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EFFECT OF APERTURE ILLUMINATION ON THE ON-AXIS POWER DENSITY OF A CIRCULAR MICROWAVE ANTENNA

by

T. R. LaSalle Weapons Development and Evaluation Laboratory



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ABSTRACT

This report describes the development of two methods of determining the on-axis microwave power density in both the Fresnel and Fraunhofer regions, for circular-aperture antennas with any arbitrary, axially symmetric aperture illumination. Both methods have been programmed for digital computation. These methods are described and are applied to a number of different aperture distributions which could conceivably occur in practice. The resultant on-axis fields are compared and some conclusions relating the aperture distribution and the resulting on-axis fields are made.

ACKNOWLEDGEMENTS

The author wishes to express gratitude to Mr. H. S. Overman, whose suggestions and guidance were essential to this project. Mr. Overman suggested the project be undertaken, proposed the use of the superposition method and assisted in the derivation of the equations.

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FOREWORD

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This report was reviewed by the following persons of the Weapons Development and Evaluation Laboratory:

- R. C. WHITAKER, Missile Safety Staff Engineer
- H. S. OVERMAN, Assistant Director, Technical Applications
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APPROVED FOR RELEASE:

/s/ R. H. LYDDANE Technical Director

INTRODUCTION

The microwave fields associated with the high power radar systems of today, and the even higher power radars expected in the future, present definite hazards to personnel, ordnance and fuels unless appropriate safety precautions are incorporated. It is, therefore, necessary to determine which regions of the various radar fields exceed established safe working levels of power density. The hazardous areas should preferably be examined through actual measurements with the radar in operation. However, such measurements are time consuming, costly and susceptible to many variables. It thus becomes essential that an accurate and reliable method of computing the theoretical power density on the axis of the beam be available both to facilitate optimum test planning and to aid in interpretation of experimental results.

In general, resort to a highly sophisticated theoretical approach is not necessary in order to estimate the maximum values of power density which may be encountered along the beam axis, which is the usual requirement when safety measures are the primary consideration. For such purposes, it is permissible to base calculations on the simplifying assumption that the antenna aperture is uniformly illuminated by the feed. This assumption yields calculated values of power density in the Fraunhofer (far) field which are at least as high as produced by any other distribution of the aperture field, hence the error introduced, if any, is on the side of safety throughout the far field. Moreover, this assumption results in predicted values of the power density maxima in the Fresnel field which, except for a few unusual cases, are not significantly lower than those based on other distributions. For these reasons, the calculation of "safe" distances for circular microwave antennas in connection with personnel hazards studies at the Naval Weapons Laboratory has been based on the assumption of a uniformly illuminated aperture. Under this assumption, far field computations are reduced to a straightforward application of the inverse square law, and the prediction of maximum hazards in the Fresnel region is made possible through formulas which approximate the upper envelope of the power density contour in this region. References (a) and (b) describe these methods in detail.

While methods based on uniform illumination are useful for establishing safe distances and other cases when only the Fresnel field maxima are of interest, they are not sufficient for a comprehensive evaluation of measurements obtained in the Fresnel field of

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non-uniformly illuminated antennas since instrumentation might be located at points of minimum or intermediate intensity. While uniform illumination theoretically gives maximum antenna gain, practical antenna design usually necessitates reduction of the power at the aperture edge to decrease the loss from "spill-over" and decrease the power in the sidelobes. Thus the aperture amplitude distribution in practical antennas is usually designed so that the power is concentrated at the aperture center and is tapered to lower values at the edge.

The effect of these tapered illuminations on the axial field has been calculated by other investigators for a few distributions expressible as analytic mathematical functions. Not all distributions of interest can be adequately approximated by simple functions, however. Even for those distributions which can be so expressed, the manual solution of the Fresnel equation for a sufficient number of points is time-consuming and difficult. It was thus desirable to develop a method by which the axial field could be conveniently calculated by computer for any arbitrary aperture distribution. Two somewhat similar methods, each having certain advantages, have been developed to fulfill this requirement. This report describes these methods and their application to the common distributions generally used to approximate the aperture illumination of practical antennas. The methods have also been applied to a number of arbitrary distributions for which the on-axis field could not readily be calculated by the usual means.

THEORY

Consider the antenna aperture of Figure 1. The scalar diffraction field at any point P located at a distance R along the axis of a circular aperture of constant phase is given by the Fresnel approximation equation, (Reference (b), Page 198).

$$\mathbf{U}_{p} = \mathbf{j} \frac{\mathbf{e}^{-\mathbf{j}\mathbf{k}\mathbf{R}}}{\lambda\mathbf{R}} \int_{0}^{2\pi} \int_{0}^{a} \mathbf{F}(\rho, \phi') \, \mathbf{e}^{-\mathbf{j}\pi} \, \rho^{2}/\lambda\mathbf{R} \, \rho \, d\rho \, d\phi' \qquad (1)$$

Antenna aperture and coordinate system.

Figure 1



where

- U_{p} is the field at a point P on the axis of the aperture
- R is the axial distance from the aperture to the point ${\bf P}$
- λ is the wave length of the radiation
- α is the radius of the aperture
- ρ is the radial coordinate in the plane of the aperture
- $\phi^{\,\prime}$ is the angular coordinate of a point in the plane of the aperture
- $F(\rho, \phi')$ is the field strength or amplitude taper in the plane of the aperture
 - k is the wave number $2\pi/\lambda$

For the case of axially symmetric aperture illumination, equation (1) reduces to

$$U_{p} = j \frac{k e^{-jkR}}{R} \int_{0}^{a} F(\rho) e^{-j\pi \rho^{2}/\lambda R} \rho d\rho$$
(2)

If we now define the dimensionless parameters

 $x \equiv \frac{R\lambda}{a^2}$ and $r \equiv \frac{\rho}{a}$,

we have

$$U_{p} = j \frac{2\pi e^{-jkR}}{x} \int_{0}^{1} F(r) e^{-j\pi r^{2}/x} r dr$$
 (3)

If the function F(r) is normalized with respect to its value at the center of the aperture, the magnitude of U_p will be the ratio of the field at the point P to that at the center of the aperture.

For the special case of uniform aperture illumination, F(r) = 1.0 and equation (3) reduces to

$$U_{p} = j \frac{2\pi e^{-j\kappa R}}{x} \int_{0}^{1} e^{-j\pi r^{2}/x} r dr \qquad (4)$$

$$= j e^{-jkR} \left[2 \sin \frac{\pi}{2x} \right] e^{-j\pi/2x} .$$
 (5)

Method of Finite Differences

One approach to obtaining a digital computer solution for the case of axially symmetrical illumination of the aperture lies in converting equation (3) directly into a finite difference equation.

Equation (3) may be rewritten to eliminate the exponential under the integral sign:

$$U_{p} = j \frac{2\pi e^{-jkR}}{x} \left[\int_{0}^{1} F(r) \cos\left(\frac{\pi r^{2}}{x}\right) r \, dr - j \int_{0}^{1} F(r) \sin\left(\frac{\pi r^{2}}{x}\right) r \, dr \right]. (3a)$$

By taking the absolute value of both sides of equation (3a) and squaring, we obtain an expression for the ratio of the power density W_p at the point on the aperture axis to the illumination power density W_o at the center of the aperture. Thus

$$\frac{W_{p}}{W_{o}} = |U_{p}|^{2} = \left(\frac{2\pi}{x}\right)^{2} \left\{ \left[\int_{0}^{1} F(r) \cos\left(\frac{\pi r^{2}}{x}\right)r \, dr\right]^{2} + \left[\int_{0}^{1} F(r) \sin\left(\frac{\pi r^{2}}{x}\right)r \, dr\right]^{2} \right\}$$

$$(6)$$

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If we divide the aperture radius <u>a</u> into N equal increments Δr_1 , where Δr_1 designates the ith increment from the periphery of the aperture (see Figure 2), we have

 $r_i = \frac{N + 1/2 - i}{N}$ and $dr \cong \Delta r_i = \frac{1}{N}$.

Further, letting e_i represent the ordinate of the normalized aperture field intensity distribution at the center of the interval Δr_i , we have

$$\frac{W_{p}}{W_{0}} \approx \left(\frac{2\pi}{xN}\right)^{2} \left\{ \left[\sum_{i=1}^{N} e_{i} \left(\frac{N+1/2-i}{N} \right) \cos \frac{\pi}{x} \left(\frac{N+1/2-i}{N} \right)^{2} \right]^{2} + \left[\sum_{i=1}^{N} e_{i} \left(\frac{N+1/2-i}{N} \right) \sin \frac{\pi}{x} \left(\frac{N+1/2-i}{N} \right)^{2} \right]^{2} \right\} .$$
(7)

It is convenient to express the dimensionless power density ratio in terms of the average power density over the aperture W_a , rather than in terms of W_o .

Now

$$\frac{W_a}{W_o} = \frac{1}{\pi} \sum_{i=1}^{N} e_i^2 2\pi r_i \Delta r_i$$

$$= \frac{2}{N} \sum_{i=1}^{N} e_i^2 \left(\frac{N + 1/2 - i}{N} \right) .$$
(8)

Substitution of this into equation (7) yields the following expression:

$$\frac{W_{p}}{W_{a}} = \frac{2\pi^{2}}{N x^{2} \sum_{\substack{i=1 \\ i=1}}^{N} e_{i}^{2} \left(\frac{N+1/2-i}{N}\right)} \left\{ \left| e_{i} \left(\frac{N+1/2-i}{N}\right) \cos \frac{\pi}{x} \left(\frac{N+1/2-i}{N}\right)^{2} \right| + \left| e_{i} \left(\frac{N+1/2-i}{N}\right) \sin \frac{\pi}{x} \left(\frac{N+1/2-i}{N}\right)^{2} \right| \right\} \right\}$$
(9)

Method of Superposition

An alternative approach follows from the concept that the aperture amplitude distribution may be approximated by a number of uniform fields distributed over coaxial disks or "sub-apertures" of varying radius. At each point on the aperture axis, the solutions for each of the uniformly illuminated sub-apertures may then be combined, by the principle of superposition, to yield the net power density at the field point. This concept is illustrated in Figure 3.

For each of the sub-apertures, equation (5) takes the form

$$(U_p)_1 = 2 \sin \frac{\pi r_1^2}{2x} \left(\cos \frac{\pi r_1^2}{2x} - j \sin \frac{\pi r_1^2}{2x} \right) \Delta e_1$$
 (10)

where the subscript i pertains to the ith sub-aperture, and $(U_p)_i$ is the field at any point P on the aperture axis due to the ith sub-aperture, $\Delta e_i = (e_i - e_{i-1})$ is the amplitude of the field associated with the ith uniformly illuminated sub-aperture, and r_i is the radius of the ith sub-aperture.

Note that the phase angle component $j e^{-jkR}$ has been dropped. Since this angle is independent of r_i , it will not alter the relative phase of the contributions of the various sub-apertures and hence serves no useful purpose in this analysis.

If the difference in radius between successive sub-apertures is chosen to be a constant, $\frac{1}{N}$, and if the i's progress from the periphery toward the center, we have $r_i = \frac{N+1-i}{N}$.

Substitution of the above quantity in equation (8) yields

$$\begin{aligned} \left(U_{p} \right)_{i} &= 2 \ \Delta e_{i} \ \sin \frac{\pi}{2x} \left(\frac{N+1-i}{N} \right)^{2} \left[\cos \frac{\pi}{2x} \left(\frac{N+1-i}{N} \right)^{2} \right] \\ &- j \ \sin \frac{\pi}{2x} \left(\frac{N+1-i}{N} \right)^{2} \right] \\ &= 2 \left[\Delta e_{i} \ \sin \frac{\pi}{2x} \left(\frac{N+1-i}{N} \right)^{2} \cos \frac{\pi}{2x} \left(\frac{N+1-i}{N} \right)^{2} \right] \\ &- j \ \Delta e_{i} \ \sin^{2} \frac{\pi}{2x} \left(\frac{N+1-i}{N} \right)^{2} \right] \end{aligned}$$
(11)





NORMALIZED APERTURE RADIUS Y



Approximation of aperture distribution by finite increments with N = 10.

Summing the contributions of the N sub-apertures,

$$\sum_{i=1}^{N} (U_{p})_{i} = 2 \left[\sum_{i=1}^{N} \Delta e_{i} \sin \frac{\pi}{2x} \left(\frac{N+1-i}{N} \right)^{2} \cos \frac{\pi}{2x} \left(\frac{N+1-i}{N} \right)^{2} - j \sum_{i=1}^{N} \Delta e_{i} \sin^{2} \frac{\pi}{2x} \left(\frac{N+1-i}{N} \right)^{2} \right].$$
(12)

Taking the absolute value and squaring gives

$$\frac{W_{p}}{W_{o}} = \left| \sum_{i=1}^{N} (U_{p})_{i} \right|^{2} = 4 \left\{ \left[\sum_{i=1}^{N} \Delta e_{i} \sin \frac{\pi}{2x} \left(\frac{N+1-i}{N} \right)^{2} \cos \frac{\pi}{2x} \left(\frac{N+1-i}{N} \right)^{2} \right]^{2} + \left[\sum_{i=1}^{N} \Delta e_{i} \sin^{2} \frac{\pi}{2x} \left(\frac{N+1-i}{N} \right)^{2} \right]^{2} \right\}$$

$$(13)$$

In this method

$$\frac{W_{a}}{W_{o}} = \frac{1}{\pi} \sum_{i=1}^{N} \Delta e_{i}^{2} \pi \left(\frac{N+1-i}{N} \right)^{2} = \sum_{i=1}^{N} \Delta e_{i}^{2} \left(\frac{N+1-i}{N} \right)^{2}$$
(14)

where

$$\Delta e_{i}^{2} = e_{i}^{2} - e_{i-1}^{2}$$

Finally, upon substituting equation (14) into equation (13), we have

$$\frac{W_{p}}{W_{a}} = \frac{4}{\sum_{\substack{1=1\\1=1}}^{N} \left(e_{1}^{2} - e_{1-1}^{2}\right) \left(\frac{N+1-1}{N}\right)^{2}} \left\{ \left[\sum_{\substack{1=1\\1=1}}^{N} \left(e_{1} - e_{1-1}\right) \sin \frac{\pi}{2x} \left(\frac{N+1-1}{N}\right)^{2} \cos \frac{\pi}{2x} \left(\frac{N+1-1}{N}\right)^{2}\right]^{2} + \left[\sum_{\substack{1=1\\1=1\\1=1}}^{N} \left(e_{1} - e_{1-1}\right) \sin^{2} \frac{\pi}{2x} \left(\frac{N+1-1}{N}\right)^{2}\right]^{2} \right\}$$
(15)

Equations (9) and (15) were programmed for the IBM 7090 and STRETCH (IBM 7030) computers and represent the two methods of obtaining the on-axis fields of arbitrary aperture distributions.

While the method of superposition was found to give more accurate results than the finite differences method for a given value of N, either method will give results as precise as desired by choosing a large enough value for N. It is desirable, however, to use as low a value of N as is consistent with the necessary accuracy, since each e_1 must be taken either from a graph of the aperture distribution (if it is irregular) or calculated from the mathematical formula for the distribution (if it can be represented by a simple mathematical function). In the following calculations a value of N = 50 was used.

While the method of superposition is more accurate, it does not lend itself well (although it could be modified to do so) to calculations of the field when the aperture distribution is not single valued or monotonic, e.g. Taylor distributions, distributions with blocking, etc. For distributions of this type, the method of finite differences is especially useful.

In this report the method of superposition was used to calculate the fields of all single valued distributions, with the method of finite differences being incorporated for the remaining aperture illuminations. In all the calculations it is assumed that the field is in phase across the entire aperture.

DISCUSSION

The aperture distributions for which the on-axis fields are calculated are uniform illumination; linear, square law, $(1 - r^2)^n$ and (cosine)ⁿ tapers; Taylor distributions; some irregular arbitrary distributions and distributions with "blocking", where the field strength or power density is zero near the center of the aperture to simulate the effect of the antenna primary feed blocking the center illumination. For the linear, square law $((1 - r^2)^n$ taper with n = 1) and (cosine)ⁿ tapers, four variations of each taper are used, i.e., tapers in which the edge illumination is 5, 10, 20 and ∞ db down from the illumination at the center of the aperture. (It should be noted that these descriptive terms, linear tapers, square law tapers, etc. pertain to the field intensity distribution in the aperture and not to the power density distribution, which is proportional to the square of the field intensity.)





Figure 3

Approximation of aperture distribution by uniformly illuminated sub-apertures with N = 10.

While the on-axis fields have been determined in previous literature on this subject for many of the distributions contained herein (see, for example, reference (e)), these fields have been recalculated, along with a number of new distributions, using the methods of this report. This fulfills several functions. First, the resulting fields of these common distributions are presented, for a number of edge-to-center illumination ratios, in one paper, thus providing a convenient comparison of the resulting fields; second, it provides a basis for comparing the results of these methods with those obtained in previous literature, verifying that the results are identical for every distribution for which the on-axis field has been previously calculated; and finally, these distributions simulate a large number of the possible tapers which may occur in antennas, and by choosing the appropriate distribution in this report a good approximation of the on-axis field for the aperture distribution of interest may be obtained.

Linear tapers and square law tapers are two of the most commonly used aperture distributions in which the amplitude is increased from a low value at the aperture edge to a maximum at the center of the aperture. Linear amplitude distributions are given by the equation $\alpha(r) = 1 - (1 - \alpha)r$ where $\alpha(r)$ is the normalized amplitude taper, r is the normalized radial distance from the aperture center and a is the ratio of the amplitude at the aperture edge to that at the center. Using similar notation, square law distributions may be represented by $\alpha(r) = 1 - (1 - \alpha)r^2$.

The two families of amplitude tapers, $(1 - r^2)^n$ and $(\cos ine)^n$ cover a wide range of possible aperture distributions in which the amplitude is gradually decreased from a maximum at the center to a somewhat lower value at the aperture edge. The rate of decrease or slope may be increased by increasing the value of the parameter n. The on-axis fields have been calculated herein for n = 1/2, 1, 3/2, 2, 3, and 4 at four different edge-to-center illumination ratios for the (cosine)ⁿ tapers, and for n = 1, 2, 3, and 4 with one illumination ratio ($_{\infty}$ db) in the case of the tapers $\alpha(r) = (1 - r^2)^n$. The (cosine)ⁿ tapers are expressed by $\alpha(r) = (1 - \alpha) (\cos \frac{\pi}{2} r)^n$.

Taylor aperture distributions for circular aperture antennas offer an appreciable improvement in beam width and sidelobe levels over conventional distributions, and are thus likely to be utilized in antenna design. One Taylor distribution is included to provide an example of the form of the on-axis field resulting from distributions of this type. This Taylor distribution, from reference (c), produces a sidelobe level 25 db down from the intensity on the axis and has a transition integer of $\overline{n} = 8$. Since this is not a monotonic distribution, the method of finite differences was used to calculate the on-axis field.

Reflector antennas frequently incorporate a primary feed at the aperture center which blocks out the center portion of the aperture illumination. To determine the effect blocking will have upon the field, 5 and ∞ db cosine tapers with zero illumination for $r \leq 0.1$ were included. For these distributions also, the method of finite differences was utilized.

Four irregular distributions which could be approximately simulated by 5 db $\operatorname{cosine}^{1/2}$, $_{\infty}$ db $\operatorname{cosine}^{1/2}$, 5 db cosine^4 and $_{\infty}$ db cosine^4 are included to emphasize the usefulness of the methods of this report in determining the fields of irregular distributions and to determine the extent of the deviation occurring in the on-axis fields when these approximations are made.

RESULTS

The on-axis fields were determined by computer for the aperture distributions discussed in the previous section and the results are presented in the figures of Appendix A in a manner believed to best facilitate comparison:

The on-axis fields for the aperture distributions (linear, square law and cosineⁿ tapers) which have four edge-to-center illumination ratios are presented with the four resultant fields for each taper on the same graph (Figures 5 through 13). In addition, Figures 14 through 22 present the (cosine)ⁿ tapers with the edge-tocenter ratio held constant (at each of the values 5 db, 10 db, 20 db and ∞ db down from that at the aperture center) and the taper varied by letting n take on values 1/2, 1, 3/2, 2, 3 and 4. Since for each edge-to-center ratio there exist six distribution functions (one for each value of n), the fields for each db level are presented in two figures for clarity with n = 1/2, 3/2 and 3 on one graph and n = 1, 2 and 4 on another. From these arrangements both the effect of varying the edge-to-center illumination ratio for a given distribution function, and the effect of varying the distribution function for a given edge-to-center illumination ratio may be observed. The on-axis fields resulting from the $(1 - r^2)^n$ tapers (with n = 1, 2, 3 and 4), the Taylor distribution and the irregular tapers are presented in Figures 22 through 27. All four fields from the $(1 - r^2)^n$ tapers are presented on the same graph. Each of the fields from the irregular tapers is plotted with the regular taper that is being approximated.

The effect, on the on-axis field, of blocking due to a central feed horn was found to be so slight that it would not be observable if the fields were plotted. Thus these tapers were not presented in the figures of Appendix A; however, the computer tabulations for these distributions are included in Appendix B, listing W_p/W_a at various distances x.

All of the power density fields in the figures of Appendix A are plotted on a logarithmic scale using the dimensionless coordinates W_p/W_a as ordinates and $x \left[= \frac{R\lambda}{a^2} \right]$ as abscissae. The corresponding aperture distributions are included in the upper right hand corner of each figure.

ERROR ANALYSIS

To obtain an estimate of the error resulting from the use of these methods (with N = 50), the exact solutions of the Fresnel equation for the 5 db and ∞ db square law and (cosine)⁴ tapers were computed. These represent the two extremes of deviation, with the 5 db square law taper deviating least from uniform illumination and the ∞ db (cosine)⁴ having the greatest deviation from uniform illumination. It is assumed that the error occurring in the calculations of the on-axis fields for other tapers will not exceed that of these extreme tapers. Both the 5 db and the ∞ db illumination ratios were calculated for each of the two tapers to determine the effect of edge-to-center illumination ratios upon the error.

The accuracy of W_p/W_a in the tables of Appendix B is limited to three significant figures since the computer input data (the $e_i s$) were only given to three decimal places. Comparison of the exact values of W_p/W_a with those given in Appendix B at various values of x from 0.1 to 100, showed that for the majority of cases there was no error occurring in the first three significant figures. In no instance did the superposition method give an error in excess of 1.0% and only in the most extreme distribution (∞ db cosine⁴) did the method of finite differences have an error greater than this. This amounted to 1 - 3% and can be expected to occur when this method is used for the more extreme distributions (∞ db cosine³, cosine⁴ and (1 - r²)⁴). In both methods the error is greatest at low values of x.

It is also of interest to observe the effect that varying the value of N has upon the accuracy of the calculations. While the method of superposition gives the exact solution of the Fresnel equation for a uniformly illuminated aperture, there is a slight amount of deviation when the method of finite differences is used. The on-axis field for a uniformly illuminated aperture was calculated using values of N = 10, 25, 50, 75, 100, 150, 200, 500, and 1000. The resulting values of W_p/W_a were compared with the exact solution and the percentage of error was plotted as a function of N for various values of x in Figure 4.

As can be seen from the graph, a linear relationship exists (on a logarithmic scale) between the error and N, and if it is assumed that other distributions will have a similar error for the same value of N, Figure 4 may be used to choose the appropriate value of N for whatever accuracy is desired.

The curves of Figure 4 are applicable only to the method of finite differences, since no error occurs when the method of superposition is used for uniform illumination.

CONCLUSIONS

Examination of the resulting fields reveals a number of significant effects of non-uniform aperture distributions upon the on-axis field. These may be summarized as follows:

1. The deep nulls which occur in the Fresnel field of a uniformly illuminated aperture are filled in considerably when the distribution is tapered. This is most pronounced for the distributions which deviate most from uniform illumination.

2. There is a decrease in power density in the far field (a shifting of the curve to the left) although the slope of this far field (inverse square law) curve remains the same. Upon closer analysis it is found that the values of W_p/W_a in the far field are precisely the values predicted by the far field formula

$$\frac{W_{p}}{W_{a}} = \frac{G_{M}A}{4\pi R^{2}} \quad \text{where} \quad G_{M} = \frac{\left|\int_{0}^{1}A(r) dr\right|^{2}}{\int_{0}^{1}A^{2}(r) dr} \quad G_{o},$$

 $G_{\rm M}$ and $G_{\rm o}\left[=\frac{4\pi}{\lambda^2}\right]$ being the gain of the aperture for tapered and

uniform illumination, respectively.



Figure 4

Error as a function of the number of increments N for uniform illumination using the method of finite differences.

3. The envelope of the maxima in the Fresnel field of a uniformly illuminated aperture is a constant value, i.e, $W_p/W_o = 4.0$, while for a tapered aperture distribution the peaks tend to either increase or decrease as x decreases depending upon the particular distribution. From an analysis of the resulting curves and from theoretical considerations, a formula for this envelope may be found, namely that as x approaches zero the maxima approach the value

 $\left(\frac{W_p}{W_a}\right)_{\max} = \frac{W_o}{W_a} (1 + \alpha)^2 = \frac{(1 + \alpha)^2}{2 \int_0^1 A^2(r) r dr}$

For tapers which approach W_o very rapidly from the value at the aperture edge (square law and (cosine)^{1/2} tapers), the maxima decrease in field strength as x decreases, while for most other tapers the field strengths of the maxima increase as x decreases.

4. As the edge-to-center ratio is decreased, the values of x at which the near field maxima and minima occur decreases, i.e., there is a slight shift of the peaks and nulls to the left.

5. The edge-to-center illumination ratio has more effect upon the on-axis field than the particular type of taper used.

6. "Blocking" of the center portion of an aperture (from center out to $r \leq 0.1 a$) has only a small effect upon the on-axis field. The far field is decreased by about 1%, while the near field peaks are increased on the order of 5%.

SUMMARY

1. Two equations which lend themselves well to computer solutions have been developed, predicting the on-axis power density for any arbitrary aperture distribution.

2. These equations have been programmed for computer solution and are readily available for use as a tool in the study of radar fields.

3. The on-axis fields were calculated for a number of aperture distributions which were felt to approximate many of the distributions occurring in practice. By choosing the distribution in this report which best simulates an actual distribution under study, a good approximation of the on-axis field may be obtained.

4. Analysis of the resulting on-axis fields reveals a number of significant effects which tapered distributions have upon the field as compared to uniform distribution. These are:

a. The nulls occurring in the near field are partially or completely filled in.

b. The far field gain is reduced.

c. The envelope of the Fresnel field peaks is no longer constant but increases or decreases as x decreases.

d. The values of x at which the Fresnel field peaks occur decrease.

e. The edge-to-center illumination ratio has more effect upon the on-axis field than the particular type of taper used.

f. Blocking of a small center portion of the aperture $(r \le 0.1 a)$ has little effect upon the on-axis field.

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APPENDIX A

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•		irregular	dist	ribu	itio	n					

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- Figure 27 On-axis field of a Taylor distribution (sidelobes 25 db down, n = 8)

NOTATION FOR ALL FIGURES

 W_p = Power density at a field point on the aperture axis W_a = Average power density over the aperture

X = Dimensionless parameter proportional to the distance from aperture to field point, along the aperture axis

$$=\frac{R\lambda}{a^2}$$

R = Distance from aperture to field point along the aperture axis

- a = Radius of aperture
 - λ = Wave length of radiation
 - r = Normalized distance from center of aperture in the plane of the aperture

A(r) = Normalized field intensity distribution across the aperture



















Figure 10





DM d POWER DENSI λE TAJJR

20 db 80 db

0

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5 db

A(r) 🕏

5 db db 01 ----- 20 db db 00

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APERTURE DISTRIBUTION



On-axis fields for cosine⁴ aperture distributions.






On-axis fields for 10 db cosineⁿ aperture distributions.





DIMENSIONLESS DISTANCE FROM APERTURE, X





Figure 18

0 ••••• n=3/2 N=1/2 5=U -----APERTURE DISTRIBUTION =4 Acin DIMENSIONLESS DISTANCE FROM APERTURE, X 0 0 Ă(r) õ ₽**M** RELATIVE POWER DENSITY 6 M





DIMENSIONLESS DISTANCE FROM APERTURE, X





On-axis fields for $^\infty$ db cosine^n aperture distributions.







Comparison of the on-axis fields of an irregular distribution and a 5 db $\cos h^{2}$ approximation of the irregular distribution.









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0.166	0.29439		.282	1.87209	1.550	2.81833
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2.89439	0.234	1.70554		550	1.08642
2.12003	0.236	1.55343		560	1.17690
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4.11987	0.254	1.02942	.0	.850	3.70422
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4.24807	0.264	1.32148		001	3.73680
3.86468	0.266	1.41515		150	3.64033
3.41677	0.268	1.51770		200	3,53052
2.94203	0.270	1,62791		250	3.41249
04730	0.274	1.74450 1.86650		350	215615
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1.54042	0.290	2,90643	• •	750	2.27314
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Table 3. Wp/Wa versus x for 10 db linear distribution.

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Table 4. Wp/Wa versus x for 20 db linear distribution.

