8412	.....	.1556	.9107	.....	.0893	301	202.8	.5453	.0390	.4156	.7048	.0300	.2652
265	194.8	.8848	.....	.1152	.9385	.....	.0615	302	202.8	.5406	.0583	.4011	.7017	.0447	.2536
266	221.4	.....	.0158	.9842	.....	.0197	.9803	303	202.8	.5377	.0803	.3821	.6962	.0610	.2428
267	221.1	.....	.0444	.9556	.....	.0547	.9453	304	202.8	.5363	.0987	.3650	.6894	.0756	.2350
268	220.8	.....	.0787	.9213	.....	.0963	.9037	305	202.8	.5307	.1392	.3302	.6840	.1044	.2116
269	220.5	.....	.1102	.8898	.....	.1322	.8677	306	202.8	.5204	.2120	.2677	.6701	.1584	.1715
270	194.8	.8688	.1312	.....	.9180	.0820	.....	307	199.8	.6663	.0379	.2958	.7960	.0270	.1770
271	195.3	.8418	.1582	.....	.8998	.1002	.....	308	199.8	.6620	.0603	.2777	.7915	.0426	.1659
272	195.8	.8135	.1865	.....	.8808	.1192	.....	309	199.8	.6583	.0852	.2565	.7860	.0603	.1537
273	196.3	.7658	.2142	.....	.8620	.1380	.....	310	199.8	.6560	.1063	.2377	.7825	.0755	.1419
274	218.7	.0591	.0313	.9097	.1153	.0371	.8476	311	199.8	.6476	.1456	.2068	.7748	.1013	.1240
275	218.7	.0540	.0499	.8961	.1057	.0573	.8359	312	199.8	.6382	.2193	.1425	.7603	.1534	.0863
276	218.7	.0493	.0675	.8833	.0974	.0772	.8255	313	198.8	.7024	.0614	.2362	.8193	.0423	.1385
277	218.7	.0436	.0927	.8637	.0858	.1061	.8080	314	198.8	.6954	.1093	.1953	.8098	.0749	.1154
278	193.3	.9528	.0472	.....	.9711	.0289	.....	315	198.8	.6885	.1510	.1604	.8020	.1031	.0950
279	193.8	.9228	.0772	.....	.9524	.0476	.....	316	198.8	.6789	.2164	.1048	.7904	.1476	.0621
280	218.7	.0411	.1223	.8365	.0783	.1393	.7825	317	196.8	.7936	.0377	.1687	.8804	.0245	.0951
281	218.7	.0307	.1684	.8009	.0584	.1913	.7504	318	196.8	.7899	.0575	.1526	.8767	.0376	.0856
282	194.3	.8981	.1019	.....	.9370	.0630	.....	319	196.8	.7867	.0749	.1384	.8732	.0494	.0774
283	214.8	.1682	.0366	.8032	.2823	.0379	.6798	320	196.8	.7828	.0974	.1198	.8683	.0642	.0675
284	214.8	.1544	.0531	.7905	.2752	.0548	.6700	321	196.8	.7764	.1333	.0903	.8622	.0871	.0507
285	214.8	.1524	.0698	.7779	.2697	.0718	.6585	322	196.8	.7656	.1836	.0508	.8533	.1183	.0284
286	214.8	.1474	.0879	.7648	.2614	.0911	.6476	323	195.8	.8333	.0564	.1103	.9015	.0371	.0614
287	214.8	.1482	.1303	.7295	.2480	.1331	.6189	324	195.8	.8270	.0934	.0797	.6959	.0597	.0444
288	214.8	.1287	.1835	.6878	.2266	.1868	.5867	565	199.8	.6629	.0226	.3145	.7992	.0172	.1836
289	210.8	.2700	.0337	.6962	.4338	.0315	.5348	566	198.8	.7069	.0190	.2741	.8266	.0126	.1609
290	210.8	.2670	.0545	.6785	.4260	.0512	.5228	567	198.8	.7021	.0435	.2544	.8231	.0300	.1470
291	210.8	.2627	.0490	.6683	.4197	.0651	.5152	568	196.8	.7930	.0203	.1667	.8837	.0123	.1040
292	210.8	.2592	.0842	.6567	.4155	.0788	.5057	569	195.8	.8402	.0159	.1439	.9116	.0105	.0779
293	210.8	.2514	.1205	.6282	.4030	.1140	.4830	570	195.8	.8391	.0363	.1245	.9068	.0244	.0689
294	210.8	.2471	.1810	.5720	.3906	.1672	.4422	1135	193.3	.9661	.....	.0339	.9799	.....	.0201

TABLE 9  
EXPERIMENTAL DATA AT 12 ATM. (continued)

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION	
		N <sub>2</sub>	AR	N <sub>2</sub>	AR			N <sub>2</sub>	AR	N <sub>2</sub>	AR
1136	212.8	.1072	.8928	.1768	.8232	1174	199.8	.6227	.3200	.7438	.2269
1137	210.8	.1699	.8301	.2717	.7283	1175	198.8	.6730	.2711	.7845	.1925
1138	204.8	.3896	.6104	.5327	.4673	1176	196.8	.8044	.0061	.8876	.0052
1139	199.8	.6152	.3848	.7357	.2643	1177	196.8	.7998	.0188	.8863	.0121
1140	193.0	.9778	.0222	.9867	.0133	1178	196.8	.7973	.0340	.8832	.0224
1141	221.5	.....	.0198	.....	.0273	1179	195.8	.8308	.1209	.8961	.0774
1142	221.2	.....	.0554	.....	.0677	1180	194.3	.9237	.0075	.9592	.0047
1143	221.0	.....	.0726	.....	.0879	1181	194.3	.9223	.0184	.9575	.0116
1144	219.8	.....	.2094	.....	.2405	1182	194.3	.9233	.0224	.9575	.0153
1145	218.7	.....	.3670	.....	.4032	1183	194.3	.9182	.0370	.9538	.0227
1146	217.7	.....	.5377	.....	.5677	1184	194.3	.9158	.0484	.9512	.0293
1147	216.8	.....	.5439	.....	.5727	1185	194.3	.9138	.0667	.9474	.0424
1148	216.4	.....	.9159	.....	.9190	1186	193.3	.9684	.0069	.9835	.0045
1149	218.7	.0665	.0207	.1262	.0236	1187	193.3	.9676	.0143	.9830	.0042
1150	218.7	.0622	.0431	.1173	.0497	1188	193.3	.9662	.0233	.9798	.0139
1151	214.8	.1639	.0277	.3039	.0277	1777	221.5	.....	.0120	.....	.0131
1152	214.8	.1954	.0299	.2898	.0303	1778	221.2	.....	.0397	.....	.0488
1153	214.8	.1643	.0453	.2869	.0463	1779	221.0	.....	.0567	.....	.0694
1154	214.9	.1026	.3876	.1785	.3839	1780	216.8	.....	.7226	.....	.7403
1155	214.8	.0787	.5847	.1359	.5695	1781	216.6	.....	.7871	.....	.7999
1156	214.8	.0662	.7090	.1151	.6831	1782	216.4	.....	.8576	.....	.8639
1157	214.8	.0591	.7811	.1004	.7566	1783	218.7	.0642	.0106	.1236	.0124
1158	214.8	.0511	.8776	.0899	.8448	1784	214.8	.1618	.0253	.2838	.0266
1159	210.8	.2265	.3393	.3554	.3098	1785	214.8	.1603	.0324	.2810	.0340
1160	210.8	.2143	.4317	.3343	.3865	1786	214.8	.1643	.0120	.2881	.0127
1161	210.8	.1940	.5738	.3060	.5081	1787	212.8	.2209	.....	.3698	.....
1162	210.8	.1817	.7027	.2865	.6189	1788	206.8	.4024	.0148	.5787	.0123
1163	210.8	.1740	.7958	.2772	.6975	1789	199.8	.6618	.0243	.7957	.0169
1164	206.8	.4075	.0117	.5854	.0106	1790	199.8	.6602	.0347	.7929	.0242
1165	206.8	.4035	.0375	.5755	.0317	1791	198.8	.7052	.0229	.8259	.0158
1166	206.8	.3570	.3151	.5096	.2589	1792	196.8	.7948	.0138	.8834	.0089
1167	206.8	.3414	.4626	.4836	.3747	1793	195.8	.8356	.0433	.9052	.0274
1168	206.8	.3203	.6032	.4598	.4848	1794	194.3	.9068	.0289	.9482	.0182
1169	202.8	.4970	.3674	.6387	.2724	1795	194.3	.9102	.....	.9522	.....
1170	202.8	.4835	.4568	.6250	.3366	1796	193.3	.9582	.....	.9774	.....
1171	199.8	.6670	.0111	.8015	.0077	1797	193.3	.9564	.0082	.9770	.0048
1172	199.8	.6635	.0238	.7982	.0160	1798	193.3	.9555	.0249	.9743	.0152
1173	199.8	.6642	.0298	.8016	.0183	1799	193.0	.9679	.0321	.9807	.0193

TABLE 10  
EXPERIMENTAL DATA AT 14 ATM.

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		
		N <sub>2</sub>	AR	N <sub>2</sub>	AR			N <sub>2</sub>	AR	N <sub>2</sub>	AR	N <sub>2</sub>
194	223.7	.0603	.0307	.1308	.0692	235	204.8	.6525	.0682	.7761	.0507	.1732
195	219.7	.1716	.0254	.2923	.7077	236	204.8	.6475	.0943	.7713	.0593	.1594
196	216.7	.2586	.7414	.4055	.5945	237	204.8	.6426	.1179	.7658	.0951	.1494
197	211.8	.4055	.5945	.5725	.4275	238	204.8	.6425	.1406	.7627	.1023	.1350
198	207.8	.5506	.4404	.7035	.2965	239	204.8	.6299	.2082	.7520	.1479	.1001
199	203.8	.7025	.2975	.8198	.1802	240	202.8	.7392	.0403	.8419	.0282	.1299
200	200.8	.8272	.1726	.9017	.0993	241	202.8	.7351	.0671	.8303	.0470	.1227
201	198.8	.9149	.0851	.9537	.0463	242	202.8	.7270	.0857	.8275	.0595	.1130
202	226.5	.0215	.9785	.0263	.9737	243	202.8	.7254	.1035	.8249	.0723	.1028
203	226.2	.0452	.9546	.0523	.9447	244	202.8	.7159	.1462	.8168	.1021	.0811
204	225.9	.0620	.9150	.0983	.9017	245	202.8	.7075	.1964	.8081	.1344	.0575
205	225.6	.0902	.8096	.1268	.8732	246	201.8	.7721	.0651	.8594	.0452	.0954
206	197.8	.0412	.0682	.9740	.0260	247	201.8	.7655	.1066	.8544	.0722	.0734
207	198.3	.9318	.0682	.9565	.0435	248	201.8	.7601	.1554	.8463	.1044	.0493
208	198.8	.8998	.0682	.9355	.0645	249	201.8	.7486	.2039	.8374	.1351	.0275
209	199.3	.6757	.1243	.9204	.0796	250	199.8	.8650	.0439	.9204	.0285	.0510
210	224.7	.0422	.9410	.0821	.8981	251	199.8	.8602	.0713	.9145	.0475	.0380
211	224.7	.0391	.9341	.0766	.8915	252	199.8	.8564	.0962	.9088	.0623	.0288
212	224.7	.0357	.9384	.0697	.8851	253	199.8	.9533	.1146	.9069	.0750	.0181
213	224.7	.0329	.9514	.0641	.8756	254	199.8	.8510	.1292	.9057	.0533	.0111
214	224.7	.0273	.9769	.0533	.8570	255	199.8	.8693	.0251	.9251	.0164	.0586
215	224.7	.0173	.1209	.0353	.1342	256	198.8	.9114	.0510	.9442	.0332	.0226
216	219.7	.1672	.0197	.2854	.0197	257	198.8	.9042	.0772	.9410	.0485	.0105
217	219.7	.1644	.0306	.2826	.0321	556	225.5	.0000	.1190	.0000	.1407	.8593
218	219.7	.1613	.0473	.2735	.0493	559	203.8	.7041	.0000	.8108	.0000	.1812
219	219.7	.1599	.0607	.2706	.0633	560	202.8	.7365	.0639	.8345	.0458	.1197
220	219.7	.1509	.0976	.2562	.1006	561	201.8	.7773	.0623	.8631	.0418	.0951
221	214.8	.1420	.1531	.2400	.1580	562	199.8	.8712	.0405	.9234	.0269	.0497
222	214.8	.3098	.0239	.4611	.0219	628	200.8	.8098	.0000	.8897	.0000	.1103
223	214.8	.3194	.0369	.4511	.0346	1064	197.8	.9693	.0000	.9835	.0000	.0165
224	214.8	.3080	.0490	.4595	.0396	1065	217.7	.1041	.8959	.1713	.8287	.0000
225	214.8	.3031	.0671	.4499	.0624	1066	214.8	.2014	.7986	.3079	.6921	.0000
226	214.8	.2906	.1150	.4355	.1037	1067	209.8	.3866	.6134	.5224	.4776	.0000
227	214.8	.2779	.1691	.4172	.1546	1068	204.8	.6032	.3968	.7230	.2770	.0000
228	209.8	.4715	.0242	.6339	.0200	1069	201.8	.7552	.2448	.8367	.1533	.0000
229	209.8	.4641	.0440	.6263	.0364	1070	198.0	.9577	.0423	.9749	.0251	.0000
230	209.8	.4626	.0512	.6201	.0670	1071	197.7	.9752	.0248	.9846	.0154	.0000
231	209.8	.4579	.1067	.6114	.0674	1072	197.5	.9842	.0158	.9909	.0091	.0000
232	209.8	.4482	.1505	.6000	.1218	1073	197.4	.9890	.0110	.9939	.0061	.0000
233	209.6	.4362	.2252	.5954	.1804	1074	226.6	.0000	.0138	.9939	.0061	.9818
234	204.8	.6558	.0430	.7805	.0316	1075	226.4	.0000	.0382	.0000	.0480	.9520

TABLE 10  
EXPERIMENTAL DATA AT 14 ATM. (continued)

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION	
		N2	AR	N2	AR			N2	AR	N2	AR
1076	226.3	.....	.0499	.9501	.....	1117	207.8	.4931	.3793	.6267	.2969
1077	225.5	.....	.1330	.8670	.....	1118	207.8	.4829	.4651	.6148	.3496
1078	224.7	.....	.2356	.7644	.....	1119	204.8	.6684	.0111	.7917	.0081
1079	223.2	.....	.4624	.5376	.....	1120	204.8	.6659	.0233	.7915	.0159
1080	222.2	.....	.6800	.3200	.....	1121	204.8	.6633	.0393	.7860	.0290
1081	221.6	.....	.8804	.1196	.....	1122	204.8	.6208	.3073	.7355	.2187
1082	221.4	.....	.9653	.0347	.....	1123	201.8	.7926	.0119	.8749	.0079
1083	224.7	.....	.0449	.9551	.....	1124	201.8	.7934	.0227	.8774	.0151
1084	219.7	.1703	.0209	.9791	.0258	1125	201.8	.7896	.0380	.8731	.0255
1085	219.7	.1594	.0730	.9270	.2684	1126	201.8	.7875	.0525	.8711	.0352
1086	219.7	.1529	.0997	.9003	.2578	1127	201.8	.7866	.0619	.8706	.0417
1087	219.7	.1295	.2491	.7509	.2171	1128	198.8	.9592	.0076	.9609	.0041
1088	219.7	.0967	.4596	.5433	.1599	1129	198.8	.9260	.0207	.9588	.0124
1089	219.7	.0746	.6313	.3687	.1253	1130	198.8	.9232	.0262	.9591	.0156
1090	219.7	.0608	.7751	.2249	.1036	1131	198.8	.9266	.0389	.9538	.0248
1091	219.7	.0559	.8547	.1453	.0946	1132	197.8	.9766	.0062	.9860	.0032
1092	217.7	.2291	.0198	.7802	.3568	1133	197.8	.9725	.0139	.9840	.0082
1093	217.7	.2127	.0979	.6894	.3393	1134	197.8	.9664	.0255	.9793	.0161
1094	217.7	.1870	.2463	.5667	.2961	1755	226.2	.....	.0504	.....	.0409
1095	217.7	.1563	.4359	.4078	.2489	1756	221.4	.....	.9318	.....	.9322
1096	217.7	.1283	.6746	.1971	.2054	1757	224.7	.0189	.1225	.0349	.1412
1097	217.7	.1093	.8810	.0097	.1783	1758	219.7	.1664	.0085	.2818	.0090
1098	214.8	.3146	.0175	.6679	.4743	1759	219.7	.1440	.0181	.2791	.0194
1099	214.8	.3063	.0530	.6407	.4616	1760	211.8	.2580	.0492	.4512	.0442
1100	214.8	.3011	.0898	.6091	.4507	1761	211.8	.3986	.0477	.5545	.0408
1101	214.8	.2699	.2737	.4564	.4014	1762	204.8	.6563	.0237	.7830	.0173
1102	214.8	.2469	.4283	.3248	.3567	1763	201.8	.7464	.2536	.8291	.1709
1103	214.8	.2187	.6567	.1246	.3301	1764	199.8	.8590	.1034	.9115	.0669
1104	214.8	.2135	.7334	.0531	.3217	1765	198.8	.9192	.0089	.9535	.0057
1105	211.8	.4064	.0473	.5463	.5681	1766	198.8	.9171	.0231	.9516	.0149
1106	211.8	.3939	.1114	.4948	.5473	1767	198.8	.9162	.0303	.9501	.0193
1107	211.8	.3854	.1701	.4445	.5351	1768	198.8	.9156	.0445	.9494	.0285
1108	211.8	.3462	.4446	.2092	.4779	1769	198.8	.9117	.0549	.9469	.0346
1109	211.8	.3242	.5921	.0836	.4557	1770	197.8	.9673	.0077	.9814	.0047
1110	209.8	.4608	.0130	.5062	.6410	1771	197.8	.9659	.0158	.9804	.0097
1111	209.8	.4750	.0313	.4938	.6353	1772	197.8	.9650	.0248	.9791	.0154
1112	209.8	.4696	.0614	.4700	.6265	1773	198.0	.9507	.0493	.9684	.0316
1113	209.8	.4297	.3123	.2580	.5723	1774	198.7	.9662	.0338	.9786	.0214
1114	209.8	.4002	.5358	.0640	.5274	1775	197.5	.9791	.0209	.9870	.0130
1115	207.8	.5382	.0951	.3568	.6831	1776	197.4	.9851	.0149	.9912	.0088
1116	207.8	.5180	.2138	.2683	.6582	1868	197.7	.9632	.0368	.9766	.0232

TABLE 11  
EXPERIMENTAL DATA AT 16 ATM.

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION				
		N2	AR	N2	AR			N2	AR	N2	AR			
130	227.7	.0670	.....	.9130	.....	.8535	171	209.8	.6352	.0328	.3320	.7615	.0246	.2138
131	224.7	.1589	.....	.8412	.....	.7431	172	209.8	.6290	.0500	.3209	.7574	.0379	.2047
132	220.7	.2741	.....	.7259	.....	.5909	173	209.8	.6275	.0777	.2948	.7489	.0586	.1925
133	216.7	.3981	.....	.6019	.....	.4644	174	209.8	.6233	.1166	.2601	.7434	.0876	.1690
134	211.8	.5444	.....	.4556	.....	.2958	175	209.8	.6075	.1773	.2152	.7287	.1328	.1385
135	207.8	.7174	.....	.2826	.....	.1755	176	206.8	.7593	.0206	.2201	.8455	.0146	.1399
136	204.8	.8501	.....	.1499	.....	.0946	177	206.8	.7542	.0345	.2113	.8412	.0248	.1340
137	202.8	.9292	.....	.0708	.....	.0392	178	206.8	.7515	.0565	.1920	.8368	.0399	.1233
138	231.2	.....	.0125	.9875	.....	.9841	179	206.8	.7487	.0750	.1763	.8339	.0545	.1117
139	230.9	.....	.0412	.9588	.....	.9500	180	206.8	.7435	.1114	.1452	.8291	.0781	.0928
140	230.6	.....	.0744	.9256	.....	.9064	181	206.8	.7277	.1631	.1092	.8179	.1145	.0675
141	230.3	.....	.1043	.8957	.....	.8793	182	205.8	.7915	.0433	.1652	.8705	.0291	.1004
142	201.8	.9725	.0272	.....	.....	.....	183	205.8	.7845	.0653	.1503	.8665	.0430	.0905
143	202.3	.9424	.0576	.....	.....	.....	184	205.8	.7823	.0952	.1225	.8575	.0688	.0737
144	202.8	.9153	.0847	.....	.....	.....	185	205.8	.7680	.1576	.0743	.8469	.1080	.0451
145	203.3	.8658	.1142	.....	.....	.....	186	203.8	.8830	.0232	.0938	.9309	.0153	.0539
146	229.7	.8308	.0123	.9570	.....	.9254	187	203.8	.8764	.0395	.0840	.9263	.0250	.0487
147	229.7	.0315	.0238	.9448	.....	.9154	188	203.8	.8731	.0581	.0688	.9208	.0406	.0385
148	229.7	.0262	.0343	.9395	.....	.9113	189	203.8	.8735	.0616	.0649	.9161	.0440	.0398
149	229.7	.0271	.0407	.9322	.....	.9043	190	203.8	.8648	.1166	.0186	.9143	.0750	.0107
150	229.7	.0232	.0678	.9090	.....	.8711	191	203.8	.8643	.1232	.0125	.9125	.0903	.0072
151	229.7	.0124	.1249	.8626	.....	.8337	192	202.8	.9208	.0400	.0393	.9525	.0250	.0225
152	224.7	.1604	.0156	.8240	.....	.7162	193	202.8	.9183	.0637	.0180	.9460	.0437	.0103
153	224.7	.1576	.0289	.8135	.....	.7079	547	220.7	.2728	.....	.7272	.4132	.....	.5868
154	224.7	.1560	.0367	.8073	.....	.7036	548	216.7	.3943	.....	.6057	.5491	.....	.4509
155	224.7	.1525	.0467	.8008	.....	.6971	549	212.8	.5040	.....	.4960	.6542	.....	.3458
156	224.7	.1452	.0790	.7758	.....	.6740	550	204.8	.8448	.....	.1552	.9070	.....	.0930
157	224.7	.1337	.1375	.7286	.....	.6307	551	202.8	.9322	.....	.0678	.9604	.....	.0396
158	219.7	.3048	.0178	.6774	.....	.5411	552	225.7	.1413	.0100	.8487	.2250	.0158	.7593
159	219.7	.3914	.0304	.6693	.....	.5328	553	224.7	.1587	.0121	.8292	.2653	.0115	.7232
160	219.7	.2974	.0478	.6549	.....	.5222	554	219.7	.3030	.0142	.6827	.4469	.0134	.5397
161	219.7	.2941	.0557	.6502	.....	.5191	555	209.8	.6306	.0622	.3072	.7612	.0488	.1900
162	219.7	.2651	.1130	.6019	.....	.4821	556	206.8	.7391	.1599	.1010	.8236	.1134	.0630
163	219.7	.2747	.1553	.5681	.....	.4569	1000	201.8	.9808	.....	.0192	.9897	.....	.0103
164	214.8	.4557	.0215	.5226	.....	.3737	1001	221.7	.1232	.8768	.....	.1940	.8060	.....
165	214.8	.4576	.0316	.5147	.....	.3683	1002	218.7	.2239	.7761	.....	.3309	.6691	.....
166	214.8	.4524	.0458	.5016	.....	.3580	1003	214.8	.5809	.6293	.....	.4960	.5040	.....
167	214.8	.4507	.0607	.4886	.....	.3481	1004	209.8	.5809	.4191	.....	.6905	.3095	.....
168	214.8	.4419	.1003	.4576	.....	.3286	1005	204.8	.8179	.1821	.....	.8765	.1235	.....
169	214.8	.4278	.1684	.4039	.....	.2884	1006	201.5	.9368	.0632	.....	.9592	.0408	.....
170	209.8	.6389	.0194	.3417	.....	.2210	1007	202.0	.9650	.0350	.....	.9774	.0226	.....

TABLE 11  
EXPERIMENTAL DATA AT 16 ATM. (continued)

RUN NO.	TEMP. DEG. F.	LIQUID MOL FRACTION N <sub>2</sub>	LIQUID MOL FRACTION O <sub>2</sub>	VAPOR MOL FRACTION N <sub>2</sub>	VAPOR MOL FRACTION O <sub>2</sub>	RUN NO.	TEMP. DEG. F.	LIQUID MOL FRACTION N <sub>2</sub>	LIQUID MOL FRACTION O <sub>2</sub>	VAPOR MOL FRACTION N <sub>2</sub>	VAPOR MOL FRACTION O <sub>2</sub>
1004	201.6	.9852	.0148	.9910	.0090	1049	211.8	.5058	.4295	.6296	.3262
1004	226.0	.9302	.0698	.9323	.0677	1050	209.8	.6467	.0124	.7697	.0093
1010	226.3	.805A	.1942	.8147	.1853	1051	209.8	.6392	.0502	.7615	.0375
1011	226.7	.6902	.3098	.7078	.2922	1052	209.8	.6166	.1911	.7328	.1423
1012	227.2	.4736	.5264	.4974	.4974	1053	209.8	.6016	.2864	.7158	.2112
1013	229.2	.2391	.7609	.2686	.7314	1054	206.8	.7649	.0096	.8550	.0061
1014	230.8	.0573	.9427	.0690	.9310	1055	206.8	.7601	.0411	.8470	.0299
1015	231.0	.0407	.9593	.0478	.9522	1056	206.8	.7413	.1920	.8256	.1327
1016	231.1	.0348	.9657	.0410	.9590	1057	205.8	.7774	.1904	.8546	.1273
1017	224.7	.1558	.8065	.0393	.7046	1058	203.8	.8889	.0170	.9358	.0094
1018	224.7	.1049	.6110	.1795	.5378	1059	203.8	.8900	.0298	.9318	.0200
1019	224.7	.0819	.4680	.1437	.4151	1060	203.8	.8777	.0904	.9213	.0602
1020	224.7	.0603	.3719	.1135	.3336	1061	202.8	.9316	.0405	.9569	.0256
1021	224.7	.0510	.2146	.0856	.1955	1062	201.8	.9795	.0060	.9884	.0038
1022	224.7	.0390	.0894	.0662	.0830	1063	201.8	.9808	.0112	.9897	.0063
1023	224.7	.0346	.0990	.0599	.0920	1733	231.3	.9932	.0068	.9932	.0095
1024	221.7	.2285	.6974	.3569	.0711	1734	231.2	.9814	.0186	.9761	.0239
1025	221.7	.2152	.6376	.3339	.1427	1735	230.6	.9227	.0773	.9227	.0910
1026	221.7	.2006	.6036	.3241	.1790	1736	229.7	.0278	.0443	.0513	.0515
1027	221.7	.1475	.2015	.2274	.6013	1737	228.7	.9899	.3101	.6899	.3408
1028	221.7	.1319	.0498	.2048	.7521	1738	225.7	.8487	.0166	.2273	.0178
1029	219.7	.3018	.6760	.4465	.0208	1739	224.7	.1652	.9341	.2694	.7306
1031	219.7	.2687	.6164	.4248	.0881	1740	224.7	.1373	.1341	.2246	.1385
1031	219.7	.2589	.4909	.3819	.2277	1741	224.7	.1217	.2173	.2011	.2197
1032	219.7	.2390	.3682	.3513	.2954	1742	224.7	.0832	.4512	.1312	.4478
1033	219.7	.2229	.2787	.3293	.4438	1743	224.7	.0352	.9595	.0684	.9240
1034	219.7	.2091	.1834	.3114	.1500	1744	214.8	.4561	.0144	.6076	.0117
1035	219.7	.1863	.0492	.2854	.6740	1745	212.8	.5290	.9999	.6740	.3260
1036	216.7	.3752	.5480	.5273	.4070	1746	209.8	.6243	.0775	.7470	.0581
1037	216.7	.3644	.5034	.5133	.3731	1747	206.8	.7357	.1429	.8232	.1009
1038	216.7	.3417	.3192	.4709	.2401	1748	206.8	.7589	.0066	.8468	.0056
1039	216.7	.3140	.1311	.4341	.1009	1749	205.8	.7707	.1967	.8438	.1365
1040	216.7	.3005	.0414	.4192	.0317	1750	203.8	.8788	.0661	.9224	.0440
1041	214.8	.4632	.5254	.6153	.0091	1751	203.8	.8864	.0164	.9311	.0109
1042	214.8	.4447	.4599	.5944	.0759	1752	202.8	.9247	.0434	.9525	.0286
1043	214.8	.4259	.3407	.5624	.3297	1753	201.8	.9741	.0155	.9841	.0098
1044	214.8	.4061	.2256	.5384	.1628	1754	226.6	.9887	.0113	.9887	.0141
1045	214.8	.3783	.5753	.5055	.4607	1860	231.3	.9918	.0082	.9918	.0103
1046	211.8	.5556	.0665	.6920	.2401	1861	224.7	.1455	.0833	.2387	.0860
1047	211.8	.5306	.2475	.6596	.1895	1862	224.7	.0354	.9548	.0590	.9327
1048	211.8	.5174	.3409	.6422	.2611	1866	206.8	.7591	.0164	.8481	.0117



TABLE 12  
EXPERIMENTAL DATA AT 18 ATM.

RUN NO.	TEMP. DEGR.	LIQUID MOL FRACTION N2	LIQUID MOL FRACTION AP	LIQUID MOL FRACTION O2	VAPOR MOL FRACTION N2	VAPOR MOL FRACTION AR	VAPOR MOL FRACTION O2	RUN NO.	TEMP. DEGR.	LIQUID MOL FRACTION N2	LIQUID MOL FRACTION AR	LIQUID MOL FRACTION O2	VAPOR MOL FRACTION N2	VAPOR MOL FRACTION AR	VAPOR MOL FRACTION O2
56	231.8	.0873	.....	.9127	.1427	.....	.8573	109	214.8	.5674	.1665	.2662	.6829	.1306	.1865
57	227.8	.1959	.....	.8041	.3043	.....	.6957	110	209.8	.7935	.0189	.1875	.8716	.0114	.1171
58	224.7	.2784	.....	.7216	.4168	.....	.5832	111	209.8	.7874	.0341	.1786	.8696	.0211	.1093
59	220.7	.4023	.....	.5977	.5400	.....	.4600	112	209.8	.7851	.0539	.1610	.8624	.0368	.1007
70	216.7	.5320	.....	.4680	.6655	.....	.3345	113	209.8	.7810	.0733	.1457	.8597	.0494	.0909
71	211.8	.7120	.....	.2880	.8176	.....	.1824	114	209.8	.7754	.1114	.1133	.8560	.0777	.0663
72	208.8	.8451	.....	.1549	.8966	.....	.1034	115	209.8	.7623	.1844	.0533	.8399	.1269	.0332
73	206.8	.9283	.....	.0717	.9576	.....	.0424	116	207.8	.8780	.0177	.1043	.9257	.0102	.0640
74	235.2	.....	.0372	.9628	.....	.0435	.9565	117	207.8	.8736	.0310	.0954	.9249	.0186	.0566
75	234.9	.....	.0682	.9318	.....	.0805	.9195	118	207.8	.8745	.0486	.0768	.9230	.0310	.0460
76	234.6	.....	.1035	.8965	.....	.1202	.8798	119	207.8	.8670	.0662	.0668	.9195	.0421	.0384
77	234.3	.....	.1340	.8660	.....	.1553	.8447	120	207.8	.8598	.0905	.0496	.9137	.0598	.0264
78	205.3	.9886	.0114	.....	.9922	.0078	.....	121	207.8	.8587	.1217	.0196	.9048	.0818	.0134
79	205.8	.9603	.0397	.....	.9737	.0263	.....	122	206.8	.9213	.0305	.0482	.9456	.0302	.0242
80	206.3	.9341	.0659	.....	.9563	.0437	.....	123	206.8	.9143	.0471	.0386	.9451	.0393	.0155
81	206.8	.9040	.0960	.....	.9348	.0652	.....	124	206.8	.9159	.0603	.0238	.9404	.0522	.0074
82	233.7	.0345	.0240	.9414	.0593	.0291	.9116	125	205.8	.9067	.0811	.0123	.9782	.0101	.0116
83	233.7	.0292	.0475	.9233	.0510	.0553	.8937	126	205.8	.9671	.0127	.0202	.9824	.0029	.0147
84	233.7	.0238	.0621	.9141	.0450	.0712	.8838	127	205.8	.9696	.0045	.0258	.9824	.0029	.0147
85	233.7	.0172	.1076	.8752	.0306	.1225	.8459	128	205.8	.9670	.0136	.0194	.9787	.0101	.0112
86	229.7	.1411	.0168	.8431	.2270	.0182	.7548	129	205.8	.9617	.0323	.0060	.9755	.0215	.0030
87	229.7	.1303	.0221	.8476	.2206	.0240	.7554	534	231.8	.0852	.....	.9148	.1512	.....	.8488
88	229.7	.1350	.0356	.8294	.2192	.0371	.7437	535	224.7	.2765	.....	.7235	.4096	.....	.5904
89	229.7	.1307	.0455	.8238	.2114	.0481	.7404	536	211.8	.7270	.....	.2730	.8222	.....	.1778
90	229.7	.1182	.0729	.8089	.1981	.0770	.7250	537	208.8	.8426	.....	.1574	.9089	.....	.0911
91	229.7	.1105	.1193	.7702	.1816	.1277	.6907	538	235.2	.....	.0384	.9616	.....	.0468	.9532
92	224.7	.2754	.0153	.7093	.4066	.0148	.5786	539	229.7	.1440	.0111	.8450	.2325	.0119	.7556
93	224.7	.2656	.0246	.7098	.3951	.0232	.5817	540	224.7	.2770	.0271	.6959	.4075	.0263	.5662
94	224.7	.2718	.0350	.6932	.3933	.0336	.5731	541	224.7	.2742	.0400	.6857	.4040	.0385	.5575
95	224.7	.2599	.0484	.6917	.3903	.0459	.5638	542	219.7	.4326	.0183	.5492	.5750	.0158	.4092
96	224.7	.2626	.0940	.6434	.3807	.0914	.5279	543	219.7	.4285	.0424	.5291	.5649	.0361	.3990
97	224.7	.2479	.1393	.6128	.3703	.1307	.4991	544	214.8	.6028	.0431	.3540	.7258	.0346	.2396
98	219.7	.4205	.0182	.5613	.5570	.0135	.4295	545	207.8	.8698	.0333	.0969	.9242	.0228	.0530
99	219.7	.4316	.0268	.5416	.5541	.0219	.4239	546	214.8	.5873	.1498	.2629	.6982	.1183	.1831
100	219.7	.4276	.0430	.5294	.5584	.0342	.4075	563	209.8	.7885	.0968	.1146	.8580	.0692	.0728
101	219.7	.4218	.0557	.5225	.5472	.0449	.4080	564	205.8	.9719	.0233	.0048	.9796	.0170	.0034
102	219.7	.4218	.0899	.4883	.5456	.0789	.3755	936	205.8	.9710	.....	.0290	.9822	.....	.0178
103	219.7	.4038	.1551	.4411	.5227	.1295	.3478	937	224.7	.1669	.8331	.....	.2503	.7497	.....
104	214.8	.5917	.0180	.3902	.7251	.0121	.2628	938	221.7	.2698	.7302	.....	.3778	.6222	.....
105	214.8	.5882	.0269	.3849	.7224	.0190	.2596	939	216.7	.4584	.5416	.....	.5761	.4239	.....
106	214.8	.5906	.0423	.3670	.7181	.0317	.2503	940	209.8	.7692	.2308	.....	.8388	.1612	.....
107	214.8	.5806	.0601	.3593	.7128	.0449	.2423	941	207.8	.8705	.1295	.....	.9116	.0884	.....
108	214.8	.5797	.0974	.3229	.7083	.0749	.2168	942	206.0	.9587	.0413	.....	.9725	.0275	.....

TABLE 12  
EXPERIMENTAL DATA AT 18 ATM. (continued)

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION N2	LIQUID MOL FRACTION AR	VAPOR MOL FRACTION N2	VAPOR MOL FRACTION AR	RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION N2	LIQUID MOL FRACTION AR	VAPOR MOL FRACTION N2	VAPOR MOL FRACTION AR
943	205.6	.9748	.0252	.9825	.0175	986	214.8	.6009	.0127	.7312	.0094
944	205.5	.9797	.0203	.9863	.0137	987	214.8	.5568	.3236	.6686	.2490
945	235.4	.....	.....	.....	.....	988	212.8	.6834	.0119	.7895	.0094
946	235.3	.....	.9819	.....	.9771	989	212.8	.6763	.0542	.7805	.0405
947	235.0	.....	.9735	.....	.9694	990	212.8	.6678	.0966	.7716	.0720
948	233.7	.....	.9442	.....	.9340	991	212.8	.6553	.1892	.7544	.1433
949	232.4	.....	.9761	.....	.9709	992	212.8	.6420	.2815	.7408	.2083
950	231.4	.....	.6108	.....	.5826	993	209.8	.8003	.0124	.8727	.0091
951	230.5	.....	.4230	.....	.4001	994	209.8	.7974	.0425	.8677	.0305
952	230.3	.....	.1811	.....	.1732	995	209.8	.7730	.1992	.8411	.1416
953	229.7	.....	.0936	.....	.0903	996	207.8	.8863	.0106	.9304	.0073
954	229.7	.....	.8241	.....	.7395	997	207.8	.8817	.0404	.9258	.0266
955	229.7	.....	.1066	.....	.6279	998	206.8	.9308	.0057	.9583	.0034
956	229.7	.....	.5901	.....	.5318	999	206.8	.9278	.0160	.9569	.0098
957	229.7	.....	.4583	.....	.4172	1707	235.5	.....	.0100	.....	.0121
958	229.7	.....	.3260	.....	.3013	1708	235.4	.....	.0212	.....	.0247
959	229.7	.....	.1714	.....	.1637	1709	230.3	.....	.9206	.....	.9216
960	226.7	.....	.7104	.....	.6038	1710	233.7	.....	.0160	.....	.0186
961	226.7	.....	.6062	.....	.3222	1711	229.7	.....	.9054	.....	.8974
962	226.7	.....	.3178	.....	.4395	1712	226.7	.....	.9006	.....	.8398
963	226.7	.....	.5146	.....	.2321	1713	226.7	.....	.2381	.....	.2287
964	226.7	.....	.2654	.....	.0852	1714	224.7	.....	.0600	.....	.0566
965	224.7	.....	.0955	.....	.0372	1715	219.7	.....	.0300	.....	.0256
966	224.7	.....	.8288	.....	.5575	1716	219.7	.....	.0763	.....	.0653
967	224.7	.....	.6463	.....	.5272	1717	219.7	.....	.2002	.....	.1708
968	224.7	.....	.5447	.....	.4490	1718	214.8	.....	.0376	.....	.0302
969	224.7	.....	.4081	.....	.3375	1719	214.8	.....	.0571	.....	.0369
970	224.7	.....	.2827	.....	.2378	1720	214.8	.....	.0124	.....	.0101
971	224.7	.....	.1079	.....	.0922	1721	216.7	.....	.1342	.....	.1093
972	221.7	.....	.0343	.....	.0303	1722	212.8	.....	.3802	.....	.2945
973	221.7	.....	.5487	.....	.4261	1723	209.8	.....	.0201	.....	.0138
974	221.7	.....	.6651	.....	.3621	1724	209.8	.....	.0323	.....	.0235
975	221.7	.....	.3819	.....	.2985	1725	208.8	.....	.....	.....	.....
976	221.7	.....	.1475	.....	.1177	1726	207.8	.....	.0196	.....	.0135
977	219.7	.....	.0448	.....	.0359	1727	207.8	.....	.0881	.....	.0613
978	219.7	.....	.5541	.....	.4128	1728	207.8	.....	.0346	.....	.0239
979	219.7	.....	.3653	.....	.2759	1729	207.8	.....	.1539	.....	.1070
980	219.7	.....	.2680	.....	.2012	1730	206.8	.....	.0075	.....	.0049
981	216.7	.....	.0617	.....	.0491	1731	206.8	.....	.0210	.....	.0161
982	216.7	.....	.4425	.....	.3120	1732	205.8	.....	.0269	.....	.0178
983	216.7	.....	.3886	.....	.2727	1863	219.7	.....	.1509	.....	.1295
984	216.7	.....	.3667	.....	.2499	1864	214.8	.....	.0216	.....	.0172
985	216.7	.....	.2365	.....	.1684	1867	205.8	.....	.0246	.....	.0163
		.....	.1091	.....	.0794			.....	.....	.....	.....
		.....	.4188	.....	.3326			.....	.....	.....	.....
		.....	.4188	.....	.5880			.....	.....	.....	.....
		.....	.4721	.....	.....			.....	.....	.....	.....
		.....	.9774	.....	.....			.....	.....	.....	.....
		.....	.9774	.....	.....			.....	.....	.....	.....
		.....	.9790	.....	.....			.....	.....	.....	.....
		.....	.5434	.....	.....			.....	.....	.....	.....
		.....	.3271	.....	.....			.....	.....	.....	.....
		.....	.2563	.....	.....			.....	.....	.....	.....
		.....	.0063	.....	.....			.....	.....	.....	.....

TABLE 13  
EXPERIMENTAL DATA AT 20 ATM.

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION N2	LIQUID MOL FRACTION AP	LIQUID MOL FRACTION O2	VAPOR MOL FRACTION N2	VAPOR MOL FRACTION AR	VAPOR MOL FRACTION O2	TEMP. DEG.R	RUN NO.	LIQUID MOL FRACTION N2	LIQUID MOL FRACTION AR	LIQUID MOL FRACTION O2	VAPOR MOL FRACTION N2	VAPOR MOL FRACTION AR	VAPOR MOL FRACTION O2
1	232.5	.1749	.....	.8251	.2724	.....	.7276	214.8	42	.7389	.0444	.2167	.8230	.0321	.1449
2	223.7	.4232	.....	.5768	.5633	.....	.4367	214.8	43	.7353	.0647	.2000	.8226	.0481	.1293
3	214.1	.7715	.....	.2285	.8504	.....	.1496	214.8	44	.7315	.0763	.1923	.8149	.0581	.1270
4	211.0	.8987	.....	.1013	.9368	.....	.0622	214.8	45	.7234	.1231	.1535	.8048	.0943	.1009
5	235.6	.0940	.....	.9060	.1553	.....	.8447	214.8	46	.7184	.1789	.1027	.7964	.1362	.0674
6	227.6	.3144	.....	.6856	.4331	.....	.5659	212.8	47	.8161	.0644	.1195	.8814	.0457	.0729
7	221.7	.4803	.....	.5197	.6164	.....	.3836	212.8	48	.8123	.0449	.1429	.8766	.0319	.0915
8	212.8	.8222	.....	.1778	.8911	.....	.1189	212.8	49	.8177	.0171	.1652	.8848	.0114	.1038
9	239.5	.....	.0980	.9920	.....	.0102	.9898	212.8	51	.8115	.0711	.1174	.8873	.0504	.0772
10	235.4	.....	.0161	.9839	.....	.0197	.9803	212.8	52	.8023	.1073	.0904	.8646	.0769	.0585
11	239.2	.....	.0449	.9551	.....	.0519	.9491	212.8	53	.7960	.1451	.0590	.8646	.0564	.0585
12	238.9	.....	.0581	.9419	.....	.0633	.9367	211.8	54	.8608	.0253	.1139	.8592	.1037	.0371
13	208.8	.9913	.0087	.....	.9943	.0057	.....	211.8	55	.8552	.0539	.0909	.9109	.0171	.0720
14	209.3	.9628	.0372	.....	.9734	.0266	.....	211.8	56	.8492	.0942	.0566	.9058	.0373	.0569
15	209.8	.9364	.0634	.....	.9557	.0443	.....	211.8	57	.8466	.1243	.0290	.8977	.0659	.0364
16	210.3	.9096	.0904	.....	.9356	.0644	.....	210.8	58	.9045	.0103	.0852	.8870	.0941	.0189
17	234.7	.1067	.0211	.8722	.1800	.0222	.7977	210.8	59	.9012	.0237	.0751	.9409	.0064	.0527
18	234.7	.1045	.0307	.8649	.1738	.0341	.7921	210.8	60	.8979	.0380	.0641	.9361	.0171	.0468
19	234.7	.1084	.0341	.8575	.1727	.0373	.7901	210.8	61	.8988	.0448	.0564	.9343	.0262	.0395
20	234.7	.1034	.0594	.8373	.1680	.0646	.7674	210.8	62	.8988	.0575	.0437	.9339	.0281	.0381
21	234.7	.1170	.0102	.8727	.1865	.0113	.8022	210.8	63	.8947	.0901	.0153	.9318	.0401	.0281
22	234.7	.1163	.0175	.8662	.1831	.0187	.7982	209.8	64	.8943	.0254	.0307	.9264	.0639	.0098
23	229.7	.2591	.0090	.7315	.3751	.0095	.6154	209.8	65	.9445	.0453	.0102	.9657	.0160	.0183
24	229.7	.2657	.0151	.7192	.3754	.0152	.6094	209.8	65	.9445	.0453	.0102	.9628	.0308	.0064
25	229.7	.2515	.0231	.7254	.3689	.0231	.6080	214.1	517	.7804	.....	.2196	.8555	.....	.1445
26	229.7	.2482	.0326	.7192	.3610	.0324	.6056	221.7	518	.4981	.....	.5019	.8555	.....	.1445
27	229.7	.2456	.0476	.7066	.3704	.0471	.5825	217.7	519	.6394	.....	.3606	.6319	.....	.3681
28	229.7	.2337	.1037	.6626	.3503	.1003	.5825	209.8	520	.9467	.0360	.0152	.7486	.....	.2514
29	224.7	.3893	.0247	.5860	.5213	.0212	.5494	212.8	521	.8216	.0777	.1007	.9635	.0268	.0097
30	224.7	.3824	.0370	.5806	.5184	.0324	.4576	214.8	522	.7427	.0804	.1769	.8795	.0546	.0659
31	224.7	.3733	.0581	.5686	.5094	.0508	.4492	219.7	523	.5686	.0183	.4132	.8194	.0601	.1205
32	224.7	.3711	.0863	.5426	.5018	.0767	.4215	229.7	524	.2521	.0115	.7364	.6902	.0154	.2944
33	224.7	.3644	.1326	.5029	.4974	.1164	.3862	234.7	525	.1144	.0090	.8766	.3689	.0117	.6194
34	224.7	.3475	.2330	.4195	.4677	.2052	.3271	234.7	526	.1194	.0235	.8571	.1881	.0097	.8022
35	219.7	.5486	.0371	.4143	.6318	.0291	.2891	229.7	527	.2440	.0116	.7444	.1235	.0260	.8506
36	219.7	.5525	.0371	.4104	.6827	.0269	.2894	229.7	528	.2446	.0660	.6895	.3466	.0119	.6551
37	219.7	.5467	.0589	.3944	.6560	.0462	.2978	219.7	529	.5611	.0675	.3714	.3466	.0619	.5915
38	219.7	.5244	.0990	.3766	.6486	.0812	.2702	210.8	530	.9091	.0423	.0486	.6859	.0516	.2626
39	219.7	.5132	.1530	.3338	.6436	.1246	.2318	211.8	531	.8499	.1213	.0288	.9439	.0268	.0293
40	219.7	.5042	.2283	.2675	.6247	.1809	.1944	227.6	532	.3153	.....	.6847	.9007	.0543	.0150
41	214.8	.7411	.0255	.2334	.8254	.0189	.1557	212.8	533	.8210	.....	.1790	.4583	.....	.5417
								212.8	557	.8262	.0576	.1162	.8867	.0416	.0717

TABLE 13  
EXPERIMENTAL DATA AT 20 ATM. (continued)

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION	
		N <sub>2</sub>	AR	N <sub>2</sub>	AR			N <sub>2</sub>	AR	N <sub>2</sub>	AR
834	208.7	.9951	.0049	.0035	.0035	876	221.7	.4510	.2474	.5695	.2058
835	209.0	.9792	.0208	.0144	.0144	877	221.7	.4420	.3213	.5593	.2652
836	209.4	.9599	.0401	.0275	.0275	878	221.7	.4154	.4958	.5281	.4042
837	212.8	.7936	.2064	.1487	.1487	879	219.7	.5591	.0132	.6831	.0107
838	217.7	.5707	.4293	.3297	.3297	880	219.7	.5575	.0472	.6776	.0380
839	229.7	.1290	.8710	.8079	.8079	881	219.7	.5508	.0786	.6689	.0636
840	231.7	.0671	.9329	.8968	.8968	882	219.7	.5029	.3786	.6113	.3010
841	209.3	.2697	.7303	.6303	.6303	883	217.7	.6227	.0770	.7294	.0606
842	219.7	.5615	.4385	.3126	.3126	884	217.7	.6126	.1353	.7181	.1064
843	239.2	.9371	.0629	.0288	.0288	885	217.7	.5891	.2892	.6894	.2247
844	238.8	.9371	.0629	.0727	.0727	886	214.8	.7420	.0138	.8307	.0108
845	238.5	.9068	.0932	.1074	.1074	887	214.8	.7443	.0301	.8274	.0223
846	237.9	.8395	.1605	.1807	.1807	888	214.8	.7409	.0591	.8201	.0443
847	236.6	.6637	.3363	.3630	.3630	889	214.8	.7059	.2679	.7848	.1965
848	235.6	.4975	.5025	.5267	.5267	890	209.3	.9674	.0134	.9813	.0093
849	234.7	.2873	.7127	.7243	.7243	891	209.3	.9673	.0211	.9785	.0141
850	234.3	.1599	.8401	.8450	.8450	892	209.3	.9634	.0305	.9751	.0205
851	234.7	.7928	.1164	.1243	.1243	1684	238.9	.0807	.0626	.1329	.0376
852	234.7	.6154	.3344	.3489	.3489	1685	234.7	.0807	.1706	.1329	.1798
853	234.7	.5134	.4557	.4704	.4704	1686	234.7	.0038	.6748	.0065	.7040
854	234.7	.4268	.5585	.5752	.5752	1687	231.7	.1680	.1451	.2531	.1455
855	234.7	.3022	.6968	.7098	.7098	1688	231.7	.0785	.8097	.1221	.7783
856	231.7	.6885	.1482	.1501	.1501	1689	229.7	.2489	.0138	.3670	.0139
857	231.7	.4828	.3945	.3858	.3858	1690	229.7	.2389	.0651	.3494	.0540
858	231.7	.2904	.6179	.5982	.5982	1691	229.7	.2357	.0790	.3447	.0767
859	231.7	.0682	.8408	.8086	.8086	1692	229.7	.2295	.1105	.3365	.1071
860	231.7	.3752	.6193	.6193	.6193	1693	227.7	.2959	.0610	.4200	.0576
861	229.7	.5320	.4620	.4521	.4521	1694	227.6	.3111	.0000	.4378	.0000
862	229.7	.4023	.5926	.4022	.4022	1695	224.7	.2954	.7046	.4018	.5982
863	229.7	.2578	.7460	.5506	.5506	1696	221.7	.4034	.5966	.5080	.4920
864	229.7	.1601	.8393	.6503	.6503	1697	224.7	.3940	.0121	.5268	.0109
865	227.7	.5948	.1229	.1156	.1156	1698	224.7	.3429	.3241	.4575	.2901
866	227.7	.5303	.2022	.1873	.1873	1699	219.7	.5377	.1531	.6519	.1245
867	227.7	.4104	.3442	.3377	.3377	1700	212.8	.8273	.0000	.8876	.0000
868	227.7	.2222	.7778	.5078	.5078	1701	212.8	.8277	.0187	.8860	.0137
869	227.7	.0569	.9431	.6703	.6703	1702	211.8	.8508	.1248	.8955	.0885
870	224.7	.5890	.0192	.0176	.0176	1703	210.8	.9039	.0455	.9353	.0320
871	224.7	.5479	.0690	.0606	.0606	1704	210.8	.9034	.0191	.9380	.0133
872	224.7	.2161	.7839	.4261	.4261	1705	209.3	.9732	.0089	.9823	.0061
873	224.7	.0811	.9189	.3996	.3996	1706	209.3	.9698	.0195	.9809	.0135
874	221.7	.4399	.5601	.5299	.5299	1859	238.9	.0000	.0689	.0000	.0759
875	221.7	.3825	.6175	.6044	.6044	1865	209.3	.9664	.0240	.9776	.0169
		.3825	.1525	.1272	.1272						

TABLE 14  
EXPERIMENTAL DATA AT 23 ATM.

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION		RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR MOL FRACTION	
		N2	AR	N2	AR			N2	AR	N2	AR
724	240.2	.1125	.8675	.1742	.8258	756	240.2	.1054	.0281	.1640	.0301
725	236.7	.2048	.7952	.3004	.6996	757	240.2	.1033	.0450	.1606	.0480
726	229.7	.4082	.5918	.5301	.4699	758	240.2	.1005	.0583	.1555	.0618
727	223.7	.5871	.4129	.6956	.3044	759	240.2	.0925	.0952	.1434	.1012
728	218.2	.8068	.1932	.8656	.1344	760	240.2	.0841	.1432	.1302	.1526
729	215.3	.9233	.0767	.9506	.0494	761	240.2	.0653	.2390	.1003	.2506
730	213.8	.9607	.0193	.9877	.0123	762	240.2	.0303	.4482	.0451	.4636
731	236.7	.0767	.9233	.1140	.8860	763	240.2	.0059	.6265	.0116	.6415
732	232.7	.2043	.7957	.2814	.7186	764	236.7	.2063	.0070	.2963	.0077
733	226.7	.4147	.5853	.5160	.4840	765	236.7	.1992	.0389	.2906	.0392
734	220.7	.6574	.3426	.7367	.2633	766	236.7	.1959	.0579	.2850	.0574
735	216.7	.8409	.1591	.8836	.1164	767	236.7	.1934	.0735	.2796	.0737
736	215.3	.9108	.0892	.9349	.0651	768	236.7	.1875	.0929	.2734	.0932
737	214.5	.9488	.0512	.9635	.0365	769	236.7	.1780	.1313	.2593	.1315
738	214.1	.9662	.0338	.9765	.0235	770	236.7	.1703	.1704	.2486	.1701
739	213.9	.9728	.0272	.9801	.0199	771	236.7	.1600	.2276	.2486	.2263
740	213.7	.9821	.0179	.9871	.0129	772	236.7	.1253	.4463	.2339	.4343
741	213.5	.9942	.0059	.9950	.0050	773	236.7	.1054	.6107	.1839	.5894
742	244.7	.0000	.0134	.0000	.0157	774	236.7	.0935	.7365	.1541	.5894
743	244.6	.0000	.0233	.0000	.0269	775	236.7	.0812	.8847	.1372	.7064
744	244.5	.0000	.0331	.0000	.0378	776	232.7	.3161	.0153	.1205	.0478
745	244.4	.0000	.0407	.0000	.0467	777	232.7	.3050	.0693	.4323	.0154
746	244.2	.0000	.0611	.0000	.0718	778	232.7	.2961	.1243	.4169	.0656
747	243.9	.0000	.0948	.0000	.1084	779	232.7	.2808	.2100	.4037	.1167
748	243.4	.0000	.1528	.0000	.1709	780	232.7	.2661	.2933	.3808	.1948
749	242.3	.0000	.2852	.0000	.3092	781	232.7	.2436	.4509	.3604	.2709
750	241.3	.0000	.4386	.0000	.4621	782	232.7	.2235	.6114	.3308	.4118
751	240.2	.0000	.6679	.0000	.6809	783	232.7	.2087	.7707	.3053	.5545
752	239.8	.0000	.8177	.0000	.8229	784	229.7	.4072	.0149	.2873	.6968
753	240.2	.1134	.0078	.1753	.8144	785	229.7	.4093	.0257	.5290	.0135
754	240.2	.1141	.0141	.1732	.8120	786	229.7	.4025	.0395	.5245	.0232
755	240.2	.1071	.0223	.1680	.8080	787	229.7	.3996	.0545	.5214	.0396
										.5154	.0497
											.4343

TABLE 14  
EXPERIMENTAL DATA AT 23 ATM. (continued)

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION N2	AR	O2	VAPOR MOL FRACTION N2	AR	O2	RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION N2	AR	O2	VAPOR MOL FRACTION N2	AR	O2
786	229.7	.3955	.0684	.5361	.5174	.0614	.4212	820	218.2	.7919	.1018	.1063	.8512	.0767	.0721
789	229.7	.3655	.0973	.5142	.5053	.0870	.4077	821	218.2	.7798	.1898	.0304	.8351	.1440	.0209
790	229.7	.3655	.1250	.4886	.5013	.1103	.3885	822	216.7	.8622	.0273	.1105	.9054	.0201	.0744
791	229.7	.3742	.1770	.4488	.4842	.1563	.3594	823	216.7	.8503	.1216	.0280	.8909	.0919	.0172
792	229.7	.3541	.3147	.3312	.4574	.2756	.2670	824	216.7	.8550	.0743	.0708	.8954	.0559	.0488
793	229.7	.3277	.4964	.1759	.4258	.4325	.1417	825	215.3	.9255	.0076	.0669	.9492	.0054	.0454
794	226.7	.5041	.0184	.4775	.6175	.0162	.3663	826	215.3	.9242	.0226	.0532	.9466	.0168	.0366
795	226.7	.4953	.0501	.4547	.6096	.0437	.3467	827	215.3	.9223	.0347	.0431	.9462	.0243	.0295
796	226.7	.4899	.0822	.4279	.6057	.0705	.3239	828	215.3	.9184	.0467	.0349	.9429	.0336	.0235
797	226.7	.4794	.1392	.3813	.5899	.1164	.2936	829	215.3	.9187	.0604	.0210	.9414	.0438	.0148
798	226.7	.4666	.2455	.2879	.5718	.2114	.2169	830	215.3	.9158	.0767	.0075	.9390	.0562	.0049
799	226.7	.4479	.3526	.1995	.5494	.2978	.1528	831	213.8	.9827	.0058	.0115	.9901	.0031	.0067
800	223.7	.6066	.0106	.3828	.7104	.0091	.2805	832	213.8	.9830	.0103	.0067	.9884	.0075	.0041
801	223.7	.6035	.0246	.3719	.7102	.0204	.2695	833	213.8	.9831	.0137	.0032	.9881	.0098	.0022
802	223.7	.6005	.0362	.3633	.7048	.0297	.2655	918	213.5	.9946	.0023	.0031	.9963	.0016	.0021
803	223.7	.6003	.0519	.3476	.7035	.0423	.2542	919	215.3	.9212	.0377	.0411	.9447	.0273	.0280
804	223.7	.5982	.0652	.3367	.7008	.0530	.2462	920	216.7	.8591	.0757	.0653	.8977	.0572	.0451
805	223.7	.5940	.0932	.3129	.6935	.0762	.2303	921	218.2	.8063	.0080	.1857	.8670	.0064	.1266
806	223.7	.5882	.1185	.2932	.6882	.0967	.2151	922	220.7	.7170	.0235	.2595	.7940	.0185	.1875
807	223.7	.5731	.2137	.2131	.6699	.1739	.1562	923	220.7	.6765	.2474	.0761	.7548	.1925	.0528
808	223.7	.5478	.3766	.0756	.6409	.3008	.0583	924	223.7	.6025	.0258	.3717	.7094	.0209	.2697
809	220.7	.7121	.0193	.2687	.7978	.0140	.1882	925	223.7	.6105	.....	.3895	.7142	.....	.2658
810	220.7	.7031	.0593	.2376	.7855	.0459	.1686	926	226.7	.4305	.4799	.0896	.5317	.3999	.0684
811	220.7	.7006	.093A	.2056	.7815	.0737	.1449	927	229.7	.3160	.6183	.0656	.4111	.5354	.0535
812	220.7	.6824	.1904	.1272	.7658	.1481	.0861	928	229.7	.3092	.6908	.....	.4022	.5978	.....
813	220.7	.6693	.2913	.0394	.7472	.2253	.0275	929	232.7	.2113	.7446	.0442	.2896	.6725	.0380
814	218.2	.8080	.0092	.1828	.8663	.0082	.1255	930	236.7	.2018	.0268	.7714	.2951	.0268	.0781
815	218.2	.8068	.0209	.1723	.8616	.0158	.1226	931	239.6	.....	.9093	.0907	.....	.9122	.0678
816	218.2	.8055	.0330	.1615	.8613	.0260	.1127	932	240.2	.1138	.0080	.8782	.1757	.0083	.8160
817	218.2	.8033	.044A	.1518	.8613	.0340	.1047	933	240.2	.1093	.0389	.8517	.1641	.0431	.7928
818	218.2	.8030	.0540	.1430	.8610	.0408	.0982	934	240.2	.0297	.4579	.5124	.0456	.4712	.4832
819	218.2	.7971	.0743	.1286	.8552	.0571	.0877	935	240.2	.0090	.6332	.3578	.0112	.6492	.3396

TABLE 15  
EXPERIMENTAL DATA AT 26 ATM.

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION N2	LIQUID MOL FRACTION AR	VAPOR MOL FRACTION N2	VAPOR MOL FRACTION AR	RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION N2	LIQUID MOL FRACTION AR	VAPOR MOL FRACTION N2	VAPOR MOL FRACTION AR
610	245.1	.1071	.....	.1659	.....	646	242.7	.0502	.8991	.0730	.8773
611	240.7	.2319	.....	.3236	.....	647	240.7	.2281	.0049	.3203	.0051
612	234.7	.4057	.....	.5152	.....	648	240.7	.2290	.0077	.3190	.0082
613	228.7	.5976	.....	.6942	.....	649	240.7	.2256	.0118	.3148	.0120
614	222.7	.8094	.....	.8626	.....	650	240.7	.2268	.0173	.3133	.0178
615	219.7	.9250	.....	.9464	.....	651	240.7	.2189	.0271	.3125	.0277
616	218.2	.9790	.....	.9868	.....	652	240.7	.2214	.0310	.3093	.0307
617	240.7	.1055	.8945	.1481	.8519	653	240.7	.2137	.0608	.2994	.0608
618	237.7	.2004	.7994	.2700	.7300	654	240.7	.1901	.1587	.2693	.1560
619	231.7	.4090	.5920	.4973	.5027	655	240.7	.1512	.3826	.2132	.3709
620	225.7	.6378	.3622	.7109	.2891	656	240.7	.1194	.6170	.1722	.5985
621	221.2	.8373	.1627	.8753	.1247	657	240.7	.1072	.7296	.1549	.6969
622	219.2	.9301	.0690	.9471	.0529	658	240.7	.0963	.8469	.1409	.8055
623	218.8	.9494	.....	.9612	.....	659	237.7	.3134	.0044	.4187	.0043
624	218.4	.9654	.0346	.9736	.0264	660	237.7	.3115	.0131	.4159	.0122
625	218.2	.9739	.0261	.9806	.0194	661	237.7	.3123	.0144	.4150	.0156
626	217.8	.9864	.0136	.9896	.0104	662	237.7	.3101	.0252	.4111	.0238
627	217.8	.9950	.....	.9966	.....	663	237.7	.3085	.0432	.4095	.0409
629	244.5	.....	.0050	.....	.....	664	237.7	.3034	.0644	.4024	.0519
630	244.5	.....	.8300	.....	.9310	665	237.7	.2971	.0920	.3949	.0869
631	244.6	.....	.8530	.....	.8585	666	237.7	.2813	.2021	.3707	.1918
632	244.7	.....	.8067	.....	.8134	667	237.7	.2569	.3154	.3435	.2927
633	244.9	.....	.7719	.....	.7790	668	237.7	.2261	.5436	.3015	.4991
634	245.2	.....	.7087	.....	.7221	669	237.7	.2032	.7612	.2725	.6964
635	245.6	.....	.6519	.....	.6624	670	234.7	.3880	.0743	.4936	.0687
636	246.0	.....	.5594	.....	.5760	671	234.7	.3765	.1626	.4845	.1484
637	246.7	.....	.4805	.....	.4999	672	234.7	.3433	.3138	.4378	.2808
639	248.1	.....	.3591	.....	.3827	673	234.7	.3211	.5075	.4085	.4491
640	249.0	.....	.1702	.....	.1888	674	234.7	.3134	.5817	.3987	.5133
641	249.0	.....	.0728	.....	.0807	675	234.7	.3075	.6407	.3921	.5642
642	242.7	.1533	.0661	.2282	.0672	676	231.7	.4964	.0100	.6039	.0087
643	242.7	.1351	.2041	.1935	.2063	677	231.7	.4966	.0147	.6039	.0127
644	242.7	.0965	.4374	.1375	.4335	678	231.7	.4966	.0259	.6020	.0229
645	242.7	.0873	.5017	.1244	.4962	679	231.7	.0000	.0000	.5988	.0322
		.0571	.7902	.0825	.7739						
			.1527		.1437						

TABLE 15  
EXPERIMENTAL DATA AT 26 ATM. (continued)

RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR N2	VAPOR MOL FRACTION		RUN NO.	TEMP. DEG.R	LIQUID MOL FRACTION		VAPOR N2	VAPOR MOL FRACTION		
		N2	AR		N2	AR			N2	AR		N2	AR	
681	231.7	.4934	.0424	.5977	.3647	.376	715	219.2	.9397	.0216	.0386	.9571	.0161	.0268
682	231.7	.4874	.0683	.5910	.3492	.0598	716	219.2	.9393	.0303	.0304	.9553	.0228	.0220
683	231.7	.4813	.0934	.5835	.3356	.0809	717	219.2	.9367	.0406	.0226	.9527	.0311	.0163
684	231.7	.4650	.1800	.5632	.2813	.1555	718	219.2	.9334	.0513	.0153	.9490	.0375	.0135
685	231.7	.4271	.4067	.5245	.1311	.3444	719	219.2	.9332	.0552	.0117	.9491	.0422	.0087
686	231.7	.4119	.5352	.5037	.0434	.4528	720	218.2	.9799	.0085	.0116	.9851	.0066	.0083
687	228.7	.5945	.0265	.6864	.2908	.0228	721	218.2	.9780	.0167	.0053	.9838	.0126	.0036
688	228.7	.5884	.0465	.6822	.2795	.0389	722	231.7	.4934	.0329	.4736	.5985	.0288	.3727
689	228.7	.5875	.0624	.6768	.2710	.0523	723	247.2	.....	.2902	.7098	.....	.3117	.6883
690	228.7	.5749	.1455	.6641	.2143	.1216	893	249.6	.....	.0196	.9804	.....	.0222	.9778
691	228.7	.5580	.2422	.6431	.1548	.2021	894	249.4	.....	.0372	.9628	.....	.0426	.9574
692	225.7	.5335	.3975	.6216	.0528	.3256	895	249.2	.....	.0547	.9453	.....	.0615	.9385
693	225.7	.7014	.0103	.7782	.2135	.0083	896	248.8	.....	.0970	.9030	.....	.1088	.8912
694	225.7	.6996	.0209	.7755	.2072	.0173	897	245.2	.....	.0190	.8715	.....	.0204	.8204
695	225.7	.6981	.0283	.7740	.2028	.0232	898	245.2	.....	.0611	.8380	.....	.0649	.7859
696	225.7	.6963	.0393	.7713	.1965	.0321	899	245.2	.....	.1341	.7810	.....	.1424	.7331
697	225.7	.6936	.0465	.7721	.1896	.0382	900	245.2	.....	.1846	.7409	.....	.1951	.6948
698	225.7	.6929	.0615	.7675	.1821	.0504	901	245.2	.....	.3086	.6398	.....	.3215	.6031
699	225.7	.6884	.0909	.7634	.1626	.0740	902	242.7	.....	.2029	.6602	.....	.2053	.5996
700	222.7	.6708	.1924	.7408	.1040	.1552	903	242.7	.....	.9251	.0247	.....	.9041	.0238
701	222.7	.8019	.0563	.8529	.1034	.0436	904	240.7	.....	.0098	.7591	.....	.0096	.6690
702	222.7	.7967	.0855	.8472	.0857	.0671	905	240.7	.....	.0237	.7487	.....	.0237	.6599
703	222.7	.7630	.1664	.8324	.0379	.1297	906	240.7	.....	.0575	.7217	.....	.0571	.6366
704	221.2	.8652	.0117	.9014	.0897	.0089	907	237.7	.....	.6597	.1248	.....	.6035	.1096
705	221.2	.8642	.0235	.8990	.0827	.0183	908	234.7	.....	.1479	.4754	.....	.1366	.3857
706	221.2	.8561	.0491	.8921	.0685	.0394	909	231.7	.....	.0488	.4599	.....	.0429	.3612
707	221.2	.8564	.0694	.8939	.0523	.0538	910	225.7	.....	.0463	.2559	.....	.0374	.1906
708	221.2	.8517	.0931	.8896	.0396	.0708	911	225.7	.....	.2567	.0784	.....	.2049	.0590
709	221.2	.8500	.1144	.8844	.0268	.0868	912	221.2	.....	.0318	.1033	.....	.0243	.0739
710	221.2	.8463	.1360	.8816	.0136	.1049	913	221.2	.....	.0401	.0965	.....	.0310	.0706
711	220.2	.9014	.0211	.9291	.0546	.0162	914	219.2	.....	.0464	.0206	.....	.0347	.0137
712	220.2	.8982	.0365	.9252	.0467	.0231	915	218.2	.....	.....	.0206	.....	.....	.0142
713	220.2	.8902	.0915	.9163	.0136	.0701	916	218.2	.....	.0184	.0065	.....	.0135	.0044
714	219.2	.9416	.0077	.9577	.0364	.0060	917	217.8	.....	.0051	.....	.....	.0040	.....



TABLE 16

## EXPERIMENTAL DATA AT MIXED PRESSURE LEVELS

<u>Run No.</u>	<u>Press.</u> <u>Atm.</u>	<u>Temp.</u> <u>Deg. R</u>	<u>Liquid Mol Fraction</u>			<u>Vapor Mol Fraction</u>		
			<u>N<sub>2</sub></u>	<u>Ar</u>	<u>O<sub>2</sub></u>	<u>N<sub>2</sub></u>	<u>Ar</u>	<u>O<sub>2</sub></u>
50	19.5	212.8	.7875	.0869	.1256	.8562	.0623	.0815
1914	1.03	163.0	.0039	-----	.9961	.0166	-----	.9834
1915	1.05	162.5	.0130	-----	.9870	.0491	-----	.9509
1916	0.97	162.0	.0035	-----	.9965	.0144	-----	.9856
1917	0.99	162.0	.0066	-----	.9934	.0248	-----	.9752
1918	0.98	161.3	.0179	-----	.9821	.0677	-----	.9323
1919	0.99	160.3	.0364	-----	.9636	.1313	-----	.8687
1920	0.97	160.0	.0385	-----	.9615	.1404	-----	.8596
1921	1.05	159.8	.0746	-----	.9254	.2397	-----	.7603
1922	1.01	159.0	.0833	-----	.9167	.2627	-----	.7373

## VI. CORRELATION OF EXPERIMENTAL DATA

 A. Thermodynamic Equations

The problem of correlation of vapor-liquid equilibrium data at high pressures is more complicated than at low pressures since the effect of pressure on the free energy of the liquid and also the effect of deviations from ideality in the vapor must be taken into account. A derivation of the equilibrium equations which take these effects into account follows.

The effect of pressure upon the free energy of a component in the liquid is given by the relation

$$dG_i = \bar{V}_i dp \quad (2)$$

and the effect of nonideality in the vapor is accounted for by means of the fugacity coefficient defined as

$$\phi_i = \frac{f_i}{p y_i} \quad (3)$$

The activity coefficient of component  $i$  in the liquid is now defined as

$$\ln \gamma_i = \ln \frac{f_i}{f_i^* x_i} = \left[ \frac{\partial(G^E/RT)}{\partial n_i} \right]_{T,p,n_j} \quad (4)$$

The derivation of the equilibrium equations involves a seven-step process:

1. The component is taken as a vapor from a standard pressure at which the vapor behaves ideally to the vapor pressure  $p_i^\circ$ .

$$\frac{\Delta G^I}{RT} = \ln p_i^\circ + \ln \phi_i^\circ \quad (5)$$

2. The vapor is condensed at the pressure  $p_i^\circ$  to liquid.

$$\frac{\Delta G^{II}}{RT} = 0 \quad (6)$$

3. The liquid is taken from the pressure  $p_i^o$  to the pressure of mixing  $p_m$ .

$$\frac{\Delta G^{III}}{RT} = \int_{p_i^o}^{p_m} \frac{v_i^o}{RT} dp \quad (7)$$

4. The component is mixed at the pressure  $p_m$ .

$$\frac{\Delta G^{IV}}{RT} = \ln x_i \gamma_i \quad (8)$$

5. The mixture is taken from the pressure  $p_m$  to the total vapor pressure of the mixture.

$$\frac{\Delta G^V}{RT} = \int_{p_m}^p \frac{\bar{v}_i}{RT} dp \quad (9)$$

6. The component in the liquid mixture is in equilibrium with the vapor at the pressure  $p$  and composition  $y_i$ .

$$\frac{\Delta G^{VI}}{RT} = 0 \quad (10)$$

7. The vapor is taken from the pressure  $p$  and composition  $y$  to a standard pressure at which the vapor behaves ideally, and then is separated into the various components.

$$\frac{\Delta G^{VII}}{RT} = \ln py_i - \ln \phi_i \quad (11)$$

Now since the free energy is a property of state and independent of the route by which the state is obtained, the sum of all these changes should add to zero since the initial and final states are the same. Thus the following relation for equilibrium is obtained.

$$\Sigma \frac{\Delta G}{RT} = \ln p_i^o \phi_i^o + \int_{p_i^o}^{p_m} \frac{v_i^o}{RT} dp + \ln x_i \gamma_i + \int_{p_m}^p \frac{\bar{v}_i}{RT} dp - \ln py_i \phi_i = 0 \quad (12)$$

If this equation is solved for  $py_i$ , the following is obtained:

$$\ln py_i = \ln \frac{p_i^{\circ} \phi_i^{\circ} x_i \gamma_i}{\phi_i} + \int_{p_i^{\circ}}^{p_m} \frac{v_i^{\circ}}{RT} dp + \int_{p_m}^p \frac{\bar{v}_i}{RT} dp \quad (13)$$

For the correlation of the nitrogen-argon-oxygen vapor liquid data there were insufficient partial molar volume data to use this equation as it stands, and it was necessary to simplify it. Thus it was assumed that the partial molar volume of a component in solution is equivalent to the liquid molar volume of that component and that the liquid volume is independent of pressure. With these assumptions, the equilibrium relation simplifies to the following equation which is the one used in correlating the nitrogen-argon-oxygen data.

$$py_i = \left[ \frac{p_i^{\circ} x_i \gamma_i \phi_i^{\circ}}{\phi_i} \right] e^{v_i^{\circ} (p - p_i^{\circ})/RT} \quad (14)$$

These assumptions regarding the molar volume are partly justified by the fact that the correction is usually small amounting to less than 20% in most cases and any errors which are made in this correction can be partially compensated for with other parameters. However, in the neighborhood of the critical point this correction is undoubtedly larger and deviates significantly from the simplifying assumptions made here. Therefore it is improbable that this simplified equation will be applicable in the neighborhood of the critical point.

In the calculation of equilibria it is helpful to bear in mind that according to the phase rule,  $F = c - P + 2$ ;  $c$  variables must be specified (since  $P = 2$ ) before the equilibrium point can be calculated. Thus one might specify the liquid composition and the temperature (the liquid composition involves  $c - 1$  variables since  $\sum_i x_i = 1$ ) or perhaps the mole fraction of one component in the liquid, the temperature and the pressure. If it is necessary to calculate not only the equilibrium point but also the number of moles in each phase, one more variable must be specified since the phase rule includes only intensive variables. Thus for example, one might specify an overall composition of the two-phase system, the pressure and the temperature.

The ease of numerical calculation varies depending upon which variables are specified; however even in the simplest cases iterative type calculations are necessary. This iteration is necessary since the functions  $\phi_i$ ,  $\gamma_i$  and  $e^{V_i(p-p_i)/RT}$  are not specified in terms of any one set of variables. For this reason the task of manual calculation would be prohibitive and calculations were done on a GE-225 computer.

### B. Liquid Molar Volume

The liquid molar volume of the three components were determined by a least squares fit of existing data to the equation

$$V = a + b x + c x^2 + d x^3 + e x^4 + f x^5 \quad (15)$$

Table 17 lists the constants obtained and the literature source for the data. Above the critical temperature of nitrogen the molar volume of nitrogen represents an extrapolation of the data from below the critical temperature. Data close to the critical point were not fitted.

TABLE 17

LIQUID MOLAR VOLUME CORRELATION CONSTANTS

Component	a	b	c	d	e	f	Lit. Ref.
Nitrogen	- 0.7	147.1	-264.1	227.08	- 92.29	14.649	(4)
Argon	-98.7	451.5	-610.2	393.62	-122.11	14.803	(4)
Oxygen	-34.0	178.6	-221.5	139.05	.. 43.09	5.341	(5)

### C. Vapor Pressure of Pure Components

Vapor pressure data for oxygen were taken from the literature. These data were used for the calibration of the three junction thermocouple of the equilibrium cell. Vapor pressure data for nitrogen and argon were measured in the cell based upon the temperature scale obtained from the oxygen data. Initially, it was attempted to calibrate the thermocouple from literature data on all three components, but calculated temperatures disagreed by as much as 0.2°R; therefore, only the data for oxygen were used in the calibration. If the oxygen temperature scale is in error by 0.2°R, then our temperature scale is in error by 0.2°R, but the ratio of vapor pressures will be more nearly correct than as calculated from the literature data.

Our value for the boiling point of oxygen is 162.36°R compared to the accepted value of 162.34°R<sup>(6)</sup>.

The vapor pressure data were fitted to the Riedel equation<sup>(7)</sup>.

$$\ln p_1^o = A - \frac{B}{T} + C \ln T + DT^6 \quad (16)$$

The constants obtained by a least squares fit to the data are summarized in Table 18 and deviation plots of the data are given in Figures 13, 14, and 15. The agreement with the data is generally within + 0.3% although there are some deviations as high as 1% from the correlated curves.

The vapor pressure of nitrogen calculated above the nitrogen critical temperature represents an extrapolation of the data from below the critical temperature.

TABLE 18

#### CONSTANTS FOR PURE COMPONENT VAPOR PRESSURES

Component	A	B	C	D	Data Source
Nitrogen	25.2115	1598.96	-2.24519	1.5445 x 10 <sup>-15</sup>	This Work
Argon	18.7043	1621.12	-1.12969	0.4132 x 10 <sup>-15</sup>	This Work
Oxygen	21.6017	1781.43	-1.56188	0.4032 x 10 <sup>-15</sup>	8,9,10,11,12

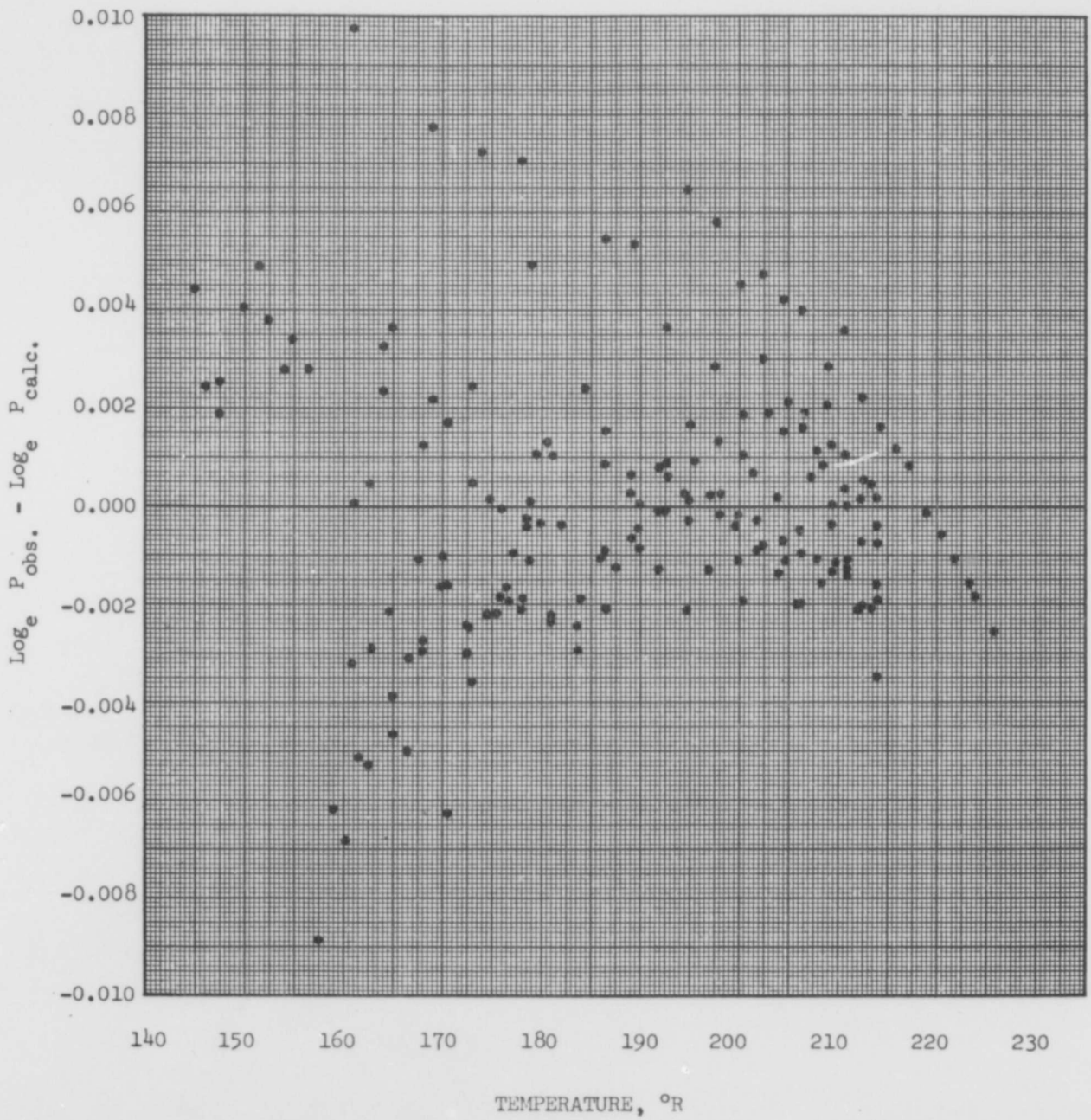


Figure 13. Deviation of APCI Nitrogen Vapor Pressure Data from Riedel Equation.

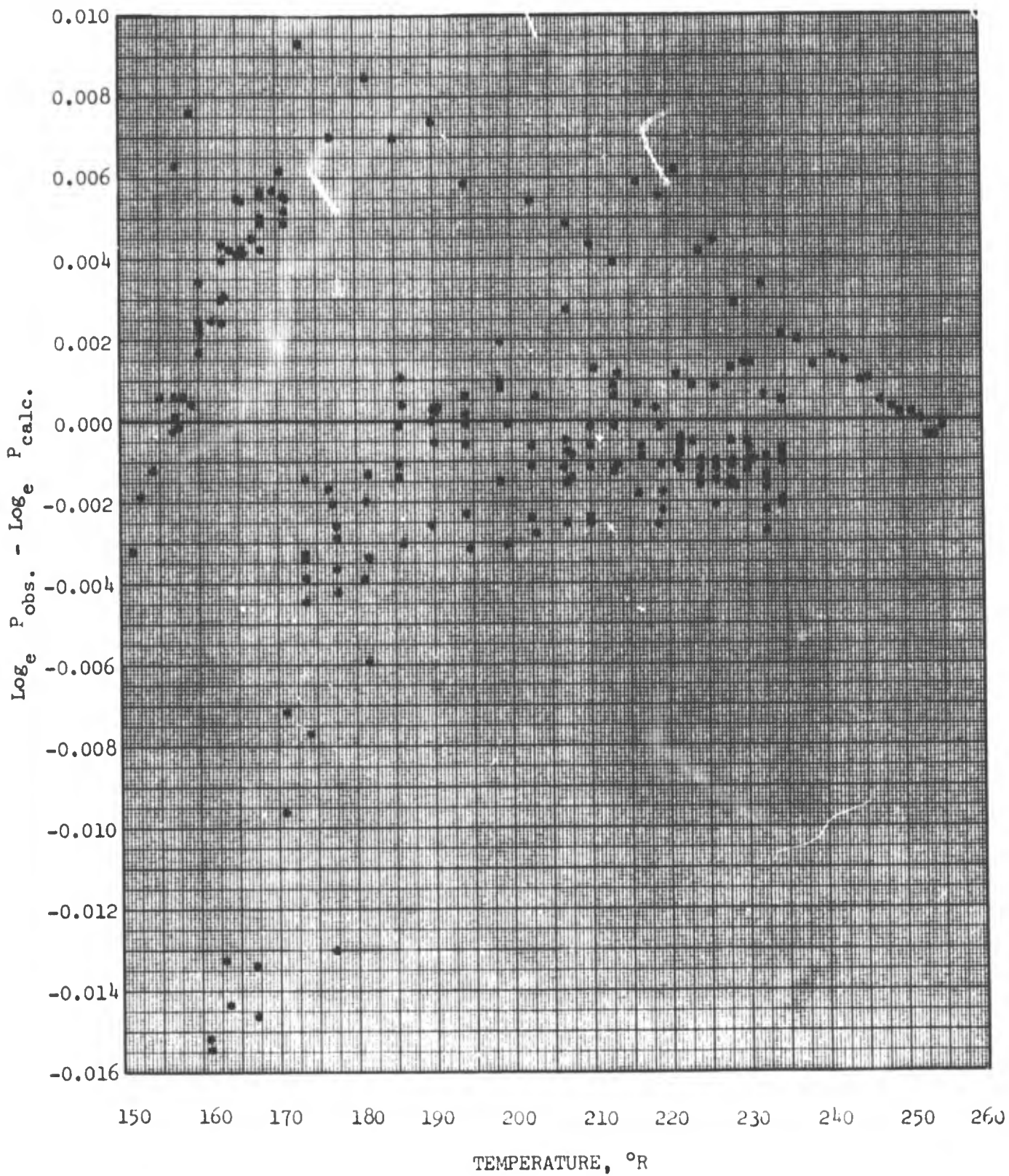


Figure 14. Deviation of APCI Argon Vapor Pressure Data from Riedel Equation.



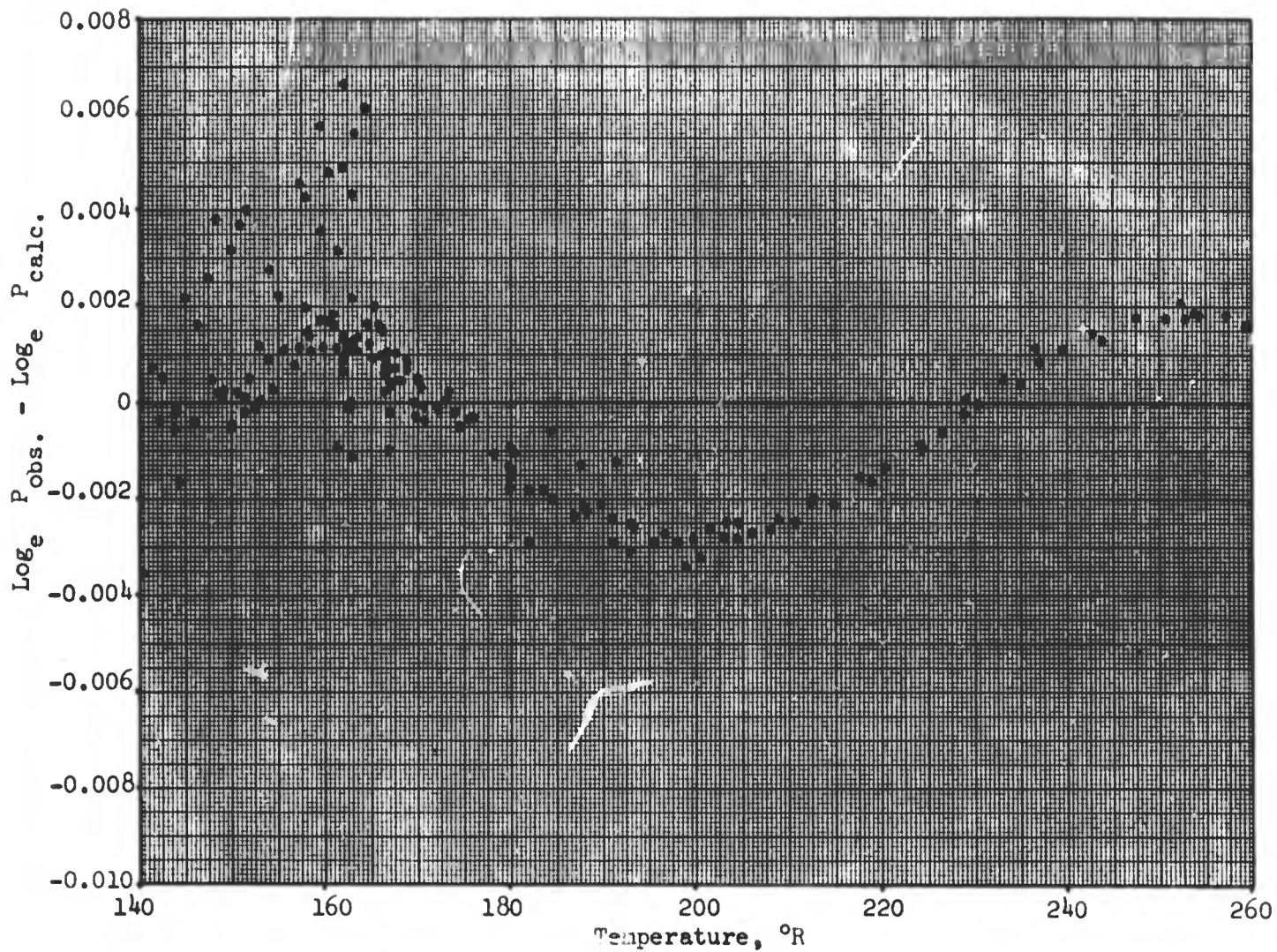


Figure 15. Deviation of Literature Oxygen Vapor Pressure Data from Riedel Equation.

A comparison of vapor pressure data from the literature for nitrogen<sup>(5,8,13,14,15)</sup> and argon<sup>(5,16,17)</sup> is given in Figures 16 and 17. The data for nitrogen deviate systematically about 0.7% from the calculated curve; the vapor pressures from the literature being too high. The data for argon are in good agreement with the correlation at high temperatures but at low temperatures the disagreement is of the order of 1%. These differences were part of the source of difficulty in correlating the data when the equilibrium cell thermocouple was calibrated from these data. This inconsistency then led to the calibration of the thermocouple from the vapor pressure of oxygen alone.

#### D. Fugacity Coefficient

The fugacity coefficient in the vapor phase is calculated from the virial equation of state terminating with the third virial coefficient

$$\frac{pV}{RT} = Z = 1 + \frac{B}{V} + \frac{C}{V^2} \quad (17)$$

The equation for the fugacity coefficient is as follows:

$$\ln \phi_i = \frac{2}{V} \sum_{j=1}^n y_j B_{ij} + \frac{3}{2V^2} \sum_{j=1}^n \sum_{k=1}^n y_j y_k C_{ijk} - \ln Z \quad (18)$$

The cross coefficients  $B_{ij}$  and  $C_{ijk}$  are calculated by methods similar to those presented by Pitzer<sup>(18)</sup> and by Prausnitz<sup>(19)</sup>. The values of the second and third coefficients are given in Tables 19 and 20.

The calculated coefficients for the pure components are in good agreement with literature data<sup>(20,30)</sup> as is indicated in Figures 18, 19, and 20. The third virial coefficient deviates more than does the second; however, an error of  $0.1 \text{ (ft}^3/\text{lb-mole)}^2$  in the third virial coefficient produces a maximum error of only about 0.2% in the calculated fugacity coefficient.

The virial equation terminated at the third virial coefficient deviates negligibly from experimental P-V-T data at densities up to one half the critical density as shown in Figures 21, 22, and 23. At the experimental pressures of measurement the density of the vapor was always less than one half the critical density.

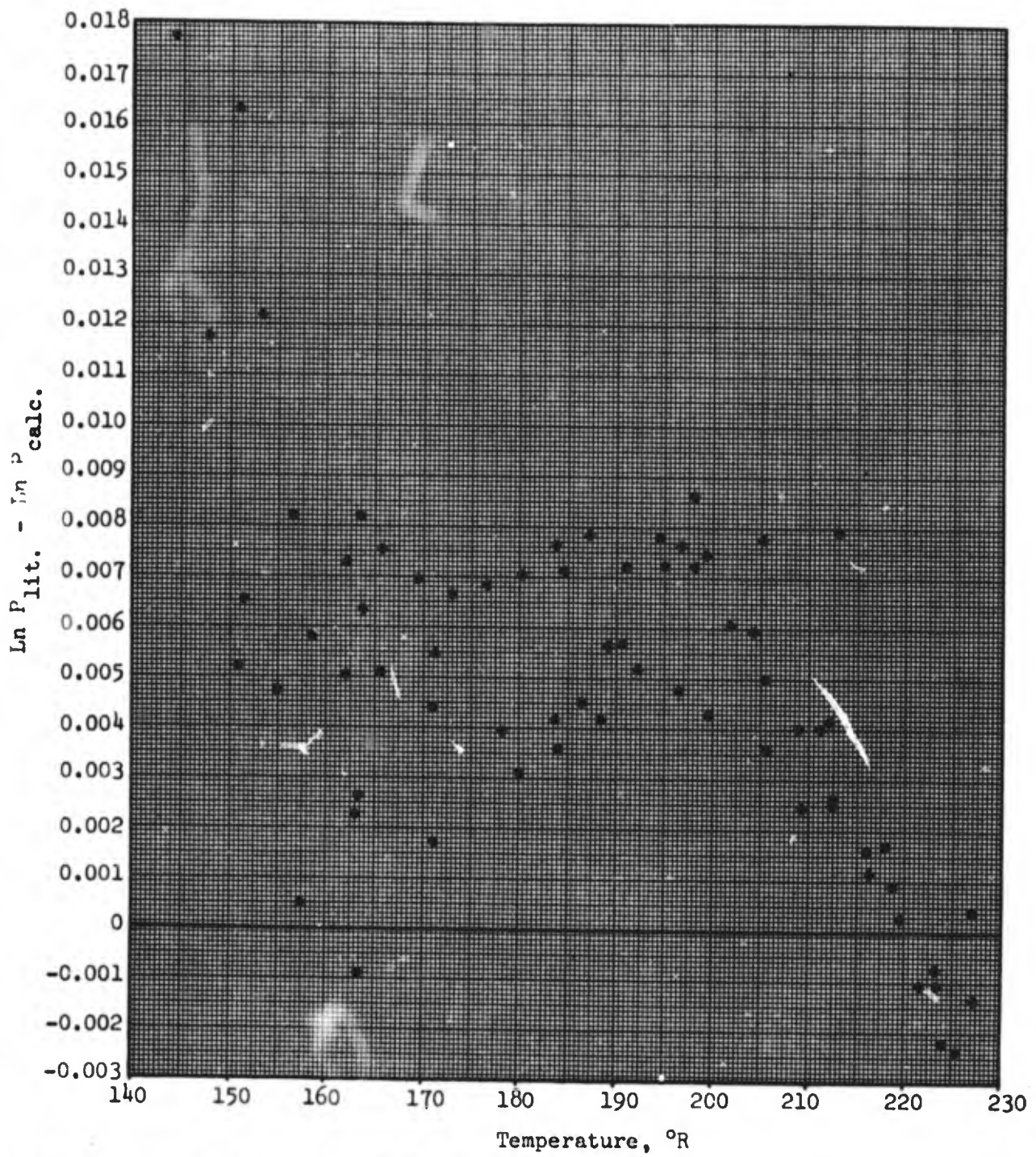


Figure 16. Deviation of Literature Vapor Pressure from APCI Correlation for Nitrogen.

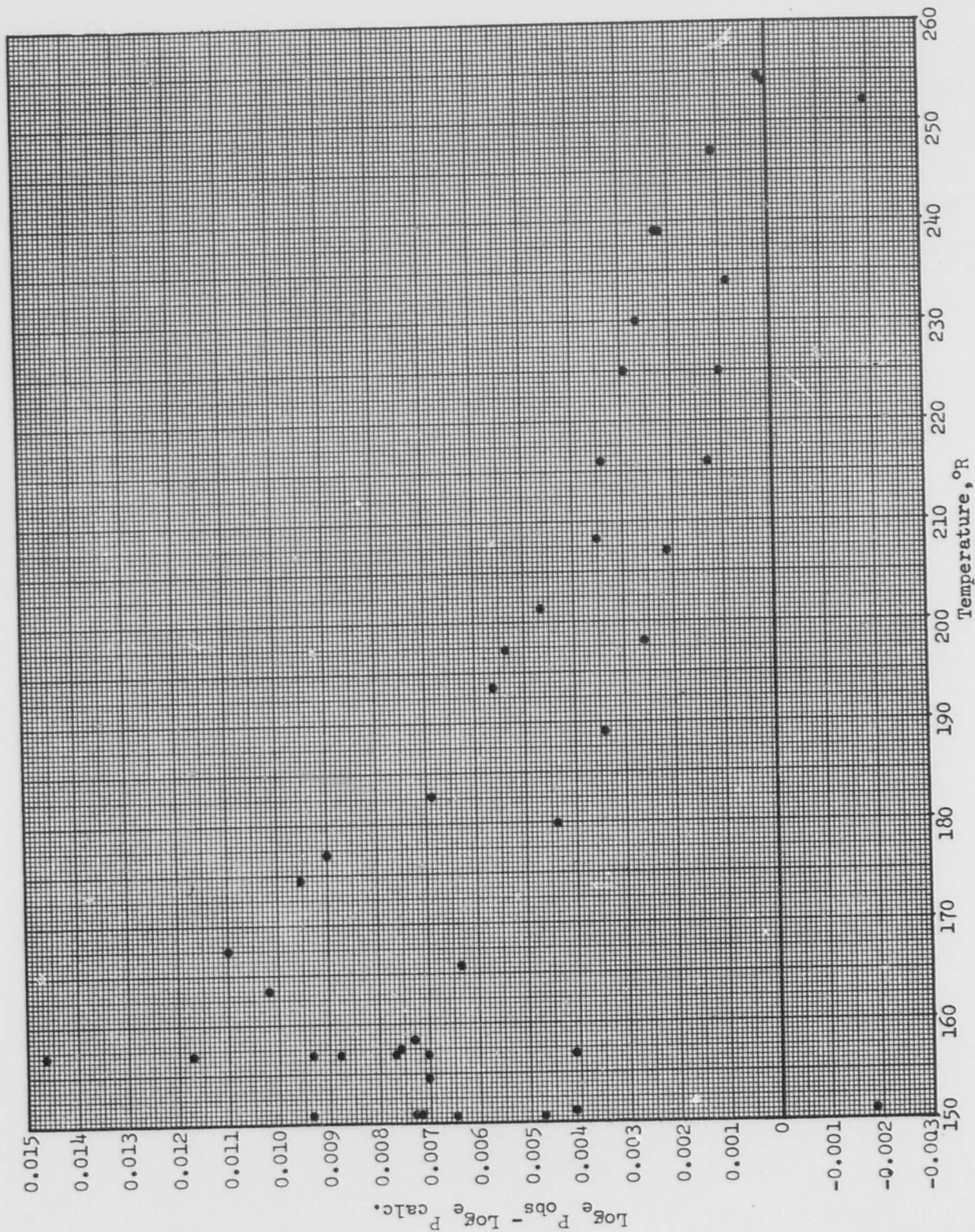


Figure 17. Deviation of Literature Vapor Pressure from APCI correlation for Argon.

TABLE 19

 SECOND VIRIAL COEFFICIENTS USED IN CALCULATIONS  
 Cubic Feet/Pound Mole

Nitrogen = 1, Argon = 2, Oxygen = 3

<u>T, °R</u>	<u>-B<sub>11</sub></u>	<u>-B<sub>12</sub></u>	<u>-B<sub>13</sub></u>	<u>-B<sub>22</sub></u>	<u>-B<sub>23</sub></u>	<u>-B<sub>33</sub></u>
130	4.886	5.063	5.340	5.150	5.484	6.054
140	4.226	4.398	4.595	4.527	4.748	5.154
150	3.703	3.868	4.015	4.014	4.168	4.475
160	3.277	3.435	3.549	3.587	3.699	3.941
170	2.922	3.074	3.165	3.226	3.311	3.508
180	2.623	2.769	2.843	2.918	2.983	3.149
190	2.366	2.507	2.568	2.653	2.704	2.845
200	2.144	2.281	2.331	2.423	2.463	2.585
210	1.951	2.083	2.125	2.221	2.253	2.360
220	1.780	1.909	1.945	2.043	2.069	2.163
230	1.629	1.754	1.784	1.885	1.906	1.990
240	1.494	1.616	1.642	1.744	1.760	1.835
250	1.373	1.493	1.514	1.617	1.630	1.697
260	1.264	1.381	1.400	1.503	1.512	1.574

TABLE 20

THIRD VIRIAL COEFFICIENTS USED IN CALCULATIONS (Cubic Feet/Pound Mole)<sup>2</sup>

Nitrogen = 1, Argon = 2, Oxygen = 3

T, °R	$\underline{C_{111}}$	$\underline{C_{112}}$	$\underline{C_{113}}$	$\underline{C_{122}}$	$\underline{C_{123}}$	$\underline{C_{133}}$	$\underline{C_{222}}$	$\underline{C_{223}}$	$\underline{C_{233}}$	$\underline{C_{333}}$
130	-1.024	-2.175	-2.371	-3.662	-3.927	-4.205	-5.581	-5.933	-6.303	-6.692
140	0.035	-0.685	-0.799	-1.614	-1.770	-1.935	-2.809	-3.020	-3.241	-3.474
150	0.578	0.110	0.043	-0.492	-0.586	-0.685	-1.264	-1.393	-1.529	-1.672
160	0.850	0.533	0.495	0.130	0.073	0.013	-0.386	-0.466	-0.551	-0.640
170	0.974	0.753	0.731	0.473	0.439	0.403	0.117	0.067	0.015	-0.041
180	1.018	0.858	0.847	0.657	0.638	0.617	0.405	0.374	0.342	0.307
190	1.019	0.898	0.894	0.750	0.740	0.728	0.566	0.547	0.527	0.506
200	0.995	0.902	0.902	0.789	0.785	0.779	0.651	0.640	0.629	0.616
210	0.960	0.885	0.888	0.797	0.796	0.795	0.690	0.684	0.679	0.672
220	0.919	0.857	0.862	0.786	0.788	0.789	0.701	0.699	0.697	0.695
230	0.877	0.824	0.830	0.765	0.768	0.771	0.695	0.696	0.697	0.697
240	0.835	0.789	0.795	0.738	0.743	0.747	0.680	0.683	0.685	0.687
250	0.795	0.754	0.760	0.709	0.714	0.719	0.660	0.663	0.667	0.670
260	0.757	0.719	0.726	0.679	0.685	0.691	0.636	0.641	0.645	0.649

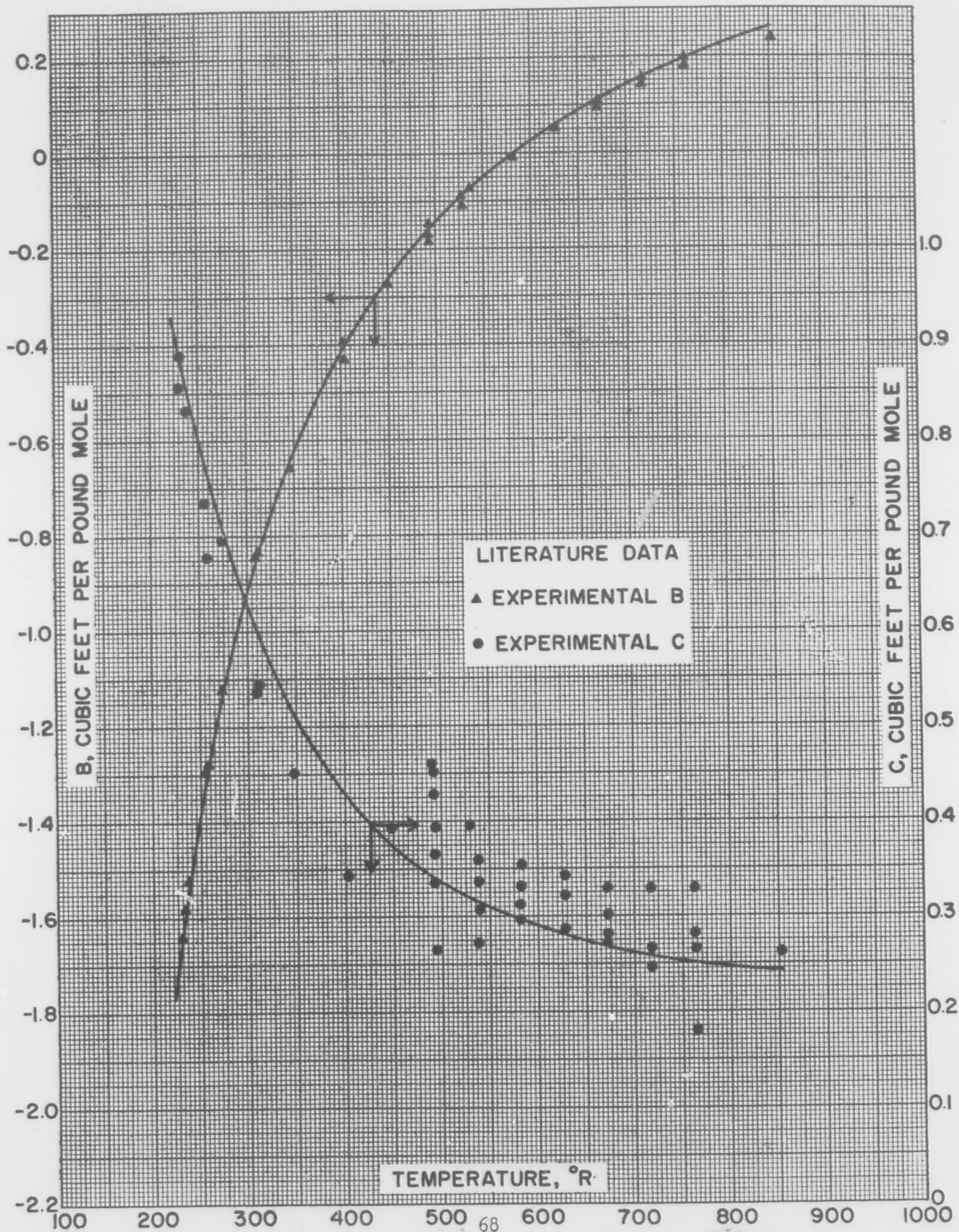


Figure 18. Calculated Second and Third Virial Coefficients, B and C, for Nitrogen.

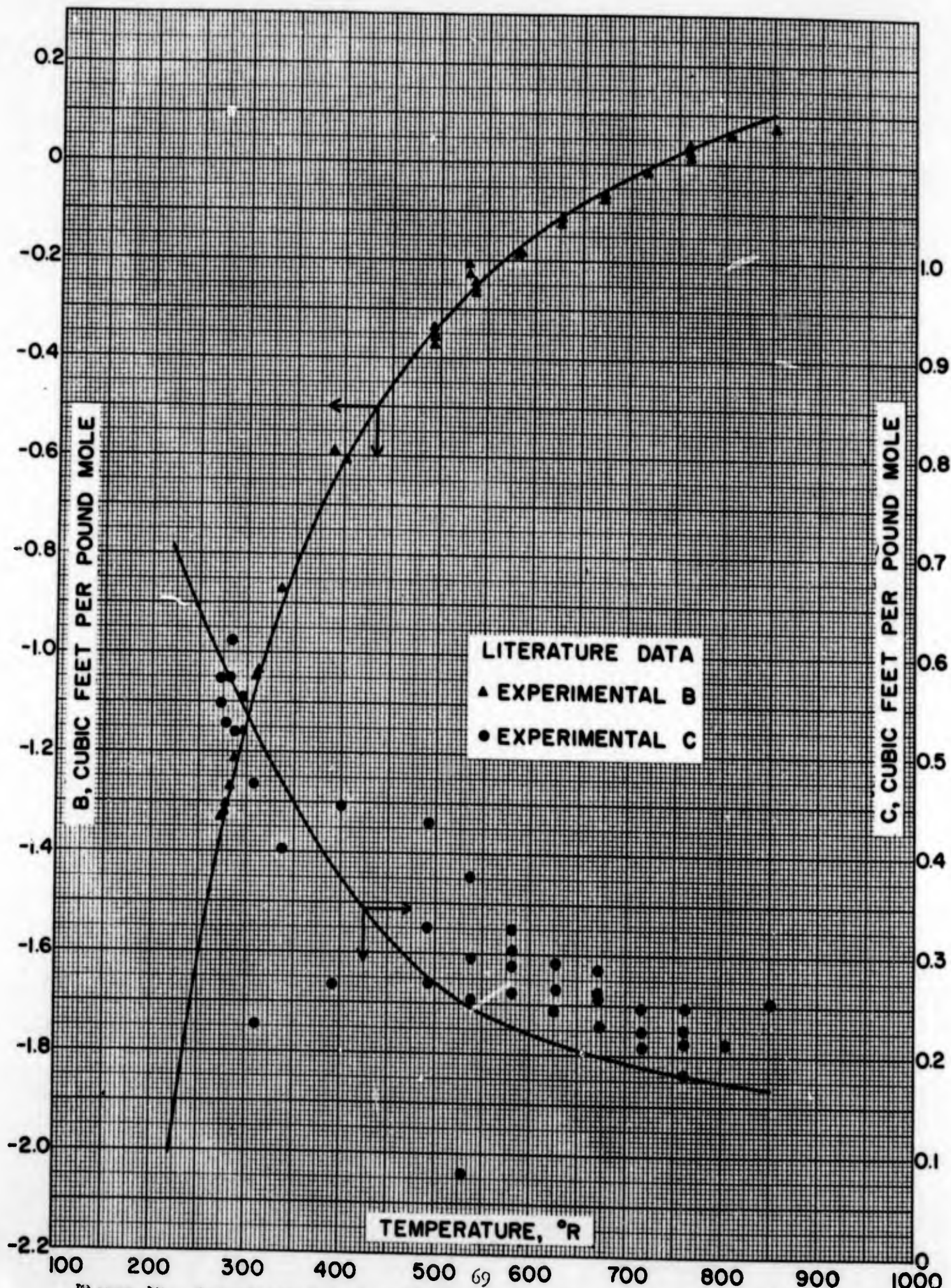


Figure 19. Calculated Second and Third Virial Coefficients, B and C, for Argon.



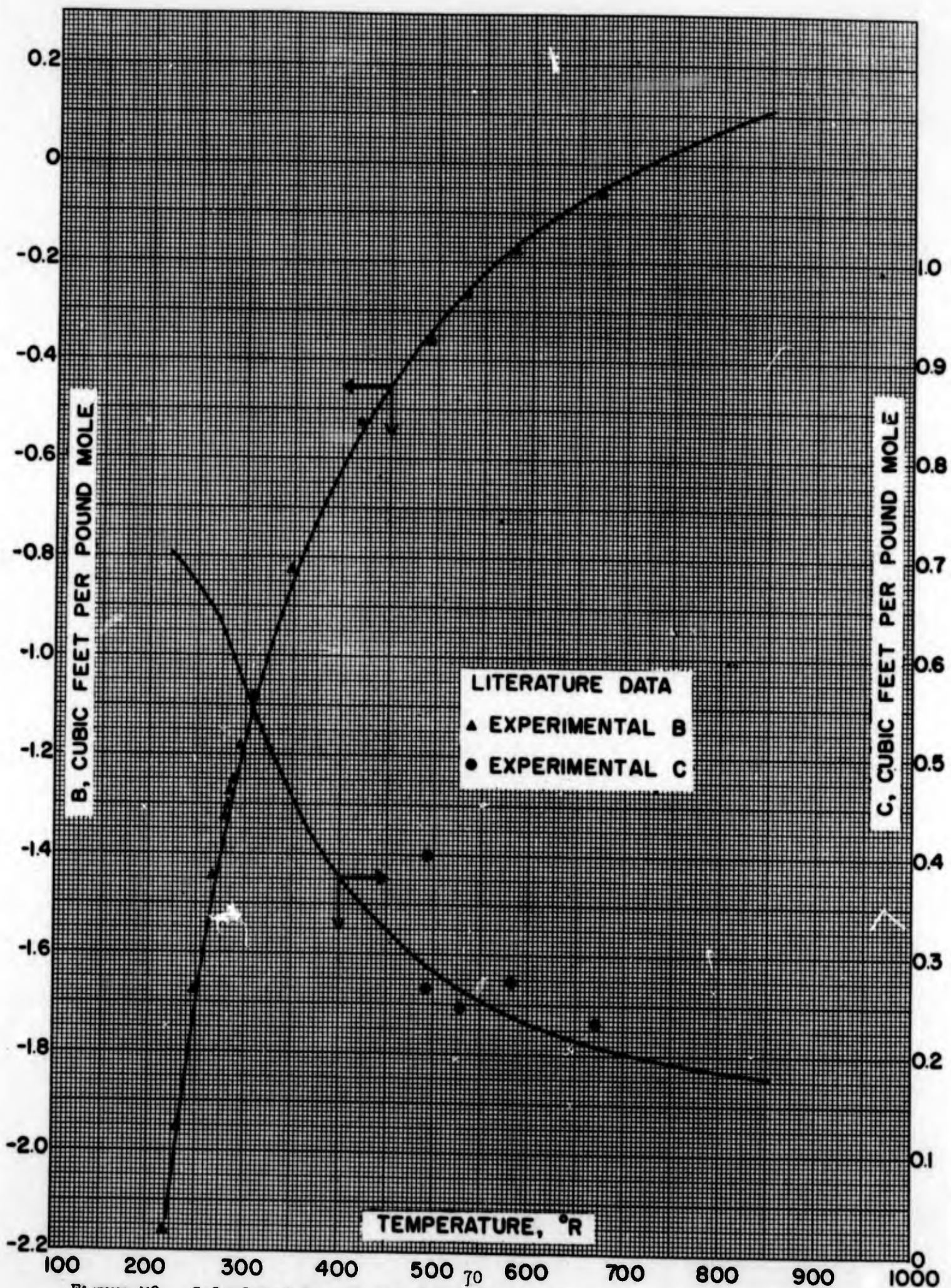


Figure 20. Calculated Second and Third Virial Coefficient, B and C, for Oxygen.

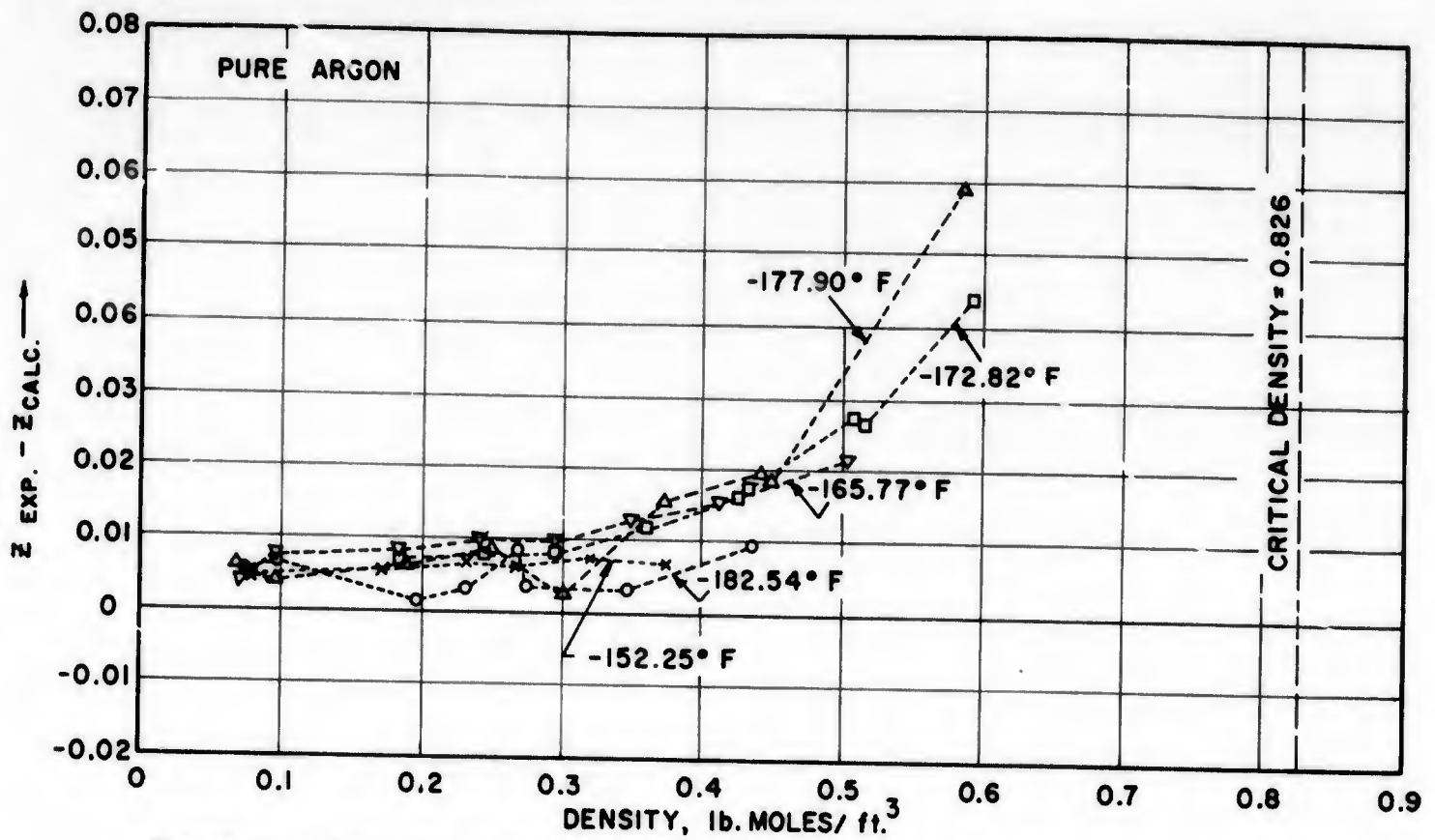


Figure 21. Comparison of Calculated and Experimental Compressibility Data, Argon.

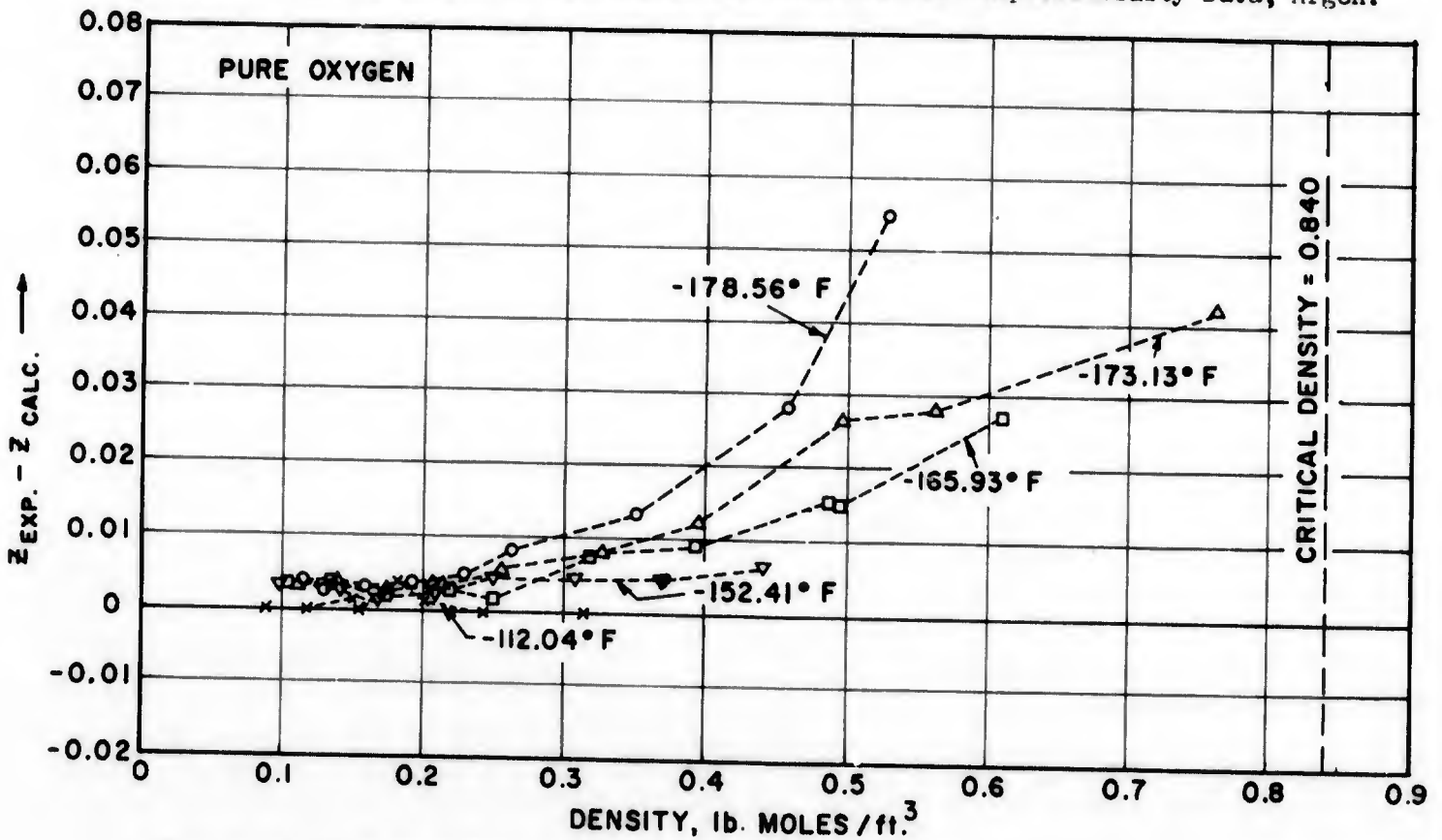


Figure 22. Comparison of Calculated and Experimental Compressibility Data, Oxygen.

Knobler and co-workers<sup>(31)</sup> have measured the cross coefficients of argon-oxygen, oxygen-nitrogen, and nitrogen-argon at 90°K. These data are shown in Figure 24 plotted along with the calculated curves. No other cross coefficient data were found.

Keunen, Virschoye and Van Urk<sup>(32)</sup> have measured the compressibility of two oxygen-nitrogen mixtures and Penning<sup>(33)</sup> has made measurements on air. Deviations in compressibility are shown plotted in Figures 25 and 26 where the difference is small as in the case of the pure components.

In view of these comparisons it is felt that the virial equation and the virial coefficients are within the experimental range of accuracy of existing P-V-T data and holds for mixtures as well as for pure components. The deviation in compressibility factor is of the order of 0.005 which probably corresponds to the uncertainty in the fugacity coefficient.

#### E. Activity Coefficient Equation

The liquid activity coefficient data calculated from the experimental data were correlated by means of the Van Laar equation. In a binary mixture it may be written as

$$\ln \gamma_1 = S_1 \left[ \frac{S_2 x_2}{S_1 x_1 + S_2 x_2} \right]^2 A_{12} \quad (19)$$

or in a multicomponent mixture as

$$\ln \gamma_i = S_i \left[ \sum_{j=1}^n \theta_j A_{i,j} - \frac{1}{2} \sum_{j=1}^n \sum_{k=1}^n \theta_j \theta_k A_{jk} \right] \quad (20)$$

where  $\theta_j = \frac{S_j x_j}{\sum_{k=1}^n S_k x_k}$

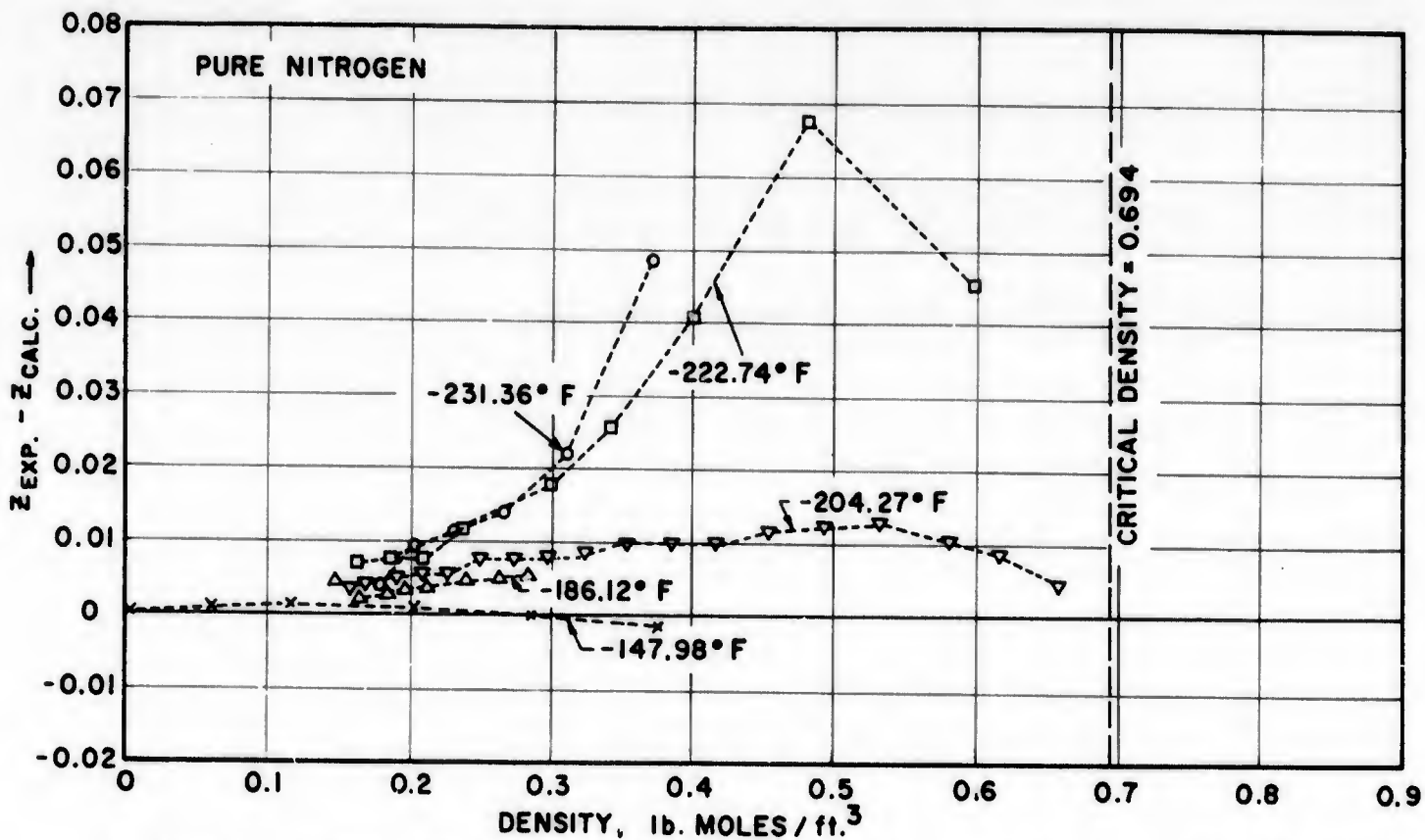


Figure 23. Comparison of Calculated and Experimental Compressibility Data, Nitrogen.

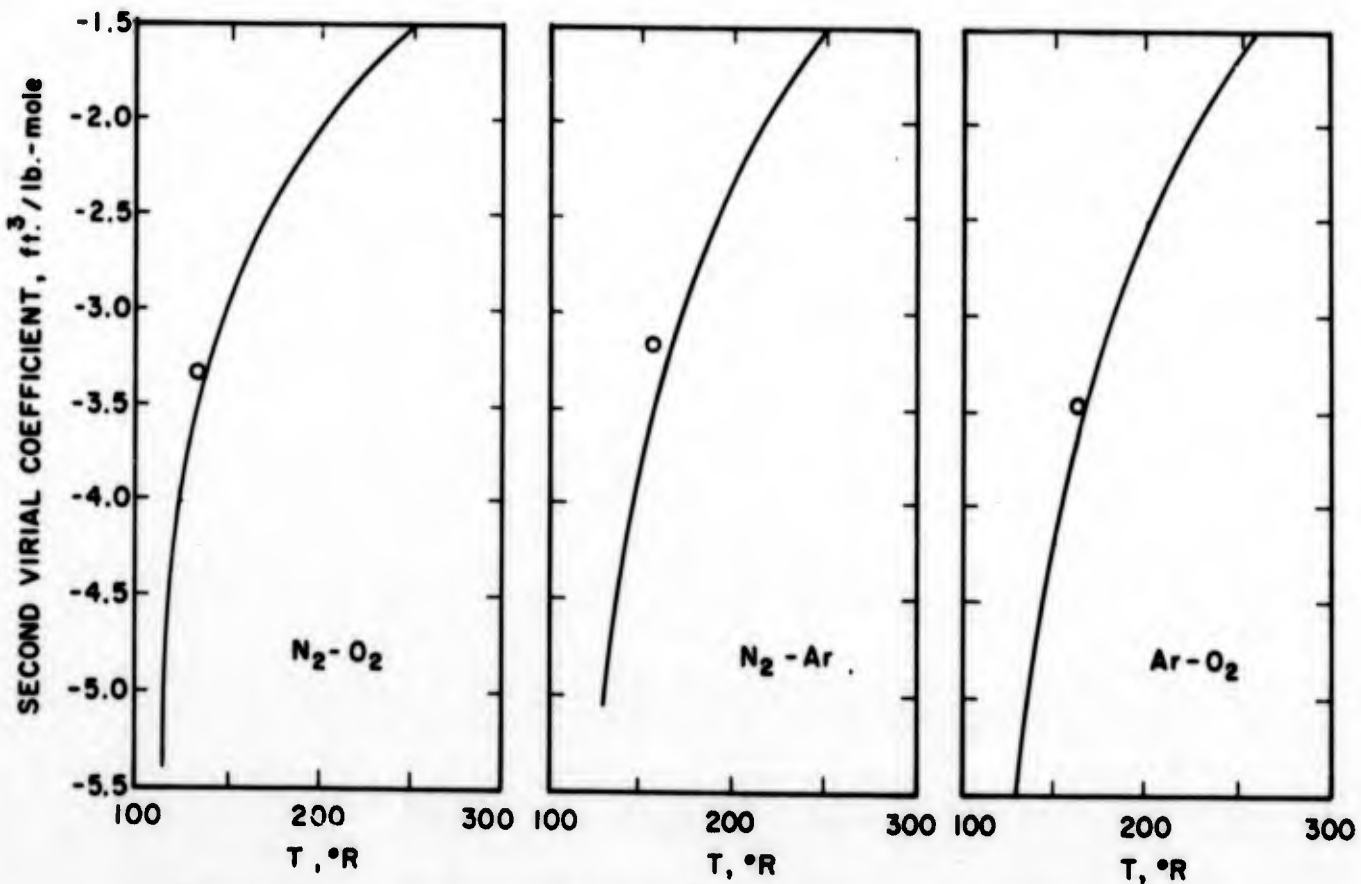


Figure 24. Comparison of Calculated and Experimental Cross Coefficients.

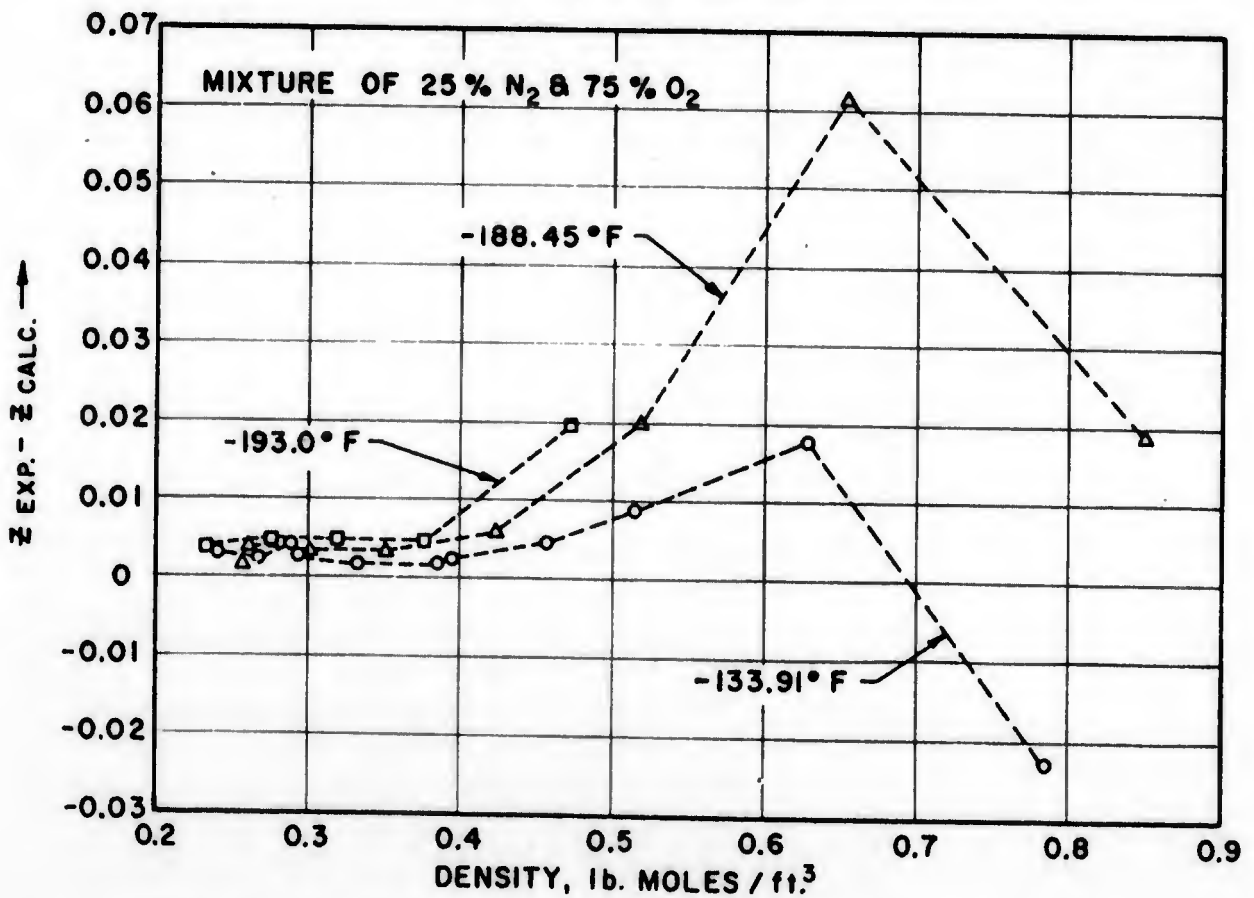
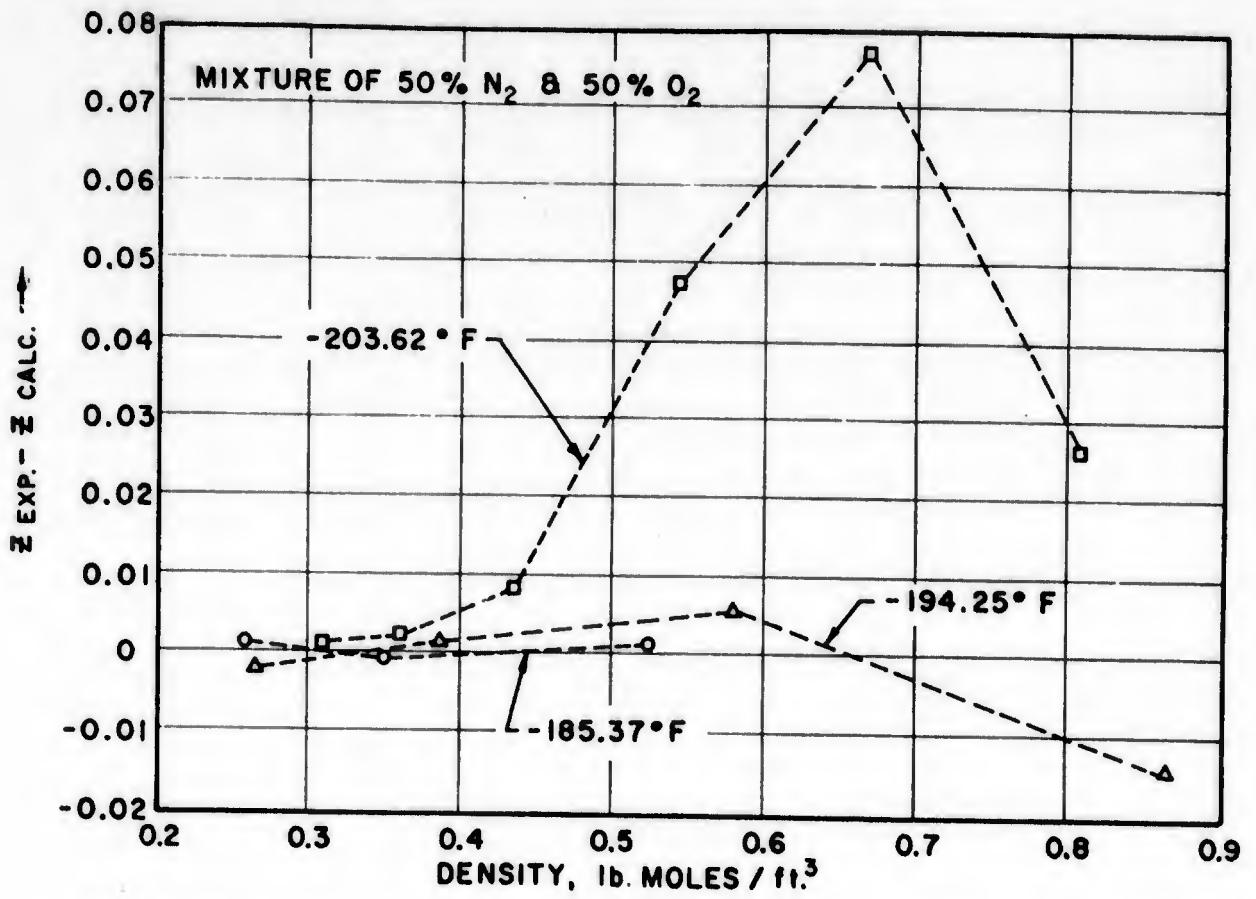


Figure 25. Comparison of Calculated and Experimental Compressibility Data, Nitrogen-Oxygen Mixture.

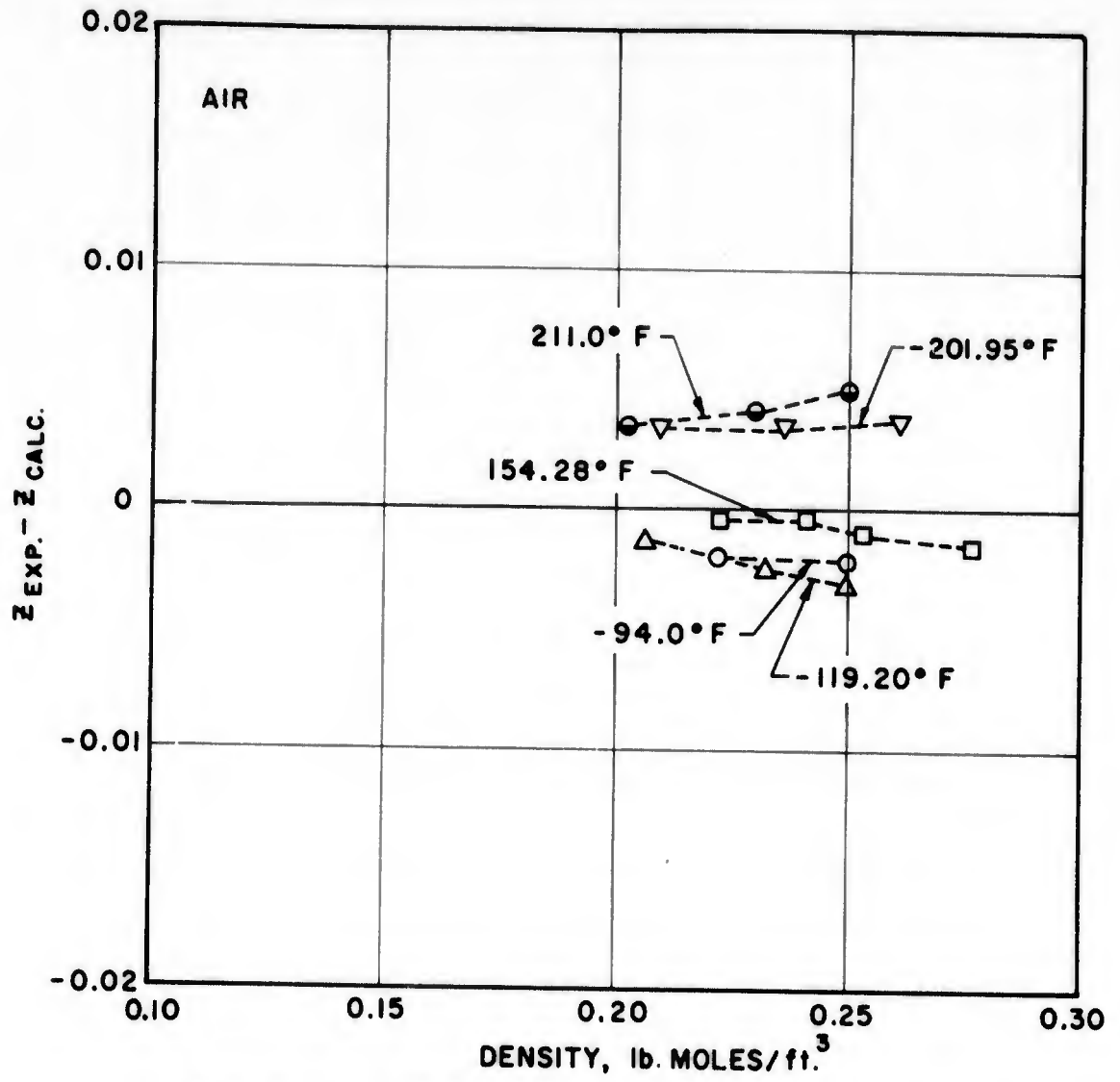


Figure 26. Comparison of Calculated and Experimental Compressibility Data, Air.

The interaction coefficients  $A_{ij}$  were assumed to be temperature dependent according to the relation

$$A_{ij} = a_{ij} + b_{ij}/T \quad (21)$$

The constants in the Van Laar equation were determined by a least squares fit to the entire set of vapor-liquid equilibrium data. The constants obtained are given in Table 21. A discussion of the correlation and comparisons with data are given in the following section.

TABLE 21  
VAN LAAR CONSTANTS FOR NITROGEN-ARGON-OXYGEN  
ACTIVITY COEFFICIENTS IN THE LIQUID PHASE

Component	Van Laar Volume	$a_{ij}$			$b_{ij}$		
		N <sub>2</sub>	Ar	O <sub>2</sub>	N <sub>2</sub>	Ar	O <sub>2</sub>
Nitrogen	1.00	0	-.1515	-.0669	0	51.8	43.9
Argon	1.00	-.1515	0	-.0837	51.8	0	40.7
Oxygen	1.00	-.0669	-.0837	0	43.9	40.7	0

## VII. COMPARISON OF CORRELATION TO DATA

The experimental vapor-liquid equilibrium data were fitted by the method of least squares to the constants in the logarithm of the activity coefficient of each component. By this method a single vapor-liquid equilibrium point provided two activity coefficient points in a binary mixture and three points in a ternary mixture. With 1962 equilibrium points this produced 5344 activity coefficient points, requiring considerable running time on the computer each time a least squares analysis was made. Each experimental point was weighted equally because equal weight seems as logical for this set of data as other methods of weighting. If the Gibbs free energy of mixing had been fitted, it would have been more logical to weight the data differently because data at low concentrations of a component would not receive sufficient weight.

A summary of the various least square analysis runs made on the computer is given in Table 22, where the curve-fit number is in the chronological order of the analysis made. Runs 1, 2, 3, and 4 show that it makes little difference in the RMS error whether the three binaries are assumed to be symmetrical or unsymmetrical in the activity coefficient. Runs 5 and 6 are equivalent to Runs 4 and 1 respectively, except that points deviating more than three times the RMS error were deleted. The percentage of points deleted was five times the theoretical number of 0.3% based on a random error distribution, and the RMS error was reduced approximately 50%--38 times the theoretical value of 1.3%--justifying the deletion of the points. Runs 5 and 6 show that it makes little difference in the RMS error whether the constants  $a_{ij}$  are set to zero or not; the error only increasing from .0235 to .0261. Because of this insensitivity, the constants  $b_{ij}$  have been fixed consistent with heat of mixing data from the literature and the coefficients  $a_{ij}$  have been adjusted to fit the activity coefficient data. Runs 7 and 8 correspond to this restriction, however, it was found that there was a systematic bias in the correlation due to errors in the vapor pressures of the pure components.

This bias is shown in Table 23 where there were 1517 nitrogen points in Run 8 with positive deviation compared with only 229 points with negative deviation. An examination of the data showed that the correlation could be improved if the vapor pressures of the pure components were adjusted slightly. An adjustment of the data was made by the use of vapor pressure data measured under the present project in place of data reported in the literature as described in Section III-G. The results of the adjustment are shown as the difference between Runs 8 and 10 in Tables 22 and 23. The RMS error dropped slightly and the number of positive and negative deviations became more nearly the same.



TABLE 22

## CONSTANTS AND ROOT MEAN SQUARE ERROR OF VARIOUS CURVE-FITS

Constant	Curve-Fit Number									
	1	2	3	4	5	6	7	8	9	10
$S_{N_2}$	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
$S_{Ar}$	1.0	.9743*	.9743	1.0	1.0	1.0	1.0	1.0	1.0	1.0
$S_{O_2}$	1.0	.9469*	.9469	1.0	1.0	1.0	1.0	1.0	1.0	1.0
$a_{N_2-Ar}$	0.0	0.0	.0696*	.0698*	.1237*	0.0	-.1415*	-.1397*	-.1555*	-.1515*
$b_{N_2-Ar}$	24.54*	24.54	11.61*	11.16*	1.01*	24.60*	51.8	51.8	51.8	51.8
$a_{N_2-O_2}$	0.0	0.0	.1849*	.1818*	.2191*	0.0	-.0432*	-.0439*	-.0653*	-.0669*
$b_{N_2-O_2}$	34.81*	34.81	-.60*	0.0*	-7.74*	34.51*	43.9	43.9	43.9	43.9
$a_{Ar-O_2}$	0.0	0.0	-.1096*	-.1046*	-.0984*	0.0	-.0864*	-.0893*	-.0808*	-.0837*
$b_{Ar-O_2}$	23.31*	23.31	46.45*	44.47*	42.64*	22.78*	40.7	40.7	40.7	40.7
RMS Error	.0456	.0455	.0444	.0445	.0235	.0261	.0466	.0284	.0431	.0250
Points Deleted	0	0	0	0	87	86	0	81	0	92

\*Coefficient Varied in That Run

TABLE 23

 SUMMARY OF POSITIVE AND NEGATIVE  
 DEVIATIONS OF EXPERIMENTAL POINTS FROM CORRELATION

Run No.	Nitrogen		Argon		Oxygen	
	Plus	Minus	Plus	Minus	Plus	Minus
8	1517	229	829	935	533	1201
10	1135	614	1024	733	570	1176

Run 10 has been adopted as the final correlation although there still remain systematic deviations in the data as shown in Figures 27 to 31. The various regions designated in these figures correspond to the following:

Region I, nitrogen mole fraction greater than 0.5

Region II, argon mole fraction greater than 0.5

Region III, oxygen mole fraction greater than 0.5

Region IV, mole fraction of all three components less than 0.5.

These figures indicate systematic deviations at low temperatures; a relatively even distribution at between 170 and 180°R; systematic deviations between 190 and 210°R; a relatively even distribution between 220 and 230°R; and systematic deviations above 230°R. This pattern exists somewhat independent of the region examined, but is most predominant in Regions II, III, and IV.

A comparison of calculated vs. measured activity coefficients in each of the binaries are presented in Figures 32 to 45. The data were divided into approximately 20°R intervals and plotted on separate graphs. The solid lines represent the calculated activity coefficient at the two extremes of temperature. In this comparison the same systematic deviation is observed as in Figures 27 to 31 for the nitrogen-oxygen and nitrogen-argon system, the largest systematic error being approximately 2.5% in the nitrogen-argon system. The oxygen-argon system seems to show no systematic deviations.

