Army Research Laboratory



Closed-Loop Water Recycling System

L. Vande Kieft DYNAMIC SCIENCE, INC.

W. Hillstrom W. Gault M. Rose U.S. ARMY RESEARCH LABORATORY

ARL-MR-220

May 1995



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1. AGENCY USE ONLY (Leave blank)		3. REPORT TYPE AND C Final, January-Dece	DATES COVERED
4. TITLE AND SUBTITLE Closed-Loop Water Recycling Sy	rstem		funding numbers VO #: 4G592-392-06
6. AUTHOR(S) L. Vande Kieft,* W. Hillstrom, V	V. Gault, and M. Rose		
7. PERFORMING ORGANIZATION NAM	E(S) AND ADDRESS(ES)	8.	PERFORMING ORGANIZATION REPORT NUMBER
U.S. Army Research Laboratory ATTN: AMSRL-WT-TB Aberdeen Proving Ground, MD	21005-5066		ARL-MR-220
9. SPONSORING / MONITORING AGENO	Y NAME(S) AND ADDRESS(ES) 10). SPONSORING/MONITORING AGENCY REPORT NUMBER
11. SUPPLEMENTARY NOTES			
12a. DISTRIBUTION / AVAILABILITY ST	ATEMENT	1:	26. DISTRIBUTION CODE
Approved for public release; dist	ribution is unlimited.		
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ACKNOWLEDGMENT

The authors are grateful to Mr. Richard Schwanke, of the U.S. Army Research Laboratory's (ARL) Risk Management Office, for sampling the effluent from the prototype filter and having it analyzed for contaminant content, to Mr. Raymond Cregar for making his facility available for this experiment and ultimate installation of the system, and to Mr. Ona Lyman for reviewing the manuscript.

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1. PURPOSE

The primary purpose of this project was to provide employees at explosives processing facilities the means of handling explosives-contaminated water in a manner that is environmentally friendly and that complies with all laws and regulations.

Closely related to this is the issue of safety. Cleanliness is imperative in an explosives processing operation. Steam-down and wash-down operations can only be permitted if the waste water is disposed of properly or handled in other ways consistent with regulation. The proposed system avoids the problem of waste water disposal. It is safe, effective, and within the existing permits and regulations.

2. BACKGROUND

The Explosives Modeling Facility, an explosives processing pilot plant facility which is part of the U.S. Army Research Laboratory (ARL), is in operation on Spesutie Island at the Aberdeen Proving Ground (APG), MD. Explosives operations performed here include melting, casting, pressing, sawing, machining, and x-raying energetic materials, primarily explosives, gun propellants, and pyrotechnic formulations.

The problem is that most of these operations generate Reactive Hazardous Waste (RHW). In addition, as a result of the processing, the spaces within which these operations are performed become contaminated with reactive dust. The normal, and formerly approved, approach to cleaning these spaces has been a steam wash-down. Until recently, at the conclusion of a processing operation involving energetic materials, the operating bays involved would be steamed down to remove all traces of these materials. The contaminated water, or "pink water," would flow into a trough, and be led to a filter at one end of the building (B-1171). The filtered water would then be discharged to the environment.

Approximately five years ago, the Directorate of Safety, Health, and the Environment (DSHE) of the Aberdeen Proving Ground Support Activity (APGSA) made a determination that this process contributed to contamination of the environment. The filter, which was simple but effective, was considered to be at fault. It consisted of a box of sawdust, mounted at the end of the trough which led steam-down water from the operating bays to the filter.

The APGSA removed this filter and replaced it with a concrete structure—a wide, shallow trough, separated into three chambers by metal baffle plates. These chambers were filled with activated charcoal. Waste water from the steam-down entered one end of this structure, passed through the chambers, and exited the other end as discharge water. This new system proved unsatisfactory for several reasons. Surface water run-off carried debris into the filter chambers, small animals made their homes there, and the filter design was defective, forcing flow patterns which overexposed small volumes of the filter medium while leaving much of it underexposed. Also, no tests were performed to ensure that the resulting filtering was sufficiently effective to meet requirements.

These problems were partially alleviated by the installation of locally fabricated metal panels to cover the filtration system. Some additional modifications were made, but none was able to solve the principal problem—the flow rate of the entering waste water during explosives sawing operations. Flow rates were slow enough to avoid overflow during steam-down operations, but not during sawing. The sawing operation requires a minimum flow rate to maintain closure on a safety interlock switch, so this flow rate cannot be adjusted lower to meet the capacity of the filter.

In addition to these problems, certain agencies took soil samples from the surrounding area, and in one sample found evidence of explosive material. Even though repeat testing found no further evidence of contamination, this analysis was deemed to provide sufficient reason to prohibit further use of the new filter. Concomitantly, operations requiring the use of the filter were discontinued.

Simple filtration and discharge are permitted operations under the National Pollutant Discharge Elimination System (NPDES). Building 1171, the principal site in question here, is covered by an NPDES permit which is held by the APG Safety Office. It was thought that if a filter could be demonstrated to filter adequately, and to possess sufficient flow-rate capability, it might have a significant probability of approval. Continued interaction with people from the environmental office served to discourage that idea. As a result, the concept of a closed-loop system evolved. Since the filter was still the principal element of the system, an experiment was devised to demonstrate its effectiveness.

3. FILTER EXPERIMENT

The earlier filter was able to process the waste water at the required flow rates. Its active ingredient was damp, slightly compacted cellulose whose particle size spanned a wide range; it was provided as

sweepings from the Wood Model Shop. This design was considered adequate a decade ago but had never, to our knowledge, been tested by today's standards.