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0.230 3.97893 0.550 3.98246 0.234 4.004859 0.550 3.99603 0.235 4.004859 0.550 3.99603 0.234 4.004859 0.550 3.99603 0.235 4.004859 0.550 4.03720 0.2442 4.074859 0.550 4.03720 0.2442 4.10170 0.560 4.10770 0.2445 4.10170 0.560 4.10770 0.2552 4.16453 0.500 4.16543 0.2552 4.16453 0.700 4.16543 0.2566 4.16563 4.7168 4.16570 0.2566 4.16763 0.8003 4.25143 0.2568 4.47563 1.250 4.255143 0.2568 4.47963 1.250 4.255143 0.2568 4.47963 1.250 4.255143 0.2568 4.47963 1.250 4.255143 0.2568 4.47963 1.250 4.495543 0.2568 4.47963 1.250 3.56543 0.2568 4.47963 1.250 <t< td=""><td></td><td>0.226</td><td>5.98618 7 97787</td><td>20</td><td>000</td><td>11009.5</td></t<>		0.226	5.98618 7 97787	20	000	11009.5
0.230 3.97293 0.530 3.82546 0.235 4.002605 0.550 3.99726 0.236 4.002605 0.550 3.99726 0.235 4.002605 0.550 4.102729 0.246 4.017395 0.550 4.102729 0.244 4.10170 0.560 4.16342 0.244 4.10179 0.560 4.16342 0.244 4.113141 0.750 4.16342 0.255 4.19456 0.590 4.16342 0.255 4.19456 0.800 4.22069 0.255 4.19456 0.800 4.27316 0.256 4.19456 1.1050 4.27316 0.256 4.49366 1.1050 4.37526 0.256 4.49339 0.750 4.37539 0.256 4.49339 0.750 4.3753 0.256 4.49339 0.750 4.37339 0.256 4.49339 0.750 4.37339 0.258 4.49339 0.250 4.37339 0.266 4.49339 1.1050 3.75695		0.228	3.97082		520	3.75163
0.232 3.97986 0.540 3.99981 0.234 4.06682 0.550 3.96981 0.242 4.06882 0.550 3.96981 0.244 4.10170 0.550 3.96981 0.248 4.10170 0.550 4.07720 0.248 4.10170 0.550 4.07720 0.255 4.10170 0.500 4.15737 0.256 4.27371 0.500 4.15786 0.256 4.27973 0.500 4.7168 0.256 4.27373 0.700 4.27578 0.256 4.238995 0.700 4.275618 0.256 4.37399 0.950 4.47568 0.256 4.47399 0.950 4.47568 0.256 4.47399 0.950 4.255174 0.256 4.47399 0.950 4.255174 0.258 4.47399 0.950 4.47568 0.258 4.47399 1.100 4.2550 0.258 4.47399 1.250 2.55079 0.258 4.57368 1.250 2.47339		0.230	3.97293	0	530	3.82546
0.234 3.999128 0.550 3.99903 0.244 4.05606 0.550 4.07214 0.244 4.10170 0.550 4.07214 0.244 4.10170 0.550 4.07214 0.244 4.10170 0.550 4.07214 0.244 4.10170 0.550 4.1545 0.246 4.1141 0.500 4.25046 0.255 4.25148 0.750 4.25148 0.256 4.19433 0.750 4.25148 0.256 4.19433 0.750 4.256180 0.256 4.47359 0.950 4.25618 0.256 4.47359 0.950 4.4755 0.256 4.47359 0.950 4.4755 0.256 4.47358 1.1000 4.4755 0.256 4.47368 1.150 3.51574 0.256 4.47368 1.250 3.51574 0.250 2.26163 1.260 3.51574 0.250 2.2758 4.47358 1.250 0.250 2.28157 1.250 3.51574		0.232	3.97986	0	540	3.89821
0.238 4.02505 4.10170 0.580 4.10335 0.244 4.10170 0.580 4.27371 0.245 4.10170 0.580 4.27371 0.255 4.16543 0.750 4.25146 0.255 4.16543 0.750 4.25146 0.256 4.19435 0.750 4.25146 0.256 4.23791 0.750 4.25146 0.256 4.24768 0.750 4.25146 0.256 4.43599 0.750 4.25146 0.256 4.43599 0.750 4.25146 0.256 4.43599 1.050 3.87861 0.256 4.43599 1.1050 3.87861 0.256 4.43596 1.150 3.73319 0.277 4.44768 1.150 3.73319 0.278 4.44768 1.150 3.73319 0.278 4.44768 1.150 3.73319 0.278 4.44768 1.150 3.75319 0.278 4.44768 1.250 3.75319 0.278 4.44768 1.250		0.236	5.99128 4.00682	00	560	4 03720
0.240 4.04859 0.580 4.1532 0.242 4.10170 0.550 4.15141 0.248 4.10170 0.550 4.27376 0.248 4.10170 0.550 4.27376 0.252 4.22790 0.700 4.26180 0.256 4.27793 0.700 4.26180 0.256 4.27793 0.700 4.26180 0.256 4.27793 0.950 4.255173 0.256 4.37525 4.22790 4.256180 0.256 4.379905 0.950 4.256180 0.256 4.37593 0.950 4.355272 0.256 4.47788 1.100 3.37972 0.256 4.47788 1.150 3.76619 0.277 4.4768 1.160 3.5572 0.278 4.47788 1.250 3.76619 0.278 4.47788 1.150 3.76957 0.278 4.47768 1.160 3.75619 0.278 4.47768 1.250 3.76619 0.278 4.47768 1.750 3.76957 <td></td> <td>0.238</td> <td>4.02606</td> <td>0</td> <td>570</td> <td>4.10214</td>		0.238	4.02606	0	570	4.10214
0.242 4.07395 0.590 4.27378 0.244 4.15141 0.500 4.27378 0.255 4.25116 0.850 4.47158 0.255 4.256186 0.750 4.47157 0.255 4.256186 0.750 4.47157 0.256 4.256186 0.850 4.47157 0.256 4.256186 0.750 4.47157 0.256 4.47396 0.850 4.47567 0.266 4.47396 0.850 4.47567 0.266 4.47396 0.950 4.47567 0.266 4.47396 1.1000 4.49567 0.277 4.47366 1.1600 3.565726 0.278 4.55837 1.2500 3.565726 0.278 4.437366 1.2500 3.5696572 0.278 4.55837 1.2500 3.5696572 0.288 4.451266 1.2500 3.5696572 0.288 4.55837 1.2500 3.5696572 0.288 4.561261 1.7000 3.5696573 0.288 4.561261 1.700	•	0.240	4.04859	0	580	4.16342
0.244 4.10170 0.600 4.25141 0.255 4.15243 0.700 4.56180 0.255 4.25116 0.800 4.56180 0.255 4.25116 0.800 4.56180 0.256 4.1543 0.700 4.56180 0.256 4.25433 0.700 4.56180 0.266 4.47661 1.100 3.55122 0.266 4.47661 1.100 3.55124 0.266 4.47661 1.100 3.55124 0.266 4.47661 1.100 3.55124 0.266 4.47661 1.100 3.55124 0.266 4.47661 1.150 3.556143 0.274 4.47661 1.150 3.55124 0.274 4.47661 1.150 3.55124 0.278 4.47661 1.150 3.55124 0.274 4.558655 1.500 4.3753 0.278 4.56167 1.500 3.55712 0.278 4.573667 1.500 3.55712 0.278 4.561675 1.450 2.55712		0.242	4.07395	0	069	4.22069
0.245 4.15141 0.750 4.415141 0.254 4.15141 0.750 4.4191 0.255 4.22990 0.850 4.56148 0.255 4.2290 0.800 4.56148 0.255 4.2290 0.800 4.56148 0.256 4.23707 0.900 4.56148 0.266 4.38999 0.900 4.37525 0.266 4.44768 1.000 4.4758 0.266 4.44768 1.100 3.3752 0.266 4.47399 0.900 4.25590 0.266 4.4759 1.100 3.3792 0.270 4.4768 1.100 3.3792 0.274 4.54936 1.500 3.3061 0.274 4.54936 1.500 3.3791 0.274 4.54936 1.500 3.3791 0.274 4.55063 1.500 3.3754 0.274 4.55865 1.4500 2.4373 0.288 4.55865 1.500 2.4373 0.288 4.51646 1.4600 2.5010		0.244	4.10170	0	600	4.27371
0.255 4.19453 0.750 4.55148 0.256 4.22790 0.850 4.25148 0.256 4.28433 0.950 4.2551574 0.256 4.38905 0.950 4.2551574 0.256 4.47961 1.1000 3.87861 0.256 4.47739 0.950 4.37525 0.256 4.47739 1.1000 3.37919 0.272 4.47399 1.1000 3.37919 0.272 4.47399 1.1000 3.37919 0.272 4.477399 1.300 2.69657 0.272 4.477399 1.300 2.69731 0.272 4.477399 1.300 2.69657 0.272 4.57865 1.2500 3.16892 0.286 4.47739 1.3500 2.69657 0.288 4.60972 1.5500 3.16892 0.288 4.61341 1.500 2.50101 0.288 4.61241 1.750 2.7953 0.288 4.61241 1.750 2.309334 0.288 4.61341 2.5500 0.5742 <td></td> <td>0.246</td> <td>4.13141</td> <td>0</td> <td>550</td> <td>4.47168</td>		0.246	4.13141	0	550	4.47168
0.255 4.19493 0.400 4.99143 0.256 4.29116 0.850 4.37529 0.256 4.29135 0.900 4.37529 0.256 4.4768 4.25999 1.000 3.87861 0.266 4.479399 1.1050 3.78953 4.37529 0.266 4.4768 4.47599 1.1050 3.789514 0.266 4.477399 1.49836 1.1050 3.789514 0.274 4.477399 1.49836 1.1050 3.73919 0.274 4.55837 1.400 3.73919 3.73919 0.274 4.55837 1.4030 2.55712 3.55142 0.286 4.4768 1.500 3.73919 3.73919 0.274 4.55837 1.400 2.55714 3.7373 0.288 4.561241 1.750 3.7373 0.51477 0.284 4.56455 1.550 2.45773 0.550 2.65714 0.284 4.561241 1.750 1.400 2.56712 0.55743 0.284 4.561241 1.750 1.400 <t< td=""><td></td><td>0.248</td><td>4.16263</td><td></td><td></td><td>4.56180</td></t<>		0.248	4.16263			4.56180
0.255 4.254190 0.4500 4.37270 0.266 4.35905 1.000 3.4729 0.266 4.47961 1.000 3.47359 0.266 4.47961 1.000 3.51574 0.266 4.47961 1.000 3.51574 0.266 4.47769 1.000 3.51574 0.266 4.47769 1.000 3.51574 0.274 4.47789 1.000 3.51574 0.274 4.47789 1.2500 3.66892 0.274 4.57366 1.100 3.51574 0.276 4.57363 1.2500 3.66913 0.280 4.57366 1.2500 3.66913 0.281 4.57366 1.2550 2.375134 0.288 4.51037 1.4500 2.55013 0.288 4.51261 1.5500 2.43733 0.288 4.51261 1.500 2.43733 0.288 4.5134 1.500 2.55017 0.291 4.5983 1.500 2.500 0.292 4.5134 1.500 2.500		0027.0	4.19495			49196.4
0.256 4.25707 0.900 4.275726 0.256 4.37995 1.1000 3.8761574 0.256 4.37596 1.3500 3.8761576 0.256 4.37596 1.1000 3.51574 0.257 4.47395 1.1000 3.51574 0.256 4.373915 1.1000 3.51574 0.277 4.47395 1.2000 3.5965153 0.278 4.57366 1.2000 3.51574 0.277 4.57365 1.2000 3.5165124 0.277 4.57365 1.2000 3.16835 0.288 4.55337 1.2550 3.16835 0.288 4.61241 1.7500 2.43735 0.288 4.61241 1.7500 2.43735 0.288 4.61241 1.7500 2.43735 0.288 4.61241 1.7500 2.69731 0.288 4.61241 1.7500 2.69731 0.288 4.61241 1.7500 2.69731 0.293 2.29845 1.2500 2.7750 0.293 2.21641 1.7500 <			4.22.790	50		10264.4
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0.264 4.41961 1.100 3.51574 0.276 4.44768 1.4190 3.51574 0.276 4.44768 1.250 3.06611 0.276 4.47366 1.250 3.06611 0.276 4.55837 1.250 3.06611 0.276 4.55837 1.250 3.06611 0.276 4.55837 1.250 3.06611 0.276 4.55837 1.250 3.06611 0.284 4.56456 1.450 2.5512 0.284 4.56456 1.450 2.5512 0.284 4.61037 1.450 2.550 2.0101 0.284 4.61241 1.700 1.99314 0.292 4.61241 1.700 1.99314 0.293 4.61241 1.700 1.99314 0.294 4.58955 1.600 2.99101 0.293 4.51241 1.770 1.99314 0.293 4.51241 1.770 1.99314 0.293 4.51241 1.770 1.99314 0.293 4.51241 1.770 1.993		0.262	66666.4		020	3.69657
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0.268 4.4739 1.200 3.06892 0.270 4.49736 1.350 3.00611 0.275 4.54067 1.350 3.00611 0.276 4.57366 1.350 2.00611 0.280 4.57366 1.350 2.00611 0.281 4.57466 1.400 2.55712 0.281 4.57466 1.450 2.55713 0.281 4.55645 1.450 2.55713 0.281 4.56456 1.450 2.55713 0.281 4.56456 1.450 2.55713 0.281 4.61241 1.550 2.31541 0.292 4.61241 1.550 2.30971 0.294 4.61241 1.750 2.20071 0.294 4.61241 1.750 1.89381 0.294 4.59373 1.800 1.89381 0.293 4.583855 1.900 0.99374 0.294 4.59366 1.500 1.44310 0.230 4.58365 2.500 0.56971 0.330 4.58365 2.500 0.56976		0.266	4.44768		150	3.33919
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0.277 4.55837 1.500 2.5514 0.276 4.55837 1.500 2.5514 0.288 4.57356 1.500 2.5514 0.288 4.57356 1.500 2.5514 0.288 4.57356 1.500 2.5514 0.288 4.59675 1.550 2.5513 0.288 4.60975 1.500 2.9514 0.289 4.61241 1.500 2.9911 0.291 4.61037 1.600 2.9911 0.292 4.51261 1.700 1.800 0.291 4.61037 1.700 1.800 0.292 4.51261 1.700 1.800 0.293 4.51261 1.700 1.800 0.294 4.58955 1.700 1.801 0.293 4.58955 1.700 1.6495 0.200 0.3100 0.3500 0.5741 0.300 4.58955 1.7500 1.72745 0.310 4.58955 1.7500 1.72745 0.310 4.58955 2.5000 0.54955		0.270	4.49836	•	250	3.00611
0.278 4.57365 1.400 2.55735 0.280 4.57365 1.450 2.4733 0.284 4.59675 1.550 2.255735 0.286 4.59675 1.550 2.231541 0.286 4.60450 1.650 2.2010 0.286 4.60472 1.550 2.2010 0.290 4.61261 1.700 2.0373 0.292 4.61261 1.700 2.0373 0.293 4.61261 1.700 2.0373 0.293 4.61261 1.700 2.0105 0.294 4.61273 1.700 1.8968 0.299 4.51261 1.700 1.8968 0.299 4.51241 1.700 1.4410 0.291 4.5819 2.500 0.56995 0.310 4.57819 2.500 0.51477 0.310 4.57819 3.5000 0.51477 0.350 3.4741 7.000 0.51477 0.350 3.4741 5.500 0.18017 0.450 3.75819 5.000 0.100		2/2.0	4.52065		200	241C8.5
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Table 5. Wp/Wa versus x for $^\infty$ db linear distribution.

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Table 6. Wp/Wa versus x for 5 db square law distribution.

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	0.460	0.480	0.490	0.510	0.520	0.530	0,540	0.560	0.570	0.590	0.600	0.650	0.750	0.800	006.0	0.950	1.050	1.100	1.200	1.250	1.350	1.450	1.500	1,550	1.650	1.750	1.800	1.900	2.000	2 500	3,500	4.000	5.000	5.500	6.500	7.000	000.8	8.500	100.000	aw distribut		•	
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	2.69791	2.52948	2.45191	2.31563	2.25859	2.20972	2.16942	2.11517	2.10123	2.09585	2.10957	2.12782	2.18455	2.22187	2.31133	2,36220	2.41650	2.53176	2,65293	2.71427	2.83598	2.89544	3.00962	3.06366	3.16419	3.25317	3.29289	3.36219	3.41749	3.49379	3.40937	3,27871	2.92796	2.73904	5.39199	2.24863	2.04127	1.97940	1.93544	20 db squar			
×	0.216	0.220	0.222	0.226	0.228	0.230	0.252	0.236	0.238	0.240	0.244	0.246	0.250	0.252	0.256	0.258	0.262	0.264	0.268	0.270	0.274	0.276	0.280	0.282 0.284	0.286	0.290	0.292	0.296	0.298	0.310	0.330	0.340	0.360	0.370	0.390	. 0.400	0.420	0.430	0.450	rsus x for			
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×	0.100	0.104	0.106	0.110	0.112	0.114	0.116	0.120	0.122	0.124	0.128	0.130	0.134	0.136	0.140	0.142	0.146	0.148	0.152	0.154	0.158	0.160	0.164	0.166	0.170	0.174	0.176	0.180	0.182	0.186	0.190	0.192	0.196	0,198	0.202	0.204	0.208	0.210	0.212	Tal			
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d as	56399 (6120 (7170	88101 88101 8878	11902	36011	47817	70405	.81030 .91135	.00679 .09634	45227	74803	77977	53949	.38548	03206	66502	.48654	14933	.99236 .84360	57060	19594	21848	.01771	.92633 84045	75969	.68372 .61220	08471	57793	.35589	28976	20258	17300	13037	11472	09080	
_ ×	0.460 0.470 2.400 2.400 2.2000 2.2000 2.2000 2.2000 2.2000 2.2000 2.2000 2.2000 2.2000 2.2000 2.2000 2.2000 2.2000 2.2000 2.2000 2.2000 2.2000 2.2000 2.2000 2.200000000	0.490 2	0.510	0.530	0.550 3	0.560	0.580 3	0.590 4	0.650	0.750 4	0,800 4	4 006.0	0.950 4	1.050	1.150 3	1.200 3	1.300	1.400 2	1.450 2	1.550 2	1.650	1.750 2	1.800 1	006.1	1.950 1 2.000 1	2.500 1	3.500	4.000 0	0000	0000.9	6.500 0 7.000 0	7.500 0	8.000 0 0 8.500 0	0 000 6	
		•										•				•															-	•		-	
	2.66998 2.64549	2.61637	2.61364	2.63578	2.65534	2.70925	2.77953	2.81947	2.90626	2.99872	3.04582	3.13943	3.18512	3.27241	3.35217	3.38859	3.45348	3.48166	3.52892	3.56369	3.58581	3.59549	3.59581	3.58781	3.579703.56899	3.48105	3.18926	3.01944 2.85279	2.69993	2.46297	2.338607	2.31879	2,32575	2.40874	
• X	0.216 0.218	0.222	0.226	0.230	0.232	0.236	0.240	0.242	0.246	0.250	0.252	0.256	0.258	0.262	0.266	0.268	0.272	0.276	0.278	0.282	0.286	0.290	0.292	0.296	0.298	0.310	0.330	0.340	0.360	0.380	0.390	0.410	0.420	0.440	
																									•										!
d a	2.99740 3.09768	3.18239	3.06653	2.88427	2.82419 2.80281	2.82230	2.95468	3.04198	3.19096	3.24594	3.23049	3.12925	3.05640	2.90375	2,78554	2.75075	2.73865	2.79824	2.90948	2.97578	3.11160	3,17459	3.27775.2	3.33929	3.35239	3.34336	3.29213	3.25352	3,15752	3.04677	2.98965	2.87880	2.82744	2.73773	
	0.100	0.106	0110	0.114	0.116	0.120	0.124	0.126 0.128	0.130	0.134	0.136	0.140	0.142	0.146	0.150	0.152	0.156	0.158	0.162	0.166	0.170	0.172	0.176	0.180	0.182	0.186	0.1.0	0.192	0.196	0.200	0.202	0.206	0.208	0.212	, (
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	0.34101	0.18426	0.16107	0.17002	0.26966	0.35309	0.45435	0,029	0.83487	0.97853	1.12687	1.27806	2.02733	3.20921	3.58972	3.84457	3.99570	4.06508	4.0702	3.96011	3.86398	3.75211	3.63033	3.50298	3.57529	3.11565	2.99058	2.86922	2.75210	2 53171	2.42865	2.33035	2.23669	2 06281	1.98224	1.36632	0.98741	0.14297	60//C"O	0.37647	0.31287	0.26401	0.22570	0.19512	0.17033	0 13303	0.11880	0.00097	
	0.460	0.480	0.490	0.500	0.520	0.530	0.540	00000	0.570	0.580	0.590	0.600	0.05.0	0.750	0.800	0.850	006.0	056.0	1.050	001.1	1.150	1.200	1.250	1.300	1 350	1.450	1.500	1.550	1.600		1.750	1.800	1.850	0.50	2.000	2.500	3.000	3.500	4.000	5.000	5.500	6.000	6.500	2.000	005.7	2002 0	000.6	100.000	
	. '																	•		-																						•			•	••			ير
	2.51336	2.06070	1.83525	1.61540	1.20505	1.01978	0.85056	0.69898	0.45309	0.36010	0.28741	0.23494	0.20235	0.19428	0.21717	0.25669	0.31169	0.38095	0.45321	0.66147	0.77482	0.89589	1.02340	1.15607	1.29272	1.43617	1.71516	1.85669	1.99700	92051.5	2.40265	2.53045	2.65355	241/1.2	2.99005	3.42264	3.68012	3.76714	5.0003 F	3.24619	2.91315	2.54818	2.17422	1.80958	1.46805	1.13745	0.66329	0.48046	
×	0.216	0.220	0.222	0.224	0.228	0.230	0.232	0.234	0.236	0.240	0.242	0.244	0.246	0.250	0.252	0.254	0.256	0.258	0,260	0.264	0.266	0.268	0.270	0.272	0.274	0.270	0.280	0.282	0.284	982.0	0.290	0.292	0.294	962.0	0.300	0.310	0.320	0.330	0.40	0.360	0.370	0.380	0.390	0.400	0.410	074°0	0.440	0.450	
																															• •			•															
	0.21947	1.38083	2.33121	3.12226	3.52986	3.11811	2.44355	1.6/207	200/6.0	0.22644	0.26601	0.55647	1.03421	2.22465	2.77828	3.22027	3.51206	3.63599	14545.2	3.40128	2.68790	2.23927	1.77866	1.33928	0.94891	19920.0	0.25012	0.20065	0.24112	0.35346	0.80656	1.09936	1.41994	1.13585	2.40904	2.70787	2.97549	3.20528	3.59249	C1455 1	3.67717	3.68015	3.64046	3.56149	3.44730	0.502AU	010101 0	2.73216	
×	0.100	0.104	0.106	0.108	0.112	0.114	0.116	0.118	0.120	0.124	0.126	0.128	0.130	0.134	0.136	0.138	0.140	0.142	0.144	0.140	0.150	0.152	0.154	0.156	0.158	0.160	0.164	0.166	0.168	2	0.174	0.176	0.178	0.180	0.184	0.186	0.188	0.190	0.192	0.194	0.198	0.200	0.202	0.204	0.206	802.0	0.110	0.214	

Table 10. Wp/Wm versus x for 5 db (cosine)^{1/2} distribution.

×	đ	X	B	×	
001 0	0 64490	210 0	7 205 77	0.400	1212 0
0.102	2446.0	0.218	211524	0.470	CTTA 0
0.104	1.63592	0.220	1.92609	0.480	0.4552
0.106	2.37841	0.222	1.74110	0.490	0.4645
0.108	2,96829	0.224	1.56318	0.500	0.5014
011.0	3,25350	0.226	1.39483	0.510	0.5626
0.114	2.82173	0.230	1.09515	0.5.0	0.7436
0.116	2,26638	0.232	0.96703	0.540	0.8570
0.118	1.65870	0.234	0.85496	0.550	0.9819
0.120	1.12546	0.236	0.75970	0.560	1.1156
0.122	0.76030	0.238	0.68171	0.570	1,2558
0.126	0.68879	0 242	0.57808	080.0	1 5475
0.128	0.95735	0.244	0.55209	0.600	1.6957
0.130	1.36331	0.246	0.54276	0.650	2.4102
0.132	1.83971	0.248	0.54943	0.700	3.0167
0.134	2,31938	0.250	0.57132	0.750	3,4813
0.136	2.74380	0.252	0.60754	0.800	3.8072
851.0	3.06880	0,256	60/C9.0	008.0	
0.142	3.32846	952.0	0.79187	050.0	4.1573
0.144	3,25755	0.260	0.87483	1.000	4.1355
0.146	3.07108	0.262	0.96663	1.050	4.0727
0.148	2.79404	0.264	1.06609	1.100	3.9809
0.150	2.45608	0.266	1.17206	061.1	2698.2
	210012	2020	1.64540		
	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		1 51784		1974 5
0.158	1.08134	0.274	1.63884	1,350	3,3435
0.160	0.84802	0.276	1,76107	1.400	3,2092
0.162	0.68708	0.278	1,88360	1.450	3.0778
0.164	0.60296	0.280	2.00559	1.500	2,9502
0.166	10033 0	292.0	C2921.5	0009 1	
021.0	105000	0 285	2.16071	1.650	2.595.5
0.172	0.96802	0.288	2.47324	1.700	2.4870
0.174	1.19129	0.290	2.58189	1.750	2.3839
0.176	1,44414	0.292	2.68619	1.800	2.2857
0.178	1.71424	0.294	2.78571	1.850	2.1924
0.180	1.98979	0.296	2.88009	1.900	2.1038
281.0	6 F1F30	0 200	105301	000.6	0610'S
0.186	2.74782	0.310	3.37674	2.500	1.3324
0.188	2.95107	0.320	3.54466	3.000	0.9611
061.0	3.12031	0.330	3.56545	3.500	0.7224
0.192	3.25234	0.340	3.46082	4.000	0.5613
0.194	44047 P	00010	5.63634		0.44400
061.0	23555.5	0.370	2.67315 2.67315	5.500	LEOE O
0.200	3.39296	0.380	2.34100	6.000	0.2562
0.202	3,33732	0.390	2.00968	6.500	0.2190
0.204	3.25077	0.400	1.69425	2.000	0.1893
0.206	3.13704	0.410	1.40571	7.500	0.1652
0.208	C1000.5	0.420	0 93604	8,500 8,500	0541.0
	57180	0.440	0.76140	000 6	0.1152
0.214	2.49276	0.450	0.62772	100.000	6000.0
Tal	ble 11. WD/Wa.v	ersur x for	· 10 dh (cosin	a) ² distribut	i nn .

	21			-	
×	W.B.	×			Wa
0.10	1.31295	0.216	2.0450.8	0 460	ACCTR O
0.10	1.60859	0.218	1.95569	0440	0 87271
0.10	2.06557	044	1 82126		
0.10	06 2.51832	0.000	1 69788		0.95420
0.10	08 2.82861	0.224	1.57538		APRCO 1
0.11	92099	0.226	1.46727	0.510	1.12088
0.11	12 2.79048	0.228	1.37075	0.520	1.22789
11.0	4 2.48911	0.230	1.28677	0.530	1.34675
	16 2.10145	0.232	1.21600	. 0.540	1.47479
		0.234	1.15884	0,550	1.60959
		0.236	1.11548	0.560	1.74901
	968951 23112	0.238	1.08589	0.570	1.89115
		0,240	1.06986	085.0	2.03435
		0.242	1.06/02	065.0	2.17720
		0.244	1.07684	0.600	2.31848
	1.89650	0.540	1.09869	0.650	2.97137
		0.250	1.15185	00/ 0	3.49300
	16 0 76007		196/1.1	06/ 0	3.868/0
	102263230	203°0	200521		COLLIA P
0.14	3.00198	0.256	1.36002	006.0	10666.0
0.14	12 2.97808	0.258	1.43634	0.950	4.27474
0.14	14 2.86980	0.260	1.51845	1.000	4.21060
. 0.14	16 2.69325	0.262	1.60539	1.050	4.11355
0.14	18 2.46879	0.264	1.69623	1.100	3.99433
0.15	2.21846	0.266	1.79006	1.150	3.86103
0.15	1.96381	0.268	1.88600	1.200	3.71969
1.0	1.72423	0.270	1.98323	1.250	3.57470
		2/20	2.08094	1.300	3.42926
		4/2.0 2.0	2.1 /840	065.1	3.28561
	1 17725	0/ 2°0	264/2°2	1.400	55041°5
0.16	4 1.17287	0.280	2.46264	1 500	3.00945 2.87866
0.16	6 1.22023	0.282	2.55272	1 550	2.75333
0.16	.8 1.31371	0.284	2.63963	1.600	2.63366
0.17	0 1.44585	0.286	2.72294	1.650	2.51968
0.17	2 1.60802	0.288	2.80227	1.700	2.41133
0.17	1.79107	0.290	2.87730	1.750	2.30849
1.0	6 1.98579	0.292	2.94776	1.800	2.21096
1.0	8 2.18343	0.294	3.01342	1.850	2.11853
		962.0	5 10000 E	006.1	2.05098
	71867	002.0	2012302	000 6	1 94807
0.18	6 2.85836	0.310	3 35149	2.500	72773.1
0.18	8 2.97198	0.320	3.39421	000 2	0.91888
0.19	0 3.05734	0.330	3,32392	3,500	0.68952
0.19	2 3.11337	0.340	3.16366	4.000	0.53519
61.0	4 3.14002	0.350	2.93888	4.500	0.42685
			2 101460		0.04460
0.20	0 3.05559	0.380	2.10878	6.000	0.24383
0.20	2 2.97981	0.390	1.84034	6.500	0.20836
0.20	4 2.88490	0.400	1.59652	7.000	0.18008
0.20	6 2.77405	0.410	1.38432	7.500	0.15716
0.20	8 2.65058	0.420	1.20789	8.000	0.13834
	8//1C.2 0	0.430	CU240.1	000.8	0.12270
0.21	4 2.23704	0.450	0.90300	100.000	06000.0
-	TALLA 19 Day			. K.	

Wp/Wa versus x for 20 db (cosine)" distribution. able 12.

