

**FINAL DESIGN CONCEPT REPORT
SR-24, Ellsworth Road to Ironwood Drive
Interim Phase II**

**TRACS No. 024 MA 001 H8915 01L/02L
Federal Project No. STP-024-A(200)T**

PREPARED FOR:



**ARIZONA DEPARTMENT OF TRANSPORTATION
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Expires 09/30/17

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January 31, 2017

PROJECT DETERMINATION FORM

Project Number	County and ADOT District	Project Name and Highway
024 MA 001 H8915 01L/02L	Maricopa/Pinal	SR-24, Ellsworth Road to Ironwood Rd-Interim Phase II
Fed No. STP-024-A(200)T	Central District	SR-24

Project Description: Final Design Concept Report (DCR) – SR-24, Ellsworth Road to Ironwood Road – Interim Phase II

Existing Program	Program Year	Programmed Budget	Operating Partnership					
	N/A	N/A	Category					
Yes	No	DCR Construction Cost Estimate	S	F	T	D	Z	N/A
	x	\$136,512,143			X			

Public Hearing: In the Highway Development Process, at least one public hearing or the opportunity for a hearing will be offered for any project that:

<input type="checkbox"/>	Requires a significant amount of new right-of-way;	<input type="checkbox"/>	Otherwise has a significant social, economic, environmental or other effect
<input type="checkbox"/>	Substantially changes the layout or function of connecting roadway or the facility being improved;	<input type="checkbox"/>	Is controversial on environmental grounds;
<input type="checkbox"/>	Has a significant adverse impact on abutting real property;	<input type="checkbox"/>	Or has significant floodplain encroachment
<input checked="" type="checkbox"/>		X *	None of the above conditions apply

Recommends:

Yes:	No:	Public Forum	Environmental Category		
X *		Offer a combined Location / Design Hearing	Class I	Class II	Class III
	x	Offer Separate Location/Design Hearing			X
	x	Hold a Design Public Hearing			

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Comments:

*An EA was completed in May 2011 for the DCR for SR802/now SR 24 from Loop 202 Santan to Ironwood Rd. An EA re-evaluation will be completed for the SR 24 Interim Phase II DCR for Ellsworth Rd. to Ironwood Rd. The current EA re-evaluation included scoping letters to Agencies and adjacent/affected property owners. In the future, as final design progresses to the next stages of development with more details and Construction schedule information available, a Project Public information meeting will be held.

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EXECUTIVE SUMMARY

Introduction

In 2011, ADOT in conjunction with Federal Highway Administration (FHWA), completed a Design Concept Report (DCR) and an Environmental Assessment (EA) for the Gateway Freeway (SR-24) Corridor between the Santan Freeway (SR 202) and Ironwood Drive, formally known as SR 802.

In 2014, ADOT completed the construction and opened to traffic the first segment of this SR24 corridor from SR202 to Ellsworth Road.

Currently, ADOT in conjunction with FHWA, is in the process of developing a solution that includes construction of an interim roadway within the footprint of the future segment of SR-24 between Ellsworth Road and Ironwood Drive. ADOT and FHWA are also revisiting the vertical alignment for the ultimate SR-24 design in order to identify cost saving improvements.

The purpose of this study is to update the original Design Concept Report (DCR) and complete an Environmental Reevaluation of the original Environmental Assessment (EA) completed in 2011.

The purpose of the interim improvements is to provide a transportation corridor that supports existing and predicted traffic demands and improving connectivity in the region until 2027 when funding is anticipated to become available for the final SR 24 build-out.

This update is intended to preserve the access control plan for this corridor and does not change any access points or their locations from what was outlined in the 2011 DCR. Additionally, this update maintains the horizontal geometry of the original DCR, but modifies the vertical geometry/profile for SR24 from east of Williams Field Road to Ironwood Drive.

Finally, this update to the 2011 DCR is intended to follow the same document format; it references the original DCR throughout the report and provides updated information where relevant and required.

Regional Planning

No updates, see the ADOT 2011 SR-24 DCR

Programming

The Arizona Transportation Board has an approved Five-Year Transportation Facilities Construction Program in Fiscal Year (FY) 2017. However, no funding has been provided for the SR-24 corridor in the ADOT Five-Year Transportation Program.

Two projects are currently planned within or adjacent to the study corridor and are included in the Regional Transportation Plan Freeway Program (RTPFP) in Group 3 (2027 - 2035) as shown below.

Current Projects in the RTPFP Group 3

Route	Freeway Segment	Type of Work	RTPFP Budget (\$000)	RTPFP Group	RTPFP Group (years)
SR 24	SR 202L, Santan - Ellsworth Rd, Ph2	Freeway Upgrade	46,900	3	2027 - 2035
SR 24	Ellsworth Rd - Meridian Rd	New Freeway	212,600	3	2027 - 2035

Additional funding would need to be provided by ADOT and/or FHWA for the segment of SR-24 from Meridian Road to Ironwood Drive, since that segment of the freeway is located outside of Maricopa County and is not eligible for RTP funds.

Transit

No updates, see the ADOT 2011 SR-24 DCR

Phoenix-Mesa Gateway Airport

No updates, see the ADOT 2011 SR-24 DCR

MITIGATION MEASURES

No updates at this time. As part of the Environmental Assessment Re-evaluation currently being prepared for this study, Mitigation Measures will be updated.

1.0 INTRODUCTION

1.1 PROJECT LOCATION

The limits of the original Design Concept Report (DCR) for the State Route 24 (SR-24) Freeway, completed in April 2011 by ADOT, began at the SR 202L freeway and extended to Ironwood Drive. The segment from SR 202L to Ellsworth Road (Phase I of the ADOT DCR 2011) was subsequently constructed and opened to traffic in 2014. The project limits for this DCR update begins west of the existing, interim at-grade intersection of SR-24 at Ellsworth Road and extend east to Ironwood Drive, a distance of approximately 4.6 miles.

This project is located in or adjacent to the cities of Mesa and Apache Junction and the towns of Gilbert and Queen Creek, in Maricopa and Pinal Counties in Arizona (Figure 1). The proposed project is within the Arizona Department of Transportation's (ADOT) Central District.

The study area limits consist of approximately 4.6 miles of the new SR-24 corridor from Ellsworth Road to Ironwood Drive. Figure 2 on page 1-3 shows the defined study area for the SR-24 corridor study that encompasses these project limits.

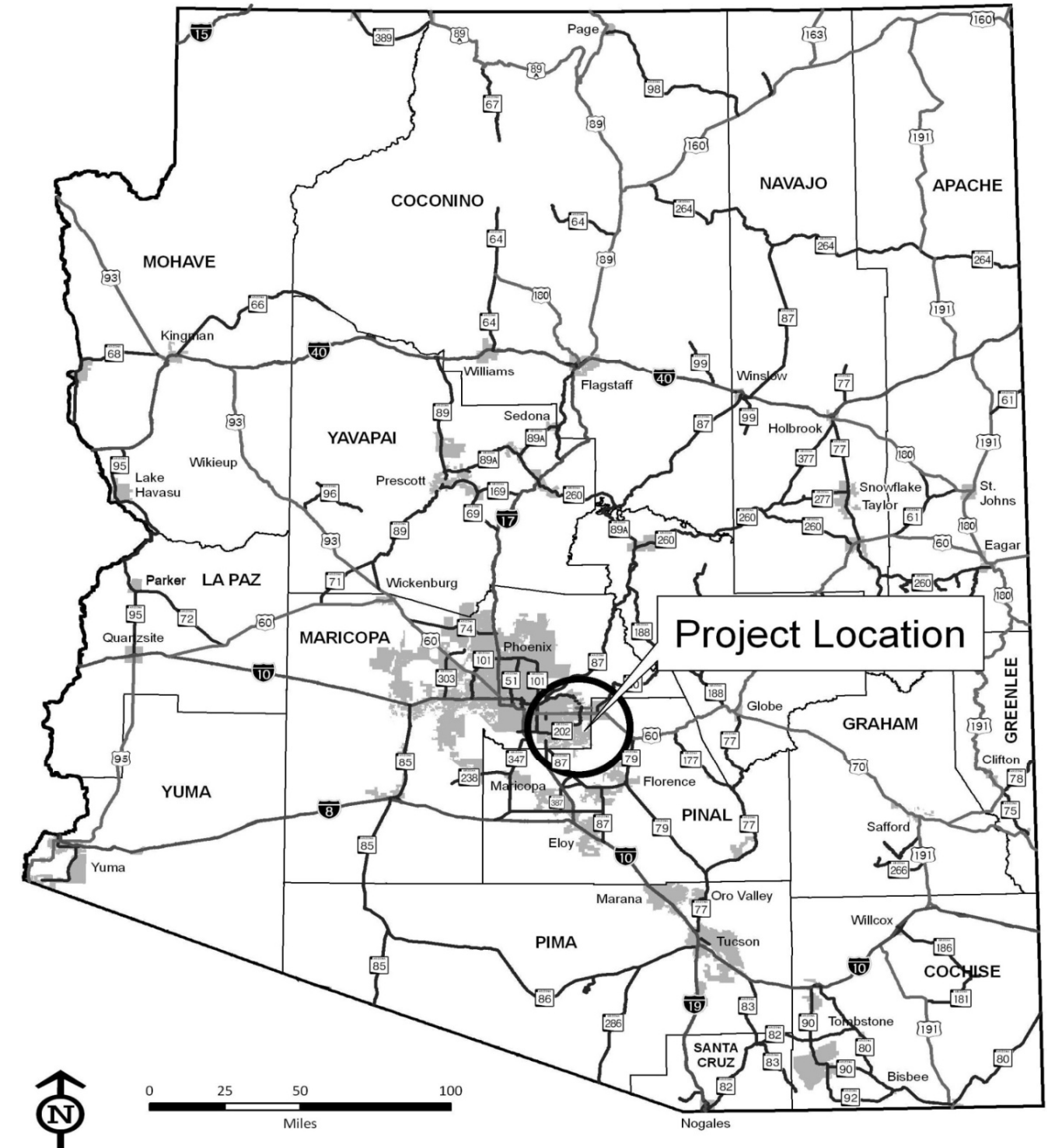
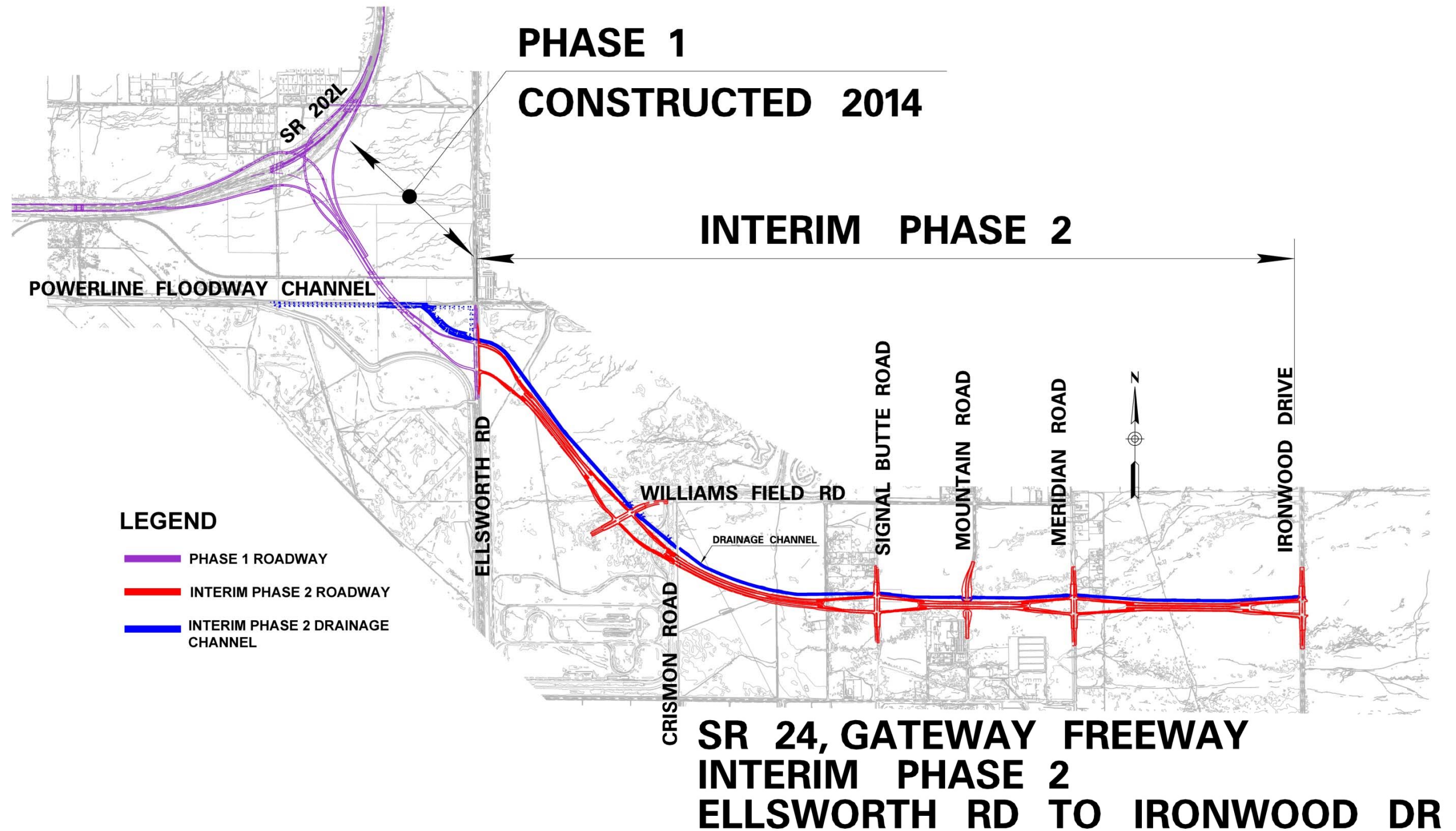


Figure 1 – Project Location Map

Figure 2 – Study Area for Interim SR-24 Phase 2



1.2 NEED FOR THE PROJECT

See ADOT DCR 2011 Section 1.2 for Need of the SR-24 project. The goals for developing an interim solution for the remaining 4.6 miles of the proposed SR-24 corridor between Ellsworth Road and Ironwood Drive are as follows:

- Promote economic development by linking future economic activity centers, supporting future population and employment growth sooner rather than later with an interim solution.
- Provide a corridor with the projected capacity to improve transportation options between the cities of Mesa and Apache Junction and the towns of Gilbert and Queen Creek, in Maricopa and Pinal Counties in the southeast Valley.

1.3 CHARACTERISTICS OF THE CORRIDOR

This segment of SR-24 will furnish a vital transportation artery in southeastern Maricopa County that will provide high capacity freeway access between the southeastern Maricopa and northern Pinal County communities to the Phoenix metropolitan area. This new freeway will also support the planned growth of Phoenix-Mesa Gateway Airport and the planned residential, commercial, industrial and warehouse/distribution center developments within the study area. SR-24 will also provide a vital link between the Regional Freeway System and the future State Highway System corridors that have been identified within Pinal County.

1.3.1 Roadway Characteristics

See ADOT DCR 2011 Section 1.3.1

Within the project limits, Ellsworth Road is classified as a six lane arterial street, with three lanes in the northbound and southbound directions of travel that are separated by a raised median. Phase I of the ADOT DCR 2011 was constructed and completed in 2014. In the vicinity of SR-24, Ellsworth Road was widened to five lanes, with two lanes in the northbound direction and three lanes in the southbound direction separated by a raised median.

Within the project limits, Williams Field Road is classified as a future six lane arterial street, with three lanes in the westbound and eastbound directions of travel separated by a raised median. Williams Field Road currently does not exist between Ellsworth and Signal Butte Roads, and is a two lane roadway between Signal Butte and Meridian Roads. Funding for Williams Field Road is not currently identified in the RTP Arterial Streets Program and would likely be constructed as adjacent development occurs in the area.

Within the project limits, Crismon Road is classified as a future four lane arterial street, with two lanes in the northbound and southbound directions of travel separated by a raised median. Crismon Road does not currently exist in the vicinity of SR-24. Funding for Crismon is not currently identified in the RTP Arterial Streets Program and would likely be constructed as adjacent development occurs in the area.

Within the project limits, Signal Butte Road is classified as a future six lane arterial street, with three lanes in the northbound and southbound directions of travel separated by a raised median. Signal Butte Road does not currently exist in the vicinity of SR-24. Funding for the construction of Signal Butte Road is identified in Group 2 (2019 - 2026) of the RTP Arterial Streets Program.

Within the project limits, Mountain Road is classified as a four lane major collector street, with two lanes in the northbound and southbound directions of travel separated by a striped median. Mountain Road is currently a two lane roadway at the SR-24 crossing.

Within the project limits, Meridian Road is classified as a future six lane arterial street, with three lanes in the northbound and southbound directions of travel separated by a raised median. Meridian Road does not currently exist in the vicinity of SR-24. Funding for Meridian Road is not currently identified in the RTP Arterial Streets Program and would likely be constructed as adjacent development occurs in the area.

Ironwood Drive is an existing four lane major arterial street with two lanes in the northbound and southbound directions of travel separated by an open median. Ironwood Drive is classified as a Regionally Significant Road with a six lane roadway section. The Pinal County Small Area Transportation Study (SATS) identified Ironwood Drive as a long-term priority for widening the existing roadway to a six lane facility.

1.3.2 Transit Facilities and Routes

See ADOT DCR 2011 Section 1.3.2

1.3.3 Land Use

See ADOT DCR 2011 Section 1.3.3

City of Mesa has requested that the new right-of-way accommodate a future multi-use path that may follow the SR-24 corridor. At this time the area north of the channel maintenance road, within the new right of way between Ellsworth Road and Ironwood Drive, has been set aside for a future trail.

1.3.4 Phoenix-Mesa Gateway Airport

See ADOT DCR 2011 Section 1.3.4

1.3.5 Utilities and Railroads

Existing utilities within the study area were identified based on information obtained from ADOT as-built drawings, as well as facility plans and quarter-section maps obtained from each local jurisdiction and utility company. These utilities are presented in Table 1 on the following page

Table 1 – Existing Utility Crossings

Cross Street	Utility Description
Ellsworth	Southwest Gas 10" gas line; Mesa 16" & 20" DIP water lines, 13-2" Conduits; Century Link telephone lines; SRP underground 12KV power line
222nd St	SRP 12kV overhead power line
Signal Butte Road	SRP 12kV overhead power line
Mountain Road	Southwest Gas 4" PE gas line; Mesa 12" PVC sanitary sewer and 16" ACP water line
Meridian Road	SRP 12kV overhead power line
Approx Sta 273+00	WAPA 230kV overhead power line on lattice towers.
Ironwood Drive	MediaCom CATV fiber optic line

1.3.6 Drainage

See detailed drainage report in Appendix D for additional information.

1.3.7 Right-of-Way

Right of Way was acquired for Phase 1 of the ADOT 2011 DCR. All new improvements east of Ellsworth Road will require new right-of-way. Any improvements west of Ellsworth Road will fit within the existing right-of-way that was acquired as part of Phase 1 of the ADOT DCR 2011.

1.3.8 Structures

There are no existing bridge or retaining wall structures between Ellsworth Road and Ironwood Drive.

1.3.9 Signing and Lighting

There is no existing Signing and Lighting within this study area between Ellsworth and Ironwood Drive.

1.3.10 Freeway Management Systems

There is no existing Freeway Management System (FMS) within the study area between Ellsworth and Ironwood Drive

1.3.11 Geotechnical Conditions

There are no updates see section 1.3.11 from the ADOT DCR 2011.

1.3.12 Previous Projects

The ADOT Milepost Strip Map Shows the project listed in Table 2 below:

Table 2 – Previous Projects

Freeway Corridor	Project Number and/or TRACS Number	Milepost	As-Built Date	Description
SR 24	024 MA 000 H6867 01C	0.00 - 1.00	2015	SR 202L to Ellsworth Road

2.0 TRAFFIC AND CRASH DATA

Supporting Traffic and Crash Data analysis and mitigation measures for the Interim Phase 2 preferred alternative has been provided in Appendix E to this report.

3.0 EVALUATION OF ALTERNATIVES

3.1 BACKGROUND

In 2011 ADOT completed the DCR for SR-24, Gateway Freeway (SR 202L – Ironwood Drive). The DCR provided an implementation plan of three phases. In May of 2014 ADOT completed construction of Phase 1 based on the DCR. Phase 2 of the DCR is to complete the remaining elements of the ultimate SR202L/SR-24 TI, widen SR 202L between Recker Road and the east Power Road ramps, widen SR 202L between the SR202L/SR-24 TI and Guadalupe Road, and extend the SR-24 mainline improvements east to Meridian Road as depicted in Figure 27 from ADOT 2011 DCR

The Phase 3 of the DCR is to extend the ultimate freeway improvements from Meridian Road to Ironwood Drive as depicted in Figure 28 from ADOT 2011 DCR

In March 2015 MAG completed a feasibility study for interim Phase 2, between Ellsworth and Ironwood, which looked at interim concepts that would:

- Promote economic development by linking future economic activity centers, supporting future population and employment growth sooner rather than later with an interim solution
- Provide a corridor with the projected capacity to improve transportation options between the cities of Mesa and Apache Junction and the towns of Gilbert and Queen Creek, in Maricopa and Pinal Counties in the southeast Valley.

The MAG 2015 Feasibility study developed 4 interim SR-24 Options; A1, A2, B and C.

3.2 ALTERNATIVES EVALUATION PROCESS – TIER 1

The Tier 1 process was used in the original ADOT 2011 DCR to evaluate the location of SR-24 corridor.

3.3 ALTERNATIVES EVALUATION PROCESS – TIER 2

3.3.1 Introduction

The alternatives from the MAG feasibility study were evaluated with the Tier 2 analysis. The Tier 2 evaluation process quantitatively examined how well each alignment alternative would address the primary objectives of the evaluation criteria.

3.3.2 Description of Alternatives

Alternative A1: Undivided, Two Lanes in Each Direction

The strategy behind Alternative A1 would be to provide a simple four-lane typical section using the SR-24 mainline horizontal geometry as proposed in the ADOT DCR 2011. See Figure 3 on page 3-3. This alternative includes the following:

- 8-foot paved outside shoulders.
- 12-foot travel lanes.
- At-Grade intersections at crossroads.
- Mainline Profile at-grade, future cross roads above grade

Alternative A2: Divided, Two Lanes in Each Direction

The strategy behind Alternative A2 would be to provide a simple four-lane typical section using the SR-24 mainline horizontal geometry as proposed in the ADOT DCR 2011. Opposing lanes of traffic would be separated by the 26 foot graded median planned for the ultimate freeway typical section. This alternative would make use of the interim pavement surface in the ultimate condition. See Figure 3 on page 3-3. This alternative further included the following:

- 4-foot paved inside shoulders and 10-foot paved outside shoulders.
- Roadway pavement placed in the ultimate location.
- Ultimate Median grading.
- At-Grade intersections at crossroads.
- Mainline Profile at-grade, future ultimate crossroads above grade over Mainline

With this alternative, the interim outside edge of pavement would be 8ft into the future 12ft lane.

Alternative B: Undivided, One Lane in Each Direction

Alternative B would implement the horizontal geometry of the future ramps from the crossroad to the mainline. From the mainline and between ramp terminals, a temporary alignment could be incorporated that largely uses the mainline offset to the outside lane(s) and auxiliary lanes. This alternative could be implemented using the eastbound or westbound ramp alignments from the crossroad to crossroad because it is intended to be a two-lane roadway separated by a double yellow stripe. See Figure 4 on page 3-4. This alternative further included the following:

- 8-foot paved outside shoulders.
- Roadway pavement placed in the ultimate location.

- At-grade intersections at interchange crossroads.
- Mainline Profile at-grade between successive interchange entrance ramps to exit ramps. Ultimate profile is above grade over future interchange cross roads.

Alternative B was removed from consideration because the traffic operation analysis would not be feasible as well as compatibility with the ultimate buildout.

Alternative C: Divided, Two Lanes in Each Direction

Alternative C also would implement the horizontal geometry of the future ramps from the crossroad to the mainline. From the mainline and between ramp terminals, a temporary alignment could be incorporated that largely uses the mainline offset to the outside lane(s) and auxiliary lanes. See Figure 4 on page 3-4. This alternative further included the following:

- 6-foot paved inside shoulders and 12-foot outside paved shoulders.
- Roadway pavement placed in the ultimate location.
- At-grade intersections.
- Ultimate Outside Grading
- Mainline Profile at-grade between successive interchange entrance ramps to exit ramps. Ultimate profile is above grade over future interchange cross roads.

In all alternatives the Mainline Ultimate profile was reevaluated to coordinate with the interim alternatives. In all options the horizontal geometry of SR-24, Ramps, and Crossroads were not reevaluated from the ADOT DCR 2011 recommended alternative. No Changes to access points from the ADOT DCR 2011. SR-24 must not cutoff connectivity of Mountain Road between Williams Field Road and Pecos Road and must be a grade separated crossing the SR-24 alignment.

3.3.3 Evaluation Criteria

- Right-of-Way
- Traffic Analysis
- Compatibility with the planned Ultimate Cross Section
- Local Access
- Pump Station
- Estimated Construction Cost

A description of each of the evaluation criteria was developed for use of the Project Team in conducting the alternative evaluations.

Right-of-Way

The interim SR-24 and its impacts to the ultimate configuration should minimize right-of-way acquisition impacts. Right-of-way that is established should fit the footprint of the interim configuration as well as the ultimate configuration. This performance measure was quantified by reviewing the ultimate grading footprint based on the alternative options being at or above grade.

Traffic Analysis

The interim SR-24 should operate at an acceptable level for the interim buildout in the year 2025 while still providing capability with the ultimate buildout and providing mobility throughout the corridor.

Compatibility with Ultimate

The interim SR-24 alternative should be compatible with the ultimate SR-24 and minimize “Throw-away” by constructing the interim roadway that can be used in the ultimate SR-24 roadway. The location of the interim lane lines relative to the ultimate lane lines, having lanes fall in the same location could result in less restripe in the ultimate configuration.

Development Impacts

The interim SR-24 should seek to minimize impacts to the opportunity for future development.

The interim SR-24 should minimize the amount of earthwork needed with the goal to achieve a balanced earthwork project.

Pump Station

The interim SR-24 vertical profile reevaluation goal should be to eliminate the need for a Pump Station for the interim as well as for the ultimate configuration

Estimated Construction Cost

The interim SR-24 should be a cost-effective solution. Impacts to the ultimate configuration construction costs should also be considered.

Figure 3 - Typical Sections Options A1 & A2

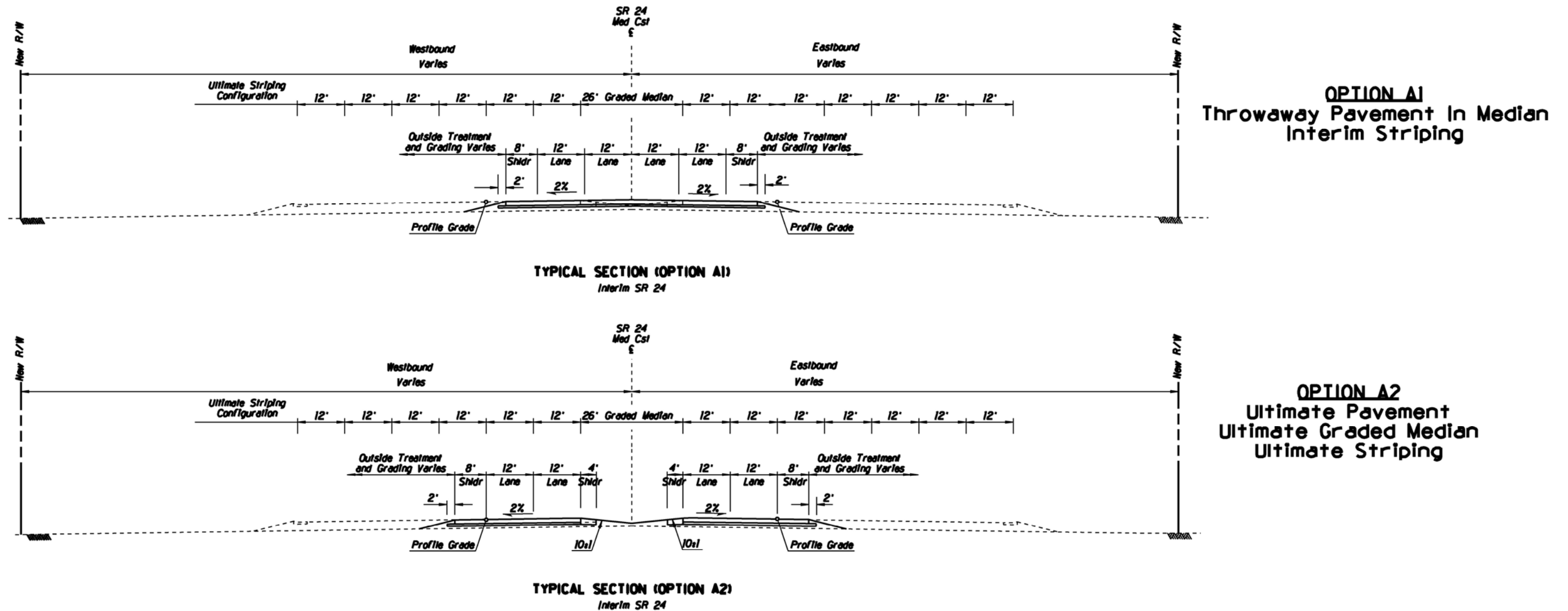
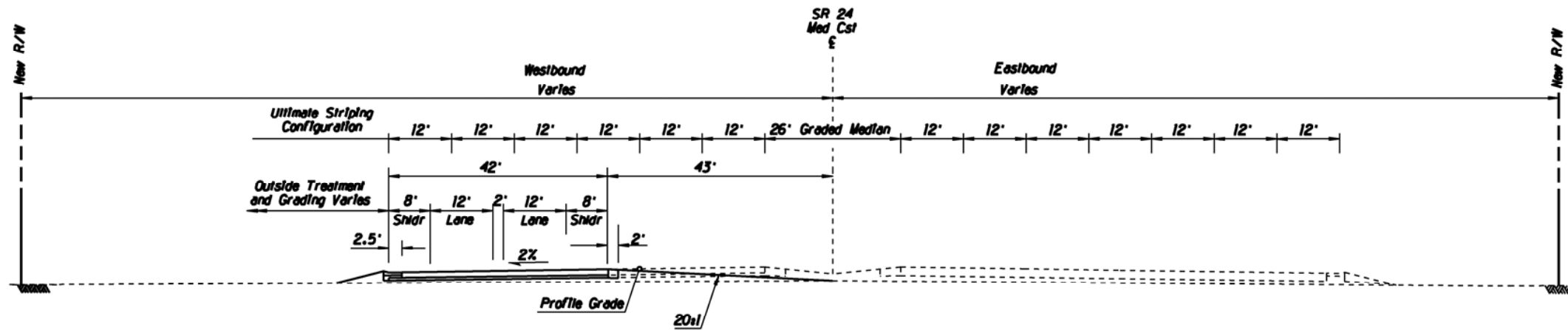
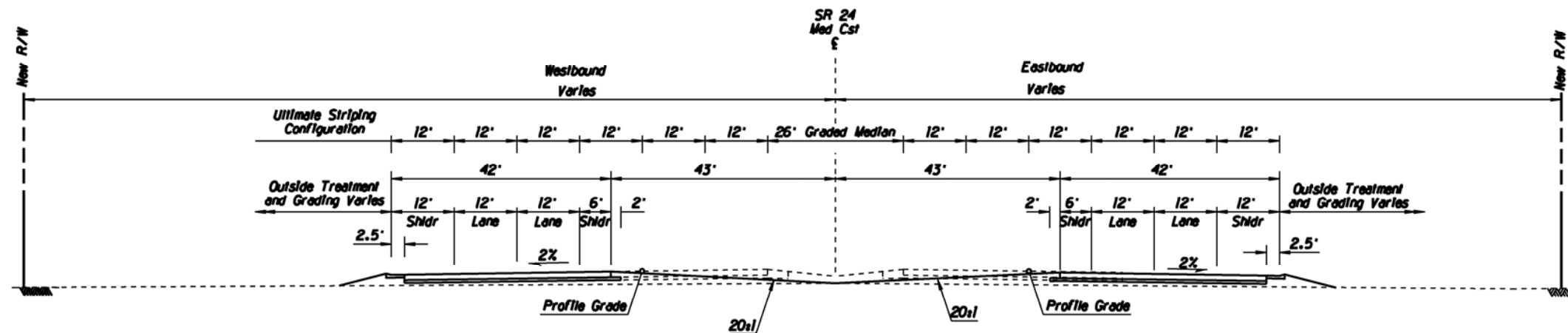


Figure 4 - Typical Sections Options B & C



TYPICAL SECTION (OPTION B)
Interim SR 24

OPTION B
Ultimate Pavement
Ultimate C&G
Interim Striping



TYPICAL SECTION (OPTION C)
Interim SR 24

OPTION C
Ultimate Pavement
Ultimate C&G in both directions
Ultimate Striping

3.3.4 Evaluation of Alternatives

Right-of-Way

Alternatives A1 and A2 would require the future interchange cross roads at Williams Field, Signal Butte and Meridian to be above grade to cross over the at Grade SR-24. This would require additional Right-of-Way at the interchanges because the ramps would tie into the cross roads approx 23ft above grade which would require additional grading footprints on the outside of the ultimate ramps and cross roads. Right-of-way outside of the interchange areas could be reduced from the ADOT DCR 2011 foot print since the outside grading slopes would be at or near grade.

Alternatives C would keep the approx same footprint as the ADOT DCR 2011 footprint at the interchanges as the crossroads would be at approx existing grade, however the ultimate grading footprint would be reduced in the areas between interchanges as the ultimate profile would be at-grade or slightly above grade, reducing the footprint of the ultimate grading.

Traffic Analysis

All alternatives would operate at a similar Level of Service. Each alternative has the same number of lanes. The difference between alternatives is the location of the lanes in relation to the ultimate buildout.

Compatibility with Ultimate

Alternative A1 would be the least compatible with the ultimate configuration. 40% of the roadway width would be throwaway because it is located within the ultimate open median area. Additionally, areas with superelevation would be completely incompatible because the Axis of Rotation in the Ultimate configuration is not located on the centerline of SR-24, which would be the required location of superelevation for the interim condition.

Alternative A2 and Alternative C would be completely compatible with the ultimate configuration. The location of the lane lines in both alternatives would both fall on future lane lines in the ultimate configuration. However, Alternative C allows for a simpler construction operation for the ultimate as all construction will happen in the median between EB and WB interim traffic lanes.

Development Impacts

Alternatives A1 and A2 require the interchange crossroads to be built above grade and over an at-grade SR-24 in the ultimate condition. This increases the amount of area needed for Right-of-Way to fit the footprint of the slopes and impacts how parcels can access the crossroad near the interchange area because of the elevated footprint.

Alternative C keeps the interchange crossroads near existing ground similar to the ADOT DCR 2011 preferred alternative and therefore keeping the same opportunity for future development in those areas.

Pump Station

All alternatives eliminate the need for a pump station based on modifying the profile of SR-24 to be at-grade or above grade.

Estimated Construction Cost

Alternatives A1 and A2 have similar interim construction costs, however in the ultimate configuration the A1 will cost more because of the amount of throw away in the future condition.

Alternative C would have a slightly higher interim construction costs than Alternatives A1 and A2 because it builds the most pavement. However, in the ultimate condition the structures at Williams Field, Signal Butte and Meridian would cost less than Alternatives A1 and A2 because the size of the required structures is reduced if the structures are on the mainline vs the structures being on the crossroads. Also the required box culverts crossing for the drainage channel would be shorter because the crossroads are at existing grade in alternative C and in Alternatives A1 and A2 the crossroads are above grade requiring the box culvert lengths to be longer due to the grading slope lengths.

3.3.5 Evaluation Matrix

The scoring for each evaluation criterion was based on a range from 1.0 to 5.0, with 1.0 representing the lowest and 5.0 representing the highest scores. The multi-discipline team reviewed each alternative based on the evaluation criteria. The resultant score of each criterion was determined by group discussion and overall consensus by the evaluation team. The composite alternative score is the sum of each individual evaluation criteria score. The final alternative scores are shown in the Table 3.

Table 3 - Alternative Screening Matrix

Evaluation Criteria	Alternative A1	Alternative A2	Alternative C
Right-of-Way	2	2	5
Traffic Analysis	4	4	4
Compatibility with Ultimate	2	5	5
Local Access	3	3	4
Pump Station	5	5	5
Estimated Construction Cost	5	5	4
Total Score:	21	24	27

3.3.6 Recommendation

Based on the alternatives evaluation and screening process results, the Project Team recommends the selection of the Alternative C as the Preferred Alternative for this study.

4.0 MAJOR DESIGN FEATURES OF THE PREFERRED ALTERNATIVE

4.1 INTRODUCTION

This section describes the design controls and design features for the Preferred Alternative for SR-24 and the service interchanges within the study limits. The interim facility controls will be the same as the ultimate facility controls. This will enable interim improvements to be compatible for ultimate design criteria.

4.2 DESIGN CRITERIA

SR-24 is classified as a controlled access Urban Principal – Freeway/Expressway. The interim facility will not operate as a Freeway/Expressway, however the criteria used for the interim design is the same as the ultimate facility design criteria. A summary of the design controls for Interim SR-24 is provided in Table 4.

Table 4 – Design Controls for Interim SR-24

Description of Criteria	Values for Design
Design Year:	2030
Design Speed:	65 mph
Superelevation:	0.06 ft/ft maximum
Cross Slope:	2.00%
Lane Width:	12 ft.
Shoulder Width:	
- Median:	6 FT.
- Outside:	12 ft.
Maximum Horizontal Curve:	3 degree, 27 minutes
Maximum Gradient:	3%
Taper rate:	65:1
Slope Standards:	
- Cut Slopes:	Varies, 3:1 maximum
- Fill slopes:	Varies, 3:1 maximum
Minimum Vertical Clearance:	
- Highway structure:	16.5 ft.
- Pedestrian overpass:	17.5 ft.

A summary of design controls for the service interchange ramps is provided in Table 5.

Table 5 – Design Controls for Service Interchange Ramps

Description of Criteria	Values for Design
Design Year:	2030
Design Speed:	
- Nose of gore (exit ramps):	60 mph
- Nose of gore (entrance ramp):	55mph
- Ramp body:	50 mph
- Ramp terminal:	35 mph
Superelevation:	0.06 ft/ft maximum
Cross Slope:	2.0%
Pavement Width:	
- Two lane exit ramp:	34 ft., plus 2 ft. offset to barrier
- Entrance ramp:	28 ft., plus 2 ft. offset to barrier
Lane Width:	12 ft.
Maximum Horizontal Curve:	6 degree, 53 minutes
Maximum Gradient:	+4%, -5%
Taper rate:	65:1
Slope Standards:	
- Cut Slopes:	Varies, 3:1 maximum
- Fill slopes:	Varies, 3:1 maximum
Minimum Vertical Clearance:	
- Highway structure:	16.5 ft.
- Pedestrian overpass:	17.5 ft.