A comparison of calculated and measured equilibria in the binary and ternary systems is given in Figures 46 to 82 which show tie lines in a ternary phase diagram at constant temperature and pressure. The figures are ordered

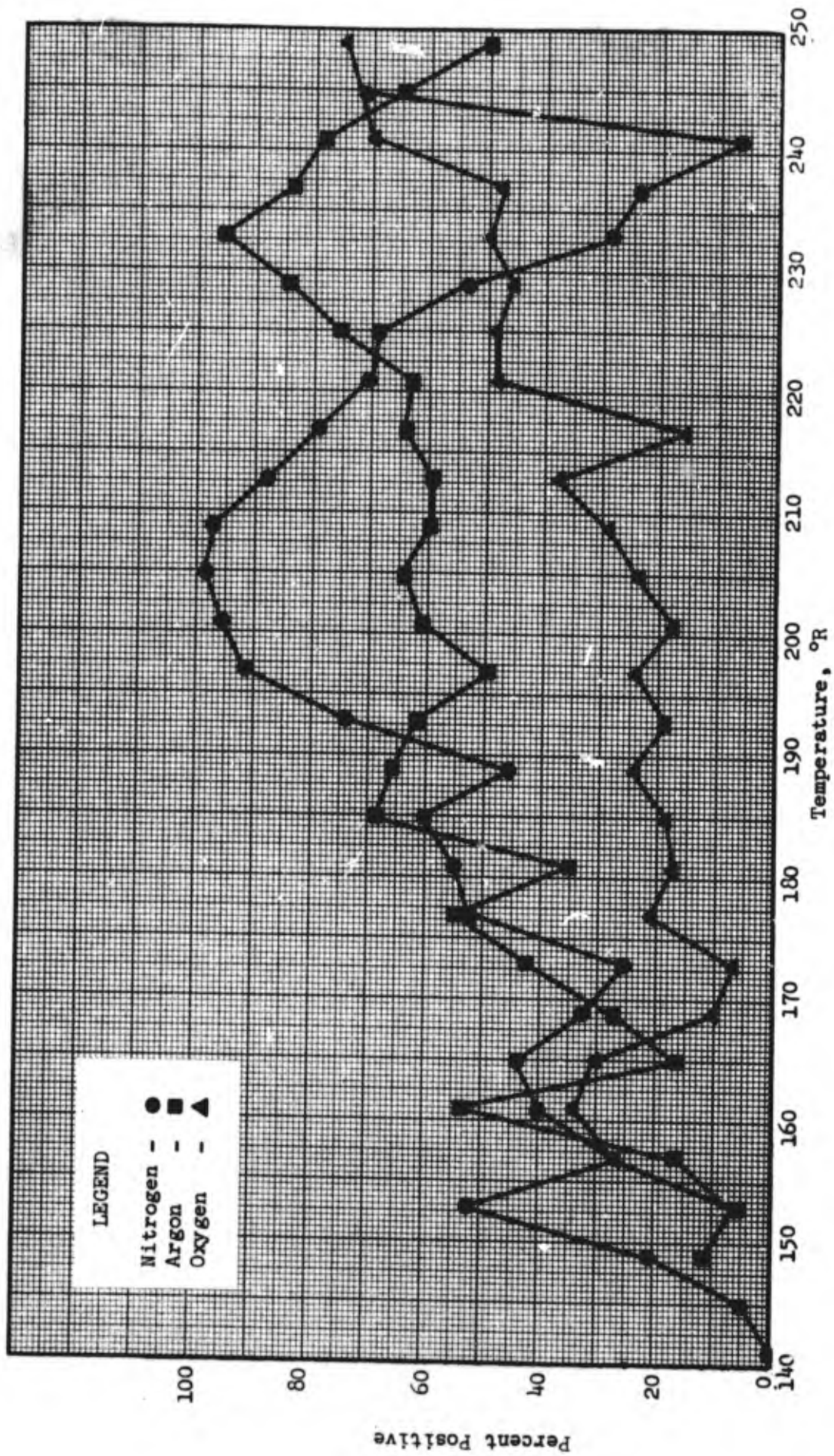


Figure 27. Summary of Bias of Points in Region I.

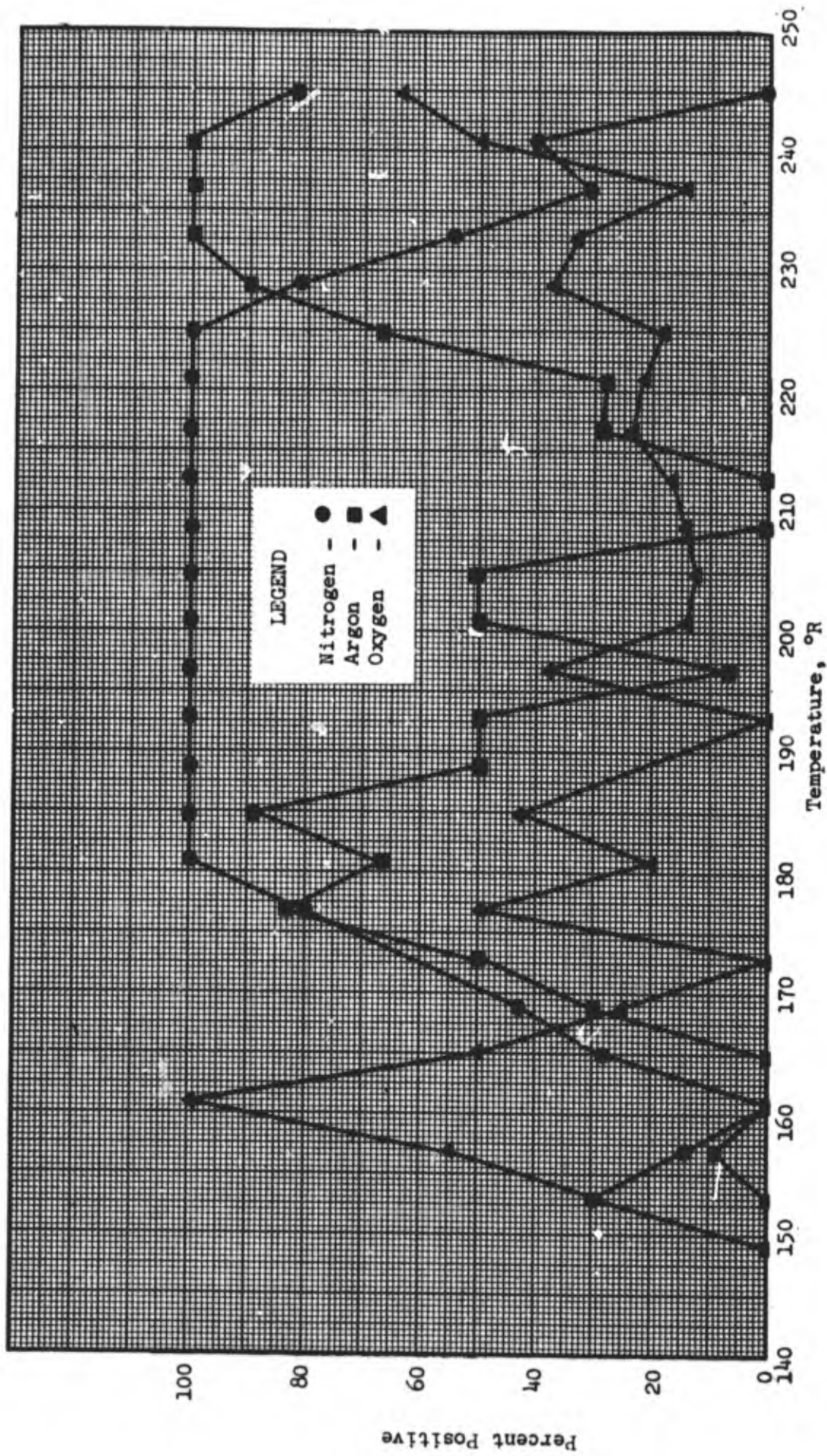


Figure 28. Summary of Bias of Points in Region II.

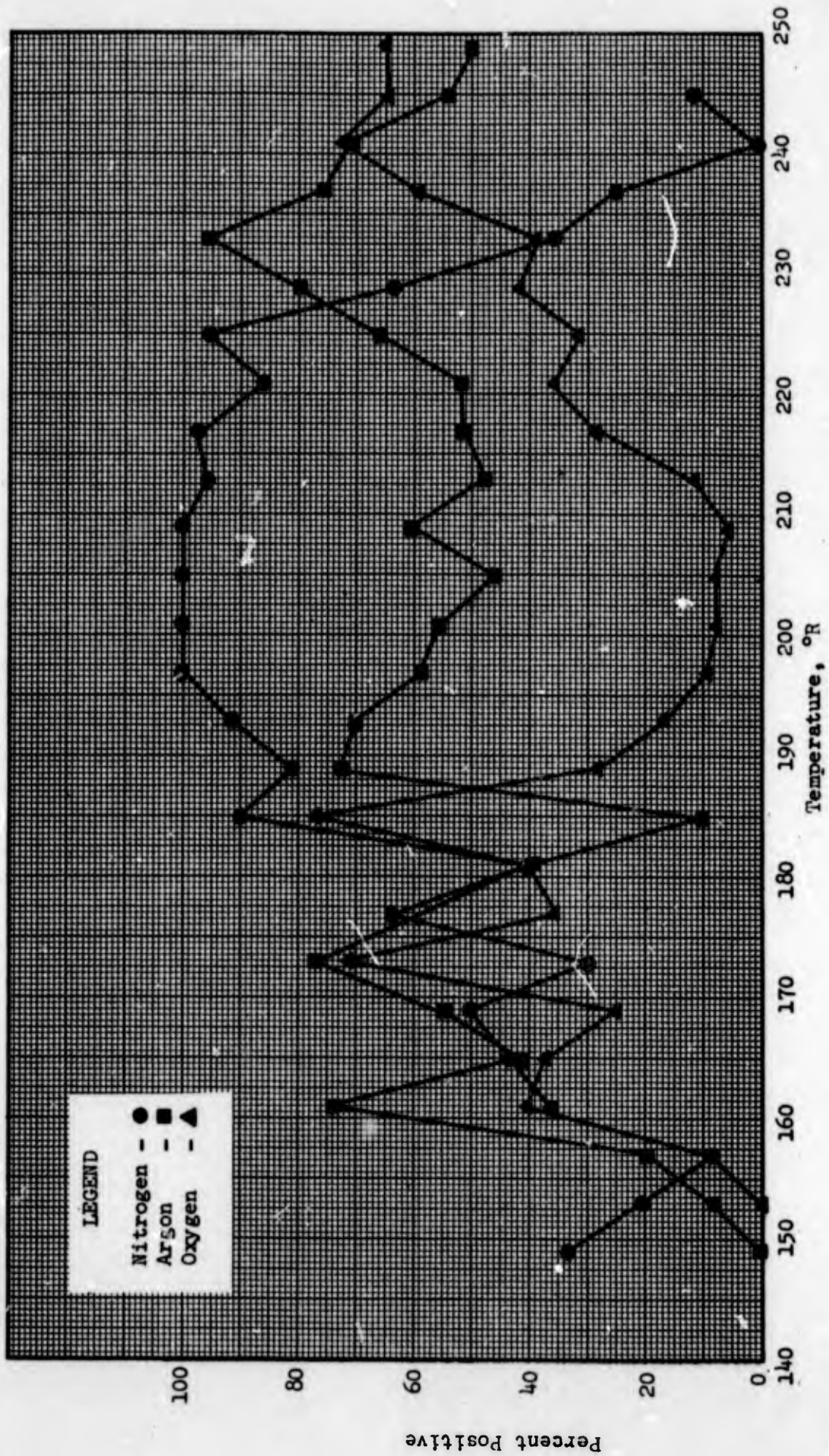


Figure 29. Summary of Bias of Points in Region III.

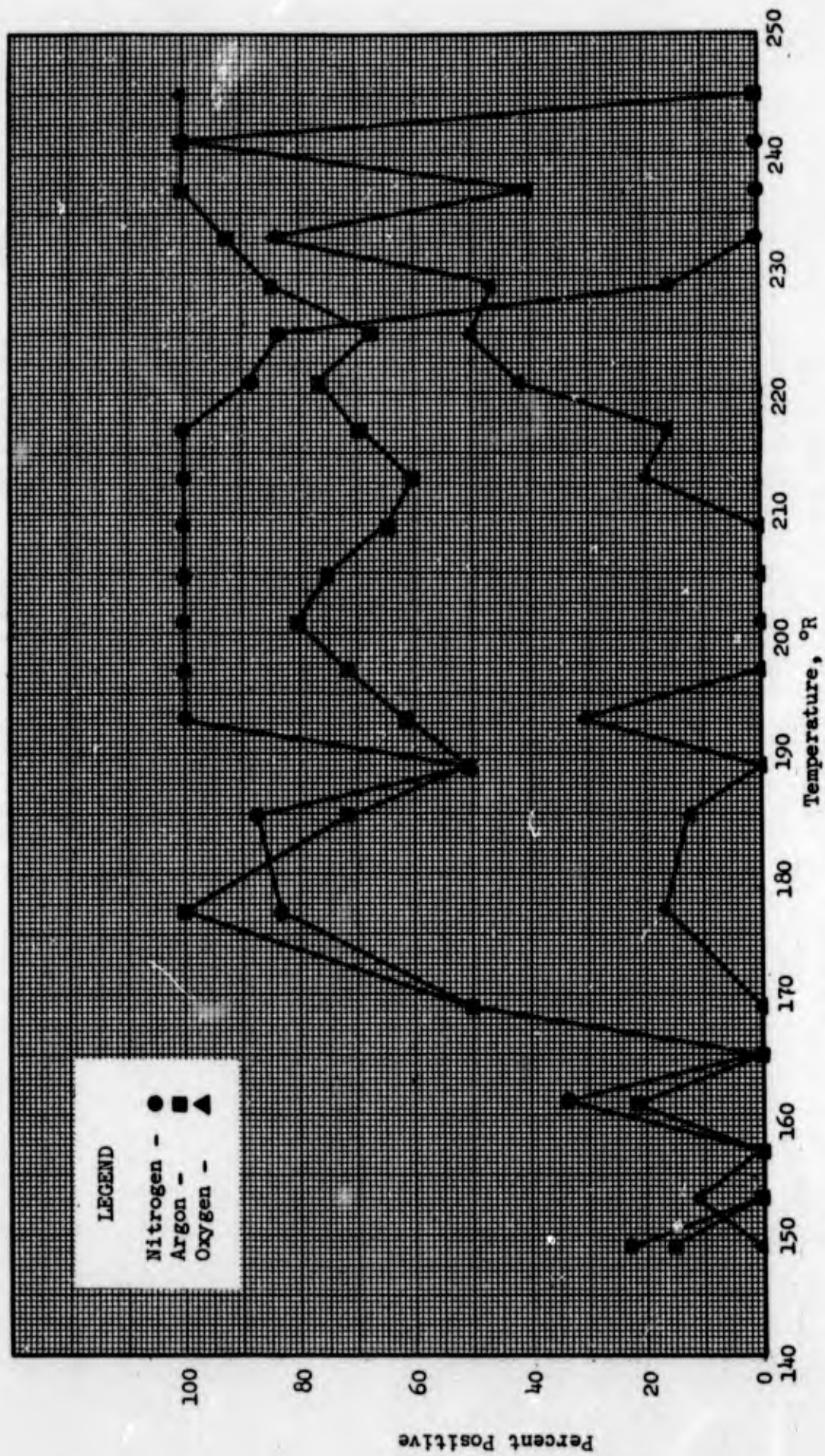


Figure 30. Summary of Bias of Points in Region IV.

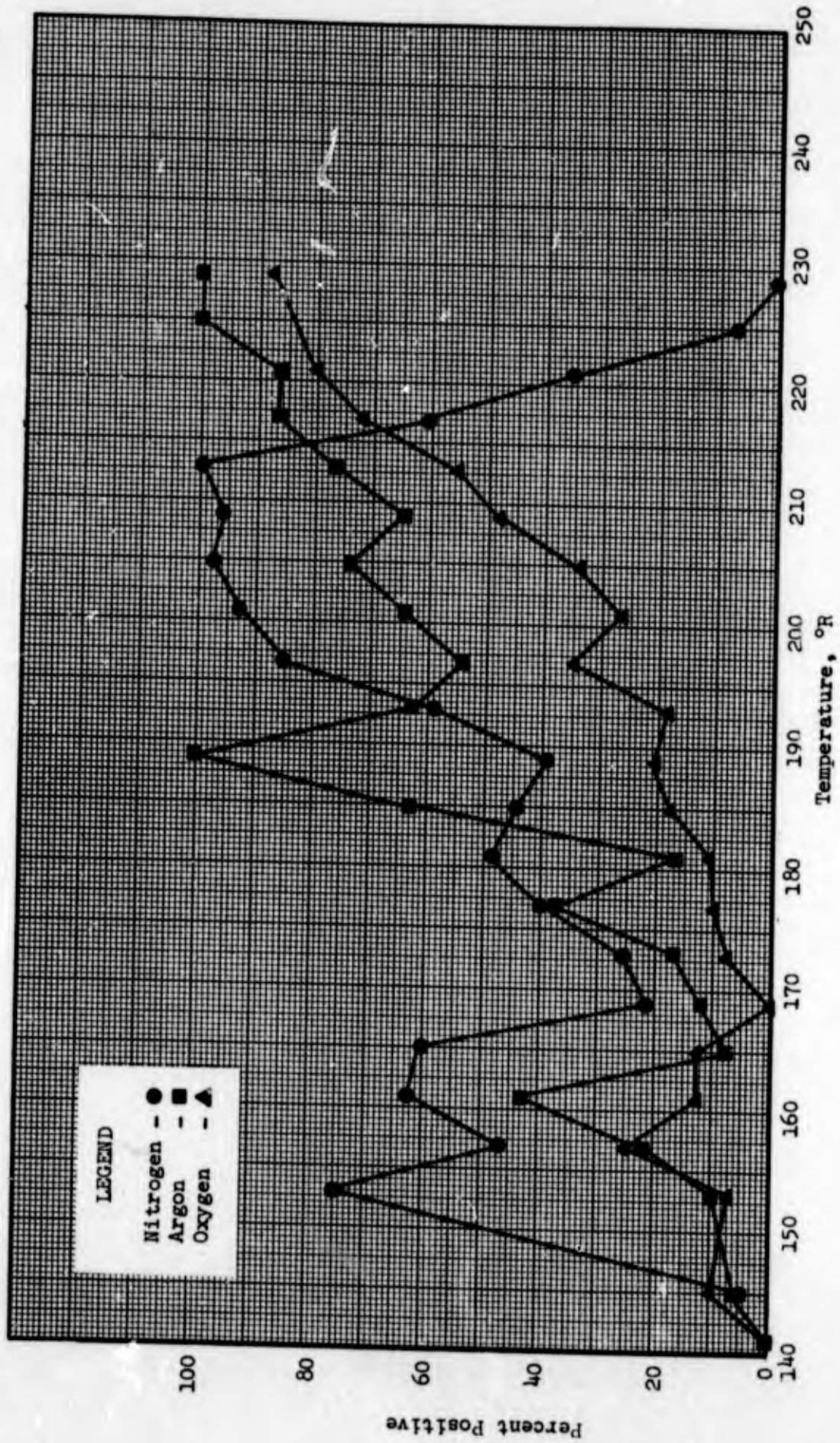


Figure 31. Summary of Bias of Points in all Regions.

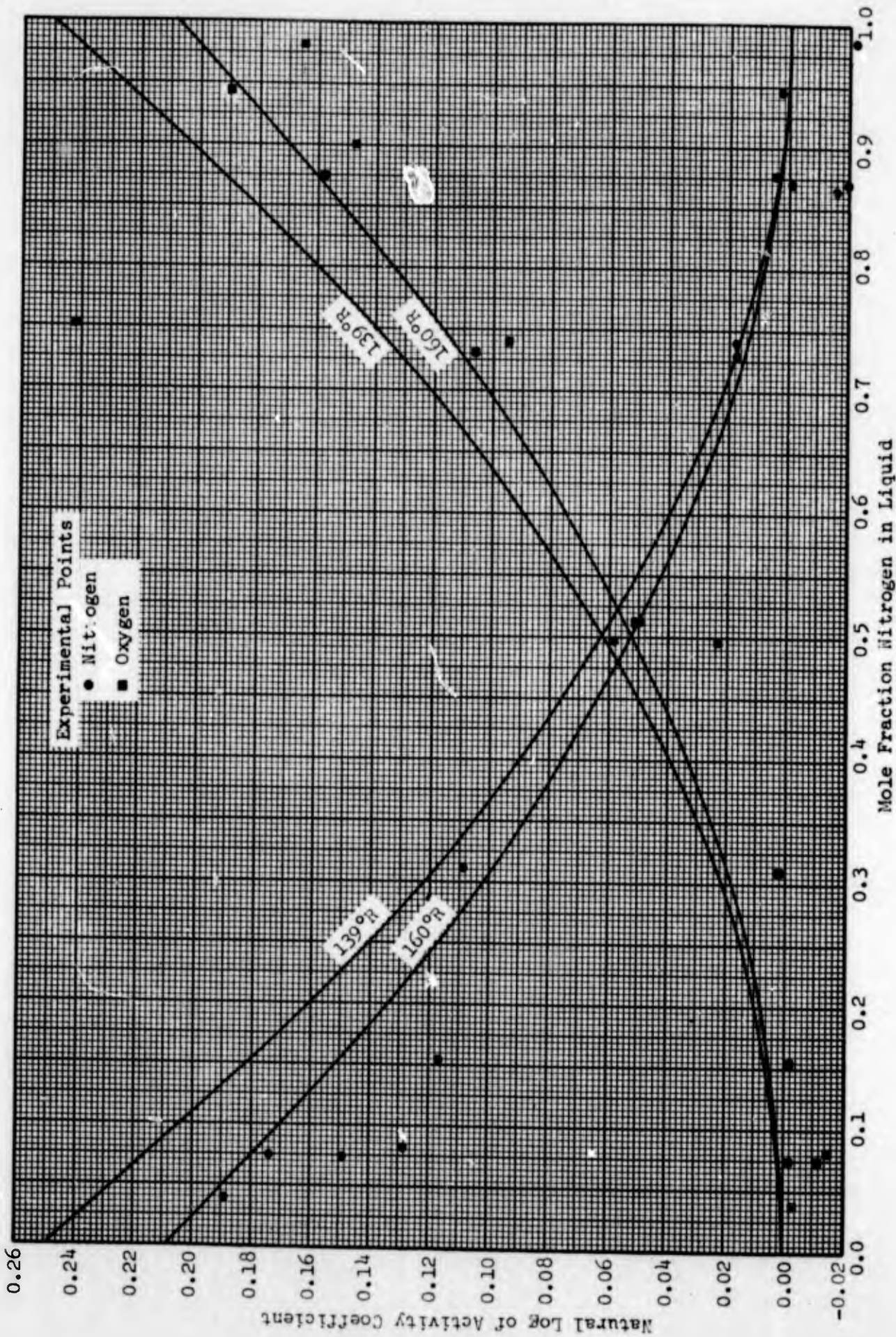


Figure 32. Activity Coefficients in the Nitrogen-Oxygen Binary System, Calculated vs. Experimental.



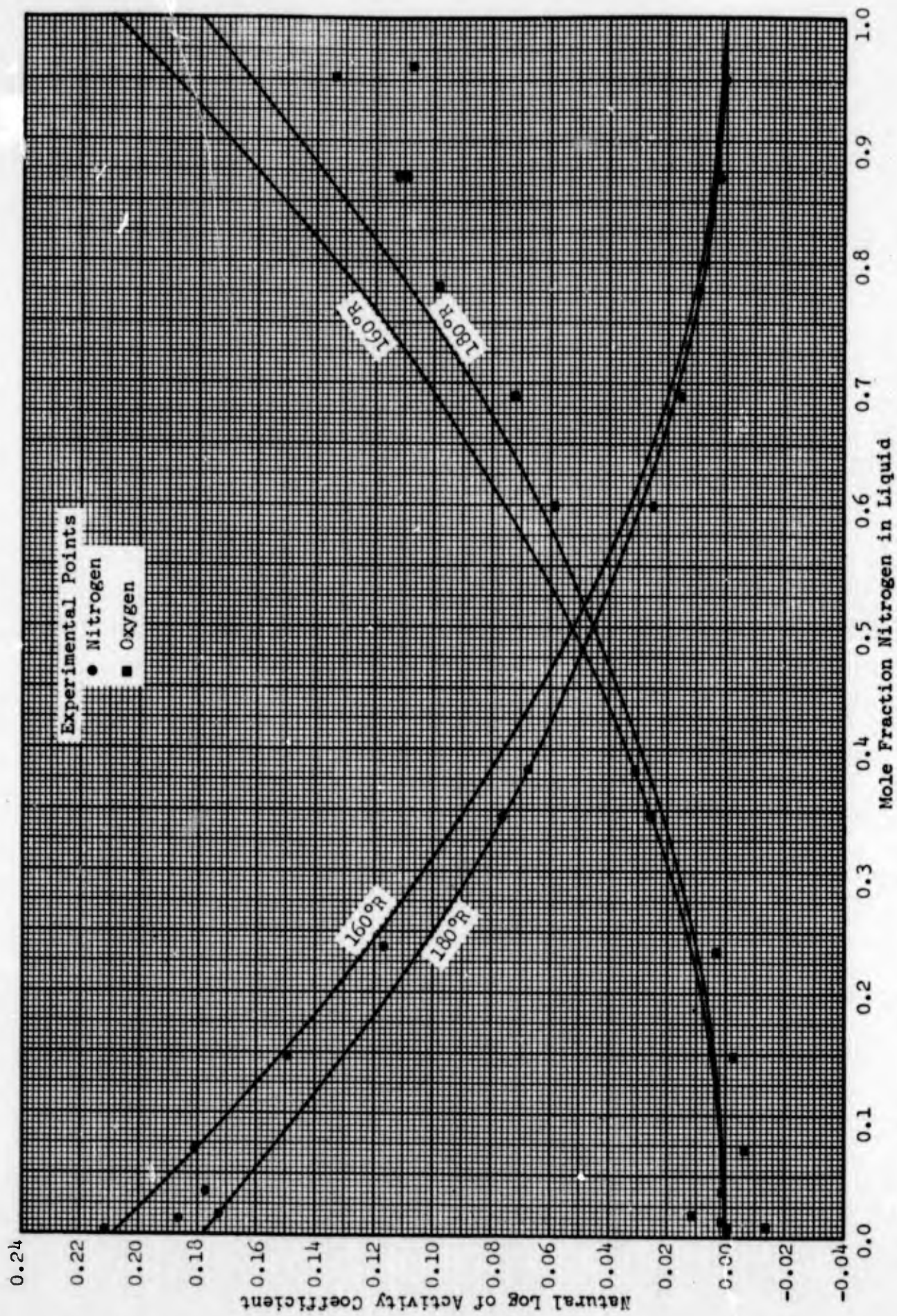


Figure 33. Activity Coefficients in the Nitrogen-Oxygen Binary System, Calculated vs. Experimental.

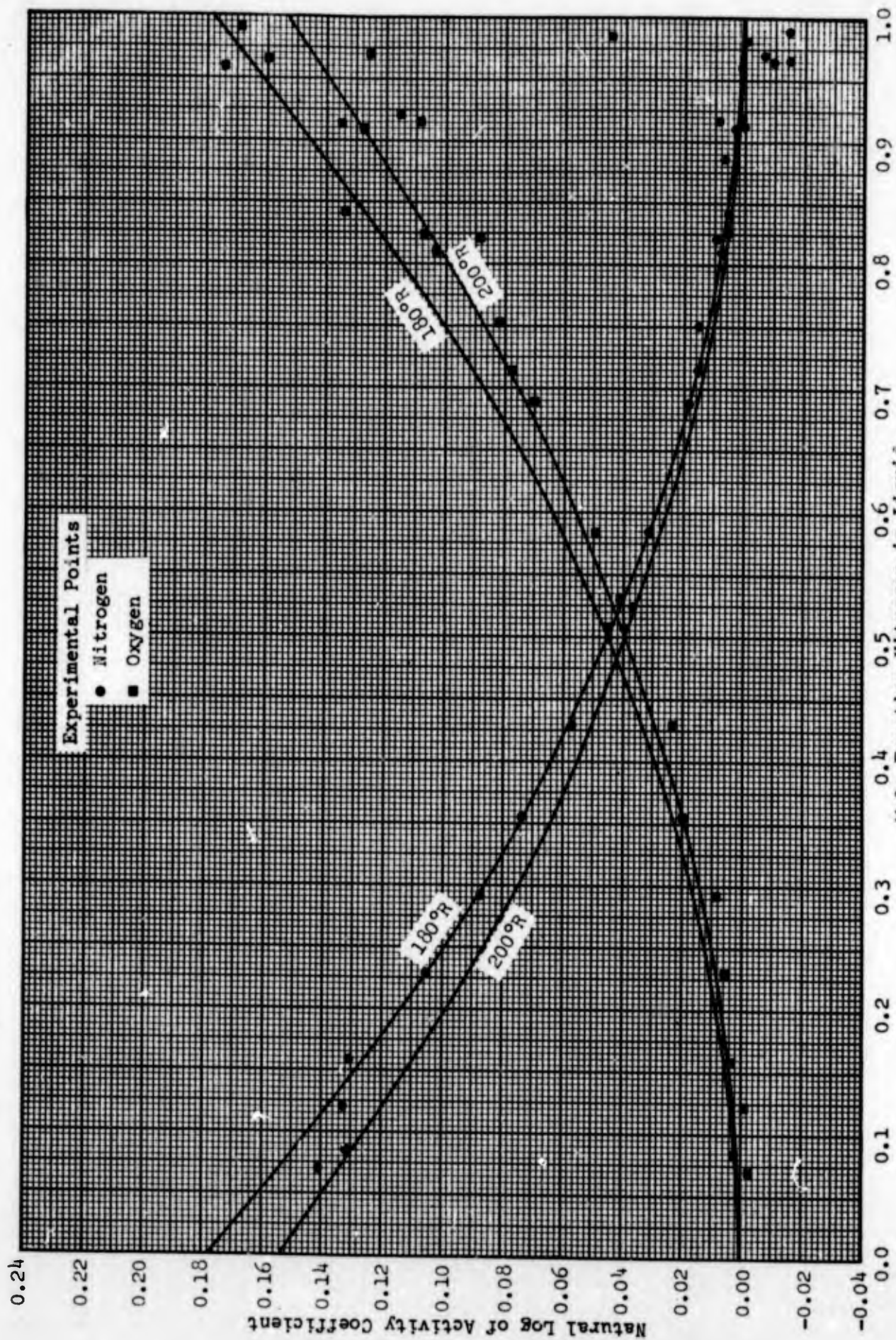


Figure 34. Activity Coefficients in the Nitrogen-Oxygen Binary System, Calculated vs. Experimental.

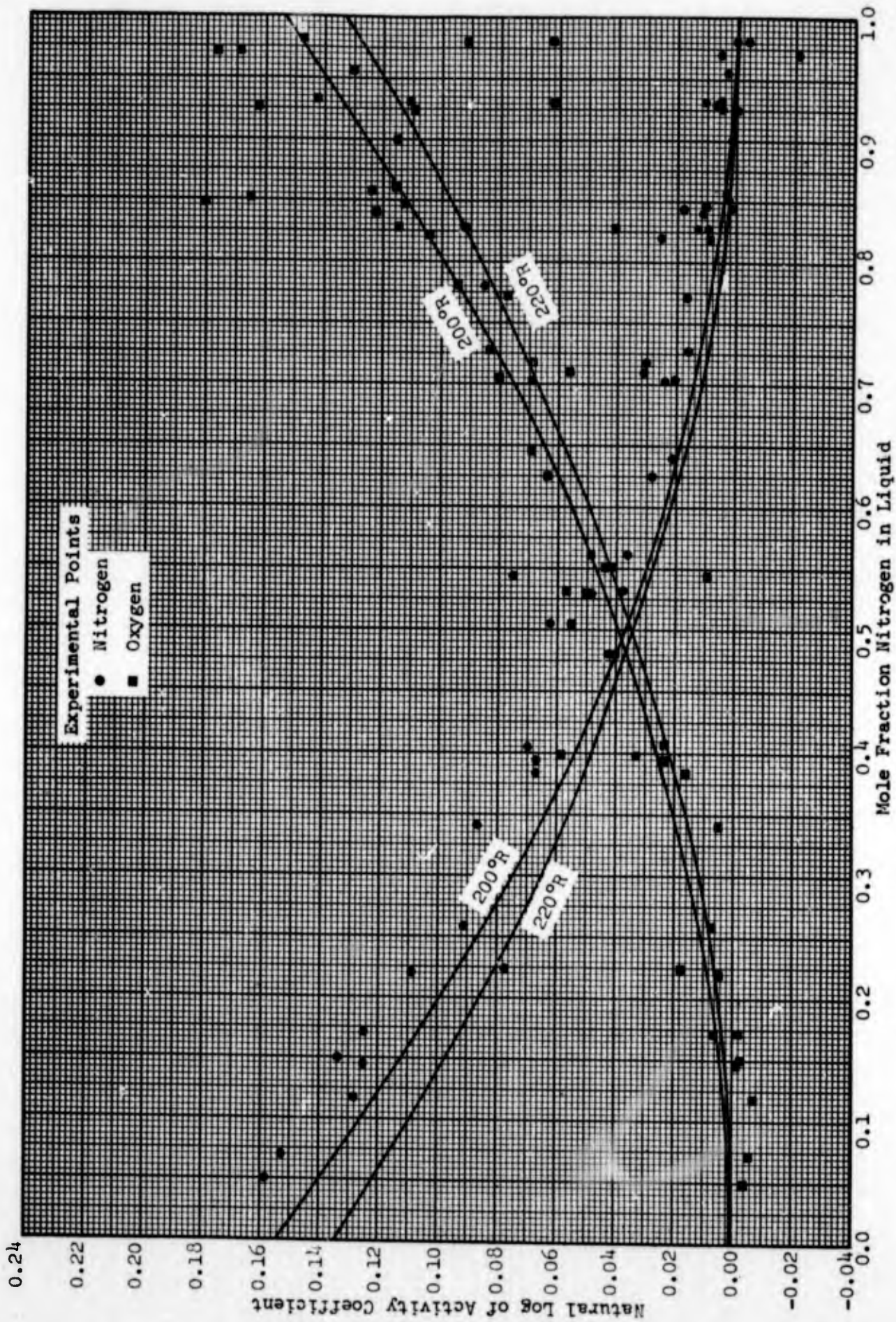


Figure 35. Activity Coefficients in the Nitrogen-Oxygen Binary System, Calculated vs. Experimental.

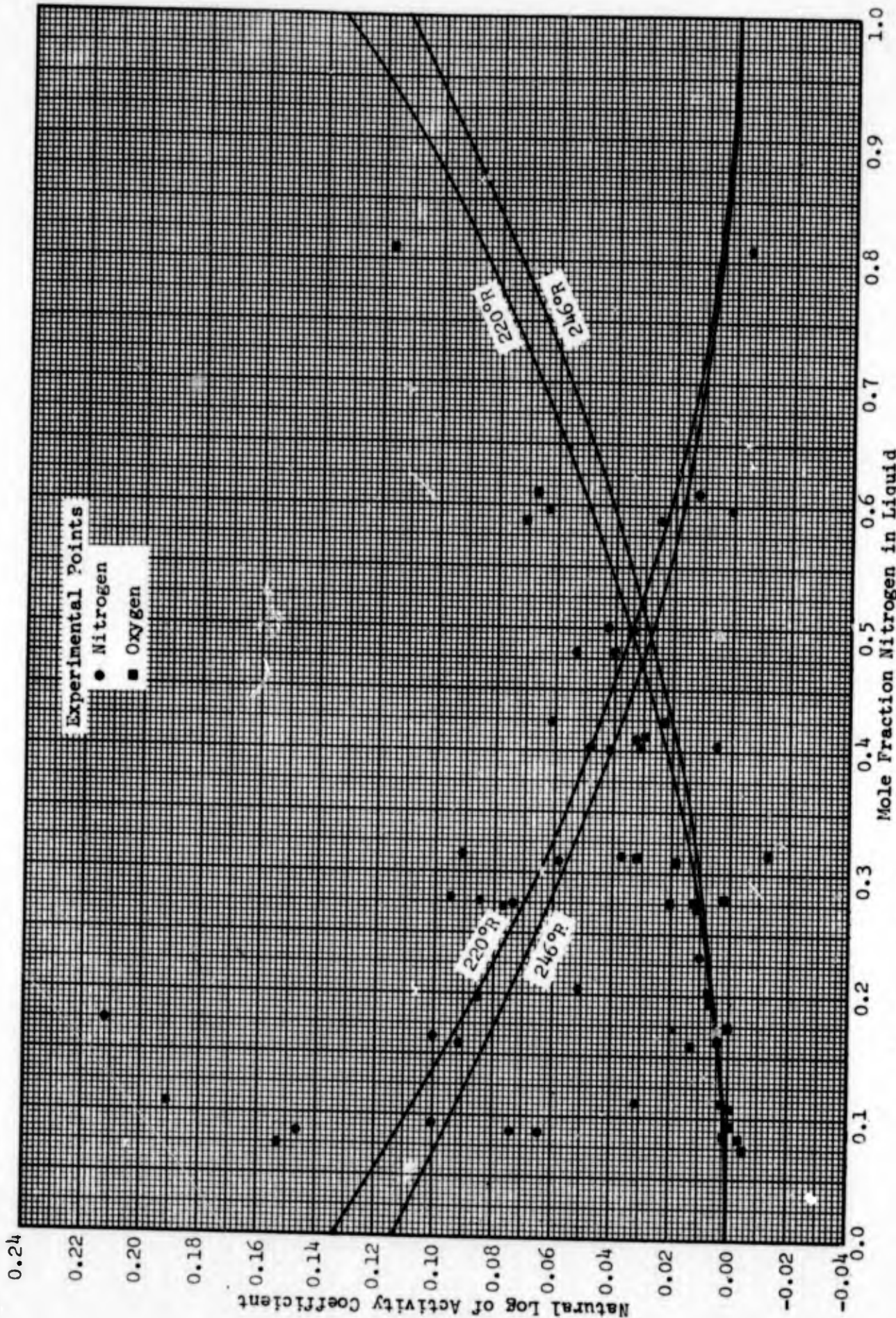


Figure 36. Activity Coefficients in the Nitrogen-Oxygen Binary System, Calculated vs. Experimental.

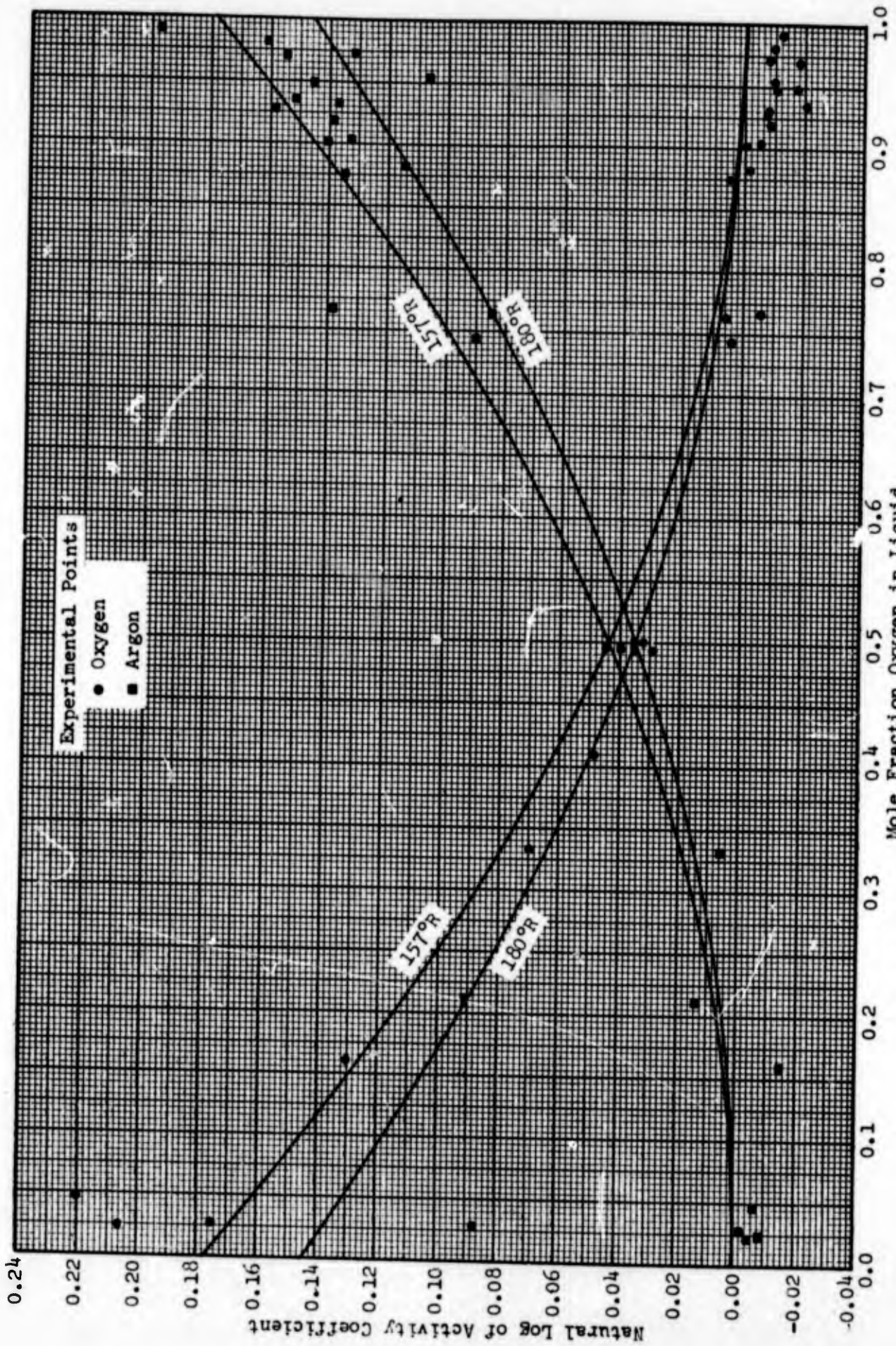


Figure 37. Activity Coefficients in the Oxygen-Argon Binary System, Calculated vs. Experimental.

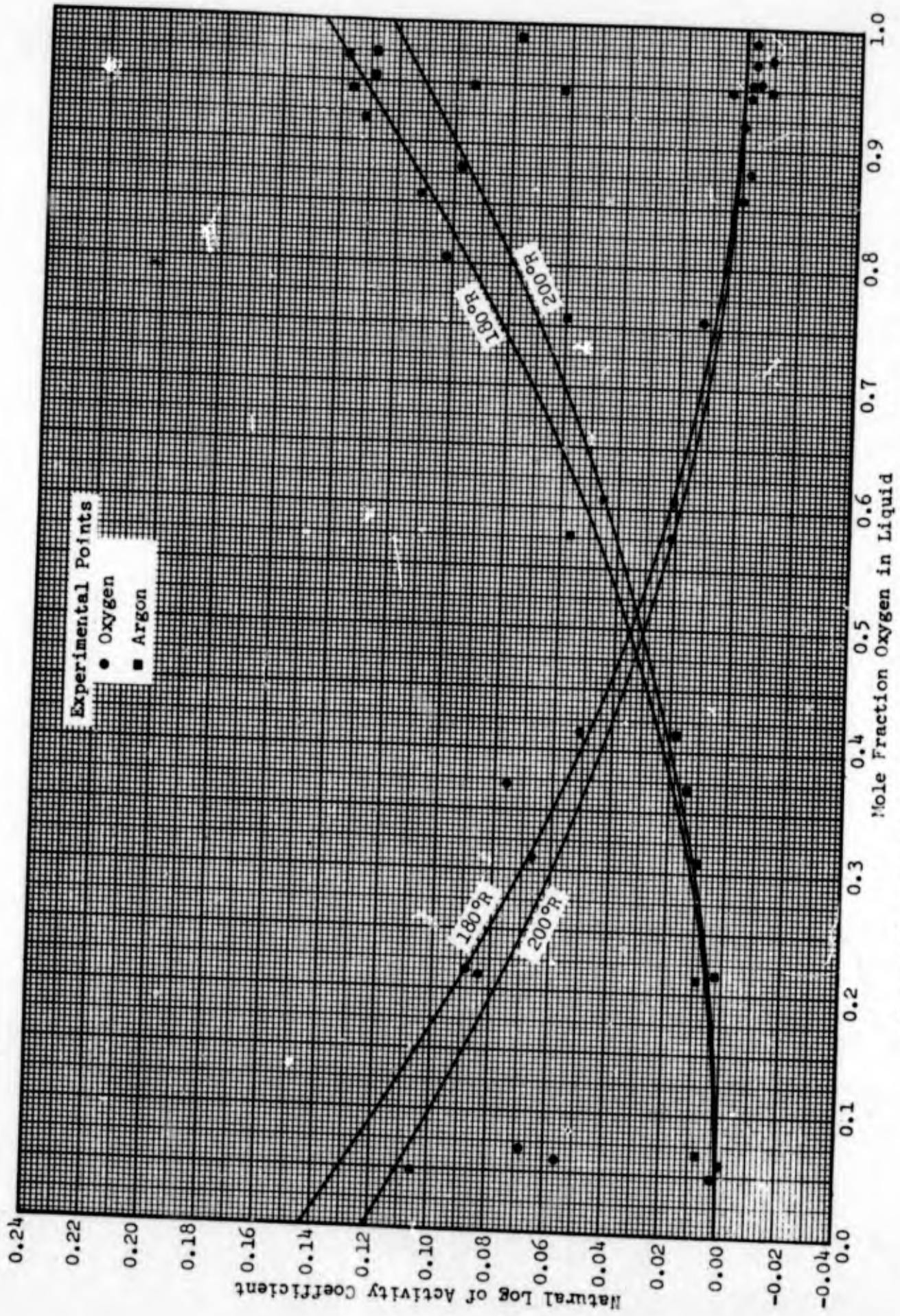


Figure 38. Activity Coefficients in the Oxygen-Argon Binary System, Calculated vs. Experimental.

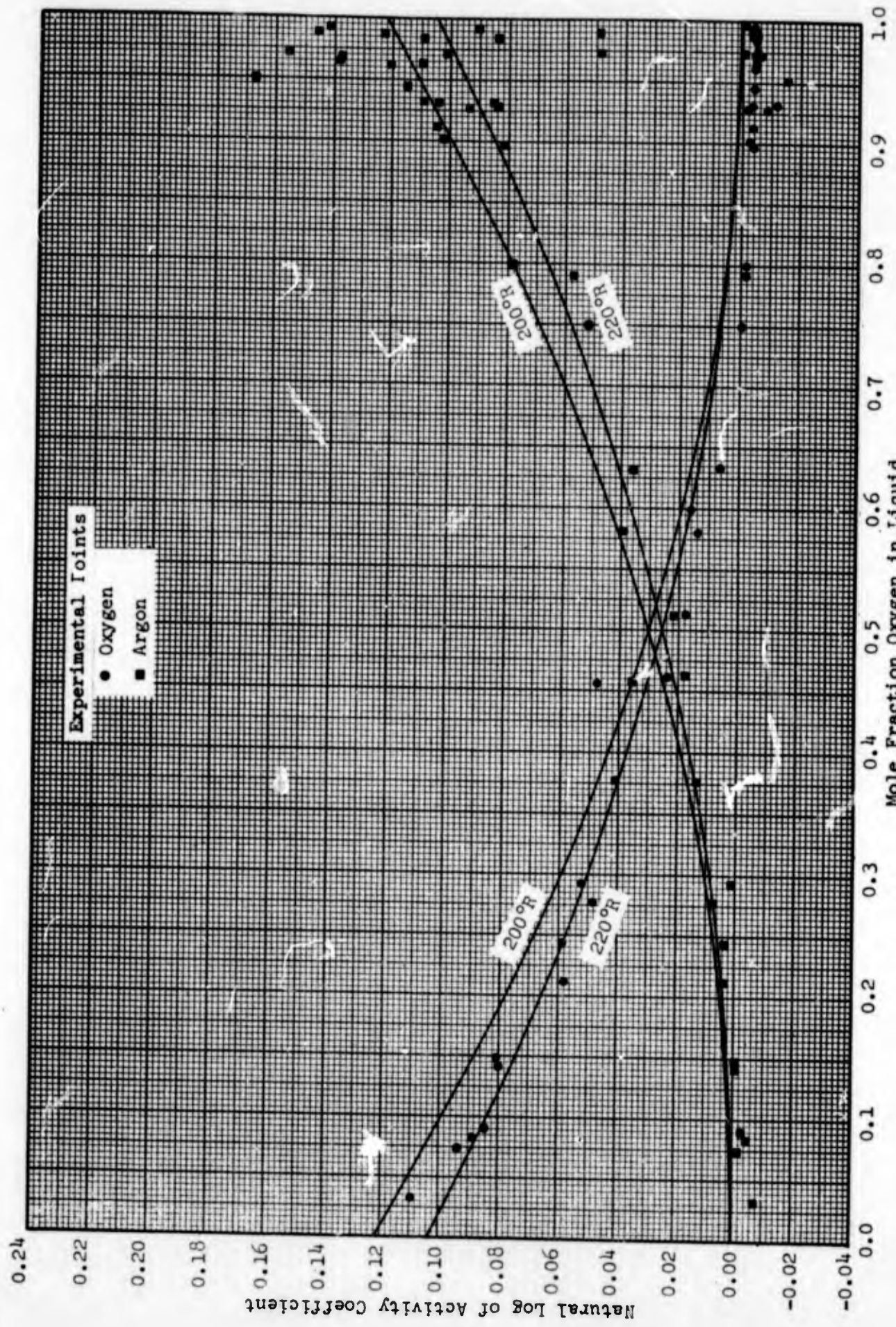


Figure 39. Activity Coefficients in the Oxygen-Argon Binary System, Calculated vs. Experimental.

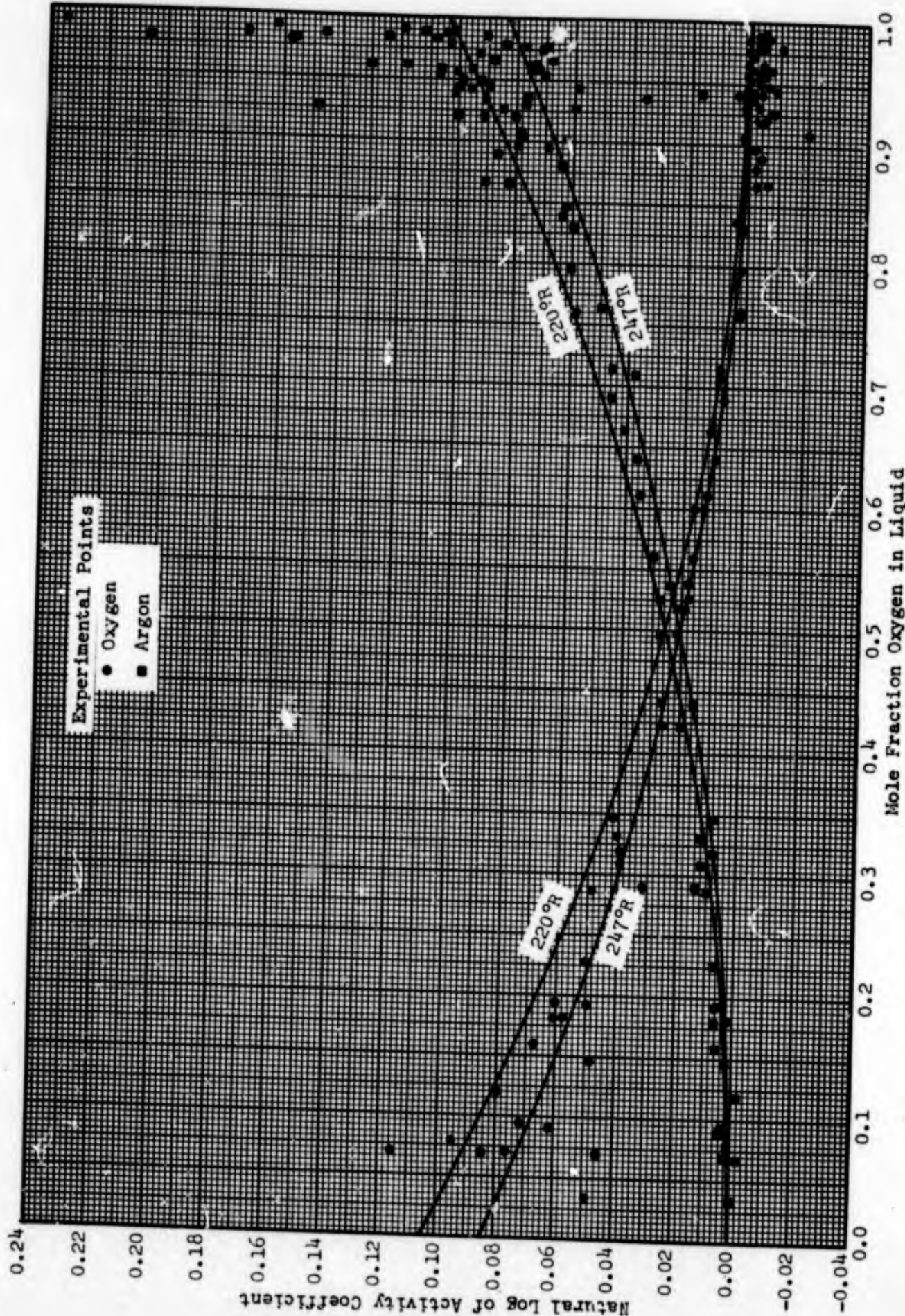


Figure 40. Activity Coefficients in the Oxygen-Argon Binary System, Calculated vs. Experimental.



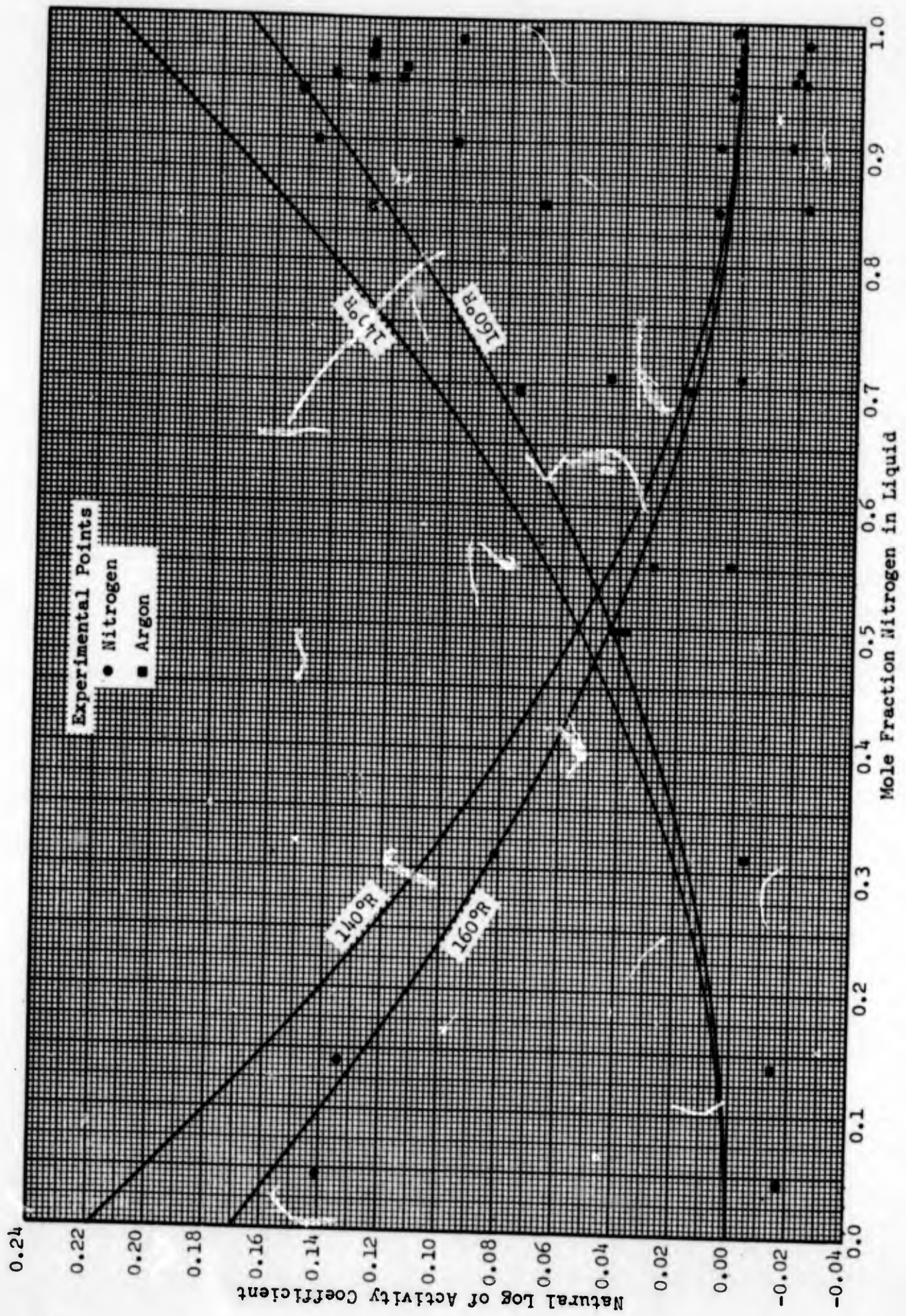


Figure 41. Activity Coefficients in the Nitrogen-Argon Binary System, Calculated vs. Experimental.

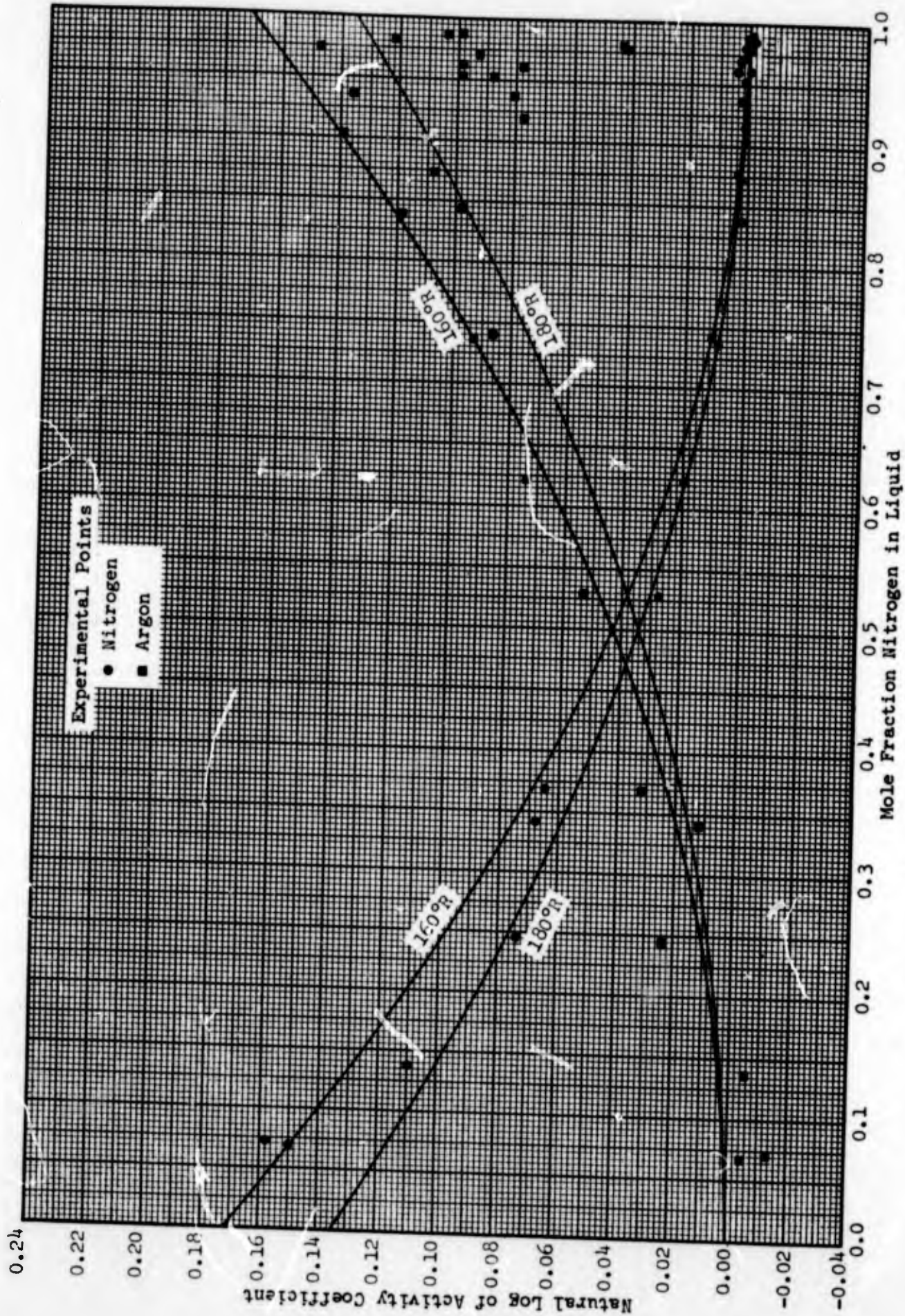


Figure 42. Activity Coefficients in the Nitrogen-Argon Binary System, Calculated vs. Experimental.

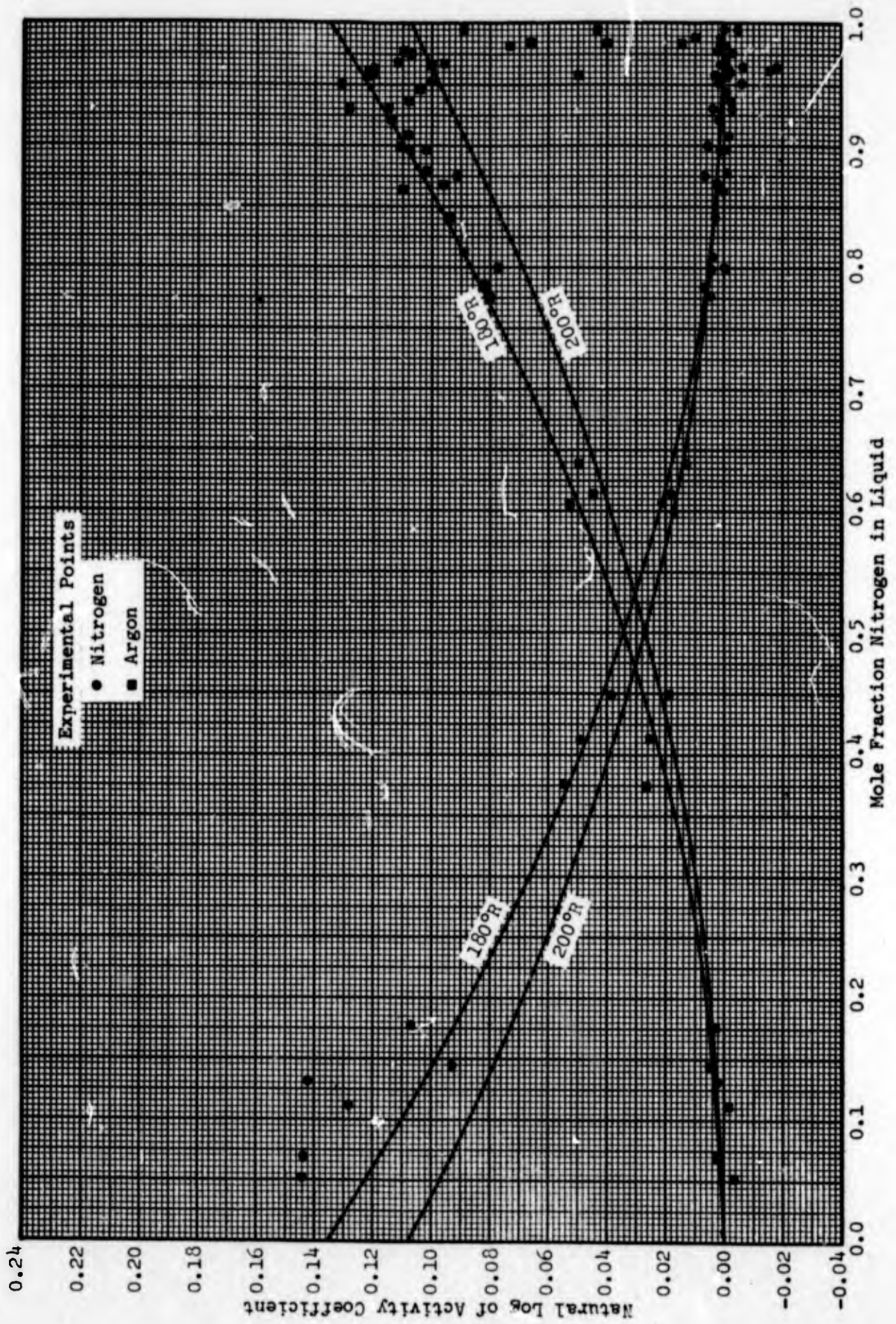


Figure 43. Activity Coefficients in the Nitrogen-Argon Binary System, Calculated vs. Experimental.

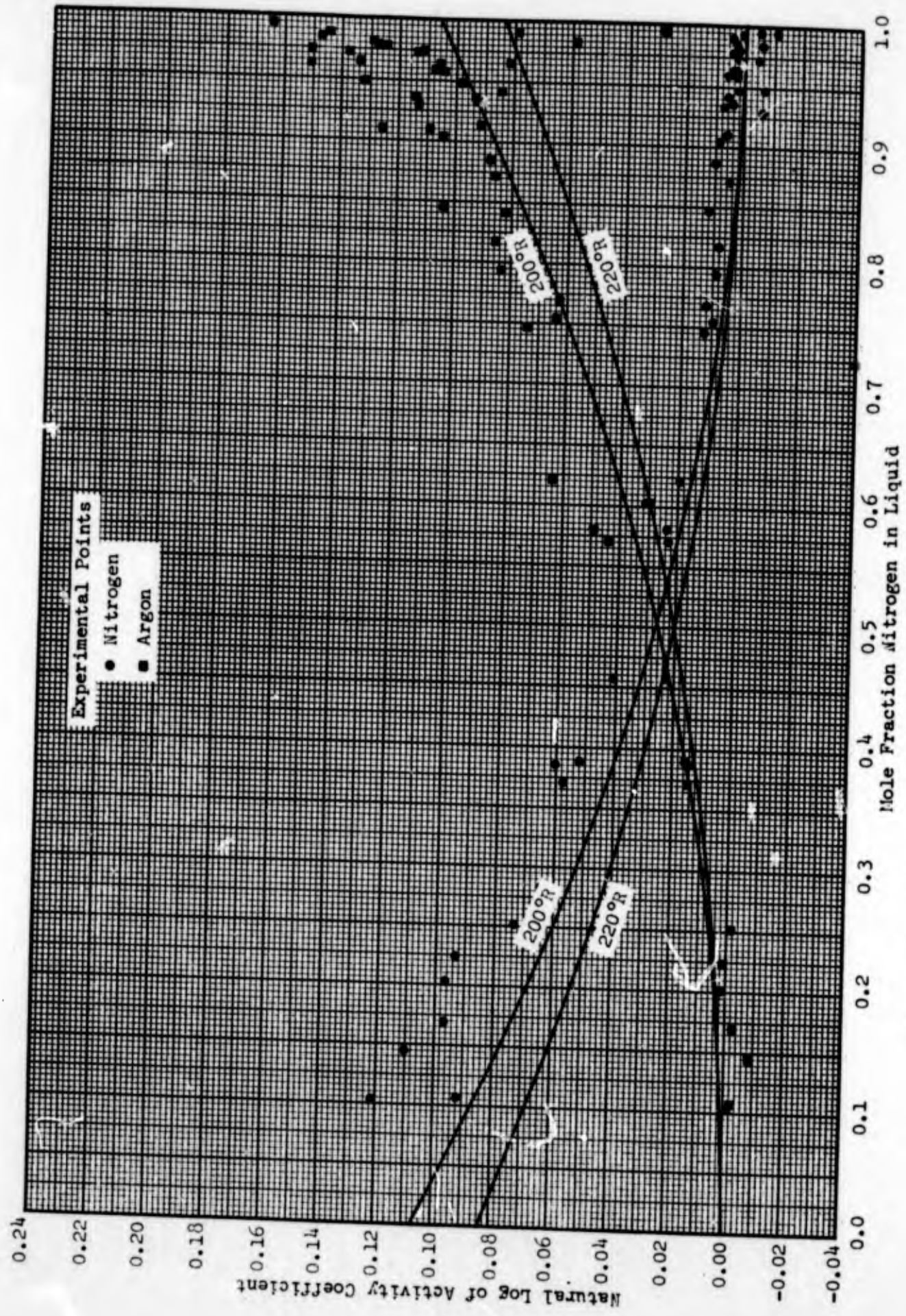


Figure 44. Activity Coefficients in the Nitrogen-Argon Binary System, Calculated vs. Experimental.

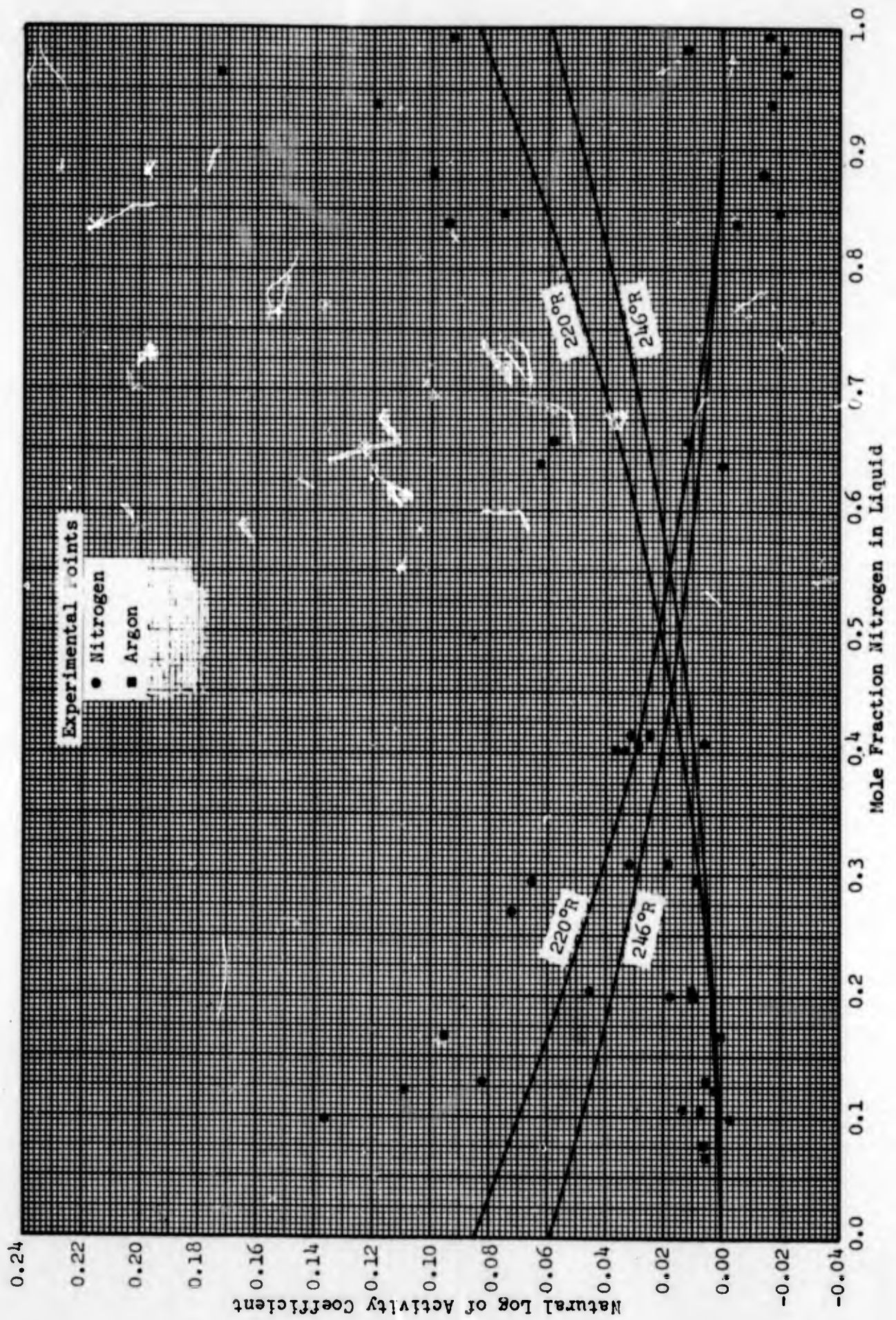


Figure 45. Activity Coefficients in the Nitrogen-Argon Binary System, Calculated vs. Experimental.

according to increasing pressure. The liquid phase corresponds to tie line points on the left and the vapor phase corresponds to tie line points on the right, and lines have been drawn connecting all points in both phases. These data show systematic deviations consistent with the deviations in activity coefficients. The largest error occurs at 20 atm where the difference corresponds to an error of 2.5% in the calculation of the pressure.

From an examination of the differences between calculated and measured data it is concluded that the correlation represents the data with a difference less than 2.5% in relative volatility and pressure in most regions. The largest difference is probably about 2.5%. The experimental data scatter less than this with an accuracy of about  $\pm 0.5\%$  in the pressure and  $\pm 1\%$  in the relative volatility.

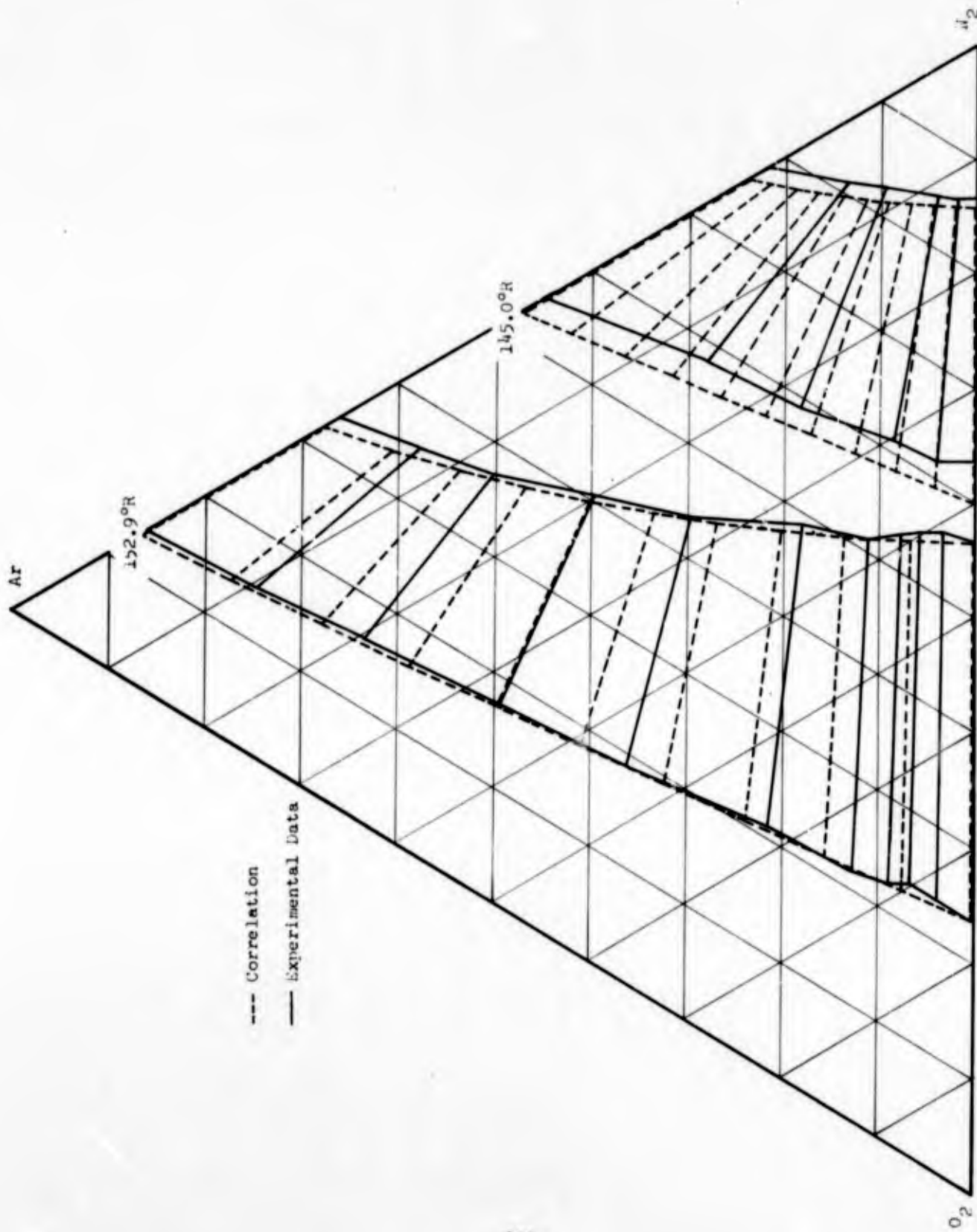
A comparison of the correlation with literature data can probably be best made in terms of comparisons with the Latimer<sup>(34)</sup> correlation, since it represents a good summary of existing data. This comparison is given in Figures 83 to 85 for each of the binary systems. In the nitrogen-oxygen system the difference varies up to about 2% depending on the composition and pressure. In the nitrogen-argon system the difference varies up to 10% at 20 atm, and in the argon-oxygen system the difference varies up to about 5%.

Factors which influence this correlation are:

1. The properties of "liquid" nitrogen above the critical temperature of nitrogen.
2. The partial molar volume of the components at pressures approaching the critical pressure of a mixture.
3. The assumption of a separate free energy expression for the vapor phase and the liquid phase.

These factors are inherent problems in the correlation of data by means of activity coefficients based upon the pure liquid component as the standard state. The systematic errors observed with this correlation probably are due to the uncertainty of these factors.

An alternate but more difficult approach would be to correlate the data in terms of an equation of state applicable to both the vapor and the liquid phases. This method would eliminate the need for a pure liquid reference state. The partial molar volume could be calculated from the equation of state, and the free energy equation would be continuous in going from vapor to liquid.



--- Correlation  
 — Experimental Data

Figure 46. Comparison of Experimental Data and the Correlation, 1 Atmosphere.

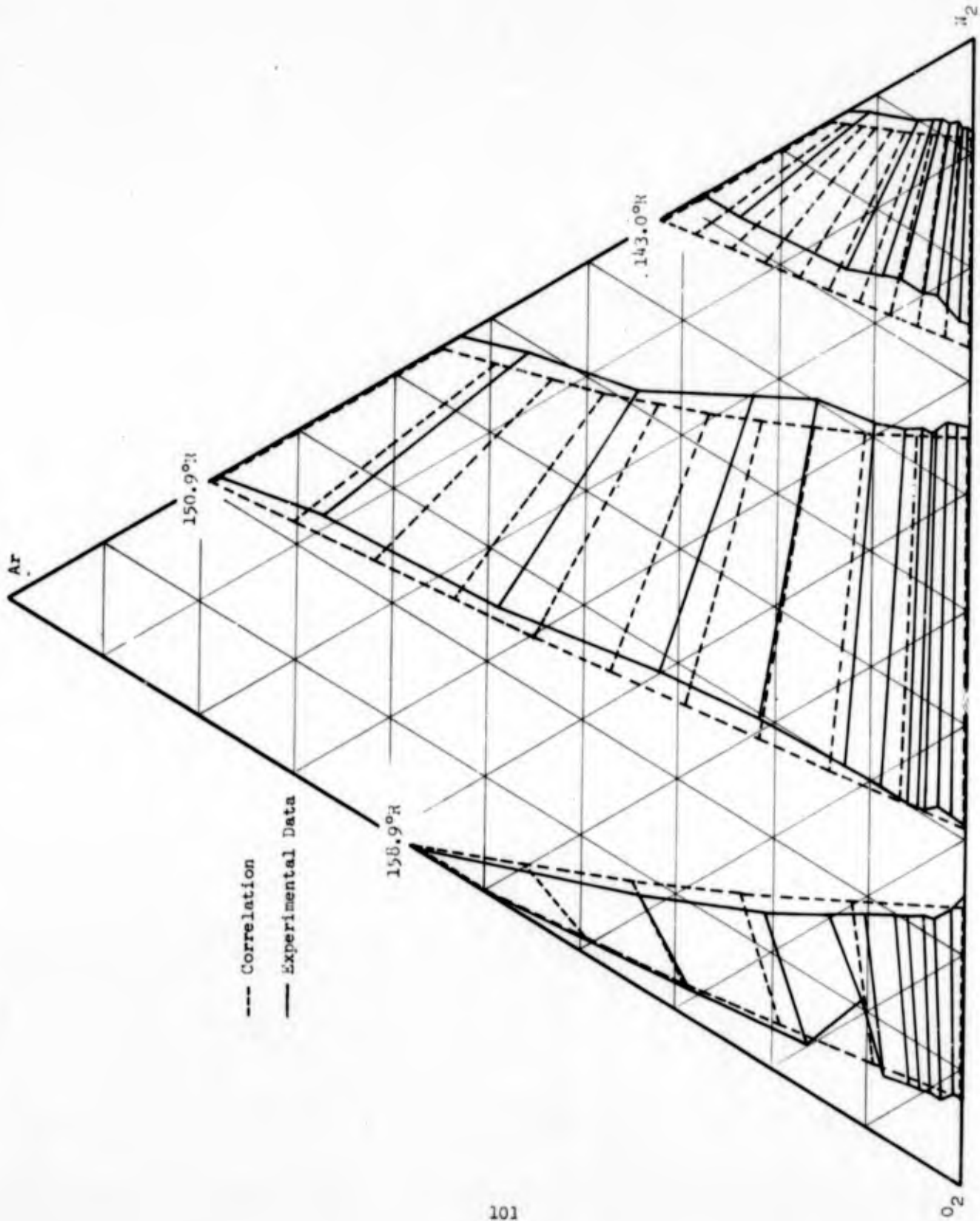


Figure 47. Comparison of Experimental Data and the Correlation, 1 Atmosphere.



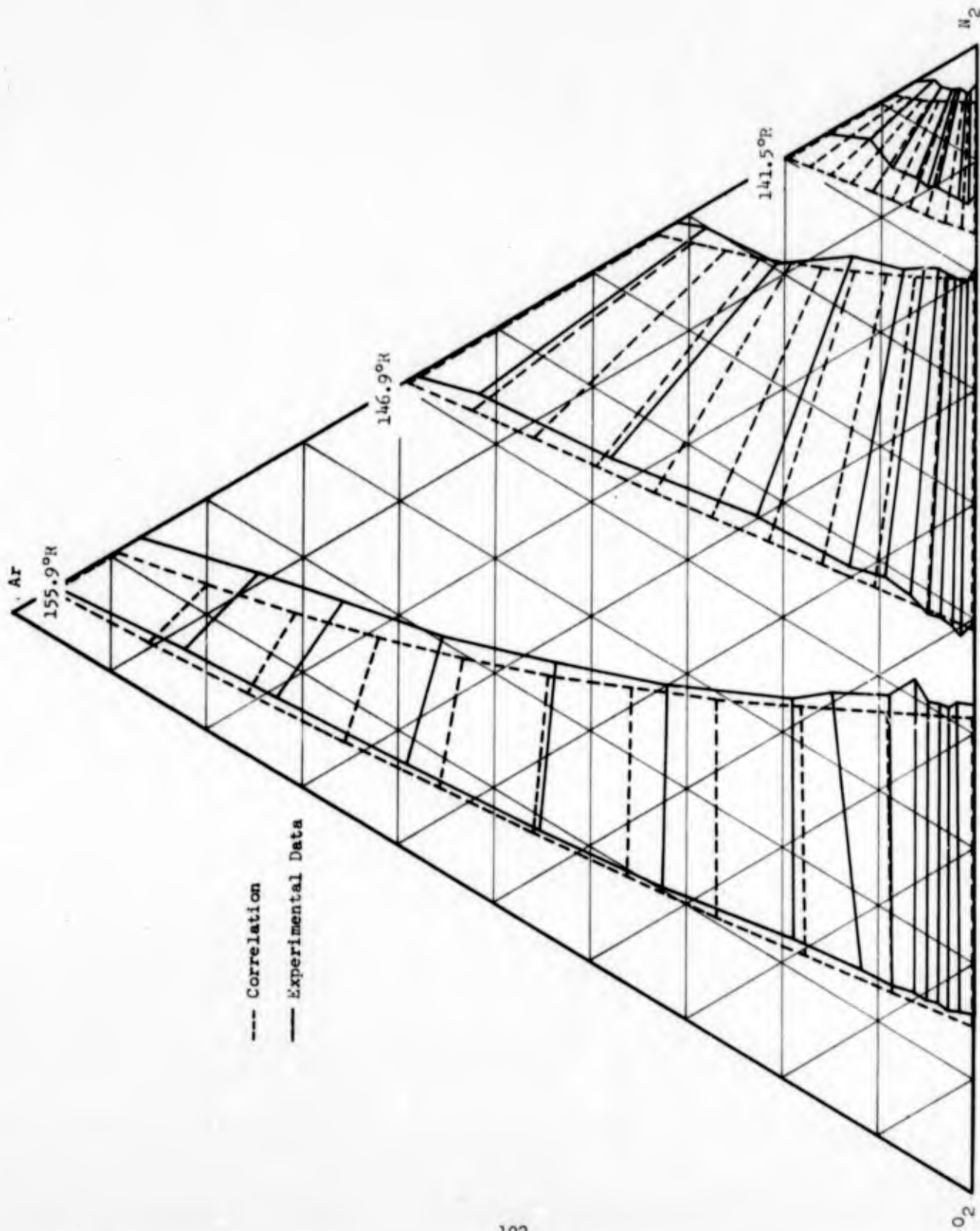


Figure 48. Comparison of Experimental Data and the Correlation, 1 Atmosphere.

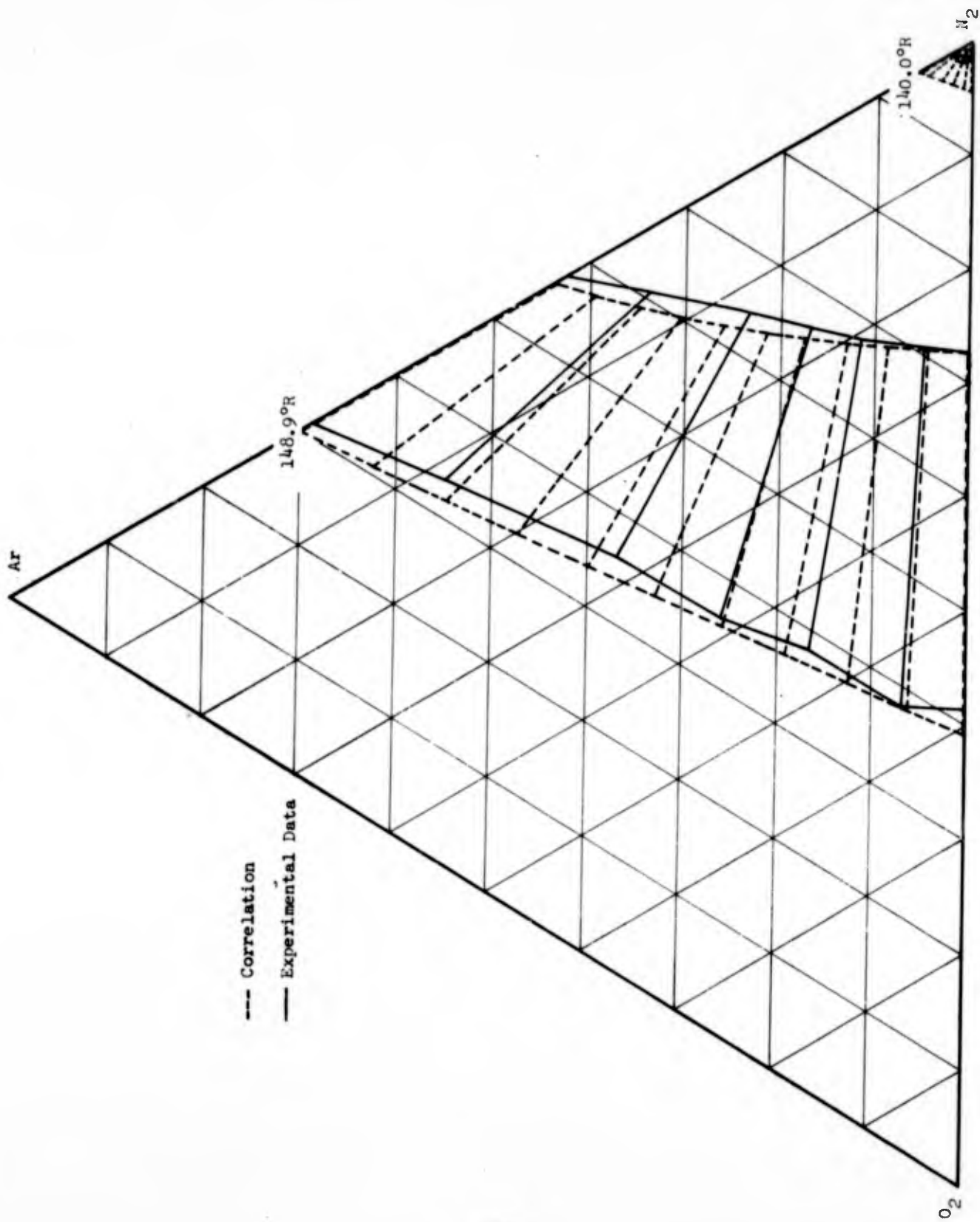


Figure 49. Comparison of Experimental Data and the Correlation, 1 Atmosphere.

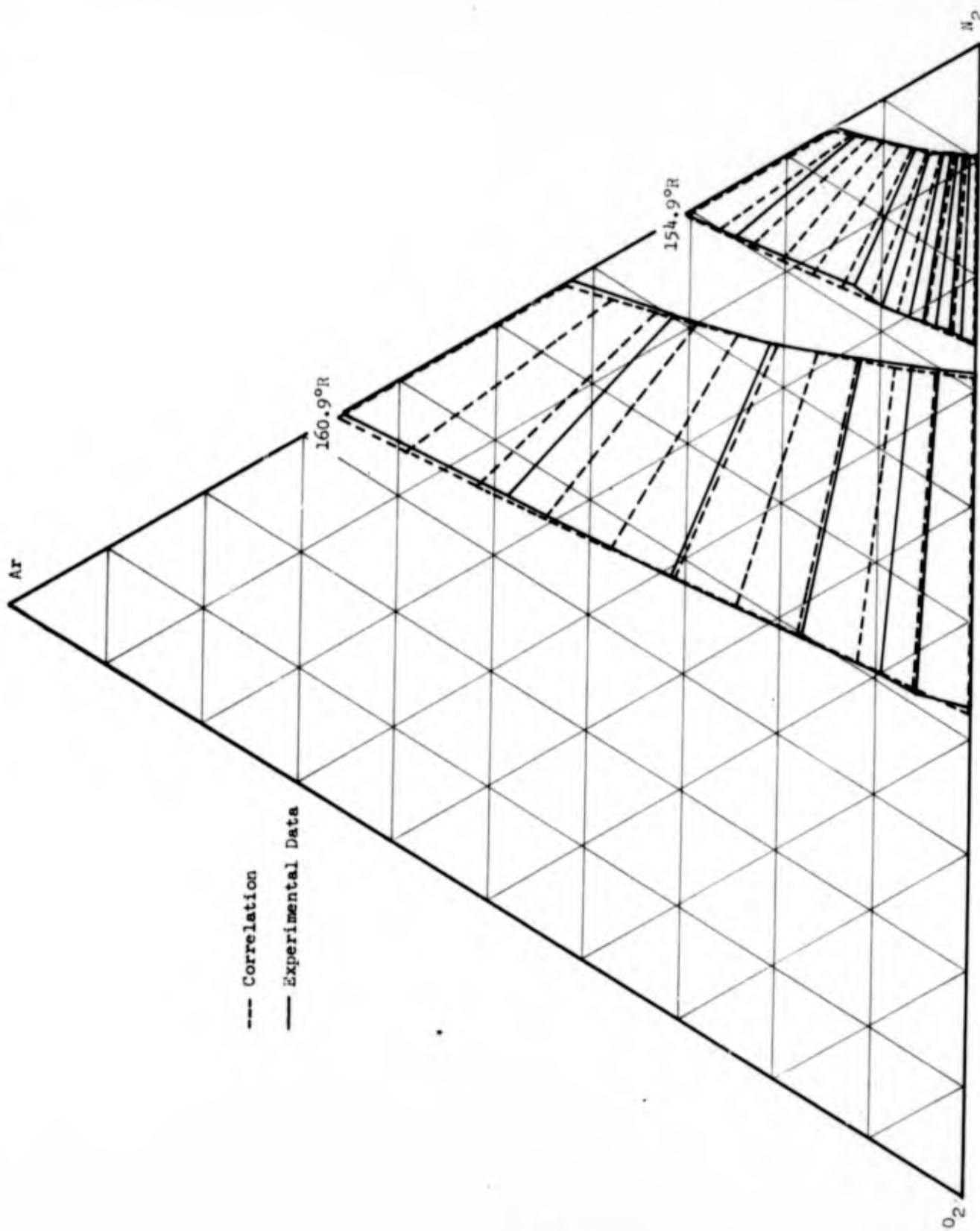


Figure 50. Comparison of Experimental Data and the Correlation, 2 Atmospheres.

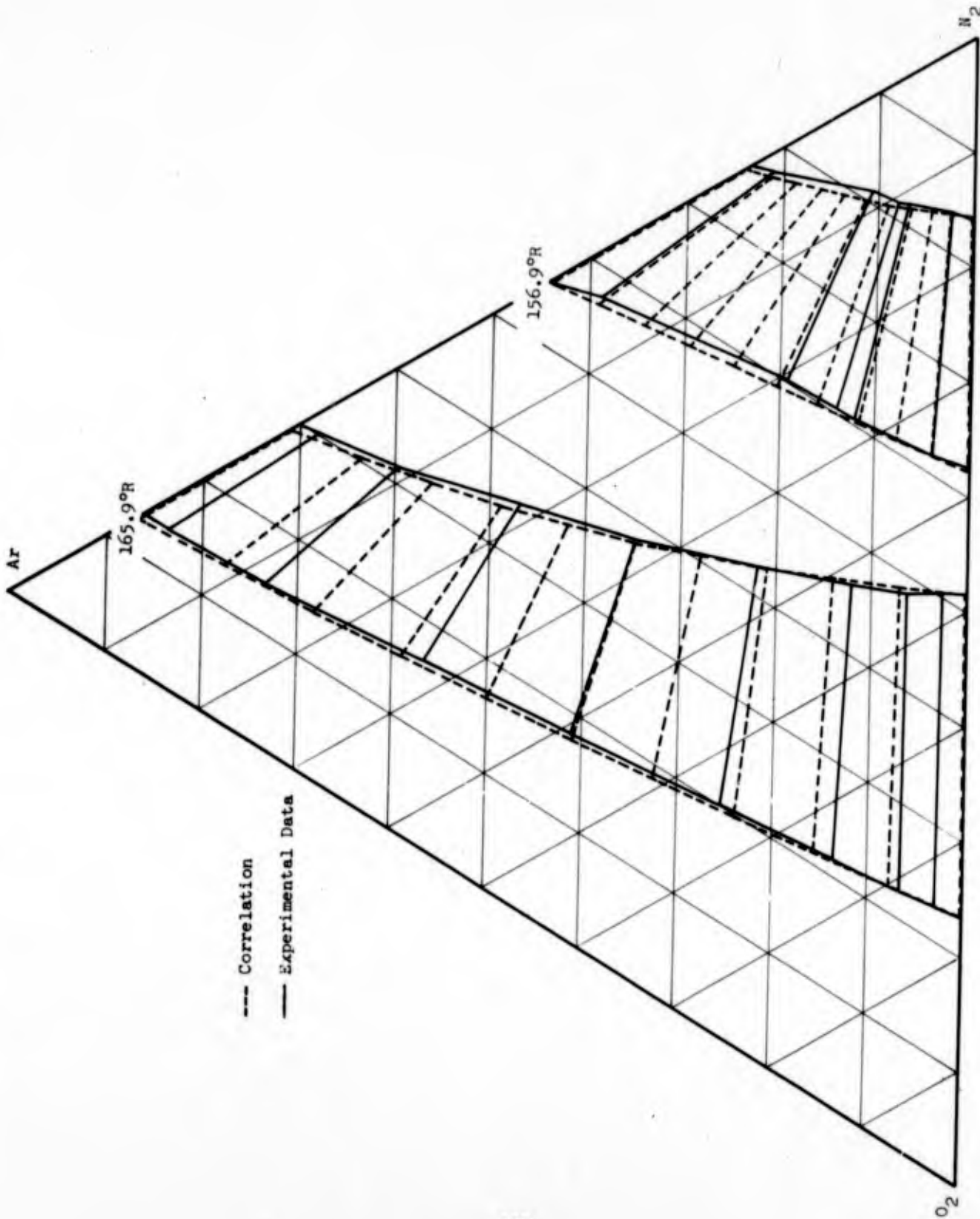


Figure 51. Comparison of Experimental Data and the Correlation, 2 Atmospheres.

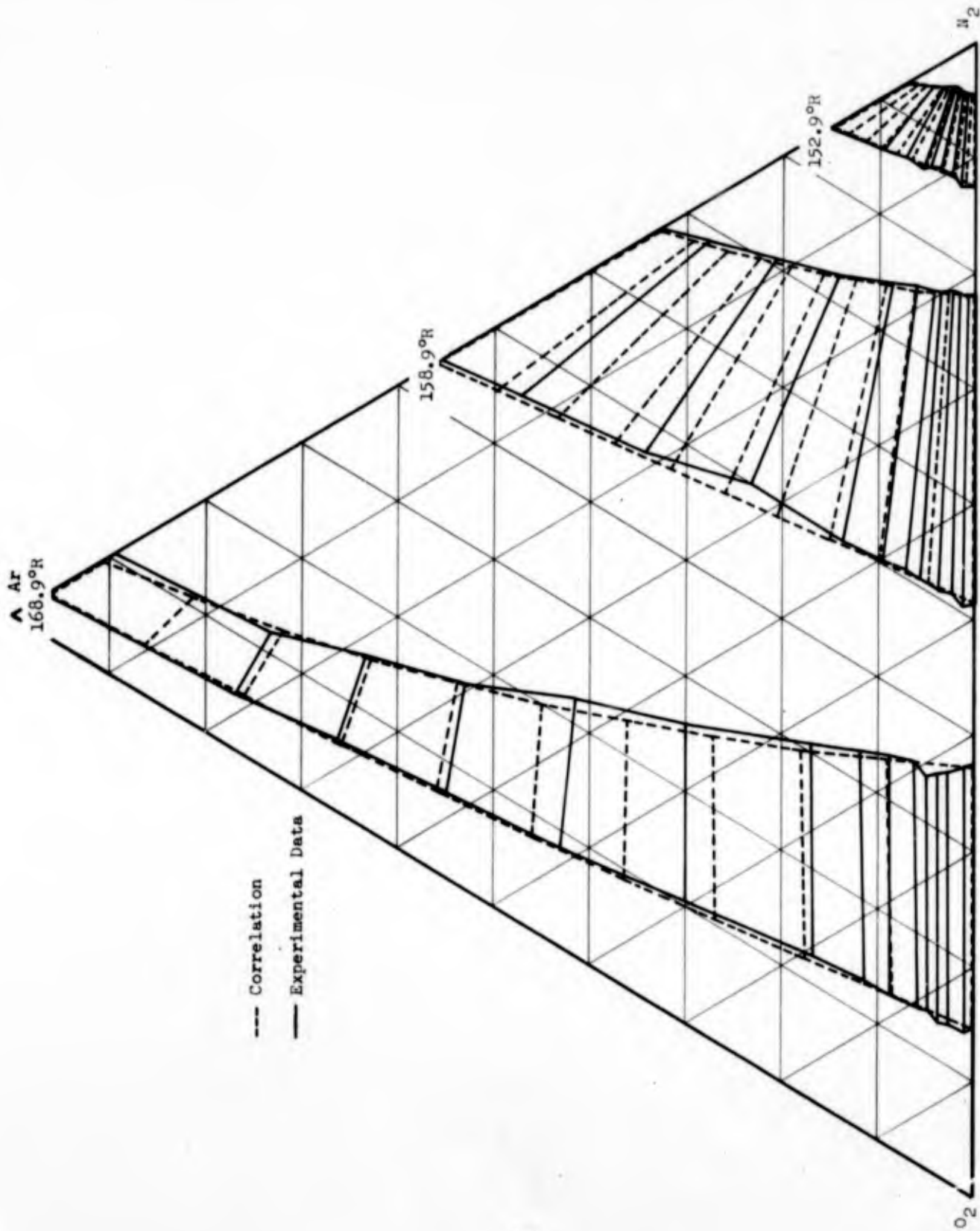


Figure 52. Comparison of Experimental Data and the Correlation, 2 Atmospheres.

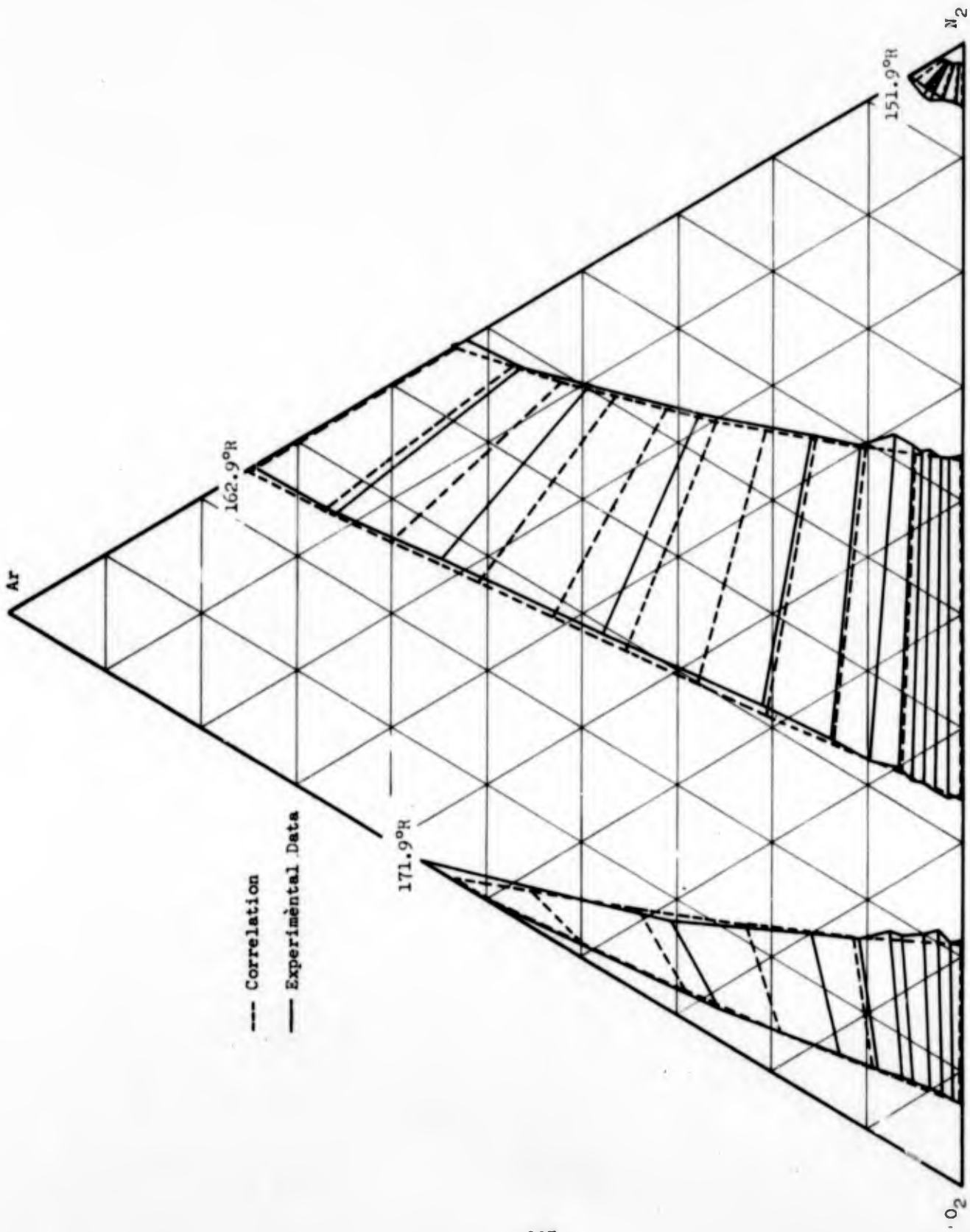


Figure 53. Comparison of Experimental Data and the Correlation, 2 Atmospheres.

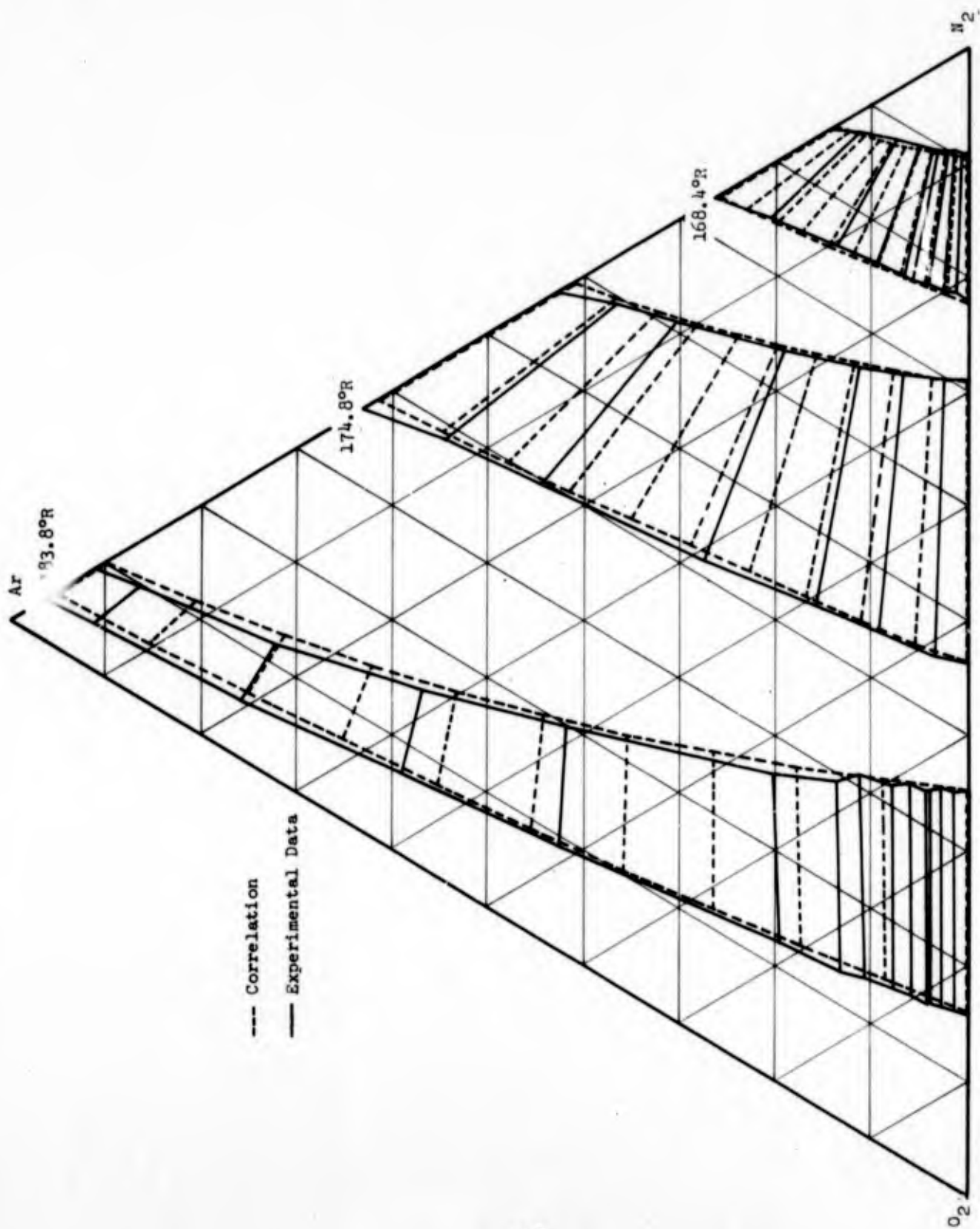


Figure 54. Comparison of Experimental Data and the Correlation, 4 Atmospheres.

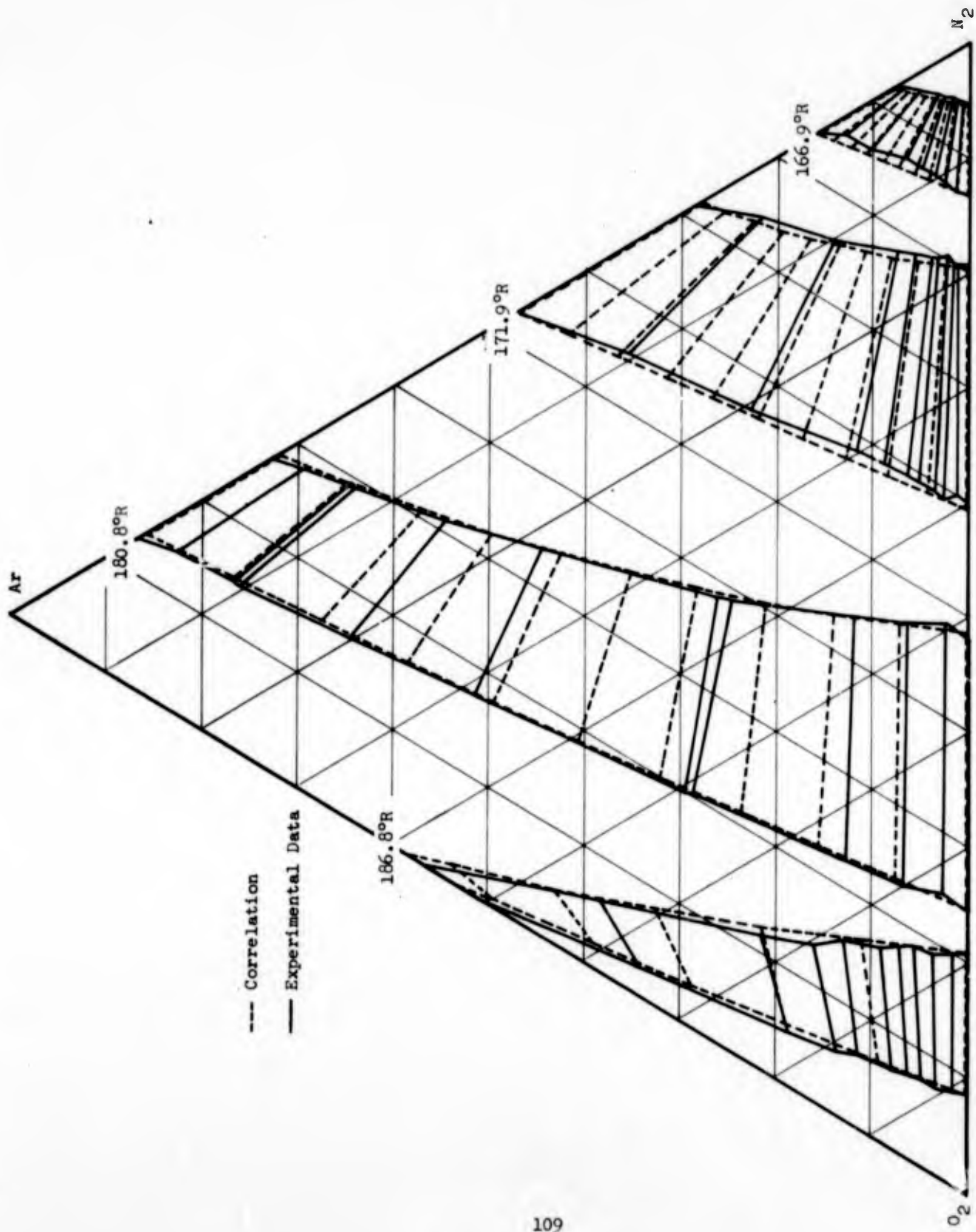


Figure 55. Comparison of Experimental Data and the Correlation, 4 Atmospheres.



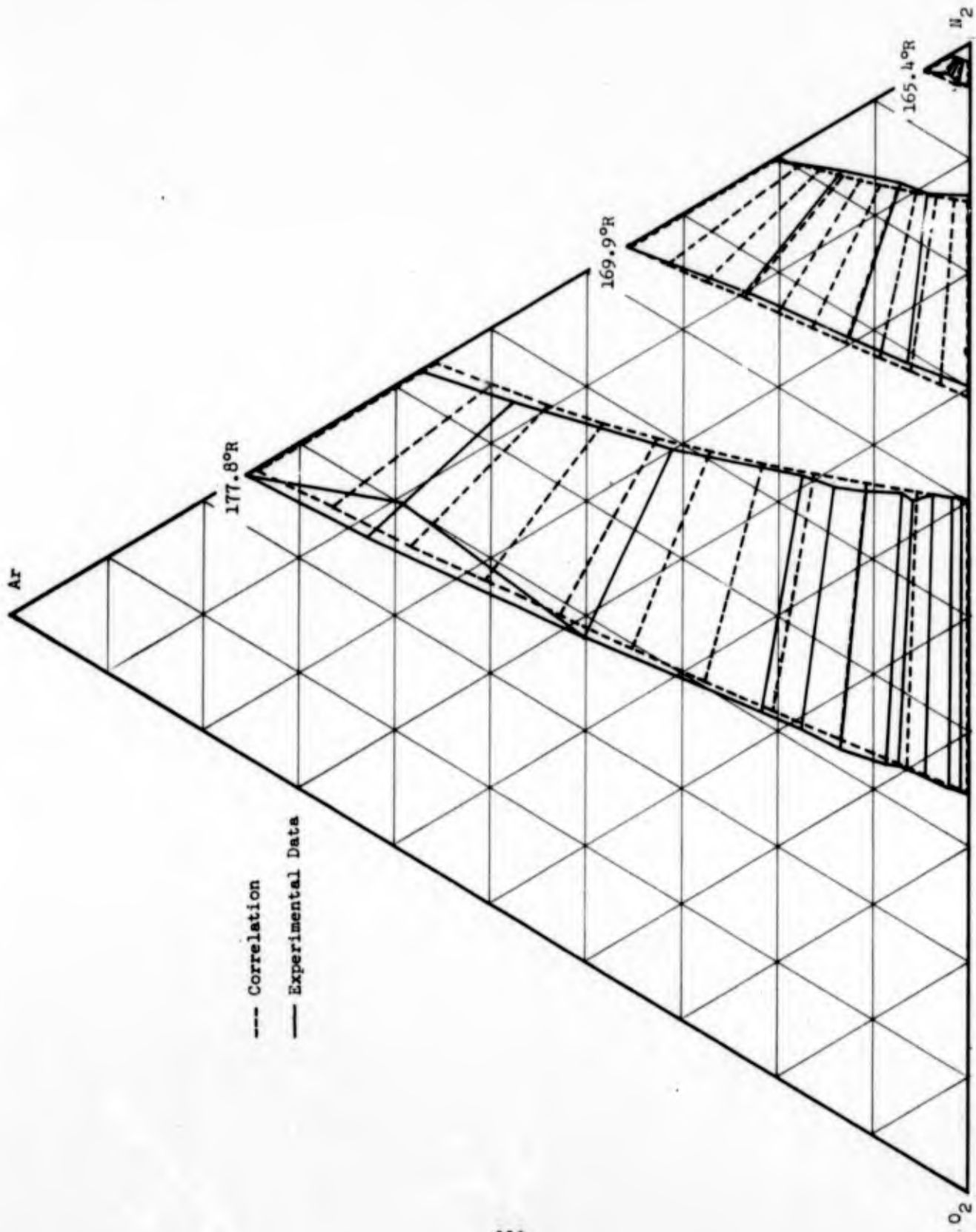


Figure 56. Comparison of Experimental Data and the Correlation, 4 Atmospheres.

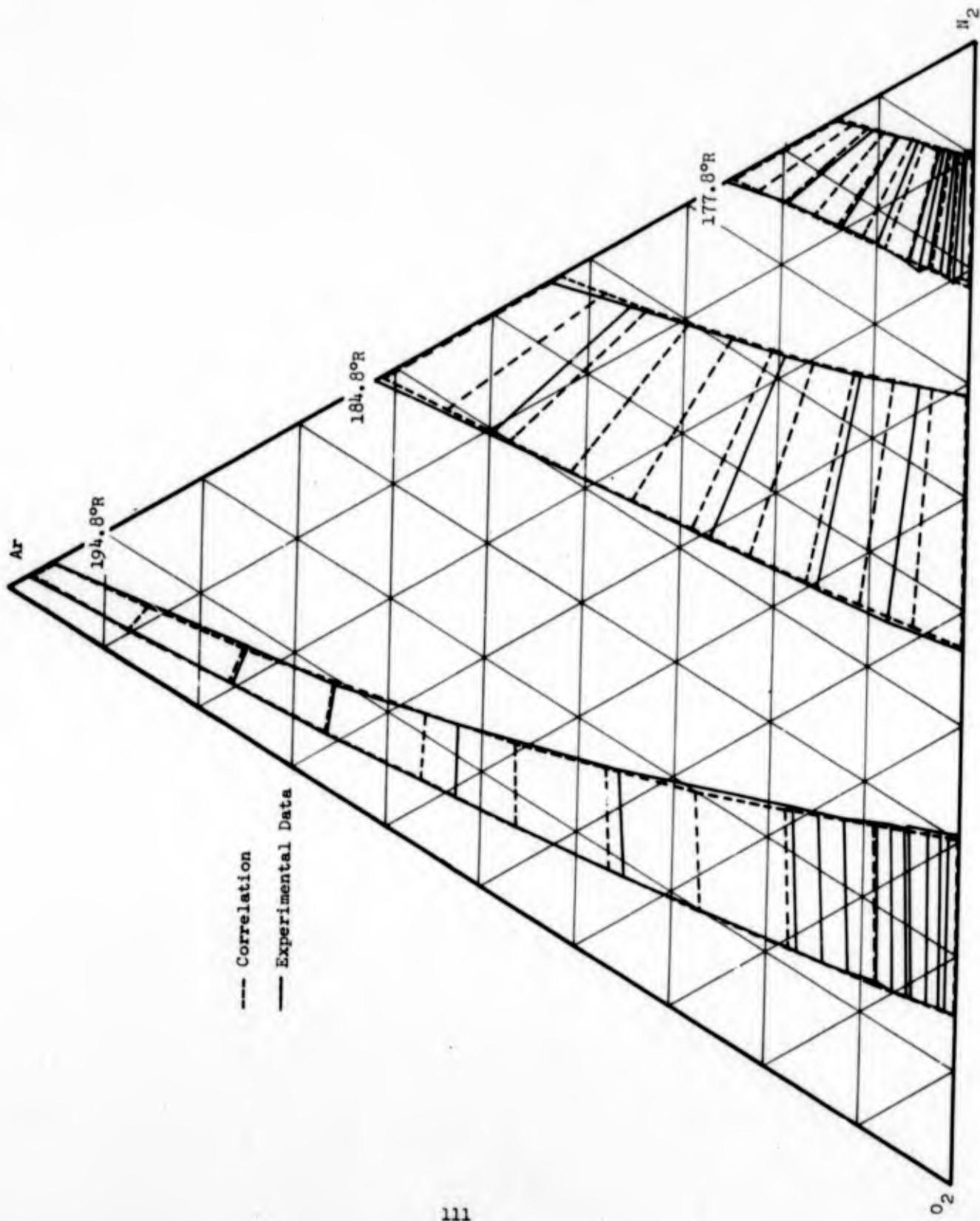


Figure 57. Comparison of Experimental Data and the Correlation, 6 Atmospheres.

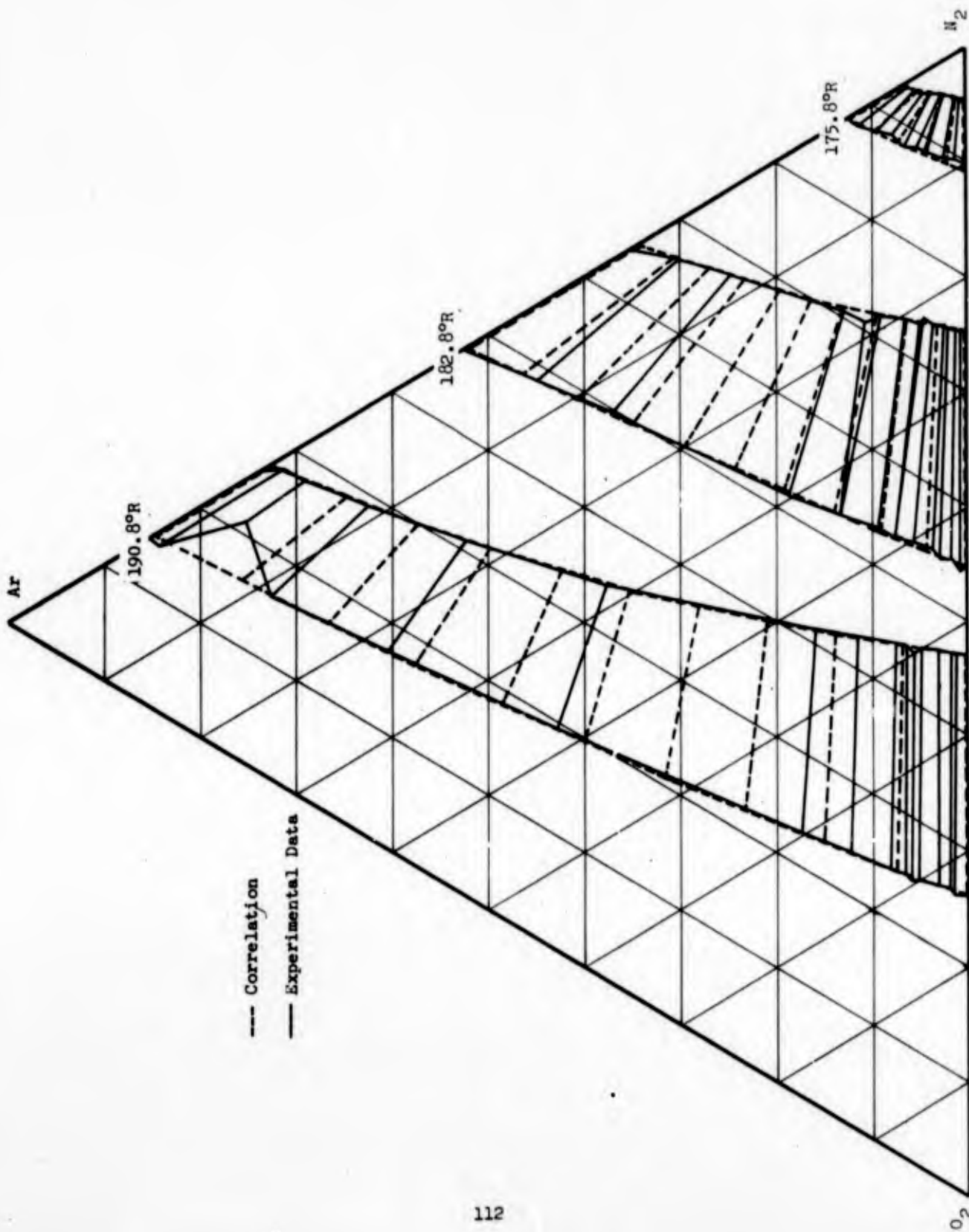


Figure 58. Comparison of Experimental Data and the Correlation, 6 Atmospheres.

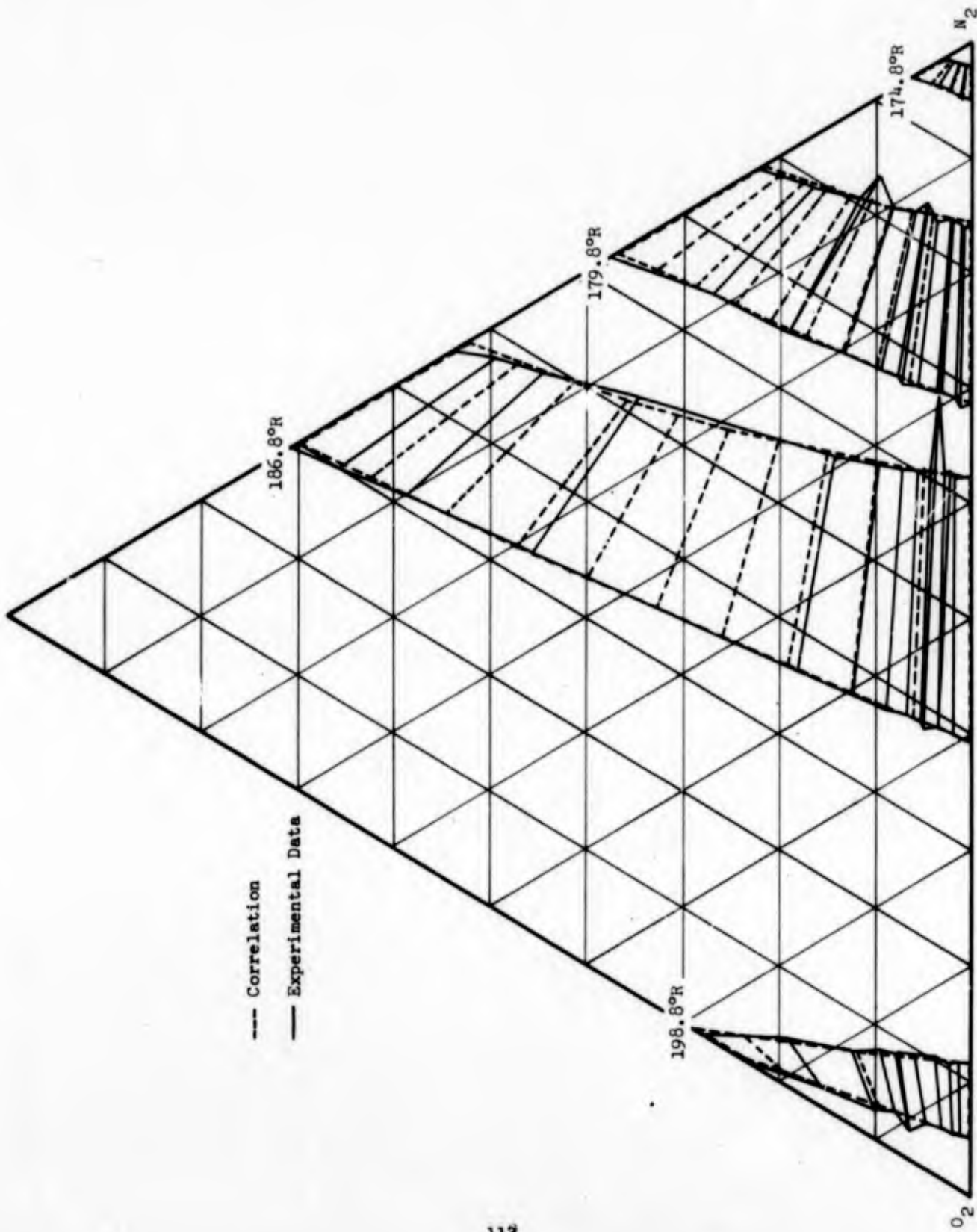


Figure 59. Comparison of Experimental Data and the Correlation, 6 Atmospheres.

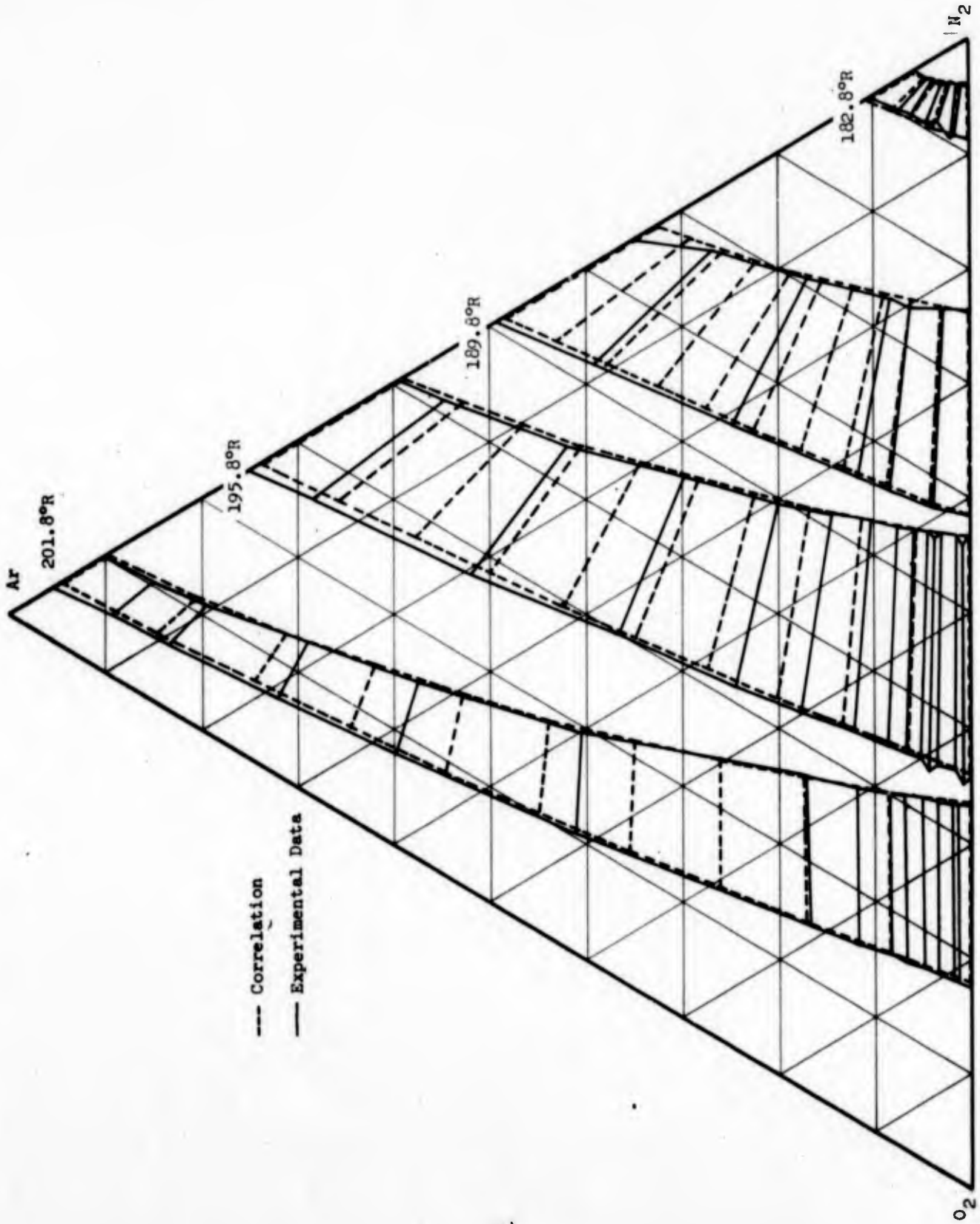


Figure 60. Comparison of Experimental Data and the Correlation, 8 Atmospheres.

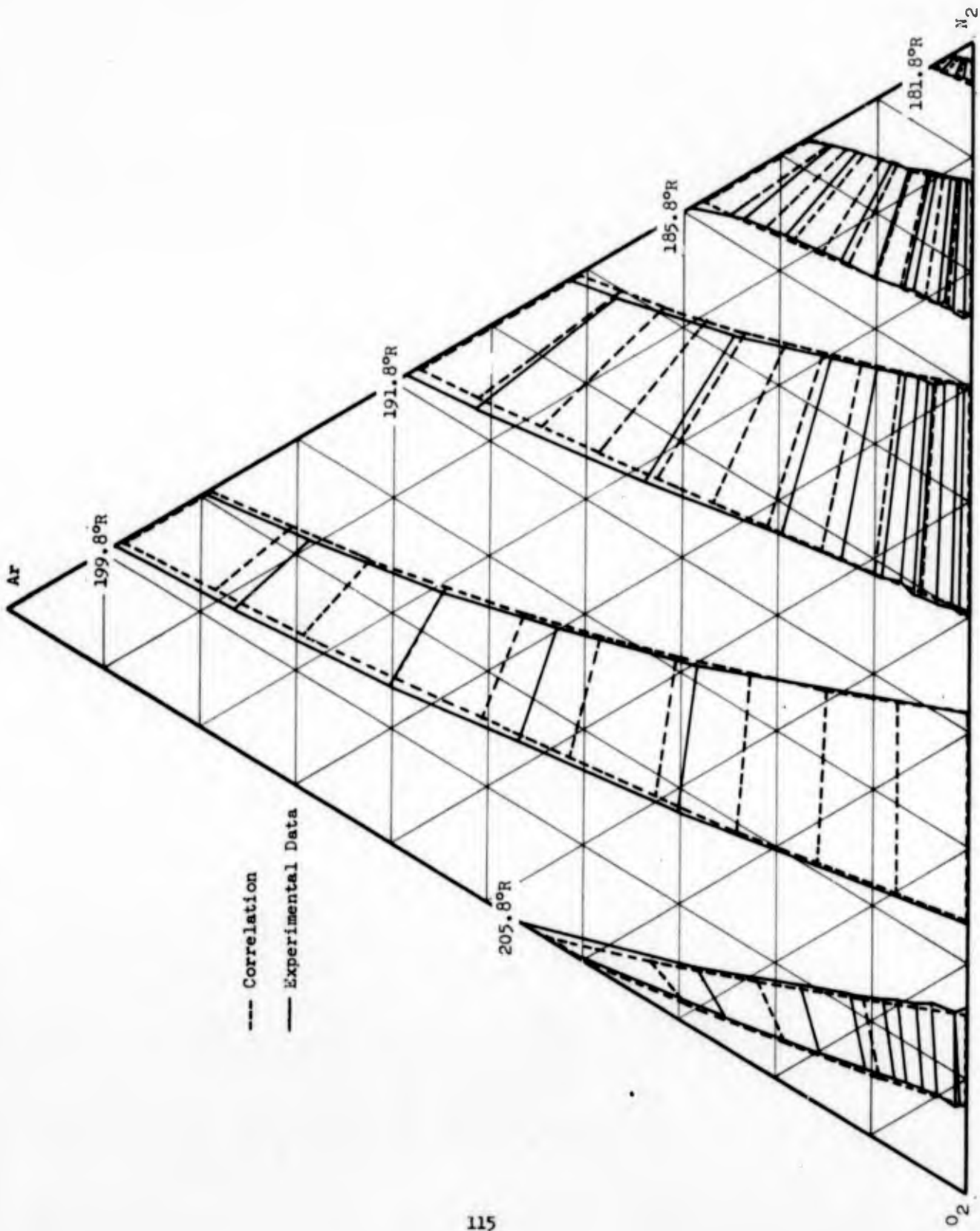


Figure 61. Comparison of Experimental Data and the Correlation, 8 Atmospheres.

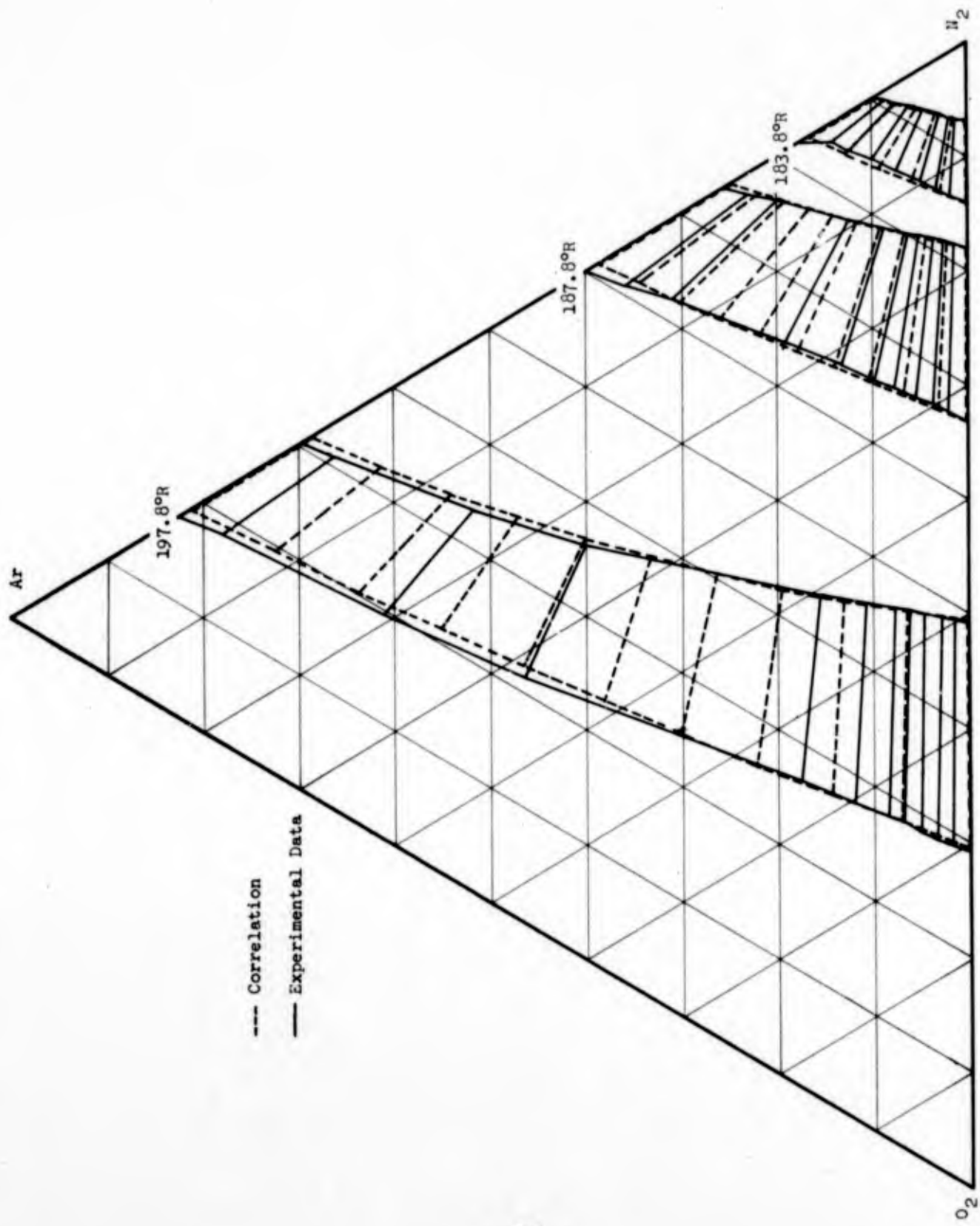


Figure 62. Comparison of Experimental Data and the Correlation, 8 Atmospheres.

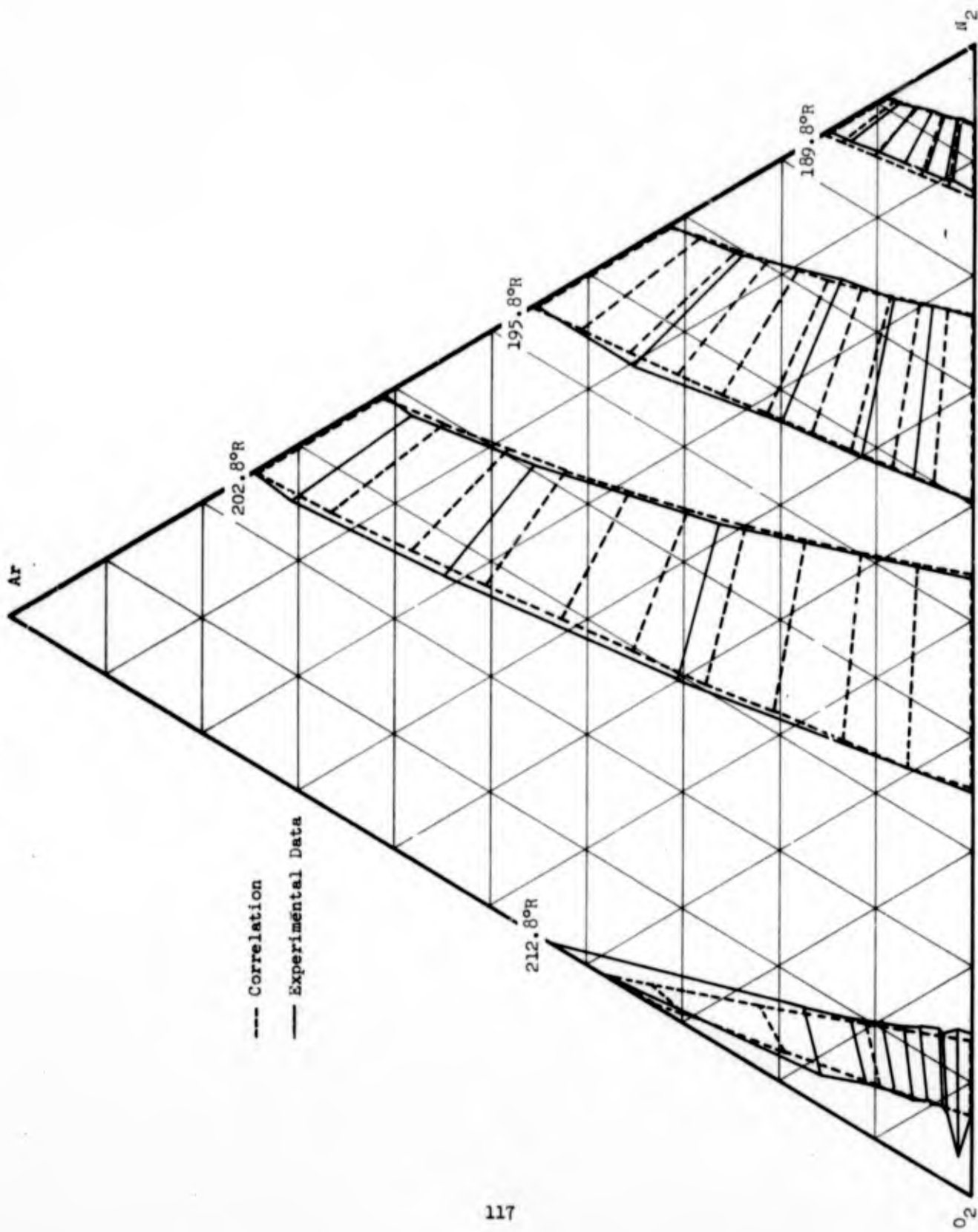


Figure 63. Comparison of Experimental Data and the Correlation, 10 Atmospheres.



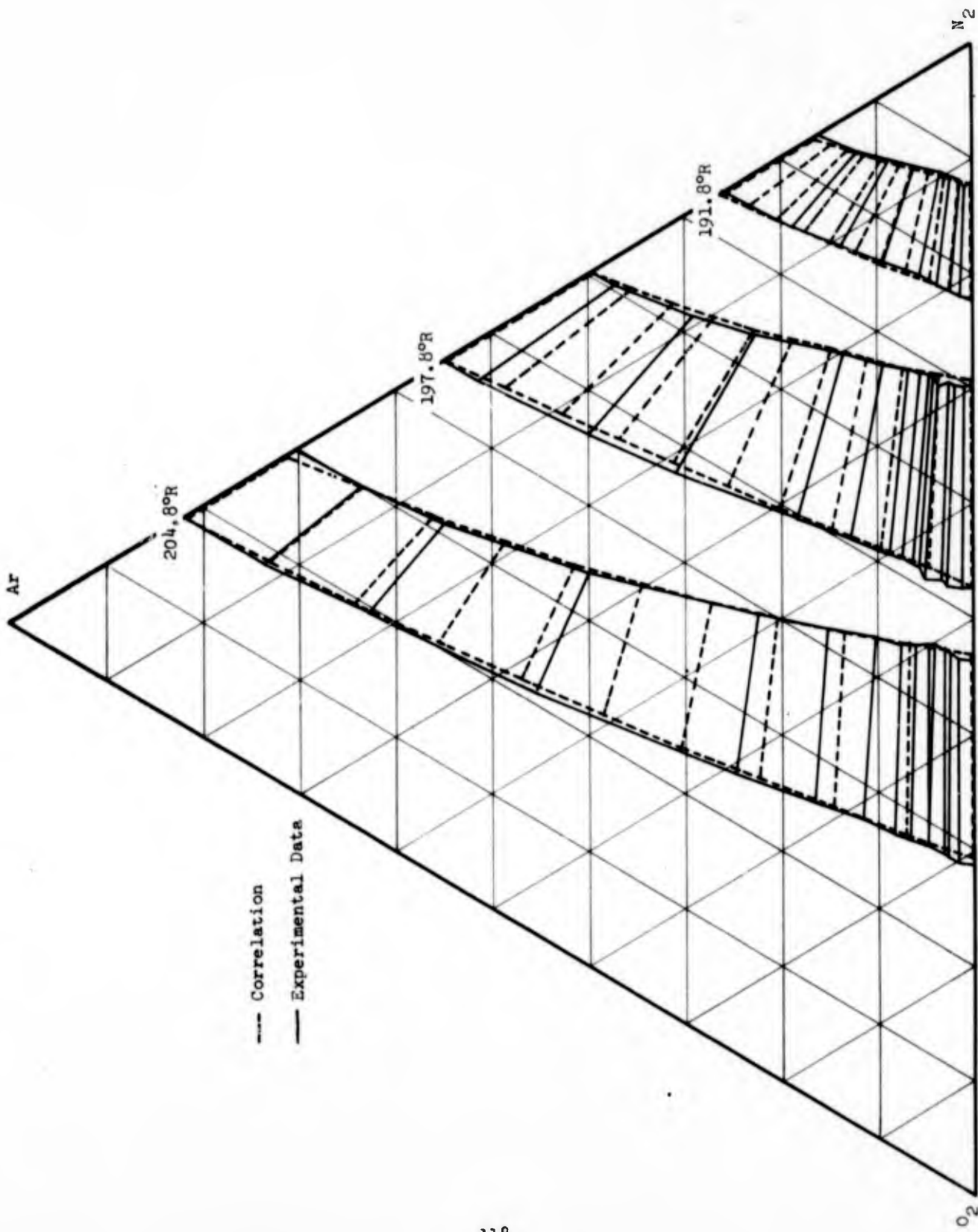


Figure 64. Comparison of Experimental Data and the Correlation, 10 Atmospheres.

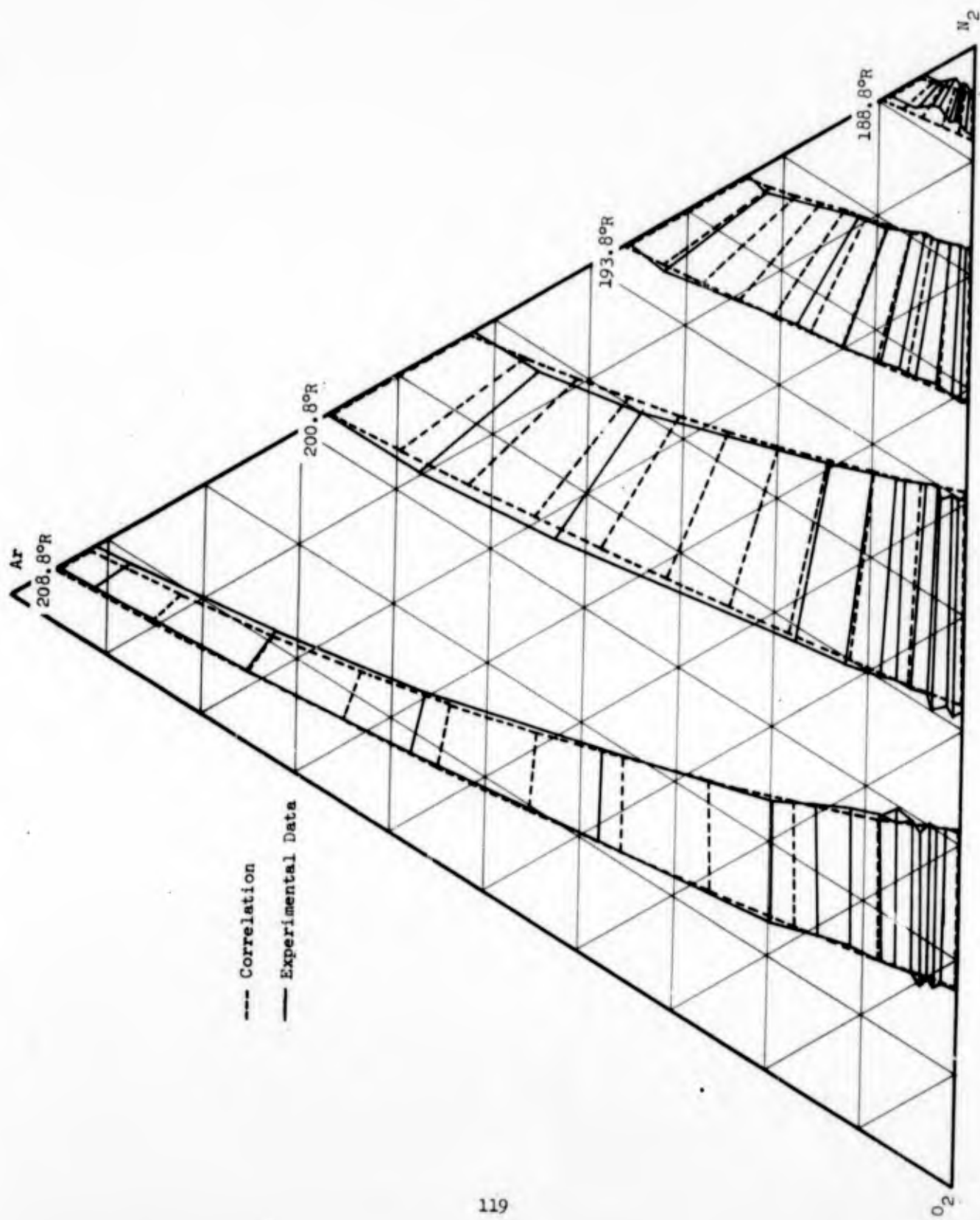


Figure 65. Comparison of Experimental Data and the Correlation, 10 Atmospheres.