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0.100 1.75043 0.216 1.98962 0.100 2.30799 0.226 1.78050 0.1104 2.317352 0.226 1.78050 0.1114 2.313652 0.226 1.47495 0.1116 2.313652 0.2330 1.47495 0.1116 2.313652 0.2336 1.47495 0.1120 2.313652 0.2340 1.46643 0.1121 2.313652 0.2340 1.46643 0.1122 1.793443 0.2340 1.45671 0.1128 2.313155 0.2340 1.35485 0.1128 1.79728 0.2441 0.2440 0.1128 1.5773 0.2441 1.45674 0.1128 1.5773 0.2441 1.45876 0.1128 2.01173 0.2541 1.43673 0.1128 2.01173 0.2544 1.41871 0.1286 1.66601 0.2740 0.2644 0.1128 2.01173 0.2740 0.2644 0.1128 2.01149	L	R.	•	×	N.		` X	a a
0.100 1.7043 0.216 1.99962 0.110 2.560743 0.2216 1.98654 0.111 2.57232 1.54045 0.111 2.517232 0.222 1.60623 0.111 2.517352 0.2316 1.54465 0.112 2.517232 0.2316 1.54693 0.112 2.517232 0.2316 1.55485 0.1120 1.79014 0.2316 0.2316 1.55485 0.1121 1.79172 0.2316 0.2316 1.35545 0.1122 1.55474 0.2316 1.35545 1.35545 0.1132 2.511083 0.248 1.35560 1.35561 0.1132 2.511083 0.248 1.35561 1.4181 0.1132 2.55210 0.248 1.35562 1.4181 0.1132 2.51113 0.248 0.248 1.4183 0.1132 2.5111 0.278 0.248 1.4183 0.1132 2.61833 0.278 0.264 1.4183 0.1132 2.618443 0.278 0.278 1.4183							•	-
0.1102 2.01799 0.222 1.78050 0.1112 2.5173852 0.2228 1.47495 0.1112 2.573852 0.2228 1.47495 0.1112 2.573852 0.2238 1.47495 0.1118 2.734815 0.2338 1.47495 0.1122 1.79014 0.2338 1.33099 0.1123 2.03315 0.2344 1.35565 0.1124 2.01773 0.2344 1.35566 0.128 2.01773 0.2344 1.35566 0.128 2.01773 0.2444 1.41817 0.1316 1.551713 0.2444 1.41767 0.1318 2.61677 0.2444 1.41767 0.1318 2.61677 0.2444 1.41767 0.144 2.481356 0.2546 1.41767 0.1318 2.61777 0.2444 1.4176 0.144 2.481356 0.2546 1.4176 0.1554 1.54149 0.2546 1.4176 0.144 2.481356 0.2726 2.01282 0.1564 1.54149 0.2766 </td <td>100</td> <td>1.75043</td> <td></td> <td>0.216</td> <td>1.98962</td> <td></td> <td>0.460</td> <td>1.101.1</td>	100	1.75043		0.216	1.98962		0.460	1.101.1
0.110 2.57535 0.224 1.66632 0.1114 2.31490 0.224 1.47495 0.1118 2.31315 0.230 1.47495 0.1120 1.57914 0.234 1.47495 0.1121 2.57535 0.231 1.47495 0.1120 1.57914 0.234 1.47495 0.1120 1.57914 0.2316 1.47495 0.1121 2.57515 0.2342 1.355487 0.1126 2.01173 0.2442 1.47495 0.1284 1.564413 0.2442 1.47495 0.1284 2.61677 0.2442 1.47495 0.1302 2.48356 0.2442 1.47495 0.1402 2.48356 0.2568 1.44776 0.1412 2.48356 0.272 2.48797 0.1412 2.48567 0.2568 1.4776 0.1422 2.48567 0.2568 1.4776 0.1422 2.45963 0.2440 1.4776 0.1524 1.55684 0.2568 1.4776 0.1526 1.45693 0.2786	201.	2.01799		0.218	1.88158		0.4.0	4001.I
0.1112 2.76174 0.226 1.5485 0.1112 2.31470 2.37852 0.228 1.42695 0.1112 2.31470 0.232 1.42695 0.1122 1.53315 0.233 1.42695 0.1122 1.53485 0.234 1.42695 0.1122 1.54443 0.234 1.42695 0.1128 2.01173 0.234 1.42695 0.1128 2.01173 0.240 1.42697 0.1128 2.01173 0.244 1.42697 0.1132 2.61516 0.244 1.45676 0.1132 2.61517 0.244 1.45676 0.1132 2.61517 0.244 1.45676 0.1134 2.6177 0.256 1.481776 0.1132 2.6173 0.2564 1.45673 0.1134 2.61743 0.2564 1.45673 0.1136 2.81736 0.2564 1.45673 0.1136 2.81736 0.2564 1.45673 0.1136 2.81736 0.2564 1.48174 0.1136 2.61739	+01.	1/040.2		0.22.0	00001.1	•	0.480	0761.1
0.1112 2.57232 0.228 1.47495 0.1122 2.57232 0.233 1.47495 0.1122 2.57233 0.234 1.35573 0.1123 1.56443 0.234 1.35573 0.1124 2.01315 0.234 1.35586 0.1128 1.563348 0.234 1.35586 0.1128 1.563348 0.234 1.35586 0.1128 2.61577 0.244 1.35586 0.1130 2.67577 0.244 1.35586 0.1131 2.61677 0.244 1.4786 0.1131 2.6177 0.254 1.4786 0.1140 2.67677 0.254 1.4786 0.1141 2.67677 0.254 1.62711 0.1142 2.67679 0.266 1.4776 0.1142 2.67641 0.254 1.67712 0.1152 1.54139 0.266 2.97866 0.1142 2.67631 0.266 2.97866 0.1154 1.54139 0.266 2.97879 0.1156 1.54139 0.274 2.672357	901.	201448		2220	1,58840		0.44.0	
0.1114 2.57232 0.230 1.42693 0.1114 2.31490 0.233 1.42693 0.1126 1.79014 0.233 1.47495 0.1126 1.57133 0.234 1.36545 0.1126 1.5713 0.234 1.36545 0.1130 2.6443 0.234 1.36546 0.1131 2.61443 0.244 1.4183 0.1132 2.61435 0.244 1.46647 0.1132 2.61435 0.244 1.46647 0.1132 2.61736 0.244 1.46647 0.1138 2.61837 0.244 1.46647 0.1146 2.61843 0.264 1.46647 0.1148 2.61843 0.264 1.46917 0.1148 2.61843 0.264 1.46917 0.1148 2.618433 0.264 1.46917 0.1148 2.618433 0.264 1.47495 0.1148 2.618433 0.264 1.47495 0.1148 2.618433 0.264 1.47495 0.1166 1.651447 0.264 1.7	0011	2 73050		10.00	22000.1			TORA I
1114 2.31490 0.235 1.42693 0.1128 1.79728 0.234 1.35520 0.122 1.79728 0.234 1.35550 0.128 1.79728 0.234 1.35550 0.128 1.79728 0.244 1.35550 0.130 2.61577 0.244 1.41831 0.131 2.61577 0.254 1.45873 0.132 2.61577 0.254 1.45873 0.133 2.61577 0.254 1.45873 0.136 2.65853 0.2556 1.458743 0.144 2.65633 0.2556 1.45763 0.150 2.55561 0.272 2.012475 0.155 1.55643 0.274 2.56383 0.156 1.555445 0.274 2.56439 0.156 1.555445 0.274 2.663707 0.156 1.55544 0.274 2.56439 0.156 1.55546 0.274 2.56739 0.158 1.55549 0.274 2.66739 0.158 1.555447 0.274 2.56739	112	2.57232		0.228	1.47495		0.520	1.6023
1116 2.03315 0.234 1.355713 0.122 1.58348 0.234 1.355713 0.126 1.58348 0.234 1.355713 0.126 1.58348 0.234 1.355713 0.128 1.58348 0.244 1.355713 0.128 2.01173 0.244 1.355713 0.130 2.48356 0.244 1.41831 0.131 2.6577 0.254 1.48756 0.131 2.65775 0.254 1.41831 0.142 2.65637 0.256 1.62711 0.144 2.76541 0.254 1.62711 0.150 1.91459 0.256 1.76985 0.151 0.256 0.274 2.69561 0.152 1.91459 0.266 2.01242 0.156 1.54139 0.274 2.55259 0.156 1.5433 0.274 2.69369 0.156 1.54139 0.274 2.69300 0.156 1.54139 0.274 2.69300 0.156 1.54139 0.266 2.17476	114	2.31490	•	0.230	1.42693		0.530	1.7323
1118 1.79014 0.234 1.35713 1128 1.9778 0.240 1.35585 1128 1.9778 0.244 1.35585 1138 2.25210 0.244 1.41831 1138 2.25510 0.244 1.41831 1138 2.61356 0.244 1.45874 1138 2.61356 0.244 1.45874 1138 2.61356 0.244 1.45874 1138 2.61356 0.244 1.45874 1138 2.61376 0.254 1.65717 1142 2.61376 0.254 1.65717 1148 2.61083 0.264 2.09756 1148 2.61083 0.276 2.09756 1156 1.5561 0.276 2.09756 1156 1.56768 0.276 2.75579 1156 1.56768 0.274 2.56969 1156 1.55616 0.276 2.91275 1168 1.56768 0.274 2.56969 1156 1.56768 0.274 2.56959 1156	.116	2.03315		0.232	66062.1		0.540	1,8683
1122 1.63233 0.238 1.35550 1124 1.79728 0.244 1.35550 1128 1.79728 0.244 1.35550 1130 2.01173 0.244 1.41831 1131 2.01173 0.244 1.45674 1131 2.6757 0.244 1.45674 1134 2.6757 0.256 1.4676 1140 2.6757 0.256 1.4766 1141 2.65853 0.256 1.76961 1152 1.56852 0.256 1.76961 1152 1.56853 0.256 1.76976 1152 1.56853 0.266 2.97875 1154 0.266 0.274 2.55596 1155 1.5518 0.274 2.55526 1155 1.5518 0.274 2.55526 1155 1.5518 0.274 2.55529 1156 1.5518 0.274 2.55529 1156 1.5518 0.274 2.55529 1156 1.5518 0.274 2.55529 1158	118	41067.1		0.234	1.36713		0.550	2.0083
1122 1.58348 0.234 1.35485 1126 2.01173 0.244 1.36565 1130 2.67677 0.244 1.36565 1131 2.67677 0.244 1.36565 1136 2.67677 0.244 1.41831 1136 2.67677 0.244 1.46871 1136 2.67677 0.2554 1.46871 0.144 2.67677 0.2561 1.56402 0.144 2.67677 0.2561 1.65711 0.144 2.67677 0.2561 1.66701 0.144 2.67677 0.2561 1.75968 0.156 1.54139 0.266 2.01247 0.156 1.54139 0.266 2.09541 0.156 1.54139 0.266 2.01247 0.156 1.54139 0.272 2.01247 0.156 1.54139 0.274 2.656405 0.156 1.54139 0.266 2.01247 0.156 1.54139 0.266 2.01247 0.158 2.07616 0.2726 2.01269	120	1.63233		0.236	1.35520		0.560	2.1503
1.6443 0.240 1.5556 1.172 1.9778 0.244 1.45873 1.132 2.25210 0.244 1.45873 1.138 2.61083 0.244 1.45873 1.138 2.61083 0.244 1.45873 1.138 2.61083 0.244 1.45874 1.140 2.61083 0.254 1.45874 1.141 2.61083 0.2554 1.65711 1.141 2.61083 0.2554 1.65711 1.144 2.61083 0.2554 1.65711 1.144 2.61083 0.256 1.755640 1.1556 1.55641 0.2564 1.76542 1.1564 2.65833 0.264 2.01242 1.1556 0.2544 0.264 2.18375 1.156 1.55644 0.274 2.55259 1.156 1.5564 0.276 2.18375 1.156 1.5547 0.276 2.18375 1.156 1.5547 0.276 2.55250 1.176 2.5549 0.276 2.5756403 1	.122	1.58348		0.238	1.35485		0.570	2.2927
1.126 1.79728 0.242 1.41831 1.128 2.61173 0.244 1.45678 1.136 2.67677 0.244 1.45678 1.136 2.67677 0.246 1.45678 1.140 2.67677 0.256 1.45678 1.141 2.67677 0.256 1.45678 1.141 2.65853 0.264 2.67677 1.142 2.65853 0.256 1.6701 1.148 2.65853 0.264 2.09786 1.148 2.65863 0.264 2.09786 1.156 1.50186 0.264 2.09786 1.158 1.56186 0.274 2.650307 1.156 1.56186 0.274 2.75576 1.170 2.65863 0.274 2.75576 1.170 2.67025 0.274 2.75579 1.166 1.56186 0.274 2.67048 1.177 2.67025 0.274 2.67048 1.177 2.61739 0.274 2.67048 1.177 2.01747 0.274 2.67048	124	1.64443	·	0.240	1.36565		0.580	2.4341
1128 2.01173 0.244 1.41873 1134 2.67677 0.248 1.56402 1136 2.67677 0.256 1.56402 1136 2.67677 0.256 1.56402 1142 2.67677 0.256 1.56402 1148 2.67677 0.256 1.62711 1148 2.67677 0.256 1.6601 1150 1.91459 0.256 1.928875 1151 1.91459 0.266 2.09756 1152 1.91459 0.266 2.09756 1152 1.91459 0.266 2.09756 1152 1.91459 0.266 2.09756 1156 1.55711 0.266 2.09756 1158 1.56171 0.274 2.55529 1158 1.55611 0.274 2.55529 1172 2.07447 0.274 2.68080 1166 1.54139 0.274 2.55529 1172 2.07447 0.274 2.55529 1172 2.07447 0.274 2.57559 1	.126	1.79728		0.242	1.38703		0.590	2.5735
1130 2.25210 0.246 1.45675 1131 2.61083 0.254 1.56763 1140 2.61083 0.254 1.56763 1141 2.61083 0.255 1.56763 1141 2.61083 0.256 1.56763 1142 2.61083 0.256 1.56763 1144 2.61083 0.256 1.66711 1150 2.61753 0.256 1.92776 1154 1.75568 0.266 2.01242 155 1.75768 0.276 2.01242 156 1.75768 0.276 2.75575 155 1.75768 0.276 2.75575 156 1.75768 0.276 2.575663 156 1.54139 0.278 2.60300 166 1.75551 0.278 2.575643 166 1.54139 0.278 2.69337 166 1.54139 0.278 2.69337 177 2.15549 0.278 2.55250 178 2.75549 0.276 2.57373 178	.128	2.01173		0.244	1.41831		0.600	2.7097
1132 2.48356 0.248 1.5073 1134 2.867677 0.255 1.56402 1142 2.86533 0.255 1.56402 1142 2.86533 0.255 1.596601 1142 2.86533 0.255 1.59863 1144 2.48840 0.255 1.92889 2.65853 0.266 2.09756 1.92889 1152 1.791459 0.256 2.1835516 1156 1.751459 0.274 2.555926 1156 1.50186 0.274 2.555926 1166 1.50186 0.274 2.555926 1166 1.50186 0.274 2.555926 1166 1.50186 0.274 2.555926 1170 1.62711 0.274 2.555926 1166 1.50186 0.274 2.65030 11717 2.01743 0.274 2.65030 11717 2.01743 0.274 2.555926 1177 1.62714 0.274 2.65030 1177 1.62714 0.274 2.61309	.130	2.25210		0.246	1.45878		0.650	3,3209
1134 2.67677 0.250 1.56402 1142 2.86527 0.255 1.769601 1142 2.86527 0.255 1.769601 1142 2.86527 0.256 1.769601 1142 2.86527 0.256 1.769601 1148 2.678938 0.256 1.97869 1154 1.91459 0.266 2.01782 1156 1.91459 0.266 2.01742 1156 1.514139 0.266 2.01742 1156 1.514139 0.274 2.55559 1156 1.54139 0.274 2.560300 1156 1.54139 0.274 2.55529 1158 1.54139 0.274 2.55529 1166 1.54139 0.274 2.55529 1172 2.07054 0.280 2.01509 1172 2.07054 0.274 2.562300 1172 2.07054 0.274 2.56230 1172 2.07034 0.274 2.56230 1172 2.0703 0.274 2.56030	.132	2.48356		0.248	1.50763	•	0.700	3.7874
136 2.81083 0.254 1.62711 144 2.85735 0.256 1.76961 144 2.857435 0.256 1.767691 146 2.481435 0.256 1.769755 154 2.657633 0.2254 1.847755529 155 1.75368 0.2266 2.928435529 155 1.75368 0.2266 2.755529 155 1.75368 0.2766 2.755529 156 1.54139 0.2766 2.75529 156 1.54376 0.2766 2.75529 156 1.54376 0.2766 2.75529 156 1.54376 0.2766 2.75529 156 1.54347 0.280 2.75693 166 1.75376 0.2864 3.01669 176 2.95371 0.276 2.76931 178 2.95371 0.2964 3.26914 177 2.95371 0.2966 3.26914 178 2.95394 0.2966 3.2692314 <t< td=""><td>134</td><td>2.67677</td><td></td><td>0.250</td><td>1.56402</td><td></td><td>0.750</td><td>4.1063</td></t<>	134	2.67677		0.250	1.56402		0.750	4.1063
.138 2.87436 0.256 1.6960 .144 2.48653 0.256 1.92686 .144 2.48653 0.256 1.92686 .152 1.92641 0.256 1.92686 .152 1.92641 0.256 2.09756 .152 1.75368 0.266 2.9756 .156 1.75368 0.272 2.03756 .156 1.75368 0.274 2.55529 .159 1.62711 0.274 2.55529 .150186 0.274 2.55520 .150183 0.274 2.55309 .166 1.45913 0.274 2.55309 .166 1.454547 0.274 2.55309 .170 1.62713 0.274 2.55309 .166 1.454547 0.286 2.55309 .1717 2.91609 0.274 2.55309 .166 1.73651 0.274 2.54397 .172 2.0733 0.274 2.55309 .173 1.87613 0.274 2.54397 .178 2.17801 <t< td=""><td>.136</td><td>2.81083</td><td></td><td>0.252</td><td>1.62711</td><td></td><td>0.800</td><td>4.2965</td></t<>	.136	2.81083		0.252	1.62711		0.800	4.2965
1140 2.86527 0.256 1.76985 1142 2.86527 0.256 1.76975 1148 2.678938 0.266 2.01742 1154 2.678938 0.266 2.01742 1154 2.69641 0.266 2.01742 1154 1.91459 0.266 2.01742 1154 1.91459 0.266 2.01742 1154 1.5711 0.266 2.03766 1.54139 0.274 2.613969 1.5611 1.5714 0.274 2.613975 1.5611 0.274 2.613975 0.266 1.5613 0.280 2.43975 0.269 1.56143 0.280 2.43975 0.266 1.56143 0.280 2.43975 0.2604 1.66 1.56146 0.280 3.07046 1.772 2.07905 0.2943 3.07046 1.778 2.17801 0.294 3.16504 1.778 2.07314 0.296 3.07046 1.778 2.07313 0.294 3.17036 1.778 <td>.138</td> <td>2.87436</td> <td></td> <td>0.254</td> <td>1.69601</td> <td></td> <td>0.850</td> <td>4.3835</td>	.138	2.87436		0.254	1.69601		0.850	4.3835
142 2.78938 0.258 1.84775 1144 2.48840 0.264 2.01245 155 1.91459 0.266 2.01245 154 2.48840 0.266 2.01245 155 1.91459 0.266 2.01245 154 1.75368 0.276 2.01245 156 1.54139 0.276 2.43575 156 1.54139 0.278 2.55259 156 1.54139 0.278 2.55259 156 1.54139 0.278 2.56963 166 1.54139 0.286 2.75547 156 1.54547 0.286 2.75599 166 1.54547 0.286 2.69300 170 2.37660 0.288 2.75599 1717 2.37660 0.294 3.12014 174 2.172514 0.294 3.12014 175 2.4894 0.294 3.12014 176 2.37601 0.2917 3.70169 177 2.3601 0.278 2.95706 186 <td< td=""><td>.140</td><td>2.86527</td><td></td><td>0.256</td><td>1.76985</td><td>•</td><td>0.900</td><td>4.391</td></td<>	.140	2.86527		0.256	1.76985	•	0.900	4.391
144 2.455853 0.260 1.75368 1150 2.29641 0.266 2.19459 155 1.75368 0.266 2.18355 156 1.75368 0.276 2.45569 156 1.75368 0.276 2.09756 156 1.75368 0.276 2.09756 166 1.49963 0.274 2.55259 166 1.49963 0.274 2.560300 166 1.49963 0.274 2.560307 166 1.55747 0.274 2.560307 166 1.75574 0.280 2.60307 176 1.73651 0.274 2.560307 178 2.07447 0.280 2.60307 178 1.73651 0.294 3.01609 178 2.0733 0.294 3.01609 178 2.17801 0.294 3.1609 178 2.17801 0.294 3.1609 178 2.17801 0.294 3.1609 178 2.17801 0.294 3.1609 188	.142	2,78938		0.258	1.84776		0.020	1245.4
148 2.99841 0.266 2.09756 154 1.91459 0.276 2.18355 154 1.91459 0.276 2.43956 154 1.75468 0.276 2.43955 155 1.75468 0.276 2.55250 156 1.50186 0.278 2.55250 156 1.50186 0.278 2.55369 156 1.50186 0.278 2.55369 156 1.50186 0.278 2.55370 156 1.55186 0.278 2.55370 166 1.5188 3.01609 2.75547 177 2.07860 0.288 2.75547 178 2.07861 0.294 3.01609 177 2.07861 0.294 3.1504 178 2.17801 0.296 3.27054 178 2.17801 0.294 3.1504 178 2.17801 0.294 3.1504 178 2.17801 0.296 3.27039 178 2.17801 0.296 3.1504 188 3.03	.144	2.65855		0.250	68826.1		1.000	
152 1.91459 0.266 2.17556 154 1.57368 0.276 2.55559 156 1.57368 0.277 2.55559 156 1.54139 0.278 2.55559 156 1.54139 0.274 2.55559 156 1.54139 0.274 2.55547 156 1.54547 0.280 2.43755 156 1.54547 0.280 2.55599 1772 2.078025 0.286 2.95790 1772 2.078025 0.286 3.07046 1772 2.078025 0.288 3.07046 1772 2.078025 0.299 3.12014 1772 2.07333 0.299 3.12014 178 2.178015 0.294 3.12014 178 2.178043 0.203 3.12014 178 2.178015 0.294 3.12014 178 2.178015 0.30314 0.3014 186 3.00314 0.3030 3.31650 188 3.00314 0.310 3.31650 188 </td <td>-140</td> <td>2 20C C</td> <td></td> <td></td> <td></td> <td>-</td> <td></td> <td></td>	-140	2 20C C				-		
152 1.914769 0.276 2.55259 154 1.56711 0.276 2.55259 156 1.54179 0.277 2.55259 156 1.54547 0.278 2.55259 156 1.54547 0.278 2.55259 166 1.54546 0.278 2.55259 158 1.54547 0.2882 2.55259 166 1.55576 0.2882 2.55599 174 2.15601 0.2882 2.95720 174 2.15559 0.2882 3.01669 174 2.15601 0.288 3.01669 174 2.15559 0.288 3.01699 175 2.02025 0.2943 3.12014 174 2.17601 0.299 3.12014 175 2.182 0.2914 3.12014 174 2.178 0.2914 3.12014 178 2.17890 0.2914 3.12014 178 2.178 0.2914 3.12014 186 2.03314 0.2910 3.19060 194	. 148	1 40620 2		0.266	00/60.2		1.150	
156 1.753563 0.272 2.43955 156 1.62711 0.274 2.55295 156 1.49963 0.274 2.55295 156 1.49963 0.274 2.55295 156 1.50186 0.274 2.55295 156 1.550186 0.274 2.55295 156 1.550186 0.274 2.55293 156 1.550186 0.278 2.55397 156 1.73651 0.286 2.75547 170 1.62714 0.286 2.75547 1717 2.087055 0.286 2.75547 174 2.07805 0.294 3.01609 177 2.17801 0.296 3.07046 178 2.43366 0.294 3.1604 178 2.43366 0.294 3.16504 178 2.43945 0.294 3.16504 188 3.00314 0.3003 3.2604 188 3.03713 0.310 3.3703 196 2.94435 0.300 2.99787 198 <	001.	69660 2						
156 1.5711 0.276 2.52250 156 1.50186 0.274 2.52250 156 1.50186 0.276 2.68080 156 1.5516 0.280 2.52250 166 1.5518 0.274 2.55250 176 1.5751 0.280 2.58260 177 2.17601 0.286 2.95720 177 2.17801 0.286 3.01609 177 2.17801 0.292 2.89397 178 2.17801 0.296 3.07604 178 2.17801 0.294 3.16504 178 2.17801 0.294 3.16704 178 2.17801 0.294 3.17046 178 2.17801 0.294 3.17046 178 2.17801 0.294 3.17046 178 2.0733 0.294 3.17046 186 3.00314 0.300 3.7037 188 3.03314 0.300 3.7037 190 3.03314 0.300 3.7037 198 3.03310 </td <td></td> <td>75.169</td> <td></td> <td>0.270</td> <td>25529</td> <td></td> <td>1.250</td> <td>3.5455</td>		75.169		0.270	25529		1.250	3.5455
158 1.54139 0.274 2.52250 166 1.49963 0.276 2.60300 166 1.54547 0.288 2.60300 166 1.55516 0.288 2.69300 170 1.52576 0.286 2.69300 1717 2.172025 0.286 3.0060 177 2.178025 0.298 3.00160 177 2.178025 0.298 3.12014 178 2.178025 0.299 3.12014 178 2.178025 0.299 3.12014 178 2.178015 0.291 3.12014 178 2.178015 0.293 3.12014 186 2.75599 0.294 3.12014 188 2.03314 0.290 3.13001 188 2.03314 0.310 3.31650 188 2.03314 0.310 3.31650 188 2.04379 3.30179 3.1703 190 3.03314 0.330 3.18071 191 3.03319 0.330 3.31877 192	156	1.62711		0.272	2.43975		1.300	3.3934
.160 1.49963 0.276 2.60300 .162 1.50186 0.278 2.56080 .164 1.55547 0.282 2.82663 .170 1.62576 0.282 2.82663 .172 2.07054 0.286 2.75547 .172 2.07054 0.286 2.95540 .172 2.02025 0.286 2.955720 .174 2.17601 0.286 2.955720 .174 2.17601 0.290 3.07646 .174 2.17561 0.290 3.17649 .178 2.17601 0.290 3.17649 .180 2.48943 0.290 3.1504 .180 2.65380 0.2310 3.27035 .182 2.94425 0.310 3.31570 .188 3.03714 0.310 3.31570 .192 3.03714 0.310 3.31570 .193 3.03714 0.310 3.31570 .193 3.03714 0.310 3.31570 .193 3.03714 0.310 3.31570 <td< td=""><td>158</td><td>1.54139</td><td>1</td><td>0.274</td><td>2.52250</td><td></td><td>1,350.</td><td>3.2449</td></td<>	158	1.54139	1	0.274	2.52250		1,350.	3.2449
.162 1.50186 0.278 2.68080 .164 1.54547 0.280 2.75547 .166 1.73651 0.280 2.75547 .170 1.67054 0.286 2.95547 .171 1.67054 0.286 2.95547 .172 2.08055 0.286 2.95720 .174 2.17801 0.296 3.07646 .178 2.13560 0.290 3.07646 .178 2.433460 0.294 3.1604 .180 2.433460 0.294 3.1604 .182 2.433460 0.294 3.1504 .182 2.433460 0.203 3.1504 .182 2.94425 0.310 3.24015 .184 2.94425 0.310 3.31570 .196 3.00314 0.310 3.31570 .196 3.03713 0.310 3.31570 .196 2.94435 0.310 3.31570 .196 2.94249 0.310 2.99713 .196 2.94249 0.340 2.99713 .	.160	1.49963		0.276	2.60300		1.400	3.1011
.164 1.54547 0.280 2.75547 .170 1.6551 0.288 2.95397 .172 2.17801 0.286 3.01609 .172 2.17801 0.286 3.07666 .172 2.17801 0.286 3.07046 .172 2.17801 0.292 3.07046 .176 2.33660 0.292 3.07046 .178 2.43943 0.294 3.16504 .180 2.65099 0.294 3.16504 .182 2.65399 0.294 3.16504 .182 2.65399 0.294 3.16504 .182 2.94425 0.310 3.34874 .186 3.00314 0.310 3.34874 .190 3.03314 0.310 3.34874 .191 3.03314 0.310 3.34874 .192 3.03314 0.310 3.34874 .193 3.03319 0.310 3.34874 .194 3.03319 0.310 3.34874 .194 3.03319 0.320 3.370371 .	.162	1.50186		0.278	2.68080		1.450	2,9626
.166 1.52576 0.2882 2.8265 .172 2.12025 0.286 2.95720 .174 2.17801 0.286 3.01609 .174 2.17801 0.286 3.02046 .174 2.17801 0.286 3.01609 .175 2.17801 0.290 3.01609 .178 2.17801 0.294 3.12014 .180 2.5599 0.296 3.26014 .182 2.48943 0.294 3.12014 .182 2.48943 0.294 3.26034 .183 2.75599 0.294 3.27015 .184 2.75599 0.230 3.24015 .186 2.9453 0.310 3.24073 .190 3.00314 0.310 3.24073 .191 3.00314 0.310 3.24703 .192 3.03318 0.310 3.24874 .193 3.03318 0.310 3.21874 .194 3.03319 0.350 2.95879 .194 3.03316 0.350 2.91478 .19	.164	1.54547		0.280	2.75547		1.500	2.850
.170 2.05054 0.2864 2.0704 .174 2.17501 0.2864 3.01609 .174 2.13501 0.286 3.01609 .176 2.33560 0.292 3.15046 .180 2.65080 0.299 3.01609 .180 2.65080 0.292 3.15046 .181 2.48943 0.296 3.26504 .182 2.65080 0.299 3.15046 .182 2.94425 0.298 3.27033 .186 2.94425 0.310 3.27033 .192 3.03734 0.310 3.19908 .192 3.03734 0.310 3.19988 .192 3.03734 0.310 3.19988 .192 3.03734 0.330 3.19988 .192 3.03734 0.330 3.19988 .192 3.03734 0.330 3.19988 .192 3.03734 0.330 3.19988 .193 2.94249 0.350 2.79147 .203 2.94249 0.340 2.79147	.166	1.62576		0.282	2.82663		0003 1	
172 2.17801 0.288 3.07046 174 2.17801 3.17016 3.07046 178 2.43366 0.292 3.17016 188 2.43366 0.292 3.17016 188 2.43366 0.294 3.07046 188 2.43366 0.294 3.17016 188 2.43366 0.294 3.17016 188 2.94425 0.310 3.24015 196 3.00314 0.310 3.24015 196 3.03714 0.310 3.34015 196 3.03714 0.310 3.34015 196 3.03714 0.310 3.34015 196 3.03714 0.310 3.34015 196 3.03716 0.320 2.99778 197 3.03715 0.340 2.99718 208 2.94249 0.360 2.99739 208 2.94249 0.360 1.98736 208 2.94249 0.360 1.98736 208 2.94249 0.360 1.798473 208 <t< td=""><td>.168</td><td>1.75651.1</td><td></td><td>0.284</td><td><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre><pre></pre></td><td></td><td>1 650</td><td>0040 0</td></t<>	.168	1.75651.1		0.284	<pre></pre>		1 650	0040 0
176 2.17801 178 2.17801 180 2.33660 182 2.45599 184 2.75599 186 2.75599 186 2.75599 186 2.75599 186 2.75599 186 2.75599 186 2.75599 186 2.94425 186 3.00314 190 3.1300 190 3.0314 191 3.0314 192 3.0314 193 3.0314 194 3.0314 195 3.0314 196 3.0314 197 3.1900 198 3.03314 198 3.03314 198 3.03314 198 3.03318 198 3.03319 198 3.03319 200 3.34874 2019 3.350 2019 3.350 2019 3.350 2019 3.360 2014		1.87004			101609		002	01090
176 2.33660 0.292 3.12014 178 2.48943 0.294 3.12014 180 2.48943 0.294 3.16503 182 2.75599 0.299 3.24015 184 2.94425 0.300 3.27034 186 3.094425 0.310 3.24015 198 3.094425 0.310 3.34874 198 3.03734 0.310 3.19080 192 3.03734 0.310 3.19764 192 3.03734 0.330 3.19788 192 3.03734 0.340 2.99778 193 3.03714 0.340 2.99778 194 3.0370 2.99778 2.99778 194 3.0370 2.99778 2.99778 194 3.0370 2.99778 2.99778 196 2.94749 0.370 2.98778 198 2.94249 0.370 2.98778 200 2.94549 0.370 1.975819 2014 2.78194 0.370 1.75819 2018	2/ 1.	2.17801	•	0.290	3.07046		1.750	2.258
.178 2.48943 0.294 3.16503 .180 2.753080 0.296 3.27034 .182 2.9514 0.310 3.27033 .186 2.94425 0.310 3.27033 .186 2.94425 0.310 3.27033 .196 2.94425 0.310 3.27033 .196 2.94425 0.310 3.27033 .192 3.03734 0.310 3.19080 .192 3.03734 0.310 3.19080 .192 3.03734 0.350 2.99783 .192 3.03738 0.350 2.99786 .192 3.03719 0.350 2.99786 .192 3.03719 0.350 2.99786 .196 2.94249 0.370 2.98776 .200 2.94249 0.370 2.758197 .201 2.94249 0.370 2.758197 .202 2.78194 0.350 1.778875 .203 2.78194 0.360 1.758175 .203 2.5734 0.340 1.758175 <	.176	2.33660		0.292	3.12014		1.800	2.161
.180 2.63080 0.296 3.2004 .182 2.95599 0.309 3.24015 .184 2.94425 0.310 3.24015 .196 3.00314 0.310 3.24015 .190 3.00314 0.310 3.24015 .192 3.00314 0.310 3.24015 .192 3.03714 0.310 3.24015 .192 3.03714 0.310 3.24015 .192 3.03714 0.310 3.24015 .194 3.03718 0.310 2.9978 .194 3.03752 0.340 2.9978 .194 3.03752 0.350 2.9978 .195 2.94249 0.370 2.59147 .200 2.94249 0.360 1.98736 .201 2.94234 0.350 1.98736 .202 2.78194 0.370 2.23877 .203 2.55767 0.360 1.75817 .203 2.55767 0.410 1.7314 .203 2.23121 0.450 1.17314 .212 </td <td>.178</td> <td>2.48943</td> <td></td> <td>0.294</td> <td>3.16503</td> <td></td> <td>1.850</td> <td>2,0695</td>	.178	2.48943		0.294	3.16503		1.850	2,0695
.182 2.75599 0.298 3.224015 184 2.94425 0.310 3.24874 186 2.94425 0.310 3.34874 190 3.00314 0.320 3.196874 192 3.00314 0.320 3.196874 194 2.94249 0.350 2.99778 194 2.94249 0.350 2.9778 196 2.94249 0.350 2.9778 200 2.86960 0.370 2.23878 200 2.86960 0.370 1.75819 200 2.86960 0.380 1.75819 200 2.86960 0.390 1.75819 201 2.96736 0.410 1.75819 208 2.45736 0.410 1.75819 208 2.45736 0.410 1.75819 208 2.45736 0.420 1.75819 208 2.45736 0.420 1.75819 208 2.45736 0.420 1.75819 208 2.45736 0.420 1.75819 208 2.52121 0.420 1.7314	.180	2.63080		0.296	3.20504		1.900	1.982
.186 2.981.34 0.310 3.4874 .186 3.00314 0.320 3.31570 .192 3.03718 0.320 3.31670 .192 3.03718 0.320 3.319570 .192 3.03718 0.350 2.75068 .194 3.03352 0.350 2.750668 .194 3.03752 0.350 2.750668 .196 2.997793 0.350 2.75068 .200 2.96749 0.350 2.57879 .201 2.96749 0.350 2.58797 .200 2.86960 0.390 1.798371 .201 2.86950 0.390 1.75819 .202 2.68234 0.410 1.75877 .203 2.57367 0.410 1.75877 .206 2.57367 0.410 1.73371 .208 2.57367 0.410 1.73371 .212 2.52121 0.450 1.17314 .212 2.22121 0.450 1.03568	.182	2.75599		0.298	3,24015		0000 0	006.1
198 3.03734 0.320 3.1570 192 3.03734 0.330 3.19680 194 3.03734 0.330 3.19680 194 3.03738 0.350 2.75068 194 3.03752 0.350 2.75068 194 3.03738 0.350 2.76068 194 3.0370 2.99793 0.370 2.99793 196 2.99793 0.370 2.98736 0.370 2.98736 200 2.94249 0.370 2.98736 0.370 2.98736 201 2.94249 0.370 2.98736 0.350 1.75819 201 2.94249 0.330 1.75819 1.75819 202 2.78194 0.330 1.75819 2.58179 203 2.57357 0.400 1.55819 2.56501 204 2.457357 0.410 1.75819 2.51212 212 2.22121 0.430 1.17573 2.514 213 2.22121 0.450 1.0358 2.5167	.184	2.86154		0.500	5.01 2.C			244
192 3.03738 0.330 3.19080 192 3.04719 0.340 2.9978 194 3.04719 0.340 2.9978 194 2.94249 0.350 2.95046 198 2.94249 0.350 2.50147 198 2.94249 0.370 2.23878 200 2.786960 0.340 1.958179 201 2.78194 0.370 2.258179 202 2.78194 0.370 1.758179 203 2.68234 0.330 1.758173 204 2.68234 0.400 1.558173 204 2.57367 0.400 1.558173 208 2.57367 0.400 1.558173 208 2.57367 0.400 1.558173 208 2.57367 0.410 1.33714 212 2.22121 0.450 1.17314 212 2.22121 0.450 1.03569	001.	01200 2		0.320	3.31570		3.000	0.891
.192 3.04719 0.340 2.99778 .194 2.90352 0.350 2.90766 .194 2.903522 0.350 2.76068 .196 2.94249 0.370 2.59147 .200 2.94249 0.370 2.23878 .200 2.94249 0.330 1.958179 .200 2.78690 1.756179 1.9581736 .201 2.780 1.758173 1.9581736 .202 2.86960 0.3300 1.758173 .203 2.68234 0.400 1.758173 .206 2.557367 0.410 1.75877 .208 2.457367 0.420 1.755877 .208 2.457367 0.420 1.7514 .212 2.22121 0.430 1.17314 .212 2.22121 0.450 1.0356	061	3.03738		0.330	3.19080	÷	3.500	0.668
.194 3.03352 0.350 2.76068 .196 2.99793 0.350 2.50147 .198 2.99793 0.350 2.50147 .200 2.86960 0.370 2.53878 .202 2.78194 0.390 1.98736 .203 2.78194 0.390 1.75819 .204 2.68234 0.390 1.75819 .204 2.68234 0.400 1.55879 .205 2.78134 0.400 1.55879 .206 2.68234 0.410 1.35579 .212 2.45878 0.410 1.36508 .212 2.22121 0.430 1.1673 .212 2.22121 0.450 1.03568	192	3.04719		0.340	2.99778		4.000	0.510
.196 2.99793 0.360 2.50147 .208 2.94249 0.370 2.23878 .200 2.94249 0.370 2.231878 .201 2.94249 0.370 1.98736 .202 2.78194 0.390 1.75819 .203 2.68234 0.390 1.75819 .204 2.68234 0.400 1.55879 .206 2.57357 0.410 1.3571 .208 2.45878 0.420 1.25507 .203 2.34043 0.430 1.1573 .212 2.22121 0.450 1.0356 .212 2.22121 0.450 1.0356	194	3,03352		0.350	2.76068		4.500	0.4130
.198 2.94249 0.370 2.25148 .200 2.94249 0.380 1.75819 .202 2.78194 0.390 1.75819 .204 2.68234 0.390 1.75819 .204 2.68234 0.390 1.75819 .204 2.68234 0.300 1.55819 .206 2.57357 0.410 1.39371 .208 2.45878 0.420 1.255371 .208 2.34043 0.430 1.1574 .212 2.22121 0.450 1.0356147 .212 2.22121 0.450 1.0356147	.196	2.99793	•	0.360	2.50147		5 000	0.336
.200 2.789560 0.390 1.75619 .202 2.789561 0.390 1.75619 .204 2.68234 0.390 1.75619 .205 2.57367 0.400 1.55619 .206 2.57367 0.400 1.55619 .208 2.45787 0.410 1.39371 .208 2.45788 0.420 1.25550 .212 2.34043 0.430 1.17314 .212 2.22121 0.440 1.03567	198	2.94249	•	0.2.0	8/952.2	•		
200 2.68234 0.400 1.55879 204 2.57367 0.410 1.39371 206 2.57367 0.410 1.39371 208 2.45878 0.420 1.25508 208 2.45878 0.420 1.25508 212 2.34043 0.430 1.17314 212 2.22121 0.450 1.03568 212 2.22121 0.450 1.0358	002	20102		0.005	0010201		500	102.0
206 2.57357 0.410 1.3377 2.206 2.45878 0.420 1.26508 2.45878 0.420 1.26508 2.126508 2.212 2.2212 0.440 1.11573 2.12 2.2212 0.450 1.0355 0.450 1.0358		4610/°2		065.0	1 55879		000.7	0.1740
208 2.45878 0.420 1.26508 2.45878 0.430 1.17514 2.212 2.22121 0.440 1.11673 2.12 2.22121 0.450 1.09368	402	5 57767		0.410	17595.1	,	7.500	0.151
210 2.34043 0.430 1.17314 212 2.22121 0.440 1.11673 214 2.12355 0.450 1.0358	208	2.45878		0.420	1.26508		8.000	0.133
212 2.22121 0.440 1.11673 214 2.10355 0.450 1.09368	210	2.34043		0.430	1.17314		8.500	0.1185
.21▲ 2.10355 0.450 1.09368	-212	2.22121		0.440	1.11673	•	000.6	0.1056
	.214	2.10355	•	0.450	1.09368		100.000	0000

