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COMPUTER PROGRAMS FOR MUTUAL COUPLING IN A FINITE PLANAR RECTAN--ETC(U)
JUL 78 J LUZWICK, R F HARRINGTON N00014-76-C-0225

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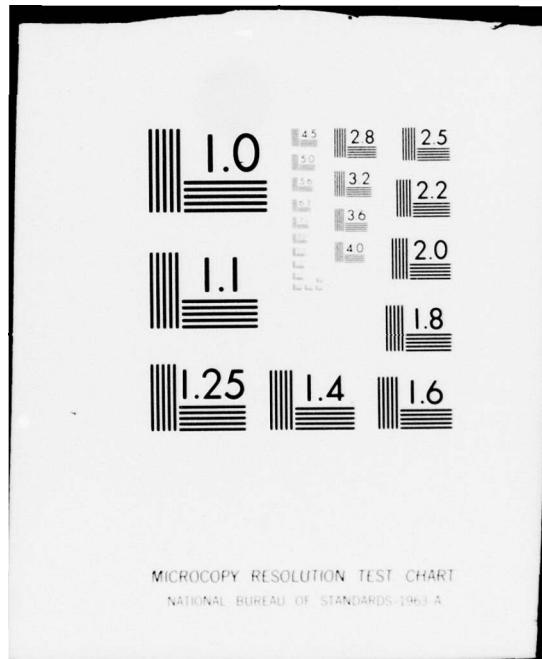
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MICROCOPY RESOLUTION TEST CHART
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) A computer program is given to implement the equations derived in Technical Report TR-78-7, "Mutual Coupling in a Finite Planar Rectangular Waveguide Antenna Array." The aperture dimensions can be less than or equal to the feeding waveguide dimensions. Three specific uniformly spaced array lattices are considered - linear, rectangular, and isosceles triangular. For the linear and rectangular lattice cases, the Toeplitz symmetry property of the admittance matrix is utilized to save storage space and computation time.		

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20. ABSTRACT (cont.)

The program consists of a main program and several subroutines which calculate both the half-space admittance and scattering matrices. The computer program is described and listed, along with sample input-output data.

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I. INTRODUCTION

Computer programs for calculating the half-space admittance and scattering matrices for a finite planar rectangular waveguide antenna array are described and listed in this report. The aperture dimensions can be less than or equal to the feeding waveguide dimensions and the elements are uniformly spaced in each of two directions in either a rectangular or isosceles triangular lattice. The general theory and method of computation are given in the report [1]. Equations drawn from reference [1] are preceded by 1-. For instance, (1-5) denotes equation five of reference [1].

In summary, the procedure is an application of the method of moments to an integral equation formulation of the problem. The unknowns to be determined are the coefficients of the equivalent magnetic currents, which are proportional to the tangential electric field in the aperture regions. A single expansion function is used to approximate the electric field in each aperture.

The computer program subroutine AY which calculates the modal coefficients A_{ik}^{TE} , A_{ik}^{TM} (1-30,31) and the characteristic admittances Y_k^{TE} , Y_k^{TM} (1-34,35) is described and listed in Section II. The subroutine YHSP which calculates elements of the first column of the half-space admittance matrix Y^{hs} (1-12) is described and listed in Section III. The subroutines FCT and FCTA which supply the integrands respectively of the single integrals of (1-68) and the double integrals of (1-59) to the numerical integration subroutines QG8 and QG6A-QG6B for calculation of Y^{hs} are described and listed in Section IV. The subroutine INT which transfers data (limits of integrations and integrand specification) from subroutine YHSP to subroutine QG8 is described and listed in Section V. The subroutines QG6A-QG6B and QG8 which are respectively a six-point double and an eight-point single Gaussian quadrature numerical integration subroutine are described and listed in Section VI. The subroutine CSMTZ which solves equation (1-15) where $[Y^{wg} + Y^{hs}]$ is symmetric Toeplitz (occurs for the uniformly spaced linear array lattice case) is described and listed in Section VII. The subroutines MATMLT, TRMMLT, MULTTR,

MATVCA, and LINSLV which solve equation (1-15) where $[Y^{wg} + Y^{hs}]$ is symmetric block-Toeplitz (occurs for the uniformly spaced rectangular array lattice case) is described and listed in Section VIII. The subroutines LINEQ and DECOMP-SOLVE which are respectively a complex matrix inversion and a Gaussian elimination - LU decomposition complex linear equation solver subroutine are described and listed in Section IX. The subroutine TOPGEN generates a complete matrix (half-space admittance or scattering) given one column is described and listed in Section X. A main program which uses subroutines AY, YHSP, TOPGEN, CSMTZ, DECOMP, SOLVE, and LINSLV to obtain the half-space admittance and scattering matrices is described and listed in Section XI along with sample input-output data.

II. DESCRIPTION OF THE SUBROUTINE AY

The subroutine AY(A,Y) stores the submatrices defined by (1-30) and (1-31) in A and the admittances defined by (1-34) and (1-35) in Y,

A_k^{TE} is stored in $A(k = (m+1)/2 + n/2 * LM)$

Y_k^{TE} is stored in $Y(k = (m+1)/2 + n/2 * LM)$

$m = 1, 3, 5, \dots, LM$

$n = 0, 2, 4, \dots, LN$

A_k^{TM} is stored in $A(k = LM*LN + (m+1)/2 + (n-2)/2 * LM)$

Y_k^{TM} is stored in $Y(k = LM*LN + (m+1)/2 + (n-2)/2 * LM)$

$m = 1, 3, 5, \dots, LM$

$n = 2, 4, 6, \dots, LN$.

Note that only odd m and even n modes are calculated and that the first subscript of A_{ik}^{TE} and A_{ik}^{TM} in (1-30) and (1-31) has been dropped since the same expansion function is used in every waveguide region, $A_{1k} = A_{2k} = \dots = A_{Nk} = A_k$. The variables AL, ALL, BL, BL1, LM, LN, ER, and ETA in the COMMON statement are respectively a/λ , a'/λ , b/λ , b'/λ , LM, LN, ϵ_r , and η where λ is the free space wavelength. Minimum allocations are given by

COMPLEX Y(2 * LM * LN + LM)
 DIMENSION A(2 * LM * LN), F(LM), STE(LN),
 STM(LN).

DO loop 10 stores

$$\frac{b'}{a' \pi \lambda^3} \sqrt{\frac{2\epsilon_n}{aa' bb'}} \cos \frac{n\pi}{2} \frac{\sin \frac{n\pi b'}{2b}}{\frac{n\pi b'}{2b}} \text{ in STE } (\frac{n}{2} + 1)$$

$$\frac{-nb'}{a'b\pi\lambda^3} \sqrt{\frac{2}{aa' bb'}} \cos \frac{n\pi}{2} \frac{\sin \frac{n\pi b'}{2b}}{\frac{n\pi b'}{2b}} \text{ in STM } (\frac{n}{2}) .$$

If $n = 0$, statement 30 calculates STE(1) using $\sin(0)/0 = 1$. DO loop 12 stores

$$\frac{2\lambda^2}{(\frac{m}{2} - \frac{1}{a'^2})} \sin \frac{m\pi}{2} \cos \frac{m\pi a'}{2a} \text{ in } F(\frac{m+1}{2}) .$$

If $|m - a/a'| < \epsilon$ (a small number), statement 13 calculates $F((m+1)/2)$ by replacing $(1/(m^2/a^2 - 1/a'^2)) \cos(m\pi a'/2a)$ by its limit $(-\pi a^2/4)$ as m approaches a/a' . DO loop 20 calculates the coefficients A_k^{TE} , A_k^{TM} , V_k^{TE} , and V_k^{TM} . Statement 31 stores A_k^{TE} in $A(k)$ where

$$A_k^{TE} = A(k) = \frac{m}{\sqrt{(\frac{m}{2a})^2 + (\frac{n}{2b})^2}} \text{ STE}(\frac{n}{2} + 1) F(\frac{m+1}{2})$$

where

$$k = (m+1)/2 + n/2 * LM \quad \left\{ \begin{array}{l} m = 1, 3, 5, \dots, LM \\ n = 0, 2, 4, \dots, LN \end{array} \right.$$

Statement 33 stores A_k^{TM} in $A(k)$ where

$$A_k^{TM} = A(k) = \frac{STE\left(\frac{n}{2}\right) F\left(\frac{m+1}{2}\right)}{\sqrt{\left(\frac{m}{2a}\right)^2 + \left(\frac{n}{2b}\right)^2}}$$

where

$$k = LM * LN + (m+1)/2 + (n-2)/2 * LM \quad \begin{cases} m = 1, 3, 5, \dots, LM \\ n = 2, 4, 6, \dots, LN \end{cases}$$

Statement 22 or 24 stores Y_i^{TE} of (1-34) in $Y(i)$ where

$$i = (m+1)/2 + n/2 * LM \quad \begin{cases} m = 1, 3, 5, \dots, LM \\ n = 0, 2, 4, \dots, LN \end{cases}$$

If the calculated value of $(k_i/k)^2 - \varepsilon_r^2$ is zero, then statement 23 replaces $(k_i/k)^2 - \varepsilon_r^2$ by $10^{-6} \varepsilon_r^2$. Statement 32 stores Y_i^{TM} of (1-35) in $Y(i)$ where

$$i = LM * LN + (m+1)/2 + (n-2)/2 * LM \quad \begin{cases} m = 1, 3, 5, \dots, LM \\ n = 2, 4, 6, \dots, LN \end{cases}$$

C LISTING OF THE SUBROUTINE AY
C

```
SUBROUTINE AY(A,Y)
COMPLEX U,Y(55)
DIMENSION A(50),F(5),STE(5),STM(5)
COMMON AL1,BL1,PI,PI2,PI3,U/R1/ETA/R5/AL,BL
COMMON /R6/ER,LN,LM,NT
A1=SQRT(1./(AL*AL1*BL*BL1))
A2=A1*BL1/(AL*AL1*PI)
A3=1.414214*A2
A4=1./(AL*AL)
A5=1./(AL1*AL1)
A6=PI3*AL1/AL
A7=2.*AL
B1=BL1/BL
B2=B1*PI3
B3=-1.414214*A1*B1/(PI*AL1)
B4=2.*BL
ETA2=ETA*ETA
```

```
LNI=LN+1
30 STE(1)=A2
JN1=2
JN2=2
DO 10 JN=1,LN
C1=JN1*B2
C2=SIN(C1)/C1*(-1)**JN
IF(JN.EQ.LN) GO TO 11
STE(JN2)=A3*C2
11 STM(JN)=JN1*B3*C2
JN1=JN1+2
JN2=JN2+1
10 CONTINUE
JM1=1
DO 12 JM=1,LM
JM2=JM+1
IF(ABS(JM-AL/AL1).LT.0.001) GO TO 13
F(JM)=2./(JM1*JM1*A4-A5)*COS(JM1*A6)*(-1)**JM2
GO TO 14
13 F(JM)=-PI*AL*AL/2.*(-1)**JM2
14 JM1=JM1+2
12 CONTINUE
KTE=0
KTM=LNI*LM
KTM1=LN*LM
JN2=0
DO 20 JN=1,LN1
JN1=JN-1
BN=JN2/B4
JM1=1
DO 21 JM=1,LN
AM=JM1/A7
C1=AM*AM*BN*BN
C2=SQRT(C1)
C1=C1-ER
KTE=KTE+1
IF(C1) 22,23,24
22 Y(KTE)=SQRT(-C1)/ETA
GO TO 25
23 C1=1.E-6*ER
24 Y(KTE)=-U*SQRT(C1)/ETA
25 IF(JN.EQ.LN1) GO TO 26
31 A(KTE)=JM1*STE(JN)*F(JM)/C2
26 IF(JN.EQ.1) GO TO 27
KTM=KTM+1
KTM1=KTM1+1
32 Y(KTM)=ER/(Y(KTE)*ETA2)
33 A(KTM1)=STM(JN1)*F(JM)/C2
27 JM1=JM1+2
21 CONTINUE
JN2=JN2+2
20 CONTINUE
RETURN
END
```

III. DESCRIPTION OF THE SUBROUTINE YHSP

The subroutine YHSP (N,X,Y,YSP) uses the single integrals of (1-68) and the double integrals of (1-59) to calculate elements of the first column of the Y^{hs} matrix (1-12). There are N apertures. X(I) and Y(I) are respectively the x and y center coordinates of the Ith aperture.