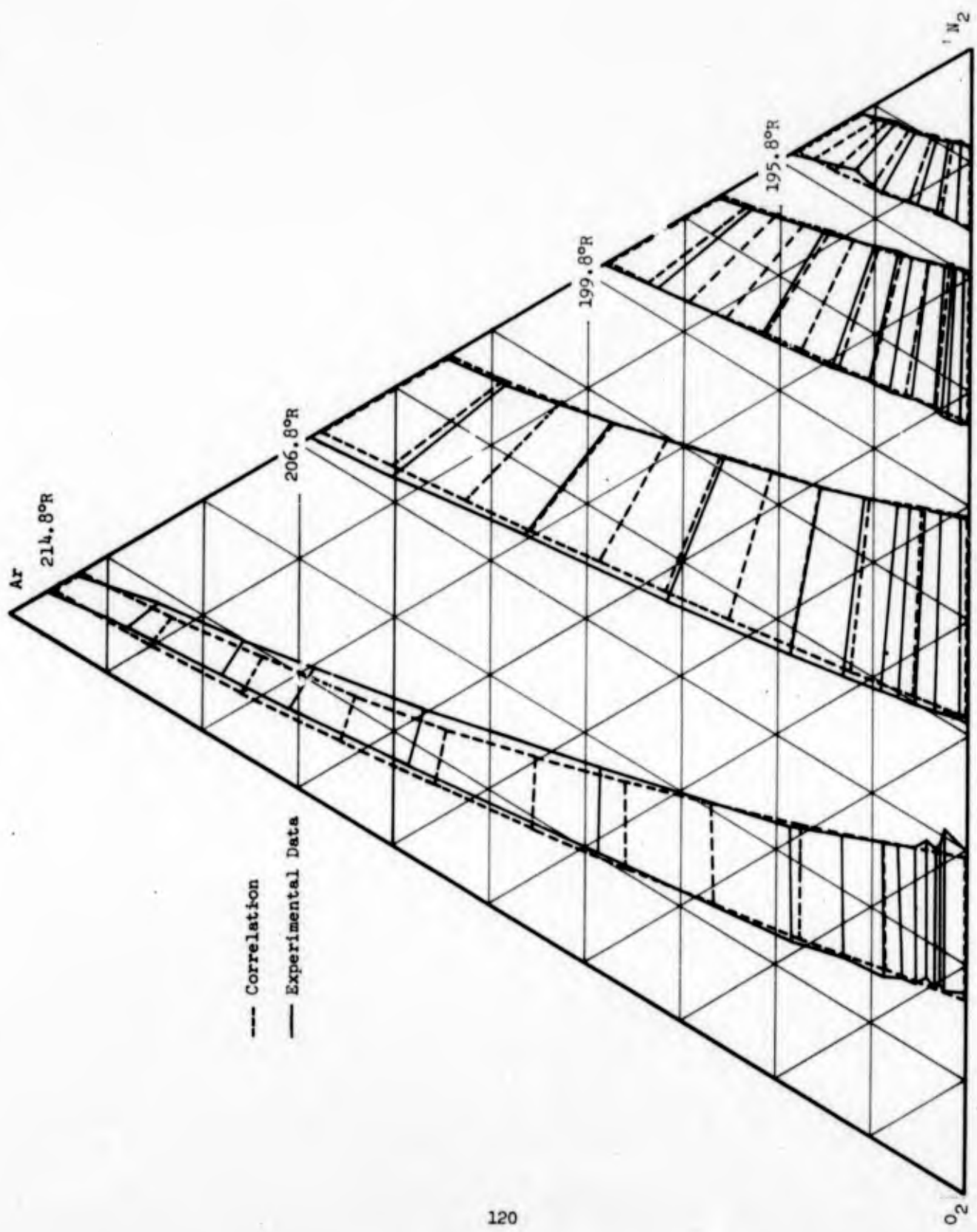


Figure 66. Comparison of Experimental Data and the Correlation, 12 Atmospheres.

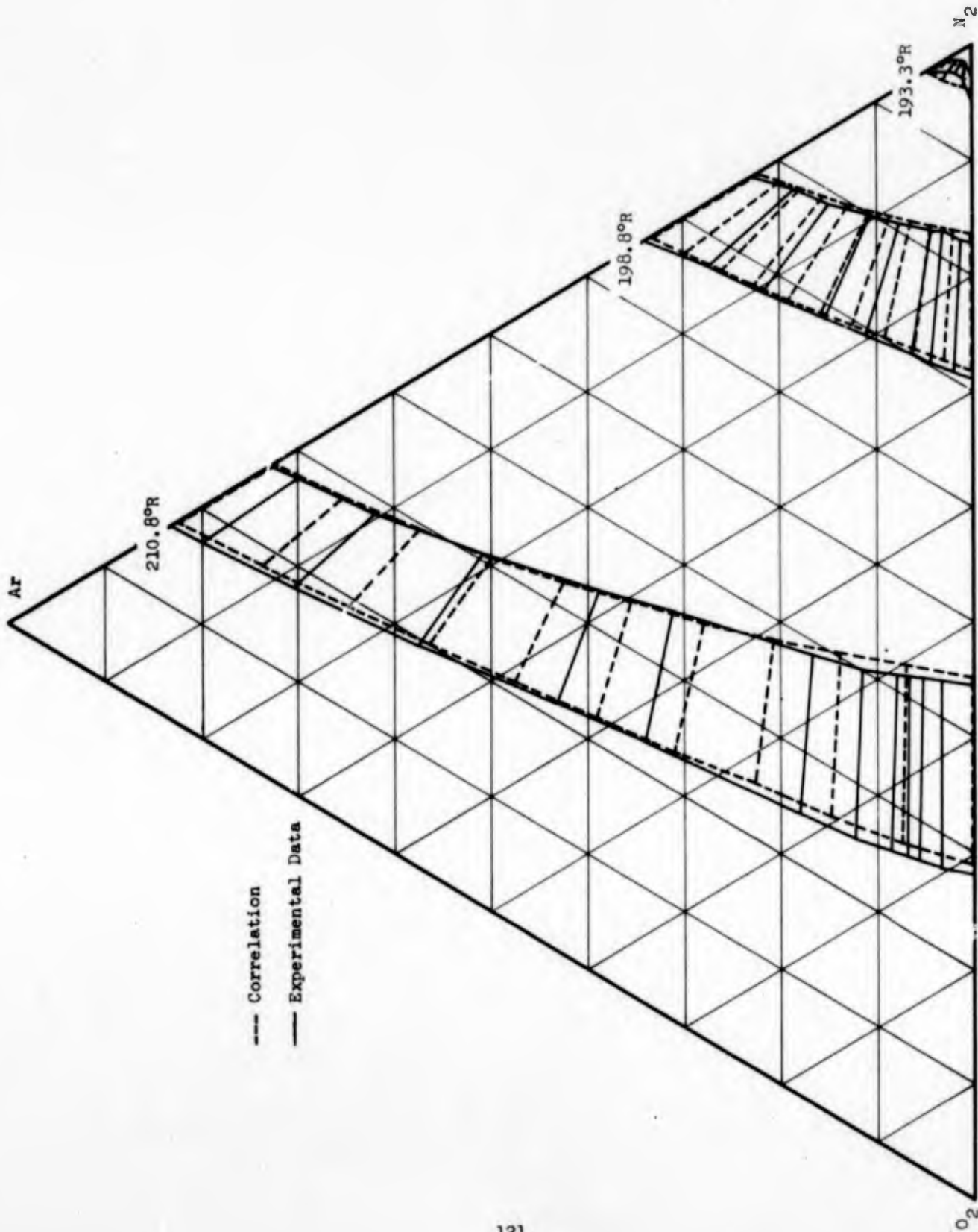


Figure 67. Comparison of Experimental Data and the Correlation, 12 Atmospheres.

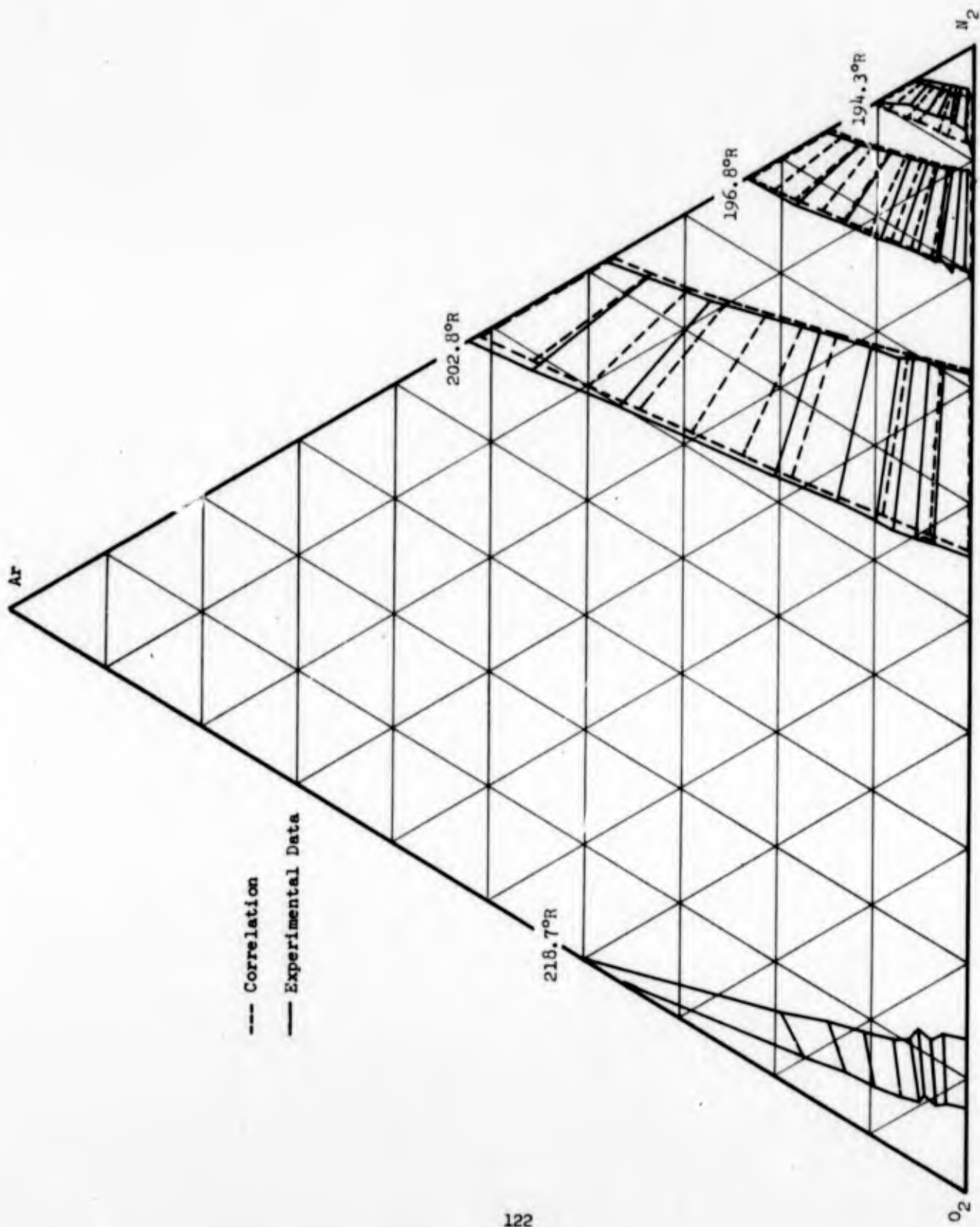


Figure 68. Comparison of Experimental Data and the Correlation, 12 Atmospheres.

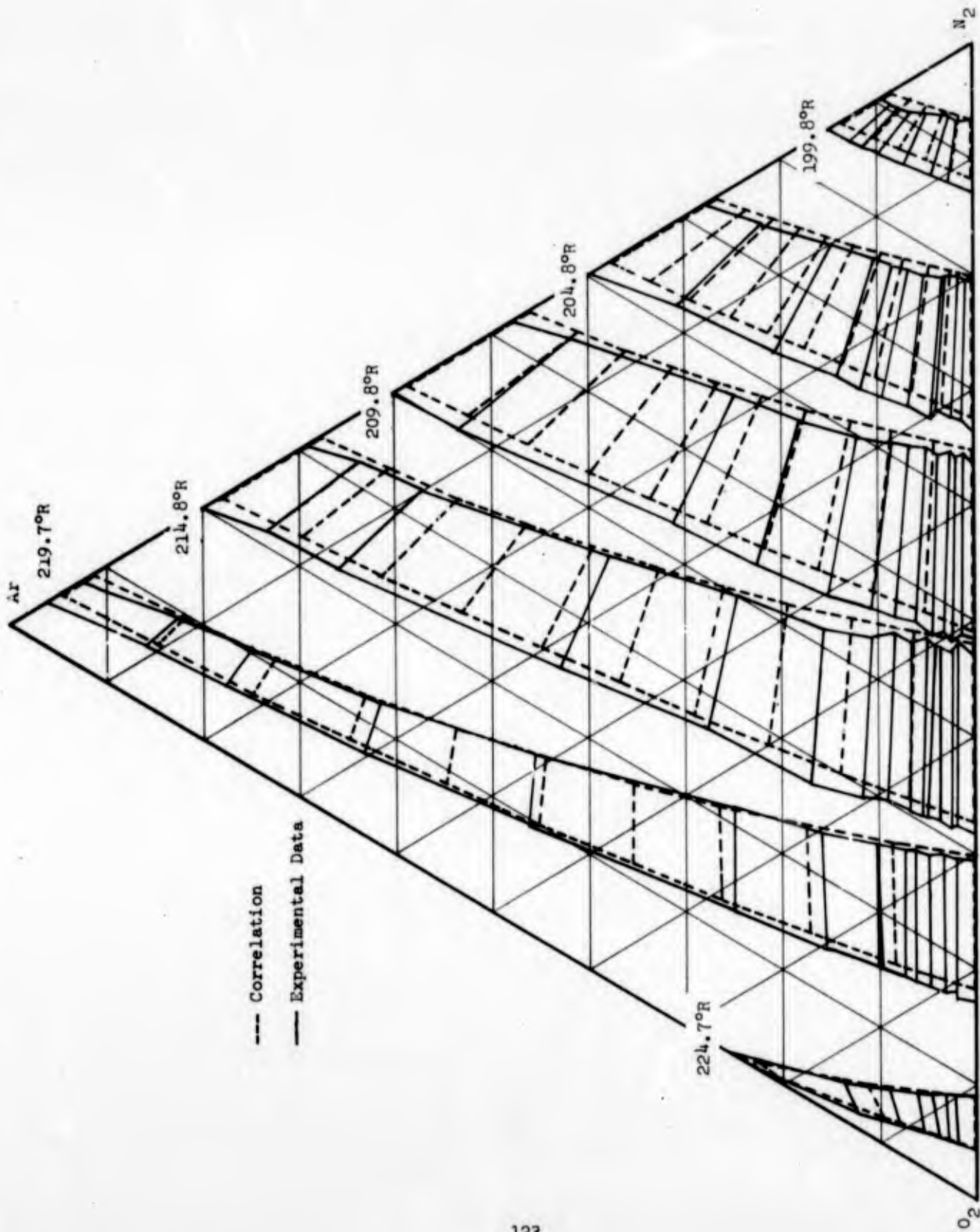


Figure 69. Comparison of Experimental Data and the Correlation, 14 Atmospheres.

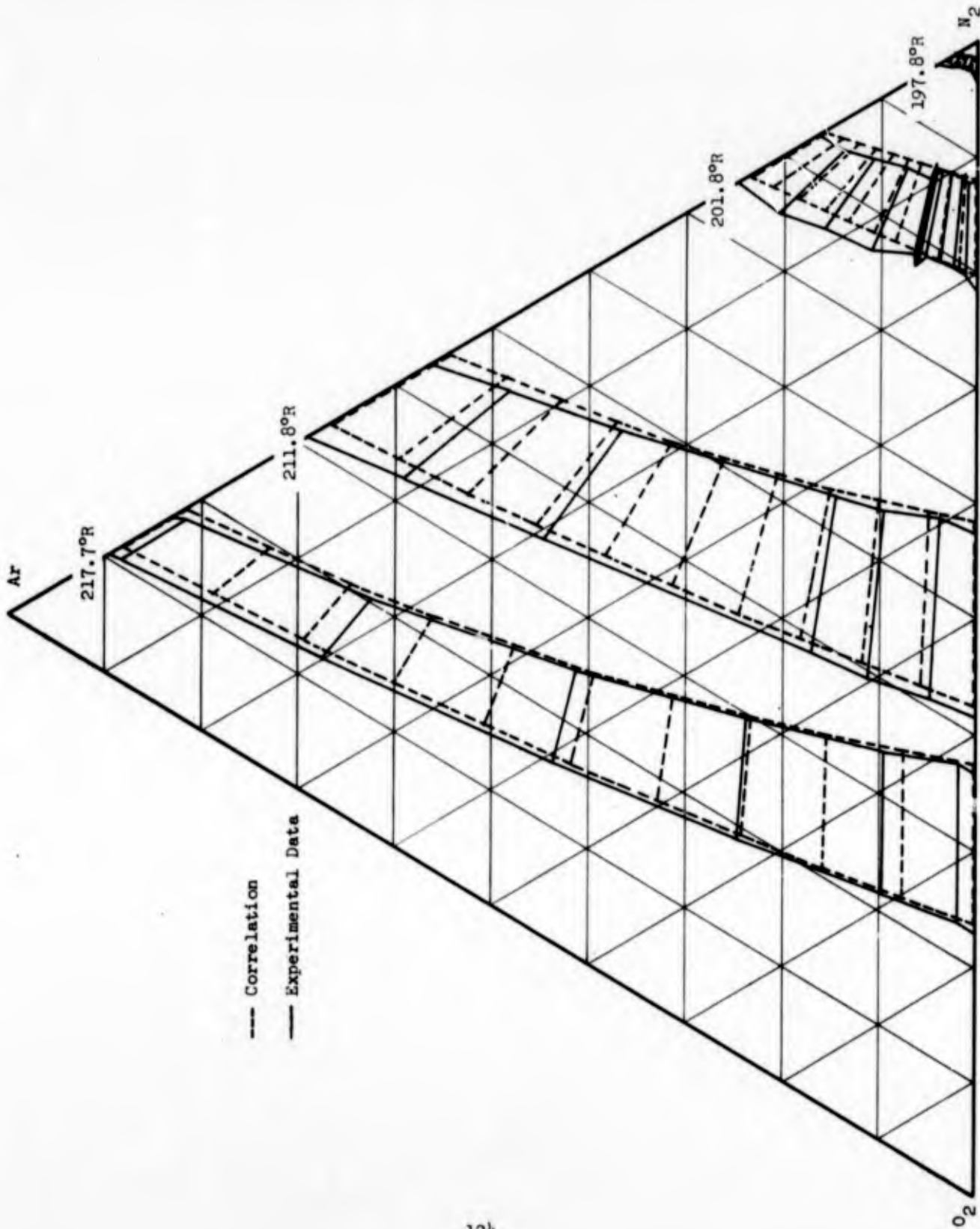


Figure 70. Comparison of Experimental Data and the Correlation, 14 Atmospheres.

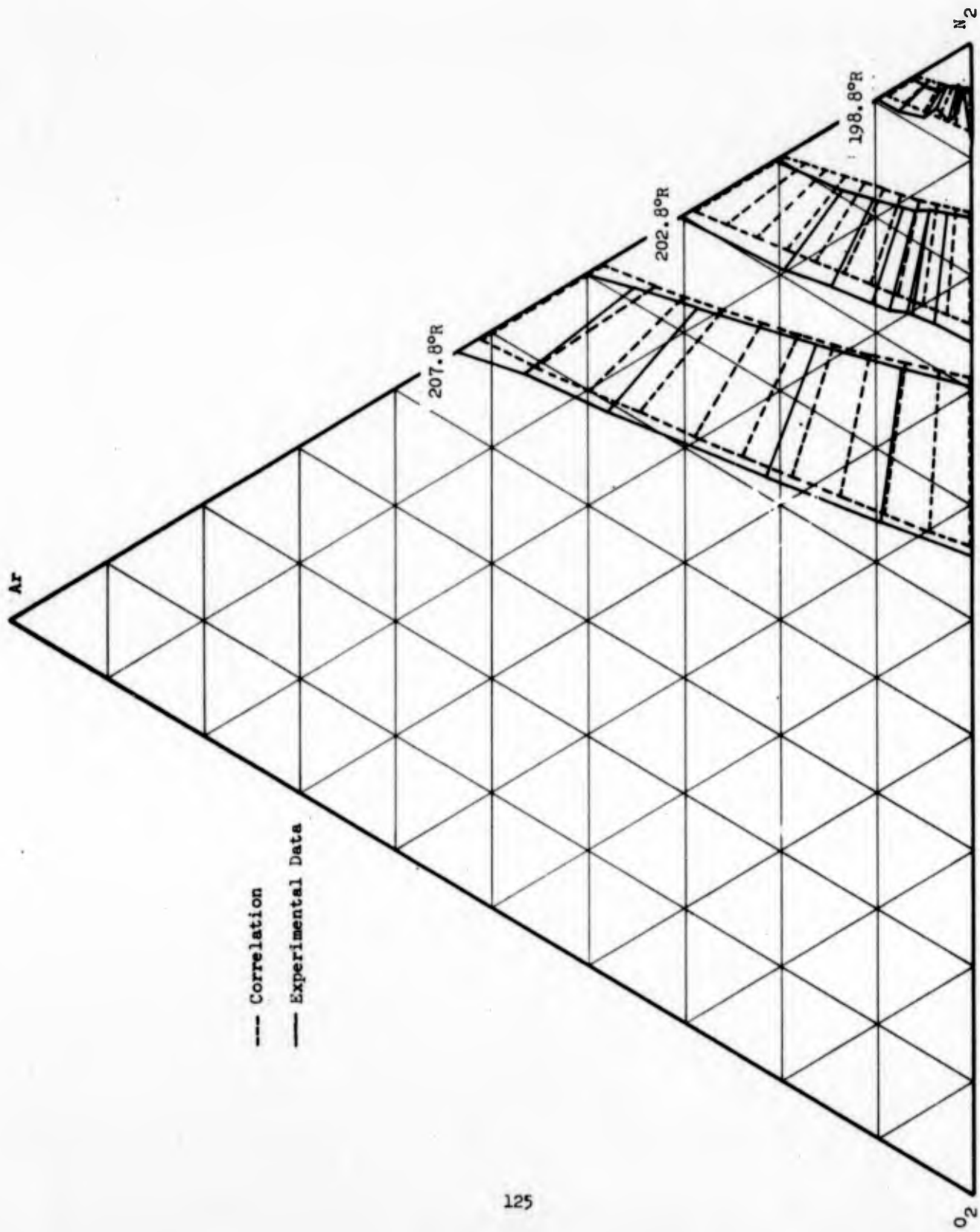


Figure 71. Comparison of Experimental Data and the Correlation, 14 Atmospheres.



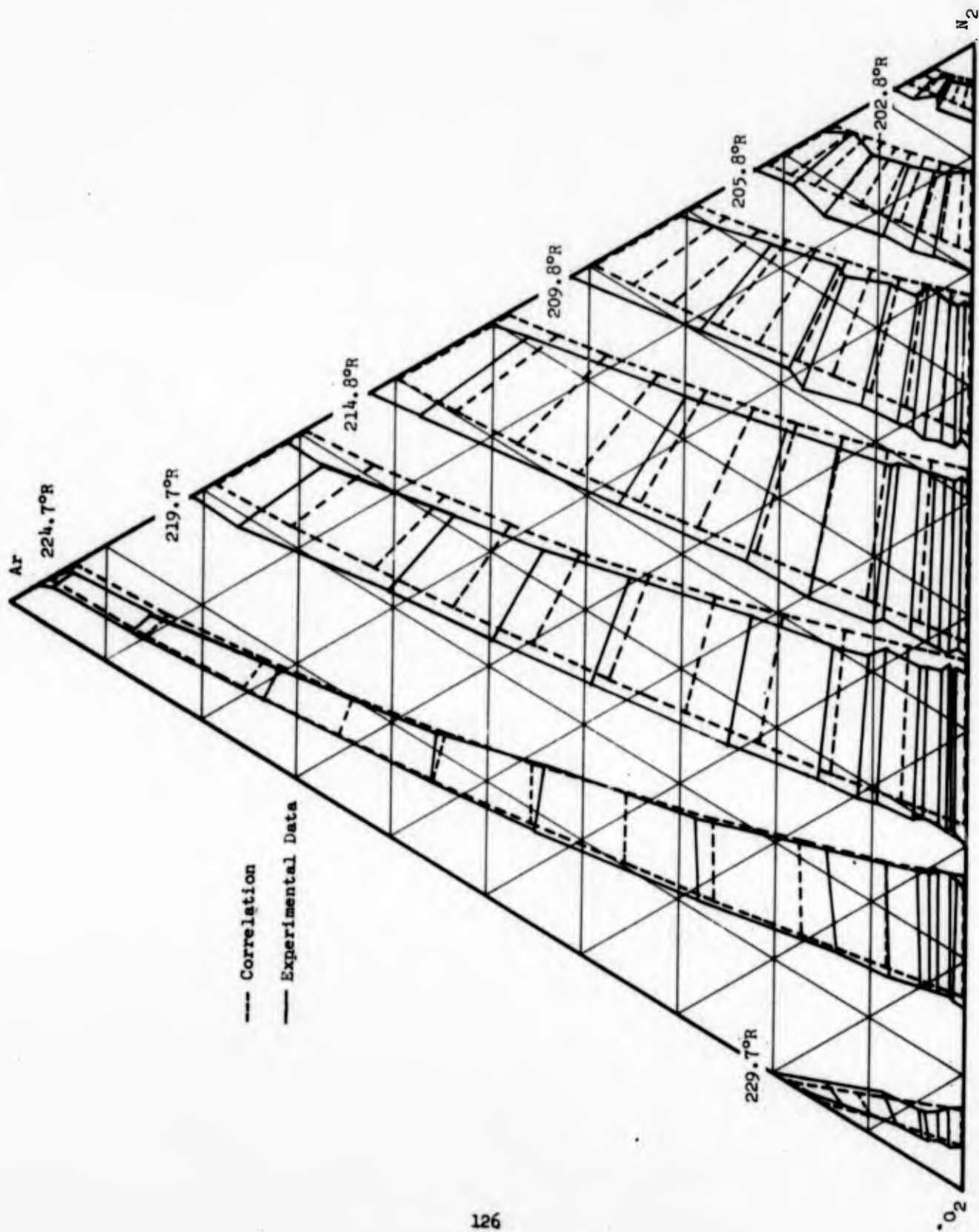


Figure 72. Comparison of Experimental Data and the Correlation, 16 Atmospheres.

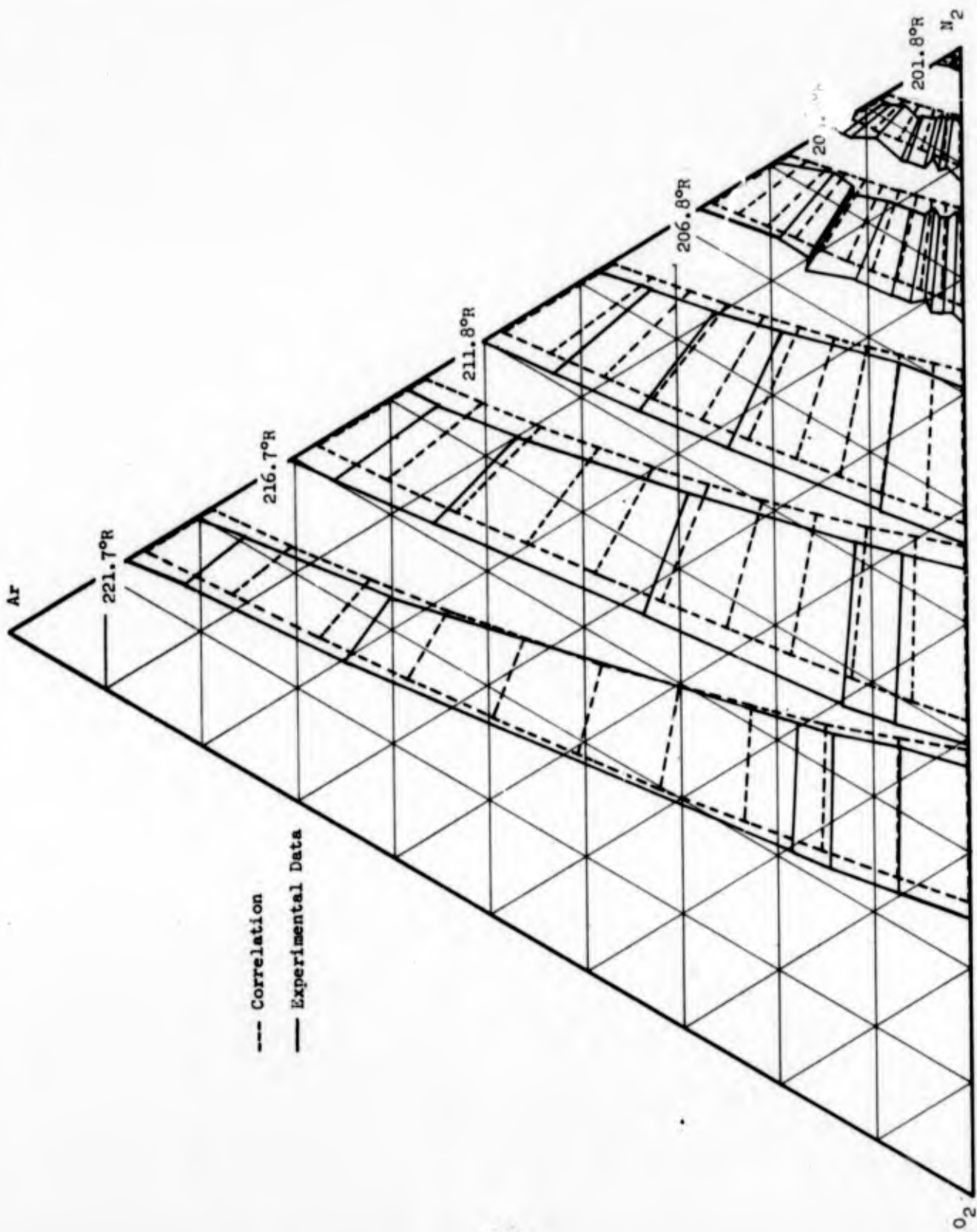
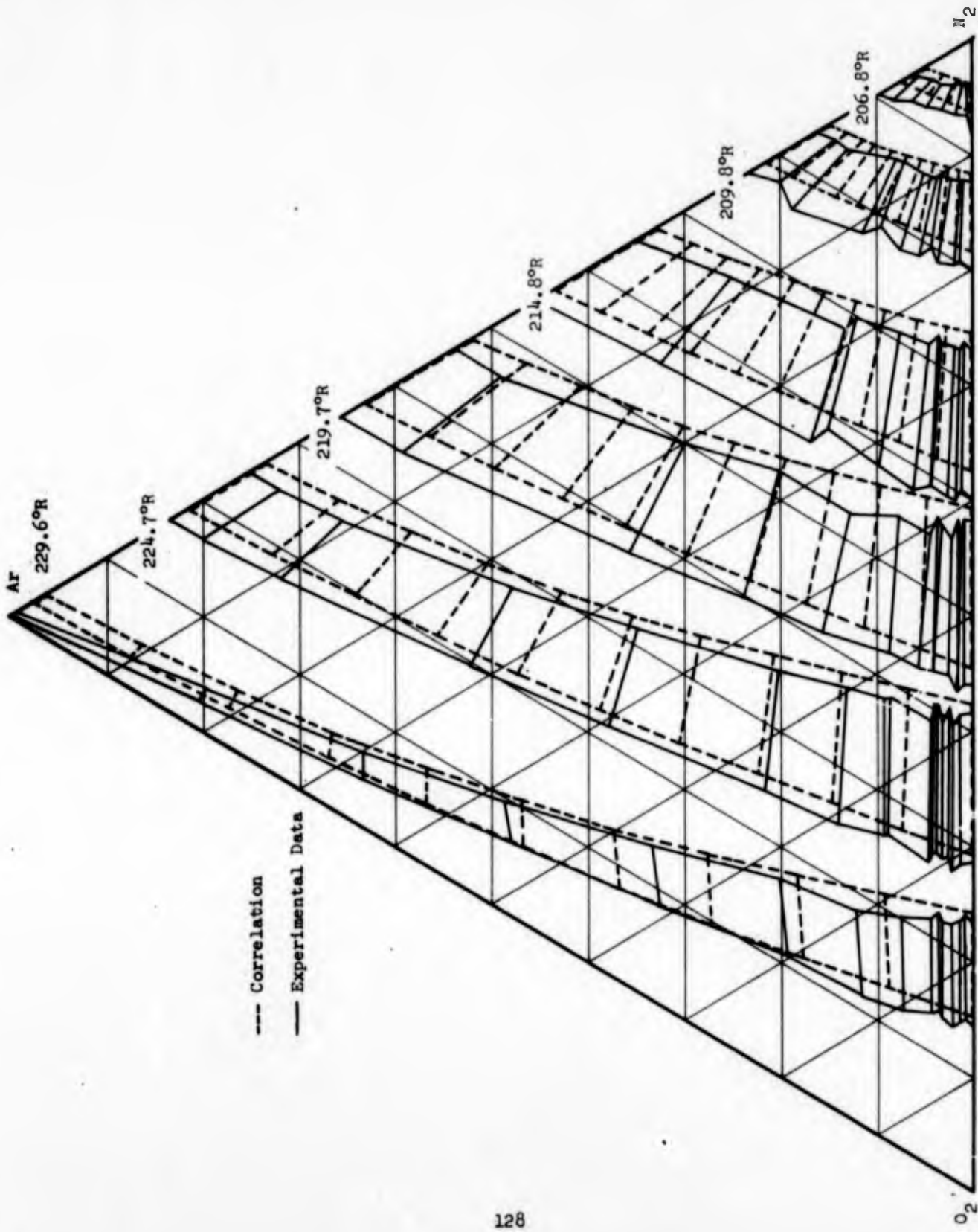


Figure 73. Comparison of Experimental Data and the Correlation, 16 Atmospheres.



--- Correlation  
 — Experimental Data

Figure 74. Comparison of Experimental Data and the Correlation, 18 Atmospheres.

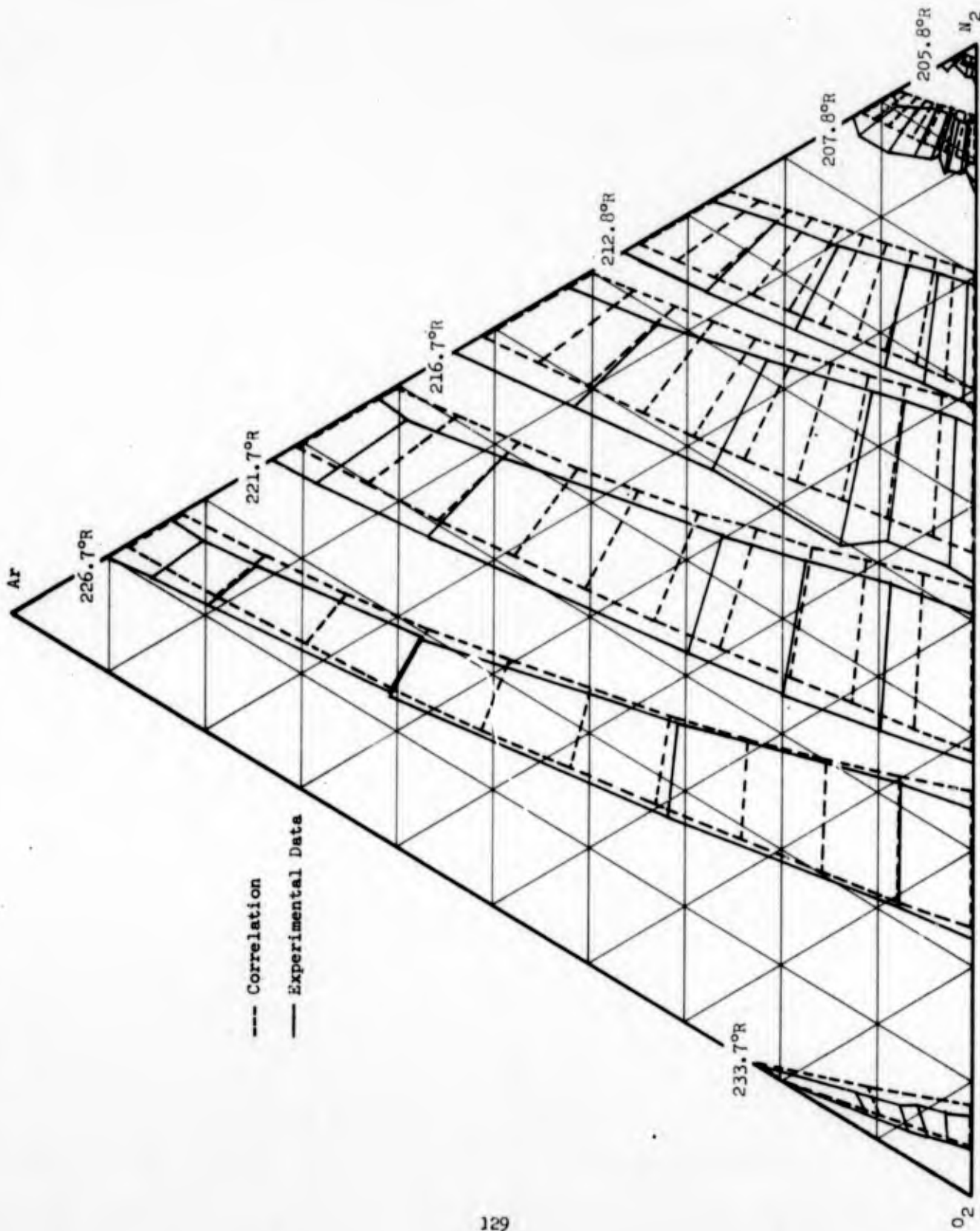


Figure 75. Comparison of Experimental Data and the Correlation, 18 Atmospheres.

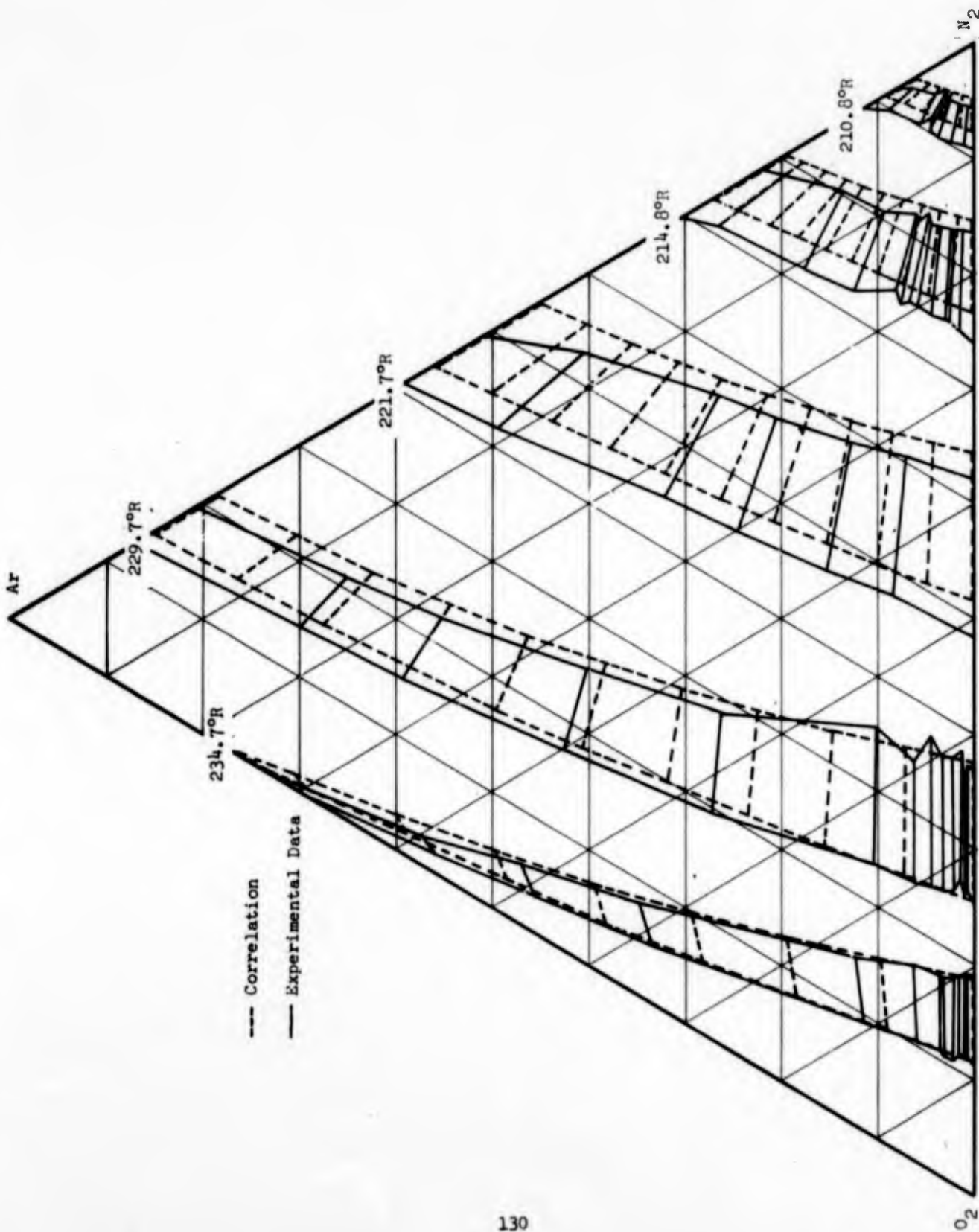


Figure 76. Comparison of Experimental Data and the Correlation, 20 Atmospheres.

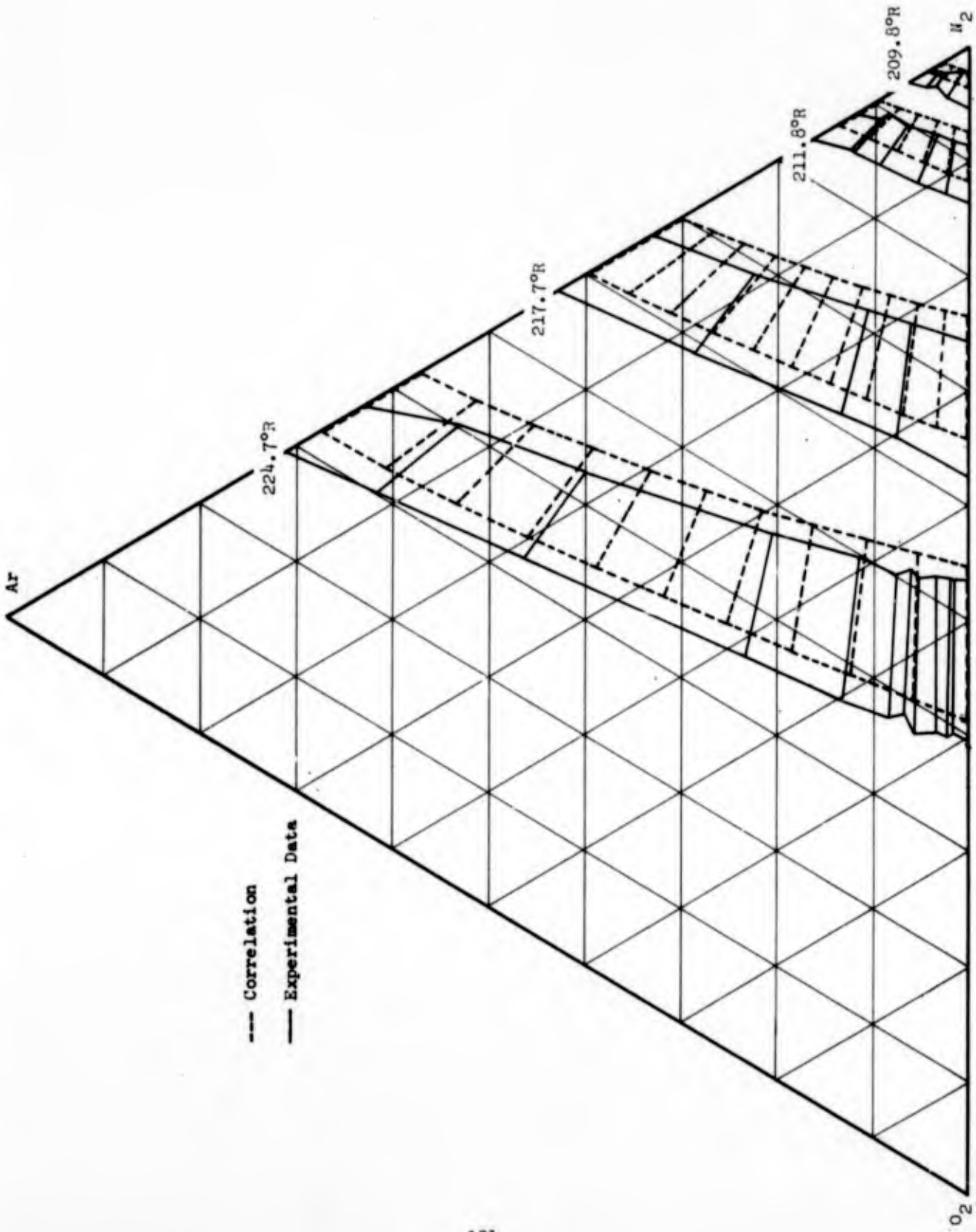


Figure 77. Comparison of Experimental Data and the Correlation, 20 Atmospheres.

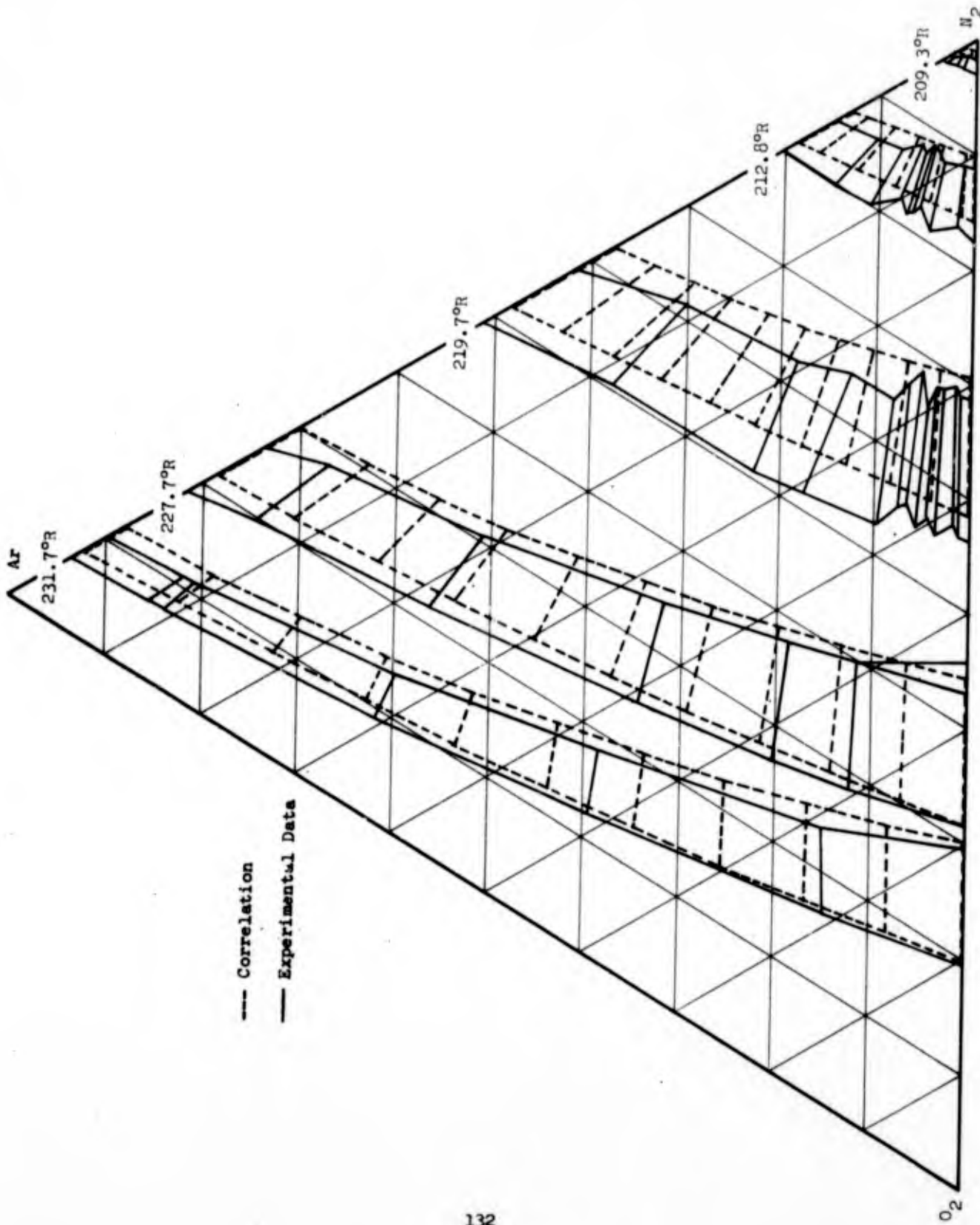


Figure 78. Comparison of Experimental Data and the Correlation, 20 Atmospheres.

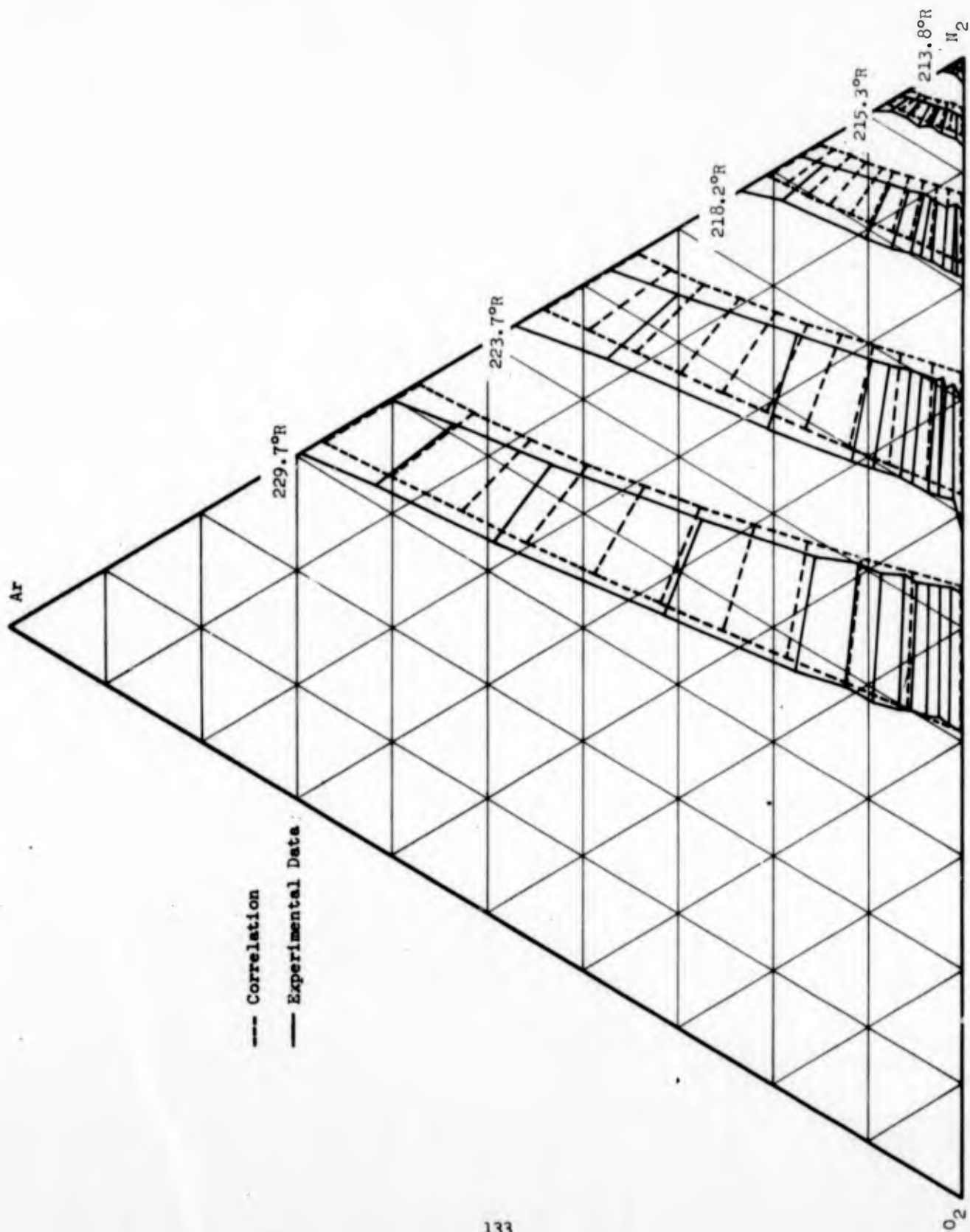


Figure 79. Comparison of Experimental Data and the Correlation, 23 Atmospheres.



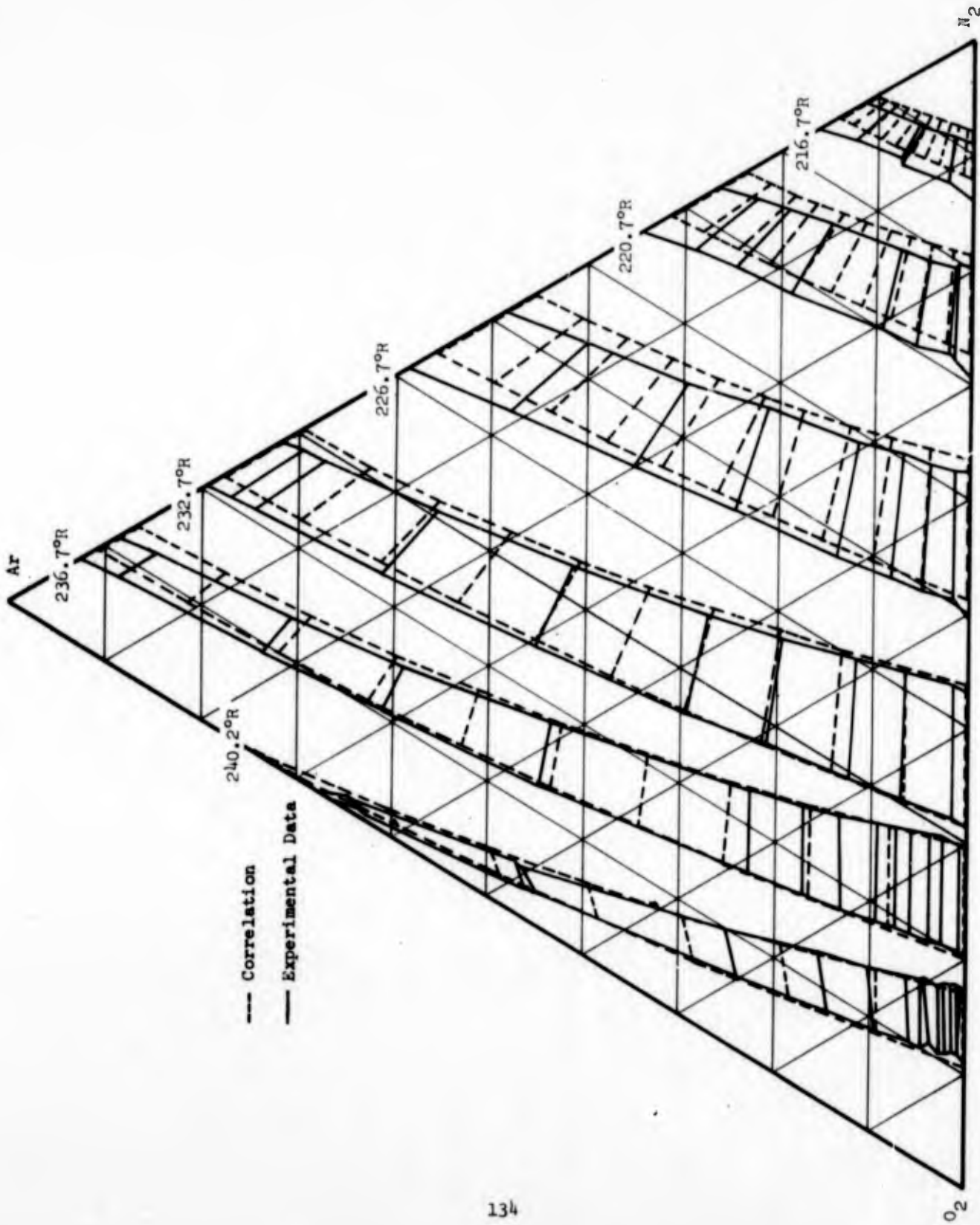


Figure 80. Comparison of Experimental Data and the Correlation, 23 Atmospheres.

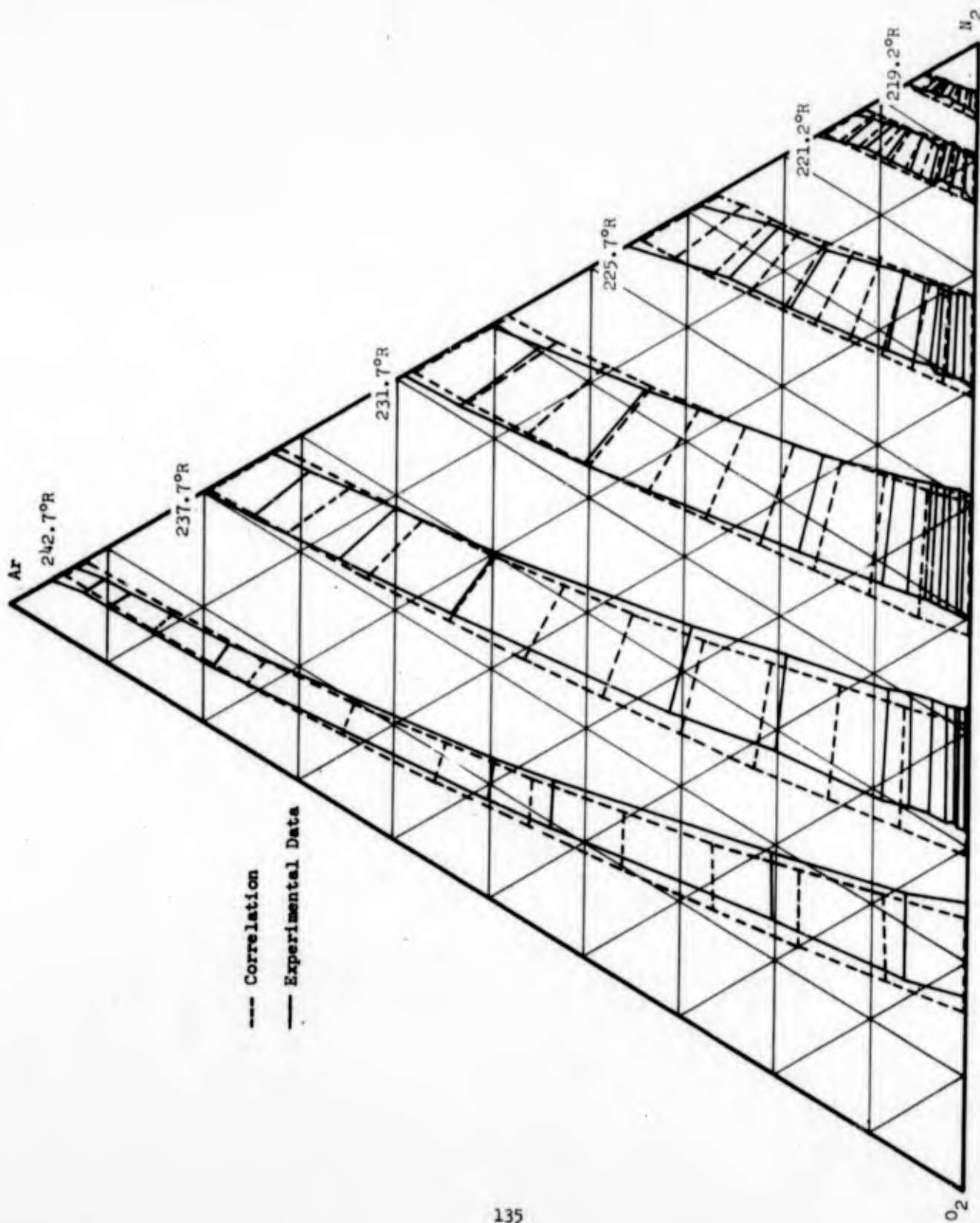


Figure 81. Comparison of Experimental Data and the Correlation, 26 Atmospheres.

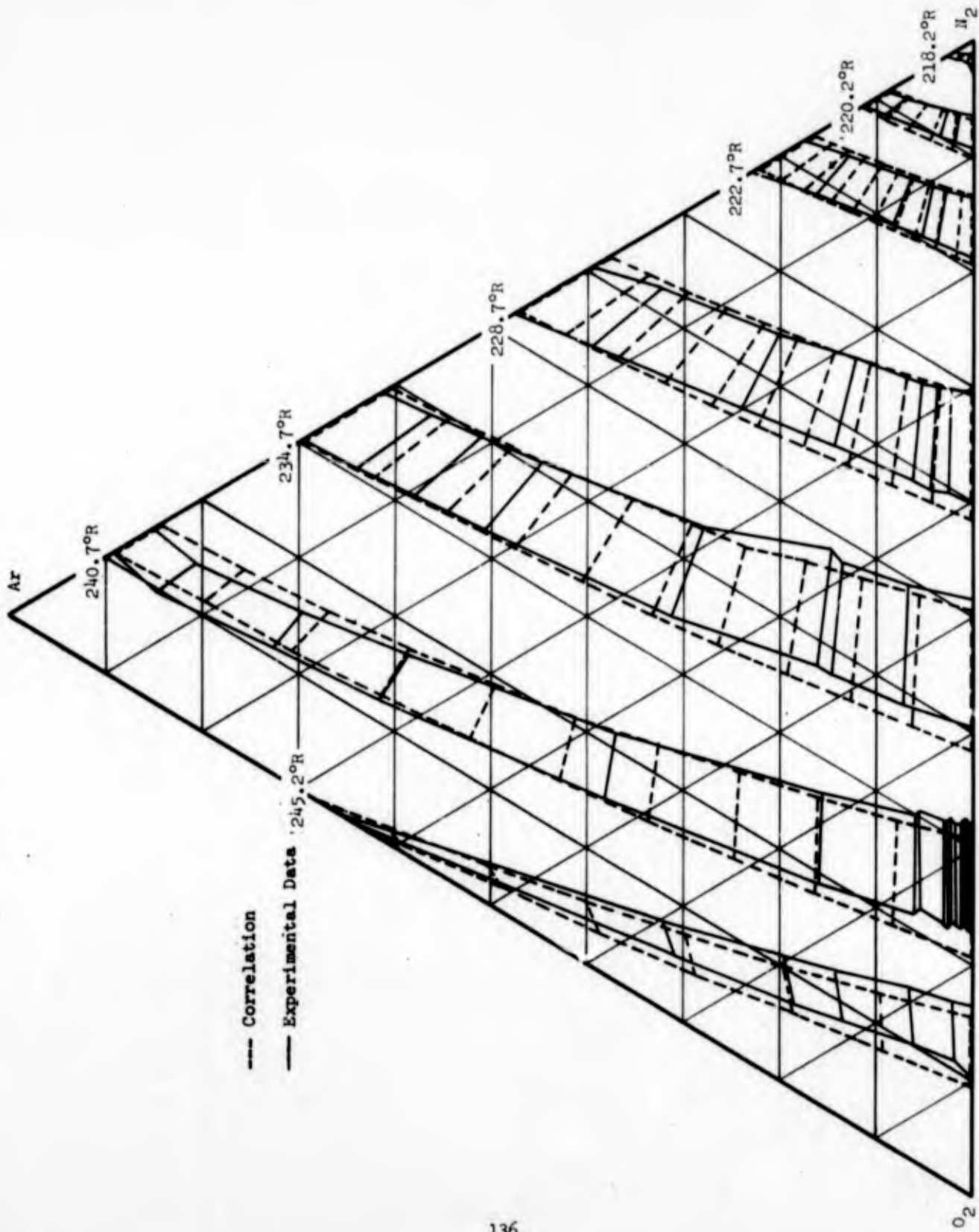


Figure 82. Comparison of Experimental Data and the Correlation, 26 Atmospheres.

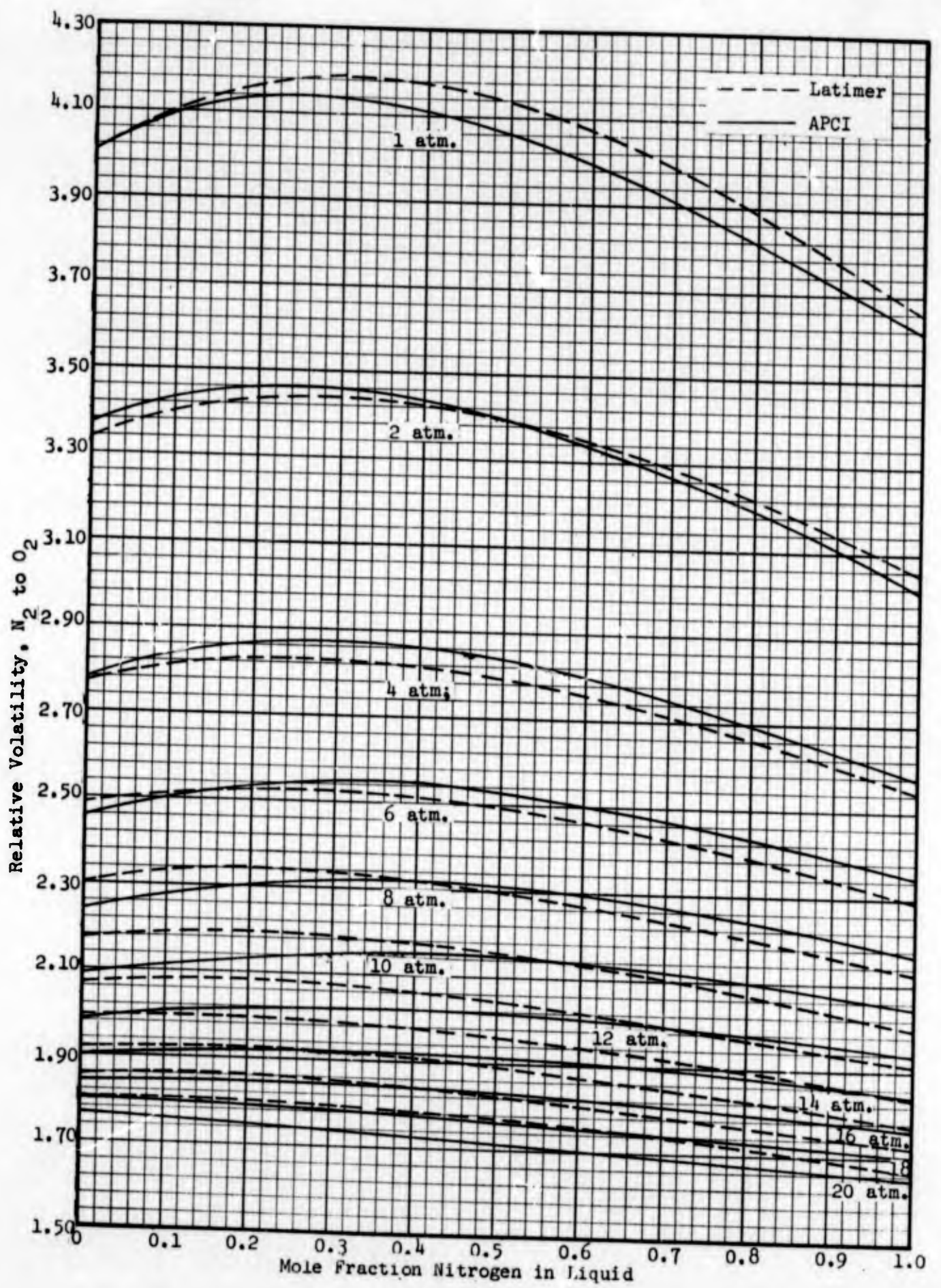


Figure 83. Comparison of APCI Correlation to Latimer Correlation for Nitrogen-Oxygen System.

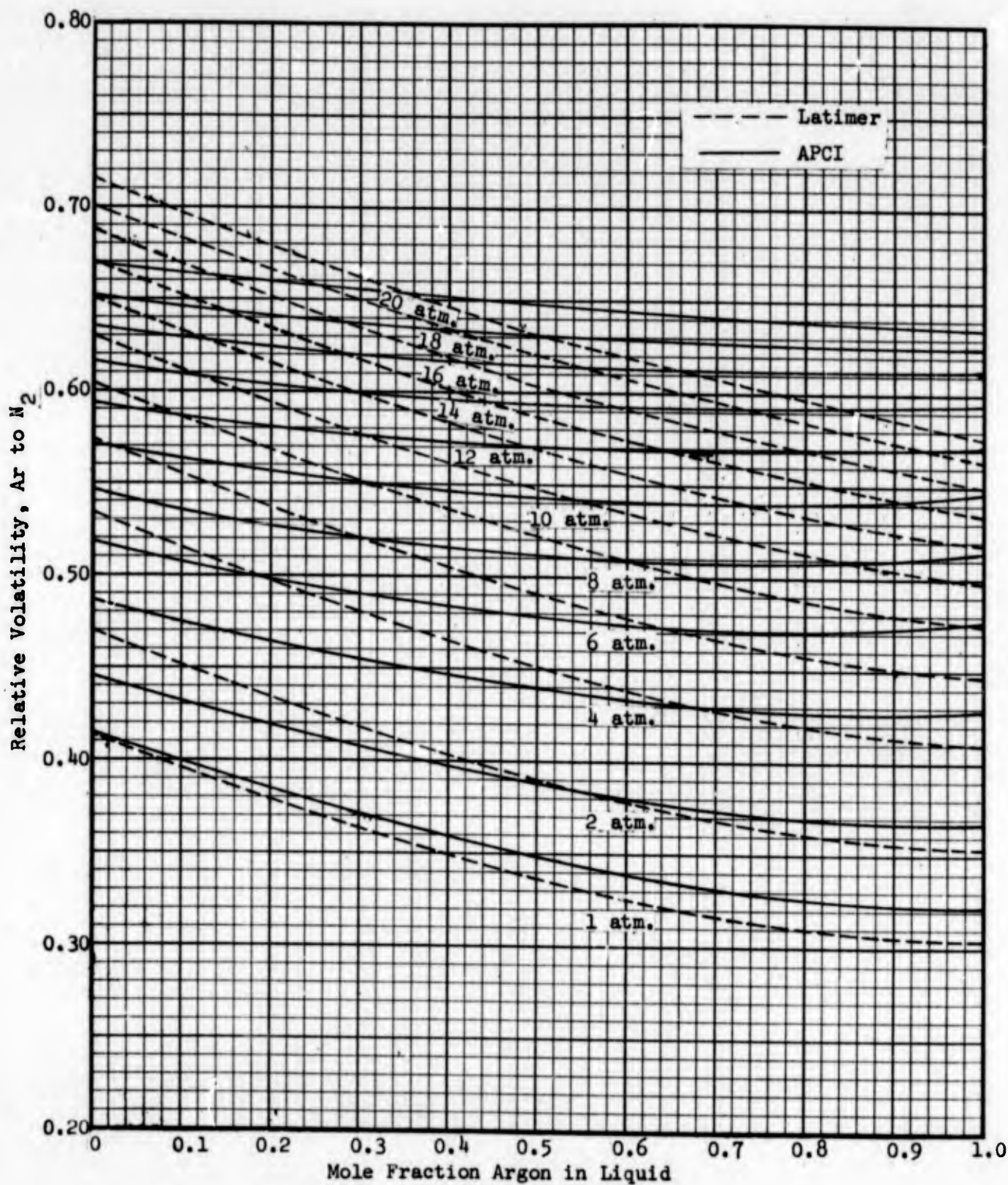


Figure 84. Comparison of APCI Correlation to Latimer Correlation for Argon-Nitrogen System.

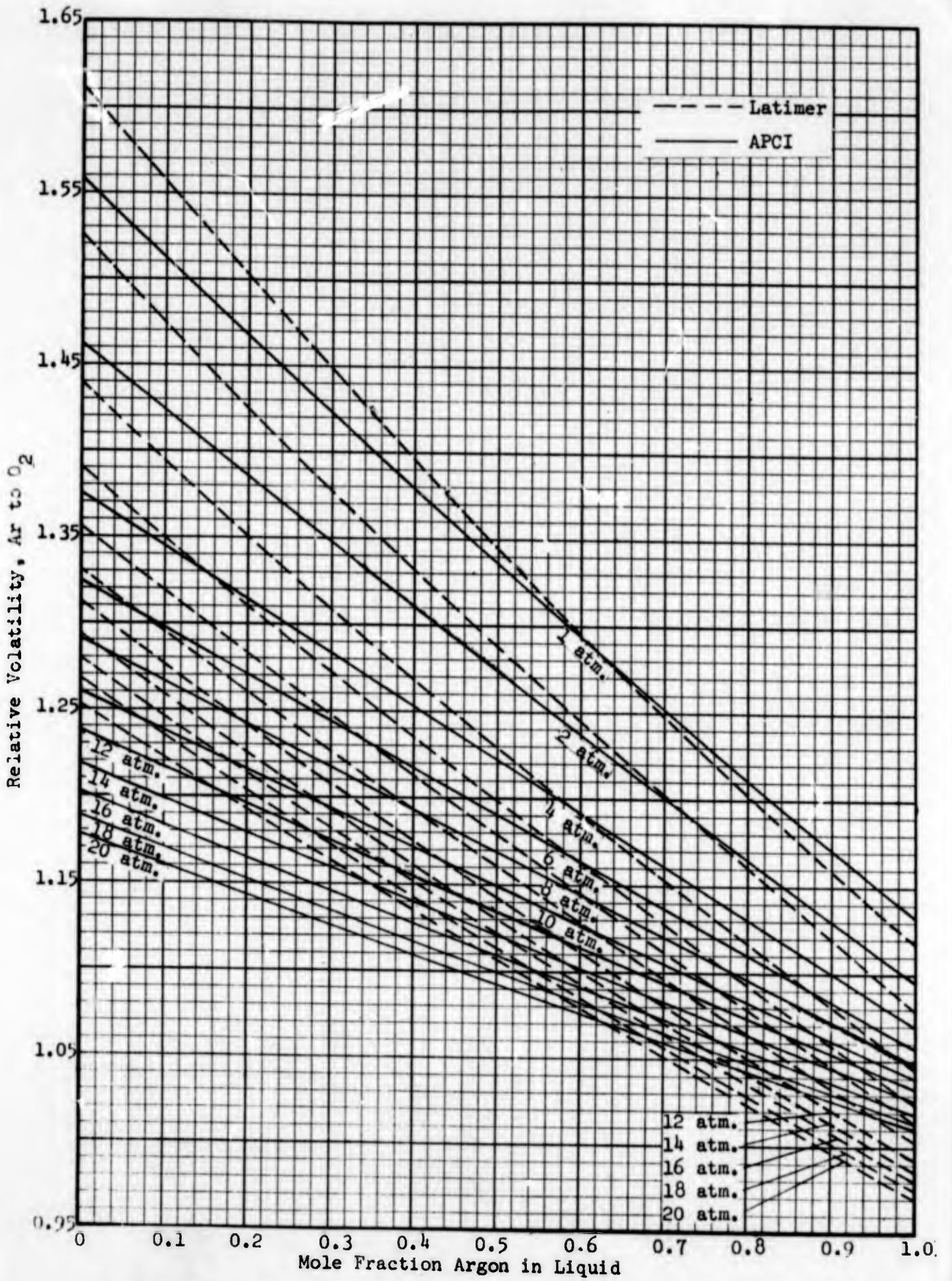


Figure 85. Comparison of APCI Correlation to Latimer Correlation for Argon-Oxygen System.

## VIII. ENTHALPY CORRELATION

Enthalpy data obtained from the literature were correlated for computer usage in calculating the enthalpy of the vapor and enthalpy of the liquid according to the equations

$$H_{\text{vap.}} = \sum_i x_i H_i^* + \sum_i x_i (H_{g_i} - H_i^*) \quad (22)$$

$$H_{\text{liq.}} = \sum_i x_i H_i^* + \sum_i x_i (H_{g_i}^{\circ} - H_i^*) - \sum_i x_i \Delta H_{vi}^{\circ} \\ + \sum_i x_i V_i^{\circ} (p - p_i^{\circ}) + \sum_i x_i \Delta \bar{H}_{m_i} \quad (23)$$

Reported below are the correlations to the data with referencing and commentary about accuracy.

 A. Heat of Mixing

1. Argon-Oxygen - The data of Pool and co-workers<sup>(35)</sup> at 84°K appear more consistent than that of Knobler and co-workers<sup>(36)</sup> at 86°K. Pool's least squares fit of the data converted to BTU/lb-mole is:

$$H_m = x_{O_2} x_{Ar} [103 + 13.5 (x_{O_2} - x_{Ar})] \quad (24)$$

2. Nitrogen-Argon - The only data found were that of Pool and co-workers<sup>(35)</sup> at 84°K. Their least squares fit converted to BTU/lb-mole is:

$$H_m = x_{Ar} x_{N_2} [86.9 - 23.2 (x_{Ar} - x_{N_2})] \quad (25)$$

3. Nitrogen-Oxygen - The only data found were that of Knobler, van Heijningen and Beenakker<sup>(36)</sup> at 77°K. Weighting the points at oxygen mole fraction of 0.14 half as heavily as the rest, a method of averages curve fit gives within 10% accuracy:

$$H_m = x_{N_2} x_{O_2} [82.8 + 29 (x_{O_2} - x_{N_2})] \text{ BTU/lb-mole.} \quad (26)$$

For a heat of mixing of the form  $H_m = x_1 x_2 [A + B (x_1 - x_2)]$ , the partial molal heat of mixing is:

$$\overline{\Delta H_{m1}} = x_2^2 [A + B (3x_1 - x_2)] \quad (27)$$

$$\overline{\Delta H_{m2}} = x_1^2 [A + B (x_1 - 3x_2)] \quad (28)$$

B. Ideal Gas Heat Capacity 140-250°R

1. Argon - from Nat. Bur. Stds.<sup>(37)</sup>:  $C_p^\circ = 4.9647 \text{ BTU/mole } ^\circ\text{R}$  (29)

2. Oxygen - tabulation by Wooley<sup>(38)</sup>:  $C_p^\circ = 6.9558 \text{ BTU/mole } ^\circ\text{R}$  (30)

3. Nitrogen - from Goff and Gratch<sup>(39)</sup>. Least squares curve fit:  
 $C_p^\circ = 6.950571 + 0.27735687 \times 10^{-5}T + 0.3438922 \times 10^{-8}T^2$  (31)  
 Sum of squares error =  $1 \times 10^{-9}$ .

C. Latent Heat

1. Nitrogen - The correlation is a least squares curve fit of the data from Mage, Jones, Katz, and Roebuck<sup>(40)</sup> and of Strobridge<sup>(41)</sup>  
 $\Delta H_{vi}^\circ$  in BTU/lb-mole, T in °R.

$$\ln \Delta H_{vi}^\circ = 6.36376 + 0.121474 \ln (226.91 - T) + 0.0880106 [\ln (226.91 - T)]^2 - 0.00987388 [\ln (226.91 - T)]^3 \quad (32)$$

Root mean square error = 8.1 BTU/lb-mole

A simpler fit is:  $\ln \Delta H_{vi}^\circ = 6.19701 + 0.354836 \ln (226.91 - T)$  (33)

Root mean square error = 22 BTU/lb-mole

2. Argon - The correlation is a least squares curve fit of the data of Flubacher, Leadbetter, and Morrison<sup>(42)</sup> and of Din<sup>(4)</sup>.

$\Delta H_{vi}^\circ$  in BTU/lb-mole, T in °R

$$\ln \Delta H_{vi}^\circ = 7.35231 - 0.733687 \ln (271.30 - T) + 0.331584 [\ln (271.30 - T)]^2 - 0.0317968 [\ln (271.30 - T)]^3 \quad (34)$$

Root mean square error = 2.8 BTU/lb-mole

A simpler fit is:  $\ln \Delta H_{vi}^\circ = 6.20952 + 0.366142 \ln (271.30 - T)$  (35)

Root mean square error = 27.6 BTU/lb-mole



3. Oxygen - The correlation is a least squares fit synthesized from the data given by Fukurawa and McCoskey<sup>(43)</sup>, Alikhanov<sup>(44)</sup>, Claitor and Crawford<sup>(45)</sup> and the graphical data of Wilbers<sup>(46)</sup>.

$\Delta H_{vi}^{\circ}$  in BTU/lb-mole, T in °R

$$\ln \Delta H_{vi}^{\circ} = 5.61017 + 0.733877 \ln (278.60 - T) - 0.0572340 [\ln (278.60 - T)]^2 + 0.0016562 [\ln (278.60 - T)]^3 \quad (36)$$

Root mean square error = 6.9 BTU/lb-mole

$$\text{A simple fit is: } \ln \Delta H_{vi}^{\circ} = 6.16014 + 0.384736 \ln (278.60 - T) \quad (37)$$

Root mean square error = 77 BTU/lb-mole

- D. Enthalpy of the Real Gas - The commonly used symbol  $(H - H^*)_T$  represents the effect of pressure at constant temperature on the enthalpy of a real gas. This quantity can be computed from the virial equation of state terminating with the third virial coefficient.

$$\frac{PV}{RT} = Z = 1 + \frac{B}{V} + \frac{C}{V^2} \quad (38)$$

Since B and C are functions of temperature only, the following equation is derived:

$$\frac{(H_{gi} - H_i^*)_T}{RT} = \left[ \frac{1}{V} (B - T \frac{dB}{dT}) + \frac{1}{V^2} (C - \frac{1}{2} T \frac{dC}{dT}) \right] \quad (39)$$

The coefficients for argon, oxygen, and nitrogen are given in Section VID.

- E. Saturated Pure Component Heat Capacity

1. Argon Liquid - from WADD Compendium<sup>(5)</sup>

$$C_p = 0.22 + 0.00468 \frac{T}{(151 - T)^{1/2}} \quad (40)$$

$C_p$  units cal/gm-°K, T in °K

2. Oxygen Liquid - insufficient data to correlate.

3. Nitrogen Liquid - Correlation of Strobridge<sup>(41)</sup>

$$C_s = \frac{6.24688186T}{(126.26-T)^2} + 39.39006895 + 0.6821295539T - 0.01052432772T^2 \quad (41)$$

$$+ 0.00006001046981T^3$$

$C_s$  units joule/gm-mole °K, T in °K

4. Argon Vapor - from Din<sup>(4)</sup>

$$C_s = 325.63362 - 8.8669510T + 0.08828184T^2 - 0.00031196544T^3 \quad (42)$$

$C_s$  units joule/gm-mole °K, T in °K

5. Oxygen Vapor - from Claitor and Crawford<sup>(45)</sup>

$$C_s = -468.26228 - 2.6649068T + 0.010328679T^2 + 9.0958184 \times 10^{-5}T^3 \quad (43)$$

$$+ 1.4860065 \times 10^{-7}T^4$$

$C_s$  units BTU/lb-mole °F, T in °F

6. Nitrogen Vapor - from Strobridge<sup>(41)</sup>

$$C_s = 48.332643 - 0.7791322T - 0.0065282424T^2 + 1.7403752 \times 10^{-4}T^3 \quad (44)$$

$$- 7.9049655 \times 10^{-7}T^4$$

$C_s$  units joule/gm °K, T in °K

Enthalpy data presented in the Appendix were calculated for the vapor from the virial equation of state and the ideal gas heat capacities; the reference state is the ideal gas at 0°R. The liquid enthalpy was calculated from a curve fit of liquid enthalpy data for the pure components calculated from the latent heat of vaporization and the enthalpy of the vapor. The

following are the analytical equations obtained for the saturated liquid enthalpy of nitrogen, argon, and oxygen; temperature in °R.

Nitrogen:

$$H_{\text{liq.}} = -9774 + 158.74T - 1.2087T^2 + 4.3451 \times 10^{-3}T^3 - 5.589 \times 10^{-6}T^4 \quad (45)$$

Argon:

$$H_{\text{liq.}} = -3634 + 12.71T - 2.976 \times 10^{-2}T^2 + 6.08 \times 10^{-5}T^3 + 1.418 \times 10^{-7}T^4 \quad (46)$$

Oxygen:

$$H_{\text{liq.}} = -882 - 56.32T + 0.58608T^2 - 2.2058 \times 10^{-3}T^3 + 3.131 \times 10^{-6}T^4 \quad (47)$$

Based upon the scatter in the experimental enthalpy data, these equations are estimated to be correct within + 20 BTU/lb-mole. Because of this large uncertainty no correction was made for the effect of the heat of mixing and the effect of pressure on the enthalpy of the liquid. The enthalpy was calculated simply as

$$H_{\text{liq.}} = \sum_i x_i H_{i \text{ liq.}} \quad (48)$$

The correction for the heat of mixing varies up to 25 BTU/lb-mole and the correction for the effect of pressure on the enthalpy is only significant at the higher pressures where it varies up to 40 BTU/lb-mole. A check on the thermodynamic consistency of the data was made by comparison of calculated values of the saturated heat capacity with experimental data by means of the following equation neglecting the second term.

$$C_{\text{sat.}} = \left( \frac{\partial H}{\partial T} \right)_{\text{sat.}} - v \left( \frac{\partial p}{\partial T} \right)_{\text{sat.}} \quad (49)$$

The comparison of the data is given in Table 24.

At low temperatures the calculated and experimental heat capacities are in good agreement for nitrogen and oxygen, and somewhat poorer agreement for argon. The largest deviations of about 10% occur at high temperatures where the effect of pressure on the enthalpy may begin to be significant. The agreement is considered good enough that the calculated heat capacities given in the appendix are based upon a temperature differentiation of the enthalpy equations.

TABLE 24

COMPARISON OF CALCULATED AND EXPERIMENTAL  
SATURATED LIQUID HEAT CAPACITIES, BTU/lb-MOLE-°R

Temperature °F	Nitrogen		Argon		Oxygen	
	Exp. (41)	Calc.	Exp. (5)	Calc.	Exp. (47)	Calc.
-320	....	....	....	....	12.8	12.4
-310	13.9	14.0	10.7	9.8	12.9	12.9
-300	14.2	14.1	10.9	10.2	13.0	13.1
-290	14.6	14.6	11.2	10.6	....	13.2
-280	15.1	15.5	11.5	11.2	....	13.3
-270	15.8	16.6	11.7	11.9	....	13.4
-260	16.9	17.8	12.0	12.6	....	13.6
-250	18.9	18.9	12.2	13.5	....	14.0
-240	....	....	13.1	14.4	....	14.6
-230	....	....	14.6	15.5	....	15.6

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APPENDIXES

	<u>Page</u>
I. Graphical Presentation of Correlation . . . . .	150
A. K-Values Vs. Pressure . . . . .	150
B. Relative Volatility of Argon to Nitrogen in Ternary System . . . . .	176
C. Relative Volatility of Argon to Oxygen in Ternary System . . . . .	188
D. Relative Volatility of Argon to Nitrogen, Binary System . . . . .	200
E. Relative Volatility of Argon to Oxygen, Binary System . . . . .	202
F. Pressure Activity Coefficients . . . . .	204
G. Mixture Vapor Pressures Vs. Temperature . . . . .	244
II. Tabular Presentation of Correlation . . . . .	260
A. Isobaric Table . . . . .	260
B. Isothermal Table . . . . .	274
III. Bibliography from Literature Search . . . . .	294
IV. Nomenclature Table . . . . .	312



## APPENDIX I

## GRAPHICAL PRESENTATION OF CORRELATION

A. K-Values Vs. Pressure

The 36 graphs to follow present the K-values defined as:

$$K_i = \frac{y_i}{x_i} \quad (50)$$

of the three components as a function of pressure along selected isotherms. Envelopes defining the binary compositions are drawn as dashed lines.

The graphs are grouped in order of component: nitrogen, argon, oxygen. Inside each group they are ordered with respect to increasing mole fraction nitrogen in the liquid.

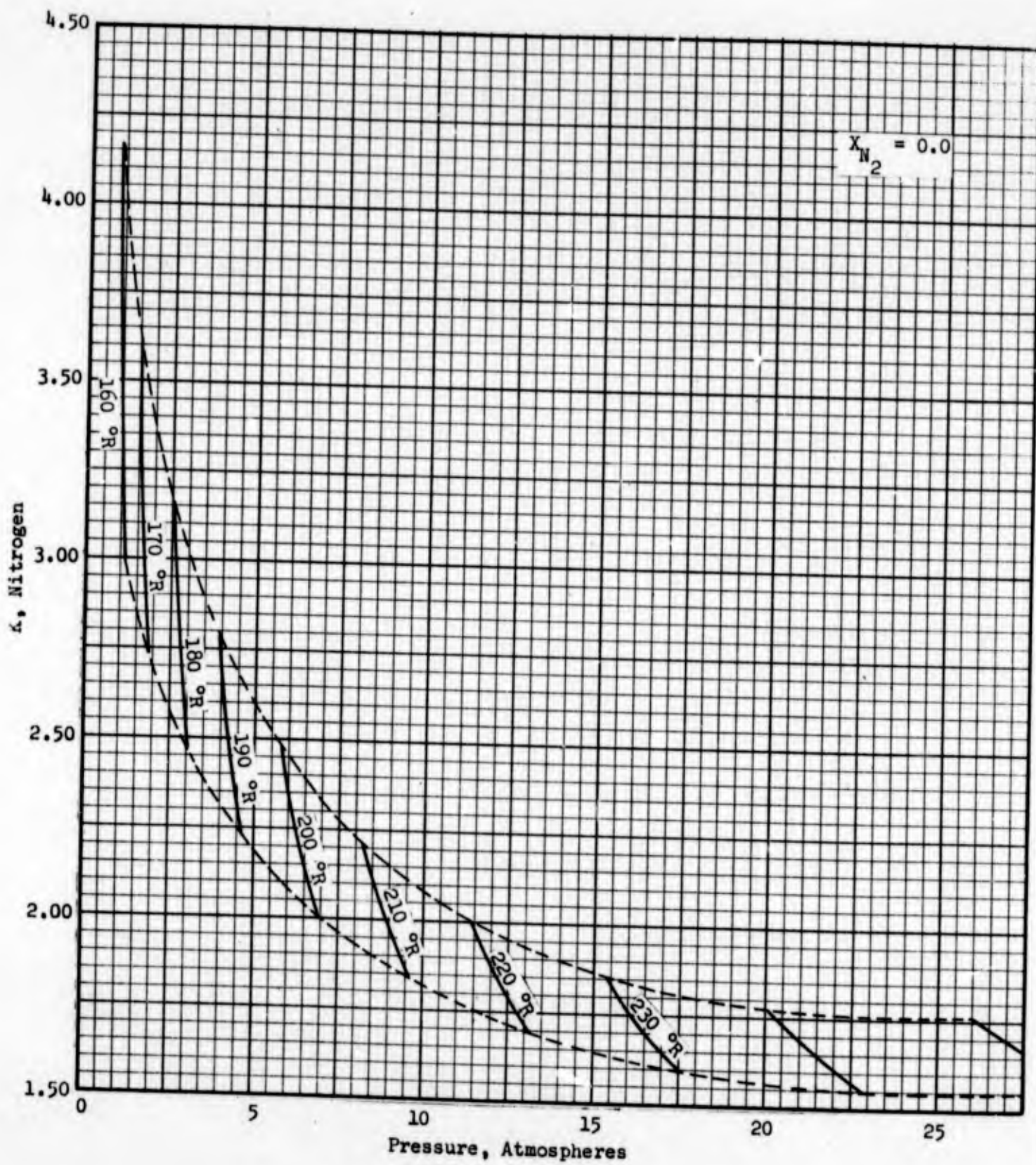


Figure 86. K-Values of Nitrogen.

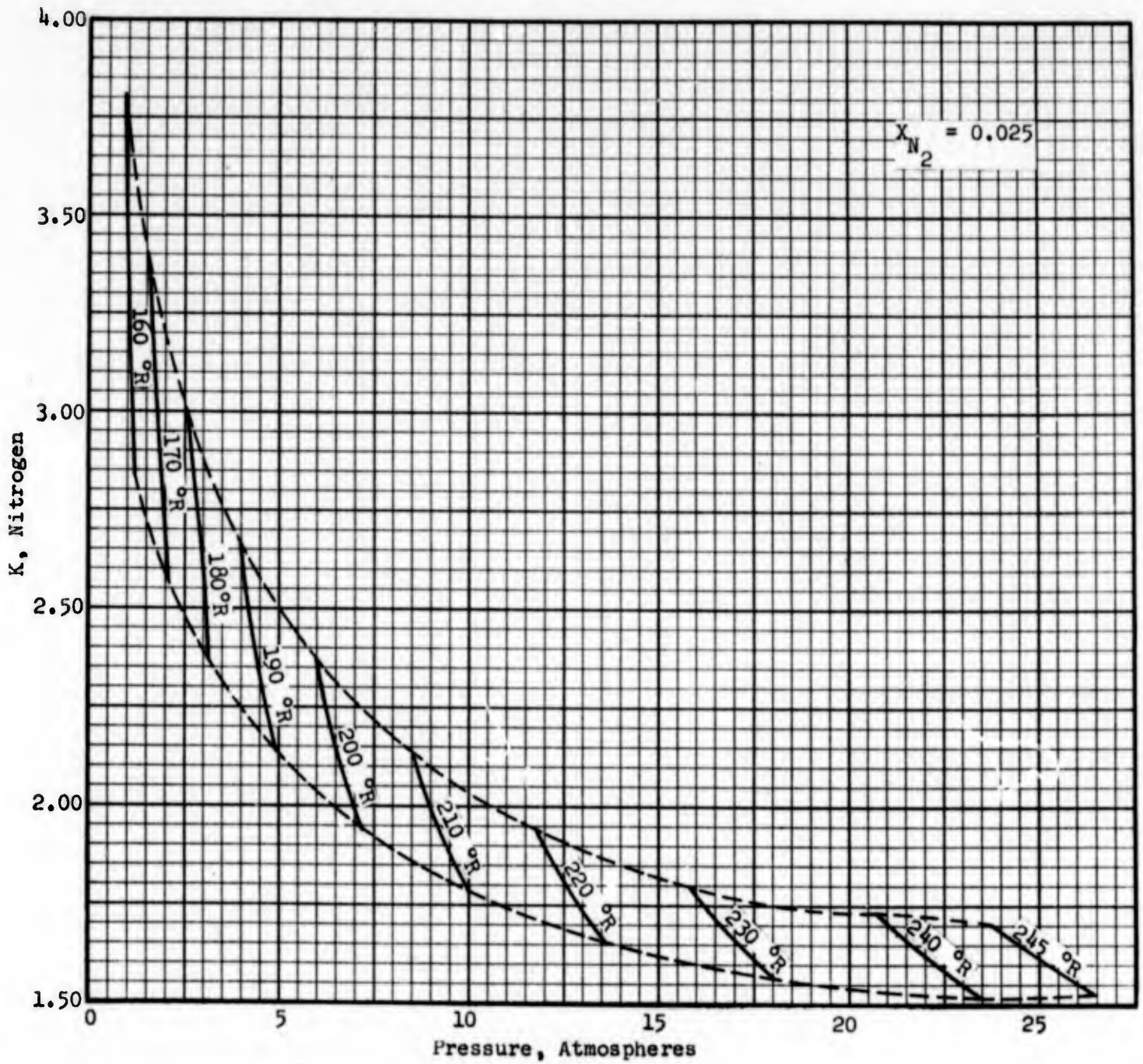


Figure 87. K-Values of Nitrogen.

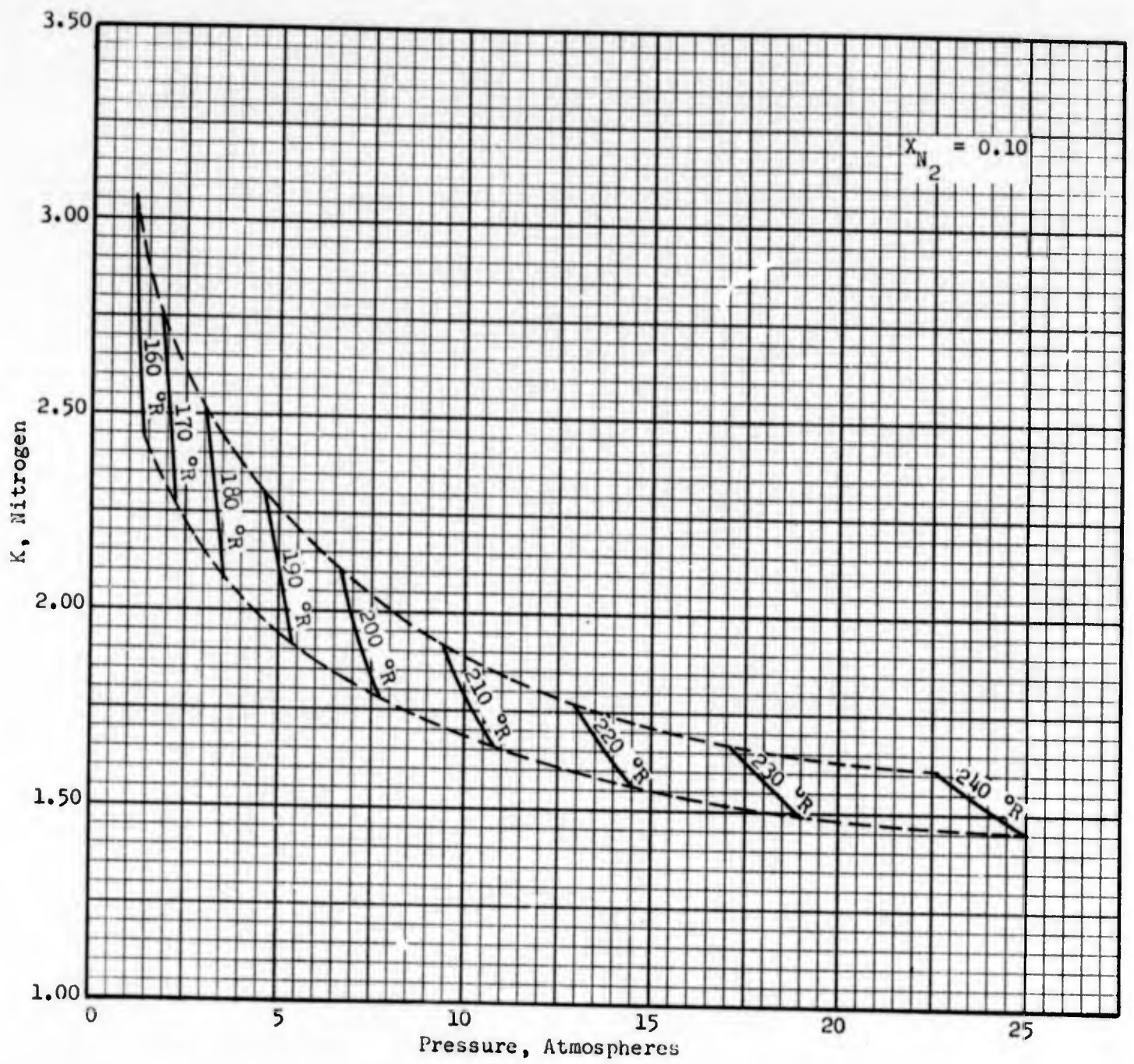
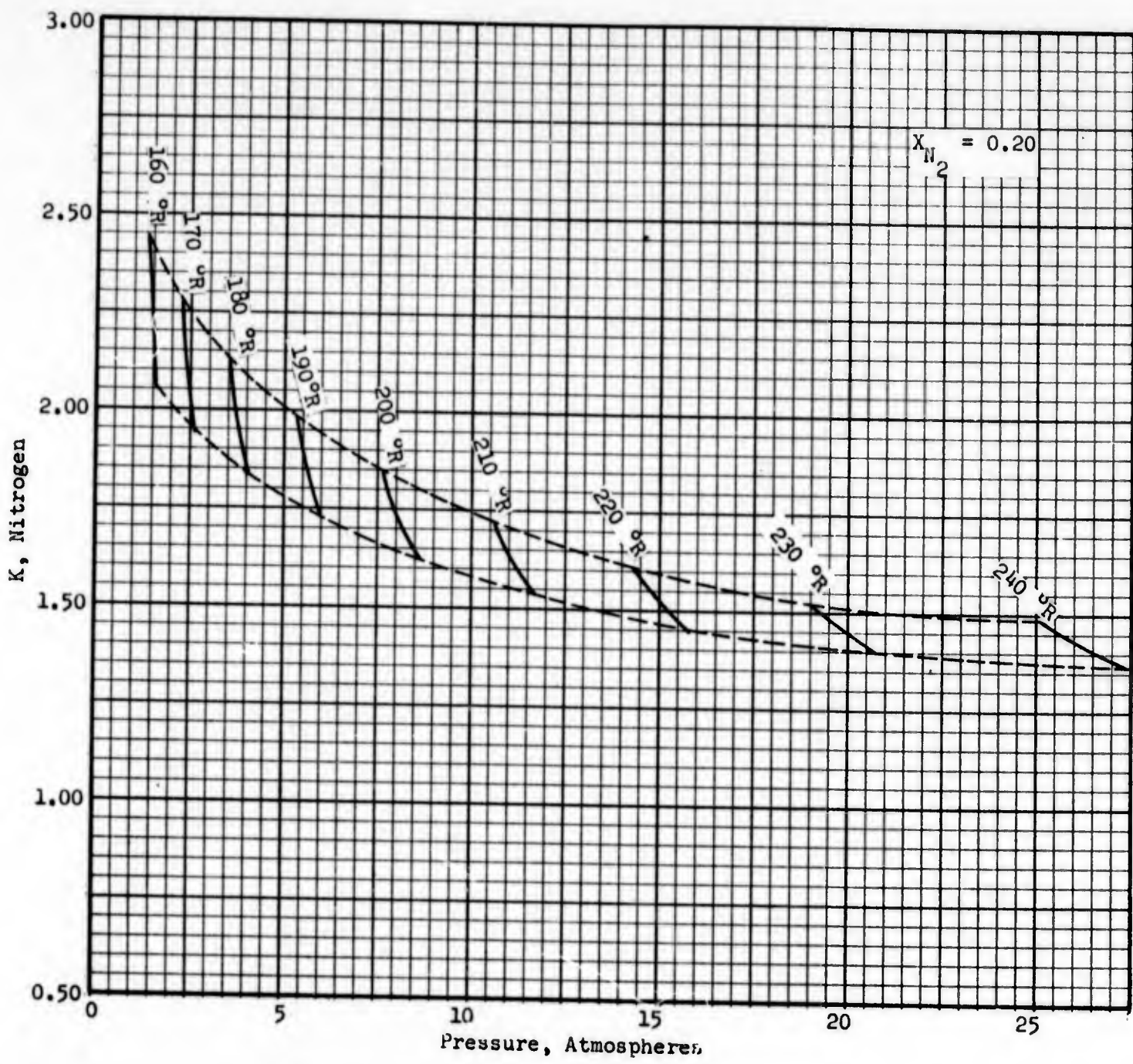


Figure 88. K-Values of Nitrogen.



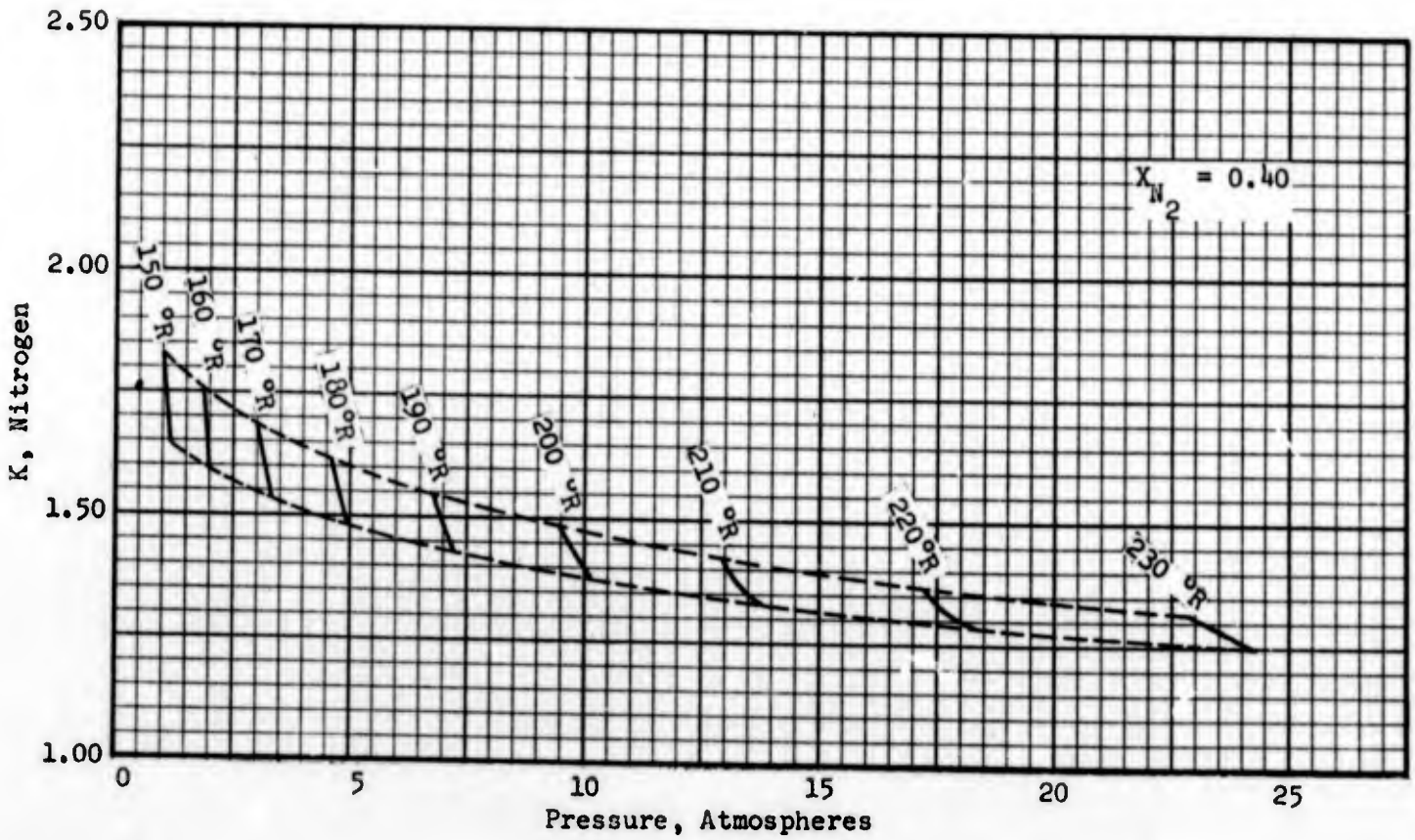
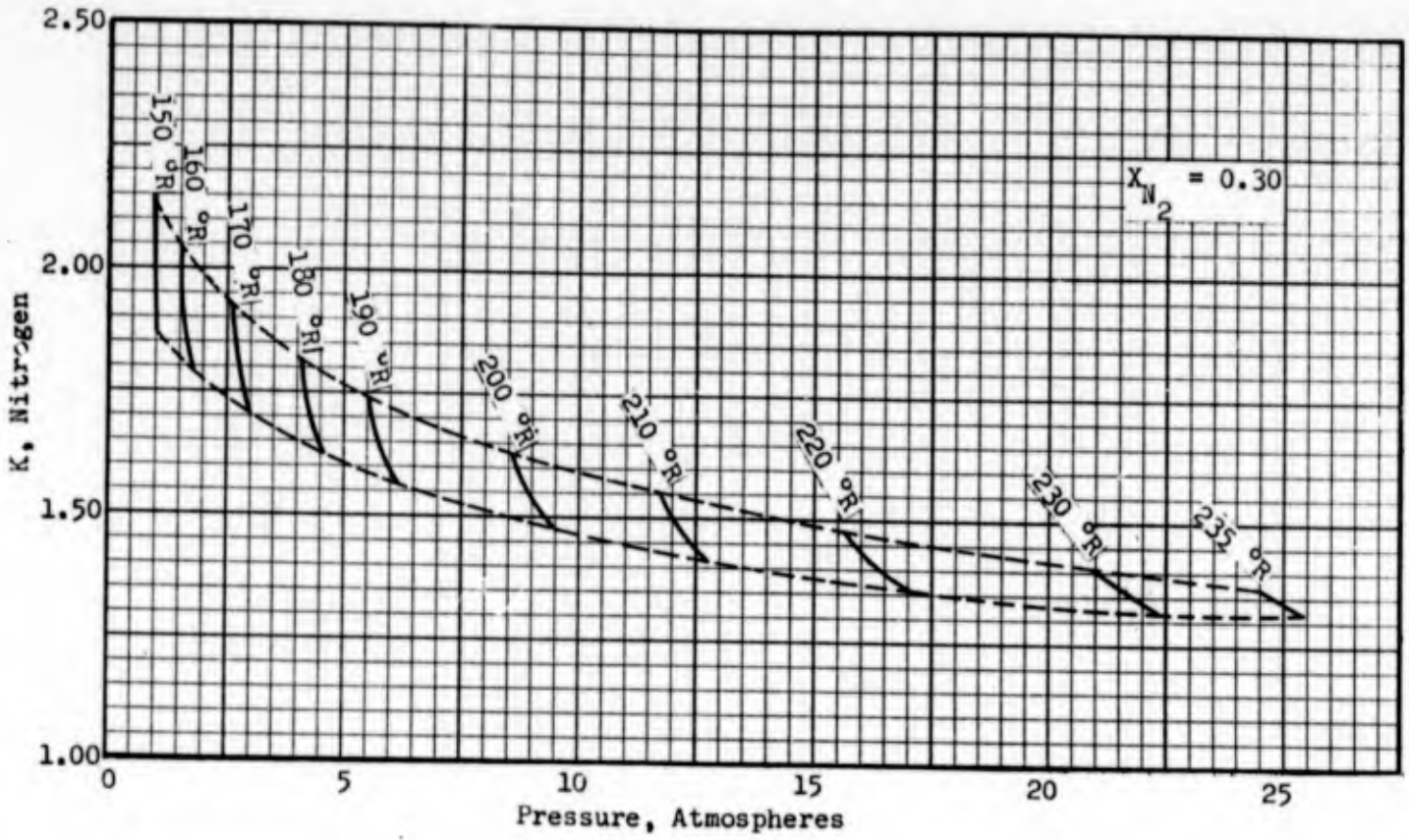


Figure 90. K-Values of Nitrogen.

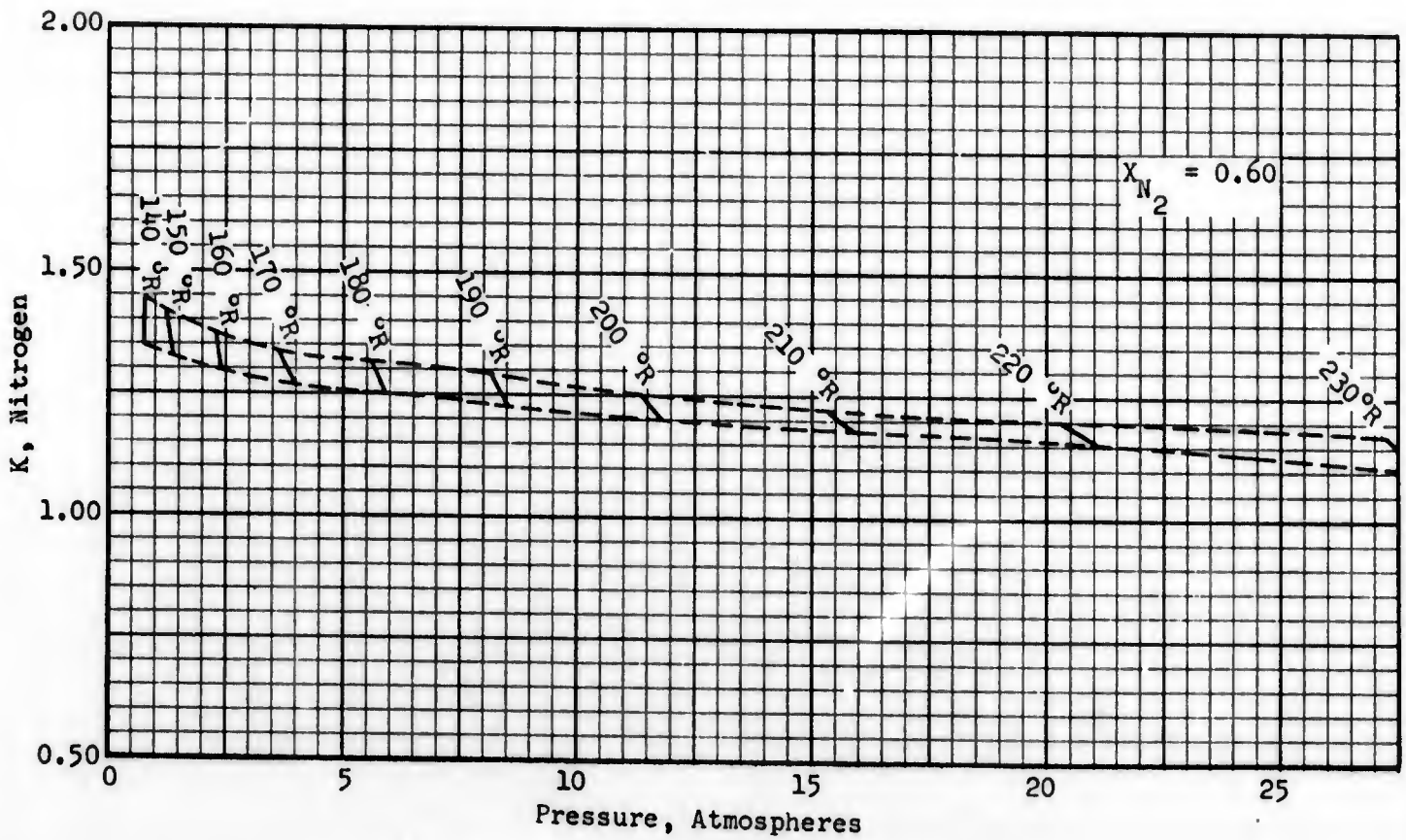
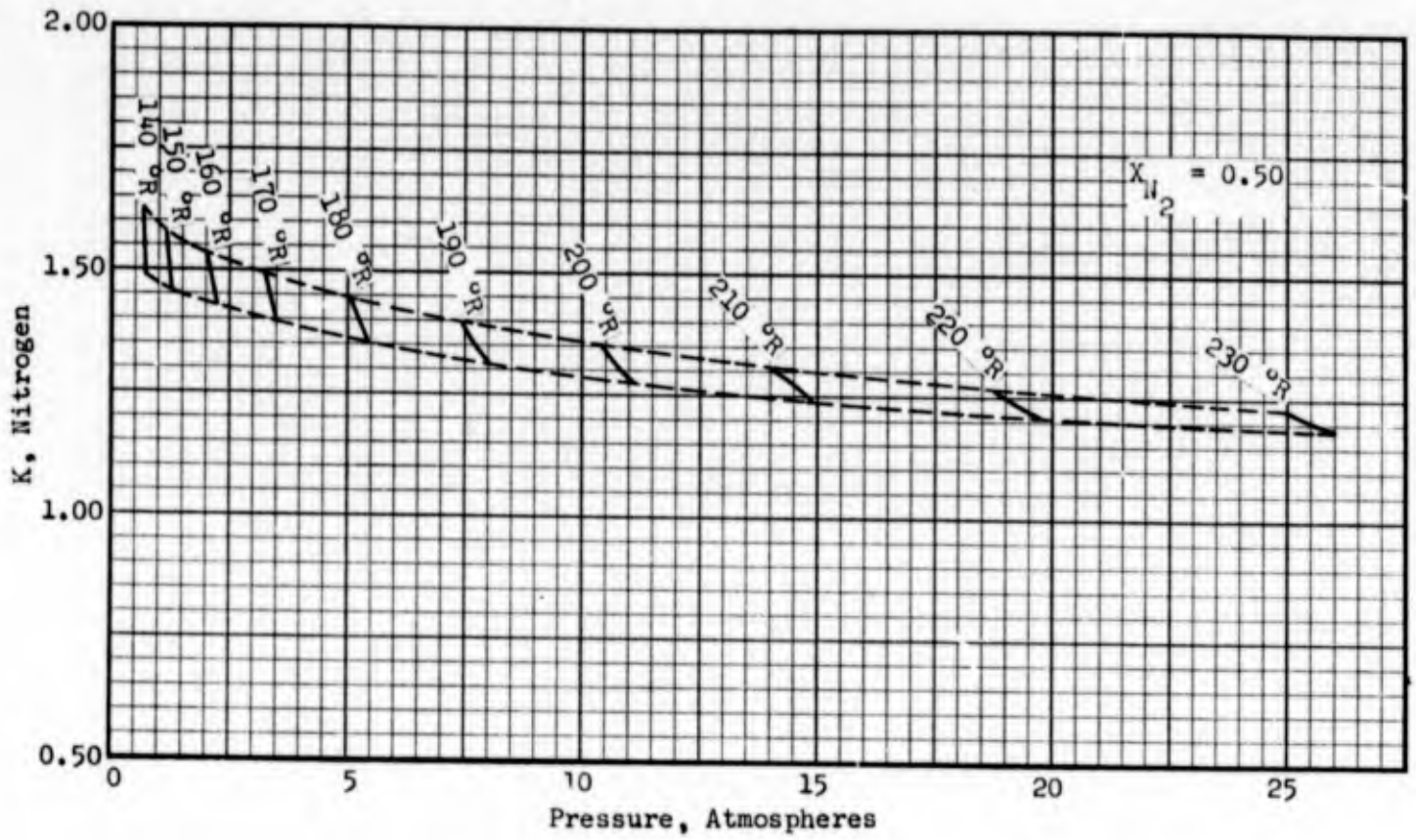


Figure 91. K-Values of Nitrogen.

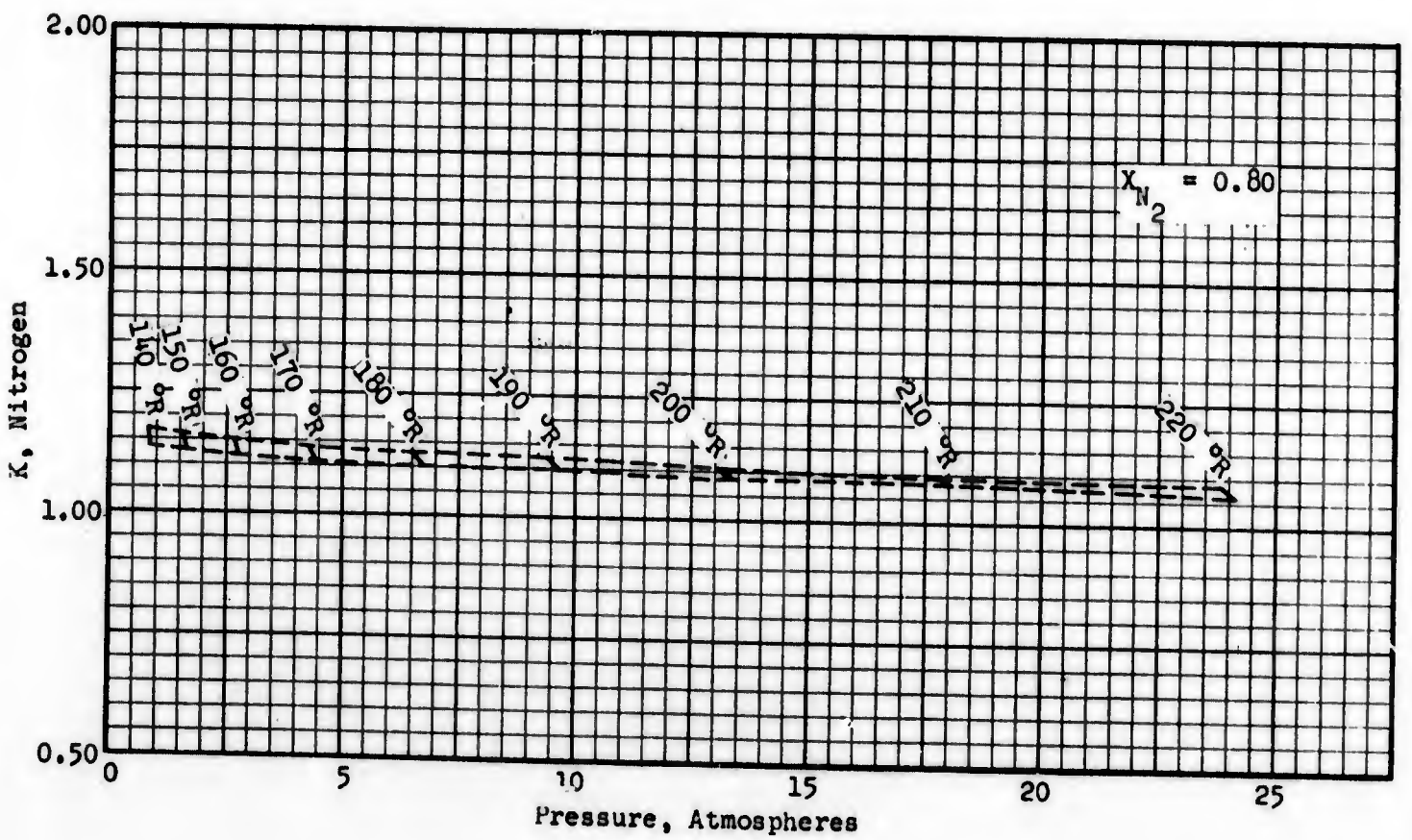
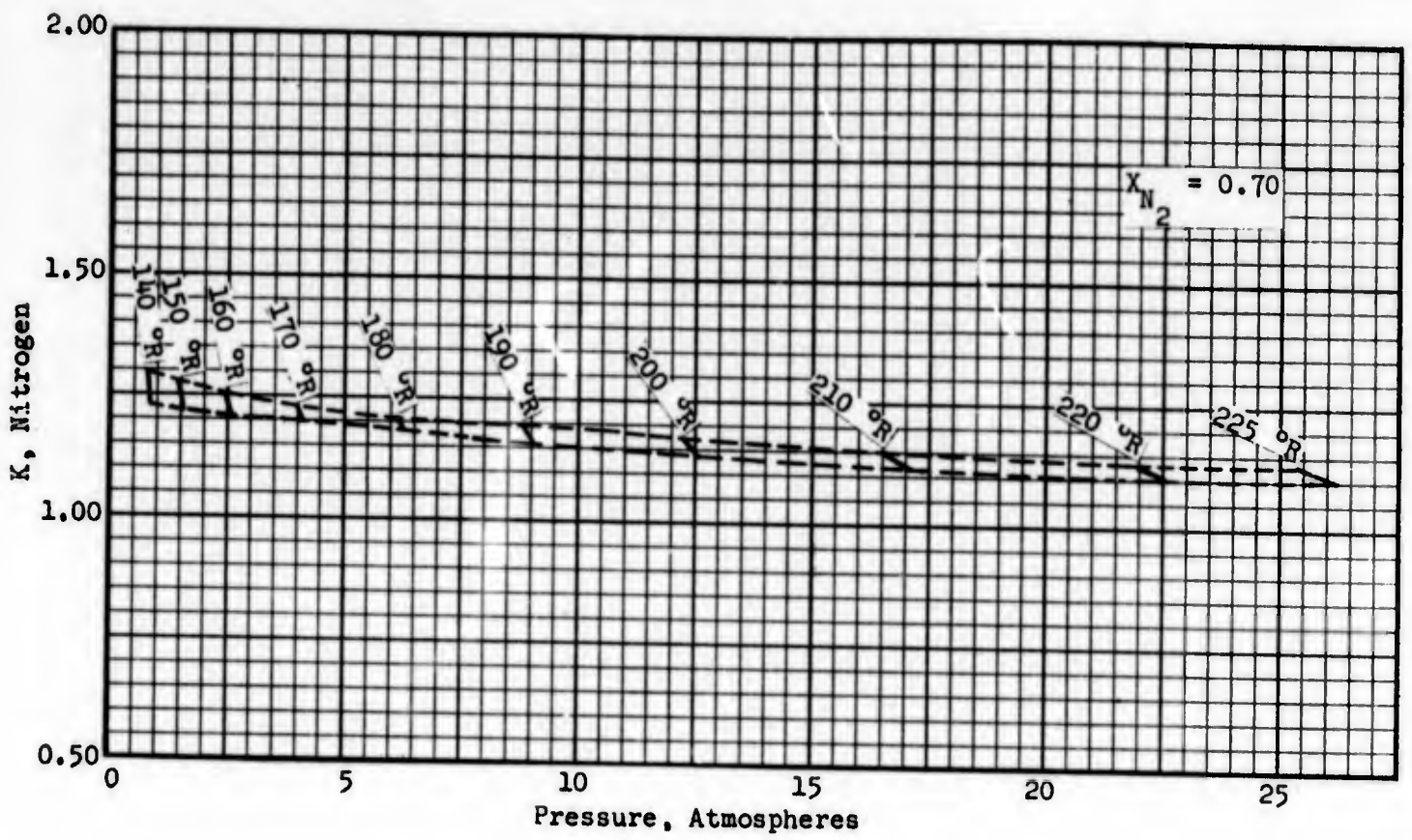


Figure 92. K-Values of Nitrogen.



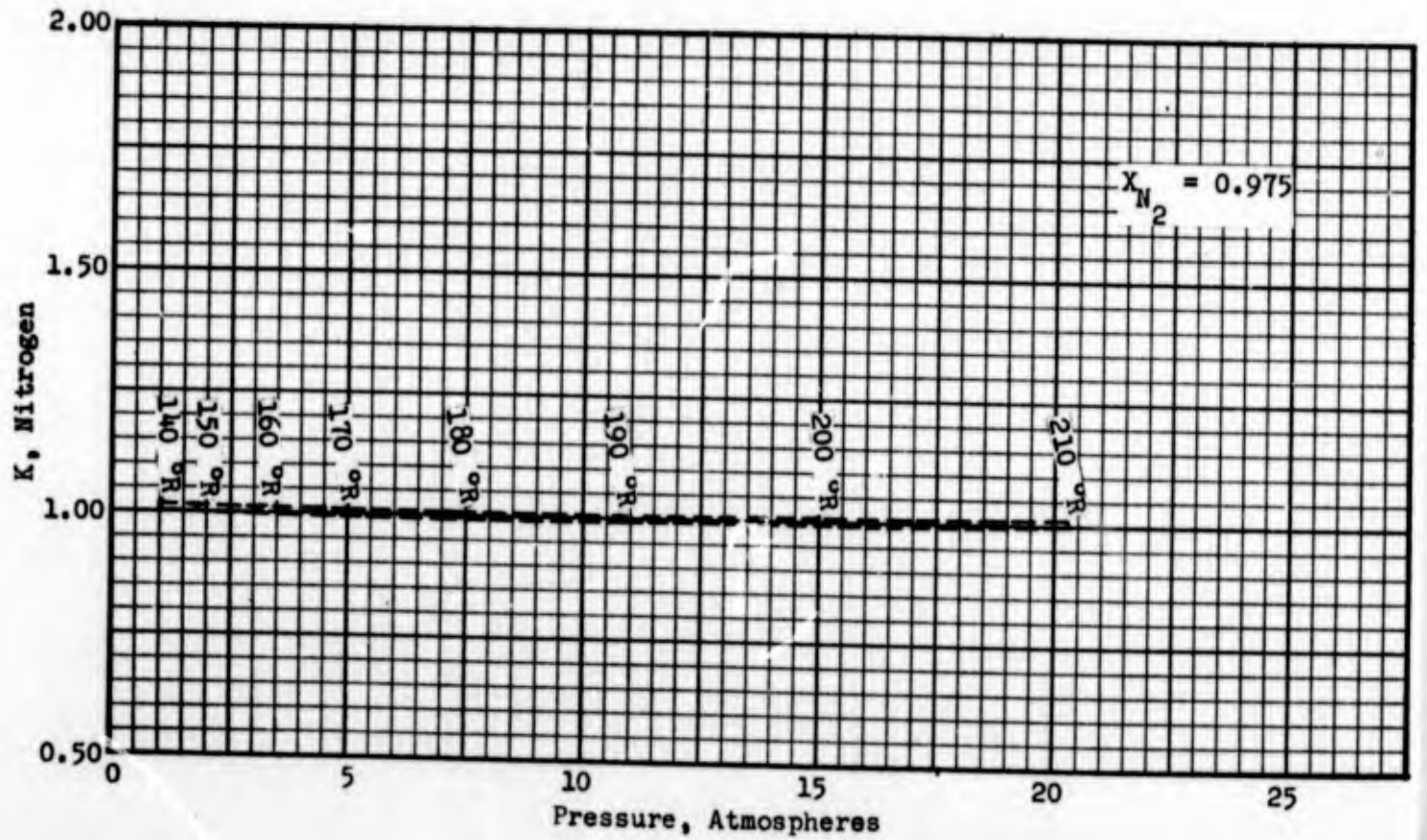
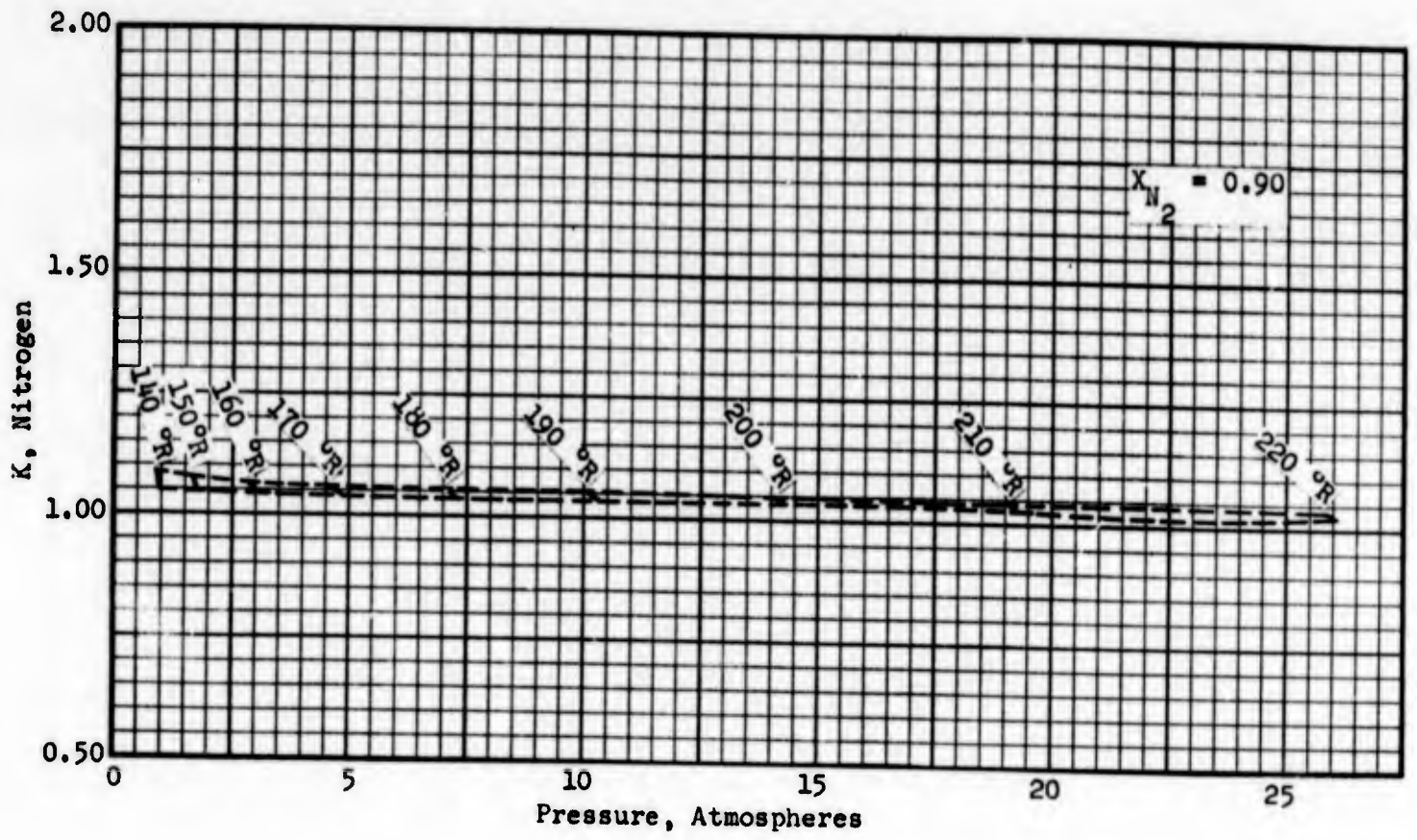


Figure 93. K-Values of Nitrogen.

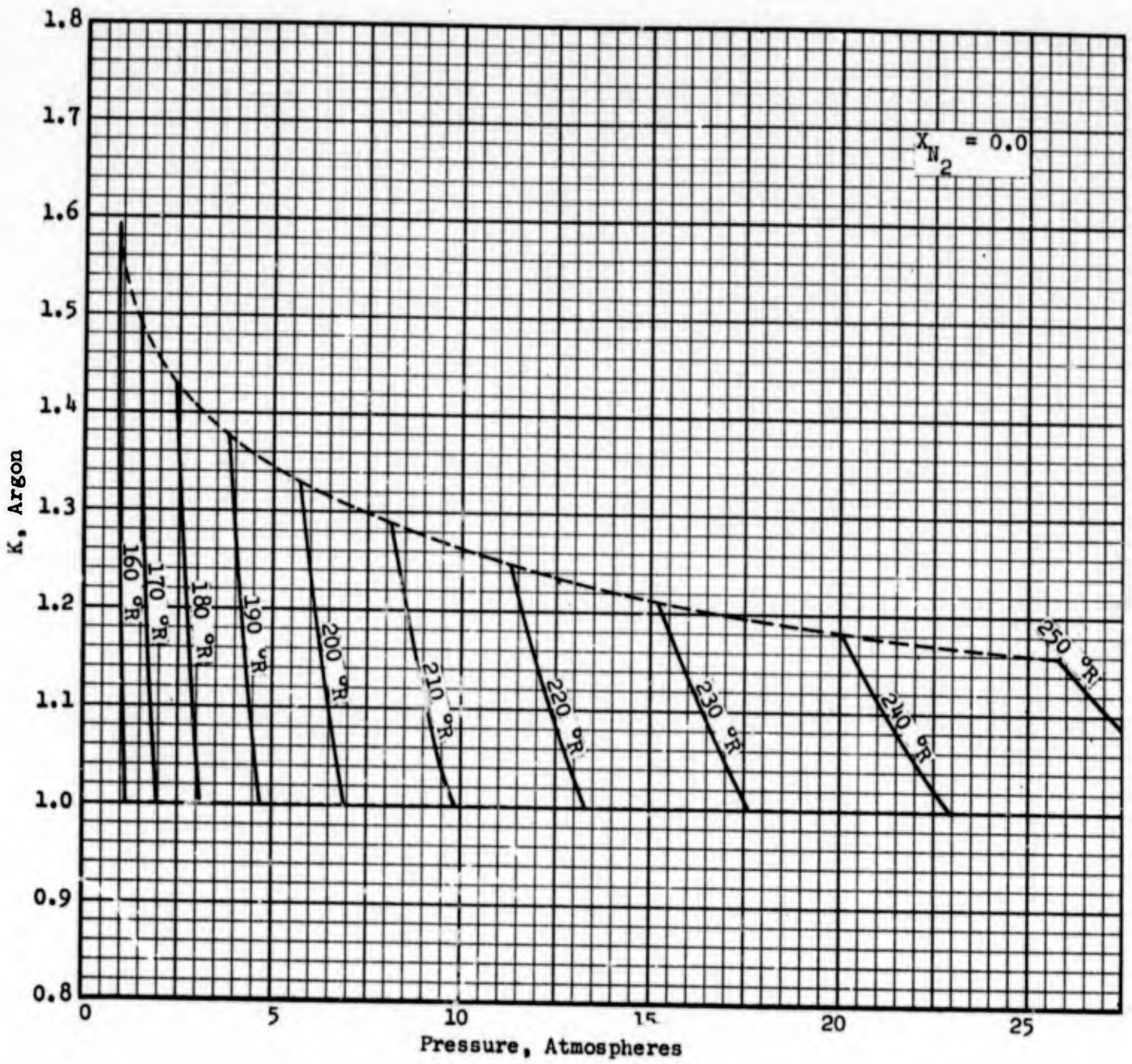


Figure 94. K-Values of Argon.

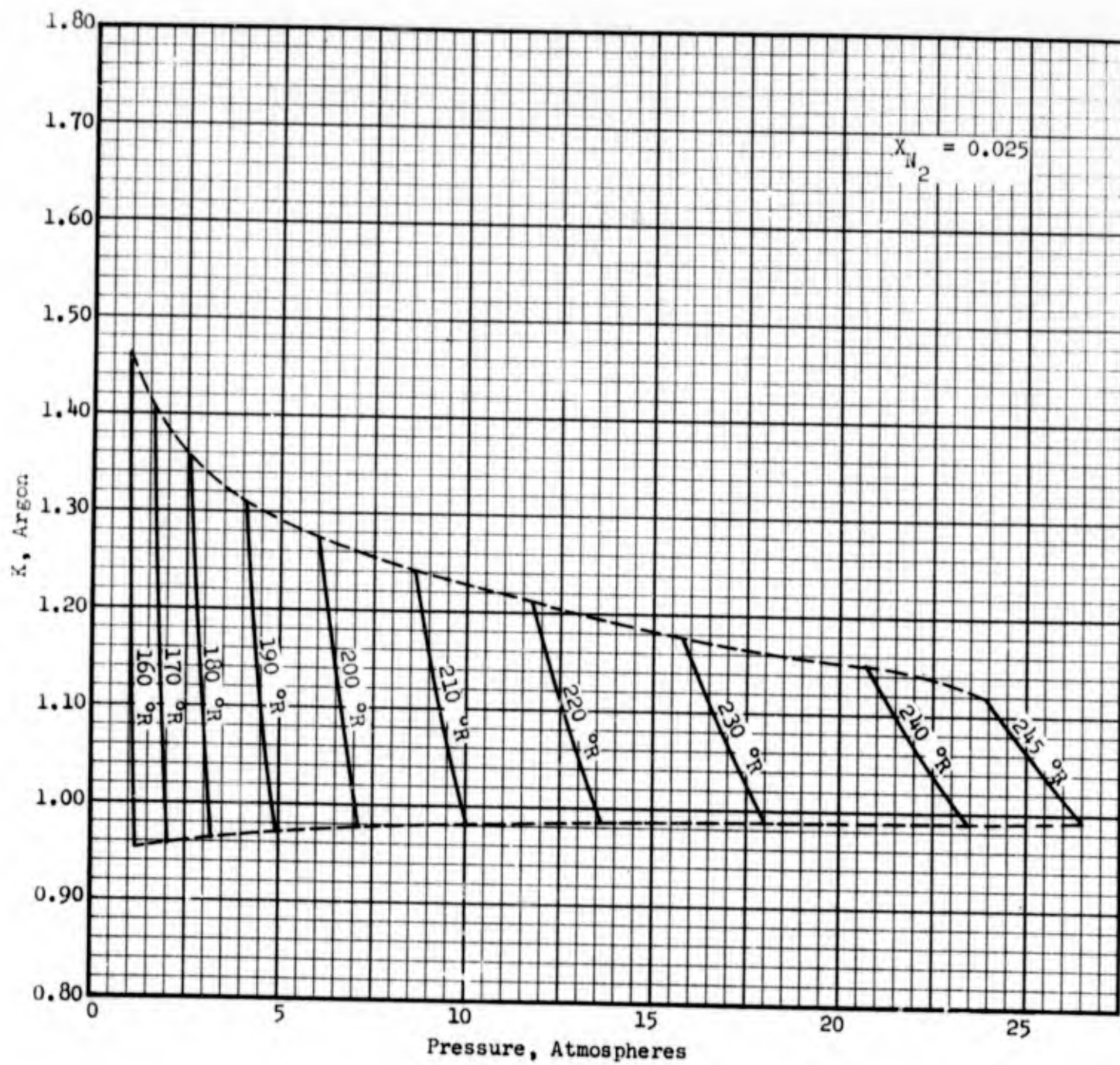


Figure 95. K-Values of Argon

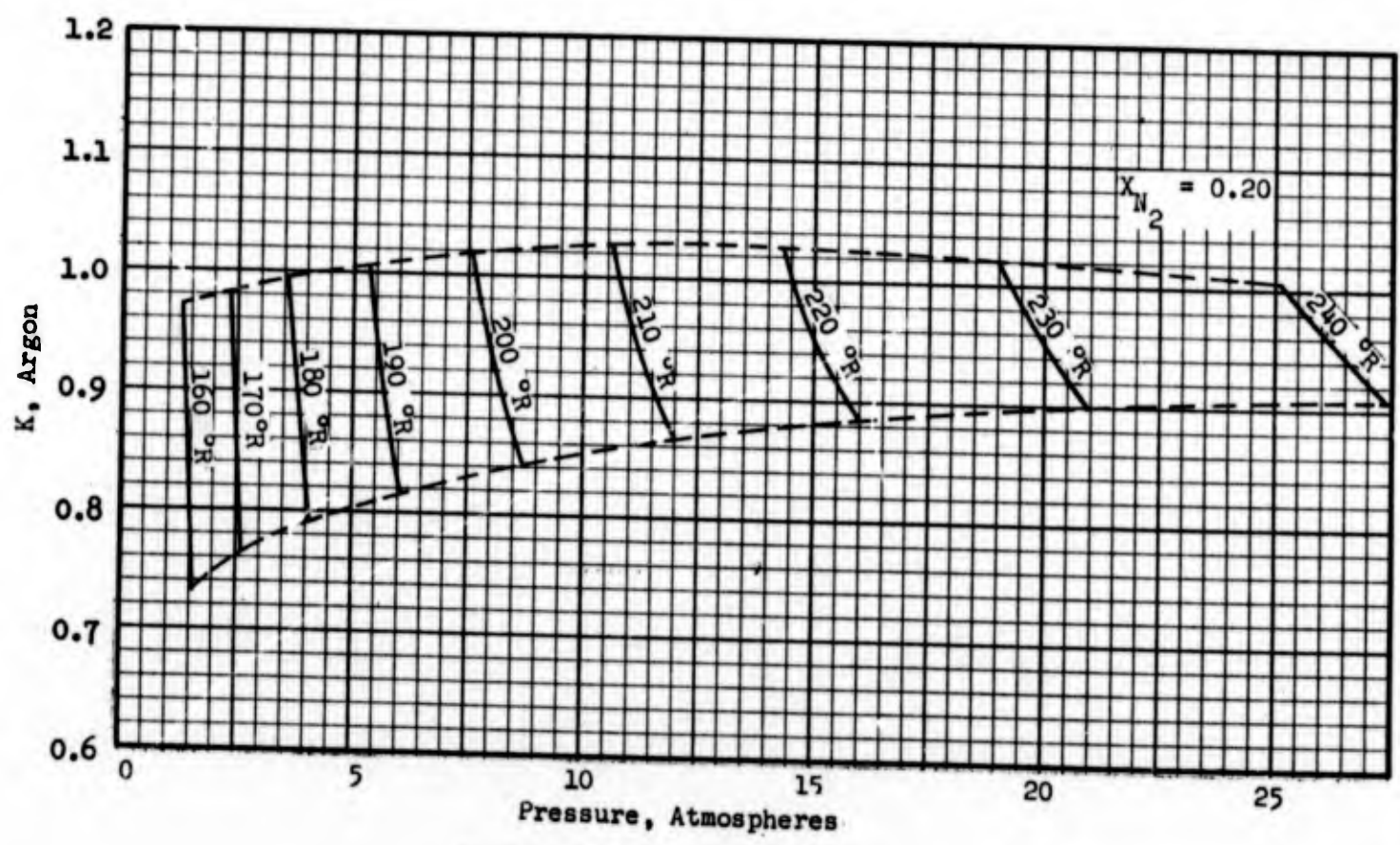
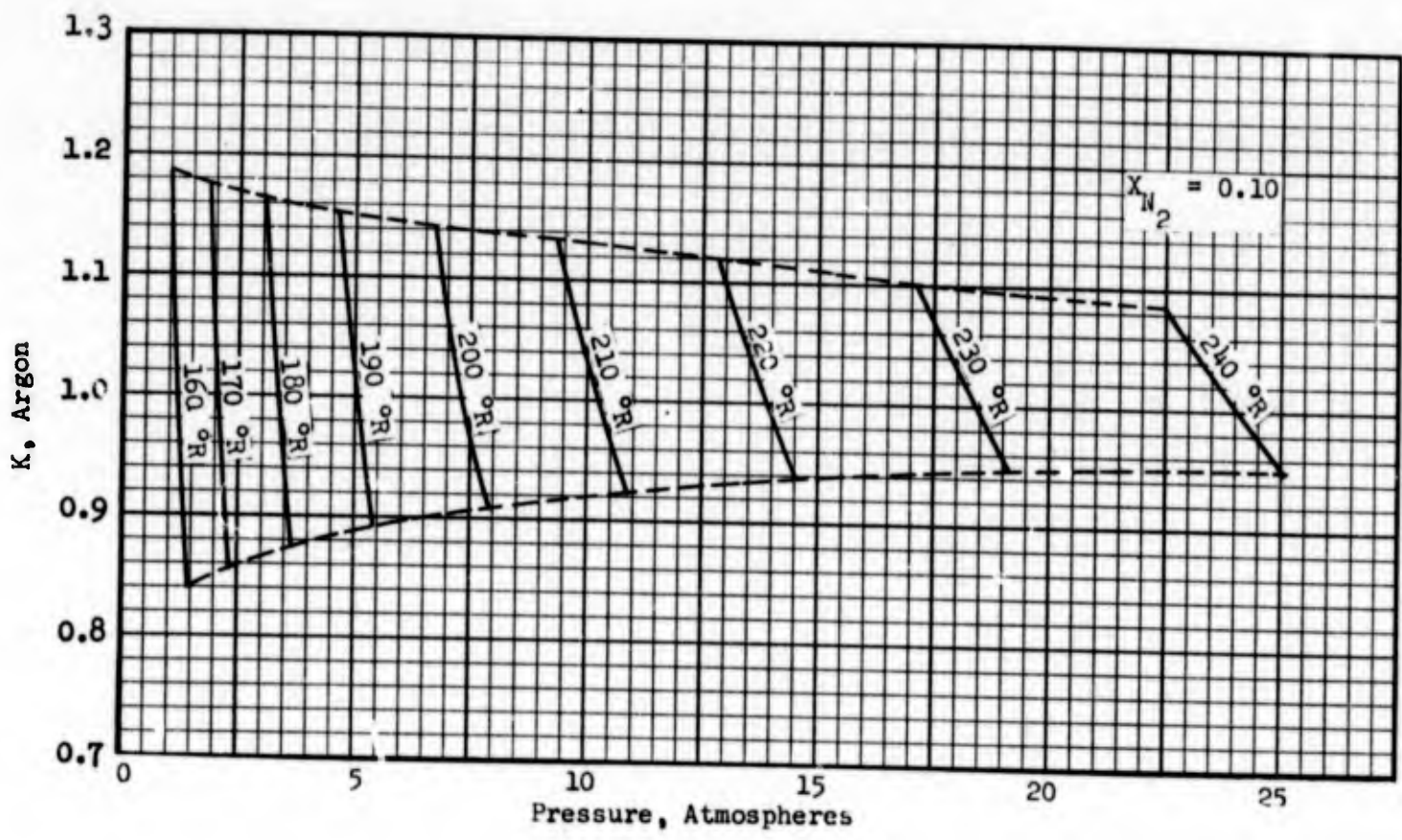


Figure 96. K-Values of Argon.