A test was performed to determine whether this system would adequately filter waste water under the conditions obtaining at this facility. The worst-case scenario to be satisfied resulted from the explosives sawing operation, so the test was designed to represent this set of conditions. The normal flow rate for the saw was approximately 5 gal/min continuously, so the filter was required to pass this rate of flow without overflowing. Explosive dust, such as would result from a sawing operation, was prepared in the amount that would accumulate from a half-day operation. TNT was chosen because it is the most representative of the materials processed in this facility. A hose was arranged so as to supply water to a catch pan similar to the one in the saw, and the normal flow rate for the sawing operation was used. The water was run from the catch pan into a filter similar to that formerly used, and the effluent was directed into a large, clean drum. The explosive dust was slowly added to the water in the catch pan, just as though a sawing operation were being performed. The water carried the dust into the filter where the dust was trapped and retained.

The effluent water from the filter was thoroughly analyzed. Sample parameters included oil and grease, total suspended solids (TSS), ammonia, and total Kjeldahl nitrogen (TKN). The measurement of TKN nitrogen involves the use of a specific digestion process. The end result includes all organic, inorganic, and free nitrogen, including the nitrogen from TNT.

The analyses of these samples were done by General Physics (GP) Environmental Services, Gaithersburg, MD, under GP Work Order No. 92-06-133. The Sample Analysis Report is included here as Appendix A. The data from this experiment are shown in Table 1 and can be better understood by plotting them as in Figure 1.

The final result was that the water processed by the cellulose filter exceeded (i.e., was more pure than) the Maryland Department of the Environment standard for potable water. It was cleaner than the raw water supplied for the test.

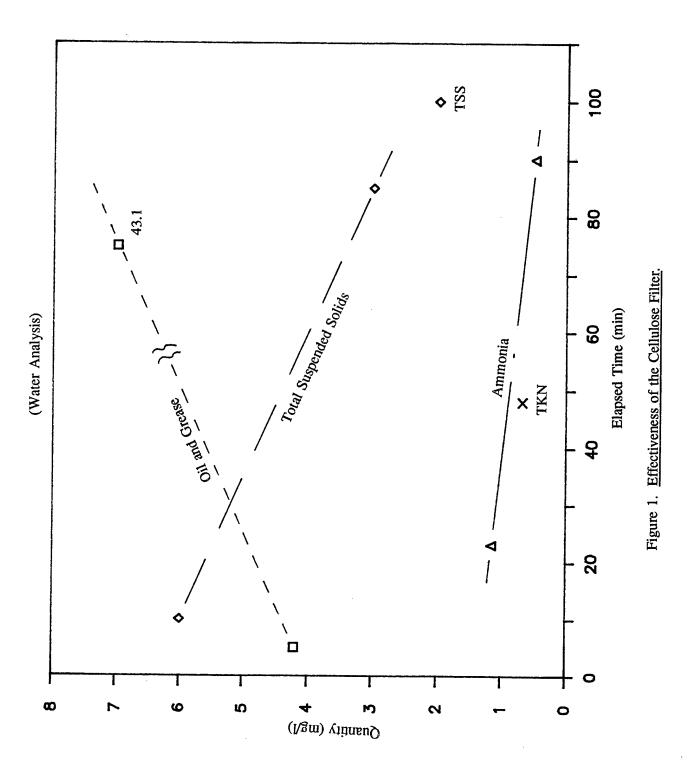
The data points were derived from the analysis reproduced in Appendix A. The data point for oil and grease plotted in the upper right corner, should be much higher than shown, but plotting it correctly would

ARL	Time	Comments	Assay	
Sample No.	of Sample		Substance	Quantity (mg/l)
477-2168-BRL-686	1100	1 liter directly from hose	oil and grease	4.20
478-2168-BRL-687	1110	1 liter directly from hose	TSS	6.00
479-2168-BRL-688	1120–1121 and 1125–1126	1/2 liter each interval	ammonia	1.15
480-2168-BRL-689	1138 and 1158	1/2 liter at each time	TKN	0.680
481-2168-BRL-690	1215	1 liter effluent	oil and grease	43.1
482-2168-BRL-691	1225	1 liter effluent	TSS	3.00
483-2168-BRL-692	1230	1 liter effluent	ammonia	0.500
484-2168-BRL-693	1240	1 liter from pan	TSS	2.00

Table 1. Data From the Filter Experiment

have condensed all the other information into an unacceptablly small region. The validity of this data point is doubtful because neither oil nor grease were included in the contaminants introduced in testing this filter. If they originated at the saw used to saw the explosive, they might be expected to have appeared in the earlier sample that was analyzed for oil and grease. A possible explanation might be found in the composition of the filter aggregate itself, viz., sawdust from the Wood Model Shop. It is not known whether this material had been exposed to these contaminants prior to their insertion into the filter as the filter medium. Regardless, this has no bearing on the efficiency of this material in removing explosives from a pink water stream.

Analyses were done for oil and grease, TSS, TKN, and ammonia. Unfortunately, not all of these were performed on all of the samples taken; however, sufficient analyses were performed to establish levels and trends for these contaminants. The concentration of TSS was shown to decrease, even from the level found in the supply water. The final measurement of 3 mg/l was an order of magnitude lower than allowed for the quarterly average. Appendix B is a letter from the State of Maryland Department of the Environment establishing the standards for water that are acceptable for discharge under Permit No. 90-DP-2517, the permit under which discharge from B-1171 had been allowed. An even higher level of TSS, i.e., 60 mg/l, is permitted as a daily maximum.



The last sample, taken at the 100-min time, was also analyzed for TSS; however, this sample was taken from the empty saw pan, essentially from the source of the water. It could be argued that the source water was becoming less TSS-contaminated as time progressed, that the hose supplying the water for the test was becoming cleaner, and that the filter had no effect. However, throughout the interval in which the TSS were decreasing, TNT powder corresponding to a half day of sawing was added to the source water, and because of the effective filtering action of the cellulose, it was not detected in the TSS analysis.

Analysis for TKN was performed on only one sample, plotted at the 48-min time. The standard indicates that monitoring is required, but that no limits have been set. The analysis showed only 0.680 mg/l, a very low level. The standard for potable water, established by the Maryland Department of the Environment, is 10 mg/l NO₃ as nitrogen, again considerably above the concentration in the filtrate.