Minimum allocations are given by

```
COMPLEX YSP(N)
DIMENSION X(N), Y(N) .
```

The constants D(1) - D(6) are the multiplying factors $K_2 - K_5$ and $K_7 - K_8$ (1-61 to 64, 1-66 to 67) of the integrands of (1-59),

$$D(1) = \lambda \{ (1 - 1/4a'^2) (x_i - x_j + a') \cos \frac{\pi}{a'} (x_j - x_i)$$

$$+ \frac{a'}{\pi} (1 + 1/4a'^2) \sin \frac{\pi}{a'} (x_j - x_i) \}$$

$$D(2) = \lambda \{ (1 - 1/4a'^2) (x_i - x_j + a') \sin \frac{\pi}{a'} (x_j - x_i)$$

$$- \frac{a'}{\pi} (1 + 1/4a'^2) \cos \frac{\pi}{a'} (x_j - x_i) \}$$

$$D(3) = (1 - 1/4a'^2) \cos \frac{\pi}{a'} (x_j - x_i)$$

$$D(4) = (1 - 1/4a'^2) \sin \frac{\pi}{a'} (x_j - x_i)$$

$$D(5) = \lambda \{ (1 - 1/4a'^2) (x_j - x_i + a') \cos \frac{\pi}{a'} (x_j - x_i)$$

$$- \frac{a'}{\pi} (1 + 1/4a'^2) \sin \frac{\pi}{a'} (x_j - x_i) \}$$

$$D(6) = \lambda \{ (1 - 1/4a'^2) (x_j - x_i + a') \sin \frac{\pi}{a'} (x_j - x_i)$$

$$+ \frac{a'}{\pi} (1 + 1/4a'^2) \cos \frac{\pi}{a'} (x_j - x_i) \}$$

(a' , x_i , and x_j are distances per unit wavelength).

The constants TH1 - TH9 are angles at which a rotating line from the origin (line O-A in Fig. 1) will intersect different straight line segment junctions defined by $x = x_j - x_i - a'$, $x_j - x_i$, $x_j - x_i + a'$, and $y = y_j - y_i - b'$, $y_j - y_i$, $y_j - y_i + b'$ (see Fig. 1).

The CALL INT(N4, N5, N6, P1, P2, XL, XU) statements between 12 and 11 select the correct $\rho_1(\theta)$ and $\rho_2(\theta)$ expressions used in $M_1(\theta) - M_6(\theta)$ (1-77 to 82), select the integrand for each subarea (I-IV) in which the single integration is being performed, and supply the θ limits of integration.

For

$N4 = 0,$	$\rho_1(\theta) = 0$
$N4 = 1,$	$\rho_1(\theta) = P1/\cos \theta$
$N4 = 2,$	$\rho_1(\theta) = P1/\sin \theta$
$N5 = 0,$	$\rho_2(\theta) = 0$
$N5 = 1,$	$\rho_2(\theta) = P2/\cos \theta$
$N5 = 2,$	$\rho_2(\theta) = P2/\sin \theta$
$N6 < 2,$	Integration over a subarea I-IV is still being performed
$N6 = 2,$	Multiplying factors for subareas I and III are used
$N6 = 3,$	Multiplying factors for subareas II and IV are used

where P1 and P2 are lines which define the subareas of integration (I-IV) and, therefore, represent the limits of integration for the variable ρ . For instance, in Fig. 1, the lines which define the limits of integration along line OA in subarea IV are $P1 = y_j - y_i$ and $P2 = y_j - y_i + b'$. XL and XU represent respectively the θ_{lower} and θ_{upper} limits of integration.

The arguments of the CALL INT statements will vary since the area of integration (I-IV) can move throughout the first quadrant of the uv plane (assumes $x_i \leq x_j$). There will be overlapping into other quadrants

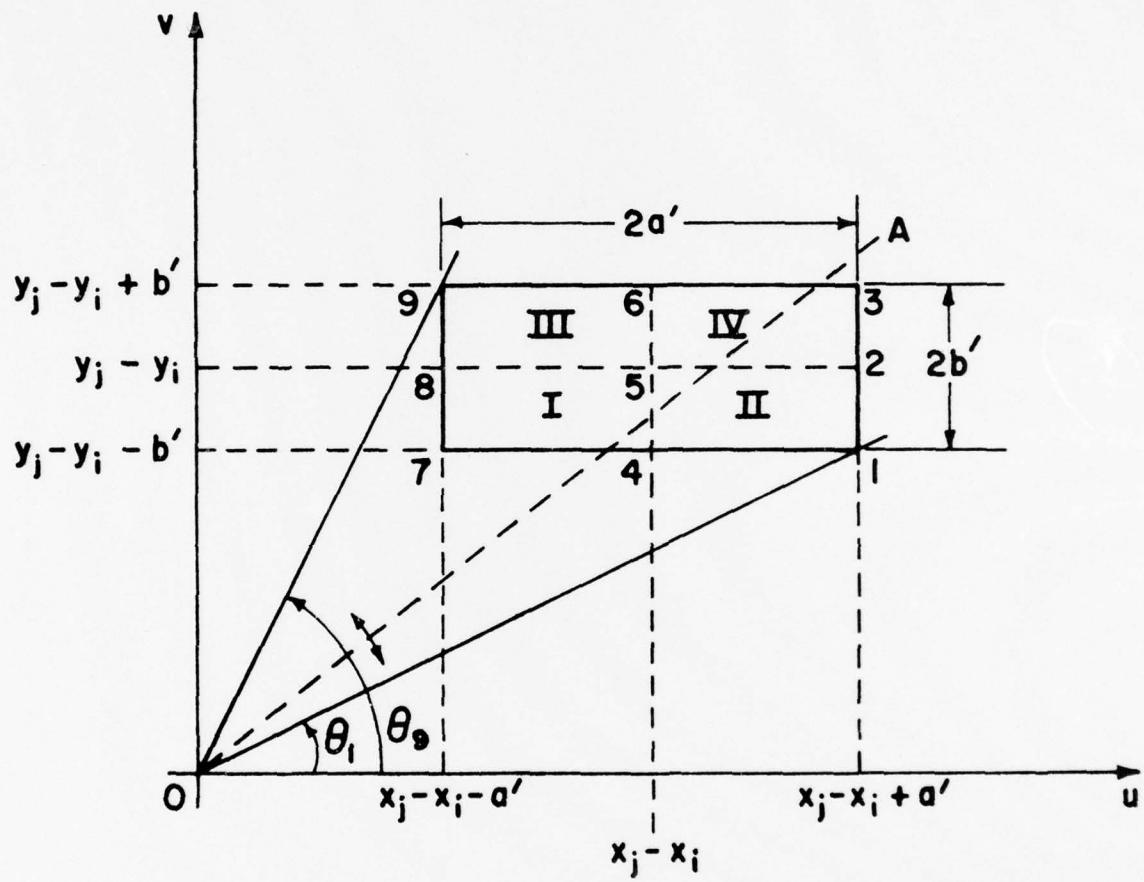


Fig. 1. Integration subareas for solution involving the single integrals of (1-68).

when $x_i = x_j$, $y_i \neq y_j$, $x_i \neq x_j$, $y_i = y_j$, and $x_i = x_j$, $y_i = y_j$. There are four specific cases to consider for determining the integrations to be performed:

Case 1) $x_i \neq x_j$, $y_i \neq y_j$ - this integration will require twelve CALL INT statements representing the twelve integration areas of subareas (I-IV). The twelve statements are located between statements 13 and 14.

Case 2) $x_i = x_j$, $y_i \neq y_j$ - this integration will require only four CALL INT statements because of symmetry considerations. The four statements are located between statements 14 and 15.

Case 3) $x_i \neq x_j$, $y_i = y_j$ - this integration like case 2 will require only four statements which are located between statements 15 and 11.

Case 4) $x_i = x_j$, $y_i = y_j$ - this integration which represents the calculation of the self-admittance will require only two CALL INT statements which are located between statements 12 and 13.

If $(x_j - x_i) > 4a$, a solution involving the double integrals of (1-59) is used. The calling statement is CALL QG6A(XL,XU,YL,YU,N9,Z). The variables XL, XU, YL, YU represent respectively the lower and upper limits of integration for the u and v variables of integration in (1-59).

If N9 = 1, the first of the four double integrals of (1-59) are evaluated (if N9 = 2, the second, etc.). There are three specific cases to consider for determining the integrations to be performed:

Case 1) $x_i \neq x_j$, $y_i \neq y_j$ - this integration will require four CALL QG6A statements representing the four subareas of integration (I-IV). The four statements are located between statements 11 and 25.

Case 2) $x_i = x_j, y_i \neq y_j$ - this integration will require only two CALL QG6A statements because of symmetry considerations. The two statements are located between statements 25 and 26.

Case 3) $x_i \neq x_j, y_i = y_j$ - this integration like case 2 will require only two CALL QG6A statements which are located between statements 26 and 10.

C LISTING OF THE SUBROUTINE YHSP
C

```

SUBROUTINE YHSP(N,X,Y,YSP)
COMPLEX G3,G5,G7,G9,S(10),SA,SB,U,U1,YSP(6)
DIMENSION X(6),Y(6)
COMMON A1,B1,PI,PI2,PI3,U/R1/ETA/R2/D(6),S
COMMON /R3/G1,G2,G3,G4,G5,G6,G7,G8,G9,G10,G11
COMMON /R5/AL,BL/R7/YY3,YY4
U1=U/(A1*B1*ETA)
DO 10 J=1,N
X1=X(1)
X2=X(J)
Y1=Y(1)
Y2=Y(J)
XX1=X2-X1-A1
XX2=X2-X1
XX3=X2-X1+A1
XX4=X1-X2+A1
YY1=Y2-Y1-B1
YY2=Y2-Y1
YY3=Y2-Y1+B1
YY4=Y1-Y2+B1
XA=(X2-X1)/G1
DI=4.*AL
C1=COS(XA)
C2=SIN(XA)
D(3)=C1*G10
D(4)=C2*G10
C1=C1*G11
C2=C2*G11
D(1)=XX4*D(3)+C2
D(2)=XX4*D(4)-C1
D(5)=XX3*D(3)-C2
D(6)=XX3*D(4)+C1
IF(XX2.GT.DI) GO TO 11
TH1=ATAN2(YY1,XX3)
TH2=ATAN2(YY2,XX3)
TH3=ATAN2(YY3,XX3)
TH4=ATAN2(YY1,XX2)
TH6=ATAN2(YY3,XX2)
TH7=ATAN2(YY1,XX1)

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TH8=ATAN2(YY2,XX1)
TH9=ATAN2(YY3,XX1)
IF(J.EQ.1) GO TO 12
TH5=ATAN2(YY2,XX2)
12 IF(J.GT.1) GO TO 13
CALL INT(0,1,0,0.,XX3,0.,TH3)
CALL INT(0,2,3,0.,YY3,TH3,PI3)
YSP(J)=4.*((YY3*S(9))-S(10))
GO TO 10
13 IF((X1.EQ.X2).AND.(Y1.NE.Y2)) GO TO 14
IF((X1.NE.X2).AND.(Y1.EQ.Y2)) GO TO 15
IF(TH7.GT.TH5) GO TO 16
CALL INT(2,1,0,YY1,XX2,TH4,TH7)
CALL INT(1,1,1,XX1,XX2,TH7,TH5)
CALL INT(1,2,2,XX1,YY2,TH5,TH8)
GO TO 17
16 CALL INT(2,1,0,YY1,XX2,TH4,TH5)
CALL INT(2,2,1,YY1,YY2,TH5,TH7)
CALL INT(1,2,2,XX1,YY2,TH7,TH8)
17 SA=YY4*S(9)
SB=S(10)
IF(TH8.GT.TH6) GO TO 18
CALL INT(2,1,0,YY2,XX2,TH5,TH8)
CALL INT(1,1,1,XX1,XX2,TH8,TH6)
CALL INT(1,2,2,XX1,YY3,TH6,TH9)
GO TO 19
18 CALL INT(2,1,0,YY2,XX2,TH5,TH6)
CALL INT(2,2,1,YY2,YY3,TH6,TH8)
CALL INT(1,2,2,XX1,YY3,TH8,TH9)
19 SA=SA+YY3*S(9)
SB=SB-S(10)
YSP(J)=SA+SB
IF(TH4.GT.TH2) GO TO 20
CALL INT(2,1,0,YY1,XX3,TH1,TH4)
CALL INT(1,1,1,XX2,XX3,TH4,TH2)
CALL INT(1,2,3,XX2,YY2,TH2,TH5)
GO TO 21
20 CALL INT(2,1,0,YY1,XX3,TH1,TH2)
CALL INT(2,2,1,YY1,YY2,TH2,TH4)
CALL INT(1,2,3,XX2,YY2,TH4,TH5)
21 SA=YY4*S(9)
SB=S(10)
IF(TH5.GT.TH3) GO TO 22
CALL INT(2,1,0,YY2,XX3,TH2,TH5)
CALL INT(1,1,1,XX2,XX3,TH5,TH3)
CALL INT(1,2,3,XX2,YY3,TH3,TH6)
GO TO 23
22 CALL INT(2,1,0,YY2,XX3,TH2,TH3)
CALL INT(2,2,1,YY2,YY3,TH3,TH5)
CALL INT(1,2,3,XX2,YY3,TH5,TH6)
23 SA=SA+YY3*S(9)
SB=SB-S(10)
YSP(J)=YSP(J)+SA+SB
GO TO 10
14 CALL INT(2,2,0,YY1,YY2,PI3,TH8)
CALL INT(2,1,2,YY1,XX1,TH8,TH7)
SA=YY4*S(9)
SB=S(10)