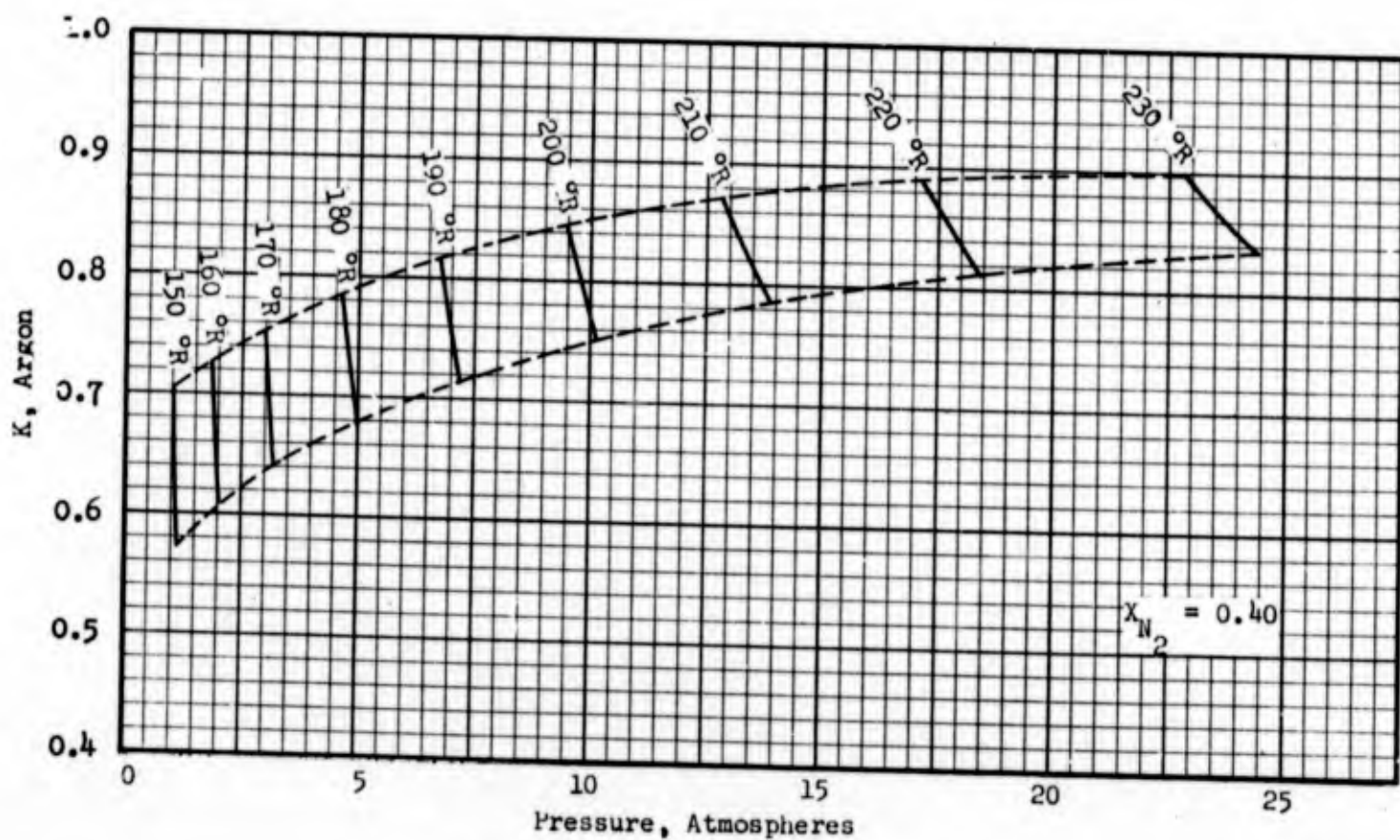
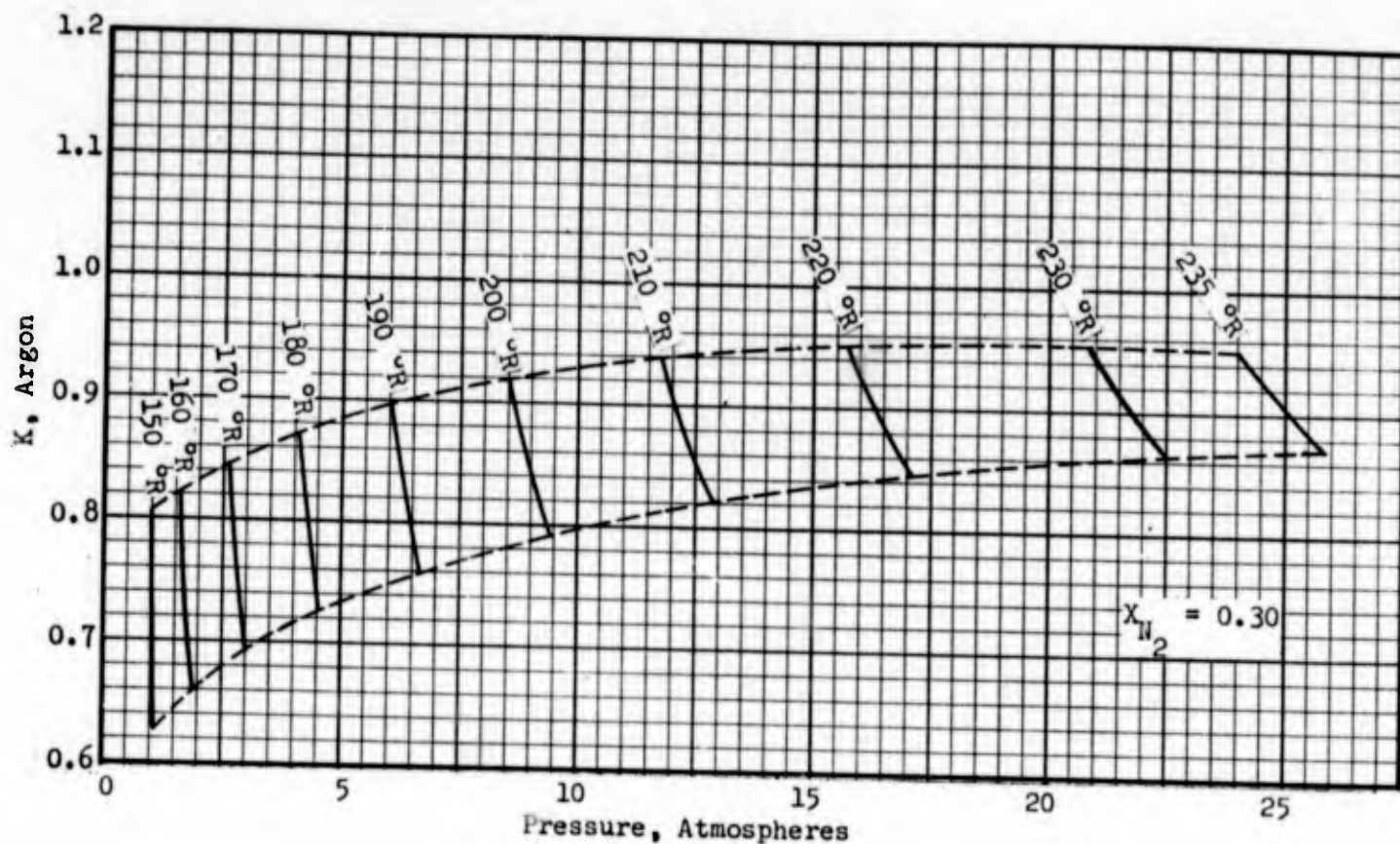


Figure 97. K-Values of Argon.

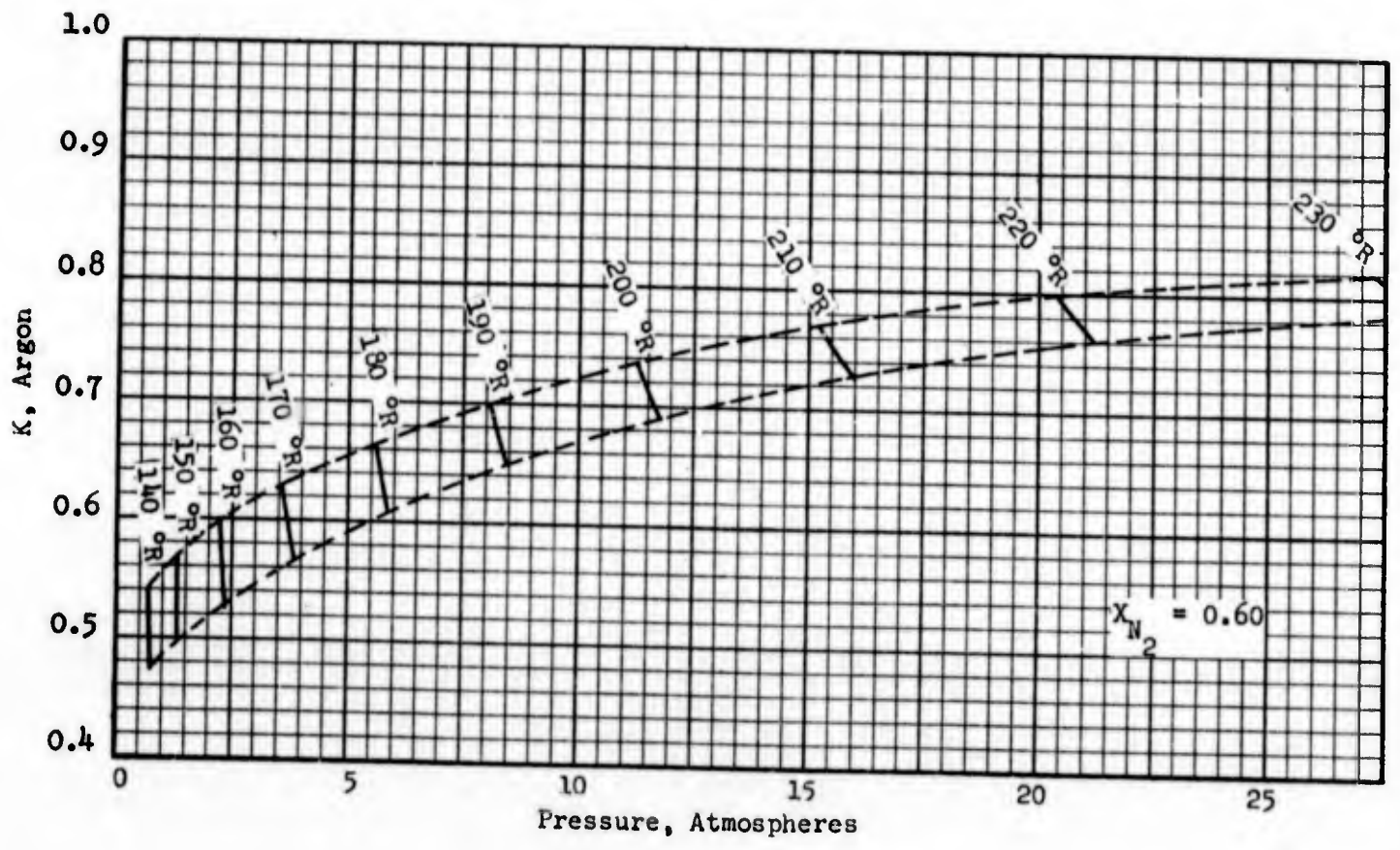
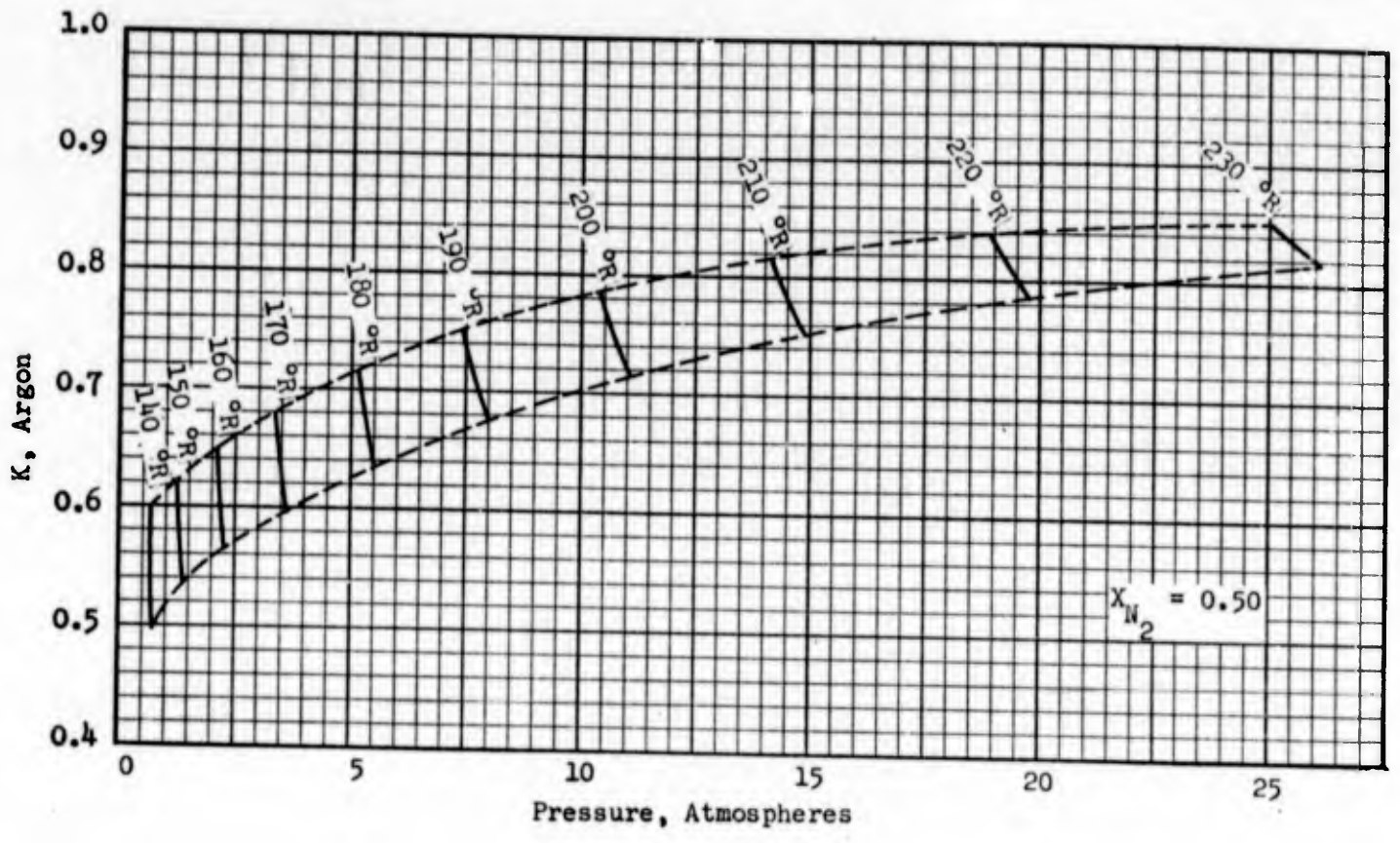


Figure 98. K-Values of Argon.

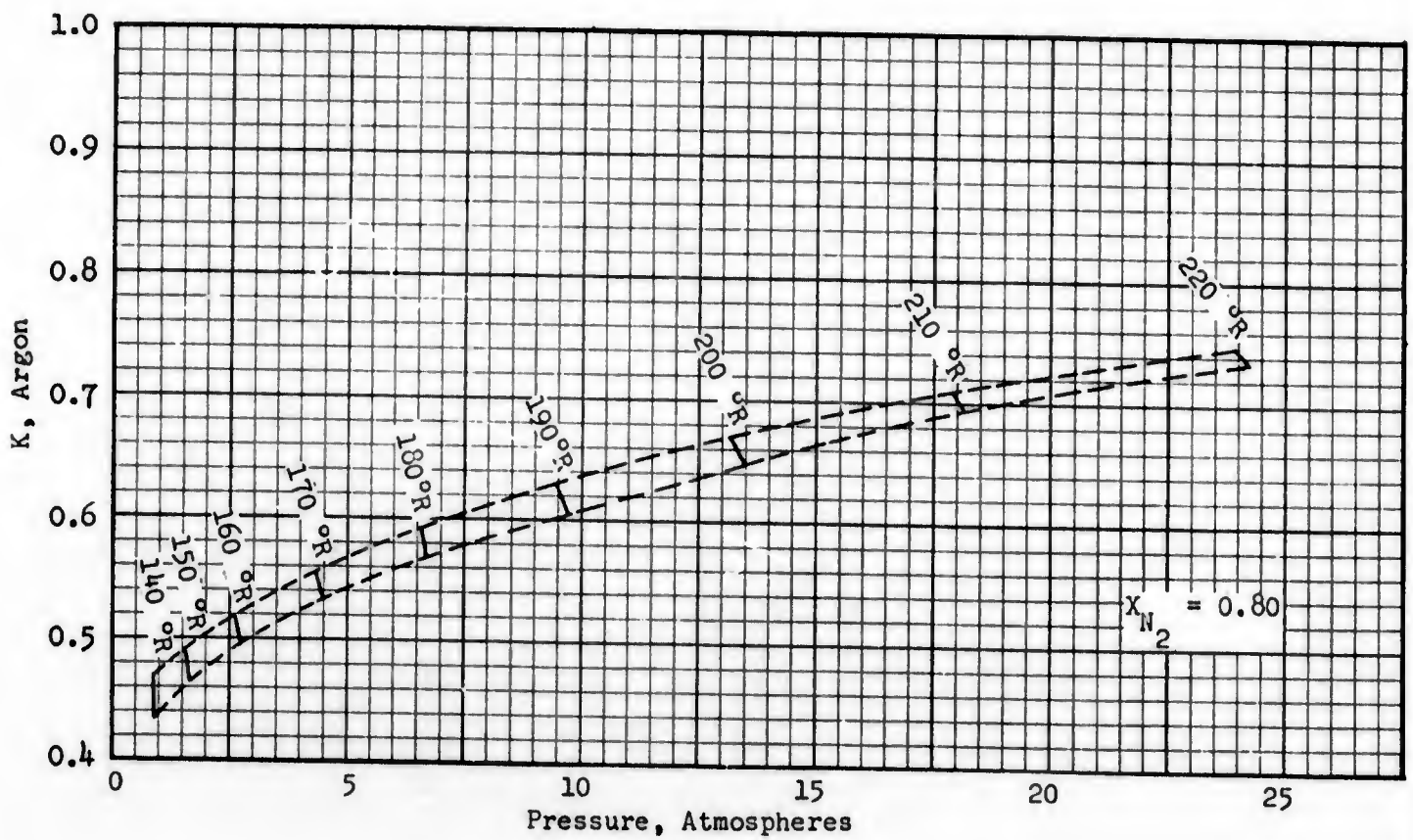
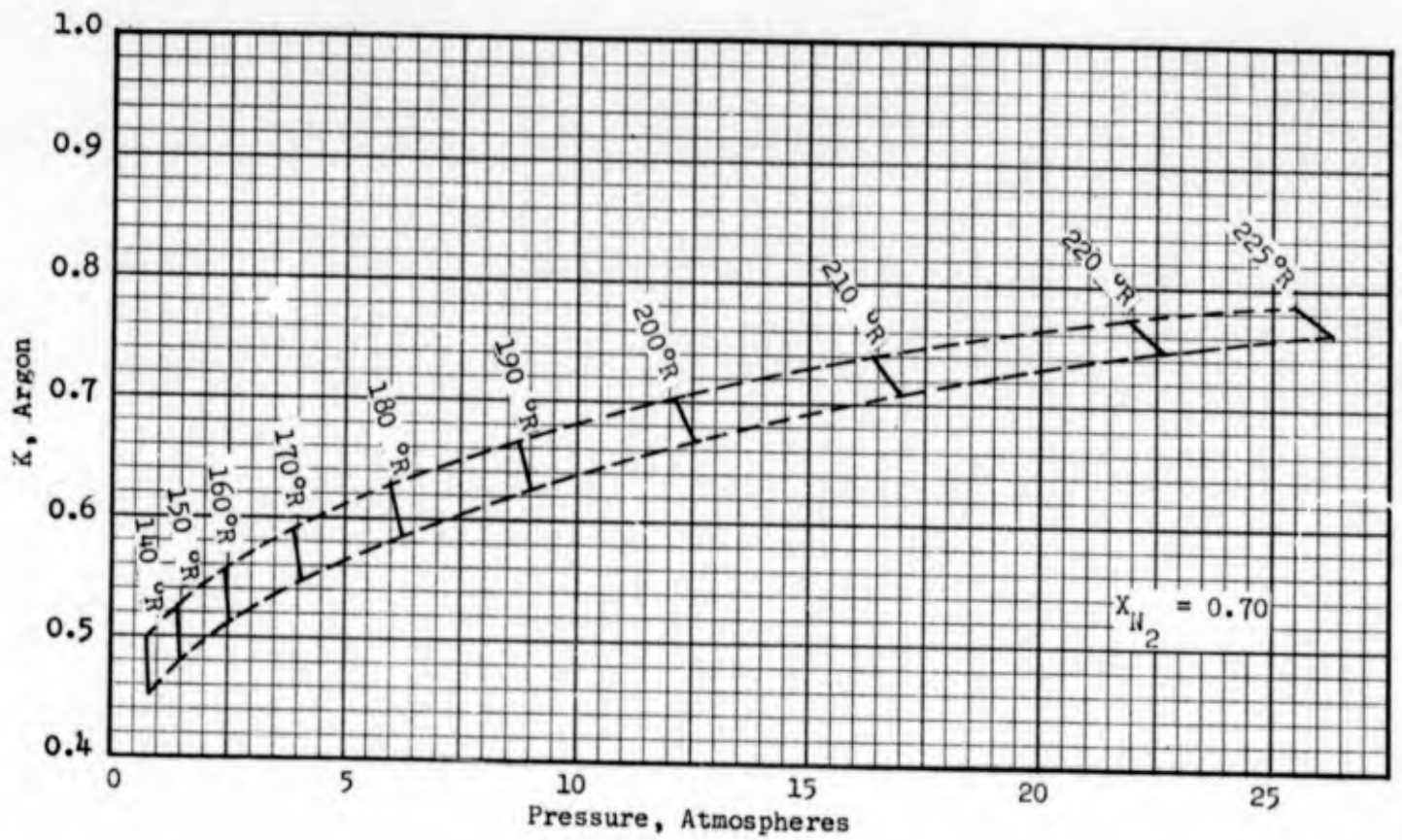


Figure 99. K-Values of Argon.

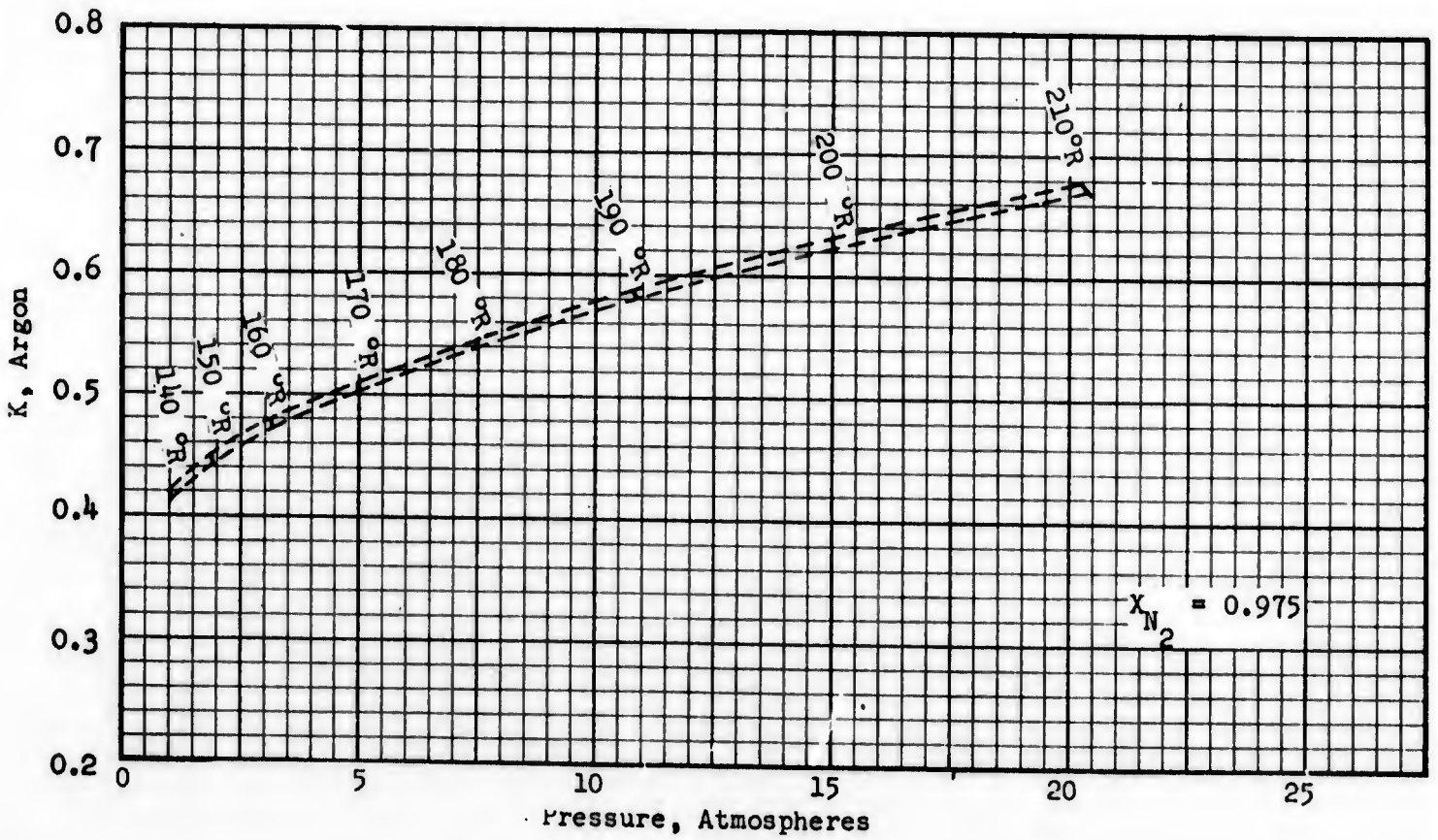
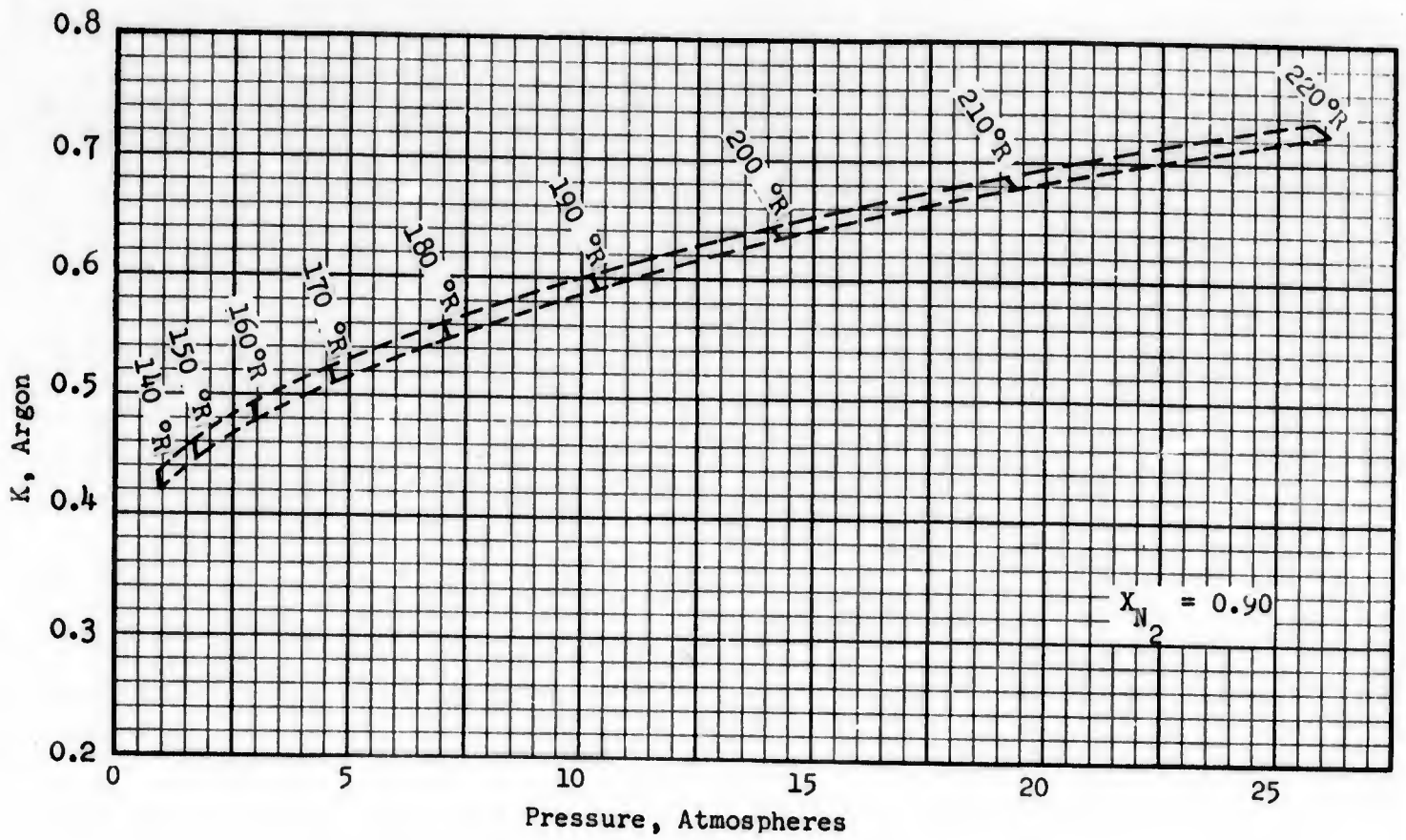


Figure 100. K-Values of Argon.



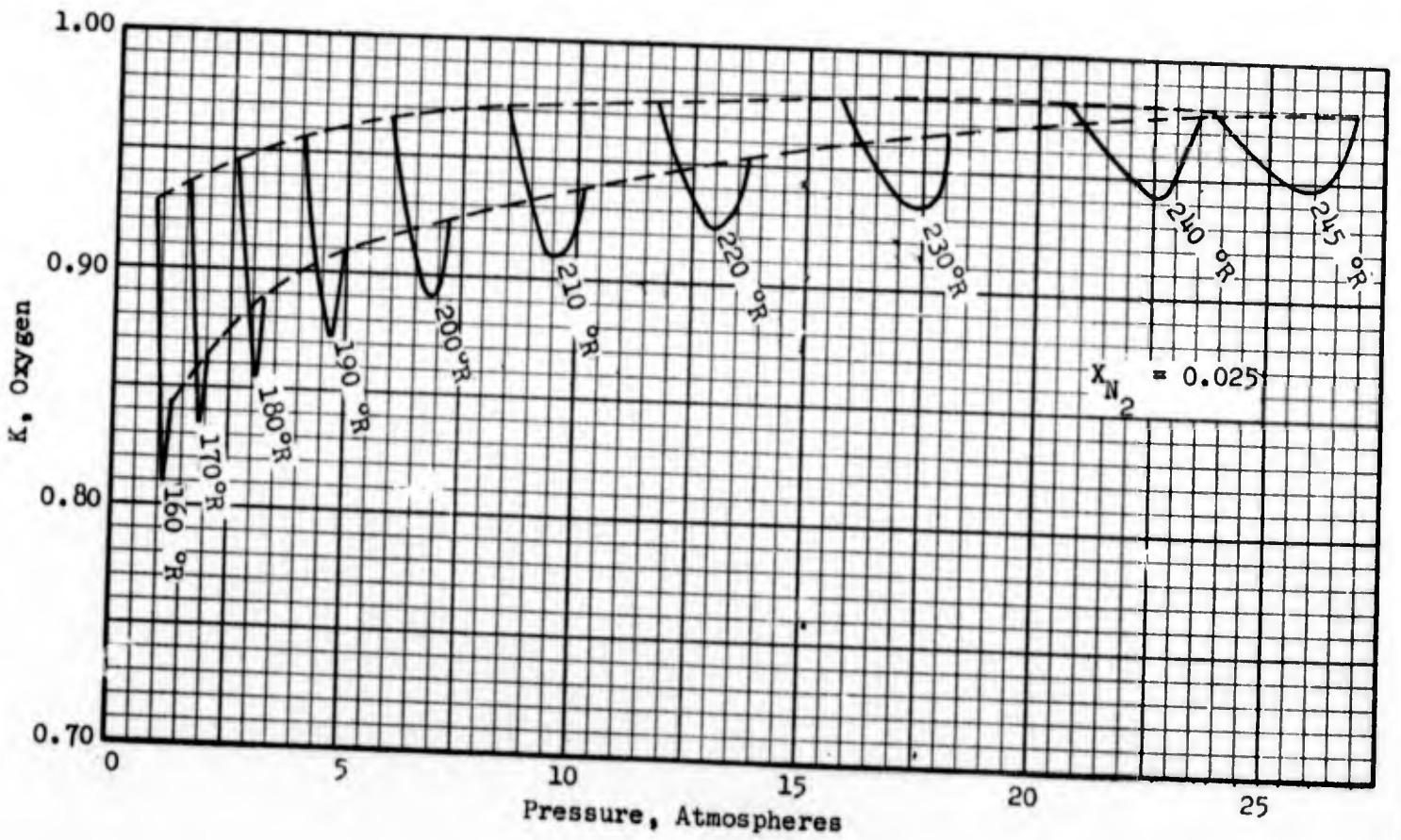
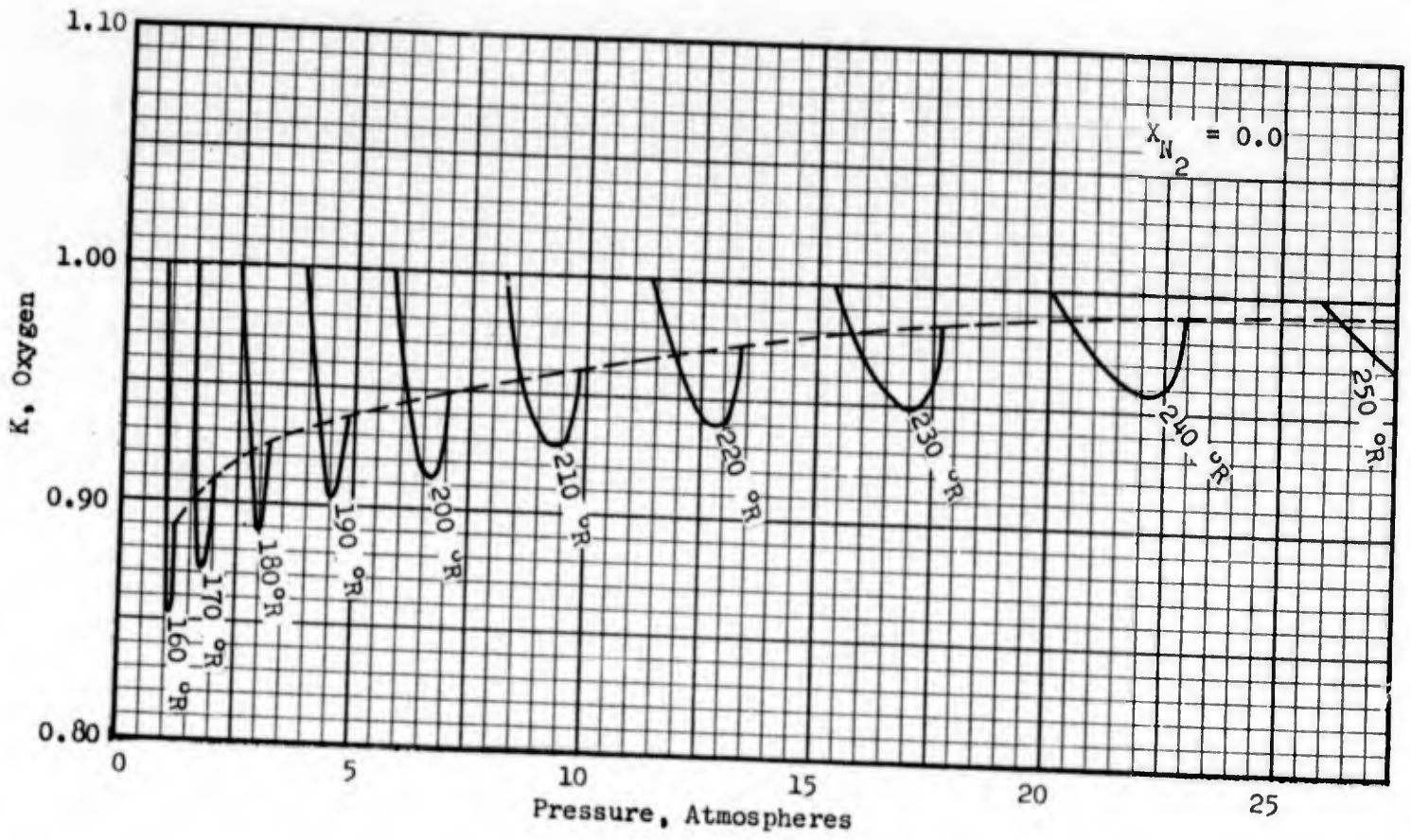


Figure 101. K-Values of Oxygen.

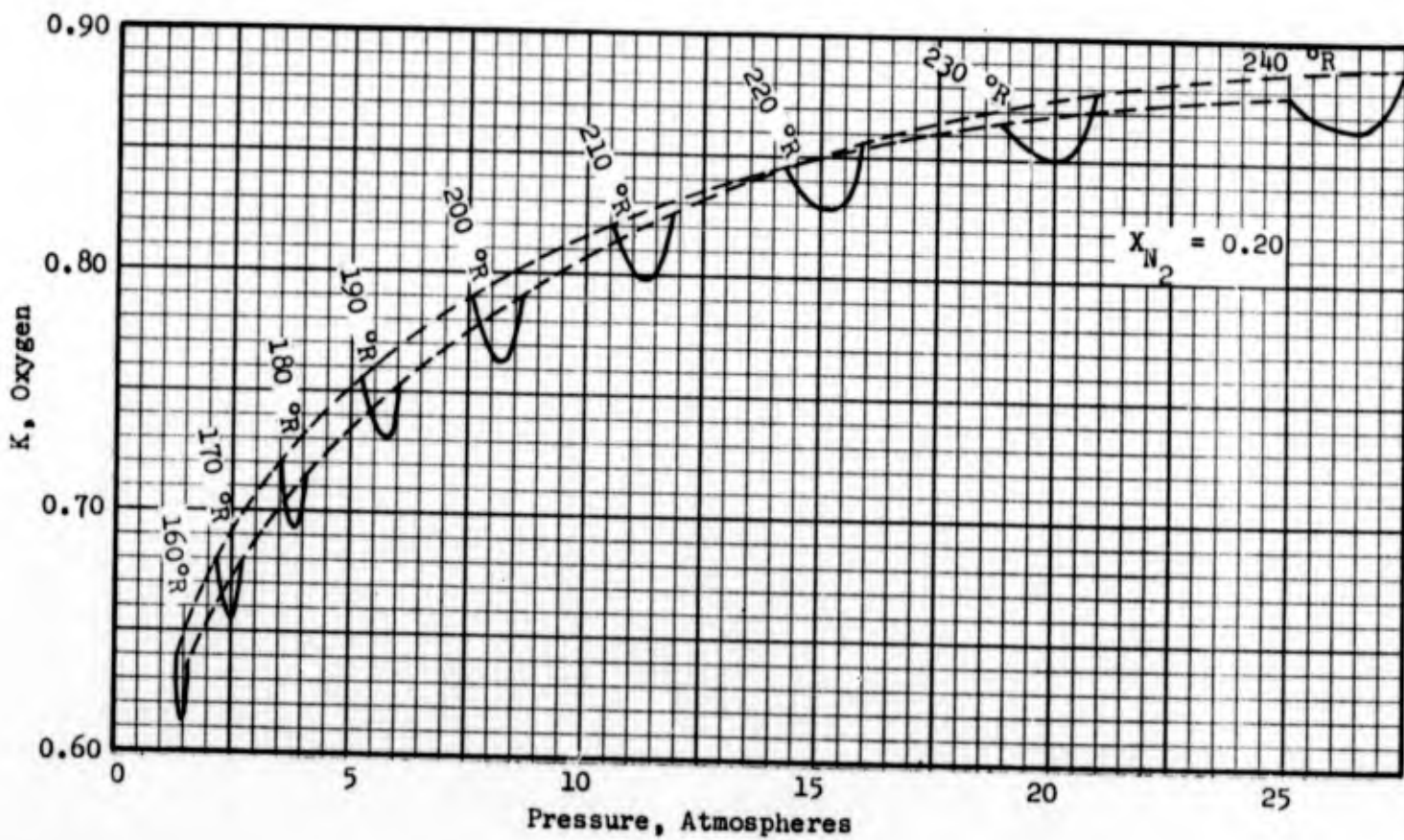
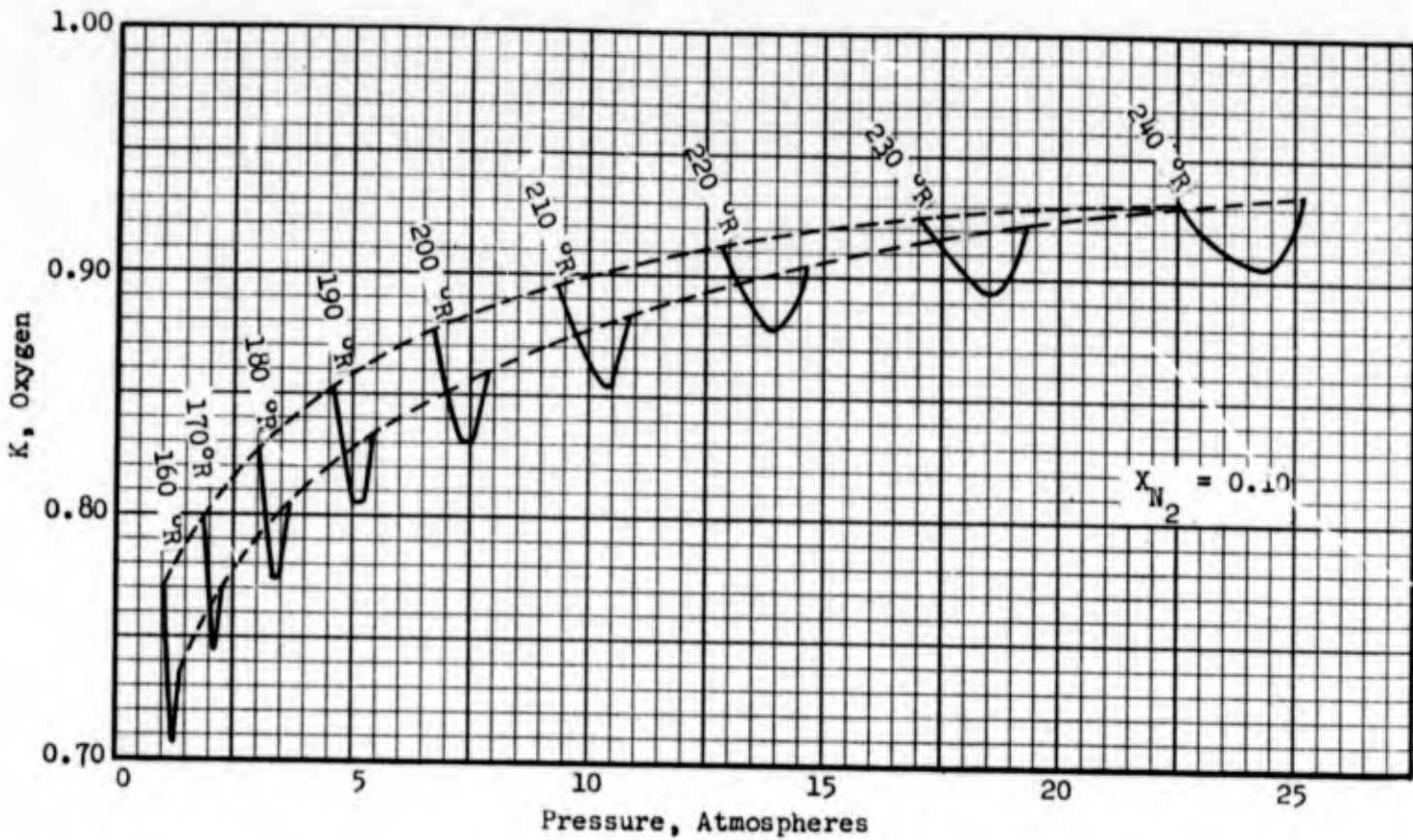


Figure 102. K-Values of Oxygen.

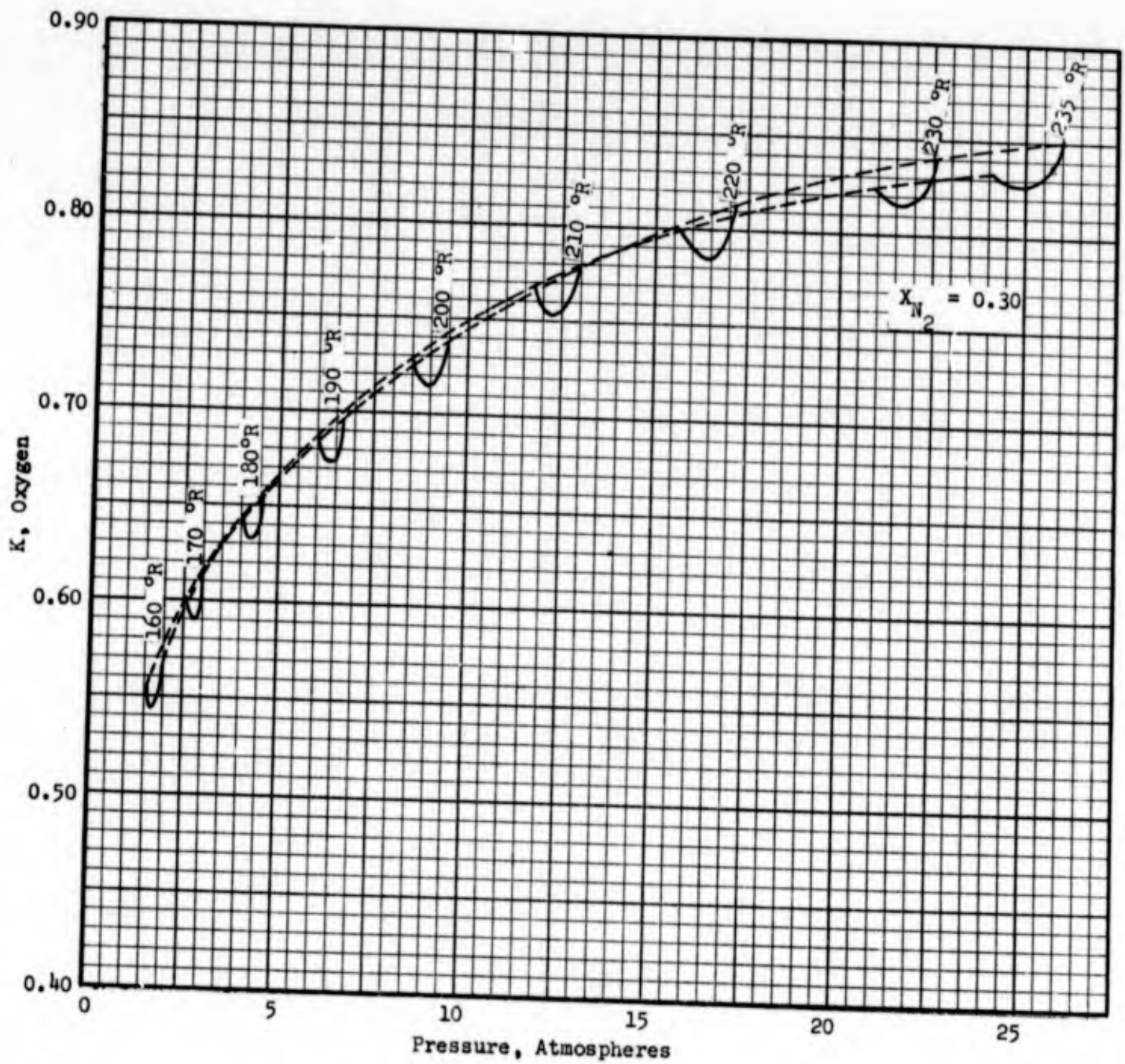


Figure 103. K-Values of Oxygen.

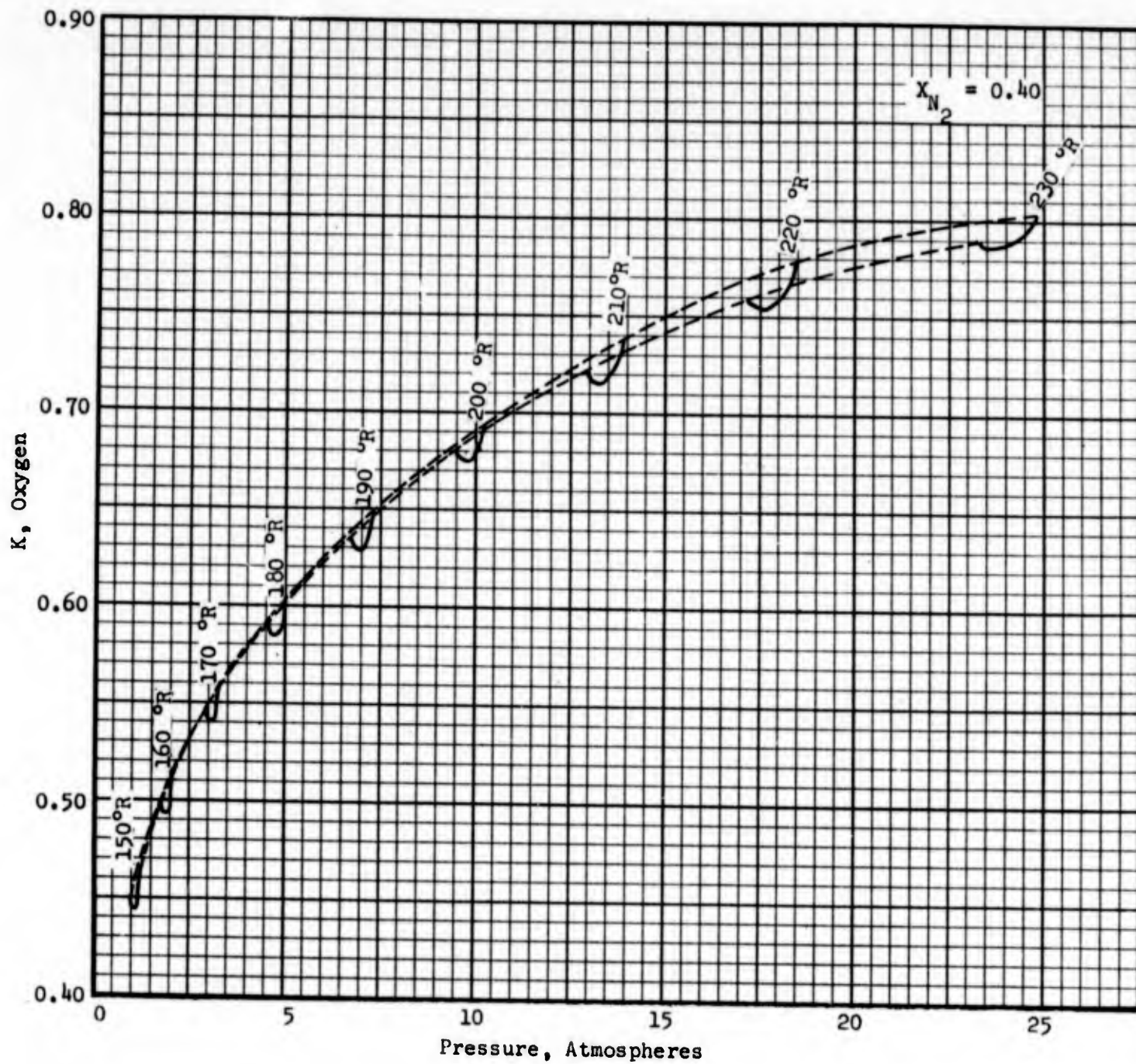


Figure 104. K-Values of Oxygen.

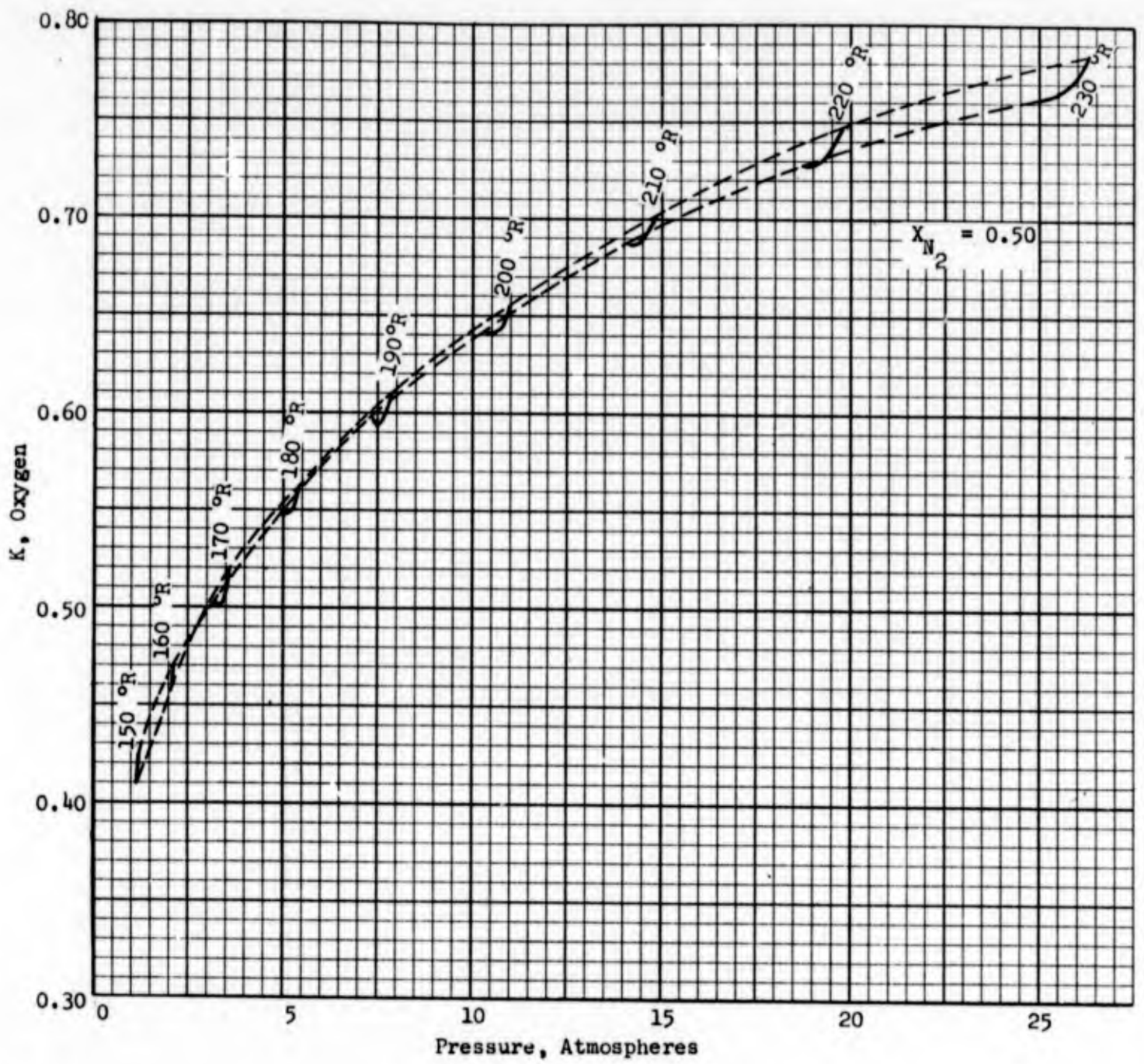


Figure 105. K-Values of Oxygen

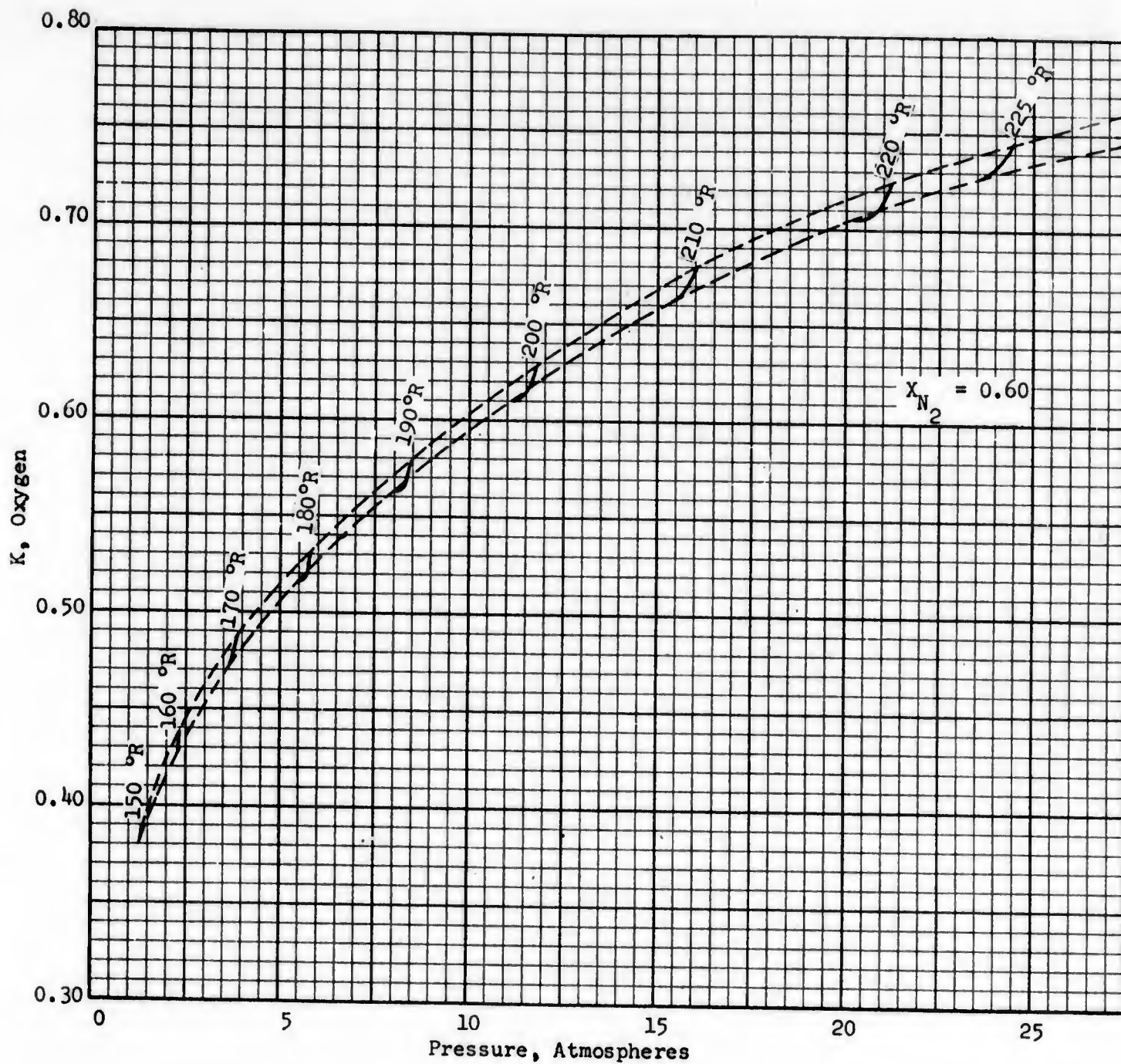


Figure 106. K-Values of Oxygen

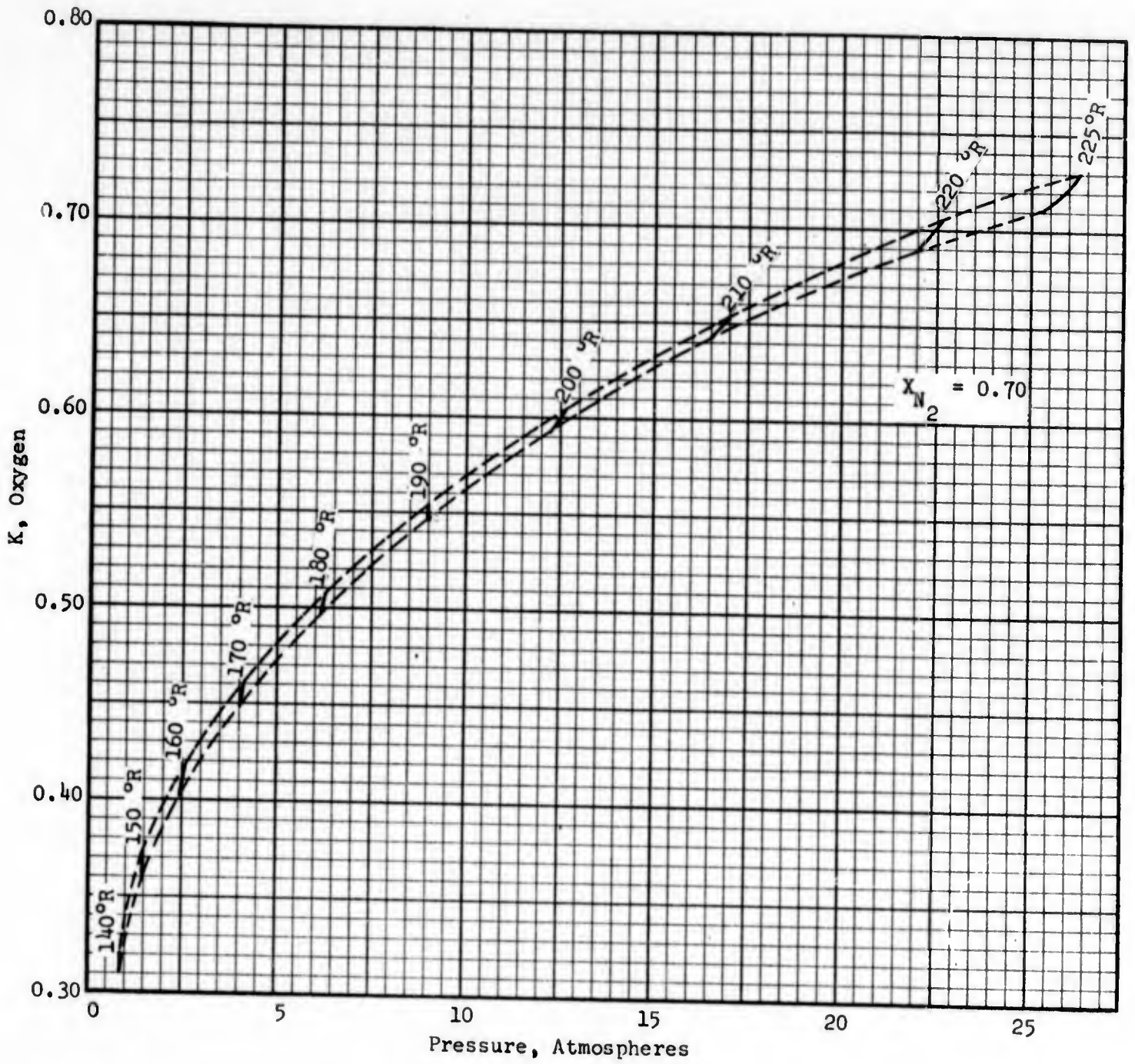


Figure 107. K-Values of Oxygen.

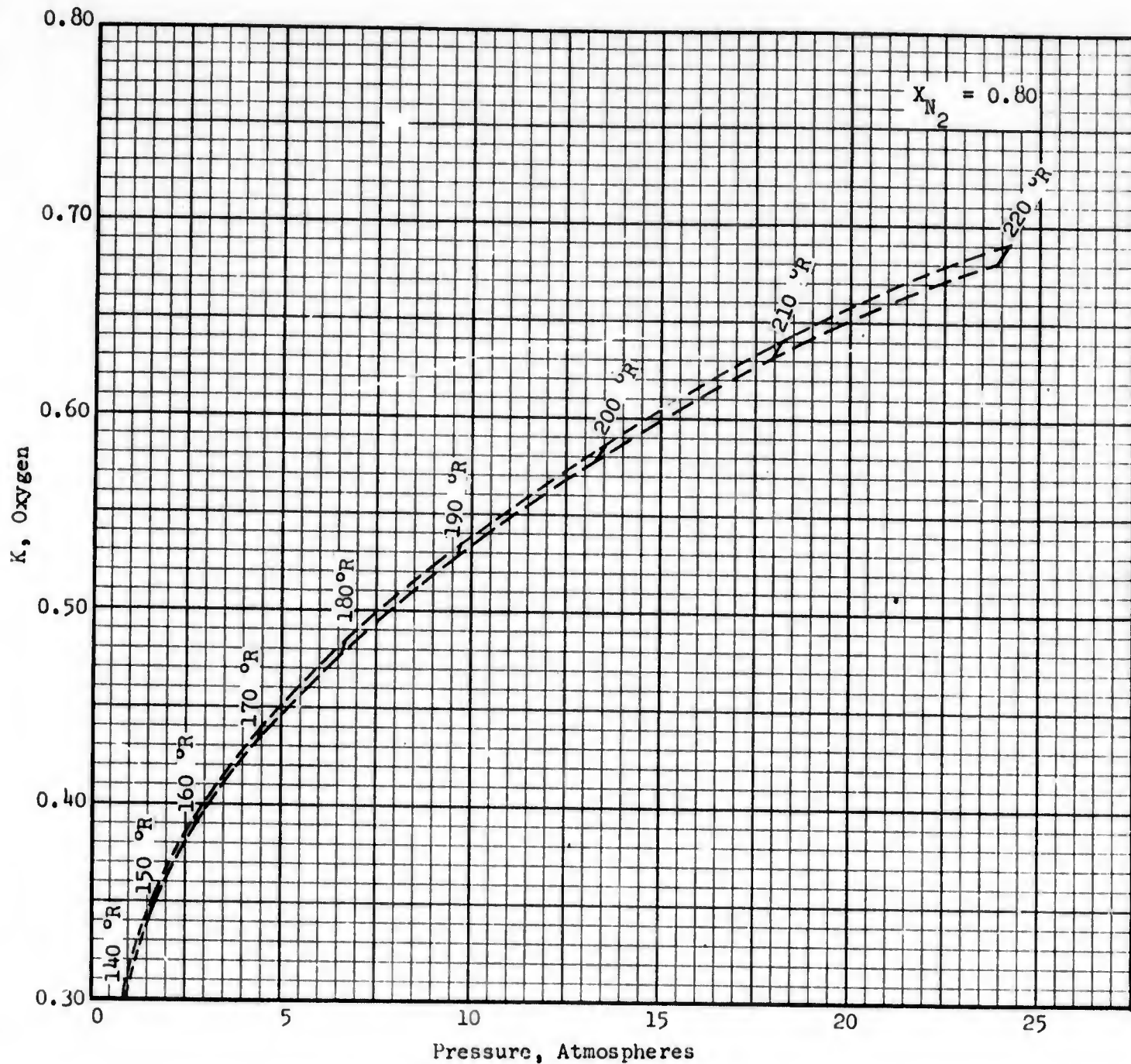


Figure 108. K-Values of Oxygen.



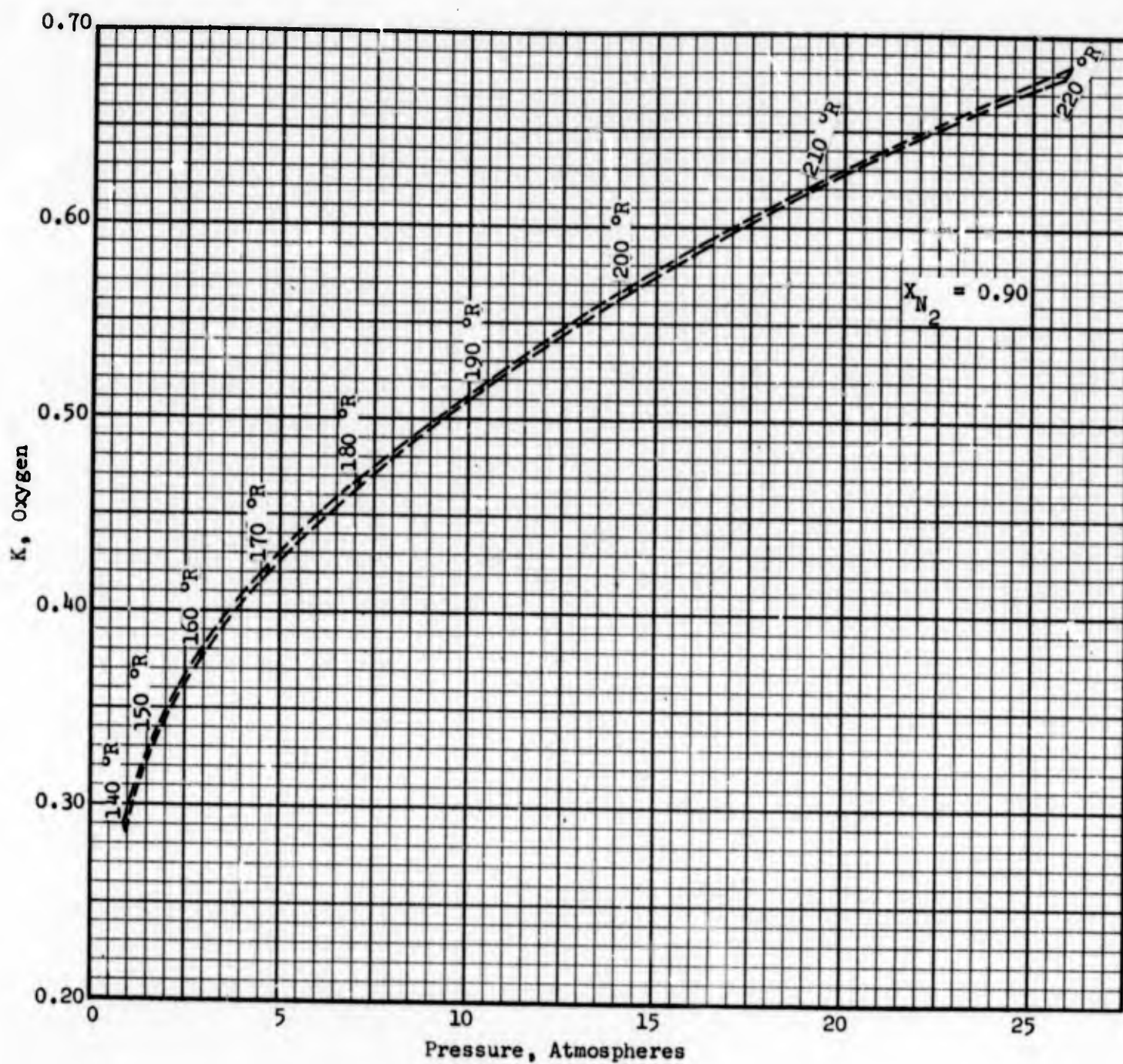


Figure 109. K-Values of Oxygen.

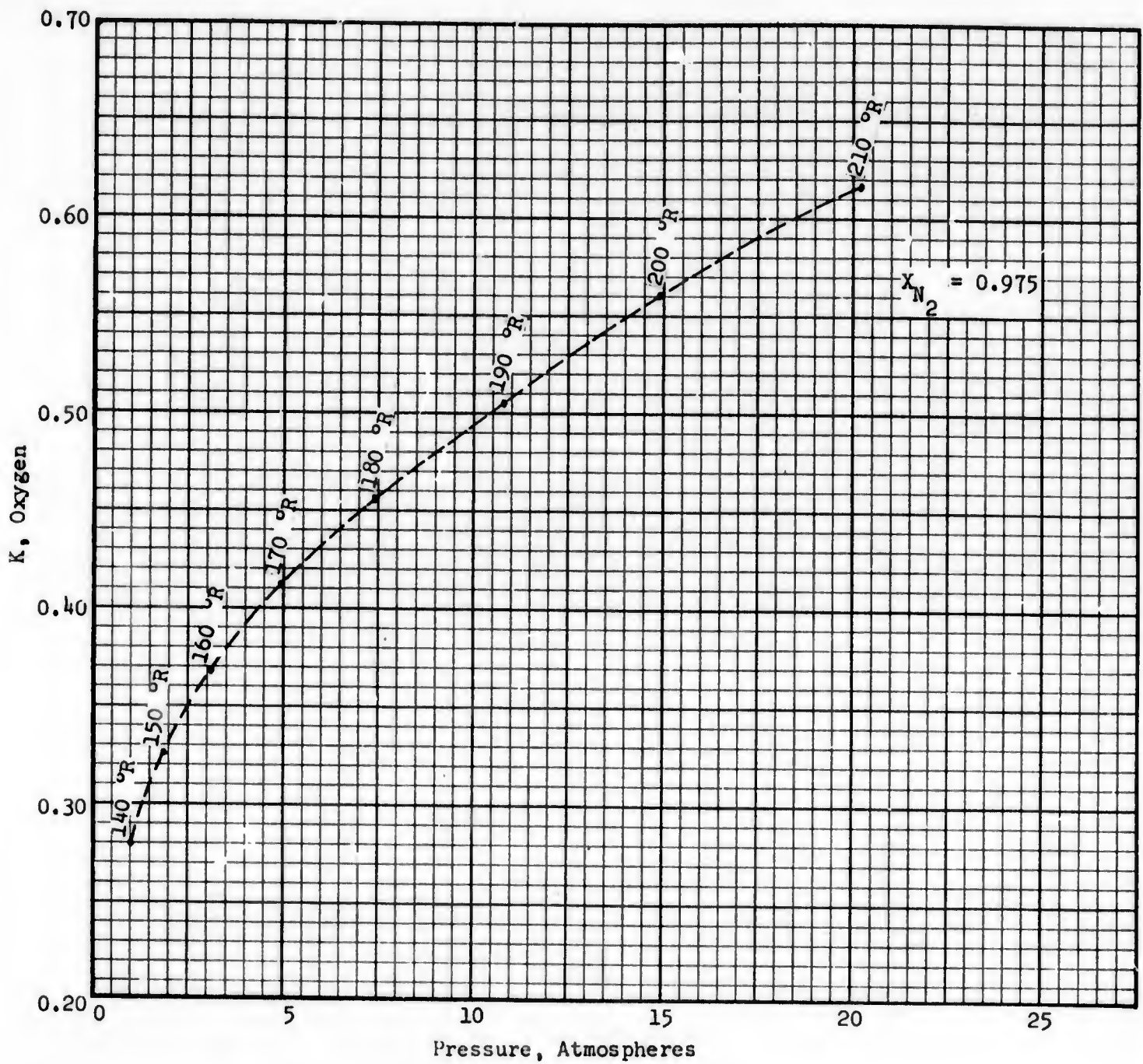


Figure 110. K-Values of Oxygen.

B. Relative Volatility of Argon to Nitrogen in Ternary System

The 12 graphs to follow present the relative volatility of argon to nitrogen defined

$$\alpha_{\text{Ar-N}_2} = \frac{y_{\text{Ar}}}{x_{\text{Ar}}} \frac{x_{\text{N}_2}}{y_{\text{N}_2}} \quad (51)$$

as a function of mole fraction argon in the liquid along selected isobars. The graphs are arranged in order of increasing mole percent nitrogen in the liquid.

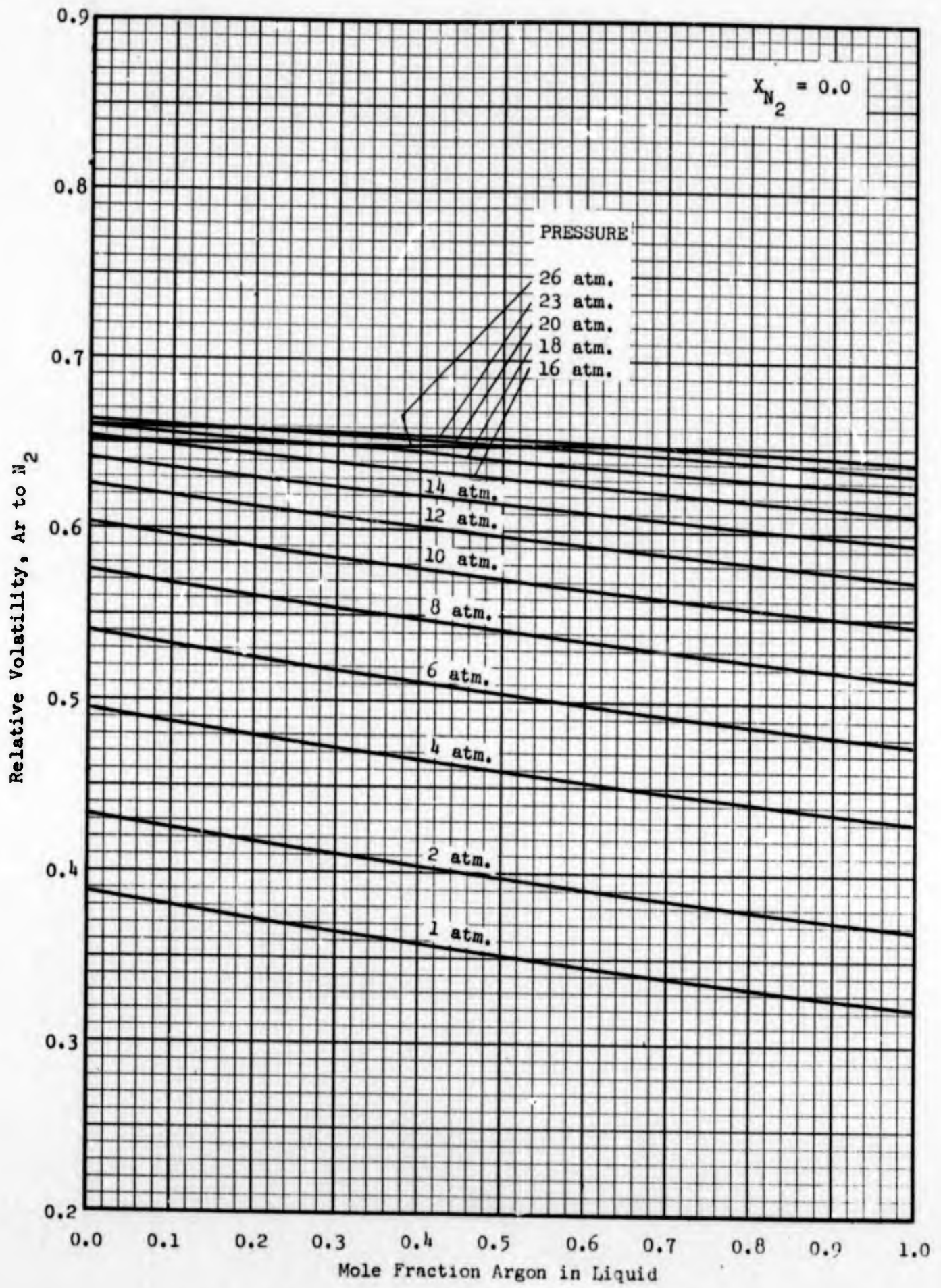


Figure 111. Relative Volatility of Argon to Nitrogen.

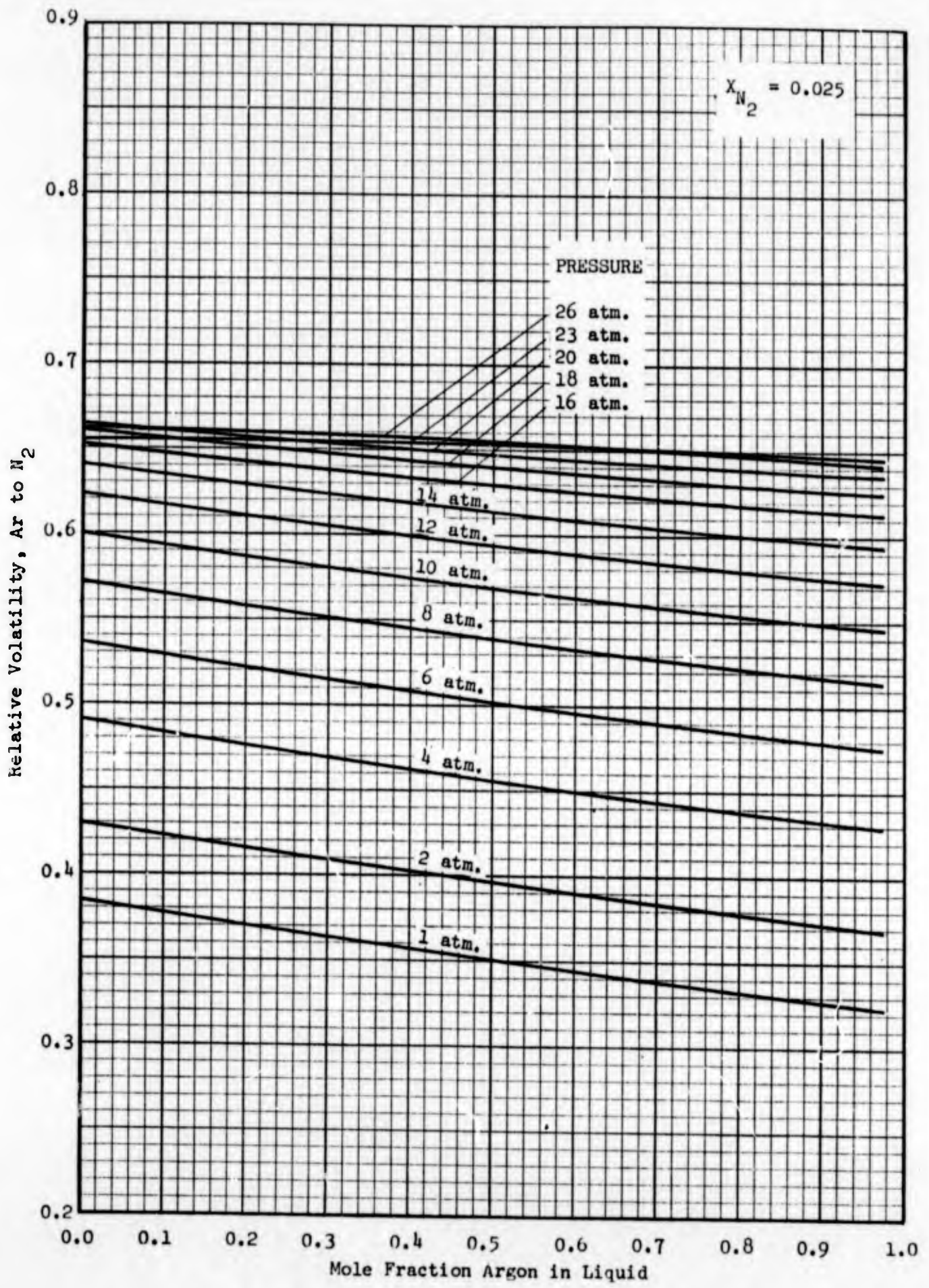


Figure 112. Relative Volatility of Argon to Nitrogen.

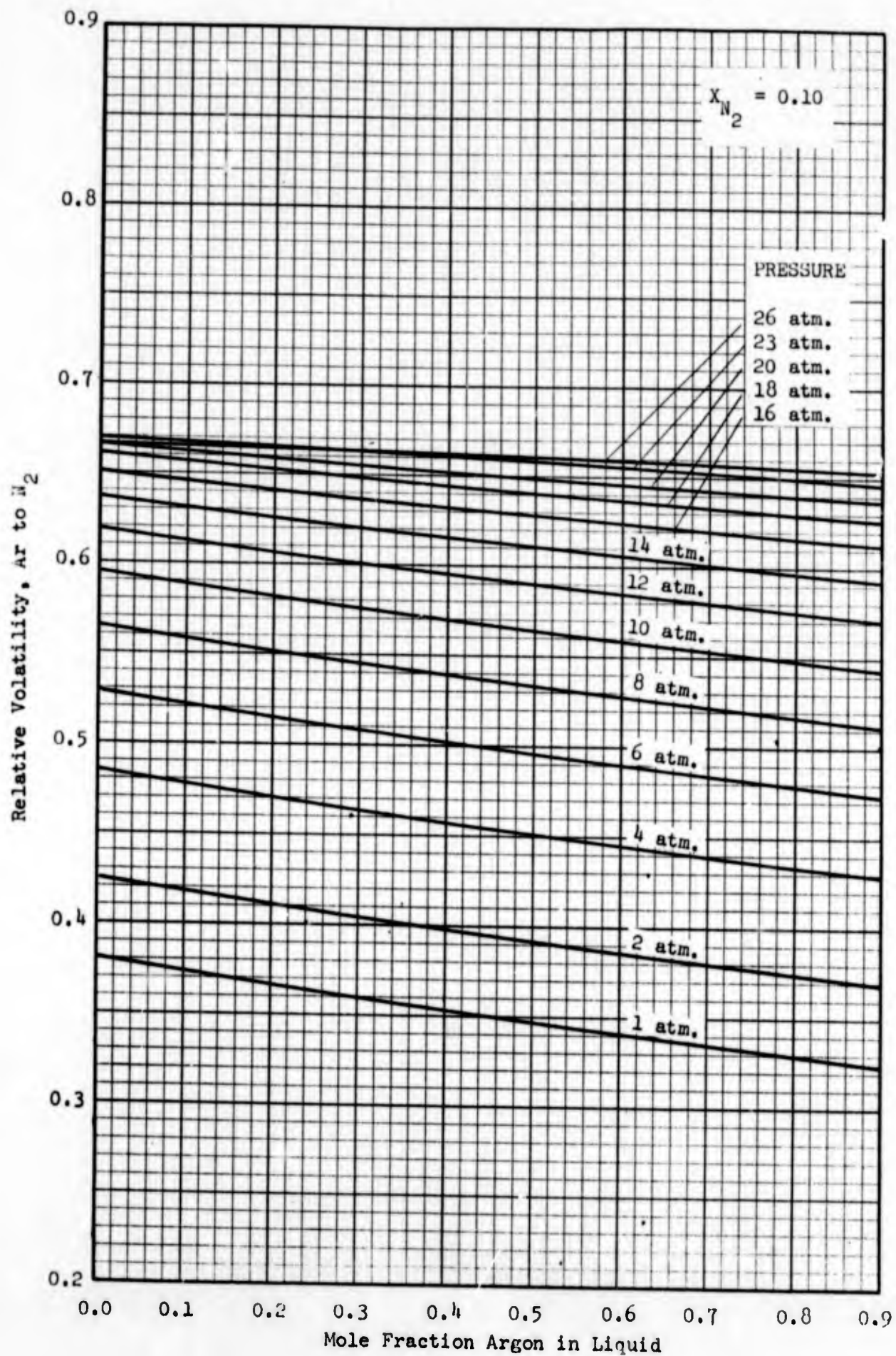


Figure 113. Relative Volatility of Argon to Nitrogen.

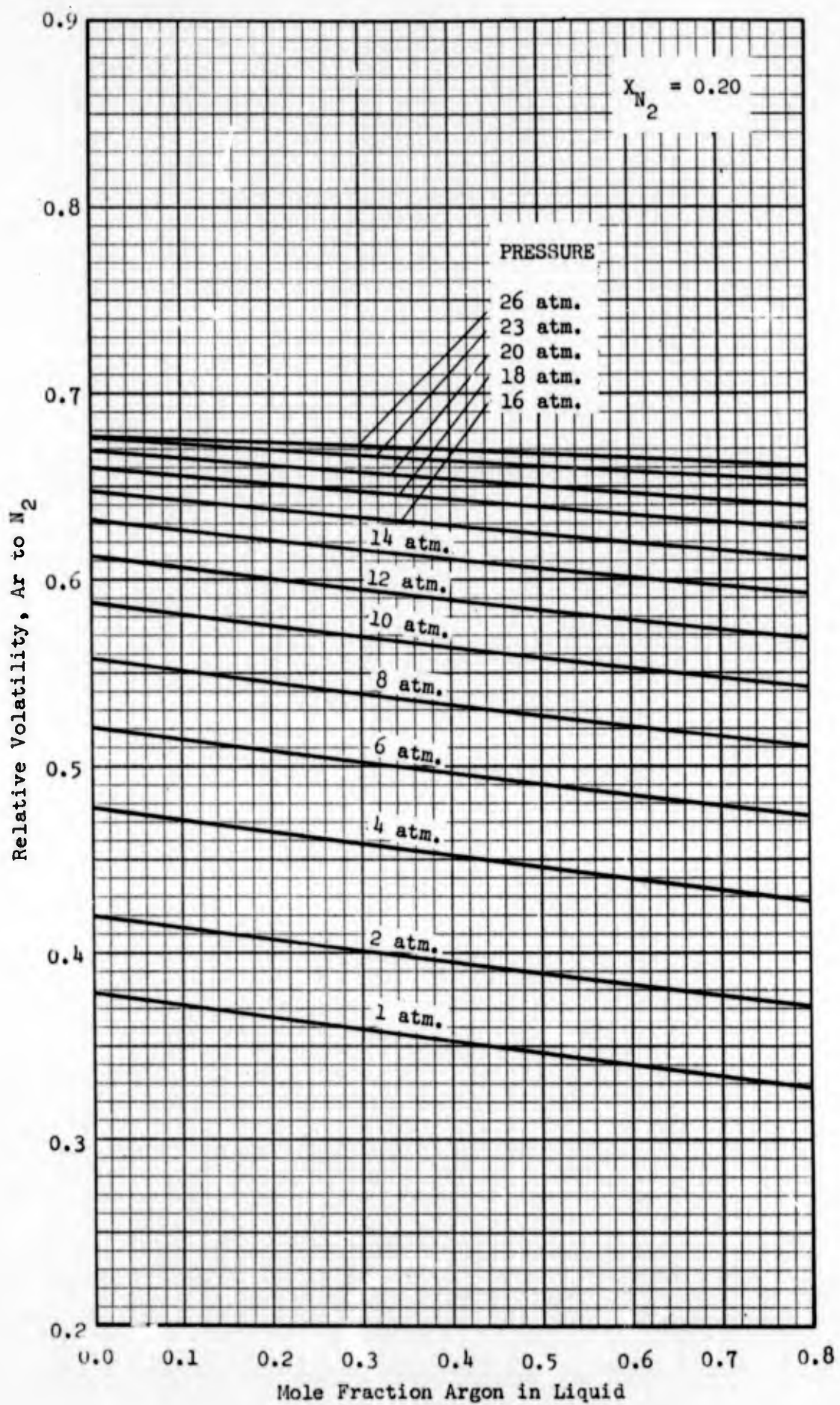


Figure 114. Relative Volatility of Argon to Nitrogen.

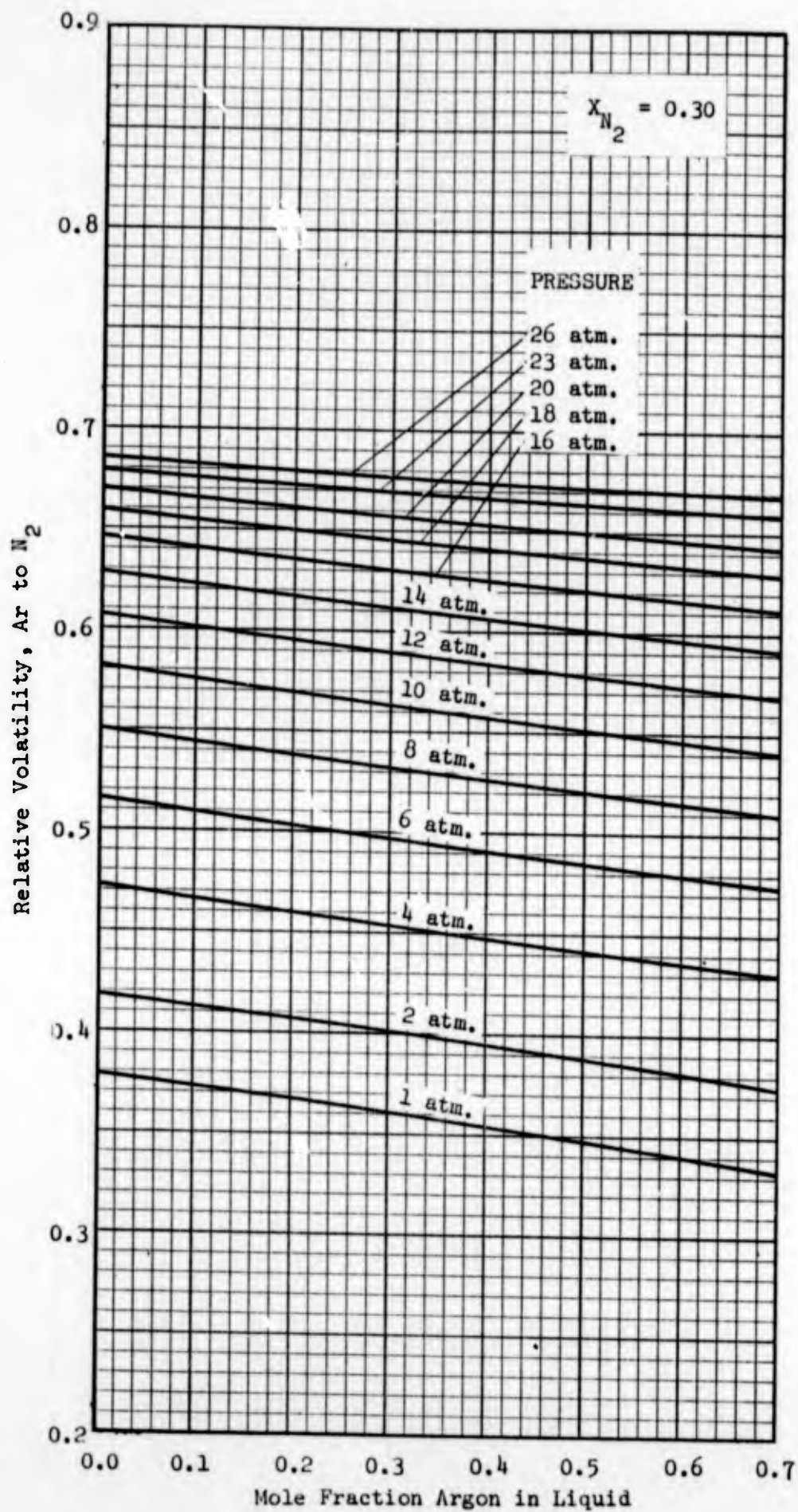


Figure 115. Relative Volatility of Argon to Nitrogen.



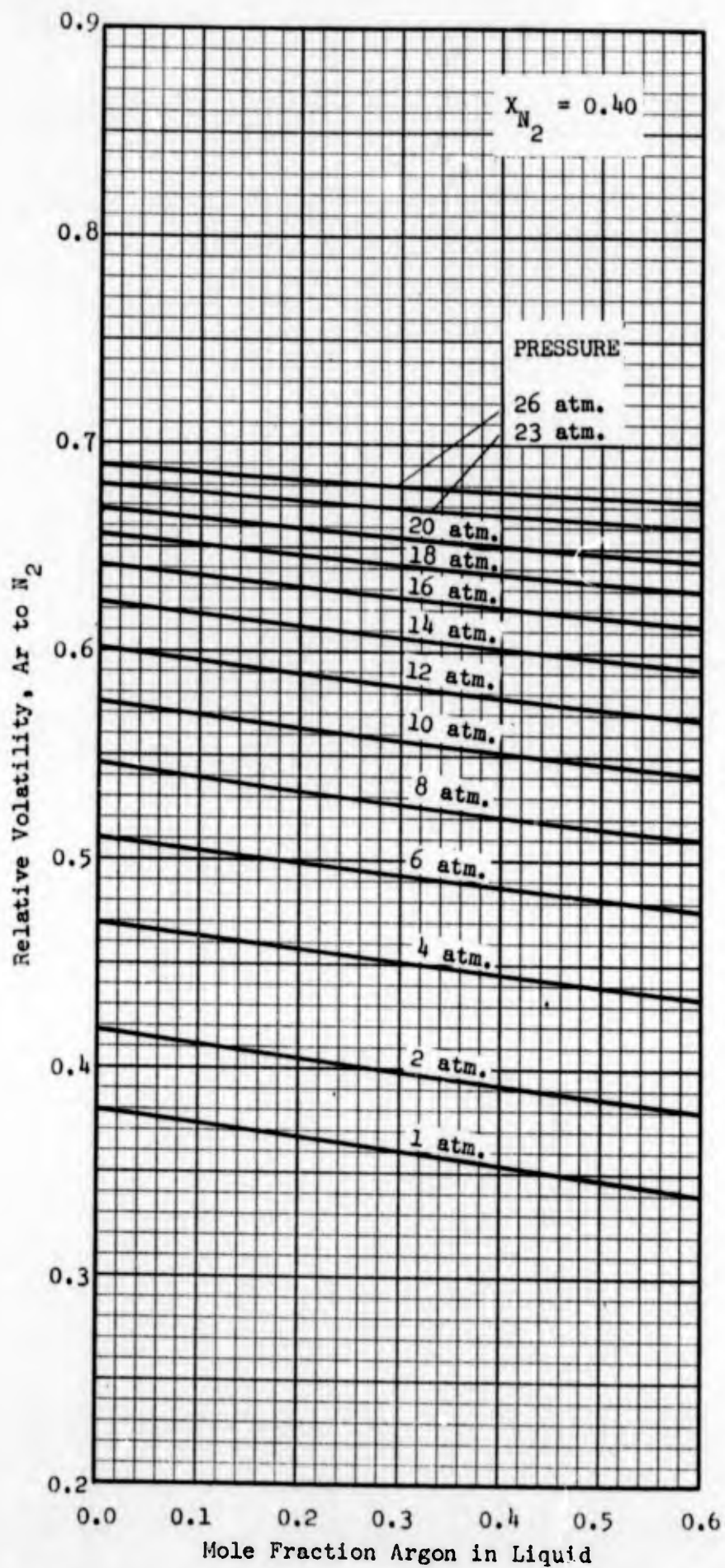


Figure 116. Relative Volatility of Argon to Nitrogen.

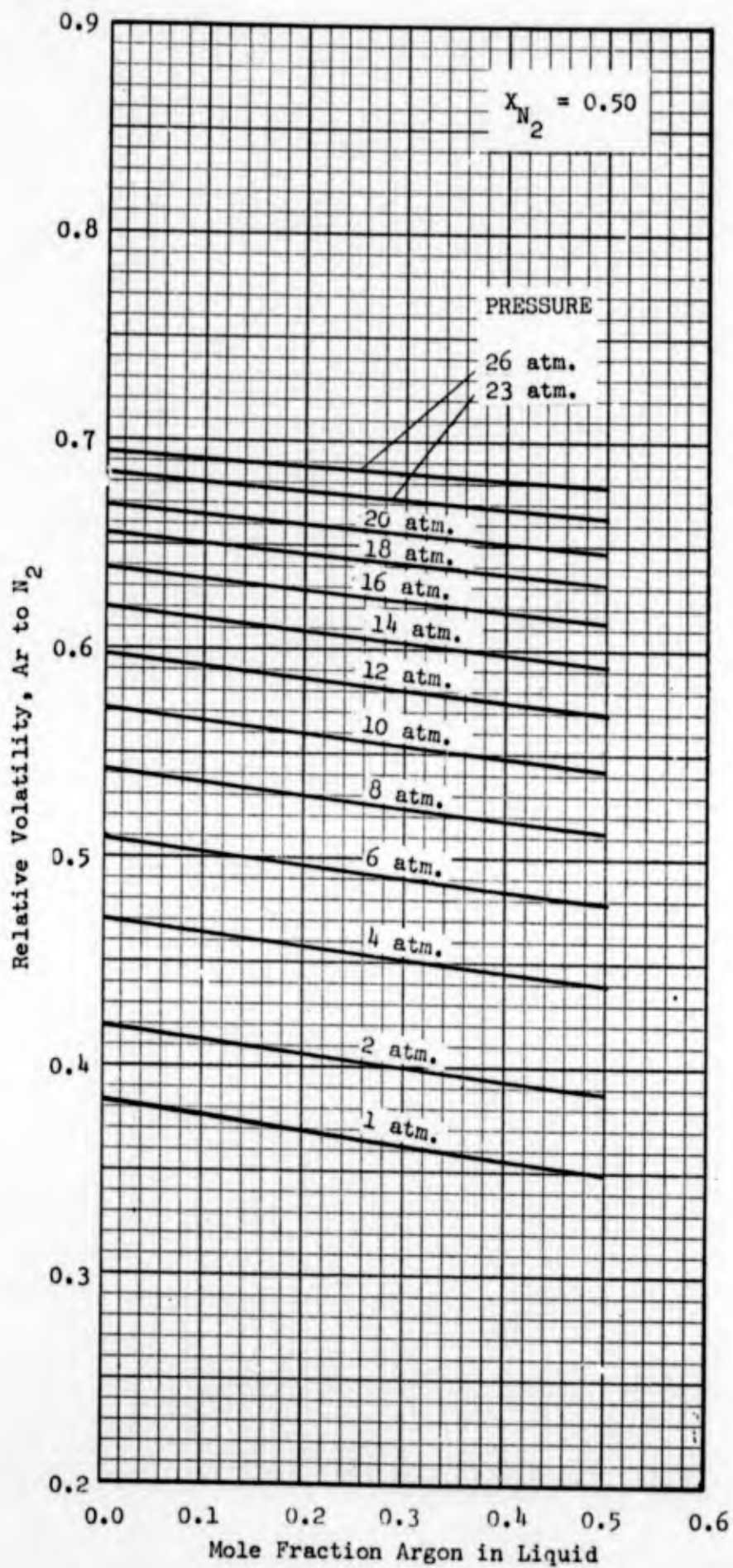


Figure 117. Relative Volatility of Argon to Nitrogen.

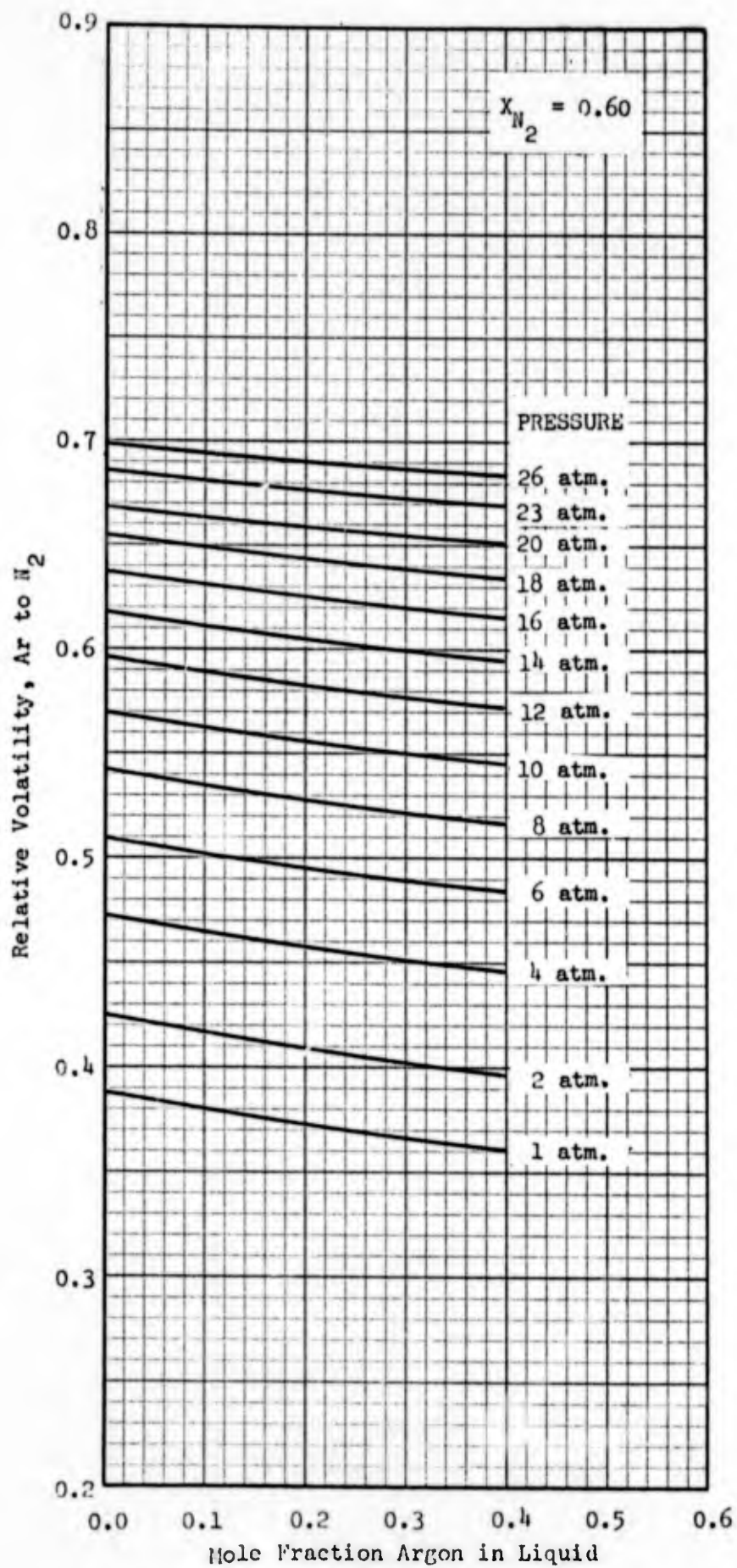


Figure 118. Relative Volatility of Argon to Nitrogen.

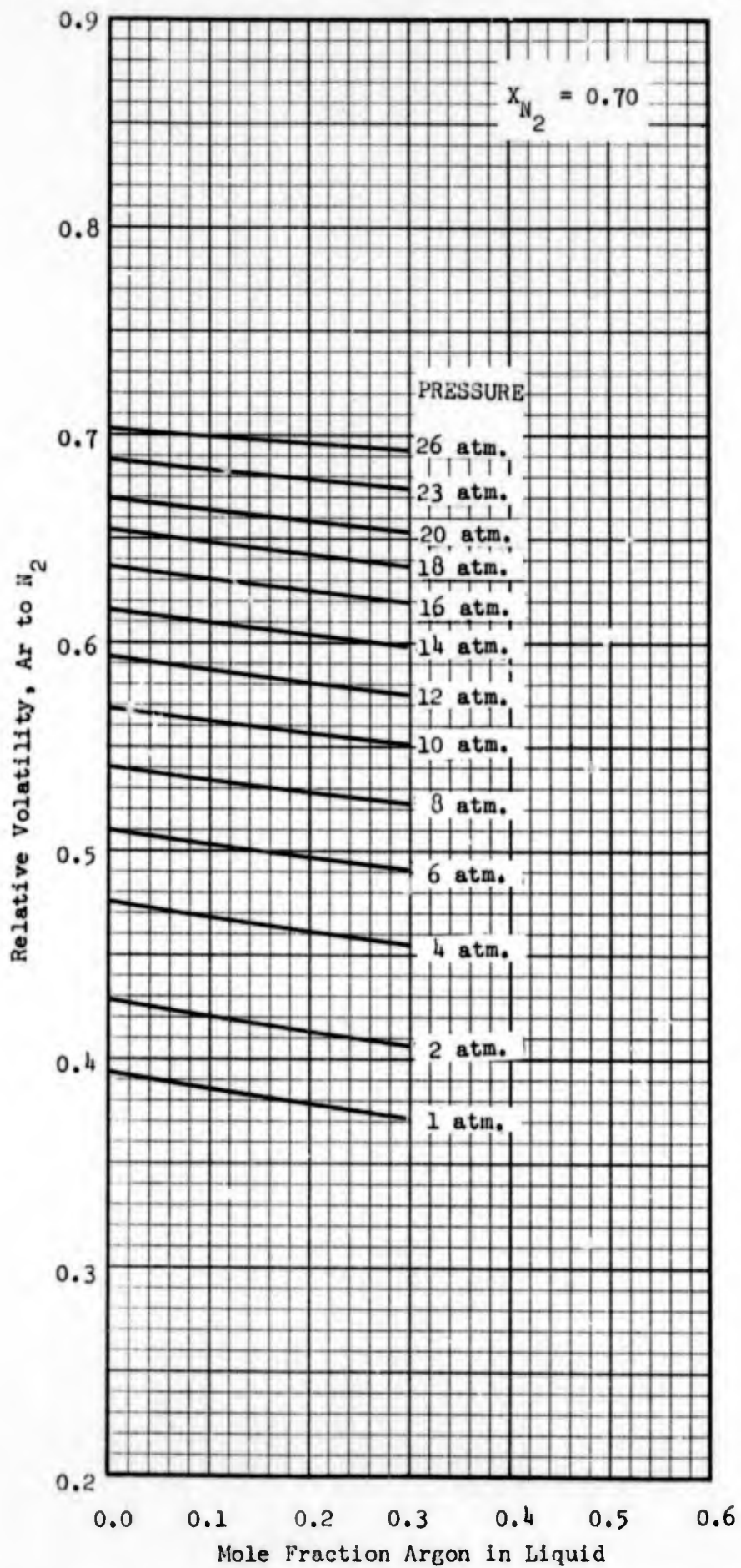


Figure 119. Relative Volatility of Argon to Nitrogen.

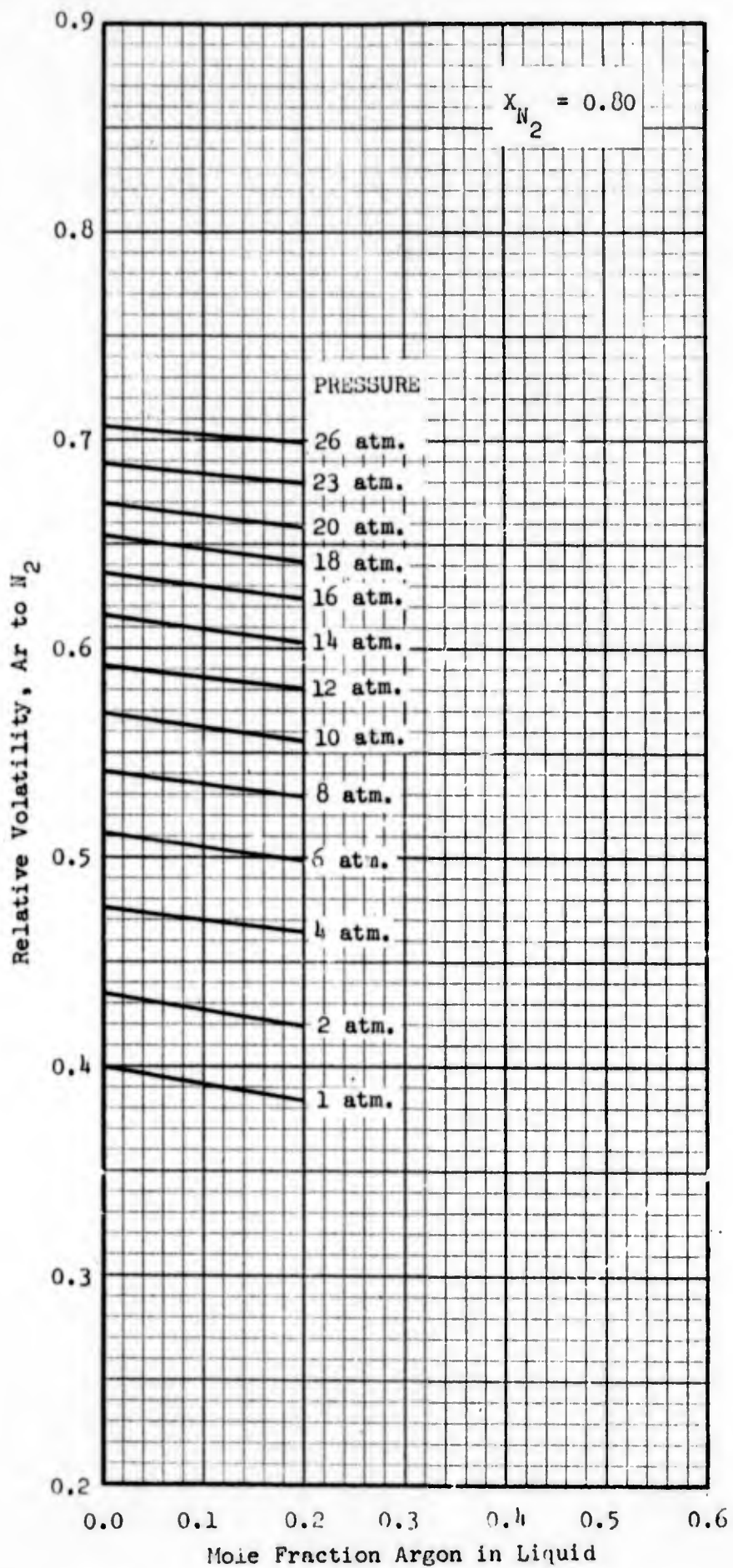


Figure 120. Relative Volatility of Argon to Nitrogen.

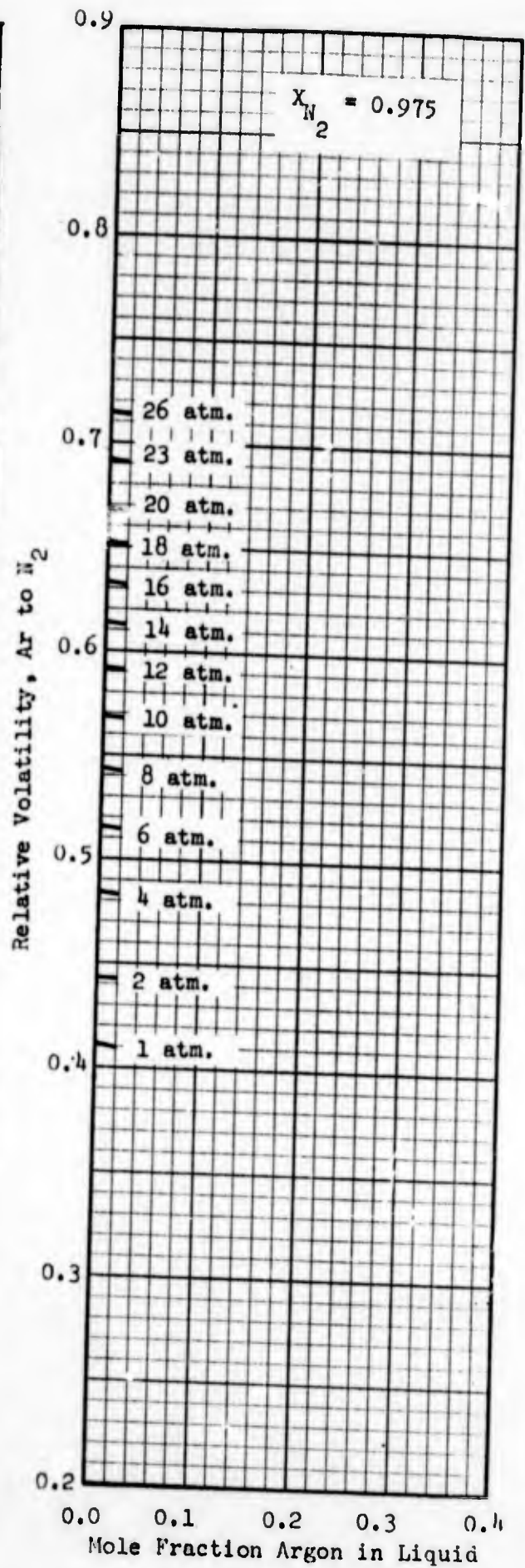
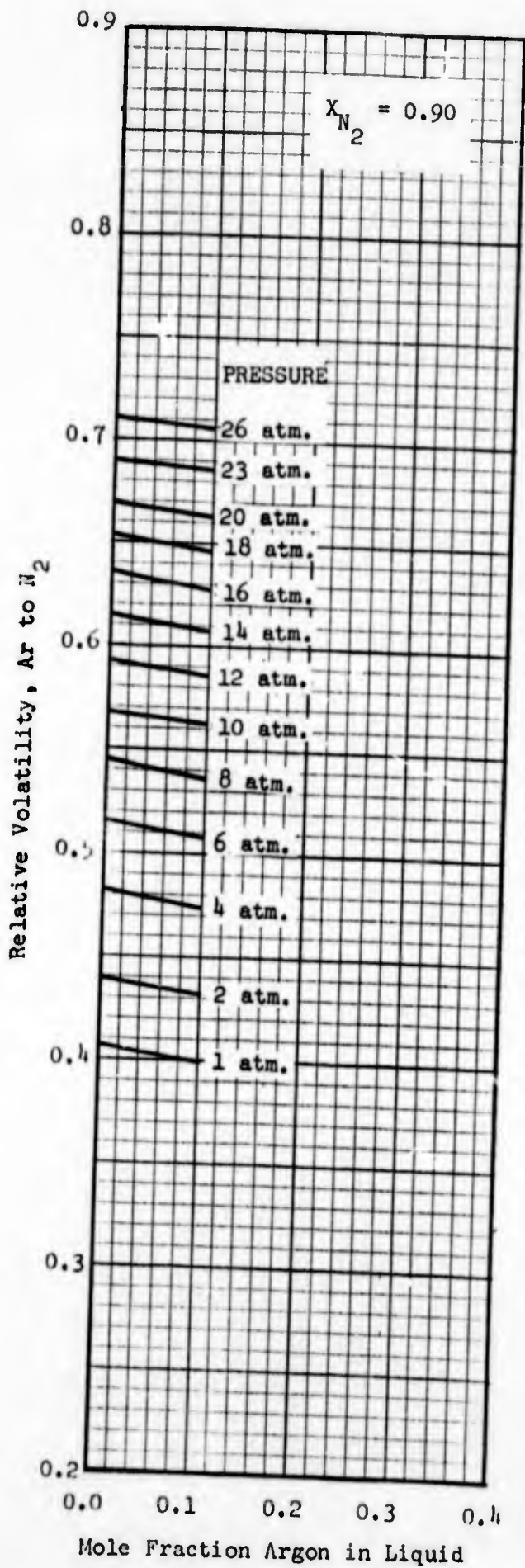


Figure 121. Relative Volatility of Argon to Nitrogen.

C. Relative Volatility of Argon to Oxygen  
in Ternary System

The 12 graphs to follow present the relative volatility of argon to oxygen defined

$$\alpha_{\text{Ar-O}_2} = \frac{y_{\text{Ar}}}{x_{\text{Ar}}} \cdot \frac{x_{\text{O}_2}}{y_{\text{O}_2}} \quad (52)$$

as a function of mole fraction argon in the liquid along selected isobars. The graphs are arranged in order of increasing mole percent nitrogen in the liquid.

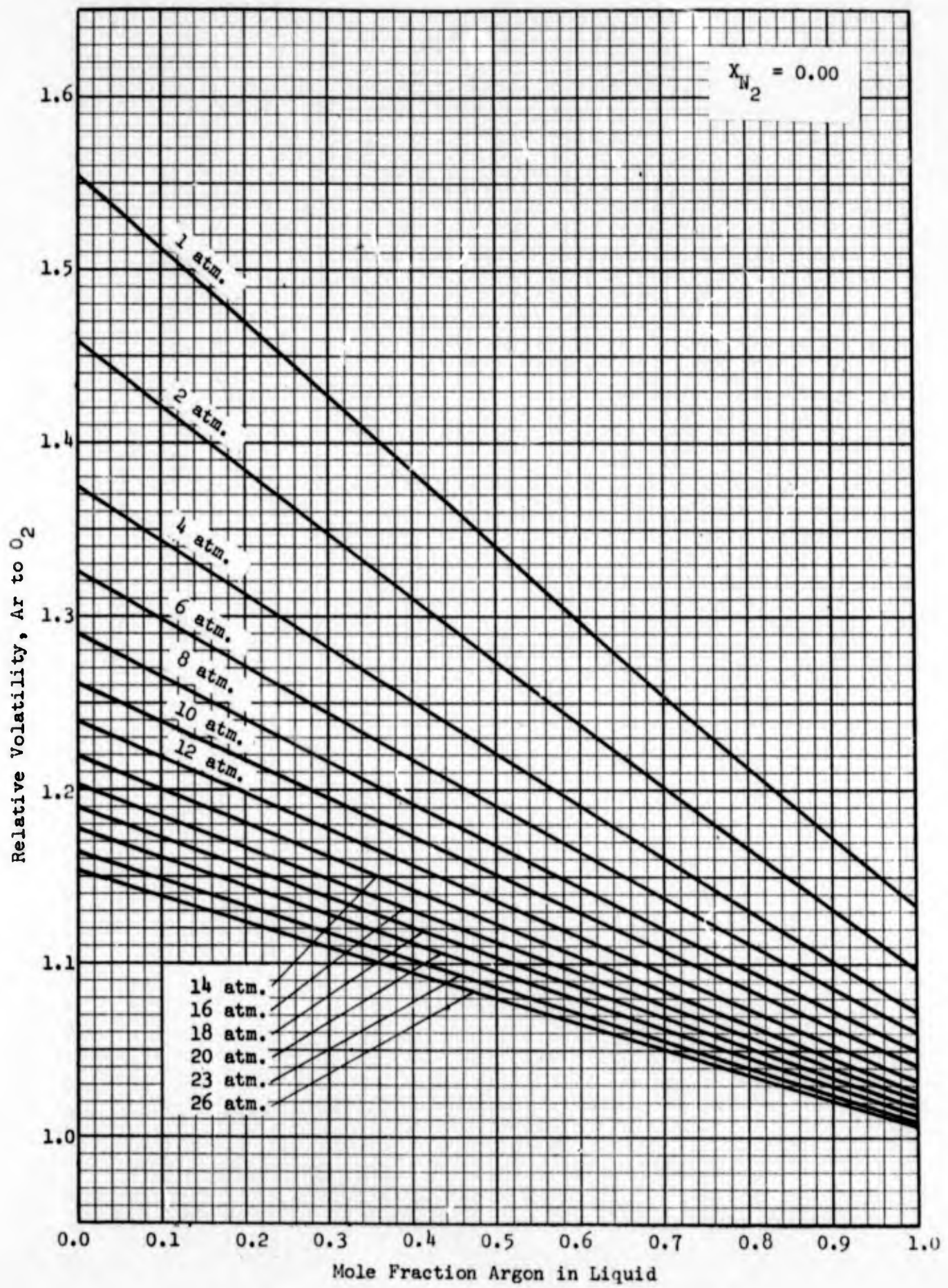


Figure 122. Relative Volatility of Argon to Oxygen.



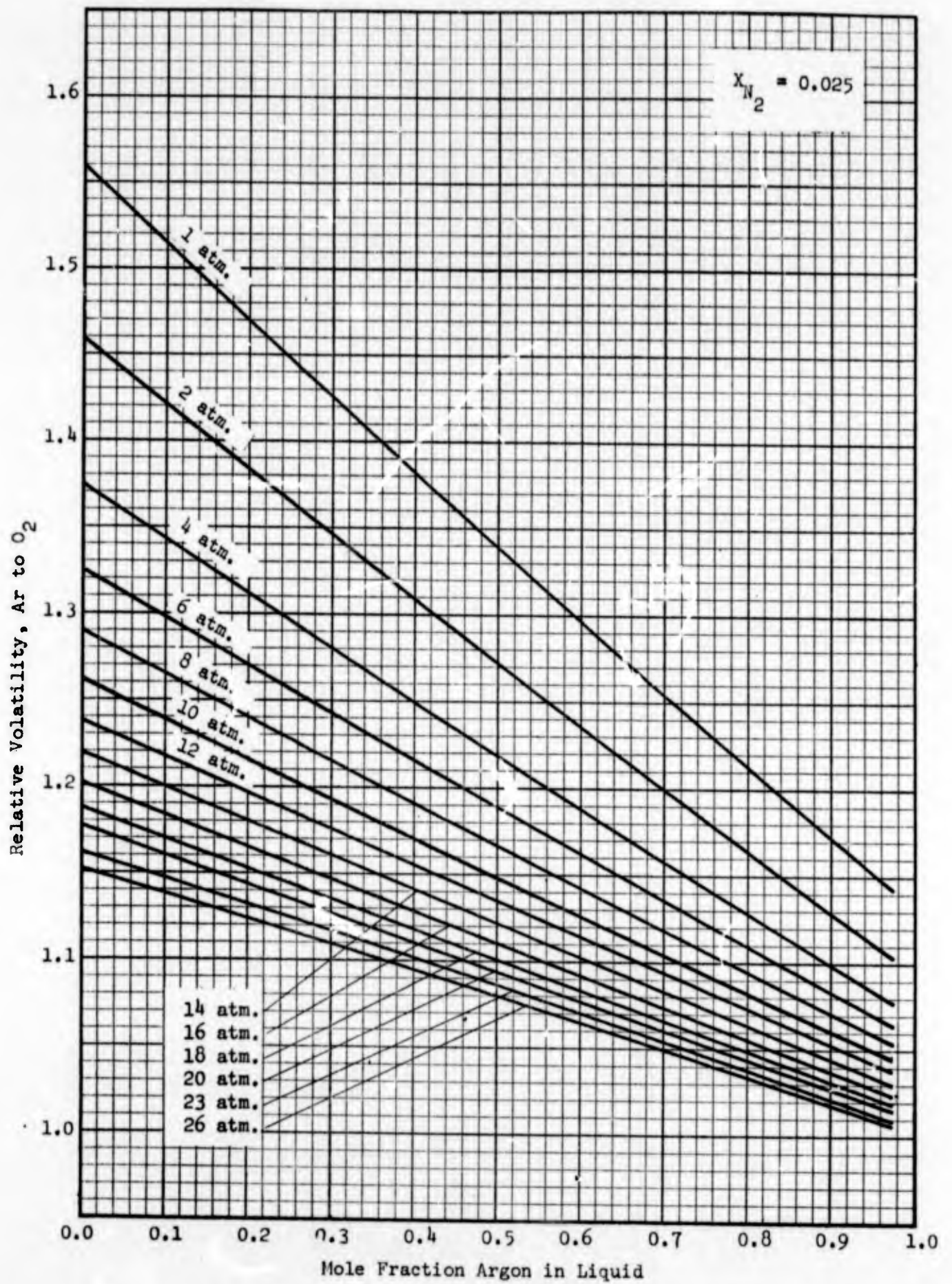


Figure 123. Relative Volatility of Argon to Oxygen.

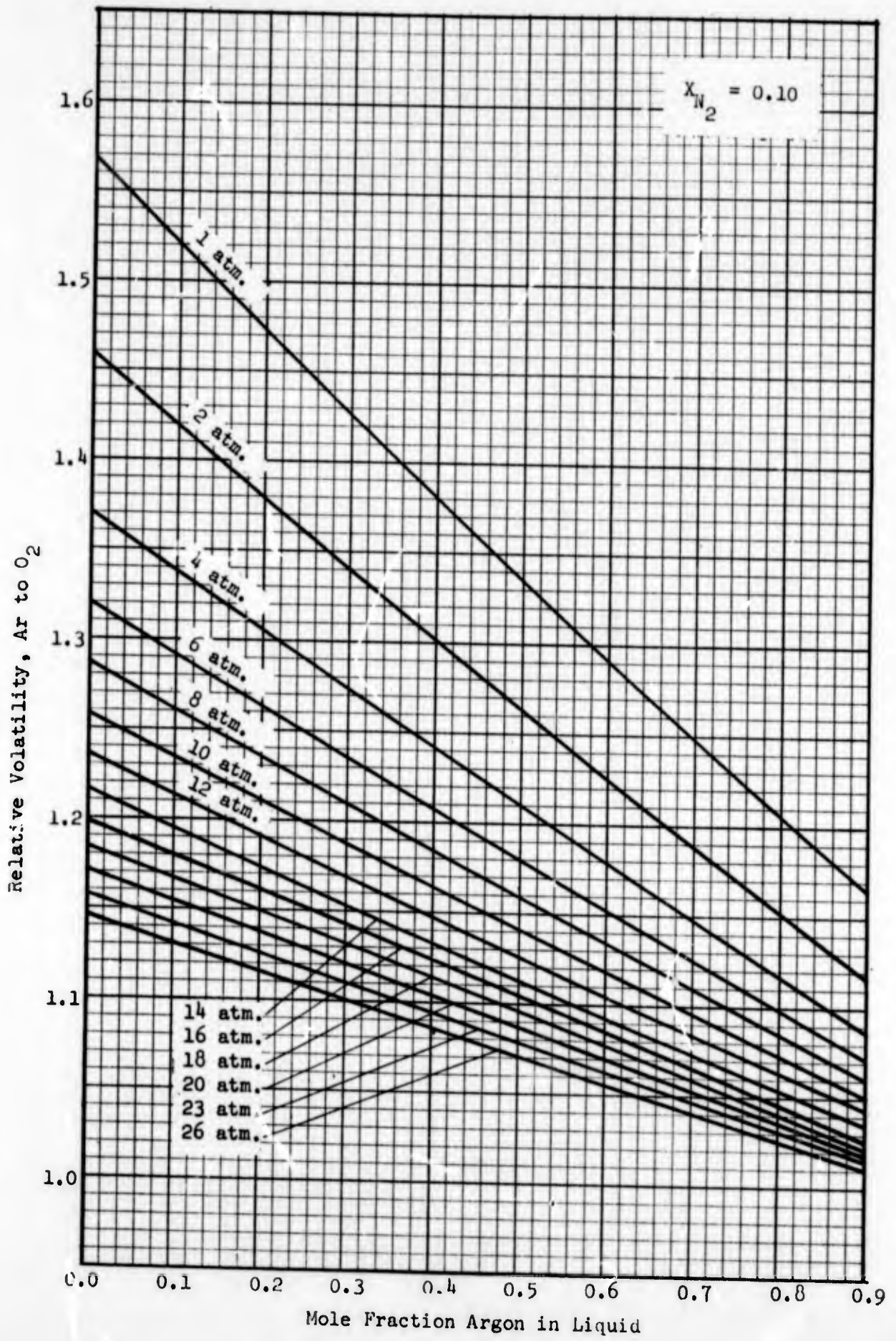


Figure 124. Relative Volatility of Argon to Oxygen.

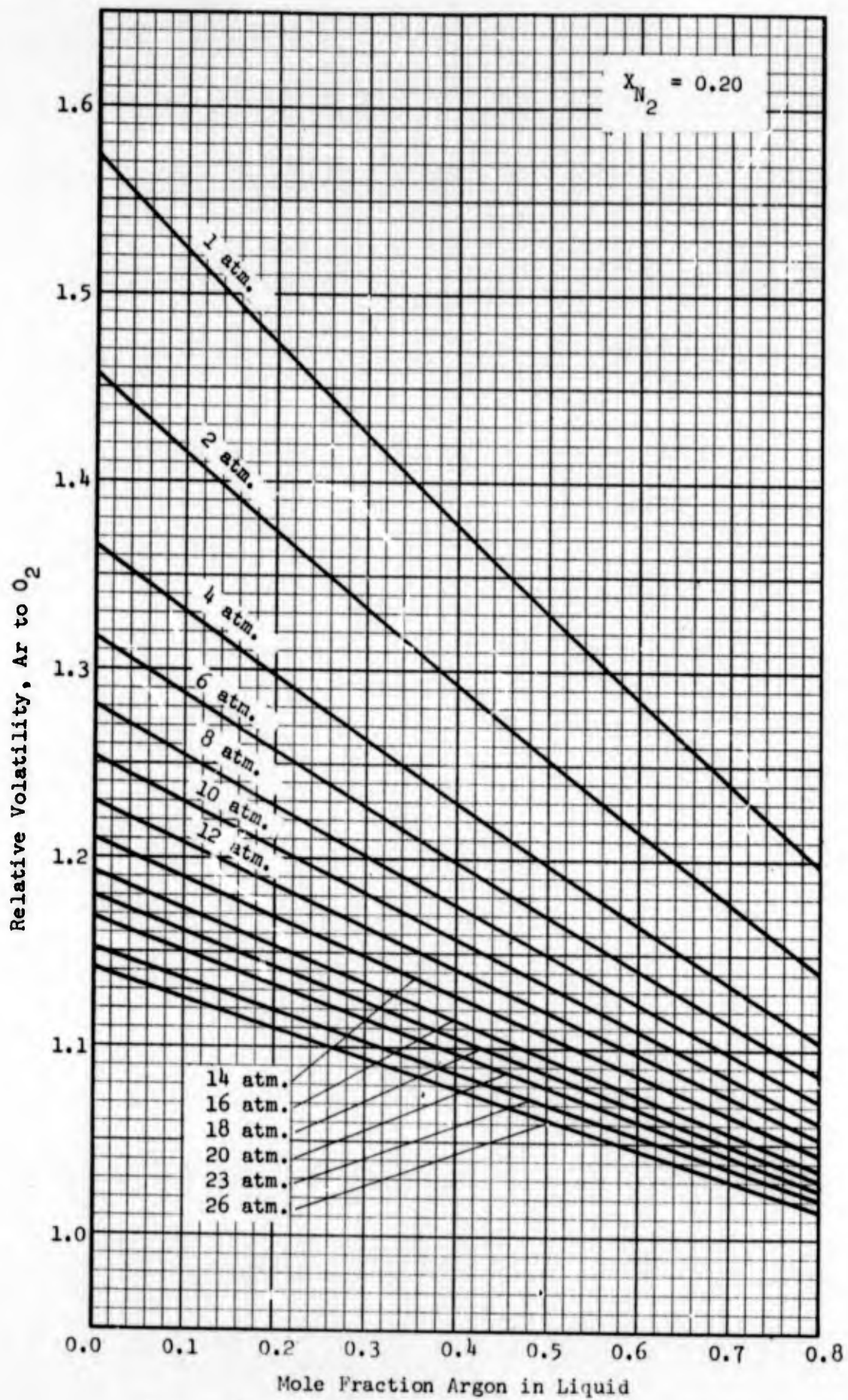


Figure 125. Relative Volatility of Argon to Oxygen.

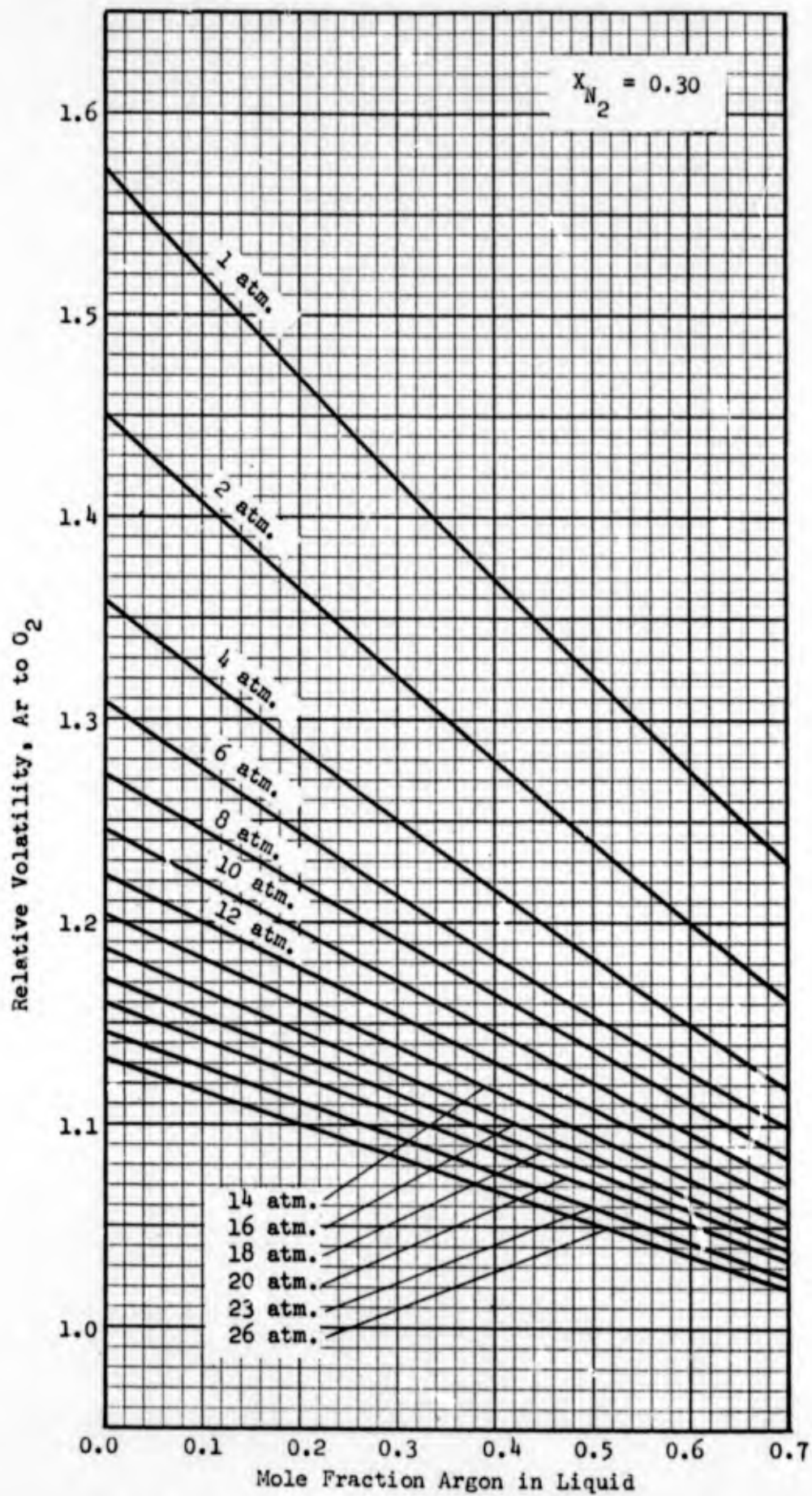


Figure 126. Relative Volatility of Argon to Oxygen.

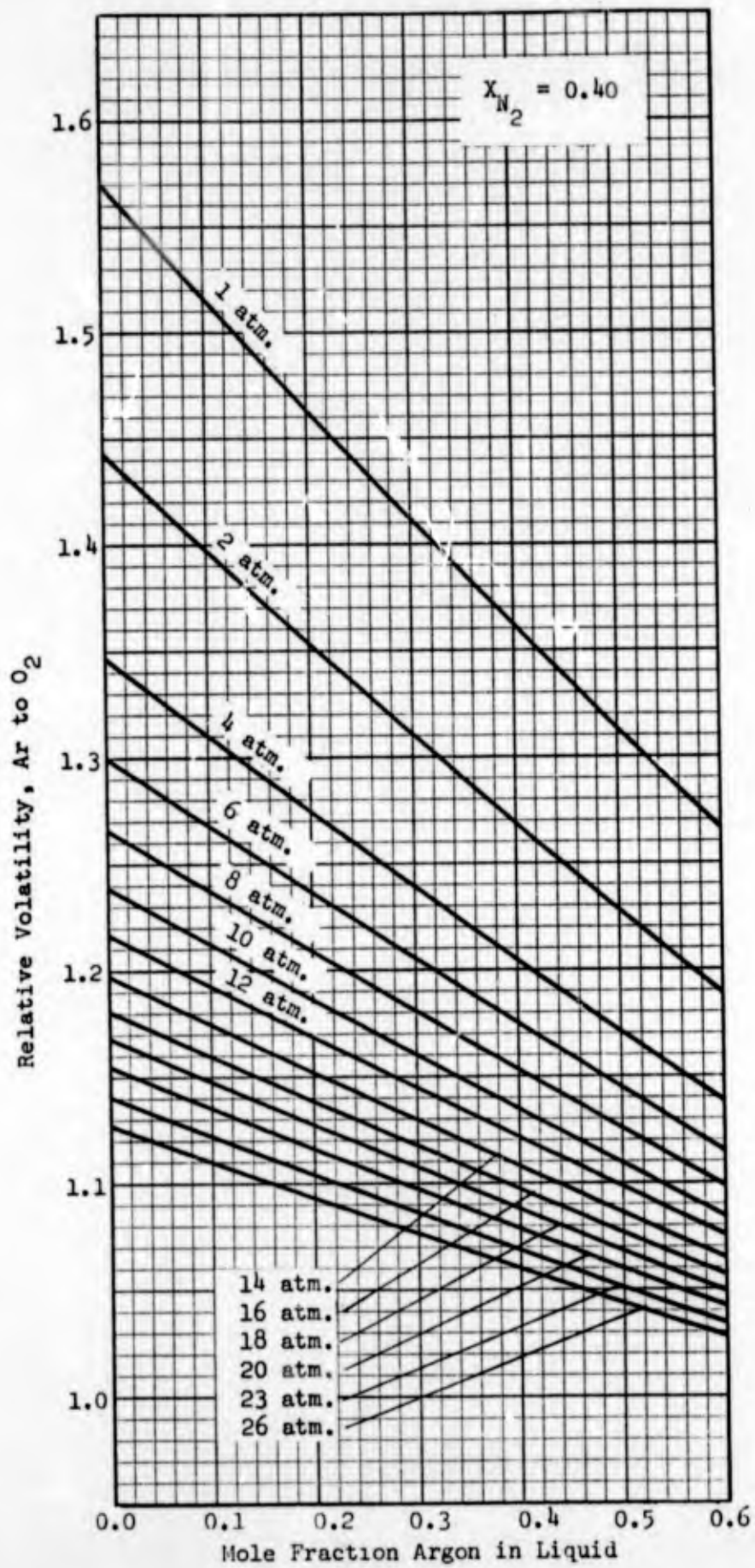


Figure 127. Relative Volatility of Argon to Oxygen.

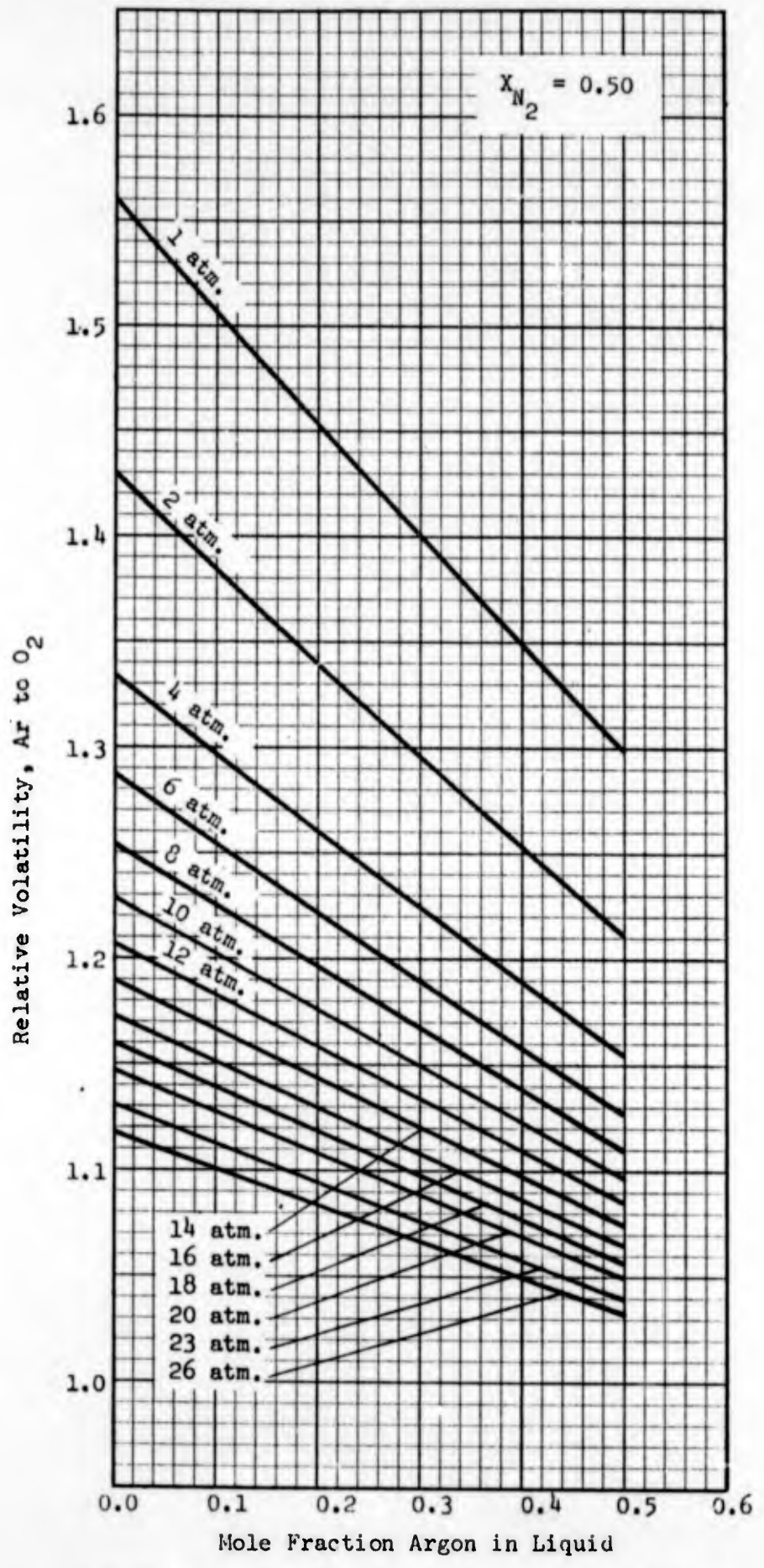


Figure 128. Relative Volatility of Argon to Oxygen.

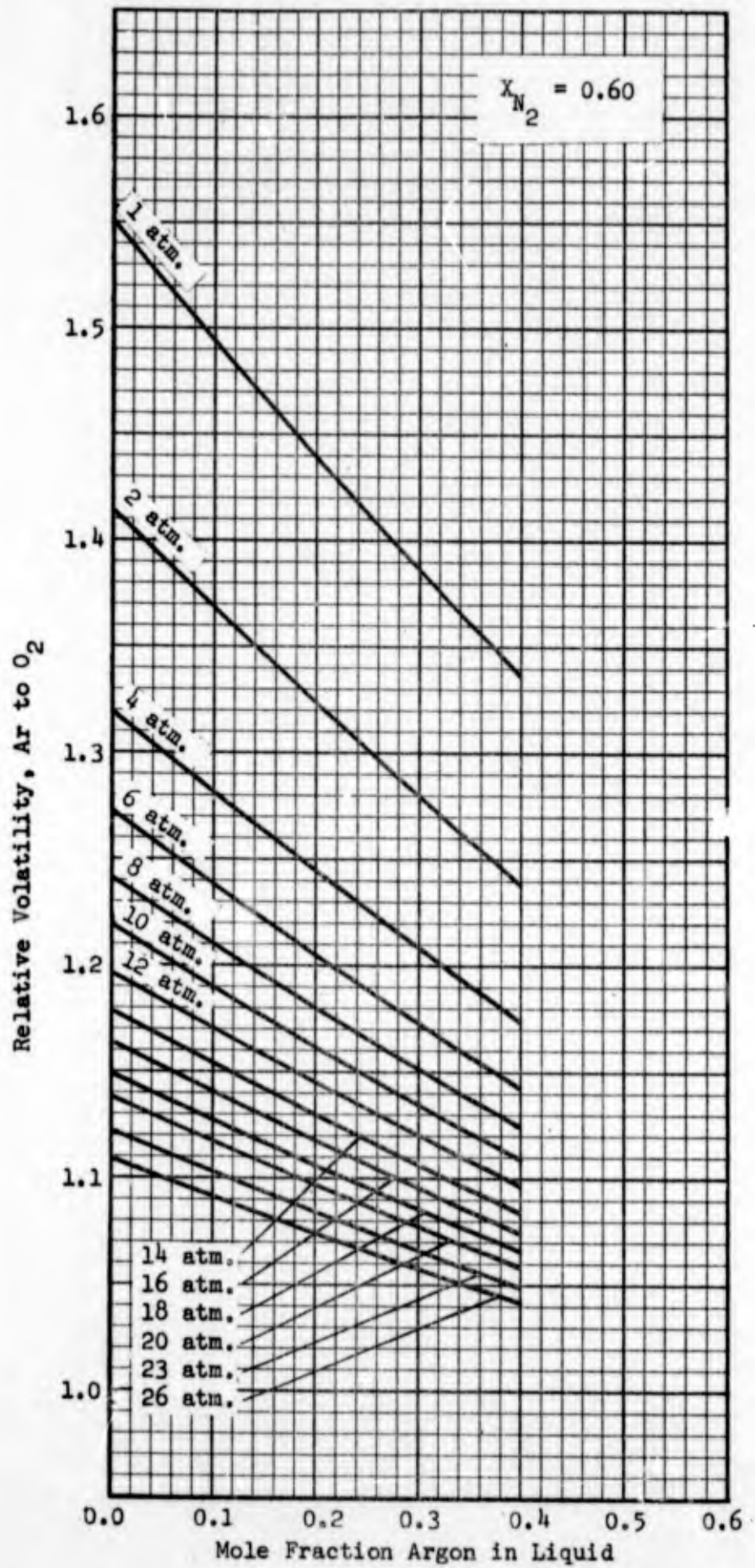


Figure 129. Relative Volatility of Argon to Oxygen.

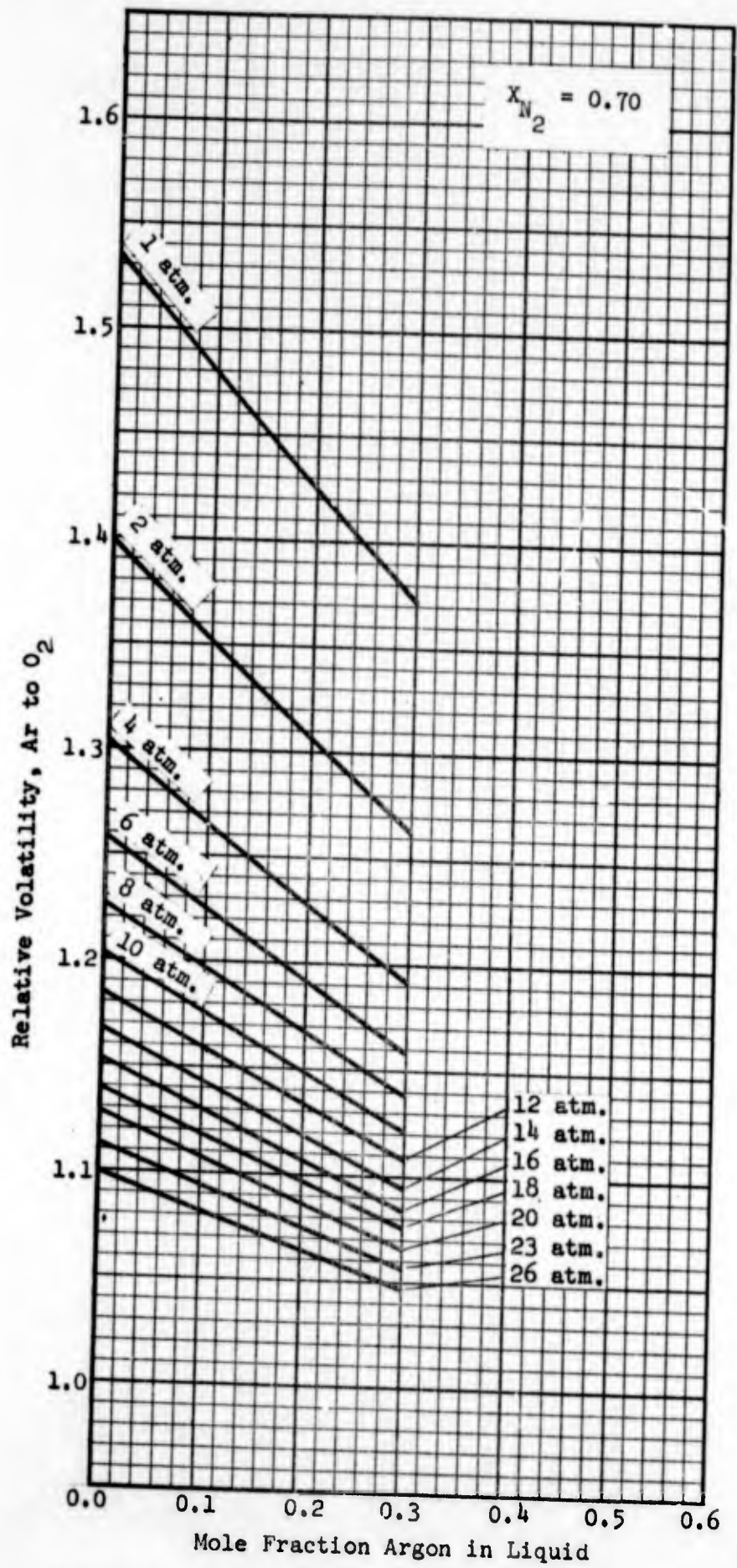


Figure 130. Relative Volatility of Argon to Oxygen.