Two samples were analyzed for ammonia. Again, the concentration was very low, and it decreased with time during the test. The standard specifies a daily maximum concentration of 90 mg/l, far above our highest assay of 1.15 mg/l.

The experiment previously described completely documented and validated the performance of the cellulose filter. Permits already exist which allow this contaminated filter to be turned in and destroyed as explosive waste, and which allow the discharge of water from this facility, providing that the water meets the currently established standard.

4. CONCEPT

It was earlier proposed that a system be installed in place of the current system to incorporate the cellulose filter and to include a settling tank. According to our experimental data, the settling tank is not necessary, but it would provide an extra measure of protection to the environment into which we would again discharge (clean) waste water. The settling tank would periodically be cleaned and the waste turned in and destroyed, as would the contaminated cellulose.

To avoid any controversy over discharge to the environment, the concept was modified to allow the water to be reused instead of being discharged. The early procedure would be reinstituted, viz., filtration of the pink water with a cellulose filter of the former design; however, no discharge, other than a

minuscule amount of evaporation, would be permitted. This concept would be implemented by closing the loop on the former procedure, i.e., returning the filtered discharge to the supply sump for further use.

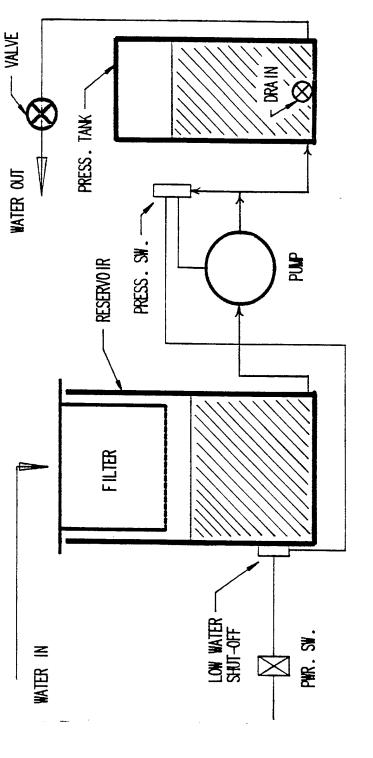
As mentioned earlier, this procedure has been evaluated by the ARL Risk Management Office and found to purify the waste stream so as to make it suitable for discharge under the current license. Thus, it is more than suitable for recycling to the explosives sawing operation and to the steam wash-down system.

The potential for one further problem still exists. After considerable use, the recycled water may dissolve some nonparticulate contaminants. This may become evident by discoloration of the water. If this should occur, these contaminants could be removed by adding activated charcoal to the cellulose filter. As the water cycles through the system, it would be purified of these contaminants. In the event that this procedure is not approved, the contaminated water would be turned in as RHW. It would still be very advantageous to use this system because it would concentrate the contaminants, thus requiring turn-in of a far lower volume of RHW than if all pink water were turned in after only one use.

5. DESIGN

A prototype device has been designed, and this design has been approved by ARL Risk Management and by the APG Department of Safety, Health, and the Environment (DSHE). Figure 2 shows a schematic diagram of this design. The pink water is led from the discharge trough to the input of the filter. Effluent from the filter is held in the reservoir until the pressure switch activates the pump. Water is then pumped from the reservoir into the pressure tank, and from there, directed back to the current operation, viz., steam wash-down or explosives sawing. The water path is indicated by the arrows, indicating flow direction and/or pressure (e.g., to the pressure switch). A low-water limit switch is indicated near the bottom of the reservoir. Its function is to prevent the pump from running dry.

In operation, in the event that the water becomes contaminated (e.g., if the filter were allowed to become saturated), this system can clean itself. The contaminated filter could be removed and turned in for disposal as Resource Conservation and Recovery Act (RCRA) RHW, under existing permits. A clean filter could then be installed, and the system operated with the outlet run directly into the inlet. In this way, the system water would be repeatedly filtered until it again met the purity criterion.





Some water will be lost to evaporation, so occasional replenishment will be required; however, the lost vapor would be pure and so would constitute no hazard to the environment.

A simple implementation of this device has been locally fabricated. It differs in one respect from the schematic diagram of Figure 2. The initial plan was to use gravity feed from the trough directly to the filter. In implementing the design, it seemed more practical to use a third container, buried in the ground at the end of the trough to accept the pink water, and to pump the pink water from there to the cellulose filter at the inlet to the reservoir. Thus, a prefilter was needed, so that explosive particulates would not impede the pumping action or produce a hazard. A coarse bag filter acts as a prefilter, taking large particulate matter from the stream. This filter is sufficiently fine so that the centrifugal pump in this tank can pump the stream easily and safely. The pump impeller and housing are both plastic to add to the safety margin.

Environmental security is further assured by an overpack tank which surrounds the buried tank. In the event of a leak from this tank, the liquid would be contained in the overpack tank.

Figure 3 shows most of the elements of the system. The tank which was buried is shown on the right in the figure. The reservoir, which contains the cellulose filter, is in the left background, and the pressure tank with the pump on top is in the left foreground. A meter stick was placed in the center of the photo to show scale.

A detail of the tank which was buried is shown in Figure 4. The water enters the inlet on top and is distributed by the plastic Tee into the prefilter. This prefilter is shown attached to the Tee in Figure 5. The water is pumped from the buried tank to the inlet of the rectangular tank, which contains the cellulose filter. A detail of this part of the system is shown in Figure 6. When assembled, the water distribution plumbing is supported in notches in the top of the tank, and the filter box is suspended from the plumbing. Plastic hangers were locally fabricated to suspend the filter box from the plastic piping without damaging it. Figures 7 and 8 show the filter box from above and beneath, respectively.

Figure 9 shows the reservoir, with the filter box resting on its top. When this container is full of water, hydrostatic pressure tends to bow out the walls. A belly band was made and installed as shown to make the sides more rigid, and to prevent this bowing. Locking feet were also installed, one near each wheel, so that when the reservoir is correctly located, it can be locked in place.