```

```
CALL INT(2,2,0,YY2,YY3,PI3,TH9)
CALL INT(2,1,2,YY2,XX1,TH9,TH8)
SA=SA+YY3*S(9)
SB=SB-S(10)
YSP(J)=2.*(SA+SB)
GO TO 10
15 CALL INT(1,2,0,XX1,YY1,TH7,TH4)
CALL INT(1,1,2,XX1,XX2,TH4,0.)
YSP(J)=YY4*S(9)+S(10)
CALL INT(1,2,0,XX2,YY1,TH4,TH1)
CALL INT(1,1,3,XX2,XX3,TH1,0.)
YSP(J)=2.*(YSP(J)+YY4*S(9)+S(10))
GO TO 10
11 IF((X1.EQ.X2).AND.(Y1.NE.Y2)) GO TO 25
IF((X1.NE.X2).AND.(Y1.EQ.Y2)) GO TO 26
CALL QG6A(XX1,XX2,YY1,YY2,1,SA)
SB=SA
CALL QG6A(XX2,XX3,YY1,YY2,2,SA)
SB=SB+SA
CALL QG6A(XX1,XX2,YY2,YY3,3,SA)
SB=SB+SA
CALL QG6A(XX2,XX3,YY2,YY3,4,SA)
YSP(J)=SA+SB
GO TO 10
25 CALL QG6A(XX1,XX2,YY1,YY2,1,SA)
SB=2.*SA
CALL QG6A(XX1,XX2,YY2,YY3,3,SA)
YSP(J)=2.*SA+SB
GO TO 10
26 CALL QG6A(XX1,XX2,YY1,YY2,1,SA)
SB=2.*SA
CALL QG6A(XX2,XX3,YY1,YY2,2,SA)
YSP(J)=2.*SA+SB
10 CONTINUE
DO 30 I=1,N
YSP(I)=U1*YSP(I)
30 CONTINUE
RETURN
END
```

IV. DESCRIPTION OF THE SUBROUTINES FCT AND FCTA

The subroutine FCT (W,X) supplies the integrands for the single numerical integration subroutine QG8. The W(I) are the integrands of equation (1-68) evaluated at $\theta = X$ where X is the variable of integration for QG8.

The logic between statements 40 and 6 determines the $\rho_1(\theta)$ and $\rho_2(\theta)$ expressions used in $M_1(\theta) - M_6(\theta)$ (1-77 to 82).

For

N4 = 0 ,	C = $\rho_1(\theta) = 0$
N4 = 1 ,	C = $\rho_1(\theta) = P1/\cos \theta$
N4 = 2 ,	C = $\rho_1(\theta) = P1/\sin \theta$
N5 = 0 ,	D = $\rho_2(\theta) = 0$
N5 = 1 ,	D = $\rho_2(\theta) = P2/\cos \theta$
N5 = 2 ,	D = $\rho_2(\theta) = P2/\sin \theta$.

W(1) - W(8) represent respectively $L_1(\theta) - L_8(\theta)$ (1-69 to 76).

The logic statements between 41 and 37 supply the limiting expressions (1-84 to 99) when $|\frac{\pi}{a} \cos \theta \pm k| < \epsilon$ (a small value). For a first order zero $(\frac{\pi}{a} \cos \theta \pm k)$ in the denominator of $L_1(\theta) - L_8(\theta)$ (1-69 to 76), the ϵ value of E1 = 0.0002 was used while for higher order zeros, $\epsilon = E2 = 0.002$ was used.

The subroutine FCTA(N9,X,Y,Z) supplies the integrands for the double numerical integration subroutines QG6A and QG6B. N9 specifies which of the four double integrals of (1-59) will be evaluated (if N9 = 1, the first of the four, if N9 = 2, the second, etc.). X and Y are the variables of integration respectively for QG6A and QG6B. Z is the integrand of one of the four double integrals of (1-59) evaluated at X and Y. The integrands of the double integrals of (1-59) are transferred from subroutine YHSP to subroutine FCTA through the COMMON/R2/ and COMMON/R7/ statements.

C LISTINGS OF THE SUBROUTINES FCT AND FCTA
C

14

```
SUBROUTINE FCT(W,X)
COMPLEX E(8),F(8),G3,G5,G7,G9,SA,SB,U,W(8)
COMMON A1,B1,PI,PI2,PI3,U/R3/G1,G2,G3,G4,G5,G6,G7,G8,G9,G10,GL1
COMMON /R4/N4,N5,N6,P1,P2,XL,XU
C1=COS(X)
C2=SIN(X)
E1=0.0002
E2=0.002
P=C1/A1
S=PI*(P-2.)
T=PI*(P+2.)
40 IF(N4.NE.0) GO TO 1
C=0.
GO TO 3
1 IF(N4.EQ.2) GO TO 2
C=P1/C1
GO TO 3
2 C=P1/C2
3 IF(N5.NE.0) GO TO 4
D=0.
GO TO 6
4 IF(N5.EQ.2) GO TO 5
D=P2/C1
GO TO 6
5 D=P2/C2
6 Y=C1-2.*A1
P=D*S
E(1)=COS(P)+U*SIN(P)
P=C*T
E(2)=COS(P)+U*SIN(P)
Z=C1+2.*A1
P=D*T
F(1)=COS(P)-U*SIN(P)
P=C*T
F(2)=COS(P)-U*SIN(P)
E(3)=(E(1)-E(2))/Y
F(3)=(F(1)-F(2))/Z
SA=D*E(1)
SB=C*E(2)
E(4)=(SA-SB)/Y
SA=D*SA
SB=C*SB
E(6)=(SA-SB)/Y
SA=D*F(1)
SB=C*F(2)
F(4)=(SA-SB)/Z
E(5)=E(3)/Z
F(5)=F(3)/Z
SA=D*SA
SB=C*SB
F(6)=(SA-SB)/Z
E(7)=E(4)/Y
F(7)=F(4)/Z
E(8)=E(5)/Y
F(8)=F(5)/Z
41 IF(ABS(Y).LT.E1) GO TO 20
IF(ABS(Z).LT.E1) GO TO 21
W(1)=G3*(E(3)-F(3))
```

```

      GO TO 22
20 W(1)=-G3*F(3)+0.5*(D-C)
      GO TO 22
21 W(1)=G3*E(3)+0.5*(D-C)
22 IF(ABS(Y).LT.E1) GO TO 23
    IF(ABS(Z).LT.E1) GO TO 24
    W(2)=-G2*(E(3)+F(3))
    GO TO 25
23 W(2)=-G2*F(3)-0.5*U*(D-C)
    GO TO 25
24 W(2)=-G2*E(3)+0.5*U*(D-C)
25 IF(ABS(Y).LT.E2) GO TO 26
    IF(ABS(Z).LT.E2) GO TO 27
    W(5)=G3*(E(4)-F(4))+G6*(E(5)+F(5))
    GO TO 28
26 H=0.25*(D*D-C*C)
    W(5)=-G3*F(4)+G6*F(5)+H
    GO TO 28
27 H=0.25*(D*D-C*C)
    W(5)=G3*E(4)+G6*E(5)+H
28 W(3)=C1*W(5)
    W(5)=C2*W(5)
    IF(ABS(Y).LT.E2) GO TO 29
    IF(ABS(Z).LT.E2) GO TO 30
    W(6)=-G2*(E(4)+F(4))+G7*(E(5)-F(5))
    GO TO 31
29 W(6)=-G2*F(4)-G7*F(5)-U*H
    GO TO 31
30 W(6)=-G2*E(4)+G7*E(5)+U*H
31 W(4)=C1*W(6)
    W(6)=C2*W(6)
    C1=C1*C2
    IF(ABS(Y).LT.E2) GO TO 32
    IF(ABS(Z).LT.E2) GO TO 33
    W(7)=C1*(G3*(E(6)-F(6))+G4*(E(7)+F(7))-G9*(E(8)-F(8)))
    GO TO 34
32 H=(D*D*D-C*C*C)/6.
    W(7)=C1*(-G3*F(6)+G4*F(7)+G9*F(8)+H)
    GO TO 34
33 H=(D*D*D-C*C*C)/6.
    W(7)=C1*(G3*E(6)+G4*E(7)-G9*E(8)+H)
34 IF(ABS(Y).LT.E2) GO TO 35
    IF(ABS(Z).LT.E2) GO TO 36
    W(8)=C1*(-G2*(E(6)+F(6))+G5*(E(7)-F(7))+G8*(E(8)+F(8)))
    GO TO 37
35 W(8)=C1*(-G2*F(6)-G5*F(7)+G8*F(8)-U*H)
    GO TO 37
36 W(8)=C1*(-G2*E(6)+G5*E(7)+G8*E(8)+U*H)
37 CONTINUE
      RETURN
      END
      SUBROUTINE FCTA(N9,X,Y,Z)
      COMPLEX G,G3,G5,G7,G9,S(10),U,Z
      COMMON AL1,BL1,PI,PI2,PI3,U/R2/D(6),S
      COMMON /R3/G1,G2,G3,G4,G5,G6,G7,G8,G9,G10,G11/R7/YY3,YY4
      P1=X/G1
      C1=COS(P1)
      C2=SIN(P1)
      C3=SQRT(X*X+Y*Y)
      C4=PI2*C3

```

```
G=(COS(C4)-U*SIN(C4))/C3
IF(N9.EQ.2) GO TO 1
IF(N9.EQ.3) GO TO 2
IF(N9.EQ.4) GO TO 3
Z=G*(YY4+Y)*(C1*(D(1)+X*D(3))+C2*(D(2)+X*D(4)))
RETURN
1 Z=G*(YY4+Y)*(C1*(D(5)-X*D(3))+C2*(D(6)-X*D(4)))
RETURN
2 Z=G*(YY3-Y)*(C1*(D(1)+X*D(3))+C2*(D(2)+X*D(4)))
RETURN
3 Z=G*(YY3-Y)*(C1*(D(5)-X*D(3))+C2*(D(6)-X*D(4)))
RETURN
END
```

V. DESCRIPTION OF THE SUBROUTINE INT

The subroutine INT(N4, N5, N6, P1, P2, XL, XU) transfers the data N4, N5, N6 which is supplied by the subroutine YHSP and required by the subroutine FCT through the COMMON/R4/ statement, calls the single numerical integration subroutine QG8, and calculates the S(9) and S(10) terms which represent the four single integrals of (1-68). The arguments N4, N5, N6, P1, P2, XL, and XU are defined in the description of the subroutine YHSP and will not be repeated here.