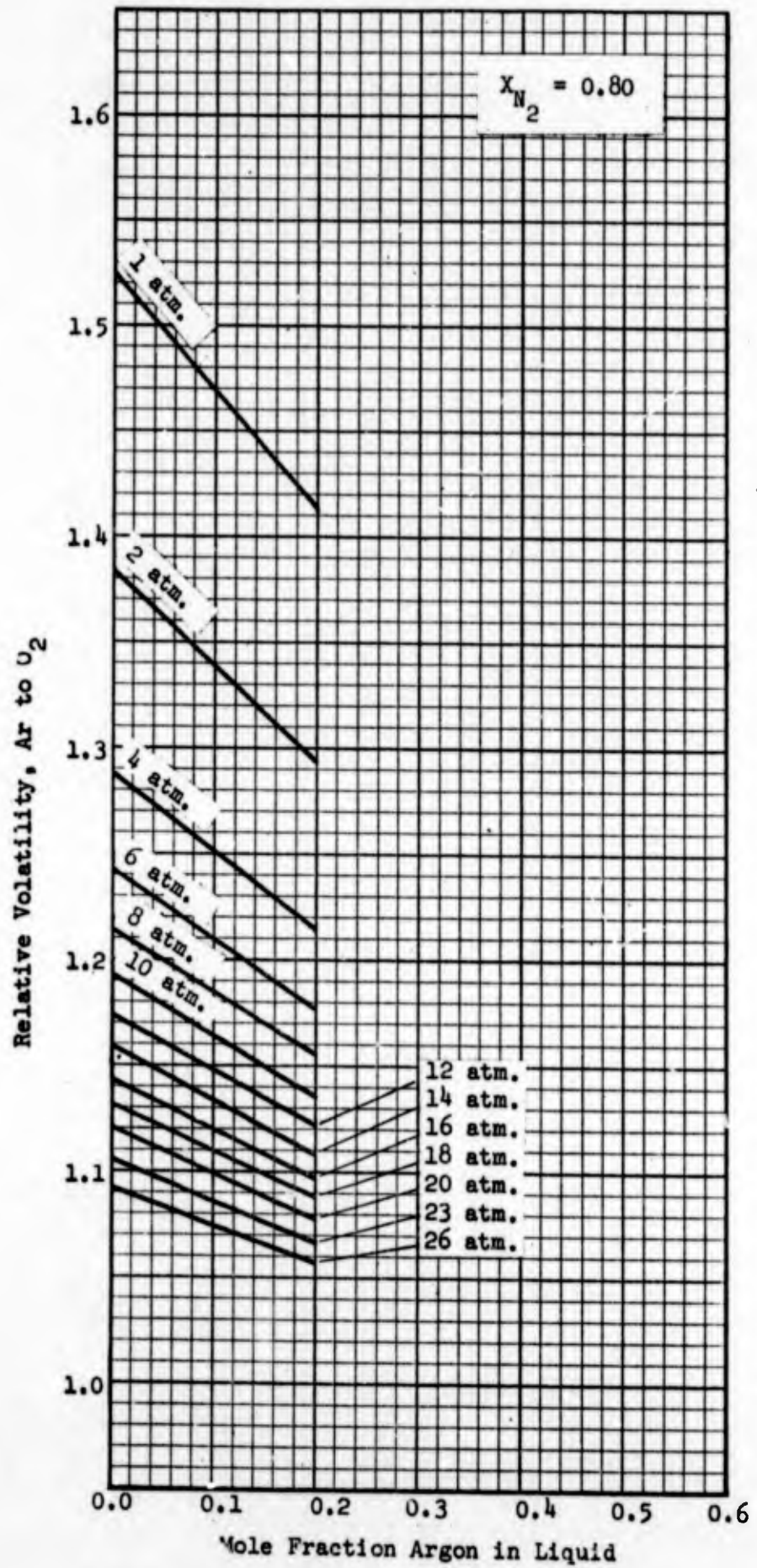


Figure 131. Relative Volatility of Argon to Oxygen.

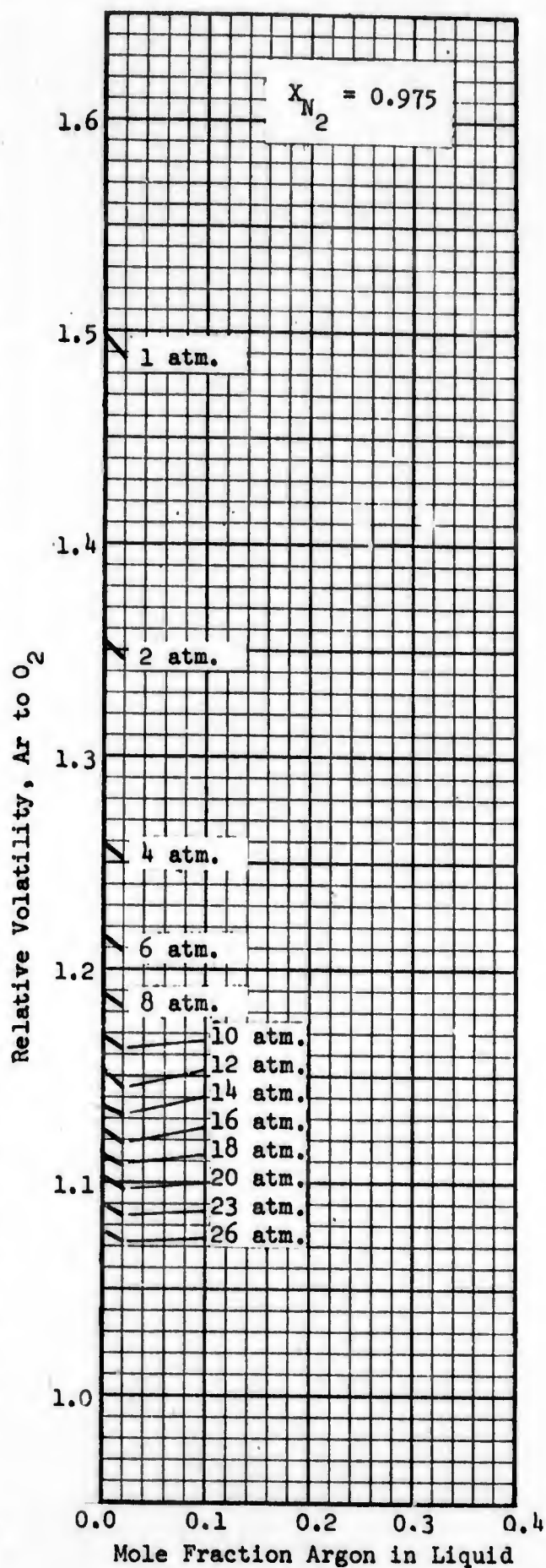
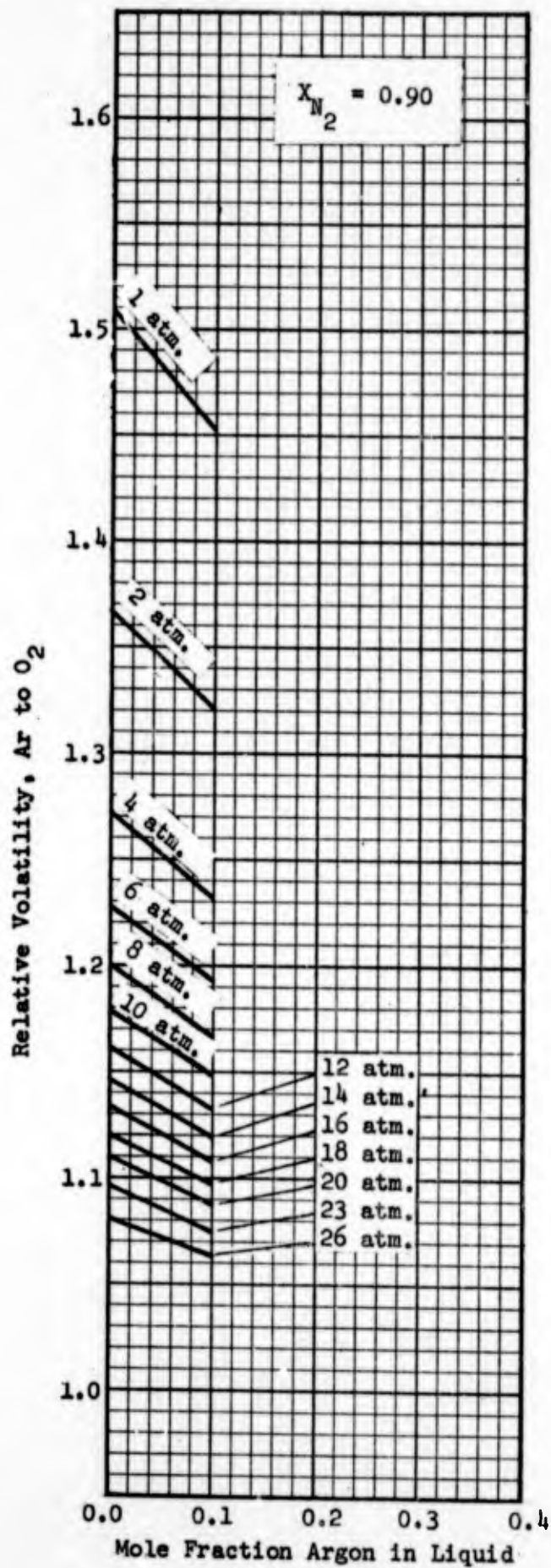


Figure 132. Relative Volatility of Argon to Oxygen.

D. Relative Volatility of Argon to Nitrogen,  
Binary System

The graph to follow presents the relative volatility of argon to nitrogen in the binary system along selected isobars.

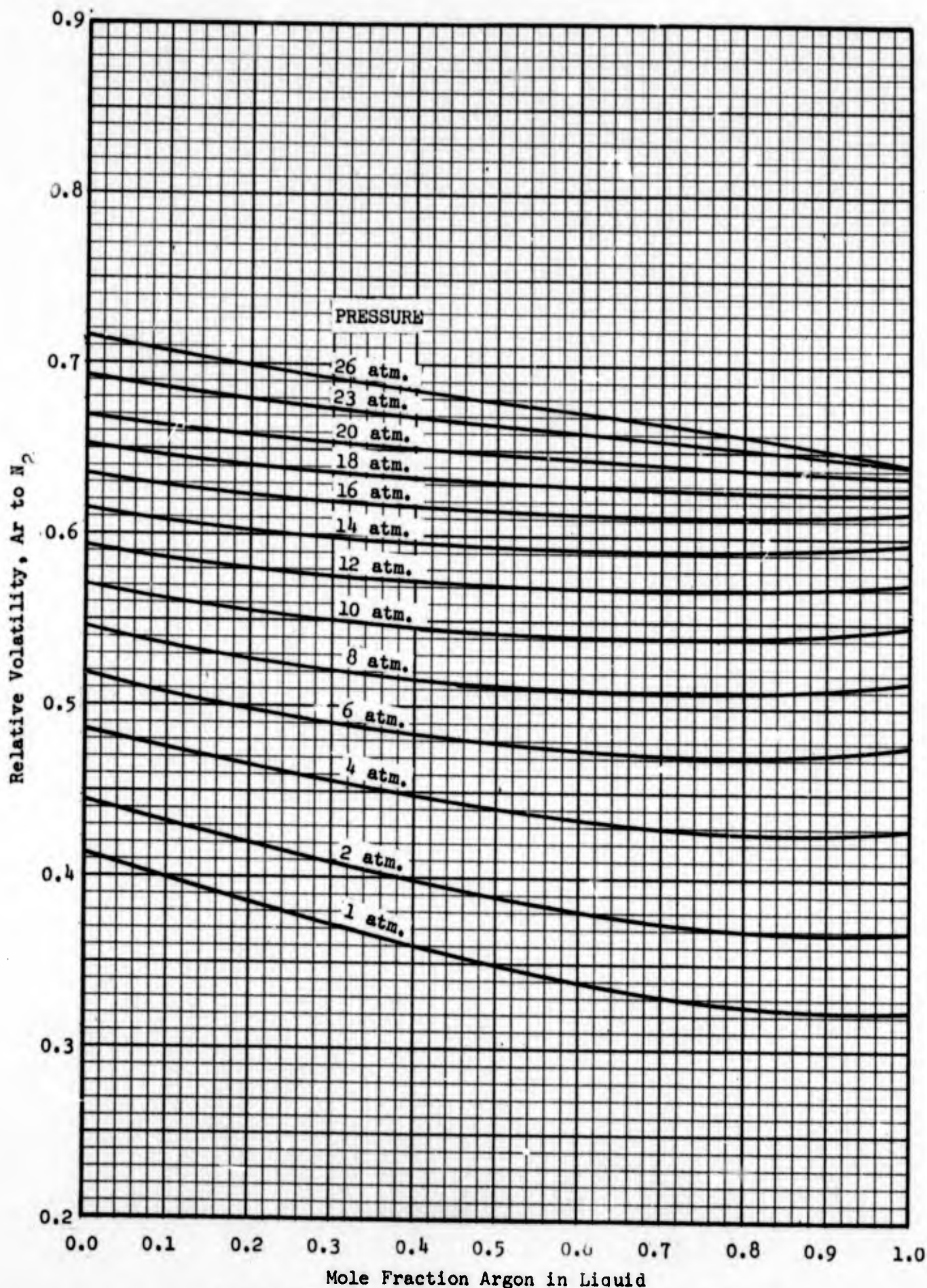


Figure 133. Relative Volatility of Argon to Nitrogen with no Oxygen present in the System.

E. Relative Volatility of Argon to Oxygen,  
Binary System

The graph to follow presents the relative volatility of argon to oxygen in the binary system along selected isobars.

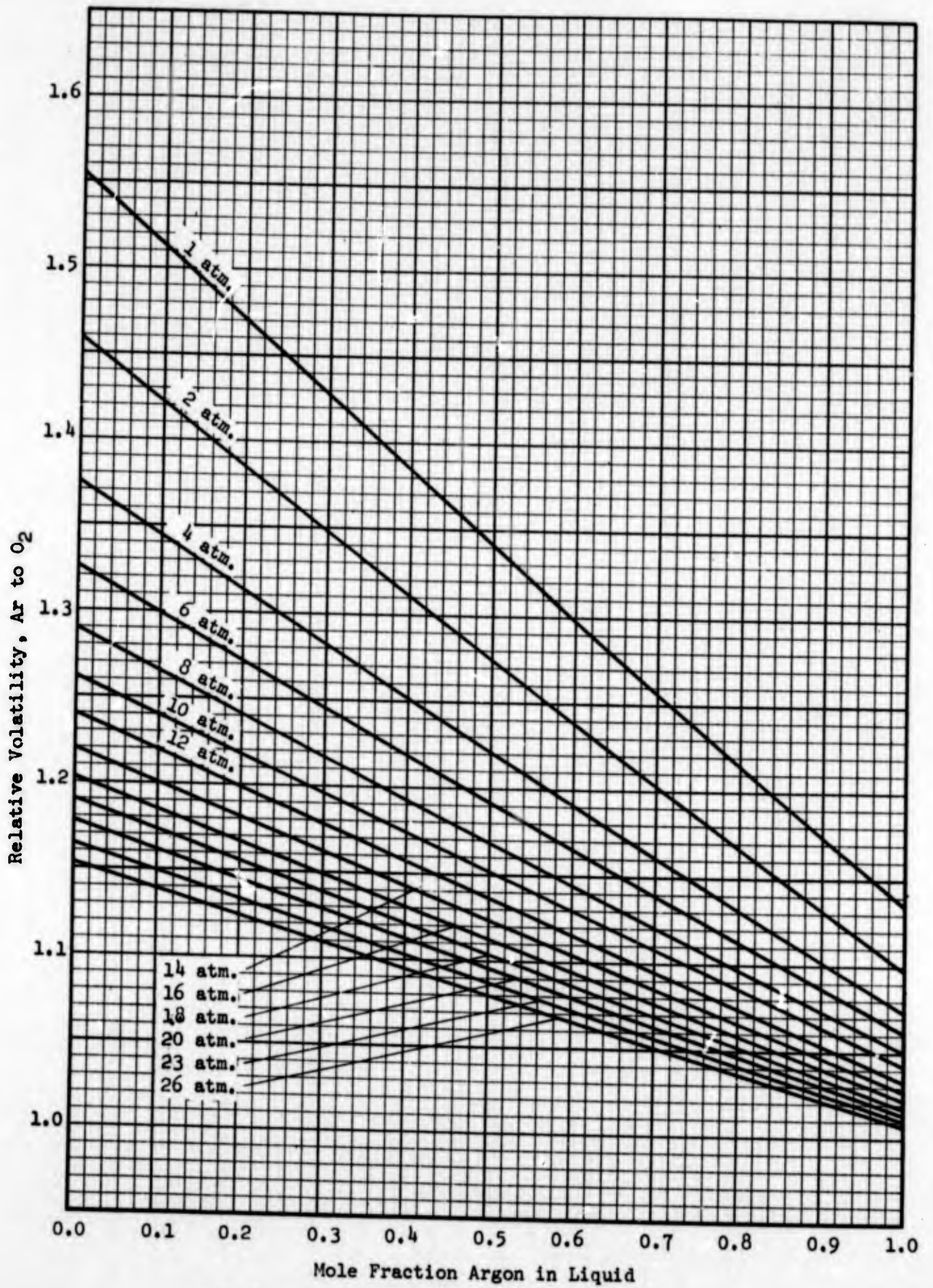


Figure 134. Relative Volatility of Argon to Oxygen with no Nitrogen present in the System.

F. Pressure Activity Coefficients

The 39 graphs to follow present the pressure activity coefficients of oxygen-argon-nitrogen as a function of composition. The pressure activity coefficient is defined as

$$\gamma_{pi} = \frac{y_i P}{x_i p^0} \quad (53)$$

This function is best understood as expressing the deviations from Raoult's Law.

The graphs are grouped in order of component: nitrogen, argon, oxygen. Inside each group they are ordered with respect to pressure.

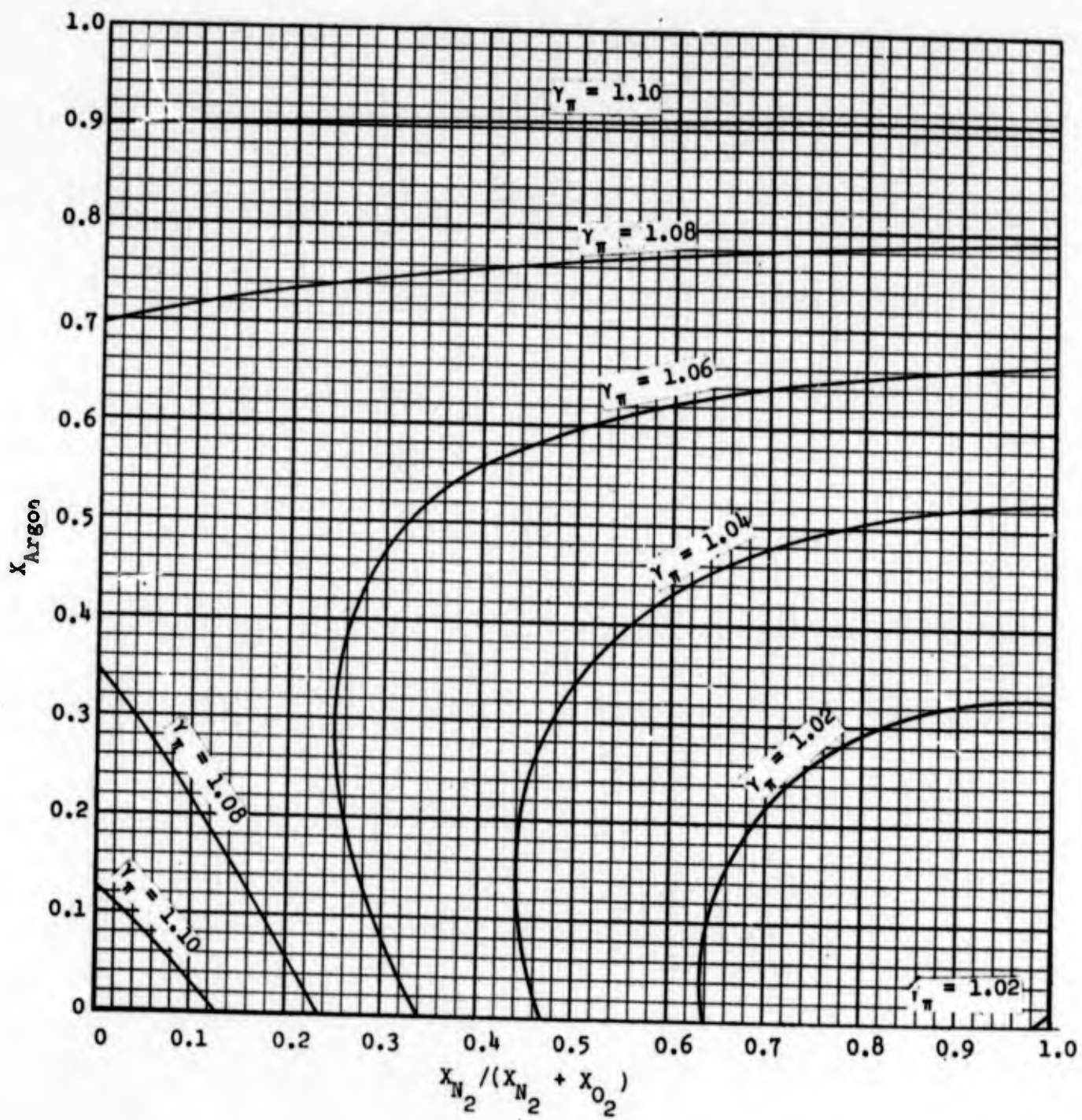


Figure 135. Nitrogen Pressure Activity Coefficients, 1 Atmosphere



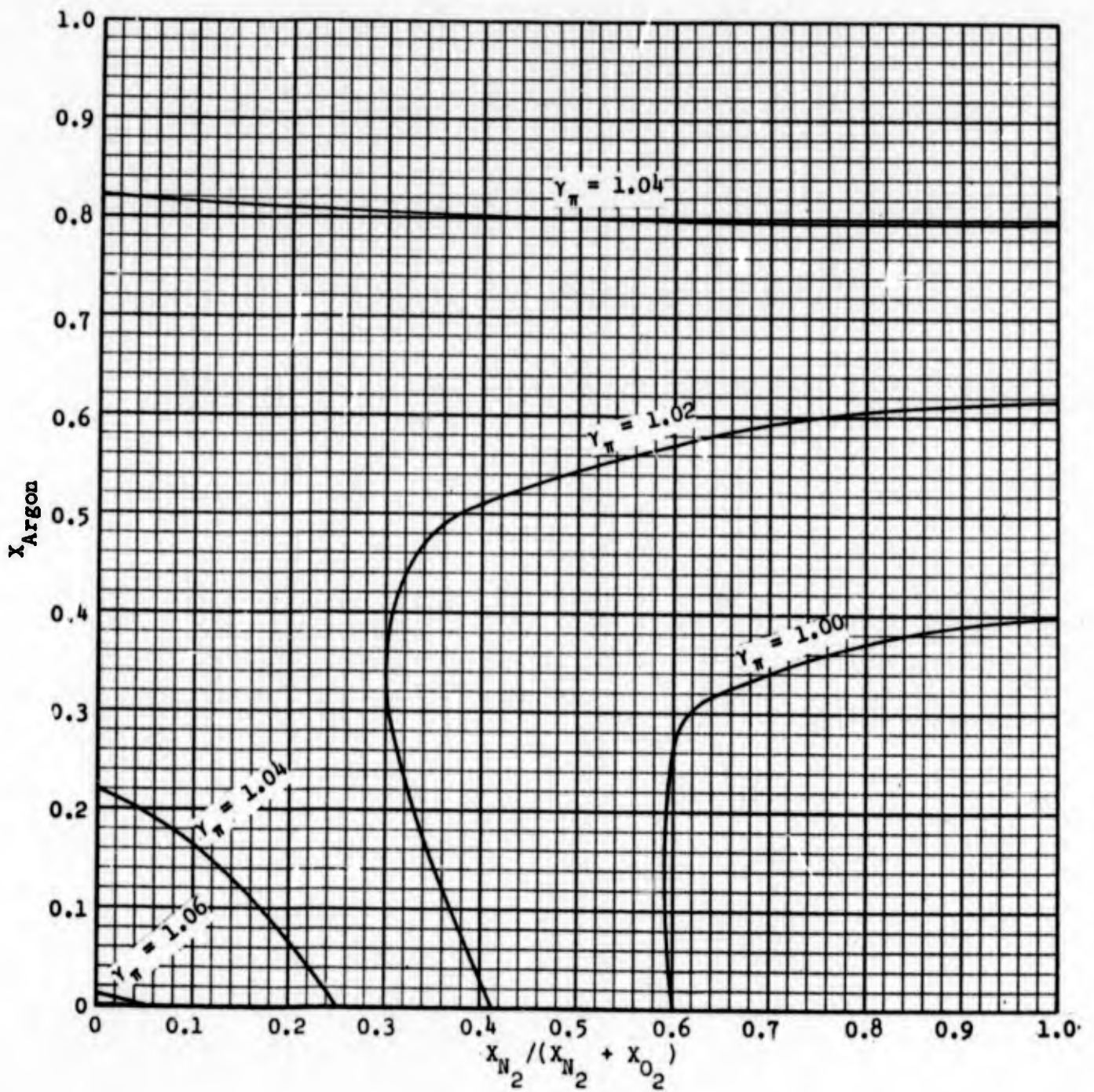


Figure 136. Nitrogen Pressure Activity Coefficients, 2 Atmospheres

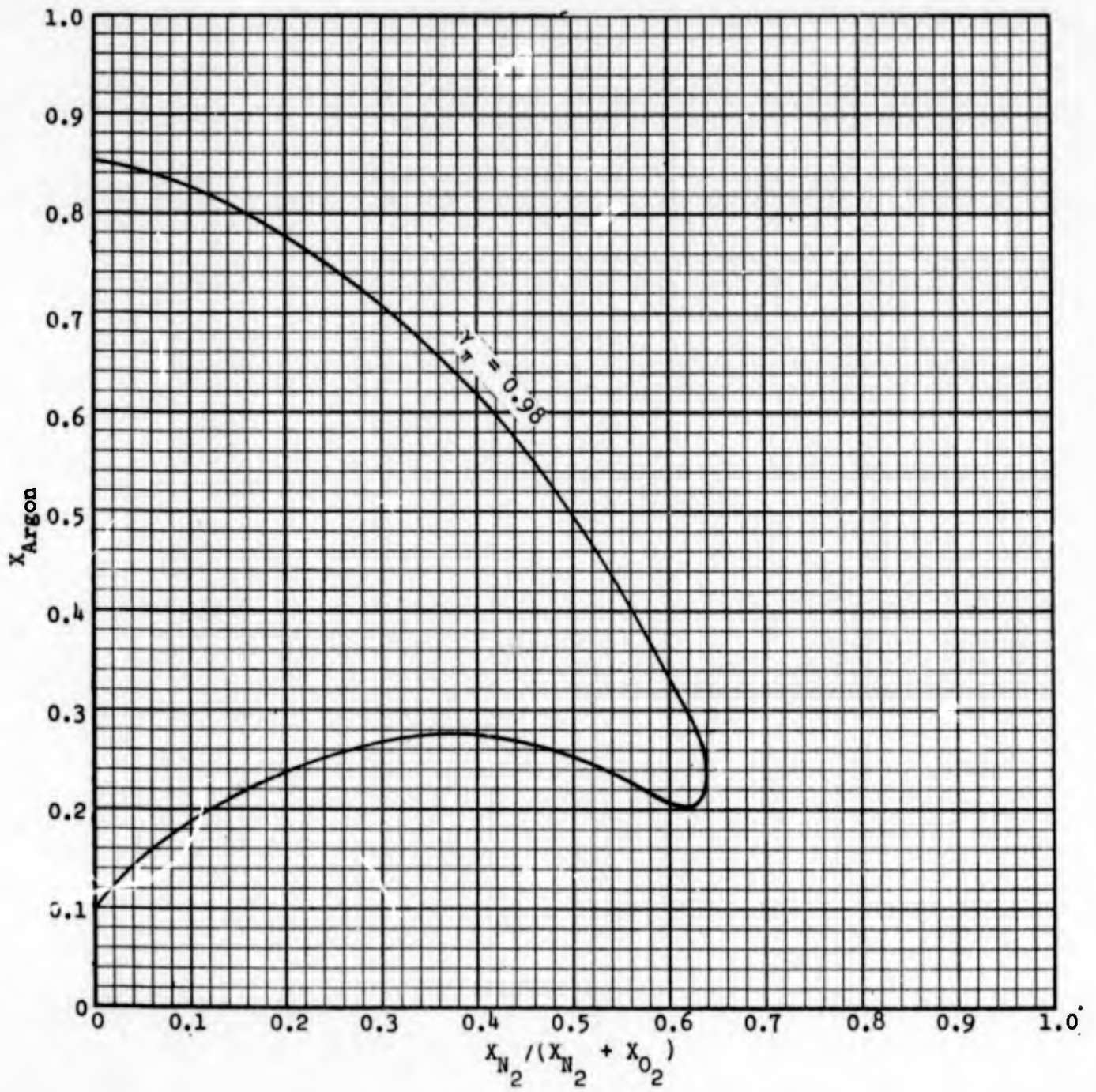


Figure 137. Nitrogen Pressure Activity Coefficients, 4 Atmospheres

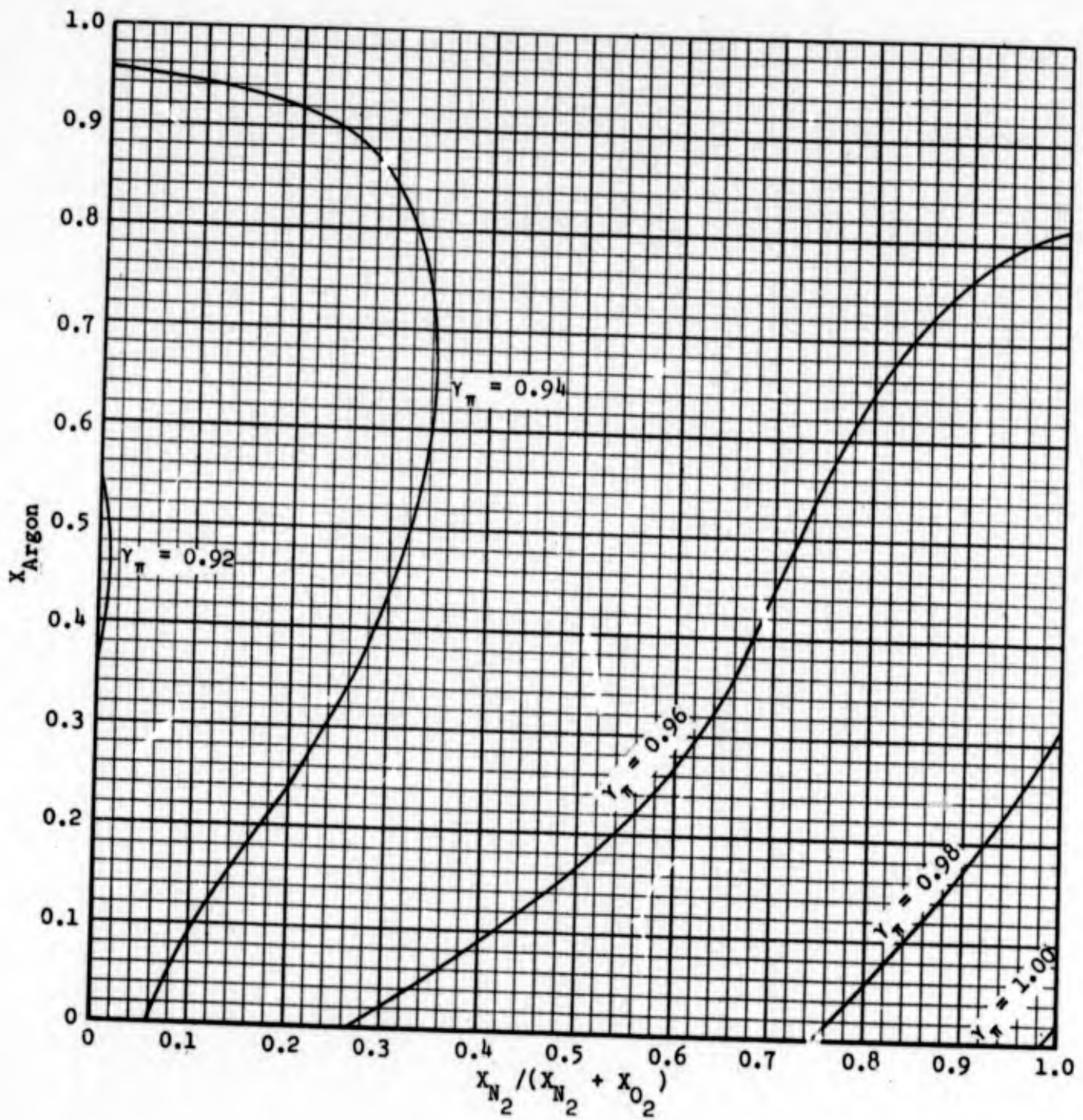


Figure 138. Nitrogen Pressure Activity Coefficients, 6 Atmospheres.

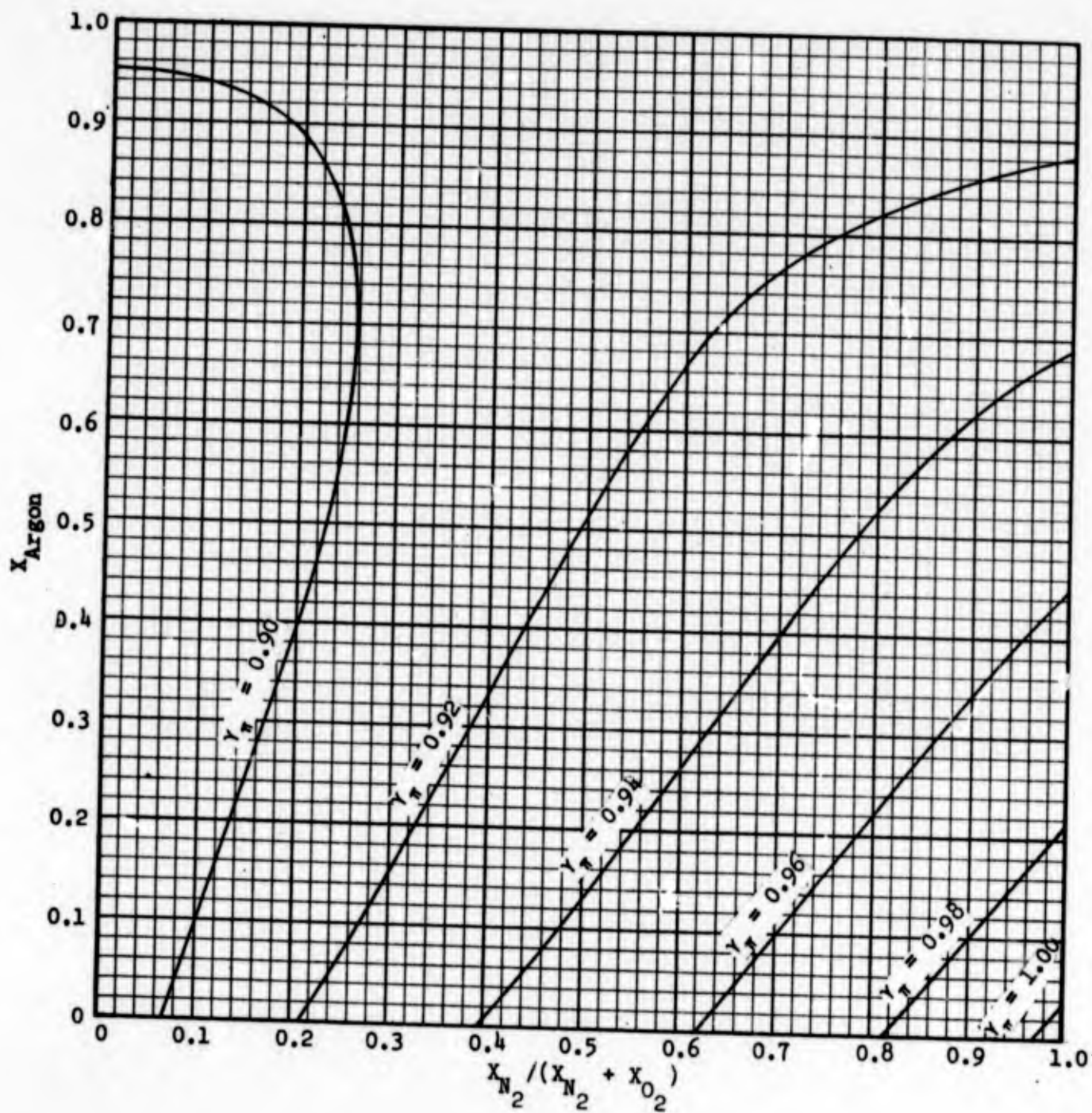


Figure 139. Nitrogen Pressure Activity Coefficients, 8 Atmospheres.

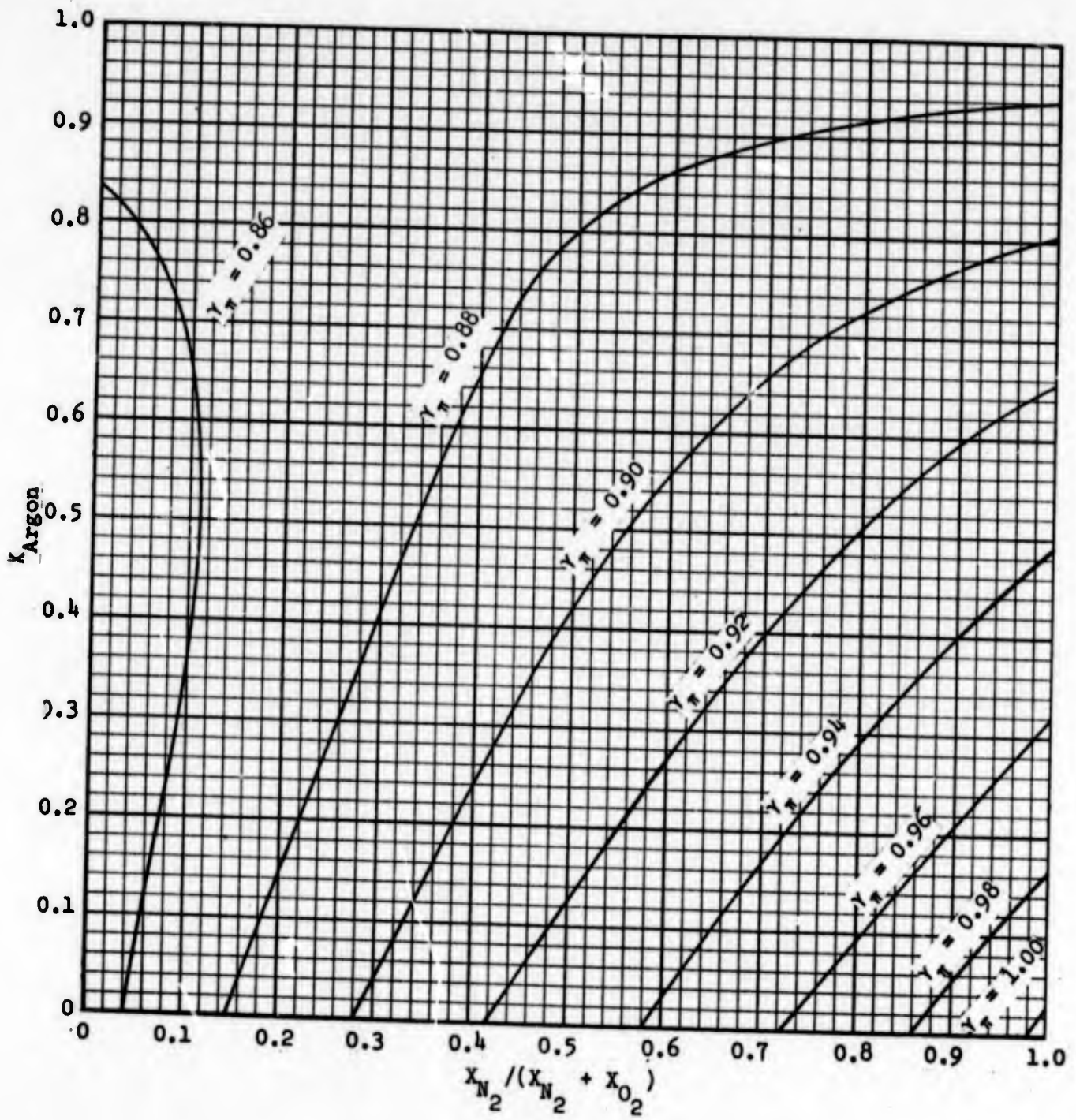


Figure 140. Nitrogen Pressure Activity Coefficients, 10 Atmospheres.

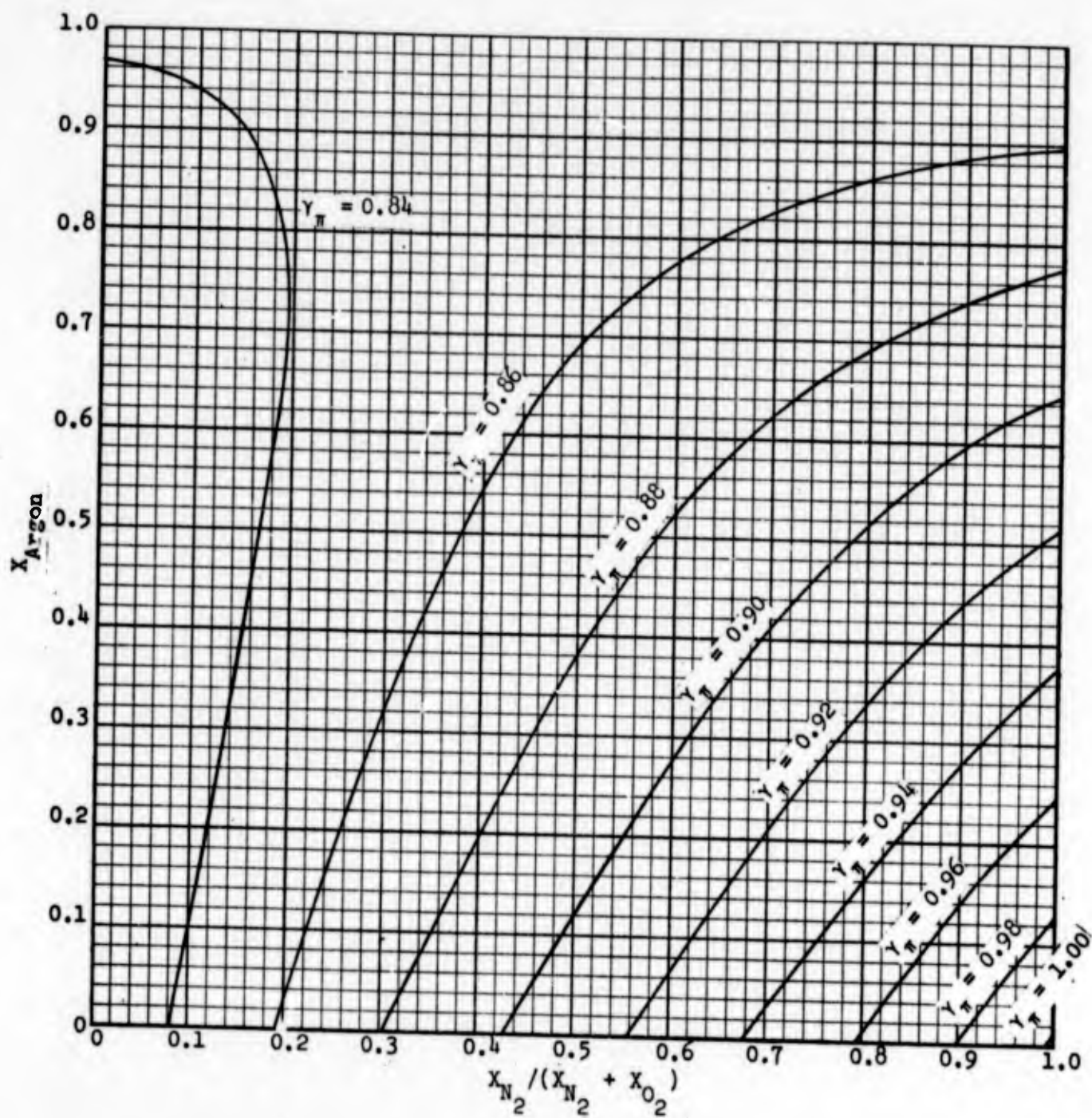


Figure 141. Nitrogen Pressure Activity Coefficients, 12 Atmospheres.

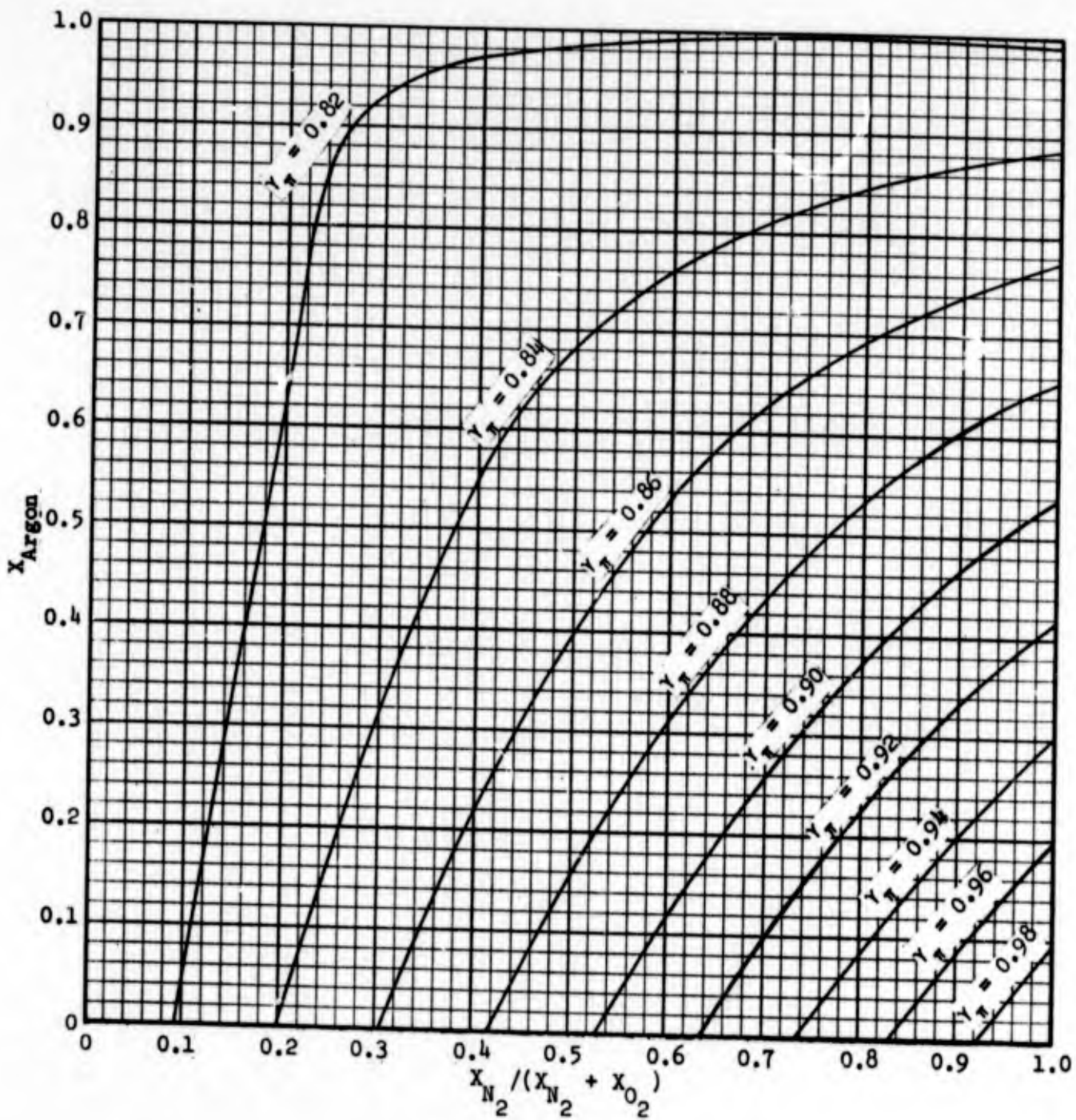


Figure 142. Nitrogen Pressure Activity Coefficients, 14 Atmospheres.

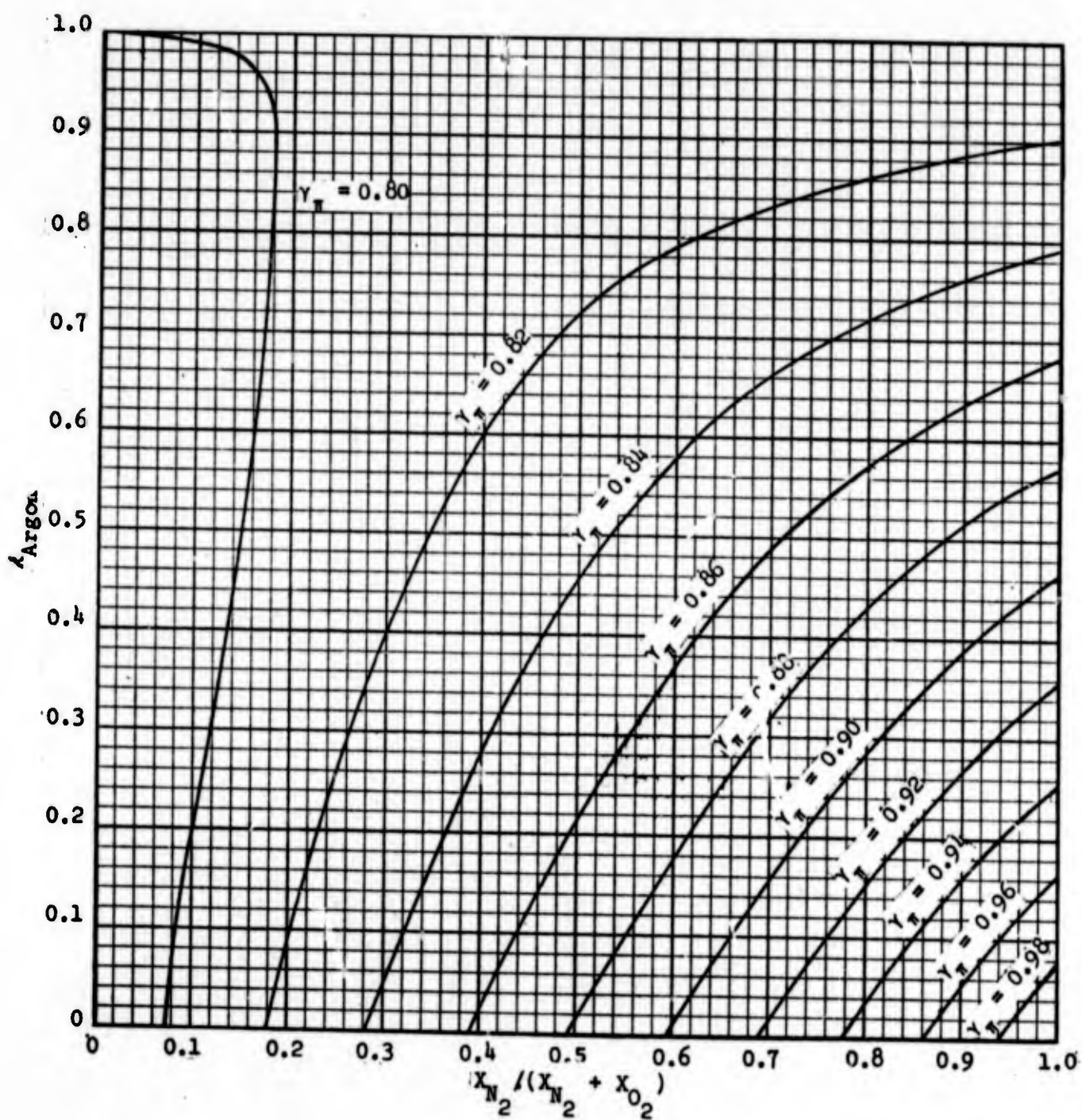


Figure 143. Nitrogen Pressure Activity Coefficients, 16 Atmospheres.



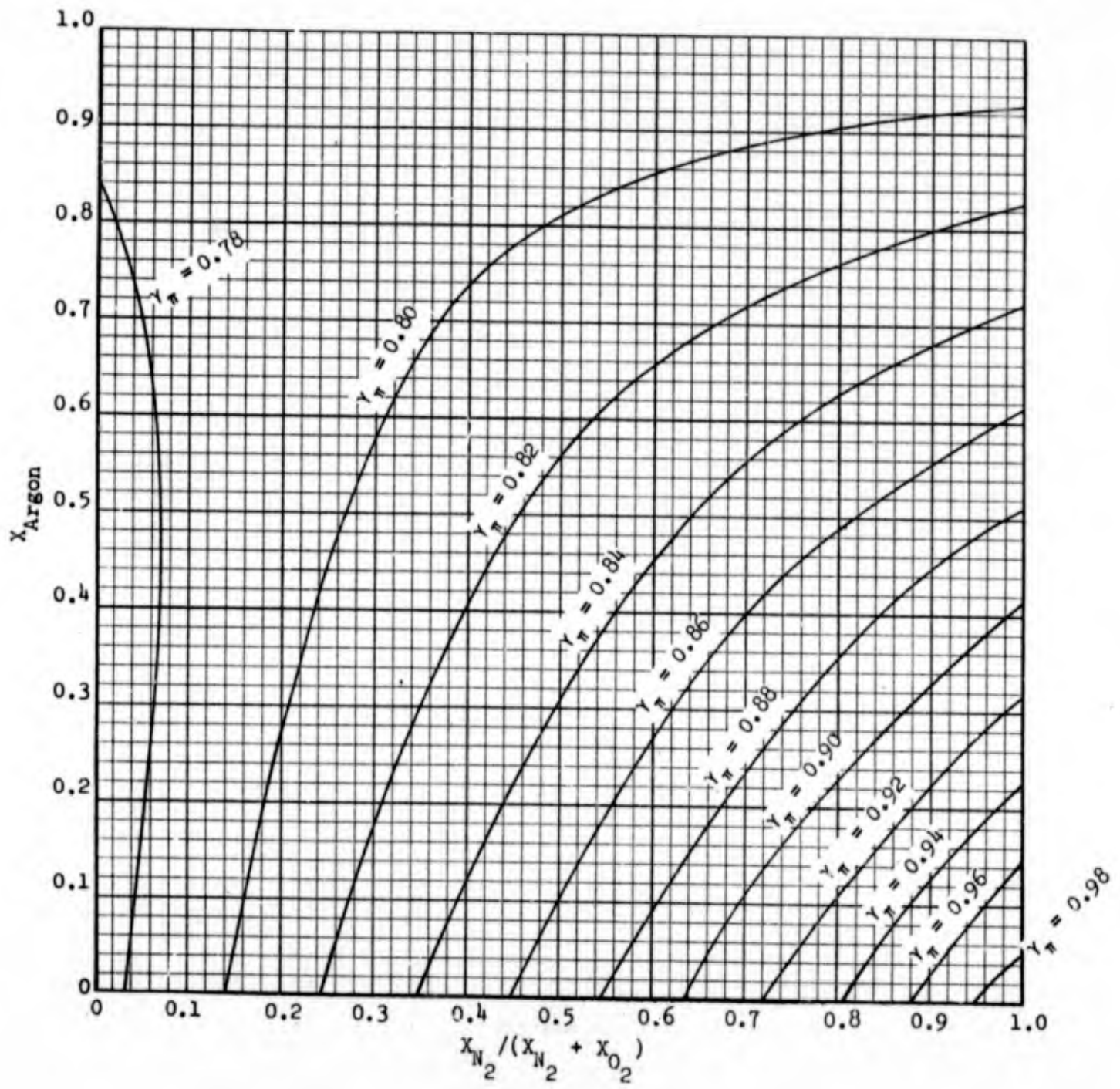


Figure 144. Nitrogen Pressure Activity Coefficients, 18 Atmospheres.

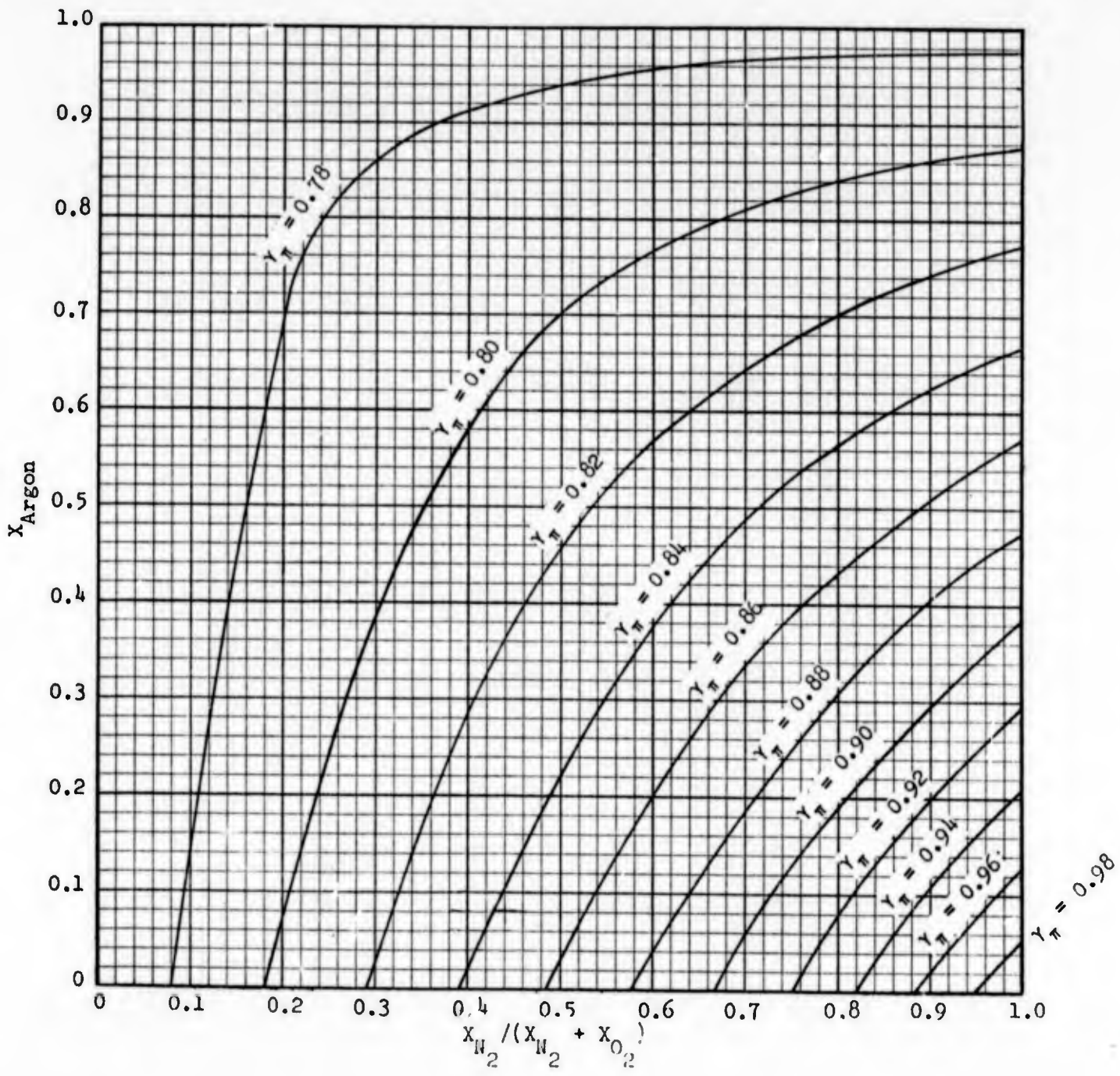


Figure 145. Nitrogen Pressure Activity Coefficients, 20 Atmospheres.

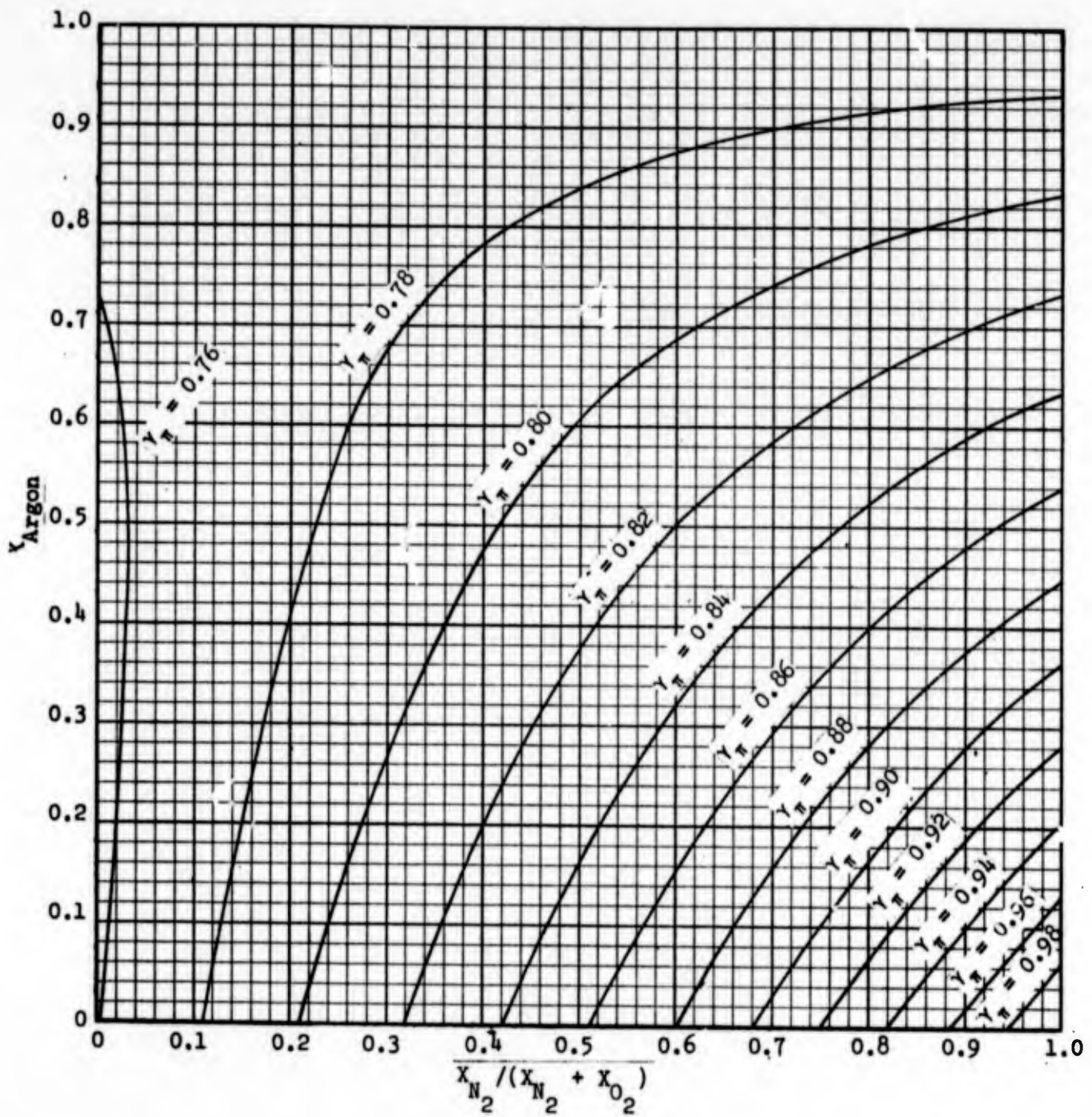


Figure 146. Nitrogen Pressure Activity Coefficients, 23 Atmospheres.

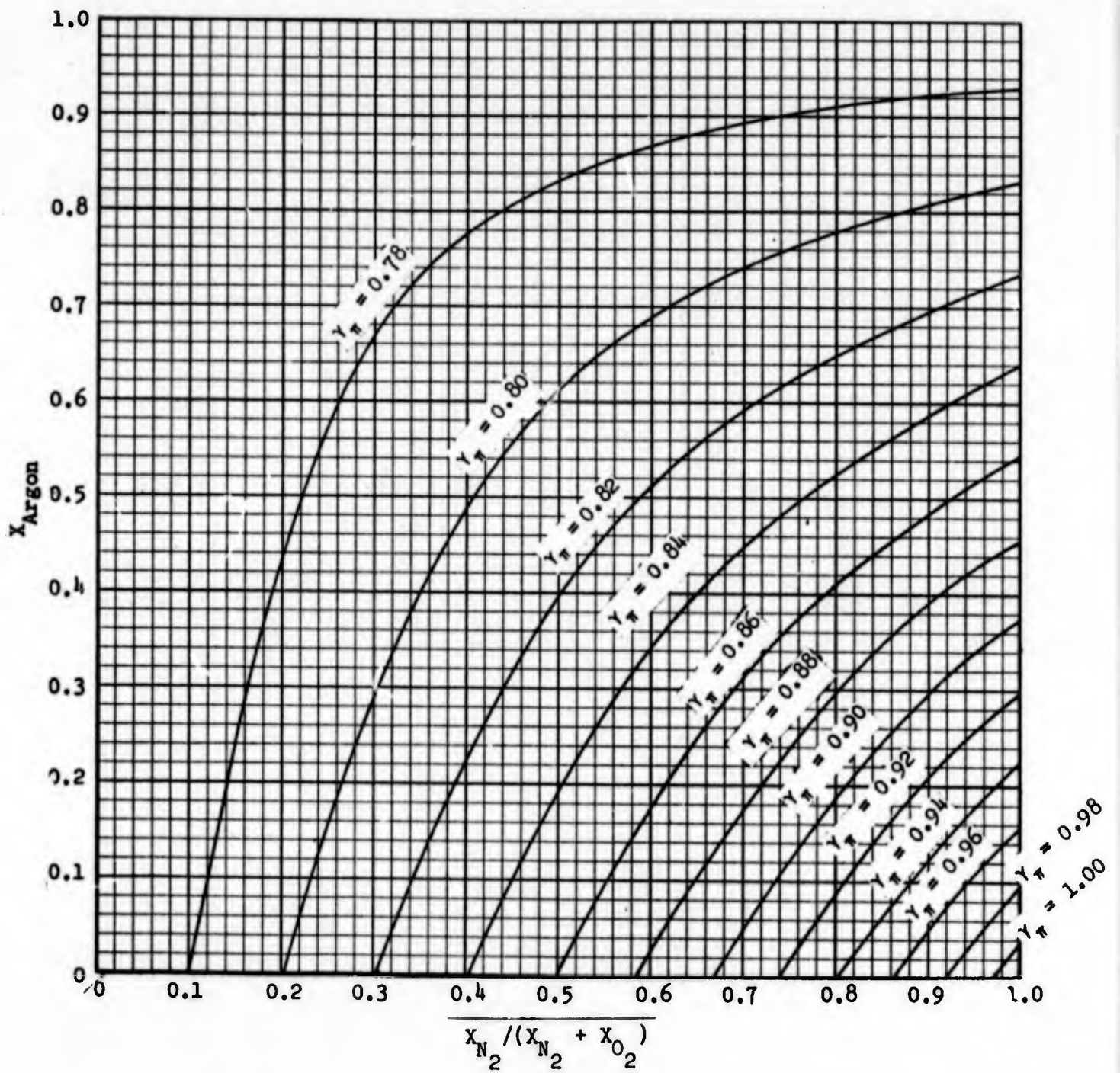


Figure 147. Nitrogen Pressure Activity Coefficients, 26 Atmospheres.

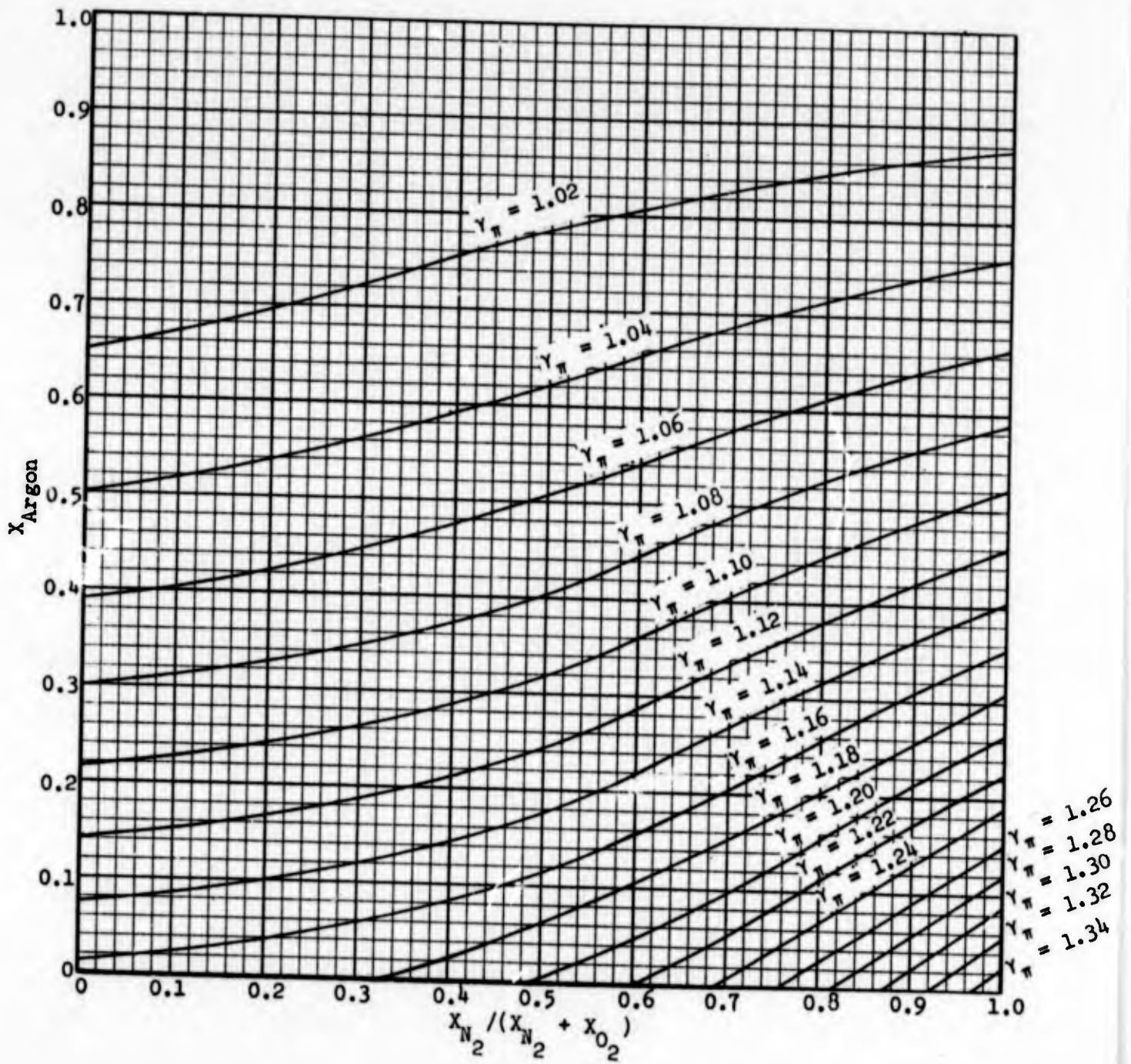


Figure 148. Argon Pressure Activity Coefficients, 1 Atmosphere.

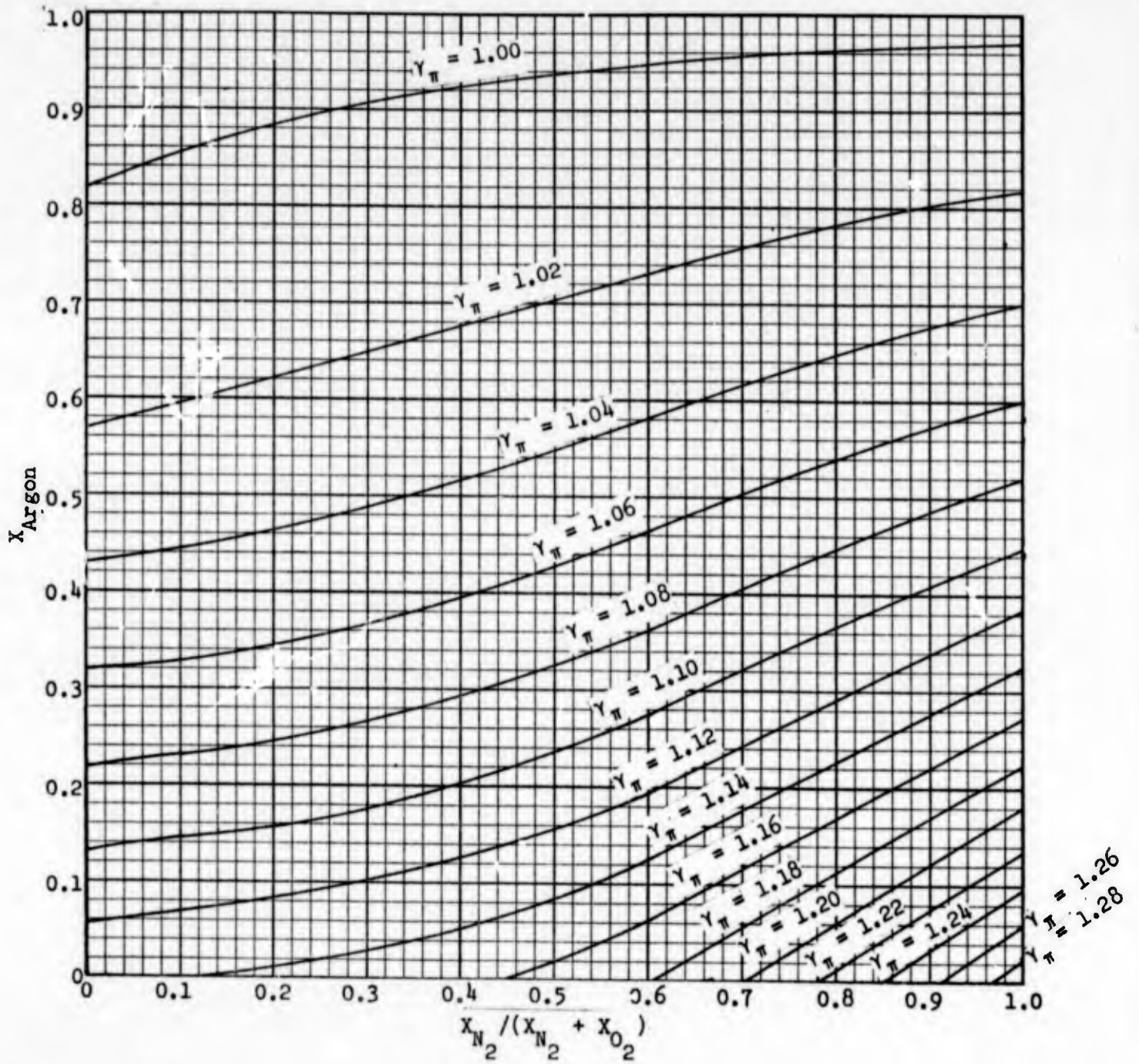


Figure 149. Argon Pressure Activity Coefficients, 2 Atmospheres.

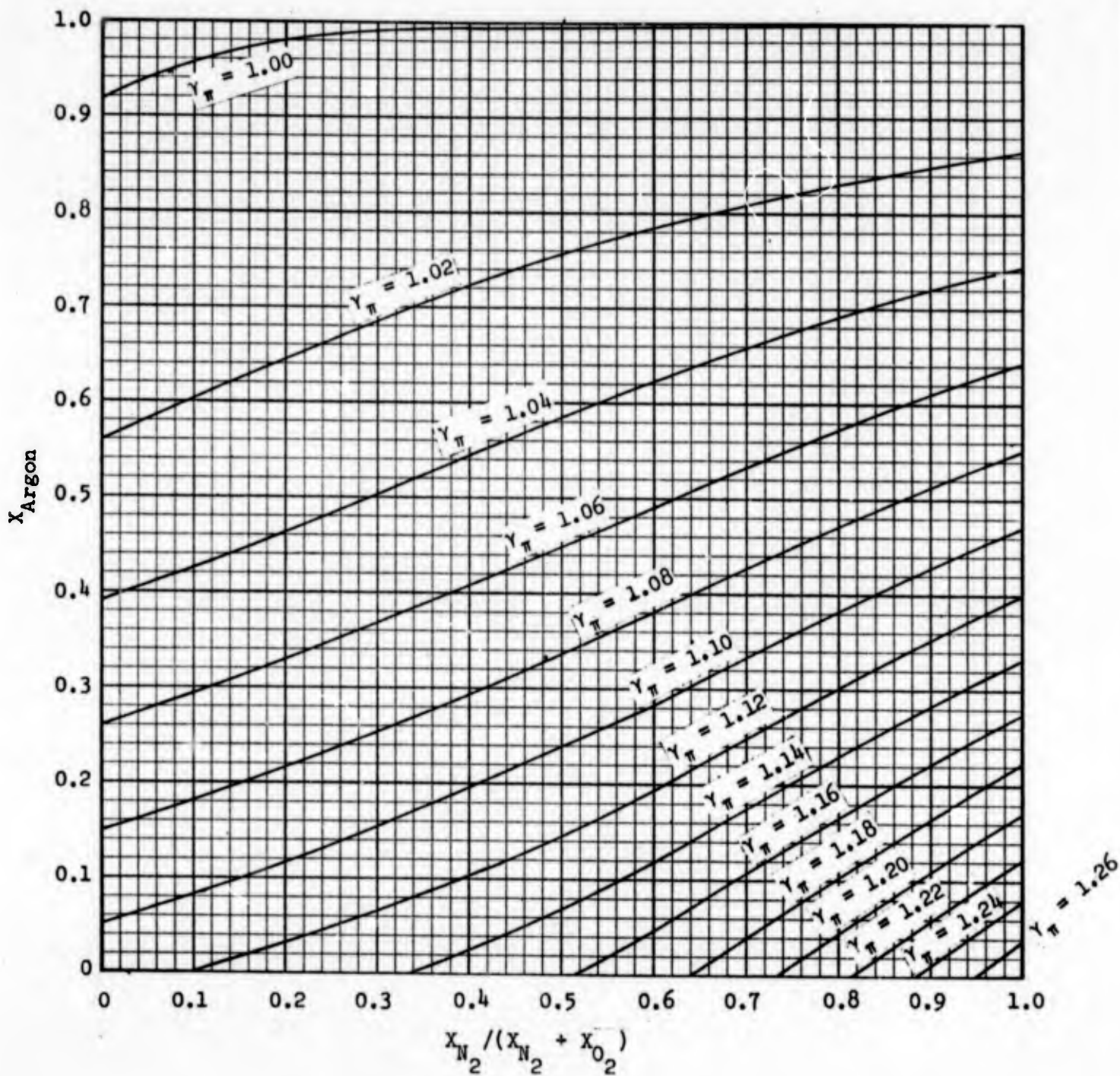


Figure 150. Argon Pressure Activity Coefficients, 4 Atmospheres.

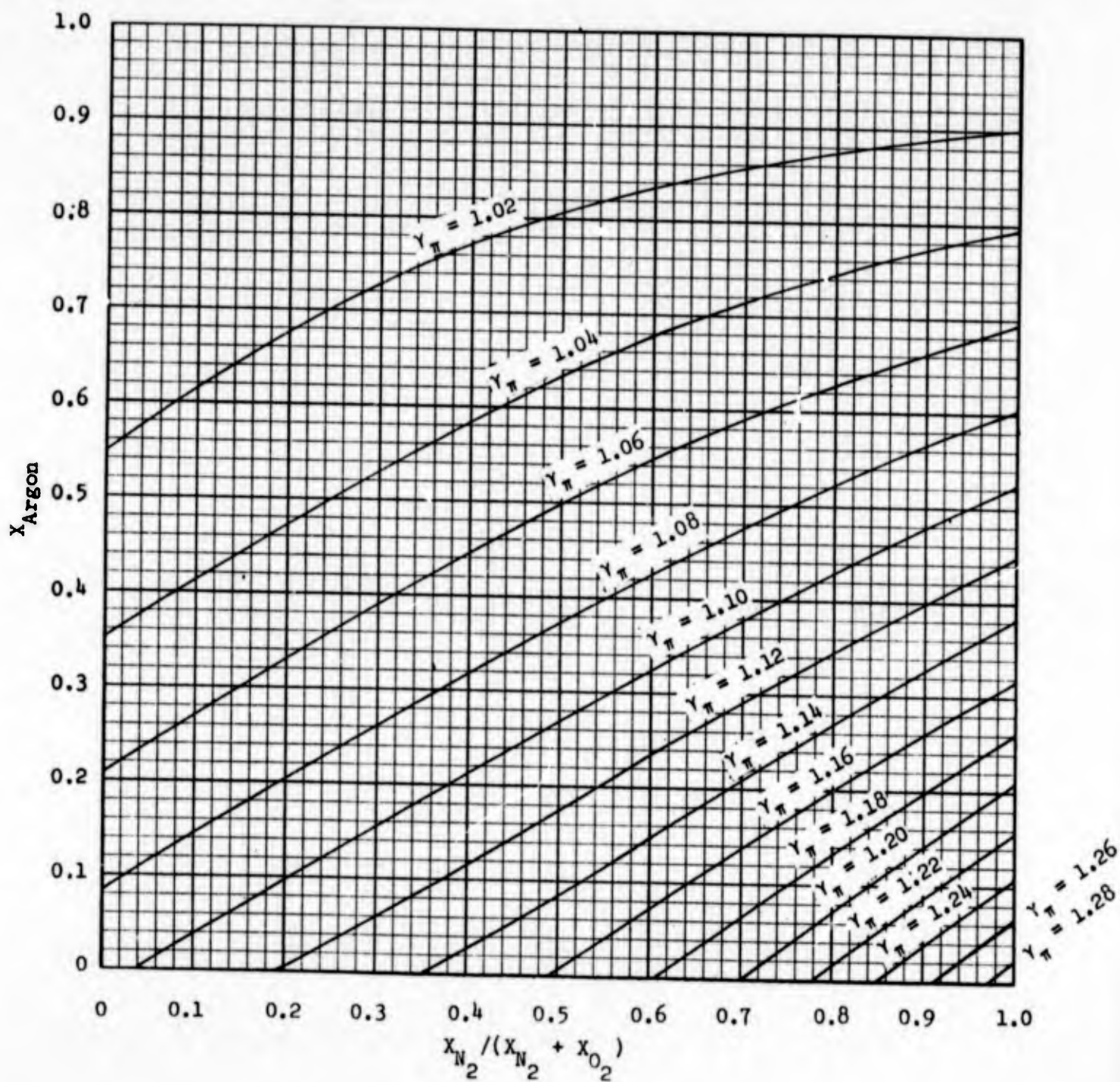


Figure 151. Argon Pressure Activity Coefficients, 6 Atmospheres.



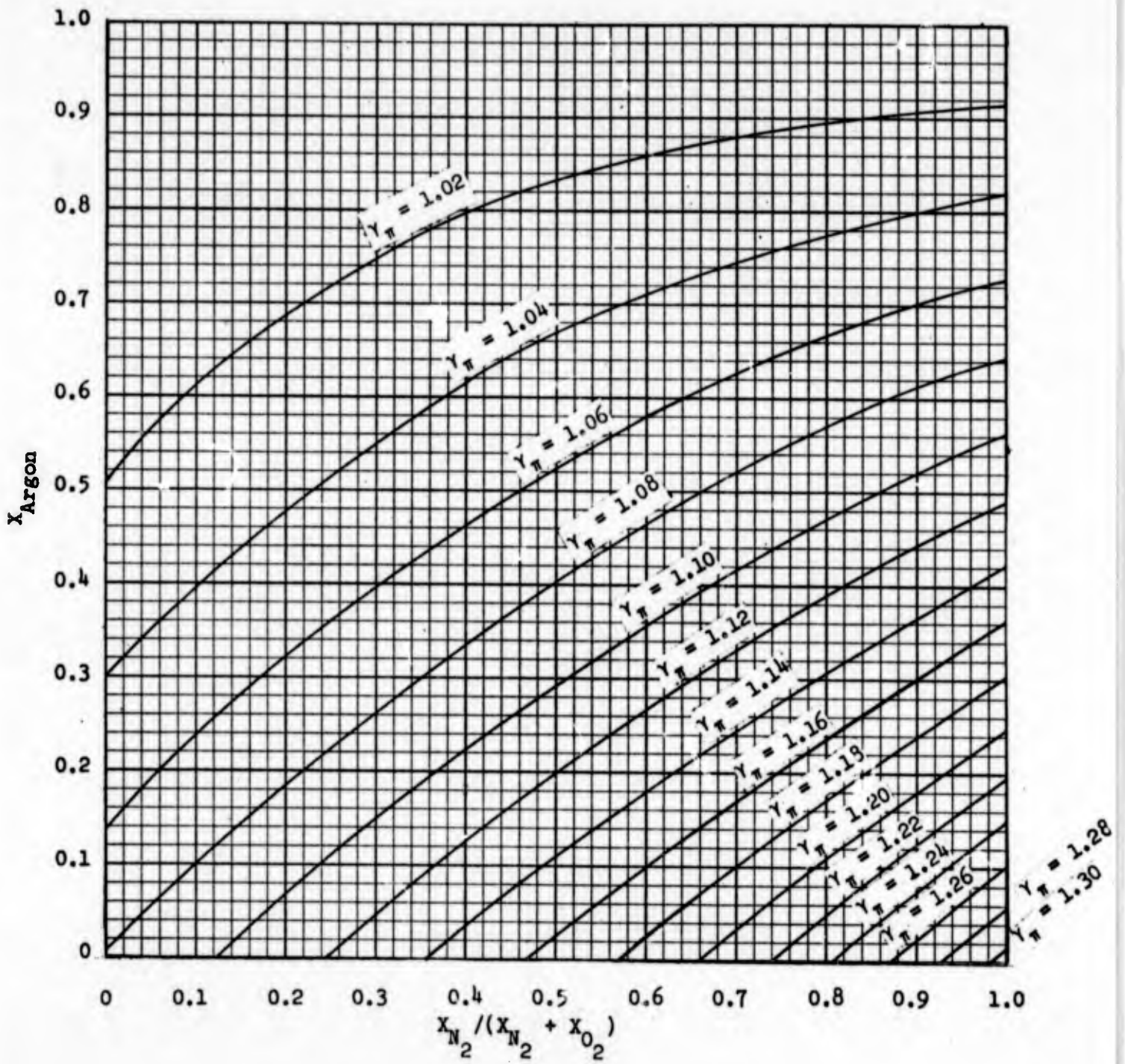


Figure 152. Argon Pressure Activity Coefficients, 8 Atmospheres.

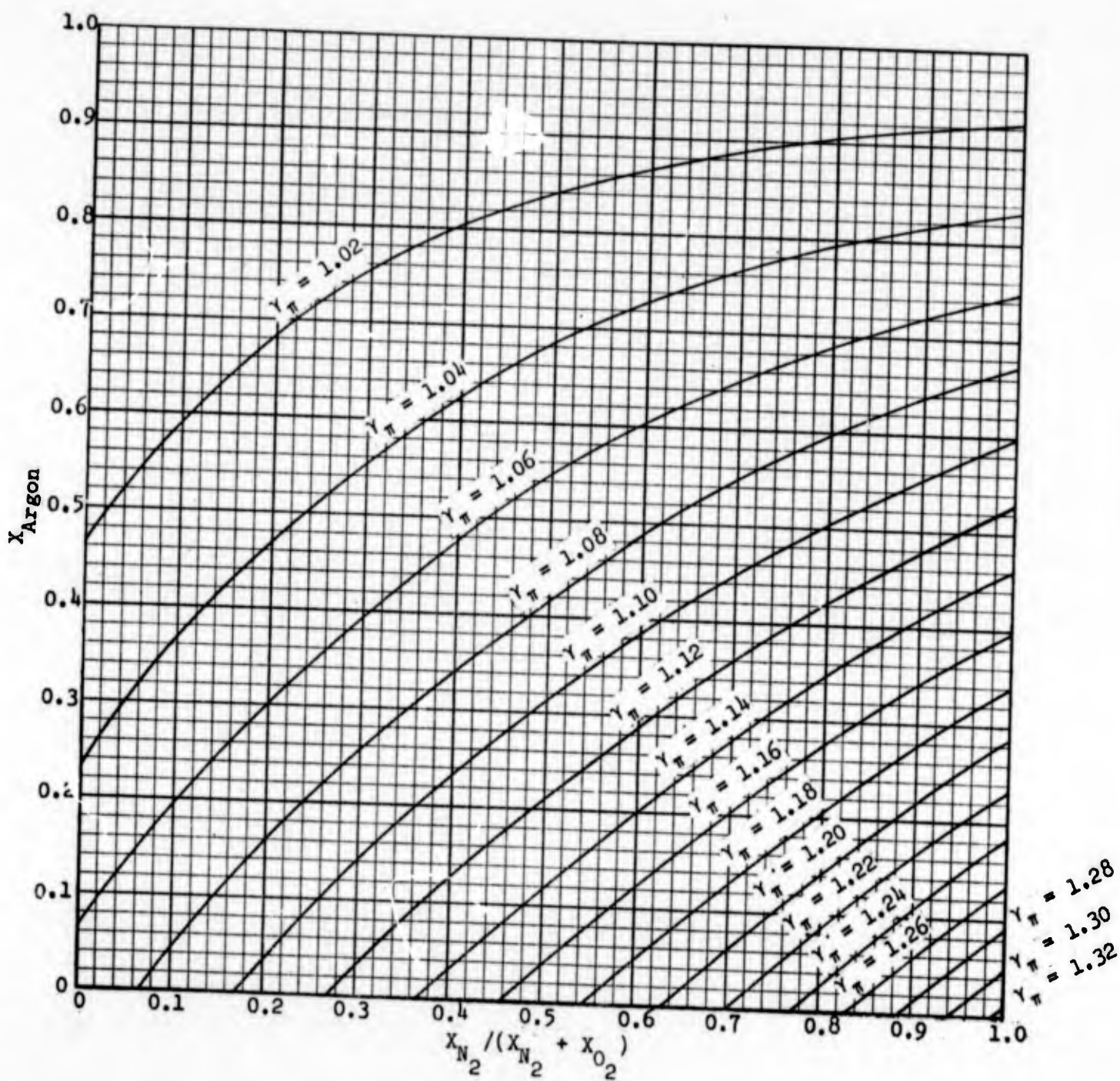


Figure 153. Argon Pressure Activity Coefficients, 10 Atmospheres.

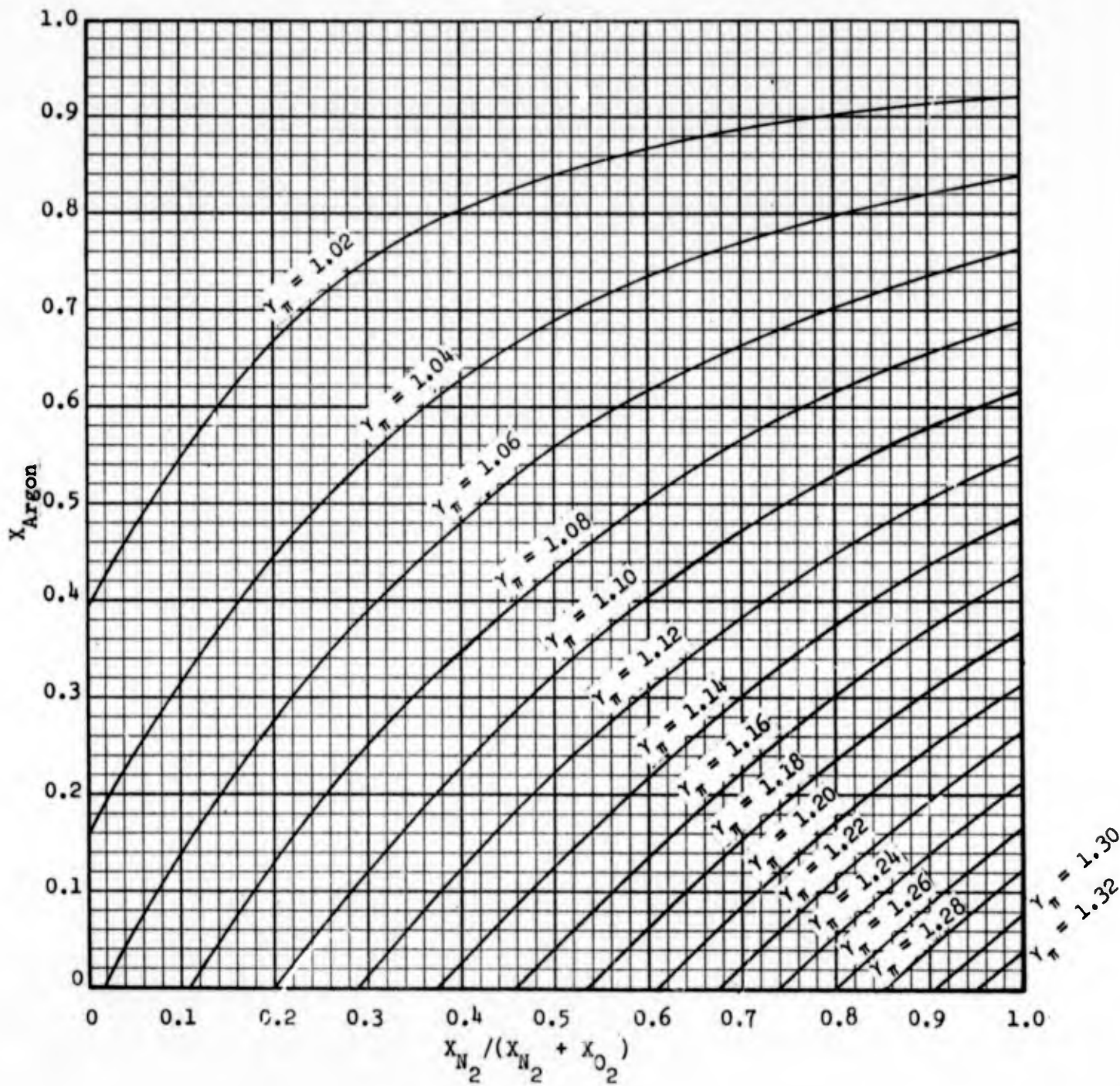


Figure 154. Argon Pressure Activity Coefficients, 12 Atmospheres.

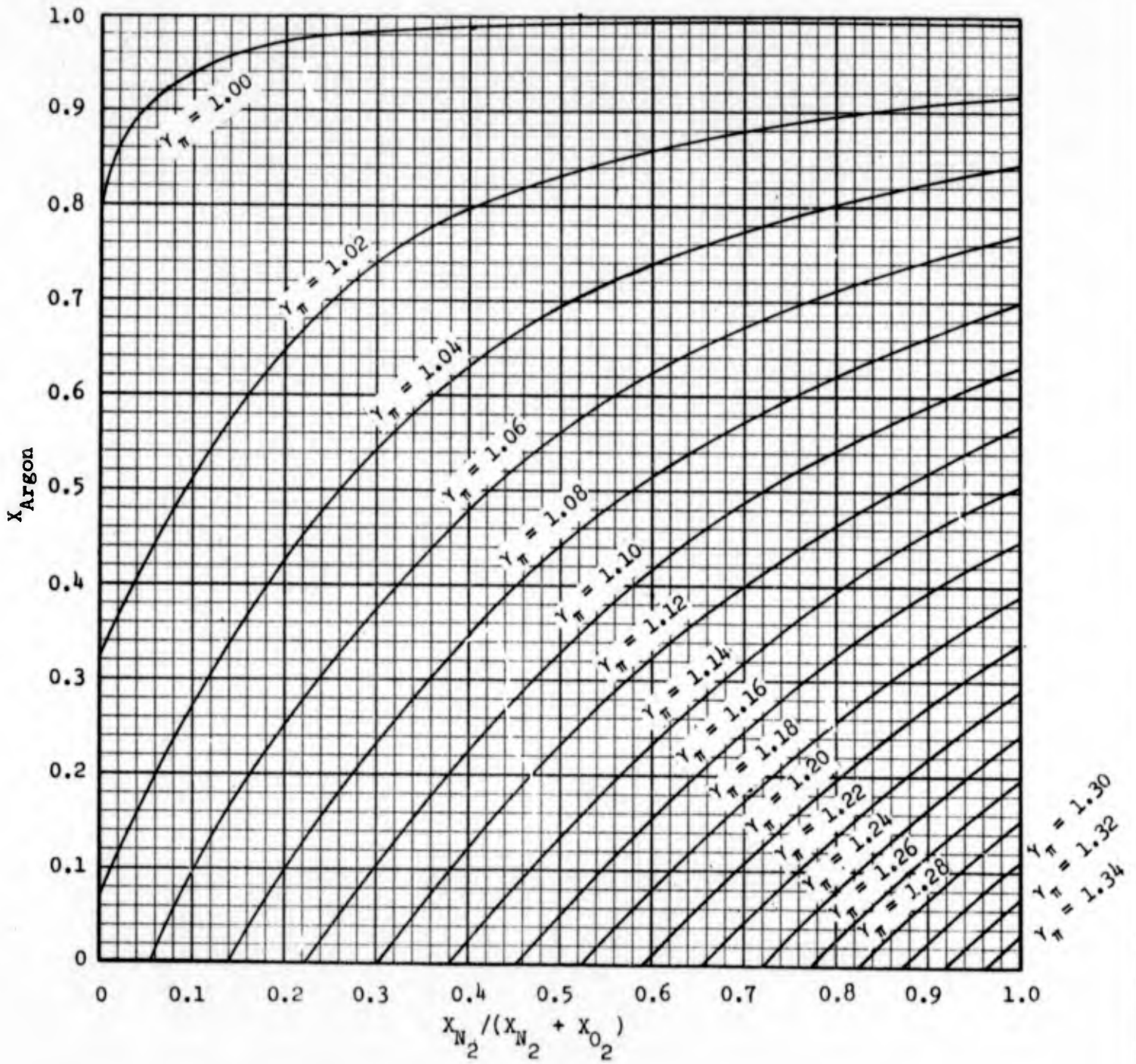


Figure 155. Argon Pressure Activity Coefficients, 14 Atmospheres.

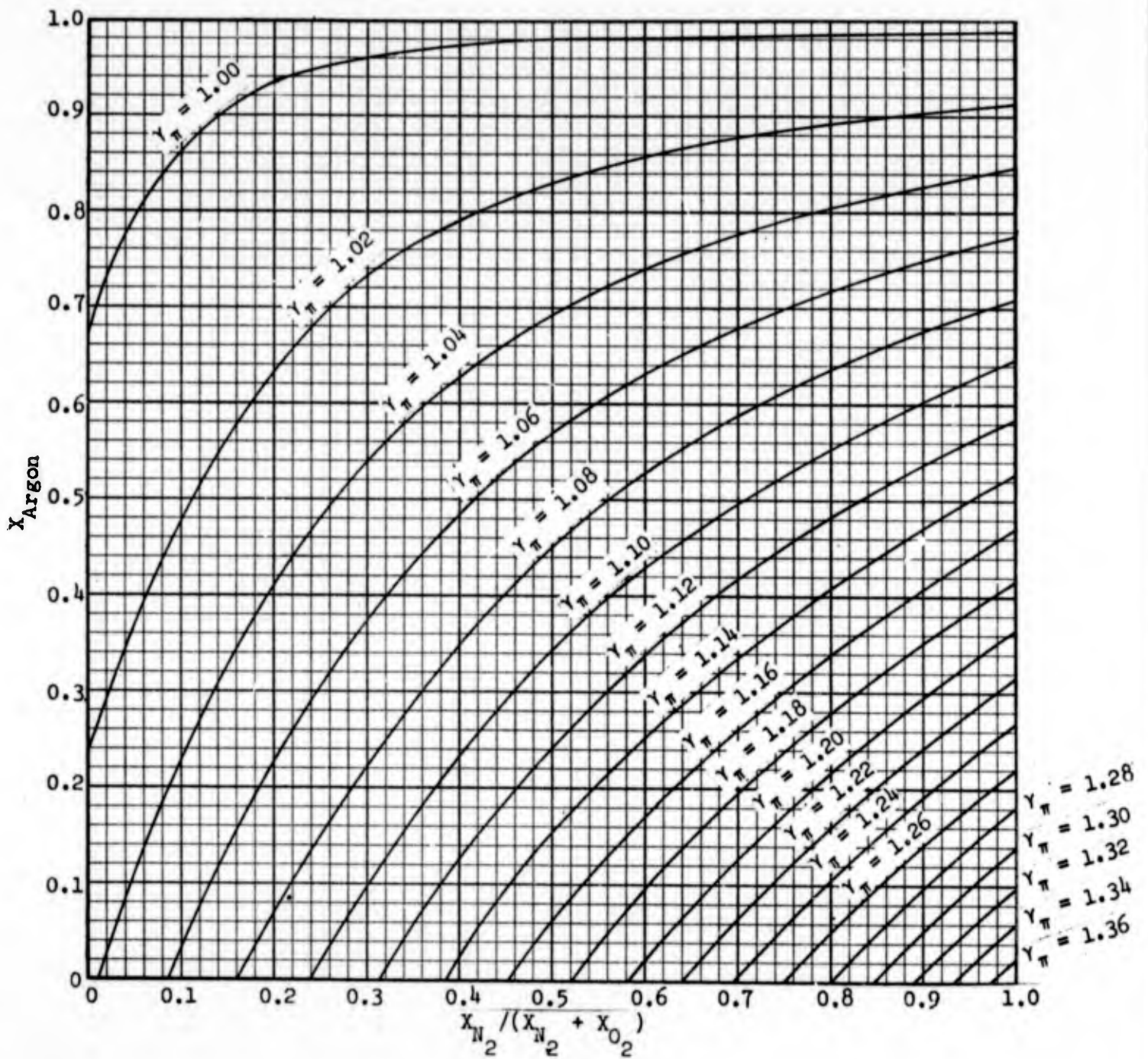


Figure 156. Argon Pressure Activity Coefficients, 16 Atmospheres.

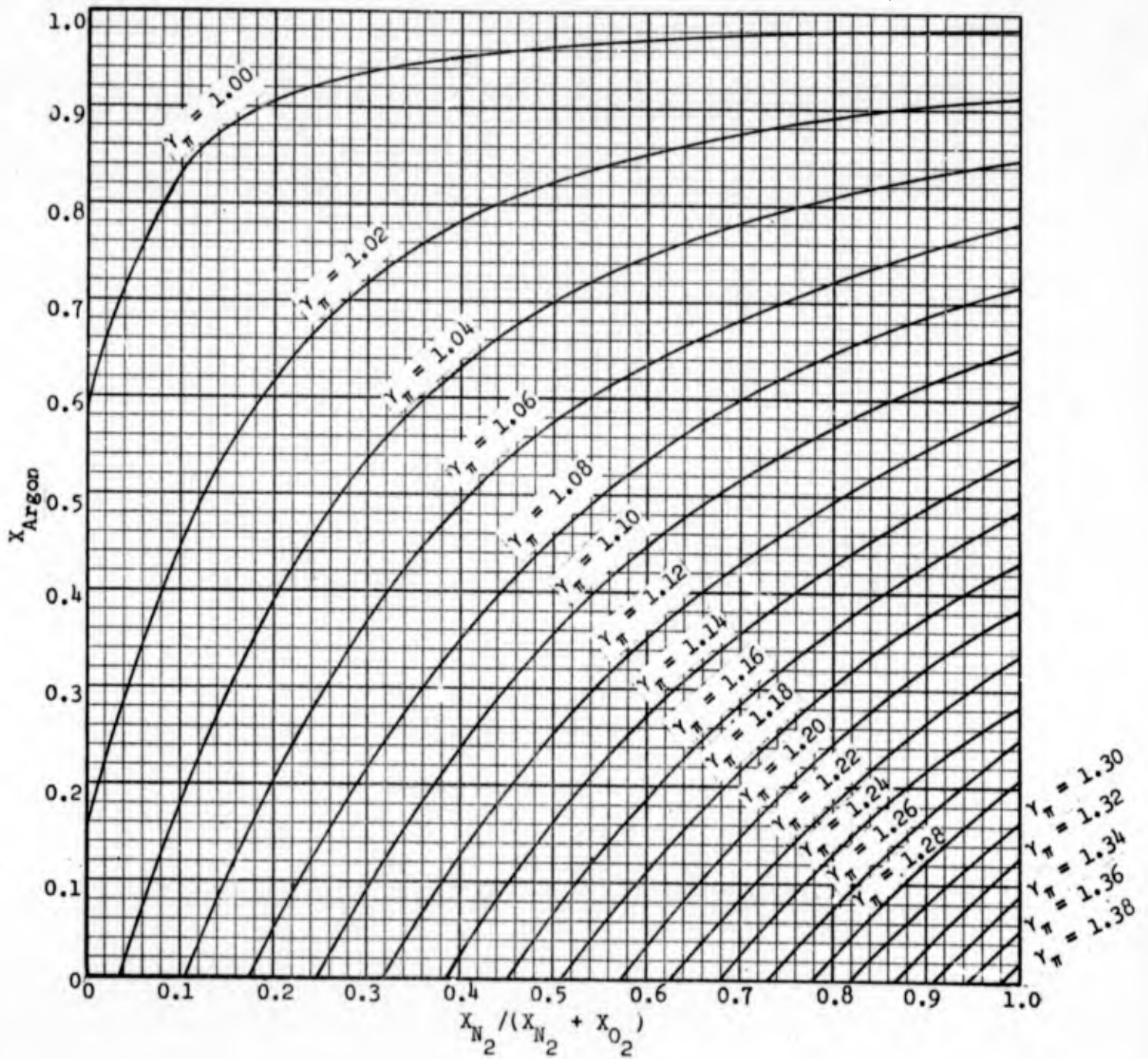


Figure 157. Argon Pressure Activity Coefficients, 18 Atmospheres.

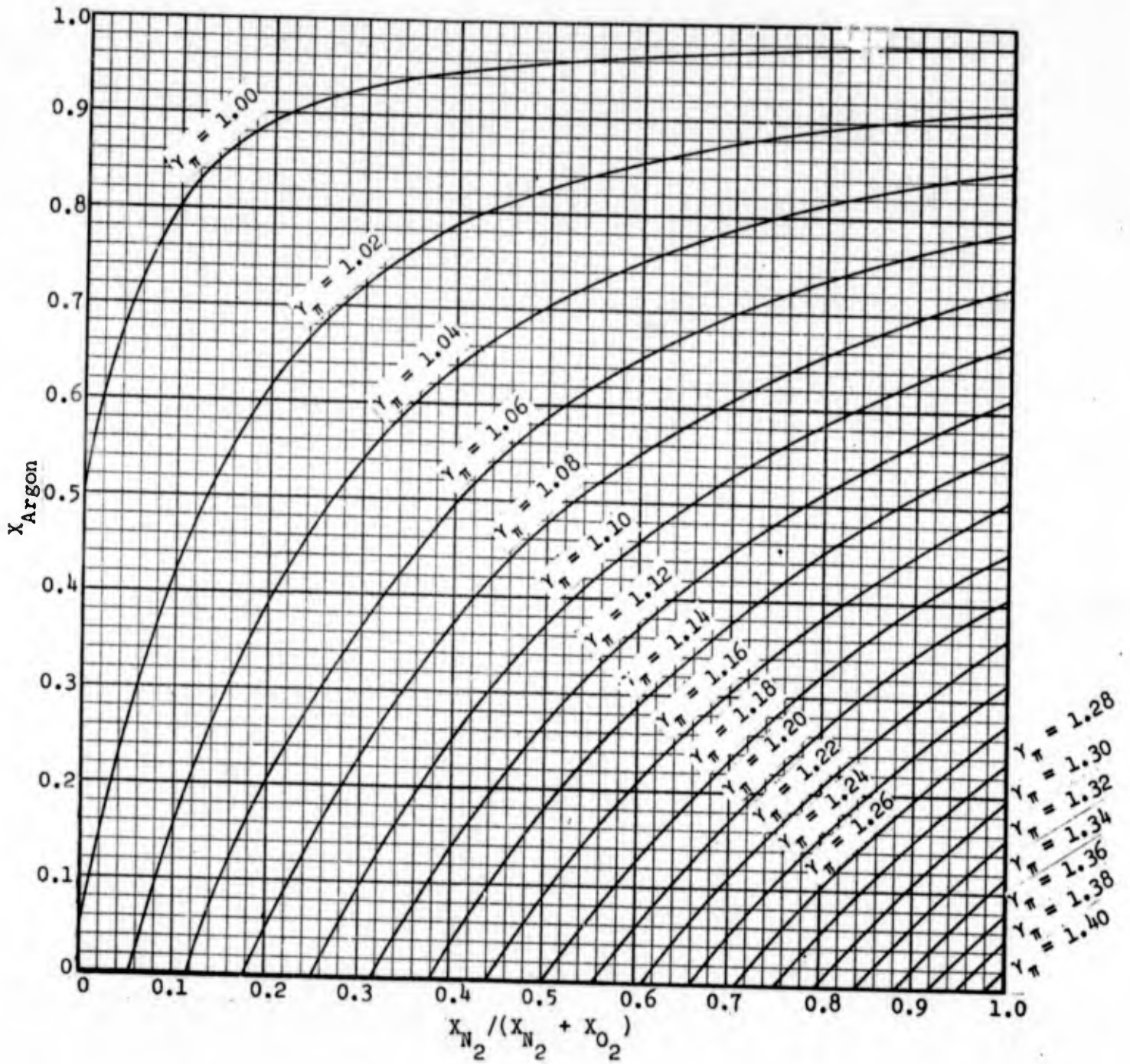


Figure 158. Argon Pressure Activity Coefficients, 20 Atmospheres.

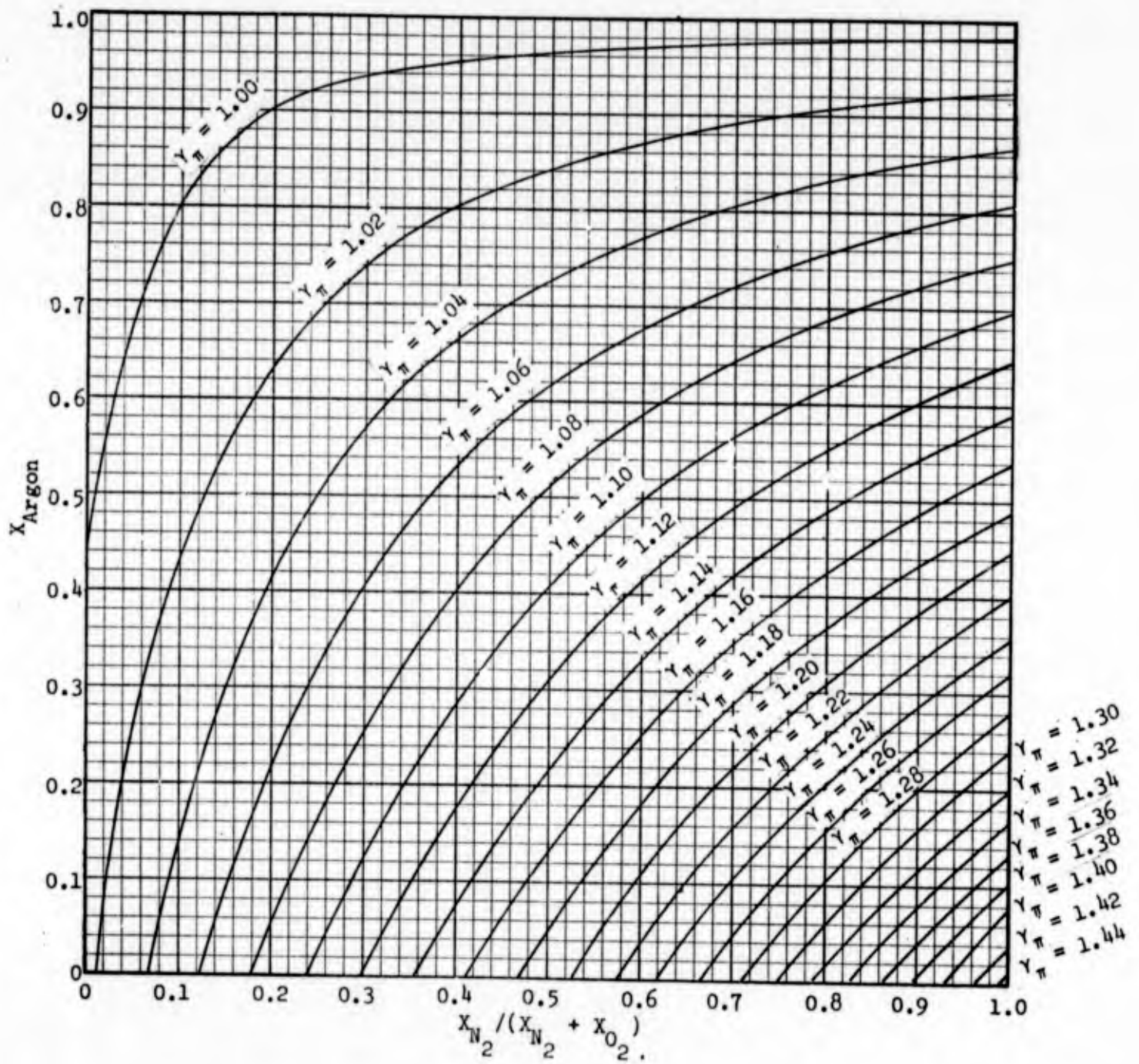


Figure 159. Argon Pressure Activity Coefficients, 23 Atmospheres.



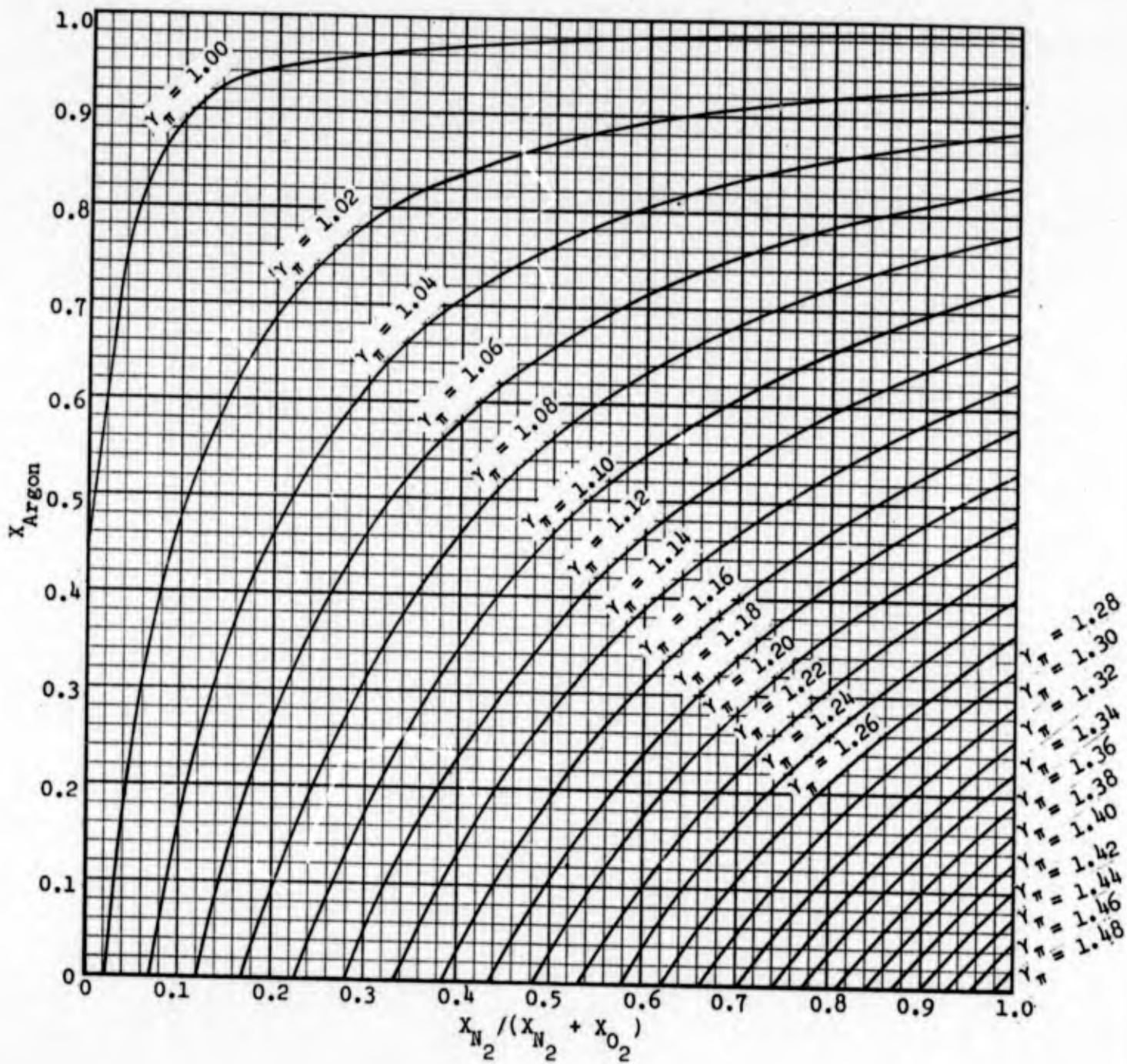


Figure 160. Argon Pressure Activity Coefficients, 26 Atmospheres.

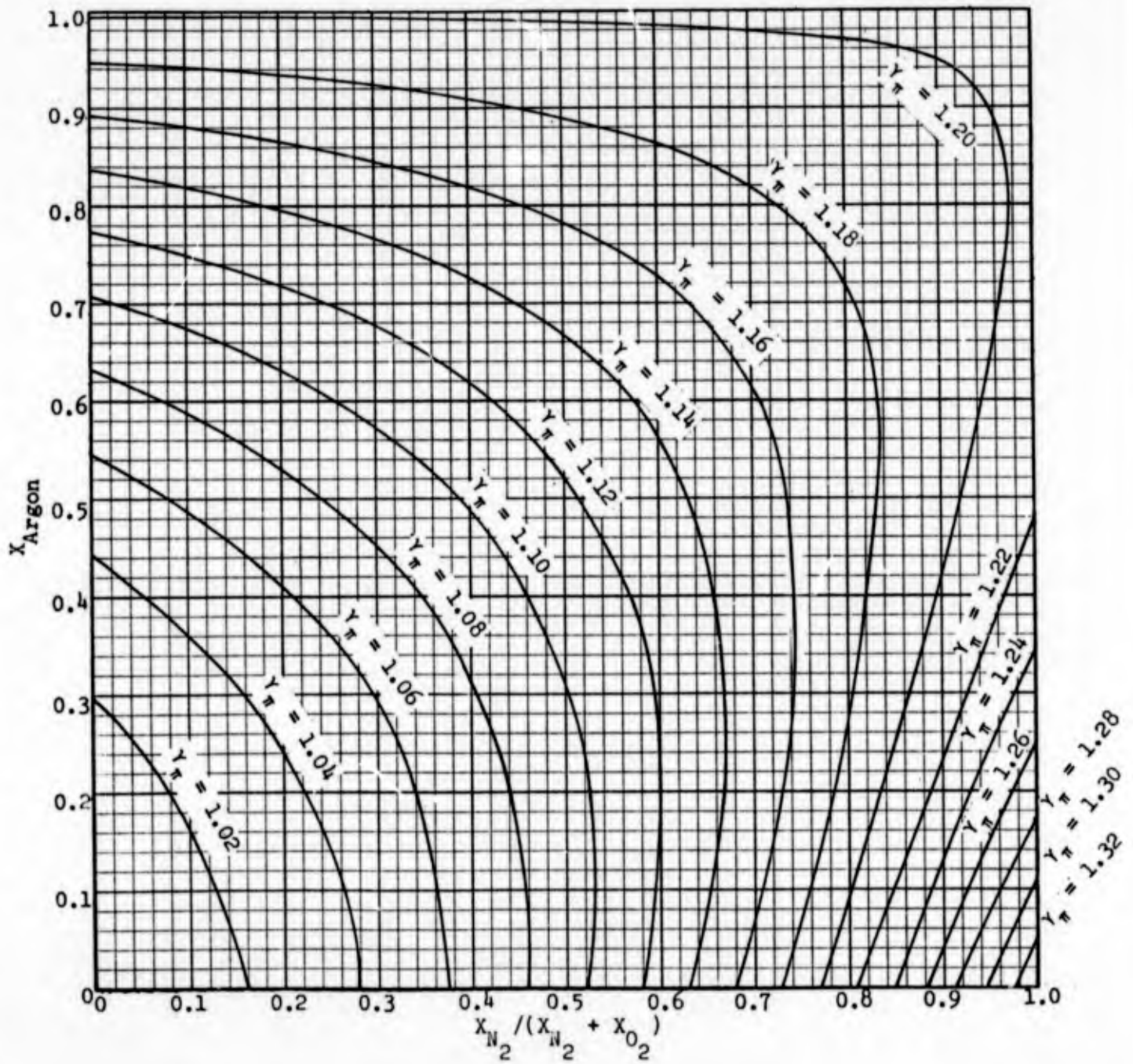


Figure 161. Oxygen Pressure Activity Coefficients, 1 Atmosphere.

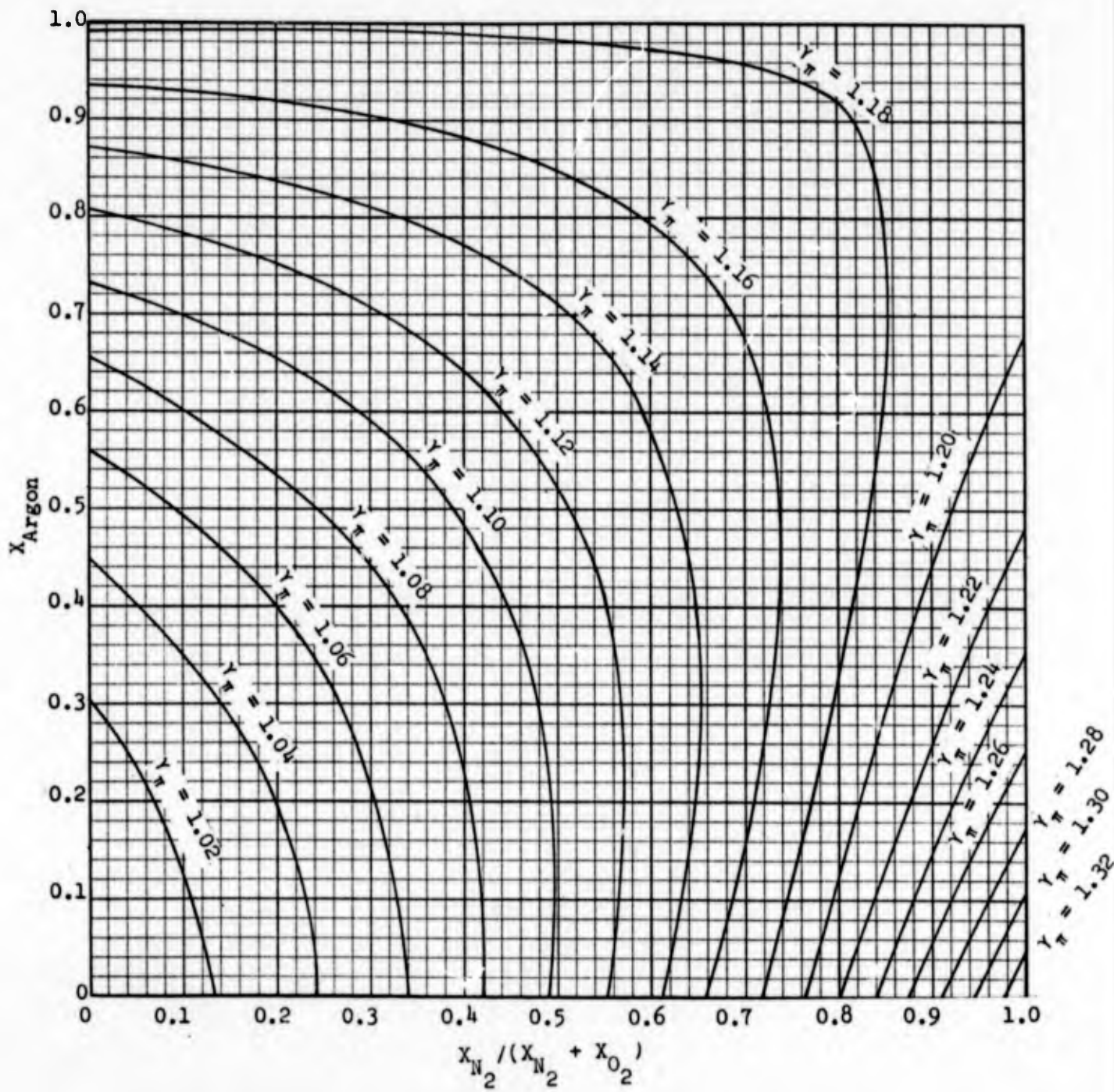


Figure 162. Oxygen Pressure Activity Coefficients, 2 Atmospheres.

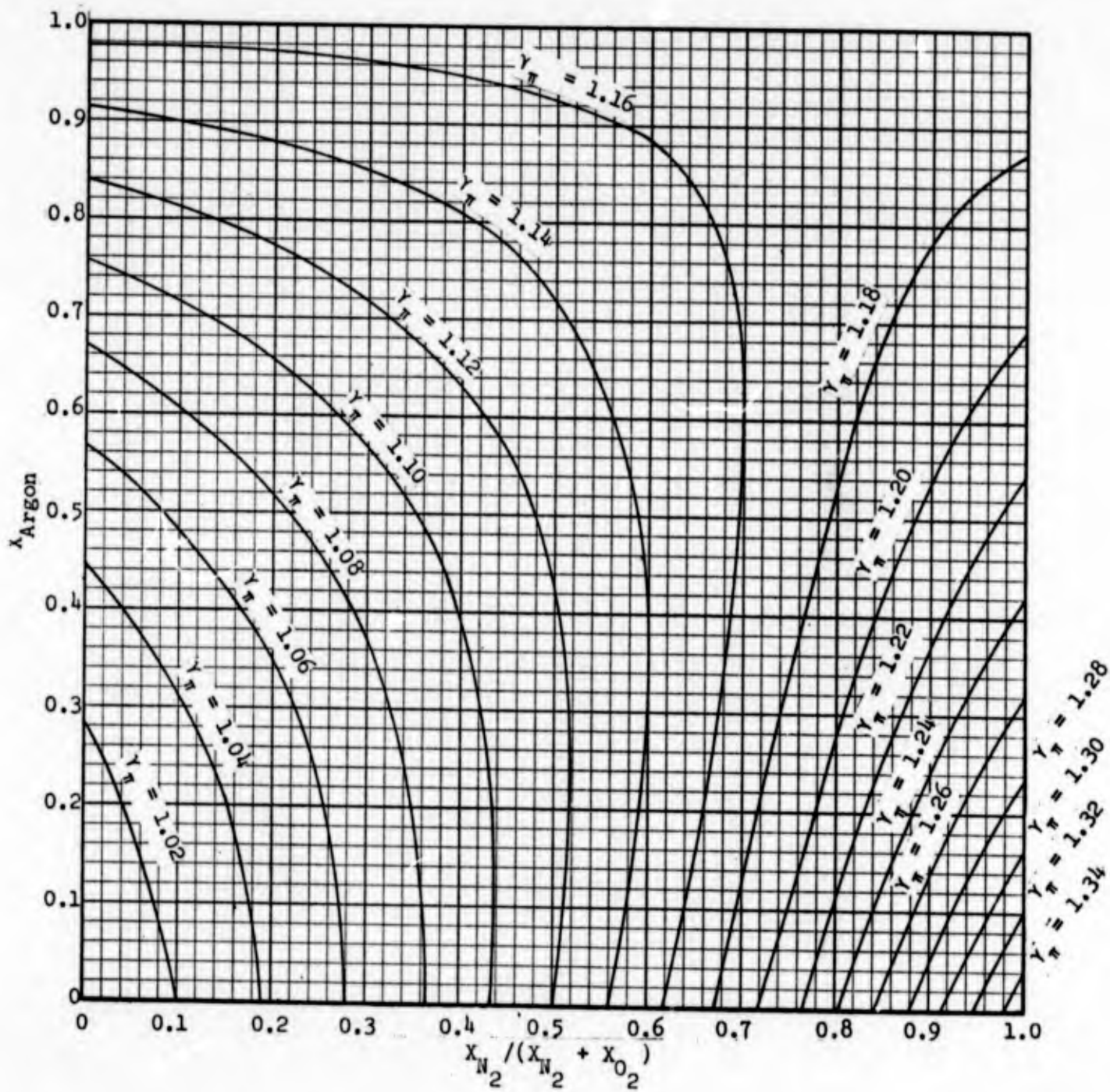


Figure 163. Oxygen Pressure Activity Coefficients, 4 Atmospheres.

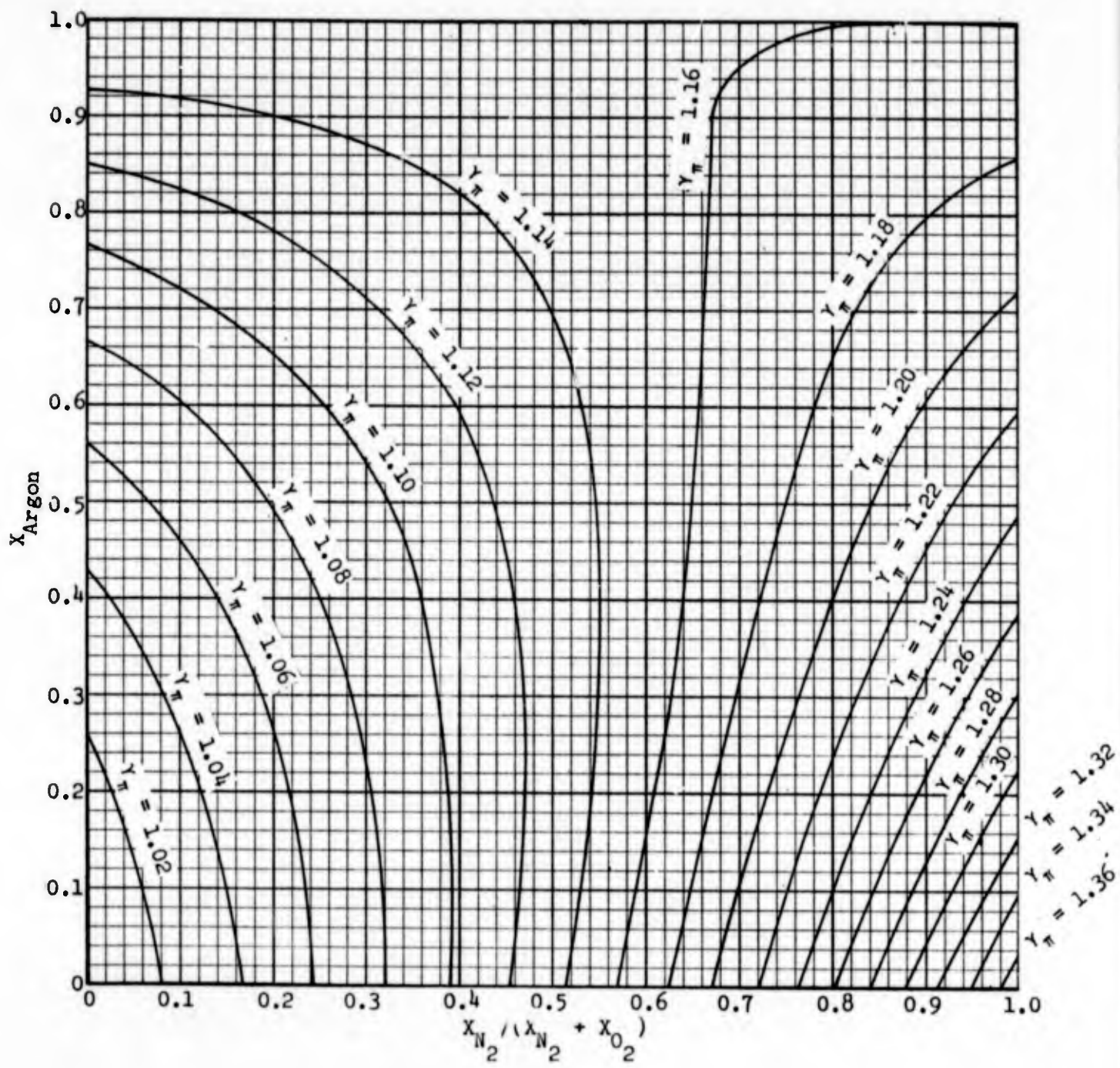


Figure 164. Oxygen Pressure Activity Coefficients, 6 Atmospheres.

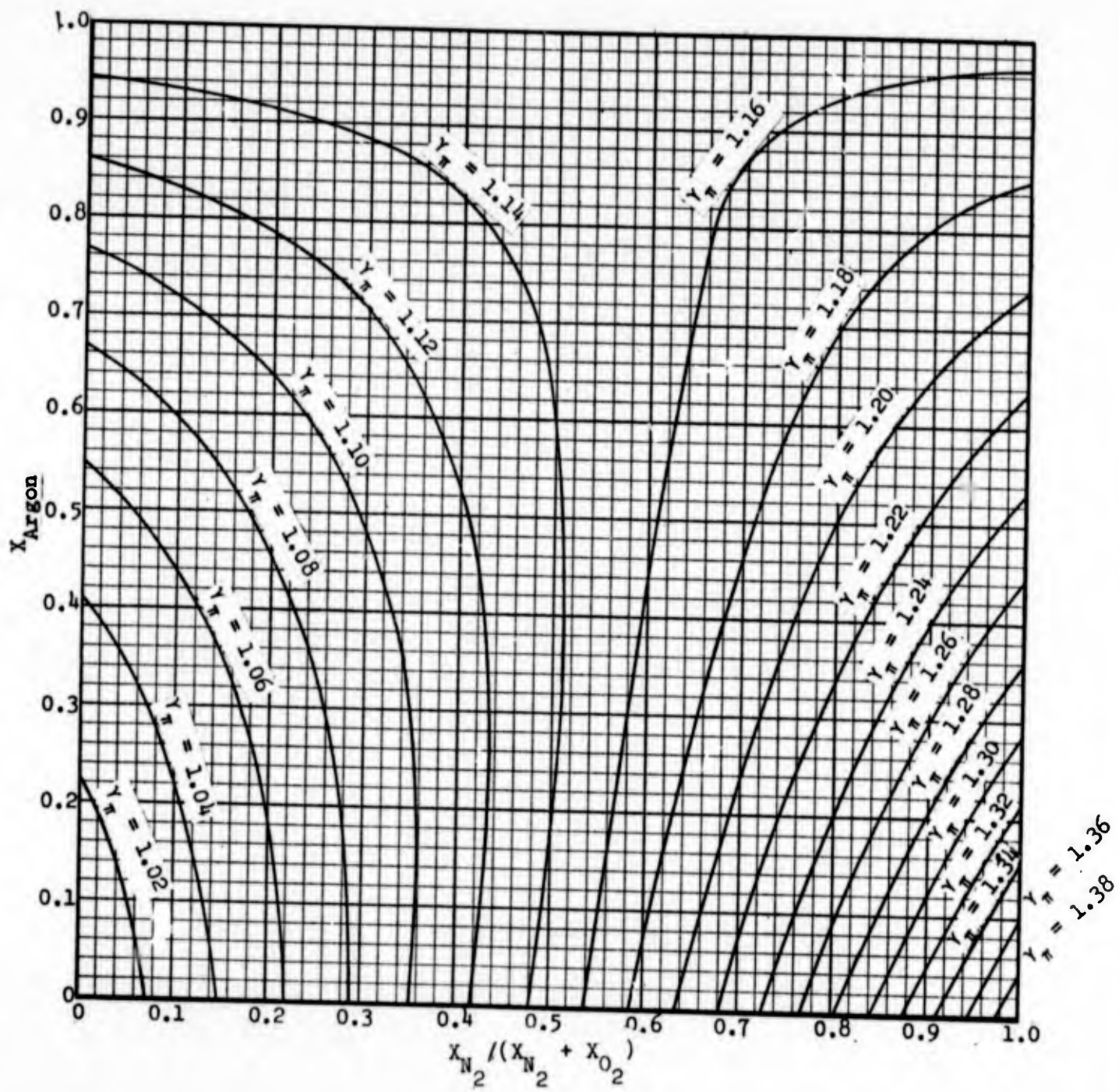


Figure 165. Oxygen Pressure Activity Coefficients, 8 Atmospheres.

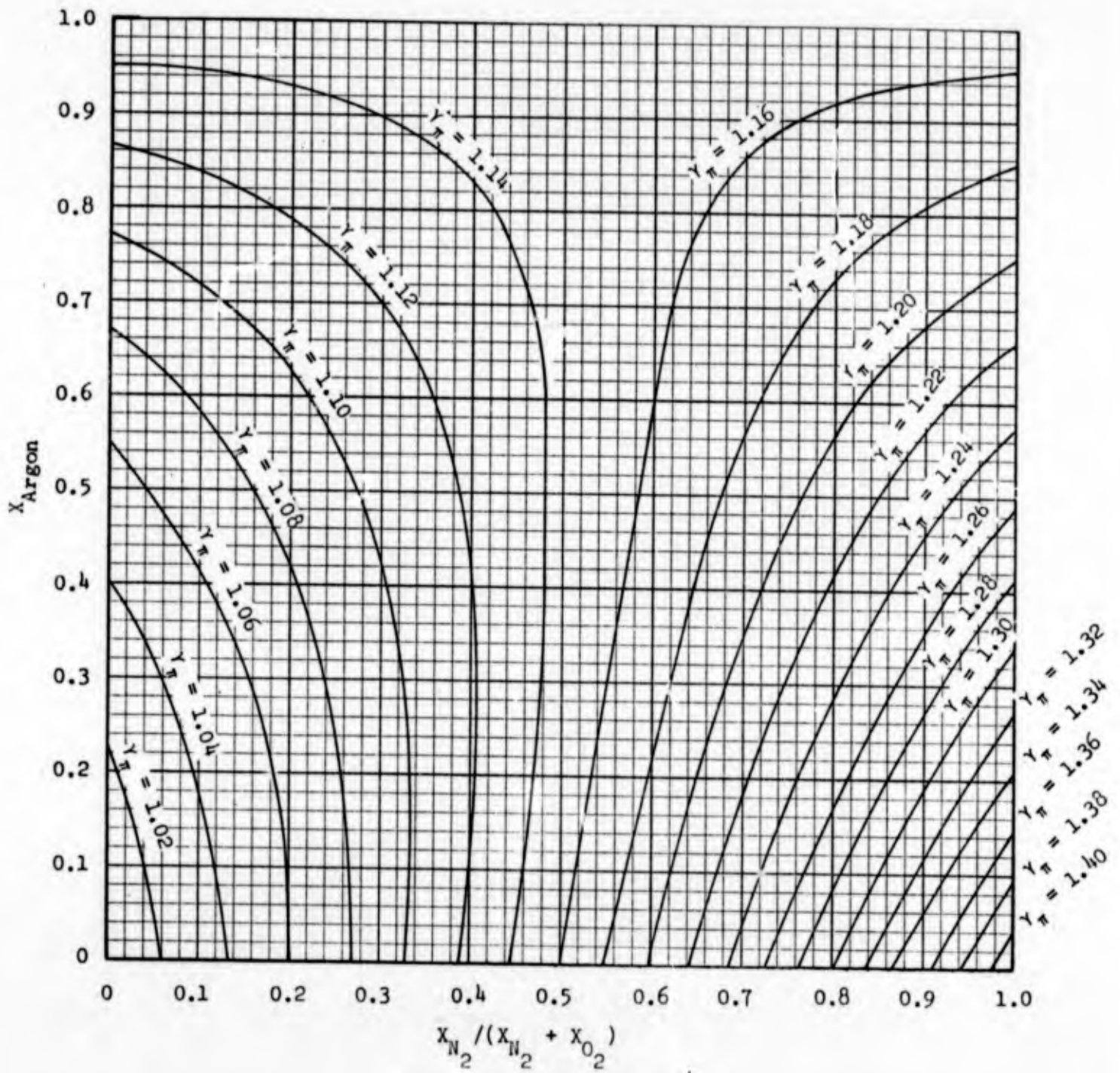


Figure 166. Oxygen Pressure Activity Coefficients, 10 Atmospheres.

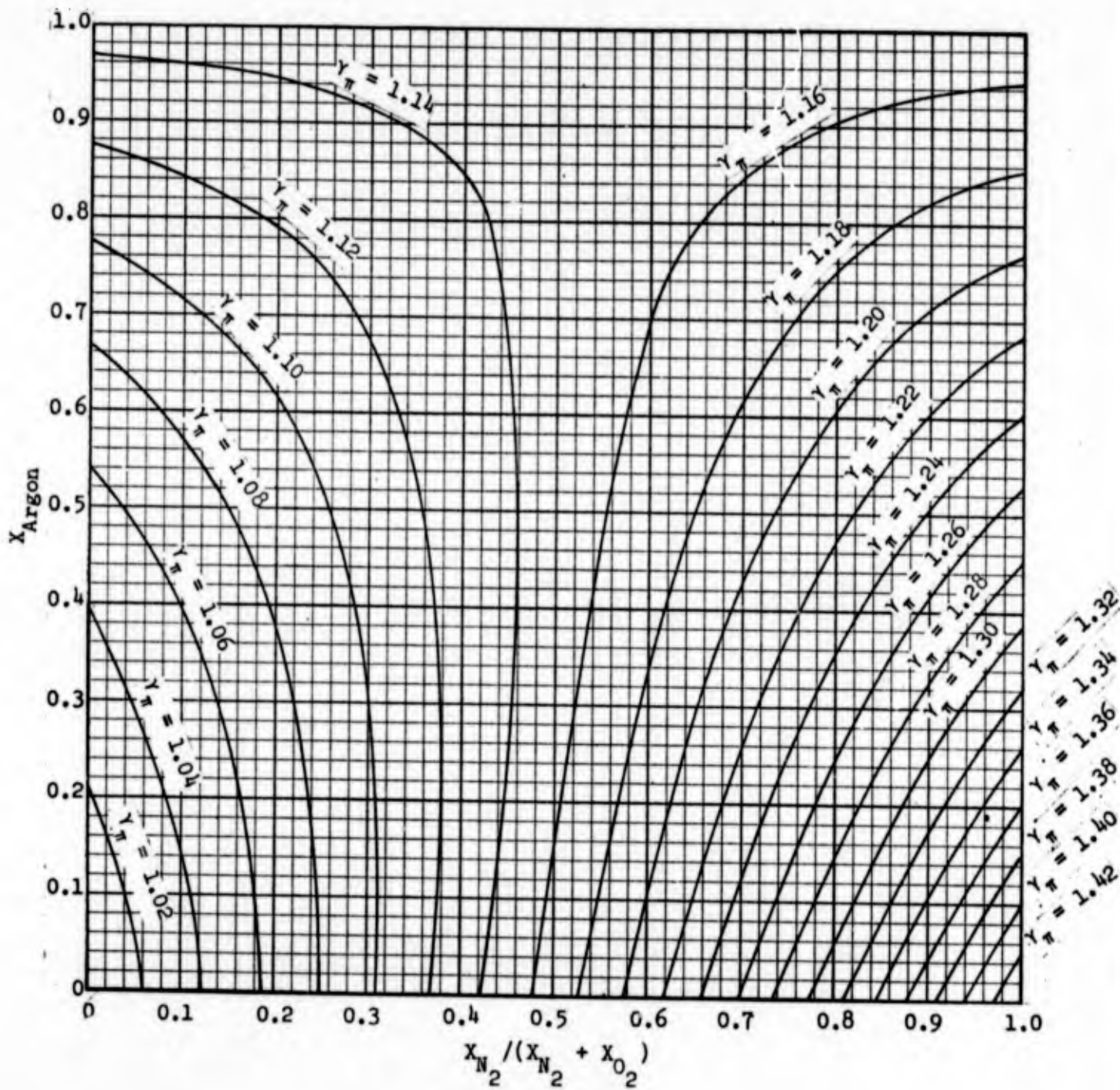


Figure 167. Oxygen Pressure Activity Coefficients, 12 Atmospheres.



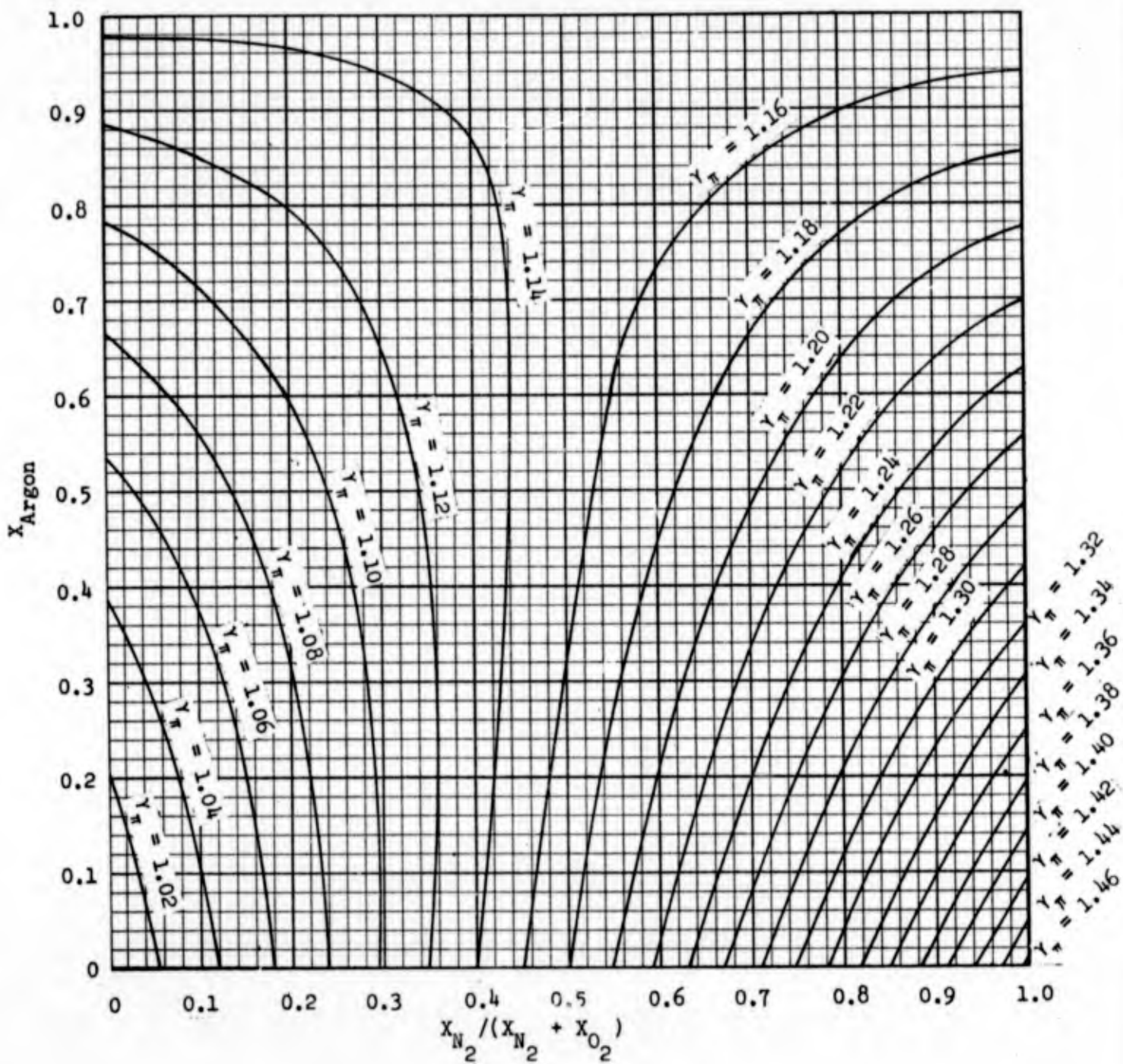


Figure 168. Oxygen Pressure Activity Coefficients, 14 Atmospheres,

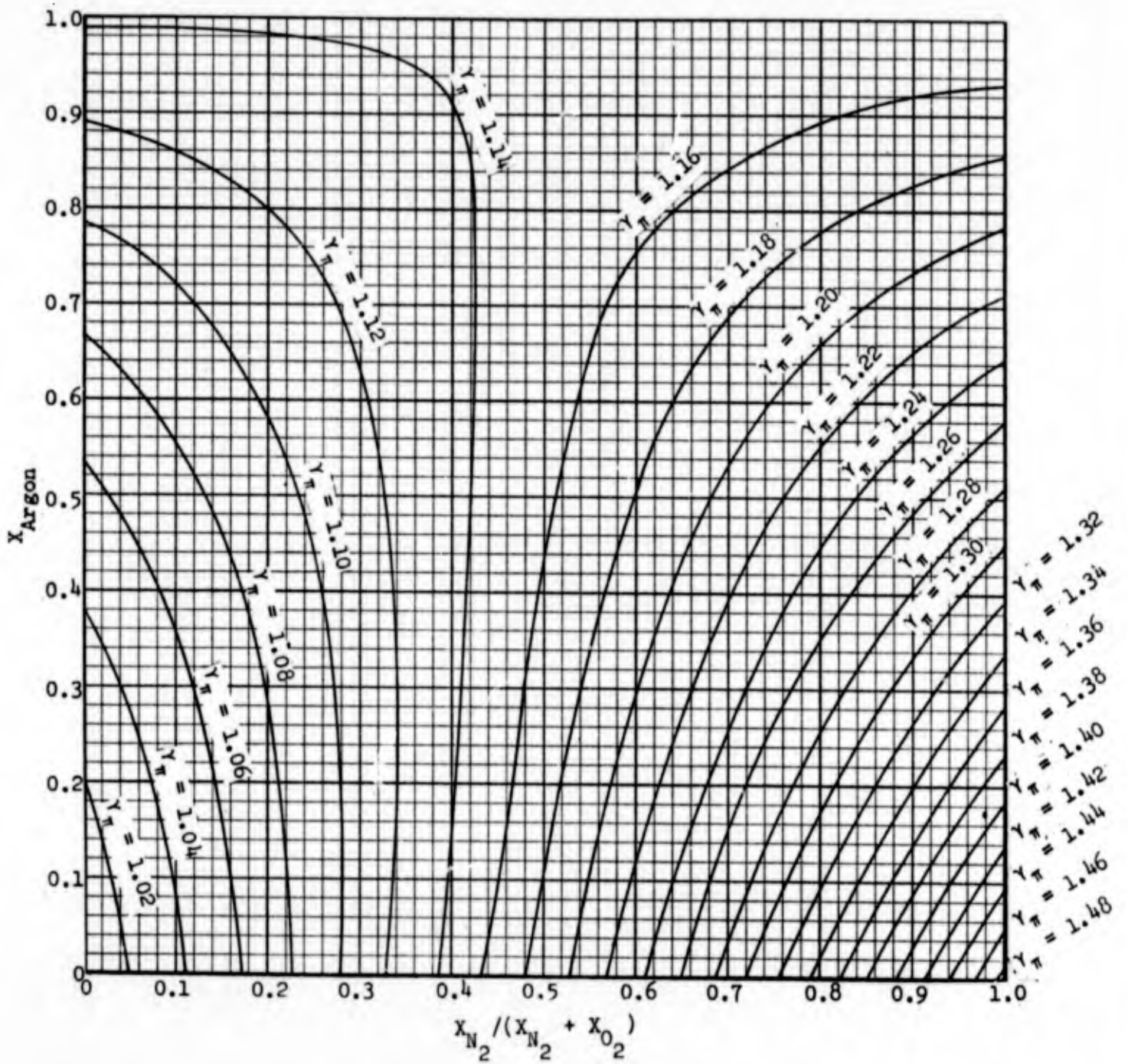


Figure 169. Oxygen Pressure Activity Coefficients, 16 Atmospheres.