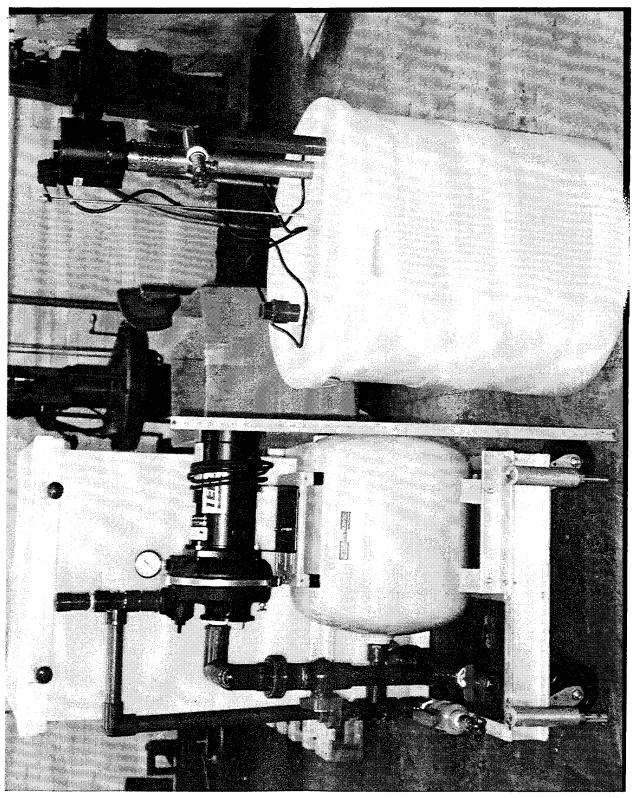


Figure 3. Photograph of the prototype system.

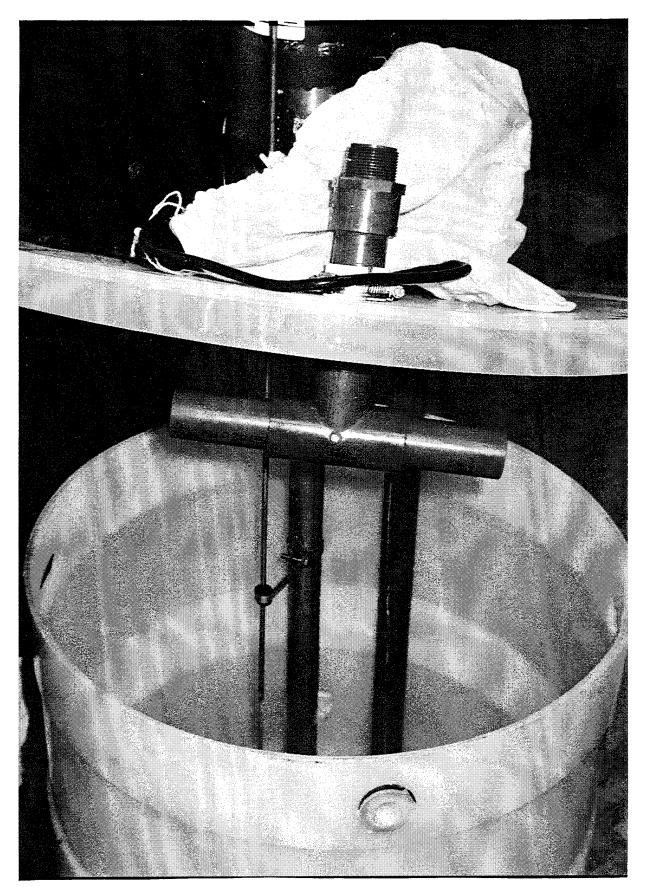


Figure 4. Initial-tank detail showing first element in the system through which the water flows.



Figure 5. Initial-tank detail showing the prefilter attached.

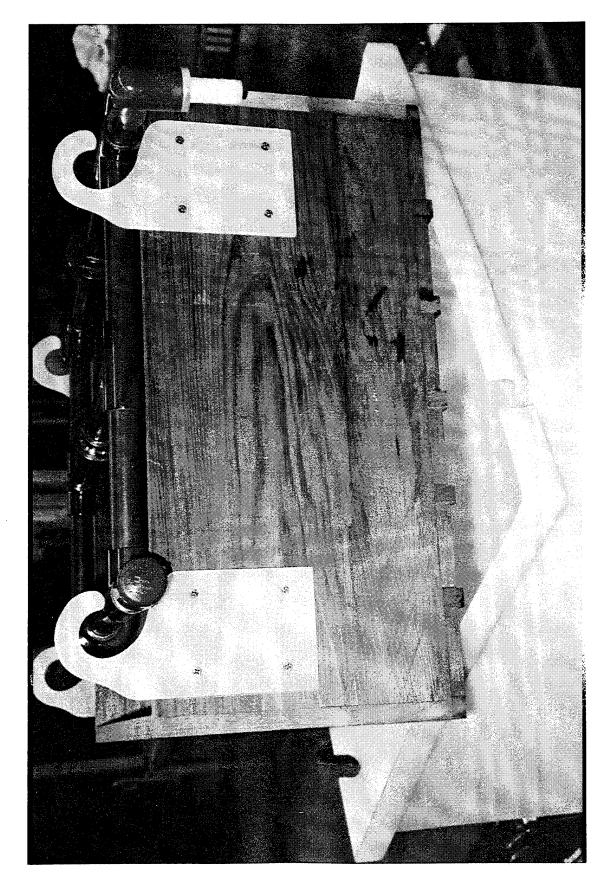
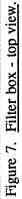


Figure 6. Detail of rectangular tank showing cellulose filter box and water distribution plumbing.