The following logical statements are located between statements 3 and 4. If N6 is less than 2, no S(9) or S(10) term is calculated (one or two more intermediate integrations are required before evaluation). Also, if N6 = 0, the variable S which represents the result of intermediate integrand evaluations of subroutine QG8 is reset to zero. If N6 = 2, S(9) represents the first single integral (I) of (1-68) and S(10) represents the third (III). If N6 = 3, S(9) represents the second integral (II) of (1-68) and S(10) represents the fourth (IV).

C LISTING OF THE SUBROUTINE INT

```

C
SUBROUTINE INT(N4,N5,N6,P1,P2,XL,XU)
COMPLEX S(10),T(8)
COMMON /R2/D(6),S/R4/N7,N8,N9,P3,P4,XL1,XU1
N7=N4
N8=N5
N9=N6
P3=P1
P4=P2
XL1=XL
XU1=XU
IF(N6.NE.0) GO TO 1
DO 2 I=1,8
S(I)=(0.,0.)
2 CONTINUE
1 CALL QG8(T)
DO 3 I=1,8
S(I)=S(I)+T(I)
3 CONTINUE
IF(N6.LT.2) GO TO 4
IF(N6.EQ.2) S(9)=D(1)*S(1)+D(2)*S(2)+D(3)*S(3)+D(4)*S(4)
IF(N6.EQ.3) S(9)=D(5)*S(1)+D(6)*S(2)-D(3)*S(3)-D(4)*S(4)
IF(N6.EQ.2) S(10)=D(1)*S(5)+D(2)*S(6)+D(3)*S(7)+D(4)*S(8)
IF(N6.EQ.3) S(10)=D(5)*S(5)+D(6)*S(6)-D(3)*S(7)-D(4)*S(8)
4 CONTINUE
RETURN
END

```

VI. DESCRIPTION OF THE SUBROUTINES QG6A, QG6B, AND QG8

The combination of subroutines QG6A(XL, XU, YL, YU, N9, Z) and QG6B(X, YL, YU, N9, Z) perform a six-point Gaussian quadrature double numerical integration on the double integrals of (1-59). The basic integral under consideration can be represented as

$$I = \int_{XL}^{XU} dx \int_{YL}^{YU} dy F(x, y) . \quad (1)$$

This integral can be transformed from the integration intervals (XL, XU), (YL, YU) to the intervals (-1, 1), (-1, 1) by the transformation

$$x' = \frac{2x - (XU + XL)}{(XU - XL)} \quad (2)$$

$$y' = \frac{2y - (YU + YL)}{(YU - YL)} \quad (3)$$

so that (1) becomes

$$I = \left(\frac{XU-XL}{2} \right) \left(\frac{YU-YL}{2} \right) \int_{-1}^1 dx' \int_{-1}^1 dy' F\left(\left[\frac{XU-XL}{2} x' + \frac{XU+XL}{2}\right], \left[\frac{YU-YL}{2} y' + \frac{YU+YL}{2}\right]\right) . \quad (4)$$

A double six-point Gaussian quadrature formula [2, Section 7.2] is used to evaluate (4),

$$I = \left(\frac{XU-XL}{2} \right) \left(\frac{YU-YL}{2} \right) \sum_{i=1}^6 \sum_{j=1}^6 A_i^{(6)} A_j^{(6)} F(x_i^{(6)}, y_j^{(6)}) \quad (5)$$

where $x_i^{(6)}$, $y_j^{(6)}$ are the roots of the Legendre polynomial of degree 6 - $P_6(x_i^{(6)})$ or $y_j^{(6)} = 0$ (the Legendre polynomials are orthogonal on the (-1, 1) interval). The coefficients $A_i^{(6)}$, $A_j^{(6)}$ are defined as

$$A_i^{(6)} = \frac{1}{3 P'_6(x_i^{(6)}) P_5(x_i^{(6)})} \quad (6)$$

$$A_j^{(6)} = \frac{1}{3 P'_6(y_j^{(6)}) P_5(y_j^{(6)})} \quad (7)$$

(' represents derivative) and are tabulated [2, p. 337].

In the calling arguments, (XL, XU, YL, YU) represents respectively the lower and upper limits of integration for the x and y variables, N9 is used in the subroutine FCTA to specify the function to be integrated (if N9 = 1, the first double integral integrand of (1-59) is specified, if N9 = 2, the second, etc.) and Z is the result of the integration.

Subroutine QG8(Y) performs a single eight-point Gaussian quadrature numerical integration on the single integrals of (1-68). In the calling argument, Y is the result of the integration. The variables N4, N5, N6, P1, P2, XL, and XU in the COMMON/R4/ statement are defined in the description of subroutine YHSP and will not be repeated here.

```
C      LISTINGS OF THE SUBROUTINE QG6A,QG6B,AND QG8
C
SUBROUTINE QG6A(XL,XU,YL,YU,N9,Z)
COMPLEX Z,Z1,Z2
A=0.5*(XL+XU)
B=XU-XL
C=0.4662348*B
X=A+C
CALL QG6B(X,YL,YU,N9,Z1)
X=A-C
CALL QG6B(X,YL,YU,N9,Z2)
Z=0.08566225*(Z1+Z2)
C=0.3306047*B
X=A+C
CALL QG6B(X,YL,YU,N9,Z1)
X=A-C
CALL QG6B(X,YL,YU,N9,Z2)
Z=Z+0.1803808*(Z1+Z2)
C=0.1193096*B
X=A+C
CALL QG6B(X,YL,YU,N9,Z1)
X=A-C
CALL QG6B(X,YL,YU,N9,Z2)
Z=B*(Z+0.2339570*(Z1+Z2))
RETURN
END
SUBROUTINE QG6B(X,YL,YU,N9,Z)
COMPLEX Z,Z1,Z2
A=0.5*(YL+YU)
B=YU-YL
C=0.4662348*B
Y=A+C
CALL FCTA(N9,X,Y,Z1)
```

```
Y=A-C
CALL FCTA(N9,X,Y,Z2)
Z=0.08566225*(Z1+Z2)
C=0.3306047*B
Y=A+C
CALL FCTA(N9,X,Y,Z1)
Y=A-C
CALL FCTA(N9,X,Y,Z2)
Z=Z+0.1803808*(Z1+Z2)
C=0.1193096*B
Y=A+C
CALL FCTA(N9,X,Y,Z1)
Y=A-C
CALL FCTA(N9,X,Y,Z2)
Z=B*(Z+0.2339570*(Z1+Z2))
RETURN
END
SUBROUTINE QG8(Y)
COMPLEX T(8),T1(8),Y(8)
COMMON /R4/N4,N5,N6,P1,P2,XL,XU
A=.5*(XL+XU)
B=XU-XL
C=.4801449*B
X=A+C
CALL FCT(T,X)
DO 1 I=1,8
T1(I)=T(I)
1 CONTINUE
X=A-C
CALL FCT(T,X)
DO 2 I=1,8
Y(I)=.05061427*(T(I)+T1(I))
2 CONTINUE
C=.3983332*B
X=A+C
CALL FCT(T,X)
DO 3 I=1,8
T1(I)=T(I)
3 CONTINUE
X=A-C
CALL FCT(T,X)
DO 4 I=1,8
Y(I)=Y(I)+.1111905*(T(I)+T1(I))
4 CONTINUE
C=.2627662*B
X=A+C
CALL FCT(T,X)
DO 5 I=1,8
T1(I)=T(I)
5 CONTINUE
X=A-C
CALL FCT(T,X)
DO 6 I=1,8
Y(I)=Y(I)+.1568533*(T(I)+T1(I))
6 CONTINUE
C=.09171732*B
X=A+C
CALL FCT(T,X)
```

```
DO 7 I=1,8
T1(I)=T(I)
7 CONTINUE
X=A-C
CALL FCT(T,X)
DO 8 I=1,8
Y(I)=B*(Y(I)+.1813419*(T(I)+T1(I)))
8 CONTINUE
RETURN
END
```

VII. DESCRIPTION OF THE SUBROUTINE CSMTZ

The subroutine CSMTZ(N , A , B , X) solves the set of equations

$$L_N s_N = d_N \quad (8)$$

where L_N is an $N \times N$ complex symmetric Toeplitz matrix. In the argument of CSMTZ, N is the number of unknowns in (8), A is the input array whose elements are the first row of L_N , B is the input array whose elements are those of d_N , and X is the output array whose elements are those of s_N . It is assumed that (8) is normalized so that the first element of the first row of L_N is equal to unity.

This subroutine solves equation (1-15)

$$[Y^{wg} + Y^{hs}] \vec{V} = \vec{I}^{imp} \quad (1-15)$$

where $[Y^{wg} + Y^{hs}]$ is a symmetric Toeplitz admittance matrix (linear array lattice case).

The two main advantages of the algorithm used in this subroutine are

- (1) It solves equation (1-15) directly without inversion of $[Y^{wg} + Y^{hs}]$ requiring roughly $2N^2$ multiplications and divisions.
- (2) It requires only the first row of $[Y^{wg} + Y^{hs}]$ and, therefore, minimizes the storage requirement for the subroutine.

The derivation of the algorithm can be found in [3, 4] and will not be repeated here. However, the algorithm logic will be presented using the notation developed in [3, 4]. The following notation will be used (the same used by Zohar in [3, 4]): Greek letters are used for scalars, capital letters for square matrices, lower case letters for column matrices, \sim denotes transpose, and $\hat{\cdot}$ is a reversal symbol - \hat{g}_k denotes the reversed order of g_k , that is, $(\hat{g}_k)_{il} = (g_k)_{k+l-i,1}$.

The matrix L_N of (8) is bordered as follows,

$$L_N = \begin{bmatrix} 1 & \tilde{r}_{N-1} \\ r_{N-1} & L_{N-1} \end{bmatrix} \quad (9)$$

where $\tilde{r}_{N-1} = [A(2), A(3), \dots, A(N)]$ ($A(i)$ indicates the i th component (numbered columnwise) of array A). In (8), $\tilde{d}_N = [\delta_1, \delta_2, \dots, \delta_N]$. The algorithm is based on a recursion relation with initial values given by

$$s_1 = \delta_1, \quad \rho_1 = -A(2), \quad \lambda_1 = 1 - A(2) * A(2). \quad (10)$$

Recursion of s_i , \hat{e}_i , and λ_i for $i=1, 2, \dots, N-2$ is given by

$$\theta_i = \delta_{i+1} - \tilde{s}_i \hat{r}_i \quad (11)$$

$$\eta_i = -A(i+2) - \tilde{r}_i \hat{e}_i \quad (12)$$

$$s_{i+1} = \begin{bmatrix} s_i + (\theta_i / \lambda_i) \hat{e}_i \\ \theta_i / \lambda_i \end{bmatrix} \quad (13)$$

$$e_{i+1} = \begin{bmatrix} e_i + (\eta_i / \lambda_i) \hat{e}_i \\ \eta_i / \lambda_i \end{bmatrix} \quad (14)$$

$$\lambda_{i+1} = \lambda_i - \eta_i^2 / \lambda_i. \quad (15)$$

The last computed values are θ_{N-1} , η_{N-2} , s_N , e_{N-1} , and λ_{N-1} . Note that \tilde{a}_N , g_N , and γ appearing in [3] are not needed because of symmetry.

Minimum allocations are given by

COMPLEX A(N), B(N), E(N), ES(N-1), X(N).