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0.100	0.31878	0.216	2.92178	0.460	0.58036
0.102	0.66152	0.218	2.68614	0.470	0.45895
0.104	1.52405	0.220	2.44616	0.480	0.37679
0.106	2.57183	0.222	2.20618	0.490	0.33095
0.108	3,46943	0.224	- 1.97019	0.500	0.3180
0110	3.97989	0.226	1.74176	0.510	0.33462
0.112	4.00826	0.228	1.52402	0.520	0.37703
411.0	10565.5	0.230	1.31967	0.530	0.44176
	2 01500	0.252	1.15098	0.240	16626.0
	060000 T	0.276	08666.0	0 cc. 0	11029°0
0.122	0.66296	0.238	0.67527	0.570	0.8604
0.124	0.35667	0.240	0.56365	0.580	1166.0
0.126	0.35682	0.242	0.47305	0.590	1.12756
0.128	0.63609	0.244	0.40351	0.600	1.26783
0.130	1.12955	0.246	0.35482	0.650	1.97606
0.132	1 . /5145	0.248	0.52655	0./00	2.6112
	2 02514	00210	06461 0		
	3.50015	0.254	52525°0	0.850	TABAF
0.140	3.87449	0.256	25000		100.1
0.142	4.04181	0.258	0.46219	0.950	3.97454
0.144	4.02838	0.260	0.53717	1,000	3.98580
0.146	3.84975	0.262	0.62516	1.050	3.95114
0.148	3.53427	0.264	0.72482	1.100	3.88314
0.150	3.11831	0.266	0.83480	1.150	3.79163
201.0	2.64183	0.268	5/555.0	1.200	3.68420
0 . 104	2.1444B		1 08029	002.1	5,00000
	1.22717	77 C U	1 35107	350	
0.160	0.86218	0.276	149281	400	19091 E
0.162	0.58467	0.278	1.63721	1.450	3.06611
0.164	0.40429	0.280	1.78317	1.500	2.94395
0.166	0.32404	0.282	1.92964	1.550	2.82528
0.168	0.34117	0.284	2.07566	1.600	2.71065
0.170	0.44812	0.286	2.22031	1 650	2.60039
2/1.0	0.653/2	982.0	2.362/6	1 /00	
0 - 1 / 4	0.00000	062.0		007.1	0000000
0.178	0001511	APC.0	2.76963	1 .850	2.20516
0.180	1.87240	0.296	2.89635	006.1	2.11760
0.182	2.22970	0.298	3.01775	1,950	2.03431
0.184	2.57792	0.300	3.13339	2.000	1.95510
0.186	2.90554	0.310	3.61457	2,500	1.34879
0.188	3.20295	0.320	3,91972	3,000	02016.0
			4 02104		
194	3.84768	0.350	3.86467	4 500	0.45585
961.0	3.96759	0.360	3.60894	5.000	0.3720
0.198	4.03808	0.370	3.28563	5.500	0.30923
0.200	4.06022	0.380	2.92281	6.000	0.26096
202.0	4.05629	065.0	0444C.V	000 1	
0 204	10536.5		1 81799	7.500	0.16837
802.0	3,72394	0.420	1.48760	8,000	0.14824
0.210	3.55462	0.430	1.19792	8,500	0.13150
0.212	3.36105	0.440	0.94921	000.6	0.11744
0.214	3.14839	0.450	0.74334	100.000	960000
•	Table 14. Th/L	T AURTAN OL	TOT 5 db Costor	a distribution	6

		72191.1	1 06454	1.05074	1.06295	1.09806	1.15301	1.22481	COUIC.1	1 51424	1.62743	1.74557	1.86692	1.99001	26166.5	3.50367	3.77792	3.94640	4.02888	4.04462	3.93974	3.84365	3.73045	3.60646	5.4/644 7 7/782	22110	3.08060	2.95297	2.82930	2.1014	2.48648	2.38217	2.28285	2.09868	2.01349	1.93266	1.85597	0.91847	0.69020	0.53621	0.42792	0.24910	0.24469	0.20915	0.18078	08/01-0	0.123222	0.11003	06000.0		
, M		0.400	0 480	0.490	0.500	0.510	0.520	0.530			0.570	0.580	0.590	0.600	002.0	0.750	0.800	0.850	006.0	000 1	1.050	1.100	1.150	1.200	002 1	1 350	1.400	1.450	1.500	000	1.650	1.700	1.750	1 850	006.1	1.950	2.000	000 1	3.500	4.000	4.500		6.000	6.500	7.000	000.0	8.500	000.6	100.000	istribut 's	1
												•								:														1					:			•								je d	
		0.82764	2.63578	2.44906	2.26657	2.09104	1.92485	100/1.1	1 50078	27882.1	1.29278	1.21337	1.15065	1.10459	1.06115	1.06274	1.07892	1.10887	1.15166	1 27156	1.34683	1.43060	1.52190	1.61966	1 83071	1.14117	2.05442	2.16915	2.28451	2.24469	2,62658	2.73695	2.84450	3.04906	3.14520	3.23676	3.32343	3.88523	3.95498	3.90213	3.75043	2,25350	2.95580	2.65158	2.35579	2110	1.61534	1.43484	1.29055	or 10 db cosir	
		0.218	0.220	0.222	0.224	0.226	0.228	0.230	0.214	0.236	0.238	0.240	0.242	0.244	0.248	0.250	0.252	0.254	962.0	0.260	0.262	0.264	0.266	0.268	0, 2, 0	0.274	0.276	0.278	0.280	282.0	0.286	0.288	0.290	462.0	0.296	0.298	0.300	0.320	0.330	0.340	0.350	0.370	0.380	0.390	0.400	0.410	0.430	0.440	0.450	versus x f	
																			•											•	•													•						ip/wa	
	1 06071	1 34300	2.02124	2.83365	3.52082 .	3.90206	3.90787	195/5.5	2.35434	1.75033	1.30430	1.07970.1	1.09354	1, 71768	2.20038	2.71154	3.18315	3.56456	2.82139	3.91627	3.76627	3.51219	3,18294	2,80991	2.05324	1 . 72134	1.44653	1.24134	1.11265	1.08710	1.18107	1.33492	1.53765	2.04126	2.31771	2.59525	2.86372	3 . 33981	3.53450	3.69427	3.81653	3.94487	3.95206	3.92364	3.86235	2 65471	3.51604	3.35954	3.18932	Table 15. W	
X	0 1 0	0.102	0.104	0.106	0.108	0.110	0.112	0.114	0.118	0.120	0.122	0.124	0.126	921.0	.0.132	0.134	0.136	0.138	041.0	0.144	0.146	0.148	0.150	0.152	0.156	0.158	0.160	0.162	0.164	0.168	0.170	0.172	0.174	0.178	0.180	0.182	0.184	0.188	0.190	0.192	0.194	0,198	0.200	0.202	0.204		0.210	0.212	0.214	6-1	

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0.1118 2.05444 0.234 2.43752 0.550 2.95537 0.1126 2.43745 0.242 2.35630 0.550 3.05412 0.1138 2.79745 0.244 2.36537 0.550 3.05412 0.1138 2.79745 0.244 2.36537 0.550 3.05412 0.1138 2.79745 0.246 2.36537 0.550 3.74293 0.1138 3.27795 0.250 2.45167 0.500 3.155175 0.140 3.25917 0.256 2.45175 0.7500 4.23728 0.141 3.25917 0.256 2.45175 0.7900 4.23728 0.142 3.25917 0.256 2.45175 0.7900 4.23728 0.142 3.25917 0.256 2.73758 1.1000 4.23738 0.142 3.25917 0.2568 2.73758 1.1000 4.23798 0.142 3.25914 0.2508 2.73758 1.1000 4.23798 0.152 2.65733 0.25	0.116	3.13706	0.232	2.47732	0.540	2.75893
0.122 2.51261 0.236 2.40641 0.560 2.9552 0.1128 2.49865 0.244 2.35783 0.560 3.1553 0.1138 2.49365 0.244 2.35783 0.560 3.1553 0.1138 2.49365 0.244 2.35783 0.560 3.1553 0.1138 3.44241 0.254 2.425963 0.700 4.3403 0.1148 3.46241 0.255 2.425963 0.700 4.3403 0.148 3.46421 0.255 2.426913 0.700 4.3403 0.148 3.46421 0.256 2.57554 0.790 4.3403 0.148 3.49665 0.266 2.43693 1.200 3.4783 0.148 3.4973 0.266 2.73943 1.200 3.47843 0.152 0.2653 0.2593 1.200 3.2503 3.47843 0.148 3.4973 0.266 2.49645 1.4740 2.26760 0.152 0.2653 2.5753 <td< td=""><td>0.118</td><td>2.85444</td><td>0.234</td><td>2.43752</td><td>0.550</td><td>2.85637</td></td<>	0.118	2.85444	0.234	2.43752	0.550	2.85637
0.1122 2.54572 0.243 2.36404 0.50 3.05432 0.1132 2.74742 0.243 2.37682 0.500 3.15537 0.1132 2.74742 0.243 2.37682 0.500 3.15537 0.1135 2.74742 0.244 2.37682 0.700 4.24556 0.1143 3.222847 0.750 0.500 4.24557 0.1143 3.527847 0.750 0.500 4.24557 0.1155 3.57541 0.250 2.45167 0.700 4.27556 0.1155 3.57541 0.250 2.45167 0.700 4.27556 0.1155 3.57541 0.250 2.45167 0.700 4.27556 0.1155 3.57541 0.250 2.45167 0.700 4.27556 0.155 3.57341 0.250 2.45167 0.700 4.734703 0.155 3.57344 0.250 2.45167 0.700 4.73450 0.155 3.57344 0.250 2.45167 0.700 4.73450 0.156 2.45167 0.25045 0.2500 <	0.120	2.61261	0.236	2.40641	0.560	2.95525
0.1124 2.49665 0.240 2.35030 0.550 3.15533 0.1134 3.22263 0.750 0.750 3.54783 0.750 3.75573 0.1136 3.41747 0.244 2.426083 0.750 4.24556 0.750 3.75556 0.1138 3.4113 0.7554 2.426083 0.750 4.34243 0.1144 3.464241 0.2554 2.426083 0.750 4.34203 0.1148 3.75913 0.7554 2.57554 0.7900 4.34203 0.1148 3.75913 0.2566 2.57554 0.7900 4.34203 0.1148 3.75913 0.29653 1.1050 4.347803 0.1156 2.75654 0.2564 2.75903 4.77863 0.1156 2.75653 0.25564 0.7500 4.79903 0.1156 2.75653 0.25564 0.7722 1.7760 1.77863 0.1156 2.45851 0.27613 1.77443 1.7760 1.77864 0.1156 2.458553 <td>0.122</td> <td>2.45372</td> <td>0.238</td> <td>2.38404</td> <td>0.570</td> <td>3.05432</td>	0.122	2.45372	0.238	2.38404	0.570	3.05432
0.125 2.34347 0.224 2.35500 0.5500 3.75794 0.1132 3.77546 0.246 2.37636 0.500 3.75794 0.1136 3.77594 0.260 2.37648 0.600 3.75794 0.1136 3.75594 0.260 2.37648 0.600 4.05570 0.1136 3.55043 0.270 2.55544 0.700 4.05570 0.1442 3.55043 0.2564 2.57543 0.900 4.20554 0.144 3.55043 0.2564 2.57554 0.900 4.73203 0.155 3.55043 0.2564 2.773355 1.1000 4.73203 0.156 3.05743 0.2664 2.773355 1.1000 4.73803 0.156 2.796493 1.1700 3.77510 3.775103 3.775103 0.156 2.79543 0.2744 3.02959 1.7500 3.775103 0.156 2.79543 0.27443 1.2700 3.775103 3.775103 0.156 2.47843 1.77744 1.7500 3.77512 3.725104 0.156 <td< td=""><td>0.124</td><td>2.39865</td><td>0.240</td><td>2.37030</td><td>0.580</td><td>3.15253</td></td<>	0.124	2.39865	0.240	2.37030	0.580	3.15253
0.1128 2.58456 0.244 2.37570 0.4500 3.7570 0.1138 3.52653 0.244 2.37838 0.4500 4.32432 0.1138 3.52693 0.2248 2.45163 0.4500 4.32432 0.1138 3.52693 0.2254 2.45163 0.4500 4.32432 0.1400 3.52893 0.2256 2.57554 0.4500 4.32034 0.144 3.52917 0.2256 2.57554 0.4050 4.32034 0.152 3.49663 0.2266 2.79395 1.1050 3.49403 0.155 3.49663 0.272 2.57554 1.1050 3.49403 0.156 2.45161 0.274 3.08899 1.1050 3.79403 0.156 2.45553 0.274 3.08899 1.1600 3.79443 0.156 2.45553 0.26963 1.1600 3.79443 0.156 2.45553 0.26963 1.4730 3.78443 0.156 2.45553 1.1750 2.84359 1.7500 3.7843 0.156 2.45553 1.27444 3.744	0.126	2.44747	0.242	2.36500	0050	7.24899
0.1130 0.77945 0.2646 2.77945 0.7500 4.75756 0.1136 1.52861 0.2806 2.799563 0.7500 4.737595 0.144 1.550451 0.2806 2.575543 0.45167 0.7500 4.737595 0.144 1.550451 0.2806 2.575543 0.4506 4.29556 0.144 1.59529 0.2866 2.575543 0.4000 4.29556 0.144 1.59529 0.2866 2.575543 0.4000 4.29556 0.155 1.6951 0.2866 2.793955 1.1000 4.79936 0.156 2.79513 0.2866 2.793955 1.1600 3.77510 0.156 2.79513 0.2866 2.793555 1.1600 3.77510 0.156 2.79513 0.2866 2.793555 1.1750 3.1764 0.156 2.48561 0.274 3.02955 1.1750 3.1764 0.156 2.48551 0.2743 3.02955 1.1750 3.1764 0.156 2.48551 0.2743 3.02955 1.14790 3.7761	0.128	2.58356	0.244	2.76782	0 600	VPCAT F
0.1132 7.02059 0.2548 7.39525 0.7950 4.34232 0.1138 3.595293 0.2554 2.448113 0.7950 4.34232 0.1142 3.595293 0.2554 2.57554 0.7950 4.32232 0.1143 3.595293 0.2554 2.57554 0.7950 4.32423 0.1144 3.59529 0.2554 2.57554 0.7950 4.32235 0.1152 3.19732 0.2562 2.57554 0.7950 4.32243 0.1152 3.19732 0.2564 2.791983 1.1500 4.32610 0.1152 3.19732 0.2564 2.99953 1.1600 3.79104 0.1152 2.40558 0.276 3.09393 1.2000 3.77643 0.1166 2.40558 0.276 3.09493 1.2000 3.77643 0.1166 2.40558 0.276 3.04443 1.4000 2.97540 0.1166 2.40558 0.2764 3.01443 1.7600 2.97540 0.1166 2.41265 3.14443 1.7600 2.97540 2.97540 0.1176 <td>0.130</td> <td>27945</td> <td>0.246</td> <td>27878</td> <td>0.650</td> <td>3 75750</td>	0.130	27945	0.246	27878	0.650	3 75750
0.1135 3.22253 0.750 2.43167 0.750 4.32235 0.1140 3.542887 0.2556 2.57554 0.900 4.32203 0.1145 3.54917 0.2556 2.57554 0.900 4.32203 0.1150 3.54917 0.2556 2.57554 0.900 4.32203 0.154 3.54917 0.2562 2.673913 0.1900 4.32203 0.154 3.35917 0.2662 2.673613 0.1900 4.3203 0.154 2.49665 0.270 2.67363 0.1900 4.34203 0.156 2.49553 1.100 3.47983 1.2560 3.47983 0.156 2.48528 0.270 2.62543 1.2600 3.47983 0.168 2.47528 0.270 2.99953 1.2600 3.47843 0.168 2.47528 0.2713 2.62783 3.25640 3.73640 0.168 2.414228 0.2708 3.62943 1.4760 2.84783 0.172 2.58045 0.27131 1.4760 2.7513 2.7513 0.176 2.45863	0.132	3,000	0.248	00000		05870
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0.144 3.54241 0.258 2.57534 0.950 4.07963 0.144 3.5955 0.2568 2.67811 1.100 3.79104 0.152 3.19755 1.050 3.49665 3.197355 1.050 3.497813 0.154 3.49665 2.79098 1.150 3.79104 3.79104 0.154 2.79584 0.268 2.909555 1.250 3.47983 0.158 2.78828 0.274 3.08999 1.150 3.725403 0.158 2.48558 0.274 3.08999 1.450 2.87887 0.166 2.48558 0.274 3.04455 1.450 2.87887 0.166 2.48551 0.284 3.1440 1.450 2.87813 0.166 2.48551 0.284 3.36113 1.450 2.87815 0.166 2.41651 0.284 3.36113 1.450 2.87835 0.172 2.54553 0.27433 1.750 2.81843 2.90756 0.172 2.54653 0.27433 1.750 2.81843 2.750 0.174 2	0.140	3.62887	962.0	2,22963	006.0	4.2925
0.144 3.59529 0.266 2.65223 1.000 4.07938 0.150 3.35917 0.266 2.73555 1.1000 3.79104 0.151 3.35917 0.266 2.73555 1.1000 3.79103 0.156 2.706393 1.2700 3.794035 1.250 3.47943 0.156 2.706493 2.909553 1.260 3.47943 0.156 2.48528 0.274 3.025493 1.250 3.47983 0.160 2.448528 0.274 3.025953 1.400 3.028843 0.164 2.448528 0.276 3.14740 2.47863 3.14868 0.170 2.44852 0.286 3.3413 1.400 2.97864 0.1717 2.45855 0.288 3.41361 1.750 2.97863 0.172 2.45855 0.288 3.41361 1.750 2.97843 0.174 2.45855 0.288 3.41351 1.750 2.97843 0.174 2.45855 0.288 3.41361 1.750 2.97936 0.178 2.45693 0.288	. 142	5.64241	0.258	2.57554	056.0	4.20054
0.146 3.49665 0.262 2.53311 1.050 3.49665 0.156 3.19735 1.1050 3.49665 0.156 3.19735 1.200 3.49665 0.156 2.790965 1.200 3.47461 0.156 2.78035 0.266 2.90555 1.200 3.47461 0.156 2.48558 0.274 3.08899 1.250 3.17444 0.166 2.48558 0.274 3.08899 1.450 2.78989 0.166 2.44551 0.274 3.08899 1.450 2.62781 0.166 2.44551 0.274 3.08493 1.450 2.62783 0.166 2.44551 0.286 3.36413 1.450 2.62743 0.172 2.54565 0.286 3.36413 1.550 2.67843 0.172 2.54565 0.286 3.36413 1.750 2.84843 0.172 2.54565 0.286 3.36413 1.750 2.84843 0.172 2.54565 0.286 3.36413 1.750 2.84843 0.172 2.65743 <td>0.144</td> <td>3,59529</td> <td>0.260</td> <td>2.62523</td> <td>1.000</td> <td>4.07998</td>	0.144	3,59529	0.260	2.62523	1.000	4.07998
0.148 355917 0.264 2.73355 1100 357600 0.154 2706791 1150 357600 357600 357600 357600 357600 357600 357600 357600 357600 357600 357600 357600 357600 31766 31766 31766 31766 31766 31766 31766 31766 31766 31776 302863 302863 302863 302863 302863 302863 302863 302863 302864 3	0.146	3.49665	0.262	2.67811	1.050	3.94091
0.150 3.19732 0.266 2.79098 1.150 3.47943 0.1152 2.06594 2.70649 3.07649 3.47943 0.1156 2.48528 0.274 3.026953 1.250 3.47943 0.1166 2.48528 0.274 3.029593 1.250 3.47943 0.1161 2.48528 0.274 3.028953 1.250 3.47843 0.1162 2.41425 0.274 3.028953 1.250 3.47843 0.1162 2.41425 0.288 3.26413 1.450 2.99256 0.117 2.452545 0.288 3.56115 1.450 2.99256 0.117 2.53069 0.288 3.5413 1.500 2.99256 0.117 2.53069 0.288 3.51413 1.500 2.99356 0.117 2.55045 0.288 3.5111 1.600 2.99356 0.117 2.55545 0.288 3.50115 1.700 2.99356 0.117 2.55545 0.288 3.50115 1.700 2.9433 0.118 2.45545 0.288 <t< td=""><td>0.148</td><td>3.35917</td><td>0,264</td><td>2.73355</td><td>1.100</td><td>3.79104</td></t<>	0.148	3.35917	0,264	2.73355	1.100	3.79104
0.152 3.02584 0.268 2.84983 1.200 3.47883 0.156 2.58025 0.270 2.99955 1.300 3.17848 0.156 2.48528 0.274 3.02959 1.300 3.17848 0.166 2.48528 0.274 3.02959 1.300 3.17848 0.166 2.48528 0.276 3.02959 1.400 2.68888 0.166 2.48518 0.278 3.14740 1.400 2.68888 0.166 2.41028 0.288 3.25049 1.450 2.55783 0.172 2.533069 0.288 3.35413 1.650 2.55783 0.172 2.553069 0.288 3.35413 1.650 2.39256 0.172 2.553069 0.288 3.41261 1.750 2.99433 0.172 2.553069 0.288 3.55116 1.760 2.39256 0.172 2.553069 0.299 3.54019 1.750 2.98432 0.172 2.553069 0.294 3.55116 1.750 2.97342 0.188 3.141261 3	0.150	3,19732	0.266	2.79098	1.150	3.63600
0.1154 2.45541 0.272 2.95955 1.250 3.17444 0.1166 2.48528 0.274 3.08899 1.450 2.88888 0.1164 2.48528 0.274 3.08899 1.450 2.88888 0.1164 2.48528 0.274 3.02859 1.450 2.88888 0.1164 2.48528 0.278 3.14740 1.450 2.88888 0.1164 2.48561 0.280 3.25979 1.450 2.88888 0.1172 2.45851 0.286 3.36131 1.450 2.88888 0.1172 2.553069 0.286 3.36131 1.550 2.59739 0.1172 2.553069 0.286 3.36133 1.770 2.88708 0.1176 2.753926 0.290 3.41261 1.770 2.84735 0.1176 2.853069 0.290 3.41261 1.770 2.84735 0.1176 2.98605 0.290 3.51126 1.99041 1.99041 0.1176 2.98508 3.41261 3.510459 1.87073 2.984773 0.1178 2.910	0.152	3.02584	0.268	2 84983	1 200	3.47983
0.156 2.70679 0.274 3.02959 1.300 3.17464 0.162 2.42558 0.274 3.08959 1.450 2.47513 0.164 2.42558 0.274 3.08959 1.450 2.45813 0.166 2.42558 0.274 3.08959 1.450 2.45813 0.166 2.42558 0.286 3.31311 1.450 2.45813 0.168 2.45851 0.286 3.31613 1.450 2.45143 0.170 2.45845 0.286 3.31613 1.450 2.45143 0.174 2.45545 0.286 3.351413 1.760 2.48473 0.174 2.735926 0.286 3.46191 0.294 3.46193 0.174 2.85345 0.294 3.56115 1.7760 2.18273 0.174 2.85455 0.2943 3.5713 1.7650 2.5773 0.174 2.85456 0.2943 3.57143 1.770 2.18263 0.174 2.86356 3.35743 1.770 2.18265 2.7731 0.180 3.57143 3.5	0.154	2.85841	0.270	2.90955	1.250	3.32540
0.158 2.58025 0.276 3.08899 1.350 3.02887 0.166 2.48528 0.276 3.08899 1.450 2.48758 0.166 2.41425 0.284 3.25979 1.450 2.62783 0.166 2.41425 0.284 3.25979 1.550 2.62783 0.166 2.41425 0.284 3.25979 1.550 2.62783 0.172 2.55369 0.284 3.1211 1.600 2.9455 0.172 2.55369 0.284 3.4131 1.600 2.9455 0.172 2.55369 0.284 3.4131 1.600 2.9455 0.172 2.55369 0.284 3.4131 1.650 2.9455 0.172 2.55369 0.284 3.4181 1.700 2.94315 0.172 2.55369 0.294 3.54089 1.750 2.94318 0.1180 3.11235 0.294 3.57431 1.900 1.94318 0.1180 3.11235 0.294 3.57431 1.950 1.75013 0.184 3.74019 0.294	0.156	2.70679	0.272	2.96963	1 300	3.17464
0.166 2.48528 0.276 3.0869 1.450 2.7513 0.166 2.41425 0.278 3.14740 1.450 2.5573 0.166 2.41425 0.284 3.25979 1.550 2.55070 0.170 2.5369 0.284 3.31311 1.550 2.55070 0.172 2.53699 0.284 3.31311 1.550 2.59770 0.172 2.53699 0.284 3.31311 1.550 2.59730 0.174 2.53699 0.284 3.3181 1.550 2.59436 0.174 2.98605 0.284 3.41261 1.700 2.18235 0.176 2.98605 0.299 3.4508 1.750 2.68435 0.178 2.98605 0.299 3.57408 1.750 2.98731 0.188 3.24019 0.296 3.57408 3.57408 1.900 1.900 0.188 3.54089 0.294 3.57408 3.5709 1.750 2.98731 0.188 3.54019 0.230 3.77314 3.500 0.19337 0.198	951.0	2.58025	0.274	00001	1 350	7.02887
0.166 2.42558 0.280 3.25445 1.450 2.4513 0.166 2.41425 0.286 3.25445 1.550 2.55733 0.166 2.41455 0.286 3.25445 1.550 2.55733 0.172 2.53069 0.286 3.35413 1.600 2.39256 0.172 2.53069 0.286 3.35413 1.600 2.39256 0.172 2.55069 0.286 3.35413 1.600 2.39256 0.176 2.55908 0.292 3.50115 1.700 2.18205 0.176 2.95098 0.294 3.50115 1.700 2.18205 0.184 3.11235 0.294 3.51069 1.9003 1.99433 0.182 3.11235 0.294 3.57433 1.900 1.9903 0.182 3.11235 0.294 3.57433 1.900 1.75050 1.182 3.11235 0.294 3.57433 1.900 1.75050 1.182 3.53465 3.54134 1.900 1.750738 1.7500 0.133374 1.184 3.5414	160	C ARCOR	0 276	00000 2		
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0.170 2.45851 0.286 3.36413 1.600 2.39256 0.172 2.55369 0.286 3.41261 1.700 2.18208 0.174 2.55369 0.286 3.41261 1.700 2.18208 0.176 2.98609 3.41261 1.700 2.18208 0.178 2.98609 3.41261 1.700 2.18208 0.178 2.98605 0.294 3.55169 1.9600 2.98433 0.188 3.11235 0.294 3.54089 1.9600 1.9631 0.188 3.11235 0.294 3.54069 1.9600 1.9631 0.188 3.13459 0.294 3.54069 1.9500 1.75050 0.188 3.44191 0.310 3.75585 3.70148 4.500 0.41081 0.190 3.55449 0.300 3.75585 3.70148 4.500 0.41081 0.190 3.54456 3.75121 3.75148 3.70148 4.500 0.41081 0.190 3.54456 3.44265 3.64156 0.3738 0.3738 0.196 <t< td=""><td>166</td><td>000000</td><td></td><td></td><td></td><td>2 50700</td></t<>	166	000000				2 50700
0.170 2.53069 0.286 3.41261 1.760 2.18205 0.174 2.62545 0.286 3.41261 1.760 2.18205 0.174 2.85908 0.299 3.41261 1.700 2.18205 0.176 2.85908 0.299 3.456135 1.700 2.18205 0.178 2.98605 0.294 3.51433 1.750 2.18205 0.180 3.11235 0.294 3.51743 1.900 1.99031 0.186 3.3407 0.296 3.51743 1.900 1.82713 0.186 3.34407 0.200 3.64059 1.950 1.87513 0.186 3.34407 0.300 3.64059 1.950 1.13836 0.192 3.54401 0.300 3.73914 2.000 1.13836 0.198 3.55486 0.37712 3.73914 3.500 0.41081 0.198 3.55886 3.73914 3.500 0.41081 3.77342 0.198 3.56169 0.377121 3.75914 3.500 0.41081 0.196 3.57339 3	16.0	0 45051	702.0			33005 5
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0.204 3.53976 0.400 2.60450 7.000 0.15880 0.206 3.47444 0.410 2.48145 7.500 0.13857 0.208 3.47644 0.410 2.48145 7.500 0.12196 0.208 3.47004 0.410 2.48145 7.500 0.12196 0.210 3.3868 0.430 2.31112 8.500 0.10815 0.210 3.23249 0.440 2.26418 9.000 0.9656 0.214 3.14347 0.450 2.24134 100.000 0.00079	202	3.59391	0.390	2.75032	6,500	0.18379
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0.208 3.40004 0.420 2.38340 8.000 0.12196 0.210 3.31868 0.430 2.31112 8.500 0.016815 0.212 3.23249 0.440 2.26418 9.000 0.09556 0.214 3.13347 0.450 2.24134 100.000 0.00079	0.206	3.47444	0.410	2.48145	7.500	0.13857
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.	0.460 0.470	0.490	0.510	0.530	0.540	0.560	0.580	0.590	0.600	0.700	0.750	0.850	006.0	0.950	1.050	1.100	061.1	1.250	1.300	1.400	1.450	1.500	1.600	1.650	1.750	1.800	1.850	1.950	2.000	2 200	3 .500	4.000	2,000	5.500	6.000	0000	7.500	8.000	000 6	100.000	stribution.
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×	0.216 0.218	0.222	0.226	0.230	0.232	0.236	0.238	0.242	0.244	0.248	0.250	0.254	0.256	0.258	0.262	0.264	0.268	0.270	0.272	0.276	0.278	0.280	0.284	0.286	0.288	0.292	0.294	0.298	0.300	0.310	0.330	0.340	0.350	0.370	0.380	0.390	0410	0.420	0.430	0.450	ersus x fo
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×	0.100	0.106	0.110	0.112	0.116	0.120	0.122	0.126	0.128	0.132	0.134	0.138	0.140	0.142	0.146	0.148	0.1.0	0.154	0.156	0.158	0.162	0.164	0.168	0.170	0.172	0.176	0.178	0.180	0.184	0.186	0.190	0.192	0.194	0.198	0.200	0.202	0.204	0.208	0.210	0.214	F