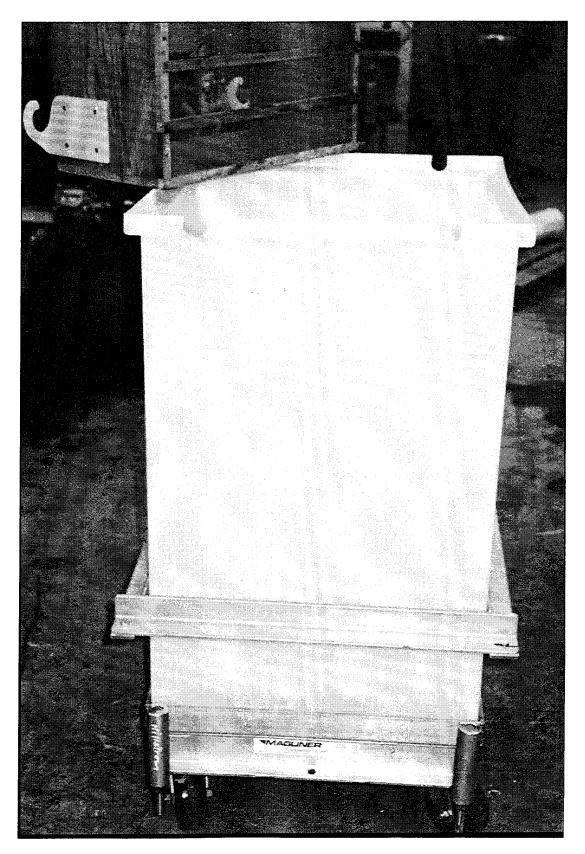


Figure 9. Reservoir showing belly band and locking feet.

The concept described here is being evaluated under local conditions of use, and should be considered for wider application to the energetic materials processing community at large. This will involve the following:

(1) Refining the prototype system and incorporating improvements as indicated.

(2) Operating the system under the entire spectrum of tasks normally performed at this facility (primarily casting, sawing, and steam wash-down). This must include sawing explosives, which requires a large volume flow rate of cooling water to provide the maximum stress on the recycling system.

(3) Monitoring the recycled water for pollutants, periodically and as a function of filter saturation.

(4) Evaluating the process of filter disposal as RHW.

(5) Developing a plan for improving and finalizing the design of the next generation of this system.

7. PAYOFF

This facility is by no means unique in its requirements. All military and civilian facilities that process energetic materials have similar problems, and the solutions that have been implemented are cumbersome, expensive, and still in part, environmentally polluting.

Implementation of this system has enabled the evaluation and further development of a system capable of recycling pink water, so that safety requirements at explosives processing facilities (and likely many other types of facilities) can be met. This system, or something very similar to it, will most likely find widespread application throughout industry in the avoidance of environmental pollution.

APPENDIX A:

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SAMPLE ANALYSIS REPORT

GP Work Order # 92-06-133

SAMPLE ANALYSIS REPORT

Prepared For:

Dir. of Safety, Health & Env. Bldg. EA 4430, Aberdeen Edgewood, MD 21010-5401

ARM 410

Prepared By:

GP Environmental Services 202 Perry Parkway Gaithersburg, Maryland 20877

July 13, 1992

Paul Ioannides, Laboratory Director

GP ENVIRONMENTAL SERVICES WET CHEMISTRY ANALYSIS RESULTS

	GP ID: 9206133-01A Client ID: 477-2168-BRL 686					Collected: 0 6 /17/92 Matrix: WATER
	Parameter	Hethod	Result	Det.Lîm.	Units	Dil. Analyzed by
М	Dil and Grease, Gravimetric	MCAWW 413.1	4.20	1.10	mg∕L	CM 07/07/92
1	X		mg/l			
	GP ID: 9206133.02A Client ID: 478-2168-BRL 687					Collected: 06/17/92 Matrix: WATER
Ú	Parameter	Method	Result	<u>Det,Lim,</u> 1.00	Units mg/L	Dil. Analyzed by CM 06/22/92
	Total Suspended Solids	MCAWW 160.2	6.00	1.00	11/3/ L	un (0),22,72
	GP ID: 9206133-03A					Collected: 06/17/92
	Client ID: 479-2168-BRL 688					Matrix: WATER
	Parameter	Hethod	Result	Det.Lim.	Units	Dil. Analyzed by
	Amnonia	MCAWW 350.3	1.15	0.0300	mg/L	1 VHM 07/10/92
				•		
	GP ID: 9206133-04A					Collected: 06/17/92
	Client ID: 480-2163-BRL 689					Matrix: WATER
	Parameter	Method	Result	Det.Lim.	Units	Dil. Analyzed by
	Total Kjeldahl Nitrogen	MCAWW 351.4	0.680	0.0300	mg/L	1 VHM 07/02/92
	GP ID: 9206133-05A Client ID: 481-2168 <u>-BRL 690</u>					Collected: 06/17/92 Matrix: WATER
			• · · · · · • •		114244	Dil. Analyzed by
	Parameter	Method	Result	Det.Lim.	Units	CM 07/07/92

Notes and definitions for this report: BQL = Below Quantitation Limit Page 2

GP ENVIRONMENTAL SERVICES WET CHEMISTRY ANALYSIS RESULTS

lient 10: 482-2168 BRL 691						ix: WATER
Parameter	Method	Result	Det.Lim.	Units	Dil.	Analyzed by
Total Suspended Solids	NCAWN 160.2	3.00	1.00	mg∕L		CH 06/22/92
GP ID: 9206133-07A Client ID: 483-2168-BRL 692						ected: 06/17/92 ix: WATER
Parameter	Method	Result	Det.Lim.	Units	<u>oil.</u>	Analyzed by
Amnon 1 a	MCAWW 350.3	0.500	0.0300	ng∕L	1	VHM 07/10/92
GP 1D: 9206133-08A					Col	lected: 06/17/92
Client ID: 484-2168-BRL-693					Mati	TIX: WATER
Parameter	Method	Result	Det.Lim.	Units	Dil.	Analyzed by
Total Suspended Solids	MCAWW 160.2	2.00	1.00	mg/L		CM 06/22/92

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Notes and definitions for this report: BQL = Below Quantitation Limit Разе 3

APPENDIX B:

EFFLUENT STANDARD



STATE OF MARYLAND DEPARTMENT OF THE ENVIRONMENT 2500 Broening Highway Baltimore, Maryland 21224 (410) 631- 3304

William Donald Schaefer Governor

Robert Perciasepe Secretary

April 29, 1992

CERTIFIED MAIL

Mr. Michael Flannery Department of the Army Aberdeen Proving Ground Aberdeen MD 21005

Dear Mr. Flannery:

Enclosed are the modified pages of your validated State Discharge Permit No. 90-DP-2517A. Please insert these into your copy of the discharge permit replacing or supplementing the appropriate existing pages.