The initial values for recursion are first computed: $s_1 = X(1)$, $\rho_1 = E(1)$, and $\lambda_1 = LA$. DO loop 10 is the main recursion loop whose index is $i(i=1,2,\dots,N-2)$. DO loop 11 computes $S1 = \tilde{s}_i \hat{r}_i$ and $E1 = \tilde{r}_i \hat{e}_i$. Following statement 11, η_i and θ_i are computed. DO loop 12 computes s_{i+1} and stores e_i in dummy array ES because e_i is needed in DO loop 13 to recompute itself. DO loop 13 computes e_i . Following 13, λ_{i+1} is computed and the index i of DO loop 10 is stopped. DO loops 14 and 15 compute s_N .

```

C      LISTING OF THE SUBROUTINE CSMTZ
C
SUBROUTINE CSMTZ(N,A,B,X)
COMPLEX A(6),B(6),E(6),ES(5),X(6)
COMPLEX E1,ET,ET1,LA,S1,TH,TH1
X(1)=B(1)
E(1)=-A(2)
LA=A(1)-A(2)*A(2)
N1=N-2
N2=N-1
DO 10 I=1,N1
E1=(0.,0.)
S1=(0.,0.)
DO 11 J=1,I
S1=S1+X(J)*A(I-J+2)
E1=E1+E(I-J+1)*A(J+1)
11 CONTINUE
ET=-A(I+2)-E1
TH=B(I+1)-S1
TH1=TH/LA
ET1=ET/LA
DO 12 K=1,I
X(K)=X(K)+TH1*E(I-K+1)
ES(K)=E(K)
12 CONTINUE
DO 13 K=1,I
E(K)=ES(K)+ET1*ES(I-K+1)
13 CONTINUE
X(I+1)=TH/LA
E(I+1)=ET1
LA=LA-ET*ET1
10 CONTINUE
S1=(0.,0.)
DO 14 J=1,N2
S1=S1+X(J)*A(N-J+1)
14 CONTINUE
TH=B(N)-S1
TH1=TH/LA
DO 15 K=1,N2
X(K)=X(K)+TH1*E(N-K)
15 CONTINUE
X(N2+1)=TH1
RETURN
END

```

VIII. DESCRIPTION OF THE SUBROUTINES MATMLT, TRMMLT, MULTTR,
MATVCA, AND LNSLV

The subroutines MATMLT, TRMMLT, MULTTR, MATVCA, LNSLV, and the following recursion relationships are taken from a research report by D. H. Sinnott [5]. These subroutines represent an efficient algorithm for solving equation (1-15)

$$[Y^{wg} + Y^{hs}] \vec{V} = \vec{I}^{imp} \quad (1-15)$$

where $[Y^{wg} + Y^{hs}]$ is a symmetric block-Toeplitz admittance matrix. The two main advantages of this algorithm are:

- (1) It solves equation (1-15) directly without inversion of $[Y^{wg} + Y^{hs}]$ and is, therefore, more efficient.
- (2) Storage requirements are considerably less than that required for an inversion solution. Approximately one quarter of the matrix $[Y^{wg} + Y^{hs}]^{-1}$ must be stored for an inversion solution while only the first row of blocks of $[Y^{wg} + Y^{hs}]$ is required for the given algorithm solution.

Recall the form of the block-Toeplitz matrix Y ,

$$[Y] = Y^{(n)} = \begin{bmatrix} Y_0 & Y_1 & \dots & Y_n \\ Y_1 & Y_0 & \dots & Y_{n-1} \\ \vdots & & & \\ Y_n & Y_{n-1} & \dots & Y_0 \end{bmatrix} \quad (1-108)$$

where Y_0 is the submatrix which defines the self-admittance of an element of the array (specified number of apertures - see Fig. 1-5) and $Y_{|i-j|}$, $i \neq j$, is the submatrix which defines the mutual admittance between elements i and j of the array. The parenthesized superscripts, as in $Y^{(s)}$, are used to identify the order of the matrix since the algorithm to be presented is defined recursively on n . Since $Y^{(n)}$ is also symmetric, all submatrices Y_i are symmetric. The submatrices are $N_p \times N_p$ complex matrices where N_p is the shortest row or column dimension of the array lattice.

Since the submatrices are of order $N_p \times N_p$, then $Y^{(n)}$ is of order $N_p \cdot (n+1) \times N_p \cdot (n+1)$. A recursive system of equations defines further sets of $N_p \times N_p$ matrices,

$$\left. \begin{aligned} \psi_o^{(0)} &= Y_o^{-1} Y_1 \\ \Delta^{(-1)} &= Y_o^{-1} \\ \Delta^{(m-1)} &= [I_N - (\psi_{m-1}^{(m-1)})^2]^{-1} \Delta^{(m-2)} \\ \psi_m^{(m)} &= -\Delta^{(m-1)} \left[\sum_{s=0}^{m-1} \psi_s^{(m-1)T} Y_{m-s} - Y_{m+1} \right] \\ \psi_r^{(m)} &= \psi_r^{(m-1)} - \psi_{m-r-1}^{(m-1)} \psi_m^{(m)}, \quad 0 \leq r \leq m-1 \end{aligned} \right\} \quad (16)$$

for $m=1, 2, \dots, n-1$ (superscript T denotes transpose). Then the $N_p \times N_p$ submatrices of $Z = Y^{-1}$, defined by

$$Z = \begin{bmatrix} z_{00} & z_{01} & z_{02} & \cdots & z_{0n} \\ z_{10} & z_{11} & z_{12} & \cdots & z_{1n} \\ \vdots & \vdots & & & \\ z_{n0} & z_{n1} & \cdots & \cdots & z_{nn} \end{bmatrix} \quad (17)$$

are given by

$$z_{00} = \Delta^{(n-1)} \quad (18)$$

$$z_{r0} = -\psi_{r-1}^{(n-1)} \Delta^{(n-1)}, \quad 1 \leq r \leq n \quad (19)$$

$$\begin{aligned} z_{rs} &= z_{r-1,s-1} + \psi_{r-1}^{(n-1)} \Delta^{(n-1)} \psi_{s-1}^{(n-1)T} \\ &\quad - \psi_{n-r}^{(n-1)} \Delta^{(n-1)} \psi_{n-s}^{(n-1)T} \quad 1 \leq r, s \leq n \end{aligned} \quad (20)$$

where $\psi_{-1}^{(n-1)} = -I_{N_p}$, the unit matrix of order N_p and $\psi_r^{(n-1)} = 0$ for $r \geq n$.

The solution for \vec{V} , partitioned into subvectors of length N_p denoted V_r ($r=0,1,\dots,n$) is

$$V_r = \sum_{s=0}^n z_{rs} I_s \quad (21)$$

where I_s is the s th subvector of I of length N_p . Next define the matrices ϕ_r where

$$\phi_r = \Delta^{(n-1)} \psi_r^{(n-1)T}, \quad r=0,1,\dots,n-1 \quad (22)$$

and the vectors a_r and b_r where

$$\left. \begin{aligned} a_r &= \sum_{s=0}^{n-r} \phi_{s-1} I_{s+r} \\ b_r &= \sum_{s=0}^{n-r} \phi_{n-s-1} I_{s+r} \end{aligned} \right\} r=0,1,\dots,n \quad (23)$$

so that the general solution for $r \geq 1$ is

$$V_r = \sum_{s=0}^r \psi_{s-1} a_{r-s} - \sum_{s=1}^r \psi_{n-s} b_{r-s+1}. \quad (24)$$

The algorithm can be briefly summarized by the following steps:

- (1) Use the recursion equations (16) to define $\psi_r^{(n-1)}$ and $\Delta^{(n-1)}$.
- (2) Form the matrices ϕ_r by equation (22).
- (3) Form the vectors a_r and b_r by equation (23).
- (4) Form the voltage subvectors, V_r , by equation (24).

Using this algorithm, the number of multiplications and divisions required to invert $Y^{(n)}$ varies as $(n+1)^2 \cdot N_p^3$ with increasing n and N . This should be compared with a variation as $[(n+1) \cdot N_p]^3$ for a general elimination method and demonstrates a considerable improvement when n is large.

Since the computer program was taken from [5], no further description of it will be provided other than mentioning that there are numerous comment cards in LNSLV written using the same notation as the algorithm just described. For the subroutines MATMLT, TRMMLT, MULTTR, and MATVCA, comment cards which describe the matrix multiplication operation performed follow the subroutine statement cards.

In summary, the subroutine LNSLV(CE, V, YS, NP, NW) solves equation (1-15) for \vec{V} given $[Y^{wg} + y^{hs}]$ and \vec{I}^{imp} . The arguments of the subroutine statement card represent the following parameters: the first N elements of CE are elements of \vec{I}^{imp} , V is the output magnetic current coefficient column matrix, YS is the input matrix $[Y^{wg} + Y^{hs}]$ partitioned in terms of blocks of dimension $NP \times NP$ (only one row of blocks are required $[Y_0, Y_1, \dots, Y_n]$), NP is the smaller of the row or column dimensions for the array lattice, and NW uses the same definition as NP but replaces the word smaller with larger.

Minimum allocations are given by

COMPLEX A(NP*NP), B(NP*NP), C(NP*NP)

in subroutines MATMLT, TRMMLT, MULTTR, and MATVCA, and by

COMPLEX CE(N+NP*NW+1), PS(2*(NW+1)*NP*NP),

V(N), YS((NW+1)*NP*NP)

in subroutine LNSLV.

C LISTINGS OF THE SUBROUTINES MATMLT, TRMMLT, MULTTR,
C MATVCA, AND LNSLV

29

C SUBROUTINE MATMLT(A,B,C,NP)
C CALCULATES C=A*B
COMPLEX A(4),B(4),C(4),D
IJ=0
L=1
DO 10 I=1,NP
DO 11 J=1,NP
IJ=IJ+1
D=(0.,0.)
KJ=L
JK=J
DO 12 K=1,NP
D=D+A(JK)*B(KJ)
JK=JK+NP
KJ=KJ+1
12 CONTINUE
C(IJ)=D
11 CONTINUE
L=L+NP
10 CONTINUE
RETURN
END
SUBROUTINE TRMMLT(A,B,C,NP)
C CALCULATES C=-TRANSPOSE(A)*B
COMPLEX A(4),B(4),C(4),D
IJ=0
L=1
DO 10 I=1,NP
M=1
DO 11 J=1,NP
IJ=IJ+1
D=(0.,0.)
KI=M
KJ=L
DO 12 K=1,NP
D=D+A(KI)*B(KJ)
KI=KI+1
KJ=KJ+1
12 CONTINUE
M=M+NP
C(IJ)=C(IJ)-D
11 CONTINUE
L=L+NP
10 CONTINUE
RETURN
END
SUBROUTINE MULTTR(A,B,C,NP)
C CALCULATES C=A*TRANSPOSE(B)
COMPLEX A(4),B(4),C(4),D
IJ=0
DO 10 I=1,NP
DO 10 J=1,NP
IJ=IJ+1
D=(0.,0.)
IK=I
JK=J
DO 11 K=1,NP

```

D=D+A(JK)*B(IK)
IK=IK+NP
JK=JK+NP
11 CONTINUE
C(IJ)=D
10 CONTINUE
RETURN
END
SUBROUTINE MATVCA(A,B,C,N,N1)
C POSITIVE ACCUMULATION OF A*B IN C IF N1=1 OR NEGATIVE ACCUMULATION
C A*B IN C IF N1=2
COMPLEX A(4),B(4),C(4),D
DO 10 I=1,N
D=(0.,0.)
IJ=1
DO 11 J=1,N
D=D+A(IJ)*B(J)
IJ=IJ+N
11 CONTINUE
GO TO (12,13),N1
12 C(I)=C(I)+D
GO TO 10
13 C(I)=C(I)-D
10 CONTINUE
RETURN
END
SUBROUTINE LNSLV(CE,V,YS,np,nw)
COMPLEX CE(13),PS(32),V(6),YS(16)
DIMENSION IA(2)
100 FORMAT(//10X,'ILLEGAL CALL TO LNSLV -- NW =',I4)
101 FORMAT(//10X,'ILLEGAL CALL TO LNSLV -- NP =',I4)
IF(NW.LT.2) GO TO 10
IF(NP.LT.2) GO TO 11
C CALC DEL(-1) AND PS((0).0)
N=NW-1
NPW=NP*NW
N2=NP*NP
DO 12 I=1,N2
PS(I)=YS(I)
12 CONTINUE
CALL LINEQ(PS,np)
CALL MATMLT(PS,YS(N2+1),PS(N2+1),NP)
C IA(1) = START ADDRESS IN PS ARRAY OF PS((M-1),0)
C IA(2) = START ADDRESS IN PS ARRAY OF PS((M),0)
C IA(1)-N2 = START ADDRESS IN PS ARRAY OF DEL(M-2)
C IA(2)-N2 = START ADDRESS IN PS ARRAY OF DEL(M-1)
C IST+1=2*NW*N2+1 = START ADDRESS OF AN ADDITIONAL SCRATCH AREA
IA(1)=N2+1
IA(2)=NW*N2+N2+1
IST=2*NW*N2
MZ=N2+N2+1
MM=0
C ITERATE ON M=1,2,...,N. FOR M=N, ONLY CALC DEL(M-1).
DO 13 M=1,N
IO=IA(1)+MM
MM=MM+N2
II=IA(2)+MM
C IO IS START ADDRESS OF PS((M-1),M-1)
C II IS START ADDRESS OF PS((M),M)
C CALC DEL(M-1)