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4.44422 0.524 2.0367 0.500 0.33037 4.5922 0.528 1.50517 0.520 0.33037 4.59223 0.5134 0.520 0.540 0.540 0.540 4.59223 0.233 1.53559 0.540 0.540 0.540 0.540 2.13163 0.234 0.234 0.5656 0.590 0.5748 0.570 0.5964 2.131647 0.244 0.2442 0.56546 0.590 0.5748 0.5748 0.5718 0.244 0.2448 0.49704 0.560 0.5748 0.5718 0.244 0.49704 0.500 0.5748 0.750 0.5718 0.256 0.36575 0.36775 0.750 0.36775 1.69338 0.2576 0.36775 0.47376 0.750 0.45797 1.69338 0.2564 0.36775 0.4507 0.750 0.45797 1.69338 0.2564 0.36775 0.47176 1.550 0.45797 1.69333 0.2564 0.36775 0.4729 0.750 0.45797 1.69333<	2.82761	0.222	2.56476	0.490	0.42137.
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2.3353 0.234 0.540 0.540 0.5731 1.3111 0.234 0.234 0.540 0.540 0.5731 0.31867 0.234 0.244 0.49405 0.540 0.5731 0.31867 0.234 0.2345 0.59662 0.5960 0.5731 0.31867 0.234 0.244 0.49746 0.560 1.16570 0.31867 0.234 0.3534 0.35473 0.5736 0.5731 0.31867 0.2346 0.38773 0.500 0.7826 0.47735 1.21022 0.2554 0.38773 0.7826 0.7856 0.7856 0.7856 1.3117 0.2554 0.38773 0.7736 0.7856 0.7760 2.45746 1.3117 0.2554 0.38773 0.7756 0.7756 2.45746 2.45746 1.32551 0.2764 0.2564 0.45754 1.2500 3.46754 3.46754 1.32554 0.2772 1.09617 1.2500 3.46754 1.2500 3.46754 1.32554 0.2724 1.235648 1.2500 3.46754	49222	922°0	2.04323 1 BOS17		180/5.0
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1.61306 0.294 2.91343 1.850 2.67134 1.61306 0.294 2.91914 1.850 2.09731 2.33179 0.296 3.19509 2.09731 2.09731 2.8110 0.296 3.19509 2.000 1.93733 3.14853 0.310 3.87648 2.900 1.93733 3.14853 0.310 3.87764 2.000 1.33872 3.14853 0.310 3.87764 2.000 1.33872 3.14853 0.310 3.87764 2.000 1.33872 3.14853 0.310 3.87764 2.000 0.38875 3.14853 0.330 4.24555 3.500 0.56751 4.03304 0.340 4.35636 4.000 0.56751 4.03304 0.340 4.35636 4.000 0.56751 4.37295 0.3706 3.73212 5.500 0.3706 4.37295 0.37018 5.500 0.3706 0.3706 4.37295 0.37018 5.500 0.3706 0.3706 4.37295 0.37018 5.500 0.3706 0.27195 4.37295 0.37018 0.3708 0.3706 0.27195 4.4750 0.3708 0.3708	0.92877	0,290	2.62374	052.1	2,36844
2.393379 0.296 3.06018 1.900 2.09731 2.78119 0.298 3.19599 1.950 2.01534 3.48515 0.310 3.175608 2.000 1.93733 3.48515 0.310 3.87764 2.500 1.93733 3.48515 0.320 3.87664 2.500 1.93733 3.48515 0.330 3.87645 3.000 0.98875 3.48515 0.330 3.8764 2.500 0.33735 4.03304 0.330 4.42655 3.000 0.72951 4.03319 0.330 4.42616 2.500 0.72951 4.03308 0.350 4.3519 0.37036 0.37036 4.33319 0.3703 3.75234 4.500 0.37036 4.33212 0.3703 3.75795 5.500 0.37036 4.45119 0.3703 3.35795 5.500 0.37036 4.45119 0.3703 3.35795 5.500 0.2195 4.41750 0.380 3.35795 5.500 0.2195 4.41750 0.410 2.17408	840C2 1	762 0 700 0		1 850	
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2.78110 0.300 3.32608 2.000 1.93733 3.48515 0.310 3.8764 2.500 1.3372 3.48515 0.320 3.8764 2.500 1.3372 3.48515 0.320 3.8764 2.500 1.3372 3.74515 0.320 4.42655 3.500 0.72951 4.03304 0.330 4.42636 3.500 0.72951 4.03304 0.350 4.42636 3.500 0.72951 4.2503 0.350 4.42636 3.500 0.72951 4.33319 0.350 4.42658 3.500 0.37060 4.37295 0.3703 3.73212 5.500 0.37060 4.37295 0.3703 3.73212 5.500 0.37060 4.51757 0.3703 3.73212 5.500 0.37060 4.51757 0.3703 3.73212 5.500 0.37060 4.51757 0.3703 2.35718 5.500 0.25960 4.51176 0.3703 2.35718 5.500 0.25960 4.51176 0.3703 2.35600 <t< td=""><td>97292.5</td><td>0.298</td><td>3.19599</td><td>1 .950</td><td>2.01534</td></t<>	97292.5	0.298	3.19599	1 .950	2.01534
3.14853 0.310 3.87764 2.500 1.33872 3.40515 0.320 4.24555 3.500 0.56875 3.40515 0.320 4.24555 3.500 0.72951 4.233204 0.340 4.24555 3.500 0.56751 4.23319 0.340 4.43619 0.56751 0.72951 4.2350 0.350 4.43619 0.56751 0.56751 4.2350 0.350 4.35619 0.5700 0.56751 4.35010 0.350 4.35634 4.000 0.56751 4.35029 0.3706 4.35634 5.500 0.37066 4.35029 0.3701 3.773212 5.500 0.37766 4.45175 0.3701 3.773212 5.500 0.37066 4.45175 0.3701 3.773212 5.500 0.22195 4.45175 0.380 3.75212 5.500 0.22195 4.45175 0.300 2.356018 7.500 0.22195 4.45175 0.400 2.408 7.500 0.19186 4.50110 0.410 2.17408 7.500 0.16753 4.45175 0.41758 8.500 0.11708 4.66173 0.440 1.289563 0.01	2.78110	0 300	3.32608	2.000	1.93733
3.48515 0.320 4.24555 3.000 0.9875 3.78219 0.330 4.42655 3.000 0.72951 4.03219 0.330 4.42615 3.500 0.72951 4.03319 0.330 4.42615 3.500 0.72951 4.03319 0.350 4.42618 4.500 0.55731 4.037295 0.3706 4.35128 4.500 0.37006 4.37295 0.3703 3.35795 6.000 0.37066 4.317295 0.380 3.35795 6.000 0.37066 4.317295 0.380 3.35795 6.000 0.22195 4.3172 0.390 2.35795 6.000 0.22195 4.317867 0.410 2.17408 7.500 0.19186 4.317867 0.410 2.17408 7.500 0.13085 4.317867 0.410 2.17408 7.500 0.19186 4.317867 0.410 1.481458 8.500 0.11686 4.315661 0.430 1.2805	3.14853	0.310	3.87764	2.500	1.33872
3.78219 0.330 4.42636 3.500 0.72951 4.03304 0.340 4.42619 3.500 0.75951 4.23319 0.350 4.3519 3.500 0.45332 4.23008 0.350 4.302312 5.500 0.37066 4.35008 0.370 4.55212 5.500 0.37056 4.47295 0.370 3.35795 5.500 0.37056 4.47295 0.370 3.35795 5.500 0.37056 4.451255 0.370 3.35795 5.500 0.37056 4.4175 0.370 2.556018 5.500 0.25960 4.4175 0.410 2.17408 7.500 0.16753 4.4175 0.410 2.17408 7.500 0.16753 4.19661 0.420 1.48199 8.500 0.16753 4.05073 0.430 1.280563 8.500 0.11686 4.05073 0.440 1.280563 9.500 0.11686	3.48515	0.320	4.24555	3.000	0.96875
4.03304 0.340 4.43619 4.000 0.5551 4.23319 0.350 4.36687 0.35034 4.500 0.45332 4.38008 0.350 4.5687 5.000 0.3706 0.3706 4.38018 0.370 3.73212 5.500 0.3706 0.3706 4.31257 0.370 3.73212 5.500 0.3706 0.3706 4.50110 0.370 3.73212 5.500 0.3706 0.3706 4.50110 0.370 2.35500 0.22155 5.500 0.22155 4.50110 0.370 2.56004 7.000 0.19189 4.5158 7.000 0.19185 7.500 0.14750 4.13661 0.430 1.481458 8.500 0.14750 4.0561 0.430 1.481458 8.500 0.11686 4.05653 0.440 1.20563 0.000 0.11686	3.78219	0.330	4.42636	3.500	0.72951
4.33008 0.350 4.35687 5.000 0.37005 4.317295 0.370 3.73212 5.000 0.3705 4.317295 0.370 3.73212 5.500 0.37760 4.31757 0.370 3.73212 5.500 0.37760 4.51295 0.370 3.73212 5.500 0.37760 4.51297 0.370 3.73212 5.500 0.37760 4.5110 0.370 2.35795 6.500 0.22195 4.50110 0.370 2.356004 7.000 0.22195 4.50110 0.370 2.556004 7.500 0.19189 4.50110 0.410 2.17408 7.500 0.14750 4.13661 0.410 1.41558 8.500 0.14750 4.02079 0.430 1.481458 8.500 0.13085 4.02079 0.430 1.20563 9.000 0.11686	4.03304	0.340	4.43619	4 000	0.56751
4.32295 0.370 3.35795 5.500 0.37760 4.51257 0.380 3.35795 6.000 0.229560 4.51175 0.390 2.356004 7.000 0.22195 4.45175 0.390 2.356004 7.000 0.12195 4.4175 0.410 2.356004 7.500 0.13185 4.4175 0.410 2.17408 7.500 0.15185 4.137661 0.420 2.17408 7.500 0.15175 4.13661 0.420 2.17408 7.500 0.15175 4.02073 0.440 1.20563 8.500 0.11686 3.81673 0.440 1.20563 9.000 0.11686		0000	4 30634	000 v	0 17006
4.51257 0.380 3.35795 6.000 0.25960 4.50110 0.390 2.96018 6.000 0.25950 4.4175 0.400 2.56004 7.000 0.19189 4.4175 0.410 2.56004 7.000 0.19189 4.4175 0.410 2.17408 7.500 0.16753 4.135661 0.420 2.17408 7.500 0.16753 4.19661 0.420 1.481958 8.500 0.13085 4.00051 0.430 1.20563 8.500 0.13085 3.01673 0.440 1.20563 9.000 0.11686	20000 A	0.370	3.73212	5.500	0.30760
4.50110 0.390 2.96018 6.500 0.22195 4.44175 0.400 2.56004 7.000 0.19189 4.33867 0.400 2.17408 7.000 0.16753 4.35867 0.410 2.17408 7.500 0.14750 4.19561 0.420 1.81458 8.000 0.14750 4.19561 0.440 1.81458 8.000 0.13085 4.02079 0.440 1.20563 9.000 0.13085	4.51257	0.380	3.35795	6.000	0.25960
4.44175 0.400 2.56004 7.000 0.16753 4.33867 0.410 2.17408 7.500 0.16753 4.13661 0.420 1.81458 7.000 0.14750 4.19661 0.420 1.81458 8.000 0.13085 4.02079 0.430 1.48999 8.500 0.13085 3.01673 0.440 1.20563 9.000 0.13085	4.50110	0.390	2.96018	6.500	0.22195
4.3586/ 0.410 2.1408 1.200 0.14750 4.19661 0.420 1.81458 8.000 0.14750 4.05079 0.430 1.48999 8.500 0.13085 3.05079 0.440 1.20563 9.000 0.13085 3.05079 0.440 1.20563 9.000 0.11686	4.44175	0.400	2.56004	2.000	0.191.89
4.19661 0.420 1.41458 8.000 0.13050 4.02079 0.430 1.48999 8.500 0.13085 3.81673 0.440 1.20563 9.000 0.11666 7.00000 0.440 1.20563 9.000 0.11666	4	0.410	2.1 /408	000.1	0.101.0
a.02079 0.440 1.46593 9.000 0.11066 3.81673 0.440 1.20563 9.000 0.11666 2.50000 0.440 1.20563 9.000 0.11666	4.19661	0.420	1.61458	8.000	00141.0
	4.020/9 7 81671	0.430	1 20563	000 8	0 11686
0005C'S	3.59000	0.450	0.96421	100.000	96000.0

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	. 2000	1.67700		04004.1	1 78660	37764	1.39083	1.42330	1.47228	1.53517	50409.1 71703	1.78796	1.88020	1.98025	2.49416	2.95788	3.52429	600VL . E	3.83486	3.85654	3.83018	3.76848	3.68162	19676.5	3.34098	3.21643	3.09139	2.96767	20867 C	2.61538	2.50626	2.40175	2.20132	2.11617	2.03004	1.94820	1.87048	1.23519	0.89147	0.67028	5602C.0	0.33929	0.28193	0.23787		0.15343	0.13507	0.11981	0.10/00			cion.
×	0.7	0.400		0.480		015-0	0.520	0.530	0.540	0.550	0 0 0 0 0	2,580	0.590	0.600	0.650	0.700		0.11	006.0	0.950	1.000	1.050	1.100	0000	. 250	1.300	1.350	1.400	005	1.550	1.600	1.650	1. /00	1.800	1.850	1.900	1.950	2.500	3.000	3.500	000 V	5.000	5.500	6.000	000	7.500	8.000	8.500	000.6			distribut
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D a		20022.5			060/100	21102.0	2.54803	2.35628	2.17743	2.01329	1.86530	101021	1.52753	1.45189	1.39484	1.35609	21025.1	00100.1	1.37207	1.41463	1.47059	1.53883	1.61818	1.10/48	A1110 1	2.02325	2.14062	2.26221	2.58697	2.64208	2.77059	2.89862	3.02559	27272	3.39144	3.50674	3.61786	4.17710	4.48101	4.63290	49049° 4	4.34605	4.08606	3.78566	99094°	2.83331	2.54391	2.28261	2.05367	*>CC9.1		10 db (cos
×		912.0	10.000	0.550		0.226	0.228	0.230	0.232	0.234	0.236	0.240	0.242	0.244	0.246	0.248	0,250	0.554	0.256	0.258	0.260	0,262	0.264	0,250		0.272	0.274	0.276	8/2.0	0.282	0.284	0.286	0,288	662°0	0.294	0.296	0.298	0.310	0.320	0.330	0.540	0.360	0.370	0.380	065.0	0.410	0.420	0.430	0.440	0.4.0		rsus x for
																									÷		•										,														٠ ا	p/Ta ve:
		1.000.			11000.0	10016	4.75577	4.39674	3.74485	2.96648	2.22804	C0599.1	1.32821	1.56436	2.00531	2.57345	3.18531	12390 V	4.58701	4.76550	4.77690	4.63356	4.36000	5.98868 7 55501	100000 1	2.64845	2.23683	1.88605	1.61269	C/924.1	1.32724	1.40611	1.55923	1 / /464	2.33774	2.65726	2.98400	6/ COS. 5	3.89261	4.14129	4.35210	4.564642	4.72699	4.76349	4.75763	4.62999	4.51546	4.37272	4.20627	4.02072		le 19. W
M S		0.1.0	201.0	401-0			0.112	0.114	0.116	0.118	0.120	221.0	0.126	0.128	0.130	0.132	0.134	951.0	0.140	0.142	0.144	0.146	0.148	0.1.0		0.156	0.158	0.160	0.162	0.166	0.168	0.170	0 172	0.1/4	0.178	0.180	0.182	0.184	0.188	0.190	261.0	0.196	861.0	0.200	0.202	0.204	0.208	0.210	0.212	412.0	l	Tab

001.0	3.61640	0.216	4 * 5 / P / B	0.460	5.4211/
201.0	3.34214	0.218	4.18630	0.470	3.40016
P01.0	3,69037	0.220	4.09428	0.480	3.59284
901.0	C/ 021.4	2220	4.00239 7.01210	0.430	201212.5
	CC4C4 4	0.226	2 82500	005.0	NATAR
0.112	4.73684	0.228	3.74206	0.5.0	3.46928
1110	4.57796	0.230	3.66438	0.530	3.50703
0.116	4.29189	0.232	3.59282	0.540	3.54937
0.118	3.95222 7.67105	0.234	3.52805	0.550	3,59507
	26160°C	00000	1001 4.5	0015 0	5 69227
0.124	3.25891	0.240	3.37904	0.580	3.74191
0.126	3.25236	0.242	3.34525	0.590	3.79124
0.128	3.35914	0.244	3.31950	0.600	3.83962
0.130	3.55351	0.246	3.30165	0.650	4.05178
0.132	3.80108	0.248	3,29152	0.700	4.19341
0.134	4.05550	0.250	5.28882 7.20720	000 0	
971.0	4.31600	2020	3.63360	0.800	20002 V
01140	A.65733	0.256	3,32156	006.0	4.10557
0.142	70757.4	0.258	3.34462	056.0	3.98256
0.144	4.72436	0.260	3.37294	000	3.84163
0.146	4.65526	0.262	3.40599	1.050	3.69027
0.148	4.53103	0.264	3.44327	1.100	3.53406
0.150	4.36618	0.266	3.48422	1.150	3.37705
0.152	4.17668	0.268	3.52834	1.200	3.22208
0.154	3.97843	0.270	3.57511	1.250	3.07111
0.156	3.78598	0.272	3.62402	1.300	2,92542
0.158	3.61.173	0.274	3.67460	1,350	2.78580
0.160	3,46536	0.276	3.72638	1 400	2,65269
0.162	19265	8/2.0	5, 1, 1945 2, 1, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2,	400	
0.164			3.83183 7.00460	0001	12200 0
0.168	1 25256	0.284	3.93716	1.600	2.18646
0.170	3.29362	0.286	3.98889	1.650	2.08571
0.172	3.36593	0.288	4.03960	1.700	1.99077
. 174 .	3.46406	0.290	4.08899	1.750	1.90132
0.176	3.58198	0.292	4.13683	1.800	1.81/06
	0401/ C	200	A 22698	006	1.66287
0.182	3.99294	0.298	4.26894	0.050	1.59236
0.184	4.12995	0.300	4.30861	2.000	1.52587
0.186	4.25887	0.310	4.46925	2.500	1.03205
0.188	06476.4	0,25,0	6.2636.4	000.5	
261.0	4 - 56 715	0.340	4.56686	000 0	26725.0
194	4.62974	0.350	4 49646	4.500	0.34086
0.196	4.67710	0.360	4.39426	5.000	0.27769
861.0	4.70512	0.370	4 27215	5.500	0.23047
0.200	4.71425	0.380	4.14059	6.000	0.19428
0.202	4.70542	0.390	4.00821	6.500	0.16596
0.204	4.6/941	0.400	5,88169 * 76603	000° 2	0.1261.0
0.206	4.65952	0.410			
802.0	04090°4	0.4.0	3.57RA4	8.500	0.09763
212	4.44571	0.440	3.50945	000.6	0.08717
0.214	4.36389	0.450	3.45725	100.000	0.00071

Table 20. Wp/Wa versus x for 20 db (cosine) $^{3/2}$ distribution.

0 8 8

0.1.00
	4.5995.A	4.66.855	4.73668	4.80283	4.86607	4,92566	4.98105 5.03176	5.07754	5.11817	5.15356	5.18367	5.20855 20000	5.24302	5.24807	5.15923	5.00441	4.80744	ACONC. 4	4.12156	3.89254	3.67162	3.46106	3.26202	3.0.495	C8448.2	2.58403	2.44220	2.31024	19/81.5	1,96688	1.86783	1.77551	1.60898	1.53383	1.46354	1.33604	0.88828	0.62977	0.46850	19195.0	0.23364	0.19366	0.16310	0.13921	0.12020	0.09221	0.08175	0.07296	0.00059		cion.
×	0.460	0.470	0.480	0.490	0.500	0.510	025.0	0.540	0.550	0.560	0.570	0.580	0.600	0.650	0.700	0.750	0.800	008.0	0.450	1.000	1.050	1.100	1.150	1.200		1.350	1.400	1.450	1.500	1.600	1.650	1.700	008-1	1.850	1.900	000.5	2.500	3.000	3 500	4.000	1000	5.500	6.000	6.500	000.7		000° 8	000 6	100.000	· · · · · · · · · · · · · · · · · · ·	distribut
e e	4 43487	03950	4.44653	4.45577	4.46702	4.48004	4.49460 A 51043	4.52728	4.54488	4.56300	4.58138	6/:665. 9	4.61591	4.65307	4.66954	4.68509	4.69959	2621/.4	4.73566	4.74493	4.75272	4.75901	4.76377	4.76700	4,/5859 A 76889	4.76759	4.76486	4.76073	4.75526	4.74054	4.73143	4.72125	4.69798	4.68506	4.67138	40/CQ.4	4.56142	4.47745	4.39811		A 27771	4.21780	4.21502	4.22817	4.25550	4 74478	A 40156	4.46441	4.53098		8 dh (cosine)
X	0.216	0 218	0.220	0.222	0.224	0.226	0.228	0.232	0.234	0.236	0.238	0.240	0.244	0.246	0.248	0.250	0.252	0.254 23C		0.260	0.262	0.264	0.266	0,268	0.2.0	12 S S S S S S S S S S S S S S S S S S S	0.276	0.278	0.280	0.284	0.286	0.288	262.0	0.294	0.296	862.0	0.310	0.320	0.330	0.340	045.0	0.370	0.380	0.390	0.400	0.410	0.440	0.440	0.450	•	versus y for
	4.58876	4 60094	4.59871	4.58283	4 ,55848	4.53289	00216.4	4.50697	4.52185	4.54517	4.57245	4.59896	CCU20.4	4.63848	4 63316	4.61942	4.59929	4501C.4	4 52682	4.50701	4.49256	4.48447	4.48317	4.48847	4 51507	4.53589	4.55812	4.58126	4.60396	4.64339	4.65831	4.66920	5/C/9.4	4.67537	4.66883	20809.4 20105 1	4.62872	4.61042	4.59072	4.57026	000000 V	4.51032	4.49257	4.47665	4.46290	40105 A	0/0440 V	4.43339	4.43280		10 21 Wh/Wa
×	0 1 0 0	0.102	0.104	0.106	0.108	0.110	211.0	0.116	0.118	0.120	0.122	0.124		0.130	0.132	0.134	0.136	0.158	0.140	0.144	0.146	0.148	0.150	0.152	0.104	0.158	0.160	0.162	0.164	0.168	0.170	0.172	0.176	0.178	0.180	0.182	0.186	0.188	0.190	0.192	1 1 9 4	961.0	0.200	0.202	0.204	0.206	8010	010.0	0,214		Tah

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0.216 0.216 0.222 0.222 0.2224 0.2224 0.223 0.223 0.223 0.233 0.233 0.233	3.68232 3.40834 3.12622 2.84117 2.554117		
0.218 0.220 0.228 0.228 0.228 0.228 0.230 0.230	3.40834 3.12622 2.84117 2.55803	4.0	50 0.88180
0.222 0.228 0.228 0.228 0.230 0.230	2.55803	4.0	70 0.69759 80 0.55597
0.228 0.228 0.238 0.238		4.0	90 0.45439 00 0.38976
0.230	2.28116		10 0.35865
0.232	1.76130		30 0.38569
	1.52461	5.0	40 0.43079
0.236	1.10978		50 0.49845
0.238	0.93506	5.0	70 0.68028
0.240	0.78367	5°0	80 0.78894
0.244	0.55320		00 1 020020
0.246	0.47438	9.0	50 1.68742
0.248	0.41950	0.7	21902.2 00
	0.38/98	0 0	50 2.82555
0.254	0.39164	8° C	50 3.218/2 50 7 49544
0.256	0.42468		10 3 6727B
0.258	0.47688	6.0	50 3.76844
0.260	0.54686	1.0	3.80136
0.262	0.63319		50 3.78636
0.266	0.84687		00 3. /393 00 00 00 00 00 00 00
0.268	91276.0	C.	3.56631
0.270	1.11176	1.2	50 3.46080
0.274	11/62.1	م	00 3,34801
0.276	1.56831		3.11326
8/2.0	1.73137	4.	50 2.99567
0.282	2.06587		
0.284	2.23491	Ū.	0 2.65724
0.286	2.40366	.1.6	50 2.55144
0.288	2.57110		00 2.44970
	2,000 20		00 2.35216
0.294	3.05655		00 01 C 01
0.296	3.21014	6.1	0 2.08475
0.298	3,35849	1.9	2.00377
0.300	3.50105	00	0 1.92665
01210	C1211.4	5 N N	0 1.33340
0.330	10100 N	0 4 7 F	0 96568
0.340	11987.4		
0.350	4.67013	4.5(0.45234
0.360	4.42809	5.0(0.36931
0.570	4.09686	5°.0	0 0.30701
0.390	3.28911		
0.400	2.86304	.00.7	0 0.19156
0.410	2.44784	7.50	0 0.16724
0.420	2.05705	0.8	0 0.14726
	2200/ 1		0 0.13064
0.450	1.11028	100.001	0.00095

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		2.03793	1.85943	1.011.1	1.52700	1.47611	1,45055	1.44744	1.46393	1.49730	86446.1	1.67391	1.75101	1.83410	2.29035	2.72910	C2060.5	559CC.C	100019 1	3.66985	3.65850	3.61102	3.53735	3.44539	3.34124	3,22959	3.11393	2.99689	2,88037	21, Col , S	C6500.5		2.34111	2.24521	2,15361	2.06627	1.98311	1.90399	1 75728	1.21113	0.87528	0.65863	0.51213	C4804.0	012220 012220	50010 U	0.20011	0.17299	0.15102	0.13296	0.11795	0.10533	0.00086	
	×	0.460	0.470	0.480	0.440	0.510	0.520	0.530	0.540	0.550	000000	0.580	065.0	0.600	0.650	0.700	051.0	0.800		0.45.0	000.1	050.1	1.100	1.150	1.200	1.250	1.300	1.350	1.400	1.450	000.1		1.650	1.700	1.750	1.800	1.850	006.1	000 6	2.500	3.000	3.500	4.000	005.4	000 0		6.500	2.000	7.500	8.000	8.500	000.6	100.000	
	83	4.50579	4.26723	4.02020	3.1033C	P1010 1	3.03457	2.80728	2.59357	2,39565	20130 5	042101	1.79226	1.69281	1.61451	1.55717	1,52035	C420C-1	000CC 1		1.61700	1.68521	1 76688	1.86074	1.96544	2.07969	2.20218	2.33164	2.46683	2.60654	2.14963		3.18858	3 3 3 4 8 9	3.47974	· 3.62236	3,76205	3.89816	4 15340	4.71005	5.10112	5.32200	5,38323	5.30681	5.12014	4.0018U	0/02014	06608.2	19949	3,10693	2,78962	2.50375	2.25270	;
·	×	0.216	0.218	0.220	- 222.0	0.226	0.228	0.230	0.232	0.234	0.236	0.240	0.242	0.244	0.246	0.248	0.250	522.0	402.0		0.260	0.262	0.264	0.266	0.268	0.270	0.272	0.274	0.276	0.278	0.280		0.286	0.288	0.290	0.292	0.294	0.296	852.0	0.310	0.320	0.330	0.340	0.350	0.360	0.2.0	092.0	0.004.0		0.420	0.430	0.440	0.450	
						•														_	•								_						_		_																	4
8 1	a Na	1.51152	1.81249	2.70062	3.825UC	5.43091	5.52488	5.13479	4.39629	3.49931	2.63662	1 58780	1.52863	1.77875	2.271.14	2.91794	3 62333	4.29750	4.86660	2.012.C		10000 S	5.08864	4.67051	4.17637	3.64808	3.12483	2.64070	2.22316	1.89223	1.66047		0001C.1	1.74623	1.98232	2.27753	2,61580	2.98106	28/02 2	10100 V	4.42275	4.71996	4.97524	5.18374	5.34250	5.45025	92/00*0	TICIC'C	540/6°C		5.12066	4.93766	4.73097	
•	×	0.100	0.102	0.104	901.0		0.112	0.114	0.116	0.118	0.120	124	0.126	0.128	0.130	0.132	0.134	0.136	0.138		0 144	146	0.148	0.150	0.152	0.154	0.156	0.158	0.160	0.162	0.164	0.166	170	0.172	0.174	0.176	0.178	0.180	0.182	196	0.188	061.0	0.192	0.194	0.196	0.198			402°0	802.0	0.210	0.212	0.214	

Table 23. Wp/Wa versus x for 10 db (cosine)² distribution.