The effective date of the modification is indicated on the new cover page. The effective date for those limitations or conditions not affected by the modification remains as specified on the first page of the permit.

Should you have any questions concerning the modification, please call Mr. Edward Gertler of the Industrial Discharge Program at (410) 631-3323. Questions regarding the other aspects of the permit should be referred to the Enforcement Program at (410) 631-3409.

Sincerel

Richard Collins, Director Hazardous and Solid Waste Management Administration

RC:cat

cc:

Enclosures

Mr. Harold Dye Mr. Lawrence Liu Mr. Horacio Tablada



STATE OF MARYLAND DEPARTMENT OF THE ENVIRONMENT 2500 Broening Highway Baltimore, Maryland 21224

(410) 631-3304

William Donald Schaefer Robert Perciasepe Governor Secretary STATE DISCHARGE EFFECTIVE DATE PERMIT NUMBER 90-DP-2517A OF MODIFICATION May 6, 1992 NPDES PERMIT NUMBER MD0003565A EFFECTIVE DATE August 8, 1991 EXPIRATION DATE August 8, 1996

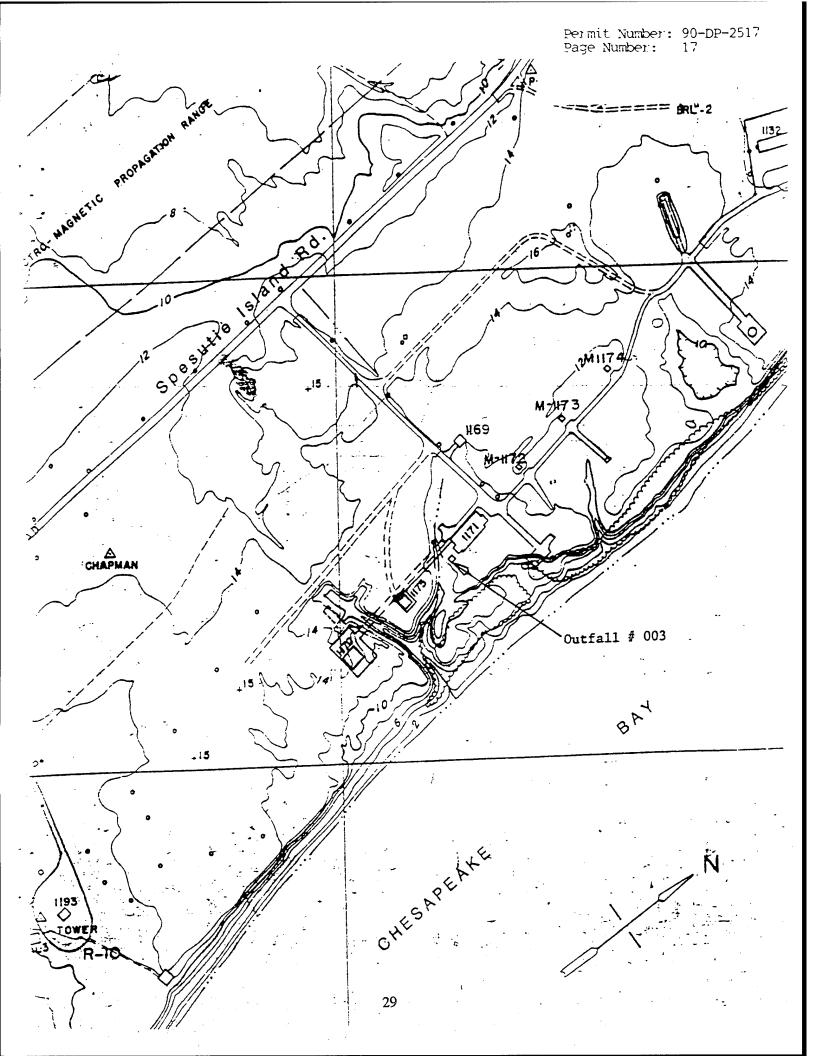
Pursuant to the provisions of Title 9 of the Environment Article, Annotated Code of Maryland and regulations promulgated thereunder and the provisions of the Clean Water Act, 33 U.S.C. § 1251 et seq. and implementing regulations 40 CFR Parts 122, 123, 124, and 125, the Department of the Environment, hereinafter referred to as the "Department," hereby authorizes

> Department of the Army Aberdeen Proving Ground Aberdeen, Maryland 21005

TO DISCHARGE FRO	N
	a facility testing weapon systems, ordnance, and chemical warfare agents
LOCATED AT	1
1///	Aberdeen Proving Ground, Harford County, Maryland
VIA OUTFALL	•
	003, 004, 005, 006, 007, 009, 010, 012, 013, and 014 as identified and describen herein
то	
	Gunpowder River (006), Dipple Creek (012), Woodrest Creek (009, 013), and Bush River (014), which are protected for shellfish harvesting, to Deer Creek (005), which

ek (009, 013), and Bush Deer Creek (005), which is protected for public water supply and recreational trout fishing, and to Sod Run (007), Swan Creek (010), tributary of Chesapeake Bay (003) and Romney Creek (004) which, along with the above-mentioned waterways, are protected for water contact recreation, fishing, aquatic life, and wildlife in accordance with the following special and general conditions and map made a part hereof.