The local arterial streets will be designed in accordance with the local jurisdiction functional classification requirements.

4.3 SR-24 INTERIM FREEWAY CONCEPT

Introduction

The Preferred Alternative was developed to provide an interim facility to extend SR-24 between Ellsworth Road and Ironwood Drive to provide additional regional connectivity while providing the capacity needed for the projected 2025 traffic demand. This preferred alternative was also developed with consideration to the ultimate SR-24 concept as described in the ADOT DCR 2011. The horizontal geometry developed in the ADOT DCR 2011 for SR-24 and associated ramps and roadways within project limits was not reevaluated as part of the scope of this DCR. However, the vertical geometry that was developed in the ADOT DCR 2011 for SR-24 and associated ramps and roadways within the project limits was part of the reevaluation process. The Preferred Interim Alternative plans are included in Appendix C.

The locations of the bridge structures, retaining walls, noise walls, drainage basins and other improvements included in this project account for the ultimate SR-24 facilities.

In coordination with the City of Mesa, the interim concept will accommodate a City of Mesa trail within the proposed Right-of-Way that the city may open prior to the ultimate construction of SR-24.

SR-24 Interim Eastbound Mainline

In the interim condition there will be two general-purpose lanes in the eastbound direction of travel on SR-24 between Ellsworth Road and Ironwood Drive. Between the interchanges the lanes would be located on same horizontal alignment as the two outside lines as shown in the ADOT DCR 2011. At the interchanges, the lanes would follow the entrance and exit ramps alignments in the interim condition. All ramps will be designed to accommodate a minimum of two lanes of traffic. This will require approximately 6ft of additional pavement width for a portion of the exit ramps that were designed as one lane exits in the ADOT DCR 2011. Mainline pavement would be constructed between the back of gore of the entrance ramps and exit ramps of successive interchanges.

The west half of the Ellsworth Road TI has been constructed as part of Phase 1 of the DCR. Currently there is an end of Freeway condition at the Eastbound exit ramp at Ellsworth Road. The interim SR-24 project would construct the Eastbound two lane entrance ramp per the ADOT DCR 2011 horizontal layout.

The Williams Field Road exit ramp (2 lanes) will be designed per the ADOT DCR 2011 horizontal layout. The Williams Field Road entrance ramp (2 lanes) will be designed per the ADOT DCR 2011 horizontal layout.

The Signal Butte Road exit ramp will be designed per the ADOT DCR 2011 horizontal layout, but will be wider to accommodate the 2 lanes instead of 1 lane as depicted in the ADOT DCR 2011. The Signal Butte Road entrance ramp (2 lanes) will be designed per the ADOT DCR 2011 horizontal layout.

The Meridian Road exit ramp will be designed per the ADOT DCR 2011 horizontal layout, but will be wider to accommodate the 2 lanes instead of 1 lane as depicted in the ADOT DCR 2011. The Meridian Road entrance ramp (2 lanes) will be designed per the ADOT DCR 2011 horizontal layout.

The Ironwood Drive exit ramp will be designed per the ADOT DCR 2011 horizontal layout, and was already designed to accommodate 2 lanes of traffic for an end of freeway condition.

SR-24 will be an at-grade or elevated freeway between Ellsworth Road and Ironwood Drive.

Ultimately new overpasses will be provided at Ellsworth Road, Williams Field Road, Signal Butte Road, Meridian Road and Ironwood Drive. In the interim condition none of the overpasses will be constructed as all mainline traffic will be on the ramps. New freeway underpasses will be provided at Crismon Road and Mountain Road. Currently Crismon Road does not exist across the alignment of SR-24, it is recommended that Crismon Road is built with the ultimate construction of SR-24.

SR-24 Interim Westbound Mainline

In the interim condition there will be two general-purpose lanes in the westbound direction of travel on SR-24 between Ironwood Drive and Ellsworth Road. Between the interchanges the lanes would be located on same horizontal alignment as the two outside lines as shown in the ADOT DCR 2011. At the interchanges, the lanes would follow the entrance and exit ramps alignments in the interim condition. All ramps will be designed to accommodate a minimum of two lanes of traffic. This will require approximately 6ft of additional pavement width for a portion of the exit ramps that were designed as one lane exits in the ADOT DCR 2011. Mainline pavement would be constructed between the back of gore of the entrance ramps and exit ramps of successive interchanges. The Ironwood Drive entrance ramp (2 lanes) will be designed per the ADOT DCR 2011 horizontal layout.

The Meridian Road exit ramp will be designed per the ADOT DCR 2011 horizontal layout, but will be wider to accommodate the 2 lanes instead of 1 lane as depicted in the ADOT DCR 2011. The Meridian Road entrance ramp (2 lanes) will be designed per the ADOT DCR 2011 horizontal layout.

The Signal Butte Road exit ramp will be designed per the ADOT DCR 2011 horizontal layout, but will be wider to accommodate the 2 lanes instead of 1 lane as depicted in the ADOT DCR 2011. The Signal Butte Road entrance ramp (2 lanes) will be designed per the ADOT DCR 2011 horizontal layout.

The Williams Field Road exit ramp will be designed per the ADOT DCR 2011 horizontal layout, but will be wider to accommodate the 2 lanes instead of 1 lane as depicted in the ADOT DCR 2011. The Williams Field Road entrance ramp (2 lanes) will be designed per the ADOT DCR 2011 horizontal layout.

The Ellsworth Road exit ramp will be designed per the ADOT DCR 2011 horizontal layout, but will be wider to accommodate the 2 lanes instead of 1 lane as depicted in the ADOT DCR 2011. Need to Determine if Traffic Dictates the need to have a grade separation at Ellsworth for the interim condition.

4.4 SERVICE TRAFFIC INTERCHANGES AND GRADE SEPARATIONS

4.4.1 Introduction

As with the ADOT DCR 2011, new traffic interchanges will be provided on SR-24 to facilitate access to the existing and planned roads at Ellsworth Road, Williams Field Road, Signal Butte Road, Meridian Road and Ironwood Drive. However, for the Interim Concept only a portion of the interchanges are built. The full grade separations will not be constructed in the interim condition, see Figure 5 on page 4-3. The SR-24 profile has been revised to allow the interim condition to be built at or near existing grade, see Figure 6 on page 4-4. This profile adjustment also eliminates the need for a drainage pump station as the profile is no longer depressed.

Figure 5 – Interim Construction at Interchange

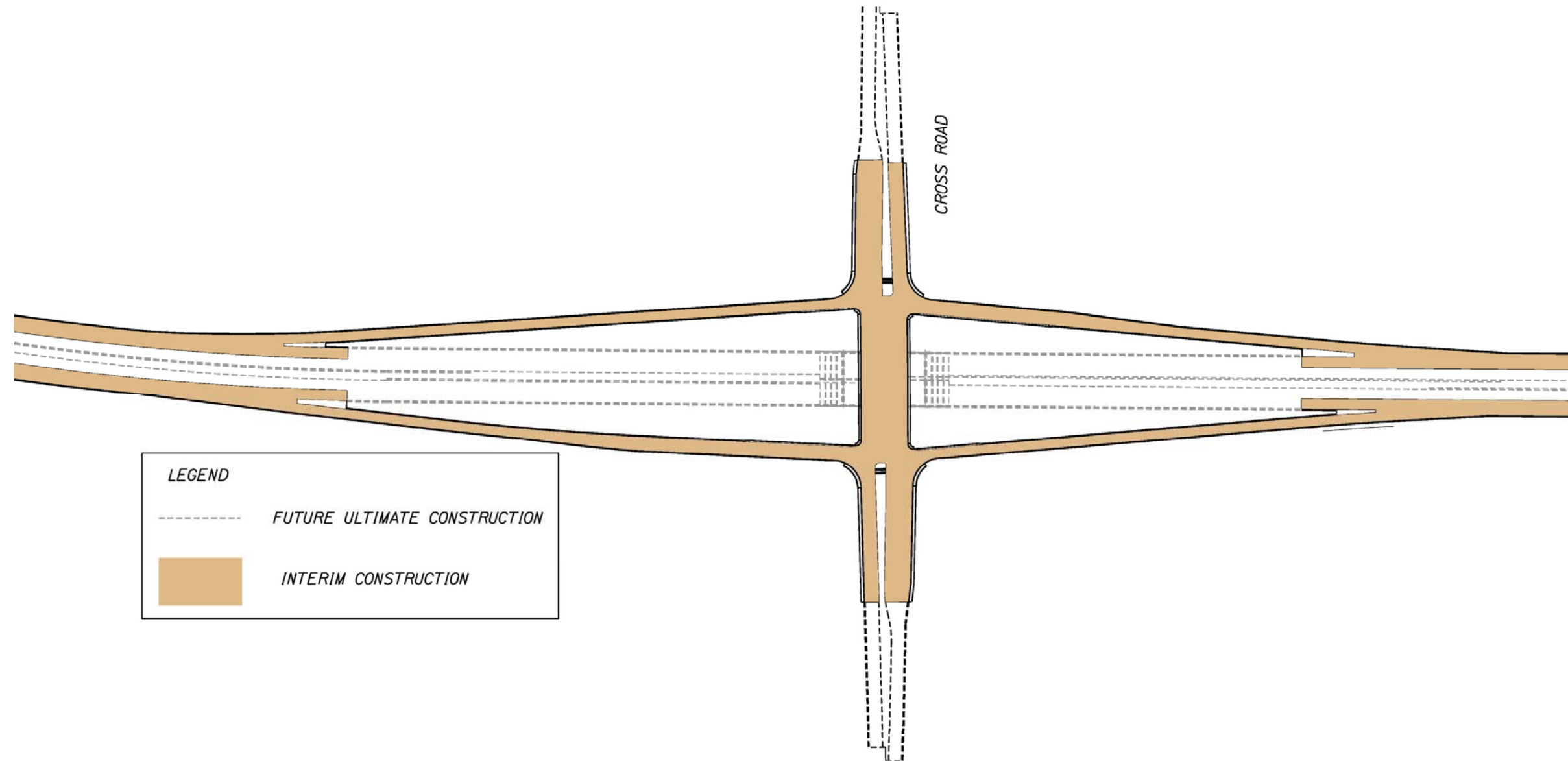
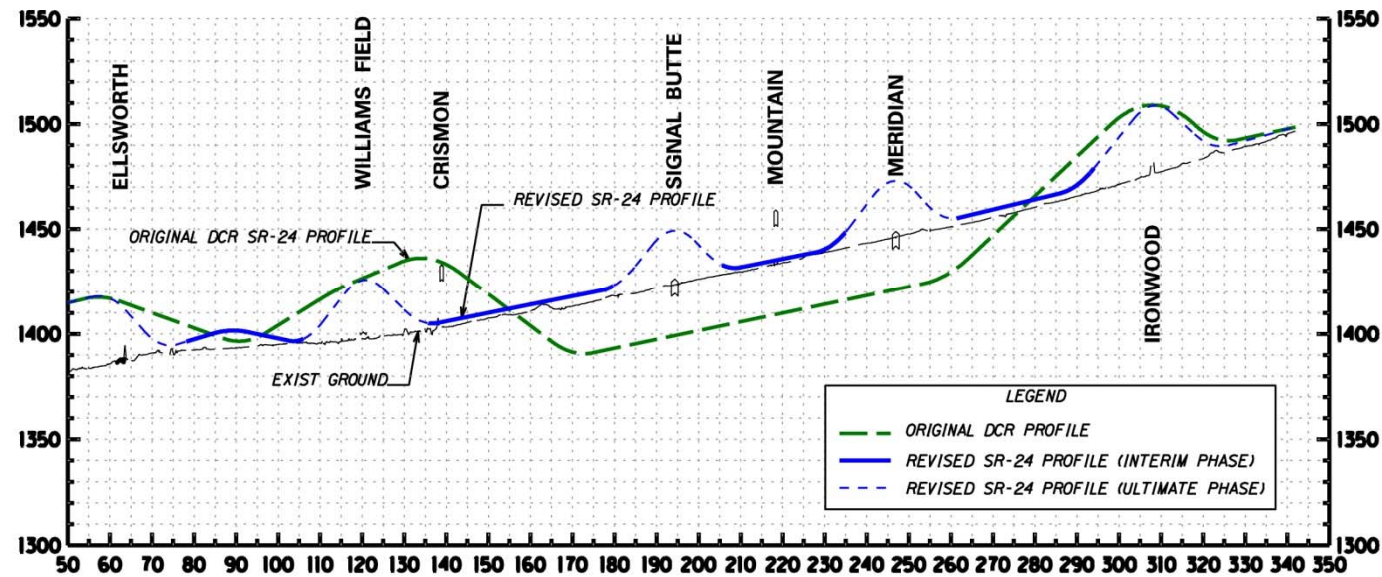


Figure 6 - Revised SR-24 Profile



4.4.2 Ellsworth Road Interim TI

See the ADOT DCR 2011 for a discussion on the ultimate Ellsworth Road Full Diamond TI. Phase I of the DCR construction was completed in May of 2014. Ellsworth Road was constructed as a 5 lane arterial street, with three through lanes in the southbound direction and two through lanes in the northbound direction. Ellsworth is planned as a six lane arterial street. Ellsworth Road was constructed and striped with 2 left turn lanes for the northbound to westbound left-turn movement. Ellsworth Road was constructed to accommodate 2 left turn lanes for the southbound to eastbound left turn movement; however it was striped out for future restripe when the eastbound entrance ramp is constructed. For the interim condition, NB Ellsworth Road will be widened to add additional pavement for the future third through lane northbound. The southbound to eastbound dual left-turn lanes will be striped and the eastbound entrance and westbound exit ramps will be per the ADOT DCR 2011 design. The existing eastbound exit ramp will be restriped to accommodate the through movement for the eastbound SR-24 traffic.

Mainline Structures at Ellsworth will not be part of the interim project. The traffic operational analysis indicates the intersections will operate at adequate capacity for the interim Design Year 2025

Existing Catch basins and storm drains impacted along NB Ellsworth Road will be extended to accommodate the widened pavement. The existing box culvert that was constructed as part of Phase 1 in 2014 will be extended for the NB Ellsworth widening and headwalls will be added.

Existing and Planned utilities may be impacted.

4.4.3 Williams Field Road Full Diamond TI

See the ADOT DCR 2011 for a discussion on the ultimate Williams Field Road Full Diamond TI. For the interim condition the grade separation will not be constructed. In the interim condition it is assumed that Williams Field Road could be open during the interim condition.

4.4.4 Crismon Road Grade Separation

A grade separation was developed for Crismon Road in the ADOT DCR 2011 and the Horizontal alignment has not changed from the ADOT DCR 2011. However, the ultimate section for Crismon Road was updated to reflect the Mesa 2040 Transportation Plan, which has Crismon Road as a four lane arterial road instead of a six lane arterial road as described in the ADOT DCR 2011. With this interim design the DCR vertical alignment was reevaluated to help better provide a cost effective solution for the interim design SR-24. At Crismon Road the SR-24 profile was lowered to be near existing grade and Crismon Road has been designed to be above grade to cross over SR-24 with a structure. By having the Crismon Road vertical alignment go over SR-24 it greatly reduces the amount of embankment that is needed for SR-24. Since, Crismon Road does not currently exist within the project limits, it is recommended to not construct Crismon Road as part of the interim SR-24 project. The portion of Crismon Road within the ADOT Right of Way will be included as part of the ultimate SR-24 project.

4.4.5 Signal Butte Road Full Diamond TI

See the ADOT DCR 2011 for a discussion on the ultimate Signal Butte Road Full Diamond TI. In the interim condition the configuration of Signal Butte will remain the same as described in the ADOT DCR 2011. However, the ultimate vertical alignment for SR-24 has been adjusted to be above grade at Signal Butte Road with an overpass structure instead of SR-24 being depressed with an underpass structure at Signal Butte Road. All SR-24 traffic will use the entrance and exit ramps through the intersection with Signal Butte Road in the interim condition, the overpass structure will not be built in the interim condition.

If funding for the interim condition will not allow SR-24 to be built the full length of the project from Ellsworth Road to Ironwood Drive, then Signal Butte Road has been determined, in discussions with FHWA, ADOT and the City of Mesa, as the location for the logical terminus of SR-24. Ironwood Drive is the only improved road, east of Ellsworth Road, which currently provides regional connectivity to communities to the south of the project, in particular the Town of Queen Creek. The roadway network would need to provide connectivity that allows traffic on Ironwood Drive, south of the SR-24 Corridor, to be able to connect to Signal Butte Road. Once funding is determined for the SR-24 interim phase 2 then coordination between FHWA, ADOT, MAG, City of Mesa, Pinal County and Town of Queen Creek will need to occur to improve the roadway network to allow Signal Butte to be the logical terminus. If Signal Butte Road is the terminus the City of Mesa will need to include improvements in the STIP to the north and south of SR 24 to ensure Signal Butte can accommodate an end of roadway condition.

4.4.6 Mountain Road Grade Separation

A grade separation crossing has been developed for Mountain Road as depicted in Appendix C. The profile of the crossing has changed from the ADOT DCR 2011. The ultimate vertical alignment for SR-24 has been adjusted to be at existing grade at the Mountain Road crossing; In the ADOT DCR 2011 the SR-24 vertical alignment was below grade with a depressed section. With the change to the vertical alignment of

SR-24, the Mountain Road profile was adjusted to be above grade with an underpass structure. The horizontal alignment and layout of Mountain Road was not changed. By raising the grade of Mountain Road the connection to the existing roadway, at existing grade, will require additional Right-of-way impacts to the north and south of SR-24 to allow for the side slopes. Fuji Films has a developed parcel on the south west quadrant of Mountain Road and SR-24 which will be impacted by raising the grade of Mountain Road. The northern most driveway will be eliminated due to the grade difference between the existing driveway and the proposed Mountain Road grade, approx 10ft above existing. There are two additional existing driveways that provide access into the Fuji Property to the south that will not be impacted. A retaining wall will be required to maintain Fuji Films on site retention basins along the frontage of their property with Mountain Road.

4.4.7 Meridian Road Full Diamond TI

See the ADOT DCR 2011 for a discussion on the ultimate Meridian Road Full Diamond TI. For the interim condition the configuration of Meridian Road will remain the same as described in the ADOT DCR 2011. However, the ultimate vertical alignment for SR-24 has been adjusted to be above grade at Meridian Road with an overpass structure instead of SR-24 being depressed with an underpass structure at Meridian Road. All SR-24 traffic will use the entrance and exit ramps through the intersection with Meridian Road in the interim condition, the overpass structure will not be built in the interim condition. The ADOT DCR 2011 also determined Meridian Road TI would be the End of Freeway for Phase 2 of the implementation plan, however Meridian Road is not currently an improved road between Ray Road and Ocotillo Road. In discussions with ADOT, FHWA and City of Mesa Staff it was determined that Meridian Road TI would not support an end of freeway condition without improving Meridian Road between Ray Road and Ocotillo Rd. Based on the current development priorities of the City of Mesa, the city would not support improving Meridian Road for the interim end of freeway condition.

In the interim condition it is assumed that Meridian Road will not be in operation and all SR-24 traffic will continue through the future ramp intersections.

4.4.8 Ironwood Drive Full Diamond TI

See the ADOT DCR 2011 for a discussion on the ultimate Ironwood Drive Full Diamond TI. The Ironwood Drive Interim TI would have no changes to the end of freeway condition as depicted in the ADOT DCR 2011 appendix C.

4.5 ACCESS CONTROL

Access Control will be acquired for SR-24 in accordance with ADOT and FHWA Access Control Policy Requirements. Currently, the plans in appendix C have shown full access control and and Right-In Right-Out access control limits.

Since the ADOT 2011 DCR, ADOT has changed their access control policies in 2014, however additional development planning has occurred based on the previous policies which will require variances. Variances

to ADOT's access control policy are expected at the North East quadrant of the future Ellsworth Interchange and the South East quadrant of the future Meridian Interchange, based on discussions with ADOT Right-of-Way group.

4.6 RIGHT-OF-WAY

The proposed right-of-way requirements are shown on the Preferred Alternative Concept Plans in Appendix C. The right-of-way shown in the interim plans has been designed to accommodate the ultimate configuration. The footprint of SR-24 has been reduced by adjusting the profile grade to be at-grade grade between the interchanges. The total estimated right-of-way acquisition required for this alternative is 294 acres, with a total anticipated cost of \$56 million. Compared to the ADOT 2011 DCR, the right-of-way acquisition required has been reduced by approx 90 acres.

Temporary Construction Easements (TCE's) may be required for the construction of the Preferred Alternative. The TCE locations and limits will be determined during final design.

4.7 DRAINAGE

4.7.1 On-Site Drainage Systems

SR-24 is discussed in this section as an interim project between Ellsworth Road and Ironwood Drive, but provisions are made for the ultimate configurations and runoff flows. The pavement will be normal crowned at most locations to allow for continued drainage to the outside shoulder and to roadside ditches. The proposed interim two lanes of traffic would be located at the outside limit of the ultimate section. In super-elevated sections, catch basins would be placed along the median barrier rail to collect runoff.

On-Site Existing Conditions

The existing drainage improvements on the corridor are related to Segment I of the project finalized in May 2014 between SR 202L and Ellsworth Road, and the improved Ellsworth Road and Ironwood Drive. At Mountain Road the on-site drainage is limited to roadside ditches.

Currently, on-site freeway drainage is collected in catch basins and conveyed through lateral pipes into existing off-site drainage systems. Runoff is also collected by catch basin inlets within the limits of the Ellsworth Road improvements. Ironwood Drive is a median-separated facility and runoff sheet flows off the edge of the pavement to the outside ditches; median flows are intercepted at the culverts crossing the road.

The existing on-site drainage system would see minor modifications including:

- Several cross pipes that currently discharge into the Ellsworth Basin across the future SR-24 channel would be cut short and discharge into the SR-24 channel once that is built.
- Should the need for a grade-separated crossing at Ellsworth Road be justified by the traffic analysis, the footprint of the temporary basin between the existing on- and off-ramps at Ellsworth Road would be reduced to construct the mainline embankment.
- At Mountain Road a grade-separated crossing is proposed. Mountain Road would cross above SR-24 through a bridge and the roadway section would be improved. Existing roadway side ditches north of the project would be intercepted by the SR-24 channel.
- Ironwood Drive would be improved within the access control limits. Curb and gutter and catch basins would direct and intercept the on-site runoff on each side of the road. Storm drain pipes would convey the flow to the SR-24 channel or the RCBC crossing Ironwood Drive.

In areas of super-elevation, catch basins along the concrete median half barrier are provided to intercept and remove drainage flows from the roadway.

Proposed On-Site Drainage Features

Due to the mix of developed (developing) urban, suburban and undeveloped landscape within the project area, the recommended alternative for pavement drainage is sheet flow over the edge of pavement to adjacent roadway ditches. Concrete half barrier or curb and gutter are recommended adjacent to the outside shoulder of the roadway for superelevated or grade-elevated roadway segments (approaches to grade-separated crossings).

The pavement will have a 2% cross grade draining to the outside for a majority of the project, except for the superelevated sections.

The proposed drainage system would include installation of shallow linear detention basins for water quality treatment, roadside ditches, catch basins and storm drain pipes. Such features are only loosely indicated on the plans and calculations were not done at this design stage; this work is deferred to a later design phase.

ADOT C-15.91 catch basins would be installed along curb and gutter sections to collect the pavement runoff. Similarly, ADOT C-15.92 catch basins would be installed in locations with concrete half barrier. Additional catch basins (flanking inlets) would be added at sag curves and superelevation transitions to reduce bypass flows. Flanking inlets could be supplemented by slotted drains.

Runoff collected in the catch basins will be conveyed to cut ditches or storm drains. New storm drain would be installed to convey flows to a discharge point, or a connection between the new catch basins and existing storm drain laterals is made, where possible.

The on- and off- ramps would not include catch basins unless curb and gutter is required.

The areas between on- and off- ramps at Ellsworth Road, Williams Field Road, Signal Butte Road, Meridian Road and Ironwood Drive would be used for water quality retention basins. These areas would be regraded to a more traditional infield configuration when the ultimate project is constructed.

Several existing pipes would be shortened to discharge into the SR-24 channel (between Powerline Floodway and Ellsworth Road). The remaining pipes not being used would be abandoned in place, capped and filled with sand/cement slurry.

In addition to the general approach described above, see Draft Initial Drainage Report for future on-site drainage features by segment.

Final Design Issues

Several issues will need to be considered with the final design of the drainage features. They include runoff spread, interception and conveyance of pavement runoff generated throughout the interim project, which was not evaluated. See Draft Initial Drainage Report for additional details.

4.7.2 Off-Site Drainage Systems

This section is intended as an update to the analysis performed by ADOT for the project area as part of the SR-24 Gateway Freeway FDCR and extensive references will be made to the FDCR report and its accompanying Initial Drainage Report. The update relies heavily on the extensive regional evaluation done by FCDMC for the East Mesa ADMPU using hydrologic models modified for the purpose of the SR-24 interim project.

Existing Conditions

Several existing or proposed regional drainage facilities in the project area will have an influence upon or be affected by the project. They are:

- Powerline Flood Retarding Structure (FRS) and Vineyard FRS in Pinal County, designed to provide flood protection to Central Arizona Project (CAP) Canal and to downstream areas in Pinal County and Maricopa County;
- Powerline Floodway, a concrete-lined channel that extends from the Powerline FRS to the East Maricopa Floodway; it is primarily designed to drain the FRS structures;
- Ellsworth Channel, which runs along the east and west sides of Ellsworth Road between Pecos Road and the Powerline Floodway;
- Former General Motors Proving Grounds perimeter channel, which will be improved by developers;
- East Maricopa Floodway, which serves as a regional outfall for eastern Maricopa County;
- Pecos Road Channel is one of the proposed drainage improvements in the East Mesa ADMPU, it is intended to run along Pecos Road and to discharge into Ellsworth Channel.

The SR 202L Santan drainage channel is not affected by this project.

Pertinent pre- and post-project hydrology was developed by ADOT for the SR-24 Gateway Freeway FDCR Initial Drainage Report. The most current hydrologic analysis in the project watershed was performed by FCDMC in the East Mesa ADMPU. The latter study updated the existing condition regional hydrology to reflect major infrastructure improvements in the area. See Draft Initial Drainage Report for additional details.

Proposed Options

The interim SR-24 project could be constructed in the next 3- to 10 years. The proposed off-site drainage system would be based on the default conceptual drainage design provided with the SR-24 Gateway Freeway DCR, but sized for a revised hydrology that accounts for development likely to occur in the watershed within this timeframe. This concept shows an off-site channel on the north side of SR-24 that is sized for the larger existing (pre-project) condition design flows. The SR-24 channel outfalls into the Powerline Floodway, which would be widened to the confluence with Ellsworth Channel. A detention/retention basin at Ellsworth Road (Ellsworth Basin) would regulate the SR-24 channel peak flow before the outfall into Powerline Floodway. This concept represents the baseline approach to off-site drainage design.

The interim SR-24 project would contribute additional flows to the existing off-site runoff due to the new pavement surface. Although on-site runoff will increase, the proposed off-site collection infrastructure would not be affected as the on-site and off-site peak flows are far apart. The peak flows approaching the SR-24 alignment would only be affected by the development in the upstream watershed.

With the projected reduction in flows as development occurs in the watershed, the off-site drainage would need to be reassessed for opportunities of peak flow and runoff volume reduction. For that purpose, three possible options for the proposed off-site drainage infrastructure were presented to the stakeholders, and examined. These options were in addition to the baseline design, and were all inspired by alternatives presented and discussed in East Mesa ADMPU, and in the City of Mesa SDMP: See Draft Initial Drainage Report for additional details.

The three options were discussed with ADOT, MAG, State Land Department, Pinal County, City of Mesa and FCDMC. All options were eventually eliminated from consideration in relation to the Interim SR-24 project because they would require facilities located outside of the current environmentally-cleared footprint.

Therefore, the baseline SR-24 off-site drainage configuration, amended with the relocation of Ellsworth Channel at the Airport, was selected to be applied for further hydrologic analysis and conceptual hydraulic design.

Proposed Conceptual Design

The channel design was optimized to maintain hydraulic conditions within the design parameters described above. In addition, several factors specific to the project were considered regarding existing basin at Ellsworth Road, the inflow from adjacent developments, sediment basins, widening of Powerline Floodway, existing and proposed cross culverts. See Draft Initial Drainage Report for additional details.

4.8 STRUCTURES

4.8.1 New Bridge Structures

See section 4.8.1 ADOT 2011 DCR

With the adjustment to the SR-24 profile to be above the cross roads at the interchanges, it changes structures at Signal Butte and Meridian Road. These will be future overpasses instead of underpasses.

Crismon Road will now become a future Underpass.

Mountain Road will remain an underpass but will be above grade over the at-grade SR-24. Details of these bridges are shown in table 6 below.

Table 6 – New Bridge Structure Concepts

Bridge Description	Bridge Length	Number of Spans	C _L -C _L Span Lengths	Deck Width	Max Superstructure Depth
Crismon Road Underpass (Future)	316'	2	155', 155'	107.33'	7.5'
Signal Butte Road TI Overpass (SR 24 WB) (Future)	227'	2	111', 111'	74.5'	8.5'*
Signal Butte Road TI Overpass (SR 24 EB) (Future)	227'	2	111', 111'	74.5'	8.5'*
Mountain Road Underpass	309'	2	151', 152'	81.33'	6.5'
Meridian Road TI Overpass (SR 24 WB) (Future)	227'	2	111', 111'	74.5'	8.5'*
Meridian Road TI Overpass (SR 24 EB) (Future)	227'	2	111', 111'	74.5'	8.5'*

4.8.2 Widening of Existing Bridge Structures

No Updates see section 4.8.3 ADOT 2011 DCR

4.8.3 Retaining Walls

No Updates see section 4.8.3 ADOT 2011 DCR

4.8.4 Noise Walls

Updates for the current study are in process. Depending on the outcome ADOT would prepare a Hot Spot or noise wall analysis if needed.

4.9 UTILITIES

See Section 4.9 ADOT 2011 DCR. The only update is the Ultimate pump station has been eliminated with the SR-24 vertical alignment changes. No electric or gas service will be required.

4.10 EARTHWORK

Approximately 282,000 cubic yards of excavation and 112,000 cubic yards of borrow are anticipated to be needed for the interim phase 2 project.

4.11 GEOTECHNICAL AND PAVEMENT DESIGN

4.11.1 Subsurface Conditions

No updates see section 4.11.1 ADOT 2011 DCR

4.11.2 Pavement Structural Sections

The pavement structural sections for the SR-24 mainline and the SR-24 service interchange ramps, have been reevaluated based on updated traffic volumes. A memo has been provided as Appendix F. The recommended pavement structural sections have been provided in Table 7.

Table 7 – Pavement Structural Sections for SR-24

Item	AB-2 (in)	Plain PCCP (in)	AR-ACFC ¹ (in)	Total Thickness (in)
Mainline SR 24	4	11.0	1	16
Service Interchange Ramps	4	10.0	1	15
Ramp Gore Areas	4	11.0	1	16

1. It is assumed that the AR-ACFC will not be placed with the interim project and will be placed with the Ultimate.

4.11.3 Landscaping

It is recommended that landscaping should not be part of the interim SR-24 and be designed and constructed with the Ultimate build out. The slopes should be seeded to protect from erosion.

The area north of the drainage channel within the proposed right-of-way that accommodates a future City of Mesa trail will be seeded with the interim project.

4.12 FREEWAY SIGNING AND PAVEMENT MARKING

A signing concept plan was developed to ensure an effective signing plan could be developed for the Preferred Interim Alternative. The concept signing plan is provided in Appendix C.

The final sign locations will be determined during the development of the final design plans and will consider existing and new locations of utilities, bridge structures, retaining and noise walls, drainage features, lighting standards, FMS components, and other appurtenances.

A pavement marking concept was also developed to incorporate the existing and new lane configurations, service interchange ramps, and local arterial streets and is included with the concept signing plan. The pavement marking design would be developed in accordance with applicable provisions of the current version of the ADOT Signing and Marking Standard Drawings that reference the requirements for lane lines, edge lines and intersection pavement markings.

4.13 LIGHTING AND TRAFFIC SIGNALS

Interim lighting and traffic signal plans are included in Appendix C. See ADOT 2011 DCR for additional information.

4.14 CONSTRUCTION PHASING AND TRAFFIC CONTROL

Traffic will be managed through detailed traffic control plans and by procedures and guidelines specified in Part VI of the Manual of Uniform Traffic Control Devices (MUTCD), 2009 Version, and by the Arizona Supplement to Part VI of the MUTCD. The final construction phasing and traffic control plans will be developed during final design.

Ellsworth Road, Mountain Road and Ironwood Drive are the only existing roadways that exist or remain in place through the interim SR-24 corridor, which will require the majority of the traffic control through the interim corridor.

Coordination will be required with the City of Mesa to determine the project phasing restrictions that will be used for this project. These restrictions could include limits to crossroad lane reductions due to City of Mesa concerns about arterial street capacity, freeway access, and emergency vehicle access.

It is expected that Mountain Road will require a detour to complete construction of the above grade roadway over SR-24.

Access to existing properties will be maintained at all times. The final construction phasing and traffic control plans will be prepared during final design.

An Emergency Management Plan in coordination with maintenance of traffic will be required during construction to inform emergency vehicles and personnel to access the construction area during an emergency. This Emergency Management Plan will be prepared as part of the final design.

4.15 FREEWAY MANAGEMENT SYSTEMS AND MULTIMODAL PLANNING DATA COLLECTION

4.15.1 FMS Communications and Trunk Line

See Section 4.15.1 ADOT 2011 DCR. Phase 1 of the DCR was completed in 2014. The FMS Trunkline was not installed as part of the SR-24 between Ray Road and Ellsworth Road. It is expected as part of this Interim Phase 2 project that the conduit for the FMS trunk line would be part of the interim project and would be installed. The City of Mesa would install fiber for traffic signal communication.

4.15.2 FMS Devices

See Section 4.15.2 ADOT 2011 DCR. FMS Devices are not expected to be installed as part of the interim project.

4.15.3 MPD Devices

See Section 4.15.3 ADOT 2011 DCR. MPD Devices are not expected to be installed as part of the interim project.

4.16 PHOENIX-MESA GATEWAY AIRPORT COORDINATION

No updates see Section 4.16 ADOT 2011 DCR.

4.17 PEDESTRIAN FEATURES

If existing pedestrian features within the interim SR-24 project limits do not meet either Americans with Disabilities Act Accessibility Guidelines (ADAAG) or Public Rights-of-Way Accessibility Guidelines (PROWAG), they will be required to be upgraded. All new pedestrian features designed with the interim SR-24 project will be required to meet PROWAG.

5.0 ITEMIZED ESTIMATE OF PROBABLE COSTS

The order of magnitude of project cost for the Preferred Alternative is \$136,512,142. which includes \$4,592,734 for design, \$55,641,000 for right-of-way, and \$76,278,408 for construction. The total project estimate includes approximately \$112,431,314 for the segment of SR-24 within Maricopa County and \$24,080,828 for the segment within Pinal County.

The SR-24 Ultimate (Ellsworth to Meridian) freeway project has been moved to Phase V of the program which is unfunded. MAG is currently working on a re-balancing of the over-all RTP program. The re-balancing will result in Project Programming changes, bringing projects back into the program. The results of the re-balancing effort will appear in the (FY2018-2022) Tentative 5-Year Construction Program which will be released for public review and comment in spring 2017. Additional funding would need to be provided by Pinal County (or other sources) for the segment of SR-24 from Meridian Road to Ironwood Road, since that segment of the freeway is located outside of Maricopa County and is not eligible for RTP funds.