```

```

CALL MATMLT(PS(I0),PS(I0),PS(IST+1),NP)
IJ=IST
DO 14 I=1,NP
DO 14 J=1,NP
IJ=IJ+1
PS(IJ)=-PS(IJ)
IF(I.EQ.J) PS(IJ)=PS(IJ)+1.
14 CONTINUE
CALL LINEQ(PS(IST+1),NP)
ID=IA(1)-N2
IDI=IA(2)-N2
CALL MATMLT(PS(IST+1),PS(ID),PS(ID1),NP)
IF(M.EQ.N) GO TO 15
C CALC PS((M),M)
MZZ=MZ
MS=IA(1)
IJ=IST
DO 16 I=1,N2
IJ=IJ+1
PS(IJ)=YS(MZZ)
MZZ=MZZ+1
16 CONTINUE
MZZ=MZ-N2
DO 17 IS=1,M
CALL TRMMLT(PS(MS),YS(MZZ),PS(IST+1),NP)
MS=MS+N2
MZZ=MZZ-N2
17 CONTINUE
MZ=MZ+N2
CALL MATMLT(PS(ID1),PS(IST+1),PS(I1),NP)
C CALCULATE PS((M),R) FOR R=0,1,...,M-1. (IR=R)
IOR=IA(1)
I1R=IA(2)
IMR=I0
DO 18 IR=1,M
CALL MATMLT(PS(IMR),PS(I1),PS(IST+1),NP)
IMR=IMR-N2
IJ=IST
DO 18 I=1,N2
PS(I1R)=PS(IOR)-PS(IJ+1)
IJ=IJ+1
I1R=I1R+1
IOR=IOR+1
18 CONTINUE
I=IA(1)
IA(1)=IA(2)
IA(2)=I
13 CONTINUE
C HAVE FINISHED ITERATION ON PS. NOW PUT PHI(R) INTO PS(IA(2))
15 IPHI=IA(2)-N2
IPSI=IA(1)
IOR=IA(1)
I1R=IA(2)
DO 19 I=1,N
CALL MULTTR(PS(IPHI),PS(IOR),PS(I1R),NP)
IOR=IOR+N2
I1R=I1R+N2
19 CONTINUE
C PUT PHI(-1) IN PS(IPHI)
J=IPHI

```

```

DO 20 I=1,N2
PS(J)=-PS(J)
J=J+1
20 CONTINUE
C   NOW HAVE PHI(S),S=-1,0,1,... N-1 STARTING AT PS(IPHI)
C   AND      PSI(S),S= 0,1,2,... N-1 STARTING AT PS(IPSI)
IB=NW*NP+1
IC=1
J=2*NW*NP
DO 21 I=1,J
YS(I)=(0..0.)
21 CONTINUE
IV=1
DO 22 J=1,NW
NR=NW-J+1
I1S=IPHI
I2S=IPHI+N*N2
IVS=IV
DO 23 I=1,NR
CALL MATVCA(PS(I1S),CE(IVS),YS(IC),NP,1)
CALL MATVCA(PS(I2S),CE(IVS),YS(IB),NP,1)
I1S=I1S+N2
I2S=I2S-N2
IVS=IVS+NP
23 CONTINUE
IB=IB+NP
IC=IC+NP
IV=IV+NP
22 CONTINUE
C   NOW CALCULATE V IN I LOCATIONS
J=NW*NP
DO 24 I=1,J
CE(I)=-YS(I)
24 CONTINUE
IV=NP+1
IB=IV+J
IC=1
DO 25 IR=1,N
I1S=IPSI
I2S=(N-1)*N2+IPSI
IBS=IB
ICS=IC
DO 26 IS=1,IR
CALL MATVCA(PS(I1S),YS(ICS),CE(IV),NP,1)
CALL MATVCA(PS(I2S),YS(IBS),CE(IV),NP,2)
I1S=I1S+N2
I2S=I2S-N2
IBS=IBS-NP
ICS=ICS-NP
26 CONTINUE
IB=IB+NP
IC=IC+NP
IV=IV+NP
25 CONTINUE
DO 27 I=1,NPW
V(I)=CE(I)
27 CONTINUE
RETURN
10 WRITE(3,100) NW
RETURN
11 WRITE(3,101) NP
RETURN
END

```

IX. DESCRIPTION OF THE SUBROUTINES LINEQ, DECOMP, AND SOLVE

The subroutine LINEQ(C,LL) is used in subroutine LINSLV to invert a complex matrix. The input to LINEQ consists of a square complex matrix of order $LL \times LL$ stored columnwise in C and the dimension variable LL. The output from LINEQ is C^{-1} stored columnwise in C.

Minimum allocations are given by

```
COMPLEX C(LL*LL)
DIMENSION LR(LL).
```

The subroutines DECOMP(N,IPS,UL) and SOLVE(N,IPS,UL,B,X) are called from the main program to solve the matrix equation

$$[Y^{wg} + Y^{hs}] \vec{V} = \vec{I}^{imp} \quad (1-15)$$

when the array lattice is isosceles triangular. This subroutine combination uses the method of Gaussian elimination and LU decomposition described in [6, Section 9]. The input to DECOMP consists of N and the N by N matrix of coefficients $[Y^{wg} + Y^{hs}]$ which is stored by columns in UL. The output from DECOMP is IPS and UL. The output is fed into SOLVE. The rest of the input to SOLVE consists of N and the column of coefficients \vec{I}^{imp} stored in B. Solve puts the solution \vec{V} to the matrix equation in X.

Minimum allocations are given by

```
COMPLEX UL(N*N)
DIMENSION SCL(N), IPS(N)
```

in subroutine DECOMP, and by

```
COMPLEX UL(N*N), B(N), X(N)
DIMENSION IPS(N)
```

in subroutine SOLVE.

DECOMP and SOLVE require roughly $N^3/3$ multiplications and divisions to solve a system of N linear equations whereas using LINEQ in a method which requires an inverse needs roughly $N^3 + N^2$ multiplications and divisions to solve the same system of equations.

```
SUBROUTINE LINEQ(C,LL)
COMPLEX C(4),STOR,STO,ST,S
DIMENSION LR(2)
DO 10 I=1,LL
LR(I)=I
10 CONTINUE
M1=0
DO 11 M=1,LL
K=M
K2=M1+K
S1=ABS(REAL(C(K2)))+ABS(AIMAG(C(K2)))
DO 12 I=M,LL
K1=M1+I
S2=ABS(REAL(C(K1)))+ABS(AIMAG(C(K1)))
IF(S2-S1) 12,12,13
13 K=I
S1=S2
12 CONTINUE
LS=LR(M)
LR(M)=LR(K)
LR(K)=LS
K2=M1+K
STOR=C(K2)
J1=0
DO 14 J=1,LL
K1=J1+K
K2=J1+M
STO=C(K1)
C(K1)=C(K2)
C(K2)=STO/STOR
J1=J1+LL
14 CONTINUE
K1=M1+M
C(K1)=1./STOR
DO 15 I=1,LL
IF(I-M) 16,15,16
16 K1=M1+I
ST=C(K1)
C(K1)=0.
J1=0
DO 17 J=1,LL
K1=J1+I
K2=J1+M
C(K1)=C(K1)-C(K2)*ST
J1=J1+LL
17 CONTINUE
15 CONTINUE
M1=M1+LL
11 CONTINUE
J1=0
DO 18 J=1,LL
IF(J-LR(J)) 19,20,19
19 L RJ=LR(J)
J2=(L RJ-1)*LL
DO 21 I=1,LL
K2=J2+I
K1=J1+I
S=C(K2)
```

```

C(K2)=C(K1)
C(K1)=S
21 CONTINUE
  LR(J)=LR(LRJ)
  LR(LRJ)=LRJ
  IF(J-LR(J)) 19,20,19
20 J1=J1+LL
18 CONTINUE
  RETURN
END
SUBROUTINE DECOMP(N,IPS,UL)
COMPLEX UL(36),PIVOT,EM
DIMENSION SCL(6),IPS(6)
DO 5 I=1,N
  IPS(I)=I
  RN=0.
  J1=I
  DO 2 J=1,N
    ULM=ABS(REAL(UL(J1)))+ABS(AIMAG(UL(J1)))
    JI=J1+N
    IF(RN-ULM) 1,2,2
1  RN=ULM
2  CONTINUE
  SCL(I)=1./RN
5  CONTINUE
  NM1=N-1
  K2=0
  DO 17 K=1,NM1
    BIG=0.
    DO 11 I=K,N
      IP=IPS(I)
      IPK=IP+K2
      SIZE=(ABS(REAL(UL(IPK)))+ABS(AIMAG(UL(IPK))))*SCL(IP)
      IF(SIZE-BIG) 11,11,10
10  BIG=SIZE
    IPV=I
11  CONTINUE
    IF(IPV-K) 14,15,14
14  J=IPS(K)
    IPS(K)=IPS(IPV)
    IPS(IPV)=J
15  KPP=IPS(K)+K2
    PIVOT=UL(KPP)
    KP1=K+1
    DO 16 I=KP1,N
      KP=KPP
      IP=IPS(I)+K2
      EM=-UL(IP)/PIVOT
18  UL(IP)=-EM
    DO 16 J=KP1,N
      IP=IP+N
      KP=KP+N
      UL(IP)=UL(IP)+EM*UL(KP)
16  CONTINUE
    K2=K2+N
17  CONTINUE
  RETURN
END
SUBROUTINE SOLVE(N,IPS,UL,B,X)
COMPLEX UL(36),B(6),X(6),SUM

```

```
DIMENSION IPS(6)
NP1=N+1
IP=IPS(1)
X(1)=B(IP)
DO 2 I=2,N
IP=IPS(I)
IPB=IP
IM1=I-1
SUM=0.
DO 1 J=1,IM1
SUM=SUM+UL(IP)*X(J)
1 IP=IP+N
2 X(I)=B(IPB)-SUM
K2=N*(N-1)
IP=IPS(N)+K2
X(N)=X(N)/UL(IP)
DO 4 IBACK=2,N
I=NP1-IBACK
K2=K2-N
IPI=IPS(I)+K2
IP1=I+1
SUM=0.
IP=IPI
DO 3 J=IP1,N
IP=IP+N
3 SUM=SUM+UL(IP)*X(J)
4 X(I)=(X(I)-SUM)/UL(IPI)
RETURN
END
```

X. DESCRIPTION OF THE SUBROUTINE TOPGEN

The subroutine TOPGEN(N, NP, NT, NW, X, Y, T, T1, KR) generates a complete matrix T given one column T1.