TO



Permit Number: 90-DP-2517 2 Page Number:

SPECIAL CONDITIONS -:

EFFLUENT LIMITATIONS AND MONITORING REQUIREMENTS ż

Beginning on the effective date of the permit and lasting through the expiration date the permittee is authorized to discharge from outfalls 003 and 004, consisting of washdown water from shell cases and equipment.

Such discharge shall be monitored by the permittee and limited at exit from charcoal filters as specified below:

EQUIREMENTS		Sample	BOX :	estimated	grab	grab	grab	grab
MONITORING REQUIREMENTS	•	Measurement Frequency	1/month			1/month	1/month ⁴³	1/month
· · ·	(Specify)	Daily <u>Maxim</u> um	Ð	15 mc/l				-
EFFLUENT LIMITATIONS	<u>Other Units (Specify)</u>	Quarterly <u>Average</u>	£	Ð	Ð	(1)	(1)	
EFFLUENT	η	Daily <u>Maximum</u>	N/A	N/A	N/A	N/A	N/A	
	(Ibs/day)	Quarterly <u>Average</u>	N/A	N/A	N/A	N/A	N/A	
CONSTITUENT			Flow (gpd)	Oil and Grease	Total Suspended Solids	Total Ammonia (as N)	Total Nitrogen (as N)	

The pH shall not be less than 6.0 nor greater than 9.0 and shall be monitored once per month by grab sample.

There shall be no discharge of floating solids or persistent foam in other than trace amounts. Persistent foam is foam that does not dissipate within one half-hour of point of discharge.

Monitoring required without limits. Ξ

During the months of June, July, and August only. 2

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I. SPECIAL CONDITIONS

B. EFFLUENT LIMITATIONS AND MONITORING REQUIREMENTS

Beginning on the effective date of the permit and lasting through the expiration date the permittee is authorized to discharge from outfalls 005, 006, and 007, consisting of vehicle and aircraft washwater, and stormwater. Such discharge shall be monitored by the permittee and limited at ditch from ponds (005 and 006) and ditch from third sediment pond (007) as specified below:

CONSTITUENT		EFFLUENT LIMITATIONS	MITATIONS		MONITORING REQUIREMENTS	QUIREMENTS
	(Ibs/day)		<u>Other Units (Specify)</u>	(Specify)		
	Quarterly <u>Average</u>	Daily <u>Maximum</u>	Quarterly <u>Average</u>	Daily <u>Maximum</u>	Measurement <u>Frequency</u> ⁽¹⁾	Sample <u>Type</u>
Flow, gpd	N/A	N/A	ß	3	1/month	grab
Total Petroleum Hydrocarbons	N/A	N/A	3	15 mg/l	1/month	grab
Total Suspended Solids ⁽³⁾	N/A	N/A	30 mg/l	60 mg/l	1/month	grab
The pH shall not be less than 6.0 ⁽⁴⁾ nor greater than 9.0 and shall be monitored once per month by grab sample.	han 6.0 ⁽⁴⁾ nor g	jreater than 9	.0 and shall b	e monitored on	ce per month by gr	ab sample.

There shall be no discharge of floating solids or persistent foam in other than trace amounts. Persistent foam is foam that does not dissipate within one half-hour of point of discharge.

All parameters to be sampled when there has been no precipitation during the previous 24 hours. Ξ

⁽²⁾ Monitoring required without limits.

Net TSS limit for Outfall 005 only. Background sample for intake water will be taken at culvert uphill from oil-water separator. ල

The lower pH limit for Outfall 007 will be the ambient pH of the intake water at the time of discharge. £

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I. SPECIAL CONDITIONS

C. EFFLUENT LIMITATIONS AND MONITORING REQUIREMENTS

Beginning on the effective date of the permit and lasting through the expiration date the permittee is authorized to discharge from outfalls 009, 010, 012, and 013, consisting of noncontact cooling water. Such discharge shall be monitored by the permittee and limited at 2-ft. corrugated pipe (009), 2-ft. storm drain pipe (010), 200 ft. downstream from head wall (012), and at exit from pond before riprap (013) as specified below:

MONITORING REQUIREMENTS		Sample <u>Type</u>	estimated	<u>م</u>	grab
MONITORING		Measurement Frequency ⁽¹⁾	1/month	1/month	<pre><0.1 mg/l 1/month ⁽³⁾⁽⁴⁾</pre>
 <u>-</u>	(Specify)	Daily <u>Maximum</u>	(2)	R	<0.1 mg/l
EFFLUENT LIMITATIONS	<u>Other Units (Specify)</u>	Quarterly <u>Average</u>	(2)	ß	N/A
EFFLUENT	(lbs/day)	Daily <u>Maximum</u>	N/A	N/A	N/A
	<u>/sql)</u>	Quarterly <u>Average</u>	N/A	N/A	N/A
CONSTITUENT			Flow, gpd	Temperature, [°] F	Total Residual Chlorine

There shall be no discharge of floating solids or persistent foam in other than trace amounts. Persistent foam is foam that does not dissipate within one half-hour of point of discharge.

All parameters to be sampled when there has been no precipitation for 24 hours. ε

⁽²⁾ Monitoring required without limits.

⁽³⁾ To be analyzed within 15 minutes after collection of the sample.

Outfall 009 and 010 to be monitored from 90 and 180 days, respectively, after the effective date of the permit through the expiration date. €

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SPECIAL CONDITIONS

1.

D. DEFINITIONS

- 1. The "monthly, quarterly, semi-annual, or annual average" effluent limitation by concentration means the highest allowable value calculated by computing the arithmetic mean of all the daily determinations of concentration made during any calendar month, 3-month, 6-month, or 12-month period respectively.
- 2. The "daily maximum" effluent limitation by concentration means the highest allowable reading of any daily determination of concentration.
- 3. "Daily determination of concentration" means one analysis performed on any given sample representing 24-hours flow, with one number in mg/l as an outcome.
- 4. "Grab Sample" means an individual sample collected in less than 15 minutes.
- 5. "i-s" = immersion stabilization means a calibrated device immersed in the effluent stream until the reading is stabilized.