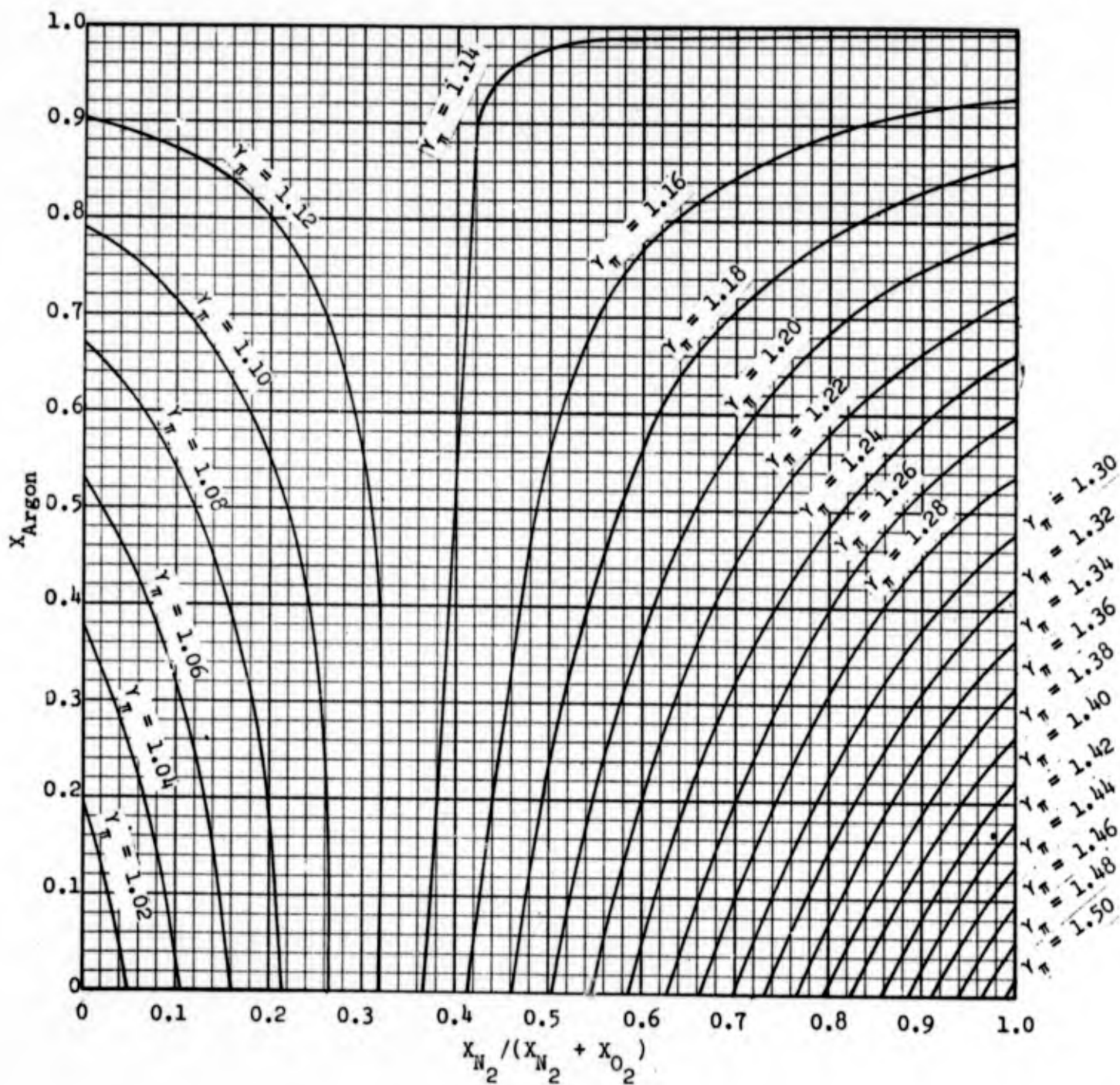


Figure 170. Oxygen Pressure Activity Coefficients, 18 Atmospheres.

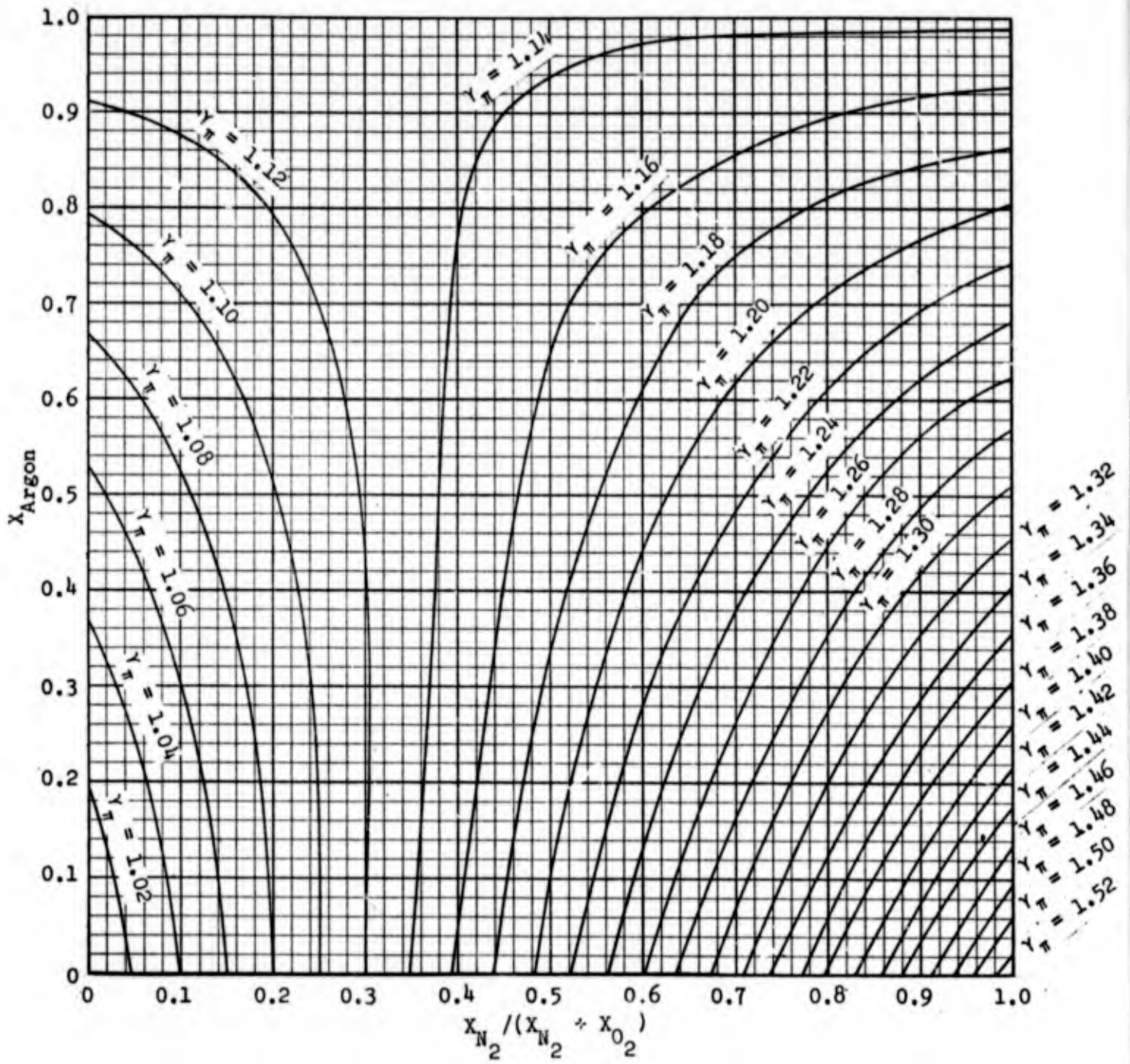


Figure 171. Oxygen Pressure Activity Coefficients, 20 Atmospheres.

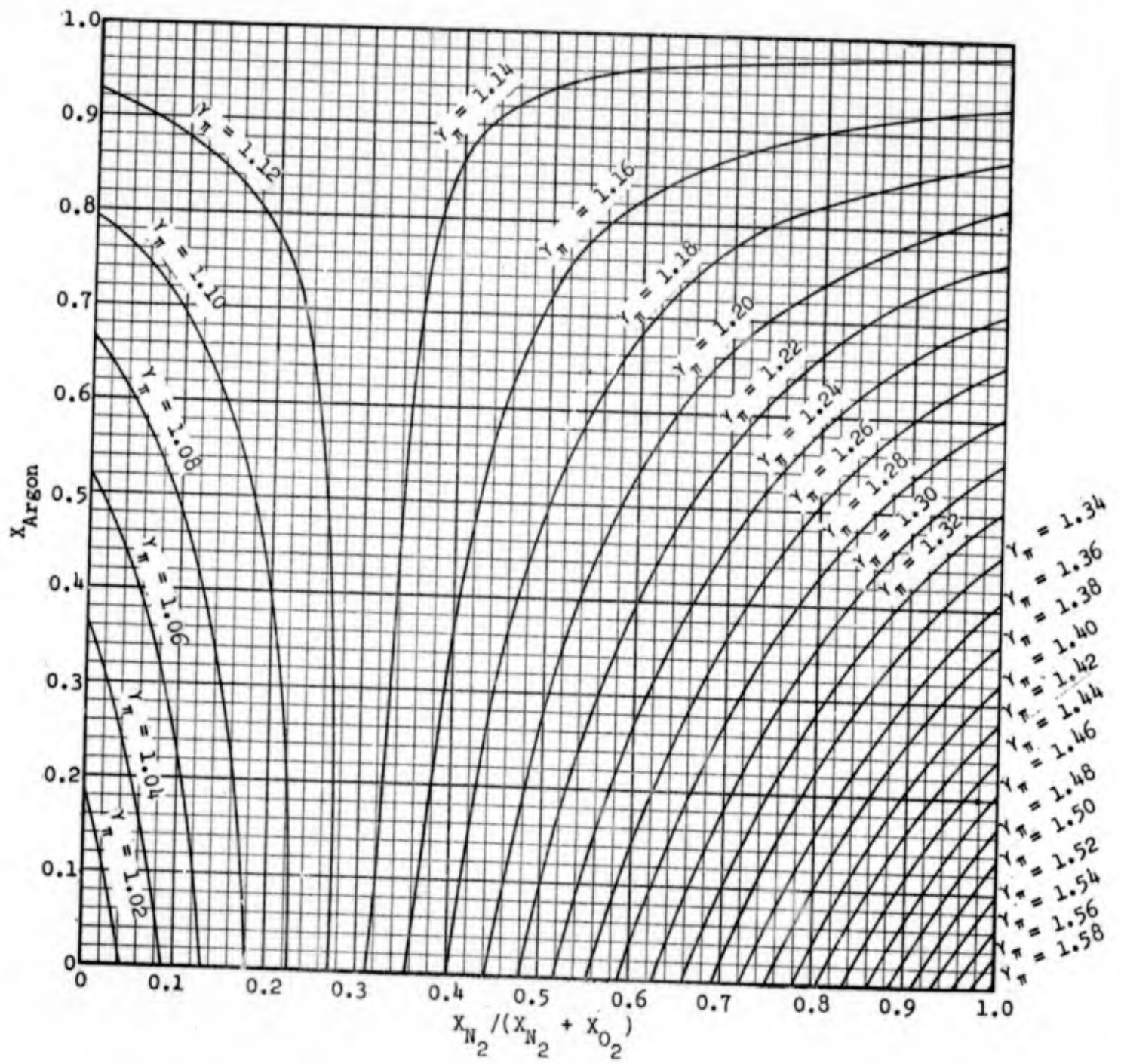


Figure 172. Oxygen Pressure Activity Coefficients, 23 Atmospheres.

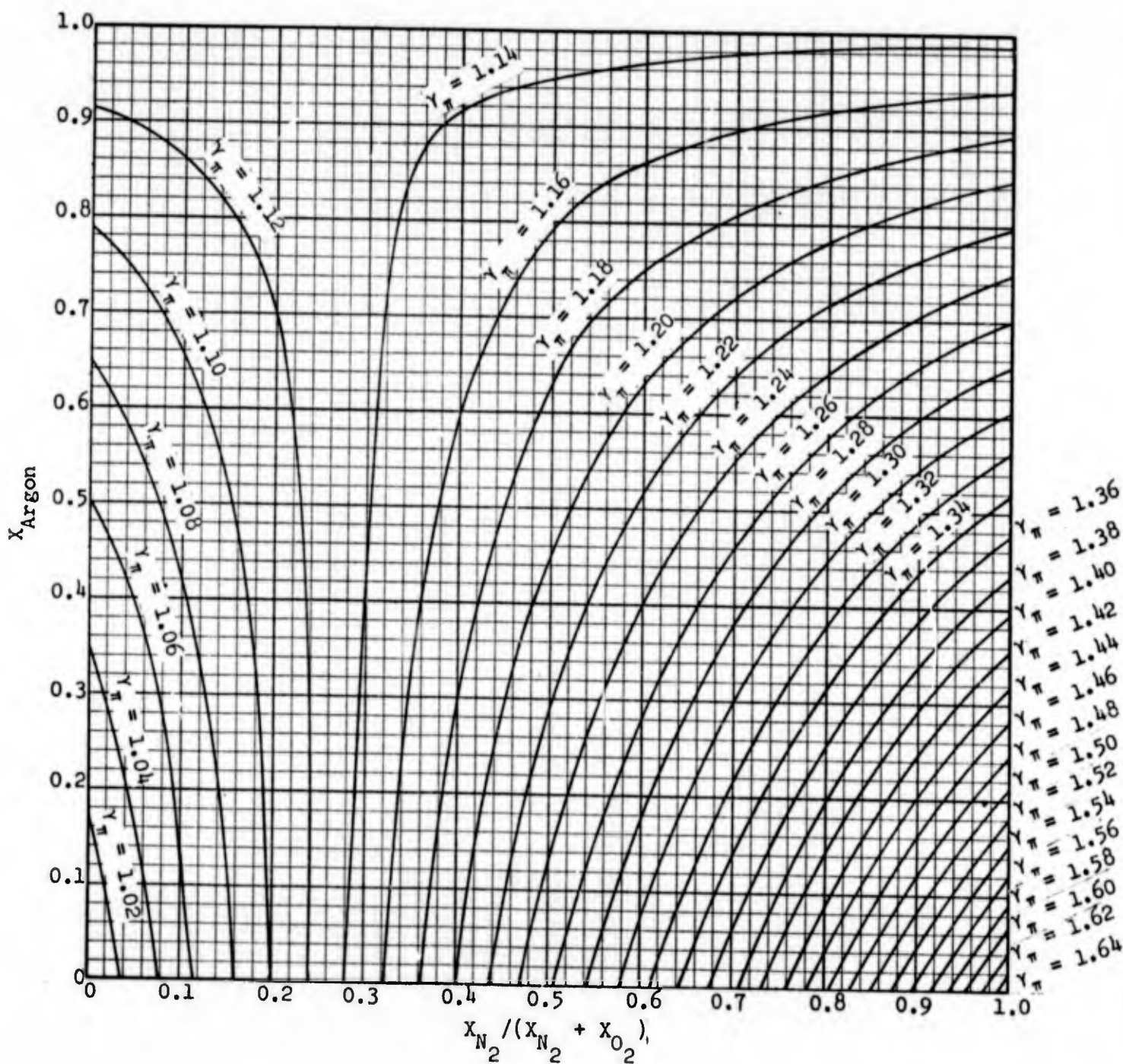


Figure 173. Oxygen Pressure Activity Coefficients, 26 Atmospheres.

G. Mixture Vapor Pressures Vs. Temperatures

The 13 graphs to follow present the vapor pressure of a number of specific mixtures as it varies with temperature. These graphs are plotted as  $\log P$  vs.  $1/T$ . The graphs are ordered with respect to increasing mole fraction argon in the liquid.

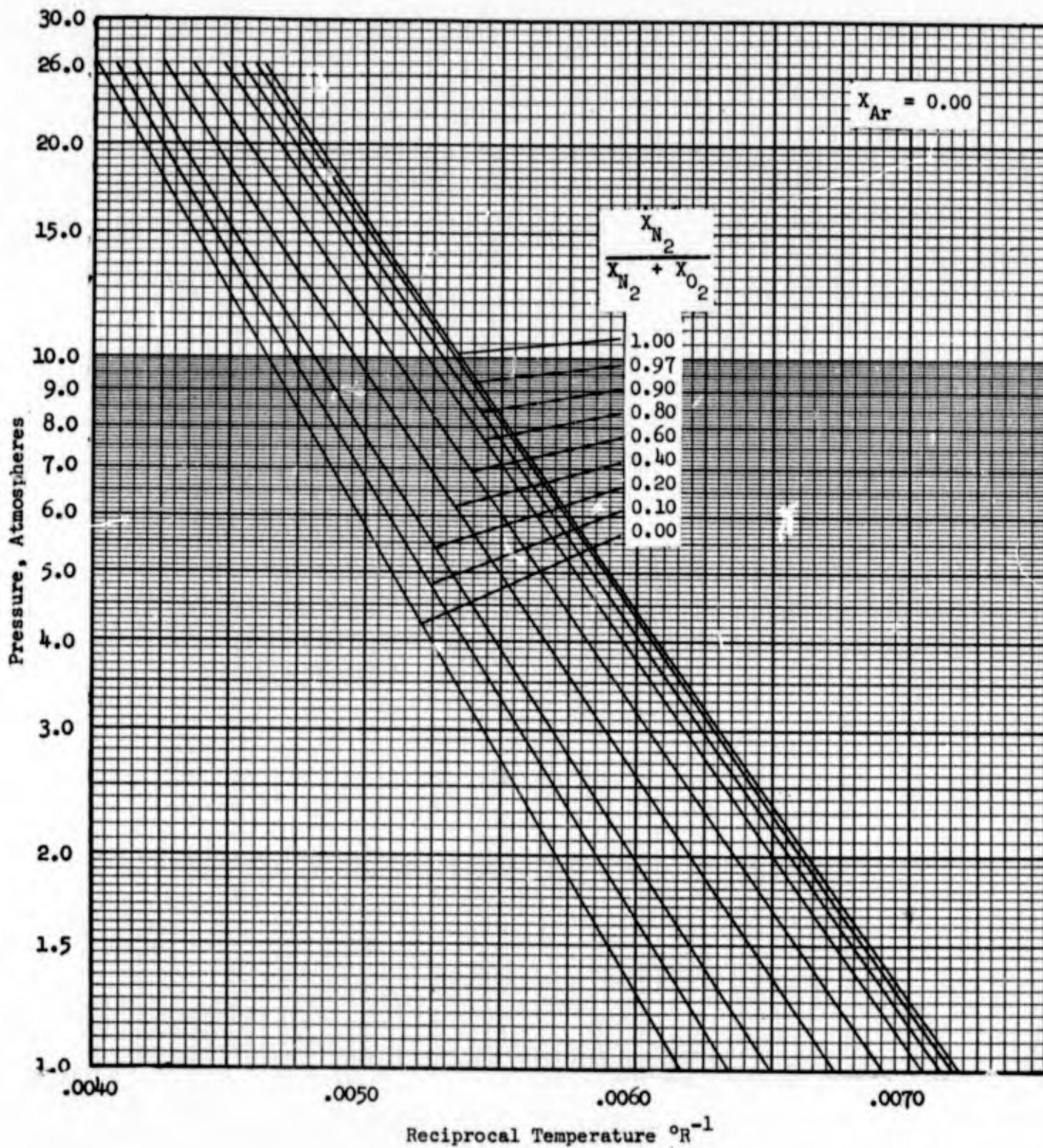


Figure 174. Vapor Pressures of Specific Mixtures of  $N_2$ -Ar- $O_2$ .



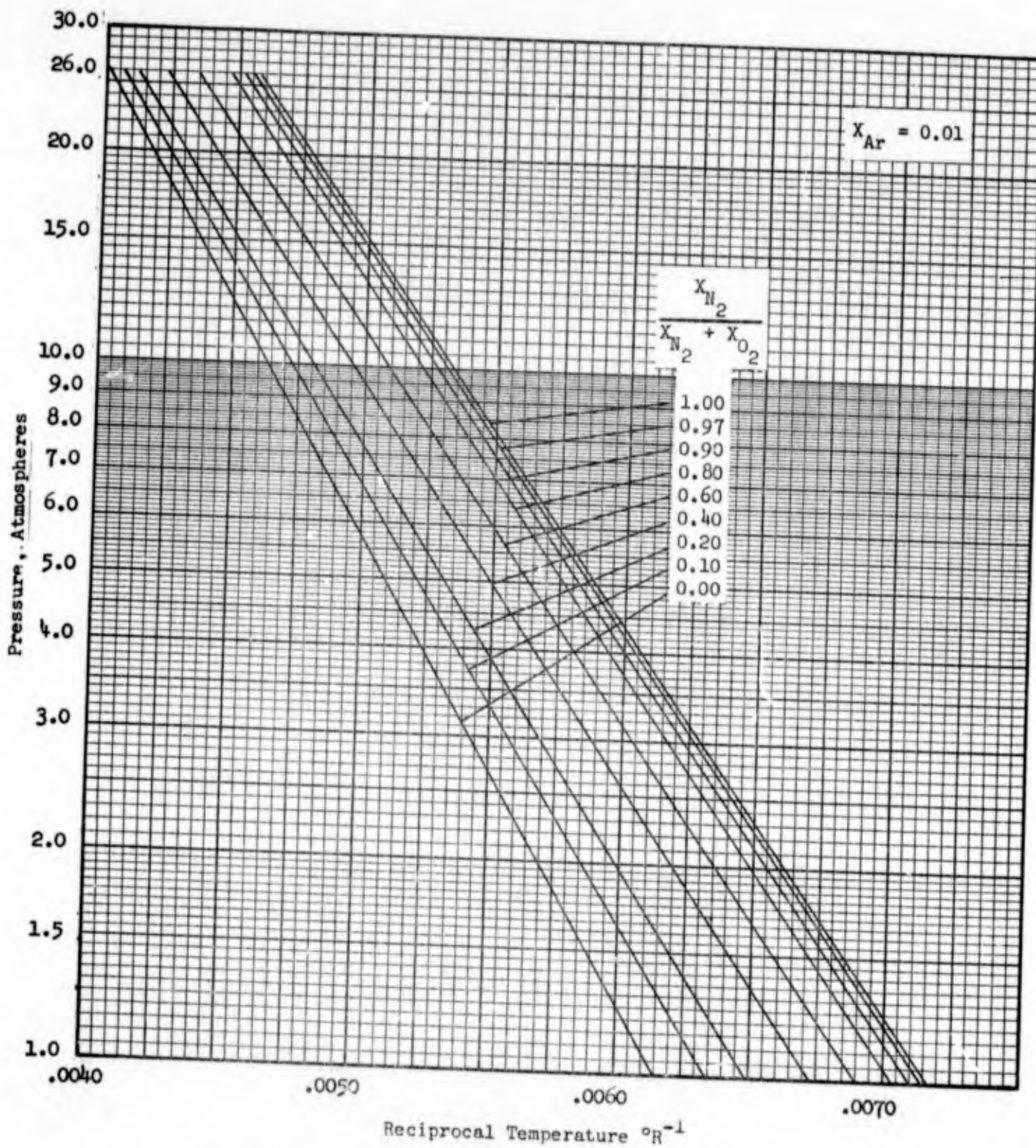


Figure 175. Vapor Pressures of Specific Mixtures of  $N_2$ -Ar- $O_2$ .

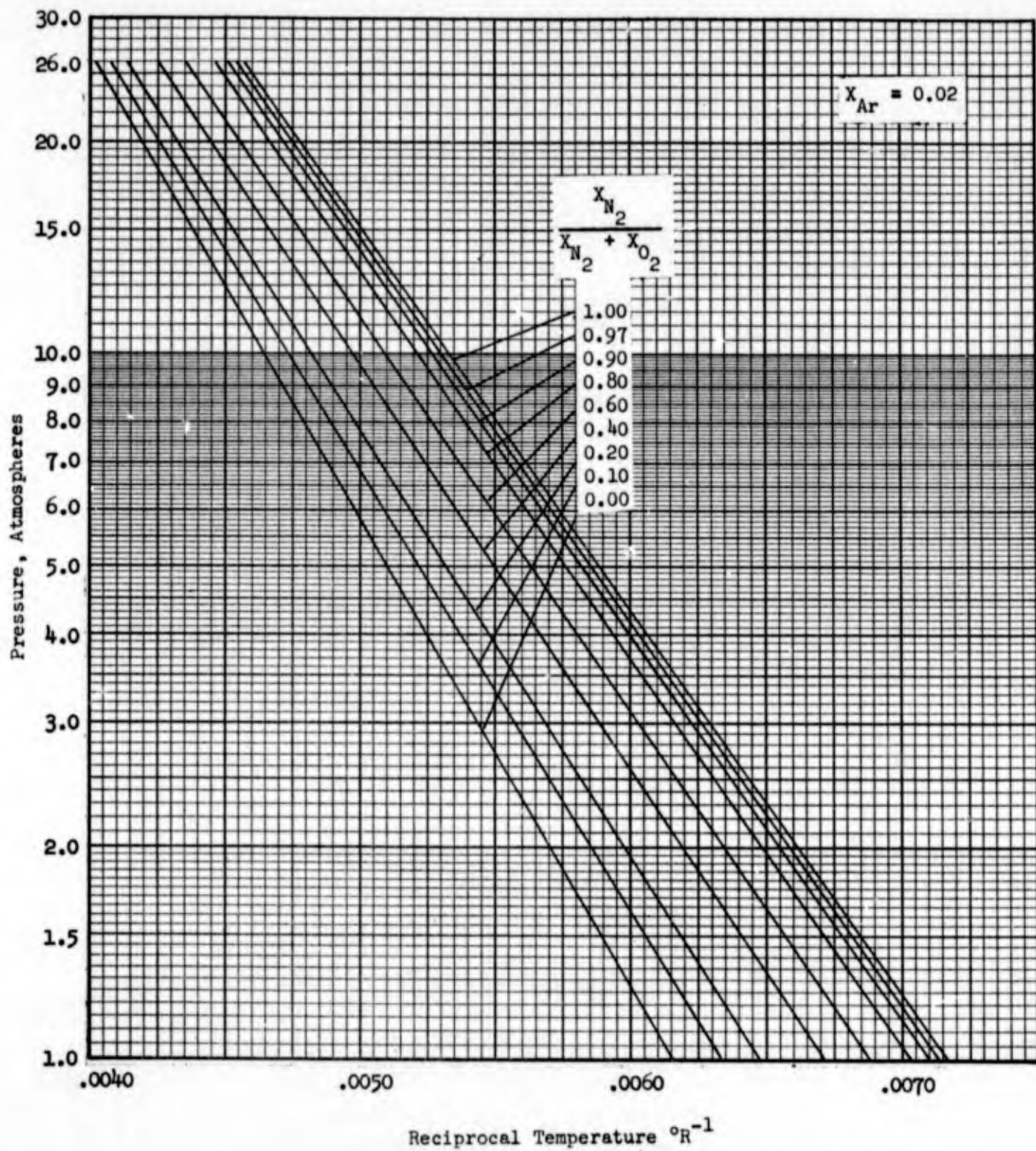


Figure 176. Vapor Pressures of Specific Mixtures of  $N_2$ -Ar- $O_2$ .

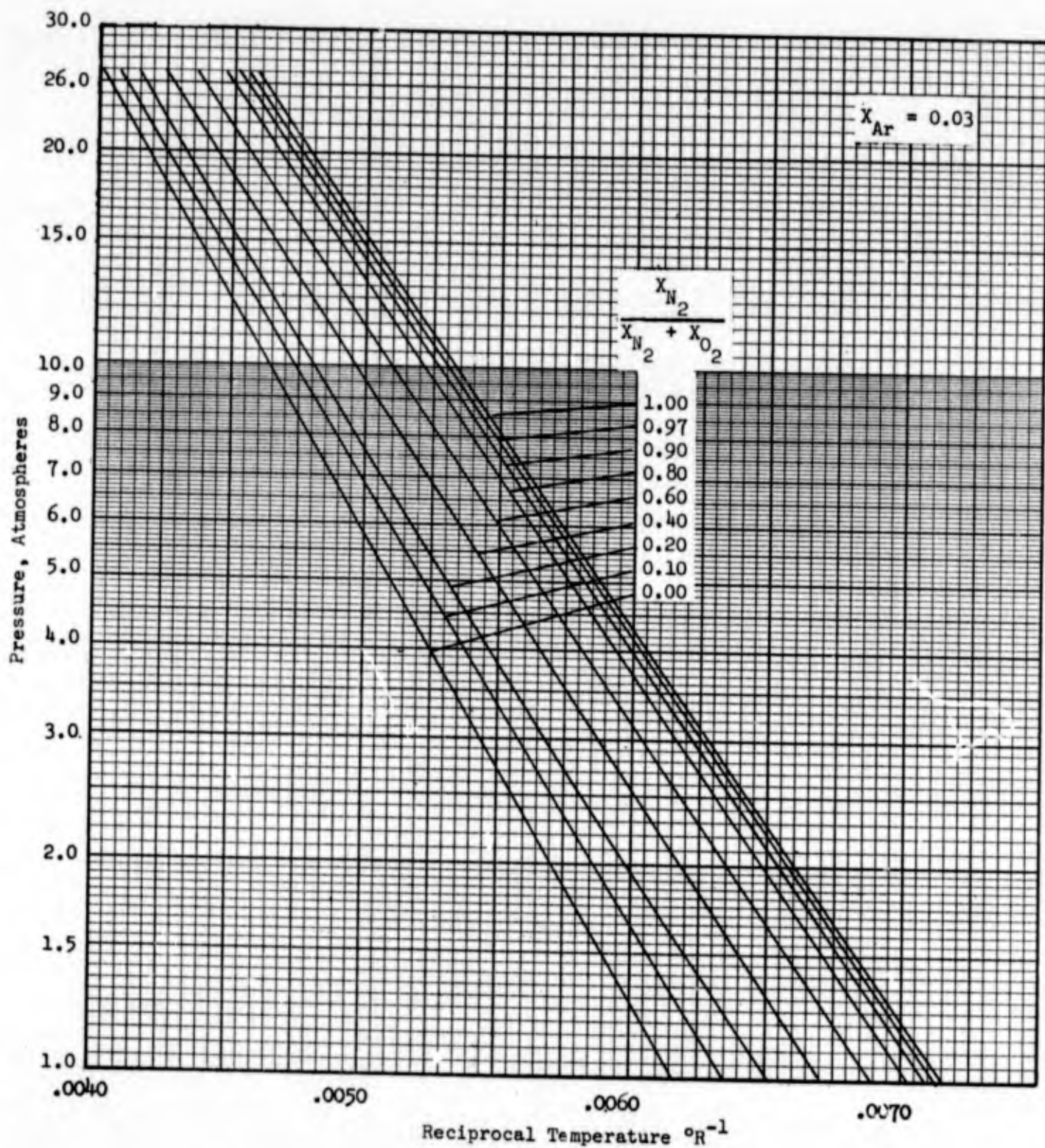


Figure 177. Vapor Pressures of Specific Mixtures of  $N_2$ -Ar- $O_2$ .

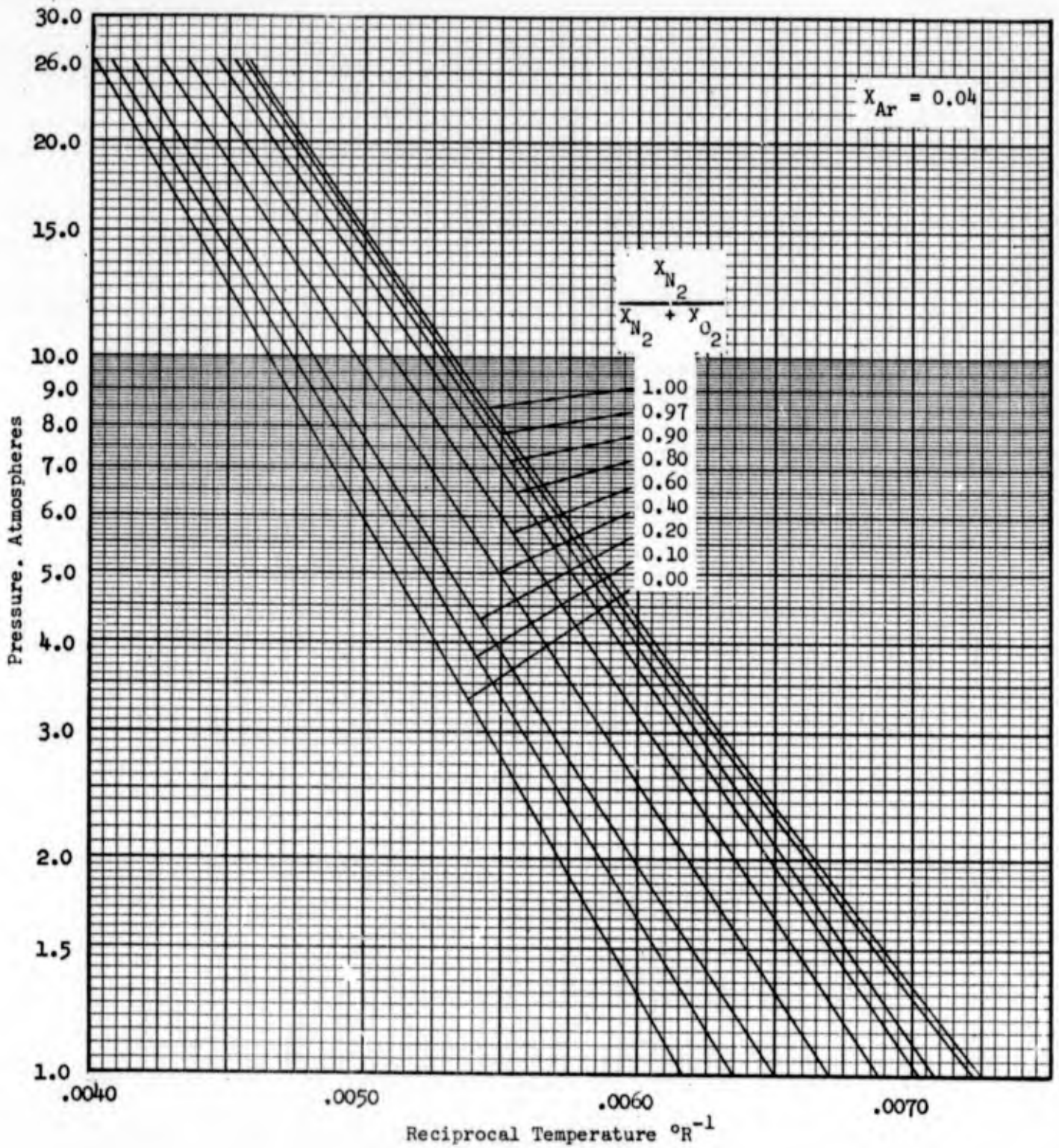


Figure 178. Vapor Pressures of Specific Mixtures of  $N_2$ -Ar- $O_2$ .

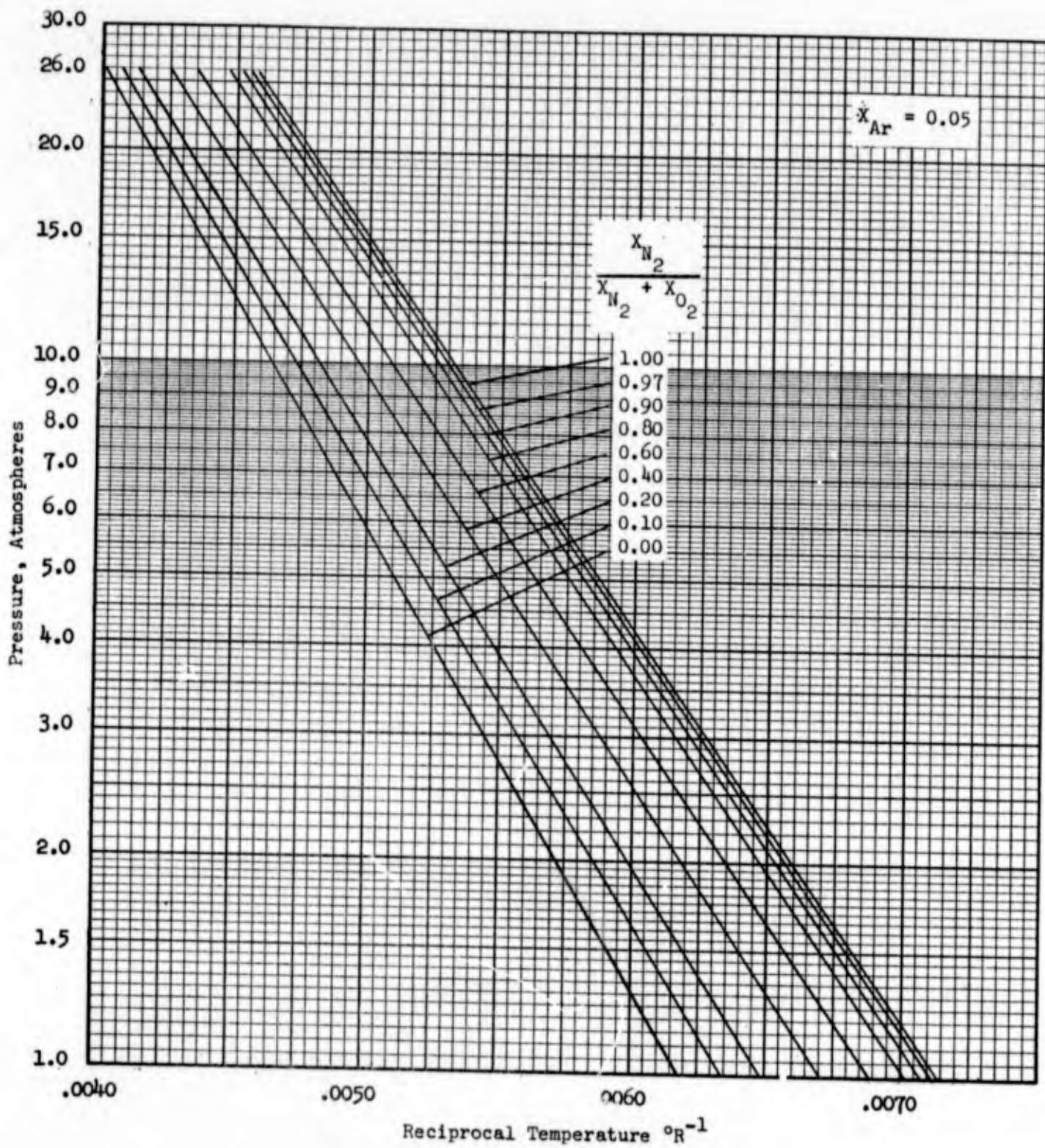


Figure 179. Vapor Pressures of Specific Mixtures of  $N_2$ -Ar- $O_2$ .

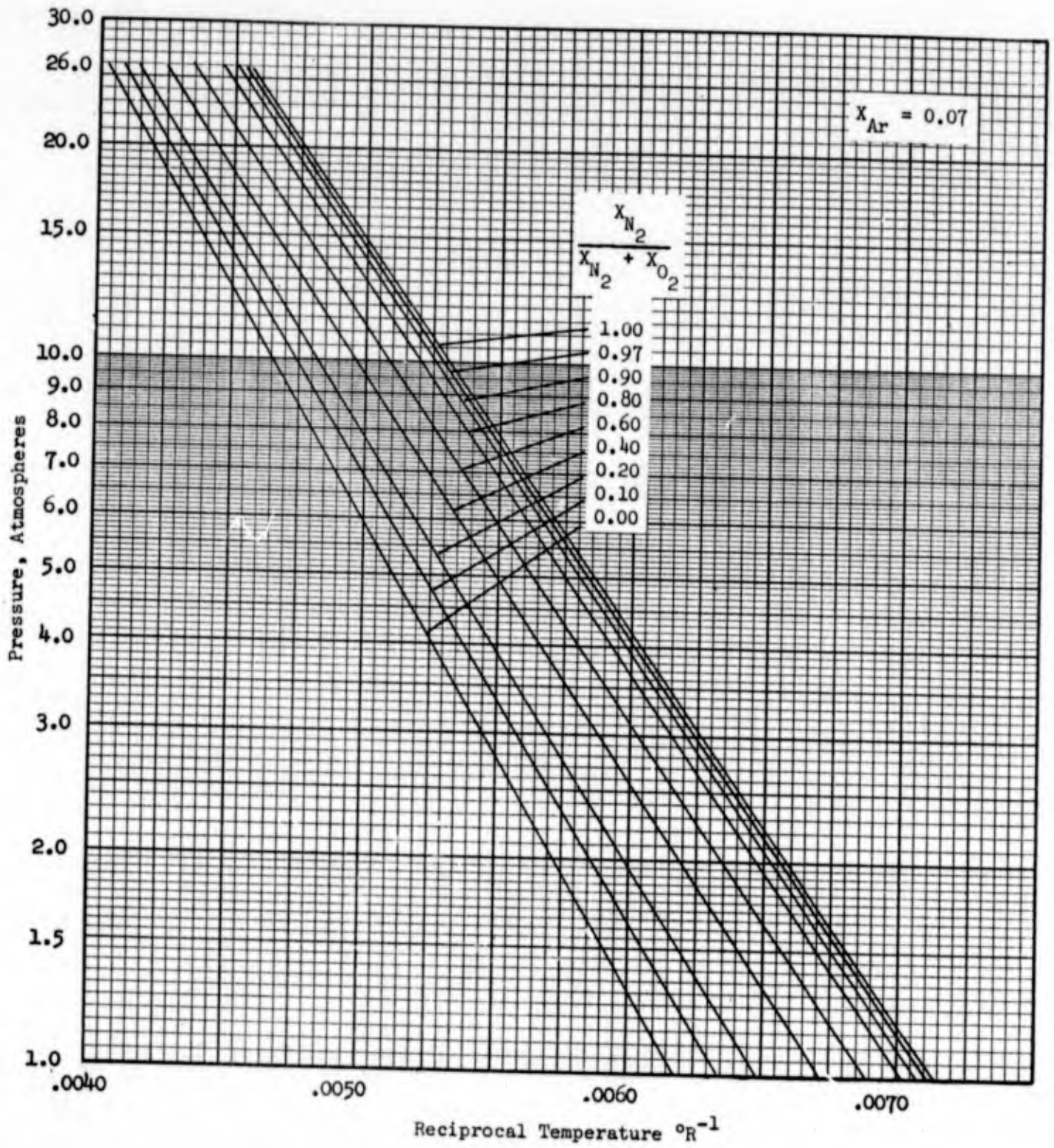


Figure 180. Vapor Pressures of Specific Mixtures of  $N_2$ -Ar- $O_2$ .

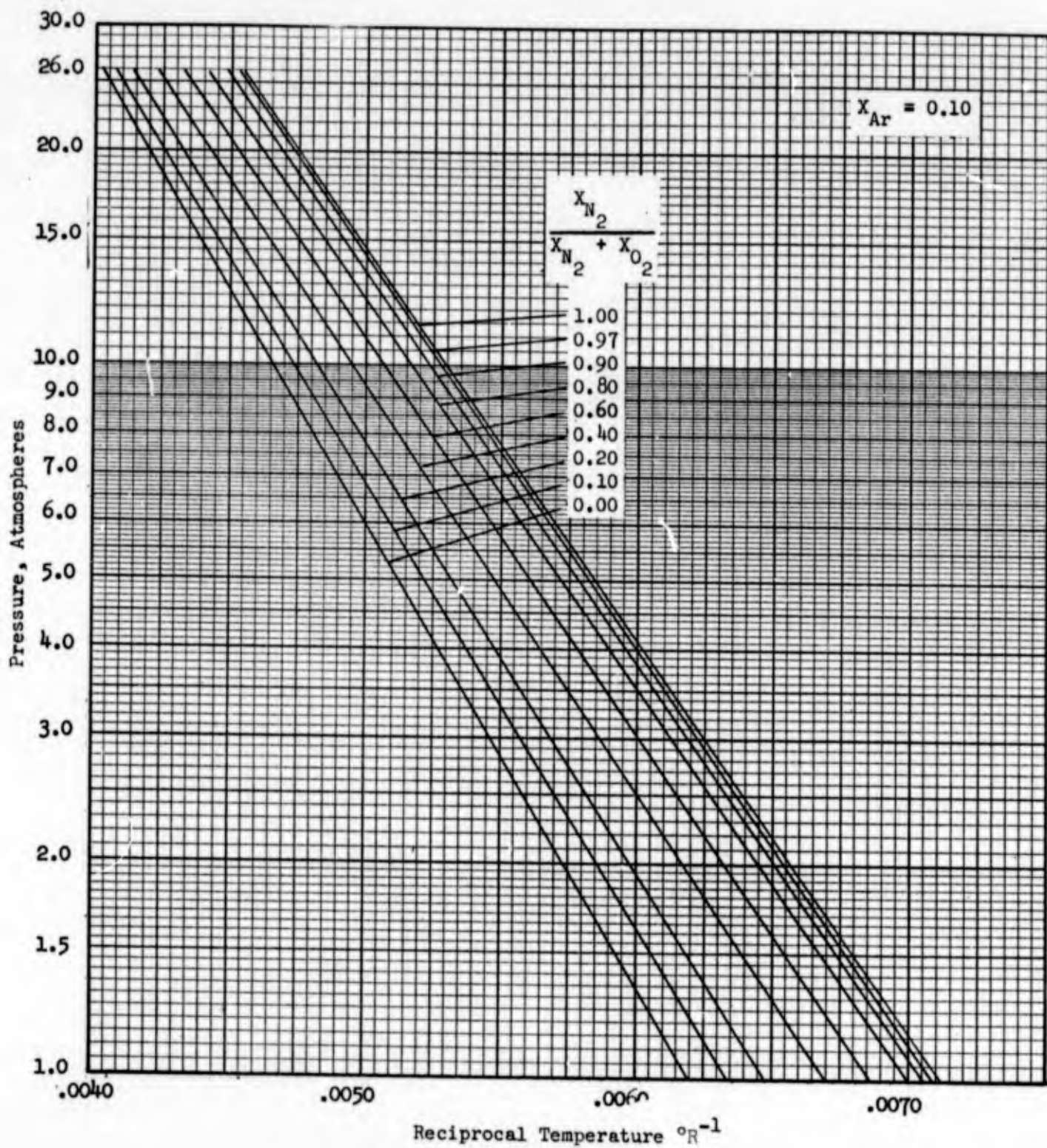


Figure 181. Vapor Pressures of Specific Mixtures of  $N_2$ -Ar- $O_2$ .

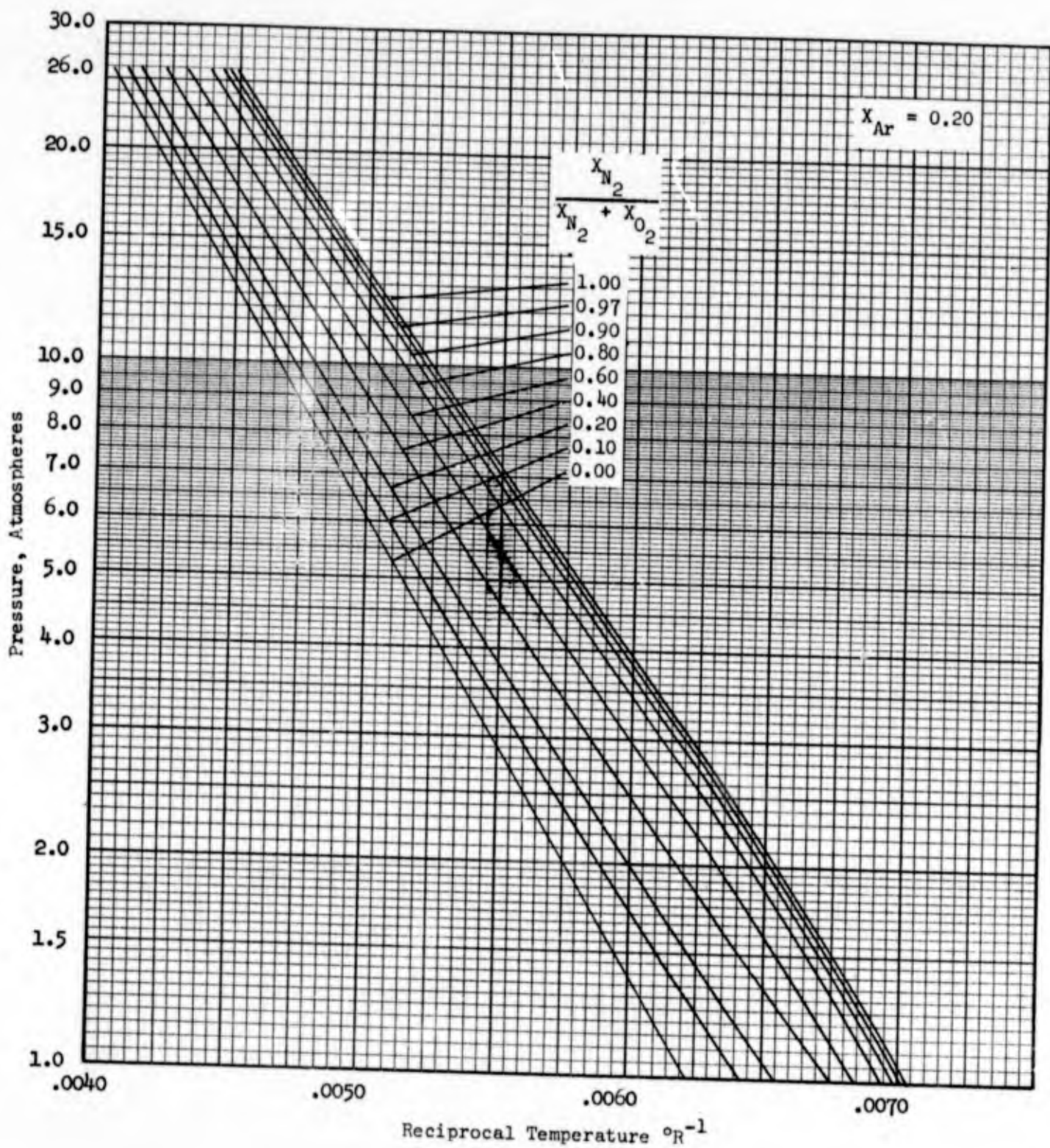


Figure 182. Vapor Pressures of Specific Mixtures of  $N_2$ -Ar- $O_2$ .



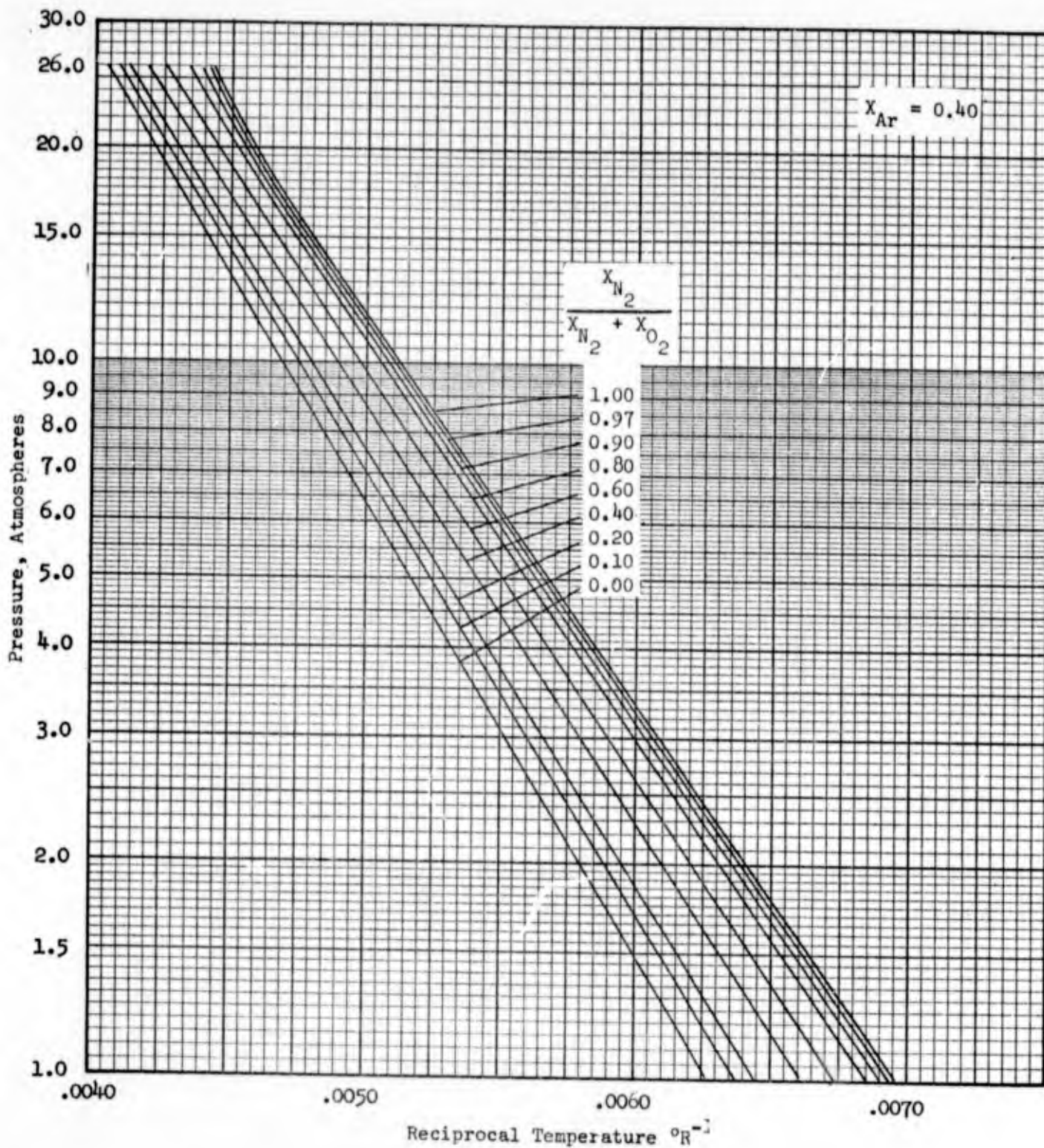


Figure 183. Vapor Pressures of Specific Mixtures of  $N_2$ -Ar- $O_2$ .

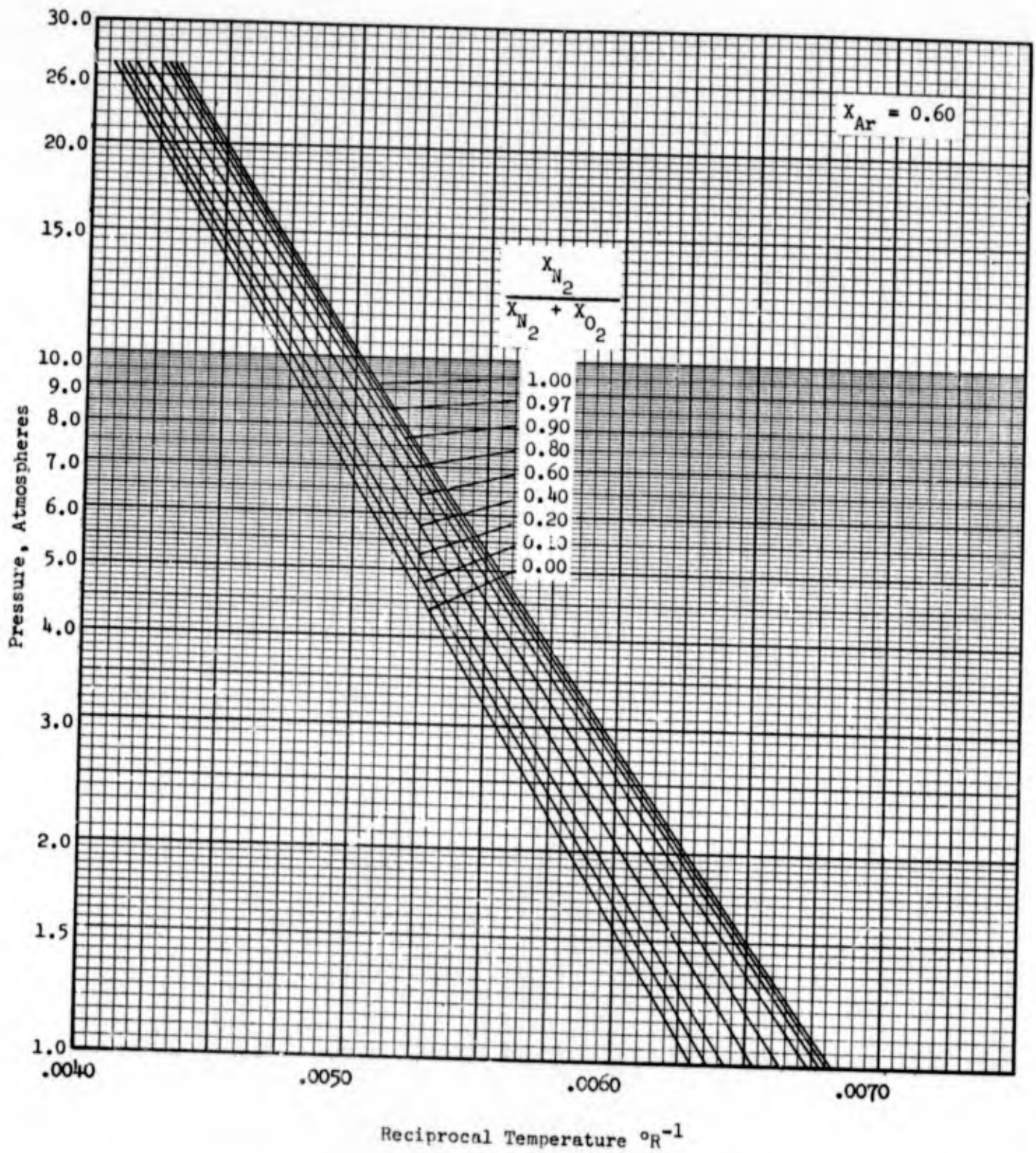


Figure 184. Vapor Pressures of Specific Mixtures of  $N_2$ -Ar- $O_2$ .

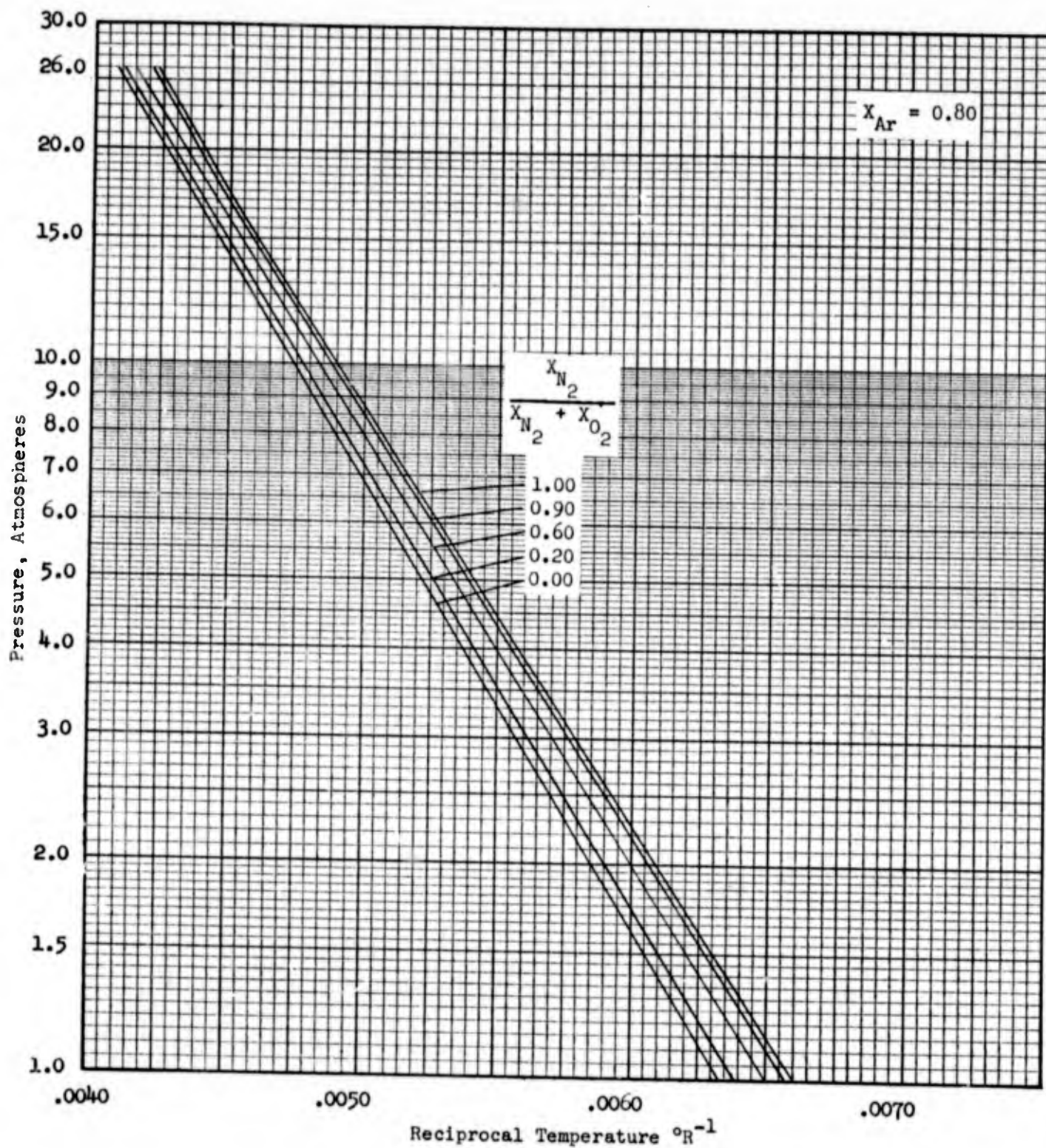


Figure 185. Vapor Pressures of Specific Mixtures of  $N_2$ -Ar- $O_2$ .

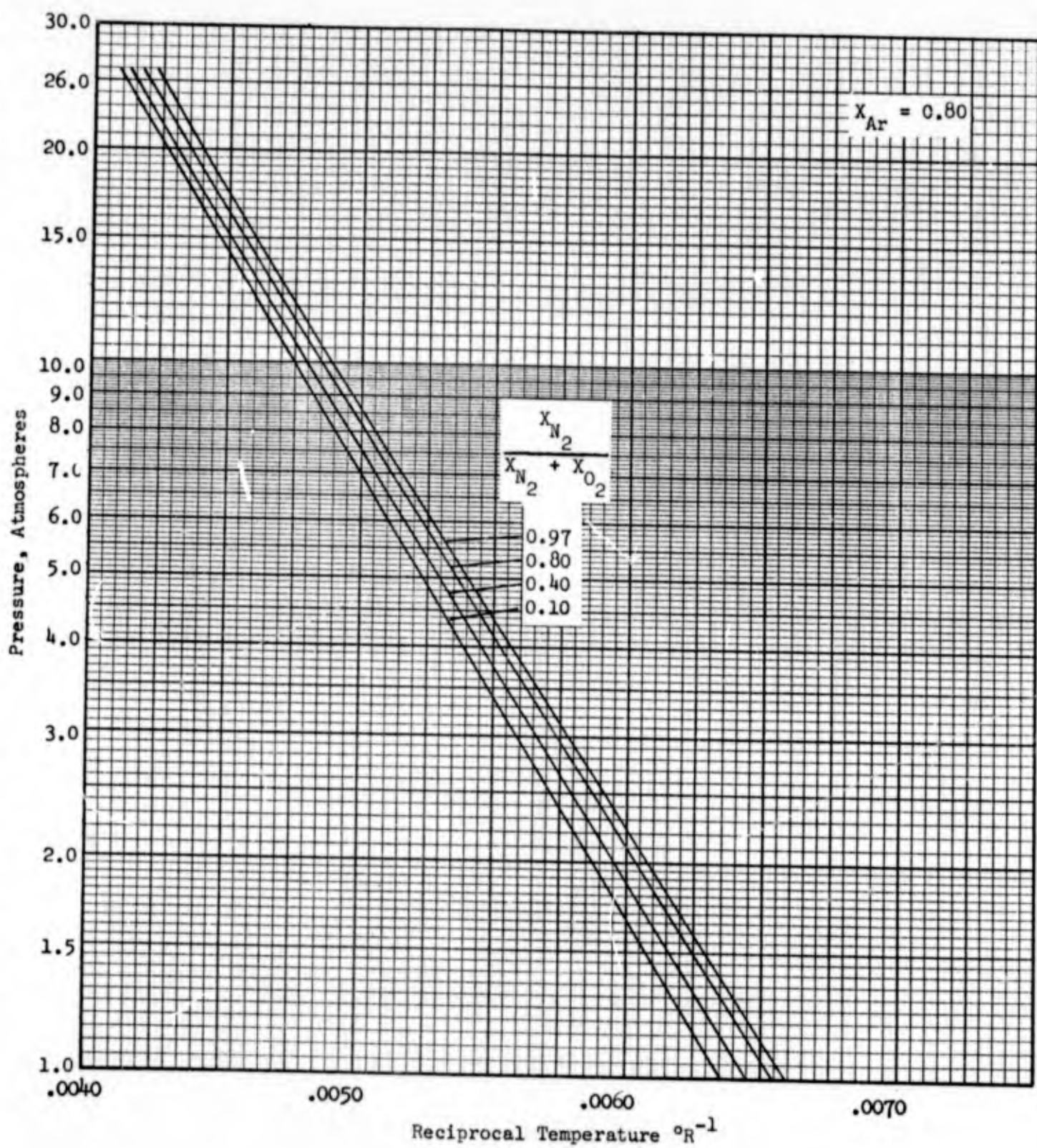


Figure 186. Vapor Pressures of Specific Mixtures of  $N_2$ -Ar- $O_2$ .

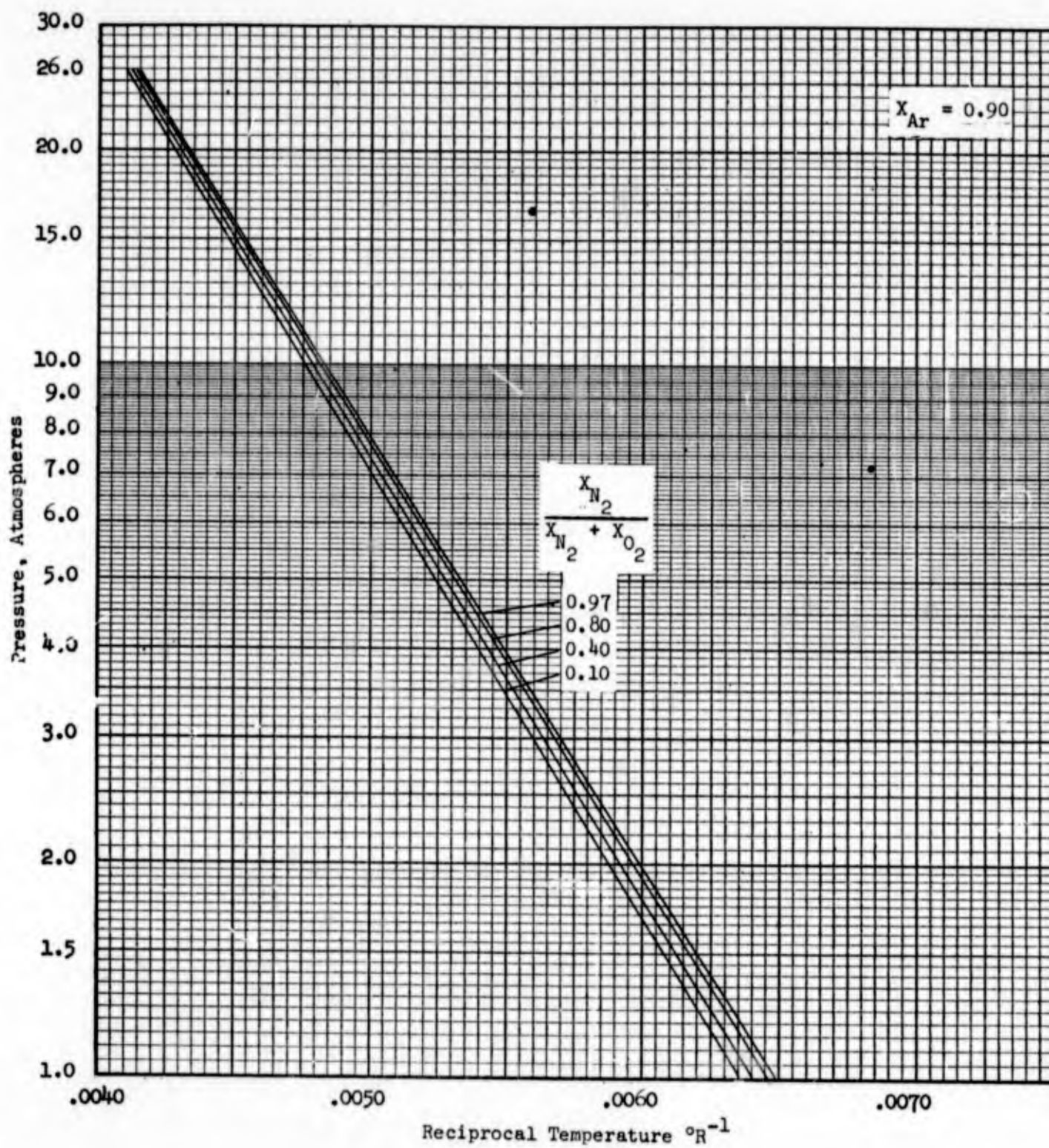


Figure 187. Vapor Pressures of Specific Mixtures of  $N_2$ -Ar- $O_2$ .

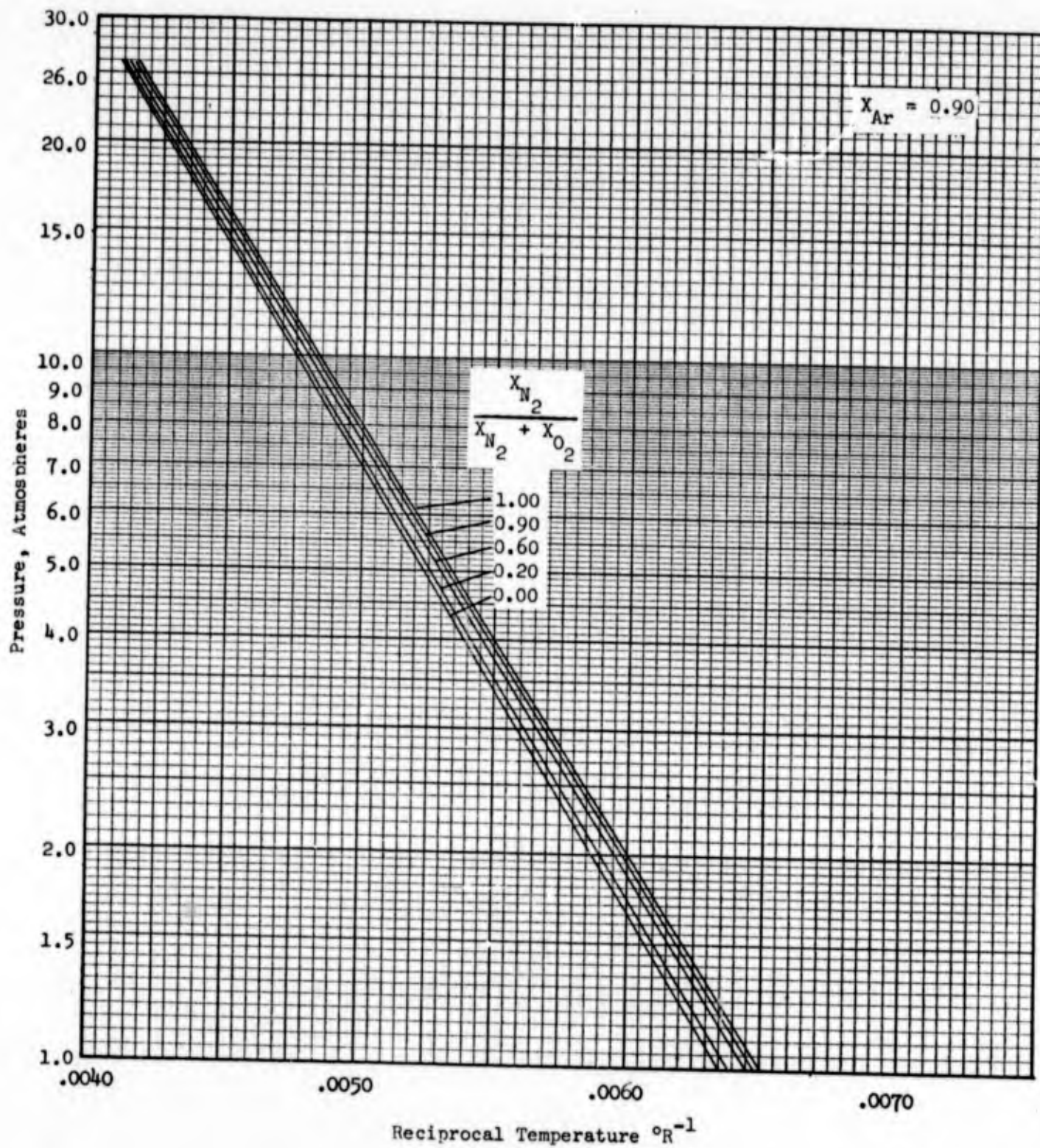


Figure 188. Vapor Pressures of Specific Mixtures of  $N_2$ -Ar- $O_2$ .

## APPENDIX II

## TABULAR PRESENTATION OF CORRELATION

A. Isobaric Table

The table to follow presents values calculated at even pressure levels of 1, 2, 4, 6, 8, 10, 12, 14, 16, 18, 20, 23, and 26 atmospheres. They are arranged in order of increasing liquid mole fraction ratio

$$\frac{N_2}{N_2 + O_2}$$

and sub-ordered according to increasing mole fraction of argon. The quantities calculated are vapor composition, temperature, relative volatility, pressure, activity coefficient, enthalpy, and heat capacity.

Table 25. Isobaric Calculated Values

PRESSURE = 1. ATM.

LIQUID MOLE FRACTION			VAPOR MOLE FRACTION			TEMP	RELATIVE VOL			PRESSURE ACT COEF			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
N <sub>2</sub> /N <sub>2</sub> +O <sub>2</sub>	AR	O <sub>2</sub>	N <sub>2</sub>	AR	O <sub>2</sub>		R	N <sub>2</sub> /AR	N <sub>2</sub> /O <sub>2</sub>	AR/O <sub>2</sub>	N <sub>2</sub>	AR	O <sub>2</sub>	LIQ	VAP	LIQ
0.	0.	0.	0.	0.	1.0000	162.4	2.579	4.010	1.957	1.118	1.169	0.999	-1841.	1893.	13.2	7.486
0.	0.01	0.	0.0194	0.9805	162.3	2.581	4.007	1.953	1.117	1.161	1.000	-1844.	1897.	13.1	7.374	
0.	0.02	0.	0.0388	0.9694	162.2	2.584	4.004	1.948	1.115	1.158	1.000	-1847.	1902.	13.1	7.342	
0.	0.03	0.	0.0582	0.9584	162.1	2.587	4.001	1.944	1.113	1.155	1.000	-1850.	1907.	13.1	7.311	
0.	0.04	0.	0.0776	0.9473	162.0	2.590	3.998	1.940	1.111	1.151	1.001	-1853.	1911.	13.0	7.281	
0.	0.05	0.	0.0970	0.9363	161.9	2.602	3.995	1.935	1.110	1.148	1.001	-1856.	1916.	13.0	7.251	
0.	0.07	0.	0.1358	0.8972	161.7	2.613	3.992	1.926	1.107	1.142	1.002	-1860.	1920.	12.9	7.192	
0.	0.10	0.	0.1746	0.8581	161.5	2.629	3.979	1.913	1.103	1.132	1.003	-1866.	1924.	12.9	7.167	
0.	0.20	0.	0.2837	0.7163	161.7	2.682	3.941	1.869	1.091	1.104	1.010	-1893.	1997.	12.6	6.847	
0.	0.40	0.	0.4796	0.5204	159.4	2.784	3.852	1.802	1.076	1.090	1.024	-1936.	2024.	11.9	6.466	
0.	0.60	0.	0.6625	0.3399	156.5	2.888	3.744	1.727	1.078	1.026	1.072	-1978.	2062.	11.3	6.096	
0.	0.80	0.	0.8293	0.1707	157.7	2.991	3.632	1.614	1.087	1.008	1.127	-2019.	2097.	10.7	5.806	
0.	0.90	0.	0.9134	0.0865	157.9	3.042	3.572	1.574	1.099	1.003	1.162	-2032.	2109.	10.4	5.691	
0.10	0.	0.9135	0.	0.0865	157.7	2.921	4.111	1.968	1.103	1.168	1.018	-1834.	1899.	13.0	7.410	
0.10	0.01	0.3095	0.0119	0.6786	157.6	2.824	4.104	1.963	1.107	1.164	1.012	-1837.	1907.	13.1	7.386	
0.10	0.02	0.3056	0.0237	0.6747	157.4	2.831	4.100	1.958	1.100	1.161	1.012	-1839.	1913.	13.1	7.361	
0.10	0.03	0.3017	0.0354	0.6630	157.6	2.836	4.099	1.954	1.099	1.157	1.013	-1842.	1919.	13.1	7.337	
0.10	0.04	0.2978	0.0470	0.6593	157.4	2.841	4.096	1.949	1.098	1.154	1.013	-1844.	1925.	13.1	7.313	
0.10	0.05	0.2939	0.0585	0.6474	157.5	2.845	4.093	1.944	1.096	1.151	1.013	-1846.	1932.	13.0	7.289	
0.10	0.07	0.2863	0.0812	0.6329	157.9	2.859	4.074	1.934	1.094	1.144	1.014	-1851.	1934.	13.0	7.242	
0.10	0.10	0.2752	0.1145	0.6103	157.4	2.869	4.058	1.920	1.090	1.139	1.015	-1859.	1924.	12.9	7.173	
0.10	0.20	0.2389	0.2247	0.5304	157.2	2.717	4.003	1.873	1.080	1.104	1.022	-1880.	1999.	12.9	6.991	
0.10	0.40	0.1759	0.4176	0.4672	157.0	2.612	3.887	1.803	1.070	1.061	1.049	-1926.	2026.	11.9	6.646	
0.10	0.60	0.1169	0.6036	0.2709	156.9	2.704	3.766	1.724	1.072	1.029	1.082	-1969.	2071.	11.3	6.147	
0.10	0.80	0.0595	0.7933	0.1471	156.9	2.801	3.646	1.613	1.086	1.009	1.134	-2009.	2113.	10.7	5.746	
0.10	0.90	0.0223	0.8937	0.0763	157.1	2.908	3.576	1.573	1.099	1.004	1.166	-2029.	2123.	10.4	5.634	
0.20	0.	0.3095	0.	0.6905	154.0	2.641	4.199	1.973	1.088	1.171	1.026	-1814.	1939.	13.0	7.422	
0.20	0.01	0.3042	0.0096	0.6801	154.0	2.646	4.199	1.968	1.084	1.168	1.026	-1816.	1932.	13.0	7.402	
0.20	0.02	0.2998	0.0192	0.6699	154.0	2.651	4.193	1.963	1.083	1.164	1.026	-1819.	1929.	13.1	7.382	
0.20	0.03	0.2958	0.0288	0.6599	154.1	2.659	4.187	1.958	1.082	1.161	1.027	-1821.	1927.	13.1	7.362	
0.20	0.04	0.2918	0.0383	0.6499	154.1	2.668	4.181	1.953	1.081	1.158	1.027	-1824.	1924.	13.1	7.342	
0.20	0.05	0.2878	0.0477	0.6400	154.1	2.676	4.175	1.948	1.080	1.154	1.027	-1826.	1921.	13.0	7.322	
0.20	0.07	0.2778	0.0666	0.6207	154.1	2.674	4.112	1.938	1.078	1.148	1.028	-1831.	1916.	13.0	7.283	
0.20	0.10	0.2688	0.0946	0.6014	154.2	2.688	4.094	1.923	1.075	1.139	1.030	-1839.	1908.	12.9	7.224	
0.20	0.20	0.2403	0.1806	0.5051	154.3	2.735	4.032	1.874	1.068	1.110	1.036	-1863.	1981.	12.6	7.031	
0.20	0.40	0.2123	0.3606	0.3197	154.8	2.829	3.967	1.801	1.067	1.084	1.055	-1911.	1931.	11.9	6.646	
0.20	0.60	0.2162	0.5598	0.2200	155.4	2.921	3.779	1.729	1.080	1.032	1.093	-1959.	1977.	11.3	6.292	
0.20	0.80	0.2144	0.7602	0.1254	156.2	3.009	3.647	1.612	1.086	1.011	1.146	-2004.	2019.	10.7	5.917	
0.20	0.90	0.2093	0.8744	0.0663	156.7	3.092	3.588	1.573	1.099	1.004	1.180	-2024.	2027.	10.4	5.824	
0.40	0.	0.7279	0.	0.2721	148.7	2.629	4.194	1.969	1.095	1.167	1.005	-1748.	1977.	13.2	7.422	
0.40	0.01	0.7226	0.0076	0.2625	148.8	2.634	4.119	1.964	1.049	1.163	1.005	-1751.	1976.	13.2	7.427	
0.40	0.02	0.7172	0.0151	0.2529	148.8	2.648	4.114	1.959	1.049	1.179	1.005	-1754.	1974.	13.2	7.437	
0.40	0.03	0.7118	0.0226	0.2432	148.9	2.659	4.108	1.953	1.048	1.176	1.006	-1757.	1972.	13.2	7.437	
0.40	0.04	0.7064	0.0300	0.2336	148.9	2.668	4.103	1.948	1.048	1.172	1.006	-1760.	1971.	13.2	7.432	
0.40	0.05	0.7010	0.0374	0.2240	149.0	2.676	4.098	1.943	1.047	1.169	1.006	-1763.	1969.	13.1	7.377	
0.40	0.07	0.6956	0.0491	0.2093	149.1	2.687	4.087	1.933	1.047	1.162	1.006	-1773.	1966.	13.1	7.347	
0.40	0.10	0.6794	0.0703	0.1903	149.3	2.683	4.072	1.917	1.046	1.152	1.007	-1779.	1961.	13.0	7.301	
0.40	0.20	0.6244	0.1426	0.2331	149.9	2.737	4.010	1.868	1.044	1.122	1.071	-1819.	1964.	12.6	7.149	
0.40	0.40	0.5675	0.2977	0.1948	151.2	2.841	3.967	1.775	1.040	1.074	1.088	-1871.	1920.	11.9	6.811	
0.40	0.60	0.5743	0.4776	0.1402	152.0	2.930	3.788	1.689	1.042	1.039	1.116	-1932.	1895.	11.3	6.423	
0.40	0.80	0.5121	0.7010	0.0878	154.0	3.025	3.657	1.629	1.064	1.016	1.154	-1991.	1829.	10.7	5.944	
0.40	0.90	0.4393	0.8782	0.0777	155.9	3.092	3.586	1.574	1.099	1.008	1.177	-2024.	1794.	10.4	5.691	
0.60	0.	0.8048	0.	0.1952	144.0	2.679	3.993	1.991	1.084	1.161	1.026	-1863.	1976.	13.0	7.483	
0.60	0.01	0.8021	0.0096	0.1856	144.0	2.682	3.991	1.986	1.084	1.214	1.029	-1867.	1969.	13.0	7.471	
0.60	0.02	0.8021	0.0111	0.1816	144.1	2.689	3.986	1.981	1.084	1.210	1.029	-1872.	1968.	13.0	7.459	
0.60	0.03	0.8024	0.0167	0.1769	144.1	2.699	3.980	1.976	1.084	1.204	1.024	-1876.	1967.	13.0	7.446	
0.60	0.04	0.8029	0.0224	0.1722	144.2	2.708	3.975	1.971	1.084	1.202	1.024	-1880.	1966.	13.0	7.434	
0.60	0.05	0.8034	0.0280	0.1675	144.3	2.719	3.969	1.966	1.083	1.198	1.023	-1884.	1965.	13.0	7.421	
0.60	0.07	0.8047	0.0394	0.1580	144.5	2.729	3.979	1.916	1.083	1.190	1.023	-1892.	1963.	13.0	7.396	
0.60	0.10	0.8076	0.0566	0.1397	144.7	2.742	3.966	1.901	1.083	1.179	1.021	-1904.	1960.	12.9	7.357	
0.60	0.20	0.7957	0.1183	0.1990	146.5	2.787	3.937	1.854	1.079	1.148	1.020	-1944.	1948.	12.6	7.224	
0.60	0.40	0.7391	0.2907	0.1102	148.4	2.835	3.867	1.805	1.076	1.099	1.020	-1924.	1923.	12.6	6.926	
0.60	0.60	0.6920	0.4191	0.0871	150.6	2.949	3.777	1.723	1.074	1.049	1.043	-1973.	1888.	11.3	6.596	
0.60	0.80	0.6451	0.6900	0.0539	153.9	3.037	3.660	1.646	1.083	1.021	1.109	-2016.	1837.	10.7	6.259	
0.60	0.90	0.5982	0.8647	0.0367	158.2	3.071	3.592	1.578	1.099	1.013	1.180	-2044.	1801.	10.4	5.723	
0.80	0.	0.9284	0.	0.0716	142.0	2.761	3.811	1.984	1.013	1.273	1.014	-1876.	1949.	14.0	7.914	
0.80	0.01	0.9246	0.0047	0.0613	142.0	2.769	3.811	1.979	1.013	1.268	1.018	-1879.	1946.	13.9	7.903	
0.80	0.02	0.9208	0.0094	0.0513	142.1	2.777	3.812	1.973	1.013	1.263	1.018	-1882.	1947.	13.9	7.892	
0.80	0.03	0.9222	0.0142	0.0417	142.2	2.785	3.812	1.968	1.013	1.257	1.019	-1885.	1947.	13.8	7.881	
0.80	0.04	0.9237	0.0189	0.0324	142.3	2.793	3.813	1.963	1.013	1.252	1.019	-1888.	1946.	13.8	7.870	
0.80	0.05	0.9162	0.0237	0.0231	142.4	2.804	3.813	1.958	1.013	1.247	1.019	-1891.	1945.	13.7	7.859	
0.80	0.07	0.9071	0.0334	0.0139	142.6	2.816	3.814	1.952	1.012	1.238	1.019	-1896.	1944.	13.6	7.837	
0.80	0.10	0.8934	0.0481	0.0044	142.8	2.828	3.814	1.947	1.012	1.224	1.017	-1901.	1943.	13.5	7.803	
0.80	0.20	0.8452	0.0994	0.0594	143.0	2.859	3.814	1.939	1.019	1.191	1.018	-1911.	1941.	13.4	7.763	
0.80	0.40	0.7239	0.													



Table 20. (cont.)

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION			TEMP	RELATIVE VOL			PRESSURE ACT COEF			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
N2/N2+O2	AR	N2	AR	O2		R	N2/AR	N2/O2	AR/O2	N2	A	O2	L10	VAP	L10
0.	0.	0.	0.	1.0000	175.3	2.307	3.368	1.460	1.002	1.136	0.999	-1670.	1159.	13.3	7.664
0.	0.01	0.	0.	0.0145	0.9855	175.2	2.311	3.365	1.456	1.000	1.133	-1673.	1154.	13.3	7.634
0.	0.02	0.	0.	0.0288	0.9712	175.1	2.315	3.363	1.452	1.000	1.130	-1677.	1148.	13.2	7.604
0.	0.03	0.	0.	0.0429	0.9571	175.0	2.320	3.361	1.449	1.000	1.127	-1680.	1143.	13.1	7.575
0.	0.04	0.	0.	0.0568	0.9432	174.9	2.324	3.358	1.445	1.000	1.125	-1683.	1137.	13.1	7.546
0.	0.05	0.	0.	0.0705	0.9295	174.8	2.329	3.356	1.441	1.000	1.122	-1686.	1132.	13.1	7.517
0.	0.07	0.	0.	0.0974	0.9026	174.6	2.337	3.351	1.434	1.000	1.116	-1692.	1122.	13.1	7.461
0.	0.10	0.	0.	0.1345	0.8639	174.4	2.350	3.343	1.422	1.000	1.109	-1701.	1107.	13.0	7.379
0.	0.20	0.	0.	0.2572	0.7428	173.6	2.392	3.313	1.385	1.040	1.004	-1730.	1061.	12.8	7.126
0.	0.40	0.	0.	0.4663	0.5337	172.3	2.474	3.242	1.310	1.029	1.045	-1782.	983.	12.3	6.667
0.	0.60	0.	0.	0.6499	0.3901	171.4	2.593	3.160	1.237	1.027	1.017	-1830.	916.	11.7	6.299
0.	0.80	0.	0.	0.8235	0.1765	170.6	2.632	3.070	1.166	1.034	1.001	-1873.	854.	11.2	5.930
0.	0.90	0.	0.	0.9106	0.0894	170.4	2.671	3.022	1.132	1.047	0.997	-1894.	824.	10.9	5.740
0.10	0.	0.2764	0.	0.	0.7236	170.7	2.353	3.438	1.461	1.057	1.139	-1661.	1127.	13.4	7.678
0.10	0.01	0.2730	0.0117	0.7154	170.7	2.357	3.434	1.457	1.055	1.137	1.015	-1664.	1123.	13.4	7.653
0.10	0.02	0.2696	0.0233	0.7072	170.6	2.361	3.430	1.453	1.054	1.134	1.015	-1667.	1119.	13.3	7.629
0.10	0.03	0.2662	0.0348	0.6991	170.6	2.365	3.427	1.449	1.053	1.131	1.016	-1670.	1115.	13.3	7.605
0.10	0.04	0.2628	0.0462	0.6910	170.6	2.369	3.424	1.445	1.052	1.128	1.016	-1672.	1111.	13.3	7.581
0.10	0.05	0.2594	0.0576	0.6831	170.6	2.372	3.421	1.441	1.051	1.125	1.016	-1675.	1107.	13.3	7.558
0.10	0.07	0.2529	0.0800	0.6673	170.4	2.380	3.410	1.433	1.048	1.120	1.017	-1680.	1099.	13.2	7.511
0.10	0.10	0.2431	0.1130	0.6439	170.4	2.391	3.398	1.421	1.049	1.112	1.019	-1689.	1080.	13.1	7.441
0.10	0.20	0.2122	0.2185	0.5692	170.2	2.428	3.356	1.382	1.036	1.087	1.025	-1717.	1052.	12.8	7.219
0.10	0.40	0.1557	0.4192	0.4201	169.9	2.501	3.266	1.306	1.027	1.047	1.046	-1778.	985.	12.3	6.803
0.10	0.60	0.1034	0.6032	0.2934	169.8	2.572	3.173	1.234	1.027	1.020	1.078	-1820.	922.	11.7	6.403
0.10	0.80	0.0324	0.7941	0.1535	169.9	2.642	3.075	1.164	1.034	1.003	1.124	-1868.	860.	11.2	6.056
0.10	0.90	0.0266	0.8943	0.0791	170.0	2.676	3.025	1.130	1.048	0.998	1.152	-1891.	827.	10.9	5.780
0.20	0.	0.4844	0.	0.5156	167.0	2.380	3.460	1.457	1.045	1.143	1.032	-1641.	1101.	13.5	7.695
0.20	0.01	0.4996	0.0097	0.5307	167.0	2.384	3.464	1.453	1.045	1.140	1.032	-1644.	1098.	13.4	7.677
0.20	0.02	0.4948	0.0194	0.5259	167.0	2.387	3.460	1.449	1.044	1.137	1.032	-1647.	1095.	13.4	7.657
0.20	0.03	0.4499	0.0291	0.5210	167.0	2.391	3.455	1.445	1.043	1.134	1.033	-1650.	1092.	13.4	7.636
0.20	0.04	0.4452	0.0387	0.5161	167.0	2.394	3.450	1.441	1.042	1.131	1.033	-1653.	1089.	13.3	7.616
0.20	0.05	0.4404	0.0483	0.5113	167.0	2.398	3.446	1.437	1.041	1.128	1.033	-1656.	1086.	13.3	7.594
0.20	0.07	0.4359	0.0674	0.5016	167.1	2.405	3.436	1.429	1.039	1.123	1.034	-1661.	1080.	13.3	7.559
0.20	0.10	0.4169	0.0959	0.4873	167.1	2.416	3.422	1.417	1.037	1.119	1.035	-1670.	1071.	13.2	7.495
0.20	0.20	0.3710	0.1802	0.4397	167.3	2.451	3.375	1.377	1.030	1.090	1.041	-1698.	1042.	12.9	7.296
0.20	0.40	0.2823	0.3734	0.3444	167.7	2.520	3.270	1.301	1.023	1.050	1.060	-1754.	985.	12.3	6.902
0.20	0.60	0.1939	0.5622	0.2439	168.4	2.587	3.180	1.229	1.024	1.022	1.090	-1809.	927.	11.7	6.496
0.20	0.80	0.1016	0.7665	0.1320	169.1	2.651	3.079	1.162	1.039	1.005	1.131	-1862.	865.	11.2	6.056
0.20	0.90	0.0323	0.8785	0.0692	169.6	2.681	3.027	1.129	1.048	0.999	1.156	-1888.	831.	10.9	5.814
0.40	0.	0.6964	0.	0.3036	161.3	2.380	3.441	1.441	1.021	1.154	1.075	-1578.	1061.	13.9	7.747
0.40	0.01	0.6911	0.0073	0.3016	161.4	2.393	3.437	1.437	1.020	1.151	1.074	-1582.	1059.	13.9	7.731
0.40	0.02	0.6858	0.0146	0.2996	161.5	2.397	3.433	1.433	1.020	1.148	1.074	-1585.	1057.	13.9	7.714
0.40	0.03	0.6805	0.0219	0.2976	161.5	2.401	3.429	1.429	1.019	1.145	1.075	-1588.	1055.	13.9	7.698
0.40	0.04	0.6751	0.0292	0.2956	161.6	2.405	3.425	1.425	1.019	1.142	1.075	-1592.	1053.	13.4	7.682
0.40	0.05	0.6698	0.0366	0.2936	161.6	2.409	3.421	1.421	1.018	1.139	1.075	-1596.	1051.	13.4	7.666
0.40	0.07	0.6591	0.0513	0.2896	161.8	2.417	3.413	1.412	1.017	1.134	1.075	-1603.	1048.	13.3	7.633
0.40	0.10	0.6429	0.0735	0.2839	162.0	2.429	3.401	1.401	1.016	1.129	1.075	-1613.	1042.	13.2	7.584
0.40	0.20	0.5883	0.1490	0.2626	162.6	2.468	3.360	1.362	1.014	1.100	1.079	-1648.	1023.	12.9	7.410
0.40	0.40	0.4731	0.3102	0.2167	164.1	2.542	3.279	1.288	1.015	1.059	1.092	-1716.	982.	12.3	7.051
0.40	0.60	0.3438	0.4942	0.1620	165.7	2.609	3.193	1.220	1.024	1.029	1.114	-1784.	933.	11.7	6.656
0.40	0.80	0.1910	0.7162	0.0929	167.7	2.666	3.084	1.157	1.039	1.008	1.145	-1858.	874.	11.2	6.189
0.40	0.90	0.1014	0.8884	0.0362	168.9	2.690	3.030	1.127	1.049	1.001	1.163	-1881.	837.	10.9	5.901
0.60	0.	0.8536	0.	0.1464	157.2	2.359	3.338	1.415	1.000	1.160	1.135	-1497.	1031.	13.6	7.797
0.60	0.01	0.8286	0.0059	0.1656	157.3	2.364	3.336	1.411	1.000	1.157	1.134	-1499.	1031.	13.6	7.781
0.60	0.02	0.8236	0.0118	0.1647	157.4	2.368	3.334	1.408	1.000	1.154	1.134	-1501.	1029.	13.6	7.764
0.60	0.03	0.8185	0.0178	0.1638	157.5	2.374	3.332	1.404	1.000	1.151	1.133	-1505.	1028.	13.6	7.748
0.60	0.04	0.8134	0.0237	0.1629	157.6	2.379	3.330	1.400	0.999	1.148	1.133	-1510.	1027.	13.9	7.755
0.60	0.05	0.8083	0.0297	0.1619	157.6	2.383	3.328	1.396	0.999	1.145	1.133	-1514.	1026.	13.9	7.741
0.60	0.07	0.7981	0.0418	0.1601	157.8	2.393	3.324	1.389	0.999	1.142	1.132	-1519.	1024.	13.9	7.728
0.60	0.10	0.7826	0.0602	0.1573	158.1	2.400	3.317	1.378	0.999	1.139	1.131	-1527.	1022.	13.4	7.700
0.60	0.20	0.7289	0.1237	0.1475	159.0	2.456	3.294	1.341	1.000	1.110	1.120	-1540.	1010.	13.3	7.657
0.60	0.40	0.6089	0.2658	0.1293	161.0	2.545	3.241	1.273	1.000	1.100	1.120	-1584.	1005.	13.1	7.510
0.60	0.60	0.4622	0.4407	0.0971	163.4	2.622	3.172	1.210	1.007	1.072	1.130	-1671.	975.	12.3	7.183
0.60	0.80	0.2699	0.6717	0.0583	166.4	2.679	3.085	1.152	1.021	1.037	1.141	-1755.	936.	11.7	6.786
0.60	0.90	0.1475	0.8201	0.0324	168.2	2.698	3.033	1.124	1.039	1.013	1.160	-1837.	880.	11.2	6.270
0.80	0.	0.9274	0.	0.0726	154.0	2.366	3.192	1.384	1.000	1.064	1.171	-1676.	1042.	13.9	8.044
0.80	0.01	0.9227	0.0050	0.0723	154.0	2.363	3.192	1.380	0.999	1.061	1.170	-1679.	1040.	13.8	7.985
0.80	0.02	0.9180	0.0101	0.0719	154.1	2.369	3.193	1.377	0.999	1.058	1.170	-1682.	1038.	13.7	7.933
0.80	0.03	0.9133	0.0152	0.0715	154.2	2.375	3.193	1.374	0.999	1.055	1.170	-1685.	1036.	13.7	7.881
0.80	0.04	0.9086	0.0203	0.0711	154.3	2.381	3.194	1.370	0.999	1.052	1.170	-1689.	1034.	13.7	7.830
0.80	0.05	0.9038	0.0254	0.0707	154.4	2.387	3.194	1.367	0.999	1.049	1.170	-1693.	1032.	13.6	7.780
0.80	0.07	0.8942	0.0398	0.0700	154.6	2.399	3.189	1.360	0.999	1.046	1.170	-1700.	1029.	13.6	7.730
0.80	0.10	0.8796	0.0516	0.0688	154.9	2.407	3.185	1.350	0.999	1.043	1.170	-1708.	1026.	13.9	7.758
0.80	0.20	0.8285	0.1067	0.0648	156.0	2.426	3.196	1.350	0.999	1.040	1.204	-1459.	990.	13.4	7.719
0.80	0.40	0.7106	0.2336	0.0590	158.4	2.535	3.184	1.317	0.992	1.140	1.191	-1513.	989.	13.8	7.509
0.80	0.60	0.5976	0.3941	0.0443	16										

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION			TEMP	RELATIVE VOL			PRESSURE ACT COEF			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LR MOLE-R	
N2/N2+O2	AR	N2	AR	O2		R	N2/AR	N2/O2	AR/O2	N2	AR	O2	LIO	VAP	LIO
0.	0.	0.	0.	1.0000	190.6	2.020	2.776	1.375	0.981	1.111	1.000	-1466.	1224.	13.4	8.122
0.	0.01	0.	0.	0.0137	190.5	2.023	2.775	1.372	0.986	1.109	1.001	-1470.	1218.	13.4	8.694
0.	0.02	0.	0.	0.0272	190.4	2.026	2.773	1.369	0.985	1.106	1.001	-1473.	1212.	13.4	8.665
0.	0.03	0.	0.	0.0405	190.3	2.030	2.772	1.366	0.985	1.104	1.002	-1477.	1207.	13.4	8.637
0.	0.04	0.	0.	0.0537	190.2	2.033	2.770	1.362	0.984	1.102	1.002	-1480.	1201.	13.4	8.610
0.	0.05	0.	0.	0.0668	190.1	2.037	2.768	1.359	0.983	1.100	1.003	-1484.	1196.	13.3	7.982
0.	0.07	0.	0.	0.0924	189.9	2.043	2.765	1.353	0.982	1.096	1.004	-1489.	1191.	13.3	7.959
0.	0.10	0.	0.	0.1299	189.6	2.053	2.759	1.344	0.980	1.089	1.005	-1500.	1185.	13.3	7.950
0.	0.20	0.	0.	0.2471	188.8	2.084	2.738	1.313	0.974	1.070	1.013	-1533.	1121.	13.1	7.605
0.	0.40	0.	0.	0.4548	187.5	2.148	2.688	1.251	0.967	1.038	1.034	-1593.	1037.	12.7	7.166
0.	0.60	0.	0.	0.6410	186.5	2.207	2.627	1.190	0.967	1.016	1.066	-1647.	964.	12.3	6.771
0.	0.80	0.	0.	0.8190	185.8	2.264	2.560	1.131	0.976	1.003	1.110	-1698.	896.	11.9	6.389
0.	0.90	0.	0.	0.9044	185.5	2.292	2.524	1.101	0.983	1.000	1.137	-1723.	862.	11.8	6.196
0.10	0.	0.2393	0.	0.7407	186.2	2.063	2.831	1.372	0.994	1.120	1.020	-1452.	1193.	13.7	8.150
0.10	0.01	0.2363	0.0116	0.7521	186.1	2.066	2.828	1.369	0.994	1.117	1.021	-1455.	1188.	13.6	8.126
0.10	0.02	0.2334	0.0230	0.7434	186.1	2.069	2.825	1.365	0.993	1.115	1.021	-1459.	1184.	13.6	8.102
0.10	0.03	0.2305	0.0344	0.7351	186.0	2.072	2.822	1.362	0.992	1.113	1.021	-1462.	1180.	13.6	8.078
0.10	0.04	0.2277	0.0457	0.7267	186.0	2.075	2.820	1.359	0.991	1.110	1.022	-1465.	1175.	13.6	8.054
0.10	0.05	0.2248	0.0569	0.7183	186.0	2.078	2.817	1.356	0.990	1.108	1.022	-1469.	1171.	13.5	8.031
0.10	0.07	0.2192	0.0792	0.7017	185.9	2.083	2.811	1.349	0.988	1.105	1.023	-1479.	1163.	13.5	7.984
0.10	0.10	0.2109	0.1120	0.6772	185.8	2.092	2.802	1.340	0.986	1.097	1.024	-1489.	1155.	13.4	7.915
0.10	0.20	0.1843	0.2174	0.5983	185.5	2.119	2.772	1.308	0.979	1.077	1.030	-1517.	1118.	13.2	7.691
0.10	0.40	0.1353	0.4150	0.4497	185.2	2.173	2.707	1.246	0.971	1.044	1.049	-1578.	1037.	12.8	7.269
0.10	0.60	0.0896	0.6045	0.3054	185.0	2.224	2.638	1.186	0.971	1.020	1.078	-1637.	968.	12.4	6.846
0.10	0.80	0.0492	0.7961	0.1588	185.1	2.273	2.564	1.129	0.978	1.008	1.117	-1693.	900.	12.0	6.444
0.10	0.90	0.0229	0.8957	0.0814	185.2	2.294	2.526	1.100	0.985	1.002	1.141	-1720.	865.	11.8	6.246
0.20	0.	0.4170	0.	0.5831	182.4	2.094	2.861	1.366	0.997	1.128	1.041	-1431.	1166.	13.8	8.119
0.20	0.01	0.4126	0.0099	0.5776	182.4	2.097	2.857	1.363	0.996	1.125	1.041	-1434.	1162.	13.8	8.104
0.20	0.02	0.4082	0.0198	0.5721	182.4	2.100	2.854	1.359	0.995	1.123	1.042	-1438.	1159.	13.8	8.146
0.20	0.03	0.4038	0.0297	0.5666	182.4	2.102	2.851	1.356	0.994	1.120	1.042	-1441.	1155.	13.8	8.125
0.20	0.04	0.3994	0.0395	0.5611	182.4	2.105	2.847	1.353	0.993	1.118	1.042	-1445.	1152.	13.7	8.104
0.20	0.05	0.3951	0.0493	0.5557	182.4	2.107	2.844	1.349	0.992	1.116	1.042	-1448.	1149.	13.7	8.083
0.20	0.07	0.3864	0.0688	0.5444	182.4	2.112	2.837	1.343	0.990	1.113	1.043	-1455.	1142.	13.7	8.041
0.20	0.10	0.3735	0.0979	0.5286	182.5	2.120	2.827	1.333	0.988	1.104	1.044	-1465.	1132.	13.6	7.978
0.20	0.20	0.3316	0.1932	0.4752	182.6	2.145	2.792	1.301	0.982	1.083	1.049	-1498.	1099.	13.3	7.771
0.20	0.40	0.2566	0.3868	0.3686	183.0	2.194	2.720	1.240	0.974	1.049	1.065	-1562.	1035.	12.9	7.363
0.20	0.60	0.1760	0.5714	0.2588	183.6	2.239	2.645	1.181	0.974	1.024	1.090	-1625.	971.	12.4	6.944
0.20	0.80	0.0883	0.7742	0.1376	184.3	2.291	2.568	1.126	0.980	1.008	1.124	-1687.	904.	12.0	6.497
0.20	0.90	0.0452	0.8834	0.0715	184.8	2.361	2.529	1.099	0.986	1.003	1.145	-1717.	867.	11.8	6.255
0.40	0.	0.6560	0.	0.3441	176.3	2.124	2.890	1.346	0.992	1.146	1.090	-1372.	1121.	14.1	8.277
0.40	0.01	0.6506	0.0077	0.3417	176.4	2.127	2.886	1.343	0.991	1.143	1.090	-1376.	1119.	14.0	8.266
0.40	0.02	0.6453	0.0155	0.3393	176.4	2.129	2.883	1.340	0.991	1.140	1.090	-1380.	1117.	14.0	8.242
0.40	0.03	0.6400	0.0232	0.3369	176.5	2.132	2.880	1.337	0.990	1.138	1.090	-1384.	1115.	14.0	8.224
0.40	0.04	0.6347	0.0310	0.3345	176.5	2.135	2.876	1.333	0.990	1.135	1.090	-1387.	1112.	13.9	8.206
0.40	0.05	0.6293	0.0387	0.3321	176.6	2.137	2.873	1.330	0.989	1.133	1.090	-1391.	1110.	13.9	8.188
0.40	0.07	0.6186	0.0543	0.3271	176.8	2.143	2.857	1.324	0.988	1.128	1.090	-1399.	1108.	13.9	8.153
0.40	0.10	0.6025	0.0778	0.3197	177.0	2.151	2.827	1.315	0.986	1.120	1.090	-1410.	1099.	13.8	8.098
0.40	0.20	0.5482	0.1575	0.2943	177.7	2.176	2.794	1.284	0.982	1.098	1.091	-1449.	1077.	13.5	7.915
0.40	0.40	0.4348	0.3259	0.2393	179.2	2.223	2.725	1.226	0.979	1.061	1.100	-1529.	1029.	13.0	7.527
0.40	0.60	0.3104	0.5141	0.1756	180.9	2.264	2.652	1.171	0.979	1.033	1.110	-1600.	975.	12.5	7.095
0.40	0.80	0.1684	0.7334	0.0942	182.9	2.297	2.573	1.120	0.985	1.013	1.139	-1674.	915.	12.0	6.597
0.40	0.90	0.0882	0.8595	0.0523	184.1	2.369	2.531	1.096	0.989	1.006	1.163	-1718.	872.	11.8	6.312
0.60	0.	0.8076	0.	0.1924	171.7	2.120	2.798	1.320	0.986	1.173	1.194	-1296.	1086.	14.2	8.369
0.60	0.01	0.8023	0.0064	0.1913	171.8	2.123	2.796	1.317	0.986	1.170	1.193	-1301.	1084.	14.2	8.354
0.60	0.02	0.7971	0.0127	0.1902	171.9	2.127	2.794	1.314	0.985	1.167	1.192	-1305.	1083.	14.1	8.338
0.60	0.03	0.7918	0.0192	0.1891	172.0	2.130	2.792	1.311	0.985	1.164	1.192	-1310.	1082.	14.1	8.322
0.60	0.04	0.7865	0.0256	0.1879	172.1	2.133	2.790	1.308	0.985	1.161	1.191	-1315.	1080.	14.1	8.306
0.60	0.05	0.7812	0.0321	0.1868	172.2	2.137	2.788	1.305	0.984	1.159	1.190	-1319.	1079.	14.0	8.289
0.60	0.07	0.7704	0.0451	0.1845	172.4	2.143	2.784	1.299	0.984	1.153	1.189	-1329.	1076.	14.0	8.257
0.60	0.10	0.7542	0.0649	0.1810	172.6	2.153	2.778	1.290	0.983	1.144	1.188	-1343.	1072.	13.9	8.208
0.60	0.20	0.6808	0.1332	0.1684	173.7	2.184	2.747	1.262	0.981	1.119	1.183	-1389.	1056.	13.6	8.038
0.60	0.40	0.5739	0.2848	0.1413	175.9	2.239	2.708	1.209	0.980	1.076	1.181	-1482.	1021.	13.0	7.866
0.60	0.60	0.4261	0.4667	0.1073	178.5	2.283	2.648	1.160	0.984	1.043	1.185	-1573.	976.	12.5	7.228
0.60	0.80	0.2413	0.6943	0.0629	181.6	2.317	2.574	1.115	0.989	1.019	1.195	-1661.	916.	12.0	6.690
0.60	0.90	0.1293	0.8347	0.0340	183.4	2.317	2.533	1.093	0.992	1.009	1.201	-1734.	876.	11.8	6.367
0.80	0.	0.9152	0.	0.0848	168.0	2.095	2.699	1.288	0.986	1.216	1.239	-1109.	1057.	14.3	8.462
0.80	0.01	0.9102	0.0095	0.0843	168.1	2.099	2.699	1.286	0.986	1.212	1.237	-1115.	1056.	14.2	8.447
0.80	0.02	0.9052	0.0181	0.0839	168.2	2.103	2.699	1.283	0						

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION			TEMP	RELATIVE VOL			PRESSURE ACT COEF			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LR MOLE-R	
N2/N2+O2	AR	N2	AR	O2		R	N2/AR	N2/O2	AR/O2	N2	AR	O2	Liq	Vap	Liq
0.	0.	0.	0.	1.0000	200.9	1.851	2.453	1.325	0.931	1.094	1.001	-1327.	1256.	13.6	8.566
0.	0.01	0.	0.	0.0132	200.8	1.853	2.452	1.323	0.931	1.092	1.002	-1331.	1251.	13.6	8.538
0.	0.02	0.	0.	0.0262	200.7	1.856	2.450	1.320	0.930	1.090	1.002	-1334.	1245.	13.6	8.511
0.	0.03	0.	0.	0.0391	200.6	1.859	2.448	1.317	0.930	1.089	1.003	-1338.	1239.	13.6	8.484
0.	0.04	0.	0.	0.0519	200.5	1.862	2.446	1.315	0.929	1.087	1.003	-1342.	1234.	13.6	8.457
0.	0.05	0.	0.	0.0646	200.4	1.865	2.444	1.312	0.928	1.085	1.004	-1345.	1228.	13.6	8.430
0.	0.06	0.	0.	0.0895	200.2	1.870	2.444	1.307	0.928	1.082	1.005	-1352.	1217.	13.6	8.376
0.	0.07	0.	0.	0.1241	199.9	1.878	2.439	1.299	0.928	1.078	1.007	-1363.	1201.	13.6	8.302
0.	0.10	0.	0.	0.2412	199.1	1.905	2.422	1.272	0.925	1.068	1.015	-1397.	1151.	13.4	8.080
0.	0.20	0.	0.	0.4481	197.8	1.956	2.361	1.218	0.919	1.034	1.036	-1460.	1063.	13.1	7.623
0.	0.40	0.	0.	0.6358	196.8	2.004	2.332	1.164	0.920	1.016	1.066	-1519.	986.	12.8	7.223
0.	0.60	0.	0.	0.8163	196.0	2.049	2.277	1.111	0.928	1.009	1.107	-1573.	913.	12.6	6.833
0.	0.80	0.	0.	0.9972	195.7	2.071	2.247	1.085	0.935	1.003	1.132	-1599.	877.	12.4	6.636
0.10	0.	0.2172	0.	0.7828	196.6	1.888	2.497	1.322	0.945	1.108	1.024	-1308.	1227.	13.6	8.468
0.10	0.01	0.2145	0.0115	0.7740	196.6	1.891	2.494	1.319	0.945	1.106	1.025	-1311.	1222.	13.6	8.504
0.10	0.02	0.2119	0.0228	0.7653	196.5	1.893	2.492	1.317	0.944	1.104	1.025	-1315.	1217.	13.6	8.566
0.10	0.03	0.2093	0.0342	0.7566	196.5	1.895	2.490	1.314	0.943	1.102	1.025	-1319.	1213.	13.6	8.536
0.10	0.04	0.2067	0.0454	0.7479	196.4	1.898	2.488	1.311	0.943	1.100	1.026	-1322.	1208.	13.6	8.512
0.10	0.05	0.2042	0.0566	0.7393	196.4	1.900	2.486	1.308	0.942	1.098	1.026	-1326.	1204.	13.6	8.488
0.10	0.07	0.1991	0.0787	0.7223	196.2	1.912	2.481	1.303	0.941	1.094	1.027	-1333.	1195.	13.6	8.447
0.10	0.10	0.1916	0.1114	0.6971	195.9	1.934	2.474	1.294	0.939	1.088	1.029	-1343.	1182.	13.6	8.371
0.10	0.20	0.1676	0.2166	0.6157	195.5	1.978	2.459	1.267	0.933	1.070	1.035	-1378.	1139.	13.6	8.148
0.10	0.40	0.1231	0.4149	0.4620	195.3	1.978	2.398	1.212	0.927	1.042	1.053	-1444.	1062.	13.2	7.722
0.10	0.60	0.0815	0.6954	0.3132	195.3	2.018	2.341	1.160	0.926	1.021	1.079	-1507.	988.	12.9	7.306
0.10	0.80	0.0410	0.7972	0.1618	195.3	2.037	2.281	1.109	0.932	1.008	1.114	-1567.	916.	12.6	6.883
0.10	0.90	0.0207	0.8960	0.0827	195.4	2.075	2.249	1.084	0.937	1.004	1.136	-1596.	879.	12.4	6.662
0.20	0.	0.3870	0.	0.6130	192.0	1.918	2.525	1.317	0.955	1.120	1.046	-1289.	1199.	14.2	8.663
0.20	0.01	0.3829	0.0101	0.6077	192.0	1.920	2.523	1.314	0.955	1.118	1.049	-1298.	1195.	14.1	8.641
0.20	0.02	0.3787	0.0201	0.6012	192.0	1.922	2.520	1.311	0.954	1.116	1.049	-1302.	1192.	14.1	8.610
0.20	0.03	0.3746	0.0301	0.5953	192.0	1.924	2.517	1.308	0.953	1.114	1.049	-1306.	1188.	14.1	8.579
0.20	0.04	0.3705	0.0401	0.5894	192.0	1.927	2.514	1.305	0.952	1.112	1.049	-1310.	1184.	14.1	8.548
0.20	0.05	0.3664	0.0500	0.5836	192.9	1.929	2.512	1.302	0.951	1.110	1.050	-1313.	1181.	14.1	8.517
0.20	0.07	0.3583	0.0698	0.5719	192.9	1.933	2.504	1.297	0.950	1.109	1.050	-1317.	1173.	14.0	8.474
0.20	0.10	0.3463	0.0892	0.5549	192.9	1.939	2.498	1.290	0.948	1.099	1.051	-1321.	1162.	14.0	8.417
0.20	0.20	0.3069	0.1998	0.4973	193.0	1.959	2.469	1.260	0.942	1.080	1.056	-1357.	1127.	13.8	8.235
0.20	0.40	0.2318	0.3896	0.3834	193.4	1.997	2.410	1.207	0.934	1.049	1.070	-1427.	1059.	13.4	7.815
0.20	0.60	0.1844	0.5772	0.2664	193.9	2.032	2.348	1.155	0.932	1.027	1.092	-1495.	990.	13.0	7.386
0.20	0.80	0.0884	0.7749	0.1408	194.6	2.084	2.284	1.106	0.935	1.011	1.122	-1561.	919.	12.6	6.933
0.20	0.90	0.0440	0.8863	0.0720	195.0	2.079	2.250	1.083	0.939	1.008	1.146	-1593.	881.	12.4	6.689
0.40	0.	0.6232	0.	0.3768	186.5	1.955	2.537	1.298	0.966	1.144	1.103	-1226.	1152.	14.9	8.794
0.40	0.01	0.6232	0.0000	0.3800	186.6	1.957	2.534	1.295	0.966	1.144	1.103	-1230.	1149.	14.9	8.775
0.40	0.02	0.6178	0.0101	0.3861	186.7	1.959	2.532	1.292	0.965	1.141	1.103	-1234.	1147.	14.9	8.756
0.40	0.03	0.6125	0.0202	0.3923	186.7	1.961	2.529	1.289	0.964	1.139	1.102	-1238.	1144.	14.9	8.737
0.40	0.04	0.6072	0.0322	0.3986	186.8	1.963	2.526	1.287	0.963	1.137	1.102	-1242.	1142.	14.4	8.718
0.40	0.05	0.6019	0.0403	0.3978	186.9	1.965	2.523	1.284	0.963	1.134	1.102	-1246.	1140.	14.4	8.698
0.40	0.07	0.5912	0.0565	0.3923	187.0	1.969	2.518	1.279	0.961	1.130	1.102	-1255.	1135.	14.4	8.660
0.40	0.10	0.5792	0.0809	0.3439	187.2	1.975	2.509	1.271	0.959	1.123	1.102	-1267.	1127.	14.3	8.602
0.40	0.20	0.5213	0.1834	0.3153	187.9	1.994	2.480	1.244	0.954	1.101	1.102	-1308.	1103.	14.0	8.495
0.40	0.40	0.4096	0.3366	0.2939	189.5	2.028	2.420	1.193	0.946	1.086	1.108	-1389.	1051.	13.6	7.991
0.40	0.60	0.2991	0.5270	0.1840	191.2	2.057	2.357	1.146	0.942	1.068	1.120	-1469.	993.	13.1	7.588
0.40	0.80	0.1946	0.7441	0.1014	193.2	2.078	2.289	1.101	0.942	1.050	1.130	-1548.	924.	12.7	7.027
0.40	0.90	0.0803	0.8662	0.0535	194.3	2.086	2.253	1.080	0.943	1.048	1.148	-1586.	885.	12.5	6.741
0.60	0.	0.7895	0.	0.2105	181.9	1.945	2.501	1.273	0.973	1.180	1.171	-1153.	1112.	14.8	8.939
0.60	0.01	0.7841	0.0047	0.2092	181.6	1.947	2.499	1.270	0.973	1.177	1.170	-1156.	1110.	14.7	8.921
0.60	0.02	0.7787	0.0134	0.2079	181.7	1.949	2.497	1.268	0.972	1.174	1.169	-1160.	1107.	14.7	8.902
0.60	0.03	0.7732	0.0202	0.2066	181.8	1.952	2.495	1.265	0.971	1.171	1.169	-1164.	1105.	14.7	8.884
0.60	0.04	0.7677	0.0270	0.2053	182.0	1.954	2.493	1.263	0.971	1.169	1.169	-1168.	1103.	14.7	8.866
0.60	0.05	0.7622	0.0338	0.2040	182.1	1.957	2.491	1.260	0.970	1.167	1.167	-1172.	1101.	14.6	8.848
0.60	0.07	0.7511	0.0476	0.2013	182.3	1.961	2.487	1.255	0.969	1.165	1.165	-1177.	1095.	14.6	8.811
0.60	0.10	0.7343	0.0644	0.1971	182.6	1.968	2.481	1.248	0.967	1.152	1.163	-1202.	1077.	14.5	8.755
0.60	0.20	0.6765	0.1402	0.1833	183.7	2.011	2.460	1.224	0.963	1.127	1.150	-1259.	1030.	14.2	8.564
0.60	0.40	0.5499	0.2982	0.1519	186.1	2.049	2.413	1.170	0.956	1.085	1.151	-1347.	1041.	13.7	8.151
0.60	0.60	0.4021	0.4842	0.1137	188.8	2.076	2.358	1.135	0.952	1.051	1.150	-1441.	992.	13.2	7.677
0.60	0.80	0.2233	0.7117	0.0649	191.9	2.092	2.292	1.096	0.949	1.024	1.154	-1534.	929.	12.7	7.117
0.60	0.90	0.1182	0.8489	0.0369	193.6	2.094	2.256	1.077	0.946	1.013	1.156	-1580.	888.	12.5	6.792
0.80	0.	0.9068	0.	0.0933	177.4	1.954	2.431	1.244	0.984	1.224	1.250	-1071.	1079.	14.0	9.080
0.80	0.01	0.9015	0.0098	0.0927	177.6	1.957	2.430	1.241	0.983	1.223	1.257	-1076.	1076.	14.0	9.071
0.80	0.02	0.8961	0.0177	0.0917	177.7	1.961	2.430	1.239	0.982	1.219	1.255	-1082.	1077.	14.0	9.053
0.80	0.03	0.8908	0.0254	0.0911	177.9	1.964	2.430	1.237	0.981	1.215	1.253	-1088.	1076.	14.0	9.035
0.80	0.04	0.8854	0.0331	0.0906	178.1	1.970	2.429	1.235	0.981	1.211	1.251	-1094.	1075.	14.0	9.017
0.80	0.05	0.8800	0.0408	0.0900	178.3	1.976	2.427	1.232	0.980	1.208	1.249	-1100.	1074.	14.0	9.000
0.80	0.07	0.8691	0.0544	0.0895	178.7	1.985	2.424	1.222	0.979	1.201	1.246	-1111.	1072.	14.0	8.982
0.80	0.10	0.8525	0.0736	0.0890	180.0	2.013	2.417	1.201	0.972	1.191	1.241	-1129.	1059.	14.0	8.967
0.80	0.20	0.7945	0.1233	0.0822	183.0	2.080	2.392	1.161	0.966	1.160	1.225	-1186.	1050.	14.3	8.716
0.80	0.40	0.6827	0.2681	0.0693	186.5	2.092	2.352	1.124	0.961	1.107	1.201	-1300.	1030.	13.8	8.298
0.80															

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION			TEMP	RELATIVE VOL			PRESSURE ACT COEF			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
N2/N2+O2	AR	N2	AR	O2		N2/AR	N2/O2	AR/O2	N2	AR	O2	LIQ	VAP	LIQ	VAP
0.0	0.0	0.0	0.0	1.0000	208.9	1.737	2.240	1.290	0.000	1.000	1.000	-1216.1275		14.0	9.920
0.0	0.01	0.0	0.0128	0.9872	208.6	1.739	2.230	1.287	0.007	1.079	1.003	-1220.1269		13.9	9.993
0.0	0.02	0.0	0.0256	0.9744	208.7	1.742	2.238	1.285	0.007	1.077	1.003	-1224.1263		13.9	9.966
0.0	0.03	0.0	0.0384	0.9618	208.6	1.744	2.237	1.283	0.007	1.075	1.004	-1227.1258		13.9	9.940
0.0	0.04	0.0	0.0512	0.9494	208.5	1.746	2.236	1.280	0.006	1.074	1.004	-1231.1252		13.9	9.914
0.0	0.05	0.0	0.0640	0.9370	208.4	1.749	2.234	1.278	0.006	1.073	1.005	-1235.1246		13.9	9.888
0.0	0.07	0.0	0.0874	0.9126	208.2	1.753	2.232	1.273	0.005	1.070	1.006	-1242.1235		13.9	9.837
0.0	0.10	0.0	0.1233	0.8767	208.0	1.760	2.228	1.266	0.004	1.065	1.006	-1253.1219		13.9	9.762
0.0	0.20	0.0	0.2369	0.7632	207.1	1.782	2.213	1.242	0.002	1.052	1.017	-1288.1168		13.7	9.524
0.0	0.40	0.0	0.4430	0.5570	205.0	1.825	2.177	1.193	0.000	1.030	1.037	-1354.1077		13.5	9.089
0.0	0.60	0.0	0.6319	0.3681	204.7	1.865	2.135	1.144	0.002	1.014	1.046	-1414.0996		13.3	7.886
0.0	0.80	0.0	0.8143	0.1857	204.9	1.903	2.086	1.096	0.000	1.000	1.060	-1471.0920		13.1	7.288
0.0	0.90	0.0	0.9063	0.0939	203.7	1.921	2.060	1.072	0.000	1.000	1.120	-1498.0822		13.0	7.086
0.10	0.01	0.2018	0.0	0.7983	204.8	1.766	2.275	1.287	0.905	1.098	1.027	-1193.1246		14.2	9.076
0.10	0.02	0.1909	0.0114	0.7893	204.7	1.770	2.273	1.285	0.905	1.096	1.028	-1197.1241		14.2	9.052
0.10	0.03	0.1800	0.0227	0.7804	204.7	1.772	2.271	1.282	0.904	1.094	1.028	-1201.1236		14.2	9.028
0.10	0.04	0.1702	0.0339	0.7715	204.6	1.774	2.270	1.279	0.904	1.092	1.029	-1204.1231		14.2	9.004
0.10	0.05	0.1608	0.0451	0.7627	204.6	1.776	2.268	1.277	0.903	1.091	1.029	-1208.1226		14.2	8.981
0.10	0.07	0.1481	0.0562	0.7540	204.6	1.778	2.266	1.274	0.903	1.089	1.030	-1212.1222		14.2	8.957
0.10	0.10	0.1302	0.0782	0.7367	204.5	1.782	2.262	1.269	0.901	1.085	1.031	-1219.1213		14.1	8.911
0.10	0.20	0.1102	0.1108	0.7117	204.4	1.788	2.256	1.262	0.900	1.080	1.032	-1230.1199		14.1	8.841
0.10	0.40	0.1000	0.2190	0.6781	204.0	1.807	2.236	1.237	0.896	1.065	1.038	-1266.1155		14.0	8.617
0.10	0.60	0.1146	0.4145	0.4709	203.5	1.844	2.191	1.180	0.890	1.039	1.056	-1336.1074		13.7	8.167
0.10	0.80	0.1364	0.7979	0.1641	203.3	1.878	2.142	1.140	0.890	1.021	1.061	-1401.0998		13.4	7.706
0.10	0.90	0.1592	0.8971	0.0827	203.4	1.909	2.089	1.094	0.894	1.009	1.114	-1464.0922		13.2	7.336
0.20	0.01	0.3649	0.0	0.6351	201.0	1.794	2.299	1.281	0.910	1.114	1.054	-1167.1218		14.8	9.140
0.20	0.02	0.3511	0.0102	0.6289	201.0	1.796	2.296	1.279	0.910	1.112	1.054	-1171.1214		14.8	9.116
0.20	0.03	0.3373	0.0204	0.6226	201.0	1.798	2.294	1.276	0.910	1.110	1.055	-1175.1210		14.8	9.104
0.20	0.04	0.3235	0.0306	0.6165	201.0	1.799	2.292	1.274	0.910	1.108	1.055	-1179.1207		14.8	9.092
0.20	0.05	0.3097	0.0408	0.6103	201.0	1.801	2.289	1.271	0.910	1.106	1.055	-1183.1203		14.8	9.080
0.20	0.07	0.2959	0.0510	0.6042	201.0	1.803	2.287	1.269	0.910	1.104	1.055	-1187.1199		14.8	9.068
0.20	0.10	0.2821	0.0612	0.5981	201.0	1.806	2.285	1.263	0.910	1.102	1.056	-1194.1191		14.8	9.056
0.20	0.20	0.2683	0.1001	0.5736	201.1	1.812	2.275	1.256	0.913	1.099	1.057	-1204.1180		14.3	8.929
0.20	0.40	0.2170	0.1975	0.5135	201.1	1.829	2.251	1.231	0.907	1.077	1.061	-1243.1142		14.2	8.714
0.20	0.60	0.1464	0.3887	0.3944	201.4	1.861	2.200	1.183	0.899	1.049	1.075	-1317.1070		13.6	8.285
0.20	0.80	0.1464	0.5810	0.2727	201.9	1.899	2.147	1.136	0.897	1.027	1.095	-1388.0999		13.5	7.846
0.20	0.90	0.1749	0.7819	0.1432	202.6	1.916	2.092	1.092	0.898	1.012	1.121	-1457.0925		13.2	7.393
0.40	0.01	0.6068	0.0	0.3932	194.6	1.831	2.315	1.264	0.941	1.147	1.114	-1107.1169		15.0	9.328
0.40	0.02	0.5962	0.0104	0.3872	194.7	1.833	2.312	1.262	0.940	1.145	1.113	-1111.1166		15.0	9.307
0.40	0.03	0.5857	0.0204	0.3812	194.8	1.835	2.310	1.259	0.939	1.142	1.113	-1116.1164		15.0	9.287
0.40	0.04	0.5751	0.0304	0.3752	194.9	1.837	2.308	1.257	0.938	1.140	1.113	-1120.1161		15.0	9.266
0.40	0.05	0.5646	0.0404	0.3692	194.9	1.839	2.306	1.255	0.937	1.138	1.113	-1124.1159		15.0	9.246
0.40	0.07	0.5490	0.0504	0.3632	195.1	1.842	2.297	1.247	0.935	1.135	1.112	-1128.1156		15.0	9.225
0.40	0.10	0.5334	0.0604	0.3572	195.3	1.847	2.289	1.240	0.933	1.131	1.112	-1137.1151		14.8	9.184
0.40	0.20	0.5005	0.1000	0.3316	196.0	1.862	2.264	1.216	0.927	1.124	1.112	-1190.1143		14.7	9.122
0.40	0.40	0.3905	0.3445	0.2649	197.5	1.869	2.211	1.170	0.917	1.099	1.115	-1193.1138		14.5	9.013
0.40	0.60	0.2734	0.5343	0.1983	199.3	1.911	2.155	1.127	0.910	1.069	1.115	-1277.1061		14.1	8.475
0.40	0.80	0.1449	0.7514	0.1037	201.3	1.928	2.095	1.087	0.906	1.042	1.124	-1361.0999		13.7	8.001
0.40	0.90	0.1749	0.8708	0.0544	202.4	1.934	2.066	1.068	0.905	1.020	1.138	-1443.0929		13.3	7.475
0.60	0.01	0.7748	0.0	0.2252	189.3	1.847	2.293	1.241	0.959	1.167	1.166	-1036.1120		15.3	9.534
0.60	0.02	0.7636	0.0100	0.2223	189.4	1.849	2.291	1.239	0.958	1.164	1.165	-1041.1125		15.3	9.514
0.60	0.03	0.7524	0.0200	0.2193	189.6	1.851	2.289	1.237	0.957	1.161	1.164	-1046.1123		15.3	9.494
0.60	0.04	0.7412	0.0300	0.2164	189.8	1.853	2.288	1.235	0.956	1.158	1.163	-1051.1121		15.2	9.473
0.60	0.05	0.7300	0.0400	0.2135	189.9	1.855	2.286	1.232	0.955	1.157	1.163	-1056.1120		15.2	9.453
0.60	0.07	0.7188	0.0500	0.2106	190.1	1.857	2.284	1.230	0.954	1.155	1.162	-1061.1118		15.2	9.432
0.60	0.10	0.7076	0.0600	0.2077	190.4	1.860	2.282	1.228	0.953	1.153	1.161	-1067.1116		15.1	9.391
0.60	0.20	0.6591	0.1499	0.1950	191.6	1.866	2.274	1.219	0.951	1.150	1.177	-1086.1109		15.1	9.326
0.60	0.40	0.5310	0.3088	0.1603	194.0	1.882	2.254	1.197	0.944	1.134	1.170	-1136.1091		14.8	9.115
0.60	0.60	0.3844	0.4974	0.1187	196.8	1.911	2.209	1.156	0.932	1.092	1.160	-1235.1049		14.3	8.659
0.60	0.80	0.2103	0.7220	0.0664	200.0	1.930	2.157	1.110	0.923	1.057	1.156	-1333.0988		13.8	8.150
0.60	0.90	0.1115	0.8530	0.0356	203.7	1.941	2.087	1.065	0.914	1.020	1.154	-1429.0932		13.3	7.565
0.80	0.01	1.0000	0.0	0.0000	184.9	1.847	2.243	1.214	0.976	1.238	1.278	-957.1089		15.6	9.758
0.80	0.02	0.9888	0.0081	0.0097	185.1	1.848	2.242	1.212	0.977	1.234	1.276	-963.1088		15.6	9.737
0.80	0.03	0.9776	0.0162	0.0191	185.2	1.850	2.241	1.210	0.976	1.231	1.274	-968.1087		15.6	9.716
0.80	0.04	0.9664	0.0243	0.0285	185.3	1.851	2.240	1.208	0.975	1.227	1.272	-974.1086		15.6	9.694
0.80	0.05	0.9552	0.0324	0.0379	185.4	1.852	2.239	1.206	0.974	1.224	1.270	-980.1085		15.6	9.673
0.80	0.07	0.9340	0.0405	0.0473	185.6	1.853	2.238	1.204	0.973	1.220	1.268	-986.1084		15.6	9.652
0.80	0.10	0.9128	0.0486	0.0567	185.9	1.854	2.237	1.202	0.972	1.217	1.266	-992.1083		15.6	9.631
0.80	0.20	0.8431	0.0626	0.0943	186.3	1.857	2.235	1.199	0.969	1.203	1.268	-1019.1078		15.3	9.543
0.80	0.40	0.6465	0.2709	0.0734	190.9	1.925	2.196	1.140	0.948	1.118	1.241	-1074.1066		15.0	9.319
0.80	0.60	0.4898	0.4634	0.0523	194.5	1.946	2.155	1.108	0.938	1.073	1.250	-1190.1036		14.4	8.838
0.80	0.80	0.2716	0.6961	0.0323	194.7	1.951	2.101	1.077	0.921	1.036	1.172	-1304.0995		13.9	8.293
0.80	0.90	0.1440	0.8376	0.0179	201.0	1.947	2.059	1.063	0.913	1.019	1.183	-1419.0934		13.4	7.653
0.90	0.01	0.9521	0.0	0.0479	182.9	1.842	2.200	1.190	0.980	1.270	1.333	-915.1072		15.6	9.876
0.90	0.02	0.9411	0.011												

LIQUID MOLE FRACTION			VAPOR MOLE FRACTION			TEMP	RELATIVE VOL			PRESSURE ACT COEF			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
N2/N2+O2	AR	O2	N2	AR	O2		N	N2/AR	N2/O2	AR/O2	N2	AR	O2	LIG	VAP	LIG
0.0	0.0	1.0	0.0	0.0	1.0	215.4	1.000	0.000	1.000	0.852	1.000	1.000	-1121.	1285.	14.3	9.498
0.0	0.01	0.99	0.0126	0.000	0.9874	215.5	1.000	0.000	1.000	0.852	1.000	1.000	-1125.	1279.	14.3	9.472
0.0	0.02	0.98	0.0250	0.000	0.9750	215.6	1.000	0.000	1.000	0.852	1.000	1.000	-1129.	1274.	14.3	9.446
0.0	0.03	0.97	0.0374	0.000	0.9626	215.7	1.000	0.000	1.000	0.852	1.000	1.000	-1133.	1268.	14.3	9.420
0.0	0.04	0.96	0.0498	0.000	0.9502	215.8	1.000	0.000	1.000	0.852	1.000	1.000	-1137.	1262.	14.3	9.394
0.0	0.05	0.95	0.0618	0.000	0.9378	215.9	1.000	0.000	1.000	0.851	1.000	1.000	-1140.	1256.	14.3	9.368
0.0	0.10	0.90	0.1211	0.000	0.8789	216.7	1.076	2.078	1.240	0.851	1.000	1.000	-1148.	1245.	14.3	9.319
0.0	0.20	0.80	0.2334	0.000	0.7666	218.0	1.095	2.084	1.218	0.849	1.044	1.018	-1159.	1228.	14.2	9.245
0.0	0.30	0.70	0.4389	0.000	0.5611	217.5	1.731	2.030	1.173	0.848	1.025	1.039	-1195.	1177.	14.1	9.011
0.0	0.40	0.60	0.6286	0.000	0.3714	211.4	1.765	1.991	1.128	0.851	1.011	1.058	-1262.	1083.	14.0	8.577
0.0	0.50	0.50	0.8126	0.000	0.1874	210.7	1.798	1.948	1.084	0.858	1.004	1.105	-1323.	999.	13.8	8.143
0.10	0.0	0.90	0.9053	0.000	0.0947	210.4	1.812	1.924	1.062	0.863	1.002	1.127	-1408.	882.	13.6	7.599
0.10	0.01	0.89	0.1800	0.013	0.8007	211.6	1.682	2.115	1.259	0.872	1.008	1.030	-1095.	1257.	14.6	9.576
0.10	0.02	0.88	0.1858	0.013	0.8007	211.5	1.684	2.112	1.254	0.871	1.008	1.030	-1099.	1252.	14.6	9.548
0.10	0.03	0.87	0.1835	0.013	0.7928	211.4	1.686	2.110	1.252	0.870	1.008	1.031	-1103.	1247.	14.6	9.520
0.10	0.04	0.86	0.1813	0.013	0.7839	211.4	1.687	2.108	1.249	0.869	1.008	1.031	-1107.	1242.	14.6	9.492
0.10	0.05	0.85	0.1791	0.013	0.7751	211.3	1.689	2.106	1.247	0.869	1.008	1.032	-1111.	1237.	14.6	9.464
0.10	0.07	0.83	0.1747	0.013	0.7476	211.3	1.693	2.103	1.243	0.869	1.007	1.032	-1114.	1232.	14.6	9.436
0.10	0.10	0.90	0.1682	0.013	0.7217	211.1	1.698	2.098	1.236	0.867	1.073	1.035	-1122.	1223.	14.5	9.408
0.10	0.20	0.80	0.1474	0.014	0.6377	210.8	1.714	2.094	1.213	0.864	1.059	1.041	-1134.	1209.	14.5	9.336
0.10	0.30	0.70	0.1083	0.013	0.4780	210.3	1.746	2.080	1.169	0.859	1.036	1.058	-1171.	1163.	14.3	9.112
0.10	0.40	0.60	0.0716	0.014	0.3230	210.0	1.778	1.966	1.125	0.859	1.019	1.082	-1242.	1079.	14.1	8.680
0.10	0.50	0.50	0.0360	0.014	0.1680	210.0	1.802	1.949	1.082	0.862	1.008	1.113	-1310.	1000.	13.9	8.253
0.20	0.0	0.80	0.8011	0.000	0.0000	210.0	1.814	1.925	1.061	0.866	1.003	1.131	-1374.	921.	13.7	7.814
0.20	0.01	0.79	0.3441	0.010	0.6457	207.9	1.702	2.134	1.254	0.880	1.107	1.059	-1057.	1229.	14.9	9.663
0.20	0.02	0.78	0.3404	0.010	0.6393	207.9	1.704	2.132	1.251	0.880	1.109	1.059	-1071.	1225.	14.8	9.640
0.20	0.03	0.77	0.3366	0.010	0.6329	207.9	1.705	2.130	1.249	0.887	1.104	1.059	-1075.	1221.	14.8	9.618
0.20	0.04	0.76	0.3329	0.010	0.6265	207.9	1.707	2.128	1.247	0.887	1.102	1.060	-1079.	1217.	14.8	9.596
0.20	0.05	0.75	0.3292	0.010	0.6201	207.9	1.708	2.126	1.244	0.886	1.100	1.060	-1083.	1213.	14.8	9.573
0.20	0.07	0.73	0.3219	0.010	0.6074	207.9	1.710	2.124	1.242	0.886	1.098	1.060	-1087.	1209.	14.8	9.551
0.20	0.10	0.70	0.3109	0.010	0.5885	207.9	1.713	2.120	1.237	0.884	1.095	1.060	-1095.	1201.	14.8	9.506
0.20	0.20	0.80	0.2752	0.010	0.5262	207.9	1.718	2.113	1.230	0.883	1.074	1.062	-1107.	1189.	14.7	9.446
0.20	0.30	0.70	0.2063	0.010	0.4030	208.2	1.732	2.092	1.208	0.877	1.047	1.066	-1146.	1150.	14.6	9.221
0.20	0.40	0.60	0.1389	0.010	0.2777	208.7	1.760	2.068	1.163	0.870	1.027	1.097	-1222.	1075.	14.3	8.782
0.20	0.50	0.50	0.0748	0.010	0.1452	209.3	1.785	2.041	1.121	0.866	1.007	1.121	-1296.	1001.	14.1	8.334
0.30	0.0	0.70	0.3599	0.000	0.2744	209.6	1.807	1.991	1.080	0.868	1.012	1.121	-1367.	924.	13.7	7.861
0.30	0.01	0.69	0.3589	0.000	0.4111	211.4	1.735	2.140	1.238	0.917	1.147	1.123	-1004.	1176.	15.4	9.695
0.30	0.02	0.68	0.3574	0.000	0.4079	211.4	1.737	2.147	1.236	0.917	1.145	1.123	-1009.	1175.	15.4	9.674
0.30	0.03	0.67	0.3573	0.000	0.4014	211.6	1.738	2.144	1.234	0.916	1.143	1.122	-1013.	1173.	15.3	9.652
0.30	0.04	0.66	0.3579	0.000	0.3981	211.6	1.740	2.142	1.231	0.915	1.140	1.122	-1018.	1170.	15.3	9.630
0.30	0.05	0.65	0.3527	0.000	0.3949	211.7	1.742	2.138	1.227	0.914	1.138	1.122	-1022.	1167.	15.3	9.608
0.30	0.07	0.63	0.3522	0.000	0.3883	211.8	1.745	2.133	1.222	0.913	1.136	1.121	-1026.	1164.	15.3	9.587
0.30	0.10	0.60	0.3364	0.000	0.3784	212.0	1.749	2.126	1.216	0.912	1.132	1.121	-1035.	1159.	15.2	9.543
0.30	0.20	0.70	0.4836	0.000	0.3449	212.8	1.762	2.103	1.194	0.909	1.125	1.120	-1049.	1150.	15.2	9.477
0.30	0.30	0.70	0.3755	0.000	0.2739	214.3	1.785	2.056	1.152	0.902	1.105	1.119	-1093.	1122.	15.0	9.454
0.30	0.40	0.60	0.2613	0.000	0.3954	208.0	1.804	2.006	1.112	0.891	1.071	1.121	-1181.	1063.	14.5	8.993
0.30	0.50	0.50	0.1376	0.000	0.3054	208.0	1.818	1.954	1.075	0.882	1.043	1.127	-1267.	1000.	14.2	8.497
0.40	0.0	0.60	0.6718	0.000	0.3251	209.1	1.823	1.927	1.057	0.875	1.021	1.138	-1352.	927.	13.8	7.953
0.40	0.01	0.59	0.7621	0.000	0.2380	195.0	1.754	2.135	1.217	0.943	1.193	1.200	-934.	1133.	15.8	10.175
0.40	0.02	0.58	0.7564	0.000	0.2346	196.0	1.756	2.133	1.215	0.942	1.190	1.199	-939.	1131.	15.8	10.152
0.40	0.03	0.57	0.7507	0.000	0.2312	196.1	1.757	2.131	1.213	0.941	1.187	1.198	-944.	1129.	15.8	10.129
0.40	0.04	0.56	0.7450	0.000	0.2278	196.2	1.759	2.128	1.211	0.940	1.184	1.197	-949.	1127.	15.7	10.106
0.40	0.05	0.55	0.7392	0.000	0.2244	196.4	1.760	2.126	1.209	0.939	1.181	1.196	-954.	1125.	15.7	10.083
0.40	0.07	0.53	0.7319	0.000	0.2208	196.7	1.762	2.124	1.207	0.938	1.179	1.195	-959.	1124.	15.7	10.060
0.40	0.10	0.50	0.7044	0.000	0.2219	197.0	1.765	2.122	1.203	0.936	1.173	1.193	-969.	1120.	15.6	10.014
0.40	0.20	0.60	0.6445	0.000	0.2049	198.7	1.783	2.097	1.179	0.934	1.165	1.190	-985.	1114.	15.6	9.944
0.40	0.30	0.70	0.5155	0.000	0.1872	200.7	1.805	2.055	1.137	0.925	1.140	1.181	-1036.	1095.	15.3	9.707
0.40	0.40	0.60	0.3696	0.000	0.1227	203.6	1.820	2.008	1.103	0.910	1.097	1.189	-1137.	1059.	14.8	9.266
0.40	0.50	0.50	0.2005	0.000	0.0883	206.7	1.828	1.956	1.070	0.897	1.060	1.180	-1238.	997.	14.3	8.658
0.50	0.0	0.50	0.1147	0.000	0.0362	208.4	1.828	1.929	1.055	0.877	1.016	1.153	-1326.	929.	13.9	8.045
0.50	0.01	0.49	0.8935	0.000	0.1065	191.2	1.799	2.097	1.192	0.970	1.250	1.296	-857.	1092.	16.1	10.494
0.50	0.02	0.48	0.8878	0.000	0.1032	191.9	1.791	2.096	1.190	0.969	1.248	1.294	-863.	1091.	16.1	10.469
0.50	0.03	0.47	0.8821	0.000	0.1000	191.7	1.793	2.095	1.188	0.968	1.243	1.292	-868.	1090.	16.1	10.444
0.50	0.04	0.46	0.8764	0.000	0.0968	191.6	1.795	2.094	1.186	0.967	1.239	1.290	-874.	1088.	16.1	10.418
0.50	0.05	0.45	0.8706	0.000	0.0936	191.5	1.797	2.093	1.185	0.966	1.235	1.287	-880.	1087.	16.0	10.392
0.50	0.07	0.43	0.8628	0.000	0.0898	191.2	1.799	2.092	1.183	0.965	1.232	1.285	-886.	1086.	16.0	10.367
0.50	0.10	0.40	0.8340	0.000	0.0860	192.7	1.773	2.070	1.179	0.962	1.225	1.281	-898.	1084.	15.9	10.315
0.50	0.20	0.50	0.7725	0.000	0.0930	194.2	1.794	2.076	1.157	0.949	1.214	1.275	-916.	1080.	15.9	10.238
0.50	0.30	0.70	0.6529	0.000	0.0773	197.5	1.820	2.046	1.124	0.930	1.195	1.255	-975.	1068.	15.6	9.975
0.50	0.40	0.60	0.4659	0.000	0.0580	201.2	1.835	2.007	1.094	0.910	1.175	1.223	-1092.	1036.	15.0	9.423
0.50	0.50	0.50	0.2598	0.000	0.0332	205.4										