ITEM DESCRIPTION	UNIT	QUANTITY	UNIT PRICE	EXTENDED AMOUNT
REMOVAL OF CONCRETE CURB AND GUTTER	L.FT.	1,900	\$ 6.00	\$ 11,400.00
REMOVAL OF SIGNS	L.SUM	1	\$ 4,000.00	\$ 4,000.00
ROADWAY EXCAVATION	CU.YD.	25,795	\$ 6.00	\$ 154,770.00
CHANNEL EXCAVATION SR-24	CU.YD.	298,514	\$ 3.00	\$ 895,542.00
BORROW	CU.YD.	54,985	\$ 15.00	\$ 824,775.00
AGGREGATE BASE CLASS 2	CU.YD.	42,000	\$ 45.00	\$ 1,890,000.00
AGGREGATE SUBBASE, CLASS 6	CU.YD.	8,700	\$ 18.00	\$ 156,600.00
PORTLAND CEMENT CONCRETE PAVEMENT (10")	SQ.YD.	141,288	\$ 32.00	\$ 4,521,216.00
PORTLAND CEMENT CONCRETE PAVEMENT (11")	SQ.YD.	126,263	\$ 35.00	\$ 4,419,205.00
ASPHALTIC CONCRETE (7" AC OVER 10" AB)	SQ.YD.	12,857	\$ 30.00	\$ 385,710.00
PIPE, CORRUGATED METAL, SLOTTED, 18"	L.FT.	724	\$ 110.00	\$ 79,640.00
STORM DRAIN PIPE, 24"	L.FT.	25,621	\$ 60.00	\$ 1,537,260.00
STORM DRAIN PIPE, 30"	L.FT.	1,756	\$ 80.00	\$ 140,480.00
STORM DRAIN PIPE, 36"	L.FT.	665	\$ 100.00	\$ 66,500.00
RCP CULVERT (3-36") (ELLSWORTH BASIN)	L.SUM	1	\$ 30,000.00	\$ 30,000.00
CONCRETE CATCH BASIN (C-15.80)(H=8' OR LESS)	EACH	37	\$ 2,800.00	\$ 103,600.00
CONCRETE CATCH BASIN (C-15.91)(H=8' OR LESS)	EACH	142	\$ 3,200.00	\$ 454,400.00
CONCRETE CATCH BASIN (C-15.92)(H=8' OR LESS)	EACH	16	\$ 3,500.00	\$ 56,000.00
MANHOLE (C-18.10)(NO.3)(FOR PIPES 6" TO 36")	EACH	47	\$ 3,500.00	\$ 164,500.00
FOUNDATION FOR SIGN POST (CONCRETE)	EACH	82	\$ 180.00	\$ 14,760.00
BRIDGE SIGN STRUCTURE (TAPERED TUBE,SINGLE BEAM)	EACH	8	\$ 16,000.00	\$ 128,000.00
FOUNDATION FOR BRIDGE SIGN STRUCTURE (TAPERED TUBE)	EACH	16	\$ 7,000.00	\$ 112,000.00
CANTILEVER SIGN STRUCTURE (SD9.10, TYPE 3C)	EACH	7	\$ 40,000.00	\$ 280,000.00
CANTILEVER SIGN STRUCTURE (SD9.10, TYPE 4C)	EACH	8	\$ 41,000.00	\$ 328,000.00
FOUNDATION FOR CANTILEVER SIGN STRUCTURE (SD9.10, TYPE 3C)	EACH	7	\$ 7,500.00	\$ 52,500.00
FOUNDATION FOR CANTILEVER SIGN STRUCTURE (SD9.10, TYPE 4C)	EACH	8	\$ 7,500.00	\$ 60,000.00
BREAKAWAY SIGN POST S4X7.7	L.FT.	495	\$ 25.00	\$ 12,375.00
FOUNDATION FOR BREAKAWAY SIGN POST S4X7.7	EACH	39	\$ 280.00	\$ 10,920.00
SLIP BASE	EACH	79	\$ 150.00	\$ 11,850.00
SIGN POST (PERFORATED) (2 1/2 T)	L.FT.	1,007	\$ 12.00	\$ 12,084.00
REGULATORY, WARN, OR MARKER, SIGN PANEL W/TYP VIII/IX SHE	SQ.FT.	958	\$ 14.00	\$ 13,412.00
EXTRUDED ALUMINUM SIGN PANEL	SQ.FT.	4,000	\$ 22.00	\$ 88,000.00
OBLITERATE PAINTED MARKING (STRIPE)	L.FT.	42,000	\$ 0.20	\$ 8,400.00
IMPACT ATTENUATION DEVICE (SAND BARREL CRASH CUSHION)	EACH	28	\$ 8,000.00	\$ 224,000.00
MILEPOST MARKER (S-10)	EACH	9	\$ 220.00	\$ 1,980.00
PAVEMENT MARKING (WHITE THERMOPLASTIC) (0.090")	L.FT.	144,000	\$ 0.30	\$ 43,200.00
PAVEMENT MARKING (YELLOW THERMOPLASTIC) (0.090")	L.FT.	120,000	\$ 0.30	\$ 36,000.00
PAVEMENT MARKING (TRANSVERSE) (THERMOPLASTIC) (ALKYD) (0.0	L.FT.	6,000	\$ 0.50	\$ 3,000.00
PAVEMENT LEGEND (EXTRUDED THERMOPLASTIC) (ALKYD) (0.090")	EACH	29	\$ 110.00	\$ 3,190.00
PAVEMENT MARKING, PREFORMED, TYPE I, WHITE STRIPE	L.FT.	37,500	\$ 3.45	\$ 129,375.00
PAVEMENT MARKING, PREFORMED, TYPE I, FREEWAY ARROW	EACH	118	\$ 250.00	\$ 29,500.00
PAVEMENT MARKER, RAISED, TYPE C	EACH	2,500	\$ 3.25	\$ 8,125.00
PAVEMENT MARKER, RAISED, TYPE D	EACH	160	\$ 2.75	\$ 440.00
POLE (TYPE H) (STANDARD BASE)	EACH	86	\$ 1,900.00	\$ 163,400.00
POLE (TYPE T) (50 FT.)	EACH	75	\$ 3,000.00	\$ 225,000.00
BREAKAWAY BASE FOR LIGHTING POLE OR SIGNAL FLASHER	EACH	86	\$ 800.00	\$ 68,800.00
POLE FOUNDATION (TYPE H) (STANDARD BASE)	EACH	86	\$ 900.00	\$ 77,400.00
POLE FOUNDATION (TYPE T)(40 FT. THRU 55 FT.)	EACH	75	\$ 3,000.00	\$ 225,000.00
MAST ARM (20 FT.)(ALUMINUM TRUSS)	EACH	86	\$ 1,100.00	\$ 94,600.00
ELECTRICAL CONDUIT (2") (PVC)	L.FT.	55,000	\$ 15.00	\$ 825,000.00
ELECTRICAL CONDUIT (3") (PVC)	L.FT.	5,000	\$ 18.00	\$ 90,000.00
ELECTRICAL CONDUIT (3-3") (PVC)	L.FT.	54,000	\$ 22.00	\$ 1,188,000.00

Continued on Next Page

Continued from Previous Page

ITEM DESCRIPTION	UNIT	QUANTITY	UNIT PRICE	EXTENDED AMOUNT
PULL BOX (NO. 7) (WITH EXTENSION)	EACH	20	\$ 600.00	\$ 12,000.00
PULL BOX (NO. 4)	EACH	190	\$ 700.00	\$ 133,000.00
PULL BOX (NO. 6)	EACH	60	\$ 900.00	\$ 54,000.00
PULL BOX (NO. 9)	EACH	10	\$ 2,600.00	\$ 26,000.00
CONDUCTOR (NO. 8)	L.FT.	220,000	\$ 0.75	\$ 165,000.00
CONDUCTOR (INSULATED BOND) (NO. 8)	L.FT.	55,000	\$ 0.50	\$ 27,500.00
TRAFFIC SIGNAL (ELLSWORTH RD TI)	L.SUM	1	\$ 175,000.00	\$ 175,000.00
TRAFFIC SIGNAL (WILLIAMS FIELD RD TI)	L.SUM	1	\$ 275,000.00	\$ 275,000.00
TRAFFIC SIGNAL (SIGNAL BUTTE RD TI)	L.SUM	1	\$ 275,000.00	\$ 275,000.00
TRAFFIC SIGNAL (MERIDIAN RD TI)	L.SUM	1	\$ 275,000.00	\$ 275,000.00
TRAFFIC SIGNAL (IRONWOOD RD TI)	L.SUM	1	\$ 250,000.00	\$ 250,000.00
LUMINAIRE (HORIZONTAL MOUNT) (267 WATT LED)	EACH	86	\$ 850.00	\$ 73,100.00
LUMINAIRE (VERTICAL MOUNT) (267 WATT LED)	EACH	75	\$ 850.00	\$ 63,750.00
LOAD CENTER CABINET (TYPE IV) (240/480 VOLT)	EACH	5	\$ 10,000.00	\$ 50,000.00
SEEDING (CLASS II)	ACRE	179	\$ 3,250.00	\$ 581,750.00
CHAIN LINK FENCE, TYPE 1 (72")	L.FT.	66,140	\$ 18.00	\$ 1,190,520.00
CONCRETE CURB AND GUTTER (TYPE B, C OR C-1)	L.FT.	66,595	\$ 15.00	\$ 998,925.00
CONCRETE CURB AND GUTTER (TYPE D, STD C-05.10)	L.FT.	15,097	\$ 18.00	\$ 271,746.00
CONCRETE CURB (C-05.10) (TYPE A)	L.FT.	8,665	\$ 15.00	\$ 129,975.00
CONCRETE CURB AND GUTTER, TYPE A (MAG DET. 220)	L.FT.	2,330	\$ 15.00	\$ 34,950.00
CONCRETE SINGLE CURB (MAG DET. 222)	L.FT.	1,680	\$ 15.00	\$ 25,200.00
CONCRETE SIDEWALK (C-05.20)	SQ.FT.	79,556	\$ 3.50	\$ 278,446.00
CONCRETE SIDEWALK RAMP (TYPE B C-05.30)	EACH	32	\$ 2,000.00	\$ 64,000.00
CONCRETE SIDEWALK RAMP (TYPE F C-05.30)	EACH	8	\$ 1,500.00	\$ 12,000.00
CONCRETE BARRIER (SINGLE FACE WITH 2.5' GUTTER)	L.FT.	1,525	\$ 60.00	\$ 91,500.00
CONCRETE BARRIER (SINGLE FACE WITH 4.5' GUTTER)	L.FT.	1,659	\$ 65.00	\$ 107,835.00
RIGHT-OF-WAY MARKER	EACH	172	\$ 1,000.00	\$ 172,000.00
RETAINING WALL (REGULAR)	SQ.FT.	6,700	\$ 55.00	\$ 368,500.00
CONCRETE CHANNEL LINING (6")	SQ.YD.	164,015	\$ 50.00	\$ 8,200,750.00
WEIR SPILLWAY FROM ELLSWORTH BASIN	L.SUM	1	\$ 350,000.00	\$ 350,000.00
RCB CULVERT (4-10' X 4' X 35') (ELLSWORTH RD)	L.SUM	1	\$ 50,000.00	\$ 50,000.00
RCB CULVERT (3-12' X 8' X 200') (WILLIAMS FIELD RD)	L.SUM	1	\$ 450,000.00	\$ 450,000.00
RCB CULVERT (3-8' X 8' X 200') (CRISMON RD)	L.SUM	1	\$ 300,000.00	\$ 300,000.00
RCB CULVERT (3-8' X 8' X 202') (SIGNAL BUTTE RD)	L.SUM	1	\$ 300,000.00	\$ 300,000.00
RCB CULVERT (3-8' X 8' X 295') (MOUNTAIN RD)	L.SUM	1	\$ 550,000.00	\$ 550,000.00
RCB CULVERT (3-8' X 8' X 190') (MERIDIAN RD)	L.SUM	1	\$ 300,000.00	\$ 300,000.00
RCB CULVERT (3-8' X 8' X 173') (IRONWOOD RD)	L.SUM	1	\$ 180,000.00	\$ 180,000.00
MOUNTAIN ROAD UNDERPASS	L.SUM	1	\$ 2,876,150.00	\$ 2,876,150.00
ITEM TOTAL:				\$ 40,202,506.00
PROJECT WIDE				
MAINTENANCE AND PROTECTION OF TRAFFIC (2%)		2.0%		\$ 804,050.12
DUST AND WATER PALLIATIVE (2%)		2.0%		\$ 804,050.12
CONSTRUCTION SURVYING (4%)		4.0%		\$ 1,608,100.24
EROSION CONTROL (1%)		1.0%		\$ 402,025.06
MOBILIZATION (8% OF ALL CONSTRUCTION ITEMS)		8.0%		\$ 3,216,200.48
CONTRACTOR QUALITY CONTROL (2%)		2.0%		\$ 804,050.12
PROJECT WIDE SUBTOTAL:				\$ 7,638,476.14
UNIDENTIFIED ITEMS (20% OF ITEM TOTAL AND PROJECT WIDE SUBTOTAL)				\$ 9,568,196.43
PROJECT WIDE TOTAL:				\$ 17,206,672.57

OTHER COST			
ENGINEERING DESIGN (INCLUDES SURVEYING AND GEOTECHNICAL) (8% OF ALL ITEMS):	8.00%	\$	4,592,734.29
ENVIRONMENTAL MITIGATION (UNKNOWN AT THIS TIME):	0.00%	\$	-
CONSTRUCTION ENGINEERING:	9.00%	\$	5,166,826.07
CONSTRUCTION CONTINGENCIES:	5.00%	\$	2,870,458.93
UTILITY RELOCATION:		\$	300,000.00
RIGHT-OF-WAY:		\$	55,641,000.00
OTHER COST TOTAL:		\$	68,571,019.28
SUMMARY			
ITEM TOTAL		\$	40,202,506.00
PROJECT WIDE		\$	17,206,672.57
OTHER COST		\$	68,571,019.28
ICAP (8.36%)	8.36%	\$	10,531,944.54
TOTAL PROJECT COST:		\$	136,512,142.39

6.0 IMPLEMENTATION PLAN

6.1 INTRODUCTION

The ADOT 2011 DCR recommended a three phase implementation plan to systematically build the Preferred Alternative over time as funding becomes available. Phase 1 – SR 202L to Ellsworth Road was subsequently constructed and open to traffic in 2014. This DCR update proposes an additional Interim phase into the implementation plan, Interim Phase 2.

6.2 INTERIM PHASE 2 – ELLSWORTH ROAD TO IRONWOOD DRIVE

The phase 2 project will build the outside lanes and ramps of the ultimate SR-24 between Ellsworth Road and Ironwood Drive.

Ellsworth Road will be widened for the future third northbound lane and right turn lane to eastbound SR-24.

Williams Field Road will be constructed to the ultimate roadway width within ADOT maintained PCCP pavement limits.

Signal Butte Road will be constructed to the ultimate roadway width within ADOT maintained PCCP pavement limits

Mountain Road will be constructed as an above grade overpass to cross over SR-24.

Meridian Road will be constructed to the ultimate roadway width within ADOT maintained PCCP pavement limits

Ironwood Drive will be constructed to the ultimate roadway width within ADOT maintained PCCP pavement limits

The ultimate offsite drainage channel will be constructed north of SR-24 between Powerline floodway and Ironwood Drive. The Ellsworth Road basin will be modified to function as an off-line retention and water quality basin. The need for a pump station has been eliminated by raising the grade of the SR-24 profile and has been eliminated. The Powerline Floodway will be widened to its ultimate configuration.

The estimated construction cost for Interim Phase 2 is approximately \$139,016,495. The order of magnitude cost estimate is provided in section 5 of this DCR update.

7.0 AASHTO CONTROLLING DESIGN CRITERIA

No updates see Section 7 ADOT 2011 DCR.

8.0 SOCIAL, ECONOMIC AND ENVIRONMENTAL CONCERNS

ADOT, in coordination with FHWA, completed an EA for the SR 24 Gateway Freeway (formerly known as SR 802) in April 2011. The 2011 EA evaluated the selected alternative for SR 24 that included construction of a controlled-access high-speed transportation facility from SR 202L MP 34.50 to Ironwood Road. On May 6, 2011, FHWA issued a Finding of No Significant Impact (FONSI) for the SR 24 project (NH-802-A[AUG], 802 MA 999 H6867 01L). An EA Reevaluation is currently being prepared to evaluate the proposed Phase II Interim Improvements and proposed modifications to the selected alternative that was evaluated in the 2011 EA. However, the reevaluation cannot be completed and approved by FHWA until after the project is fiscally constrained.

**FINAL DESIGN CONCEPT REPORT
SR-24, Ellsworth Road to Ironwood Drive
Interim Phase II**

APPENDIX A – SUMMARY OF COMMENTS

SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
in Maricopa County and Pinal County, Arizona

TRACS No. H8915 01L/02L
Federal Project No. 024 A (200)

Draft IDCR Comment Response Document

ADOT Project Manager: Ronald McCally
Consultant: **PARSONS**

INDEX OF COMMENTS RECEIVED

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A-Will Comply
B-Consultant To Evaluate
C-ADOT To Evaluate
D-No Further Action Required

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Draft IDCR Comment Response Document

Client Project Manager: Ronald McCally
Consultant: **PARSONS**

OVERALL COMMENT NO.	REVIEWER COMMENT NO.	DWG, SHT, PAGE NO.	COMMENT	INITIAL CODE	FINAL CODE	DESIGNER RESPONSE
			JOHN WENNES, ADOT ENVIRONMENTAL			
1	1	Pg. 1-1 Draft IDCR	MITIGATION MEASURES – Replace paragraph with the following text: “No updates at this time. As part of the Environmental Assessment Re-evaluation currently being prepared for this study, Mitigation Measures will be updated.”	A	A	Will revise
2	2	Pg. 1-4 Draft IDCR	Section 1.3.3, Second paragraph, second row – include “of” after “the area north”	A	A	Will revise
3	3	Pg. 4-2 Draft IDCR	Section 4.4.1, First paragraph, second row – include “roads” after “planned”.	A	A	Will revise
4	4	Pg. 8-1 Draft IDCR	Section 8, First paragraph – replace all text with “Updates for the current study are in process.”	A	A	Will revise
			TED LEHMAN, JE FULLER - HYDROLOGY			
5	1	App. D, Draft Initial Drain. Report	Sub-basin E6A appears to have been left developed, while the report suggests it should have been reverted to undeveloped conditions	A	A	Will revise. The basin unit hydrograph was revised to reflect undeveloped conditions, but tests indicate further revisions are needed to simulate that condition appropriately

A-Will Comply
B-Consultant To Evaluate
C-ADOT To Evaluate
D-No Further Action Required

**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
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OVERALL COMMENT NO.	REVIEWER COMMENT NO.	DWG, SHT, PAGE NO.	COMMENT	INITIAL CODE	FINAL CODE	DESIGNER RESPONSE
6	2	App. D, Draft Initial Drain Report	Sub-basins GM16-GM20 are combined downstream of the SR24 channel and detention basin. Review of the development plans, topography, and discussions between the Premier (working on the Ellsworth Channel realignment) and Parsons team members suggest that any outflow from these sub-basins is more likely to be collected by the new SR24 channel, probably near its intersection with Crismon Road.	A	A	Model has been revised
TAMMY MIVSHEK, ADOT TRAFFIC ENGINEERING						
7	1	IDCR 4-4	4.4.2 Ellsworth Road Interim TI, it states "The traffic operational analysis indicates the intersections will operate at adequate capacity for the Interim Design Year 2025." In the Traffic Analysis Report on page 17, Table 5 it shows that the overall operation of the NB and WB approach the overall LOS for AM and PM Peak hours are at F(E) for NB and F(F) for WB for the SR 24/Ellsworth WB Ramp under Option A. Under Option B, the LOS during AM and PM Peak Hours is F(F) for the NB approach and F(F) for the WB approach at the WB Ramp per Table 7 on Page 19 of the Traffic Analysis Report. At present the intersection is operating under acceptable conditions with some delays in the turning movement.	B	A	The overall level of service is acceptable with the mitigated lane configurations shown in figures 6 and 7 of the report.

A-Will Comply
B-Consultant To Evaluate
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D-No Further Action Required

**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
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TRACS No. H8915 01L/02L
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Draft IDCR Comment Response Document

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Consultant: **PARSONS**

OVERALL COMMENT NO.	REVIEWER COMMENT NO.	DWG, SHT, PAGE NO.	COMMENT	INITIAL CODE	FINAL CODE	DESIGNER RESPONSE
8	2	IDCR 4-8	4.12 Freeway Signing and Pavement Marking, it states "A signing concept plan was developed to ensure an effective signing plan should be developed for the Preferred Interim Alternative." The Interim concept appears to be directed at the Ultimate condition and not the Interim. It doesn't make sense to sign for roads that don't exist yet. Also, would we want to have sign structures sitting out there without signs on them and to be sitting there for however long in between the interim and ultimate? What if during the Ultimate Design the structures are in the way of future sound walls, etc.	B	D	Even though some of the roads do not exist today, we are assuming they will be there at time of construction or soon after. For the DCR we will depict the striping as if the roads existing other than at Meridian.
9	3	IDCR 4-8	4.12 Freeway Signing and Pavement Marking. These are going to be at-grade intersections but I don't see any signing pertaining to the x-roads at the TIs. Only Ellsworth, Mountain and Ironwood are open but there is nothing showing what will be used in order to guide or control traffic on these roadways. The other roads for the x-roads may be used as turn around points for the Interim condition but again there is no traffic control or guide signing. For the roads that lead to nowhere it would also be a good idea for barricades to be placed at the end of the roadway.	B	D	We are updating the original DCR. The traffic plans were at the same level of detail. Intersections to be signalized except Meridian Road

A-Will Comply
B-Consultant To Evaluate
C-ADOT To Evaluate
D-No Further Action Required

**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
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OVERALL COMMENT NO.	REVIEWER COMMENT NO.	DWG, SHT, PAGE NO.	COMMENT	INITIAL CODE	FINAL CODE	DESIGNER RESPONSE
10	4	IDCR 4-8	4.13 Lighting and Traffic Signals. There were no comments made pertaining to the Interim condition. Is there lighting going to be placed on the Interim condition. It appears that the mainline will be divided without barrier put in place but lighting is not going to be placed on the ramps? Also, no mention of any signals in the Interim. The Ellsworth signal would need to be updated because of the new ramps. The end of roadway, whether it be Signal Butte, if that option is selected and the roadway built, or Ironwood, will lead into a roadway that will have traffic on it. Will traffic control be set up utilizing a signal light at that location? What about Mountain Road. What type of traffic control will be used on this roadway, a stop condition or a signal light. SR 24 will not be able to move freely through these locations.	A	A	We are adding Signals and Lighting. All cross roads will have signals with the ramps for the interim condition except for Meridian.
11	5	IDCR 4-8	4.14 Construction Phasing and Traffic Control. It may be advisable that an Emergency Management Plan be put into effect as well with the traffic control in order for emergency vehicles and personnel to enter into the construction area since there will be limited points in which to enter in case of an emergency. It probably would be helpful for emergency personnel to know where the access points would be to the project if something were to happen during construction of SR 24.	D	A	This appears to be a final design issue. Text will be included indicating an Emergency Management Plan needs to be prepared during final design.

A-Will Comply
B-Consultant To Evaluate
C-ADOT To Evaluate
D-No Further Action Required

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**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
in Maricopa County and Pinal County, Arizona**

TRACS No. H8915 01L/02L
Federal Project No. 024 A (200)

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OVERALL COMMENT NO.	REVIEWER COMMENT NO.	DWG, SHT, PAGE NO.	COMMENT	INITIAL CODE	FINAL CODE	DESIGNER RESPONSE
12	6	IDCR, App. C T-1.01	The raised pavement markers should all be Type C since there are median islands separating the traffic lanes on the x-roads. Type C should be used on all the lane lines. The spacing for the RPM's on the broken white should be at 40 ft. spacing and not 20 ft. spacing and on the turn lane lines they should be spaced at 20 ft. Also, Type D RPMs should also be used on the median island noses as per Std. Dwg. M-1 as well as the yellow paint.	A	A	Will revise.
13	7	IDCR, App. C T-1.01 - T-1.10	Ellsworth Rd Ramp "A" Connector is listed as "Future" per C-3.01. As far as the DCR is concerned all of the work will be done on the East of Ellsworth Rd. Why is there new sign panels and sign structure being placed for Ramp A depicting two lanes for WB L202 and one lane for NB L202. There is nothing in the DCR that states that this ramp will be widened to two lanes for WB direction during the Interim.	A	D	The connector ramp will not be constructed with interim project
14	8	IDCR, App. C T-1.01	Per the 1st paragraph under 4.4.2 Ellsworth Road Interim TI on Page 4-4 of the DCR it states, "For the interim condition, NB Ellsworth Road will be widened to add additional pavement for the future third through lane northbound." This 3rd lane in the NB direction was also depicted in Appendix C on sheet C-4.01 but is not shown on the pavement marking sheet T-1.01.	B	A	Discussion needed based on Traffic Operations at Ellsworth Road. The project team will meet with the City of Mesa to discuss the third left turn lane. The results of this meeting will impact the report. Meeting resulted in 2 Lt turn lanes at this location based on operations and maintenance preferred by the City of Mesa. Updates will reflect this.

A-Will Comply
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15	9	IDCR, App. C T-1.01 - T-1.10	Again many of the signs on here are more representative of the Ultimate condition and not of the Interim condition. We shouldn't be signing for roadways that do not exist at this time nor should we have signing such as "Right Lane Exit Only" signs in the interim. Some of the signs on these pages do not comply with the 2009 MUTCD or the current MOAS as shown.	A	A	Even though some of the roads do not exist today, we are assuming they will be there at time of construction or soon after. For the DCR we will depict the striping as if the roads existing other than at Meridian
16	10	IDCR, App. C T-1.01 - T-1.10	On the x-roads there is no signing shown or barriers for end of roadway conditions on the non-existent roads. On all of the x-roads, with the exception of Meridian Rd, it shows that the striping will match existing striping regardless of whether the road exists or not. At Meridian no striping is shown on T-1.08 even though on C-4.06 it shows a portion of the x-road will be built. In the interim the only roads in existence will be Ellsworth, Mountain, and Ironwood. The x-road sheets should be more representative of the conditions that will exist when the Interim project is completed. If the Interim conditions do include x-roads around SR 24 even though the roadways are not in place is beneficial to traffic who can use them to make turn around. It does not show on the x-roads if it will be free flow through them, stop condition, or signal light.	B	A	Even though some of the roads do not exist today, we are assuming they will be there at time of construction or soon after. For the DCR we will depict the striping as if the roads existing other than at Meridian. At the time of final design it will be determined which cross roads will be developed. We will add a discussion to the DCR.
17	11	IDCR, App. C T-1.01 - T-1.10	Why isn't there a W10-2 Expressway Ends XX Miles located on EB SR 24 before Ironwood?	B	A	Warning and regulatory signs will be freeway size and not expressway size.

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18	12	Traffic Analysis Report	On Page 6, 1st Paragraph under Existing Intersection Configuration it states that the NB approach on Ellsworth consists of four through lanes at the EB off-ramp. Technically there are four lanes going through this intersection but in reality there are only two through lanes. The other two lanes are actually two left turn storage lanes for the WB on-ramp.	A	A	The text of the report will be updated to clarify that two left turn lanes are queue storage for the northbound left turn lanes at the intersection of Ellsworth Road and SR 24 EB Ramps.
19	13	Traffic Analysis Report	On Page 8 the left turn arrow in Figure 1A is missing.	A	A	The figure will be corrected.
20	14	Traffic Analysis Report	On Page 9, it appears that the data in Table 2 is backwards for 1A and 1B.	A	A	The figure will be corrected.
21	15	Traffic Analysis Report	On Page 9 in the first sentence of the 2nd paragraph under Crash Analysis it states, " identified a one-year total of 24 crashes (without any fatalities) on 24 from Loop 202 . . ." Should it not say " identified a one-year total of 24 crashes (without any fatalities) on SR 24 from Loop 202. . ."	A	A	The table will be corrected.
22	16	Traffic Analysis Report	On Page 11 under Projected Segment Traffic Volumes, it states an "end of freeway" condition. Ellsworth is the "end of freeway" condition and Signal Butte in Option B or Ironwood in Option A would be an "end of expressway" condition. Per the ADOT Roadway Design Guide (2012), "Full access control gives preference to through traffic by providing access only through selected public roads and by prohibiting at-grade crossings or direct access from abutting property. Partial access control still gives preference to through traffic but permits some crossings at grade	B	A	The report will be updated to state that Ellsworth Road is an end of expressway condition in Option A.

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			and some private driveway connections." The 2009 MUTCD defines a Freeway as a divided highway with full access control and an Expressway as a divided highway with partial control of access. "End of freeway" exists at Ellsworth Rd with the at-grade signalized intersection. In the Interim SR 24 could only be labeled as an Expressway with the at-grade intersections with partial controlled access from Ellsworth Rd to Signal Butte Rd/Ironwood Rd, depending on the Option selected.			
23	17	Traffic Analysis Report	On Page 4-4 of the DCR, 1st paragraph under 4.4.2 Ellsworth Road Interim TI it states, "For the interim condition, NB Ellsworth Road will be widened to add additional pavement for the future third through lane northbound." The DCR does not state that the third lane would be opened to traffic but is shown as a possibility in Appendix C C-4.01. The projected traffic volumes do not show any projections with the possibility of this third NB through lane	B	A	The project team will evaluate the recommended intersection geometry at the intersection of Ellsworth Road and SR 24 WB Ramp due to the impact to the SR 24 EB on ramps and Ellsworth Road. Pavement widening on Ellsworth Road is to accommodate the 12-foot lane shift of the existing NB through lanes. The additional pavement width will be used for the third northbound left turn lane.
24	18	Traffic Analysis Report	Currently Signal Butte Rd does not exist in the area of SR 24. From what I understand in the DCR under Option A that this road will not be built by 2025. Under Option B it would become the logical terminus but would still have to be built. Why is it under Option A that you are showing through movements NB and SB through the intersections to a nonexistent road?	B	D	Signal Butte Road is expected to be built at time of construction or soon after. We are showing the ultimate striping, Final Designer will provide appropriate striping at time of construction. City of Mesa is planning to construct Signal Butte Road from Ray Road to Pecos Road.
25	19	Traffic Analysis Report	In Figure 4 and Figure 5, on the diagram you are showing Meridian Rd as Moeur Rd.	A	A	Will change

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26	20	Traffic Analysis Report	On Page 18, 20, Figure 6, and Figure 7 for the Mitigated intersections, adding a third left turn lane for the WB on ramp at Ellsworth would improve the level of service for Option A and Option B but there are other factors that also need to be considered. By adding the third left turn lane this would mean widening Ellsworth Rd with another lane on top of the third NB through lane. Also, the WB on-ramp would need to be widened to three lanes from the existing two in order to accommodate the third left turn lane. By adding the third lane on the ramp there would need to be enough room in order to merge that third lane prior to Ramp A or leaving the third lane as the Ramp A lane from the Ellsworth intersection.	B	A	The project team will evaluate the recommended intersection geometry at the intersection of Ellsworth Road and SR 24 WB Ramp due to the impact to the SR 24 EB on ramps and Ellsworth Road. Pavement widening on Ellsworth Road is to accommodate the 12-foot lane shift of the existing NB through lanes. The additional pavement width will be used for the third northbound left turn lane. Ellsworth Road will not be widened to three through lanes. The WB on ramp would need to be widened to add an additional lane.
27	21	Traffic Analysis Report	Figure 7, the proposed lane configuration diagrams label 3A and 3B as Ironwood Dr when they should be Signal Butte Rd.	A	A	The figure will be corrected.
28	22	Traffic Analysis Report	Page 26 under 2025 Option A Scenario, 1st paragraph Ironwood Rd would not be an "end of freeway" but an "end of expressway" condition. Also it states that Mountain Rd would be "grade separated" over SR 24 but in the next paragraph it states, "Grade separation of interchanges is not recommended in the 2025 Option A scenario." Maybe it should be re-stated that all other interchanges besides Mountain Rd will not be grade separated.	D	A	Mountain Road will not be an interchange. It will just be a grade separated crossing. It will not have direct access to SR-24 The text will be clarified to better explain why Mountain Road isn't a TI.
29	23	Traffic Analysis Report	Page 27, third paragraph under 2025 Option A Mitigated Analysis, third line states, "...ramp through movement During AM both peak hour." Please clarify.	A	A	The report will be updated to state that the northbound left turn turning movement conflicts with the westbound ramp movements. The word "through" will be deleted.

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30	24	Traffic Analysis Report	Page 27 under 2025 Option B Scenario, 1st paragraph, Signal Butte would be "end of expressway" condition and not "end of freeway."	B/C	A	The report will be updated to designate that Signal Butte Road will be an "end of expressway" condition.
			EUNICE CHAN, FHWA			
31	1	Pg 3, Traffic Analysis Report	2025 Opt A Mitigated Analysis references expected delays for the NB left turn movement at the intersection of Ellsworth Rd and WB SR24 Ramps and no further mitigation is recommended. a. Include discussion of the severity of the impact to justify the recommendation for no mitigation. Appendix H seems to indicate that even with the mitigation measures, there will be a 76.8 s/veh delay for the NBL movement on Ellsworth and SR 24 WB Ramps, and a 102.9 s/veh delay for the EBT movement on Ellsworth Rd and SR 24 EB Ramps.	B	A	The predicted overall level of service for the 2025 Option A mitigated condition is level of service D or better. The predicted delay for northbound left turning vehicles is in the AM peak hour only. For intersection with heavy through movements, turning movement delays in the peak hour are not uncommon.
32	2	Pg 4, Traffic Analysis Report	2035 Horizon Year – mentions that vehicles are expected to queue on the westbound on ramp and northbound left turn lane at the intersection of Meridian Rd and SR 24 WB Ramps and no mitigation is recommended. a. Include discussion of the severity of the impact to justify the recommendation for no mitigation. For example, Appendix K indicates LOS F during peak hours for the NBL in 2035, but the delay is only 58.1 s/veh.	B	A	The predicted overall level of service for the 2035 horizon year is level of service D or better. The predicted delay for northbound and westbound turning vehicles is in the AM peak hour only. For intersection with heavy through movements, turning movement delays in the peak hour are not uncommon.

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33	3	Pg 6, Traffic Analysis Report	Existing Roadway Network – Include sentence on posted speed limit for Meridian Road.	A	A	The report will be updated.
34	4	Pg 11, Traffic Analysis Report	Design Concept Report Alternatives and Projected Segment Traffic Volumes discussions appear to be the same?	A	A	The report will be updated.
35	5	Pg 17, Traffic Analysis Report	Table 5: a. Clarify "recommended lane configurations" in the first sentence. Figure 6 only labels the "Mitigated" configurations. Are the recommended lane configurations the ones that are unlabeled? b. Include discussion of the severity of unmitigated peak hour delays (Appendix G). For example, not incorporating the recommended mitigation would result in LOS F with a delay of 137.2 s/veh for the NBL and 564.1 veh/s for WBT at the intersection of Ellsworth Rd and SR 24 WB Ramps.	A B	A A	a. Table 5 refers to the unmitigated lane configurations. The text and figures will be updated. b. Table 5 refers to the unmitigated lane configurations. An alternative analysis is shown in Table 6 with the mitigated levels of service. Discussion referring to Table 6 and the mitigated analysis will be added to this section.
36	6	Pg 18, Traffic Analysis Report	Table 6 – See comment 1. Table shows LOS C for EB through movements at Ellsworth Rd and EB SR 24 Ramps. But Appendix H shows LOS F?	A	A	Table will be updated.
37	7	Pg 19, Traffic Analysis Report	Table 7 – See comment 5.a.	A	A	Table 7 refers to the unmitigated lane configurations. The text and figures will be updated.

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38	8	Pg 21, Traffic Analysis Report	Table 9 – See comment 2.a.	A	A	Table 9 refers to the unmitigated lane configurations. The text and figures will be updated.
39	9	Traffic Analysis Report	Figure 6 - Didn't see a difference between the original and the mitigated configuration for 3A or 3B? What was the mitigation?	A	A	The mitigated lane configuration at Signal Butte Road and SR 24 WB off ramps is three (3) northbound left turn lanes. The figure will be updated.
40	10	Traffic Analysis Report	Figure 8 – Reason for calling out the lane configurations on Meridian Rd and not for the other crossroads?	D	D	The lane configuration was shown on Meridian Road to clarify a six lane cross section north of SR 24 and a four lane cross section south of SR 24.
41	11	Pg 3-1, Draft IDCR	a. Provide description of Tier 1 analysis and background on why it was not used for evaluating the four alternatives. b. Section 3.3.2 Description of Alternatives should reference or include typical sections of each alternative.	D	D	a. Tier 1 analysis was used for determining the SR 24 Corridor Alignment in the original DCR. b. Will include typical sections of each
42	12	Pg 3-2, Draft IDCR	a. Was Alternative B removed from consideration for reasons other than the feasibility of the traffic operation analysis? b. Clarify last sentence under subheading, "Compatibility with Ultimate."	D	D	a. That and the compatibility with the ultimate. b. Will clarify

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43	13	Pg 3-3, Draft IDCR	a. Traffic Analysis – All alternatives would operate at a similar Level of Service, which is -? Provide additional discussion. b. Suggest including a table that shows how each of the four alternatives quantitatively addresses the primary objectives of the evaluation criteria as part of the Tier 2 evaluation process. While this is generally discussed per alternative, it is not presented in a way that allows comparison of similarities and differences between the alternatives and the extent to which they meet (or don't meet) the primary objectives. c. Second sentence under "Development Impacts" should include "of" between "amount" and "area" d. Under "Estimated Construction Cost" subheading, the Alternatives in the second paragraph should be capitalized for uniformity (see also para 4.5 on pg 4-5). • What were the costs for each alternative? It appears that only the estimated cost for the preferred alternative is given (pg. 5-1).	D	D	a. Our scope was to update the existing DCR therefore was structured to provide a traffic analysis on the selected alternative. b. Will add table c. Will revise d. Will revise • Our scope was to update the existing DCR therefore was structured to provide a traffic analysis on the selected alternative.
44	14	Pg 4-2, Draft IDCR	Include discussion of number of GP lanes in the WB direction under subheading, "SR 24 Interim Westbound Mainline."	A	A	Will add two GP lanes

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45	15	Pg. 4-4, Draft IDCR	4.4.5 Signal Butte Road Full Diamond TI 1. General note: in order for Signal Butte to be the logical terminus, City of Mesa needs to include improvements in the STIP (to the north and south) to ensure Signal Butte can handle the end of freeway traffic	A	A	Text will be added to denote the City of Mesa needs to include improvements.
46	16	Pg. 4-7, Draft IDCR	Section 4.8.4 Noise Walls notes no updates. Verify if any updates/additional mitigation measures are needed to reflect the change from a depressed freeway to an at grade or above grade freeway between Williams Field Rd and Ironwood and the change from at grade to above grade bridges at Crimson and Mountain.	B	C	Decision from FHWA pending. Depending on outcome ADOT would prepare a Hot Spot or noise wall Analysis if needed.
47	17	Pg. 5-2, Draft IDCR	a. Does the project wide erosion control (1%) cover permanent erosion control measures or just BMPs during construction? Verify whether permanent seeding for all disturbed areas is included within this 1% or include a line item in the cost estimate as there will be no landscaping under the interim condition. b. Ensure all existing pedestrian features within the interim scope of work/project limits are upgraded, if needed, and any new features designed to meet ADA/PROWAG.	B A	A A	a. Will add seeding item b. Will add a statement regarding upgrading existing facilities to meet ADA/Prowag

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KEN AKOH-ARREY, ADOT DRAINAGE						
OVERALL COMMENT NO.	REVIEWER COMMENT NO.	DWG, SHT, PAGE NO.	COMMENT	INITIAL CODE	FINAL CODE	DESIGNER RESPONSE
48	1	App. D, Draft Initial Drain. Report	Existing condition HEC-1 Schematic is not matching the input in HEC-1 output. Sub-basin labels such as P1, P2, etc., are not on the schematic. Is there another schematic which should have been included? In fact, the labels on this schematic map are only of the E-series.	A	A	The ADMPU schematic will be included for reference. The project Schematic represents only the watershed pertaining to SR 24, which was revised for the project (see Section 4.4, Draft Initial Drainage Report). The Hydrologic model includes the entire East Mesa ADMPU area, incorporating E, P and R sub-basin groups. The ADMPU model was maintained intact in its coverage to ensure that the revised information is available to FCDMC and City of Mesa for further updates as a comprehensive regional tool.
49	2	Pgs 21-22, Draft Initial Drain. Report	The Interim option – the Baseline option, modeled with existing condition will convey more flow than any of the three ultimate condition options that were eliminated from consideration. However, Figure 6 is not showing a pump station as shown for those three options. Will this option get by without a pump station? How so? What is different?	A	A	The interim and revised ultimate roadway profiles are fully above ground and the pump station is not needed in any of the options that were analyzed. The reference to a pump station in the exhibits is incorrect and it was removed.
50	3	Pg 27, Draft Initial Drain. Report	Section 4.6 - This section should include discussion on the pump station as a conceptual design appurtenant that supplements the performance of the channel, if there is going to be one.	D	D	The pump station is not needed.
51	4	Pg 27, Draft Initial Drain. Report	Section 4.6 - The second bullet states that flow from PPGN (Wood Patel, 2014) in excess of the 100-year, 24-hr storm would flow across Ellsworth Rd. to the Ellsworth Retention Basin and fill it up limiting the flow that can be clipped from the channel's hydrograph for attenuation. Is this a potential problem? What is the recommended solution so that more discharge is not sent downstream than is being intended?	D	D	Note that the statement refers to "flows in excess of the 100-year, 24-hour event", which is a condition in excess of the design and is applicable for extreme events only. At the moment this is an assumption, as the PPGN development is in very early stages of planning and a detailed grading plan is not available to indicate the location where emergency flows would leave the development.