Minimum allocations are given by

```
COMPLEX T(N*N), T1(N), T2(N,N)
DIMENSION D(6), X(6), Y(6)
```

The variables in the argument of TOPGEN are defined as follows: N is the dimension of the square matrix T, N_p is the shortest row or column dimension of the array lattice, NT specifies the array lattice type-1 for rectangular and 2 for isosceles triangular, NW is the largest row or column dimension of the array lattice, X(I) and Y(I) are the center coordinates of the Ith aperture and T is the output matrix which is generated from one column T1 of T. KR is a parameter which determines whether or not D(I) is calculated $(D(I) = (X_1 - X_I)^2 + (Y_1 - Y_I)^2)$. If KR = 1, D(I) is evaluated whereas if KR = 2, this step is skipped (D(I) has been determined already by a previous call to TOPGEN).

DO loops 11, 12, 13, and 14 generate [T] given $\overline{T1}$ for a uniformly spaced rectangular array lattice while DO loops 16, 17, 18, 19, 21, and 22 does the same for a uniformly spaced isosceles triangular array lattice. For the rectangular array lattice, [T] which is symmetric block-Toeplitz is determined by forming one column of blocks and generating the rest of [T] using the Toeplitz property. For the isosceles triangular array lattice, the elements T_{ij} below the diagonal of [T] (excluding the elements of the first column which are given (T1)) are determined by comparing the distance squared between the centers of the apertures i and j, $D1$ ($D1$ of $T_{ij} = (x_j - x_i)^2 + (y_j - y_i)^2$), to the distance values associated with the elements of the first column, D (D of $T_{i1} = (x_1 - x_i)^2 + (y_1 - y_i)^2$). When $D1 = D$, the value used for T_{ij} which has an associated $D1$ value is the same as the corresponding element of the first column with an associated D value. The elements above the diagonal are determined from symmetry, $y_{ij} = y_{ji}$ (consequence of Galerkin's method).

```

SUBROUTINE TOPGEN(N,NP,NT,NW,X,Y,T,T1,KR)
COMPLEX T(36),T1(6),T2(6,6)
DIMENSION D(6),X(6),Y(6)
NPW=NP*NW
NPWP=NPW*NP
N1=N-1
IF(NT.EQ.2) GO TO 10
DO 11 I=1,NW
L1=1
DO 12 J=1,NP
DO 12 K=1,NP
L=1+IAbs(K-J)+NP*(I-1)
T2(I,L1)=T1(L)
L1=L1+1
12 CONTINUE
11 CONTINUE
DO 13 I=1,NW
DO 13 II=1,NW
IF(I.EQ.1) II=II
IF(I.GT.1) II=I-II+1
IF((I.GT.1).AND.(II.LE.0)) II=II-I+1
I2=1
DO 14 J=1,NP
DO 14 K=1,NP
L1=(I-1)*NPWP+(II-1)*NP+(J-1)*NPW+K
T(L1)=T2(II,I2)
I2=I2+1
14 CONTINUE
13 CONTINUE
RETURN
10 IF(KR.EQ.2) GO TO 15
DO 16 I=1,N
D(I)=(X(I)-X(1))*(X(I)-X(1))+(Y(I)-Y(1))*(Y(I)-Y(1))
16 CONTINUE
15 II=1
K1=1
DO 17 I=1,N1
DO 18 J=II,N
D1=(X(J)-X(I))*(X(J)-X(I))+(Y(J)-Y(I))*(Y(J)-Y(I))
DO 19 K=1,N
IF(ABS(D1-D(K)).LT.0.01) T(K1)=T1(K)
IF(ABS(D1-D(K)).LT.0.01) GO TO 20
19 CONTINUE
20 K1=K1+1
18 CONTINUE
IF(I.EQ.1) II=II+1
II=II+1
K1=K1+II-1
17 CONTINUE
J2=0
DO 21 J=1,N
J1=J
DO 22 I=1,J
J3=J2+I
IF(I-J) 23,24,23
24 T(J1)=T1(1)
GO TO 22
23 T(J3)=T(J1)
J1=J1+N
22 CONTINUE
J2=J2+N
21 CONTINUE
RETURN
END

```

XI. DESCRIPTION OF THE MAIN PROGRAM WITH SAMPLE INPUT-OUTPUT DATA

The main program computes the x,y coordinates of the centers of the apertures in the array, the complex coefficients v_i which determine the magnetic currents M^i according to (1-6) and the scattering coefficients S_{ij} according to (1-103) and (1-104). The main program calls the subroutines AY, YHSP, TOPGEN, CSMTZ, DECOMP, SOLVE, and LNSLV.

The data cards are read into the main program according to

```

READ (1,100) N, AL, ALL, BL, BL1, ER, LM, LN
100 FORMAT (I4, 5F7.4, 2I3)
      READ (1,102) NC, NR, NT, NE, DX, DY, DT
102 FORMAT (4I4, 3F7.4).

```

The variables AL, ALL, BL, and BL1 are respectively a/λ , a'/λ , b/λ , and b'/λ where λ is the free space wavelength. ER is the relative dielectric constant ϵ_r of (1-34) and (1-35) inside the waveguide. The variables LM and LN are respectively the total number of m and n modes used in determining A_{ik}^{TE} (1-30) and A_{ik}^{TM} (1-31) (only odd m starting with m=1 and even n starting with n=0 (TE) or n=2 (TM) are considered due to the $\sin \frac{m\pi}{2} \cos \frac{n\pi}{2}$ factor appearing in (1-33)). LM which represents the contribution of the mth waveguide mode to Y^{wg} should be chosen so that the contribution of the $(1/(m^2/a^2 - 1/a'^2)) \cos(m\pi a'/2a)$ factor in (1-33) results in very small A_{ik}^{TE} and A_{ik}^{TM} values. LN which represents the contribution of the nth mode to Y^{wg} should be chosen so that the argument $n\pi b'/2b$ of the $\sin(\)/()$ factor in (1-33) is greater than π . NC is the number of columns of apertures measured in the x direction. NR is the number of rows of apertures measured in the y direction. NT specifies the array lattice type, 1 for rectangular and 2 for isosceles triangular. NE is the driven aperture number. DX is the distance per unit wavelength between the closest outer waveguide edges in the x direction while DY is the same but in the y direction (see Fig. 1-1). DT is the waveguide wall thickness per unit wavelength.

Minimum allocations are given by

```
COMPLEX CE(N+NP*NW+1), S(N*N), S3(N),
V(N), YO(2*LM*LN+LM), YS(N*N),
YS1((NW+1)*NP*NP), YSP(N)
DIMENSION A(2*LM*LN), IPS(N), X(N), Y(N)
```

in the main program, by

```
COMPLEX Y(2*LM*LN + LM)
DIMENSION A(2*LM*LN), F(LM), STE(LN), STM(LN)
```

in the subroutine AY, by

```
COMPLEX YSP(N)
DIMENSION X(N), Y(N)
```

in the subroutine YHSP, by

```
COMPLEX T(N*N), T1(N), T2(N,N)
DIMENSION D(N), X(N), Y(N)
```

in the subroutine TOPGEN, by

```
COMPLEX A(N), B(N), E(N), ES(N-1), X(N)
```

in the subroutine CSMTZ, by

```
COMPLEX UL(N*N)
DIMENSION SCL(N), IPS(N)
```

in the subroutine DECOMP, by

```
COMPLEX UL(N*N), B(N), X(N)
DIMENSION IPS(N)
```

in the subroutine SOLVE, and by

```
COMPLEX CE(N+NP*NW+1), PS(2*(NW+1)*NP*NP),
V(N), YS((NW+1)*NP*NP)
```

in the subroutine LINSLV where NP is the smaller of the number of rows or columns of apertures for the rectangular array lattice while NW uses the same definition but replaces the word smaller by larger.

DO loop 11 calculates the x and y coordinates of the centers of the apertures if the array has a rectangular lattice while DO loop 15 does the same if the lattice is isosceles triangular. Referring to equations (1-30) to (1-35), statement 40 stores

A_k^{TE} in $A(k = (m+1)/2 + n/2 * LM)$

Y_k^{TE} in $Y0(k = (m+1)/2 + n/2 * LM)$

$m = 1, 3, 5, \dots, LM$

$n = 0, 2, 4, \dots, LN$

A_k^{TM} in $A(k = LM*LN + (m+1)/2 + (n-2)/2 * LM)$

$Y_k^{TM} = Y0(k = LM*LN + (m+1)/2 + (n-2)/2 * LM)$

$m = 1, 3, 5, \dots, LM$

$n = 2, 4, 6, \dots, LN .$

Note that only odd m and even n modes are calculated and that the first subscript of A_{ik}^{TE} and A_{ik}^{TM} in (1-30) and (1-31) has been dropped since the same expansion function is used in every waveguide region -

$A_{1k} = A_{2k} = \dots = A_{Nk} = A_k$. DO loop 18 calculates Y^{wg} . Statement 41 stores the first column of Y^{hs} in YSP. Statement 42 generates the complete Y^{hs} matrix given the first column and stores it in YS by columns. DO loop 19 and statement 43 generate \vec{I}^{imp} defined by (1-106) and (1-107) and store it in CE.

If the array is linear, DO loop 21 is used to calculate $[Y^{wg} + Y^{hs}]$ and statement 44 calculates the coefficient vector \vec{V} defined by (1-15) and stores it in V.

If the array contains at least two rows and columns and has a rectangular lattice, statement 20 and DO loops 24, 25 calculate the symmetric submatrix blocks of $[Y^{wg} + Y^{hs}]$ given $[Y^{wg}]$ and a column of $[Y^{hs}]$. If the array contains at least two rows and columns and has an isosceles triangular lattice, DO loop 27 calculates $[Y^{wg} + Y^{hs}]$ given $[Y^{wg}]$ and $[Y^{hs}]$. Once $[Y^{wg} + Y^{hs}]$ has been determined for these two cases, statement 26 stores \vec{V} in V for the rectangular array while statements 45 and 46 store \vec{V} in V for the isosceles triangular array.

DO loop 31 calculates one column of the scattering matrix defined by (1-103) and (1-104) and stores it in S3. Statement 47 generates the complete scattering matrix [S] given the first column and stores it in S.

The following is a listing of the main program with sample input-output data. Figure 2 shows the coupled power ($20 \log |S_{i1}|$) and phase of S_{i1} ($i = 2, 6$) between a driven element and the rest of the elements for the 2×3 waveguide-fed rectangular aperture array example used in the sample input-output data.

```

C      LISTING OF THE MAIN PROGRAM AND SAMPLE DATA
C
//XXXX WATFIV  (XXXX,XX,1,2), "XXXX",REGION=250K
$JOB      XXXX,TIME=1,PAGES=30
C
C      MAIN PROGRAM
C      THIS PROGRAM CALLS THE SUBROUTINES AY,YHSP,TOGEN,CSMTZ,
C      DECOMP,SOLVE, AND LNSLV
COMPLEX CE(13),G3,G5,G7,G9,S(36),S3(6),U,V(6)
COMPLEX Y0(55),YS(36),YS1(16),YSP(6),YWG
DIMENSION A(50),IPS(6),X(6),Y(6)
COMMON AL1,BL1,PI,PI2,PI3,U/R1/ETA
COMMON /R3/G1,G2,G3,G4,G5,G6,G7,G8,G9,G10,G11
COMMON /R5/AL,BL/R6/ER,LN,LN,NTS
100 FORMAT(I4,5F7.4,2I3)
101 FORMAT(/5X,"N",5X,"AL",5X,"AL1",4X,"BL",5X,"BL1",4X,"ER",5X,"LN",
13X,"LN"/2X,I4,2X,5F7.4,2X,I3,2X,I3)
102 FORMAT(4I4,3F7.4)
103 FORMAT(/4X,"NC",5X,"NR",5X,"NT",5X,"NE",5X,"DX",5X,"DY",5X,"DT",
12X,I4,3X,I4,3X,I4,3X,I4,2X,3F7.4)
104 FORMAT(/4X,"X"/(2X,5E14.7))
105 FORMAT(/4X,"Y"/(2X,5E14.7))
106 FORMAT(/4X,"Y-WG"/2X,2E14.7)
107 FORMAT(/4X,"Y-HALF SPACE"/(2X,5E14.7))
108 FORMAT(/4X,"V -- UNKNOWN VECTOR"/(2X,5E14.7))
109 FORMAT(/4X,"S -- SCATTERING MATRIX"/(2X,5E14.7))
READ(1,100) N,AL,AL1,BL,BL1,ER,LN,LN
WRITE(3,101) N,AL,AL1,BL,BL1,ER,LN,LN
READ(1,102) NC,NR,NT,NE,DX,DY,DT
WRITE(3,103) NC,NR,NT,NE,DX,DY,DT
PI=3.141593
PI2=2.*PI
PI3=PI/2.
ETA=376.730
U=(0..1.)
N1=N+1
N2=LN*LN+1
NN=N*N
AL2=AL/2.+DT
BL2=BL/2.+DT
DX2=DX/2.