LIQUID MOLE FRACTION			VAPOR MOLE FRACTION			IFMP	RELATIVE VOL			PRESSURE ACT COEF			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LR MOLE-R		
N <sub>2</sub> /N <sub>2</sub> +O <sub>2</sub>	AR	O <sub>2</sub>	N <sub>2</sub>	AR	O <sub>2</sub>		R	N <sub>2</sub> /AR	N <sub>2</sub> /O <sub>2</sub>	AR/O <sub>2</sub>	N <sub>2</sub>	AR	O <sub>2</sub>	LIQ	VAP	LIQ	VAP
0.0	0.0	1.0000	0.0000	0.0000	0.0000	221.4	1.998	1.980	1.239	0.825	1.097	1.003	-1077.120	14.0	10.012		
0.0	0.01	0.9899	0.0101	0.0123	0.9877	221.3	1.998	1.979	1.237	0.824	1.095	1.003	-1071.128	14.0	9.986		
0.0	0.02	0.9798	0.0202	0.0246	0.9754	221.2	1.997	1.977	1.235	0.824	1.094	1.004	-1065.127	14.0	9.961		
0.0	0.03	0.9697	0.0303	0.0367	0.9633	221.1	1.997	1.976	1.233	0.824	1.093	1.005	-1059.127	14.0	9.935		
0.0	0.04	0.9596	0.0404	0.0448	0.9512	221.0	1.995	1.975	1.231	0.824	1.092	1.005	-1053.126	14.0	9.910		
0.0	0.05	0.9495	0.0505	0.0577	0.9389	220.9	1.997	1.974	1.229	0.824	1.091	1.006	-1047.126	14.0	9.885		
0.0	0.07	0.9293	0.0707	0.0844	0.9136	220.8	1.999	1.971	1.225	0.824	1.089	1.008	-1041.124	14.0	9.836		
0.0	0.10	0.8991	0.1009	0.1192	0.8808	220.5	1.999	1.967	1.218	0.823	1.088	1.010	-1035.123	14.0	9.764		
0.0	0.15	0.8490	0.1510	0.2305	0.7695	219.6	1.991	1.953	1.198	0.822	1.086	1.019	-1111.118	14.0	9.532		
0.0	0.20	0.7989	0.2011	0.4354	0.5647	218.3	1.981	1.921	1.157	0.822	1.081	1.041	-1179.104	14.0	9.181		
0.0	0.30	0.6988	0.3012	0.6289	0.3712	217.2	1.959	1.884	1.115	0.825	1.080	1.069	-1242.088	14.0	8.691		
0.0	0.40	0.5987	0.4013	0.8112	0.1889	216.5	1.717	1.844	1.074	0.831	1.082	1.104	-1305.077	14.0	8.279		
0.0	0.50	0.4986	0.5014	0.9046	0.0954	216.3	1.730	1.822	1.053	0.836	1.081	1.125	-1328.071	14.0	8.067		
0.10	0.0	0.1818	0.0	0.0185	0.0	217.4	1.816	1.997	1.239	0.848	1.079	1.032	-1088.126	15.0	10.102		
0.10	0.01	0.1794	0.0112	0.0194	0.0	217.4	1.818	1.995	1.233	0.844	1.078	1.033	-1012.125	15.0	10.078		
0.10	0.02	0.1773	0.0223	0.0294	0.0	217.4	1.819	1.994	1.231	0.844	1.078	1.033	-1016.125	15.0	10.055		
0.10	0.03	0.1752	0.0334	0.0394	0.0	217.3	1.821	1.992	1.229	0.843	1.079	1.034	-1020.124	15.0	10.031		
0.10	0.04	0.1731	0.0445	0.0495	0.0	217.3	1.822	1.990	1.227	0.843	1.074	1.034	-1024.124	15.0	10.008		
0.10	0.05	0.1710	0.0556	0.0596	0.0	217.2	1.824	1.988	1.225	0.843	1.072	1.035	-1028.123	15.0	9.985		
0.10	0.07	0.1668	0.0772	0.0796	0.0	217.1	1.827	1.986	1.221	0.842	1.069	1.036	-1032.123	15.0	9.938		
0.10	0.10	0.1607	0.1094	0.1099	0.0	217.0	1.831	1.981	1.214	0.841	1.065	1.037	-1036.122	15.0	9.870		
0.10	0.20	0.1408	0.2139	0.0493	0.0	216.6	1.846	1.964	1.194	0.838	1.061	1.044	-1086.116	15.0	9.645		
0.10	0.30	0.1206	0.3126	0.0837	0.0	216.1	1.871	1.927	1.152	0.834	1.052	1.061	-1158.100	15.0	9.299		
0.10	0.40	0.1005	0.4055	0.1266	0.0	215.9	1.898	1.887	1.111	0.833	1.051	1.083	-1227.086	15.0	8.776		
0.10	0.50	0.0804	0.5096	0.1676	0.0	215.8	1.721	1.848	1.072	0.836	1.050	1.112	-1292.071	15.0	8.327		
0.10	0.60	0.0603	0.6097	0.2087	0.0	215.7	1.732	1.822	1.052	0.838	1.053	1.129	-1324.070	15.0	8.099		
0.20	0.0	0.3344	0.0	0.0356	0.0	213.8	1.833	2.010	1.231	0.863	1.101	1.063	-978.123	15.0	10.216		
0.20	0.01	0.3318	0.0192	0.0366	0.0	213.8	1.834	2.008	1.229	0.862	1.100	1.063	-982.122	15.0	10.194		
0.20	0.02	0.3272	0.0204	0.0374	0.0	213.8	1.836	2.006	1.226	0.862	1.099	1.063	-986.122	15.0	10.171		
0.20	0.03	0.3226	0.0316	0.0382	0.0	213.8	1.837	2.004	1.224	0.861	1.098	1.064	-990.122	15.0	10.150		
0.20	0.04	0.3180	0.0427	0.0393	0.0	213.8	1.838	2.002	1.222	0.861	1.095	1.064	-994.121	15.0	10.128		
0.20	0.05	0.3134	0.0538	0.0404	0.0	213.8	1.840	2.001	1.220	0.860	1.093	1.064	-998.121	15.0	10.105		
0.20	0.07	0.3094	0.0709	0.0419	0.0	213.8	1.843	1.997	1.216	0.859	1.092	1.065	-1002.120	15.0	10.080		
0.20	0.10	0.2989	0.1018	0.0433	0.0	213.8	1.847	1.991	1.209	0.857	1.089	1.066	-1019.119	15.0	9.992		
0.20	0.20	0.2645	0.1992	0.0534	0.0	213.8	1.860	1.972	1.188	0.852	1.078	1.070	-1059.112	15.0	9.769		
0.20	0.30	0.1981	0.3999	0.1100	0.0	214.0	1.884	1.932	1.147	0.845	1.045	1.082	-1137.104	15.0	9.322		
0.20	0.40	0.1331	0.5881	0.2817	0.0	214.5	1.796	1.890	1.108	0.841	1.028	1.099	-1213.088	15.0	8.862		
0.20	0.50	0.0678	0.7853	0.1469	0.0	215.2	1.726	1.846	1.069	0.841	1.011	1.121	-1285.070	15.0	8.375		
0.20	0.60	0.0343	0.8994	0.2753	0.0	215.6	1.734	1.822	1.051	0.841	1.008	1.134	-1320.070	15.0	8.118		
0.40	0.0	0.5739	0.0	0.0761	0.0	207.2	1.861	2.020	1.216	0.896	1.147	1.131	-913.118	15.0	10.510		
0.40	0.01	0.5687	0.0086	0.0777	0.0	207.3	1.862	2.018	1.214	0.895	1.144	1.131	-917.117	15.0	10.487		
0.40	0.02	0.5635	0.0173	0.0792	0.0	207.4	1.863	2.016	1.212	0.894	1.142	1.130	-922.117	15.0	10.464		
0.40	0.03	0.5583	0.0259	0.0807	0.0	207.4	1.865	2.014	1.210	0.894	1.140	1.130	-926.117	15.0	10.441		
0.40	0.04	0.5531	0.0346	0.0823	0.0	207.5	1.866	2.012	1.208	0.893	1.138	1.130	-931.117	15.0	10.418		
0.40	0.05	0.5479	0.0432	0.0839	0.0	207.6	1.867	2.010	1.206	0.892	1.136	1.130	-936.117	15.0	10.395		
0.40	0.07	0.5375	0.0606	0.0859	0.0	207.7	1.869	2.008	1.202	0.890	1.131	1.129	-945.116	15.0	10.349		
0.40	0.10	0.5219	0.0887	0.0885	0.0	207.9	1.873	2.000	1.195	0.888	1.125	1.128	-958.115	15.0	10.281		
0.40	0.20	0.4698	0.1743	0.1350	0.0	208.6	1.884	1.979	1.179	0.880	1.109	1.126	-1004.112	15.0	10.045		
0.40	0.30	0.3834	0.3553	0.2814	0.0	210.2	1.795	1.937	1.136	0.868	1.072	1.126	-1094.102	15.0	9.557		
0.40	0.40	0.2918	0.5486	0.1986	0.0	211.9	1.721	1.893	1.100	0.858	1.044	1.130	-1183.086	15.0	9.036		
0.40	0.50	0.1321	0.7809	0.1072	0.0	213.8	1.734	1.847	1.068	0.849	1.021	1.138	-1270.070	15.0	8.472		
0.40	0.60	0.0677	0.8765	0.2557	0.0	214.9	1.739	1.823	1.048	0.846	1.018	1.143	-1312.070	15.0	8.168		
0.60	0.0	0.7509	0.0	0.0492	0.0	201.7	1.870	2.009	1.197	0.928	1.198	1.213	-842.114	16.0	10.881		
0.60	0.01	0.7452	0.0078	0.0507	0.0	201.8	1.868	2.007	1.195	0.927	1.195	1.211	-847.113	16.0	10.855		
0.60	0.02	0.7394	0.0156	0.0516	0.0	201.9	1.861	2.006	1.193	0.926	1.192	1.210	-852.113	16.0	10.829		
0.60	0.03	0.7336	0.0234	0.0524	0.0	202.0	1.863	2.004	1.191	0.925	1.189	1.209	-857.112	16.0	10.804		
0.60	0.04	0.7278	0.0312	0.0533	0.0	202.1	1.864	2.002	1.189	0.925	1.187	1.208	-863.112	16.0	10.778		
0.60	0.05	0.7219	0.0390	0.0542	0.0	202.2	1.865	2.001	1.187	0.922	1.184	1.207	-868.112	16.0	10.752		
0.60	0.07	0.7102	0.0520	0.0571	0.0	202.5	1.868	1.997	1.183	0.920	1.178	1.205	-878.110	16.0	10.700		
0.60	0.10	0.6925	0.0708	0.0618	0.0	202.8	1.892	1.992	1.178	0.917	1.170	1.201	-894.110	16.0	10.622		
0.60	0.20	0.6320	0.1546	0.1134	0.0	204.0	1.793	1.974	1.159	0.908	1.149	1.192	-946.103	16.0	10.357		
0.60	0.30	0.5620	0.3243	0.1731	0.0	204.6	1.722	1.936	1.124	0.899	1.101	1.176	-1009.100	16.0	9.886		
0.60	0.40	0.4881	0.5159	0.1261	0.0	209.4	1.735	1.894	1.091	0.874	1.063	1.165	-1053.092	16.0	9.214		
0.60	0.50	0.1926	0.7377	0.0699	0.0	212.6	1.742	1.846	1.061	0.858	1.030	1.156	-1254.070	16.0	8.568		
0.60	0.60	0.1000	0.8630	0.2367	0.0	214.3	1.743	1.824	1.046	0.850	1.015	1.152	-1304.070	16.0	8.219		
0.80	0.0	0.8879	0.0	0.1122	0.0	196.8	1.887	1.976	1.173	0.962	1.261	1.313	-746.109	16.0	11.322		
0.80	0.01	0.8820	0.0086	0.1137	0.0	196.9	1.888	1.974	1.172	0.960	1.257	1.311	-752.108	16.0	11.296		
0.80	0.02	0.8760	0.0172	0.1152	0.0	197.1	1.889	1.972	1.170	0.959	1.253	1.309	-758.107	16.0	11.271		
0.80	0.03	0.8701	0.0258	0.1167	0.0	197.2	1.891	1.9									

LIQUID MOLE FRACTION			VAPOR MOLE FRACTION			TEMP	RELATIVE VOL			PRESSURE ACT COEF			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LP MOLE-R	
N2/M2+O2	AR	O2	N2	AR	O2		R	N2/AR	N2/O2	AR/O2	N2	AR	O2	LIQ	VAP	LIQ
0.0	0.0	0.0	0.0	0.0	0.0	276.4	1.557	1.899	1.219	0.802	1.046	1.002	-940.	1290.	15.2	10.571
0.0	0.01	0.0	0.0121	0.00879	0.0000	276.4	1.559	1.897	1.217	0.802	1.045	1.003	-940.	1284.	15.2	10.546
0.0	0.02	0.0	0.0242	0.01757	0.0000	276.4	1.560	1.896	1.215	0.802	1.045	1.004	-940.	1278.	15.2	10.520
0.0	0.03	0.0	0.0363	0.02634	0.0000	276.4	1.561	1.895	1.213	0.802	1.044	1.005	-940.	1272.	15.2	10.494
0.0	0.04	0.0	0.0484	0.03510	0.0000	276.4	1.562	1.893	1.212	0.802	1.043	1.006	-940.	1266.	15.2	10.472
0.0	0.05	0.0	0.0599	0.04401	0.0000	276.4	1.563	1.892	1.210	0.802	1.042	1.006	-940.	1260.	15.2	10.448
0.0	0.07	0.0	0.0832	0.05468	0.0000	275.9	1.567	1.889	1.206	0.801	1.040	1.008	-940.	1249.	15.2	10.399
0.0	0.10	0.0	0.1177	0.06823	0.0000	275.6	1.571	1.885	1.200	0.801	1.037	1.011	-940.	1232.	15.1	10.320
0.0	0.20	0.0	0.2280	0.13721	0.0000	274.8	1.584	1.871	1.181	0.800	1.029	1.020	-1035.	1179.	15.1	10.180
0.0	0.40	0.0	0.4324	0.26777	0.0000	273.4	1.610	1.839	1.143	0.801	1.015	1.041	-1103.	1082.	14.9	9.670
0.0	0.60	0.0	0.6234	0.37666	0.0000	272.4	1.635	1.804	1.104	0.804	1.005	1.069	-1167.	994.	14.8	9.254
0.0	0.80	0.0	0.8098	0.51902	0.0000	271.7	1.658	1.765	1.065	0.810	1.000	1.103	-1225.	910.	14.7	8.831
0.0	0.90	0.0	0.9039	0.69611	0.0000	271.5	1.689	1.744	1.045	0.814	0.999	1.123	-1253.	869.	14.7	8.620
0.10	0.0	0.1749	0.0	0.0251	0.0000	272.6	1.569	1.908	1.216	0.823	1.072	1.034	-930.	1261.	15.4	10.684
0.10	0.01	0.1729	0.0111	0.0111	0.0000	272.6	1.570	1.907	1.214	0.822	1.070	1.035	-934.	1256.	15.4	10.662
0.10	0.02	0.1708	0.0222	0.0222	0.0000	272.5	1.572	1.905	1.212	0.822	1.069	1.035	-938.	1251.	15.4	10.639
0.10	0.03	0.1688	0.0332	0.0332	0.0000	272.5	1.573	1.904	1.210	0.822	1.068	1.036	-942.	1246.	15.3	10.615
0.10	0.04	0.1668	0.0441	0.0441	0.0000	272.4	1.574	1.902	1.208	0.821	1.066	1.036	-946.	1241.	15.3	10.592
0.10	0.05	0.1648	0.0550	0.0550	0.0000	272.4	1.576	1.901	1.206	0.821	1.065	1.037	-950.	1236.	15.3	10.569
0.10	0.07	0.1608	0.0767	0.0767	0.0000	272.3	1.578	1.898	1.202	0.820	1.063	1.038	-958.	1226.	15.3	10.523
0.10	0.10	0.1549	0.1088	0.1088	0.0000	272.2	1.582	1.893	1.197	0.819	1.059	1.040	-970.	1211.	15.3	10.454
0.10	0.20	0.1358	0.2129	0.0513	0.0000	271.8	1.595	1.877	1.177	0.817	1.048	1.046	-1008.	1164.	15.2	10.299
0.10	0.40	0.1000	0.4117	0.0883	0.0000	271.3	1.618	1.842	1.138	0.813	1.029	1.063	-1082.	1076.	15.0	9.789
0.10	0.60	0.0661	0.6043	0.3294	0.0000	271.0	1.641	1.805	1.100	0.812	1.014	1.084	-1152.	993.	14.9	9.347
0.10	0.80	0.0331	0.7979	0.1689	0.0000	271.0	1.661	1.765	1.063	0.814	1.005	1.112	-1217.	911.	14.7	8.888
0.10	0.90	0.0167	0.8974	0.0859	0.0000	271.1	1.670	1.744	1.044	0.816	1.001	1.128	-1249.	870.	14.7	8.686
0.20	0.0	0.3237	0.0	0.0763	0.0000	271.0	1.581	1.915	1.211	0.842	1.096	1.047	-898.	1233.	15.2	10.826
0.20	0.01	0.3202	0.0102	0.0695	0.0000	271.0	1.582	1.913	1.209	0.841	1.094	1.047	-902.	1229.	15.2	10.803
0.20	0.02	0.3167	0.0204	0.0628	0.0000	271.0	1.583	1.911	1.207	0.841	1.093	1.047	-906.	1225.	15.2	10.780
0.20	0.03	0.3133	0.0306	0.0562	0.0000	271.0	1.585	1.910	1.205	0.840	1.091	1.048	-911.	1220.	15.2	10.757
0.20	0.04	0.3099	0.0407	0.0495	0.0000	271.0	1.586	1.908	1.203	0.840	1.089	1.048	-915.	1216.	15.2	10.735
0.20	0.05	0.3064	0.0508	0.0428	0.0000	271.0	1.587	1.906	1.201	0.839	1.088	1.048	-919.	1212.	15.2	10.712
0.20	0.07	0.2995	0.0709	0.0294	0.0000	271.0	1.589	1.903	1.197	0.838	1.085	1.049	-927.	1203.	15.2	10.667
0.20	0.10	0.2893	0.1089	0.0698	0.0000	271.0	1.593	1.898	1.191	0.836	1.081	1.070	-940.	1191.	15.2	10.600
0.20	0.20	0.2500	0.1994	0.0446	0.0000	271.0	1.605	1.880	1.172	0.832	1.081	1.071	-980.	1149.	15.2	10.437
0.20	0.40	0.1916	0.3927	0.0157	0.0000	271.2	1.627	1.844	1.134	0.825	1.043	1.085	-1060.	1070.	15.1	9.914
0.20	0.60	0.1287	0.5862	0.2851	0.0000	271.7	1.646	1.805	1.096	0.820	1.024	1.100	-1138.	992.	14.9	9.441
0.20	0.80	0.0654	0.7803	0.1461	0.0000	272.4	1.664	1.765	1.061	0.819	1.010	1.120	-1210.	912.	14.8	8.938
0.20	0.90	0.0331	0.8910	0.0759	0.0000	272.8	1.672	1.744	1.043	0.819	1.006	1.132	-1249.	871.	14.7	8.672
0.40	0.0	0.5612	0.0	0.4388	0.0000	272.4	1.602	1.916	1.198	0.876	1.146	1.139	-830.	1180.	16.1	11.192
0.40	0.01	0.5591	0.0080	0.4352	0.0000	272.5	1.603	1.915	1.196	0.877	1.144	1.139	-835.	1177.	16.1	11.168
0.40	0.02	0.5569	0.0175	0.4315	0.0000	272.6	1.604	1.913	1.194	0.876	1.142	1.138	-839.	1174.	16.1	11.144
0.40	0.03	0.5548	0.0263	0.4279	0.0000	272.6	1.605	1.913	1.192	0.875	1.140	1.138	-844.	1171.	16.1	11.120
0.40	0.04	0.5527	0.0351	0.4243	0.0000	272.7	1.607	1.911	1.190	0.874	1.137	1.137	-849.	1168.	16.1	11.095
0.40	0.05	0.5505	0.0438	0.4206	0.0000	272.8	1.609	1.910	1.188	0.873	1.135	1.137	-853.	1165.	16.0	11.071
0.40	0.07	0.5453	0.0614	0.4134	0.0000	272.9	1.610	1.908	1.184	0.872	1.131	1.136	-863.	1159.	16.0	11.022
0.40	0.10	0.5389	0.0878	0.4024	0.0000	273.1	1.613	1.901	1.178	0.869	1.129	1.135	-877.	1150.	15.9	10.948
0.40	0.20	0.4583	0.1744	0.3652	0.0000	273.8	1.624	1.882	1.159	0.862	1.106	1.133	-923.	1119.	15.8	10.699
0.40	0.40	0.3537	0.3588	0.2876	0.0000	275.3	1.643	1.845	1.123	0.848	1.072	1.131	-1015.	1056.	15.4	10.104
0.40	0.60	0.2444	0.5526	0.2010	0.0000	277.1	1.658	1.805	1.089	0.837	1.044	1.133	-1100.	980.	15.1	9.633
0.40	0.80	0.1276	0.7639	0.1685	0.0000	279.0	1.670	1.765	1.056	0.828	1.020	1.130	-1194.	913.	14.8	9.041
0.40	0.90	0.0654	0.8784	0.0853	0.0000	280.1	1.675	1.744	1.041	0.823	1.009	1.141	-1237.	872.	14.7	8.725
0.60	0.0	0.7410	0.0	0.2590	0.0000	276.7	1.617	1.907	1.179	0.914	1.203	1.225	-758.	1136.	16.7	11.670
0.60	0.01	0.7352	0.0076	0.2577	0.0000	276.9	1.618	1.906	1.178	0.913	1.200	1.223	-763.	1132.	16.7	11.641
0.60	0.02	0.7293	0.0153	0.2553	0.0000	277.0	1.620	1.904	1.176	0.911	1.197	1.222	-768.	1128.	16.6	11.612
0.60	0.03	0.7235	0.0230	0.2530	0.0000	277.1	1.621	1.903	1.174	0.910	1.194	1.221	-774.	1124.	16.6	11.583
0.60	0.04	0.7176	0.0307	0.2516	0.0000	277.2	1.622	1.901	1.172	0.909	1.191	1.220	-779.	1120.	16.6	11.554
0.60	0.05	0.7117	0.0385	0.2494	0.0000	277.3	1.623	1.900	1.170	0.908	1.189	1.219	-784.	1116.	16.6	11.525
0.60	0.07	0.6999	0.0540	0.2440	0.0000	277.4	1.625	1.898	1.167	0.906	1.183	1.216	-795.	1116.	16.5	11.466
0.60	0.10	0.6821	0.0776	0.2404	0.0000	277.9	1.629	1.892	1.161	0.902	1.175	1.212	-811.	1109.	16.4	11.370
0.60	0.20	0.6212	0.1570	0.2208	0.0000	279.1	1.639	1.875	1.144	0.892	1.149	1.201	-864.	1058.	16.2	11.083
0.60	0.40	0.4919	0.3300	0.1782	0.0000	281.7	1.656	1.841	1.111	0.872	1.104	1.183	-970.	1040.	15.7	10.476
0.60	0.60	0.3488	0.5224	0.1289	0.0000	284.6	1.669	1.804	1.081	0.855	1.069	1.169	-1074.	984.	15.3	9.834
0.60	0.80	0.1868	0.7427	0.0766	0.0000	287.4	1.677	1.764	1.052	0.837	1.030	1.156	-1178.	914.	14.9	9.145
0.60	0.90	0.0969	0.8660	0.0371	0.0000	289.5	1.678	1.744	1.030	0.828	1.014	1.151	-1229.	873.	14.8	8.770
0.80	0.0	0.8828	0.0	0.1172	0.0000	281.7	1.625	1.891	1.157	0.953	1.271	1.330	-683.	1062.	17.1	12.272
0.80	0.01	0.8767	0.0080	0.1166	0.0000	281.8	1.627	1.890	1.156	0.952	1.267	1.328	-688.	1061.	17.1	12.235
0.80	0.02	0.8706	0.0156	0.1158	0.0000	281.9	1.628	1.889	1.154	0.950	1.263	1.325	-693.	1060.	17.1	12.198
0.80	0.03	0.8645	0.0230	0.1151	0.0000	282.2	1.630	1.887	1.153	0.949	1.260	1.322	-701.	1058.	17.1	12.160
0.80	0.04	0.8583	0.0304	0.1143	0.0000	282.3	1									

PRFSSURE = 10. ATM

Table 25. (cont.)

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION		TEMP R	RELATIVE VOL			PRESSURE ACT COEF			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
N2/N2+O2	AR	N2	AR		O2	N2/AR	N2/O2	AR/O2	N2	AR	O2	LIG	VAP	LIG
0.0	0.0	0.0	0.0	231.3	1.533	1.841	1.703	0.785	1.037	1.002	-887.	1286.	15.8	11.188
0.0	0.01	0.0	0.0179	231.2	1.531	1.839	1.701	0.785	1.037	1.003	-891.	1286.	15.8	11.184
0.0	0.02	0.0	0.0239	231.1	1.532	1.837	1.199	0.785	1.036	1.004	-895.	1274.	15.7	11.148
0.0	0.03	0.0	0.0287	231.0	1.533	1.836	1.197	0.785	1.036	1.005	-899.	1268.	15.7	11.115
0.0	0.04	0.0	0.0329	230.9	1.534	1.834	1.196	0.785	1.034	1.006	-903.	1263.	15.7	11.091
0.0	0.05	0.0	0.0369	230.8	1.535	1.833	1.194	0.785	1.034	1.006	-907.	1257.	15.7	11.068
0.0	0.06	0.0	0.0407	230.7	1.536	1.832	1.193	0.784	1.032	1.008	-911.	1251.	15.7	11.045
0.0	0.07	0.0	0.0443	230.6	1.537	1.831	1.192	0.784	1.030	1.011	-915.	1245.	15.7	11.022
0.0	0.08	0.0	0.0478	230.5	1.538	1.830	1.191	0.784	1.028	1.014	-919.	1239.	15.6	10.999
0.0	0.09	0.0	0.0512	230.4	1.539	1.829	1.190	0.784	1.026	1.017	-923.	1233.	15.6	10.976
0.0	0.10	0.0	0.0545	230.3	1.540	1.828	1.189	0.784	1.024	1.020	-927.	1227.	15.6	10.953
0.0	0.11	0.0	0.0578	230.2	1.541	1.827	1.188	0.784	1.022	1.023	-931.	1221.	15.6	10.930
0.0	0.12	0.0	0.0610	230.1	1.542	1.826	1.187	0.784	1.020	1.026	-935.	1215.	15.5	10.907
0.0	0.13	0.0	0.0642	230.0	1.543	1.825	1.186	0.784	1.018	1.029	-939.	1209.	15.5	10.884
0.0	0.14	0.0	0.0673	229.9	1.544	1.824	1.185	0.784	1.016	1.032	-943.	1203.	15.5	10.861
0.0	0.15	0.0	0.0704	229.8	1.545	1.823	1.184	0.784	1.014	1.035	-947.	1197.	15.5	10.838
0.0	0.16	0.0	0.0735	229.7	1.546	1.822	1.183	0.784	1.012	1.038	-951.	1191.	15.5	10.815
0.0	0.17	0.0	0.0765	229.6	1.547	1.821	1.182	0.784	1.010	1.041	-955.	1185.	15.4	10.792
0.0	0.18	0.0	0.0795	229.5	1.548	1.820	1.181	0.784	1.008	1.044	-959.	1179.	15.4	10.769
0.0	0.19	0.0	0.0825	229.4	1.549	1.819	1.180	0.784	1.006	1.047	-963.	1173.	15.4	10.746
0.0	0.20	0.0	0.0855	229.3	1.550	1.818	1.179	0.784	1.004	1.050	-967.	1167.	15.4	10.723
0.0	0.21	0.0	0.0885	229.2	1.551	1.817	1.178	0.784	1.002	1.053	-971.	1161.	15.4	10.700
0.0	0.22	0.0	0.0915	229.1	1.552	1.816	1.177	0.784	1.000	1.056	-975.	1155.	15.4	10.677
0.0	0.23	0.0	0.0945	229.0	1.553	1.815	1.176	0.784	0.998	1.059	-979.	1149.	15.4	10.654
0.0	0.24	0.0	0.0975	228.9	1.554	1.814	1.175	0.784	0.996	1.062	-983.	1143.	15.4	10.631
0.0	0.25	0.0	0.1005	228.8	1.555	1.813	1.174	0.784	0.994	1.065	-987.	1137.	15.4	10.608
0.0	0.26	0.0	0.1035	228.7	1.556	1.812	1.173	0.784	0.992	1.068	-991.	1131.	15.4	10.585
0.0	0.27	0.0	0.1065	228.6	1.557	1.811	1.172	0.784	0.990	1.071	-995.	1125.	15.4	10.562
0.0	0.28	0.0	0.1095	228.5	1.558	1.810	1.171	0.784	0.988	1.074	-999.	1119.	15.4	10.539
0.0	0.29	0.0	0.1125	228.4	1.559	1.809	1.170	0.784	0.986	1.077	-1003.	1113.	15.4	10.516
0.0	0.30	0.0	0.1155	228.3	1.560	1.808	1.169	0.784	0.984	1.080	-1007.	1107.	15.4	10.493
0.0	0.31	0.0	0.1185	228.2	1.561	1.807	1.168	0.784	0.982	1.083	-1011.	1101.	15.4	10.470
0.0	0.32	0.0	0.1215	228.1	1.562	1.806	1.167	0.784	0.980	1.086	-1015.	1095.	15.4	10.447
0.0	0.33	0.0	0.1245	228.0	1.563	1.805	1.166	0.784	0.978	1.089	-1019.	1089.	15.4	10.424
0.0	0.34	0.0	0.1275	227.9	1.564	1.804	1.165	0.784	0.976	1.092	-1023.	1083.	15.4	10.401
0.0	0.35	0.0	0.1305	227.8	1.565	1.803	1.164	0.784	0.974	1.095	-1027.	1077.	15.4	10.378
0.0	0.36	0.0	0.1335	227.7	1.566	1.802	1.163	0.784	0.972	1.098	-1031.	1071.	15.4	10.355
0.0	0.37	0.0	0.1365	227.6	1.567	1.801	1.162	0.784	0.970	1.101	-1035.	1065.	15.4	10.332
0.0	0.38	0.0	0.1395	227.5	1.568	1.800	1.161	0.784	0.968	1.104	-1039.	1059.	15.4	10.309
0.0	0.39	0.0	0.1425	227.4	1.569	1.799	1.160	0.784	0.966	1.107	-1043.	1053.	15.4	10.286
0.0	0.40	0.0	0.1455	227.3	1.570	1.798	1.159	0.784	0.964	1.110	-1047.	1047.	15.4	10.263
0.0	0.41	0.0	0.1485	227.2	1.571	1.797	1.158	0.784	0.962	1.113	-1051.	1041.	15.4	10.240
0.0	0.42	0.0	0.1515	227.1	1.572	1.796	1.157	0.784	0.960	1.116	-1055.	1035.	15.4	10.217
0.0	0.43	0.0	0.1545	227.0	1.573	1.795	1.156	0.784	0.958	1.119	-1059.	1029.	15.4	10.194
0.0	0.44	0.0	0.1575	226.9	1.574	1.794	1.155	0.784	0.956	1.122	-1063.	1023.	15.4	10.171
0.0	0.45	0.0	0.1605	226.8	1.575	1.793	1.154	0.784	0.954	1.125	-1067.	1017.	15.4	10.148
0.0	0.46	0.0	0.1635	226.7	1.576	1.792	1.153	0.784	0.952	1.128	-1071.	1011.	15.4	10.125
0.0	0.47	0.0	0.1665	226.6	1.577	1.791	1.152	0.784	0.950	1.131	-1075.	1005.	15.4	10.102
0.0	0.48	0.0	0.1695	226.5	1.578	1.790	1.151	0.784	0.948	1.134	-1079.	999.	15.4	10.079
0.0	0.49	0.0	0.1725	226.4	1.579	1.789	1.150	0.784	0.946	1.137	-1083.	993.	15.4	10.056
0.0	0.50	0.0	0.1755	226.3	1.580	1.788	1.149	0.784	0.944	1.140	-1087.	987.	15.4	10.033
0.0	0.51	0.0	0.1785	226.2	1.581	1.787	1.148	0.784	0.942	1.143	-1091.	981.	15.4	10.010
0.0	0.52	0.0	0.1815	226.1	1.582	1.786	1.147	0.784	0.940	1.146	-1095.	975.	15.4	9.987
0.0	0.53	0.0	0.1845	226.0	1.583	1.785	1.146	0.784	0.938	1.149	-1099.	969.	15.4	9.964
0.0	0.54	0.0	0.1875	225.9	1.584	1.784	1.145	0.784	0.936	1.152	-1103.	963.	15.4	9.941
0.0	0.55	0.0	0.1905	225.8	1.585	1.783	1.144	0.784	0.934	1.155	-1107.	957.	15.4	9.918
0.0	0.56	0.0	0.1935	225.7	1.586	1.782	1.143	0.784	0.932	1.158	-1111.	951.	15.4	9.895
0.0	0.57	0.0	0.1965	225.6	1.587	1.781	1.142	0.784	0.930	1.161	-1115.	945.	15.4	9.872
0.0	0.58	0.0	0.1995	225.5	1.588	1.780	1.141	0.784	0.928	1.164	-1119.	939.	15.4	9.849
0.0	0.59	0.0	0.2025	225.4	1.589	1.779	1.140	0.784	0.926	1.167	-1123.	933.	15.4	9.826
0.0	0.60	0.0	0.2055	225.3	1.590	1.778	1.139	0.784	0.924	1.170	-1127.	927.	15.4	9.803
0.0	0.61	0.0	0.2085	225.2	1.591	1.777	1.138	0.784	0.922	1.173	-1131.	921.	15.4	9.780
0.0	0.62	0.0	0.2115	225.1	1.592	1.776	1.137	0.784	0.920	1.176	-1135.	915.	15.4	9.757
0.0	0.63	0.0	0.2145	225.0	1.593	1.775	1.136	0.784	0.918	1.179	-1139.	909.	15.4	9.734
0.0	0.64	0.0	0.2175	224.9	1.594	1.774	1.135	0.784	0.916	1.182	-1143.	903.	15.4	9.711
0.0	0.65	0.0	0.2205	224.8	1.595	1.773	1.134	0.784	0.914	1.185	-1147.	897.	15.4	9.688
0.0	0.66	0.0	0.2235	224.7	1.596	1.772	1.133	0.784	0.912	1.188	-1151.	891.	15.4	9.665
0.0	0.67	0.0	0.2265	224.6	1.597	1.771	1.132	0.784	0.910	1.191	-1155.	885.	15.4	9.642
0.0	0.68	0.0	0.2295	224.5	1.598	1.770	1.131	0.784	0.908	1.194	-1159.	879.	15.4	9.619
0.0	0.69	0.0	0.2325	224.4	1.599	1.769	1.130	0.784	0.906	1.197	-1163.	873.	15.4	9.596
0.0	0.70	0.0	0.2355	224.3	1.600	1.768	1.129	0.784	0.904	1.200	-1167.	867.	15.4	9.573
0.0	0.71	0.0	0.2385	224.2	1.601	1.767	1.128	0.784	0.902	1.203	-1171.	861.	15.4	9.550
0.0	0.72	0.0	0.2415	224.1	1.602	1.766	1.127	0.784	0.900	1.206	-1175.	855.	15.4	9.527
0.0	0.73	0.0	0.2445	224.0	1.603	1.765	1.126	0.784	0.898	1.209	-1179.	849.	15.4	9.504
0.0	0.74	0.0	0.2475	223.9	1.604	1.764	1.125	0.784	0.896	1.212	-1183.	843.	15.4	9.481
0.0	0.75	0.0	0.2505	223.8	1.605	1.763	1.124	0.784	0.894	1.215	-1187.	837.	15.4	9.458
0.0	0.76	0.0	0.2535	223.7	1.606	1.762	1.123	0.784	0.892	1.218	-1191.	831.	15.4	9.435
0.0	0.77	0.0	0.2565	223.6	1.607	1.761	1.122	0.784	0.890	1.221	-1195.	825.	15.4	9.412
0.0	0.78	0.0	0.2595	223.5	1.608	1.760	1.121	0.784	0.888	1.224	-1199.	819.	15.4	9.389
0.0	0.79	0.0	0.2625	223.4	1.609	1.759	1.120	0.784	0.886	1.227	-1203.	813.	15.4	9.366
0.0	0.80	0.0	0.2655	223.3	1.610	1.758	1.119	0.784	0.884	1.230	-1207.	807.	15.4	9.343
0.0	0.81	0.0	0.2685											



Table 25. (cont.)

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION		TEMP	RELATIVE VOL			PRESSURE ACT COEF			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LH MOLE-R		
N2/N2+O2	A4	N2	A4		O	N2/A4	N2/O2	A4/O2	N2	A4	O2	LIQ	VAP	LIQ	VAP
0.	0.	0.	0.	1.0000	235.5	1.913	1.799	1.189	0.772	1.030	1.002	-819.	1280.	16.3	11.876
0.	0.01	0.	0.0118	0.9882	235.4	1.914	1.798	1.187	0.772	1.029	1.003	-823.	1274.	16.3	11.855
0.	0.02	0.	0.0236	0.9764	235.1	1.915	1.796	1.185	0.772	1.028	1.003	-827.	1268.	16.3	11.831
0.	0.03	0.	0.0353	0.9647	235.2	1.916	1.795	1.184	0.772	1.028	1.004	-831.	1262.	16.3	11.807
0.	0.04	0.	0.0469	0.9531	235.1	1.917	1.793	1.182	0.772	1.027	1.005	-835.	1256.	16.3	11.784
0.	0.05	0.	0.0585	0.9415	235.0	1.918	1.792	1.180	0.772	1.026	1.006	-839.	1250.	16.2	11.761
0.	0.07	0.	0.0814	0.9186	234.9	1.919	1.788	1.177	0.772	1.025	1.008	-847.	1238.	16.2	11.715
0.	0.10	0.	0.1152	0.8848	234.6	1.922	1.784	1.172	0.772	1.023	1.011	-858.	1221.	16.2	11.646
0.	0.20	0.	0.2241	0.7760	233.7	1.930	1.767	1.155	0.771	1.017	1.020	-896.	1167.	16.1	11.425
0.	0.30	0.	0.4276	0.5725	232.4	1.948	1.734	1.121	0.771	1.007	1.042	-966.	1067.	15.9	11.001
0.	0.40	0.	0.6196	0.3804	231.4	1.968	1.699	1.086	0.774	0.999	1.049	-1030.	975.	15.7	10.581
0.	0.50	0.	0.8078	0.1922	230.7	1.991	1.662	1.051	0.778	0.995	1.101	-1089.	886.	15.7	10.143
0.	0.60	0.	0.9209	0.0971	230.5	1.989	1.643	1.034	0.782	0.995	1.119	-1117.	845.	15.6	9.912
0.10	0.	0.1661	0.	0.8339	231.5	1.913	1.793	1.189	0.793	1.039	1.038	-790.	1250.	16.2	12.057
0.10	0.01	0.1644	0.0110	0.8249	231.4	1.914	1.791	1.183	0.793	1.038	1.039	-794.	1244.	16.2	12.044
0.10	0.02	0.1623	0.0219	0.8159	231.4	1.915	1.790	1.182	0.792	1.037	1.039	-798.	1238.	16.2	12.021
0.10	0.03	0.1604	0.0327	0.8070	231.3	1.916	1.788	1.180	0.792	1.036	1.040	-802.	1232.	16.2	12.001
0.10	0.04	0.1585	0.0435	0.7981	231.3	1.917	1.787	1.178	0.792	1.035	1.040	-807.	1226.	16.2	11.975
0.10	0.05	0.1566	0.0543	0.7892	231.2	1.918	1.785	1.176	0.791	1.034	1.041	-811.	1224.	16.2	11.952
0.10	0.07	0.1528	0.0757	0.7715	231.2	1.920	1.782	1.173	0.791	1.032	1.042	-819.	1214.	16.2	11.906
0.10	0.10	0.1472	0.1075	0.7453	231.0	1.922	1.778	1.168	0.790	1.029	1.044	-831.	1199.	16.1	11.838
0.10	0.20	0.1292	0.2109	0.6599	230.7	1.932	1.762	1.150	0.787	1.020	1.050	-870.	1150.	16.1	11.612
0.10	0.30	0.0952	0.4065	0.4953	230.2	1.950	1.730	1.116	0.784	1.023	1.066	-945.	1050.	15.9	11.162
0.10	0.40	0.0630	0.6026	0.3342	229.9	1.967	1.695	1.082	0.782	1.018	1.086	-1015.	973.	15.8	10.698
0.10	0.50	0.0315	0.7974	0.1711	229.8	1.983	1.660	1.049	0.783	1.011	1.110	-1081.	889.	15.7	10.265
0.10	0.60	0.0159	0.8972	0.0869	229.8	1.990	1.642	1.032	0.784	0.998	1.124	-1113.	848.	15.6	9.944
0.20	0.	0.3089	0.	0.6911	227.8	1.918	1.787	1.180	0.812	1.088	1.075	-757.	1221.	16.3	12.268
0.20	0.01	0.3055	0.0102	0.6843	227.8	1.918	1.786	1.178	0.812	1.087	1.075	-761.	1216.	16.3	12.265
0.20	0.02	0.3022	0.0203	0.6774	227.8	1.917	1.785	1.177	0.811	1.085	1.076	-765.	1212.	16.3	12.242
0.20	0.03	0.2989	0.0305	0.6706	227.8	1.918	1.783	1.175	0.811	1.084	1.076	-770.	1207.	16.3	12.219
0.20	0.04	0.2956	0.0406	0.6638	227.8	1.919	1.782	1.173	0.810	1.082	1.076	-774.	1203.	16.3	12.195
0.20	0.05	0.2924	0.0506	0.6570	227.8	1.920	1.780	1.171	0.810	1.081	1.076	-779.	1198.	16.3	12.172
0.20	0.07	0.2859	0.0707	0.6434	227.8	1.922	1.777	1.168	0.809	1.078	1.077	-787.	1188.	16.3	12.123
0.20	0.10	0.2762	0.1008	0.6232	227.8	1.925	1.772	1.163	0.807	1.074	1.078	-800.	1177.	16.2	12.055
0.20	0.20	0.2444	0.1992	0.5565	227.8	1.934	1.757	1.145	0.803	1.062	1.081	-842.	1134.	16.1	11.820
0.20	0.30	0.1824	0.3929	0.4242	226.1	1.952	1.725	1.112	0.796	1.040	1.090	-922.	1052.	16.0	11.332
0.20	0.40	0.1228	0.5875	0.2922	226.6	1.969	1.692	1.079	0.791	1.021	1.103	-1000.	971.	15.8	10.818
0.20	0.50	0.0623	0.7873	0.1594	226.3	1.984	1.658	1.047	0.788	1.007	1.120	-1073.	889.	15.7	10.268
0.20	0.60	0.0315	0.8916	0.0768	226.8	1.993	1.641	1.031	0.787	1.001	1.129	-1109.	846.	15.6	9.976
0.40	0.	0.5420	0.	0.4580	221.2	1.921	1.775	1.167	0.851	1.147	1.155	-685.	1165.	16.8	12.752
0.40	0.01	0.5369	0.0089	0.4463	221.3	1.922	1.773	1.166	0.850	1.144	1.154	-690.	1162.	16.8	12.834
0.40	0.02	0.5319	0.0178	0.4363	221.4	1.923	1.772	1.164	0.849	1.142	1.154	-695.	1158.	16.8	12.807
0.40	0.03	0.5269	0.0267	0.4264	221.4	1.924	1.771	1.162	0.848	1.140	1.153	-700.	1155.	16.7	12.779
0.40	0.04	0.5219	0.0357	0.4165	221.5	1.925	1.769	1.160	0.848	1.138	1.153	-704.	1152.	16.7	12.751
0.40	0.05	0.5169	0.0446	0.4066	221.6	1.926	1.768	1.159	0.847	1.136	1.152	-709.	1149.	16.7	12.723
0.40	0.07	0.5068	0.0624	0.3908	221.7	1.928	1.765	1.155	0.845	1.132	1.152	-719.	1142.	16.7	12.668
0.40	0.10	0.4918	0.0892	0.3690	221.9	1.931	1.761	1.150	0.843	1.126	1.150	-733.	1133.	16.6	12.603
0.40	0.20	0.4415	0.1792	0.3293	222.6	1.940	1.746	1.134	0.835	1.107	1.147	-781.	1101.	16.8	12.497
0.40	0.30	0.3397	0.3034	0.2969	224.2	1.958	1.716	1.104	0.821	1.074	1.142	-876.	1035.	16.2	11.702
0.40	0.40	0.2340	0.5578	0.2083	226.0	1.973	1.685	1.071	0.808	1.044	1.139	-968.	965.	15.9	11.070
0.40	0.50	0.1218	0.7878	0.1104	226.0	1.986	1.654	1.043	0.797	1.018	1.139	-1057.	889.	15.7	10.396
0.40	0.60	0.0523	0.8887	0.0578	226.1	1.992	1.639	1.029	0.791	1.007	1.139	-1108.	847.	15.7	10.080
0.60	0.	0.7249	0.	0.2751	215.4	1.927	1.757	1.171	0.892	1.213	1.248	-610.	1110.	17.4	13.451
0.60	0.01	0.7199	0.0079	0.2731	215.6	1.928	1.755	1.169	0.891	1.210	1.247	-615.	1108.	17.3	13.413
0.60	0.02	0.7131	0.0159	0.2710	215.7	1.929	1.754	1.167	0.890	1.207	1.246	-621.	1106.	17.3	13.375
0.60	0.03	0.7072	0.0238	0.2689	215.8	1.930	1.753	1.166	0.888	1.204	1.244	-626.	1104.	17.3	13.337
0.60	0.04	0.7013	0.0318	0.2669	215.9	1.931	1.752	1.164	0.887	1.201	1.243	-632.	1102.	17.3	13.299
0.60	0.05	0.6954	0.0398	0.2648	216.0	1.932	1.750	1.163	0.886	1.198	1.241	-637.	1099.	17.3	13.261
0.60	0.07	0.6834	0.0599	0.2487	216.3	1.934	1.746	1.160	0.883	1.192	1.239	-648.	1095.	17.2	13.205
0.60	0.10	0.6655	0.0802	0.2343	216.6	1.937	1.744	1.155	0.880	1.184	1.234	-665.	1089.	17.1	13.171
0.60	0.20	0.6045	0.1628	0.2127	217.9	1.947	1.732	1.120	0.868	1.158	1.221	-719.	1046.	16.9	12.889
0.60	0.30	0.4759	0.3361	0.1806	220.5	1.964	1.706	1.091	0.846	1.110	1.198	-828.	1018.	16.9	12.121
0.60	0.40	0.3354	0.5313	0.1332	223.5	1.978	1.678	1.063	0.826	1.068	1.177	-939.	958.	16.1	11.338
0.60	0.50	0.1766	0.7493	0.0721	226.7	1.989	1.650	1.039	0.808	1.030	1.158	-1041.	886.	15.8	10.526
0.60	0.60	0.0924	0.8700	0.0376	226.5	1.993	1.637	1.027	0.796	1.013	1.149	-1092.	846.	15.7	10.185
0.80	0.	0.8738	0.	0.1262	216.2	1.931	1.751	1.131	0.930	1.202	1.364	-534.	1055.	17.9	14.752
0.80	0.01	0.8679	0.0072	0.1253	216.3	1.932	1.750	1.130	0.927	1.200	1.361	-540.	1054.	17.9	14.693
0.80	0.02	0.8612	0.0143</												

Table 25. (cont.)

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION			TEMP	RELATIVE VOL				PRESSURE COR COEF			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
N <sub>2</sub> /N <sub>2</sub> +O <sub>2</sub>	AR	N <sub>2</sub>	AR	O <sub>2</sub>		N	N <sub>2</sub> /AR	N <sub>2</sub> /O <sub>2</sub>	AR/O <sub>2</sub>	N <sub>2</sub>	AR	O <sub>2</sub>	LIG	VAP	LIG	VAP
0.0	0.0	0.0	0.0	1.0000	234.5	1.507	1.774	1.178	0.784	1.023	1.001	-753.	1271.	16.9	12.659	
0.0	0.01	0.0	0.0117	0.9883	234.4	1.507	1.773	1.176	0.784	1.023	1.002	-757.	1265.	16.9	12.636	
0.0	0.02	0.0	0.0234	0.9766	234.3	1.508	1.771	1.174	0.784	1.022	1.003	-762.	1259.	16.9	12.613	
0.0	0.03	0.0	0.0351	0.9650	234.2	1.509	1.769	1.173	0.784	1.022	1.004	-766.	1252.	16.9	12.591	
0.0	0.04	0.0	0.0468	0.9535	234.1	1.509	1.767	1.171	0.784	1.021	1.005	-770.	1246.	16.8	12.568	
0.0	0.05	0.0	0.0585	0.9420	234.0	1.510	1.766	1.170	0.784	1.020	1.006	-774.	1241.	16.8	12.546	
0.0	0.07	0.0	0.0807	0.9193	233.8	1.511	1.762	1.166	0.784	1.019	1.008	-782.	1229.	16.8	12.501	
0.0	0.10	0.0	0.1143	0.8857	233.6	1.513	1.757	1.161	0.783	1.018	1.011	-794.	1211.	16.7	12.435	
0.0	0.20	0.0	0.2226	0.7779	233.7	1.519	1.739	1.145	0.783	1.013	1.021	-832.	1156.	16.6	12.220	
0.0	0.30	0.0	0.4258	0.5743	233.3	1.532	1.704	1.112	0.782	1.004	1.043	-903.	1055.	16.4	11.802	
0.0	0.40	0.0	0.6181	0.3819	233.3	1.546	1.658	1.079	0.784	0.997	1.069	-967.	962.	16.2	11.378	
0.0	0.50	0.0	0.8071	0.1929	234.6	1.569	1.631	1.046	0.789	0.994	1.100	-1036.	874.	16.1	10.930	
0.0	0.60	0.0	0.9726	0.0194	234.4	1.597	1.613	1.020	0.772	0.994	1.131	-1094.	811.	16.1	10.691	
0.10	0.01	0.1635	0.0169	0.9831	235.3	1.499	1.759	1.173	0.784	1.023	1.001	-727.	1239.	16.7	12.913	
0.10	0.02	0.1597	0.0217	0.9783	235.2	1.501	1.756	1.171	0.784	1.023	1.001	-731.	1233.	16.7	12.890	
0.10	0.03	0.1578	0.0265	0.9735	235.2	1.502	1.754	1.168	0.783	1.022	1.002	-735.	1228.	16.7	12.867	
0.10	0.04	0.1560	0.0312	0.9687	235.1	1.503	1.753	1.166	0.783	1.021	1.003	-739.	1223.	16.7	12.844	
0.10	0.05	0.1541	0.0359	0.9639	235.1	1.503	1.751	1.165	0.783	1.021	1.003	-744.	1218.	16.7	12.821	
0.10	0.07	0.1504	0.0472	0.9544	235.1	1.505	1.748	1.161	0.782	1.020	1.004	-748.	1213.	16.6	12.798	
0.10	0.10	0.1449	0.0608	0.9402	234.9	1.507	1.743	1.157	0.781	1.020	1.005	-756.	1202.	16.6	12.753	
0.10	0.20	0.1272	0.2099	0.8028	234.5	1.515	1.728	1.137	0.781	1.016	1.046	-788.	1167.	16.6	12.604	
0.10	0.30	0.0938	0.4084	0.4978	234.1	1.531	1.689	1.108	0.779	1.017	1.053	-807.	1139.	16.5	12.456	
0.10	0.40	0.0620	0.6021	0.3359	233.9	1.546	1.652	1.075	0.775	1.009	1.066	-882.	1047.	16.3	11.999	
0.10	0.50	0.0311	0.7971	0.1718	233.9	1.560	1.625	1.042	0.773	1.009	1.067	-953.	959.	16.2	11.519	
0.10	0.60	0.0159	0.8971	0.0173	234.1	1.567	1.611	1.020	0.774	0.997	1.123	-1019.	874.	16.1	11.003	
0.20	0.0	0.3346	0.0	0.6654	231.6	1.494	1.747	1.168	0.804	1.026	1.020	-699.	1209.	16.7	13.200	
0.20	0.01	0.3299	0.0101	0.6898	231.6	1.497	1.745	1.166	0.803	1.025	1.020	-699.	1209.	16.7	13.176	
0.20	0.02	0.3249	0.0203	0.7143	231.6	1.498	1.744	1.165	0.803	1.024	1.020	-703.	1204.	16.7	13.153	
0.20	0.03	0.3200	0.0304	0.7388	231.6	1.499	1.743	1.163	0.802	1.023	1.021	-708.	1199.	16.7	13.129	
0.20	0.04	0.3151	0.0404	0.7633	231.6	1.499	1.741	1.161	0.802	1.021	1.021	-712.	1194.	16.7	13.105	
0.20	0.05	0.3102	0.0505	0.7878	231.6	1.500	1.740	1.160	0.801	1.020	1.021	-716.	1189.	16.7	13.081	
0.20	0.07	0.3053	0.0705	0.8123	231.6	1.502	1.737	1.156	0.800	1.020	1.022	-720.	1184.	16.6	13.057	
0.20	0.10	0.2919	0.1004	0.8368	231.6	1.505	1.732	1.151	0.799	1.023	1.022	-728.	1164.	16.6	12.961	
0.20	0.20	0.2467	0.1988	0.8039	231.6	1.514	1.718	1.135	0.794	1.021	1.025	-779.	1121.	16.4	12.710	
0.20	0.30	0.1912	0.3926	0.4772	231.9	1.530	1.688	1.103	0.787	1.020	1.024	-866.	1038.	16.5	12.207	
0.20	0.40	0.121	0.5879	0.2921	232.5	1.546	1.657	1.072	0.782	1.021	1.026	-938.	956.	16.2	11.664	
0.20	0.50	0.0519	0.7874	0.1512	233.2	1.560	1.625	1.042	0.778	1.020	1.120	-1011.	873.	16.1	11.277	
0.20	0.60	0.0151	0.8918	0.0172	233.7	1.567	1.610	1.027	0.774	1.020	1.120	-1048.	831.	16.1	10.765	
0.40	0.0	0.5346	0.0	0.4654	225.0	1.494	1.725	1.195	0.843	1.144	1.164	-643.	1151.	17.1	13.932	
0.40	0.01	0.5299	0.0101	0.4898	225.1	1.495	1.724	1.193	0.842	1.144	1.163	-648.	1146.	17.1	13.909	
0.40	0.02	0.5249	0.0203	0.5143	225.1	1.496	1.722	1.192	0.841	1.144	1.163	-653.	1141.	17.1	13.882	
0.40	0.03	0.5200	0.0304	0.5388	225.2	1.497	1.721	1.190	0.840	1.142	1.162	-658.	1136.	17.1	13.854	
0.40	0.04	0.5151	0.0404	0.5633	225.3	1.498	1.720	1.188	0.839	1.140	1.162	-663.	1131.	17.0	13.811	
0.40	0.05	0.5102	0.0505	0.5878	225.3	1.499	1.719	1.187	0.838	1.138	1.161	-668.	1126.	17.0	13.781	
0.40	0.07	0.5053	0.0705	0.6123	225.5	1.501	1.716	1.183	0.837	1.137	1.160	-673.	1121.	17.0	13.750	
0.40	0.10	0.4919	0.1004	0.6368	225.7	1.504	1.712	1.179	0.834	1.136	1.159	-678.	1116.	16.9	13.720	
0.40	0.20	0.4356	0.1989	0.5845	226.4	1.513	1.699	1.163	0.828	1.131	1.154	-719.	1086.	16.8	13.628	
0.40	0.30	0.335	0.3947	0.3003	228.0	1.531	1.673	1.131	0.812	1.025	1.148	-814.	1019.	16.5	13.315	
0.40	0.40	0.2307	0.5942	0.2107	229.0	1.547	1.646	1.094	0.799	1.023	1.143	-886.	949.	16.3	12.866	
0.40	0.50	0.1209	0.7899	0.1111	231.9	1.561	1.620	1.058	0.787	1.020	1.140	-958.	874.	16.3	11.967	
0.40	0.60	0.0514	0.8918	0.0173	233.7	1.568	1.607	1.025	0.781	1.020	1.138	-1030.	831.	16.1	11.227	
0.60	0.0	0.7189	0.0	0.2811	219.2	1.494	1.701	1.136	0.888	1.219	1.262	-545.	1094.	17.7	14.962	
0.60	0.01	0.7126	0.0101	0.2794	219.3	1.495	1.700	1.137	0.884	1.218	1.260	-550.	1092.	17.6	14.917	
0.60	0.02	0.7062	0.0203	0.2773	219.4	1.496	1.699	1.136	0.883	1.218	1.259	-556.	1089.	17.6	14.872	
0.60	0.03	0.7000	0.0304	0.2751	219.5	1.497	1.698	1.134	0.881	1.218	1.257	-561.	1087.	17.6	14.827	
0.60	0.04	0.6948	0.0404	0.2729	219.6	1.498	1.697	1.133	0.880	1.217	1.256	-567.	1085.	17.6	14.782	
0.60	0.05	0.6889	0.0505	0.2708	219.6	1.499	1.696	1.131	0.879	1.216	1.254	-572.	1083.	17.5	14.738	
0.60	0.07	0.6777	0.0705	0.2686	219.6	1.502	1.694	1.128	0.878	1.216	1.251	-578.	1080.	17.5	14.694	
0.60	0.10	0.6599	0.1004	0.2599	219.6	1.505	1.691	1.124	0.872	1.216	1.246	-588.	1072.	17.4	14.514	
0.60	0.20	0.5981	0.1984	0.2373	221.6	1.525	1.661	1.109	0.860	1.163	1.232	-655.	1049.	17.2	14.068	
0.60	0.30	0.4701	0.3949	0.1800	224.3	1.543	1.636	1.082	0.838	1.114	1.206	-765.	999.	16.8	13.181	
0.60	0.40	0.3319	0.5943	0.1348	227.3	1.568	1.636	1.057	0.817	1.071	1.192	-873.	941.	16.5	12.200	
0.60	0.50	0.1760	0.7913	0.0727	230.6	1.582	1.614	1.034	0.796	1.031	1.180	-978.	871.	16.2	11.301	
0.60	0.60	0.0511	0.8911	0.0179	233.4	1.588	1.604	1.023	0.786	1.031	1.149	-1030.	831.	16.1	10.915	
0.80	0.0	0.8706	0.0	0.1294	213.8	1.494	1.673	1.120	0.935	1.304	1.383	-468.	1039.	18.3	16.482	
0.80	0.01	0.8636	0.0101	0.1292	214.0	1.495	1.673	1.118	0.933	1.299	1.380	-474.	1034.	18.2	16.435	
0.80	0.02	0.8572	0.0203	0.1273	214.1	1.497	1.672	1.117	0.931	1.295	1.376	-481.	1033.	18.2	16.328	
0.80	0.03	0.8508	0.0304	0.1254	214.3	1.498	1.671	1.116	0.929	1.291	1.373	-487.	1031.	18.2	16.283	
0.80	0.04	0.8443	0.0404	0.1235	214.5	1.499	1.671	1.115	0.927	1.287	1.370	-493.	1030.	18.1	16.178	
0.80	0.05	0.8378	0.0505	0.1216	214.6	1.500	1.670	1.113	0.925	1.283	1.367	-499.	1029.	18.1	16.133	
0.80	0.07	0.8248	0.0705	0.1204	215.0	1.502	1.669	1.111	0.923	1.274	1.361	-511.	1027.	18.0	15.956	
0.80	0.10	0.8050	0.1004	0.1204	215.5	1.508	1.666	1.107	0.916	1.262	1.352	-530.	1023.	18.0	15.746	
0.80	0.20	0.7370	0.1984	0.1111	217.2	1.516	1.659	1.094	0.898	1.224	1.323	-592.	1010.	17.7	15.050	
0.80	0.30	0.5989	0.3023	0.0894	220.9	1.535	1.643	1.071	0.880	1.157	1.275	-716.	977.	17.1	13.792	
0.80	0.40															

Table 25. (cont.)

LIQUID MOLE FRACTION				VAPOR MOLE FRACTION			TEMP	RELATIVE VOL			PRESSURE ACT COEF			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE	
N <sub>2</sub> /N <sub>2</sub> +O <sub>2</sub>	AR	O <sub>2</sub>	N <sub>2</sub>	AR	O <sub>2</sub>	R		N <sub>2</sub> /AR	N <sub>2</sub> /O <sub>2</sub>	AR/O <sub>2</sub>	N <sub>2</sub>	AR	O <sub>2</sub>	LIG	VAP	LIG	VAP
0.0	0.0	1.0000	0.0	0.0	1.0000	244.9	1.512	1.766	1.154	0.758	1.016	1.000	-659.	1252.	17.8	14.058	
0.0	0.01	0.9894	0.0110	0.0110	0.9894	244.8	1.513	1.768	1.152	0.758	1.013	1.001	-664.	1246.	17.8	14.057	
0.0	0.02	0.9786	0.0231	0.0231	0.9786	244.7	1.513	1.768	1.150	0.758	1.013	1.002	-668.	1240.	17.8	14.056	
0.0	0.03	0.9679	0.0346	0.0346	0.9679	244.6	1.513	1.768	1.148	0.758	1.014	1.003	-672.	1233.	17.8	14.055	
0.0	0.04	0.9574	0.0460	0.0460	0.9574	244.5	1.513	1.768	1.146	0.758	1.014	1.004	-676.	1227.	17.7	14.054	
0.0	0.05	0.9470	0.0574	0.0574	0.9470	244.4	1.513	1.768	1.144	0.758	1.014	1.005	-680.	1221.	17.7	14.053	
0.0	0.06	0.9367	0.0688	0.0688	0.9367	244.3	1.514	1.768	1.142	0.758	1.013	1.006	-684.	1215.	17.7	14.052	
0.0	0.07	0.9264	0.0802	0.0802	0.9264	244.2	1.514	1.768	1.140	0.757	1.012	1.007	-688.	1209.	17.6	14.051	
0.0	0.08	0.9161	0.0916	0.0916	0.9161	244.1	1.514	1.768	1.138	0.757	1.012	1.008	-692.	1203.	17.6	14.050	
0.0	0.09	0.9058	0.1030	0.1030	0.9058	244.0	1.514	1.768	1.136	0.757	1.011	1.009	-696.	1197.	17.6	14.049	
0.0	0.10	0.8955	0.1144	0.1144	0.8955	243.9	1.514	1.768	1.134	0.757	1.011	1.010	-700.	1191.	17.6	14.048	
0.0	0.11	0.8852	0.1258	0.1258	0.8852	243.8	1.514	1.768	1.132	0.757	1.010	1.011	-704.	1185.	17.6	14.047	
0.0	0.12	0.8749	0.1372	0.1372	0.8749	243.7	1.514	1.768	1.130	0.757	1.010	1.012	-708.	1179.	17.6	14.046	
0.0	0.13	0.8646	0.1486	0.1486	0.8646	243.6	1.514	1.768	1.128	0.757	1.010	1.013	-712.	1173.	17.6	14.045	
0.0	0.14	0.8543	0.1600	0.1600	0.8543	243.5	1.514	1.768	1.126	0.757	1.010	1.014	-716.	1167.	17.6	14.044	
0.0	0.15	0.8440	0.1714	0.1714	0.8440	243.4	1.514	1.768	1.124	0.757	1.010	1.015	-720.	1161.	17.6	14.043	
0.0	0.16	0.8337	0.1828	0.1828	0.8337	243.3	1.514	1.768	1.122	0.757	1.010	1.016	-724.	1155.	17.6	14.042	
0.0	0.17	0.8234	0.1942	0.1942	0.8234	243.2	1.514	1.768	1.120	0.757	1.010	1.017	-728.	1149.	17.6	14.041	
0.0	0.18	0.8131	0.2056	0.2056	0.8131	243.1	1.514	1.768	1.118	0.757	1.010	1.018	-732.	1143.	17.6	14.040	
0.0	0.19	0.8028	0.2170	0.2170	0.8028	243.0	1.514	1.768	1.116	0.757	1.010	1.019	-736.	1137.	17.6	14.039	
0.0	0.20	0.7925	0.2284	0.2284	0.7925	242.9	1.514	1.768	1.114	0.757	1.010	1.020	-740.	1131.	17.6	14.038	
0.0	0.21	0.7822	0.2398	0.2398	0.7822	242.8	1.514	1.768	1.112	0.757	1.010	1.021	-744.	1125.	17.6	14.037	
0.0	0.22	0.7719	0.2512	0.2512	0.7719	242.7	1.514	1.768	1.110	0.757	1.010	1.022	-748.	1119.	17.6	14.036	
0.0	0.23	0.7616	0.2626	0.2626	0.7616	242.6	1.514	1.768	1.108	0.757	1.010	1.023	-752.	1113.	17.6	14.035	
0.0	0.24	0.7513	0.2740	0.2740	0.7513	242.5	1.514	1.768	1.106	0.757	1.010	1.024	-756.	1107.	17.6	14.034	
0.0	0.25	0.7410	0.2854	0.2854	0.7410	242.4	1.514	1.768	1.104	0.757	1.010	1.025	-760.	1101.	17.6	14.033	
0.0	0.26	0.7307	0.2968	0.2968	0.7307	242.3	1.514	1.768	1.102	0.757	1.010	1.026	-764.	1095.	17.6	14.032	
0.0	0.27	0.7204	0.3082	0.3082	0.7204	242.2	1.514	1.768	1.100	0.757	1.010	1.027	-768.	1089.	17.6	14.031	
0.0	0.28	0.7101	0.3196	0.3196	0.7101	242.1	1.514	1.768	1.098	0.757	1.010	1.028	-772.	1083.	17.6	14.030	
0.0	0.29	0.7000	0.3310	0.3310	0.7000	242.0	1.514	1.768	1.096	0.757	1.010	1.029	-776.	1077.	17.6	14.029	
0.0	0.30	0.6900	0.3424	0.3424	0.6900	241.9	1.514	1.768	1.094	0.757	1.010	1.030	-780.	1071.	17.6	14.028	
0.0	0.31	0.6800	0.3538	0.3538	0.6800	241.8	1.514	1.768	1.092	0.757	1.010	1.031	-784.	1065.	17.6	14.027	
0.0	0.32	0.6700	0.3652	0.3652	0.6700	241.7	1.514	1.768	1.090	0.757	1.010	1.032	-788.	1059.	17.6	14.026	
0.0	0.33	0.6600	0.3766	0.3766	0.6600	241.6	1.514	1.768	1.088	0.757	1.010	1.033	-792.	1053.	17.6	14.025	
0.0	0.34	0.6500	0.3880	0.3880	0.6500	241.5	1.514	1.768	1.086	0.757	1.010	1.034	-796.	1047.	17.6	14.024	
0.0	0.35	0.6400	0.3994	0.3994	0.6400	241.4	1.514	1.768	1.084	0.757	1.010	1.035	-800.	1041.	17.6	14.023	
0.0	0.36	0.6300	0.4108	0.4108	0.6300	241.3	1.514	1.768	1.082	0.757	1.010	1.036	-804.	1035.	17.6	14.022	
0.0	0.37	0.6200	0.4222	0.4222	0.6200	241.2	1.514	1.768	1.080	0.757	1.010	1.037	-808.	1029.	17.6	14.021	
0.0	0.38	0.6100	0.4336	0.4336	0.6100	241.1	1.514	1.768	1.078	0.757	1.010	1.038	-812.	1023.	17.6	14.020	
0.0	0.39	0.6000	0.4450	0.4450	0.6000	241.0	1.514	1.768	1.076	0.757	1.010	1.039	-816.	1017.	17.6	14.019	
0.0	0.40	0.5900	0.4564	0.4564	0.5900	240.9	1.514	1.768	1.074	0.757	1.010	1.040	-820.	1011.	17.6	14.018	
0.0	0.41	0.5800	0.4678	0.4678	0.5800	240.8	1.514	1.768	1.072	0.757	1.010	1.041	-824.	1005.	17.6	14.017	
0.0	0.42	0.5700	0.4792	0.4792	0.5700	240.7	1.514	1.768	1.070	0.757	1.010	1.042	-828.	999.	17.6	14.016	
0.0	0.43	0.5600	0.4906	0.4906	0.5600	240.6	1.514	1.768	1.068	0.757	1.010	1.043	-832.	993.	17.6	14.015	
0.0	0.44	0.5500	0.5020	0.5020	0.5500	240.5	1.514	1.768	1.066	0.757	1.010	1.044	-836.	987.	17.6	14.014	
0.0	0.45	0.5400	0.5134	0.5134	0.5400	240.4	1.514	1.768	1.064	0.757	1.010	1.045	-840.	981.	17.6	14.013	
0.0	0.46	0.5300	0.5248	0.5248	0.5300	240.3	1.514	1.768	1.062	0.757	1.010	1.046	-844.	975.	17.6	14.012	
0.0	0.47	0.5200	0.5362	0.5362	0.5200	240.2	1.514	1.768	1.060	0.757	1.010	1.047	-848.	969.	17.6	14.011	
0.0	0.48	0.5100	0.5476	0.5476	0.5100	240.1	1.514	1.768	1.058	0.757	1.010	1.048	-852.	963.	17.6	14.010	
0.0	0.49	0.5000	0.5590	0.5590	0.5000	240.0	1.514	1.768	1.056	0.757	1.010	1.049	-856.	957.	17.6	14.009	
0.0	0.50	0.4900	0.5704	0.5704	0.4900	239.9	1.514	1.768	1.054	0.757	1.010	1.050	-860.	951.	17.6	14.008	
0.0	0.51	0.4800	0.5818	0.5818	0.4800	239.8	1.514	1.768	1.052	0.757	1.010	1.051	-864.	945.	17.6	14.007	
0.0	0.52	0.4700	0.5932	0.5932	0.4700	239.7	1.514	1.768	1.050	0.757	1.010	1.052	-868.	939.	17.6	14.006	
0.0	0.53	0.4600	0.6046	0.6046	0.4600	239.6	1.514	1.768	1.048	0.757	1.010	1.053	-872.	933.	17.6	14.005	
0.0	0.54	0.4500	0.6160	0.6160	0.4500	239.5	1.514	1.768	1.046	0.757	1.010	1.054	-876.	927.	17.6	14.004	
0.0	0.55	0.4400	0.6274	0.6274	0.4400	239.4	1.514	1.768	1.044	0.757	1.010	1.055	-880.	921.	17.6	14.003	
0.0	0.56	0.4300	0.6388	0.6388	0.4300	239.3	1.514	1.768	1.042	0.757	1.010	1.056	-884.	915.	17.6	14.002	
0.0	0.57	0.4200	0.6502	0.6502	0.4200	239.2	1.514	1.768	1.040	0.757	1.010	1.057	-888.	909.	17.6	14.001	
0.0	0.58	0.4100	0.6616	0.6616	0.4100	239.1	1.514	1.768	1.038	0.757	1.010	1.058	-892.	903.	17.6	14.000	
0.0	0.59	0.4000	0.6730	0.6730	0.4000	239.0	1.514	1.768	1.036	0.757	1.010	1.059	-896.	897.	17.6	13.999	
0.0	0.60	0.3900	0.6844	0.6844	0.3900	238.9	1.514	1.768	1.034	0.757	1.010	1.060	-900.	891.	17.6	13.998	
0.0	0.61	0.3800	0.6958	0.6958	0.3800	238.8	1.514	1.768	1.032	0.757	1.010	1.061	-904.	885.	17.6	13.997	
0.0	0.62	0.3700	0.7072	0.7072	0.3700	238.7	1.514	1.768	1.030	0.757	1.010	1.062	-908.	879.	17.6	13.996	
0.0	0.63	0.3600	0.7186	0.7186	0.3600	238.6	1.514	1.768	1.028	0.757	1.010	1.063	-912.	873.	17.6	13.995	
0.0	0.64	0.3500	0.7300	0.7300	0.3500	238.5	1.514	1.768	1.026	0.757	1.010	1.064	-916.	867.	17.6	13.994	
0.0	0.65	0.3400	0.7414	0.7414	0.3400	238.4	1.514	1.768	1.024	0.757	1.010	1.065	-920.	861.	17.6	13.993	
0.0	0.66	0.3300	0.7528	0.7528	0.3300	238.3	1.514	1.768	1.022	0.757	1.010	1.066	-924.	855.	17.6	13.992	
0.0	0.67	0.3200	0.7642	0.7642	0.3200	238.2	1.514	1.768	1.020	0.757	1.010	1.067	-928.	849.	17.6	13.991	
0.0	0.68	0.3100	0.7756	0.7756	0.3100	238.1	1.514	1.768	1.018	0.757	1.010	1.068	-932.	843.	17.6	13.990	
0.0	0.69	0.3000	0.7870	0.7870	0.3000	238.0	1.514	1.									

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION		TEMP	RELATIVE VOL			PRESSURE ACT COEF			ENTHALPY		HEAT CAPACITY		
N <sub>2</sub> /N <sub>2</sub> +O <sub>2</sub>	AR	N <sub>2</sub>	AR		O <sub>2</sub>	N <sub>2</sub> /AR	N <sub>2</sub> /O <sub>2</sub>	AR/O <sub>2</sub>	N <sub>2</sub>	AR	O <sub>2</sub>	LIQ	VAP	LIQ	VAP
0.10	0.	0.1000	0.	0.1000	245.0	1.501	1.722	1.147	0.780	1.053	1.053	-559.	1184.	18.1	16.636
0.10	0.01	0.1067	0.0107	0.1037	244.9	1.501	1.720	1.146	0.780	1.052	1.053	-559.	1184.	18.1	16.614
0.10	0.02	0.1134	0.0213	0.1021	244.9	1.502	1.718	1.144	0.780	1.052	1.054	-560.	1184.	18.1	16.591
0.10	0.03	0.1201	0.0319	0.1011	244.9	1.502	1.717	1.143	0.779	1.051	1.054	-561.	1184.	18.1	16.568
0.10	0.04	0.1268	0.0425	0.1003	244.8	1.502	1.715	1.141	0.779	1.050	1.055	-562.	1183.	18.0	16.545
0.10	0.05	0.1335	0.0530	0.0996	244.8	1.503	1.713	1.140	0.779	1.049	1.055	-563.	1183.	18.0	16.522
0.10	0.06	0.1402	0.0635	0.0990	244.7	1.504	1.710	1.137	0.778	1.048	1.057	-564.	1182.	18.0	16.499
0.10	0.07	0.1470	0.0740	0.0984	244.7	1.505	1.705	1.133	0.777	1.045	1.058	-565.	1182.	18.0	16.476
0.10	0.08	0.1537	0.0845	0.0979	244.6	1.510	1.698	1.118	0.774	1.038	1.064	-566.	1181.	17.8	16.453
0.10	0.09	0.1605	0.0950	0.0975	243.9	1.520	1.686	1.090	0.769	1.024	1.078	-567.	1179.	17.7	16.430
0.10	0.10	0.1672	0.1055	0.0972	243.8	1.530	1.675	1.062	0.766	1.013	1.095	-568.	1178.	17.5	16.407
0.10	0.11	0.1740	0.1158	0.0970	244.0	1.542	1.595	1.034	0.765	1.004	1.113	-569.	1177.	17.4	16.384
0.10	0.12	0.1807	0.1265	0.0970	244.2	1.546	1.581	1.021	0.765	1.000	1.123	-570.	1177.	17.4	16.361
0.20	0.	0.2000	0.	0.2000	245.0	1.478	1.686	1.140	0.800	1.092	1.102	-534.	1147.	17.8	17.421
0.20	0.01	0.2067	0.0107	0.1967	244.9	1.479	1.685	1.139	0.799	1.091	1.102	-534.	1147.	17.8	17.398
0.20	0.02	0.2134	0.0213	0.1934	244.9	1.480	1.683	1.138	0.799	1.089	1.102	-542.	1138.	17.8	17.365
0.20	0.03	0.2201	0.0319	0.1903	244.9	1.481	1.682	1.136	0.798	1.088	1.102	-547.	1133.	17.7	17.332
0.20	0.04	0.2268	0.0425	0.1873	244.9	1.481	1.681	1.135	0.798	1.087	1.102	-551.	1129.	17.7	17.309
0.20	0.05	0.2335	0.0530	0.1844	244.9	1.482	1.680	1.133	0.797	1.086	1.102	-555.	1124.	17.7	17.286
0.20	0.06	0.2402	0.0635	0.1816	244.0	1.484	1.677	1.130	0.796	1.083	1.103	-560.	1119.	17.7	17.263
0.20	0.07	0.2470	0.0740	0.1789	241.1	1.486	1.673	1.126	0.795	1.080	1.103	-576.	1102.	17.7	17.224
0.20	0.08	0.2537	0.0845	0.1764	241.1	1.493	1.666	1.112	0.790	1.080	1.105	-618.	1059.	17.6	16.836
0.20	0.09	0.2605	0.0950	0.1740	242.3	1.508	1.635	1.085	0.762	1.047	1.118	-687.	975.	17.5	16.165
0.20	0.10	0.2672	0.1055	0.1717	243.2	1.523	1.611	1.058	0.775	1.028	1.117	-773.	893.	17.4	15.421
0.20	0.11	0.2740	0.1158	0.1695	243.2	1.539	1.588	1.032	0.769	1.011	1.125	-844.	810.	17.4	14.677
0.20	0.12	0.2807	0.1265	0.1674	243.8	1.547	1.577	1.020	0.767	1.003	1.129	-877.	767.	17.4	14.401
0.40	0.	0.4000	0.	0.4000	245.0	1.450	1.632	1.120	0.830	1.168	1.201	-463.	1078.	17.8	18.333
0.40	0.01	0.4067	0.0107	0.3967	244.2	1.451	1.632	1.124	0.830	1.166	1.201	-468.	1075.	17.8	18.285
0.40	0.02	0.4134	0.0213	0.3934	244.2	1.452	1.631	1.123	0.837	1.163	1.200	-473.	1071.	17.8	18.237
0.40	0.03	0.4201	0.0319	0.3903	244.3	1.453	1.630	1.122	0.836	1.161	1.199	-478.	1068.	17.8	18.189
0.40	0.04	0.4268	0.0425	0.3873	244.4	1.454	1.629	1.120	0.835	1.159	1.198	-482.	1065.	17.8	18.141
0.40	0.05	0.4335	0.0530	0.3844	244.4	1.455	1.628	1.119	0.835	1.157	1.197	-487.	1062.	17.8	18.093
0.40	0.06	0.4402	0.0635	0.3816	244.6	1.457	1.627	1.116	0.833	1.155	1.196	-497.	1055.	17.7	18.045
0.40	0.07	0.4470	0.0740	0.3789	244.6	1.460	1.624	1.112	0.830	1.147	1.194	-512.	1046.	17.7	18.003
0.40	0.08	0.4537	0.0845	0.3764	244.6	1.470	1.616	1.099	0.822	1.127	1.186	-560.	1014.	17.6	18.033
0.40	0.09	0.4605	0.0950	0.3740	244.4	1.481	1.601	1.074	0.806	1.091	1.173	-654.	946.	17.4	17.249
0.40	0.10	0.4672	0.1055	0.3717	244.7	1.491	1.587	1.050	0.799	1.058	1.161	-745.	880.	17.3	16.111
0.40	0.11	0.4740	0.1158	0.3695	241.7	1.512	1.575	1.028	0.779	1.026	1.148	-830.	806.	17.3	14.926
0.40	0.12	0.4807	0.1265	0.3674	243.1	1.543	1.570	1.017	0.772	1.011	1.141	-871.	760.	17.3	14.327
0.60	0.	0.6000	0.	0.6000	245.0	1.431	1.588	1.110	0.887	1.252	1.316	-383.	1008.	18.3	22.304
0.60	0.01	0.6067	0.0107	0.5967	248.3	1.432	1.588	1.108	0.887	1.249	1.313	-388.	1006.	18.3	22.261
0.60	0.02	0.6134	0.0213	0.5934	248.4	1.433	1.587	1.107	0.881	1.246	1.311	-394.	1004.	18.3	22.199
0.60	0.03	0.6201	0.0319	0.5903	248.5	1.435	1.587	1.106	0.880	1.243	1.309	-400.	1002.	18.2	22.141
0.60	0.04	0.6268	0.0425	0.5873	248.6	1.436	1.586	1.105	0.878	1.239	1.307	-405.	1000.	18.2	22.086
0.60	0.05	0.6335	0.0530	0.5844	248.6	1.437	1.586	1.104	0.877	1.236	1.305	-411.	998.	18.2	22.031
0.60	0.06	0.6402	0.0635	0.5816	249.0	1.439	1.585	1.101	0.874	1.230	1.301	-422.	994.	18.2	21.995
0.60	0.07	0.6470	0.0740	0.5789	249.4	1.443	1.584	1.097	0.870	1.221	1.295	-439.	988.	18.1	21.997
0.60	0.08	0.6537	0.0845	0.5764	249.7	1.455	1.579	1.085	0.857	1.192	1.276	-495.	967.	17.9	20.333
0.60	0.09	0.6605	0.0950	0.5740	248.8	1.478	1.571	1.063	0.833	1.137	1.240	-606.	921.	17.6	18.921
0.60	0.10	0.6672	0.1055	0.5717	246.1	1.501	1.565	1.042	0.810	1.088	1.206	-713.	867.	17.4	18.846
0.60	0.11	0.6740	0.1158	0.5695	244.1	1.526	1.562	1.024	0.788	1.042	1.171	-816.	802.	17.3	18.259
0.60	0.12	0.6807	0.1265	0.5674	242.1	1.540	1.563	1.015	0.777	1.019	1.153	-864.	765.	17.3	18.479
0.80	0.	0.8000	0.	0.8000	245.0	1.415	1.545	1.092	0.930	1.357	1.458	-304.	926.	18.9	28.371
0.80	0.01	0.8067	0.0107	0.7967	242.8	1.416	1.545	1.091	0.937	1.352	1.454	-310.	928.	18.9	28.374
0.80	0.02	0.8134	0.0213	0.7934	243.0	1.418	1.545	1.090	0.935	1.347	1.450	-316.	928.	18.9	27.966
0.80	0.03	0.8201	0.0319	0.7903	243.2	1.419	1.545	1.089	0.933	1.342	1.446	-322.	927.	18.8	27.964
0.80	0.04	0.8268	0.0425	0.7873	243.3	1.420	1.545	1.088	0.931	1.337	1.441	-328.	927.	18.8	27.906
0.80	0.05	0.8335	0.0530	0.7844	243.5	1.422	1.545	1.087	0.929	1.332	1.437	-335.	926.	18.8	27.630
0.80	0.06	0.8402	0.0635	0.7816	243.9	1.425	1.545	1.085	0.924	1.323	1.429	-347.	926.	18.8	26.763
0.80	0.07	0.8470	0.0740	0.7789	244.4	1.429	1.545	1.081	0.918	1.309	1.418	-366.	924.	18.7	26.248
0.80	0.08	0.8537	0.0845	0.7764	246.2	1.442	1.545	1.071	0.898	1.265	1.380	-429.	916.	18.6	25.919
0.80	0.09	0.8605	0.0950	0.7740	246.1	1.468	1.544	1.052	0.862	1.188	1.314	-555.	891.	17.9	20.142
0.80	0.10	0.8672	0.1055	0.7717	244.3	1.494	1.545	1.034	0.829	1.119	1.253	-680.	852.	17.9	17.661
0.80	0.11	0.8740	0.1158	0.7695	241.0	1.521	1.551	1.019	0.797	1.037	1.195	-809.	798.	17.9	15.593
0.80	0.12	0.8807	0.1265	0.7674	241.6	1.537	1.547	1.013	0.781	1.027	1.185	-857.	763.	17.3	14.640
0.90	0.	0.9000	0.	0.9000	245.0	1.407	1.523	1.082	0.973	1.421	1.546	-266.	879.	19.3	34.426
0.90	0.01	0.9067	0.0107	0.8967	246.2	1.408	1.523	1.081	0.970	1.416	1.544	-272.	880.	19.2	33.787
0.90	0.02	0.9134	0.0213	0.8934	246.4	1.410	1.523	1.080	0.967	1.410	1.544	-279.	881.	19.2	33.146
0.90	0.03	0.9201	0.0319	0.8903	246.6	1.411	1.524	1.080	0.965	1.402	1.529	-285.	882.	19.2	32.567
0.90	0.04	0.9268	0.0425	0.8873	246.8	1.413	1.524	1.079	0.963	1.396	1.523	-292.	883.	19.1	32.010
0.90	0.05	0.9335	0.0530	0.8844	247.1	1.414	1.524	1.078	0.960	1.390	1.517	-298.	884.	19.1	31.491
0.90	0.06	0.9402	0.0635	0.8816	247.4	1.418	1.525	1.076	0.958	1.378	1.506	-311.	885.	19.0	30.910
0.90	0.07	0.9470	0.0740	0.8789	247.4	1.422	1.526	1.073	0.946	1.361	1.490	-331.	886.	18.9	29.100
0.90	0.08	0.9537	0.0845	0.8764	248.4	1.436	1.526	1.064	0.922	1.308	1.441	-397.	887.	18.6	

B. Isothermal Table

The table to follow presents values calculated at even temperature intervals of five degrees from 140°R to 245°R. They are arranged in order of increasing liquid mole fraction ratio

$$\frac{N_2}{N_2 + O_2}$$

and sub-ordered according to increasing mole fraction of argon. The quantities calculated are vapor composition, pressure, equilibrium constant (K-Values), relative volatility, enthalpy, and heat capacity.

Table 26. Isothermal Calculated Values

TEMPERATURE = 140. K

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION			PRESSURE ATM	EQUIL CONST			RELATIVE VOL			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
N <sub>2</sub>	AR/AR+O <sub>2</sub>	N <sub>2</sub>	AR	O <sub>2</sub>		N <sub>2</sub>	AR	O <sub>2</sub>	N <sub>2</sub> /AR	N <sub>2</sub> /O <sub>2</sub>	AR/O <sub>2</sub>	LIG	VAP	LIG	VAP
.975	0.	1.943	0.	0.0071	1.02	1.019	0.421	0.202	2.419	3.011	1.493	-1401.	934.	14.4	7.540
.975	0.1	1.9927	0.0031	0.0003	1.02	1.018	0.421	0.202	2.421	3.009	1.491	-1401.	933.	14.4	7.547
.975	0.2	1.9924	0.0021	0.0006	1.02	1.018	0.420	0.202	2.422	3.007	1.490	-1401.	933.	14.4	7.549
.975	0.3	1.9920	0.0031	0.0009	1.02	1.017	0.420	0.202	2.423	3.005	1.488	-1402.	933.	14.4	7.543
.975	0.4	1.9917	0.0042	0.0012	1.02	1.017	0.420	0.202	2.424	3.003	1.486	-1402.	933.	14.4	7.541
.975	0.5	1.9913	0.0052	0.0015	1.02	1.017	0.419	0.202	2.425	3.001	1.485	-1402.	932.	14.4	7.539
.975	0.6	1.9910	0.0063	0.0018	1.02	1.016	0.419	0.202	2.426	3.000	1.483	-1402.	932.	14.4	7.537
.975	0.7	1.9907	0.0073	0.0021	1.02	1.016	0.419	0.203	2.427	3.000	1.482	-1402.	932.	14.4	7.539
.975	0.8	1.9903	0.0084	0.0024	1.02	1.016	0.418	0.203	2.428	3.000	1.480	-1403.	931.	14.3	7.533
.975	0.9	1.9900	0.0094	0.0027	1.02	1.015	0.418	0.203	2.429	3.000	1.479	-1403.	931.	14.3	7.531
.975	1.0	1.9897	0.0104	0.	1.02	1.015	0.418	0.203	2.430	3.000	1.477	-1403.	931.	14.3	7.529

TEMPERATURE = 145. K

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION			PRESSURE ATM	EQUIL CONST			RELATIVE VOL			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
N <sub>2</sub>	AR/AR+O <sub>2</sub>	N <sub>2</sub>	AR	O <sub>2</sub>		N <sub>2</sub>	AR	O <sub>2</sub>	N <sub>2</sub> /AR	N <sub>2</sub> /O <sub>2</sub>	AR/O <sub>2</sub>	LIG	VAP	LIG	VAP
.900	0.	0.8988	0.	0.1012	1.00	1.420	0.589	0.390	2.972	3.987	1.990	-1402.	971.	13.6	7.406
.900	0.1	0.8982	0.0214	0.1200	1.01	1.415	0.587	0.390	2.969	3.991	1.990	-1400.	964.	13.4	7.443
.900	0.2	0.8973	0.0431	0.1147	1.02	1.404	0.599	0.399	2.968	3.915	1.992	-1471.	958.	13.3	7.401
.900	0.3	0.8958	0.0637	0.1085	1.02	1.393	0.591	0.399	2.974	3.886	1.979	-1479.	952.	13.2	7.360
.900	0.4	0.8946	0.0816	0.0983	1.03	1.383	0.594	0.390	2.981	3.865	1.956	-1479.	946.	13.1	7.321
.900	0.5	0.8937	0.1034	0.0921	1.03	1.374	0.597	0.361	2.987	3.810	1.932	-1483.	941.	13.0	7.282
.900	0.6	0.8930	0.1275	0.0879	1.04	1.366	0.598	0.362	2.977	3.776	1.911	-1487.	935.	12.8	7.245
.900	0.7	0.8924	0.1492	0.0836	1.05	1.359	0.594	0.363	2.994	3.742	1.889	-1491.	929.	12.7	7.200
.900	0.8	0.8914	0.1695	0.0792	1.05	1.352	0.499	0.365	2.712	3.708	1.867	-1495.	924.	12.6	7.172
.900	0.9	0.8904	0.1776	0.0748	1.07	1.347	0.492	0.364	2.740	3.701	1.851	-1499.	920.	12.5	7.110
.900	1.0	0.8907	0.1947	0.	1.07	1.343	0.487	0.360	2.798	3.685	1.830	-1703.	916.	12.3	7.001
.700	0.	0.8988	0.	0.1012	1.10	1.264	0.512	0.338	2.900	3.827	1.915	-1499.	967.	13.7	7.535
.700	0.1	0.8980	0.0192	0.0913	1.11	1.277	0.508	0.338	2.901	3.776	1.908	-1500.	963.	13.6	7.506
.700	0.2	0.8968	0.0301	0.0813	1.11	1.278	0.501	0.339	2.934	3.750	1.900	-1401.	959.	13.5	7.476
.700	0.3	0.8942	0.0446	0.0712	1.12	1.263	0.496	0.339	2.947	3.725	1.903	-1404.	954.	13.4	7.440
.700	0.4	0.8910	0.0589	0.0612	1.12	1.257	0.491	0.340	2.959	3.700	1.905	-1407.	950.	13.3	7.420
.700	0.5	0.8870	0.0730	0.0511	1.13	1.251	0.487	0.341	2.972	3.675	1.929	-1410.	946.	13.2	7.393
.700	0.6	0.8824	0.0868	0.0410	1.13	1.246	0.482	0.341	2.985	3.650	1.912	-1413.	942.	13.0	7.366
.700	0.7	0.8809	0.1003	0.0308	1.14	1.241	0.478	0.342	2.978	3.625	1.895	-1416.	938.	12.9	7.339
.700	0.8	0.8800	0.1137	0.0204	1.14	1.237	0.474	0.341	2.911	3.600	1.879	-1419.	934.	12.8	7.313
.700	0.9	0.8809	0.1276	0.0103	1.15	1.233	0.470	0.345	2.924	3.576	1.863	-1423.	930.	12.6	7.288
.700	1.0	0.8813	0.1398	0.	1.15	1.229	0.466	0.346	2.937	3.552	1.847	-1426.	927.	12.5	7.261
.600	0.	0.8958	0.	0.0942	1.20	1.149	0.478	0.323	2.947	3.625	1.901	-1500.	964.	13.6	7.506
.600	0.1	0.8935	0.0199	0.0841	1.21	1.146	0.478	0.323	2.956	3.600	1.889	-1530.	962.	13.0	7.508
.600	0.2	0.8905	0.0389	0.0718	1.21	1.142	0.470	0.323	2.964	3.592	1.890	-1532.	959.	12.7	7.509
.600	0.3	0.8867	0.0581	0.0584	1.21	1.150	0.469	0.324	2.972	3.576	1.886	-1534.	956.	12.7	7.531
.600	0.4	0.8823	0.0773	0.0489	1.22	1.155	0.466	0.324	2.980	3.560	1.870	-1536.	953.	12.6	7.514
.600	0.5	0.8773	0.0963	0.0389	1.22	1.152	0.463	0.325	2.989	3.543	1.854	-1538.	951.	12.5	7.496
.600	0.6	0.8719	0.1152	0.0280	1.22	1.149	0.460	0.326	2.997	3.527	1.843	-1540.	948.	12.4	7.479
.600	0.7	0.8665	0.1340	0.0180	1.23	1.146	0.457	0.326	2.998	3.512	1.832	-1542.	946.	12.4	7.462
.600	0.8	0.8613	0.1527	0.0081	1.23	1.143	0.455	0.327	2.914	3.496	1.821	-1544.	943.	12.4	7.445
.600	0.9	0.8562	0.1714	0.0000	1.23	1.140	0.452	0.328	2.922	3.480	1.810	-1546.	940.	12.3	7.428
.600	1.0	0.8512	0.1899	0.	1.24	1.137	0.450	0.329	2.930	3.464	1.800	-1548.	938.	12.2	7.411
.500	0.	0.8880	0.	0.1120	1.30	1.077	0.451	0.312	2.948	3.496	1.847	-1401.	961.	14.0	7.638
.500	0.1	0.8876	0.0045	0.0981	1.31	1.075	0.450	0.312	2.992	3.440	1.842	-1401.	960.	14.0	7.630
.500	0.2	0.8862	0.0090	0.0920	1.31	1.074	0.446	0.312	2.994	3.440	1.836	-1402.	959.	13.9	7.621
.500	0.3	0.8849	0.0134	0.0858	1.31	1.072	0.447	0.312	2.980	3.433	1.830	-1403.	957.	13.8	7.612
.500	0.4	0.8836	0.0178	0.0796	1.31	1.071	0.445	0.313	2.984	3.428	1.825	-1404.	956.	13.8	7.604
.500	0.5	0.8823	0.0222	0.0734	1.31	1.069	0.444	0.313	2.988	3.417	1.819	-1405.	955.	13.8	7.596
.500	0.6	0.8811	0.0266	0.0672	1.31	1.068	0.443	0.313	2.912	3.409	1.814	-1406.	953.	13.8	7.587
.500	0.7	0.8800	0.0309	0.0609	1.32	1.067	0.441	0.314	2.916	3.402	1.808	-1407.	952.	13.8	7.579
.500	0.8	0.8807	0.0352	0.0547	1.32	1.065	0.440	0.314	2.920	3.394	1.803	-1408.	951.	13.7	7.571
.500	0.9	0.8815	0.0395	0.0485	1.32	1.064	0.439	0.314	2.924	3.386	1.797	-1409.	950.	13.7	7.562
.500	1.0	0.8824	0.0438	0.	1.32	1.063	0.438	0.315	2.928	3.379	1.792	-1477.	946.	13.7	7.554
.475	0.	0.9928	0.	0.0072	1.38	1.018	0.434	0.205	2.344	3.335	1.423	-1410.	959.	14.1	7.679
.475	0.1	0.9924	0.0011	0.0009	1.30	1.018	0.434	0.205	2.349	3.333	1.421	-1410.	958.	14.1	7.677
.475	0.2	0.9919	0.0022	0.0018	1.30	1.017	0.434	0.205	2.346	3.331	1.420	-1410.	958.	14.1	7.675
.475	0.3	0.9916	0.0033	0.0027	1.30	1.017	0.433	0.205	2.347	3.329	1.419	-1411.	958.	14.1	7.673
.475	0.4	0.9913	0.0044	0.0036	1.30	1.017	0.433	0.206	2.348	3.327	1.417	-1411.	957.	14.1	7.671
.475	0.5	0.9910	0.0054	0.0045	1.30	1.016	0.433	0.206	2.349	3.325	1.416	-1411.	957.	14.1	7.669
.475	0.6	0.9908	0.0065	0.0054	1.30	1.016	0.432	0.206	2.350	3.323	1.414	-1411.	957.	14.1	7.667
.475	0.7	0.9903	0.0076	0.0063	1.30	1.016	0.432	0.206	2.351	3.322	1.413	-1412.	956.	14.0	7.665
.475	0.8	0.9900	0.0086	0.0072	1.30	1.015	0.432	0.206	2.352	3.320	1.412	-1412.	956.	14.0	7.663
.475	0.9	0.9897	0.0097	0.0081	1.30	1.015	0.431	0.206	2.353	3.318	1.411	-1412.	956.	14.0	7.661
.475	1.0	0.9894	0.0108	0.	1.30	1.015	0.431	0.206	2.354	3.316	1.409	-1412.	956.	14.0	7.659

TEMP	LIQUID MOLE FRACTION			VAPOR MOLE FRACTION			PRESSURE	EQUIL CONST				RELATIVE VOL			ENTHALPY		HEAT CAPACITY	
	W	X	Y	W	X	Y		ATM	N2	AR	O2	N2/AR	N2/O2	AR/O2	LIQ	VAP	LIQ	VAP
0.3	0.5	0.2000	0.2423	0.1730	1.03	1.946	0.692	0.497	2.812	3.919	1.394	-1090.	930.	12.1	6.930			
0.3	0.6	0.2700	0.2940	0.1949	1.02	1.922	0.676	0.490	2.842	3.899	1.350	-1040.	924.	11.9	6.874			
0.3	0.7	0.3400	0.3243	0.1951	1.03	1.902	0.662	0.500	2.874	3.881	1.323	-1000.	911.	11.7	6.805			
0.3	0.8	0.4100	0.3536	0.1760	1.04	1.886	0.649	0.504	2.905	3.741	1.280	-1044.	899.	11.5	6.695			
0.3	0.9	0.5000	0.4221	0.1550	1.07	1.875	0.636	0.509	2.937	3.606	1.255	-1072.	888.	11.3	6.610			
0.4	0.5	0.2200	0.2441	0.1737	1.08	1.867	0.629	0.514	2.969	3.630	1.223	-1081.	876.	11.1	6.542			
0.4	0.6	0.2900	0.2949	0.1949	1.09	1.852	0.602	0.449	2.861	3.642	1.554	-1131.	1004.	12.1	7.470			
0.4	0.7	0.3600	0.3243	0.1951	1.10	1.783	0.605	0.440	2.656	3.637	1.486	-1149.	994.	12.1	7.397			
0.4	0.8	0.4300	0.3536	0.1761	1.13	1.738	0.650	0.447	2.675	3.806	1.453	-1149.	980.	12.0	7.321			
0.4	0.9	0.5200	0.4221	0.1550	1.14	1.716	0.636	0.447	2.700	3.635	1.420	-1192.	969.	12.8	7.247			
0.5	0.5	0.2400	0.2441	0.1737	1.15	1.607	0.623	0.448	2.725	3.705	1.389	-1199.	950.	12.4	7.177			
0.5	0.6	0.3100	0.2949	0.1949	1.16	1.600	0.611	0.450	2.751	3.735	1.350	-1199.	940.	12.4	7.109			
0.5	0.7	0.3800	0.3243	0.1951	1.16	1.607	0.600	0.452	2.774	3.687	1.320	-1199.	930.	12.2	7.043			
0.5	0.8	0.4500	0.3536	0.1761	1.17	1.659	0.591	0.455	2.802	3.639	1.290	-1199.	920.	12.0	6.980			
0.5	0.9	0.5400	0.4221	0.1550	1.18	1.644	0.582	0.450	2.829	3.591	1.270	-1199.	910.	11.8	6.917			
0.6	0.5	0.2600	0.2441	0.1737	1.19	1.639	0.574	0.462	2.855	3.544	1.241	-1199.	901.	11.7	6.856			
0.6	0.6	0.3300	0.2949	0.1949	1.22	1.589	0.629	0.411	2.540	3.801	1.520	-1003.	1000.	13.4	7.536			
0.6	0.7	0.4000	0.3243	0.1951	1.23	1.569	0.613	0.411	2.560	3.819	1.482	-1000.	991.	13.3	7.470			
0.6	0.8	0.4700	0.3536	0.1761	1.23	1.551	0.601	0.411	2.590	3.770	1.464	-1074.	982.	13.1	7.420			
0.6	0.9	0.5600	0.4221	0.1550	1.24	1.535	0.590	0.412	2.600	3.736	1.437	-1080.	974.	13.0	7.364			
0.7	0.5	0.2800	0.2441	0.1737	1.25	1.521	0.580	0.412	2.621	3.696	1.410	-1080.	965.	12.8	7.310			
0.7	0.6	0.3500	0.2949	0.1949	1.26	1.500	0.571	0.413	2.641	3.654	1.384	-1092.	957.	12.7	7.257			
0.7	0.7	0.4200	0.3243	0.1951	1.27	1.497	0.562	0.414	2.662	3.616	1.350	-1090.	950.	12.5	7.206			
0.7	0.8	0.4900	0.3536	0.1761	1.28	1.487	0.554	0.416	2.682	3.574	1.333	-1104.	942.	12.4	7.156			
0.7	0.9	0.5800	0.4221	0.1550	1.29	1.479	0.547	0.418	2.703	3.537	1.309	-1110.	934.	12.2	7.100			
0.8	0.5	0.3000	0.2441	0.1737	1.30	1.472	0.540	0.421	2.724	3.499	1.289	-1110.	927.	12.0	7.040			
0.8	0.6	0.3700	0.2949	0.1949	1.31	1.466	0.534	0.424	2.746	3.461	1.268	-1121.	920.	11.9	7.013			
0.8	0.7	0.4400	0.3243	0.1951	1.35	1.412	0.569	0.383	2.481	3.889	1.487	-1199.	996.	13.5	7.590			
0.8	0.8	0.5100	0.3536	0.1761	1.36	1.400	0.561	0.383	2.497	3.857	1.464	-1199.	990.	13.4	7.554			
0.8	0.9	0.6000	0.4221	0.1550	1.36	1.389	0.553	0.383	2.512	3.825	1.443	-1084.	983.	13.3	7.512			
0.9	0.5	0.3200	0.2441	0.1737	1.37	1.379	0.545	0.384	2.528	3.805	1.421	-1080.	977.	13.2	7.470			
0.9	0.6	0.3900	0.2949	0.1949	1.38	1.370	0.538	0.385	2.544	3.787	1.400	-1013.	970.	13.0	7.430			
0.9	0.7	0.4600	0.3243	0.1951	1.39	1.361	0.532	0.386	2.560	3.751	1.379	-1010.	964.	12.9	7.390			
0.9	0.8	0.5300	0.3536	0.1761	1.40	1.347	0.526	0.388	2.576	3.700	1.359	-1023.	950.	12.8	7.351			
0.9	0.9	0.6200	0.4221	0.1550	1.41	1.341	0.514	0.390	2.592	3.660	1.339	-1027.	942.	12.7	7.314			
1.0	0.5	0.3400	0.2441	0.1737	1.42	1.335	0.509	0.392	2.609	3.639	1.319	-1032.	947.	12.6	7.277			
1.0	0.6	0.4100	0.2949	0.1949	1.43	1.331	0.504	0.394	2.641	3.609	1.299	-1037.	941.	12.4	7.240			
1.0	0.7	0.4800	0.3243	0.1951	1.48	1.274	0.526	0.362	2.424	3.824	1.454	-1027.	933.	12.3	7.204			
1.0	0.8	0.5500	0.3536	0.1761	1.49	1.267	0.520	0.362	2.439	3.791	1.430	-1030.	920.	12.6	7.169			
1.0	0.9	0.6400	0.4221	0.1550	1.49	1.260	0.519	0.362	2.446	3.750	1.422	-1034.	913.	12.5	7.130			
1.1	0.5	0.3600	0.2441	0.1737	1.50	1.254	0.510	0.363	2.460	3.695	1.406	-1037.	909.	12.4	7.100			
1.1	0.6	0.4300	0.2949	0.1949	1.50	1.249	0.506	0.364	2.469	3.653	1.390	-1041.	904.	12.3	7.061			
1.1	0.7	0.5000	0.3243	0.1951	1.51	1.243	0.501	0.365	2.481	3.618	1.379	-1044.	890.	12.2	7.021			
1.1	0.8	0.5700	0.3536	0.1761	1.52	1.234	0.493	0.367	2.492	3.580	1.359	-1048.	885.	12.1	7.005			
1.1	0.9	0.6600	0.4221	0.1550	1.53	1.230	0.489	0.368	2.504	3.536	1.344	-1051.	881.	12.0	7.000			
1.2	0.5	0.3800	0.2441	0.1737	1.53	1.226	0.489	0.369	2.516	3.504	1.329	-1059.	877.	12.0	7.000			
1.2	0.6	0.4500	0.2949	0.1949	1.54	1.223	0.481	0.370	2.529	3.462	1.314	-1059.	870.	12.0	7.000			
1.2	0.7	0.5200	0.3243	0.1951	1.61	1.164	0.492	0.346	2.367	3.866	1.422	-1059.	869.	12.0	7.000			
1.2	0.8	0.5900	0.3536	0.1761	1.61	1.160	0.489	0.346	2.379	3.832	1.411	-1061.	860.	12.0	7.000			
1.2	0.9	0.6800	0.4221	0.1550	1.62	1.153	0.483	0.347	2.382	3.837	1.401	-1063.	853.	12.0	7.000			
1.3	0.5	0.4000	0.2441	0.1737	1.62	1.149	0.480	0.348	2.389	3.821	1.390	-1066.	840.	12.0	7.000			
1.3	0.6	0.4700	0.2949	0.1949	1.63	1.147	0.477	0.348	2.397	3.789	1.380	-1066.	830.	12.0	7.000			
1.3	0.7	0.5400	0.3243	0.1951	1.63	1.144	0.474	0.349	2.404	3.794	1.370	-1067.	824.	12.0	7.000			
1.3	0.8	0.6100	0.3536	0.1761	1.64	1.142	0.470	0.350	2.412	3.770	1.360	-1067.	817.	12.0	7.000			
1.3	0.9	0.7000	0.4221	0.1550	1.64	1.139	0.469	0.350	2.419	3.765	1.349	-1067.	810.	12.0	7.000			
1.4	0.5	0.4200	0.2441	0.1737	1.65	1.136	0.467	0.350	2.427	3.751	1.339	-1067.	806.	12.0	7.000			
1.4	0.6	0.4900	0.2949	0.1949	1.65	1.134	0.464	0.351	2.434	3.736	1.329	-1066.	803.	12.0	7.000			
1.4	0.7	0.5600	0.3243	0.1951	1.74	1.074	0.485	0.334	2.442	3.822	1.320	-1062.	800.	12.0	7.000			
1.4	0.8	0.6300	0.3536	0.1761	1.74	1.073	0.483	0.334	2.452	3.814	1.311	-1061.	795.	12.0	7.000			
1.4	0.9	0.7200	0.4221	0.1550	1.74	1.071	0.482	0.335	2.461	3.809	1.306	-1062.	793.	12.0	7.000			
1.5	0.5	0.4400	0.2441	0.1737	1.78	1.070	0.481	0.335	2.471	3.802	1.301	-1063.	782.	12.0	7.000			
1.5	0.6	0.5100	0.2949	0.1949	1.78	1.069	0.480	0.335	2.483	3.795	1.295	-1064.	780.	12.0	7.000			
1.5	0.7	0.5800	0.3243	0.1951	1.78	1.067	0.479	0.335	2.492	3.780	1.290	-1065.	779.	12.0	7.000			
1.5	0.8	0.6500	0.3536	0.1761	1.78	1.065	0.478	0.336	2.500	3.761	1.285	-1067.	770.	12.0	7.000			
1.5	0.9	0.7400	0.4221	0.1550	1.78	1.065	0.477	0.336	2.508	3.744	1.280	-1067.	764.	12.0	7.000			
1.6	0.5	0.4600	0.2441	0.1737	1.78	1.062	0.474	0.337	2.517	3.729	1.270	-1068.	764.	12.0	7.000			
1.6	0.6	0.5300	0.2949	0.1949	1.78	1.062	0.473	0.337	2.525	3.713	1.264	-1068.	758.	12.0	7.000			
1.6	0.7	0.6000	0.3243	0.1951	1.84	1.018	0.478	0.327	2.272	3.900	1.388	-1140.	901.	13.0	7.000			
1.6	0.8	0.6700	0.3536	0.1761	1.84	1.017	0.477	0.328	2.274	3.884	1.369	-1140.	891.	13.0	7.000			
1.6	0.9	0.7600	0.4221	0.1550	1.84	1.017	0.477	0.328	2.274	3.868	1.364	-1140.	881.	13.0	7.000			
1.7	0.5	0.4800	0.2441	0.1737	1.84	1.016	0.477	0.328	2.275	3.851	1.363	-1141.	880.	13.0	7.000			
1.7	0.6	0.5500	0.2949	0.1949	1.84	1.016	0.476	0.328	2.276	3.839	1.362	-1141.	880.	13.0	7.000			
1.7	0.7	0.6200	0.3243	0.1951	1.84	1.016	0.476	0.328	2.277	3.827	1.360	-1141.	880.	13.0	7.000			
1.7	0.8	0.6900	0.3536	0.1761	1.84	1.015	0.476	0.328	2.278	3.816	1.359	-1142.	870.	13.0	7.000			
1.7	0.9	0.7800	0.4221	0.1550	1.84	1.015	0.475	0.328	2.279	3.804	1.358	-1142.	870.	13.0	7.000			
1.8	0.5	0.5000	0.2441	0.1737	1.84	1.015	0.475											

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION			PRESSURE ATM	EQUIL CONST			RELATIVE VOL			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
NP	AR/A4=0?	NP	AR	NP		NP	AR	Q2	L	AM	N2/0?	AR/02	LIG	VAP	LIG
.100	0.0	0.2627	0.4897	0.2474	1.00	2.827	0.907	0.888	2.897	3.819	1.318	-1941.	894.	11.5	8.393
.100	0.1	0.2586	0.5551	0.1863	1.00	2.586	0.881	0.698	2.735	3.747	1.277	-1953.	874.	11.7	8.286
.100	0.2	0.2557	0.6102	0.1292	1.00	2.357	0.868	0.498	2.573	3.676	1.236	-1965.	854.	11.9	8.179
.100	0.3	0.2533	0.6628	0.0834	1.00	2.133	0.843	0.294	2.413	3.607	1.197	-1977.	835.	12.1	8.072
.100	0.4	0.2533	0.7148	0.0480	1.00	1.917	0.833	0.116	2.252	3.540	1.160	-1989.	815.	12.3	7.965
.100	0.5	0.2533	0.7668	0.0240	1.00	1.700	0.848	0.017	2.090	3.474	1.124	-1999.	795.	12.5	7.858
.100	0.6	0.2533	0.8188	0.0120	1.00	1.483	0.888	0.000	1.928	3.408	1.088	-2009.	775.	12.7	7.751
.100	0.7	0.2533	0.8708	0.0060	1.00	1.267	0.953	0.000	1.766	3.342	1.052	-2019.	755.	12.9	7.644
.100	0.8	0.2533	0.9228	0.0030	1.00	1.050	1.043	0.000	1.604	3.276	1.016	-2029.	735.	13.1	7.537
.100	0.9	0.2533	0.9748	0.0015	1.00	0.833	1.153	0.000	1.442	3.210	0.980	-2039.	715.	13.3	7.430
.100	1.0	0.2533	1.0268	0.0007	1.00	0.617	1.283	0.000	1.280	3.144	0.944	-2049.	695.	13.5	7.323
.100	1.0	0.2533	1.0788	0.0004	1.00	0.400	1.433	0.000	1.118	3.078	0.908	-2059.	675.	13.7	7.216
.100	1.0	0.2533	1.1308	0.0002	1.00	0.183	1.603	0.000	0.956	3.012	0.872	-2069.	655.	13.9	7.109
.100	1.0	0.2533	1.1828	0.0001	1.00	0.067	1.793	0.000	0.794	2.946	0.836	-2079.	635.	14.1	7.002
.100	1.0	0.2533	1.2348	0.0000	1.00	0.000	2.003	0.000	0.632	2.880	0.800	-2089.	615.	14.3	6.895
.100	1.0	0.2533	1.2868	0.0000	1.00	0.000	2.233	0.000	0.470	2.814	0.764	-2099.	595.	14.5	6.788
.100	1.0	0.2533	1.3388	0.0000	1.00	0.000	2.483	0.000	0.308	2.748	0.728	-2109.	575.	14.7	6.681
.100	1.0	0.2533	1.3908	0.0000	1.00	0.000	2.753	0.000	0.146	2.682	0.692	-2119.	555.	14.9	6.574
.100	1.0	0.2533	1.4428	0.0000	1.00	0.000	3.043	0.000	0.084	2.616	0.656	-2129.	535.	15.1	6.467
.100	1.0	0.2533	1.4948	0.0000	1.00	0.000	3.353	0.000	0.022	2.550	0.620	-2139.	515.	15.3	6.360
.100	1.0	0.2533	1.5468	0.0000	1.00	0.000	3.683	0.000	0.000	2.484	0.584	-2149.	495.	15.5	6.253
.100	1.0	0.2533	1.5988	0.0000	1.00	0.000	4.033	0.000	0.000	2.418	0.548	-2159.	475.	15.7	6.146
.100	1.0	0.2533	1.6508	0.0000	1.00	0.000	4.403	0.000	0.000	2.352	0.512	-2169.	455.	15.9	6.039
.100	1.0	0.2533	1.7028	0.0000	1.00	0.000	4.793	0.000	0.000	2.286	0.476	-2179.	435.	16.1	5.932
.100	1.0	0.2533	1.7548	0.0000	1.00	0.000	5.203	0.000	0.000	2.220	0.440	-2189.	415.	16.3	5.825
.100	1.0	0.2533	1.8068	0.0000	1.00	0.000	5.633	0.000	0.000	2.154	0.404	-2199.	395.	16.5	5.718
.100	1.0	0.2533	1.8588	0.0000	1.00	0.000	6.083	0.000	0.000	2.088	0.368	-2209.	375.	16.7	5.611
.100	1.0	0.2533	1.9108	0.0000	1.00	0.000	6.553	0.000	0.000	2.022	0.332	-2219.	355.	16.9	5.504
.100	1.0	0.2533	1.9628	0.0000	1.00	0.000	7.043	0.000	0.000	1.956	0.296	-2229.	335.	17.1	5.397
.100	1.0	0.2533	2.0148	0.0000	1.00	0.000	7.553	0.000	0.000	1.890	0.260	-2239.	315.	17.3	5.290
.100	1.0	0.2533	2.0668	0.0000	1.00	0.000	8.083	0.000	0.000	1.824	0.224	-2249.	295.	17.5	5.183
.100	1.0	0.2533	2.1188	0.0000	1.00	0.000	8.633	0.000	0.000	1.758	0.188	-2259.	275.	17.7	5.076
.100	1.0	0.2533	2.1708	0.0000	1.00	0.000	9.203	0.000	0.000	1.692	0.152	-2269.	255.	17.9	4.969
.100	1.0	0.2533	2.2228	0.0000	1.00	0.000	9.793	0.000	0.000	1.626	0.116	-2279.	235.	18.1	4.862
.100	1.0	0.2533	2.2748	0.0000	1.00	0.000	10.403	0.000	0.000	1.560	0.080	-2289.	215.	18.3	4.755
.100	1.0	0.2533	2.3268	0.0000	1.00	0.000	11.033	0.000	0.000	1.494	0.044	-2299.	195.	18.5	4.648
.100	1.0	0.2533	2.3788	0.0000	1.00	0.000	11.683	0.000	0.000	1.428	0.008	-2309.	175.	18.7	4.541
.100	1.0	0.2533	2.4308	0.0000	1.00	0.000	12.353	0.000	0.000	1.362	0.000	-2319.	155.	18.9	4.434
.100	1.0	0.2533	2.4828	0.0000	1.00	0.000	13.043	0.000	0.000	1.296	0.000	-2329.	135.	19.1	4.327
.100	1.0	0.2533	2.5348	0.0000	1.00	0.000	13.753	0.000	0.000	1.230	0.000	-2339.	115.	19.3	4.220
.100	1.0	0.2533	2.5868	0.0000	1.00	0.000	14.483	0.000	0.000	1.164	0.000	-2349.	95.	19.5	4.113
.100	1.0	0.2533	2.6388	0.0000	1.00	0.000	15.233	0.000	0.000	1.098	0.000	-2359.	75.	19.7	4.006
.100	1.0	0.2533	2.6908	0.0000	1.00	0.000	16.003	0.000	0.000	1.032	0.000	-2369.	55.	19.9	3.899
.100	1.0	0.2533	2.7428	0.0000	1.00	0.000	16.793	0.000	0.000	0.966	0.000	-2379.	35.	20.1	3.792
.100	1.0	0.2533	2.7948	0.0000	1.00	0.000	17.603	0.000	0.000	0.900	0.000	-2389.	15.	20.3	3.685
.100	1.0	0.2533	2.8468	0.0000	1.00	0.000	18.433	0.000	0.000	0.834	0.000	-2399.	-5.	20.5	3.578
.100	1.0	0.2533	2.8988	0.0000	1.00	0.000	19.283	0.000	0.000	0.768	0.000	-2409.	-25.	20.7	3.471
.100	1.0	0.2533	2.9508	0.0000	1.00	0.000	20.153	0.000	0.000	0.702	0.000	-2419.	-45.	20.9	3.364
.100	1.0	0.2533	3.0028	0.0000	1.00	0.000	21.043	0.000	0.000	0.636	0.000	-2429.	-65.	21.1	3.257
.100	1.0	0.2533	3.0548	0.0000	1.00	0.000	21.953	0.000	0.000	0.570	0.000	-2439.	-85.	21.3	3.150
.100	1.0	0.2533	3.1068	0.0000	1.00	0.000	22.883	0.000	0.000	0.504	0.000	-2449.	-105.	21.5	3.043
.100	1.0	0.2533	3.1588	0.0000	1.00	0.000	23.833	0.000	0.000	0.438	0.000	-2459.	-125.	21.7	2.936
.100	1.0	0.2533	3.2108	0.0000	1.00	0.000	24.803	0.000	0.000	0.372	0.000	-2469.	-145.	21.9	2.829
.100	1.0	0.2533	3.2628	0.0000	1.00	0.000	25.793	0.000	0.000	0.306	0.000	-2479.	-165.	22.1	2.722
.100	1.0	0.2533	3.3148	0.0000	1.00	0.000	26.803	0.000	0.000	0.240	0.000	-2489.	-185.	22.3	2.615
.100	1.0	0.2533	3.3668	0.0000	1.00	0.000	27.833	0.000	0.000	0.174	0.000	-2499.	-205.	22.5	2.508
.100	1.0	0.2533	3.4188	0.0000	1.00	0.000	28.883	0.000	0.000	0.108	0.000	-2509.	-225.	22.7	2.401
.100	1.0	0.2533	3.4708	0.0000	1.00	0.000	29.953	0.000	0.000	0.042	0.000	-2519.	-245.	22.9	2.294
.100	1.0	0.2533	3.5228	0.0000	1.00	0.000	31.043	0.000	0.000	0.000	0.000	-2529.	-265.	23.1	2.187
.100	1.0	0.2533	3.5748	0.0000	1.00	0.000	32.153	0.000	0.000	0.000	0.000	-2539.	-285.	23.3	2.080
.100	1.0	0.2533	3.6268	0.0000	1.00	0.000	33.283	0.000	0.000	0.000	0.000	-2549.	-305.	23.5	1.973
.100	1.0	0.2533	3.6788	0.0000	1.00	0.000	34.433	0.000	0.000	0.000	0.000	-2559.	-325.	23.7	1.866
.100	1.0	0.2533	3.7308	0.0000	1.00	0.000	35.603	0.000	0.000	0.000	0.000	-2569.	-345.	23.9	1.759
.100	1.0	0.2533	3.7828	0.0000	1.00	0.000	36.793	0.000	0.000	0.000	0.000	-2579.	-365.	24.1	1.652
.100	1.0	0.2533	3.8348	0.0000	1.00	0.000	38.003	0.000	0.000	0.000	0.000	-2589.	-385.	24.3	1.545
.100	1.0	0.2533	3.8868	0.0000	1.00	0.000	39.233	0.000	0.000	0.000	0.000	-2599.	-405.	24.5	1.438
.100	1.0	0.2533	3.9388	0.0000	1.00	0.000	40.483	0.000	0.000	0.000	0.000	-2609.	-425.	24.7	1.331
.100	1.0	0.2533	3.9908	0.0000	1.00	0.000	41.753	0.000	0.000	0.000	0.000	-2619.	-445.	24.9	1.224
.100	1.0	0.2533	4.0428	0.0000	1.00	0.000	43.043	0.000	0.000	0.000	0.000	-2629.	-465.	25.1	1.117
.100	1.0	0.2533	4.0948	0.0000	1.00	0.000	44.353	0.000	0.000	0.000	0.000	-2639.	-485.	25.3	1.010
.100	1.0	0.2533	4.1468	0.0000	1.00	0.000	45.683	0.000	0.000	0.000	0.000	-2649.	-505.	25.5	0.903
.100	1.0	0.2533	4.1988	0.0000	1.00	0.000	47.033	0.000	0.000	0.000	0.000	-2659.	-525.	25.7	0.796
.100	1.0	0.2533	4.2508	0.0000	1.00	0.000	48.403	0.000	0.000	0.000	0.000	-2669.	-545.	25.9	0.689
.100	1.0	0.2533	4.3028	0.0000	1.00	0.000	49.793	0.000	0.000	0.000	0.000	-2679.	-565.	26.1	0.582
.100	1.0	0.2533	4.3548	0.0000	1.00	0.000	51.203	0.000	0.000	0.000	0.000	-2689.	-585.	26.3	0.475
.100	1.0	0.2533	4.4068												



TEMP	LIQUID MOLE FRACTION		VAPOR MOLE FRACTION		PRESSURE ATM	EQUIL CONST			RELATIVE VOL			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
	N2	AR/AR-O2	N2	AR		N2	AR	O2	N2/AR	N2/O2	AR/O2	LIQ	VAP	LIQ	VAP
0.5	0.5	0.5	0.5	0.5	1.00	3.459	1.265	0.887	2.736	3.082	1.426	-1917.	950.	12.2	6.616
0.5	0.5	0.5	0.5	0.5	1.00	3.320	1.197	0.849	2.773	3.022	1.379	-1931.	927.	11.9	6.417
0.5	0.5	0.5	0.5	0.5	1.07	3.211	1.143	0.857	2.810	3.145	1.335	-1946.	897.	11.7	6.231
0.5	0.5	0.5	0.5	0.5	1.09	3.129	1.098	0.853	2.849	3.260	1.290	-1961.	869.	11.4	6.054
0.5	0.5	0.5	0.5	0.5	1.12	3.069	1.063	0.854	2.887	3.395	1.248	-1976.	842.	11.1	5.901
0.5	0.5	0.5	0.5	0.5	1.14	3.029	1.035	0.860	2.927	3.522	1.203	-1991.	816.	10.8	5.769
0.5	0.5	0.5	0.5	0.5	1.16	3.009	1.014	0.872	2.966	3.651	1.163	-2005.	789.	10.5	5.634
0.5	0.5	0.5	0.5	0.5	1.17	3.007	1.000	0.889	3.007	3.781	1.124	-2020.	762.	10.2	5.502
0.5	0.5	0.5	0.5	0.5	1.18	3.015	1.262	0.858	2.883	3.948	1.470	-1984.	994.	12.0	6.492
0.5	0.5	0.5	0.5	0.5	1.00	3.135	1.198	0.837	2.718	3.067	1.422	-1988.	967.	12.3	6.700
0.5	0.5	0.5	0.5	0.5	1.10	3.022	1.131	0.822	2.794	3.201	1.376	-1913.	937.	12.0	6.514
0.5	0.5	0.5	0.5	0.5	1.15	2.949	1.083	0.813	2.791	3.215	1.331	-1927.	909.	11.7	6.340
0.5	0.5	0.5	0.5	0.5	1.13	2.967	1.031	0.810	2.828	3.342	1.288	-1941.	883.	11.4	6.174
0.5	0.5	0.5	0.5	0.5	1.20	2.862	0.986	0.809	2.874	3.592	1.250	-1956.	859.	11.1	5.991
0.5	0.5	0.5	0.5	0.5	1.22	2.843	0.967	0.829	2.903	3.499	1.205	-1970.	833.	10.9	5.850
0.5	0.5	0.5	0.5	0.5	1.23	2.840	0.953	0.845	2.941	3.438	1.166	-1985.	808.	10.6	5.687
0.5	0.5	0.5	0.5	0.5	1.14	3.065	1.192	0.771	2.572	3.976	1.128	-1989.	782.	10.3	5.519
0.5	0.5	0.5	0.5	0.5	1.18	2.924	1.123	0.749	2.683	3.805	1.347	-1903.	1073.	13.2	7.452
0.5	0.5	0.5	0.5	0.5	1.22	2.808	1.066	0.733	2.839	3.681	1.459	-1917.	1041.	13.0	7.293
0.5	0.5	0.5	0.5	0.5	1.25	2.713	1.017	0.721	2.867	3.761	1.411	-1930.	1012.	12.7	7.075
0.5	0.5	0.5	0.5	0.5	1.28	2.635	0.976	0.713	2.899	3.894	1.369	-1945.	981.	12.4	6.911
0.5	0.5	0.5	0.5	0.5	1.31	2.572	0.941	0.709	2.932	3.927	1.327	-1957.	957.	12.1	6.759
0.5	0.5	0.5	0.5	0.5	1.33	2.523	0.912	0.709	2.966	3.961	1.287	-1969.	935.	11.9	6.614
0.5	0.5	0.5	0.5	0.5	1.37	2.466	0.880	0.711	2.800	3.494	1.249	-1994.	894.	11.4	6.341
0.5	0.5	0.5	0.5	0.5	1.39	2.445	0.852	0.726	2.834	3.432	1.211	-1910.	873.	11.1	6.208
0.5	0.5	0.5	0.5	0.5	1.41	2.444	0.840	0.737	2.869	3.369	1.179	-1923.	853.	10.8	6.074
0.5	0.5	0.5	0.5	0.5	1.44	2.440	0.828	0.744	2.904	3.308	1.139	-1936.	832.	10.6	5.939
0.5	0.5	0.5	0.5	0.5	1.43	2.362	0.820	0.830	2.844	3.813	1.315	-1734.	1067.	13.3	7.530
0.5	0.5	0.5	0.5	0.5	1.46	2.296	0.803	0.822	2.572	3.696	1.438	-1746.	1043.	13.1	7.393
0.5	0.5	0.5	0.5	0.5	1.48	2.239	0.801	0.817	2.600	3.630	1.396	-1758.	1021.	12.8	7.250
0.5	0.5	0.5	0.5	0.5	1.51	2.192	0.834	0.814	2.628	3.571	1.359	-1770.	1000.	12.6	7.133
0.5	0.5	0.5	0.5	0.5	1.53	2.153	0.811	0.813	2.657	3.513	1.322	-1782.	981.	12.4	7.014
0.5	0.5	0.5	0.5	0.5	1.55	2.122	0.799	0.814	2.685	3.455	1.287	-1793.	963.	12.1	6.900
0.5	0.5	0.5	0.5	0.5	1.57	2.097	0.773	0.817	2.715	3.399	1.252	-1807.	928.	11.9	6.791
0.5	0.5	0.5	0.5	0.5	1.58	2.079	0.750	0.822	2.744	3.344	1.218	-1819.	911.	11.7	6.684
0.5	0.5	0.5	0.5	0.5	1.61	2.067	0.745	0.826	2.774	3.290	1.180	-1827.	891.	11.4	6.579
0.5	0.5	0.5	0.5	0.5	1.63	2.061	0.735	0.827	2.774	3.290	1.180	-1841.	875.	11.2	6.479
0.5	0.5	0.5	0.5	0.5	1.64	2.059	0.726	0.837	2.804	3.236	1.154	-1853.	858.	11.0	6.374
0.5	0.5	0.5	0.5	0.5	1.66	1.980	0.799	0.852	2.487	3.693	1.483	-1665.	1061.	13.4	7.624
0.5	0.5	0.5	0.5	0.5	1.69	1.948	0.776	0.846	2.487	3.683	1.449	-1676.	1043.	13.2	7.516
0.5	0.5	0.5	0.5	0.5	1.71	1.913	0.759	0.846	2.511	3.592	1.414	-1688.	1026.	13.0	7.413
0.5	0.5	0.5	0.5	0.5	1.73	1.883	0.736	0.846	2.539	3.501	1.381	-1699.	1010.	12.8	7.319
0.5	0.5	0.5	0.5	0.5	1.75	1.850	0.719	0.846	2.563	3.402	1.349	-1707.	994.	12.6	7.222
0.5	0.5	0.5	0.5	0.5	1.77	1.837	0.704	0.848	2.607	3.393	1.316	-1717.	980.	12.4	7.132
0.5	0.5	0.5	0.5	0.5	1.79	1.820	0.691	0.850	2.632	3.304	1.286	-1727.	965.	12.2	7.045
0.5	0.5	0.5	0.5	0.5	1.81	1.806	0.680	0.854	2.657	3.250	1.256	-1738.	952.	12.0	6.960
0.5	0.5	0.5	0.5	0.5	1.83	1.797	0.670	0.859	2.682	3.212	1.226	-1748.	938.	11.8	6.877
0.5	0.5	0.5	0.5	0.5	1.84	1.795	0.661	0.868	2.708	3.167	1.199	-1758.	925.	11.6	6.794
0.5	0.5	0.5	0.5	0.5	1.87	1.791	0.726	0.850	2.412	3.504	1.453	-1597.	1055.	13.5	7.732
0.5	0.5	0.5	0.5	0.5	1.89	1.772	0.708	0.848	2.431	3.461	1.423	-1605.	1041.	13.3	7.629
0.5	0.5	0.5	0.5	0.5	1.91	1.755	0.692	0.846	2.451	3.419	1.395	-1614.	1028.	13.2	7.531
0.5	0.5	0.5	0.5	0.5	1.92	1.745	0.684	0.846	2.471	3.377	1.367	-1623.	1015.	13.0	7.439
0.5	0.5	0.5	0.5	0.5	1.94	1.735	0.664	0.846	2.491	3.336	1.339	-1632.	1003.	12.8	7.342
0.5	0.5	0.5	0.5	0.5	1.96	1.724	0.645	0.846	2.511	3.295	1.312	-1641.	991.	12.6	7.251
0.5	0.5	0.5	0.5	0.5	1.98	1.712	0.632	0.846	2.532	3.255	1.286	-1650.	980.	12.5	7.162
0.5	0.5	0.5	0.5	0.5	2.01	1.702	0.623	0.848	2.552	3.215	1.260	-1659.	969.	12.3	7.075
0.5	0.5	0.5	0.5	0.5	2.03	1.695	0.619	0.850	2.574	3.177	1.234	-1667.	958.	12.1	7.000
0.5	0.5	0.5	0.5	0.5	2.05	1.689	0.613	0.853	2.605	3.140	1.209	-1676.	947.	11.9	6.944
0.5	0.5	0.5	0.5	0.5	2.09	1.682	0.653	0.849	2.361	3.500	1.423	-1605.	937.	11.7	6.899
0.5	0.5	0.5	0.5	0.5	2.11	1.674	0.641	0.848	2.377	3.429	1.399	-1615.	1049.	13.6	7.800
0.5	0.5	0.5	0.5	0.5	2.12	1.668	0.630	0.848	2.393	3.291	1.375	-1624.	1036.	13.5	7.730
0.5	0.5	0.5	0.5	0.5	2.14	1.661	0.620	0.849	2.409	3.297	1.352	-1632.	1028.	13.3	7.679
0.5	0.5	0.5	0.5	0.5	2.15	1.651	0.611	0.849	2.425	3.224	1.329	-1641.	1019.	13.2	7.621
0.5	0.5	0.5	0.5	0.5	2.17	1.640	0.602	0.841	2.442	3.191	1.307	-1649.	1010.	13.0	7.564
0.5	0.5	0.5	0.5	0.5	2.18	1.630	0.596	0.842	2.458	3.159	1.285	-1657.	991.	12.7	7.510
0.5	0.5	0.5	0.5	0.5	2.20	1.621	0.586	0.846	2.475	3.126	1.263	-1665.	982.	12.6	7.463
0.5	0.5	0.5	0.5	0.5	2.21	1.614	0.579	0.847	2.492	3.095	1.242	-1673.	974.	12.4	7.392
0.5	0.5	0.5	0.5	0.5	2.23	1.608	0.573	0.849	2.508	3.063	1.221	-1681.	965.	12.3	7.361
0.5	0.5	0.5	0.5	0.5	2.24	1.603	0.568	0.853	2.525	3.032	1.201	-1689.	957.	12.1	7.291
0.5	0.5	0.5	0.5	0.5	2.31	1.581	0.590	0.849	2.311	3.420	1.393	-1605.	1043.	13.7	7.891
0.5	0.5	0.5	0.5	0.5	2.32	1.571	0.580	0.849	2.323	3.344	1.375	-1615.	1035.	13.6	7.849
0.5	0.5	0.5	0.5	0.5	2.33	1.561	0.562	0.849	2.336	3.268	1.356	-1624.	1028.	13.5	7.801
0.5	0.5	0.5	0.5	0.5	2.34	1.552	0.555	0.849	2.348	3.192	1.338	-1632.	1020.	13.4	7.750
0.5	0.5	0.5	0.5	0.5	2.36	1.543	0.549	0.843	2.361	3.116	1.320	-1641.	1013.	13.2	7.710
0.5	0.5	0.5	0.5	0.5	2.37	1.536	0.543	0.832	2.374	3.091	1.302	-1649.	1006.	13.1	7.675
0.5	0.5	0.5	0.5	0.5	2.38	1.529	0.537	0.834	2.387	3.064	1.284	-1657.	999.	13.0	7.635
0.5	0.5	0.5	0.5	0.5	2.41	1.523	0.531	0.835	2.400	3.040	1.267	-1665.	993.	12.9	7.595
0.5	0.5	0.5	0.5	0.5	2.42	1.518	0.526	0.837	2.413	3.016	1.250	-1673.	986.	12.8	7.556
0.5	0.5	0.5	0.5	0.5	2.43	1.513	0.521	0.839	2.426	2.991	1.233	-1681.	980.	12.6	7.517
0.5	0.5	0.5	0.5	0.5	2.44	1.508	0.517	0.843	2.439	2.967	1.216	-1689.	973.		

LIQUID MOLE FRACTION			VAPOR MOLE FRACTION			PRESSURE				EQUIL CONST		RELATIVE VOL		ENTHALPY		HEAT CAPACITY	
NP	AR/AR+O2	O2	N2	AR	O2	ATM	N2	AR	O2	N2/AR	NR/O2	NR/O2	AR/O2	LIG	VAP	LIG	VAP
0.	0.	0.	0.	1.0001	1.0001	1.16	3.865	1.939	1.000	2.519	3.865	1.934	-1807.	1167.	13.2	7.482	
0.	0.1	0.	0.1417	0.8584	0.8584	1.22	3.813	1.917	0.994	2.561	3.780	1.905	-1823.	1040.	12.9	7.173	
0.	0.2	0.	0.2645	0.7355	0.7355	1.28	3.761	1.895	0.989	2.603	3.714	1.898	-1839.	920.	12.6	6.931	
0.	0.3	0.	0.3737	0.6264	0.6264	1.33	3.709	1.874	0.984	2.645	3.648	1.892	-1855.	803.	12.4	6.759	
0.	0.4	0.	0.4733	0.5260	0.5260	1.37	3.657	1.853	0.979	2.687	3.582	1.886	-1871.	691.	12.2	6.617	
0.	0.5	0.	0.5602	0.4339	0.4339	1.41	3.605	1.832	0.974	2.729	3.516	1.880	-1888.	585.	12.0	6.499	
0.	0.6	0.	0.6346	0.3499	0.3499	1.44	3.553	1.811	0.969	2.771	3.450	1.874	-1904.	485.	11.8	6.393	
0.	0.7	0.	0.7069	0.2759	0.2759	1.47	3.501	1.790	0.964	2.813	3.384	1.868	-1920.	391.	11.6	6.297	
0.	0.8	0.	0.7674	0.2144	0.2144	1.50	3.449	1.769	0.959	2.855	3.318	1.862	-1936.	303.	11.4	6.211	
0.	0.9	0.	0.8177	0.1604	0.1604	1.52	3.397	1.748	0.954	2.897	3.252	1.856	-1952.	221.	11.2	6.135	
0.	1.0	0.	0.8577	0.1123	0.1123	1.54	3.345	1.727	0.949	2.939	3.186	1.850	-1968.	145.	11.0	6.069	
0.025	0.	0.0893	0.	0.9107	0.9107	1.56	3.293	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.025	0.1	0.1841	0.1293	0.7607	0.7607	1.57	3.264	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.025	0.2	0.2799	0.2427	0.6775	0.6775	1.58	3.235	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.025	0.3	0.3757	0.3451	0.5776	0.5776	1.59	3.206	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.025	0.4	0.4715	0.4379	0.4803	0.4803	1.60	3.177	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.025	0.5	0.5673	0.5253	0.4030	0.4030	1.61	3.148	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.025	0.6	0.6631	0.6106	0.3263	0.3263	1.62	3.119	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.025	0.7	0.7589	0.6886	0.2495	0.2495	1.63	3.090	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.025	0.8	0.8547	0.7896	0.1823	0.1823	1.64	3.061	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.025	0.9	0.9505	0.8901	0.1222	0.1222	1.65	3.032	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.025	1.0	0.9463	0.9374	0.	0.	1.66	3.003	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.100	0.	0.2701	0.	0.7299	0.7299	1.67	2.974	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.100	0.1	0.4662	0.3185	0.5411	0.5411	1.68	2.945	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.100	0.2	0.6623	0.4709	0.4377	0.4377	1.69	2.916	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.100	0.3	0.8584	0.6264	0.3576	0.3576	1.70	2.887	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.100	0.4	1.0545	0.7859	0.2851	0.2851	1.71	2.858	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.100	0.5	1.2506	0.9454	0.2200	0.2200	1.72	2.829	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.100	0.6	1.4467	1.1049	0.1609	0.1609	1.73	2.800	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.100	0.7	1.6428	1.2644	0.1018	0.1018	1.74	2.771	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.100	0.8	1.8389	1.4239	0.0427	0.0427	1.75	2.742	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.100	0.9	2.0350	1.5834	0.0036	0.0036	1.76	2.713	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.100	1.0	2.2311	1.7429	0.	0.	1.77	2.684	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.200	0.	0.5496	0.4504	0.4800	0.4800	1.78	2.655	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.200	0.1	0.7457	0.6099	0.3419	0.3419	1.79	2.626	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.200	0.2	0.9418	0.7694	0.2038	0.2038	1.80	2.597	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.200	0.3	1.1379	0.9289	0.0657	0.0657	1.81	2.568	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.200	0.4	1.3340	1.0884	0.0076	0.0076	1.82	2.539	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.200	0.5	1.5301	1.2479	0.0000	0.0000	1.83	2.510	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.200	0.6	1.7262	1.4074	0.0000	0.0000	1.84	2.481	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.200	0.7	1.9223	1.5669	0.0000	0.0000	1.85	2.452	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.200	0.8	2.1184	1.7264	0.0000	0.0000	1.86	2.423	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.200	0.9	2.3145	1.8859	0.0000	0.0000	1.87	2.394	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.200	1.0	2.5106	2.0454	0.0000	0.0000	1.88	2.365	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.300	0.	0.8711	0.	0.5289	0.5289	1.89	2.336	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.300	0.1	1.0672	0.6886	0.3908	0.3908	1.90	2.307	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.300	0.2	1.2633	0.8481	0.2527	0.2527	1.91	2.278	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.300	0.3	1.4594	1.0076	0.1146	0.1146	1.92	2.249	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.300	0.4	1.6555	1.1671	0.0000	0.0000	1.93	2.220	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.300	0.5	1.8516	1.3266	0.0000	0.0000	1.94	2.191	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.300	0.6	2.0477	1.4861	0.0000	0.0000	1.95	2.162	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.300	0.7	2.2438	1.6456	0.0000	0.0000	1.96	2.133	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.300	0.8	2.4399	1.8051	0.0000	0.0000	1.97	2.104	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.300	0.9	2.6360	1.9646	0.0000	0.0000	1.98	2.075	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.300	1.0	2.8321	2.1241	0.0000	0.0000	1.99	2.046	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.400	0.	1.2967	0.	0.4033	0.4033	2.00	2.017	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.400	0.1	1.4928	0.5628	0.2652	0.2652	2.01	1.988	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.400	0.2	1.6889	0.7223	0.1271	0.1271	2.02	1.959	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.400	0.3	1.8850	0.8818	0.0000	0.0000	2.03	1.930	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.400	0.4	2.0811	1.0413	0.0000	0.0000	2.04	1.901	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.400	0.5	2.2772	1.2008	0.0000	0.0000	2.05	1.872	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.400	0.6	2.4733	1.3603	0.0000	0.0000	2.06	1.843	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.400	0.7	2.6694	1.5198	0.0000	0.0000	2.07	1.814	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.8	6.013	
0.400	0.8	2.8655	1.6793	0.0000	0.0000	2.08	1.785	1.706	0.944	2.981	3.120	1.844	-1984.	78.	10.		