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		MIKE DUNCAN, FLOOD CONTROL DISTRICT OF MARICOPA COUNTY			
52	1	App. D - Draft Initial Drain. Report	HEC-1 model output, for run of 01DEC15 14:28 The flows from the SR24 channel and the Ellsworth Basin area are: "802ELS", "G19E26", and "G17E26", which are 1,876 cfs + 182 cfs + 0 cfs = 2,058 cfs, which exceeds the 1,650 cfs criteria of Section 4.6, page 27 of the report.	A	A The analysis in the Draft Initial Drainage Report was done for a detention volume of 96 ac-ft. Approximately 109 ac-ft of detention volume is needed to attenuate the peak flow to 1,650 cfs. An area suitable for detention has been identified at Ellsworth Rd, Ramp C, which could provide the additional volume.
53	2	App. D - Draft Initial Drain. Report	Line 1242, page 29, of the HEC-1 output has: DT 1650UP 96.0 0.0 Which means that the diversion is limited to 96 acre-feet, but section 4.6 of the report mentions 100 acre-feet.	A	See response to Comment 52/1
54	3	Draft Initial Drain. Report	The report does not address or show that the Powerline Floodway (and downstream East Maricopa Floodway) is not negatively impacted by the drainage system that encompasses the SR24 channel and the Ellsworth Basin.	B	The impact is being assessed based on the hydrology and the conceptual design work for the Ellsworth Channel Relocation, which followed the SR 24 hydrology.
55	4	App. D - Draft Initial Drain. Report	HEC-1 Schematic - At the upper left there are two concentration points shown with the same label CPE26A	A	Duplicate label was deleted
56	5	Sht. D-1.03, Plans	The bottom width for the proposed, modified Powerline Floodway channel is 55 feet. What is the design basis for this?	B	The impact is being assessed based on the hydrology and the conceptual design work for the Ellsworth Channel Relocation, which followed the SR 24 hydrology.

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57	6	Sht. C-4.07, Plans	The box culvert under Ironwood Dr is shown as 2 @ 8' x 6'. This should be 3 @ 8' x 8' to match the same culvert shown on sht. C-3.35.	A	Will adjust
58	7	Sht. D-1.01, Plans	Are there any supporting analyses to show that the approx. 750 ft. long lateral weir and 4 barrel box culvert will function as expected to meet the overall peak outflow criteria?	B	Analysis is in progress and will be made available with the Initial Drainage Report. Analysis included in drainage report.
59	8	Sht. D-1.02, Plans	The typical section uses B for top width while the table below uses T.	A	Will adjust
60	9	All sheets, Plans	Refer to Ironwood Road but it should be Ironwood Drive.	A	Will adjust
61	10	Sht. D-1.03	The channel side slopes are shown as 1.5:1. For the subject major re-construction of the Powerline Floodway, side slopes of 2:1 would be the steepest allowed by FCDMC.	A	Will adjust

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Consultant: **PARSONS**

		JEFF SHELTON, FLOOD CONTROL DISTRICT OF MARICOPA COUNTY				
62	1	App. D, Draft Initial Drain. Report	HEC-1 model 24INT100C.dat. Comparison of EMADMPU hydrology to SR-24 hydrology and the effect on the EMF. The hydrograph at CPEMF1 from model 24INT100C.dat was added to a hydrograph from PVR with peak of 600 cfs. This was then input into an unsteady EMF HEC-RAS model that was developed by the FCD to evaluate the levee status of the channel. The hydrographs for CPEMF1 and PVR were added together for the existing and future EMADMPU models and input into the unsteady EMF model for comparison to 24INT100C.dat. The results indicate that your current plan would produce water surfaces 1.37 feet higher than the future EMADMPU model in the EMF at the Powerline Floodway. Average increases of approximately 0.5 feet occur for miles up and down stream of the confluence. The results also indicate that your current plan would produce water surfaces 0.16 feet higher than the existing EMADMPU model in the EMF at the Powerline Floodway. Your model also produces reductions in the water surface for miles downstream of the confluence (see attached spreadsheets). The EMF HEC-RAS model and other supporting calculations will be provided upon request.	A	A	FCDMC provided the regional model. The material will be referenced and the effects of the added SR 24 flows described in the Initial Drainage Report.
63	2	App. D, Draft Initial Drain. Report	HEC-1 model 24INT100C.dat. Function of basin at Ellsworth Road and SR-24. The calculations in HEC-1 (802ELS) that represent the offline basin at Ellsworth are so basic that they might not adequately give a rough estimation of the effect the SR-24 drainage system has on the Powerline Floodway and EMF.	B	A	The level of hydraulic modeling involved is complex and is dependent of an advanced design stage that was not scoped for the IDCR phase of the project. The detention basin operation is being refined, but at a simplified level.

A-Will Comply
B-Consultant To Evaluate
C-ADOT To Evaluate
D-No Further Action Required

**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
in Maricopa County and Pinal County, Arizona**

TRACS No. H8915 01L/02L
Federal Project No. 024 A (200)

Draft IDCR Comment Response Document

Client Project Manager: Ronald McCally
Consultant: **PARSONS**

		MARIA DEEB, CITY OF MESA				
64	1	Pg. 1-1 Draft IDCR	Programming, Paragraph two - Define acronym: Regional Transportation Plan Freeway Program	A	A	Will define
65	2	Pg. 1-1 Draft IDCR	Mitigation Measures, Paragraph one - I will suggest not using the words: "no updates" The mitigation language currently used by ADOT has changed since 2010. Also, the concept includes updated locations for drainage structures, therefore related mitigations be required? these might affect level of impact and impact locations. And have the noise and air quality conformity runs been completed? HPT completed? Will updates only occur during design and not at this DCR stage? Suggest text with clarification if not updates are to be done at this time but will during the design phase.	A	A	Will provide updates if available at time of final DCR submittal or provide statement regarding the update to the Environmental Evaluation and mitigations
66	3	Pg. 1-3 Draft IDCR	Provide a color label that explains the pink vs. blue colors.	A	A	Will add
67	4	Pg. 1-4 Draft IDCR	Section 1.3.1, Paragraph one - Within Mesa: per the Mesa 2040 Transportation Master Plan (page 81) it is a 6L arterial separated by raised medians from Southern Avenue to Pecos Road, then a 4L with raised medians to Germann Road (medians page 77)	A	A	Will update to further extents
68	5	Pg. 1-4 Draft IDCR	Section 1.3.1, Paragraph two - Within Mesa: per the Mesa 2040 Transportation Master Plan (page 81) it is a 6L arterial separated by raised medians from Ellsworth Road to Crismon, then a 4L with raised medians to Meridian Road (medians page 77)	A	A	Will update to further extents

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69	6	Pg. 1-4 Draft IDCR	Section 1.3.1, Paragraph three - 4 lane per the 2040 plan	A	A	Will adjust Crismon Rd to 4 lanes with raised median
70	7	Pg. 1-4 Draft IDCR	Section 1.3.1, Paragraph four - medians are required on all legs of arterials to arterials, raised medians are proposed for SB from north of Williams Field to Pecos Roads	A	A	Will update to further extents (Comment 67)
71	8	Pg. 1-4 Draft IDCR	Section 1.3.1, Paragraph six - classified as 6L except in segment from south of Guadalupe Road to Williams Field Road where it is a 4L	A	A	Will update to further extents (Comment 67)
72	9	Pg. 1-4 Draft IDCR	Section 1.3.1, Paragraph six - medians are required on all legs of arterials to arterials, raised medians are proposed for Meridian from north of Williams Field to Pecos Roads	A	A	Will update to further extents (Comment 67)
73	10	Pg. 1-5 Draft IDCR	Section 1.3.6, Drainage - suggest including comment: "see detailed drainage report".	A	A	Will add
74	11	Pg. 4-1 Draft IDCR	Section 4.2, Table 1 - typo	A	A	Will fix spelling of Clearance
75	12	Pg. 4-1 Draft IDCR	Section 4.2, Table 2 - typo	A	A	Will fix spelling of Clearance
76	13	Pg. 4-2 Draft IDCR	Section 4.3, SR 24 Interim Freeway Concept - Can we add language in the introduction section that references: The interim concept will include accommodation for a trail; the City may open it prior to the freeway's ultimate construction.	A	A	Will add

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77	14	Pg. 4-8 Draft IDCR	Section 4.11.3, Landscaping - The interim landscape should support the construction of a shared use pathway.	B/C	A	We will reference seeding on the trail
78	15	Pg. 4-9 Draft IDCR	Section 4.15.1, FMS Communications and Trunk Line - Should the foundation/infrastructure be constructed with interim and at ultimate pull wire, etc. as desired/needed?	D	A	DISCUSSION NEEDED We received comment from ADOT Central Phoenix Construction District during our CRA meeting to not include FMS infrastructure as it gets damaged prior to fiber being pulled. Text to be added to DCR Update to reflect that conduit should be included along the corridor for signal use.
79	16	Pg. 4-9 Draft IDCR	Section 4.15.1, FMS Communications and Trunk Line - Per Avery R. If signals are to be operated by COM we desire to get fiber to them sooner rather than later. I would recommend that conduit be added to any bridge structures; if the freeway crosses any canals, drainage areas, etc. it would be a good idea to get a conduit crossing in those structures if they are built now. COM wants to know which traffic signals we were going to have in this interim condition so we recommend some conduit that could help us right away	B/C	A	DISCUSSION NEEDED Text to be added to DCR Update to reflect that conduit should be included along the corridor for signal use.
			ERIK GUDERIAN, CITY OF MESA			
80	1	Pg. 4-4 Draft IDCR	Section 4.4.3, Paragraph one - It should be assumed that Williams Field could be open during the interim condition. Most likely not at opening day, but at some point.	A	A	Will assume it is open.

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Draft IDCR Comment Response Document

Client Project Manager: Ronald McCally
Consultant: **PARSONS**

81	2	Pg. 4-4 Draft IDCR	Section 4.4.6, Paragraph one - Has this been proposed to Fuji in previous meetings with them? There is a new development plan for the north section of their property.	D	D	Yes, we have provided our design and have met with Fuji Film on 3/3/16. There are benefits to Fuji Film as well by reducing the R/W impacts along SR-24
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A-Will Comply
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Page 23 of 31

**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
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Draft IDCR Comment Response Document

Client Project Manager: Ronald McCally
Consultant: **PARSONS**

			MARC AHLSTROM, CITY OF MESA			
82	1	Pg. 1-5 Draft IDCR	Table 1, Ellsworth Cross Street - There is also a 20" water line in Ellsworth. Both water lines are DIP.	A	A	Will add
83	2	Pg. 4-4 Draft IDCR	Section 4.4.4, Crismon Road Grade Separation - This should be included in the cost of the freeway.	A	A	Portion inside ADOT R/W to be included in the ultimate SR 24 project.
			AL ZUBI, CITY OF MESA			
84	1	Pg. 4-4 Draft IDCR	Section 4.4.4, Crismon Road Grade Separation - Same comment on the economic impact on adjacent properties as Mountain Rd.	A	A	Portion inside ADOT R/W to be included in the ultimate SR 24 project.
85	2	Pg. 4-4 Draft IDCR	Section 4.4.4, Paragraph one - How will that be funded if not by the SR24 project?	A	A	It will be funded by SR-24 just not the interim project.
86	3	Pg. 4-4 Draft IDCR	Section 4.4.6, Mountain Road Grade Separation - Raising Mountain Rd will also have an economic impact on the other three corners/properties, by limiting access. Would ADOT take that in consideration, and not just discuss the impact with just Fuji, but the other property owners?	A	A	A statement will be added to the document about ADOT R/W acquisition process and Final Design.
87	4	Pg. 4-4 Draft IDCR	Section 4.4.6, Paragraph one - Remove reference to 2011 DCR as the nature of the grade separation changed (<i>Parsons interpretation of the highlighted text</i>)	A	A	It will be removed.

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**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
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Draft IDCR Comment Response Document

Client Project Manager: Ronald McCally
Consultant: **PARSONS**

		CHAUN HILL, MARICOPA ASSOCIATION OF GOVERNMENTS				
88	1	General, Draft IDCR	Please correct references to read "SR-24"	A	A	Will update
89	2	Pg. 1-1 Draft IDCR	<i>Executive Summary</i> - When referencing "Group 3" of the RTPFP, should this be "Phase 3"?	D	D	Latest RTPFP describes "Groups" rather than "Phases"
90	3	Pg. 1-1 Draft IDCR	<i>Section 1.3.3, Paragraph two</i> – "City of Mesa has requested that the new right-of-way accommodate a future multi-use path that may follow the SR-24 alignment." Is this request accommodated within the currently identified right-of-way footprint, or will additional right-of way be necessary?	A	A	The proposed R/W accommodates the trail.
91	4	Pg. 3-1 Draft IDCR	<i>Section 3.3, Paragraph one</i> – "Connectivity of Mountain Road between Williams Field Road and Pecos Road must not be removed in the interim alternatives." This again brings up the concern of interim and ultimate access. If interim access is provided at Mountain Road, does this provide the expectation that access will be provided in the ultimate condition? Is this the intent of the ultimate project?	A	A	Will clarify, Mountain Road is only a Grade Separated Crossing; it is not an interchange and will not have direct access to SR-24. Intent was to not cut off Mountain road with SR 24 (ie a grade separation is needed)
92	5	Pg. 5-1 Draft IDCR	QUINN CASTRO, MARICOPA ASSOCIATION OF GOVERNMENTS <i>Section 5.0</i> , – Present this section as the total corridor costs only, with a breakout of a combined segment 1 and 2 together (all within Maricopa County) and only one separate segment from Meridian to Ironwood (because it's within Pinal County). This seems to	A	A	The reason for the breakout into 3 segments was if the project was only constructed to Signal Butte (based on funding) then the costs are broken out. If funding allows project to be constructed to Ironwood, then the Signal Butte to Meridian Road estimate was

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**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
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TRACS No. H8915 01L/02L
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Draft IDCR Comment Response Document

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93	6	Pg. 6-1 Draft IDCR	<i>Section 6.2</i> , – The last paragraph needs to be revised to reflect the changes above related to the estimate.	A	A	It will be revised.
94	1	General	CHUCK CHRISTIANSEN, PREMIER ENGINEERING CORP FOR PHX-MESA GATEWAY AIRPORT The PMGAA led Ellsworth Channel Relocation project recently completed a coordinated effort to obtain existing condition (without future SR-24 extension) hydrology and future condition (with future SR-24 extension) hydrology models. The results show an increase of approximately 1200 cfs in the Powerline Floodway in the future conditions model with the future SR-24 extension constructed. The increased flows affect the channel relocation. Please provide a coordinated solution to the increase with project stakeholders and/or mitigate the increase.	C	D	The interim condition will collect flows only to Ironwood Road. However, the peak flow will be in excess of the 1,200 cfs. Attenuation can not happen without an additional detention basin. The original DCR regulated the outflow to the Powerline Floodway to 1,650 cfs. The current project follows the same conditions.

the remaining portion within Maricopa County. We can combine the estimates.

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		LANCE WEBB, CITY OF MESA					
95	1	App. E - Draft Initial Drain. Report	For the offsite channel options, Parsons has only provided adequate freeboard for the Powerline Floodway for the dirt lined, not concrete lined. The concrete lined channel will require a greater freeboard since the hydraulics of the channel at this location is supercritical and 1-ft of freeboard is not adequate. This alternative needs to be modified to meet hydraulics requirements for channel design.	B	A		Powerline Floodway widening was not tabulated in Appendix E of the Draft Initial Drainage Report, but only the SR-24 offsite channel. Powerline Floodway was not included in the Draft document because the cross section and profile are being assessed and coordinated with the conceptual design work for the Ellsworth Channel Relocation, which followed the SR 24 submittal. The analysis will be included with the Initial Drainage Report.
96	2	App. F - Draft Initial Drain. Report	Should the concrete lined option be pursued, more volume will be required to attenuate flows within the outfall basin prior to passing under the existing (already constructed) crossing under the SR 24	B	A		That is correct The concrete lined option is the most likely to be pursued for the channel. Hence, the additional detention volume was evaluated, a new location for the extra volume was identified and a practical diversion solution is being devised.
97	3	App. D - Draft Initial Drain. Report	(PARSONS Note - Repeat of Comment 93/1 by Chuck Christiansen): The PMGAA project for the relocation of the Ellsworth Channel project has been coordinating with ADOT as far as the flows to expect. The results from this report for the future conditions (with future SR-24 extension) show an increase of ~1200 CFS in the Powerline Floodway for future conditions with future SR -24 extension constructed. The increased flows for the model affect how the channel can and will be relocated. Please provide a coordinated solution to mitigate this increase in flows by likely upsizing the outfall basin to accommodate this additional flow	C	D		The interim condition will collect flows only to Ironwood Road. However, the peak flow will be in excess of the 1,200 cfs. Attenuation can not happen without an additional detention basin. The original DCR regulated the outflow to the Powerline Floodway to 1,650 cfs. The current project follows the same conditions.

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		GLENN GAELICK, ADOT ROADWAY DESIGN SUPPORT					
98	1	G-2.06	Why is there 17.5 outside lane widths here vs 17' on previous crossroads?	B	D		This was from the Original DCR, no change was made to the section widths.
99	2	G-2.07	Please clarify the need for 18.5' outside lane width vs previous 17' dimension for same on other crossroads.	B	D		This was from the Original DCR, no change was made to the section widths.
100	3	C-1.01	1) Tangent Length for Curve Ref No. 800 seems excessive. Please check. 2) POT's 49 & 50 for Exst Ellsworth Cst CL do not show up on Geometric layout sheets although they seem to be called out as Pt. No's 20899 & 20909. Please clarify. 3) L & T shown for curve Ref No. 813 do not substantiate data shown on Geo Layout sheet C-2.01. Please check.	A A A	A A A		1) Will Revise to 1396.32' 2) Will revise Point numbers to match the layout sheets. 3) Will revise the Geo layout sheets
101	4	C-1.03	POT 2094 (Signal Butte) seems to be shown as 20943 of Sht C-2.06. Please clarify.	A	A		Number should be 20943
102	5	C-2.03	Suggest value in showing SR24 Med. Cst CL Sta where Section 27's south section line crosses.	A	A		Will Add

A-Will Comply
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103	6	C-3.01	1) Recommend acquisition of access control per ADOT RDG Fig 506A on both ends of Ellsworth. 2) Suggest some investigation as to feasibility of either false work or soffit fill for construction of the SR24 overpass structure. Downside of soffit fill could be differential settlement of the exst. PCCP. False work construction would need to be accommodated in proposed clearance over Ellsworth. 3) Proximity of proposed retaining wall adjacent to Ellsworth Ramp D Lt could pose construction problems. Please investigate.	C B B	A D D	1) Discussion has occurred on this subject with ADOT RW. Some development planning has occurred based on the pre-2014 RDG Access Control Requirements. We are showing the "Full Access Control" limits in the plans per ADOT R/W request. Ellsworth Rd will require a variance at the NE Quadrant, based on approved Development Plat Plans for Cadence Parkway. 2) Soffit Fill will probably not be feasible here because the interim interchange will need to remain open. False work should work, but will confirm clearances 3) Retaining wall is approx 15' at its closest point.
104	7	C-3.05	Based on plans data there may be an excessive grade difference across the gore nose at Ellsworth Ramp D. Please check.	B	A	Profile to be revised.
105	8	C-3.07	Recommend acquisition of access control per ADOT RDG Fig 506A on both ends of Williams Field.	B	A	Discussion has occurred on this subject with ADOT R/W. Some development planning has occurred based on the pre-2014 RDG Access Control Requirements. We will show Access Control (Full & Right in Right Out per the RDG Fig 506A
106	9	C-3.09 & C-03.10	Beginning profile grade seems to be missing for Ramps A & B.	A	A	Will add
107	10	C-3.11	Ramp terminus station seems to be at odds with callouts on Sht C-3.13. Please check.	A	A	Will revise

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A-Will Comply
B-Consultant To Evaluate
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D-No Further Action Required
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Consultant: **PARSONS**

108	11	C-3.13	Would there be value in extending access control north and south of Crismon per RDG due to the likelihood that the approach embankments would limit access anyway? 1) Recommend acquisition of access control per ADOT RDG Fig 506A on both ends of Signal Butte. 2) Based on plans data there may be an excessive grade difference across the gore nose at Signal Butte Ramp C. Please check.	B/C C B	A A A	Will show access control 1) Discussion has occurred on this subject with ADOT RW. Some development planning has occurred based on the pre-2014 RDG Access Control Requirements. We will show Access Control (Full & Right in Right Out per the RDG Fig 506A 2) Profile to be revised.
109	12	C-3.19	Recommend acquisition of access control per ADOT RDG Fig 506A on both ends of Signal Butte.	C	A	1) Discussion has occurred on this subject with ADOT RW. Some development planning has occurred based on the pre-2014 RDG Access Control Requirements. We will show Access Control (Full & Right in Right Out per the RDG Fig 506A. 2) Will confirm
110	13	C-3.23	Recommend acquisition of access control per ADOT RDG Fig 506A on both ends of Mountain to encompass embankment prism and to limit access to points far enough away from the crest VC to provide reasonable decision sight distance.	B/C	A	Will show access control
111	14	C-3.24	Mainline VC data is obscured on Rt end.	A	A	Will revise
112	15	C-3.27	1) Recommend extending access ctrl to comply with ADOT RDG Fig 506A on both ends of Meridian. 2) Do proposed clearances over Meridian provided by mainline profile accommodate false work construction for the SR24 overpass structure?	C B	A A	1) Discussion has occurred on this subject with ADOT RW. Some development planning has occurred based on the pre-2014 RDG Access Control Requirements. We will show Access Control (Full & Right in Right Out per the RDG Fig 506A. 2) Will confirm
113	16	C-3.31	Graphic location of Ironwood Ramp B Gore is at odds with Gore Ctrl Point callout. Please check.	A	A	Will update the plan call out.

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A-Will Comply
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Draft IDCR Comment Response Document

Client Project Manager: Ronald McCally
Consultant: **PARSONS**

114	17	C-4.07	1) Recommend extending access ctrl to comply with ADOT RDG Fig 506A. 2) Do proposed clearances over Ironwood provided by mainline profile accommodate false work construction for the SR24 overpass structure?	A	A	1) Discussion has occurred on this subject with ADOT RW. Some development planning has occurred based on the pre-2014 RDG Access Control Requirements. We will show Access Control (Full & Right in Right Out per the RDG Fig 506A. 2) Will revise.
115	18	General	Juxtaposition of interim ramps and mainline with future mainline and/or crossroad structures raises questions about construction compatibility. Cross sections would be of value in determining any serious conflicts.	B/C	D	The interim design will allow for the future ultimate construction to be compatible.

A-Will Comply
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C-ADOT To Evaluate
D-No Further Action Required

ARIZONA DEPARTMENT OF TRANSPORTATION
ROADWAY ENGINEERING GROUP
MD 615E

DESIGN REVIEW COMMENTS

SUBMITTAL:	08-22-16 SR 24 Ellsworth Rd-Ironwood Rd Final Draft DCR Submittal	PROJECT NAME:	H8915
RETURN DATE:	08-26-16	PROJECT NO.:	
REVIEWED BY:	R. Glenn Gaelick	TRACS NO. ROUTE NO. MILE POST NO.	
DISCIPLINE/OFFICE:	Roadway Design Support Section Phone No. 602-712-7039	DESIGNER/CONSULTANT:	Parsons
ADOT FAX NUMBER:	602-712-3335	ADOT PROJECT MANAGER	McCally

ACTION CODES:

A= WILL COMPLY

*B= CONSULTANT/DESIGNER TO EVALUATE

*C= ADOT TEAM TO EVALUATE

*D= DESIGN TEAM RECOMMENDS NO FURTHER ACTION

*** REQUIRES A WRITTEN EXPLANATION AND FINAL DISPOSITION BY CONSULTANT/DESIGNER**

ITEM NO.	DWG, SHT, PAGE NO.	COMMENT	DISPOSITION	
			INIT.	FINAL
		DCR		
	3-1 – 3-2 & 3-4 – 3.5	3-1 & 3-2 talk about alternatives. 3-4 & 3-5 discuss options. Suggest uniformity.	A	A
		PLANS		
	C-1.01	Repeat from IDCR Comment - L & T shown for curve Ref No. 813 do not substantiate data shown on Geo Layout sheet C-2.01. Please check.	A	A
	C-2.06	PC & PT Sta's shown for curve 823 are not substantiated by data on C-1.03.	A	A
	C-2.07	Curve 861 PT Value is unclear.	A	A
	C-3.03	Recommend a VC at Sta 8+00.	A	A
	C-3.08	Vertical data at lower left of sheet is muddled.	A	A
	C-3.23 & 3.27	Rt side ramp width for Meridian A is shown as 16'. This is not reflected in the typical. Please clarify.	A	A
	C-3.28	Tangent grade at Rt end of sheet is muddled.	A	A

MAG

DESIGN REVIEW COMMENTS

SUBMITTAL:	08-22-16 SR 24 Ellsworth Rd-Ironwood Rd Final Draft DCR Submittal	PROJECT NAME:	H8915
RETURN DATE:	10-14-2016	PROJECT NO:	
REVIEWED BY:	Chaun Hill	TRACS NO. ROUTE NO. MILE POST NO.	
DISCIPLINE/OFFICE:	MAG Phone No. 602-254-6300	DESIGNER/CONSULTANT:	Parsons
FAX NUMBER:		ADOT PROJECT MANAGER	McCally

ACTION CODES:

A= WILL COMPLY

*B= CONSULTANT/DESIGNER TO EVALUATE

*C= ADOT TEAM TO EVALUATE

*D= DESIGN TEAM RECOMMENDS NO FURTHER ACTION

*** REQUIRES A WRITTEN EXPLANATION AND FINAL DISPOSITION BY CONSULTANT/DESIGNER**

ITEM NO.	DWG, SHT, PAGE NO.	COMMENT	DISPOSITION	
			INIT.	FINAL
		DCR		
	general	Appendix A contains a full set of the Summary of Comments and there resolution as expected. The Drainage Report contains another full set of the Summary of Comments in Appendix D and there resolution <u>NOT</u> so expected. The Traffic Report contains a set of the Summary of Comments in Appendix E and, while they are specifically the Traffic Analysis comments they still represent some repetition.	A. Drainage report sealed separately. To provide record if/when the documents are separated the comments are included.	A
		The Traffic Report contains good mitigation measures that should be considered for implementation.	A Included a reference to the measures in section 2.0	A
		In the overall report on page 5-1 there is a sentence that says the SR-24 Ultimate Project was moved out of the RTPFP and it was actually moved to Phase V of the program which is unfunded. I recognize this is a minor distinction but should be clarified please. (An unfunded phase was added to Proposition 400 for the same reason.)	A updated text.	A

City of Mesa

DESIGN REVIEW COMMENTS

SUBMITTAL:	08-22-16 SR 24 Ellsworth Rd-Ironwood Rd Final Draft DCR Submittal	PROJECT NAME:	H8915
RETURN DATE:	08-23-16	PROJECT NO:	
REVIEWED BY:	Maria Deeb	TRACS NO. ROUTE NO. MILE POST NO.	
DISCIPLINE/OFFICE:	City of Mesa Phone No. 480-644-2845	DESIGNER/CONSULTANT:	Parsons
FAX NUMBER:		ADOT PROJECT MANAGER	McCally

ACTION CODES:

A= WILL COMPLY

*B= CONSULTANT/DESIGNER TO EVALUATE

*C= ADOT TEAM TO EVALUATE

*D= DESIGN TEAM RECOMMENDS NO FURTHER ACTION

*** REQUIRES A WRITTEN EXPLANATION AND FINAL DISPOSITION BY CONSULTANT/DESIGNER**

ITEM NO.	DWG, SHT, PAGE NO.	COMMENT	DISPOSITION	
			INIT.	FINAL
		DCR		
1	general	When discussing programming in the executive summary you reference a five-year Transportation Facilities Construction Program in FY 2016. Are you referencing a document starting the programming timeline in FY2015/2016? Or FY2016/2017? We at the City reference FY 2016/2017 as FY2017. Group 3 (2027-2025) should be consistent with how you are referencing the FY above.	A. Updated the paragraph to reflect ADOT input where program stands.	A

DESIGN REVIEW COMMENTS

SUBMITTAL:	SR 24 Ellsworth Rd-Ironwood Rd Phase II DCR Submittal	PROJECT NAME:	H8915 01L & 02L
RETURN DATE:	9/26/2016	PROJECT NO:	
REVIEWED BY:	Eunice Chan	TRACS NO. ROUTE NO. MILE POST NO.	
DISCIPLINE/OFFICE:	FHWA Phone No. (602) 382-8965	DESIGNER/CONSULTANT:	Parsons
FAX NUMBER:		ADOT PROJECT MANAGER	McCally

ACTION CODES:

A= WILL COMPLY

*B= CONSULTANT/DESIGNER TO EVALUATE

*C= ADOT TEAM TO EVALUATE

*D= DESIGN TEAM RECOMMENDS NO FURTHER ACTION

*** REQUIRES A WRITTEN EXPLANATION AND FINAL DISPOSITION BY CONSULTANT/DESIGNER**

ITEM NO.	DWG, SHT, PAGE NO.	COMMENT	DISPOSITION		RESPONSE
			INIT.	FINAL	
1	Previous Comment #31	Referring to response on comment 31: Check text on bullet three- last sentence appears to be cut off.	A	A	Text has been updated.
2	Previous Comment #33	Referring to response on comment 33: Has not been updated.	A	A	Speed limit was added.
3	Previous Comment #34	Referring to response on comment 34: The second half of both paragraphs are still identical (Opt A and B). Clarify purpose of repeating this information under two separate headings on the same page?	A	A	The intent was that it was different section of the report and the description was added to each one separately. The sections ended up being on the same page.

DESIGN REVIEW COMMENTS
(CONTINUED)
ROADWAY ENGINEERING GROUP

ITEM NO.	DWG, SHT, PAGE NO.	COMMENT	DISPOSITION		RESPONSE
			INIT.	FINAL	
4	Previous Comment #35	Referring to response "b." on comment 35: Did not see this additional discussion in either the Table 5 or Table 6 section.	A	A	Text was added.
5	Previous Comment #38	Referring to response on comment 38: I don't think this was updated?	A	A	Text was added.
6	Previous Comment #41	Referring to response "a." on comment 41: Include this explanation under paragraph 3.2.	A	A	Updated comment response text to section.
7	Previous Comment #42	Referring to response "a." on comment 42: Include this explanation in the IDCR	A	A	Added comment response text to section.
8	Previous Comment #43	Referring to response "a." on comment 43: How is this statement (highlighted) supported then? Traffic analysis section pg 3-2 clarify "event horizon"	A	A	Additional text included in DCR. Also added text to 3.3.4 Traffic analysis to discuss lanes.

ADOT

DESIGN REVIEW COMMENTS

SUBMITTAL:	SR 24 Ellsworth Rd-Ironwood Rd Phase II DCR Submittal	PROJECT NAME:	H8915 01L & 02L
RETURN DATE:	9/8/2016	PROJECT NO:	
REVIEWED BY:	Tammy R. Mivshek	TRACS NO. ROUTE NO. MILE POST NO.	
DISCIPLINE/OFFICE:	ADOT Infrastructure Delivery and Operations Division Phone No. 602-712-7220	DESIGNER/CONSULTANT:	Parsons
FAX NUMBER:		ADOT PROJECT MANAGER	McCally

ACTION CODES:

A= WILL COMPLY

*B= CONSULTANT/DESIGNER TO EVALUATE

*C= ADOT TEAM TO EVALUATE

*D= DESIGN TEAM RECOMMENDS NO FURTHER ACTION

*** REQUIRES A WRITTEN EXPLANATION AND FINAL DISPOSITION BY CONSULTANT/DESIGNER**

ITEM NO.	DWG, SHT, PAGE NO.	COMMENT	DISPOSITION		RESPONSE
			INIT.	FINAL	
1	Signing & Striping	DCR On the signing and striping sheets, why are there "exit only" panels on the overhead signs considering the fact that all traffic must essentially exit at each TL. I don't want traffic thinking that there is a through situation when they all have to exit along the ramps and be placed into a stop situation at the intersections	A	A	We will leave sign as shown and modify to show two down green arrows.

**DESIGN REVIEW COMMENTS
(CONTINUED)
ROADWAY ENGINEERING GROUP**

ITEM NO.	DWG, SHT, PAGE NO.	COMMENT	DISPOSITION		RESPONSE
			INIT.	FINAL	
2	Signing & Striping	The required wrong way signing is not showing on the plans set. Wrong way signing must be incorporated into the project. Replace the lane assignment signs at the intersections (the only ones I saw are at Ellsworth) with the Wrong Way signing on the off ramps. This should not be depicted by a note on the plans.	A	A	We are at the DCR phase. During final design the note would come off and intersection wrong way signing would be shown. Quantities reflect the higher sign square footage, posts, and foundations.
3	Signing & Striping	The wrong way signing that is supposed to be placed on the overhead structures on the ramps is not being shown. This should not be depicted by a note on the plans.	A	A	We are at the DCR phase. During final design the note would come off and intersection wrong way signing would be shown. Quantities reflect the higher sign square footage, posts, and foundations.
4	Signing & Striping	All one way signing (R6-1) on roadways that have multiple lanes, the size of the sign shall be 54" x 18" per the MUTCD, per the plans these are shown as 36" x 12".	A	A	Will revise
5	Signing & Striping	The exit gore ground mounted signs are not depicted correctly per ADOT standards. They should be using the E5-1c narrow exit gore signs.	A	A	Will revise
6	Signing & Striping	The W3-3 panels are placed at 1000 ft. before the intersection. Why is Table 2C-4 of the Arizona Supplement to the MUTCD or the MUTCD distances not followed regarding the placement of warning signs?	A	A	Will review and revise accordingly.
7	Signal Plan	On Dwg. No. T-3.05, why is there a need for a mast arm and pole crossing over the on-ramp in the westbound direction since SR 24 ends at Ironwood?	A	A	The callout denotes that it is for the future. Shown to denote that it will fit for the future.

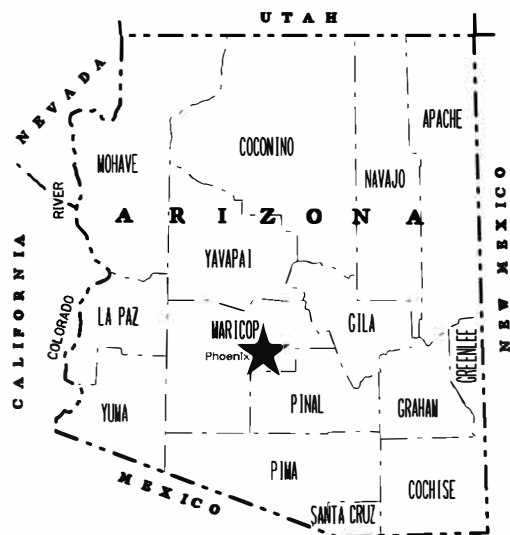
**DESIGN REVIEW COMMENTS
(CONTINUED)
ROADWAY ENGINEERING GROUP**

ITEM NO.	DWG. SHT, PAGE NO.	COMMENT	DISPOSITION INIT.	DISPOSITION FINAL	RESPONSE
8	DCR	On Page 4-8, it states that "Interim lighting and traffic signal plans <u>are</u> included in Appendix C."	A	A	We will add "area" as noted.
9	DCR	It states on Page 4-9, second line Part VI of the Manual of Uniform Traffic Control Devices (MUTCD), 2003 Version. . . , we go by the 2009 version. This needs to be updated to 2009.	A	A	We will update.