```

```

NP=AMIN0(NC,NR)
NW=AMAX0(NC,NR)
NTS=2*LM*LN
NP2=NP*NP
G1=AL1/PI
G2=AL1/PI2
G3=-U*G2
G4=G1*G1
G5=-U*G4
G6=G1*G2
G7=-U*G6
G8=G1*G4
G9=-U*G8
G10=(1.-0.25/(AL1*AL1))
G11=(1.+0.25/(AL1*AL1))*G1
S1=DX+2.*DT+AL
S2=DY+2.*DT+BL
IF(NT.EQ.2) GO TO 10
K=1
DO 11 I=1,NW
DO 11 J=1,NP
IF(NC.GT.NR) GO TO 12
X(K)=AL2+(J-1)*S1
Y(K)=BL2+(I-1)*S2
GO TO 13
12 X(K)=AL2+(I-1)*S1
Y(K)=BL2+(J-1)*S2
13 K=K+1
11 CONTINUE
GO TO 14
10 K=1
DO 15 I=1,NR
K1=2-(I-2*(I/2))
DO 15 J=1,NC
X(K)=(1+K1/2)*AL2+(J-1)*S1+K1/2*DX2
Y(K)=BL2+(I-1)*S2
K=K+1
15 CONTINUE
14 WRITE(3,104) (X(I),I=1,N)
WRITE(3,105) (Y(I),I=1,N)
40 CALL AY(A,Y0)
YWG=(0.,0.)
K=1
DO 18 I=1,NTS
IF(I.EQ.N2) K=K+LM
YWG=YWG+A(I)*Y0(K)*A(I)
K=K+1
18 CONTINUE
WRITE(3,106) YWG
41 CALL YHSP(N,X,Y,YSP)
KR=1
42 CALL TOPGEN(N,NP,NT,NW,X,Y,YS,YSP,KR)
WRITE(3,107) (YS(I),I=1,NN)
DO 19 I=1,N
CE(I)=(0.,0.)
19 CONTINUE
43 CE(NE)=2.*Y0(1)*A(1)
IF((NC.GE.2).AND.(NR.GE.2)) GO TO 20
YSP(1)=YSP(1)+YWG

```

```

DO 21 I=1,N
CE(I)=CE(I)/YSP(I)
IF(I.EQ.1) GO TO 21
YSP(I)=YSP(I)/YSP(1)
21 CONTINUE
44 CALL CSMTZ(N,YSP,CE,V)
GO TO 22
20 YSP(I)=YSP(I)+YWG
IF(NT.EQ.2) GO TO 23
DO 24 I=1,NW
DO 25 J=1,NP
DO 25 K=1,NP
L=(I-1)*NP2+(J-1)*NP+K
L1=(I-1)*NP+IABS(K-J)+1
YS1(L)=YSP(L1)
25 CONTINUE
24 CONTINUE
26 CALL LINSLV(CE,V,YS1,NP,NW)
GO TO 22
23 J=-N
DO 27 I=1,N
J=J+NI
YS(J)=YS(J)+YWG
27 CONTINUE
45 CALL DECOMP(N,IPS,YS)
46 CALL SOLVE(N,IPS,YS,CE,V)
22 WRITE(3,108) (V(I),I=1,N)
DO 31 I=1,N
S3(I)=V(I)*A(I)
IF(I.EQ.NE) S3(I)=S3(I)-1.
31 CONTINUE
KR=2
47 CALL TOPGEN(N,np,NT,NW,X,Y,S,S3,KR)
WRITE(3,109) (S(K),K=1,NN)
STOP
END
$DATA
 6 1.0000 0.6500 0.4761 0.3095 1.0000 5 5
 3 2   1   1 0.9000 0.2000 0.0515
$STOP
//


PRINTED OUTPUT
      N      AL      AL1      BL      BL1      ER      LM      LN
      6      1.0000  0.6500  0.4761  0.3095  1.0000      5      5

      NC      NR      NT      NE      DX      DY      DT
      3        2        1        1  0.9000  0.2000  0.0515

      X
0.5515000E+00 0.5515000E+00 0.2554499E+01 0.2554499E+01 0.4557498E+01
0.4557498E+01

      Y
0.2895499E+00 0.1068649E+01 0.2895499E+00 0.1068649E+01 0.2895499E+00
0.1068649E+01

      Y-WG
0.1289030E-02-0.8829894E-04

```

Y-HALF SPACE

0.1375110E-02 0.6628551E-03-0.3466108E-03 0.1446004E-03-0.1527445E-04
 -0.2117092E-05 0.8159508E-06 0.1840072E-04-0.3747291E-05-0.1479488E-06
 -0.2525312E-05 0.3105473E-05-0.3466108E-03 0.1446004E-03 0.1375110E-02
 0.6628551E-03 0.8159508E-06 0.1840072E-04-0.1527445E-04-0.2117092E-05
 -0.2525312E-05 0.3105473E-05-0.3747291E-05-0.1479488E-06-0.1527445E-04
 -0.2117092E-05 0.8159508E-06 0.1840072E-04 0.1375110E-02 0.6628551E-03
 -0.3466108E-03 0.1446004E-03-0.1527445E-04-0.2117092E-05 0.8159508E-06
 0.1840072E-04 0.8159508E-06 0.1840072E-04-0.1527445E-04-0.2117092E-05
 -0.3466108E-03 0.1446004E-03 0.1375110E-02 0.6628551E-03 0.8159508E-06
 0.1840072E-04-0.1527445E-04-0.2117092E-05-0.3747291E-05-0.1479488E-06
 -0.2525312E-05 0.3105473E-05-0.1527445E-04-0.2117092E-05 0.8159508E-06
 0.1840072E-04 0.1375110E-02 0.6628551E-03-0.3466108E-03 0.1446004E-03
 -0.2525312E-05 0.3105473E-05-0.3747291E-05-0.1479488E-06 0.8159508E-06
 0.1840072E-04-0.1527445E-04-0.2117092E-05-0.3466108E-03 0.1446004E-03
 0.1375110E-02 0.6628551E-03

V -- UNKNOWN VECTOR

-0.1237808E+01 0.2902574E+00-0.1171501E+00 0.1303046E+00-0.4720550E-02
 0.3497620E-02 0.3164612E-02 0.9165186E-02-0.1368488E-02 0.1222063E-02
 -0.5777453E-03 0.2339229E-02

S -- SCATTERING MATRIX

-0.7309630E-01-0.2173524E+00 0.8772510E-01-0.9757555E-01 0.3534873E-02
 -0.2619111E-02-0.2369745E-02-0.6863132E-02 0.1024760E-02-0.9151131E-03
 0.4326310E-03-0.1751676E-02 0.8772510E-01-0.9757555E-01-0.7309630E-01
 -0.2173524E+00-0.2369745E-02-0.6863132E-02 0.3534873E-02-0.2619111E-02
 0.4326310E-03-0.1751676E-02 0.1024760E-02-0.9151131E-03 0.3534873E-02
 -0.2619111E-02-0.2369745E-02-0.6863132E-02-0.7309630E-01-0.2173524E+00
 0.8772510E-01-0.9757555E-01 0.3534873E-02-0.2619111E-02-0.2369745E-02
 -0.6863132E-02-0.2369745E-02-0.6863132E-02 0.3534873E-02-0.2619111E-02
 0.8772510E-01-0.9757555E-01-0.7309630E-01-0.2173524E+00-0.2369745E-02
 -0.6863132E-02 0.3534873E-02-0.2619111E-02 0.1024760E-02-0.9151131E-03
 0.4326310E-03-0.1751676E-02 0.3534873E-02-0.2619111E-02-0.2369745E-02
 -0.6863132E-02-0.7309630E-01-0.2173524E+00 0.8772510E-01-0.9757555E-01
 0.4326310E-03-0.1751676E-02 0.1024760E-02-0.9151131E-03-0.2369745E-02
 -0.6863132E-02 0.3534873E-02-0.2619111E-02 0.8772510E-01-0.9757555E-01
 -0.7309630E-01-0.2173524E+00

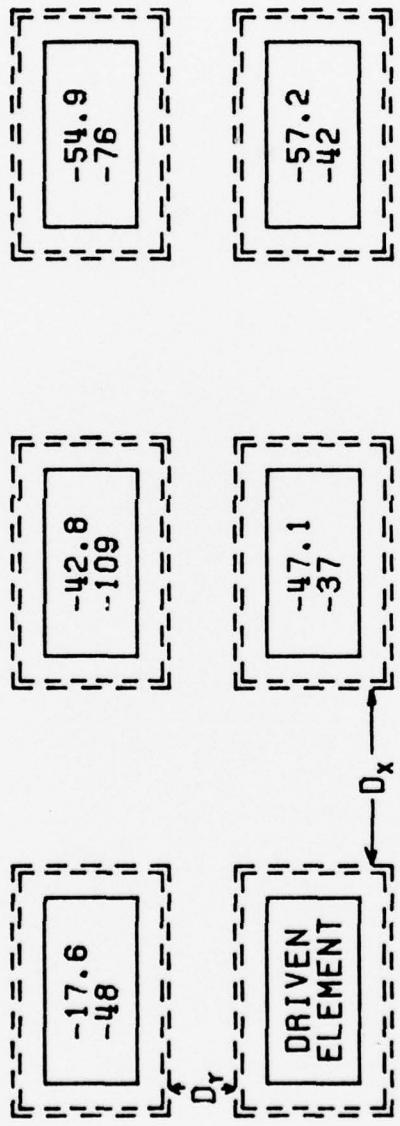


Fig. 2. The coupled power ($20 \log |S_{i1}|$) and phase of S_{i1} ($i = 2, 6$) for a 6 element waveguide-fed aperture array with a rectangular lattice where $a/\lambda = 1.0000$, $a'/\lambda = 0.6500$, $b/\lambda = 0.4761$, $b'/\lambda = 0.3095$, $D_x/\lambda = 0.9000$, $D_y/\lambda = 0.2000$ and $D_t/\lambda = 0.0515$. The upper number in each aperture represents coupled power in dB while the lower number represents the phase of S_{i1} in degrees.

REFERENCES

- [1] J. Luzwick and R. F. Harrington, "Mutual Coupling in a Finite Planar Rectangular Waveguide Antenna Array," Tech. Rept. No. 7, Contract No. N00014-76-C-0225, Office of Naval Research, June 1978.
- [2] V. I. Krylov, Approximate Calculation of Integrals, translated by A. H. Stroud, Macmillan Co., New York, 1962.
- [3] Shalhav Zohar, "Toeplitz Matrix Inversion: The Algorithm of W. F. Trench," J. Assoc. Comp. Mach., vol. 16, No. 4, October 1969, pp. 592-601.
- [4] Shalhav Zohar, "The Solution of a Toeplitz Set of Linear Equations," J. Assoc. Comp. Mach., vol. 21, No. 2, April 1974, pp. 272-276.
- [5] D. H. Sinnott, "An Improved Algorithm for Matrix Analysis of Linear Antenna Arrays," WRE-Technical Note - 1066 (AP), Weapons Research Establishment, Dept. of Defense, Salisbury, South Australia.
- [6] G. E. Forsythe and C. B. Moler, Computer Solution of Linear Algebraic Systems, Prentice-Hall, Inc., Englewood Cliffs, New Jersey, 1967, Section 9.

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