LIQUID MOLE FRACTION	VAPOR MOLE FRACTION		PRESSURE			EQUIL CONST			RELATIVE VOL			ENTHALPY		HEAT CAPACITY		
	N2	AR/AR+O2	N2	AR	O2	ATM	N2	AR	O2	N2/AR	N2/O2	AR/O2	LIG	VAP	LIG	VAP
0.0	0.	0.	0.	0.	0.	1.53	2.011	1.490	1.000	2.414	3.011	1.494	-1746.	1133.	13.0	7.546
0.1	0.	0.	0.1388	0.6613	1.60	2.269	1.388	0.957	2.442	3.041	1.451	-1756.	1089.	13.0	7.277	
0.2	0.	0.	0.2601	0.7400	1.67	2.213	1.301	0.925	2.471	3.074	1.408	-1766.	1044.	12.9	6.987	
0.3	0.	0.	0.3688	0.6313	1.73	2.073	1.229	0.902	2.500	3.107	1.363	-1775.	1007.	12.9	6.682	
0.4	0.	0.	0.4567	0.5434	1.78	2.002	1.171	0.886	2.529	3.142	1.322	-1783.	973.	12.9	6.401	
0.5	0.	0.	0.5259	0.4743	1.83	2.075	1.123	0.877	2.559	3.179	1.281	-1790.	941.	12.9	6.145	
0.6	0.	0.	0.5777	0.4209	1.87	2.208	1.085	0.873	2.589	3.216	1.242	-1796.	911.	12.9	5.907	
0.7	0.	0.	0.6236	0.3783	1.94	2.279	1.053	0.882	2.619	3.255	1.205	-1801.	881.	12.9	5.691	
0.8	0.	0.	0.6648	0.3404	1.98	2.273	1.012	0.894	2.648	3.295	1.180	-1805.	852.	12.9	5.503	
0.9	0.	0.	0.7022	0.3078	1.98	2.213	0.963	0.913	2.677	3.336	1.156	-1808.	823.	12.9	5.336	
1.0	0.	0.	0.7361	0.2801	1.93	2.085	0.918	0.932	2.706	3.379	1.133	-1810.	793.	12.9	5.189	
0.0	0.1	0.	0.0793	0.1273	1.70	2.173	1.308	0.944	2.430	3.019	1.444	-1723.	1131.	13.3	7.976	
0.0	0.2	0.	0.1756	0.2399	1.76	2.023	1.231	0.876	2.485	3.043	1.401	-1737.	1049.	13.0	7.109	
0.0	0.3	0.	0.2725	0.3415	1.82	2.002	1.168	0.859	2.485	3.079	1.360	-1751.	984.	12.9	6.719	
0.0	0.4	0.	0.3711	0.4332	1.87	2.005	1.116	0.846	2.514	3.116	1.319	-1764.	924.	12.9	6.328	
0.0	0.5	0.	0.4704	0.5252	1.92	2.279	1.073	0.836	2.543	3.254	1.280	-1776.	869.	12.9	5.938	
0.0	0.6	0.	0.5704	0.6174	1.98	2.279	1.038	0.836	2.572	3.294	1.242	-1787.	819.	12.9	5.548	
0.0	0.7	0.	0.6711	0.7100	1.99	2.227	0.998	0.845	2.601	3.337	1.205	-1797.	774.	12.9	5.158	
0.0	0.8	0.	0.7725	0.8022	2.05	2.227	0.958	0.855	2.630	3.382	1.180	-1807.	733.	12.9	4.768	
0.0	0.9	0.	0.8746	0.8944	2.07	2.173	0.912	0.864	2.659	3.429	1.156	-1817.	693.	12.9	4.378	
1.0	0.	0.	0.7361	0.2801	1.93	2.085	0.918	0.932	2.688	3.479	1.133	-1828.	653.	12.9	3.988	
1.0	0.1	0.	0.2667	0.1003	1.99	2.267	1.115	0.782	2.392	3.471	1.426	-1806.	1099.	13.0	7.489	
1.0	0.2	0.	0.2970	0.1814	2.05	2.270	1.063	0.782	2.417	3.511	1.389	-1812.	1049.	12.9	7.109	
1.0	0.3	0.	0.2499	0.2792	2.10	2.490	1.019	0.756	2.443	3.559	1.349	-1818.	1000.	12.9	6.719	
1.0	0.4	0.	0.2024	0.3836	2.14	2.424	0.952	0.749	2.469	3.609	1.312	-1823.	951.	12.9	6.328	
1.0	0.5	0.	0.2372	0.4978	2.18	2.372	0.901	0.745	2.495	3.663	1.276	-1828.	902.	12.9	5.938	
1.0	0.6	0.	0.2330	0.6091	2.22	2.330	0.824	0.745	2.521	3.723	1.241	-1833.	853.	12.9	5.548	
1.0	0.7	0.	0.2227	0.7188	2.25	2.299	0.802	0.748	2.548	3.779	1.207	-1838.	804.	12.9	5.158	
1.0	0.8	0.	0.2227	0.8269	2.28	2.277	0.805	0.754	2.575	3.837	1.174	-1843.	755.	12.9	4.768	
1.0	0.9	0.	0.2226	0.9341	2.31	2.265	0.871	0.763	2.602	3.895	1.142	-1848.	706.	12.9	4.378	
1.0	1.0	0.	0.2226	0.9341	2.31	2.265	0.871	0.763	2.629	3.953	1.110	-1853.	657.	12.9	3.988	
0.0	0.	0.	0.4950	0.5050	2.32	2.270	0.940	0.692	2.321	3.336	1.438	-1800.	1119.	13.0	7.791	
0.0	0.1	0.	0.4414	0.5784	2.36	2.207	0.920	0.672	2.343	3.387	1.403	-1814.	1069.	13.0	7.401	
0.0	0.2	0.	0.4299	0.5701	2.41	2.149	0.900	0.664	2.365	3.438	1.368	-1828.	1019.	13.0	7.011	
0.0	0.3	0.	0.4201	0.5712	2.45	2.100	0.881	0.656	2.387	3.489	1.333	-1842.	969.	13.0	6.621	
0.0	0.4	0.	0.4119	0.5735	2.49	2.059	0.865	0.656	2.410	3.540	1.302	-1856.	919.	12.9	6.231	
0.0	0.5	0.	0.4051	0.5751	2.52	2.025	0.853	0.659	2.432	3.591	1.271	-1870.	869.	12.9	5.841	
0.0	0.6	0.	0.3996	0.5767	2.56	1.998	0.844	0.657	2.455	3.642	1.241	-1884.	819.	12.9	5.451	
0.0	0.7	0.	0.3952	0.5783	2.59	1.977	0.798	0.660	2.478	3.693	1.209	-1898.	769.	12.9	5.061	
0.0	0.8	0.	0.3920	0.5808	2.62	1.961	0.784	0.669	2.501	3.744	1.180	-1912.	719.	12.9	4.671	
0.0	0.9	0.	0.3893	0.5844	2.65	1.951	0.773	0.671	2.525	3.795	1.151	-1926.	669.	12.9	4.281	
0.0	1.0	0.	0.3873	0.6111	2.67	1.947	0.763	0.680	2.549	3.846	1.123	-1941.	619.	12.9	3.891	
0.0	0.	0.	0.5793	0.4207	2.68	1.931	0.848	0.612	2.277	3.409	1.410	-1830.	1107.	13.0	7.704	
0.0	0.1	0.	0.5069	0.5076	2.72	1.890	0.823	0.597	2.299	3.460	1.374	-1844.	1057.	13.0	7.314	
0.0	0.2	0.	0.5061	0.5121	2.76	1.854	0.801	0.593	2.314	3.511	1.339	-1858.	1007.	13.0	6.924	
0.0	0.3	0.	0.5047	0.5180	2.79	1.822	0.781	0.591	2.333	3.562	1.302	-1872.	957.	13.0	6.534	
0.0	0.4	0.	0.5035	0.5237	2.82	1.795	0.763	0.589	2.352	3.613	1.267	-1886.	907.	13.0	6.144	
0.0	0.5	0.	0.5021	0.5301	2.85	1.772	0.747	0.589	2.371	3.664	1.232	-1900.	857.	13.0	5.754	
0.0	0.6	0.	0.5011	0.5361	2.88	1.754	0.734	0.592	2.391	3.715	1.200	-1914.	807.	13.0	5.364	
0.0	0.7	0.	0.5004	0.5424	2.91	1.739	0.721	0.595	2.410	3.766	1.171	-1928.	757.	13.0	4.974	
0.0	0.8	0.	0.5001	0.5488	2.94	1.727	0.711	0.599	2.430	3.817	1.142	-1942.	707.	13.0	4.584	
0.0	0.9	0.	0.5001	0.5552	2.97	1.719	0.702	0.601	2.450	3.868	1.114	-1956.	657.	13.0	4.194	
0.0	1.0	0.	0.5001	0.5616	2.99	1.714	0.694	0.601	2.470	3.919	1.086	-1970.	607.	13.0	3.804	
0.0	0.	0.	0.6724	0.3276	3.03	1.682	0.757	0.543	2.232	3.284	1.382	-1860.	1099.	13.0	7.941	
0.0	0.1	0.	0.6202	0.3898	3.06	1.656	0.734	0.543	2.248	3.335	1.347	-1874.	1049.	13.0	7.551	
0.0	0.2	0.	0.6324	0.3676	3.09	1.634	0.722	0.542	2.264	3.386	1.312	-1888.	999.	13.0	7.161	
0.0	0.3	0.	0.6483	0.3574	3.12	1.613	0.708	0.541	2.280	3.437	1.277	-1902.	949.	13.0	6.771	
0.0	0.4	0.	0.6683	0.3480	3.15	1.596	0.695	0.542	2.296	3.488	1.242	-1916.	899.	13.0	6.381	
0.0	0.5	0.	0.6922	0.3394	3.18	1.580	0.684	0.543	2.312	3.539	1.207	-1930.	849.	13.0	5.991	
0.0	0.6	0.	0.7200	0.2920	3.21	1.566	0.673	0.544	2.328	3.590	1.172	-1944.	799.	13.0	5.601	
0.0	0.7	0.	0.7517	0.2456	3.23	1.557	0.663	0.547	2.344	3.641	1.137	-1958.	749.	13.0	5.211	
0.0	0.8	0.	0.7874	0.2000	3.25	1.546	0.654	0.550	2.361	3.692	1.102	-1972.	699.	13.0	4.821	
0.0	0.9	0.	0.8267	0.1733	3.28	1.542	0.648	0.554	2.378	3.743	1.067	-1986.	649.	13.0	4.431	
0.0	1.0	0.	0.8689	0.1312	3.30	1.537	0.642	0.559	2.394	3.794	1.032	-2000.	599.	13.0	4.041	
0.0	0.	0.	0.7488	0.2512	3.34	1.484	0.683	0.504	2.189	3.295	1.346	-1868.	994.	13.0	7.281	
0.0	0.1	0.	0.7099	0.2936	3.40	1.460	0.672	0.504	2.202	3.346	1.311	-1882.	944.	13.0	6.891	
0.0	0.2	0.	0.7326	0.2861	3.42	1.445	0.661	0.503	2.219	3.397	1.276	-1896.	894.	13.0	6.501	
0.0	0.3	0.	0.7580	0.2478	3.45	1.432	0.652	0.504	2.236	3.448	1.241	-1910.	844.	13.0	6.111	
0.0	0.4	0.	0.7856	0.2186	3.47	1.420	0.643	0.505	2.251	3.499	1.206	-1924.	794.	13.0	5.721	
0.0	0.5	0.	0.8152	0.1906	3.49	1.408	0.634	0.506	2.266	3.550	1.171	-1938.	744.	13.0	5.331	
0.0	0.6	0.	0.8467	0.1646	3.52	1.401	0.627	0.507	2.281	3.601	1.136	-1952.	694.	13.0	4.941	
0.0	0.7	0.	0.8799	0.1406	3.54	1.394	0.620	0.510	2.296	3.652	1.101	-1966.	644.	13.0	4.551	
0.0	0.8	0.	0.9147	0.1184	3.56	1.390	0.613	0.512	2.311	3.703	1.066	-1980.	594.	13.0	4.161	
0.0	0.9	0.	0.9511	0.1000	3.58	1.387	0.606	0.515	2.326	3.754	1.031	-1994.	544.	13.0	3.771	
0.0	1.0	0.	0.9889	0.0112	3.60	1.388	0.602	0.519	2.341	3.805	1.000	-2008.	494.	13.0	3.381	
0.0	0.	0.	0.8107	0.1894	3.71	1.351	0.622	0.474	2.147	3.293	1.329	-1820.	1004.	14.1	8.090	
0.0	0.1	0.	0.8047	0.2049	3.73	1.341	0.622	0.474	2.167	3.344	1.294	-1834.	954.	14.0	7.700	
0.0	0.2	0.	0.7992	0.2197	3.75	1.332	0.615	0.474	2.187	3.395	1.259	-1848.	904.	14.0	7.310	
0.0	0.3	0.	0													

TEMPERATURE	LIQUID MOLE FRACTION				VAPOR MOLE FRACTION				PRESSURE	EQUIL CONST				RELATIVE VOL			ENTHALPY		HEAT CAPACITY	
	N <sub>2</sub>				O <sub>2</sub>					N <sub>2</sub>	O <sub>2</sub>	N <sub>2</sub> /O <sub>2</sub>	N <sub>2</sub> /O <sub>2</sub>	N <sub>2</sub> /O <sub>2</sub>	LIG	VAP	LIG	VAP		
	N <sub>2</sub>	AR/AR-O <sub>2</sub>	N <sub>2</sub>	O <sub>2</sub>	ATM	N <sub>2</sub>	AR	O <sub>2</sub>											N <sub>2</sub> /AR	N <sub>2</sub> /O <sub>2</sub>
0.	0.	0.	0.	1.0000	1.97	3.381	1.462	1.000	2.312	3.380	1.462	-1674.	1158.	13.3	7.659					
0.1	0.	0.	0.1362	0.8638	2.06	3.185	1.362	0.980	2.337	3.317	1.419	-1693.	1110.	13.0	7.396					
0.2	0.	0.	0.2583	0.7428	2.14	3.078	1.281	0.930	2.363	3.256	1.378	-1712.	1067.	12.6	7.164					
0.3	0.	0.	0.3648	0.6387	2.22	2.992	1.219	0.908	2.389	3.195	1.338	-1730.	1029.	12.6	6.957					
0.4	0.	0.	0.4542	0.5531	2.28	2.923	1.166	0.883	2.415	3.136	1.299	-1748.	994.	12.3	6.768					
0.5	0.	0.	0.5276	0.4824	2.34	2.863	1.119	0.863	2.441	3.075	1.261	-1766.	961.	12.1	6.595					
0.6	0.	0.	0.5877	0.4226	2.39	2.810	1.079	0.846	2.467	3.012	1.224	-1783.	929.	11.9	6.437					
0.7	0.	0.	0.6353	0.3728	2.43	2.762	1.045	0.833	2.494	2.956	1.189	-1800.	898.	11.6	6.291					
0.8	0.	0.	0.6722	0.3318	2.47	2.719	1.018	0.820	2.522	2.901	1.154	-1817.	868.	11.4	6.154					
0.9	0.	0.	0.7011	0.2982	2.50	2.679	1.011	0.807	2.549	2.857	1.121	-1833.	838.	11.3	6.023					
1.0	0.	0.	0.7222	0.2700	2.53	2.648	1.000	0.794	2.577	2.825	1.088	-1848.	807.	11.2	5.897					
0.25	0.	0.	0.6791	0.3211	2.49	2.713	1.074	0.848	2.502	2.946	1.455	-1656.	1159.	13.3	7.401					
0.25	0.1	0.	0.6749	0.3256	2.48	2.706	1.080	0.811	2.526	2.908	1.413	-1675.	1111.	13.1	7.420					
0.25	0.2	0.	0.6715	0.3374	2.46	2.681	1.217	0.886	2.381	3.228	1.373	-1693.	1071.	12.9	7.235					
0.25	0.3	0.	0.6688	0.3509	2.43	2.652	1.159	0.866	2.379	3.170	1.334	-1711.	1035.	12.6	7.039					
0.25	0.4	0.	0.6669	0.3659	2.39	2.625	1.110	0.856	2.401	3.113	1.297	-1730.	1002.	12.4	6.858					
0.25	0.5	0.	0.6659	0.3815	2.44	2.600	1.079	0.849	2.426	3.056	1.260	-1748.	971.	12.2	6.682					
0.25	0.6	0.	0.6658	0.3976	2.49	2.576	1.057	0.847	2.452	3.001	1.224	-1766.	941.	11.9	6.513					
0.25	0.7	0.	0.6674	0.4141	2.54	2.554	1.041	0.849	2.478	2.947	1.189	-1783.	912.	11.7	6.347					
0.25	0.8	0.	0.6709	0.4309	2.58	2.533	1.030	0.856	2.504	2.894	1.154	-1800.	883.	11.6	6.181					
0.25	0.9	0.	0.6761	0.4480	2.61	2.514	1.023	0.867	2.531	2.842	1.121	-1817.	854.	11.5	6.015					
0.25	1.0	0.	0.6830	0.4654	2.63	2.497	1.020	0.882	2.558	2.792	1.088	-1833.	825.	11.4	5.850					
1.00	0.	0.	0.2857	0.7143	2.46	2.687	1.171	0.816	2.370	3.284	1.434	-1618.	1148.	13.3	7.401					
1.00	0.1	0.	0.2849	0.7101	2.43	2.649	1.117	0.797	2.292	3.200	1.396	-1637.	1112.	13.2	7.401					
1.00	0.2	0.	0.2846	0.7014	2.40	2.603	1.063	0.782	2.314	3.147	1.360	-1657.	1080.	13.0	7.401					
1.00	0.3	0.	0.2847	0.6880	2.44	2.587	1.021	0.771	2.337	3.094	1.324	-1677.	1050.	12.8	7.401					
1.00	0.4	0.	0.2852	0.6709	2.71	2.326	0.986	0.765	2.360	3.042	1.288	-1697.	1021.	12.6	7.112					
1.00	0.5	0.	0.2877	0.6501	2.76	2.277	0.956	0.761	2.383	2.992	1.252	-1718.	995.	12.4	6.967					
1.00	0.6	0.	0.2929	0.6259	2.81	2.239	0.931	0.761	2.406	2.942	1.217	-1739.	969.	12.2	6.824					
1.00	0.7	0.	0.2999	0.5999	2.86	2.210	0.910	0.764	2.430	2.893	1.181	-1760.	944.	12.0	6.684					
1.00	0.8	0.	0.3082	0.5728	2.92	2.179	0.893	0.773	2.454	2.845	1.146	-1782.	920.	11.8	6.544					
1.00	0.9	0.	0.3179	0.5454	2.98	2.147	0.880	0.779	2.478	2.798	1.112	-1804.	896.	11.6	6.403					
1.00	1.0	0.	0.3276	0.5180	2.95	2.126	0.870	0.791	2.502	2.752	1.078	-1826.	871.	11.4	6.258					
2.00	0.	0.	0.4395	0.5610	2.92	2.107	0.864	0.791	2.328	3.133	1.440	-1522.	1137.	13.0	7.401					
2.00	0.1	0.	0.4266	0.5759	2.98	2.133	0.949	0.801	2.247	3.057	1.374	-1541.	1110.	12.9	7.401					
2.00	0.2	0.	0.4158	0.5888	3.03	2.079	0.917	0.804	2.266	3.001	1.342	-1562.	1084.	12.7	7.401					
2.00	0.3	0.	0.4066	0.6000	3.08	2.033	0.889	0.809	2.286	2.946	1.311	-1583.	1061.	12.5	7.401					
2.00	0.4	0.	0.3989	0.6098	3.13	1.994	0.865	0.816	2.306	2.891	1.280	-1604.	1038.	12.4	7.401					
2.00	0.5	0.	0.3925	0.6175	3.17	1.963	0.844	0.819	2.326	2.836	1.250	-1625.	1017.	12.2	7.267					
2.00	0.6	0.	0.3874	0.6236	3.21	1.937	0.826	0.826	2.346	2.781	1.221	-1647.	996.	12.0	7.133					
2.00	0.7	0.	0.3834	0.6280	3.25	1.917	0.810	0.829	2.367	2.727	1.193	-1669.	975.	11.8	7.001					
2.00	0.8	0.	0.3805	0.6311	3.29	1.901	0.797	0.834	2.387	2.671	1.165	-1692.	954.	11.6	6.869					
2.00	0.9	0.	0.3787	0.6331	3.32	1.889	0.786	0.841	2.408	2.614	1.138	-1715.	933.	11.4	6.737					
2.00	1.0	0.	0.3779	0.6342	3.35	1.880	0.778	0.842	2.429	2.559	1.111	-1738.	912.	11.2	6.604					
3.00	0.	0.	0.5639	0.4361	3.34	1.880	0.803	0.833	2.186	3.117	1.360	-1461.	1127.	13.0	8.072					
3.00	0.1	0.	0.5522	0.4505	3.41	1.841	0.806	0.818	2.203	3.076	1.352	-1481.	1100.	12.9	7.963					
3.00	0.2	0.	0.5419	0.4619	3.48	1.804	0.814	0.815	2.220	3.034	1.344	-1502.	1074.	12.7	7.852					
3.00	0.3	0.	0.5331	0.4699	3.49	1.777	0.795	0.813	2.238	2.991	1.337	-1523.	1048.	12.5	7.741					
3.00	0.4	0.	0.5255	0.4759	3.53	1.759	0.777	0.812	2.253	2.943	1.327	-1544.	1024.	12.3	7.630					
3.00	0.5	0.	0.5191	0.4807	3.57	1.73	0.762	0.812	2.271	2.896	1.319	-1565.	1001.	12.1	7.519					
3.00	0.6	0.	0.5138	0.4844	3.61	1.71	0.749	0.814	2.288	2.849	1.311	-1586.	978.	11.9	7.408					
3.00	0.7	0.	0.5095	0.4871	3.64	1.69	0.737	0.817	2.305	2.793	1.304	-1607.	955.	11.7	7.297					
3.00	0.8	0.	0.5063	0.4899	3.67	1.680	0.727	0.821	2.323	2.746	1.297	-1628.	932.	11.5	7.186					
3.00	0.9	0.	0.5040	0.4922	3.71	1.668	0.718	0.826	2.340	2.690	1.290	-1649.	909.	11.3	7.075					
3.00	1.0	0.	0.5027	0.4944	3.74	1.658	0.711	0.833	2.358	2.643	1.283	-1670.	886.	11.2	6.964					
4.00	0.	0.	0.6595	0.3405	3.78	1.649	0.768	0.868	2.146	2.905	1.354	-1390.	1117.	14.0	8.222					
4.00	0.1	0.	0.6487	0.3551	3.82	1.624	0.752	0.865	2.163	2.872	1.336	-1411.	1090.	13.9	8.111					
4.00	0.2	0.	0.6394	0.3685	3.86	1.602	0.737	0.864	2.174	2.840	1.317	-1432.	1063.	13.7	8.000					
4.00	0.3	0.	0.6312	0.3802	3.89	1.583	0.724	0.864	2.188	2.808	1.298	-1453.	1036.	13.5	7.889					
4.00	0.4	0.	0.6244	0.3909	3.93	1.566	0.711	0.864	2.202	2.776	1.280	-1474.	1010.	13.3	7.778					
4.00	0.5	0.	0.6186	0.4000	3.96	1.552	0.700	0.865	2.217	2.744	1.261	-1495.	984.	13.1	7.667					
4.00	0.6	0.	0.6137	0.4084	3.99	1.539	0.690	0.867	2.231	2.712	1.242	-1516.	958.	12.9	7.556					
4.00	0.7	0.	0.6096	0.4163	4.02	1.529	0.681	0.869	2.245	2.680	1.224	-1537.	932.	12.7	7.445					
4.00	0.8	0.	0.6064	0.4230	4.05	1.521	0.673	0.873	2.260	2.648	1.205	-1558.	906.	12.5	7.334					
4.00	0.9	0.	0.6039	0.4296	4.08	1.515	0.666	0.877												

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION		PRESSURE ATM	EQUIL CONST			RELATIVE VOL			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
N <sub>2</sub>	AR/AR+O <sub>2</sub>	N <sub>2</sub>	AR		N <sub>2</sub>	AR	O <sub>2</sub>	N <sub>2</sub> /AR	N <sub>2</sub> /O <sub>2</sub>	AR/O <sub>2</sub>	LIG	VAP	LIG	VAP
0.00	0.00	0.00	0.00	2.93	3.170	1.432	1.000	2.214	3.100	1.431	-1408.	1181.	13.3	7.767
0.01	0.0	0.134	0.0664	2.92	2.996	1.340	0.963	2.236	3.112	1.392	-1428.	1132.	13.3	7.933
0.02	0.0	0.258	0.1498	2.72	2.856	1.264	0.934	2.269	3.056	1.353	-1447.	1088.	12.9	7.306
0.03	0.0	0.382	0.1399	2.66	2.743	1.202	0.914	2.282	3.001	1.315	-1467.	1049.	12.7	7.100
0.04	0.0	0.506	0.1300	2.60	2.653	1.151	0.900	2.305	2.947	1.279	-1487.	1013.	12.5	6.908
0.05	0.0	0.630	0.1201	2.55	2.581	1.109	0.892	2.328	2.894	1.243	-1507.	978.	12.3	6.724
0.06	0.0	0.754	0.1102	2.51	2.527	1.075	0.889	2.351	2.842	1.209	-1527.	946.	12.1	6.546
0.07	0.0	0.878	0.1003	2.48	2.480	1.047	0.891	2.375	2.791	1.175	-1547.	914.	11.8	6.376
0.08	0.0	1.002	0.0904	2.45	2.440	1.024	0.898	2.399	2.742	1.143	-1567.	882.	11.6	6.212
0.09	0.0	1.126	0.0805	2.42	2.408	1.002	0.910	2.424	2.693	1.111	-1587.	851.	11.4	6.050
0.10	0.0	1.250	0.0706	2.39	2.384	0.980	0.926	2.448	2.643	1.080	-1607.	820.	11.2	5.892
0.11	0.1	0.174	0.4998	2.36	2.362	1.383	0.950	2.474	3.147	1.428	-1597.	1178.	13.4	7.625
0.12	0.1	0.348	0.1241	2.28	2.332	1.273	0.918	2.506	3.085	1.386	-1617.	1133.	13.1	7.390
0.13	0.1	0.522	0.0697	2.25	2.304	1.206	0.894	2.540	3.031	1.348	-1637.	1092.	12.8	7.166
0.14	0.1	0.696	0.0396	2.22	2.280	1.151	0.877	2.574	2.978	1.312	-1657.	1055.	12.6	6.954
0.15	0.1	0.870	0.0253	2.19	2.258	1.105	0.865	2.608	2.926	1.276	-1677.	1020.	12.4	6.752
0.16	0.1	1.044	0.0158	2.16	2.238	1.067	0.859	2.642	2.874	1.242	-1697.	988.	12.3	6.562
0.17	0.1	1.218	0.0092	2.13	2.220	1.035	0.857	2.677	2.824	1.208	-1717.	957.	12.1	6.384
0.18	0.1	1.392	0.0048	2.10	2.204	1.005	0.852	2.712	2.775	1.176	-1737.	926.	11.9	6.216
0.19	0.1	1.566	0.0024	2.07	2.190	0.978	0.856	2.747	2.727	1.144	-1757.	896.	11.7	6.058
0.20	0.1	1.740	0.0012	2.04	2.178	0.952	0.860	2.782	2.679	1.113	-1777.	866.	11.5	5.910
0.21	0.1	1.914	0.0006	2.01	2.168	0.928	0.864	2.817	2.631	1.083	-1797.	836.	11.3	5.772
0.22	0.1	2.088	0.0003	1.98	2.158	0.905	0.868	2.852	2.583	1.053	-1817.	806.	11.1	5.644
0.23	0.1	2.262	0.0001	1.95	2.148	0.883	0.872	2.887	2.535	1.023	-1837.	776.	10.9	5.526
0.24	0.1	2.436	0.0000	1.92	2.138	0.862	0.876	2.922	2.487	0.993	-1857.	746.	10.7	5.418
0.25	0.1	2.610	0.0000	1.89	2.128	0.842	0.880	2.957	2.439	0.963	-1877.	716.	10.5	5.320
0.26	0.1	2.784	0.0000	1.86	2.118	0.822	0.884	2.992	2.391	0.933	-1897.	686.	10.3	5.232
0.27	0.1	2.958	0.0000	1.83	2.108	0.803	0.888	3.027	2.343	0.903	-1917.	656.	10.1	5.154
0.28	0.1	3.132	0.0000	1.80	2.098	0.784	0.892	3.062	2.295	0.873	-1937.	626.	9.9	5.086
0.29	0.1	3.306	0.0000	1.77	2.088	0.766	0.896	3.097	2.247	0.843	-1957.	596.	9.7	5.028
0.30	0.1	3.480	0.0000	1.74	2.078	0.748	0.900	3.132	2.199	0.813	-1977.	566.	9.5	4.980
0.31	0.1	3.654	0.0000	1.71	2.068	0.731	0.904	3.167	2.151	0.783	-1997.	536.	9.3	4.942
0.32	0.1	3.828	0.0000	1.68	2.058	0.714	0.908	3.202	2.103	0.753	-2017.	506.	9.1	4.914
0.33	0.1	4.002	0.0000	1.65	2.048	0.698	0.912	3.237	2.055	0.723	-2037.	476.	8.9	4.896
0.34	0.1	4.176	0.0000	1.62	2.038	0.682	0.916	3.272	2.007	0.693	-2057.	446.	8.7	4.888
0.35	0.1	4.350	0.0000	1.59	2.028	0.667	0.920	3.307	1.959	0.663	-2077.	416.	8.5	4.880
0.36	0.1	4.524	0.0000	1.56	2.018	0.652	0.924	3.342	1.911	0.633	-2097.	386.	8.3	4.882
0.37	0.1	4.698	0.0000	1.53	2.008	0.637	0.928	3.377	1.863	0.603	-2117.	356.	8.1	4.894
0.38	0.1	4.872	0.0000	1.50	1.998	0.622	0.932	3.412	1.815	0.573	-2137.	326.	7.9	4.916
0.39	0.1	5.046	0.0000	1.47	1.988	0.607	0.936	3.447	1.767	0.543	-2157.	296.	7.7	4.948
0.40	0.1	5.220	0.0000	1.44	1.978	0.592	0.940	3.482	1.719	0.513	-2177.	266.	7.5	4.990
0.41	0.1	5.394	0.0000	1.41	1.968	0.577	0.944	3.517	1.671	0.483	-2197.	236.	7.3	5.042
0.42	0.1	5.568	0.0000	1.38	1.958	0.562	0.948	3.552	1.623	0.453	-2217.	206.	7.1	5.104
0.43	0.1	5.742	0.0000	1.35	1.948	0.547	0.952	3.587	1.575	0.423	-2237.	176.	6.9	5.176
0.44	0.1	5.916	0.0000	1.32	1.938	0.532	0.956	3.622	1.527	0.393	-2257.	146.	6.7	5.258
0.45	0.1	6.090	0.0000	1.29	1.928	0.517	0.960	3.657	1.479	0.363	-2277.	116.	6.5	5.350
0.46	0.1	6.264	0.0000	1.26	1.918	0.502	0.964	3.692	1.431	0.333	-2297.	86.	6.3	5.452
0.47	0.1	6.438	0.0000	1.23	1.908	0.487	0.968	3.727	1.383	0.303	-2317.	56.	6.1	5.564
0.48	0.1	6.612	0.0000	1.20	1.898	0.472	0.972	3.762	1.335	0.273	-2337.	26.	5.9	5.686
0.49	0.1	6.786	0.0000	1.17	1.888	0.457	0.976	3.797	1.287	0.243	-2357.	0.	5.7	5.818
0.50	0.1	6.960	0.0000	1.14	1.878	0.442	0.980	3.832	1.239	0.213	-2377.	-30.	5.5	5.960
0.51	0.1	7.134	0.0000	1.11	1.868	0.427	0.984	3.867	1.191	0.183	-2397.	-60.	5.3	6.112
0.52	0.1	7.308	0.0000	1.08	1.858	0.412	0.988	3.902	1.143	0.153	-2417.	-90.	5.1	6.274
0.53	0.1	7.482	0.0000	1.05	1.848	0.397	0.992	3.937	1.095	0.123	-2437.	-120.	4.9	6.446
0.54	0.1	7.656	0.0000	1.02	1.838	0.382	0.996	3.972	1.047	0.093	-2457.	-150.	4.7	6.628
0.55	0.1	7.830	0.0000	0.99	1.828	0.367	0.999	4.007	0.999	0.063	-2477.	-180.	4.5	6.820
0.56	0.1	8.004	0.0000	0.96	1.818	0.352	1.003	4.042	0.951	0.033	-2497.	-210.	4.3	7.022
0.57	0.1	8.178	0.0000	0.93	1.808	0.337	1.007	4.077	0.903	0.003	-2517.	-240.	4.1	7.234
0.58	0.1	8.352	0.0000	0.90	1.798	0.322	1.011	4.112	0.855	-0.027	-2537.	-270.	3.9	7.456
0.59	0.1	8.526	0.0000	0.87	1.788	0.307	1.015	4.147	0.807	-0.057	-2557.	-300.	3.7	7.698
0.60	0.1	8.700	0.0000	0.84	1.778	0.292	1.019	4.182	0.759	-0.087	-2577.	-330.	3.5	7.960
0.61	0.1	8.874	0.0000	0.81	1.768	0.277	1.023	4.217	0.711	-0.117	-2597.	-360.	3.3	8.232
0.62	0.1	9.048	0.0000	0.78	1.758	0.262	1.027	4.252	0.663	-0.147	-2617.	-390.	3.1	8.514
0.63	0.1	9.222	0.0000	0.75	1.748	0.247	1.031	4.287	0.615	-0.177	-2637.	-420.	2.9	8.806
0.64	0.1	9.396	0.0000	0.72	1.738	0.232	1.035	4.322	0.567	-0.207	-2657.	-450.	2.7	9.108
0.65	0.1	9.570	0.0000	0.69	1.728	0.217	1.039	4.357	0.519	-0.237	-2677.	-480.	2.5	9.420
0.66	0.1	9.744	0.0000	0.66	1.718	0.202	1.043	4.392	0.471	-0.267	-2697.	-510.	2.3	9.742
0.67	0.1	9.918	0.0000	0.63	1.708	0.187	1.047	4.427	0.423	-0.297	-2717.	-540.	2.1	10.074
0.68	0.1	10.092	0.0000	0.60	1.698	0.172	1.051	4.462	0.375	-0.327	-2737.	-570.	1.9	10.416
0.69	0.1	10.266	0.0000	0.57	1.688	0.157	1.055	4.497	0.327	-0.357	-2757.	-600.	1.7	10.768
0.70	0.1	10.440	0.0000	0.54	1.678	0.142	1.059	4.532	0.279	-0.387	-2777.	-630.	1.5	11.130
0.71	0.1	10.614	0.0000	0.51	1.668	0.127	1.063	4.567	0.231	-0.417	-2797.	-660.	1.3	11.502
0.72	0.1	10.788	0.0000	0.48	1.658	0.112	1.067	4.602	0.183	-0.447	-2817.	-690.	1.1	11.884
0.73	0.1	10.962	0.0000	0.45	1.648	0.097	1.071	4.637	0.135	-0.477	-2837.	-720.	0.9	12.276
0.74	0.1	11.136	0.0000	0.42	1.638	0.082	1.075	4.672	0.087	-0.507	-2857.	-750.	0.7	12.678
0.75	0.1	11.310	0.0000	0.39	1.628	0.067	1.079	4.707	0.039	-0.537	-2877.	-780.	0.5	13.090
0.76	0.1	11.484	0.0000	0.36	1.618	0.052	1.083	4.742	-0.009	-0.567	-2897.	-810.	0.3	13.502
0.77	0.1	11.658	0.0000	0.33	1.608	0.037	1.087	4.777	-0.061	-0.597	-2917.	-840.	0.1	13.924
0.78	0.1	11.832	0.0000	0.30	1.598	0.022	1.091	4.812	-0.113	-0.627	-2937.	-870.	-0.1	14.356
0.79	0.1	12.006	0.0000	0.27	1.588	0.007	1.095	4.847	-0.165	-0.657	-2957.	-900.	-0.3	14.808
0.80	0.1	12.180	0.0000	0.24	1.578	-0.008	1.099	4.882	-0.217	-0.687	-2977.	-930.	-0.5	15.280
0.														

Table with columns: LIQUID MOLE FRACTION (N2, AR, AR+O2), VAPOR MOLE FRACTION (N2, AR, O2), PRESSURE (ATM), EQUIL CONST (N2, AR, O2), RELATIVE VOL (N2/AR, N2/O2, AR/O2), ENTHALPY (BTU/LB MOLE) (LTD, VAP), HEAT CAPACITY (BTU/LB MOLE-R) (LTD, VAP). Rows represent various mole fractions and pressures.

TEMP	LIQUID MOLE FRACTION			VAPOR MOLE FRACTION			PRESSURE ATM	EQUIL CONST			RELATIVE VOL			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
	N2	AR	O2	N2	AR	O2		N2	AR	O2	N2/AR	N2/O2	AR/O2	LIG	VAP	LIG	VAP
0.0	0.0	0.0	1.0000	0.0000	0.0000	0.0000	3.90	2.796	1.378	1.000	2.150	2.796	1.378	-1474	1222	13.4	8.102
0.1	0.0	0.0	0.9999	0.0001	0.0000	0.0000	4.06	2.690	1.295	0.967	2.047	2.740	1.343	-1474	1171	13.3	7.864
0.2	0.0	0.0	0.9998	0.0002	0.0000	0.0000	4.22	2.595	1.233	0.942	2.005	2.702	1.309	-1474	1125	13.1	7.650
0.3	0.0	0.0	0.9996	0.0004	0.0000	0.0000	4.38	2.503	1.178	0.924	2.002	2.680	1.275	-1474	1081	13.0	7.453
0.4	0.0	0.0	0.9993	0.0007	0.0000	0.0000	4.53	2.420	1.133	0.911	2.100	2.611	1.243	-1474	1040	12.9	7.266
0.5	0.0	0.0	0.9989	0.0011	0.0000	0.0000	4.68	2.345	1.095	0.904	2.118	2.566	1.212	-1474	1000	12.8	7.087
0.6	0.0	0.0	0.9984	0.0016	0.0000	0.0000	4.83	2.278	1.065	0.902	2.136	2.523	1.181	-1474	972	12.8	6.911
0.7	0.0	0.0	0.9978	0.0022	0.0000	0.0000	4.97	2.220	1.041	0.904	2.155	2.481	1.151	-1474	946	12.8	6.735
0.8	0.0	0.0	0.9971	0.0029	0.0000	0.0000	5.10	2.169	1.022	0.911	2.173	2.439	1.122	-1474	924	12.8	6.557
0.9	0.0	0.0	0.9963	0.0037	0.0000	0.0000	5.22	2.125	1.009	0.922	2.192	2.399	1.094	-1474	907	12.8	6.373
1.0	0.0	0.0	0.9954	0.0046	0.0000	0.0000	5.34	2.087	1.000	0.938	2.211	2.359	1.066	-1474	893	12.8	6.181
1.0	0.1	0.0	0.8933	0.0968	0.0099	0.0037	4.12	2.655	1.313	0.950	2.023	2.770	1.370	-1455	1214	13.4	8.151
1.0	0.2	0.0	0.8033	0.1212	0.0155	0.0053	4.28	2.534	1.243	0.929	2.038	2.726	1.338	-1477	1171	13.3	7.931
1.0	0.3	0.0	0.6909	0.1510	0.0203	0.0073	4.45	2.434	1.185	0.908	2.055	2.681	1.305	-1477	1127	13.2	7.703
1.0	0.4	0.0	0.5568	0.1868	0.0251	0.0093	4.60	2.353	1.136	0.883	2.072	2.637	1.272	-1474	1084	13.1	7.474
1.0	0.5	0.0	0.4099	0.2270	0.0292	0.0113	4.75	2.287	1.095	0.862	2.090	2.593	1.241	-1474	1041	13.0	7.246
1.0	0.6	0.0	0.2600	0.2713	0.0327	0.0133	4.89	2.235	1.061	0.876	2.107	2.550	1.210	-1474	1000	12.9	7.018
1.0	0.7	0.0	0.1181	0.3187	0.0358	0.0153	5.02	2.194	1.033	0.875	2.125	2.508	1.180	-1474	962	12.9	6.791
1.0	0.8	0.0	0.0000	0.3692	0.0385	0.0174	5.15	2.160	1.010	0.877	2.143	2.467	1.151	-1474	924	12.8	6.563
1.0	0.9	0.0	0.0000	0.4227	0.0408	0.0194	5.27	2.132	0.983	0.884	2.161	2.427	1.123	-1474	887	12.8	6.335
1.0	1.0	0.0	0.0000	0.4793	0.0428	0.0214	5.39	2.109	0.960	0.894	2.179	2.387	1.095	-1474	851	12.8	6.107
1.0	0.1	0.1	0.8933	0.0968	0.0099	0.0037	4.12	2.655	1.313	0.950	2.023	2.770	1.370	-1455	1214	13.4	8.151
1.0	0.2	0.1	0.8227	0.0990	0.0170	0.0077	4.70	2.227	1.107	0.837	2.012	2.681	1.302	-1459	1167	13.3	7.931
1.0	0.3	0.1	0.7157	0.1170	0.0217	0.0117	4.91	2.157	1.064	0.823	2.027	2.620	1.272	-1458	1121	13.2	7.703
1.0	0.4	0.1	0.5722	0.1508	0.0260	0.0160	5.01	2.100	1.028	0.814	2.043	2.560	1.243	-1458	1078	13.1	7.474
1.0	0.5	0.1	0.4159	0.1870	0.0297	0.0202	5.11	2.052	0.997	0.808	2.059	2.501	1.214	-1458	1035	13.0	7.246
1.0	0.6	0.1	0.2603	0.2122	0.0321	0.0241	5.19	2.013	0.970	0.803	2.075	2.450	1.185	-1457	1000	12.9	7.018
1.0	0.7	0.1	0.1186	0.2411	0.0342	0.0281	5.24	1.980	0.948	0.805	2.091	2.404	1.156	-1457	962	12.9	6.791
1.0	0.8	0.1	0.0000	0.2742	0.0359	0.0321	5.28	1.950	0.930	0.806	2.107	2.358	1.127	-1456	924	12.8	6.563
1.0	0.9	0.1	0.0000	0.3127	0.0374	0.0360	5.31	1.924	0.915	0.814	2.123	2.310	1.100	-1456	887	12.8	6.335
1.0	1.0	0.1	0.0000	0.3559	0.0388	0.0394	5.33	1.901	0.900	0.824	2.140	2.264	1.074	-1456	851	12.8	6.107
1.0	0.1	0.2	0.8933	0.0968	0.0099	0.0037	4.12	2.655	1.313	0.950	2.023	2.770	1.370	-1455	1214	13.4	8.151
1.0	0.2	0.2	0.8227	0.0990	0.0170	0.0077	4.70	2.227	1.107	0.837	2.012	2.681	1.302	-1459	1167	13.3	7.931
1.0	0.3	0.2	0.7157	0.1170	0.0217	0.0117	4.91	2.157	1.064	0.823	2.027	2.620	1.272	-1458	1121	13.2	7.703
1.0	0.4	0.2	0.5722	0.1508	0.0260	0.0160	5.01	2.100	1.028	0.814	2.043	2.560	1.243	-1458	1078	13.1	7.474
1.0	0.5	0.2	0.4159	0.1870	0.0297	0.0202	5.11	2.052	0.997	0.808	2.059	2.501	1.214	-1458	1035	13.0	7.246
1.0	0.6	0.2	0.2603	0.2122	0.0321	0.0241	5.19	2.013	0.970	0.803	2.075	2.450	1.185	-1457	1000	12.9	7.018
1.0	0.7	0.2	0.1186	0.2411	0.0342	0.0281	5.24	1.980	0.948	0.805	2.091	2.404	1.156	-1457	962	12.9	6.791
1.0	0.8	0.2	0.0000	0.2742	0.0359	0.0321	5.28	1.950	0.930	0.806	2.107	2.358	1.127	-1456	924	12.8	6.563
1.0	0.9	0.2	0.0000	0.3127	0.0374	0.0360	5.31	1.924	0.915	0.814	2.123	2.310	1.100	-1456	887	12.8	6.335
1.0	1.0	0.2	0.0000	0.3559	0.0388	0.0394	5.33	1.901	0.900	0.824	2.140	2.264	1.074	-1456	851	12.8	6.107
1.0	0.1	0.3	0.8933	0.0968	0.0099	0.0037	4.12	2.655	1.313	0.950	2.023	2.770	1.370	-1455	1214	13.4	8.151
1.0	0.2	0.3	0.8227	0.0990	0.0170	0.0077	4.70	2.227	1.107	0.837	2.012	2.681	1.302	-1459	1167	13.3	7.931
1.0	0.3	0.3	0.7157	0.1170	0.0217	0.0117	4.91	2.157	1.064	0.823	2.027	2.620	1.272	-1458	1121	13.2	7.703
1.0	0.4	0.3	0.5722	0.1508	0.0260	0.0160	5.01	2.100	1.028	0.814	2.043	2.560	1.243	-1458	1078	13.1	7.474
1.0	0.5	0.3	0.4159	0.1870	0.0297	0.0202	5.11	2.052	0.997	0.808	2.059	2.501	1.214	-1458	1035	13.0	7.246
1.0	0.6	0.3	0.2603	0.2122	0.0321	0.0241	5.19	2.013	0.970	0.803	2.075	2.450	1.185	-1457	1000	12.9	7.018
1.0	0.7	0.3	0.1186	0.2411	0.0342	0.0281	5.24	1.980	0.948	0.805	2.091	2.404	1.156	-1457	962	12.9	6.791
1.0	0.8	0.3	0.0000	0.2742	0.0359	0.0321	5.28	1.950	0.930	0.806	2.107	2.358	1.127	-1456	924	12.8	6.563
1.0	0.9	0.3	0.0000	0.3127	0.0374	0.0360	5.31	1.924	0.915	0.814	2.123	2.310	1.100	-1456	887	12.8	6.335
1.0	1.0	0.3	0.0000	0.3559	0.0388	0.0394	5.33	1.901	0.900	0.824	2.140	2.264	1.074	-1456	851	12.8	6.107
1.0	0.1	0.4	0.8933	0.0968	0.0099	0.0037	4.12	2.655	1.313	0.950	2.023	2.770	1.370	-1455	1214	13.4	8.151
1.0	0.2	0.4	0.8227	0.0990	0.0170	0.0077	4.70	2.227	1.107	0.837	2.012	2.681	1.302	-1459	1167	13.3	7.931
1.0	0.3	0.4	0.7157	0.1170	0.0217	0.0117	4.91	2.157	1.064	0.823	2.027	2.620	1.272	-1458	1121	13.2	7.703
1.0	0.4	0.4	0.5722	0.1508	0.0260	0.0160	5.01	2.100	1.028	0.814	2.043	2.560	1.243	-1458	1078	13.1	7.474
1.0	0.5	0.4	0.4159	0.1870	0.0297	0.0202	5.11	2.052	0.997	0.808	2.059	2.501	1.214	-1458	1035	13.0	7.246
1.0	0.6	0.4	0.2603	0.2122	0.0321	0.0241	5.19	2.013	0.970	0.803	2.075	2.450	1.185	-1457	1000	12.9	7.018
1.0	0.7	0.4	0.1186	0.2411	0.0342	0.0281	5.24	1.980	0.948	0.805	2.091	2.404	1.156	-1457	962	12.9	6.791
1.0	0.8	0.4	0.0000	0.2742	0.0359	0.0321	5.28	1.950	0.930	0.806	2.107	2.358	1.127	-1456	924	12.8	6.563
1.0	0.9	0.4	0.0000	0.3127	0.0374	0.0360	5.31	1.924	0.915	0.814	2.123	2.310	1.100	-1456	887	12.8	6.335
1.0	1.0	0.4	0.0000	0.3559	0.0388	0.0394											

T	LIQUID MOLE FRACTION			VAPOR MOLE FRACTION			PRESSURE ATM	EQUIL CONST			RELATIVE VOL			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
	N2	AR/AR-O2	O2	N2	AR	O2		N2	AR	O2	N2/AR	N2/O2	AR/O2	LIQ	VAP	LIQ	VAP
0.	0.	0.	1.000	0.	0.	0.	4.78	2.631	1.353	1.000	1.944	2.631	1.353	-1407.	1239.	13.5	8.297
0.1	0.	0.	0.1979	0.7722	0.	0.	4.97	2.597	1.279	0.969	1.940	2.587	1.320	-1429.	1187.	13.4	8.069
0.2	0.	0.	0.2437	0.7265	0.	0.	5.13	2.406	1.218	0.946	1.975	2.544	1.288	-1452.	1149.	13.2	7.863
0.3	0.	0.	0.2792	0.6799	0.	0.	5.27	2.324	1.167	0.929	1.990	2.502	1.257	-1474.	1097.	13.1	7.671
0.4	0.	0.	0.3050	0.6322	0.	0.	5.40	2.257	1.129	0.917	2.006	2.461	1.227	-1495.	1057.	13.0	7.488
0.5	0.	0.	0.3228	0.5845	0.	0.	5.51	2.204	1.099	0.910	2.022	2.421	1.197	-1514.	1017.	12.9	7.312
0.6	0.	0.	0.3330	0.5368	0.	0.	5.61	2.163	1.081	0.909	2.038	2.381	1.168	-1531.	983.	12.7	7.156
0.7	0.	0.	0.3369	0.4891	0.	0.	5.70	2.133	1.069	0.911	2.054	2.342	1.140	-1547.	947.	12.6	6.993
0.8	0.	0.	0.3340	0.4414	0.	0.	5.77	2.114	1.061	0.918	2.071	2.304	1.113	-1562.	912.	12.5	6.825
0.9	0.	0.	0.3252	0.3937	0.	0.	5.83	2.104	1.058	0.928	2.087	2.266	1.086	-1576.	877.	12.4	6.657
1.0	0.	0.	0.3102	0.3460	0.	0.	5.88	2.104	1.058	0.944	2.104	2.230	1.060	-1589.	841.	12.2	6.490
0.05	0.1	0.	0.027	0.973	0.	0.	5.00	2.509	1.222	0.961	1.937	2.469	1.349	-1389.	1239.	13.4	8.334
0.05	0.2	0.	0.0571	0.9429	0.	0.	5.14	2.400	1.230	0.939	1.980	2.526	1.315	-1410.	1186.	13.3	8.142
0.05	0.3	0.	0.0859	0.9131	0.	0.	5.23	2.310	1.175	0.915	1.980	2.526	1.284	-1431.	1142.	13.3	7.948
0.05	0.4	0.	0.1144	0.8836	0.	0.	5.47	2.236	1.129	0.900	1.982	2.485	1.254	-1452.	1101.	13.2	7.767
0.05	0.5	0.	0.1382	0.8544	0.	0.	5.54	2.176	1.090	0.890	1.997	2.445	1.224	-1473.	1061.	13.1	7.595
0.05	0.6	0.	0.1572	0.8254	0.	0.	5.70	2.129	1.058	0.885	2.012	2.406	1.194	-1495.	1021.	13.0	7.427
0.05	0.7	0.	0.1715	0.7965	0.	0.	5.84	2.091	1.031	0.883	2.028	2.367	1.168	-1517.	982.	12.9	7.262
0.05	0.8	0.	0.1812	0.7676	0.	0.	5.96	2.064	1.010	0.886	2.043	2.327	1.142	-1539.	943.	12.7	7.096
0.05	0.9	0.	0.1869	0.7387	0.	0.	6.07	2.037	0.994	0.893	2.059	2.287	1.113	-1561.	904.	12.6	6.927
0.10	0.1	0.	0.0549	0.9451	0.	0.	6.17	2.036	0.982	0.903	2.075	2.246	1.087	-1583.	865.	12.5	6.752
0.10	0.2	0.	0.1129	0.8871	0.	0.	6.48	1.925	1.192	0.866	1.914	2.246	1.062	-1605.	826.	12.3	6.577
0.10	0.3	0.	0.1608	0.8291	0.	0.	6.80	1.814	1.105	0.849	1.927	2.207	1.031	-1627.	787.	12.1	6.402
0.10	0.4	0.	0.2087	0.7711	0.	0.	7.08	1.703	1.018	0.832	1.940	2.168	1.000	-1649.	748.	11.9	6.227
0.10	0.5	0.	0.2566	0.7131	0.	0.	7.36	1.592	0.931	0.815	1.953	2.129	0.969	-1671.	709.	11.7	6.052
0.10	0.6	0.	0.3045	0.6551	0.	0.	7.64	1.481	0.844	0.798	1.966	2.090	0.938	-1693.	670.	11.5	5.877
0.10	0.7	0.	0.3524	0.5971	0.	0.	7.92	1.370	0.757	0.781	1.979	2.051	0.907	-1715.	631.	11.3	5.702
0.10	0.8	0.	0.4003	0.5391	0.	0.	8.20	1.259	0.666	0.764	1.992	2.012	0.876	-1737.	592.	11.1	5.527
0.10	0.9	0.	0.4482	0.4811	0.	0.	8.48	1.148	0.575	0.747	2.005	1.973	0.845	-1759.	553.	10.9	5.352
0.15	0.1	0.	0.0898	0.9102	0.	0.	6.52	1.899	1.012	0.844	1.884	2.193	1.058	-1532.	899.	12.9	7.163
0.15	0.2	0.	0.1796	0.8204	0.	0.	6.81	1.808	0.921	0.774	1.884	2.163	1.027	-1554.	860.	12.7	6.988
0.15	0.3	0.	0.2694	0.7306	0.	0.	7.10	1.717	0.830	0.704	1.896	2.133	0.996	-1576.	821.	12.5	6.813
0.15	0.4	0.	0.3592	0.6408	0.	0.	7.39	1.626	0.739	0.634	1.908	2.103	0.965	-1598.	782.	12.3	6.638
0.15	0.5	0.	0.4490	0.5510	0.	0.	7.68	1.535	0.648	0.564	1.920	2.073	0.934	-1620.	743.	12.1	6.463
0.15	0.6	0.	0.5388	0.4612	0.	0.	7.97	1.444	0.557	0.494	1.932	2.043	0.903	-1642.	704.	11.9	6.288
0.15	0.7	0.	0.6286	0.3714	0.	0.	8.26	1.353	0.466	0.424	1.944	2.013	0.872	-1664.	665.	11.7	6.113
0.15	0.8	0.	0.7184	0.2816	0.	0.	8.55	1.262	0.375	0.354	1.956	1.983	0.841	-1686.	626.	11.5	5.938
0.15	0.9	0.	0.8082	0.1918	0.	0.	8.84	1.171	0.284	0.284	1.968	1.953	0.810	-1708.	587.	11.3	5.763
0.20	0.1	0.	0.1396	0.8604	0.	0.	7.31	1.684	0.833	0.774	1.884	2.163	1.058	-1532.	899.	12.9	7.163
0.20	0.2	0.	0.2792	0.7806	0.	0.	7.61	1.593	0.742	0.704	1.884	2.133	1.027	-1554.	860.	12.7	6.988
0.20	0.3	0.	0.4188	0.7008	0.	0.	7.90	1.502	0.651	0.634	1.896	2.103	0.996	-1576.	821.	12.5	6.813
0.20	0.4	0.	0.5584	0.6210	0.	0.	8.20	1.411	0.560	0.564	1.908	2.073	0.965	-1598.	782.	12.3	6.638
0.20	0.5	0.	0.6980	0.5412	0.	0.	8.50	1.320	0.469	0.494	1.920	2.043	0.934	-1620.	743.	12.1	6.463
0.20	0.6	0.	0.8376	0.4614	0.	0.	8.80	1.229	0.378	0.424	1.932	2.013	0.903	-1642.	704.	11.9	6.288
0.20	0.7	0.	0.9772	0.3816	0.	0.	9.10	1.138	0.287	0.354	1.944	1.983	0.872	-1664.	665.	11.7	6.113
0.20	0.8	0.	1.1168	0.3018	0.	0.	9.40	1.047	0.196	0.284	1.956	1.953	0.841	-1686.	626.	11.5	5.938
0.20	0.9	0.	1.2564	0.2220	0.	0.	9.70	0.956	0.105	0.214	1.968	1.923	0.810	-1708.	587.	11.3	5.763
0.25	0.1	0.	0.2196	0.7804	0.	0.	7.51	1.684	0.833	0.774	1.884	2.163	1.058	-1532.	899.	12.9	7.163
0.25	0.2	0.	0.4392	0.7006	0.	0.	7.81	1.593	0.742	0.704	1.884	2.133	1.027	-1554.	860.	12.7	6.988
0.25	0.3	0.	0.6588	0.6208	0.	0.	8.10	1.502	0.651	0.634	1.896	2.103	0.996	-1576.	821.	12.5	6.813
0.25	0.4	0.	0.8784	0.5410	0.	0.	8.40	1.411	0.560	0.564	1.908	2.073	0.965	-1598.	782.	12.3	6.638
0.25	0.5	0.	1.0980	0.4612	0.	0.	8.70	1.320	0.469	0.494	1.920	2.043	0.934	-1620.	743.	12.1	6.463
0.25	0.6	0.	1.3176	0.3814	0.	0.	9.00	1.229	0.378	0.424	1.932	2.013	0.903	-1642.	704.	11.9	6.288
0.25	0.7	0.	1.5372	0.3016	0.	0.	9.30	1.138	0.287	0.354	1.944	1.983	0.872	-1664.	665.	11.7	6.113
0.25	0.8	0.	1.7568	0.2218	0.	0.	9.60	1.047	0.196	0.284	1.956	1.953	0.841	-1686.	626.	11.5	5.938
0.25	0.9	0.	1.9764	0.1420	0.	0.	9.90	0.956	0.105	0.214	1.968	1.923	0.810	-1708.	587.	11.3	5.763
0.30	0.1	0.	0.3192	0.6804	0.	0.	7.51	1.684	0.833	0.774	1.884	2.163	1.058	-1532.	899.	12.9	7.163
0.30	0.2	0.	0.6384	0.6006	0.	0.	7.81	1.593	0.742	0.704	1.884	2.133	1.027	-1554.	860.	12.7	6.988
0.30	0.3	0.	0.9576	0.5208	0.	0.	8.10	1.502	0.651	0.634	1.896	2.103	0.996	-1576.	821.	12.5	6.813
0.30	0.4	0.	1.2768	0.4410	0.	0.	8.40	1.411	0.560	0.564	1.908	2.073	0.965	-1598.	782.	12.3	6.638
0.30	0.5	0.	1.5960	0.3612	0.	0.	8.70	1.320	0.469	0.494	1.920	2.043	0.934	-1620.	743.	12.1	6.463
0.30	0.6	0.	1.9152	0.2814	0.	0.	9.00	1.229	0.378	0.424	1.932	2.013	0.903	-1642.	704.	11.9	6.288
0.30	0.7	0.	2.2344	0.2016	0.	0.	9.30	1.138	0.287	0.354	1.944	1.983	0.872	-1664.	665.	11.7	6.113
0.30	0.8	0.	2.5536	0.1218	0.	0.	9.60	1.047	0.196	0.284	1.956	1.953	0.841	-168			



LIQUID MOLE FRACTION		VAPOR MOLE FRACTION		PRESSURE	EQUIL CONST			RELATIVE VOL			ENTHALPY		HEAT CAPACITY	
N2	AR/AR-O2	N2	AR O2		ATM	N2	AR	O2	N2/AR	N2/O2	AR/O2	LTO	VAP	LTO
0.	0.	0.	0.	1.000	2.479	1.330	1.000	1.330	2.479	1.330	-1339.	1294.	13.6	8.524
0.1	0.	0.1261	0.8741	0.998	2.389	1.261	0.971	1.078	2.430	1.299	-1362.	1291.	13.5	8.527
0.2	0.	0.2409	0.7594	0.995	2.278	1.204	0.949	1.091	2.400	1.269	-1385.	1284.	13.4	8.530
0.3	0.	0.3470	0.6533	0.991	2.153	1.157	0.933	1.095	2.361	1.240	-1408.	1279.	13.3	8.532
0.4	0.	0.4460	0.5535	0.986	2.017	1.117	0.922	1.099	2.323	1.211	-1431.	1268.	13.2	8.534
0.5	0.	0.5421	0.4582	0.980	1.874	1.087	0.914	1.093	2.286	1.183	-1454.	1259.	13.1	8.537
0.6	0.	0.6344	0.3650	0.973	1.726	1.065	0.907	1.087	2.250	1.156	-1477.	1251.	13.0	8.540
0.7	0.	0.7231	0.2752	0.965	1.575	1.051	0.902	1.081	2.214	1.129	-1500.	1244.	12.9	8.542
0.8	0.	0.8089	0.1884	0.956	1.423	1.043	0.900	1.075	2.178	1.103	-1523.	1238.	12.8	8.544
0.9	0.	0.8919	0.1085	0.946	1.271	1.040	0.895	1.069	2.143	1.078	-1546.	1233.	12.7	8.546
1.0	1.0	1.0000	0.0000	0.935	1.120	1.040	0.893	1.063	2.108	1.053	-1569.	1229.	12.6	8.548
0.0	0.1	0.0393	0.9607	0.935	2.373	1.278	0.983	1.087	2.450	1.224	-1319.	1295.	13.7	8.588
0.0	0.2	0.0786	0.9214	0.934	2.275	1.210	0.940	1.076	2.420	1.194	-1342.	1293.	13.6	8.590
0.0	0.3	0.1179	0.8821	0.933	2.177	1.142	0.921	1.065	2.390	1.164	-1365.	1291.	13.5	8.592
0.0	0.4	0.1572	0.8428	0.932	2.079	1.074	0.902	1.054	2.360	1.134	-1388.	1289.	13.4	8.594
0.0	0.5	0.1965	0.8035	0.931	1.981	1.006	0.883	1.043	2.330	1.104	-1411.	1287.	13.3	8.596
0.0	0.6	0.2358	0.7642	0.930	1.883	0.938	0.864	1.032	2.300	1.074	-1434.	1285.	13.2	8.598
0.0	0.7	0.2751	0.7249	0.929	1.785	0.870	0.845	1.021	2.270	1.044	-1457.	1283.	13.1	8.600
0.0	0.8	0.3144	0.6856	0.928	1.687	0.802	0.826	1.010	2.240	1.014	-1480.	1281.	13.0	8.602
0.0	0.9	0.3537	0.6463	0.927	1.589	0.734	0.807	1.000	2.210	0.984	-1503.	1279.	12.9	8.604
0.0	1.0	0.3930	0.6070	0.926	1.491	0.666	0.788	0.989	2.180	0.954	-1526.	1277.	12.8	8.606
0.1	0.0	0.2037	0.7963	0.937	2.107	1.147	0.977	1.038	2.421	1.207	-1291.	1296.	14.0	8.791
0.1	0.1	0.1079	0.8921	0.936	2.009	1.079	0.938	1.027	2.391	1.177	-1314.	1294.	13.9	8.793
0.1	0.2	0.1930	0.8070	0.935	1.911	1.011	0.900	1.016	2.361	1.147	-1337.	1292.	13.8	8.795
0.1	0.3	0.2681	0.7319	0.934	1.813	0.943	0.862	1.005	2.331	1.117	-1360.	1290.	13.7	8.797
0.1	0.4	0.3332	0.6568	0.933	1.715	0.875	0.824	0.994	2.301	1.087	-1383.	1288.	13.6	8.799
0.1	0.5	0.3883	0.5817	0.932	1.617	0.807	0.786	0.983	2.271	1.057	-1406.	1286.	13.5	8.801
0.1	0.6	0.4334	0.5066	0.931	1.519	0.739	0.748	0.972	2.241	1.027	-1429.	1284.	13.4	8.803
0.1	0.7	0.4685	0.4315	0.930	1.421	0.671	0.710	0.961	2.211	0.997	-1452.	1282.	13.3	8.805
0.1	0.8	0.4936	0.3564	0.929	1.323	0.603	0.672	0.950	2.181	0.967	-1475.	1280.	13.2	8.807
0.1	0.9	0.5187	0.2813	0.928	1.225	0.535	0.634	0.939	2.151	0.937	-1498.	1278.	13.1	8.809
0.1	1.0	0.5438	0.2062	0.927	1.127	0.467	0.596	0.928	2.121	0.907	-1521.	1276.	13.0	8.811
0.2	0.0	0.3677	0.6323	0.937	2.107	1.147	0.977	1.038	2.421	1.207	-1291.	1296.	14.0	8.791
0.2	0.1	0.2719	0.7281	0.936	2.009	1.079	0.938	1.027	2.391	1.177	-1314.	1294.	13.9	8.793
0.2	0.2	0.1761	0.8239	0.935	1.911	1.011	0.900	1.016	2.361	1.147	-1337.	1292.	13.8	8.795
0.2	0.3	0.0803	0.9197	0.934	1.813	0.943	0.862	1.005	2.331	1.117	-1360.	1290.	13.7	8.797
0.2	0.4	0.0054	1.0155	0.933	1.715	0.875	0.824	0.994	2.301	1.087	-1383.	1288.	13.6	8.799
0.2	0.5	0.0005	1.1113	0.932	1.617	0.807	0.786	0.983	2.271	1.057	-1406.	1286.	13.5	8.801
0.2	0.6	0.0000	1.2071	0.931	1.519	0.739	0.748	0.972	2.241	1.027	-1429.	1284.	13.4	8.803
0.2	0.7	0.0000	1.3029	0.930	1.421	0.671	0.710	0.961	2.211	0.997	-1452.	1282.	13.3	8.805
0.2	0.8	0.0000	1.3987	0.929	1.323	0.603	0.672	0.950	2.181	0.967	-1475.	1280.	13.2	8.807
0.2	0.9	0.0000	1.4945	0.928	1.225	0.535	0.634	0.939	2.151	0.937	-1498.	1278.	13.1	8.809
0.2	1.0	0.0000	1.5903	0.927	1.127	0.467	0.596	0.928	2.121	0.907	-1521.	1276.	13.0	8.811
0.3	0.0	0.4024	0.5976	0.937	2.107	1.147	0.977	1.038	2.421	1.207	-1291.	1296.	14.0	8.791
0.3	0.1	0.3066	0.6934	0.936	2.009	1.079	0.938	1.027	2.391	1.177	-1314.	1294.	13.9	8.793
0.3	0.2	0.2108	0.7892	0.935	1.911	1.011	0.900	1.016	2.361	1.147	-1337.	1292.	13.8	8.795
0.3	0.3	0.1150	0.8850	0.934	1.813	0.943	0.862	1.005	2.331	1.117	-1360.	1290.	13.7	8.797
0.3	0.4	0.0192	0.9808	0.933	1.715	0.875	0.824	0.994	2.301	1.087	-1383.	1288.	13.6	8.799
0.3	0.5	0.0043	1.0766	0.932	1.617	0.807	0.786	0.983	2.271	1.057	-1406.	1286.	13.5	8.801
0.3	0.6	0.0000	1.1724	0.931	1.519	0.739	0.748	0.972	2.241	1.027	-1429.	1284.	13.4	8.803
0.3	0.7	0.0000	1.2682	0.930	1.421	0.671	0.710	0.961	2.211	0.997	-1452.	1282.	13.3	8.805
0.3	0.8	0.0000	1.3640	0.929	1.323	0.603	0.672	0.950	2.181	0.967	-1475.	1280.	13.2	8.807
0.3	0.9	0.0000	1.4598	0.928	1.225	0.535	0.634	0.939	2.151	0.937	-1498.	1278.	13.1	8.809
0.3	1.0	0.0000	1.5556	0.927	1.127	0.467	0.596	0.928	2.121	0.907	-1521.	1276.	13.0	8.811
0.4	0.0	0.5969	0.4031	0.937	2.107	1.147	0.977	1.038	2.421	1.207	-1291.	1296.	14.0	8.791
0.4	0.1	0.4911	0.5089	0.936	2.009	1.079	0.938	1.027	2.391	1.177	-1314.	1294.	13.9	8.793
0.4	0.2	0.3853	0.6147	0.935	1.911	1.011	0.900	1.016	2.361	1.147	-1337.	1292.	13.8	8.795
0.4	0.3	0.2795	0.7205	0.934	1.813	0.943	0.862	1.005	2.331	1.117	-1360.	1290.	13.7	8.797
0.4	0.4	0.1737	0.8263	0.933	1.715	0.875	0.824	0.994	2.301	1.087	-1383.	1288.	13.6	8.799
0.4	0.5	0.0679	0.9321	0.932	1.617	0.807	0.786	0.983	2.271	1.057	-1406.	1286.	13.5	8.801
0.4	0.6	0.0030	1.0379	0.931	1.519	0.739	0.748	0.972	2.241	1.027	-1429.	1284.	13.4	8.803
0.4	0.7	0.0000	1.1437	0.930	1.421	0.671	0.710	0.961	2.211	0.997	-1452.	1282.	13.3	8.805
0.4	0.8	0.0000	1.2495	0.929	1.323	0.603	0.672	0.950	2.181	0.967	-1475.	1280.	13.2	8.807
0.4	0.9	0.0000	1.3553	0.928	1.225	0.535	0.634	0.939	2.151	0.937	-1498.	1278.	13.1	8.809
0.4	1.0	0.0000	1.4611	0.927	1.127	0.467	0.596	0.928	2.121	0.907	-1521.	1276.	13.0	8.811
0.5	0.0	0.7938	0.2062	0.937	2.107	1.147	0.977	1.038	2.421	1.207	-1291.	1296.	14.0	8.791
0.5	0.1	0.6880	0.3120	0.936	2.009	1.079	0.938	1.027	2.391	1.177	-1314.	1294.	13.9	8.793
0.5	0.2	0.5822	0.4178	0.935	1.911	1.011	0.900	1.016	2.361	1.147	-1337.	1292.	13.8	8.795
0.5	0.3	0.4764	0.5236	0.934	1.813	0.943	0.862	1.005	2.331	1.117	-1360.	1290.	13.7	8.797
0.5	0.4	0.3706	0.6294	0.933	1.715	0.875	0.824	0.994	2.301	1.087	-1383.	1288.	13.6	8.799
0.5	0.5	0.2648	0.7352	0.932	1.617	0.807	0.786	0.983	2.271	1.057	-1406.	1286.	13.5	8.801
0.5	0.6	0.1590	0.8410	0.931	1.519	0.739	0.748	0.972	2.241	1.027	-1429.	1284.	13.4	8.803
0.5	0.7	0.05												

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION		PRESSURE ATM	EQUIL CONST			RELATIVE VOL			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
N2	AR/AR-O2	N2	AR		N2	AR	O2	N2/AR	N2/O2	AR/O2	LIG	VAP	LIG	VAP
0.	0.	0.	0.	8.97	2.341	1.274	1.000	1.790	2.340	1.307	-1271.	1267.	13.8	8.787
0.1	0.	0.1244	0.0780	7.21	2.242	1.244	0.973	1.802	2.303	1.278	-1294.	1214.	13.7	7.982
0.2	0.	0.2382	0.1622	5.42	2.160	1.191	0.952	1.814	2.267	1.250	-1317.	1164.	13.6	7.193
0.3	0.	0.3440	0.2565	4.11	2.093	1.147	0.930	1.826	2.232	1.222	-1341.	1119.	13.5	6.433
0.4	0.	0.4437	0.3567	3.19	2.039	1.109	0.920	1.838	2.197	1.194	-1364.	1076.	13.4	5.715
0.5	0.	0.5391	0.4610	2.54	1.995	1.077	0.922	1.849	2.163	1.169	-1387.	1035.	13.4	5.021
0.6	0.	0.6318	0.3683	2.08	1.957	1.053	0.921	1.862	2.130	1.144	-1411.	996.	13.4	4.353
0.7	0.	0.7231	0.2770	1.74	1.927	1.033	0.923	1.875	2.097	1.119	-1434.	958.	13.4	3.703
0.8	0.	0.8141	0.1880	1.48	1.901	1.018	0.926	1.887	2.064	1.094	-1458.	920.	13.2	3.064
0.9	0.	0.9060	0.0941	1.27	1.878	1.007	0.941	1.900	2.032	1.070	-1481.	883.	13.1	2.434
1.0	1.0	1.0000	0.	1.11	1.858	1.000	0.955	1.913	2.002	1.047	-1504.	845.	13.0	1.812
0.05	0.1	0.0562	0.0443	7.24	2.248	1.261	0.968	1.784	2.320	1.282	-1275.	1262.	13.9	8.871
0.05	0.2	0.0540	0.1170	6.22	2.160	1.203	0.949	1.795	2.287	1.274	-1273.	1211.	13.8	8.670
0.05	0.3	0.0509	0.2059	5.23	2.087	1.159	0.927	1.807	2.252	1.246	-1296.	1160.	13.8	8.493
0.05	0.4	0.0494	0.3012	4.28	2.026	1.114	0.914	1.818	2.218	1.220	-1319.	1111.	13.8	8.321
0.05	0.5	0.0484	0.4012	3.38	1.977	1.080	0.905	1.830	2.184	1.193	-1342.	1060.	13.8	8.159
0.05	0.6	0.0477	0.5015	2.52	1.936	1.052	0.901	1.842	2.151	1.168	-1364.	1011.	13.7	7.999
0.05	0.7	0.0471	0.6019	1.70	1.904	1.028	0.900	1.854	2.119	1.143	-1387.	964.	13.7	7.839
0.05	0.8	0.0467	0.7021	0.96	1.880	1.010	0.923	1.866	2.087	1.118	-1410.	917.	13.4	7.679
0.05	0.9	0.0465	0.8020	0.52	1.861	0.995	0.919	1.878	2.056	1.093	-1433.	871.	13.3	7.517
0.05	1.0	0.0465	0.9016	0.28	1.846	0.978	0.933	1.890	2.026	1.070	-1456.	825.	13.3	7.351
0.10	0.1	0.1114	0.0798	6.08	2.114	1.141	0.987	1.753	2.280	1.268	-1278.	1248.	14.2	9.011
0.10	0.2	0.1097	0.1686	5.26	2.030	1.099	0.970	1.775	2.237	1.246	-1273.	1197.	14.2	8.836
0.10	0.3	0.1082	0.2784	4.44	1.957	1.062	0.960	1.786	2.195	1.233	-1273.	1147.	14.1	8.660
0.10	0.4	0.1075	0.3816	3.75	1.892	1.031	0.952	1.798	2.153	1.211	-1293.	1100.	14.1	8.490
0.10	0.5	0.1075	0.4819	3.18	1.835	1.004	0.944	1.807	2.114	1.187	-1314.	1054.	14.0	8.320
0.10	0.6	0.1071	0.5819	2.70	1.785	0.980	0.944	1.818	2.074	1.163	-1335.	1009.	13.9	8.152
0.10	0.7	0.1067	0.6819	2.29	1.743	0.963	0.945	1.828	2.035	1.140	-1356.	964.	13.9	7.989
0.10	0.8	0.1061	0.7819	1.92	1.701	0.945	0.946	1.839	2.000	1.118	-1377.	919.	13.8	7.829
0.10	0.9	0.1054	0.8819	1.59	1.660	0.927	0.947	1.849	1.966	1.096	-1398.	874.	13.7	7.669
0.10	1.0	0.1052	0.9819	1.30	1.620	0.909	0.947	1.861	1.932	1.074	-1419.	829.	13.7	7.505
0.20	0.1	0.2444	0.1645	5.12	1.774	1.095	0.957	1.730	2.230	1.219	-1279.	1229.	13.6	7.666
0.20	0.2	0.2394	0.2792	4.28	1.703	1.059	0.950	1.748	2.172	1.204	-1279.	1179.	13.6	7.491
0.20	0.3	0.2353	0.4044	3.54	1.637	1.028	0.940	1.757	2.145	1.221	-1279.	1130.	13.6	7.317
0.20	0.4	0.2320	0.5296	2.90	1.576	0.993	0.927	1.767	2.119	1.199	-1293.	1081.	13.6	7.143
0.20	0.5	0.2299	0.6548	2.36	1.520	0.962	0.924	1.777	2.092	1.178	-1314.	1034.	13.5	6.969
0.20	0.6	0.2285	0.7800	1.92	1.469	0.937	0.924	1.787	2.066	1.157	-1335.	987.	13.4	6.795
0.20	0.7	0.2277	0.9052	1.57	1.423	0.913	0.925	1.797	2.041	1.137	-1356.	940.	13.4	6.621
0.20	0.8	0.2274	1.0304	1.30	1.381	0.891	0.925	1.807	2.016	1.117	-1377.	893.	13.3	6.447
0.20	0.9	0.2274	1.1556	1.09	1.342	0.873	0.923	1.817	1.991	1.098	-1398.	846.	13.2	6.273
0.20	1.0	0.2274	1.2808	0.92	1.307	0.857	0.923	1.827	1.967	1.079	-1419.	799.	13.2	6.100
0.30	0.1	0.3777	0.2524	4.16	1.592	1.090	0.977	1.697	2.200	1.206	-1280.	1204.	13.4	7.294
0.30	0.2	0.3694	0.3676	3.36	1.520	1.059	0.970	1.720	2.132	1.204	-1279.	1154.	13.4	7.119
0.30	0.3	0.3629	0.4828	2.64	1.451	1.031	0.960	1.730	2.086	1.200	-1279.	1104.	13.4	6.944
0.30	0.4	0.3575	0.5980	2.00	1.387	1.004	0.950	1.737	2.044	1.188	-1293.	1054.	13.4	6.769
0.30	0.5	0.3530	0.7132	1.44	1.336	0.980	0.950	1.749	2.004	1.170	-1314.	1004.	13.4	6.595
0.30	0.6	0.3492	0.8284	0.98	1.290	0.960	0.950	1.759	1.969	1.152	-1335.	954.	13.4	6.421
0.30	0.7	0.3459	0.9436	0.63	1.249	0.943	0.950	1.762	1.937	1.134	-1356.	904.	13.4	6.247
0.30	0.8	0.3431	1.0588	0.37	1.212	0.927	0.950	1.770	1.907	1.117	-1377.	854.	13.3	6.073
0.30	0.9	0.3406	1.1740	0.22	1.179	0.913	0.950	1.778	1.880	1.099	-1398.	804.	13.3	5.900
0.30	1.0	0.3384	1.2892	0.15	1.149	0.900	0.950	1.786	1.854	1.083	-1419.	754.	13.2	5.726
0.40	0.1	0.5199	0.3207	3.18	1.440	1.088	0.971	1.669	2.067	1.224	-1280.	1181.	13.4	7.491
0.40	0.2	0.5094	0.4359	2.38	1.371	1.060	0.960	1.689	2.009	1.208	-1279.	1131.	13.4	7.317
0.40	0.3	0.5000	0.5511	1.68	1.307	1.033	0.949	1.702	1.951	1.192	-1279.	1081.	13.4	7.143
0.40	0.4	0.4916	0.6663	1.04	1.250	1.007	0.940	1.709	1.910	1.176	-1293.	1031.	13.4	6.969
0.40	0.5	0.4841	0.7815	0.58	1.200	0.980	0.940	1.715	1.871	1.161	-1314.	981.	13.4	6.795
0.40	0.6	0.4772	0.8967	0.23	1.157	0.960	0.940	1.722	1.833	1.144	-1335.	931.	13.4	6.621
0.40	0.7	0.4719	1.0119	0.07	1.119	0.943	0.940	1.729	1.804	1.131	-1356.	881.	13.4	6.447
0.40	0.8	0.4671	1.1271	0.04	1.084	0.927	0.940	1.735	1.776	1.114	-1377.	831.	13.3	6.273
0.40	0.9	0.4628	1.2423	0.02	1.052	0.913	0.940	1.742	1.749	1.101	-1398.	781.	13.3	6.100
0.40	1.0	0.4590	1.3575	0.01	1.023	0.900	0.940	1.749	1.723	1.087	-1419.	731.	13.2	5.926
0.50	0.1	0.6872	0.3330	2.24	1.334	1.080	0.976	1.596	1.984	1.273	-1280.	1160.	13.2	7.660
0.50	0.2	0.6759	0.4482	1.44	1.262	1.052	0.966	1.624	1.926	1.264	-1279.	1110.	13.2	7.486
0.50	0.3	0.6659	0.5634	0.80	1.202	1.025	0.955	1.659	1.868	1.260	-1279.	1060.	13.2	7.312
0.50	0.4	0.6568	0.6786	0.26	1.150	1.000	0.945	1.674	1.810	1.246	-1293.	1010.	13.2	7.138
0.50	0.5	0.6485	0.7938	0.09	1.104	0.975	0.945	1.689	1.762	1.231	-1314.	960.	13.2	6.964
0.50	0.6	0.6410	0.9090	0.04	1.064	0.950	0.945	1.699	1.714	1.214	-1335.	910.	13.2	6.790
0.50	0.7	0.6350	1.0242	0.01	1.029	0.925	0.945	1.709	1.666	1.197	-1356.	860.	13.2	6.616
0.50	0.8	0.6301	1.1394	0.00	0.998	0.900	0.945	1.719	1.618	1.181	-1377.	810.	13.1	6.442
0.50	0.9	0.6259	1.2546	0.00	0.971	0.875	0.945	1.729	1.570	1.164	-1398.	760.	13.1	6.268
0.50	1.0	0.6223	1.3698	0.00	0.947	0.850	0.945	1.739	1.522	1.148	-1419.	710.	13.0	6.094
0.60	0.1	0.7448	0.3299	1.28	1.241	1.079	0.979	1.538	1.941	1.285	-1280.	1139.	13.1	7.330
0.60	0.2	0.7301	0.4451	0.48	1.173	1.051	0.969	1.568	1.883	1.270	-1279.	1089.	13.1	7.156
0.60	0.3	0.7160	0.5603	0.04	1.120	1.025	0.959	1.603	1.825	1.254	-1279.	1039.	13.1	6.982
0.60	0.4	0.7023	0.6755	0.01	1.072	1.000	0.949	1.637	1.767	1.240	-1293.	989.	13.1	6.808
0.60	0.5	0.6890	0.7907	0.00	1.029	0.975	0.949	1.669	1.710	1.224	-1314.	939.	13.1	6.634
0.60	0.6	0.6761	0.9059	0.00	0.991	0.950	0.949	1.699	1.662	1.208	-1335.	889.	13.1	6.460
0.60	0.7	0.6637	1.0211	0.00	0.957	0.925	0.949	1.729	1.614	1.192	-1356.	839.	13.1	6.286
0.60	0.8	0.6518	1.1363	0.00	0.927	0.900	0.949	1.759	1.566	1.176	-1377.	789.	13.0	6.112
0.60	0.9	0.6403	1.2515	0.00	0.900	0.875	0.949	1.789	1.518	1.160	-1398.	739.	13.0	5.938
0.60	1.0	0.6292	1.3667	0.00	0.875	0.850	0.949	1.819	1.470	1.144				

LIQUID MOLE FRACTION	VAPOR MOLE FRACTION			PRESSURE	EQUIL CONST			RELATIVE VOL			ENTHALPY		HEAT CAPACITY	
	N2	AR/AR+O2	O2		N2	AR	O2	N2/AR	N2/O2	AR/O2	LIG	VAP	LIG	VAP
0.0	0.0	0.0	1.0001	8.70	2.215	1.289	1.000	1.793	2.214	1.289	-1201.	1277.	14.0	9.480
0.1	0.0	0.1227	0.8774	8.97	2.093	1.227	0.979	1.733	2.181	1.258	-1225.	1222.	14.0	8.898
0.2	0.0	0.2395	0.7647	9.21	2.023	1.177	0.956	1.744	2.148	1.232	-1248.	1172.	13.9	8.720
0.3	0.0	0.3408	0.6594	9.43	1.992	1.130	0.942	1.794	2.115	1.205	-1272.	1126.	13.9	8.591
0.4	0.0	0.4405	0.5697	9.63	1.943	1.101	0.933	1.765	2.083	1.181	-1298.	1082.	13.8	8.307
0.5	0.0	0.5362	0.4639	9.80	1.894	1.079	0.928	1.778	2.052	1.156	-1326.	1040.	13.8	8.224
0.6	0.0	0.6294	0.3708	9.95	1.874	1.049	0.927	1.767	2.021	1.132	-1343.	999.	13.7	8.099
0.7	0.0	0.7212	0.2793	10.07	1.851	1.020	0.930	1.767	1.991	1.108	-1367.	960.	13.7	7.890
0.8	0.0	0.8129	0.1873	10.18	1.833	1.018	0.937	1.806	1.961	1.082	-1391.	921.	13.6	7.714
0.9	0.0	0.9055	0.0947	10.28	1.830	1.008	0.947	1.819	1.933	1.062	-1414.	882.	13.6	7.527
1.0	1.0	1.0002	0.0	10.37	1.831	1.002	0.961	1.830	1.904	1.044	-1438.	843.	13.5	7.328
0.0	0.1	0.0333	0.9667	8.86	2.134	1.243	0.971	1.717	2.138	1.261	-1180.	1272.	14.1	9.175
0.0	0.2	0.0676	0.9324	9.06	2.059	1.190	0.949	1.727	2.109	1.234	-1203.	1226.	14.1	8.997
0.0	0.3	0.1019	0.8981	9.26	1.989	1.145	0.932	1.737	2.103	1.220	-1227.	1172.	14.0	8.820
0.0	0.4	0.1422	0.8578	9.46	1.934	1.107	0.920	1.747	2.102	1.203	-1251.	1127.	14.0	8.671
0.0	0.5	0.1885	0.8115	9.66	1.893	1.079	0.912	1.798	2.071	1.178	-1273.	1085.	13.9	8.515
0.0	0.6	0.2408	0.7592	9.86	1.862	1.057	0.904	1.768	2.041	1.154	-1298.	1045.	13.9	8.361
0.0	0.7	0.2991	0.7019	10.04	1.841	1.038	0.904	1.778	2.011	1.131	-1319.	1008.	13.8	8.204
0.0	0.8	0.3634	0.6366	10.21	1.826	1.029	0.911	1.788	1.981	1.108	-1342.	968.	13.8	8.044
0.0	0.9	0.4337	0.5633	10.37	1.820	1.020	0.927	1.800	1.953	1.085	-1365.	931.	13.7	7.876
0.0	1.0	0.5090	0.4910	10.52	1.820	1.010	0.944	1.811	1.925	1.063	-1388.	893.	13.7	7.699
0.1	0.0	0.1333	0.8667	9.90	1.928	1.143	0.987	1.688	2.131	1.255	-1118.	1285.	14.0	9.447
0.1	0.1	0.1822	0.8178	9.94	1.871	1.099	0.982	1.709	2.120	1.241	-1139.	1241.	14.0	9.303
0.1	0.2	0.2374	0.7626	10.00	1.822	1.058	0.971	1.718	2.091	1.217	-1161.	1197.	14.0	9.164
0.1	0.3	0.2981	0.7019	10.07	1.781	1.021	0.963	1.727	2.063	1.194	-1182.	1153.	14.0	9.034
0.1	0.4	0.3644	0.6356	10.14	1.747	0.988	0.956	1.736	2.035	1.172	-1203.	1093.	14.0	8.913
0.1	0.5	0.4363	0.5637	10.21	1.724	0.960	0.955	1.746	2.007	1.150	-1225.	1037.	14.0	8.792
0.1	0.6	0.5138	0.4862	10.28	1.709	0.937	0.957	1.755	1.980	1.128	-1248.	983.	14.0	8.679
0.1	0.7	0.5969	0.4031	10.35	1.701	0.918	0.964	1.765	1.954	1.107	-1269.	931.	14.0	8.571
0.1	0.8	0.6846	0.3154	10.42	1.698	0.902	0.971	1.774	1.928	1.086	-1289.	881.	14.1	8.468
0.1	0.9	0.7769	0.2231	10.49	1.700	0.887	0.978	1.784	1.902	1.066	-1310.	833.	14.1	8.371
0.1	1.0	0.8738	0.1262	10.56	1.705	0.882	0.986	1.794	1.877	1.046	-1331.	787.	14.1	8.280
0.2	0.0	0.3329	0.6671	10.88	1.713	1.023	0.922	1.676	2.084	1.249	-1054.	1232.	14.0	9.891
0.2	0.1	0.3286	0.6714	10.88	1.676	0.989	0.913	1.684	2.061	1.224	-1074.	1186.	14.0	9.745
0.2	0.2	0.3229	0.6771	10.88	1.643	0.971	0.907	1.692	2.036	1.203	-1093.	1141.	14.0	9.602
0.2	0.3	0.3162	0.6838	10.88	1.615	0.956	0.903	1.700	2.012	1.183	-1112.	1097.	14.0	9.464
0.2	0.4	0.3086	0.6905	10.88	1.591	0.941	0.900	1.708	1.987	1.163	-1131.	1057.	14.0	9.333
0.2	0.5	0.3010	0.6972	10.88	1.569	0.929	0.900	1.716	1.963	1.144	-1149.	1017.	14.0	9.205
0.2	0.6	0.2934	0.7039	10.88	1.551	0.918	0.900	1.725	1.940	1.125	-1168.	980.	14.0	9.080
0.2	0.7	0.2858	0.7106	10.88	1.536	0.908	0.900	1.733	1.917	1.106	-1187.	941.	14.0	8.960
0.2	0.8	0.2782	0.7173	10.88	1.524	0.899	0.900	1.741	1.894	1.088	-1206.	903.	14.0	8.845
0.2	0.9	0.2706	0.7240	10.88	1.514	0.891	0.900	1.749	1.871	1.070	-1225.	865.	14.0	8.737
0.2	1.0	0.2630	0.7307	10.88	1.506	0.883	0.900	1.757	1.848	1.052	-1244.	827.	14.0	8.634
0.3	0.0	0.4648	0.5352	11.88	1.549	0.938	0.888	1.683	2.085	1.228	-992.	1208.	14.0	11.316
0.3	0.1	0.4572	0.5428	11.88	1.524	0.918	0.888	1.690	2.063	1.203	-1011.	1164.	14.0	11.174
0.3	0.2	0.4496	0.5504	11.88	1.501	0.900	0.888	1.696	2.041	1.180	-1029.	1121.	14.0	11.034
0.3	0.3	0.4420	0.5580	11.88	1.479	0.883	0.888	1.702	2.019	1.158	-1047.	1078.	14.0	10.894
0.3	0.4	0.4344	0.5656	11.88	1.458	0.867	0.888	1.708	1.997	1.136	-1065.	1035.	14.0	10.754
0.3	0.5	0.4268	0.5732	11.88	1.438	0.851	0.888	1.714	1.975	1.114	-1083.	992.	14.0	10.614
0.3	0.6	0.4192	0.5808	11.88	1.419	0.836	0.888	1.720	1.953	1.092	-1101.	950.	14.0	10.474
0.3	0.7	0.4116	0.5884	11.88	1.401	0.821	0.888	1.726	1.931	1.070	-1119.	907.	14.0	10.334
0.3	0.8	0.4040	0.5960	11.88	1.384	0.806	0.888	1.732	1.909	1.048	-1137.	865.	14.0	10.194
0.3	0.9	0.3964	0.6036	11.88	1.368	0.791	0.888	1.738	1.887	1.026	-1155.	823.	14.0	10.054
0.3	1.0	0.3888	0.6112	11.88	1.353	0.776	0.888	1.744	1.865	1.004	-1173.	781.	14.0	9.914
0.4	0.0	0.5672	0.4328	13.02	1.418	0.974	0.772	1.629	1.985	1.206	-989.	1182.	14.0	13.002
0.4	0.1	0.5630	0.4382	13.02	1.401	0.957	0.772	1.635	1.963	1.181	-1007.	1138.	14.0	12.862
0.4	0.2	0.5588	0.4436	13.02	1.385	0.941	0.772	1.641	1.941	1.156	-1025.	1094.	14.0	12.722
0.4	0.3	0.5546	0.4490	13.02	1.370	0.925	0.772	1.647	1.919	1.131	-1043.	1050.	14.0	12.582
0.4	0.4	0.5504	0.4544	13.02	1.356	0.909	0.772	1.653	1.897	1.106	-1061.	1006.	14.0	12.442
0.4	0.5	0.5462	0.4598	13.02	1.343	0.893	0.772	1.659	1.875	1.081	-1079.	962.	14.0	12.302
0.4	0.6	0.5420	0.4652	13.02	1.331	0.877	0.772	1.665	1.853	1.056	-1097.	918.	14.0	12.162
0.4	0.7	0.5378	0.4706	13.02	1.320	0.861	0.772	1.671	1.831	1.031	-1115.	874.	14.0	12.022
0.4	0.8	0.5336	0.4760	13.02	1.310	0.845	0.772	1.677	1.809	1.006	-1133.	830.	14.0	11.882
0.4	0.9	0.5294	0.4814	13.02	1.301	0.829	0.772	1.683	1.787	0.981	-1151.	786.	14.0	11.742
0.4	1.0	0.5252	0.4868	13.02	1.293	0.813	0.772	1.689	1.765	0.956	-1169.	742.	14.0	11.602
0.5	0.0	0.6560	0.3440	14.70	1.312	0.917	0.687	1.608	1.966	1.187	-786.	1155.	14.0	11.499
0.5	0.1	0.6518	0.3494	14.70	1.301	0.900	0.687	1.615	1.944	1.164	-804.	1111.	14.0	11.359
0.5	0.2	0.6476	0.3548	14.70	1.291	0.883	0.687	1.621	1.922	1.141	-822.	1067.	14.0	11.219
0.5	0.3	0.6434	0.3602	14.70	1.282	0.867	0.687	1.627	1.900	1.118	-840.	1023.	14.0	11.079
0.5	0.4	0.6392	0.3656	14.70	1.274	0.851	0.687	1.633	1.878	1.095	-858.	979.	14.0	10.939
0.5	0.5	0.6350	0.3710	14.70	1.267	0.835	0.687	1.639	1.856	1.072	-876.	935.	14.0	10.799
0.5	0.6	0.6308	0.3764	14.70	1.261	0.819	0.687	1.645	1.834	1.049	-894.	891.	14.0	10.659
0.5	0.7	0.6266	0.3818	14.70	1.256	0.803	0.687	1.651	1.812	1.026	-912.	847.	14.0	10.519
0.5	0.8	0.6224	0.3872	14.70	1.251	0.787	0.687	1.657	1.790	1.003	-930.	803.	14.0	10.379
0.5	0.9	0.6182	0.3926	14.70	1.247	0.771	0.687	1.663	1.768	0.980	-948.	759.	14.0	10.239
0.5	1.0	0.6140	0.3980	14.70	1.243	0.755	0.687	1.669	1.746	0.957	-966.	715.	14.0	10.099
0.6	0.0	0.7336	0.2664	15.48	1.225	0.984	0.603	1.582	1.848	1.188	-713.	1125.	14.0	12.291
0.6	0.1	0.7307	0.2718	15.48	1.216	0.967	0.603	1.588	1.826	1.164	-731.	1081.	14.0	12.151
0.6	0.2	0.7278	0.2772	15.48	1.208	0.950	0.603	1.594	1.804	1.141	-749.	1037.	14.0	12.011
0.6	0.3	0.7249	0.2826	15.48	1.201	0.933	0.603	1.600	1.782	1.118	-767.	993.	14.0	11.871
0.6	0.4	0.7220	0.2880	15.48	1.194	0.916	0.603							

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION			PRESSURE ATM	EQUIL CONST			RELATIVE VOL			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE <sup>-1</sup>	
N2	AR/AR+O2	N2	AR	O2		N2	AR	O2	N2/AR	N2/O2	AR/O2	LIQ	VAP	LIQ	VAP
0.0	0.0	0.0	0.0	1.0000	9.80	2.103	1.265	1.000	1.663	2.103	1.264	-1130.	1285.	14.3	0.450
0.1	0.0	0.1210	0.8700	0.1210	10.10	2.024	1.210	0.977	1.672	2.072	1.239	-1154.	1229.	14.3	0.274
0.2	0.0	0.2329	0.7673	0.2329	10.38	1.948	1.162	0.959	1.681	2.041	1.214	-1178.	1178.	14.2	0.120
0.3	0.0	0.3378	0.6624	0.3378	10.62	1.882	1.116	0.946	1.690	2.011	1.190	-1202.	1130.	14.2	0.051
0.4	0.0	0.4378	0.5622	0.4378	10.84	1.820	1.074	0.938	1.700	1.982	1.166	-1226.	1084.	14.2	0.000
0.5	0.0	0.5338	0.4662	0.5338	11.03	1.763	1.037	0.934	1.710	1.955	1.141	-1250.	1041.	14.1	0.040
0.6	0.0	0.6270	0.3730	0.6270	11.20	1.710	1.005	0.933	1.721	1.929	1.115	-1274.	999.	14.1	0.480
0.7	0.0	0.7194	0.2809	0.7194	11.34	1.770	0.978	0.936	1.730	1.907	1.100	-1298.	958.	14.1	0.314
0.8	0.0	0.8117	0.1886	0.8117	11.45	1.763	0.955	0.943	1.737	1.876	1.076	-1321.	919.	14.0	0.139
0.9	0.0	0.9050	0.0953	0.9050	11.54	1.787	0.936	0.953	1.747	1.843	1.055	-1345.	879.	14.0	0.000
1.0	0.0	1.0000	0.0000	1.0000	11.60	1.787	0.920	0.967	1.757	1.817	1.034	-1369.	838.	14.0	0.000
0.0	0.1	0.0588	0.9412	0.0588	10.13	2.033	1.226	0.974	1.688	2.088	1.289	-1109.	1279.	14.4	0.592
0.0	0.2	0.1475	0.8525	0.1475	10.40	1.961	1.177	0.953	1.696	2.058	1.255	-1132.	1226.	14.4	0.388
0.0	0.3	0.2463	0.7537	0.2463	10.63	1.892	1.133	0.938	1.679	2.028	1.211	-1156.	1177.	14.4	0.232
0.0	0.4	0.3453	0.6547	0.3453	10.84	1.821	1.100	0.926	1.684	1.999	1.187	-1179.	1131.	14.3	0.084
0.0	0.5	0.4443	0.5557	0.4443	11.02	1.759	1.065	0.916	1.693	1.971	1.164	-1202.	1087.	14.3	0.037
0.0	0.6	0.5433	0.4567	0.5433	11.18	1.703	1.035	0.910	1.711	1.945	1.141	-1225.	1046.	14.3	0.000
0.0	0.7	0.6423	0.3577	0.6423	11.32	1.753	1.008	0.919	1.721	1.918	1.119	-1249.	1004.	14.2	0.638
0.0	0.8	0.7413	0.2587	0.7413	11.45	1.723	0.986	0.925	1.730	1.892	1.097	-1272.	966.	14.2	0.481
0.0	0.9	0.8403	0.1597	0.8403	11.52	1.717	0.967	0.935	1.739	1.866	1.076	-1295.	928.	14.2	0.314
0.0	1.0	0.9393	0.0607	0.9393	11.59	1.717	0.952	0.949	1.749	1.839	1.058	-1319.	889.	14.1	0.136
0.1	0.0	0.1881	0.8119	0.1881	11.13	1.891	1.127	0.936	1.642	2.043	1.248	-1049.	1260.	14.6	0.860
0.1	0.1	0.1798	0.8202	0.1798	11.39	1.798	1.090	0.922	1.650	2.016	1.222	-1066.	1215.	14.6	0.730
0.1	0.2	0.1753	0.8247	0.1753	11.62	1.713	1.058	0.901	1.668	1.990	1.200	-1088.	1172.	14.7	0.615
0.1	0.3	0.1716	0.8284	0.1716	11.83	1.704	1.030	0.874	1.686	1.963	1.179	-1109.	1132.	14.7	0.493
0.1	0.4	0.1685	0.8315	0.1685	12.02	1.685	1.007	0.876	1.699	1.937	1.158	-1131.	1093.	14.7	0.372
0.1	0.5	0.1659	0.8341	0.1659	12.19	1.659	0.987	0.876	1.710	1.912	1.137	-1152.	1056.	14.7	0.248
0.1	0.6	0.1639	0.8361	0.1639	12.34	1.639	0.970	0.869	1.699	1.887	1.116	-1174.	1020.	14.6	0.170
0.1	0.7	0.1625	0.8375	0.1625	12.47	1.625	0.959	0.872	1.699	1.863	1.097	-1195.	985.	14.6	0.076
0.1	0.8	0.1615	0.8385	0.1615	12.58	1.615	0.946	0.878	1.707	1.838	1.077	-1217.	951.	14.6	0.043
0.1	0.9	0.1610	0.8390	0.1610	12.67	1.609	0.938	0.887	1.716	1.815	1.058	-1238.	917.	14.6	0.040
0.1	1.0	0.1610	0.8390	0.1610	12.74	1.609	0.933	0.898	1.724	1.792	1.039	-1259.	883.	14.5	0.000
0.2	0.0	0.3240	0.6760	0.3240	12.44	1.659	1.024	0.836	1.620	1.985	1.229	-959.	1235.	15.3	10.393
0.2	0.1	0.3185	0.6815	0.3185	12.66	1.583	0.978	0.827	1.627	1.962	1.206	-978.	1197.	15.3	10.287
0.2	0.2	0.3133	0.6867	0.3133	12.84	1.508	0.935	0.821	1.634	1.939	1.187	-998.	1161.	15.3	10.186
0.2	0.3	0.3084	0.6916	0.3084	13.00	1.434	0.895	0.817	1.641	1.916	1.168	-1017.	1127.	15.2	10.075
0.2	0.4	0.3038	0.6962	0.3038	13.15	1.360	0.857	0.813	1.648	1.894	1.149	-1036.	1093.	15.2	9.963
0.2	0.5	0.3000	0.7000	0.3000	13.29	1.311	0.826	0.817	1.655	1.872	1.131	-1055.	1063.	15.2	9.867
0.2	0.6	0.2971	0.7029	0.2971	13.42	1.263	0.799	0.820	1.662	1.850	1.113	-1074.	1033.	15.2	9.780
0.2	0.7	0.2949	0.7051	0.2949	13.54	1.226	0.778	0.826	1.670	1.829	1.095	-1093.	1003.	15.1	9.692
0.2	0.8	0.2934	0.7066	0.2934	13.65	1.192	0.760	0.826	1.677	1.808	1.078	-1112.	973.	15.1	9.570
0.2	0.9	0.2924	0.7076	0.2924	13.76	1.160	0.745	0.833	1.684	1.787	1.064	-1131.	944.	15.1	9.449
0.2	1.0	0.2921	0.7079	0.2921	13.86	1.130	0.731	0.841	1.692	1.767	1.054	-1150.	915.	15.1	9.319
0.3	0.0	0.4826	0.5174	0.4826	13.75	1.309	0.944	0.782	1.598	1.928	1.207	-874.	1207.	15.8	10.015
0.3	0.1	0.4854	0.5146	0.4854	13.93	1.265	0.928	0.778	1.604	1.909	1.190	-891.	1176.	15.8	10.094
0.3	0.2	0.4891	0.5109	0.4891	14.10	1.224	0.913	0.775	1.610	1.890	1.173	-907.	1147.	15.8	10.192
0.3	0.3	0.4936	0.5064	0.4936	14.26	1.185	0.898	0.773	1.616	1.870	1.157	-924.	1119.	15.8	10.292
0.3	0.4	0.4989	0.5011	0.4989	14.42	1.147	0.884	0.773	1.622	1.851	1.141	-941.	1091.	15.7	10.404
0.3	0.5	0.5050	0.4950	0.5050	14.57	1.112	0.870	0.773	1.628	1.832	1.125	-957.	1065.	15.7	10.505
0.3	0.6	0.5118	0.4882	0.5118	14.72	1.079	0.856	0.776	1.635	1.813	1.109	-974.	1039.	15.7	10.592
0.3	0.7	0.5193	0.4807	0.5193	14.85	1.048	0.843	0.783	1.641	1.795	1.094	-991.	1013.	15.7	10.643
0.3	0.8	0.5275	0.4725	0.5275	14.97	1.019	0.830	0.789	1.647	1.777	1.079	-1008.	988.	15.6	10.699
0.3	0.9	0.5363	0.4637	0.5363	15.08	0.992	0.818	0.796	1.653	1.759	1.064	-1024.	964.	15.6	10.767
0.3	1.0	0.5456	0.4544	0.5456	15.18	0.967	0.807	0.796	1.660	1.741	1.049	-1041.	939.	15.6	10.868
0.4	0.0	0.6555	0.3445	0.6555	15.21	1.173	0.868	0.739	1.582	1.896	1.174	-808.	1179.	16.3	11.598
0.4	0.1	0.6592	0.3408	0.6592	15.39	1.135	0.856	0.738	1.589	1.881	1.160	-827.	1150.	16.3	11.562
0.4	0.2	0.6633	0.3377	0.6633	15.56	1.100	0.844	0.738	1.596	1.864	1.146	-847.	1121.	16.3	11.526
0.4	0.3	0.6678	0.3352	0.6678	15.71	1.067	0.833	0.738	1.602	1.848	1.132	-867.	1093.	16.3	11.487
0.4	0.4	0.6727	0.3333	0.6727	15.85	1.036	0.822	0.740	1.608	1.832	1.119	-886.	1065.	16.2	11.447
0.4	0.5	0.6779	0.3319	0.6779	15.98	1.007	0.811	0.742	1.614	1.817	1.106	-904.	1039.	16.2	11.395
0.4	0.6	0.6834	0.3309	0.6834	16.11	0.979	0.801	0.745	1.621	1.801	1.093	-922.	1013.	16.2	11.342
0.4	0.7	0.6891	0.3300	0.6891	16.23	0.953	0.791	0.749	1.627	1.786	1.080	-940.	987.	16.2	11.284
0.4	0.8	0.6950	0.3293	0.6950	16.35	0.928	0.781	0.758	1.634	1.771	1.067	-957.	964.	16.2	11.211
0.4	0.9	0.7011	0.2989	0.7011	16.46	0.904	0.771	0.768	1.640	1.756	1.054	-974.	939.	16.2	11.128
0.4	1.0	0.7074	0.2986	0.7074	16.57	0.881	0.761	0.778	1.646	1.741	1.041	-992.	915.	16.2	11.040
0.5	0.0	0.7998	0.2002	0.7998	16.46	1.291	0.930	0.710	1.594	1.873	1.138	-703.	1147.	16.8	12.434
0.5	0.1	0.8052	0.1948	0.8052	16.62	1.254	0.913	0.709	1.600	1.855	1.126	-721.	1127.	16.8	12.424
0.5	0.2	0.8109	0.1891	0.8109	16.77	1.219	0.897	0.709	1.606	1.837	1.114	-739.	1107.	16.8	12.411
0.5	0.3	0.8169	0.1832	0.8169	16.91	1.185	0.881	0.710	1.612	1.820	1.102	-757.	1089.	16.8	12.397
0.5	0.4	0.8231	0.1771	0.8231	17.04	1.153	0.865	0.713	1.617	1.803	1.090	-775.	1071.	16.8	12.380
0.5	0.5	0.8295	0.1709	0.8295	17.17	1.122	0.849	0.717	1.622	1.786	1.078	-792.	1052.	16.8	12.360
0.5	0.6	0.8361	0.1646	0.8361	17.29	1.092	0.834	0.720	1.627	1.769	1.066	-809.	1033.	16.8	12.336
0.5	0.7	0.8429	0.1583	0.8429	17.40	1.063	0.819	0.723	1.632	1.752	1.054	-826.	1013.	16.7	12.309
0.5	0.8	0.8499	0.1519	0.8499	17.51	1.035	0.804	0.726	1.637	1.735	1.042	-843.	994.	16.7	12.276
0.5	0.9	0.8570	0.1455	0.8570	17.62	1.008	0.789	0.729	1.642	1.718	1.030				

Table 26. (cont.)

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION			PRESSURE ATM	EQUIL CONST			RELATIVE VOL			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
N <sub>1</sub>	AR/AR+O <sub>2</sub>	N <sub>2</sub>	AR	O <sub>2</sub>		N <sub>2</sub>	AR	O <sub>2</sub>	N <sub>2</sub> /AR	N <sub>2</sub> /O <sub>2</sub>	AR/O <sub>2</sub>	LIO	VAP	LIO	VAP
0.0	0.0	0.0	0.0	1.0000	11.48	2.005	1.245	1.000	1.011	2.005	1.244	1098.	1289.	14.6	9.670
0.1	0.0	0.1194	0.8806	11.82	1.934	1.194	0.979	1.019	1.976	1.229	1.076	1087.	1233.	14.6	9.720
0.2	0.0	0.2384	0.7616	12.13	1.875	1.152	0.962	1.027	1.948	1.197	1.157	1100.	1180.	14.6	9.572
0.3	0.0	0.3574	0.6426	12.44	1.826	1.110	0.951	1.035	1.920	1.174	1.244	1110.	1131.	14.6	9.427
0.4	0.0	0.4764	0.5236	12.74	1.786	1.068	0.943	1.044	1.893	1.152	1.344	1119.	1084.	14.6	9.284
0.5	0.0	0.5954	0.4046	13.04	1.752	1.031	0.939	1.052	1.867	1.130	1.454	1127.	1040.	14.6	9.137
0.6	0.0	0.7144	0.2856	13.34	1.720	1.001	0.939	1.060	1.844	1.109	1.574	1135.	997.	14.6	8.994
0.7	0.0	0.8334	0.1666	13.64	1.689	1.005	0.940	1.068	1.821	1.088	1.694	1142.	955.	14.6	8.852
0.8	0.0	0.9524	0.0476	13.94	1.663	1.005	0.945	1.077	1.799	1.067	1.814	1149.	913.	14.6	8.710
0.9	0.0	1.0714	0.0286	14.24	1.642	1.005	0.950	1.085	1.778	1.047	1.934	1156.	871.	14.6	8.568
1.0	0.0	1.1904	0.0096	14.54	1.625	1.005	0.955	1.093	1.757	1.028	2.054	1163.	829.	14.6	8.426
0.0	0.1	0.4880	0.5120	11.85	1.944	1.210	0.976	1.027	1.991	1.239	1.039	1036.	1263.	14.6	9.695
0.1	0.1	0.4710	0.5290	12.17	1.879	1.164	0.957	1.014	1.963	1.216	1.160	1050.	1220.	14.6	9.601
0.2	0.1	0.4550	0.5450	12.47	1.825	1.122	0.943	1.022	1.936	1.194	1.281	1063.	1178.	14.6	9.513
0.3	0.1	0.4400	0.5600	12.77	1.780	1.082	0.932	1.030	1.909	1.172	1.352	1076.	1136.	14.6	9.427
0.4	0.1	0.4260	0.5740	13.07	1.744	1.045	0.926	1.038	1.883	1.150	1.423	1089.	1094.	14.6	9.344
0.5	0.1	0.4130	0.5870	13.37	1.714	1.014	0.923	1.046	1.857	1.129	1.494	1102.	1052.	14.6	9.265
0.6	0.1	0.4010	0.6000	13.67	1.689	1.002	0.923	1.054	1.832	1.108	1.565	1115.	1010.	14.6	9.190
0.7	0.1	0.3900	0.6130	13.97	1.671	1.007	0.926	1.062	1.807	1.087	1.636	1128.	968.	14.6	9.115
0.8	0.1	0.3800	0.6260	14.27	1.657	1.005	0.930	1.070	1.782	1.066	1.707	1141.	926.	14.6	9.040
0.9	0.1	0.3710	0.6390	14.57	1.646	1.005	0.935	1.078	1.757	1.045	1.778	1154.	884.	14.6	8.965
1.0	0.1	0.3630	0.6520	14.87	1.637	1.005	0.940	1.086	1.732	1.024	1.849	1167.	842.	14.6	8.890
0.0	0.2	0.1782	0.8218	12.95	1.762	1.120	0.914	1.022	1.950	1.229	1.039	973.	1263.	14.6	10.170
0.1	0.2	0.1733	0.8267	13.24	1.733	1.084	0.910	1.030	1.925	1.204	1.160	987.	1221.	14.6	10.076
0.2	0.2	0.1692	0.8317	13.54	1.693	1.054	0.907	1.038	1.901	1.184	1.281	1001.	1179.	14.6	10.000
0.3	0.2	0.1658	0.8366	13.84	1.660	1.028	0.904	1.046	1.876	1.163	1.402	1015.	1137.	14.6	9.924
0.4	0.2	0.1630	0.8414	14.14	1.633	1.006	0.902	1.054	1.851	1.144	1.523	1029.	1095.	14.6	9.848
0.5	0.2	0.1608	0.8462	14.44	1.611	1.007	0.902	1.062	1.826	1.124	1.644	1043.	1053.	14.6	9.772
0.6	0.2	0.1592	0.8510	14.74	1.593	1.005	0.902	1.070	1.801	1.104	1.765	1057.	1011.	14.6	9.696
0.7	0.2	0.1580	0.8558	15.04	1.580	1.005	0.902	1.078	1.776	1.084	1.886	1071.	969.	14.6	9.620
0.8	0.2	0.1572	0.8606	15.34	1.571	1.005	0.902	1.086	1.751	1.064	2.007	1085.	927.	14.6	9.544
0.9	0.2	0.1568	0.8654	15.64	1.565	1.005	0.902	1.094	1.726	1.044	2.128	1099.	885.	14.6	9.468
1.0	0.2	0.1566	0.8702	15.94	1.561	1.005	0.902	1.102	1.701	1.024	2.249	1113.	843.	14.6	9.392
0.0	0.3	0.3218	0.6782	14.42	1.629	1.034	0.888	1.027	1.927	1.267	1.039	987.	1231.	14.6	10.065
0.1	0.3	0.3182	0.6818	14.66	1.576	0.999	0.880	1.036	1.876	1.246	1.160	1001.	1189.	14.6	10.000
0.2	0.3	0.3158	0.6852	14.90	1.548	0.977	0.883	1.044	1.826	1.224	1.281	1015.	1147.	14.6	9.924
0.3	0.3	0.3144	0.6886	15.14	1.524	0.966	0.883	1.052	1.776	1.204	1.402	1029.	1105.	14.6	9.848
0.4	0.3	0.3140	0.6920	15.38	1.504	0.962	0.883	1.060	1.726	1.184	1.523	1043.	1063.	14.6	9.772
0.5	0.3	0.3144	0.6954	15.62	1.488	0.962	0.883	1.068	1.676	1.164	1.644	1057.	1021.	14.6	9.696
0.6	0.3	0.3154	0.6986	15.86	1.476	0.962	0.883	1.076	1.626	1.144	1.765	1071.	979.	14.6	9.620
0.7	0.3	0.3170	0.7018	16.10	1.468	0.962	0.883	1.084	1.576	1.124	1.886	1085.	937.	14.6	9.544
0.8	0.3	0.3190	0.7050	16.34	1.463	0.962	0.883	1.092	1.526	1.104	2.007	1099.	895.	14.6	9.468
0.9	0.3	0.3214	0.7082	16.58	1.461	0.962	0.883	1.100	1.476	1.084	2.128	1113.	853.	14.6	9.392
1.0	0.3	0.3242	0.7118	16.82	1.461	0.962	0.883	1.108	1.426	1.064	2.249	1127.	811.	14.6	9.316
0.0	0.4	0.4442	0.5558	15.06	1.476	0.944	0.798	1.022	1.944	1.189	1.039	987.	1231.	14.6	10.065
0.1	0.4	0.4398	0.5602	15.26	1.445	0.921	0.791	1.030	1.876	1.168	1.160	1001.	1189.	14.6	10.000
0.2	0.4	0.4366	0.5646	15.46	1.418	0.902	0.791	1.038	1.807	1.148	1.281	1015.	1147.	14.6	9.924
0.3	0.4	0.4344	0.5682	15.66	1.395	0.883	0.791	1.046	1.737	1.128	1.402	1029.	1105.	14.6	9.848
0.4	0.4	0.4332	0.5718	15.86	1.376	0.883	0.791	1.054	1.667	1.108	1.523	1043.	1063.	14.6	9.772
0.5	0.4	0.4330	0.5754	16.06	1.361	0.883	0.791	1.062	1.597	1.088	1.644	1057.	1021.	14.6	9.696
0.6	0.4	0.4338	0.5790	16.26	1.350	0.883	0.791	1.070	1.526	1.068	1.765	1071.	979.	14.6	9.620
0.7	0.4	0.4350	0.5826	16.46	1.343	0.883	0.791	1.078	1.456	1.048	1.886	1085.	937.	14.6	9.544
0.8	0.4	0.4364	0.5862	16.66	1.340	0.883	0.791	1.086	1.386	1.028	2.007	1099.	895.	14.6	9.468
0.9	0.4	0.4380	0.5898	16.86	1.339	0.883	0.791	1.094	1.316	1.008	2.128	1113.	853.	14.6	9.392
1.0	0.4	0.4400	0.5940	17.06	1.339	0.883	0.791	1.102	1.246	0.988	2.249	1127.	811.	14.6	9.316
0.0	0.5	0.5338	0.4662	13.77	1.541	0.988	0.798	1.021	1.993	1.171	1.039	987.	1231.	14.6	10.065
0.1	0.5	0.5322	0.4678	13.97	1.516	0.977	0.798	1.030	1.924	1.150	1.160	1001.	1189.	14.6	10.000
0.2	0.5	0.5316	0.4694	14.17	1.494	0.966	0.798	1.038	1.855	1.130	1.281	1015.	1147.	14.6	9.924
0.3	0.5	0.5318	0.4710	14.37	1.476	0.962	0.798	1.046	1.786	1.110	1.402	1029.	1105.	14.6	9.848
0.4	0.5	0.5326	0.4726	14.57	1.461	0.962	0.798	1.054	1.716	1.090	1.523	1043.	1063.	14.6	9.772
0.5	0.5	0.5338	0.4742	14.77	1.450	0.962	0.798	1.062	1.646	1.070	1.644	1057.	1021.	14.6	9.696
0.6	0.5	0.5350	0.4758	14.97	1.443	0.962	0.798	1.070	1.576	1.050	1.765	1071.	979.	14.6	9.620
0.7	0.5	0.5364	0.4774	15.17	1.440	0.962	0.798	1.078	1.506	1.030	1.886	1085.	937.	14.6	9.544
0.8	0.5	0.5380	0.4790	15.37	1.439	0.962	0.798	1.086	1.436	1.010	2.007	1099.	895.	14.6	9.468
0.9	0.5	0.5400	0.4806	15.57	1.439	0.962	0.798	1.094	1.366	0.990	2.128	1113.	853.	14.6	9.392
1.0	0.5	0.5420	0.4822	15.77	1.439	0.962	0.798	1.102	1.296	0.970	2.249	1127.	811.	14.6	9.316
0.0	0.6	0.6338	0.3662	12.97	1.476	0.944	0.708	1.022	1.944	1.189	1.039	987.	1231.	14.6	10.065
0.1	0.6	0.6322	0.3678	13.17	1.445	0.921	0.708	1.030	1.876	1.168	1.160	1001.	1189.	14.6	10.000
0.2	0.6	0.6316	0.3694	13.37	1.418	0.902	0.708	1.038	1.807	1.148	1.281	1015.	1147.	14.6	9.924
0.3	0.6	0.6314	0.3710	13.57	1.395	0.883	0.708	1.046	1.737	1.128	1.402	1029.	1105.	14.6	9.848
0.4	0.6	0.6318	0.3726	13.77	1.376	0.883	0.708	1.054	1.667	1.108	1.523	1043.	1063.	14.6	9.772
0.5	0.6	0.6326	0.3742	13.97	1.361	0.883	0.708	1.062	1.597	1.088	1.644	1057.	1021.	14.6	9.696
0.6	0.6	0.6338	0.3758	14.17	1.350	0.883	0.708	1.070	1.526	1.068	1.765	1071.	979.	14.6	9.620
0.7	0.6	0.6350	0.3774	14.37	1.343	0.883	0.708	1.078	1.456	1.048	1.886	1085.	937.	14.6	9.544
0.8	0.6	0.6364	0.3790	14.57	1.340	0.883	0.708	1.086	1.386	1.028	2.007	1099.	895.	14.6	9.468
0.9	0.6	0.6380	0.380												

TEMPERATURE = 225. R

Table 26. (con)

TEMPERATURE = 225. R	LIQUID MOLE FRACTION		VAPOR MOLE FRACTION			PRESSURE ATM	EQUIL CONST			RELATIVE VOL			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
	N <sub>2</sub>	AR/AR-O <sub>2</sub>	N <sub>2</sub>	AR	O <sub>2</sub>		N <sub>2</sub>	AR	O <sub>2</sub>	N <sub>2</sub> /AR	N <sub>2</sub> /O <sub>2</sub>	AR/O <sub>2</sub>	LIG	VAP	LIG	VAP
.00	0.	0.	0.	1.000	0.	13.35	1.923	1.028	1.000	1.569	1.922	1.225	-984.	1291.	15.1	10.391
.01	0.	0.	0.1179	0.8822	0.	13.74	1.898	1.179	0.982	1.578	1.895	1.203	-984.	1291.	15.1	10.391
.02	0.	0.	0.2280	0.7722	0.	14.08	1.867	1.340	0.968	1.583	1.880	1.181	-984.	1291.	15.1	10.391
.03	0.	0.	0.3320	0.6681	0.	14.38	1.840	1.517	0.954	1.589	1.864	1.160	-984.	1291.	15.1	10.391
.04	0.	0.	0.4316	0.5686	0.	14.65	1.817	1.679	0.948	1.597	1.848	1.139	-984.	1291.	15.1	10.391
.05	0.	0.	0.5280	0.4722	0.	14.88	1.809	1.856	0.944	1.604	1.794	1.118	-984.	1291.	15.1	10.391
.06	0.	0.	0.6223	0.3779	0.	15.08	1.871	2.037	0.945	1.611	1.760	1.098	-984.	1291.	15.1	10.391
.07	0.	0.	0.7159	0.2845	0.	15.25	1.855	2.223	0.948	1.619	1.745	1.078	-984.	1291.	15.1	10.391
.08	0.	0.	0.8037	0.1913	0.	15.39	1.845	2.412	0.955	1.626	1.722	1.059	-984.	1291.	15.1	10.391
.09	0.	0.	0.8852	0.0988	0.	15.49	1.844	2.604	0.965	1.633	1.699	1.040	-984.	1291.	15.1	10.391
.10	0.	0.	0.9602	0.0063	0.	15.55	1.849	2.800	0.979	1.641	1.676	1.022	-984.	1291.	15.1	10.391
.100	0.	0.	0.9999	0.0001	0.	15.57	1.857	3.000	0.992	1.649	1.654	1.005	-984.	1291.	15.1	10.391
.100	0.1	0.	0.0827	0.9173	0.	14.17	1.869	1.194	0.983	1.564	1.909	1.221	-984.	1291.	15.1	10.391
.100	0.2	0.	0.1719	0.8281	0.	14.46	1.780	1.315	0.943	1.578	1.898	1.199	-984.	1291.	15.1	10.391
.100	0.3	0.	0.2473	0.7527	0.	14.75	1.719	1.455	0.938	1.585	1.831	1.178	-984.	1291.	15.1	10.391
.100	0.4	0.	0.3120	0.6880	0.	15.01	1.680	1.609	0.932	1.592	1.809	1.157	-984.	1291.	15.1	10.391
.100	0.5	0.	0.3613	0.6387	0.	15.24	1.659	1.738	0.929	1.599	1.785	1.137	-984.	1291.	15.1	10.391
.100	0.6	0.	0.3987	0.6013	0.	15.43	1.638	1.820	0.920	1.606	1.761	1.117	-984.	1291.	15.1	10.391
.100	0.7	0.	0.4287	0.5713	0.	15.60	1.622	1.900	0.923	1.613	1.738	1.097	-984.	1291.	15.1	10.391
.100	0.8	0.	0.4523	0.5477	0.	15.73	1.613	1.980	0.945	1.620	1.719	1.079	-984.	1291.	15.1	10.391
.100	0.9	0.	0.4702	0.5298	0.	15.83	1.608	2.060	0.955	1.627	1.693	1.061	-984.	1291.	15.1	10.391
.100	1.0	0.	0.4822	0.5178	0.	15.90	1.605	2.140	0.963	1.634	1.671	1.043	-984.	1291.	15.1	10.391
.100	0.1	0.1	0.1678	0.8322	0.	15.31	1.878	1.110	0.920	1.591	1.872	1.217	-984.	1291.	15.1	10.391
.100	0.2	0.	0.1041	0.8959	0.	15.40	1.841	1.078	0.908	1.597	1.849	1.187	-984.	1291.	15.1	10.391
.100	0.3	0.	0.1010	0.2769	0.6224	15.87	1.811	1.024	0.893	1.563	1.826	1.168	-984.	1291.	15.1	10.391
.100	0.4	0.	0.1500	0.3618	0.4801	16.12	1.803	1.005	0.889	1.569	1.803	1.149	-984.	1291.	15.1	10.391
.100	0.5	0.	0.1902	0.4444	0.3907	16.31	1.802	0.988	0.888	1.582	1.780	1.130	-984.	1291.	15.1	10.391
.100	0.6	0.	0.1948	0.5256	0.3202	16.49	1.846	0.973	0.890	1.588	1.738	1.112	-984.	1291.	15.1	10.391
.100	0.7	0.	0.1933	0.6158	0.2412	16.65	1.833	0.962	0.893	1.594	1.717	1.093	-984.	1291.	15.1	10.391
.100	0.8	0.	0.1929	0.6880	0.1619	16.77	1.825	0.953	0.899	1.601	1.696	1.075	-984.	1291.	15.1	10.391
.100	0.9	0.	0.1921	0.7666	0.0817	16.87	1.821	0.946	0.908	1.607	1.675	1.057	-984.	1291.	15.1	10.391
.100	1.0	0.	0.1921	0.8483	0.	16.95	1.821	0.943	0.919	1.614	1.656	1.038	-984.	1291.	15.1	10.391
.200	0.	0.	0.1331	0.	0.8673	16.83	1.966	1.022	0.899	1.933	1.822	1.199	-984.	1291.	15.1	10.391
.200	0.1	0.	0.3071	0.6929	0.0134	16.92	1.939	0.998	0.892	1.938	1.802	1.172	-984.	1291.	15.1	10.391
.200	0.2	0.	0.3019	0.1965	0.5420	17.15	1.910	0.978	0.887	1.943	1.782	1.155	-984.	1291.	15.1	10.391
.200	0.3	0.	0.2975	0.2305	0.4725	17.37	1.910	0.961	0.884	1.948	1.763	1.138	-984.	1291.	15.1	10.391
.200	0.4	0.	0.2930	0.3024	0.4042	17.59	1.946	0.946	0.882	1.954	1.745	1.122	-984.	1291.	15.1	10.391
.200	0.5	0.	0.2915	0.3727	0.3370	17.77	1.953	0.932	0.882	1.958	1.728	1.106	-984.	1291.	15.1	10.391
.200	0.6	0.	0.2881	0.4419	0.2702	17.93	1.940	0.921	0.884	1.965	1.714	1.090	-984.	1291.	15.1	10.391
.200	0.7	0.	0.2862	0.5104	0.2035	18.08	1.931	0.911	0.888	1.970	1.698	1.075	-984.	1291.	15.1	10.391
.200	0.8	0.	0.2850	0.5787	0.1366	18.20	1.925	0.904	0.893	1.974	1.689	1.060	-984.	1291.	15.1	10.391
.200	0.9	0.	0.2842	0.6471	0.0688	18.30	1.921	0.899	0.891	1.978	1.680	1.044	-984.	1291.	15.1	10.391
.200	1.0	0.	0.2841	0.7154	0.	18.38	1.921	0.895	0.892	1.987	1.674	1.028	-984.	1291.	15.1	10.391
.300	0.	0.	0.4319	0.	0.5683	18.29	1.946	0.985	0.812	1.914	1.773	1.171	-984.	1291.	15.1	10.391
.300	0.1	0.	0.4257	0.6094	0.3691	18.92	1.919	0.939	0.808	1.918	1.756	1.157	-984.	1291.	15.1	10.391
.300	0.2	0.	0.4203	0.1288	0.4511	19.73	1.901	0.920	0.808	1.923	1.739	1.142	-984.	1291.	15.1	10.391
.300	0.3	0.	0.4150	0.1905	0.3941	19.92	1.885	0.907	0.804	1.927	1.722	1.126	-984.	1291.	15.1	10.391
.300	0.4	0.	0.4117	0.2506	0.3370	19.10	1.872	0.896	0.804	1.932	1.706	1.114	-984.	1291.	15.1	10.391
.300	0.5	0.	0.4083	0.3101	0.2819	19.28	1.861	0.888	0.808	1.936	1.690	1.100	-984.	1291.	15.1	10.391
.300	0.6	0.	0.4056	0.3685	0.2262	19.41	1.851	0.877	0.808	1.941	1.674	1.086	-984.	1291.	15.1	10.391
.300	0.7	0.	0.4035	0.4244	0.1704	19.54	1.848	0.870	0.811	1.945	1.658	1.072	-984.	1291.	15.1	10.391
.300	0.8	0.	0.4020	0.4841	0.1142	19.66	1.840	0.864	0.814	1.948	1.642	1.058	-984.	1291.	15.1	10.391
.300	0.9	0.	0.4011	0.5417	0.0575	19.75	1.837	0.860	0.822	1.950	1.627	1.044	-984.	1291.	15.1	10.391
.300	1.0	0.	0.4008	0.5996	0.	19.84	1.836	0.857	0.829	1.951	1.612	1.030	-984.	1291.	15.1	10.391
.400	0.	0.	0.3351	0.	0.4654	19.98	1.838	0.856	0.776	1.954	1.725	1.154	-984.	1291.	15.1	10.391
.400	0.1	0.	0.3293	0.6930	0.4180	20.17	1.824	0.844	0.774	1.958	1.710	1.140	-984.	1291.	15.1	10.391
.400	0.2	0.	0.3248	0.1048	0.3711	20.35	1.811	0.833	0.773	1.962	1.696	1.126	-984.	1291.	15.1	10.391
.400	0.3	0.	0.3201	0.1935	0.3247	20.53	1.800	0.824	0.773	1.965	1.682	1.117	-984.	1291.	15.1	10.391
.400	0.4	0.	0.3163	0.2593	0.2786	20.68	1.791	0.816	0.774	1.969	1.668	1.105	-984.	1291.	15.1	10.391
.400	0.5	0.	0.3132	0.2944	0.2326	20.82	1.783	0.808	0.775	1.973	1.654	1.094	-984.	1291.	15.1	10.391
.400	0.6	0.	0.3106	0.3030	0.1867	20.95	1.775	0.802	0.778	1.977	1.641	1.082	-984.	1291.	15.1	10.391
.400	0.7	0.	0.3089	0.3512	0.1406	21.07	1.771	0.800	0.781	1.979	1.628	1.071	-984.	1291.	15.1	10.391
.400	0.8	0.	0.3070	0.3991	0.0942	21.18	1.767	0.801	0.785	1.984	1.615	1.059	-984.	1291.	15.1	10.391
.400	0.9	0.	0.3059	0.4469	0.0474	21.28	1.765	0.804	0.789	1.988	1.602	1.048	-984.	1291.	15.1	10.391
.400	1.0	0.	0.3054	0.4948	0.	21.36	1.764	0.805	0.795	1.992	1.589	1.037	-984.	1291.	15.1	10.391
.500	0.	0.	0.2665	0.	0.3739	21.76	1.783	0.855	0.748	1.974	1.725	1.154	-984.	1291.	15.1	10.391
.500	0.1	0.	0.2619	0.6421	0.3364	21.91	1.764	0.842	0.747	1.977	1.710	1.137	-984.	1291.	15.1	10.391
.500	0.2	0.	0.2578	0.0835	0.2991	22.06	1.756	0.835	0.748	1.980	1.696	1.127	-984.	1291.	15.1	10.391
.500	0.3	0.	0.2541	0.1243	0.2620	22.20	1.749	0.828	0.749	1.983	1.681	1.117	-984.	1291.	15.1	10.391
.500	0.4	0.	0.2511	0.1845	0.2249	22.33	1.742	0.823	0.750	1.986	1.667	1.107	-984.	1291.	15.1	10.391
.500	0.5	0.	0.2484	0.2443	0.1879	22.45	1.736	0.817	0.752	1.989	1.653	1.097	-984.	1291.	15.1	10.391
.500	0.6	0.	0.2460	0.2937	0.1508	22.57	1.731	0.812	0.754	1.991	1.639	1				

TEMPERATURE = 230. R

Table 26. (cont.)

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION			PRESSURE ATM	EQUIL CONST			RELATIVE VOL			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
N <sub>2</sub>	AR/AR+O <sub>2</sub>	N <sub>2</sub>	AR	O <sub>2</sub>		N <sub>2</sub>	AR	O <sub>2</sub>	N <sub>2</sub> /AR	N <sub>2</sub> /O <sub>2</sub>	AR/O <sub>2</sub>	LIQ	VAP	LIQ	VAP
.00	0.	0.	0.	1.0000	15.44	1.055	1.207	1.000	1.936	1.055	1.207	-907.	1200.	19.6	11.012
.00	0.1	0.	0.1145	0.8837	15.86	1.707	1.165	0.982	1.943	1.030	1.186	-931.	1229.	19.6	10.960
.00	0.2	0.	0.2297	0.7745	16.23	1.748	1.129	0.968	1.949	1.006	1.166	-959.	1174.	19.6	10.908
.00	0.3	0.	0.3294	0.6708	16.57	1.708	1.098	0.958	1.955	1.702	1.146	-979.	1122.	19.6	10.796
.00	0.4	0.	0.4290	0.5713	17.12	1.648	1.072	0.952	1.961	1.736	1.126	-1003.	1072.	19.6	10.590
.00	0.5	0.	0.5256	0.4748	17.34	1.627	1.051	0.950	1.967	1.735	1.107	-1027.	1025.	19.6	10.480
.00	0.6	0.	0.6203	0.3808	17.52	1.612	1.034	0.954	1.974	1.712	1.098	-1052.	979.	19.6	10.349
.00	0.7	0.	0.7142	0.2882	17.67	1.603	1.020	0.961	1.980	1.676	1.078	-1076.	939.	19.6	10.200
.00	0.8	0.	0.8082	0.1921	17.77	1.599	1.004	0.971	1.983	1.647	1.052	-1100.	891.	19.6	10.030
.00	0.9	0.	0.9033	0.0971	17.83	1.600	1.000	0.984	1.989	1.626	1.037	-1124.	847.	19.6	9.838
.00	1.0	0.	1.0004	0.	17.89	1.605	1.178	0.980	1.992	1.603	1.023	-1148.	804.	19.6	9.619
.025	0.1	0.	0.1145	0.8837	16.30	1.753	1.130	0.963	1.930	1.019	1.163	-907.	1229.	19.7	11.191
.025	0.2	0.	0.2297	0.7745	16.66	1.708	1.106	0.951	1.944	1.706	1.143	-931.	1170.	19.7	11.101
.025	0.3	0.	0.3294	0.6708	16.98	1.671	1.078	0.943	1.950	1.772	1.143	-959.	1120.	19.7	11.013
.025	0.4	0.	0.4290	0.5713	17.27	1.608	1.054	0.937	1.956	1.736	1.124	-979.	1072.	19.7	10.925
.025	0.5	0.	0.5256	0.4748	17.52	1.605	1.034	0.935	1.962	1.727	1.105	-1003.	1025.	19.7	10.837
.025	0.6	0.	0.6203	0.3808	17.61	1.593	1.018	0.936	1.968	1.705	1.087	-1027.	979.	19.7	10.749
.025	0.7	0.	0.7142	0.2882	17.65	1.594	1.009	0.948	1.975	1.684	1.069	-1052.	939.	19.7	10.658
.025	0.8	0.	0.8082	0.1921	17.68	1.597	1.006	0.960	1.981	1.662	1.052	-1076.	897.	19.7	10.566
.025	0.9	0.	0.9033	0.0971	17.71	1.599	1.004	0.971	1.987	1.641	1.034	-1100.	855.	19.7	10.474
.025	1.0	0.	1.0004	0.	17.74	1.600	1.000	0.984	1.993	1.621	1.017	-1124.	813.	19.7	10.382
.100	0.1	0.	0.1674	0.8330	17.62	1.674	1.101	0.928	1.920	1.088	1.170	-884.	1293.	10.1	11.794
.100	0.2	0.	0.3303	0.6697	17.95	1.600	1.045	0.908	1.931	1.705	1.153	-857.	1197.	10.1	11.644
.100	0.3	0.	0.4940	0.5060	18.25	1.570	1.022	0.900	1.936	1.744	1.135	-831.	1112.	10.1	11.503
.100	0.4	0.	0.6587	0.3423	18.51	1.546	1.003	0.897	1.942	1.723	1.118	-807.	1049.	10.1	11.370
.100	0.5	0.	0.8244	0.1784	18.74	1.527	0.987	0.896	1.947	1.703	1.101	-784.	1000.	10.1	11.245
.100	0.6	0.	0.9911	0.0143	18.94	1.512	0.974	0.898	1.953	1.683	1.084	-762.	966.	10.1	11.128
.100	0.7	0.	1.1588	0.0000	19.11	1.500	0.963	0.902	1.958	1.663	1.068	-741.	940.	10.1	11.019
.100	0.8	0.	1.3275	0.0000	19.24	1.493	0.955	0.908	1.964	1.644	1.051	-721.	921.	10.1	10.916
.100	0.9	0.	1.4962	0.0000	19.35	1.489	0.949	0.917	1.969	1.625	1.036	-702.	907.	10.1	10.819
.100	1.0	0.	1.6649	0.0000	19.42	1.486	0.946	0.927	1.975	1.606	1.020	-684.	897.	10.1	10.727
.200	0.1	0.	0.2303	0.7697	19.13	1.520	1.018	0.888	1.903	1.762	1.172	-741.	1173.	10.5	12.790
.200	0.2	0.	0.4606	0.5394	19.43	1.502	0.996	0.881	1.908	1.743	1.156	-721.	1133.	10.5	12.702
.200	0.3	0.	0.6909	0.3091	19.71	1.478	0.977	0.877	1.912	1.725	1.140	-702.	1093.	10.5	12.614
.200	0.4	0.	0.9212	0.0788	19.97	1.457	0.961	0.874	1.917	1.706	1.125	-684.	1053.	10.5	12.526
.200	0.5	0.	1.1515	0.0000	20.19	1.448	0.947	0.873	1.921	1.688	1.110	-667.	1013.	10.5	12.438
.200	0.6	0.	1.3818	0.0000	20.40	1.426	0.934	0.874	1.926	1.671	1.095	-651.	973.	10.5	12.350
.200	0.7	0.	1.6121	0.0000	20.58	1.415	0.924	0.876	1.931	1.653	1.080	-636.	933.	10.5	12.262
.200	0.8	0.	1.8424	0.0000	20.73	1.406	0.916	0.880	1.936	1.636	1.065	-621.	893.	10.5	12.174
.200	0.9	0.	2.0727	0.0000	20.86	1.401	0.909	0.885	1.940	1.619	1.051	-607.	853.	10.5	12.086
.200	1.0	0.	2.3030	0.0000	20.97	1.397	0.904	0.872	1.945	1.603	1.037	-594.	813.	10.5	11.998
.300	0.1	0.	0.3303	0.6697	21.03	1.413	0.951	0.824	1.485	1.716	1.155	-621.	1173.	17.0	14.138
.300	0.2	0.	0.6606	0.3394	21.30	1.394	0.936	0.820	1.489	1.700	1.141	-607.	1133.	17.0	14.102
.300	0.3	0.	0.9909	0.1191	21.54	1.377	0.922	0.818	1.493	1.684	1.128	-594.	1093.	17.0	14.124
.300	0.4	0.	1.3212	0.0000	21.76	1.363	0.910	0.817	1.497	1.668	1.115	-581.	1053.	17.0	14.207
.300	0.5	0.	1.6515	0.0000	21.96	1.350	0.900	0.817	1.501	1.653	1.101	-567.	1013.	17.0	14.317
.300	0.6	0.	1.9818	0.0000	22.14	1.340	0.891	0.818	1.505	1.638	1.086	-554.	973.	17.0	14.333
.300	0.7	0.	2.3121	0.0000	22.31	1.332	0.883	0.821	1.508	1.623	1.076	-541.	933.	17.0	14.331
.300	0.8	0.	2.6424	0.0000	22.45	1.326	0.876	0.824	1.512	1.608	1.063	-529.	893.	17.0	14.310
.300	0.9	0.	2.9727	0.0000	22.57	1.321	0.871	0.829	1.516	1.593	1.051	-517.	853.	17.0	14.266
.300	1.0	0.	3.3030	0.0000	22.68	1.319	0.867	0.835	1.521	1.579	1.039	-506.	813.	17.0	14.198
.400	0.1	0.	0.4303	0.5697	22.74	1.316	0.864	0.842	1.525	1.565	1.027	-495.	773.	17.0	14.144
.400	0.2	0.	0.8606	0.3394	23.03	1.317	0.860	0.789	1.467	1.669	1.138	-535.	1121.	17.5	16.009
.400	0.3	0.	1.2909	0.1191	23.25	1.304	0.850	0.788	1.470	1.656	1.127	-521.	1082.	17.5	16.031
.400	0.4	0.	1.7212	0.0000	23.45	1.293	0.840	0.787	1.473	1.642	1.119	-508.	1043.	17.5	16.059
.400	0.5	0.	2.1515	0.0000	23.64	1.283	0.830	0.788	1.476	1.629	1.104	-495.	1003.	17.5	16.077
.400	0.6	0.	2.5818	0.0000	23.82	1.274	0.822	0.789	1.479	1.616	1.093	-482.	963.	17.5	16.092
.400	0.7	0.	3.0121	0.0000	23.99	1.267	0.815	0.790	1.482	1.603	1.082	-470.	923.	17.5	16.106
.400	0.8	0.	3.4424	0.0000	24.14	1.261	0.809	0.793	1.485	1.591	1.071	-458.	883.	17.5	16.120
.400	0.9	0.	3.8727	0.0000	24.27	1.256	0.804	0.796	1.488	1.579	1.061	-446.	843.	17.5	16.134
.400	1.0	0.	4.3030	0.0000	24.39	1.253	0.800	0.800	1.491	1.566	1.051	-435.	803.	17.5	16.148
.500	0.1	0.	0.5303	0.4697	24.40	1.250	0.807	0.805	1.495	1.554	1.040	-424.	763.	17.5	16.162
.500	0.2	0.	1.0606	0.2394	24.58	1.235	0.834	0.810	1.498	1.542	1.030	-413.	723.	17.5	16.176
.500	0.3	0.	1.5909	0.1191	24.77	1.227	0.856	0.764	1.446	1.620	1.141	-454.	1034.	18.0	19.349
.500	0.4	0.	2.1212	0.0000	24.95	1.221	0.842	0.764	1.450	1.609	1.132	-442.	994.	18.0	19.421
.500	0.5	0.	2.6515	0.0000	25.09	1.215	0.836	0.765	1.452	1.597	1.093	-431.	954.	18.0	19.493
.500	0.6	0.	3.1818	0.0000	25.24	1.209	0.831	0.767	1.454	1.577	1.084	-420.	914.	18.0	19.565
.500	0.7	0.	3.7121	0.0000	25.38	1.203	0.826	0.768	1.457	1.566	1.075	-410.	874.	18.0	19.637

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION			PRESSURE ATM	EQUIL CONST			RELATIVE VOL			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
N2	AR/AR+O2	N2	AR	O2		N2	AR	O2	N2/AR	N2/O2	AR/O2	LIQ	VAP	LIQ	VAP
0	0	0	0	1.0004	17.73	1.825	1.191	1.000	1.515	1.804	1.191	-827.	1201.	16.2	11.790
0.1	0	0	0.1152	0.8852	18.20	1.782	1.192	0.984	1.521	1.781	1.171	-827.	1221.	16.2	11.729
0.2	0	0	0.2237	0.7767	18.61	1.737	1.119	0.971	1.526	1.756	1.152	-828.	1144.	16.2	11.669
0.3	0	0	0.3271	0.6734	18.98	1.670	1.090	0.962	1.532	1.736	1.133	-828.	1111.	16.2	11.623
0.4	0	0	0.4245	0.5757	19.32	1.639	1.066	0.956	1.537	1.714	1.115	-828.	1079.	16.2	11.582
0.5	0	0	0.5232	0.4770	19.62	1.614	1.046	0.954	1.543	1.692	1.097	-828.	1048.	16.2	11.543
0.6	0	0	0.6183	0.3819	19.88	1.595	1.030	0.955	1.548	1.671	1.079	-828.	1018.	16.2	11.507
0.7	0	0	0.7126	0.2876	20.10	1.582	1.018	0.959	1.554	1.650	1.062	-828.	989.	16.2	11.473
0.8	0	0	0.8071	0.1931	20.29	1.574	1.009	0.965	1.559	1.629	1.045	-828.	962.	16.2	11.441
0.9	0	0	0.9027	0.0979	20.46	1.570	1.003	0.975	1.565	1.609	1.028	-828.	937.	16.2	11.410
1.0	0	0	1.0002	0	20.60	1.570	1.000	0.989	1.570	1.590	1.012	-828.	913.	16.2	11.380
0.05	0.1	0.0440	0	0.9564	18.25	1.769	1.184	0.981	1.511	1.793	1.187	-828.	1272.	16.3	12.326
0.05	0.2	0.0828	0.1100	0.8477	18.70	1.711	1.128	0.964	1.517	1.771	1.168	-827.	1214.	16.3	11.982
0.05	0.3	0.1219	0.2139	0.7444	19.11	1.669	1.077	0.955	1.522	1.749	1.149	-827.	1159.	16.3	11.632
0.05	0.4	0.1609	0.3131	0.6462	19.47	1.635	1.031	0.947	1.527	1.727	1.131	-827.	1107.	16.3	11.287
0.05	0.5	0.2002	0.4089	0.5511	19.78	1.607	1.000	0.942	1.533	1.706	1.113	-827.	1057.	16.3	11.047
0.05	0.6	0.2399	0.5022	0.4584	20.05	1.584	1.000	0.940	1.538	1.685	1.095	-827.	1009.	16.3	11.817
0.05	0.7	0.2809	0.6049	0.3765	20.29	1.567	1.015	0.942	1.543	1.664	1.078	-827.	962.	16.3	11.737
0.05	0.8	0.3239	0.7160	0.2957	20.48	1.554	1.023	0.945	1.549	1.644	1.061	-827.	917.	16.3	11.657
0.05	0.9	0.3680	0.8360	0.2167	20.64	1.544	1.035	0.952	1.554	1.624	1.045	-827.	873.	16.3	11.577
0.05	1.0	0.4130	0.9617	0	20.81	1.543	1.049	0.961	1.559	1.604	1.028	-827.	831.	16.3	11.497
0.10	0	0.1637	0	0.8363	19.82	1.637	1.081	0.930	1.565	1.585	1.013	-827.	791.	16.3	11.417
0.10	0.1	0.1600	0.0997	0.7446	20.22	1.600	1.083	0.919	1.569	1.741	1.174	-827.	1240.	16.3	12.030
0.10	0.2	0.1969	0.1870	0.6564	20.59	1.569	1.038	0.912	1.573	1.721	1.157	-827.	1189.	16.3	11.686
0.10	0.3	0.1942	0.2749	0.5712	20.91	1.542	1.018	0.907	1.574	1.701	1.140	-827.	1140.	16.3	11.340
0.10	0.4	0.1920	0.3692	0.4882	21.20	1.520	1.001	0.904	1.579	1.681	1.123	-827.	1094.	16.3	11.001
0.10	0.5	0.1905	0.4735	0.4066	21.46	1.502	0.986	0.904	1.584	1.662	1.107	-827.	1050.	16.3	11.661
0.10	0.6	0.1898	0.5890	0.3280	21.67	1.488	0.973	0.908	1.589	1.643	1.090	-827.	1007.	16.3	11.780
0.10	0.7	0.1898	0.7161	0.2493	21.86	1.478	0.964	0.909	1.593	1.625	1.073	-827.	966.	16.3	11.900
0.10	0.8	0.1908	0.8585	0.1648	22.01	1.471	0.956	0.916	1.598	1.607	1.056	-827.	926.	16.3	12.020
0.10	0.9	0.2008	0.9936	0	22.12	1.468	0.951	0.924	1.603	1.589	1.039	-827.	888.	16.3	12.140
0.10	1.0	0.2408	0.8536	0	22.18	1.468	0.949	0.934	1.608	1.572	1.023	-827.	848.	16.3	12.260
0.20	0	0.3015	0	0.6985	21.97	1.503	1.012	0.920	1.608	1.572	1.013	-827.	811.	16.3	12.380
0.20	0.1	0.2993	0.0704	0.6255	22.33	1.477	0.982	0.869	1.608	1.717	1.177	-827.	1183.	17.1	14.287
0.20	0.2	0.2909	0.1599	0.5534	22.64	1.455	0.978	0.868	1.608	1.700	1.162	-827.	1149.	17.1	14.378
0.20	0.3	0.2871	0.2503	0.4820	22.93	1.436	0.980	0.862	1.608	1.682	1.147	-827.	1118.	17.1	14.469
0.20	0.4	0.2839	0.3528	0.4135	23.19	1.420	0.966	0.862	1.608	1.664	1.133	-827.	1088.	17.1	14.561
0.20	0.5	0.2813	0.4749	0.3449	23.42	1.407	0.959	0.862	1.604	1.643	1.118	-827.	1059.	17.0	14.652
0.20	0.6	0.2797	0.6144	0.2767	23.62	1.396	0.956	0.865	1.608	1.625	1.103	-827.	1032.	17.0	14.743
0.20	0.7	0.2787	0.7740	0.2089	23.79	1.389	0.950	0.869	1.612	1.609	1.087	-827.	1007.	17.0	14.834
0.20	0.8	0.2781	0.9538	0.1398	23.93	1.383	0.942	0.874	1.616	1.593	1.074	-827.	982.	17.0	14.925
0.20	0.9	0.2781	0.6537	0.0705	24.04	1.381	0.938	0.881	1.621	1.577	1.061	-827.	957.	17.0	15.016
0.20	1.0	0.2781	0.2743	0	24.12	1.382	0.939	0.889	1.625	1.562	1.048	-827.	932.	17.0	15.107
0.30	0	0.4177	0	0.5827	24.18	1.382	0.939	0.889	1.625	1.562	1.048	-827.	932.	17.0	15.107
0.30	0.1	0.4124	0.0694	0.5226	24.59	1.375	0.939	0.832	1.467	1.673	1.140	-827.	1137.	17.0	14.830
0.30	0.2	0.4077	0.1291	0.4634	24.83	1.359	0.928	0.829	1.471	1.657	1.127	-827.	1100.	17.0	14.921
0.30	0.3	0.4037	0.1914	0.4052	25.08	1.346	0.911	0.827	1.477	1.642	1.114	-827.	1064.	17.0	15.012
0.30	0.4	0.4003	0.2525	0.3475	25.31	1.334	0.902	0.827	1.481	1.627	1.102	-827.	1029.	17.0	15.103
0.30	0.5	0.3979	0.3127	0.2901	25.52	1.325	0.893	0.829	1.483	1.613	1.089	-827.	995.	17.0	15.194
0.30	0.6	0.3952	0.3723	0.2326	25.71	1.317	0.886	0.832	1.486	1.604	1.078	-827.	962.	17.0	15.285
0.30	0.7	0.3933	0.4315	0.1754	25.87	1.312	0.881	0.835	1.490	1.590	1.064	-827.	930.	17.0	15.376

TEMPERATURE = 240. R

LIQUID MOLE FRACTION		VAPOR MOLE FRACTION			PRESSURE ATM	EQUIL CONST			RELATIVE VOL			ENTHALPY BTU/LB MOLE		HEAT CAPACITY BTU/LB MOLE-R	
N2	AR/AR+O2	N2	AR	O2		N2	AR	O2	N2/AR	N2/O2	AR/O2	LIQ	VAP	LIQ	VAP
0	0	0	0	1.0002	20.27	1.772	1.176	1.000	1.507	1.772	1.176	-744.	1209.	17.0	12.770
0.1	0	0	0.1146	0.8862	20.78	1.723	1.140	0.985	1.512	1.750	1.158	-740.	1207.	17.0	12.763
0.2	0	0	0.2219	0.7784	21.26	1.682	1.109	0.973	1.517	1.729	1.140	-740.	1149.	16.9	12.785
0.3	0	0	0.3249	0.6784	21.68	1.648	1.083	0.968	1.521	1.708	1.122	-740.	1103.	16.9	12.778
0.4	0	0	0.4244	0.5760	22.03	1.616	1.063	0.965	1.526	1.687	1.105	-740.	1059.	16.9	12.754
0.5	0	0	0.5214	0.4790	22.34	1.596	1.043	0.960	1.531	1.667	1.088	-740.	1017.	16.9	12.730
0.6	0	0	0.6168	0.3836	22.61	1.579	1.028	0.959	1.536	1.646	1.072	-740.	976.	16.9	12.706
0.7	0	0	0.7115	0.2889	22.82	1.566	1.018	0.963	1.541	1.627	1.056	-740.	937.	16.9	12.683
0.8	0	0	0.8065	0.1939	23.00	1.558	1.008	0.970	1.546	1.607	1.040	-740.	899.	16.9	12.660
0.9	0	0	0.9025	0.0978	23.16	1.555	1.003	0.979	1.550	1.588	1.024	-740.	862.	16.9	12.637
1.0	0	0	1.0002	0	23.30	1.556	1.000	0.991	1.555	1.569	1.008	-740.	826.	16.9	12.614
0.05	0.1	0.0432	0	0.9567	20.87	1.729	1.158	0.982	1.503	1.760	1.172	-740.	1290.	17.1	13.111
0.05	0.2	0.0821	0.1089	0.8492	21.27	1.685	1.117	0.968	1.508	1.741	1.154	-744.	1190.	17.1	13.139
0.05	0.3	0.1204	0.2113	0.7467	21.62	1.647	1.089	0.958	1.513	1.720	1.137	-747.	1141.	17.0	13.163
0.05	0.4	0.1587	0.3147	0.6506	21.93	1.615	1.064	0.950	1.518	1.700	1.120	-749.	1093.	17.0	13.177
0.05	0.5	0.1969	0.4186	0.5606	22.20	1.588	1.044	0.946	1.522	1.679	1.103	-749.	1047.	17.0	13.175
0.05	0.6	0.2350	0.5227	0.4769	22.44	1.566	1.023	0.946	1.527	1.659	1.087	-749.	1002.	17.0	13.146
0.05	0.7	0.2729	0.6264	0.3929	22.65	1.549	1.002	0.950	1.532	1.640	1.071	-749.	958.	16.9	13.108
0.05	0.8	0.3106	0.7294	0.3098	22.83	1.536	0.984	0.956	1.536	1.621	1.055	-749.	915.	16.9	13.069
0.05	0.9	0.3482	0.8319	0.2271	23.00	1.529	0.980	0.965	1.541	1.602	1.039	-749.	873.	16.9	13.029
0.05	1.0	0.3858	0.9344	0	23.15	1.526	0.977	0.977	1.546	1.583	1.023	-749.	832.	16.9	12.989
0.10	0	0.1614	0	0.8386	22.75	1.614	1.081	0.932	1.493	1.731	1.170	-749.	1219.	17.3	14.322
0.10	0.1	0.1580	0.0946	0.7473	23.16	1.580	1.055	0.923	1.497	1.712	1.153	-749			



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APPENDIX IV  
 NOMENCLATURE TABLE

$A_i$	=	Area of Chromatograph Peak, Section IV-B
$A_{ij}$	=	Binary interaction coefficient, Section VI-E
Ar	=	Argon
$a_{ij}$	=	Constant in binary interaction coefficient, Section VI-E and Section VIII
$B$	=	Second virial coefficient, Section VI-D and Section VIII-D
$B_{ij}$	=	Mixture second virial coefficient, Section VI-D
$b_{ij}$	=	Constant in binary interaction coefficient, Section VI-E and Section VII
$C$	=	Third virial coefficient, Section VI-D and Section VIII-D
$C_{ijkl}$	=	Mixture third virial coefficient, Section VI-D
$C_p$	=	Heat capacity at constant pressure
$C_s$	=	Heat capacity of saturated fluid
$c$	=	Number of components, Section VI-A
$F$	=	Degrees of freedom of system, Section VI-A
$^{\circ}F$	=	Degrees, Fahrenheit scale
$f_i$	=	Fugacity of component $i$
$f_i^*$	=	Fugacity of pure liquid component at the pressure and temperature of mixing
$G^E$	=	Excess free energy
$G_i$	=	Free energy of component $i$
$H$	=	Enthalpy
$H_{gi}$	=	Enthalpy of the real gas, pure component
$h_{gi}^{\circ}$	=	Enthalpy of the real liquid, pure component

NOMENCLATURE TABLE (continued)

$h_i^*$	=	Ideal gas (zero pressure) enthalpy
$H_{liq.}$	=	Liquid phase enthalpy
$h_m$	=	Heat of mixing
$h_{vap.}$	=	Vapor phase enthalpy
$K$	=	Equilibrium constant, Appendix I-A
$N_2$	=	Nitrogen
$O_2$	=	Oxygen
$P$	=	Number of phases, Section VI-A
$p$	=	Total pressure of the vapor
$p_i^o$	=	Vapor pressure of pure component $i$
$p_m$	=	Pressure of mixing
$q_i$	=	Relative response factor, Section IV-B
$R$	=	Gas constant
$^oR$	=	Degrees, Rankine scale
$S$	=	Van Laar Volume, Section VI-E and Section VII
$T$	=	Temperature, degrees Rankine
$V$	=	Molar volume of vapor, Section VI-D
$V$	=	Liquid volume in cc/gm-mole, Section VI-B
$v_i^o$	=	Molar volume of pure component $i$
$\bar{V}_i$	=	Partial molal volume of component $i$
$x$	=	Temperature $^oR$ divided by 100, Section VI-B
$x_i$	=	Mole fraction of component $i$ in the liquid
$y_i$	=	Mole fraction of component $i$ in the vapor
$Z$	=	Compressibility factor

## NOMENCLATURE TABLE (continued)

- $\alpha$  = Relative volatility, Appendix I, Sections B, C, and D
- $\gamma_i$  = Activity coefficient of component  $i$  in the liquid
- $\gamma_\pi$  = Pressure activity coefficient, Appendix I-E
- $\Delta G$  = Change in free energy
- $\overline{\Delta i}_{mi}$  = Partial molal heat of mixing
- $\Delta i_{vi}^\circ$  = Latent heat
- $\phi_i$  = Fugacity coefficient of component  $i$
- $\phi_i^\circ$  = Fugacity coefficient of pure component  $i$