6. The "daily maximum" temperature means the highest temperature observed during a 24-hour period or, if flows are of shorter duration during the operating day.

- "Bypass" means the intentional diversion of wastes from any portion of a treatment facility.
- 8. "Upset" means the exceptional incident in which there is unintentional and temporary noncompliance with technology-based permit effluent limitations because of factors beyond the reasonable control of the permittee. An upset does not include noncompliance to the extent caused by operational error, improperly designed treatment facilities, inadequate treatment facilities, lack of preventive maintenance, or careless or improper operation.
- 9. "Estimated" flow means a calculated volume or discharge rate which is based on a technical evaluation of the sources contributing to the discharge including, but not limited to, pump capabilities, water meters, and batch discharge volumes.
- 10. "Total Nitrogen" means the sum of total Kjeldahl nitrogen, nitrate, and nitrite as nitrogen.

E. <u>TOXIC POLLUTANT REPORTING</u>

The permittee shall notify the Department as soon as it is known or suspected that any toxic pollutants which are not specifically limited by this permit have been discharged at levels specified in 40 CFR Part 122.42(a).

F. <u>REMOVED SUBSTANCES</u>

- 1. Within 90 days of the effective date of the permit, unless already submitted with the application, the permittee shall submit to the Department on a form provided, the following information:
 - a. Locate, on a suitable map, all areas used for the disposal of any Removed Substances as defined by General Condition B.7;
 - b. The physical, chemical, and biological characteristics, as appropriate, quantities of any Removed Substances handled, and the method of disposal;
 - c. If disposal is handled by other than the permittee, identify the contractor or subcontractor, their mailing address, and the information specified in a and b above.

INTENTIONALLY LEFT BLANK.

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- 2 ADMINISTRATOR ATTN DTIC DDA DEFENSE TECHNICAL INFO CTR CAMERON STATION ALEXANDRIA VA 22304-6145
- 1 DIRECTOR ATTN AMSRL OP SD TA US ARMY RESEARCH LAB 2800 POWDER MILL RD ADELPHI MD 20783-1145
- 3 DIRECTOR ATTN AMSRL OP SD TL US ARMY RESEARCH LAB 2800 POWDER MILL RD ADELPHI MD 20783-1145
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ABERDEEN PROVING GROUND

5 DIR USARL ATTN AMSRL OP AP L (305)

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- 2 OFFICE OF NAVAL RESEARCH ATTN DR A FAULSTICK CODE 23 800 N QUINCY STREET ARLINGTON VA 22217-5000
- 1 COMMANDER ATTN SMCAR QA HI LIB RADFORD ARMY AMMUNITION PLANT RADFORD VA 24141-0298
- 1 OFFICE OF THE CHIEF NAVAL RESEARCH ATTN R MILLER CODE 473 800 N QUINCY STREET ARLINGTON VA 22217-5000
- 1 COMMANDER ATTN SEA 061 DR R BOWEN NAVAL SEA SYSTEMS COMMAND WASHINGTON DC 20362
- 1 COMMANDER ATTN TECHNICAL LIBRARY CODE 604 NVL EXPLSV ORD DSPSL TECHLGY CTR INDIAN HEAD MD 20640
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- 1 COMMANDER ATTN CODE G13 NAVAL SURFACE WARFARE CENTER DAHLGREN VA 22448-5000
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- 1 DIRECTOR ATTN ATOR TSL TRAC WSMR WSMR NM 88002-5502
- 1 COMMANDANT ATTN ATSF TSM CN USAFAS FORT SILL OK 73503-5600
- 3 NAVAL ORDNANCE STATION ATTN MR G NAUFLETT MR R FARNCOMB DR S PETERS INDIAN HEAD DETACHMENT INDIAN HEAD MD 20640-5000
- 1 COMMANDER ATTN R GEISLER CODE AFRPL MKPA USAF ROCKET PROPULSION LAB EDWARDS AFB CA 93523
- 3 WL MNME ATTN G PARSONS T FLOYD S STRUCK EGLIN AFB FL 32542-5000

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- 3 DIRECTOR ATTN DR G BUNTAIN M STINECIPHER K LEE LOS ALAMOS NATIONAL LABORATORY PO BOX 1663 LOS ALAMOS NM 87545
- 1 SANDIA NATIONAL LABORATORIES ATTN DR E MITCHELL PO BOX 5800 M S 0326 ALBUQUERQUE NM 87185-0326
- 1 DIRECTOR ATTN DR R CARLING SANDIA NATIONAL LABORATORIES LIVERMORE 94557-0096
- 1 HOLSTON ARMY AMMUNITION PLANT ATTN MR C SMITH BLDG 8 WEST STONE DRIVE KINGSPORT TN 37660
- 1 THIOKOL CORPORATION ATTN TECH LIBRARY ELKTON DIVISION PO BOX 241 ELKTON MD 21921-0241
- 1 AMC FIELD SAFETY ACTIVITY ATTN OS D W P YUTMEYER CHIEF CHARLESTOWN IN 47111

2 USATCES ATTN SMCAC EST J BYRD R DAVIDSON SAVANNAH IL 61074-9639

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- 1 CDR USACSTA ATTN STECS AA HT MR G APPEL
- DIR USARL 13 ATTN AMSRL WT A W BARROWS AMSRL WT TB L VANDE KIEFT W HILLSTROM E SCHLEGEL D BOWMAN **R FREY** AMSRL WT NC J SULLIVAN AMSRL WT PC **R A FIFER** AMSRL WT PA A A JUHASZ AMSRL OP RK AP E VAN RIPER **R HERRON R SCHWANKE** STEAP SH E M KANOWITZ

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