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	•	5.77934	5.80537	5.84449	5.85700	5.86462	5.86732	5.86514	5 BA661	5.83059	5.81035	5.78611	5.75812	0./2004 F FJFFF	26222°5	4.99281	4.70265	4.41417	4.154/9	3.60000 7.61872	3.38521	3.16839	2.96775	2.78247	2.45403	2.30878	2.17482	2.05119	1.83141	1.73367	1.64310	C06000 1	1.40835	1.34070	1 27762	1.16366	0.76786	0.54217	0.40235	0 24608	0.19997	0.16565	0.13944	0 10271	0.08955	0.07876	0.06981	0.00051			on.
×	•	0.460	0.4.0	0.490	0.500	0.510	0.520	0.530		0.560	0.570	0.580	0.590	0.650	002.0	0.750	0.800	0.850	005.0	000 1	1.050	1.100	1.150	1.200	1.300	1.350	1.400	1.450	1.550	1.600	1.650	1.750	1.800	1.850	1 900	000.4	2.500	3.000	005.5	4.000	5.000	5.500	6.000	000 2	7.500	0000.8	000,8	100.000			IJUGITISID
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•																																				•			•		•						•				
AND BE		5.71121	PC/ 1/ . C	5, 731.85	5.73952	5.74734	5.75517	5.76288		5.78404	5.79010	5.79551	5,80022	C1400.C	5.80955	5.81096	5.81148	5.81111	098608°C	5.80477	5.80097	5.79639	5.79105	5.78500	5.77094	5.76304	5.75463	C1 241 2	5.72683	5.71690	5.70673	5.68587	5.67528	5.66466	5.65404	5.63302	5.58349	5.54146	29600.0	0 4 8 9 6 4	5.48306	5.49533	5.51585	5.57463	5.60940	5.64559	5.68180	5.74960	•		n an (cos
	÷					•		•	٠.	•												۰.							•									·											÷	1	5
×		0.216	0.220	0.222	0.224	0.226	0.228	0.230	1220 C	0.236	0.238	0.240	0.242		0.248	0.250	0.252	0.254		0.260	0.262	0.264	0.266	0.268	0.272	0.274	0.276	0.278	0.282	0.284	0.286		0.292	0.294	0,296	0.300	0.310	0.320	0.22.0	0.350	0.360	0.370	0.380	000	0.410	0.420	0.430	0.450		9 1	
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<u>el c</u>	:	60/	976	120	765	965	763	44		46	52	524	789		960	23	155	210	400		969	169	982	973	26	683	281	122	203	102	368 200	501	966	97	282	242	68	51	6	112	212	508	181		145	173	22	93 193			l /d L
	•	5.78		5.750	5.73	5.72	5.72	5.4		5.761	5.770	5.7	5.0		5.760	5.751	5.741	5.733		5.75	5.72	5.731	5.73	5. 74 7. 7		5.785	5.795	5.801	2.818	5.814	5.81		5.79	5.791	287.9	5.762	5.751	5.74	15/.0	221.0	5.707	5 . 708	5.697	969 G	5.693	5.694	69.6	5.705		10.9K	110 60.
×	•	0.100	201.0	0.106	0.108	0.110	0.112	0.114		0.120	0.122	0.124	0.126		0.132	0.134	0.136	0.138	0.140	0.144	0.146	0.148	0.150	0.152	0.156	0.158	0.160	0.162	0.166	0.168	0.170	0.174	0.176	0.178	0.180	0.184	0.186	0.188	0.190	194	0.196	0.198	0.200	202.0	0.206	0.208	0.210	0.214		4°L	

		0,97503	0.75437	0.57868	0.44563	0.55219	C6462.0	0.27456	0.30414	0.35560	0.42566	05116.0	P1600.0	0.83517	1.47589	2.10109	2.65145	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	3.53487	3.64821	3.69657	3.69516	3.65656	18060.5	3.40811	3.30188	3.19084	3.07766	2.85217	2.74232	2.63545	2.53206	2.33673	2.24504	2,15737	10110-5	1.91764	1.32998	0.96427	0.56594	0.45229	0.36935	0,30709	0.25922	0 19166	0.16734	0.14735	0.13072	0,00096		on.
× ×		0.460	0.470	0.480	0.490	0.500	010.0	0.530	0.540	0.550	0.560	0/5.0		0.600	0.650	0.700	051.0	0,800	006.0	0.950	1.000	1.050	1.100	0000	1.250	1.300	1,350	1.400	2005	1.550	1.600	1 650	1.750	1.800	1.850	1 900	2.000	2.500	3.000	000	4.500	5.000	5.500	6.000		7.500	9,000	8.500	100.000	1	distributi
																								•															:							,				1	ine) ³
d a		4.10156	3.80519	3.49850	3.18721	2.87655	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	11399.1	1.73068	1.48595	1.26316	1.06405	0 74146	0.61925	0.52333	0.45343	0.40902	25685.0	C4910.0	0.46763	0.53516	0,62095	0.72342	0.84095	10112.0	1.26746	1.42891	1.59739	1 94956	2.13047	2.31285	2.49551	2.05722	3.03428	3.20761	3.5 /041	3.69767	4.38092	4.86180	5 1 0862	5.09565	4.85535	4.51353	4.10398	40000°C	2.74279	2.31156	1.91337	1.24206		5 db (cos
×		0.216	0.218	0.220	0.222	0.224	0.220	0220	0.232	0.234	0.236	0.238	0.440	0.244	0.246	0.248	0.250		0.256	0.258	0.260	0.262	0.264	992.0	0.270	0.272	0.274	0.276	0.280	0.282	0.284	0.286	0.290	0.292	0.294	962.0	0.300	0.310	0.320	0.330	0.350	0.360	0.370	0.380	065.0	0.410	0.420	0.430	0.450		rsus x for
•																										•																								•	/Жа ve
WD W D	•	0.42575	0.81209	1.92031	3 31649	4.55129	48665.C	4.91560	3.99588	2.88181	1.81208	CC086.0	19606.0	0.75373	1.36443	2.16571	3.03885	5.8/2/2	5 08415	5.36172	5.40073	5.21664	4.84276	4,52416	11100	2.41016	1.81138	1.29528	0.60075	0.4445	0.41662	0.50962	1.00357	1.36933	1.78816	2.24011	3.16833	3.61127	4.02149	4.58804	4.95899	5.15376	5.28533	5,35406	00012 V	5,20960	5.05912	4.86674	4.38151		le 26. Wp
X		0.100	0.102	0.104	0.106	0.108	011.0	114	0.116	0.118	0.120	0.122	1 26	0.128	0.130	0.132	0.134	0.1.36	0.1.00	0.142	0.144	0.146	0.148	0.150	451.0	0.156	0.158	0.160	0,164	0.166	0.168	0.170	0.174	0.176	0.178	0.180	0.184	0.186	0.188	0.190	461.0	961.0	961.0	. 200	202	2.206	0.208	0.210	212		Tab

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i		;		;	
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0.100	65558-1.	0.216	5,58932	0.46.0	6611 C
0.102	2.19678	0.218	5.30332	0.470	5670.5
0.104	3.27147	0.220	5.00453	0.480	1.8586
0.106	4.65548	0.222	4.69863	0.490	1.6767
0.108	5.90113	0.224	4.39090	0.500	1.5313
011.0	6.67426	0.226	4.08623	0.510	1.4197
0.112	6.82067	0.228	3.78899	0.520	163391
0.114	6.36618	0.230	3.50309	0.530	1.2864
0.116	5.47140	0.232	3,23192	0.540	1.2584
0.118	4.36698	0.234	2.97837	0.550	1.2523
0.120	3.29033	0.236	2.74482	0.560	1.2651
0.122	2.43740	0.238	2.53318	0.570	1.2942
	06466.1	0.240	2.54491	0.280	1.55.1
921.0	1.85254	242.0	2.18104	065.0	1.5914
		0.244		0.600	1004.1
	7 17770	042.0	250501		1300 0
0.134	4.33964	0.250	1.77697	0.750	2 6631
0.136	5.17782	0.252	73788		N020 C
0.138	5.89588	0.254	1.72229	0.850	3.1705
0.140	6.42709	0.256	1,72917	006.0	3.3050
0.142	6.73317	0.258	1.75738	0.950	3,3755
0.144	6.80311	0.260	1.80562	1.000	3,3950
0.146	6.64940	0.262	1.87251	1.050	3.3754
0.148	6.30273	0.264	1.95660	1.100	3.3266
0.150	5.80612	0.266	2.05638	1.150	3.2566
0.152	5.20911	0.268	2.17030	1.200	3.1718
0.154	4.56269	0.270	2.29683	1.250	3.0772
0.156	3.91516	0.272	2.43443	1 .300	2.9764
0.158	3.30898	0.274	2.58157	1.350	2.8725
0.160	2.77885	0.276	2.73676	1.400	2.7676
0.162	2.35058	0.278	2.89856	1 450	2.6631
0.164	66040.5	0.280	5.06559	000,1	2,5604
091.0	90968.1		3.63630		
	022700 1	1000 C	2 5 8 4 0 0 0		
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0.176		062*0	5.454 M		2260.5
871.0		762 U	2010114	1 .000	1010 - 1
0.180	3.49521	962.0	4 4442	1 900	1.8548
0.182	3.95274	862.0	4.60696	026.1	1.7830
0.184	4.41123	0.300	4.76466	2.000	1.7145
0.186	4.85490	0.310	5.46188	2.500	1.1874
0.188	5.27010	0.320	5.97578	3.000	0.8603
0.190	5.64555	0.330	6.28981	3 500	0.6483
0.192	5.97235	0.340	6.41142	4.000	0.5046
461.0	6 (2440) 6 46036	0020	0.0000	000° 4	0.4054
	0.0004.0	06220	5 07022	2000	2626.0 CFCC 0
0.200	6.69644	0.380	5.50786	6.000	0.2310
0.202	6.72537	0.390	5.08914	6.500	0.1975
0.204	6.69685	0.400	4.64733	7.000	0.1708
0.206	6.61482	0.410	4.20222	7.500	0.1491
802.0	6 35015	0.420	5./9423 7 76000	8,000	0.1513
	01010 9	0 440			
0.214	5.85658	0.450	2.64127	100.000	0.0008
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Ial	JIE 27. WD/Wa V	ersus x for	10 db (cosine) distribut	ion.

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WP	5.15311 4.96382	4.79226 4.63820	4.50099	4.27322	4.18031	4.03019	3.91940	3.87586 3.83883	3.80737	3.64968	3,59666	3.44754	3,34834	3.11652	2.99150 2.86461	2.73821	2.61402	2.37687	2.15879	2.05754	1.67066	1.70368	1.62716	1.48692	1.36216	1 30502	0.84896	0.60865	0.35340	0.22953	0.19055	0.13727	0.11861 0.10350	01160.0	0.07213	0.00059	1
×	0.460	0.490	0.500	0.520	0.530	0.550	0.570	0.580	0.600	0.450	0.750	0.850	0.900	000.1	1.050	1.150	1.250	1.300	1.400	1 450	1.550	1.650	1.700	008.1	1.900	1.950	2.500	3,500	4.000	5.000	5,500	6.500	7.000	000.8	000.6	100.000	1
3 3 3 3 1 1 2 1 3 3 1 1 2 1 3 3 1 1 2 1 3 3 1 1 2 1 3 1 1 1 1	7.33380 7.23306	7.07423	6.74413	6.41521	6.25698 6.10550	5.96238	5.70641	5.59555 5.49705	5.41134	5.27911	5.23258	5.17756	5.16827	5.18348	5.20668	5.28073	5.33005	5.44940	5.59117	5.66855 5.74238	5.83267	5.91806 6.00479	6.09227	6.26727	6.35378 6.43900	6.52253	6.96968	7.24711	7.50169	7.39917	7.24844	6.82450	6.57812 6.32337	6.06859	5.58285	5.35982	
×	0.216	0.220	0.224	0.228	0.230	0.234	0.238	0.240	0.244	0.246	0.250	0.254	0.256	0.260	0.262	0.266	0.268	0.272	0.276	0.278	0.282	0.286	0.288	0.292	0.294	0.298	0.310	0.320	0.340	0.360	0.370	0.390	0.400	004	0.440	0.450	
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WD	5.46507	6.17867 6.91278	7.58501	8.10918	7.88163	6.82190	5.76565	5.47641	5.52677	5.82150 6.22885	6.68707	7.52774	7.82306	8.05323	7.98573	7.55790	7.24532	6.55500	6.22592 5.93415	5.69406	5.40291	5.35780	5.45592	5.75826	5,96289 6,18965	6.42854	6.90605	7.12873	7.51086	7,78167	7.86966	7.94864	7.94134	7.84236	7.64837	7.52330	00 ~ 1
×	0.100	0.104	. 0.108	0.112	0.114 0.116	811.0	0.122	0.124	0.128	0.130	0.134	0.136	0.140	0.144	0.146	0.150	0.152	0.156	0.158	0.162	0.166	0.168	0.172	0.176	0.178	0 182	0.186	0.188	261.0	0.194	0.198	0.202	0.204	0.208	0.212	0.214	Таћ
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0.100	8.18246	0.216	7.96829	0.460	7.04945
0.102	8.17667	0.218	7.96442	0.470	6.98410
0.104	8.17114	0.220	7.96032	0.480	6.91524
0.106	8.16675	0.222	7.95598	. 0.490	6.84316
0.108	8.16374	0.224	7.95136	0 500	6.76815
0.110	8.16180	0.226	7.94644	0.510	6.69053
211.0	8.16023	0.228	7.94122	0.520	6.61059
	12801.8	0.230	7.0005	0.55.0	6.52865
911.0	82001.8	0.252	C8626.1	0.540	6.44496 77.005
	20100 B	0.076	1.46364 2017/0		C8400.0
0.122	66131.8	0.238	7.91046	0.570	6.18636
0.124	8.13016	0.240	7.90341	0.580	6.09847
0.126	8.12212	0.242	7.89609	065.0	6.01011
0.128	8.11446	0.244	7.88851	0.600	5.92150
0.130	8.10768 *	0.246	7.88070	0.650	5.48043
0.132	.8.10219	0.248	7.87267	0.700	5.05436
0.134	8.09821	0.250	7.86445	0.750	4.65335
0.136	8,09583	0.252	7.85606	0.800	4.28214
851.0	8.09496	0.254	10/ 48. /	0.820	3.94211
142	04550 8	0.25.0	7.83008	0.450	202000 L
0.144	8,09906	0.260	7.82123	000 1	0.09840
0.146	8.10157	0.262	7.81232	1.050	2.86894
0.148	6.10407	0.264	7.80338	1.100	2.66145
0.150	8.10624	0.266	7.79442	1.150	2.47366
0.152	8.10782	0.268	7.78547	1.200	2.30350
0.154	8.10861	0.270	7.77654	1.250	2.14909
0.1.00	8.10845	212.0	10/0/1/	1.300	21800.5
0.150	10101.8	0.276	7.75008	0007 1	1 76426
0.162	8,10195	0.278	7.74141	1.450	1.65764
0.164	8.09786	0.280	7.73285	1.500	1.55999
0.166	8.09296	0.282	7.72439	1.550	1.47038
0.168	8.08737	0.284	7.71606	1.600	1.38799
0.170	8.08124	0.286	7.70785	1.650	1.31211
0.172	8,07472	0.288	7.69979	1.700	1.24208
0.176	8 06104 8 06104	062.0	7.68409	1 800	17211-1
0.178	8.05415	0.294	7.67646	1.850	1.06182
0.180	8.04737	0.296	7.66899	1.900	1.01018
0.182	8.04078	0.298	7.66167	1 :950	0.96212
0.184	8.03446 9.03646	002.0	00409 L	000.2	CC/ 15.0
0.188	8.02279	0.320	7.59072	3.000	26055.0
0.190	8.01749	0.330	7.56310	3.500	0.31138
0.192	8.01255	0.340	7.53704	4.000	0.23945
0.194	8,00795	0.350	7.51144	4.500	0.18977
0.196	8.00367	0,360	7.48523	5.000	0.15405
0.198	1.999667 T 00600	0.2.0	CB/CB*/		
		092.0	02/24.1	000° 9	
0.204	7.98889	0.400	7.35714	000.7	26870.0
0.206	7.98554	0.410	7.31633	7.500	0.06882
0.208	7.98222	0.420	7.27136	8,000	0.06052
0.210	7.97889	0.430	7.22213	8,500	0.05363
212.0	84C/6*/	0.440	1110000	000 001	010000
	0611611				
				¢	

Table 29. Wp/Wa versus x for ∞ db (cosine)³ distribution.

	97152	193591	54627	40035	02662.	19338	18940	21183	.25714	.32203	2500X	60436	71905	.35760	98927	A105C.	14147	46807	59113	.64800	.65394	56128	48098	.38695	.28399	.17573	06491	84315	73477	62915	.52682	002222	24219	.15509	.07186 99243	.91667	33080	.96543	. 72808	.45315	37009	.30773	25978	00001	.16772	.14769	.13103	.11702	95000.		
×	0.460	0.470	0.480 0	0.490 0	0.500	0 000 0	0.530	0.540 0	0.550 0	0.560 0		0.590	0.600 0	0.650 1	0.700 1	0.750	0.850	006.0	0.950 3	1.000	1.050	001.1	000	1.250 3	1.300 3	1.350	1.400 . 3	1.500	1,550 2	1.600 '2	1.650 2	00/-1	1.800	1.850 2	1.900	000 0	2.500 1	3.000	3.500	4 500 0	.5.000	5.500 0	6.000		7.500	8,000	8.500 0	000.6	00.000		listribution
W D W B W B	A 37447	4.06653	3.74648	3.42034	3.09371	2 45697	15951	1.87691	1.61406	1,37341	1.15687	0.80135	0.66389	0.55364	0.47043	0.41377	0,28295	13461	0.43465	0.49559	16575.0	0.67398	0.91672	1.05803	1.21041	1.37220	1.54182	1,1,1,1 1, 89878	2.08243	2.26850	2.45534	2,641/5 2,2564 C	3.00904	3.18796	3.36258	2,00505 7 60505	4.41038	4.92049	5.21312	42005°C	4.97412	4.63191	4.21709	3.76042	3, 68/83 2 82010	2.37316	1,95855	1.58405	1.25431	4	5 db (cosine) ⁷ d
*	0 216	0.218	0.220	0.222	0.224	922.0	012 0	0.232	0.234	0.236	0.238	0.240	0.244	0.246	0.248	0,250	262.0	0.256	0,258	0.260	0.262	0.264	002.0	0.270	0.272	0.274	0.276	8/2.0	0.282	0.284	0.286	0.288	0.292	0.294	0.296	462*0	0.310	0.320	0.330	0.350	0.360	0.370	0.380	0.390	0.400	0.420	0.430	0.440	0.450		a versus x for
d a a	0 44466	0.82566	1.98279	3.46022	4.78082	90160.0		4.27527	3.09925	1.96016	1.06511	0.54654	0.76356	1.39416	2.23232	3.15312	4.03876	4.191.10	5.65182	5.70962	5.53072	5.14902	4.61123 7 07054	3.28175	2.59583	1.95774	1.40380	0.96079	0.46649	0.42257	0.50665	0.70585	1.37969	1.81417	2,28591	2,17476	3.73116	4.16776	4.56011	4.89908	10202.5	5.54195	5.62498	5.64395	5.60213	54487 A	5.16081	4.92827	4 .66392		able 30. Wp/Wi
×	001 0	0.102	0.104	0.106	0.108	0110		0.116	0.118	0.120	0.122	0.124	0.128	0.130	0.132	0.134	0.136	0110	0.142	0.144	0.146	0.148	051.0	154	0.156	0.158	0.160	0.162	1166	0.168	0.170	0.172	0.176	0.178	0.180	0.182	0.186	0.188	061.0	0.192	196	0.198	0.200	0.202	0.204	902.0	0.210	0.212	0.214		Ta

	d li				-	£,
×	84	X	84		×	Wa
0.100	2.09716	0.21	6 6.363	66	0.460	2.34930
0.102	2.43328	0.21	8 6.048	18	0.470	2.04335
0.104	3.62572	0.22	0 5.715	86	0.480	1.78077
0.106	5.19803	0.22	22 5.373	38	0.490	1.56033
0110	0.65869 7 65761			5 V V	00000	266/2.1
0.112	7.7691.7		B 4.342		0.520	1.12831
0.114	7.29154	0.23	0 4.014	46	0.530	1.05089
0.116	6.29955	0.23	12 3.701	20	0.540	1.00146
0.118	5.05165	0.23	3.406	11	0.550	0.97681
0.120	3.81790	0.2	56 3.132	01	0.560	0.97390
221.0	C.86437			24		1969610
0.126	2.06781		12 2.456	100	065.0	1.06749
0.128	2.34903	0.24	14 2.284	15	0.600	1.12446
0.130	2.98476	0.24	16 2.139	83	0.650	1.51416
0.132	3.85789	0.24	18 2.023	32	0.700	1.95835
0.134	4.83680	0.25	0 1.934	39	0.750	2.36290
0.136	5.79510	0.25	1.872	64	0.800	2.69018
0.1.08	7 25202		00 I 000		000 0	002267.5
0.142	7.62623		1 840		0.950	19201.5
0.144	7.73345	0.26	0 1.876	43	000.1	3.23662
0.146	7.58522	0.26	22 1.934	03	1.050	3.23759
0.148	7.21415	0.26	34 2.011	33	1.100	3.20658
0.150	6.66736	0.26	56 2.106	1	1.150	3.15196
0.152	6.00000	0.26	58 2.218	51	1.200	3.08039
0.154	5.26946			06	062.1	21166.2
901.0	800000 P		74 5 5 4 6 4 74 5 5 5 7 5 7 5 7 5 7 5 7 5 7 5 7 5 7 5		0001	2.30621
0.160	3.21408		796	48	400	2,71308
0.162	2.70708	0.2	78 2.965	43	1.450	2.61496
0.164	2.33131	0.26	3.141	01	1.500	2.51766
0.166	2.09728	0.2	32 3.321	74	1.550	2.42212
0.168	2,00665		34 S.206	0.0	1.600	00625.5
0,1,0			10 3.073		000. 1	C1452.2
0.174	2.50743		100 1 068	96 96	067.1	2.06789
0.176	2.87835	0.2	32 4,255	7.5	1.800	1.98754
0.178	3.31745	0.2	94 4.440	32	1.850	1.91062
0.180	3 80295		36 4.621	6/	1.900	1.85/09
0.184	4 . 82943		00 4.972	20	2.000	266669.1
0.186	5.33241	15.0	0 5.743	10	2.500	1.18142
0.188	5.80680	0.1	20 6.321	26	0000	0.85754
0.190	6.23944	0	50 6.685	2:	005.5	0.64694
0.194	6 94025		6.802	87	4.500	19205-0
0.196	7.19531	0.36	6.615	51	5.000	0.32901
0.198	7.38217	0.37	0 6.303	31	5.500	0.27360
0.200	7.50008	8. 0 0	30 5.903	36	6.000	0.23098
202.0	CINCC./		00 0.440	4 10	000 2	1100110
206	7.45905	14.0	0 4.466	03	7.500	0.14914
0.208	7.32703	0	186.2 0	45	8.000	0.13133
0.210	7.14495	0.4	19 3.519	65	8.500	0.11652
0.212	6.91923 • • • • • • • • •	44.0	060.3.090	10	000.6	0.10407
912.0	20000.0		06012 0			r9000*0
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Table	31. Wp/Wa.	versus x	for 10 db	(cosine)	distributio	D.

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	d M		d'A		£1;
X	W.B.	X	8	×	8
0.100	6.78245	0.216	9.07653	0.460	5.3977
0.102	6.93706	0.218	8.89136	0.470	5.1311
0.104	7.61231	0.220	8.69462	0.480	4.8870
901.0	8,75250 8,75250	22/2 O	8,49005	064.0	7044° 8
0110	91108	0.226	8.07101	0.510	4.2865
0.112	10.11526	0.228	7.86284	0.520	4.1274
0.114	9.85859	0.230	7.65928	0.530	3.9866
0.116	9.28758	0.232	7,46271	0.540	3.8628
811.0	011008 2	0.234	42C1 2.1	0.55.0	1001
0.122	7.19464	0.238	6.93439	0.570	3.5778
0.124	6.80279	0.240	6.78369	0.580	3.5069
0.126	6.67435	0.242	6.64744	0.590	3.4459
0.128	6.80379	0.244	6,52651	0.600	5555.5 1375 F
	-CC041 1	0.240	0,42070 5 33001	002 0	3.1465
0.134	8 20933	0.250	6.25665	0.750	3.0979
0.136	8.77473	0.252	6.19804	0.800	3.0511
0.138	9.27472	0.254	6.15464	0.850	2.9944
0.140	9.66131	0.256	6.12599	0.900	2,9248
0.142	9.904/5 9.904/5	962 0 092 0	00111.9	000 1	2.7521
0.144	C1150 0	0.262	6.12220	020-1	2.6545
0.148	9.73536	0.264	6,14583	1.100	2.5530
0.150	9.43180	0.266	6.18049	1.150	2.4500
0.152	9.05168	0.268	6.22528	1.200	2.3471
0.154	8.62804	0.270	6.27930	1,250	2.2458
0.1.00	16261.8		ACINC 9	1 150	2.0514
041.0	020111	910 0	6 48733	0007	1,0029.1
0.162	7.08347	0.278	6.56894	1,450	1.8714
0.164	6.84117	0.280	6.65519	1.500	1.7874
0.166	6.67952	0.282	6.74524	1.550	1.7074
0.168	6.60065	0.284	6.83826	1.600	1.6316
0.170	6.60220	0.286	6.9334/	1. 650	9600°1
2/1.0	6 91050 6 91050	0.200		1.750	0754.1
1.76	7.01576	0.292	7.22502	1.800	1.3660
0.178	7.25470	0.294	7.32199	1.850	1,3083
0.180	7.52398	. 0.296	7.41785	1.900	1.2537
0.182	7.81130	0.298	7.51210	1.950	1.2022
0.184	50001.8	0.200	01979 01979	2.500	0.7869
0.188	8.67018	0.320	8.33472	3.000	0.5658
061.0	8.92423	0.330	8.53145	3.500	0.4245
0.192	9.15008	0.340	8.60854	4 000	0.3294
194.0	9.54275	0.550	120/0.8	000	0.2142
	10519 0	0.370	8.24174	5.500	0.179
0.200	9.69341	0.380	7.97827	6.000	0.1501
0.202	9.73143	0.390	7.67388	6.500	0.1282
0.204	9.73120	0.400	7.34398	000 1	0.1108
0.206	9.69475	0.410	65733	000.8	0.0851
0.210	9.52422	0.430	6.31946	8.500	0.0755
0.212	9.39684	0.440	5.99421	000 6	0.0674
0.214	9.24633	0.4.0	44C89.C	100.001	
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Ta	ble 32. Wp/Wa	versus x foi	r 20 db (cosin	e) [±] distribut	ion
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	Aa	7.40914	91975.7	7.14916	6.89002	6.76144	6.63383	6.38232	6.25876	6.13684	6.01669 5 80840	5.78206	5.66773	5.12777	4.64178	4.20817	3.48181	3.17938	2.91113	082/972	11112 C	2.10163	1.94949	1.81257	20689.1	1.47583	1.38360	13665.1	1.15228	1.08766	1.02822	19750	0.87598	0.83256	0.79229 27.75	0.49029	0.34326	0.25343	0.15410	0.12505	0.10346	20/90.0	0.06401	0.05578	0.04905	0.04346	0.00031	on.
	×	0.460	0.470	0.480	0.500	0.510	0.520	0.540	0.550	0.560		0.590	0.600	0.650	0.700	051.0	0.850	006.0	0.950	000	0001 1	1.150	1.200	1.250	1 2500	1.400	1.450	1.500	1.600	1.650	1.700	067.1	1.850	1.900	0.6.1	2.500	3.000	3.500	4.500	5.000	5,500	6,000	000.7	7.500	8.000 6.500	000.8	100.000	distributi
d Ma	7	9.92605	9.91095	9.89566 9.8010	9.86456	9.84876	9.83282	9.80052	9.78419	9.76774	02101.6	9.71784	9.70105	9.68419	9.66728	9,63330 05559,9	9.61625	9.59916	9.58204	9.56489	9.53052	9.51330	9.49605	9.47879	9.46149 9.4418	9.42684	940946	9.39206 23755 0	9.35715	9.33963	9.32207	9.30446 0 79580	9.26908	9.25130	27252.6	9.12472	9.03149	8.93538	8.835U3 8.73321	8.62683	8.51692	8000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8.16761	8.04556	7.92126	0166/ /	7.53867	$\cdot \infty db (cosine)^{*}$
•	•	0.216	0.218	0.220	0.224	0.226	0.228	0.232	0.234	0.236	0 240	0.242	0.244	0.246	0.248	00220 252.0	0.254	0.256	0.258	0.25.0	0.264	0.266	0.268	0.270	ALC 0	0.276	0.278	0.280	0.284	0.286	0.288	067.0	0.294	0.296	862.0	0.310	0.320	0.330	0.350	0.360	0.370	0.380	0.400	0.410	0.420	0.430	0.450	versus x for
	8	10.44016	10.42570	10.41669	10.41787	10.41991	10.42113	10.41738	10.41192	10.40443	0406001 1078567	10.37553	10.36564	10.35633	10.34780	10.33337	10.32733	10.32188	10.31684	0021201	10.30221	10.29696	10.29132	10.28522	VV122 01	10.26374	10.25553	10.24682	10.22807	10.21811	10.20780	02/61.01	10.17519	10.16383	12251.01	10.12856	10.11643	10.10411	10.07891	10.06603	10.05295	10.0396/	10.01250	9.99861	9.98451	9,97020 0 04458	94097	ble 33. Wp/Wa
ł	ب ا	0.100	0.102	0,106	0.108	0.110	0.112	0.116	0.118	0.120	124	0.126	0.128	0.130	0.132	0.136	0.138	0.140	0.142	144	0.148	0.150	0.152	0.154	0.1.0	0.160	0.162	0.164	0.168	0.170	0.172	4/ 1. 0	0.178	0.180	0.182	0.186	0.188	061.0	261.0	0.196	0.198	002.0	402 0	0.206	0.208	012.0	0.214	Ta

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d B B	<pre></pre>	
×	<pre>0.460 0.510 0.520 0.550 0.500 0.550 0.500 0.550 0.500 0.550 0.5000 0.50000 0.50000 0.50000 0.500000000</pre>	
	95318 965318 97337 97337 97536 97636 005288 005674 005674 005667 005667 115738 115738 115358 115358	
×	 000000000000000000000000000000000000	
Was Ba	01658 021558 00853 98859 98859 98859 98859 98859 98859 99655 001752 001752 001752 99666 97721 998678 97281 998730 97281 998746 998746 998746 998746 998746 998746 9987766 998776 002190 002191 005772 998776 9987777 998777 998777 998777 9987777 9987777 9987777 9987777 9987777 9987777 9987777 9987777 9987777 997777 977777 977777 977777 977777 977777 977777 977777 977777 977777 977777 977777 977777 977777 977777 977777 9777777	
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e i		6.76738	6.74060	6.70854	6.67142	10629.9	6.53261	6.47828	6.42047	6.35953	6.29579	96622.9	61101.0	6.01893	5,64353	5.25935	4.88316	CN42C.4	CCPCR 7	3,59429	3.33368	3.09598	2.87946	2.68229	89205.5	5,18953	2.05299	1.92803	1.81350	1./0834	1 42256	1.44037	1.36442	1.29410	1.16837	1.11208	1.05964	1.01074	0,00220	0.34488	0.26538	0.21041	0.17085	0.14145	20611.0	C 101.0	0.07638	0.06717	0.05952	51550.0	
		0.460	0.470	0.480	0.490	0,510	0.520	0.530	0.540	0.550	0.560	0/0.0	0.540	0.600	0.650	0.700	0.750	0.800		0.950	1.000	1.050	1.100	1.150	1.200	002.1	1.350	1.400	1.450	005.1	009 1	1.650	1.700	06/.1	1 850	006.1	1.950	2.000		3.500	4.000	4.500	5.000	5,500	6,000	0000 2	7.500	8.000	8.500	000 001	
·	·· .								-									-		-			-																_					_	_						
		6.92031	6.92131	6.92193	6.92213	6 92114	6.91992	6.91820	6.91598	6.91327	6.91008	6.90642	6.89780	6.89288	6.88761	6.88201	6.87612	6.86998	6.85707	6.85039	6.84361	6.83676	6.82988	6.82301	6.81618 6.90043	6.80276	6.79624	6.78987	6.78369	9.11.9	6.76646	6.76122	6.75626	9616/ 9	6.74316	6.73942	6.73599	6.73290	0,12230	6.72354	6.73299	6.74620	6.76151	6.77729	20261.0	6.81790	6.81904	6.81944	.6.81467	6.78870	
•	× .	0.216	0.218	0.220	0.222	0.226	0.228	0.230	0.232	0.234	0.236	0.238	0.242	0.244	0.246	0.248	0.250		0.256	0.258	0,260	0.262	0.264	0.266	0.258	0.272	0.274	0.276	0.278	0.280	0 284	0.286	0.288	062.0	762 U	0.296	0.298	0.300	012.0	0.330	0.340	0.350	0.360	0.370	092.0	00000	0.410	0.420	0.430	0.450	
																																	,	•			•														
문i j		6.97366	6.97231	6.97080	6,96991	6,97119	6.97298	6.97490	6.97640	6.97708	6.97668	120/6.9	6.96978	6.96648	6.96327	6.96046	6.95825	8/906.9	6,95599 6,95599	6.95644	6.95720	6.95805	6.95877	6.95916	C06C6.0	6.956.89	6.95475	6.95192	6.94847	6.94448	6,94009 6,9354	6.93064	6.92587	6.92125	6.91295	6.90947	6.90652	6.90416	14206.9	6.90071	6.90072	6.90124	6.90222	6.90358	21200 3	6 90921	6.91134	6.91345	6.91547	6.91733 6.91896	
1	×	0.100	0.102	0.104	0.106	0.110	0.112	0.114	0.116	0.118	0.120		0.126	0.128	0.130	0.132	0.134	051.0	0.140	0.142	0.144	0.146	0.148	0.150	201.0	0.156	0.158	0.160	0.162	0.164	0.168	0.170	0.172	0.174	0.178	0.180	0.182	0.184	0.185	061.0	0.192	461.0	0.196	0.198	0.200	202.0	0.206	0.208	0.210	0.212	
																							-																												

			4. 1.		₽I,		i	
	X	8		×	6 M		×	E
	0.100	8.89332		0.216	8.6636		0.460	7.382
	0.102	8,88906		0.218	8.65693	•	0.470	7.286
	0.104	8.88715		0.220	8.64996		0 480	7.187
	901.0	8.88//b		222-0	8 642/		0.440	080.1
	0.110	8.89483		0.226	8.6278		0.510	6.878
	0.112	8.89972	•	0.228	8.6201		0.520	6.773
	0.114	8.90439		0.230	8.61221	~	0.530	6.667
	0.116	8.90820		0.232	8.6042		0.540	6.560
	0.110	8.91069		0.534	1960.8	۰.,		407 9 972 9
	0.122	8,91105 8,91106		0.230	8.57966		0.570	6.240
	0.124	8,90904		0.240	8.5713		0.580	6.134
	0.126	8.90579		0.242	8.5629		0.590	6.028
	0.128	8.90158		0.244	8.55454	-	0.600	5.924
	0.130	8.89664		0.246	8.5461	.	0.650	5.418
	0.132	8.89120		0.248	1122.8	~ ~	00/ 0	
	0.134	24C88.8		002200	2222.8	.		
		8 87341		0.254	8.5127	• •	0.850	977 . E
	0.140	8.86729		0.256	8.50450		006.0	3.465
	0.142	8.86115		0.258	8 4964	.0	0.950	3.184
	0.144	8.85499		0.260	8.4883		1.000	2.932
	0.146	8.84880		0.262	8.4804	.	1.050	2.706
	0.148	8,84258		0.264	1227 4.8		1.100	200.0
		0.0554 0		0.268	A571		002	2.157
	0.154	6.82383		0.270	8.4495		1.250	2.008
	0.156	8.81758		0.272	8.4420	. 60	1.300	1.874
	0.158	8.81137		0.274	8.4347	~	1.350	1.752
	0.160	8,80524		0.276	8.4274	.0	1.400	1.641
•	0.162	8.79920		0.278	8 4203	• •	450	
	0.164	8.79329		0.280	8.4132	~	000	2 7 2 1
•	001.0	20107 0		202.0	200 t 0		1.600	1.285
	021-0	8,77655		0.286	8.3925		1.650	1.214
	0.172	8.77134		0.288	8.3858		1.700	1.148
	0.174	8.76633		0.290	8.3791	6	1.750	1.088
	0.176	8.76151		0,292	8.37251		1.800	1.032
	0.178	8.75686		0.294	8.3660		008.1	086.0
	0.180	8./2536	•	952.0	00000000000000000000000000000000000000		1 950	
	0.184	8.74371 8.74371		0.300	8.3465	• •	2,000	0.845
	0.186	8.73950		0.310	8.3144		2.500	0.550
	0.188	8.73532		0.320	8.2814	~	3.000	0.386
•	0.1.90	8.73114		0.330	8.2465		3.500	0.285
	261.0	8.12692		0.340	B 166A		4.500	
	0.196	8.71823		0.360	8.12056		5.000	0.140
	0.198	8.71369		0.370	8,0693	~	5.500	0.116
	0.200	8.70900		0.380	8.0127		6.000	860.0
	0.202	8.70412		0.390	8056.7		000 -	0.082
	402.0	8,69703 54763 0			7.19.17		2000-2	0.062
		8.68819 8.68819		0.420	7.7340		8,000	0.055
	0.210	8.68242		0.430	7.6521		8,500	0.049
	0.212	8.67641		0.440	7.56591		000.6	0.043
	0.214	8.67015		0.450	7.4760		100.000	000.0
			•			o. 4		
		Table 36.	Wp/Wa	Versus X	for (1 -	r") di	stribution.	