**FINAL DESIGN CONCEPT REPORT
SR-24, Ellsworth Road to Ironwood Drive
Interim Phase II**

APPENDIX B

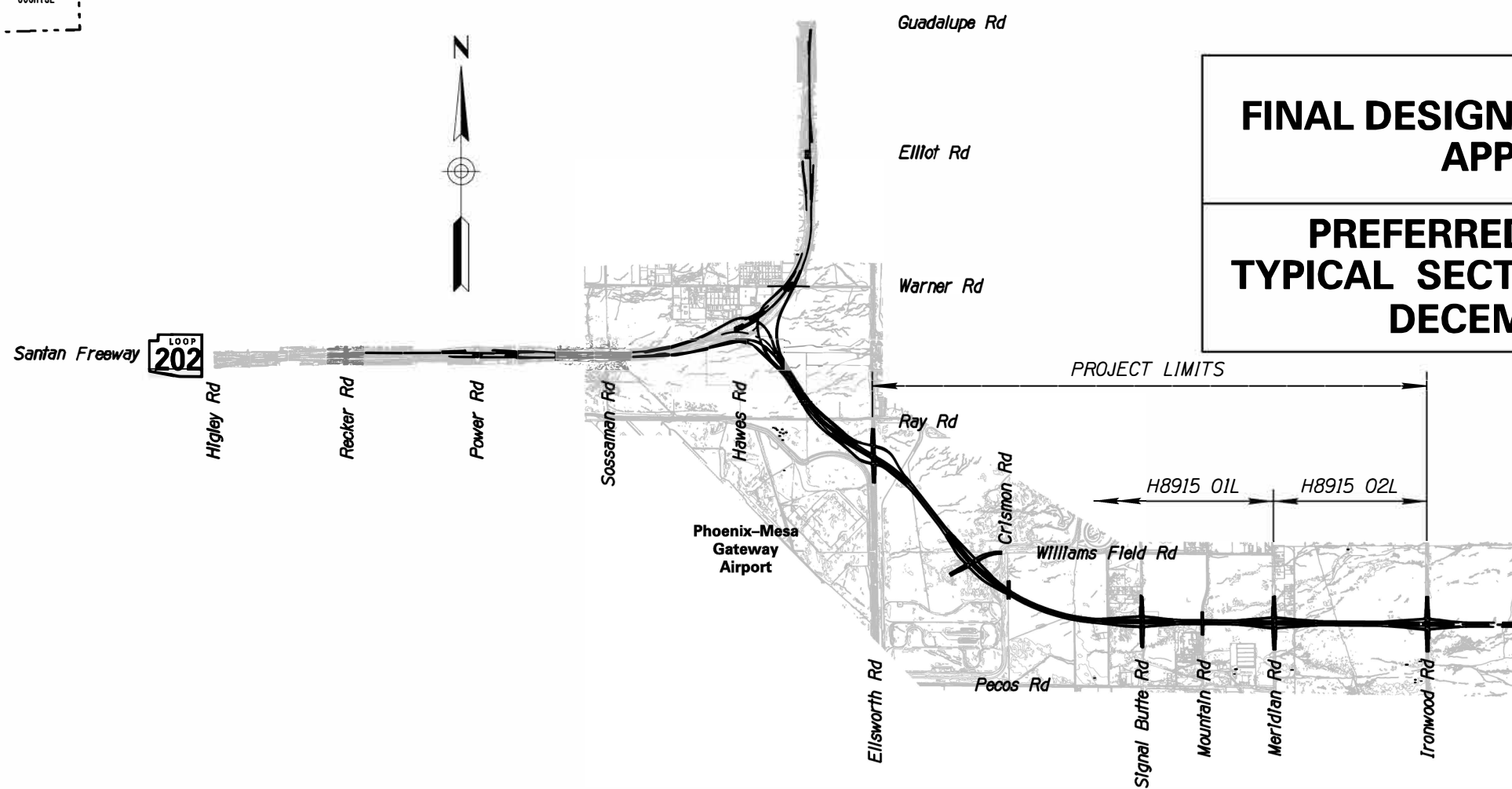
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STATE OF ARIZONA
 DEPARTMENT OF TRANSPORTATION
 INTERMODAL TRANSPORTATION DIVISION
 PROJECT PLANS



STATE HIGHWAY
 SR 24, GATEWAY FREEWAY
 024 MA 001



**FINAL DESIGN CONCEPT REPORT
 APPENDIX C**

**PREFERRED ALTERNATIVE
 TYPICAL SECTIONS AND PLANS
 DECEMBER, 2016**

24 Gateway Freeway

**SR 24, GATEWAY FREEWAY
 INTERIM PHASE 2
 ELLSWORTH ROAD TO IRONWOOD ROAD
 PROJECT NO. 024 MA 001 H8915 01L/02L
 CONTRACT NO. 2014-006.14**

ARIZONA DEPARTMENT OF TRANSPORTATION
 INTERMODAL TRANSPORTATION DIVISION
 DALLAS HAMMIT, P.E., STATE ENGINEER

AS BUILT DATA	AS BUILT DATE	OF
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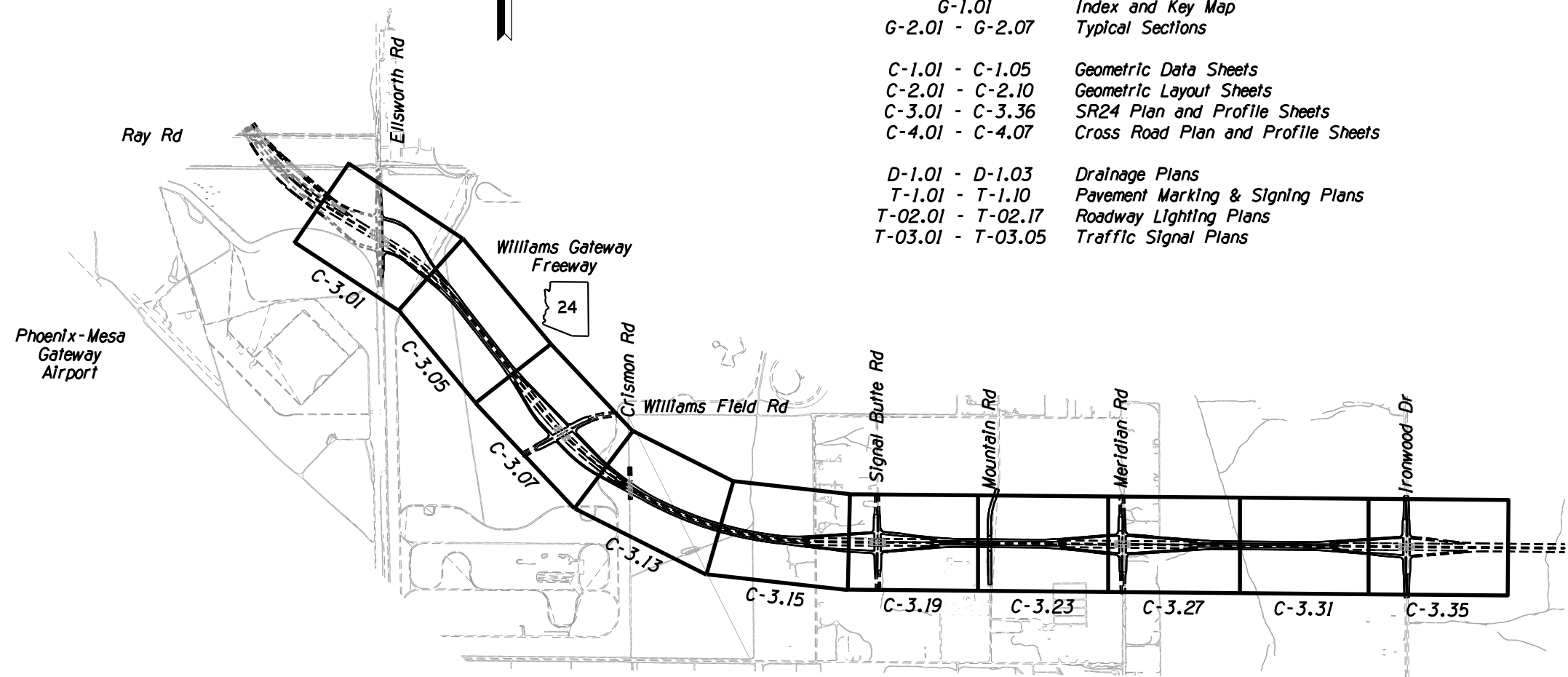
F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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INDEX OF SHEETS

Sheet No.	Sheet Type
	<i>Cover Sheet</i>
G-1.01	<i>Index and Key Map</i>
G-2.01 - G-2.07	<i>Typical Sections</i>
C-1.01 - C-1.05	<i>Geometric Data Sheets</i>
C-2.01 - C-2.10	<i>Geometric Layout Sheets</i>
C-3.01 - C-3.36	<i>SR24 Plan and Profile Sheets</i>
C-4.01 - C-4.07	<i>Cross Road Plan and Profile Sheets</i>
D-1.01 - D-1.03	<i>Drainage Plans</i>
T-1.01 - T-1.10	<i>Pavement Marking & Signing Plans</i>
T-02.01 - T-02.17	<i>Roadway Lighting Plans</i>
T-03.01 - T-03.05	<i>Traffic Signal Plans</i>



Access Control Legend (See Roadway Plans for Location)

- Right-In-Right-out Access Control only
- Full Access Control

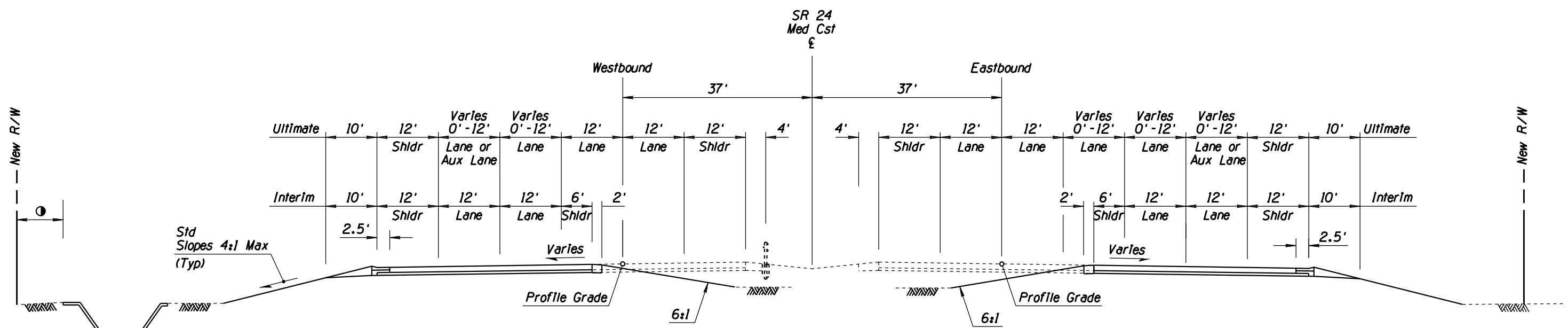
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SR 24 SHEET INDEX AND KEY MAP	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. G-1.01
TRACS NO. H8915 OIL/02L				OF

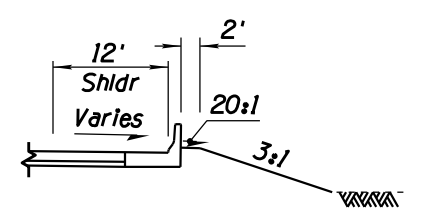
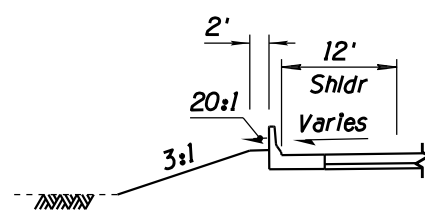
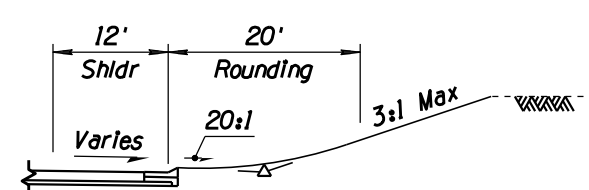
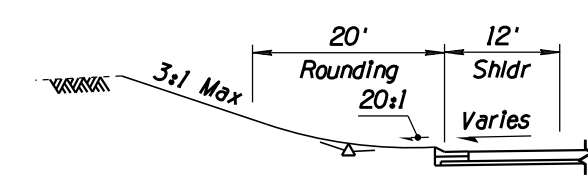
SURVEY NO. FINISHED PLANS DATE REVISIONS LOCATION DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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TYPICAL SECTION
Interim SR 24



① Area for Future City of Mesa Shared use Pathway

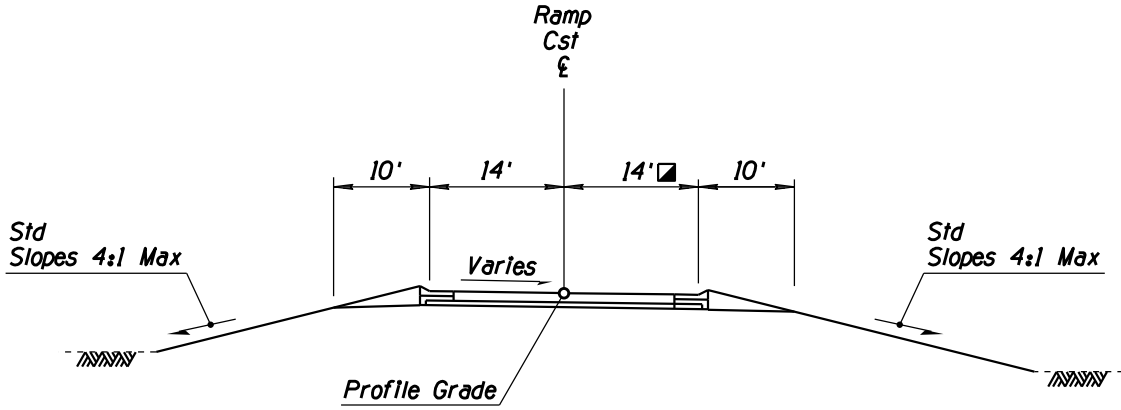
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DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			INTERIM SR 24 MAINLINE DESIGN SHEET TYPICAL SECTIONS	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. G-2.01
TRACS NO. H8915 OIL/02L				OF

SURVEY NO. FINISHED PLANS DATE LOCATION REVISIONS DATE SURVEY NO. FINISHED PLANS DATE LOCATION REVISIONS DATE SURVEY NO. FINISHED PLANS DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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TYPICAL EMBANKMENT SECTION

2-Lane Entrance & Exit Ramp
With Direction of Travel

■ 20' at Williams Field Ramp B

*Note: In the interim condition, Exit Ramps will be striped as 2 lane exits.
In the future ultimate condition, Exit Ramps will be re-striped as 1 lane exit ramps, except at Williams Field Ramp B and at any End of Freeway Exit Ramps.*

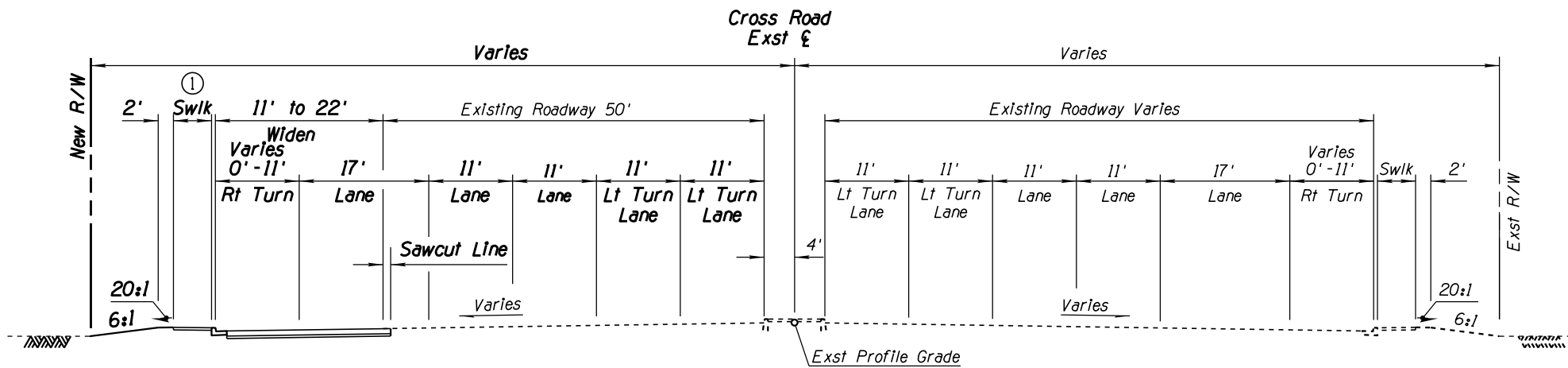
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DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SERVICE INTERCHANGE RAMPS DESIGN SHEET TYPICAL SECTIONS	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. G-2.02
TRACS NO. H8915 OIL/O2L				OF

DATE - LOCATION - REVISIONS - FINISHED PLANS - SURVEY NO. DATE - LOCATION - REVISIONS - FINISHED PLANS - SURVEY NO.

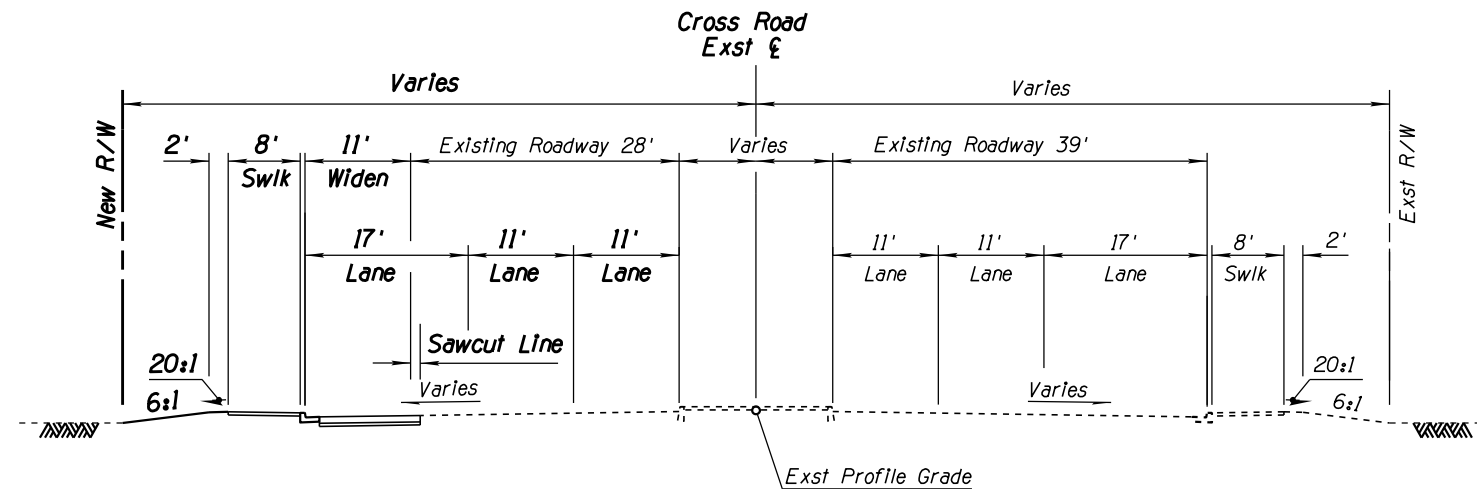
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TYPICAL SECTION
At Full Diamond Traffic Interchange
Ellsworth Road

- ① Sidewalk Width 6' Between Ramp Intersections
Sidewalk Width 8' Outside of Ramp Intersections



TYPICAL SECTION
Away From Traffic Interchange
Ellsworth Road

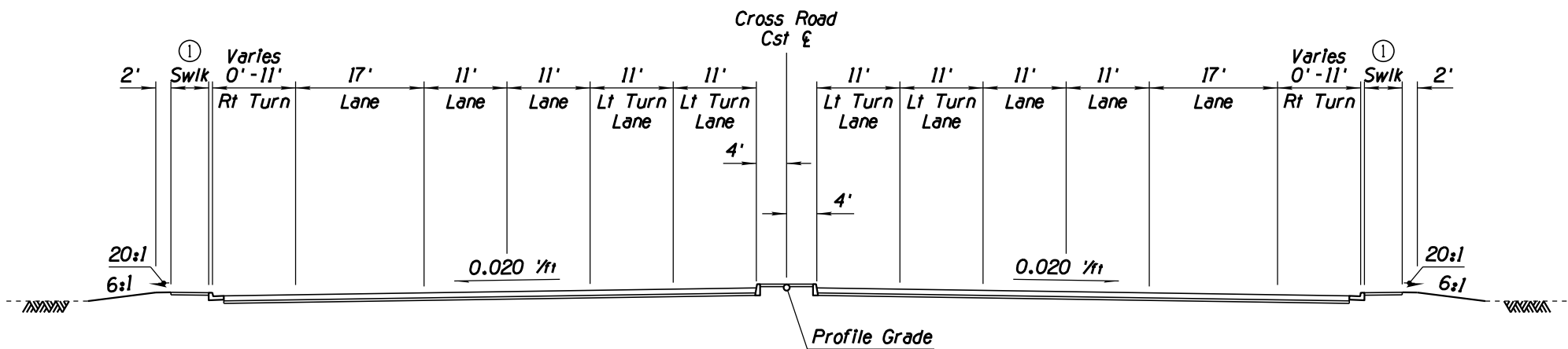
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CHECKED	S. MUELLER	05/16		
PARSONS			CROSSROADS DESIGN SHEET TYPICAL SECTIONS	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. G-2.03
TRACS NO. H8915 OIL/O2L				OF

DATE- LOCATION- REVISIONS- FINISHED PLANS- SURVEY NO. DATE- LOCATION- REVISIONS- FINISHED PLANS- SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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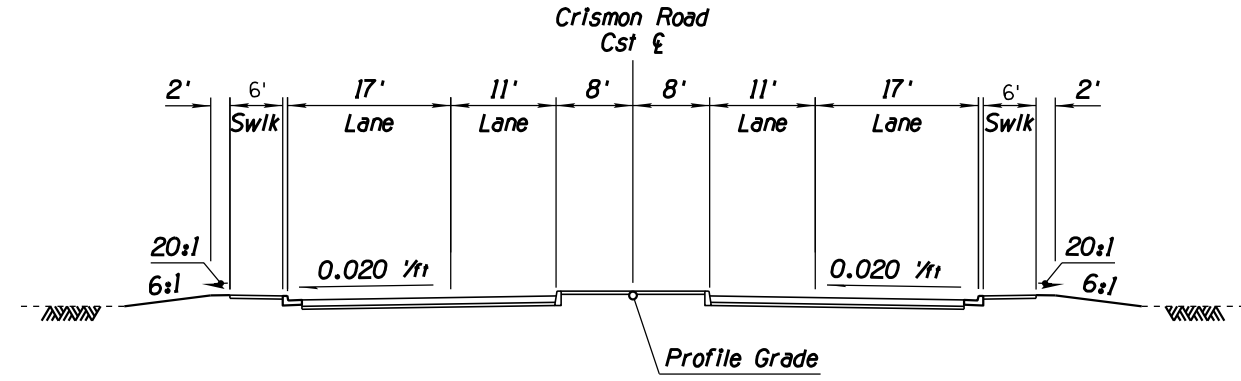
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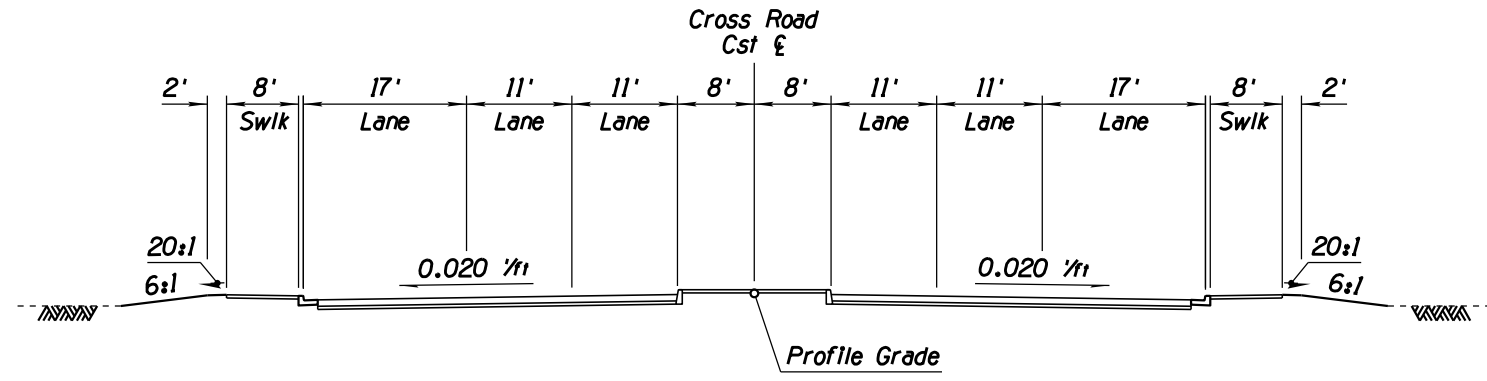
TYPICAL SECTION
At Full Diamond Traffic Interchange

Williams Field Road

- ① Sidewalk Width 5' Between Ramp Intersections
- Sidewalk Width 8' Outside of Ramp Intersections



TYPICAL SECTION
Future Crismon Road



TYPICAL SECTION
Away From Traffic Interchange
Williams Field Road

NOTE: Ultimate Striping Shown
See Pavement Marking and Signing
Plans for Interim Condition.

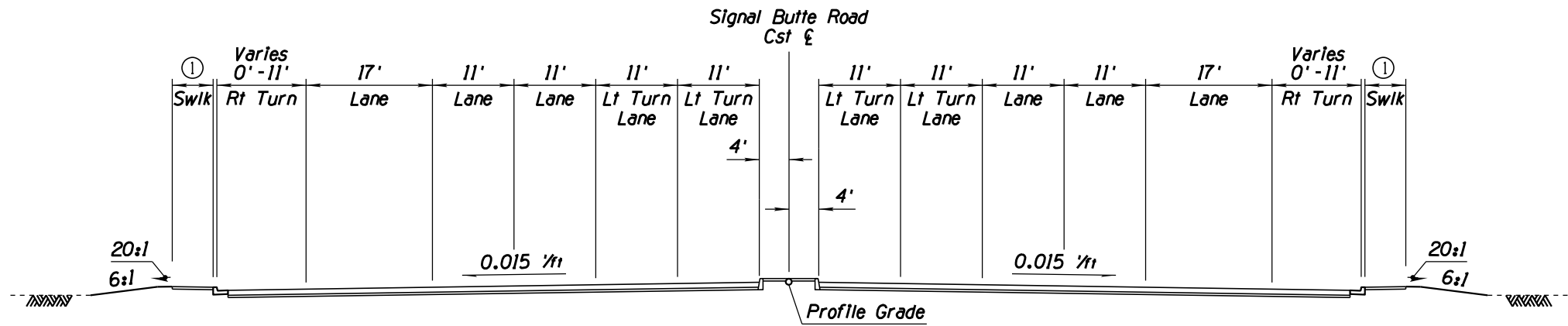
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DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			CROSSROADS DESIGN SHEET TYPICAL SECTIONS	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. G-2.04
TRACS NO. H8915 OIL/02L				OF

DATE: LOCATION: REVISIONS: FINISHED PLANS: SURVEY NO. DATE: LOCATION: REVISIONS: FINISHED PLANS: SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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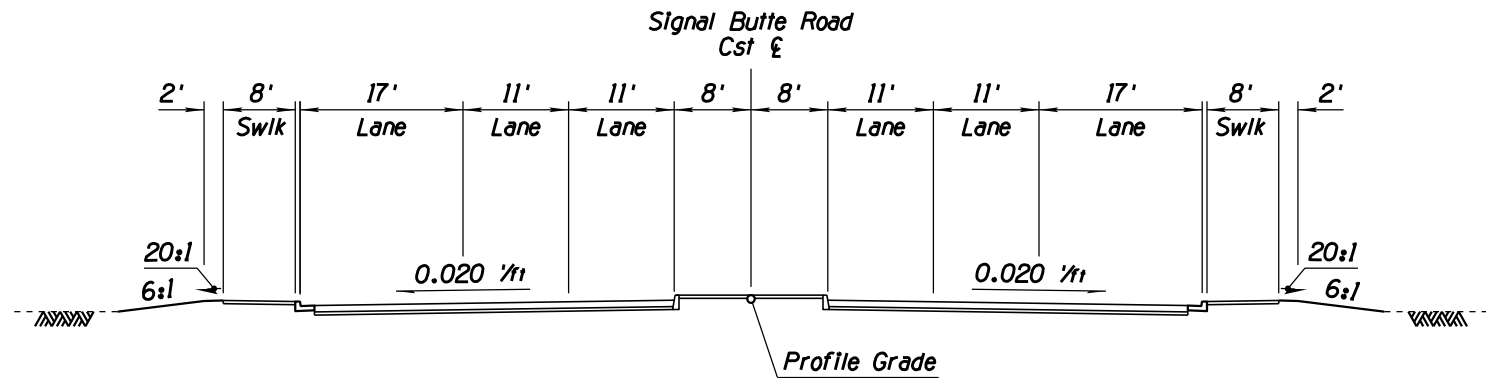


TYPICAL SECTION

At Full Diamond Traffic Interchange

Signal Butte Road

- ① Sidewalk Width 6' Between Ramp Intersections
- Sidewalk Width 8' Outside of Ramp Intersections



TYPICAL SECTION

Away From Traffic Interchange

Signal Butte Road

NOTE: Ultimate Striping Shown
See Pavement Marking and Signing
Plans for Interim Condition.

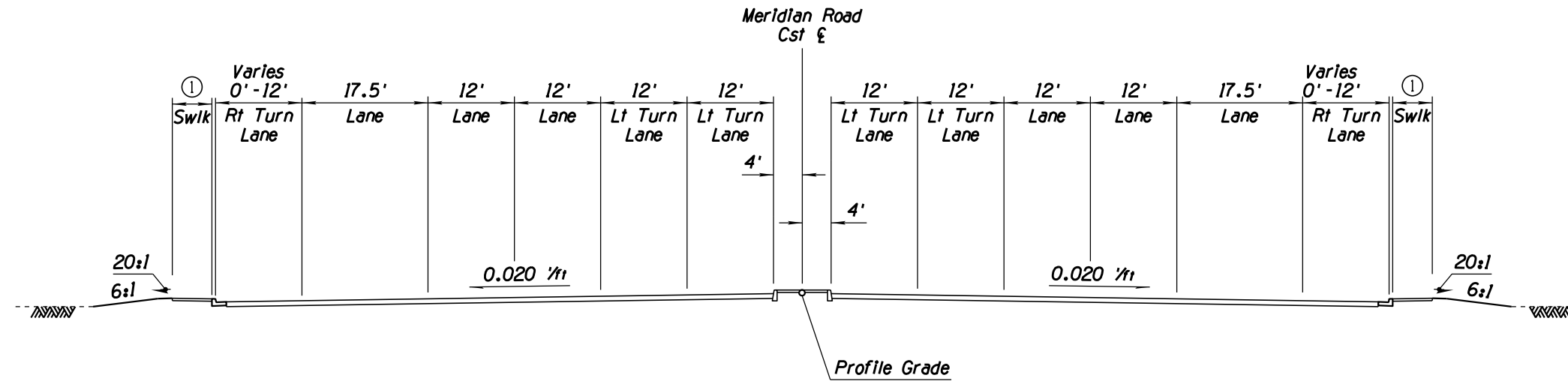
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CHECKED	S. MUELLER	05/16		
PARSONS			CROSSROADS DESIGN SHEET TYPICAL SECTIONS	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. G-2.05
TRACS NO. H8915 OIL/O2L				OF

DATE: LOCATION: REVISIONS: FINISHED PLANS: SURVEY NO. DATE: LOCATION: REVISIONS: FINISHED PLANS: SURVEY NO. DATE: LOCATION: REVISIONS: FINISHED PLANS: SURVEY NO.

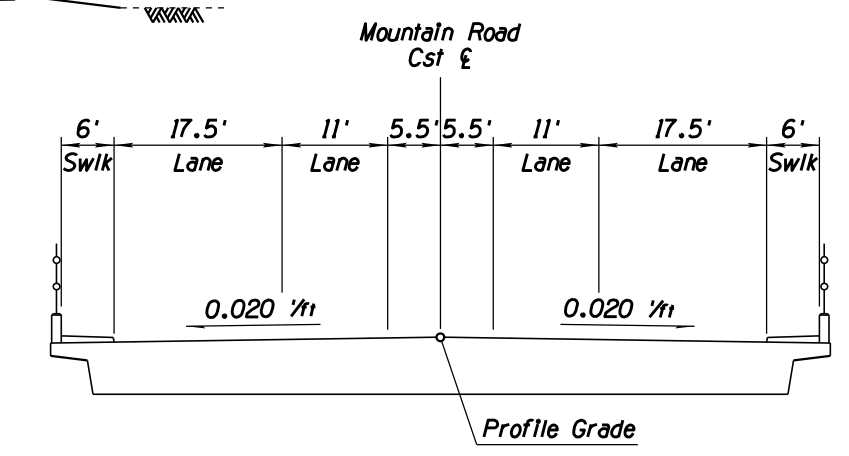
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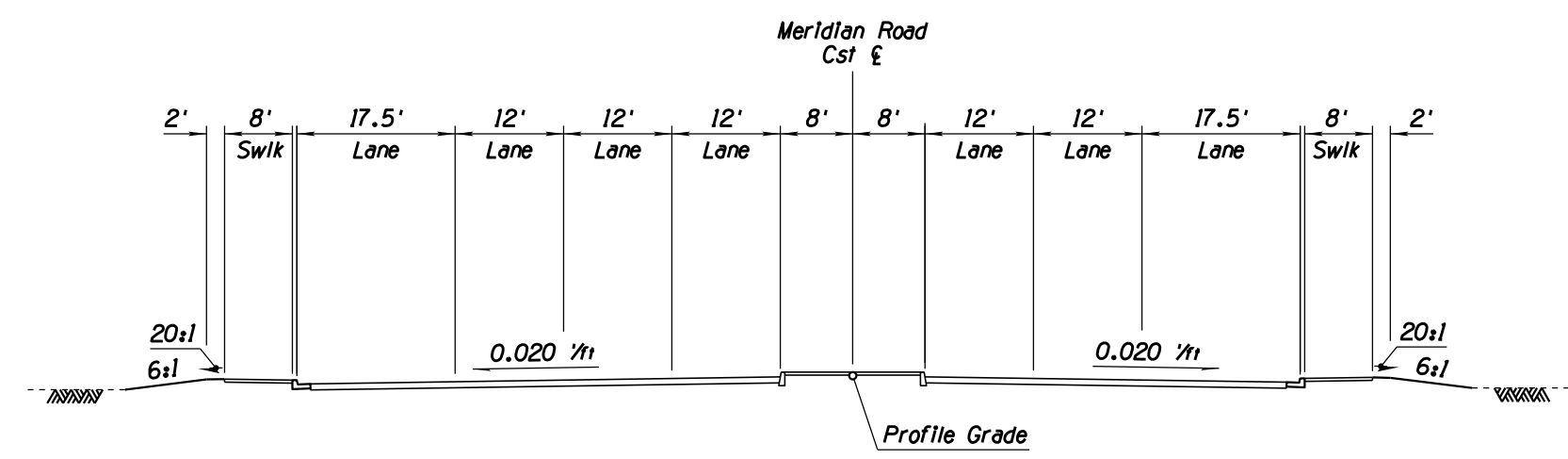


TYPICAL SECTION
At Full Diamond Traffic Interchange
Meridian Road

- ① Sidewalk Width 6' Between Ramp Intersections
- Sidewalk Width 8' Outside of Ramp Intersections



TYPICAL SECTION
At Freeway Crossing
Mountain Road



TYPICAL SECTION
Away From Traffic Interchange
Meridian Road

NOTE: Ultimate Striping Shown
See Pavement Marking and Signing
Plans for Interim Condition.

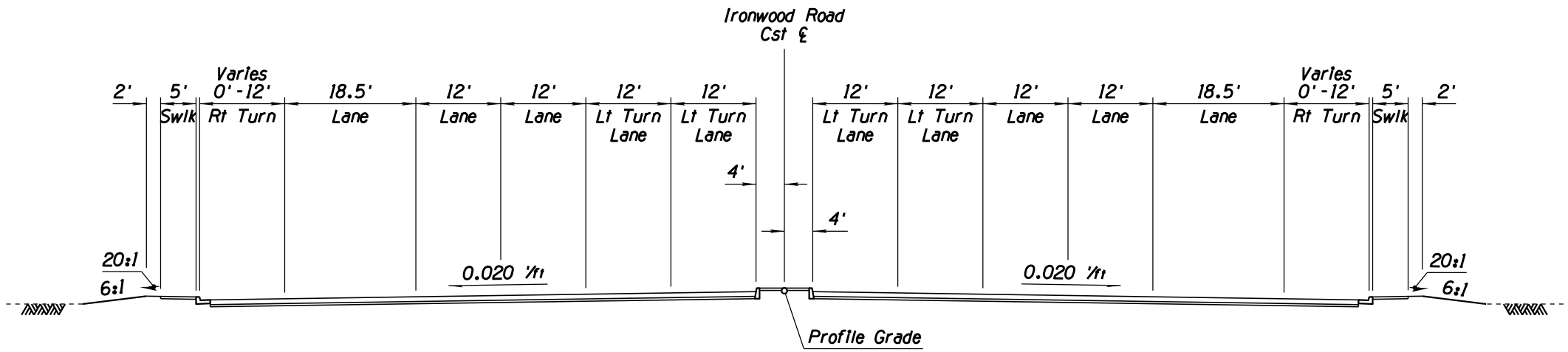
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CHECKED	S. MUELLER	05/16		
PARSONS			CROSSROADS DESIGN SHEET TYPICAL SECTIONS	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. G-2.06
TRACS NO. H8915 OIL/02L				OF

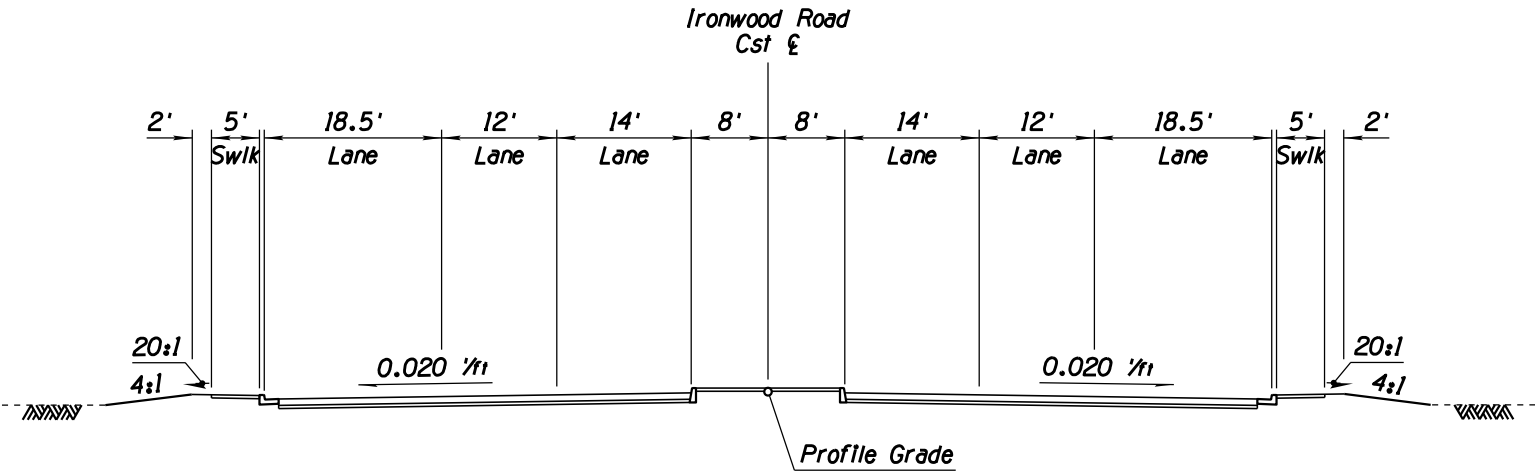
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F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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TYPICAL SECTION
At Full Diamond Traffic Interchange
Ironwood Road



TYPICAL SECTION
Away From Traffic Interchange
Ironwood Road

NOTE: Ultimate Striping Shown
See Pavement Marking and Signing
Plans for Interim Condition.

APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			DESIGN SHEET TYPICAL SECTIONS	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. G-2.07
TRACS NO. H8915 OIL/O2L				OF

SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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PLAN REF NO	LOCATION	P.I./P.O.T. STATION	COORDINATES		All Coordinates Are Ground Coordinates And All Bearings Are Grid Bearings								G.A.F. = 1.00016
	SR24 Med Cst ξ												
50020	POT	10+00.00	N=846791.245	E=782407.226									
800	PI	38+01.00	N=844408.657	E=783879.937	SIMPLE	$\Delta=27^{\circ}23'33''$	D=1^{\circ}00'00"	R=5729.58'	T=1396.32'	L=2739.25'	Ext=167.69'	e=0.030%	SEE SUPERELEVATION DIAGRAM
801	PI	75+62.62	N=842450.250	E=787153.924	SIMPLE	$\Delta=21^{\circ}06'47''$	D=1^{\circ}00'00"	R=5729.58'	T=1067.77'	L=2111.32'	Ext=98.65'	e=0.030%	SEE SUPERELEVATION DIAGRAM
802	PI	149+05.58	N=836644.843	E=791689.628	SIMPLE	$\Delta=51^{\circ}30'12''$	D=0^{\circ}45'00"	R=7639.44'	T=3685.10'	L=6867.10'	Ext=842.36'	e=0.023%	SEE SUPERELEVATION DIAGRAM
50031	POT	341+91.40	N=836473.327	E=811477.788									
	Existing Ellsworth Rd Cst ξ												
20899	POT	4+73.67	N=844651.332	E=785995.755									
50101	POT	20+00.00	N=843125.295	E=786025.412									
20909	POT	31+02.00	N=842023.502	E=786046.823									
	Existing Ellsworth Rd Ramp 'A' Cst ξ												
60100	PC	0+00.00	N=844928.799	E=783707.902									
810	PI	4+62.85	N=844576.753	E=784008.388	SIMPLE	$\Delta=12^{\circ}40'35''$	D=1^{\circ}22'30"	R=4166.97'	T=462.85'	L=921.92'	Ext=25.63'	e=0.030%	
811	PI	17+16.18	N=843822.987	E=785014.446	SIMPLE	$\Delta=22^{\circ}57'17''$	D=5^{\circ}00'00"	R=1145.92'	T=232.67'	L=459.10'	Ext=23.38'	e=0.056%	
60110	POT	27+42.33	N=843575.210	E=786016.668									
	Existing Ellsworth Rd Ramp 'B' Cst ξ												
60201	PC	0+00.00	N=844457.873	E=783964.982									
812	PI	2+77.31	N=844250.738	E=784149.364	SIMPLE	$\Delta=5^{\circ}28'20''$	D=0^{\circ}59'15"	R=5802.58'	T=277.31'	L=554.20'	Ext=6.62'	e=0.030%	
813	PI	21+31.64	N=842989.273	E=785509.065	SIMPLE	$\Delta=28^{\circ}58'01''$	D=6^{\circ}00'00"	R=954.93'	T=246.67'	L=482.78'	Ext=31.34'	e=0.055%	
60207	POT	26+58.27	N=842860.345	E=786030.561									
	Ellsworth Rd Ramp 'C' Cst ξ												
60300	POT	0+00.00	N=843575.210	E=786016.668									
814	PI	6+56.34	N=843417.687	E=786653.824	SIMPLE	$\Delta=46^{\circ}06'04''$	D=6^{\circ}00'00"	R=954.93'	T=406.34'	L=768.35'	Ext=82.86'	e=0.059%	SEE SUPERELEVATION DIAGRAM
815	PI	16+42.69	N=842525.206	E=787169.350	SIMPLE	$\Delta=9^{\circ}59'12''$	D=2^{\circ}00'00"	R=2864.79'	T=250.30'	L=499.34'	Ext=10.91'	e=0.035%	SEE SUPERELEVATION DIAGRAM
816	PI	24+01.88	N=841942.652	E=787658.153	SIMPLE	$\Delta=4^{\circ}56'14''$	D=0^{\circ}59'15"	R=5802.58'	T=250.16'	L=500.00'	Ext=5.39'	e=0.030%	SEE SUPERELEVATION DIAGRAM
60309	PT	26+51.72	N=841737.892	E=787801.857									
	Ellsworth Rd Ramp 'D' Cst ξ												
60400	POT	0+00.00	N=842860.345	E=786030.561									
817	PI	3+84.81	N=842767.989	E=786404.125	SIMPLE	$\Delta=25^{\circ}07'28''$	D=6^{\circ}30'00"	R=881.47'	T=196.42'	L=386.53'	Ext=21.62'	e=0.060%	SEE SUPERELEVATION DIAGRAM
818	PI	17+58.76	N=841899.151	E=787476.626	SIMPLE	$\Delta=12^{\circ}59'20''$	D=1^{\circ}30'00"	R=3819.72'	T=434.82'	L=865.92'	Ext=24.67'	e=0.032%	SEE SUPERELEVATION DIAGRAM
60406	PT	21+89.86	N=841556.506	E=787744.330									

CURVE DATA TABLE

APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			GEOMETRIC DATA SHEET	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-1.01
TRACS NO. H8915 OIL/O2L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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PLAN REF NO	LOCATION	P.I./P.O.T. STATION	COORDINATES		All Coordinates Are Ground Coordinates And All Bearings Are Grid Bearings								G.A.F. = 1.00016
Williams Field Rd Cst &													
61000	PC	7+33.80	N=839352.449	E=791126.718									
820	PI	11+65.52	N=839356.323	E=790695.010	SIMPLE	Δ=29°32'53"	D=3°30'00"	R=1637.02'	T=431.73'	L=844.23'	Ext=55.97'	e=0.020%/	SEE SUPERELEVATION DIAGRAM
50061	POT	20+00.00	N=838941.998	E=789948.593									
821	PI	35+61.58	N=838184.121	E=788583.256	SIMPLE	Δ=39°02'02"	D=3°30'00"	R=1637.02'	T=580.25'	L=1115.26'	Ext=99.79'	e=0.020%/	SEE SUPERELEVATION DIAGRAM
61005	PT	40+96.59	N=838284.880	E=788011.825									
Williams Field Rd Ramp 'A' Cst &													
61100	PC	0+00.00	N=840552.854	E=788728.979									
822	PI	3+62.36	N=840267.307	E=788952.073	SIMPLE	Δ=6°02'02"	D=0°50'00"	R=6875.49'	T=362.36'	L=724.06'	Ext=9.54'	e=0.020%/	SEE SUPERELEVATION DIAGRAM
61110	POT	20+62.03	N=839044.887	E=790133.951									
Williams Field Rd Ramp 'B' Cst &													
61201	PC	0+00.00	N=840654.668	E=788464.155									
823	PI	5+16.96	N=840247.297	E=788782.430	SIMPLE	Δ=7°23'58"	D=0°43'00"	R=7994.76'	T=516.96'	L=1032.49'	Ext=16.70'	e=0.020%/	SEE SUPERELEVATION DIAGRAM
824	PI	16+43.71	N=839276.231	E=789356.731	SIMPLE	Δ=13°26'00"	D=3°00'00"	R=1909.86'	T=224.92'	L=447.78'	Ext=13.20'	e=0.044%/	SEE SUPERELEVATION DIAGRAM
61210	POT	22+41.56	N=838844.932	E=789773.726									
Williams Field Rd Ramp 'C' Cst &													
61300	POT	0+00.00	N=839039.064	E=790123.459									
825	PI	16+55.45	N=837848.912	E=791274.139	SIMPLE	Δ=20°50'28"	D=1°00'00"	R=5729.58'	T=1053.70'	L=2084.12'	Ext=96.09'	e=0.027%/	SEE SUPERELEVATION DIAGRAM
61303	PT	26+85.87	N=837401.518	E=792228.145									
Williams Field Rd Ramp 'D' Cst &													
61400	POT	0+00.00	N=838839.108	E=789763.234									
826	PI	8+18.09	N=838250.963	E=790331.874	SIMPLE	Δ=17°26'15"	D=2°00'00"	R=2864.79'	T=439.33'	L=871.88'	Ext=33.49'	e=0.035%/	SEE SUPERELEVATION DIAGRAM
61404	POT	24+33.79	N=837476.065	E=791757.366									
Crismon Rd Cst &													
20921	POT	4+16.35	N=839350.140	E=791384.176									
50062	PI	20+00.00	N=837766.605	E=791403.477									
20930	POT	30+48.10	N=836718.583	E=791416.250									
Signal Butte Rd Cst &													
20923	POT	-7+11.87	N=839312.901	E=796683.786									

CURVE DATA TABLE

APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			GEOMETRIC DATA SHEET	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	LOCATION	ELLSWORTH RD TO IRONWOOD DR		DWG NO. C-1.02
SR 24				
TRACS NO. H8915 OIL/02L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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PLAN REF NO	LOCATION	P.I./P.O.T. STATION	COORDINATES	All Coordinates Are Ground Coordinates And All Bearings Are Grid Bearings								G.A.F. = 1.00016	
20931	PI	19+25.00	N=836676.256 E=796717.965										
50006	POT	20+00.00	N=836601.256 E=796718.270										
20943	POT	45+76.79	N=834024.492 E=796728.777										
	Signal Butte Rd Ramp 'A' Cst &												
63100	PC	0+00.00	N=836734.938 E=794578.268										
830	PI	3+43.87	N=836695.739 E=794919.894	SIMPLE	Δ=10°17'18"	D=1°30'00"	R=3819.72'	T=343.87'	L=685.89'	Ext=15.45'	e=0.032%/	SEE SUPERELEVATION DIAGRAM	
63110	POT	21+42.15	N=836813.244 E=796716.189										
	Signal Butte Rd Ramp 'B' Cst &												
63201	POT	0+00.00	N=836591.755 E=794545.524										
831	PI	14+31.73	N=836425.557 E=795967.572	SIMPLE	Δ=3°53'59"	D=0°45'00"	R=7639.44'	T=260.08'	L=519.95'	Ext=4.43'	e=0.020%/	SEE SUPERELEVATION DIAGRAM	
63210	POT	21+83.34	N=836389.272 E=796718.507										
	Signal Butte Rd Ramp 'C' Cst &												
63300	POT	0+00.00	N=836813.244 E=796716.189										
832	PI	15+10.46	N=836661.252 E=798218.983	SIMPLE	Δ=5°16'43"	D=0°43'00"	R=7994.76'	T=368.54'	L=736.56'	Ext=8.49'	e=0.020%/	SEE SUPERELEVATION DIAGRAM	
63303	PT	18+78.48	N=836658.057 E=798587.508										
	Signal Butte Rd Ramp 'D' Cst &												
63400	POT	0+00.00	N=836389.258 E=796719.135										
833	PI	15+04.06	N=836515.255 E=798217.911	SIMPLE	Δ=5°18'07"	D=0°50'00"	R=6875.49'	T=318.35'	L=636.24'	Ext=7.37'	e=0.020%/	SEE SUPERELEVATION DIAGRAM	
63403	PT	18+21.95	N=836512.496 E=798536.245										
	Exst Mountain Rd Cst &												
63500	PC	4+61.79	N=838092.016 E=799329.444										
850	PI	7+21.40	N=837832.415 E=799331.876	SIMPLE	Δ=20°32'46"	D=4°00'00"	R=1432.39'	T=259.61'	L=513.65'	Ext=23.34'	e=0.036%/	SEE SUPERELEVATION DIAGRAM	
851	PI	13+40.53	N=837245.418 E=799118.118	SIMPLE	Δ=20°32'36"	D=4°00'00"	R=1432.39'	T=259.61'	L=513.65'	Ext=23.34'	e=0.036%/	SEE SUPERELEVATION DIAGRAM	
63550	POT	20+00.00	N=836580.402 E=799124.348										
63506	POT	45+72.81	N=834007.704 E=799148.451										
	Mountain Rd Cst &												
63510	POC	8+12.11	N=837744.794 E=799290.069										
850	PI	7+21.40	N=837832.415 E=799331.876	SIMPLE	Δ=20°32'46"	D=4°00'00"	R=1432.39'	T=259.61'	L=513.65'	Ext=23.34'	e=0.036%/	SEE SUPERELEVATION DIAGRAM	
851	PI	13+40.53	N=837245.418 E=799118.118	SIMPLE	Δ=20°32'36"	D=4°00'00"	R=1432.39'	T=259.61'	L=513.65'	Ext=23.34'	e=0.036%/	SEE SUPERELEVATION DIAGRAM	
63550	PI	20+00.00	N=836580.402 E=799124.348										

CURVE DATA TABLE

APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			GEOMETRIC DATA SHEET	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	LOCATION	ELLSWORTH RD TO IRONWOOD DR		DWG NO. C-1.03
TRACS NO. H8915 OIL/02L				OF

DATE LOCATION REVISIONS FINISHED PLANS SURVEY NO. DATE LOCATION REVISIONS FINISHED PLANS SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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PLAN REF NO	LOCATION	P.I./P.O.T. STATION	COORDINATES	All Coordinates Are Ground Coordinates And All Bearings Are Grid Bearings								G.A.F. = 1.00016	
63511	POT	28+87.90	N=835692.541 E=799132.666										
	Meridian Rd Cst ξ												
20925	POT	-7+19.05	N=839274.553 E=801948.175										
22579	PI	15+61.92	N=836993.715 E=801973.312										
20932	PI	19+25.00	N=836630.662 E=801977.313										
50007	POT	20+00.00	N=836555.666 E=801978.145										
22580	PI	41+99.39	N=834356.413 E=802002.538										
	Meridian Rd Ramp 'A' Cst ξ												
64100	PC	0+00.00	N=836645.057 E=800087.452										
860	PI	3+00.49	N=836642.452 E=800387.928	SIMPLE	Δ=5°00'18"	D=0°50'00"	R=6875.49'	T=300.49'	L=600.59'	Ext=6.56'	e=0.020%	SEE SUPERELEVATION DIAGRAM	
64110	POT	18+92.91	N=836767.653 E=801975.803										
	Meridian Rd Ramp 'B' Cst ξ												
64200	PC	0+00.00	N=836499.495 E=800036.188										
861	PI	3+46.77	N=836496.490 E=800382.949	SIMPLE	Δ=4°58'02"	D=0°43'00"	R=7994.76'	T=346.77'	L=693.11'	Ext=7.52'	e=0.020%	SEE SUPERELEVATION DIAGRAM	
64210	POT	19+51.18	N=836343.679 E=801980.496										
	Meridian Rd Ramp 'C' Cst ξ												
64300	POT	0+00.00	N=836755.654 E=801975.935										
862	PI	19+57.07	N=836611.771 E=803927.708	SIMPLE	Δ=3°43'10"	D=0°43'00"	R=7994.76'	T=259.60'	L=519.01'	Ext=4.21'	e=0.020%	SEE SUPERELEVATION DIAGRAM	
64303	PT	22+16.48	N=836609.521 E=804187.294										
	Meridian Rd Ramp 'D' Cst ξ												
64400	POT	0+00.00	N=836343.679 E=801980.496										
863	PI	18+51.22	N=836466.633 E=803827.630	SIMPLE	Δ=4°18'17"	D=0°50'00"	R=6875.49'	T=258.41'	L=516.58'	Ext=4.85'	e=0.020%	SEE SUPERELEVATION DIAGRAM	
6440	PT	21+09.39	N=83464.393 E=804086.033										
	Ironwood Dr Cst ξ												
22582	POT	-11+54.59	N=839657.350 E=808065.089										
22583	PI	14+86.06	N=837016.726 E=808076.388										
65003	PI	20+00.00	N=836502.790 E=808078.587										
22584	POT	41+26.71	N=834376.102 E=808087.687										
	Ironwood Dr Ramp 'A' Cst ξ												

CURVE DATA TABLE

APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			GEOMETRIC DATA SHEET	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	LOCATION	ELLSWORTH RD TO IRONWOOD DR		DWG NO. C-1.04
TRACS NO. H8915 OIL/O2L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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PLAN REF NO	LOCATION	P.I./P.O.T. STATION	COORDINATES		All Coordinates Are Ground Coordinates And All Bearings Are Grid Bearings								G.A.F. = 1.00016	
65100	PC	0+00.00	N=836594.353	E=805937.233										
870	PI	2+52.94	N=836592.161	E=806190.162	SIMPLE	Δ=4°12'49"	D=0°50'00"	R=6875.49'	T=252.94'	L=505.65'	Ext=4.65'	e=0.020%/ft	SEE SUPERELEVATION DIAGRAM	
65110	POT	21+44.21	N=836714.788	E=808077.680										
	Ironwood Dr Ramp 'B' Cst &													
65200	PC	0+00.00	N=836448.792	E=805885.969										
871	PI	2+91.51	N=836446.265	E=806177.465	SIMPLE	Δ=4°10'35"	D=0°43'00"	R=7994.76'	T=291.51'	L=582.76'	Ext=5.31'	e=0.020%/ft	SEE SUPERELEVATION DIAGRAM	
65210	POT	21+99.62	N=86290.792	E=808079.494										

CURVE DATA TABLE

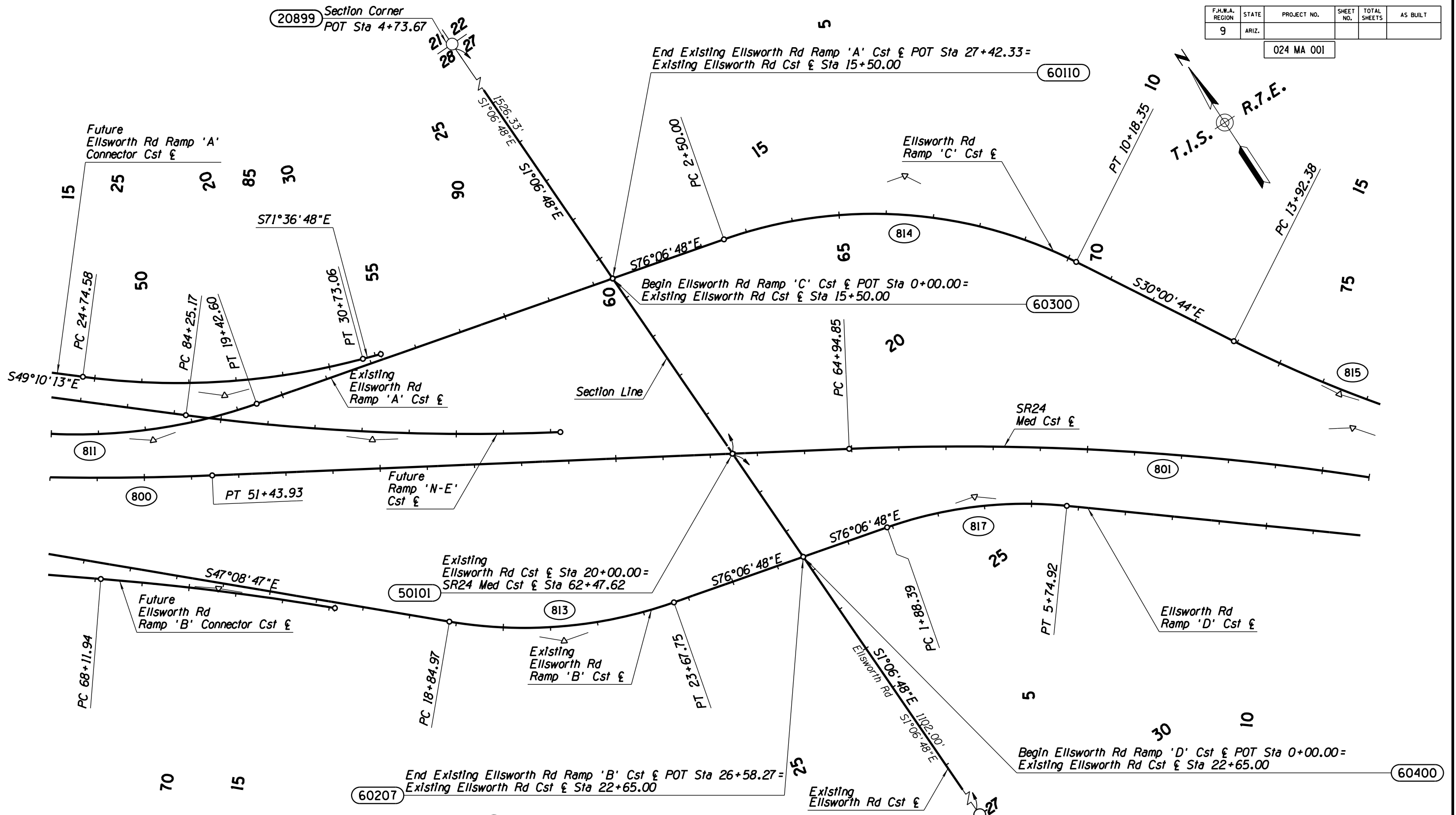
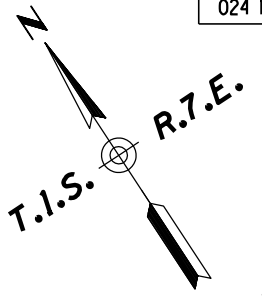
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			GEOMETRIC DATA SHEET	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-1.05
TRACS NO. H8915 OIL/O2L				<u>OF</u>

DATE LOCATION REVISIONS SURVEY NO. DATE LOCATION REVISIONS SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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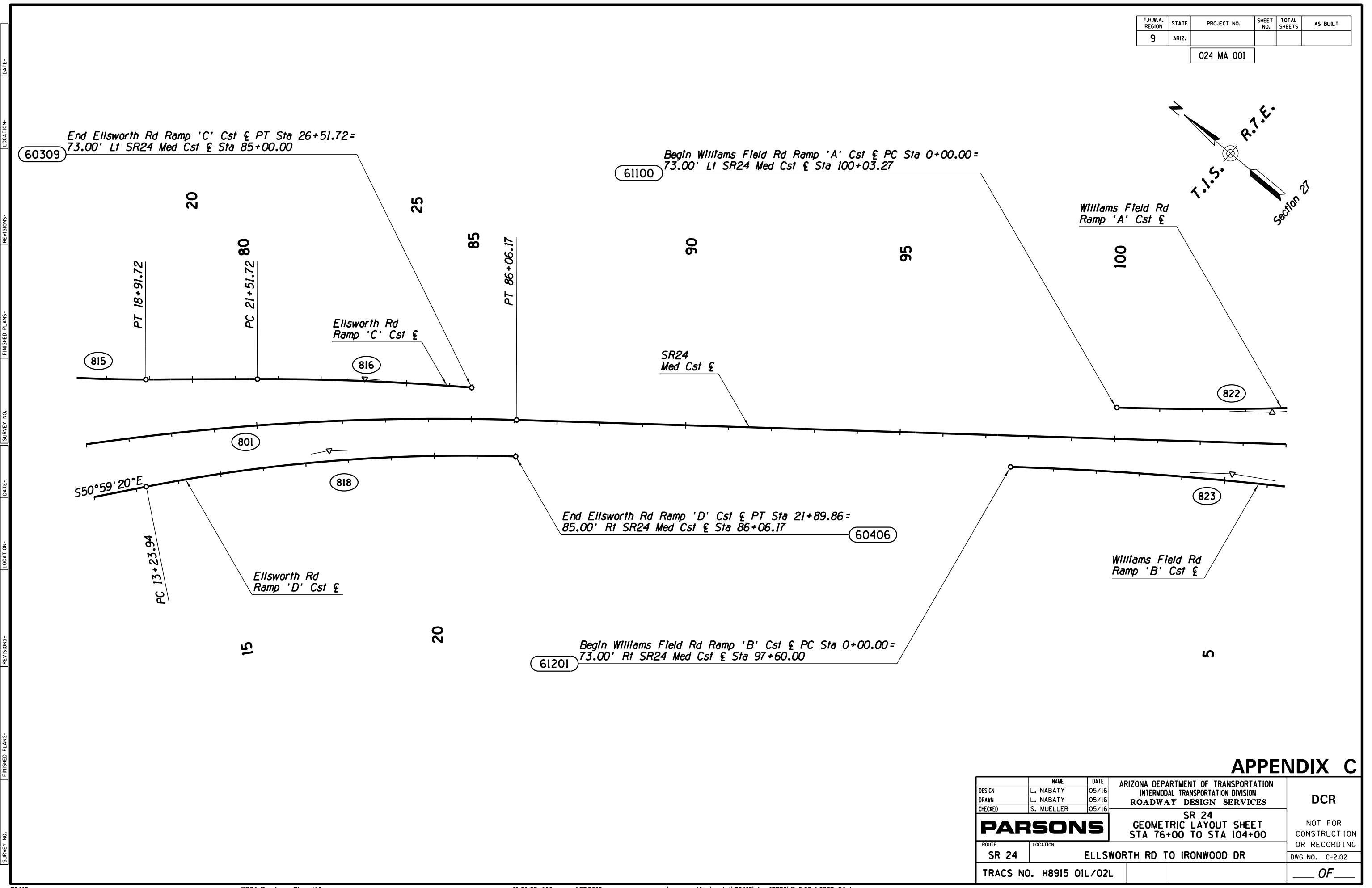
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SR 24 GEOMETRIC LAYOUT SHEET STA 48+00 TO STA 76+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-2.01
TRACS NO. H8915 OIL/02L				OF

SURVEY NO. FINISHED PLANS DATE REVISIONS LOCATION DATE FINISHED PLANS SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

024 MA 001

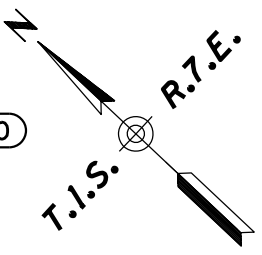


APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SR 24 GEOMETRIC LAYOUT SHEET STA 76+00 TO STA 104+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-2.02
TRACS NO. H8915 OIL/O2L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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End Williams Field Rd Ramp 'A' Cst & POT Sta 20+62.03 =
Williams Field Rd Cst & Sta 17+88.00

Begin Williams Field Rd
PC Sta 7+33.80

Begin Williams Field Rd Ramp 'C' Cst & POT Sta 0+00.00 =
Williams Field Rd Cst & Sta 18+00.00

Williams Field Rd
Ramp 'A' Cst &

Williams Field Rd
Ramp 'C' Cst &

Williams Field Rd Cst & Sta 20+00.00 =
SR24 Med Cst & Sta 120+25.00

SR24
Med Cst &
Sta 114+53.17

Williams Field Rd
Ramp 'D' Cst &

Begin Williams Field Rd Ramp 'D' Cst & POT Sta 0+00.00 =
Williams Field Rd Cst & Sta 22+12.00

End Williams Field Rd Ramp 'B' Cst & POT Sta 22+41.56 =
Williams Field Rd Cst & Sta 22+00.00

APPENDIX C

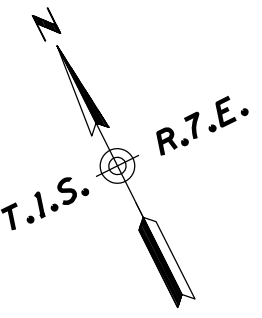
DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SR 24 GEOMETRIC LAYOUT SHEET STA 104+00 TO STA 132+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-2.03
TRACS NO. H8915 OIL/O2L				OF

SURVEY NO. FINISHED PLANS DATE REVISIONS LOCATION DATE FINISHED PLANS SURVEY NO. FINISHED PLANS DATE REVISIONS LOCATION DATE FINISHED PLANS SURVEY NO. FINISHED PLANS DATE

SURVEY NO. FINISHED PLANS DATE LOCATION REVISIONS DATE SURVEY NO. FINISHED PLANS DATE SURVEY NO. FINISHED PLANS DATE SURVEY NO. FINISHED PLANS DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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Section Corner
POT Sta 4+16.35 (20921)

27 26
34 35

Section Line

135 15
1583.65'
14°54'E

140 20

Williams Field Rd
Ramp 'C' Cst &

145 25

150

155

160

End Williams Field Rd Ramp 'C' Cst & PT Sta 26+85.87 =
73.00' Lt SR24 Med Cst & Sta 148+03.82

(61303)

(825)

(802)

SR24
Med Cst &

Crismon Rd Cst & Sta 20+00.00 =
SR24 Med Cst & Sta 139+00.06

(50062)

Williams Field Rd
Ramp 'D' Cst &

End Williams Field Rd Ramp 'D' Cst & POT Sta 24+33.79 =
73.00' Rt SR24 Med Cst & Sta 143+50.00

(61404)

15

20

Future Crismon Rd Cst &

1088.10'
50°41'54"E

1/4 Corner
POT Sta 30+48.10 (20930)

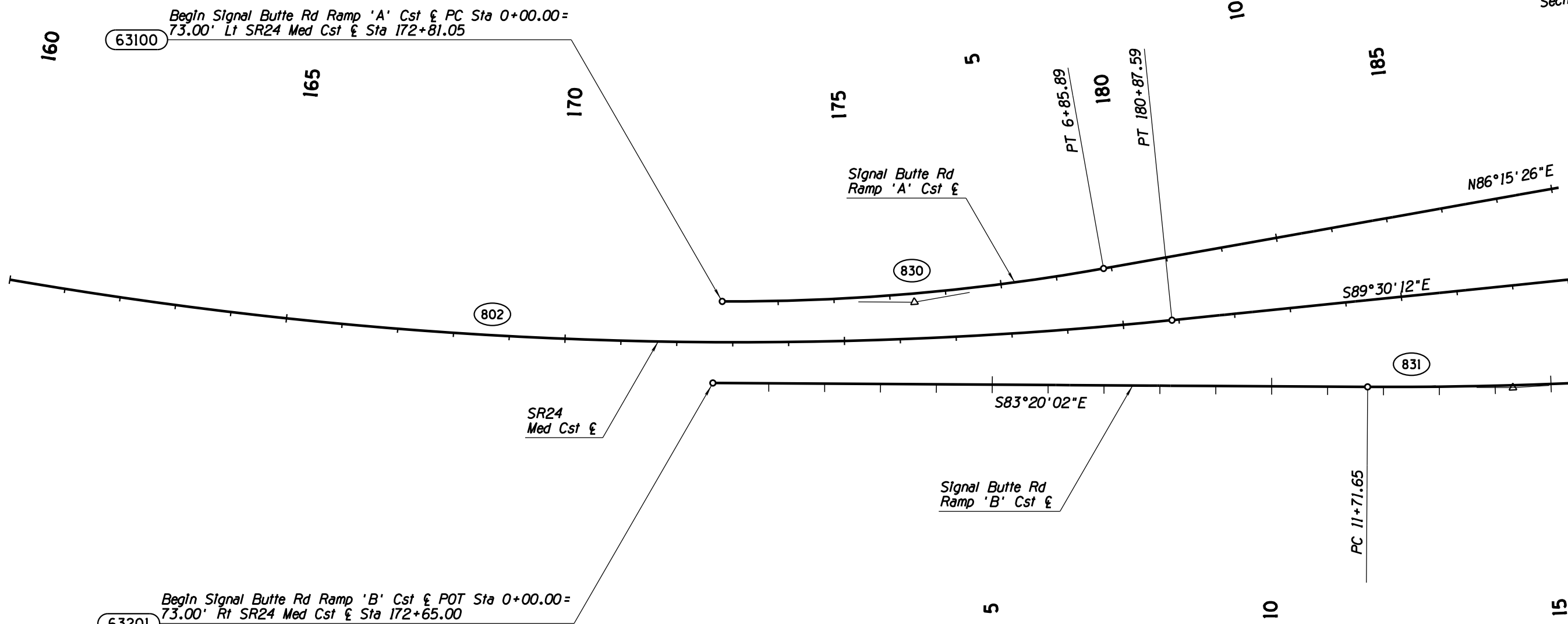
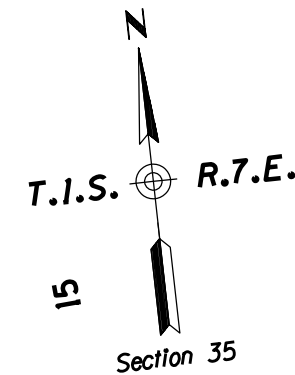
34 35

APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS		SR 24 GEOMETRIC LAYOUT SHEET STA 132+00 TO STA 160+00		NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-2.04
TRACS NO. H8915 OIL/O2L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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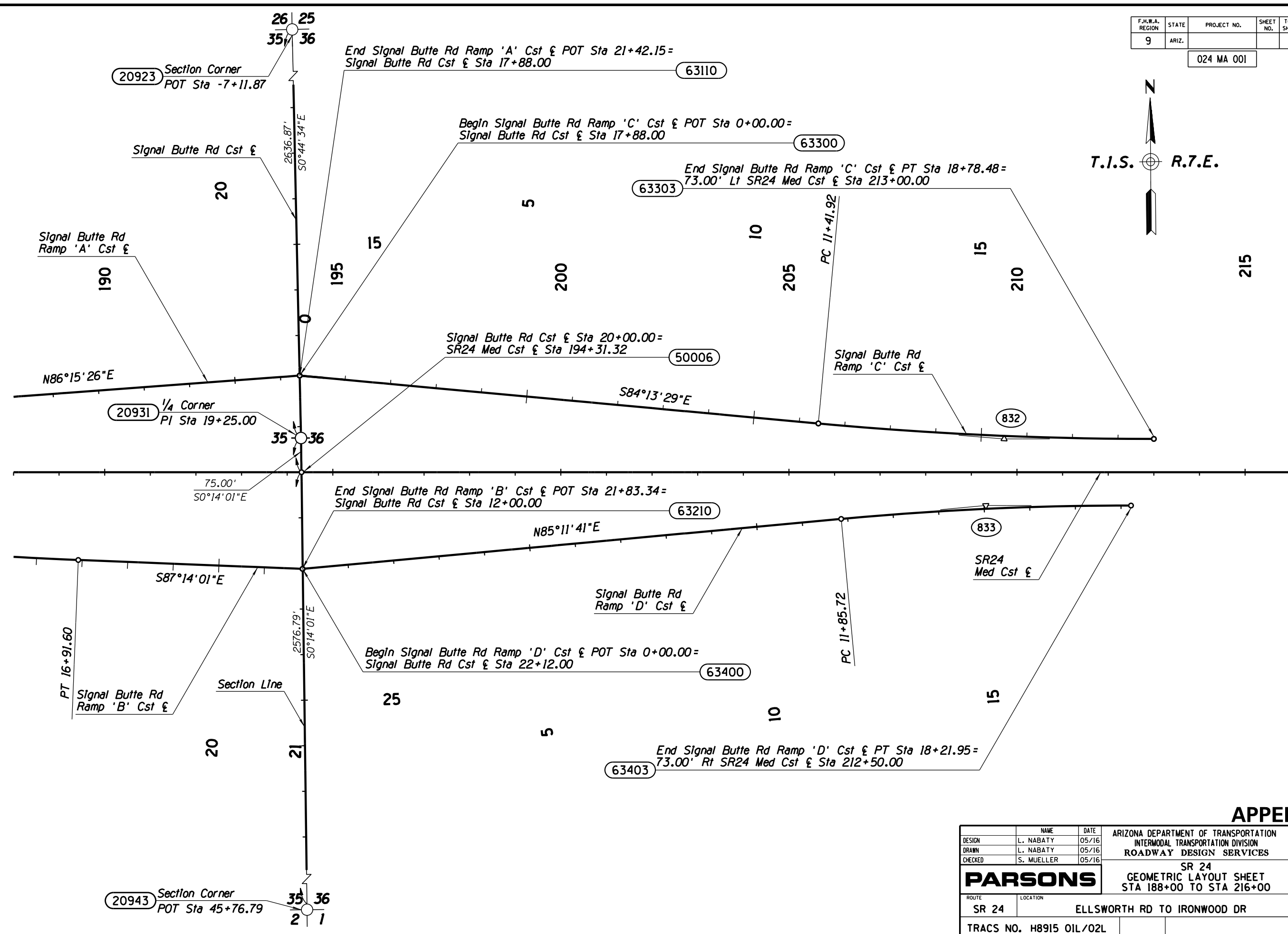
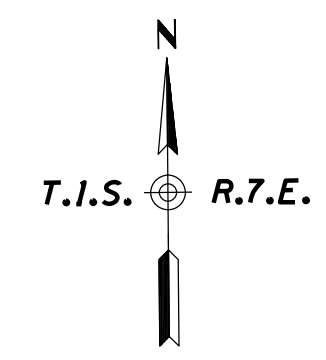
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SR 24 GEOMETRIC LAYOUT SHEET STA 160+00 TO STA 188+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-2.05
TRACS NO. H8915 OIL/O2L				OF

SURVEY NO. FINISHED PLANS DATE LOCATION REVISIONS DATE FINISHED PLANS SURVEY NO. DATE REVISIONS LOCATION DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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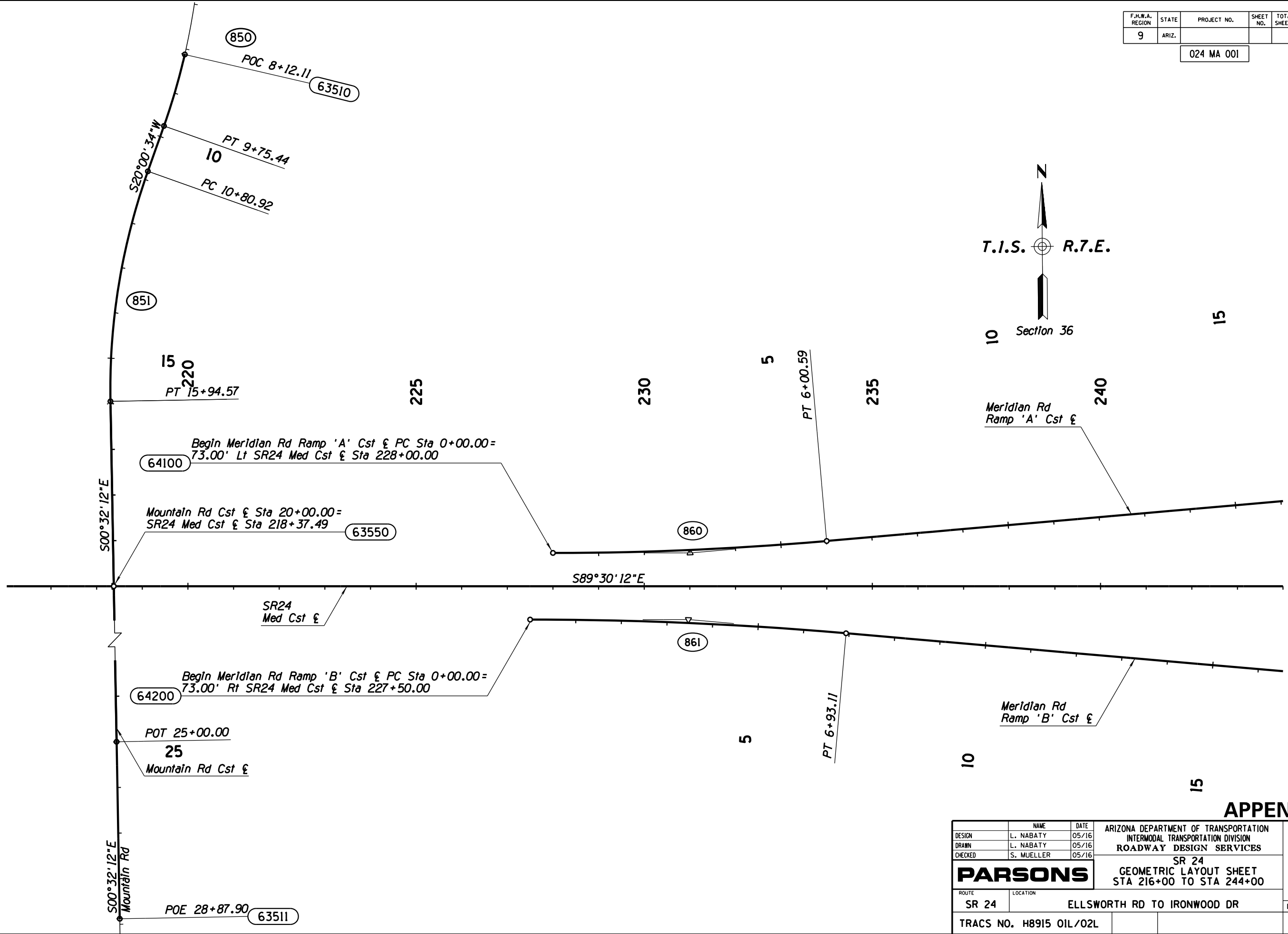
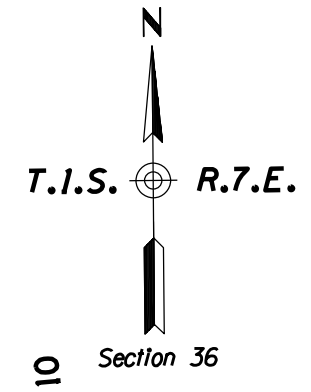
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SR 24 GEOMETRIC LAYOUT SHEET STA 188+00 TO STA 216+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-2.06
TRACS NO. H8915 OIL/02L				OF