	0.13567 0.19864 0.19864 0.19864 0.19864 0.19864 0.19864 0.19864 0.19864 0.19864 0.19864 0.19864 0.19864 0.116910 0.116900 0.116900 0.116900 0.116900 0.116900 0.116900 0.116900 0.116900 0.116900 0.116900 0.116900 0.116900 0.116900 0.116900 0.116900 0.116900 0.1160000 0.1160000 0.1160000 0.1160000 0.11600000000 0.1160000000000000000000000000000000000	tribution.
×	00000000000000000000000000000000000000	(cosine) ^¼ dis
WD WB	 2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.	roximate 5 db (
×	00000000000000000000000000000000000000	x for app
	0.20 0.20	Wp/Wa versus
	00000000000000000000000000000000000000	Table 37.

Wa.	1.22052	1.29520	1.39167	1.50583	1,63391	1.77252	1.91863	2.06959	2.2230B	2 1775 0	2 5 2011		2 82737	00000		20501.5						01024.4	4.50524	4.13925	4.00221	3.83879	3.67364	3.51002	3,35016	3,19552	3.04701	2.90514	2.77015	2,64207	08025.5	C1907.2	2 10568	000000	2.00829	1.92248	1.84151	1.76509	1.19577	0.85627	0.40660		100000.0	0.26747	0.22548	0.19262	0.16642	0.14521	0.12/80	0.11333	10100			distribution.	
×	0.460	0.470	0.480	0.490	0.500	0.510	0.520	0.530	0.540												006.0	006.0	1.000	050.1	001.1	1.150	1.200	1.250	1.300	1.350	1.400	1.450	1.500	1.550	1.600	1.000	1 750	1 BOD	1 850	1 900	1.950	2.000	2.500	3.000			5,000	5.500	6.000	6.500	7.000	7.500	8.000	000.8		· · · · ·	%	lb (cosine)" (
e Ma	1.10112	1.11931	1.15118	1 19635	1.25424	1.32414	1.40521	1,49651	1 59701			04275			00122 C			10201-2	00000 C				3.56221	3.4/024	3.58332	3.68512	3.78057	3.86936	3,95125	4.02603	4.09359	4.15383	4.20673	4.25529	66062°4	4.52161	4,04009 A 76060	4 17200	4.37661	4.37398	4.36524	4.35064	4.19936	3.94386	3.619/8		2 53387	2.20565	1,91641	1.67249	1.47674	1,32938	1.22868	1.17158	1 1 71 0 0			pproximate ^{co} d	
X	0.216	0.218	0.220	0.222	0.224	0.226	0.228	0.230	0.532	AFC O	0 045	00110	0.240	0 242							0.20	0.55	0.260	0.262	0.264	0.266	0.268	0.270	0.272	0.274	0.276	0.278	0.280	0.282	0.284	0.286		0 292	462.0	0.296	0.298	0.300	0.310	0.320	0.330	0.340		0.370	0.380	0.390	0.400	0.410	0.420	0.430			•	versus x for ap	
W.S.	2.34000	2.88430	3.23046	3.32596	3.19147	2.89670	2.53153	2.18111	1.90936	1.751.71	1.71564	1 7951 0	000000	GATCI C	040712 C	2021202	10004.3	9110/ S		000013	82010-2	80500.5	2.57888	5.25069	2.12977	2.02492	1.94212	1.88455	1.85282	1.84535	1.85888	1.88899	1.93057	1.97831	2.02707	2.07214	10601.5	100110	2.14779	2.13115	2.09947	2.05366	1.99518	1.92592	1.84812	1 . /04/4	599/9-1	50159	1.41863	1.34172	1.27280	1.21355	1.16535	1.12932	1.10528	6/960.1		38. Wp/Wa	
×	 0.1.00	0.102	0.104	0.106	0.108	0.110	0.112	0.1.14	0.116	911.0			0.124	0 105							0 * 1 * 0	241.0	0.144	0.146	0.148	0.150	0.152	0.154	0.156	0.158	0.160	0.162	0.164	0.166	0.168	0.170			178	0.180	0.182	0.184	0.186	0.188	0.190	261.0	101.0		0.200	0.202	0.204	0.206	0.208	0.210	212.0	412.0		Table	

d M

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d i

X X	No. No. <th>X X X 0.100 0.69356 0.101 0.103 0.102 1.11391 0.103 5.3556 0.104 5.3556 0.105 5.3556 0.112 5.3556 0.112 5.3556 0.112 5.3556 0.112 5.3556 0.112 5.3556 0.112 5.3556 0.112 5.31533 0.122 5.31637 0.122 1.39723 0.122 1.39723 0.122 1.39723 0.122 1.3973 0.122 1.3973 0.123 1.3973 0.126 2.34023 0.130 2.35316 0.130 3.5551 0.142 5.36163 0.142 5.36163 0.142 5.3316 0.142 5.35347 0.142 5.35347 0.142 5.35347 0.156 <</th> <th> 222 222 222 222 222 222 222 223 223 2246 2246 2246 2256 2274 2274<th>4</th><th>4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4</th><th>0.451 0.614110 0.614110 0.15171 0.15171 0.15171 0.155759 0.155759 0.155759 0.25555555555555555 0.2555555555555555555555555555555555555</th></th>	X X X 0.100 0.69356 0.101 0.103 0.102 1.11391 0.103 5.3556 0.104 5.3556 0.105 5.3556 0.112 5.3556 0.112 5.3556 0.112 5.3556 0.112 5.3556 0.112 5.3556 0.112 5.3556 0.112 5.31533 0.122 5.31637 0.122 1.39723 0.122 1.39723 0.122 1.39723 0.122 1.3973 0.122 1.3973 0.123 1.3973 0.126 2.34023 0.130 2.35316 0.130 3.5551 0.142 5.36163 0.142 5.36163 0.142 5.3316 0.142 5.35347 0.142 5.35347 0.142 5.35347 0.156 <	 222 222 222 222 222 222 222 223 223 2246 2246 2246 2256 2274 2274<th>4</th><th>4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4</th><th>0.451 0.614110 0.614110 0.15171 0.15171 0.15171 0.155759 0.155759 0.155759 0.25555555555555555 0.2555555555555555555555555555555555555</th>	4	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0.451 0.614110 0.614110 0.15171 0.15171 0.15171 0.155759 0.155759 0.155759 0.25555555555555555 0.2555555555555555555555555555555555555
0.100 0.715 0.716 0.400 0.1102 1.11731 0.716 0.400 0.1112 2.35743 0.400 0.1112 2.35745 0.250 0.1112 2.37593 0.250 0.1112 2.31754 0.250 0.1112 2.31754 0.250 0.1113 2.31754 0.250 0.1114 2.31754 0.251 0.1122 2.31863 0.251 0.1130 2.31863 0.251 0.1130 2.31863 0.251 0.1130 2.31863 0.251 0.1130 2.31863 0.251 0.1130 2.31863 0.251 0.1130 2.31863 0.251 0.1130 2.31863 0.251 0.1130 2.31863 0.251 0.1130 2.31863 0.251 0.1130 2.31863 0.251 0.1130 2.4187 0.251 0.1131 2.4165 0.251	0.100 0.110 0.101 0.101 0.101 0.101 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1111 0.1112 0.1112 0.1112 0.1112 0.1111 0.1111 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0.1112 0	0.100 0.102 0.104 0.104 0.112 0.112 0.112 0.114 0.114 0.116 0.115 0.126 0.126 0.128 0.128 0.128 0.128 0.13765 0.13765 0.13765 0.138 0.13765 0.13765 0.136 0.13765 0.136 0.13765 0.136 0.13765 0.136 0.136 0.13765 0.136 0.13765 0.136 0.13765 0.136 0.13765 0.136 0.13765 0.136 0.13765 0.136 0.13765 0.13765 0.136 0.13765 0.13765 0.13765 0.13765 0.13765 0.136 0.13765 0.13765 0.13765 0.136 0.13765 0.13765 0.13765 0.13765 0.13765 0.142 0.152 0.152 0.152 0.175	0,216 0,228 0,228 0,228 0,228 0,228 0,228 0,228 0,228 0,228 0,228 0,228 0,228 0,228 0,228 0,258 0,2780 0,2780 0,2780 0,2780 0,2780 0,2780 0,2780 0,2780 0,2780 000	4.87686 3.56493 3.56493 3.56493 3.56493 2.57089 2.57086 1.26505 1.26505 0.88256 0.88256 0.43895 0.5175900000000000000000000000000000000000	0 . 4 1 0 0 . 4 1 0 0 . 4 1 0 0 . 4 1 0 0 . 4 1 0 0 . 5 0 0 0 . 5 1 0 0 . 5 1 0 0 . 5 1 0 0 . 5 1 0 0 . 5 1 0 0 . 5 1 0 0 . 5 1 0 0 . 5 1 0 0 . 5 1 0 0 . 5 1 0 0 . 5 1 0 0 . 5 1 0 0 0 . 5 1 0 0 0 . 5 1 0 0 0 . 5 1 0 0 0 . 5 1 0 0 0 . 5 1 0 0 0 . 5 1 0 0 0 . 5 1 0 0 0 . 5 1 0 0 0 0 . 5 1 0 0 0 0 . 5 1 0 0 0 0 . 5 1 0 0 0 0 . 5 1 0 0 0 0 . 5 1 0 0 0 0 0 . 5 1 0 0 0 0 0 . 5 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.43100 0.4111 0.51411 0.51411 0.214513 0.214513 0.13511 0.235513 0.23551400000000000000000000000000000000000
0.100 1.11191 0.201 2.214 0.400 0.1105 5.13552 0.220 3.5645 0.400 0.1111 5.13552 0.220 3.5645 0.400 0.1112 5.13552 0.220 3.5646 0.510 0.1112 5.13552 0.220 3.5646 0.510 0.1112 5.13652 0.220 3.5504 0.510 0.1112 5.13652 0.220 3.5504 0.510 0.1122 1.36651 0.224 0.254 0.510 0.1122 1.36651 0.224 0.3610 0.550 0.1122 1.36651 0.224 0.4755 0.550 0.1122 1.36651 0.224 0.4755 0.550 0.1122 1.36551 0.224 0.4755 0.550 0.1122 1.36551 0.224 0.4755 0.550 0.1122 1.36551 0.254 0.4755 0.550 0.1122 1.36551 0.274 0.256 0.550 0.1122 1.1455 0.2745 0.256 0.550	0.1102 1.11791 0.270 4.27754 0.410 0.410 0.1111 5.39520 0.222 3.90089 0.410 0.410 0.1112 5.19562 0.2212 2.27554 0.510 0.1101 0.1112 5.19562 0.2212 2.27564 0.4100 0.4100 0.1112 5.19763 0.27045 0.27045 0.2710 0.1121 0.1112 5.19763 0.27045 0.27045 0.2710 0.1121 0.1112 5.19773 0.2212 2.26454 0.2100 0.2710 0.1122 0.17975 0.2704 0.2704 0.2700 0.1759 0.1122 0.23161 0.2714 0.2704 0.2700 0.1759 0.1122 0.23161 0.2704 0.2704 0.2700 0.1759 0.1123 0.23161 0.2704 0.2704 0.2700 0.1759 0.1124 0.23161 0.2754 0.2754 0.2754 0.2754 0.1126 0.2754 0.275	0.102 1.11391 0.104 2.35520 0.106 5.35520 0.112 6.19562 0.114 5.81637 0.116 5.19562 0.118 5.35520 0.128 0.138934 0.128 0.13765 0.138 2.54023 0.138 2.540551 0.138 1.75651 0.138 5.38316 0.138 5.38316 0.138 5.38316 0.142 6.41066 0.142 6.41066 0.148 5.38316 0.148 5.38316 0.152 3.12582 0.158 3.16551 0.158 3.16551 0.158 3.16561 0.158 3.16561 0.172 0.1751 0.172 0.1755 0.172 0.1755 0.172 0.1755 0.172 0.1756 0.172 0.1755 0.172 0.1755 0.175 0.1755 0.1755 0.175 0.17555 0.17555 0.17555 0.17555 0.17555 0.17555 0.17555 0.175555 0.	0.218 0.226 0.228 0.228 0.228 0.239 0.234 0.235 0.234 0.2550 0.2550 0.2550 0.2550 0.2550000000000	4.55493 3.55093 3.55078 3.55078 3.55078 3.55078 2.57089 2.57089 2.57089 2.57089 2.57089 2.57089 2.57089 2.57089 2.57089 2.57089 2.57089 2.57089 2.55708 2.57086 1.26565 0.58178	0.470 0.480 0.590 0.510 0.5500 0.5500 0.5500 0.5500 0.5500000000	0.6111 0.21413 0.214517 0.15311 0.15311 0.15311 0.15318 0.13517 0.13517 0.23552 0.235552 0.23555555555555555555555555555555555555
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0.156 3.85347 0.270 0.89131 1.250 0.156 3.12382 0.274 1.30405 1.300 0.168 2.48739 0.274 1.30405 1.300 0.168 1.81751 0.276 1.30405 1.300 0.168 0.72870 0.278 1.30405 1.4500 0.168 0.72870 0.278 1.4506 1.4500 0.172 0.72875 0.278 1.4506 1.4500 0.174 1.16119 0.288 1.78334 1.500 0.175 1.5119 0.2816 1.78334 1.550 0.176 1.5119 0.286 2.19019 1.750 0.176 1.5119 0.286 2.1918 1.750 0.176 1.5119 0.286 2.1918 1.750 0.176 1.5119 0.274 2.79582 1.750 0.176 1.96762 0.29128 1.770 1.750 0.178 2.4675 0.2918 1.770 1.750 0.188 2.4675 0.2913 2.79582 1.750	0.154 3.86347 0.272 1.0576 3.38547 0.156 3.4879 0.274 1.15706 1.300 3.7874 0.156 1.11975 0.274 1.15706 1.300 3.7874 0.156 1.11975 0.274 1.15706 1.400 3.0659 0.166 0.72877 1.15706 1.300 3.7875 0.156 0.72871 1.5706 1.400 2.9547 0.166 0.7284 1.5169 1.400 2.9542 0.174 1.16119 0.288 1.78334 1.550 2.7349 0.174 1.16119 0.288 2.29128 1.700 2.7477 0.174 1.16119 0.294 2.12089 1.750 2.7477 0.174 1.96762 0.294 2.79128 1.770 2.7477 0.174 1.96762 0.274 1.730 2.7475 2.7477 0.178 1.96762 0.274 1.770 2.7475 2.7415 0.178 1.96762 0.274 1.730 2.74475 0.71136 0.18	0.154 3.86347 0.156 3.12382 0.158 2.42879 0.160 1.81751 0.162 1.31925 0.164 0.72870 0.168 0.54666 0.172 0.87755 0.174 1.16119 0.174 1.16119 0.178 1.95762 0.178 1.95762	0.270 0.272 0.272	0.89131 1.01896 1.15706	1.350	3.38944 3.28589 3.17714 7.06591
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0.158 2.478/7 0.276 1.17006 1.450 0.166 0.758316 0.278 1.45440 1.450 0.166 0.758316 0.278 1.45440 1.450 0.170 0.78316 0.278 1.45440 1.450 0.170 0.7805 0.286 1.51463 1.550 0.172 0.87043 0.286 2.12089 1.550 0.172 1.16119 0.286 2.12089 1.750 0.178 1.53163 0.293 2.46124 1.750 0.178 1.53163 0.294 2.4258 1.750 0.180 2.44757 0.294 2.45124 1.750 0.181 3.94874 0.291 3.21738 1.750 0.183 3.94874 0.300 3.21358 1.950 0.184 3.94874 0.300 3.2500 3.500 0.188 3.94874 0.300 3.2500 3.500 0.190 4.81115 0.300 3.256416 3.500 0.190 5.9705 0.350 3.45636 4.7560 <td>0.158 5.2478/7 0.276 1.15005 3.1730 0.166 0.95316 0.288 1.45833 1.5500 2.9542 0.166 0.78875 0.288 1.45833 1.5500 2.9542 0.172 0.95316 0.288 1.51185 0.284 2.9542 0.178 0.78755 0.288 1.5118 1.5500 2.7332 0.178 1.16119 0.288 2.12089 1.5500 2.7332 0.178 1.53163 0.292 2.45124 1.750 2.5255 0.178 1.53163 0.293 2.45124 1.750 2.3415 0.180 2.44757 0.294 2.95863 1.750 2.3415 0.182 2.48175 0.294 2.95863 1.750 2.3246 0.182 2.48775 0.294 2.95863 1.790 2.7445 0.182 3.94874 0.300 3.7136 2.9500 1.9516 0.182 3.94874 0.300 3.9572 2.95664 0.7294 0.190 4.41446 3.95021 3.5000</td> <td>0.158 2.4.81751 0.160 1.81751 0.166 0.95516 0.166 0.75870 0.170 0.54666 0.172 0.87755 0.172 1.16119 0.176 1.16119 0.176 1.95762 0.178 1.95762</td> <td>. 4/2.0</td> <td>90/CI-1</td> <td>007.1</td> <td>3.17/14</td>	0.158 5.2478/7 0.276 1.15005 3.1730 0.166 0.95316 0.288 1.45833 1.5500 2.9542 0.166 0.78875 0.288 1.45833 1.5500 2.9542 0.172 0.95316 0.288 1.51185 0.284 2.9542 0.178 0.78755 0.288 1.5118 1.5500 2.7332 0.178 1.16119 0.288 2.12089 1.5500 2.7332 0.178 1.53163 0.292 2.45124 1.750 2.5255 0.178 1.53163 0.293 2.45124 1.750 2.3415 0.180 2.44757 0.294 2.95863 1.750 2.3415 0.182 2.48175 0.294 2.95863 1.750 2.3246 0.182 2.48775 0.294 2.95863 1.790 2.7445 0.182 3.94874 0.300 3.7136 2.9500 1.9516 0.182 3.94874 0.300 3.9572 2.95664 0.7294 0.190 4.41446 3.95021 3.5000	0.158 2.4.81751 0.160 1.81751 0.166 0.95516 0.166 0.75870 0.170 0.54666 0.172 0.87755 0.172 1.16119 0.176 1.16119 0.176 1.95762 0.178 1.95762	. 4/2.0	90/CI-1	007.1	3.17/14
0.164 0.95316 0.778 1.45440 0.172 0.795316 0.7882 1.45440 0.172 0.7043 0.7882 1.45440 0.172 0.87755 0.2886 1.45440 0.172 0.87755 0.2886 2.12089 1.5550 0.172 0.87755 0.2886 2.12089 1.5500 0.178 1.151153 0.29128 1.7500 1.7500 0.178 1.55163 0.29128 1.7500 1.7500 0.178 1.55163 0.29128 1.7500 1.7500 0.180 2.44757 0.29128 1.7700 1.7700 0.181 3.94874 0.29128 1.7700 1.7700 0.182 2.45752 0.295822 1.7900 1.7700 0.183 3.94874 0.310 3.95021 2.9500 0.186 3.94874 0.310 3.95021 2.9500 0.190 5.97055 0.310 3.43436 2.9500 0.194 5.97055 0.310 3.43436 5.000 0.196 5.9705	0.166 0.78316 1.61863 1.61863 1.6580 2.9547 0.178 0.78376 0.7882 1.61863 1.6500 2.6290 0.177 0.70043 0.7886 2.12089 1.6500 2.6290 0.177 0.8755 0.2886 2.12089 1.6500 2.6290 0.177 0.87755 0.2886 2.12089 1.7500 2.4275 0.178 1.53163 0.2993 2.61248 1.7500 2.4275 0.178 1.95188 1.7700 2.4275 2.7327 0.180 2.94572 0.2943 2.75582 0.71738 1.7900 2.7317 0.180 2.95048 0.2943 2.95173 1.9500 2.95174 0.180 2.94874 0.200 2.7475 2.7349 0.188 3.94874 0.310 3.95021 1.9916 0.188 3.48174 0.310 3.5506 2.7559 0.190 4.41115 0.230 3.95021 1.9916 0.7244 0.191 3.7569 3.7569 3.5000 0.7274 0	0.1162 0.1164 0.1164 0.1164 0.12810 0.169 0.172 0.172 0.172 0.172 0.172 0.174 1.16115 0.176 1.55163 0.178 1.95163 0.178 0.178 0.178 0.178 0.176 0.176 0.166 0.166 0.176 0.166 0.176 0.166 0.176 0.166 0.176 0.176 0.176 0.176 0.176 0.176 0.176 0.176 0.176 0.176 0.176 0.166 0.176 0.166 0.17				
0.166 0.95316 0.72870 0.72874 1.500 0.172 0.87755 0.87755 1.75134 1.500 0.174 1.16119 0.288 1.79134 1.500 0.174 1.16119 0.288 2.45128 1.750 0.174 1.51119 0.290 2.46124 1.750 0.178 1.51119 0.29128 1.750 0.178 1.51119 0.29128 1.750 0.178 1.51119 0.29128 1.750 0.178 1.96763 0.293 2.65173 1.750 0.180 2.44757 0.294 2.79582 1.860 0.181 3.45675 0.300 3.27136 1.950 0.188 3.45675 0.300 3.27136 1.950 0.198 4.41115 0.300 3.27136 3.500 0.198 4.41115 0.310 4.75584 3.500 0.198 5.19905 0.350 4.75584 3.500 0.198 5.19905 0.350 4.44446 3.500 0.198 5.199	0.172 0.95316 0.288 1.6116.5 2.7349 0.172 0.728175 0.288 1.78334 1.550 2.7349 0.172 0.87755 0.288 1.78134 1.550 2.7349 0.176 0.7045 0.288 2.12089 1.700 2.5265 0.176 1.53163 0.288 2.12089 1.700 2.4277 0.176 1.55163 0.299 2.46124 1.700 2.4275 0.178 1.9518 1.700 2.4757 2.29128 1.790 2.4155 0.182 2.4757 0.294 2.79582 1.780 2.2415 0.183 2.4757 0.294 2.79582 1.780 2.2415 0.184 3.4874 2.7736 2.75467 2.7146 2.75467 0.186 3.4874 2.7736 2.7736 2.7146 2.7546 0.186 3.4874 3.1736 2.7546 2.7546 2.7546 0.186 3.4874 3.1736 2.7546 3.7500 0.724 0.190 4.41115 0.300	0.1164 0.95116 0.166 0.72870 0.170 0.0445 0.172 0.84666 0.174 1.16119 0.174 1.95163 0.178 1.95765 0.180 2.44757	0/2*0	1 45840	050	1CV56 C
0.166 0.72870 0.288 1.78334 1.550 0.172 0.64666 0.288 1.95118 1.600 0.174 1.16119 0.288 2.12019 1.750 0.175 1.51613 0.288 2.12019 1.750 0.176 1.51613 0.290 2.46124 1.770 0.180 2.44757 0.293 2.55973 1.750 0.180 2.44757 0.294 2.79582 1.770 0.180 2.44757 0.294 2.79582 1.750 0.180 2.44757 0.294 2.79582 1.750 0.180 2.48174 0.294 2.79582 1.900 0.180 2.48174 0.201 3.79562 2.000 0.186 3.48178 0.300 3.27136 1.950 0.192 2.19905 0.310 3.27136 2.500 0.194 5.75076 0.350 4.4556 3.500 0.194 5.75076 0.350 3.45676 3.500 0.194 5.75076 0.350 3.45676 4.5500 </td <td>0.172 0.72870 0.2882 1.78334 1.550 2.7349 0.172 0.64666 0.2884 1.95118 1.550 2.6290 0.173 1.16119 0.2885 2.12089 1.550 2.4277 0.176 1.95163 0.292 2.46124 1.750 2.4277 0.176 1.96763 0.2932 2.46124 1.750 2.4277 0.176 1.96763 0.2932 2.46124 1.750 2.4273 0.180 2.44757 0.294 2.79582 1.780 2.4273 0.180 2.44757 0.294 2.79582 1.9906 2.1544 0.180 2.44155 0.201 2.95643 1.9576 1.9576 0.186 3.94874 0.300 3.27136 2.000 0.9647 0.190 2.19905 0.320 3.25663 3.500 0.774 0.191 4.41115 0.330 4.73696 3.500 0.7274 0.192 5.19905 0.330 4.73690 3.500 0.7295 0.192 5.1736 0.330</td> <td>0.166 0.72870 0.168 0.76466 0.172 0.64666 0.172 0.87755 0.174 1.16119 0.176 1.95163 0.178 1.95762 0.180 2.44757</td> <td>0.280</td> <td>1.61863</td> <td>1.500</td> <td>2018.5</td>	0.172 0.72870 0.2882 1.78334 1.550 2.7349 0.172 0.64666 0.2884 1.95118 1.550 2.6290 0.173 1.16119 0.2885 2.12089 1.550 2.4277 0.176 1.95163 0.292 2.46124 1.750 2.4277 0.176 1.96763 0.2932 2.46124 1.750 2.4277 0.176 1.96763 0.2932 2.46124 1.750 2.4273 0.180 2.44757 0.294 2.79582 1.780 2.4273 0.180 2.44757 0.294 2.79582 1.9906 2.1544 0.180 2.44155 0.201 2.95643 1.9576 1.9576 0.186 3.94874 0.300 3.27136 2.000 0.9647 0.190 2.19905 0.320 3.25663 3.500 0.774 0.191 4.41115 0.330 4.73696 3.500 0.7274 0.192 5.19905 0.330 4.73690 3.500 0.7295 0.192 5.1736 0.330	0.166 0.72870 0.168 0.76466 0.172 0.64666 0.172 0.87755 0.174 1.16119 0.176 1.95163 0.178 1.95762 0.180 2.44757	0.280	1.61863	1.500	2018.5
0.170 0.54666 0.2884 1.95118 1.600 0.177 0.7043 0.286 2.12089 1.750 0.178 1.5119 0.286 2.12089 1.750 0.176 1.5119 0.290 2.46124 1.750 0.176 1.55163 0.293 2.45124 1.750 0.180 2.44757 0.294 2.75089 1.750 0.180 2.44757 0.294 2.75089 1.750 0.180 2.44757 0.294 2.75089 1.750 0.181 3.94874 0.294 2.75089 1.750 0.183 3.4874 0.300 3.2136 1.950 0.184 3.94874 0.300 3.25021 2.500 0.192 5.19905 0.300 3.25021 2.500 0.192 5.19905 0.350 4.75584 2.500 0.192 5.75035 0.350 4.75584 5.000 0.193 5.75035 0.350 4.75584 5.000 0.194 5.75035 0.350 4.75584 5.000	0.168 0.54666 0.288 1.95118 1.600 2.5269 0.170 0.7043 0.288 2.12089 1.750 2.4275 0.174 1.16119 0.293 2.45124 1.750 2.4275 0.176 1.53163 0.293 2.55973 1.750 2.4275 0.188 2.4575 0.294 2.95863 1.780 2.4275 0.184 2.4575 0.294 2.95863 1.780 2.15416 0.184 3.94874 0.294 2.95863 1.950 2.15416 0.184 3.94874 0.293 3.11738 1.900 2.1916 0.184 3.94874 0.310 3.95021 2.9503 1.9516 0.190 4.41115 0.310 3.95021 2.9500 1.9516 0.190 4.81738 0.310 3.95021 3.500 0.7295 0.190 4.81115 0.330 4.74476 3.500 0.7295 0.190 5.9726 0.330 4.74476 3.500 0.7295 0.190 5.9735 0.350 4	0.168 0.64666 0.172 0.97043 0.172 0.87755 0.174 1.16119 0.176 1.55163 0.180 2.44757	0.282	1.78334	1.550	2.73490
0.170 0.70043 0.286 2.12089 1.550 0.172 0.8755 0.298 2.12089 1.760 0.176 1.5163 0.292 2.62973 1.750 0.178 1.5163 0.293 2.46128 1.750 0.178 1.5163 0.293 2.65973 1.750 0.180 2.44757 0.294 2.65973 1.750 0.181 3.4757 0.294 2.65973 1.750 0.182 2.45648 0.294 2.95863 1.750 0.183 3.94874 0.203 3.21736 1.950 0.186 3.94874 0.310 3.95021 2.9500 0.190 4.81115 0.310 3.95021 2.500 0.190 4.8128 0.310 3.95021 2.500 0.190 5.55035 0.340 4.75696 3.500 0.190 5.92640 0.360 3.43431 5.500 0.196 5.92640 0.370 4.75696 5.000 0.196 5.92640 0.380 3.43431 5.500	0.170 0.70043 0.286 2.12069 1.550 2.3255 0.172 0.8755 0.298 2.4277 1.650 2.327 0.176 1.5163 0.294 2.4573 1.750 2.327 0.178 1.5163 0.294 2.95863 1.750 2.3246 0.180 2.44757 0.294 2.95863 1.760 2.3246 0.182 2.95048 0.294 2.95863 1.990 2.9716 0.182 2.95048 0.230 3.1736 1.900 2.0711 0.186 3.94874 0.310 3.95021 1.990 2.0711 0.190 4.41115 0.310 3.95021 2.500 1.3996 0.190 4.41115 0.310 3.95021 2.500 1.3996 0.194 5.19905 0.330 4.74466 3.500 0.5664 0.194 5.95605 0.330 4.74466 3.500 0.7274 0.195 5.7506 0.330 4.74466 3.500 0.7274 0.195 5.976663 0.330 4.74466<	0.172 0.87055 0.172 0.87055 0.174 1.16119 0.176 1.55163 0.180 2.44757	0.284	1.95118	1.600	2.62909
0.174 1.5153 0.293 2.62973 1.750 0.176 1.96762 0.293 2.45124 1.750 0.178 1.96762 0.293 2.45124 1.750 0.178 1.96762 0.294 2.79582 1.900 0.180 2.45675 0.294 2.79582 1.900 0.184 3.45675 0.294 2.95082 1.900 0.186 3.45675 0.291 2.95021 2.900 0.190 4.41115 0.300 3.27756 2.900 0.192 5.19905 0.310 3.27756 2.500 0.194 5.75035 0.350 4.73690 3.500 0.194 5.75036 0.350 4.73690 3.500 0.194 5.75035 0.350 4.73690 3.500 0.194 5.75036 0.350 4.73690 3.500 0.196 5.75035 0.360 4.73690 3.500 0.196 5.75035 0.360 4.73690 3.500 0.198 5.92640 0.360 3.43483 6.500 <td>0.174 1.16119 0.298 2.45124 1.750 2.332 0.178 1.95163 0.294 2.62973 1.750 2.3415 0.182 2.95048 1.9562 2.62973 1.780 2.3324 0.182 2.95048 1.950 1.950 2.1544 0.184 3.4475 0.294 2.75882 1.950 2.1544 0.186 3.44874 0.200 2.79136 1.950 2.1544 0.190 2.4115 0.230 3.27136 2.000 2.9547 0.190 4.4115 0.310 3.26136 1.370 2.7574 0.194 5.19905 0.330 4.74446 3.500 0.7274 0.194 5.19905 0.330 4.75646 3.500 0.7274 0.195 5.75035 0.330 4.25636 3.500 0.7274 0.196 5.75035 0.330 4.25546 4.500 0.7274 0.196 5.75035 0.330 4.25546 5.5000 0.3693 0.198 5.975035 0.330 4.25546 7</td> <td>CC/18.0 2/1.0 CC/18.0 2/1.0 CC/18.1 471.0 CC/18.1 471.0 CC/18.0 2.180 CC/18.0 2/1.0 CC/18.0 2/1.0 CC/18.0 2/1.0 CC/18.0 2/1.0 F/1.0 F/1.0 F/1.0 F/1.0 F/1.0 F/1.0 CC/18.0 F/1.0 F/1.0 F/1.0 F/1.0 C/1.0 F/1.0</td> <td>0.286</td> <td>2.12089</td> <td>1.650</td> <td>2,52659</td>	0.174 1.16119 0.298 2.45124 1.750 2.332 0.178 1.95163 0.294 2.62973 1.750 2.3415 0.182 2.95048 1.9562 2.62973 1.780 2.3324 0.182 2.95048 1.950 1.950 2.1544 0.184 3.4475 0.294 2.75882 1.950 2.1544 0.186 3.44874 0.200 2.79136 1.950 2.1544 0.190 2.4115 0.230 3.27136 2.000 2.9547 0.190 4.4115 0.310 3.26136 1.370 2.7574 0.194 5.19905 0.330 4.74446 3.500 0.7274 0.194 5.19905 0.330 4.75646 3.500 0.7274 0.195 5.75035 0.330 4.25636 3.500 0.7274 0.196 5.75035 0.330 4.25546 4.500 0.7274 0.196 5.75035 0.330 4.25546 5.5000 0.3693 0.198 5.975035 0.330 4.25546 7	CC/18.0 2/1.0 CC/18.0 2/1.0 CC/18.1 471.0 CC/18.1 471.0 CC/18.0 2.180 CC/18.0 2/1.0 CC/18.0 2/1.0 CC/18.0 2/1.0 CC/18.0 2/1.0 F/1.0 F/1.0 F/1.0 F/1.0 F/1.0 F/1.0 CC/18.0 F/1.0 F/1.0 F/1.0 F/1.0 C/1.0 F/1.0	0.286	2.12089	1.650	2,52659
0.176 1.53163 0.293 2.62973 1.96762 0.1178 1.96762 0.294 2.95863 1.96763 0.1180 2.944757 0.294 2.95863 1.950 0.1180 2.944757 0.294 2.95863 1.950 0.1180 2.944757 0.294 2.95863 1.950 0.1186 3.44174 0.300 3.27136 2.900 0.1198 4.41115 0.310 3.250221 2.500 0.198 4.414466 3.9500 3.500 3.500 0.192 5.19905 0.330 4.755846 3.500 0.194 5.75035 0.350 4.76576 4.500 0.198 5.75035 0.350 4.755846 3.500 0.198 5.92640 0.350 4.755846 5.000 0.198 5.92640 0.350 4.755846 5.000 0.204 6.05473 0.360 4.755846 5.000 0.204 6.05473 0.380 3.43837 5.000 0.204 6.05473 0.380 3.43483 <td>0.176 1.5163 0.294 2.79582 1.850 2.2416 0.1178 1.96762 0.294 2.79582 1.950 2.1941 0.1180 2.44575 0.294 2.79582 1.950 2.9191 0.1180 2.45675 0.294 2.9582 1.950 2.9191 0.1182 2.94575 0.294 3.27136 1.950 2.901 0.1188 3.41115 0.310 3.27136 2.000 1.9153 0.198 4.1115 0.310 3.44446 3.500 1.9564 0.192 5.19905 0.330 4.73690 3.500 0.7274 0.198 4.83128 0.330 4.73690 3.500 0.7274 0.198 5.19905 0.330 4.73690 3.500 0.7274 0.198 5.75035 0.330 4.73599 3.500 0.7295 0.198 5.75036 0.330 4.73599 0.7595 0.7595 0.198 5.75036 0.350 4.73599 0.2595 0.2595 0.198 5.97647 0.360 <</td> <td>0.176 1.53163 0.178 1.96762 0.180 2.44757</td> <td>0,280</td> <td>82162.2</td> <td>1.00</td> <td>C//28.2</td>	0.176 1.5163 0.294 2.79582 1.850 2.2416 0.1178 1.96762 0.294 2.79582 1.950 2.1941 0.1180 2.44575 0.294 2.79582 1.950 2.9191 0.1180 2.45675 0.294 2.9582 1.950 2.9191 0.1182 2.94575 0.294 3.27136 1.950 2.901 0.1188 3.41115 0.310 3.27136 2.000 1.9153 0.198 4.1115 0.310 3.44446 3.500 1.9564 0.192 5.19905 0.330 4.73690 3.500 0.7274 0.198 4.83128 0.330 4.73690 3.500 0.7274 0.198 5.19905 0.330 4.73690 3.500 0.7274 0.198 5.75035 0.330 4.73599 3.500 0.7295 0.198 5.75036 0.330 4.73599 0.7595 0.7595 0.198 5.75036 0.350 4.73599 0.2595 0.2595 0.198 5.97647 0.360 <	0.176 1.53163 0.178 1.96762 0.180 2.44757	0,280	82162.2	1.00	C//28.2
0.180 2.44757 0.296 2.79582 1.450 0.180 2.44757 0.296 2.95653 1.450 0.182 2.94874 0.296 3.11738 1.950 0.186 3.94874 0.300 3.21138 1.950 0.188 3.94874 0.310 3.27136 1.950 0.188 3.94874 0.310 3.27136 1.950 0.198 4.41115 0.310 3.29521 2.000 0.192 5.19905 0.330 4.73590 3.500 0.194 5.75076 4.83572 4.5500 3.500 0.194 5.75076 0.350 4.85584 5.000 0.194 5.75076 0.350 4.85584 5.000 0.196 5.75076 0.350 4.85584 5.000 0.196 5.75076 0.350 4.85584 5.000 0.196 5.75076 0.350 4.85584 5.000 0.196 5.92640 0.350 3.43837 5.000 0.200 6.05416 5.500 5.500 5.000 <td>0.1178 1.96762 0.294 2.79582 1.96763 2.1544 0.180 2.44757 0.294 2.95663 1.9916 2.0711 0.186 3.94874 0.294 3.21736 1.990 2.9504 0.186 3.94874 0.310 3.95021 2.9500 1.9159 0.186 3.94874 0.310 3.95021 2.9500 1.9159 0.190 4.4446 3.96021 3.500 0.7274 0.192 5.19905 0.330 4.73690 3.500 0.7274 0.194 5.5976 0.350 4.73690 3.500 0.7274 0.194 5.5976 0.350 4.73690 0.7274 0.7274 0.194 5.5976 0.350 4.73690 0.7574 0.500 0.75295 0.196 5.92640 0.360 4.73690 3.500 0.75295 0.198 5.92640 0.370 4.73696 6.500 0.3572 0.198 5.92640 0.380 3.43483 6.500 0.3674 0.200 6.0743 0.380</td> <td>0.178 1.96762 0.180 2.44757</td> <td>0.292</td> <td>2.62973</td> <td>1.800</td> <td>2.24163</td>	0.1178 1.96762 0.294 2.79582 1.96763 2.1544 0.180 2.44757 0.294 2.95663 1.9916 2.0711 0.186 3.94874 0.294 3.21736 1.990 2.9504 0.186 3.94874 0.310 3.95021 2.9500 1.9159 0.186 3.94874 0.310 3.95021 2.9500 1.9159 0.190 4.4446 3.96021 3.500 0.7274 0.192 5.19905 0.330 4.73690 3.500 0.7274 0.194 5.5976 0.350 4.73690 3.500 0.7274 0.194 5.5976 0.350 4.73690 0.7274 0.7274 0.194 5.5976 0.350 4.73690 0.7574 0.500 0.75295 0.196 5.92640 0.360 4.73690 3.500 0.75295 0.198 5.92640 0.370 4.73696 6.500 0.3572 0.198 5.92640 0.380 3.43483 6.500 0.3674 0.200 6.0743 0.380	0.178 1.96762 0.180 2.44757	0.292	2.62973	1.800	2.24163
0.180 2.44757 0.296 2.95663 1.900 0.182 3.94874 0.300 3.11738 1.950 0.186 3.94874 0.310 3.21736 2.900 0.186 3.94874 0.310 3.25021 2.900 0.188 3.94874 0.310 3.25021 2.000 0.198 4.4115 0.310 3.95021 2.900 0.192 5.19905 0.3320 4.75690 3.500 0.192 5.19905 0.350 4.75690 3.500 0.194 5.75036 0.350 4.75690 3.500 0.194 5.75036 0.350 4.75690 3.500 0.194 5.75036 0.350 4.75696 5.000 0.196 5.92640 0.350 4.756476 5.000 0.196 5.92640 0.370 4.24317 5.500 0.200 6.03443 5.900 0.200 5.500 0.200 5.92640 0.380 3.43433 5.500 0.200 5.93768 5.99357 7.000 5.500 <td>0.180 2.44757 0.296 2.95663 1.900 2.0711 0.182 2.95048 0.298 3.11738 1.950 1.916 0.186 3.94874 0.310 3.95021 2.000 1.916 0.188 4.41115 0.310 3.95021 2.000 0.9647 0.190 4.81115 0.310 3.95021 2.500 1.3299 0.190 4.81115 0.310 3.95021 2.500 1.3299 0.190 4.8128 0.330 4.7446 3.500 0.724 0.194 5.550705 0.350 4.75584 5.500 0.727 0.196 5.92640 0.350 4.75584 5.500 0.3693 0.196 5.92640 0.350 4.75584 5.500 0.3694 0.196 5.97467 0.3303 3.85584 5.500 0.3593 0.200 6.0364 0.3503 3.43483 6.500 0.3593 0.200 6.0364 0.3803 3.43483 6.500 0.2493 0.200 5.975605 0.3303 3.</td> <td>0.180 2.44757</td> <td>0.294</td> <td>2.79582</td> <td>1.850</td> <td>2.15446</td>	0.180 2.44757 0.296 2.95663 1.900 2.0711 0.182 2.95048 0.298 3.11738 1.950 1.916 0.186 3.94874 0.310 3.95021 2.000 1.916 0.188 4.41115 0.310 3.95021 2.000 0.9647 0.190 4.81115 0.310 3.95021 2.500 1.3299 0.190 4.81115 0.310 3.95021 2.500 1.3299 0.190 4.8128 0.330 4.7446 3.500 0.724 0.194 5.550705 0.350 4.75584 5.500 0.727 0.196 5.92640 0.350 4.75584 5.500 0.3693 0.196 5.92640 0.350 4.75584 5.500 0.3694 0.196 5.97467 0.3303 3.85584 5.500 0.3593 0.200 6.0364 0.3503 3.43483 6.500 0.3593 0.200 6.0364 0.3803 3.43483 6.500 0.2493 0.200 5.975605 0.3303 3.	0.180 2.44757	0.294	2.79582	1.850	2.15446
0.182 2.95048 0.298 3.11738 1.950 0.184 3.94575 0.300 3.21136 2.950 0.186 3.94575 0.310 3.2136 2.950 0.186 3.94575 0.310 3.2136 2.950 0.190 4.81115 0.310 3.9502 3.500 0.190 4.81115 0.310 3.9502 3.500 0.190 4.8128 0.330 4.74446 3.500 0.194 5.550765 0.350 4.75676 4.76476 0.194 5.550765 0.350 4.76476 5.000 0.196 5.92640 0.370 4.56366 5.000 0.196 5.92640 0.370 4.56366 5.000 0.196 5.92640 0.370 4.56366 5.000 0.196 5.92640 0.370 4.54317 5.500 0.200 6.0340 3.43433 5.500 0.000 0.200 5.93357 0.400 2.93557 7.000 0.200 5.93366 5.93367 5.500 0.000 <td>0.182 2.95048 0.298 3.11738 1.950 1.9915 0.184 3.94874 0.300 3.95021 2.500 1.9159 0.186 3.94874 0.310 3.95021 2.500 1.3295 0.199 4.41115 0.320 3.95021 2.500 1.3299 0.199 4.8128 0.330 3.95021 2.500 0.7274 0.194 5.19905 0.350 4.76476 3.5000 0.7674 0.194 5.55075 0.350 4.75584 3.5000 0.3673 0.196 5.92640 0.350 4.75584 5.500 0.3774 0.196 5.92640 0.370 4.24317 5.500 0.3674 0.198 5.92640 0.370 4.25584 5.500 0.3674 0.198 5.92640 0.370 4.24317 5.500 0.3674 0.200 6.03473 0.380 3.45584 5.500 0.3674 0.200 6.0340 2.34343 6.500 0.21675 0.21675 0.200 6.02473 0.300 <</td> <td></td> <td>962.0</td> <td>2,95863</td> <td>1 900</td> <td>2.07117</td>	0.182 2.95048 0.298 3.11738 1.950 1.9915 0.184 3.94874 0.300 3.95021 2.500 1.9159 0.186 3.94874 0.310 3.95021 2.500 1.3295 0.199 4.41115 0.320 3.95021 2.500 1.3299 0.199 4.8128 0.330 3.95021 2.500 0.7274 0.194 5.19905 0.350 4.76476 3.5000 0.7674 0.194 5.55075 0.350 4.75584 3.5000 0.3673 0.196 5.92640 0.350 4.75584 5.500 0.3774 0.196 5.92640 0.370 4.24317 5.500 0.3674 0.198 5.92640 0.370 4.25584 5.500 0.3674 0.198 5.92640 0.370 4.24317 5.500 0.3674 0.200 6.03473 0.380 3.45584 5.500 0.3674 0.200 6.0340 2.34343 6.500 0.21675 0.21675 0.200 6.02473 0.300 <		962.0	2,95863	1 900	2.07117
0.1184 3.434874 0.310 3.557136 2.500 0.198 4.41115 0.320 4.74446 3.9500 0.190 4.83128 0.320 4.74590 3.9500 0.192 5.19905 0.320 4.75690 3.9500 0.194 5.57035 0.320 4.76690 3.500 0.196 5.75035 0.370 4.76476 4.500 0.198 5.75035 0.370 4.76476 4.500 0.198 5.92640 0.370 4.76476 4.500 0.198 5.92640 0.370 4.24317 5.000 0.200 6.07649 0.390 3.43483 5.000 0.201 6.07649 0.390 3.43483 5.500 0.202 6.07649 0.390 3.43483 5.500 0.203 5.93807 0.390 3.43483 5.500 0.2040 5.93807 0.410 2.55605 7.500 0.201 5.93807 0.410 2.55605 7.500 0.201 5.93807 0.410 2.55605	0.186 3.434875 0.300 3.57713 2.500 1.3793 0.186 3.48174 0.310 3.5671 2.500 0.3269 0.190 4.81115 0.320 4.4446 3.500 0.7274 0.192 5.19905 0.330 4.75690 3.500 0.7276 0.194 5.50705 0.330 4.75690 3.500 0.7276 0.196 5.75055 0.350 4.75676 4.500 0.7575 0.196 5.77636 0.350 4.75676 4.500 0.7579 0.196 5.77636 0.350 4.75676 4.500 0.3697 0.196 5.77636 0.350 4.75676 4.500 0.3697 0.196 5.75636 0.3703 3.43483 6.5000 0.2219 0.200 6.07649 0.300 2.4317 5.500 0.2219 0.201 6.07649 0.300 2.34343 6.500 0.21675 0.202 6.07649 0.300 2.34343 6.500 0.21675 0.203 6.07449 0.307 <t< td=""><td>0.182 2.95048</td><td>0.298</td><td>3.11738</td><td>1.950</td><td>1.99169</td></t<>	0.182 2.95048	0.298	3.11738	1.950	1.99169
0.190 4.41115 0.320 4.44446 3.000 0.190 4.83128 0.330 4.75690 3.500 0.194 5.50705 0.330 4.75690 3.500 0.194 5.75035 0.350 4.75690 3.500 0.194 5.75035 0.350 4.75690 3.500 0.194 5.75035 0.350 4.75584 5.000 0.198 5.92640 0.350 4.25584 5.000 0.198 5.92640 0.370 4.24317 5.000 0.198 5.92640 0.370 4.24317 5.000 0.200 6.07649 0.380 3.43483 6.500 0.201 6.05473 0.390 3.43483 6.500 0.202 6.07649 0.390 3.43483 6.500 0.203 5.97355 0.410 2.55605 7.500 0.204 5.97355 0.410 2.55605 7.500 0.204 5.97355 0.410 2.15772 8.000 0.204 5.97355 0.410 2.15772 8.000 0.204 5.97355 0.410 2.15772 8.000 0.210 5.65415 0.420 1.74987 8.500	0.188 4.41115 0.320 4.4446 3.000 0.9647 0.192 5.19705 0.330 4.7446 3.500 0.9647 0.192 5.19705 0.330 4.75590 3.500 0.7574 0.194 5.17055 0.330 4.76476 4.500 0.4527 0.194 5.75035 0.330 4.76476 4.500 0.4527 0.194 5.75036 0.370 4.75584 5.000 0.4527 0.198 5.92640 0.370 4.75584 5.000 0.3597 0.200 6.07649 0.370 4.25584 5.000 0.3507 0.201 6.07649 0.370 4.24317 5.000 0.3517 0.202 6.07649 0.380 3.43483 6.500 0.2219 0.2040 2.39357 7.43483 6.500 0.1675 0.204 2.355605 1.74987 8.500 0.1675 0.212 5.42821 0.440 1.74987 8.500 0.1675 0.212 5.42821 0.440 1.74987 8.500 <t< td=""><td>C/9C4.5 PHI.0</td><td>005.0</td><td>3.45021</td><td>2.500</td><td>06616.1</td></t<>	C/9C4.5 PHI.0	005.0	3.45021	2.500	06616.1
0.190 4.83128 0.330 4.73690 3.500 0.192 5.19905 0.340 4.83572 4.500 0.194 5.75036 0.350 4.835584 4.500 0.196 5.75036 0.350 4.835584 5.000 0.198 5.92640 0.360 4.63568 5.000 0.198 5.92640 0.350 4.55584 5.000 0.198 5.92640 0.370 4.55584 5.000 0.198 5.92640 0.370 4.55584 5.000 0.198 5.92640 0.380 3.43483 5.000 0.202 6.05473 0.390 3.43483 5.000 0.204 5.93807 0.410 2.55565 7.500 0.208 5.93367 0.410 2.55565 9.000 0.208 5.93367 0.410 2.55605 9.000 0.208 5.93367 0.410 2.13772 8.000 0.210 5.65416 0.430 1.74987 8.500	0.190 4.83128 0.330 4.73690 3.500 0.7274 0.192 5.19905 0.340 4.83722 4.500 0.4525 0.194 5.275036 0.350 4.83572 4.500 0.4527 0.194 5.75036 0.350 4.83572 4.500 0.4527 0.194 5.75036 0.350 4.85584 5.000 0.3697 0.198 5.92640 0.370 4.85584 5.000 0.3593 0.200 6.03467 0.370 4.55584 5.000 0.3697 0.200 6.03467 0.370 4.55584 5.000 0.3595 0.200 6.0543 0.380 3.43483 6.500 0.2595 0.2040 2.34343 6.500 0.27119 5.93367 0.1675 0.208 5.93367 0.410 2.355665 7.000 0.1675 0.208 5.83367 0.440 1.74987 8.500 0.1475 0.212 5.45821 0.440 1.74987 8.500 0.1675 0.212 5.45821 0.450	0.188 4.4115	0.320	4.4446	3.000	0.96471
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0.214 5.16685 0.450 1.09310 100.000 0	• • • • • • • • • • • • • • • • • • • •	0.214 5.16685	0.450	1.09310	100.000	0.00096

	7.49336 7.49336 7.20622 7.06070 6.92215 6.78613 6.78613 6.52163 6.25263 6.14319 6.02183 5.902183	5.7862 5.67196 5.67196 5.67196 5.67196 5.67196 5.6853 5.6853 5.6863 5.6863 5.6864 5.6864 5.6864 5.6864 5.6864 5.6865 5.68555 5.68555 5.685555 5.685555555555	2.12962 1.97683 1.71477 1.71477 1.49980 1.49980 1.40668 1.40668 1.32170 1.24398 1.17275	1.04158 0.99152 0.99152 0.89267 0.89267 0.89267 0.76956 0.76956 0.76998 0.19898 0.15759 0.15759	0.05899 0.06548 0.06548 0.05548 0.05706 0.05017 0.05017 0.03966	tribution.
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d a	5.02613 4.76901 4.657829 4.557829 4.557829 4.557829 4.557314 4.55724 4.55724 4.55725 4.7558 5.14759 5.14759 5.35568	55.5855 5.582055 6.258055 6.258055 6.258555 6.258555 6.258555 6.258555 6.258555 6.258555 6.258555 6.258555 6.258555 7.261214 7.20114 7	8.21100 8.51100 8.5521 8.5521 8.97637 9.16652 9.16652 9.54579 9.54579 9.54579 9.7166	10.29018 10.47014 10.44014 10.64634 10.99487 11.96592 11.36792 11.58962 11.58962 11.58962 11.95632 11.95632 11.95632 11.95632 11.95632 11.95632	12.17436 12.17436 12.266036 12.36922 12.42384 12.42384 12.59764 12.53764 12.63347 12.63361	Wp/Wa
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요I g	2.32178 2.12666 2.00769 1.95477 1.95477 1.73732 1.73732 1.73732 1.73732 1.73732 1.73732 1.73732 1.73732 0.82477 0.82477 0.224758 0.126500 0.1265000 0.1265000000000000000000000000000000000000	· · · · ·
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m	0.200	4.12358	0.30	3.34256	1.60	2.703
• •	0.202	4.05286	0.31	3. 78198	1.65	2.592
• •	0.206	3. 794156	0.32	4.03615	2.1	2.405
	0.208	3.61708	0.34	4.03503	1.80	2.287
5	0.210	3.41457	0.35	3.83383	1.85	2.195
4 (0.212	3.19254	0.36	3.54226	1.90	2.107
	0.214	2.95638	0.37	3.19185	1.95	2.024
	0.218	2. 46224	87.0 91.0	2.42150	000	1.944
2	0.220	2.21373	0.40	2.04324	00.5	0.967
33	0.222	1.96994	0.41	1.68949	3.50	0.727
26	0.224	1.73458	0.42	1.36991	4.00	0.565
36	0.226	1.51088	0.43	1.09064	4.50	0.451
	922.0	1.30163	0.44	0.85498	5.00	0.368
	0.530	1.10915	0.45 24 0	0.66394	0 0 0 0 0	
5	0.234	0.78143	0.40	0.41187	9	
64	0.236	0.64866	0.48	0.34604	2.00	191.0
161	0.238	0.53760	0.49	0.31619	8.7	0.166
15.	0.240	0.44853	0.50	0.31864	8.00	0.146
166	0.242	0.38144	0.51	0.34964	8.50	0.130
	0.244	0.33604	0.52	0.40549	00.6	0.116
529	0.248	0.30788	50.0 195.0	0.40460	100.001	200.0
680	0.250	0.32344	0.55	0.68722		•
664	0.252	0.35737	0.56	0.80867		
369	0.254	0.40846	0.57	0.93931		
187		0.4/044		9/9/0.1	,	
130	0.260	0.65153	6 9 5 0	1.36406		
247	0.262	0.75782	0.65	2.08471		
971,	0.264	0.87437	Q 0	2.71855		
680	0.266	0.99974	0.75	3.21864		
929	0.268	1.13256	0.80	3.58140		
440	0.272	1.41507	06.0	3.96257		
211	0.274	1.56219	0.95	4.02387		
758	0.276	1.71161	1.00	4.02501		
424	0.278	1.86217	1.05	3.98164		
	0.200	201202		3,90622 7,00017		
	0.284	07012 0		1 400001		
662	0.286	2.45574	1.25	3.57392		
576	0.268	2.59756	1.30	3.44694		
- 66 1	0.290	2. 73526	1.35	3.31798		
969	0.292	2.86820	1.40	3.18930		•
191	0.294	2.99585	1.45	3.06252		
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3.64556	0.202	3.27784	0.31	3, 78712	1.65	1.0
3.65133	0.204	3.21989	0.32	3.63832		
3.57699	0.206	3.16647	0.33	3.47249	5.1	
3.45036	0.208	3.11847	0.34	3.30496	1.80	1.84(
3.30936	0.210	3.07665	0.35	3.14761	1.85	1.76
3.19003	0.212	3.04153	0.36	3.00980	1.90	1.68
3.11819	0.214	3.01349	0.37	2.89664	1.95	1.61
3.10564	0.216	2.99274	0.38	2.81140	2.00	1.54
3.15041	0.218	2.97934	0.39	2.75509	2.50	EO
3.23985	0.220	2.97322	0.40	2.72711	3.00	0.736
3.35500	0.222	2.97418	0.41	2.72576	2 2 2	0.54
3.47512	0.224	2.98193	0.42	2.74856	4.00	0.42
3.58138	0.226	2.99609	0.43	2,79262	4.50	
3. 65948	0.228	3.01620	0.44	2.85484		
3.70083	0.230	3.04177	1450	01010 G		
3.70277	0.232	1.07225	0.45	01200 2		
3.66785	0.234	10705			00	0.19
3.60259	0.236	3.14550	14.0	19411.0	2 2 2 2	
3.51611	0.278	100001.5		06822.0	20.1	0.141
3.41862	0.240		C.4.7	40400.0	2	0.12
3.32024	0.242	04102.0		5.44098 1 550000	00.8	0.10
3,23001	0.244	1 1 2 2 2	5.0			500
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3.10109	0.248	1000V.F		06/1/ -0	100.001	0.00
3.07056	0.250	3. 47051		000000		
3.06453	0.252	3.51831	0.55	0.304//		
3.08201	0.254	1. 5650T				
3.12057	0.256	3.61030		4.1/243		•
3.17664	0.258	3.65378	0.50	A 77746		
3.24595	0.260	3.69516	5.0	A. 41097		
3.32390	0.262	3. 73418	0.65	A. 68716		
3.40587	0.264	3. 77059	56	A2708.A		
3.48748	0.266	3.80422	0, 75	A. BARSS		
3.56481	0.268	3.83489	0.80	4.78993		
3.63452	0.270	3.86248	0.85	4.67335		
3.69395	0.272	3.88691	0.90	4.51877		
3.74113	0.274	3.90810	0.95	4.34118		
3. 77481	0.276	3.92602	1.00	4.15145		
3. 79439	0.278	3.94065	1.05	3.95723		
3- 79987	0.280	3.95201	1.10	3.76381		
3. 79176	0.282	3.96013	1.15	3.57469		
5. 77101	0.284	3.96507	1.20	3.39215		
J. /3093	0.286	3.96689	1.25	3.21753		•
	0.288	3.96568	1.30	3.05158		• .
	06210	4C196.5	دي . I	2.89460		
18050.5	262.0	3.95458	1.40	2.74660		•
3.53021	0.294	3.94492	1.45	2.60738		
3.46693	0.296	3.93269	8	2.47663		
TLCUT - L	0.295	3.91802		F0737 C .		

APPENDIX C

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Methods	METD	Electromagnetic	waves	EWAV		

Electromagnetic waves Electromagnetic waves Antennas - Radiation Antennas - Radiation Т. В LaSalle, T. R. LaSalle, UNCLASSIFIED UNCLASSIFIED Hazards Hazards Title Title ŧ г. Ц. Ξ. ي. ا 2. Naval Weapons Laboratory, Dahlgren, Virginia. Naval Weapons Laboratory, Dahlgren, Virginia. WAVE ANTENNA, by T. R. LaSalle. 4 Dec 1963. WAVE ANTENNA, by T. R. LaSalle. 4 Dec 1963. 2 methods of determining the on-axis microwave This report describes the development of 2 methods of determining the on-axis microwave the aperture distribution and the resulting the aperture distribution and the resulting This report describes the development of computation. The resultant on-axis fields are compared and some conclusions relating are compared and some conclusions relating ON-AXIS POWER DENSITY OF A CIRCULAR MICRO-The resultant on-axis fields ON-AXIS POWER DENSITY OF A CIRCULAR MICRO-Fraunhofer regions, for circular-aperture Fraunhofer regions, for circular-aperture antennas with any arbitrary, axially EFFECT OF APERTURE ILLUMINATION ON THE methods have been programmed for digital EFFECT OF APERTURE ILLUMINATION OF THE methods have been programmed for digital symmetric aperture illumination. Both symmetric aperture illumination. Both UNCLASSIFIED UNCLASSIFIED power density in both the Fresnel and power density in both the Fresnel and antennas with any arbitrary, axially 14 p., 27 figs., 43 tables. 14 p., 27 figs., 43 tables. on-axis fields are made. on-axis fields are made. (NWL Report No. 1893) (NWL Report No. 1893) computation. Electromagnetic waves Electromagnetic waves Antennas - Radiation. Antennas - Radiation Т. В. T. R. LaSalle, UNCLASSIFIED LaSalle, UNCLASSIFIED Hazards - Hazards Title Title ΞŢ. ц. Ц 5 -i r. 3 Naval Weapons Laboratory, Dahlgren, Virginia. Naval Weapons Laboratory, Dahlgren, Virginia. WAVE ANTENNA, by T. R. LaSalle. 4 Dec 1963. WAVE ANTENNA, by T. R. LaSalle. 4 Dec 1963. 14 p., 27 figs., 43 tables. This report describes the development of 2 This report describes the development of 2 methods of determining the on-axis microwave methods of determining the on-axis microwave the aperture distribution and the resulting the aperture distribution and the resulting ON-AXIS POWER DENSITY OF A CIRCULAR MICROare compared and some conclusions relating are compared and some conclusions relating computation. The resultant on-axis fields computation. The resultant on-axis fields ON-AXIS POWER DENSITY OF A CIRCULAR MICRO-Fraunhofer regions, for circular-aperture Fraunhofer regions, for circular-aperture EFFECT OF APERTURE ILLUMINATION ON THE methods have been programmed for digital EFFECT OF APERTURE ILLUMINATION ON THE methods have been programmed for digital Both UNCLASS IFIED symmetric aperture illumination. Both UNCLASSIFIED power density in both the Fresnel and power density in both the Fresnel and antennas with any arbitrary, axially antennas with any arbitrary, axially symmetric aperture illumination. 14 p., 27 figs., 43 tables. on-axis fields are made. on-axis fields are made. (NWL Report No. 1893) (NWL Report No. 1893)