SURVEY NO. FINISHED PLANS DATE REVISIONS LOCATION DATE FINISHED PLANS SURVEY NO. REVISIONS LOCATION DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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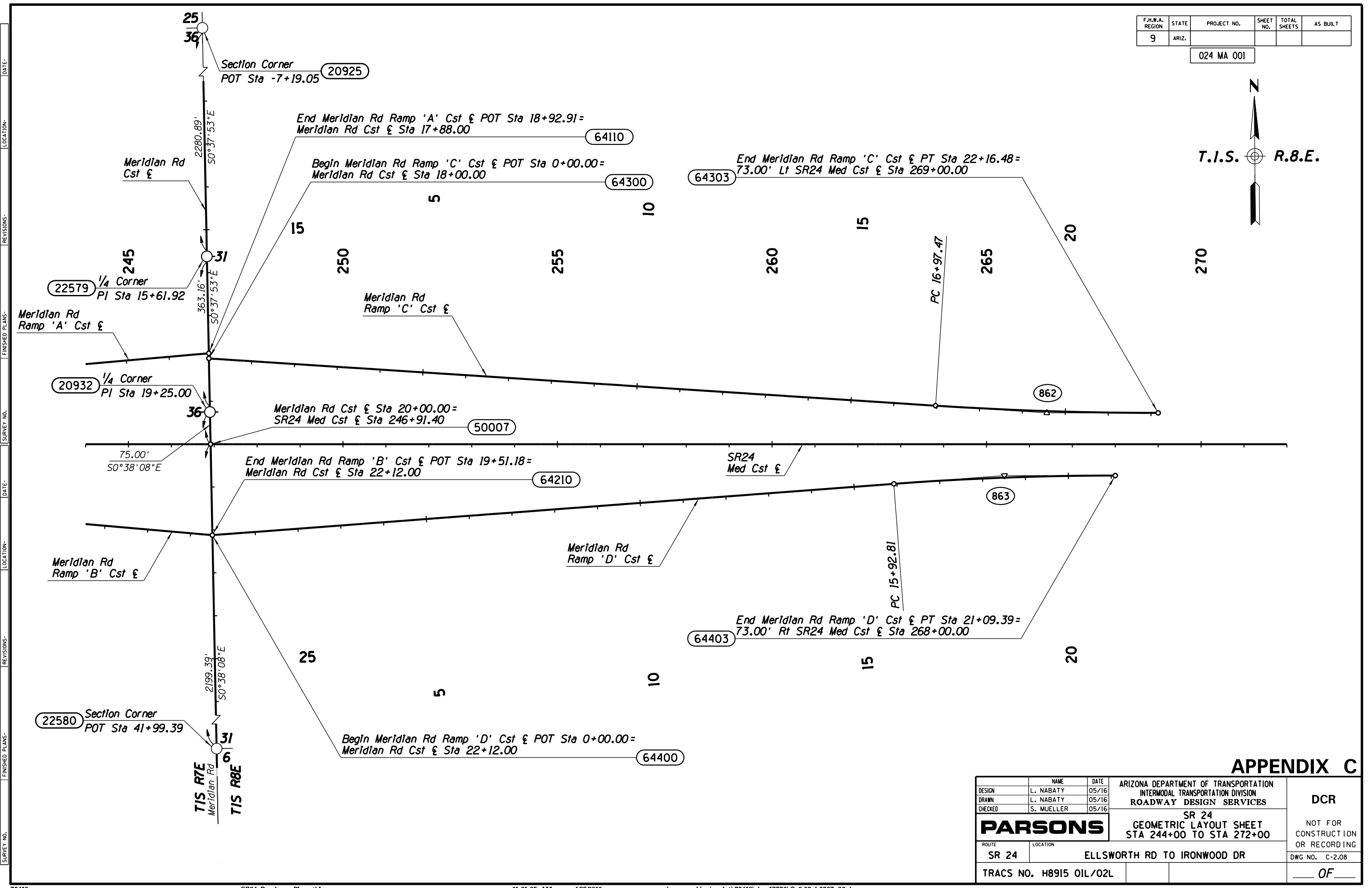
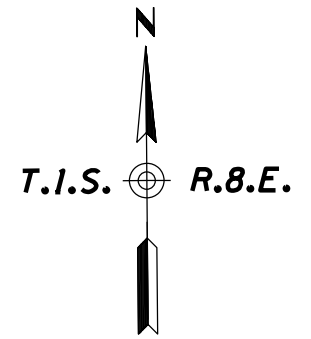
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS		SR 24 GEOMETRIC LAYOUT SHEET STA 216+00 TO STA 244+00		NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-2.07
TRACS NO. H8915 OIL/O2L				OF

SURVEY NO. FINISHED PLANS DATE REVISIONS LOCATION DATE SURVEY NO. FINISHED PLANS DATE REVISIONS LOCATION DATE SURVEY NO. FINISHED PLANS DATE REVISIONS LOCATION DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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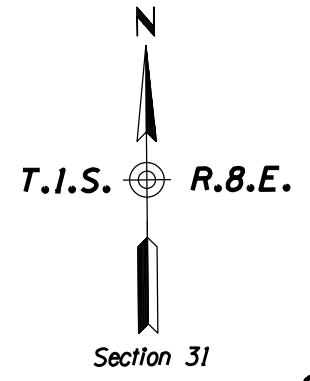
APPENDIX C

DESIGN	NAME	DATE	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DESIGN	L. NABATY	05/16		
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16	SR 24 GEOMETRIC LAYOUT SHEET STA 244+00 TO STA 272+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	LOCATION	SR 24 ELLSWORTH RD TO IRONWOOD DR		DWG NO. C-2.08
TRACS NO. H8915 OIL/O2L				OF

SURVEY NO. FINISHED PLANS DATE LOCATION REVISIONS DATE FINISHED PLANS SURVEY NO. FINISHED PLANS DATE LOCATION REVISIONS DATE FINISHED PLANS SURVEY NO.

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65100
 Begin Ironwood Dr Ramp 'A' Cst & PC Sta 0+00.00=
 73.00' Lt SR24 Med Cst & Sta 286+50.00

Ironwood Dr
 Ramp 'A' Cst &

PT 5+05.65
 5

N86°16'58"E

870

SR24
 Med Cst &

65200
 Begin Ironwood Dr Ramp 'B' Cst & PC Sta 0+00.00=
 73.00' Rt SR24 Med Cst & Sta 286+00.00

Ironwood Dr
 Ramp 'B' Cst &

PT 5+82.76
 5

10

871

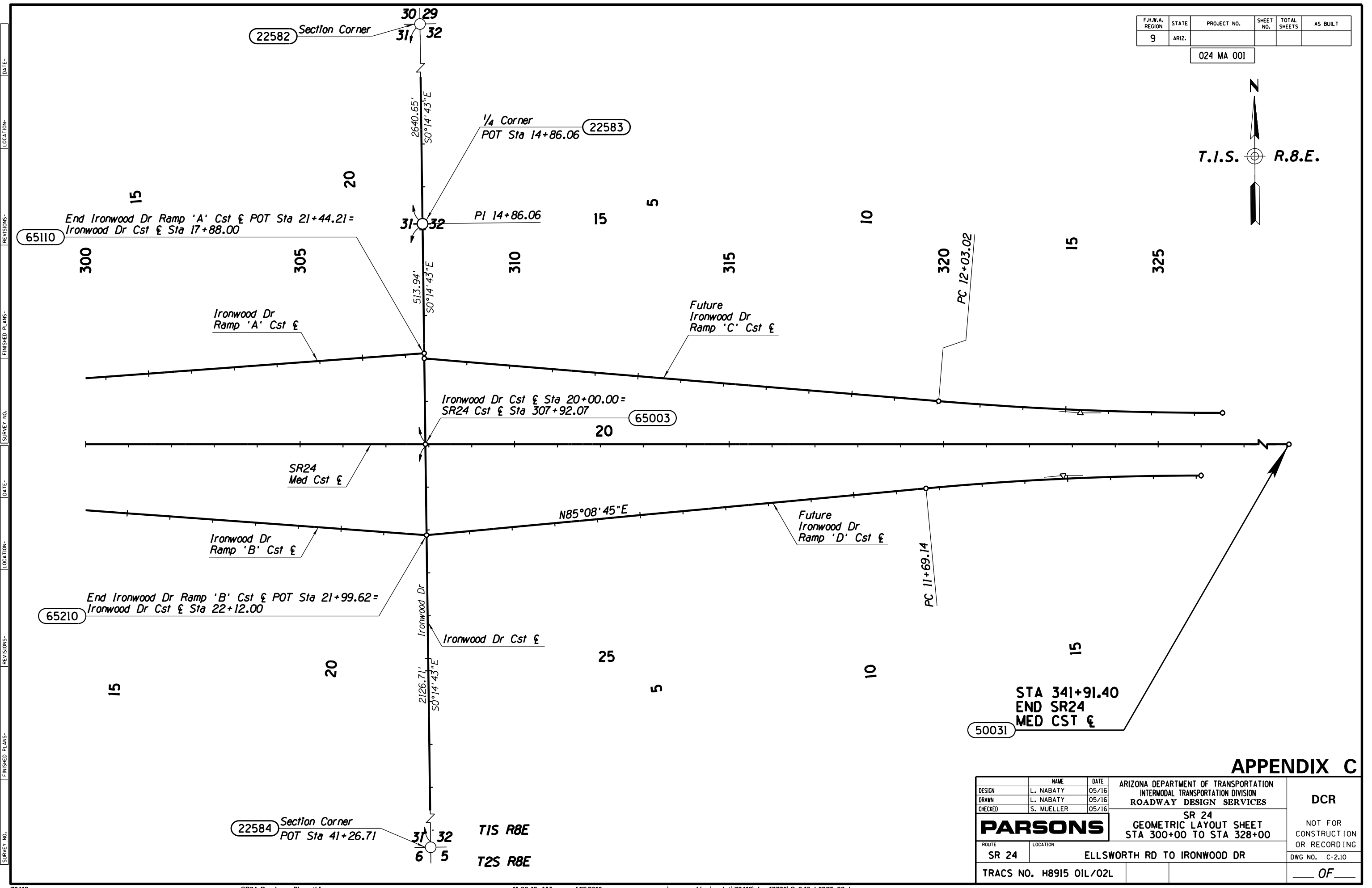
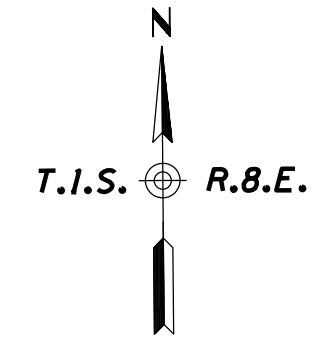
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SR 24 GEOMETRIC LAYOUT SHEET STA 272+00 TO STA 300+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-2.09
TRACS NO. H8915 OIL/O2L				OF

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APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS		SR 24 GEOMETRIC LAYOUT SHEET STA 300+00 TO STA 328+00		NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-2.10
TRACS NO. H8915 OIL/O2L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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Interim WB Roadway Section

2' Outside Shldr
12' Lane
12' Lane
2' Inside Shldr

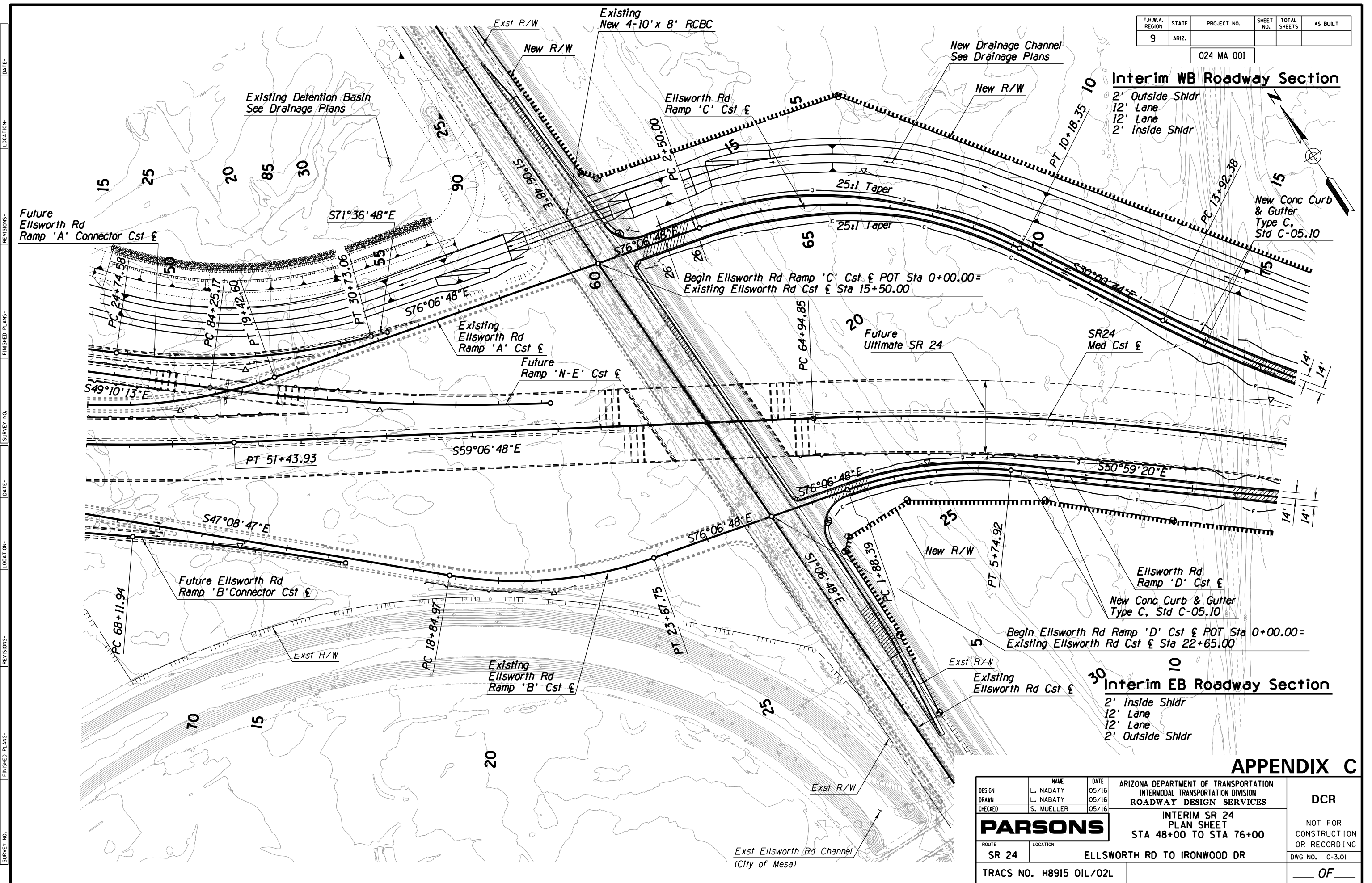
New Conc Curb & Gutter
Type C, Std C-05.10

Interim EB Roadway Section

2' Inside Shldr
12' Lane
12' Lane
2' Outside Shldr

APPENDIX C

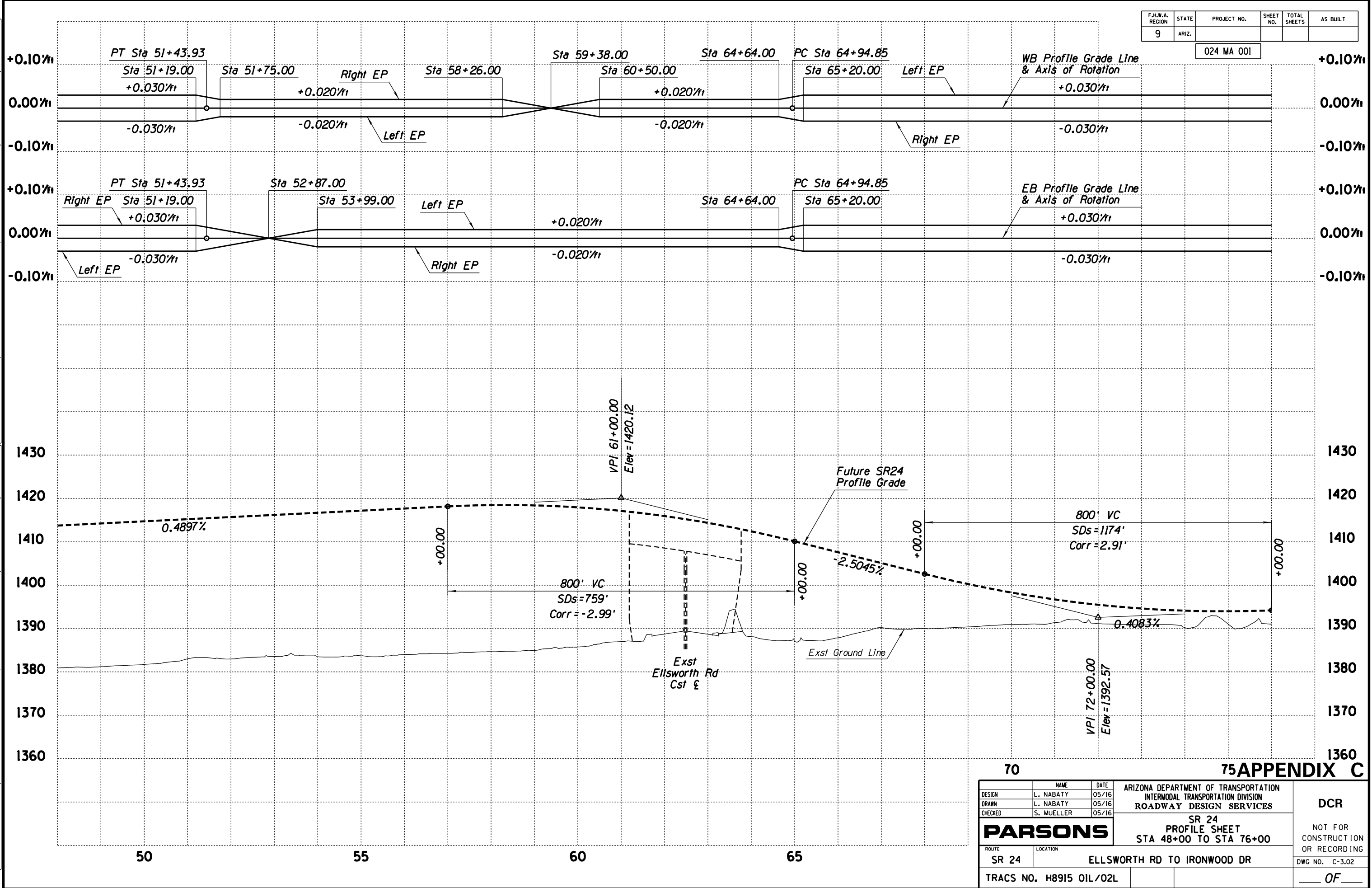
DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			INTERIM SR 24 PLAN SHEET STA 48+00 TO STA 76+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.01
TRACS NO. H8915 OIL/02L				OF



SURVEY NO. FINISHED PLANS. DATE. LOCATION. REVISIONS. DATE. SURVEY NO. FINISHED PLANS. DATE. LOCATION. REVISIONS. DATE. SURVEY NO. FINISHED PLANS. DATE. LOCATION. REVISIONS. DATE.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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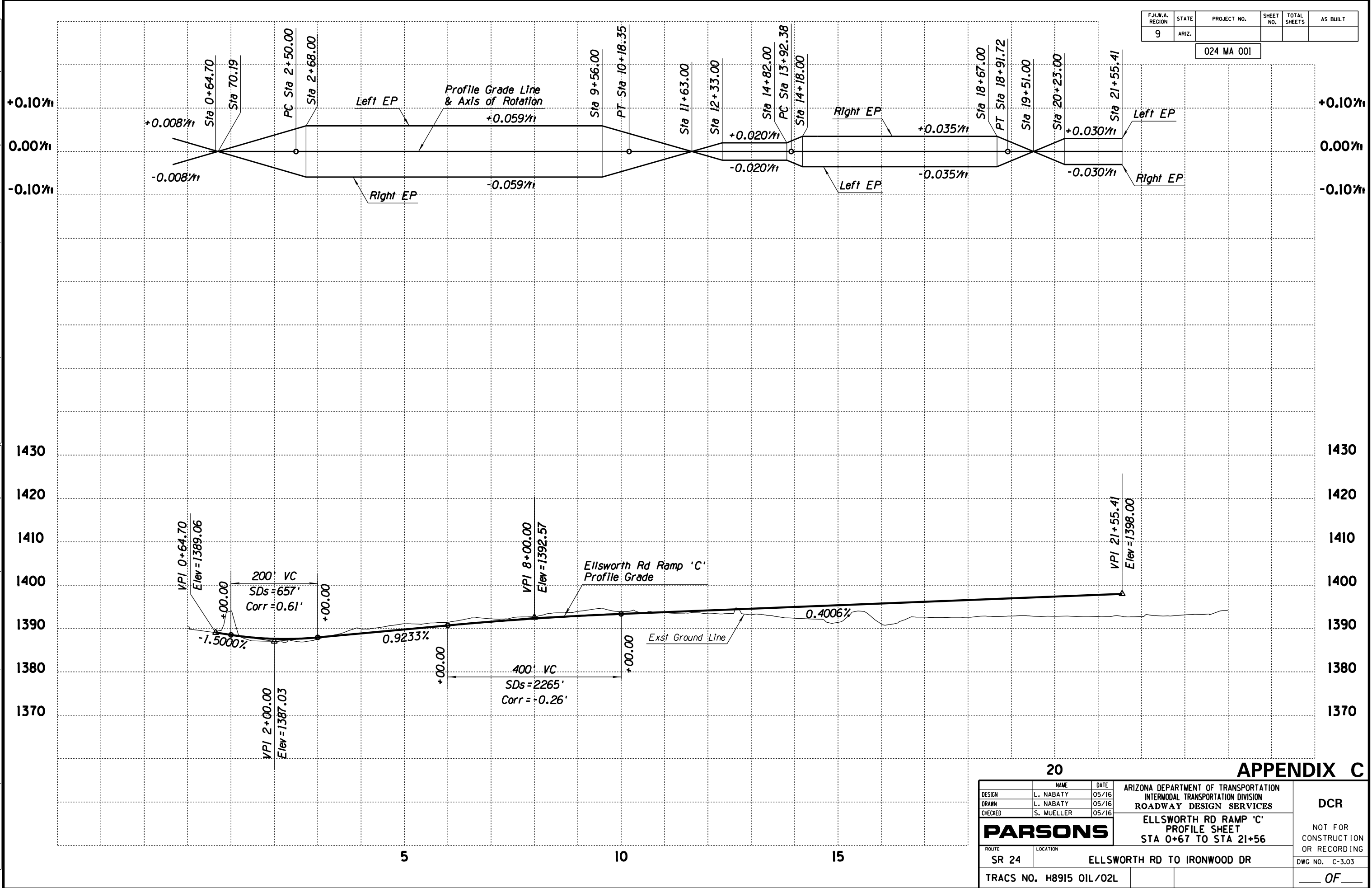


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DESIGN	L. NABATY	DATE	05/16
DRAWN	L. NABATY	DATE	05/16
CHECKED	S. MUELLER	DATE	05/16
PARSONS ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES			DCR
SR 24 PROFILE SHEET STA 48+00 TO STA 76+00			NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR
TRACS NO. H8915 OIL/02L			DWG NO. C-3.02
			OF

DATE LOCATION FINISHED PLANS SURVEY NO. DATE LOCATION FINISHED PLANS SURVEY NO. DATE LOCATION FINISHED PLANS SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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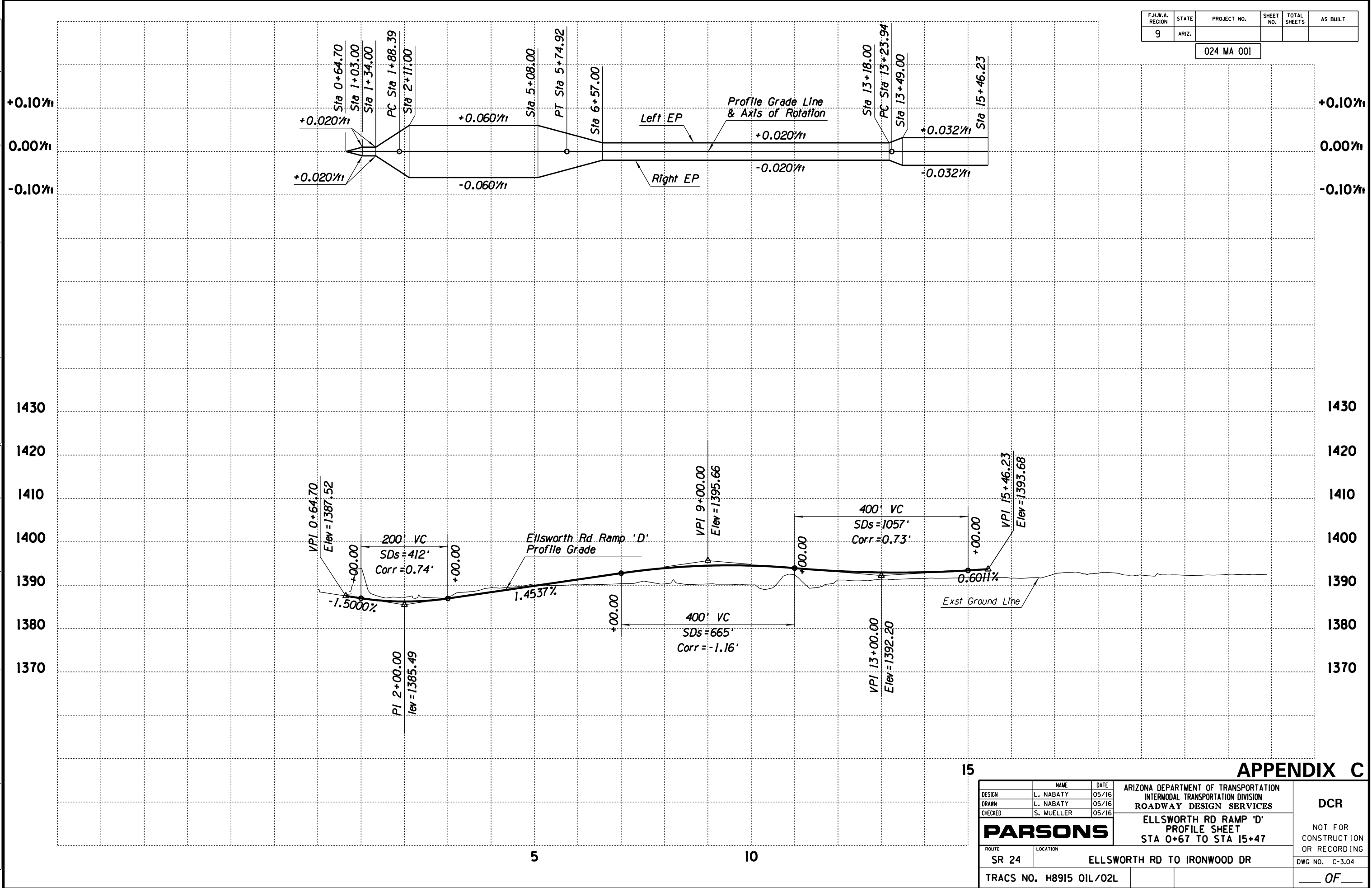
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			ELLSWORTH RD RAMP 'C' PROFILE SHEET STA 0+67 TO STA 21+56	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.03
TRACS NO. H8915 OIL/O2L				OF

SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			ELLSWORTH RD RAMP 'D' PROFILE SHEET STA 0+67 TO STA 15+47	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.04
TRACS NO. H8915 OIL/02L				OF

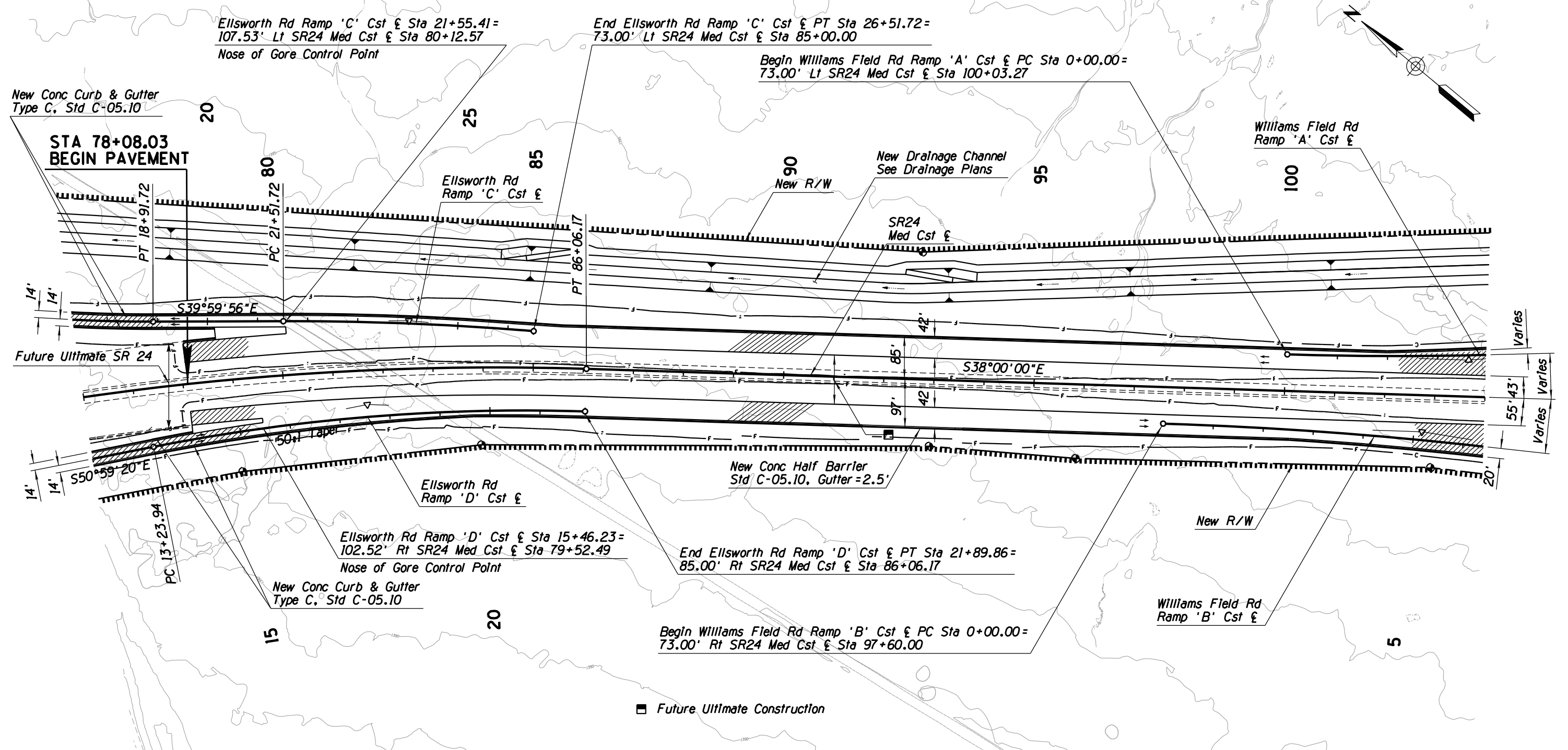
SURVEY NO. FINISHED PLANS DATE REVISIONS LOCATION DATE

Interim WB Roadway Section

12' Outside Shldr (2' at Ramps)
 12' Lane
 12' Lane
 6' Inside Shldr (2' at Ramps)

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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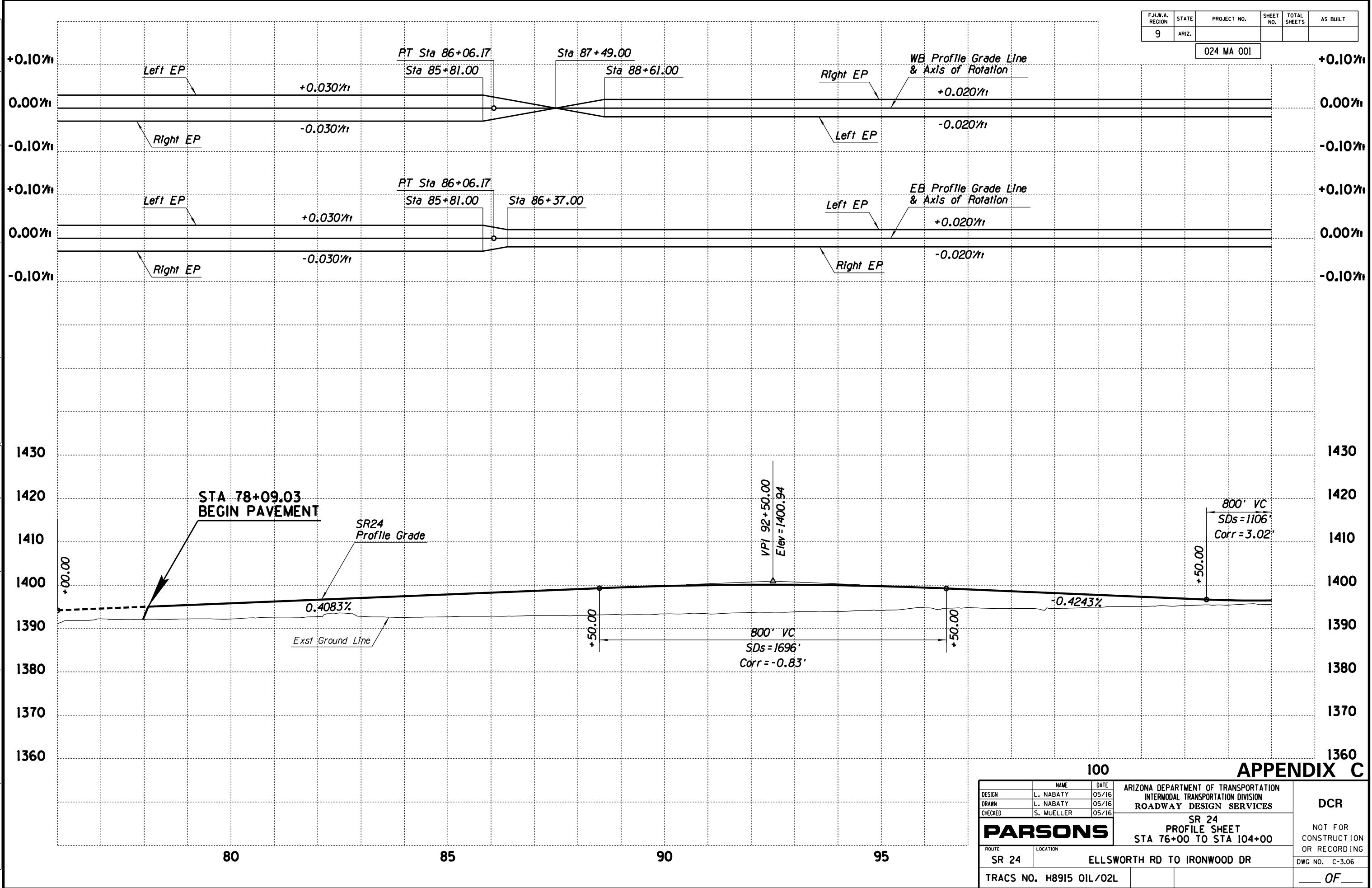


APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			INTERIM SR 24 PLAN SHEET STA 76+00 TO STA 104+00	DWG NO. C-3.05 OF
ROUTE	LOCATION			
SR 24	ELLSWORTH RD TO IRONWOOD DR			
TRACS NO. H8915 OIL/02L				

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SR 24 PROFILE SHEET STA 76+00 TO STA 104+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.06
TRACS NO. H8915 OIL/O2L				OF

DATE: LOCATION: REVISIONS: FINISHED PLANS: SURVEY NO. DATE: LOCATION: REVISIONS: FINISHED PLANS: SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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Interim WB Roadway Section

12' Outside Shldr (2' at Ramps)
12' Lane
12' Lane
6' Inside Shldr (2' at Ramps)

End Williams Field Rd Ramp 'A' Cst & POT Sta 20+62.03 =
Williams Field Rd Cst & Sta 17+88.00

New Drainage Channel
See Drainage Plans

Williams Field Rd
Ramp 'A' Cst &

New Conc Curb & Gutter
Type C, Std C-05.10

Williams Field Rd Ramp 'A' Cst & Sta 4+91.07 =
90.53' Lt SR24 Med Cst & Sta 104+93.92

Nose of Gore Control Point

Sta 106+17.00
End Pavement

PT 7+24.06

PT 15+78.02

New R/W

New 4-10' x 8' RCBC

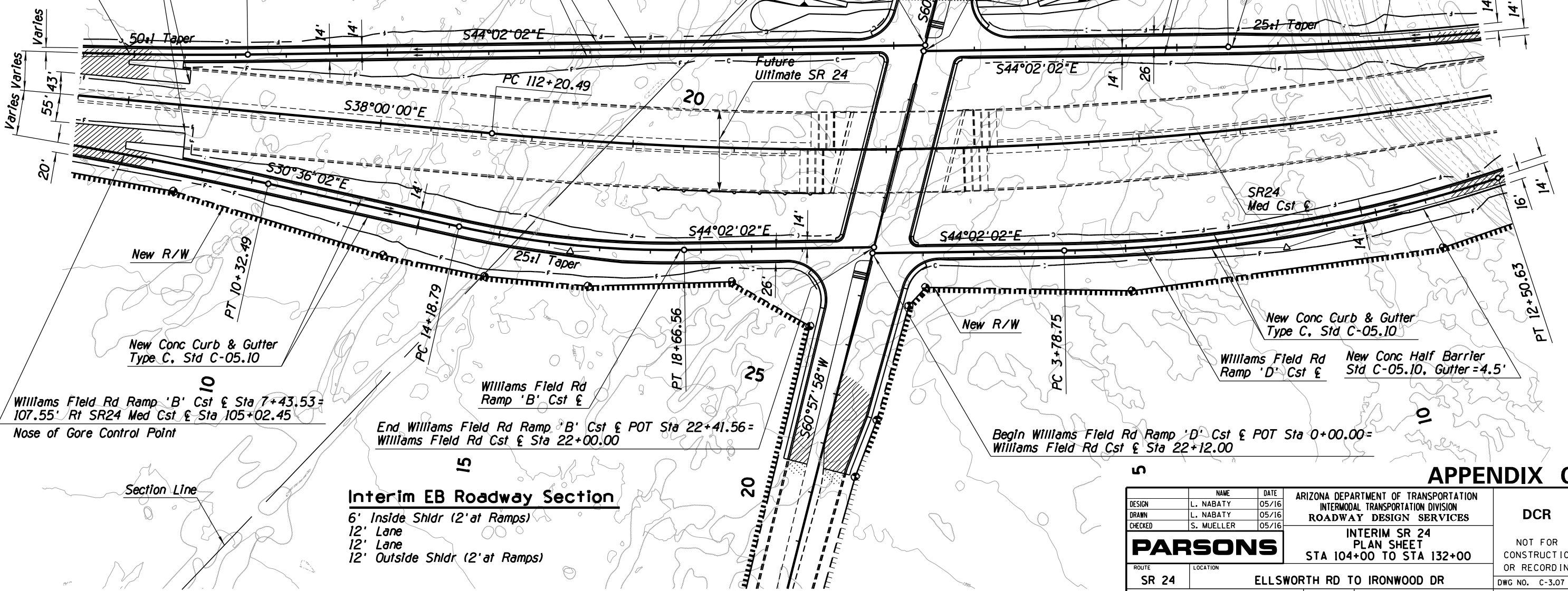
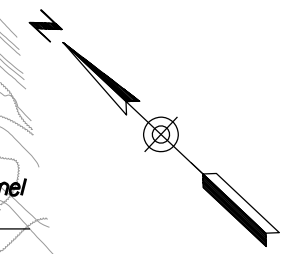
New R/W

New Conc Curb & Gutter
Type C, Std C-05.10

New Drainage Channel
See Drainage Plans

Williams Field Rd
Ramp 'C' Cst &

New Conc Half Barrier
Std C-05.10, Gutter = 2.5'



Interim EB Roadway Section

6' Inside Shldr (2' at Ramps)
12' Lane
12' Lane
12' Outside Shldr (2' at Ramps)

End Williams Field Rd Ramp 'B' Cst & POT Sta 22+41.56 =
Williams Field Rd Cst & Sta 22+00.00

Williams Field Rd
Ramp 'B' Cst &

Williams Field Rd Ramp 'B' Cst & Sta 7+43.53 =
107.55' Rt SR24 Med Cst & Sta 105+02.45

Nose of Gore Control Point

New Conc Curb & Gutter
Type C, Std C-05.10

PT 10+32.49

PT 14+18.79

PT 18+66.56

New R/W

Williams Field Rd
Ramp 'B' Cst &

New R/W

PC 3+78.75

New Conc Curb & Gutter
Type C, Std C-05.10

Williams Field Rd
Ramp 'D' Cst &

New Conc Half Barrier
Std C-05.10, Gutter = 4.5'

Begin Williams Field Rd Ramp 'D' Cst & POT Sta 0+00.00 =
Williams Field Rd Cst & Sta 22+12.00

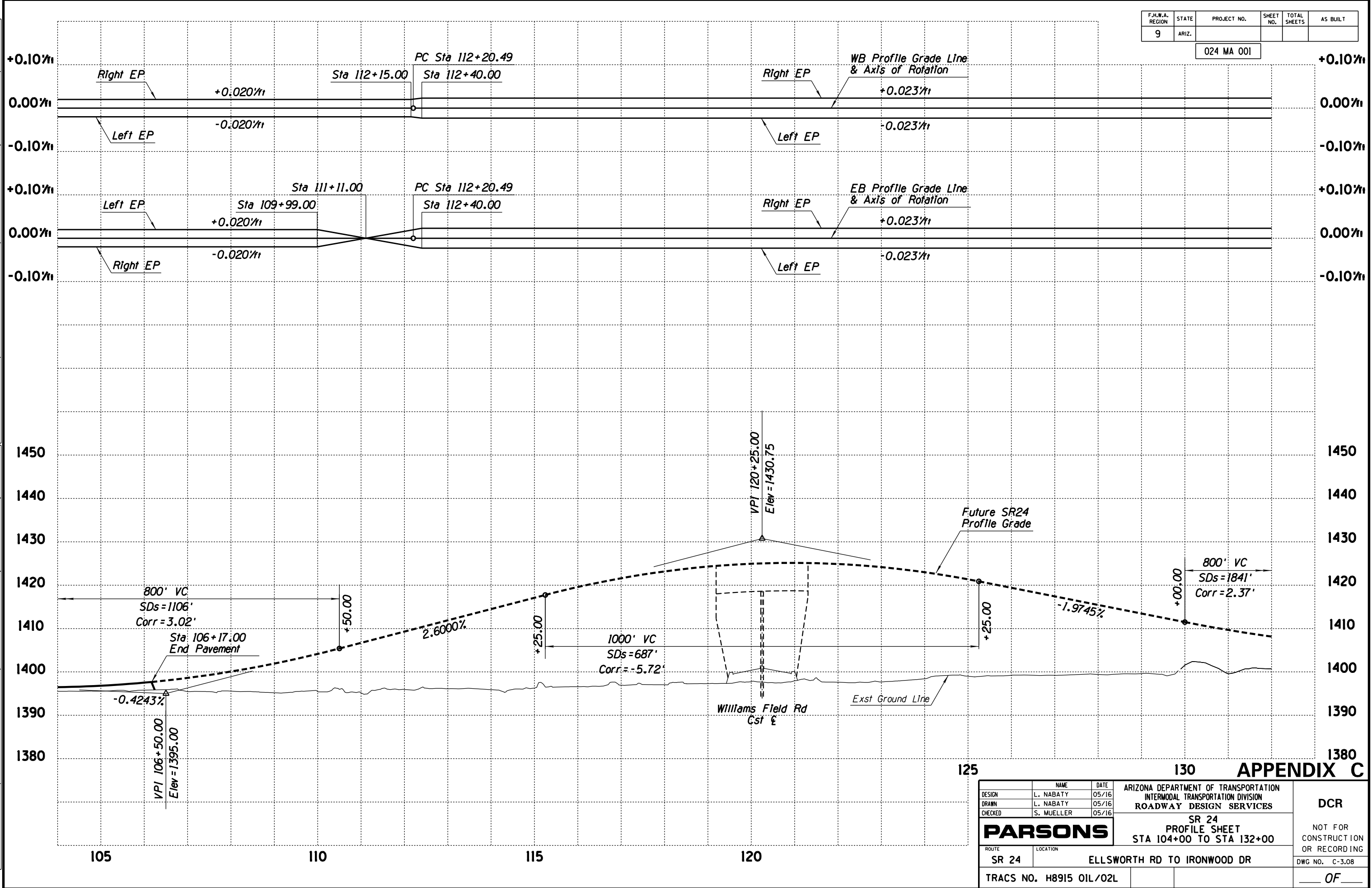
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			INTERIM SR 24 PLAN SHEET STA 104+00 TO STA 132+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.07
TRACS NO. H8915 OIL/02L				OF

DATE: LOCATION: REVISIONS: FINISHED PLANS: SURVEY NO. DATE: LOCATION: REVISIONS: FINISHED PLANS: SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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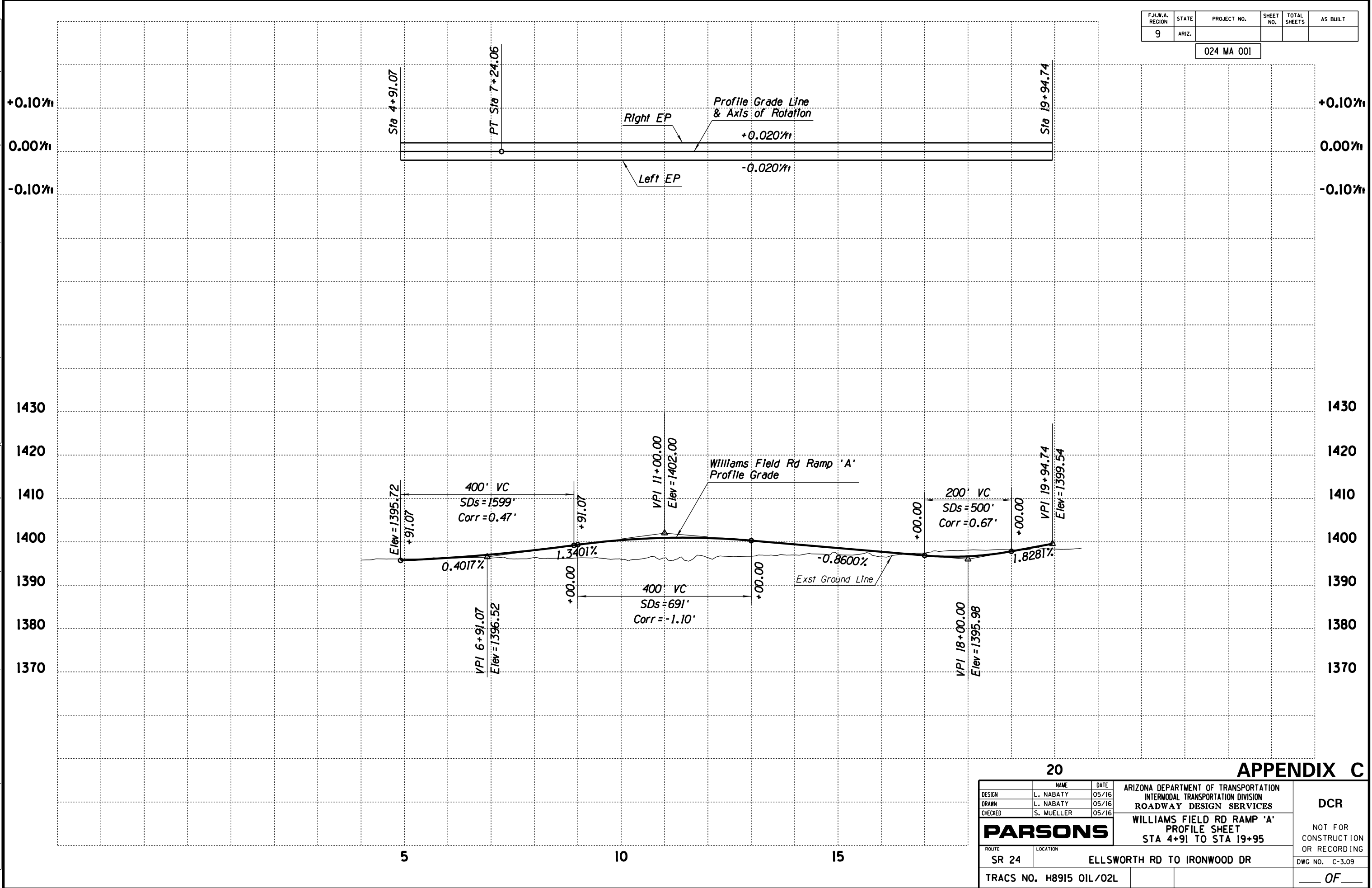


APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SR 24 PROFILE SHEET STA 104+00 TO STA 132+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.08
TRACS NO. H8915 OIL/02L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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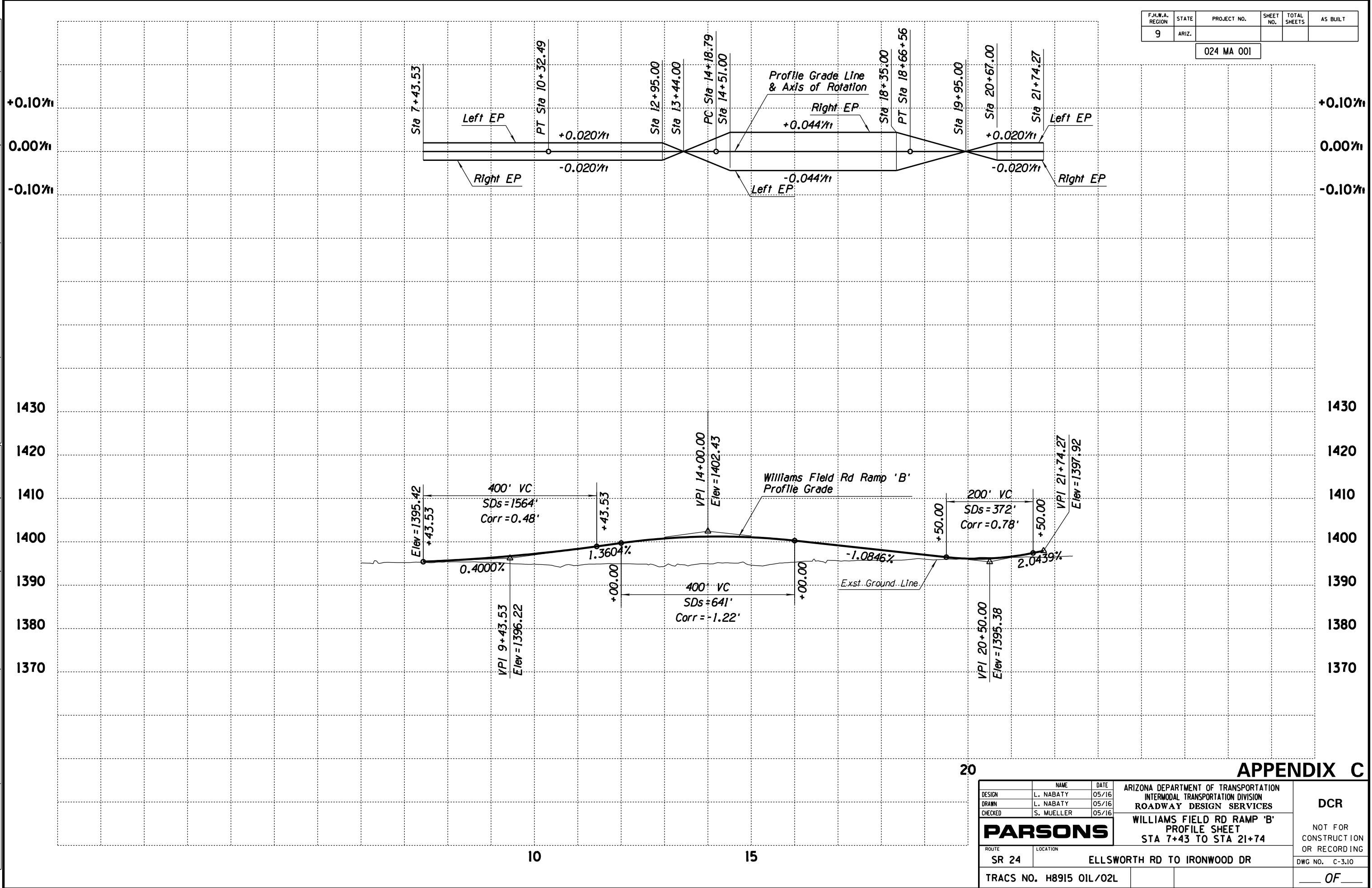
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			WILLIAMS FIELD RD RAMP 'A' PROFILE SHEET STA 4+91 TO STA 19+95	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.09
TRACS NO. H8915 OIL/02L				OF

SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE FINISHED PLANS SURVEY NO. DATE REVISIONS LOCATION DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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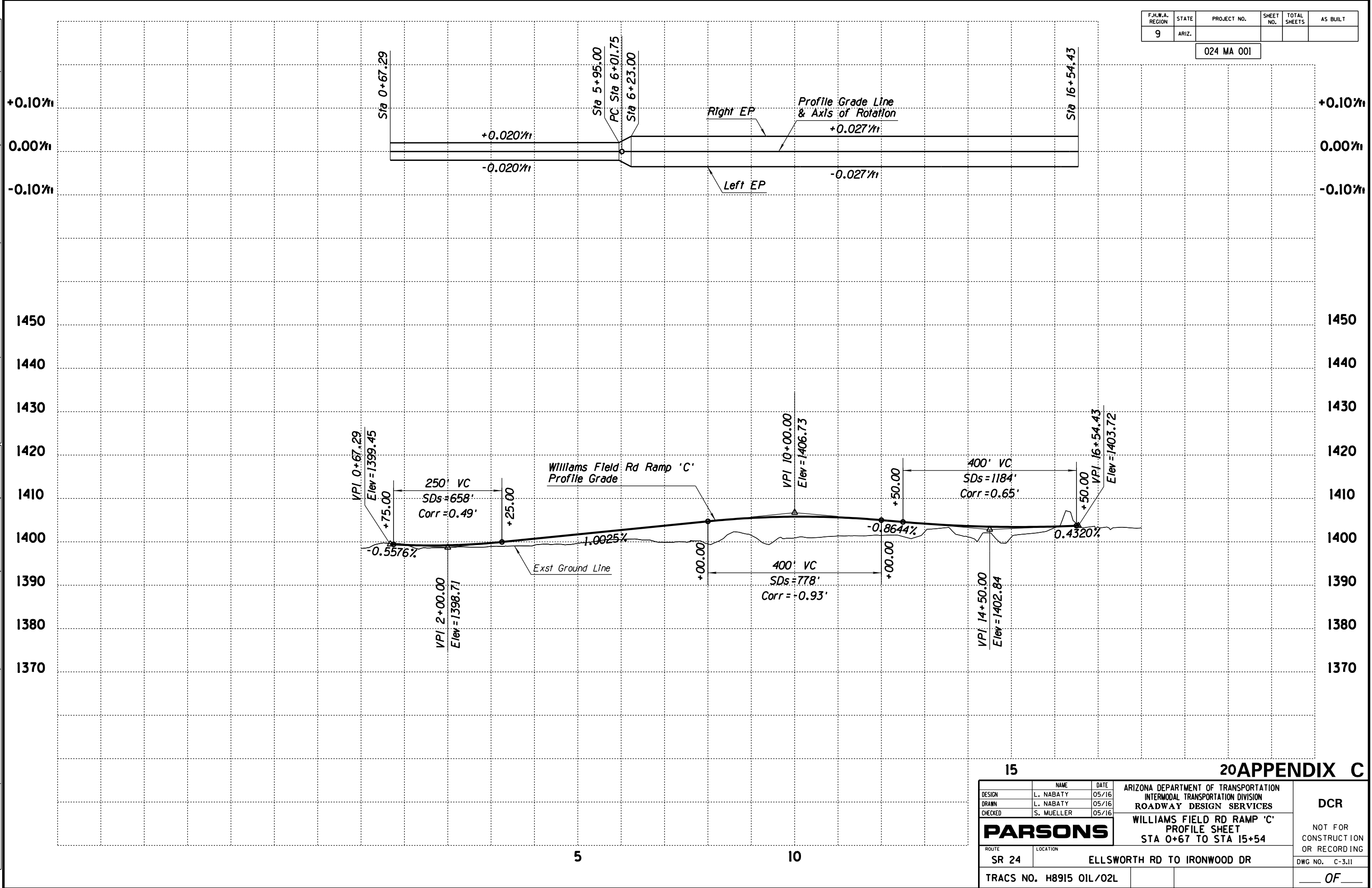
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APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			WILLIAMS FIELD RD RAMP 'B' PROFILE SHEET STA 7+43 TO STA 21+74	
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.10
TRACS NO. H8915 OIL/O2L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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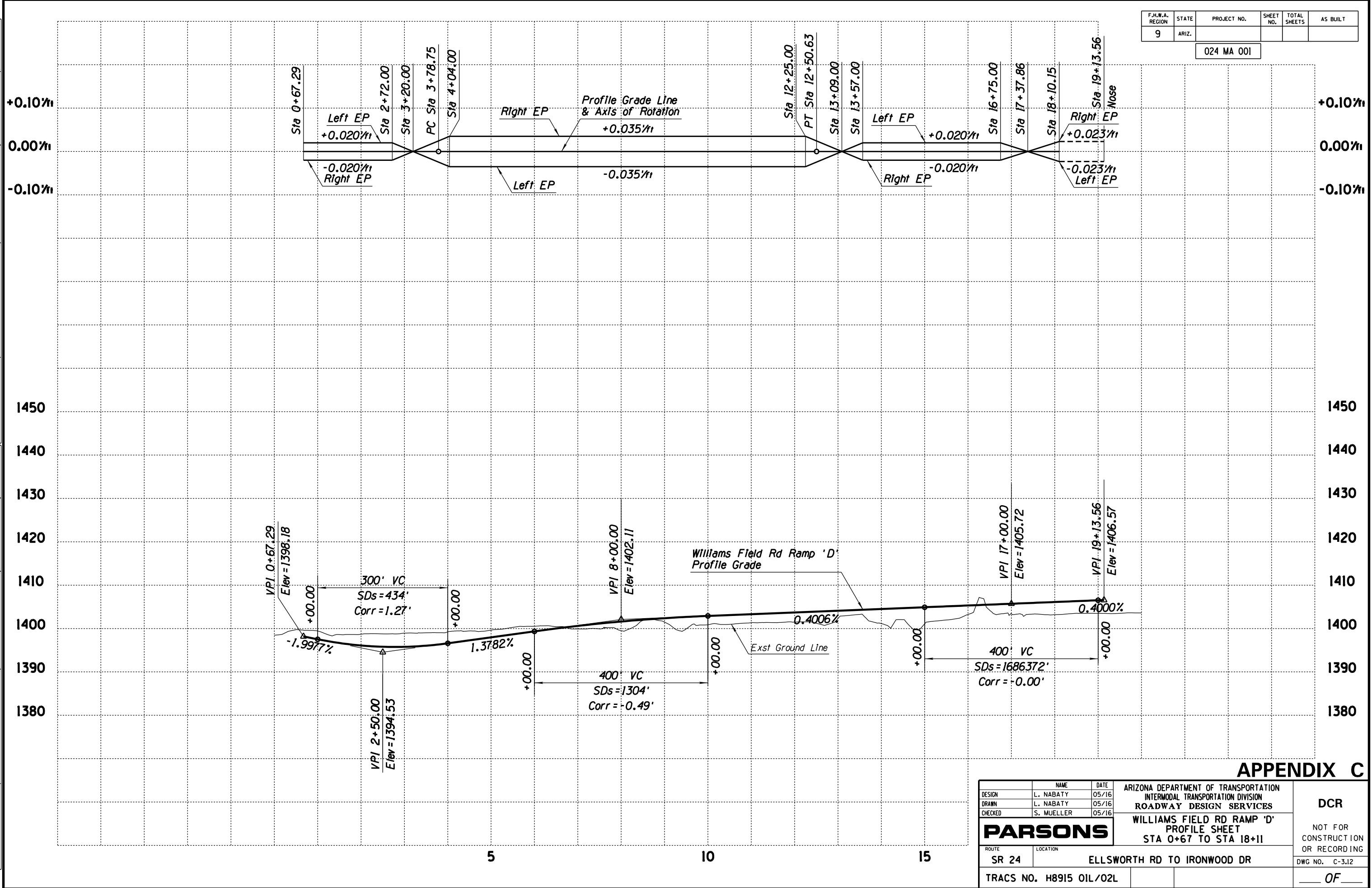
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DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			WILLIAMS FIELD RD RAMP 'C' PROFILE SHEET STA 0+67 TO STA 15+54	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.11
TRACS NO. H8915 OIL/O2L				OF

SURVEY NO. FINISHED PLANS DATE REVISIONS LOCATION DATE FINISHED PLANS SURVEY NO. REVISIONS LOCATION DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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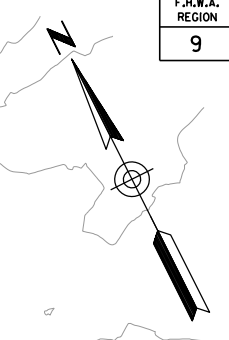
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			WILLIAMS FIELD RD RAMP 'D' PROFILE SHEET STA 0+67 TO STA 18+11	
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.12
TRACS NO. H8915 OIL/O2L				OF

SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE

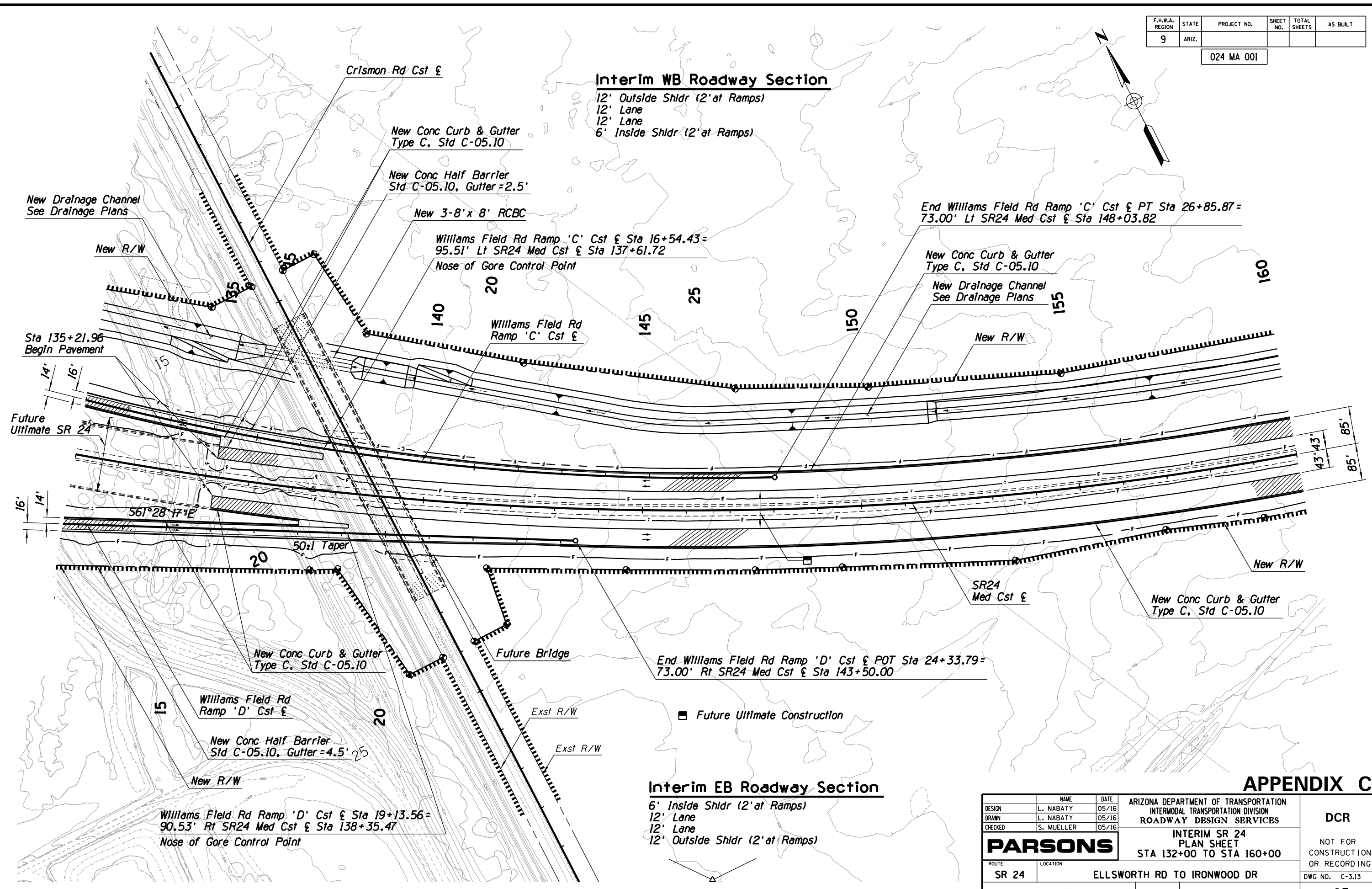
F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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Interim WB Roadway Section

12' Outside Shldr (2' at Ramps)
 12' Lane
 12' Lane
 6' Inside Shldr (2' at Ramps)



Interim EB Roadway Section

6' Inside Shldr (2' at Ramps)
 12' Lane
 12' Lane
 12' Outside Shldr (2' at Ramps)

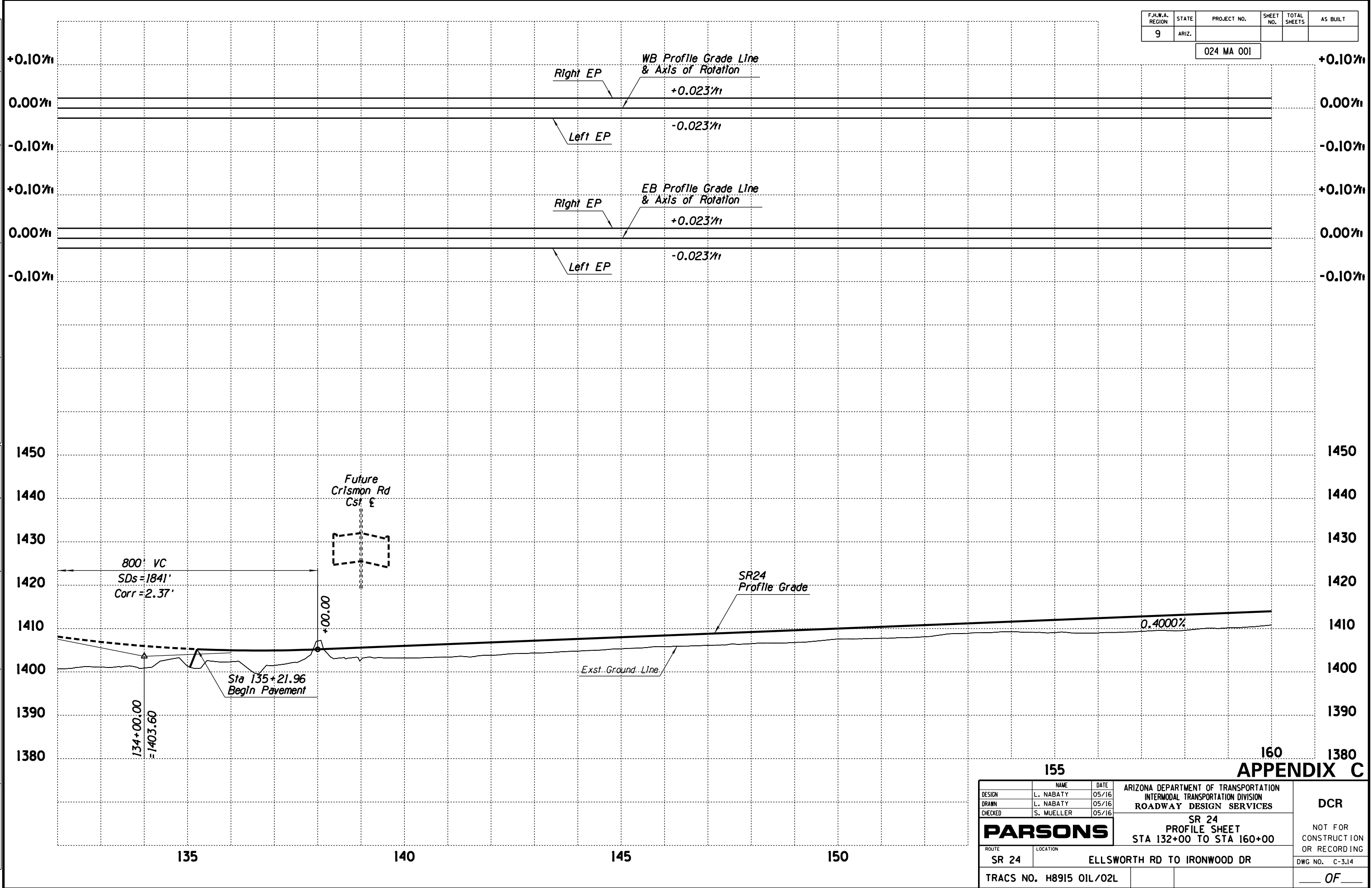
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			INTERIM SR 24 PLAN SHEET STA 132+00 TO STA 160+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.13
TRACS NO. H8915 OIL/02L				OF

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F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SR 24 PROFILE SHEET STA 132+00 TO STA 160+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.14
TRACS NO. H8915 OIL/O2L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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Interim WB Roadway Section

12' Outside Shldr (2' at Ramps)
 12' Lane
 12' Lane
 6' Inside Shldr (2' at Ramps)

Signal Butte Rd Ramp 'A' Cst & Sta 5+20.09 =
 90.53' Lt SR24 Med Cst & Sta 178+06.17
 Nose of Gore Control Point

New Conc Curb & Gutter
 Type C, Std C-05.10

Begin Signal Butte Rd Ramp 'A' Cst & PC Sta 0+00.00 =
 73.00' Lt SR24 Med Cst & Sta 172+81.05

Signal Butte Rd
 Ramp 'A' Cst &

New Drainage Channel
 See Drainage Plans

New R/W

6+85.89
 T 180+87.59

50:1 Taper

S89°30'12"E

N86°15'26"E

Future
 Ultimate SR 24

25:1 Taper

S83°20'02"E

25:1 Taper

New R/W

SR24
 Med Cst &

Signal Butte Rd
 Ramp 'B' Cst &

Sta 179+81.55
 End Pavement

New Conc Curb & Gutter
 Type C, Std C-05.10

PC 171+71.65

Begin Signal Butte Rd Ramp 'B' Cst & POT Sta 0+00.00 =
 73.00' Rt SR24 Med Cst & Sta 172+65.00

Signal Butte Rd Ramp 'B' Cst & Sta 5+89.99 =
 95.53' Rt SR24 Med Cst & Sta 178+48.27
 Nose of Gore Control Point

Future Ultimate Construction

Interim EB Roadway Section

6' Inside Shldr (2' at Ramps)
 12' Lane
 12' Lane
 12' Outside Shldr (2' at Ramps)

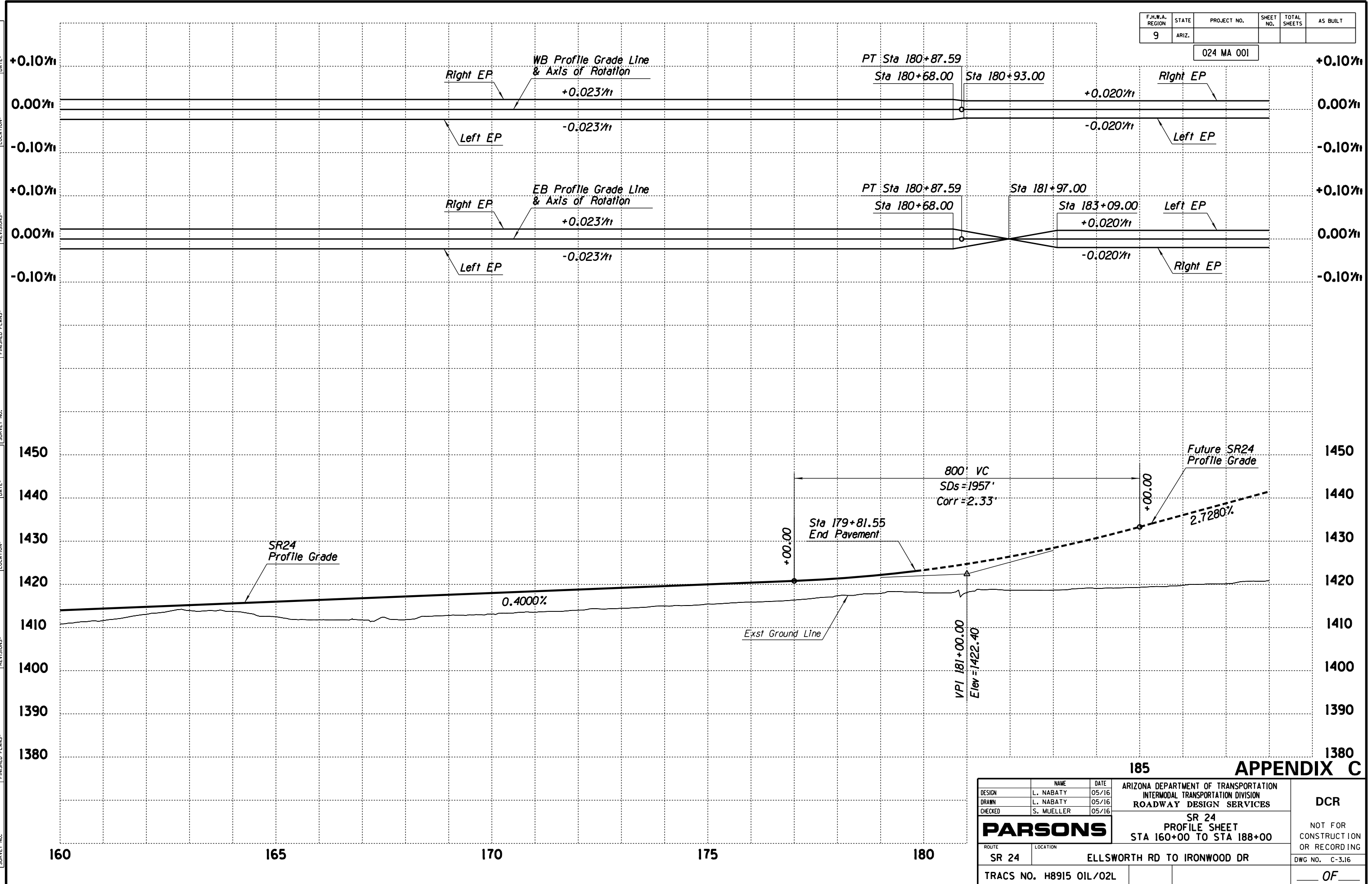
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			INTERIM SR 24 PLAN SHEET STA 160+00 TO STA 188+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.15
TRACS NO. H8915 OIL/02L				OF

DATE: LOCATION: REVISIONS: FINISHED PLANS: SURVEY NO. DATE: LOCATION: REVISIONS: FINISHED PLANS: SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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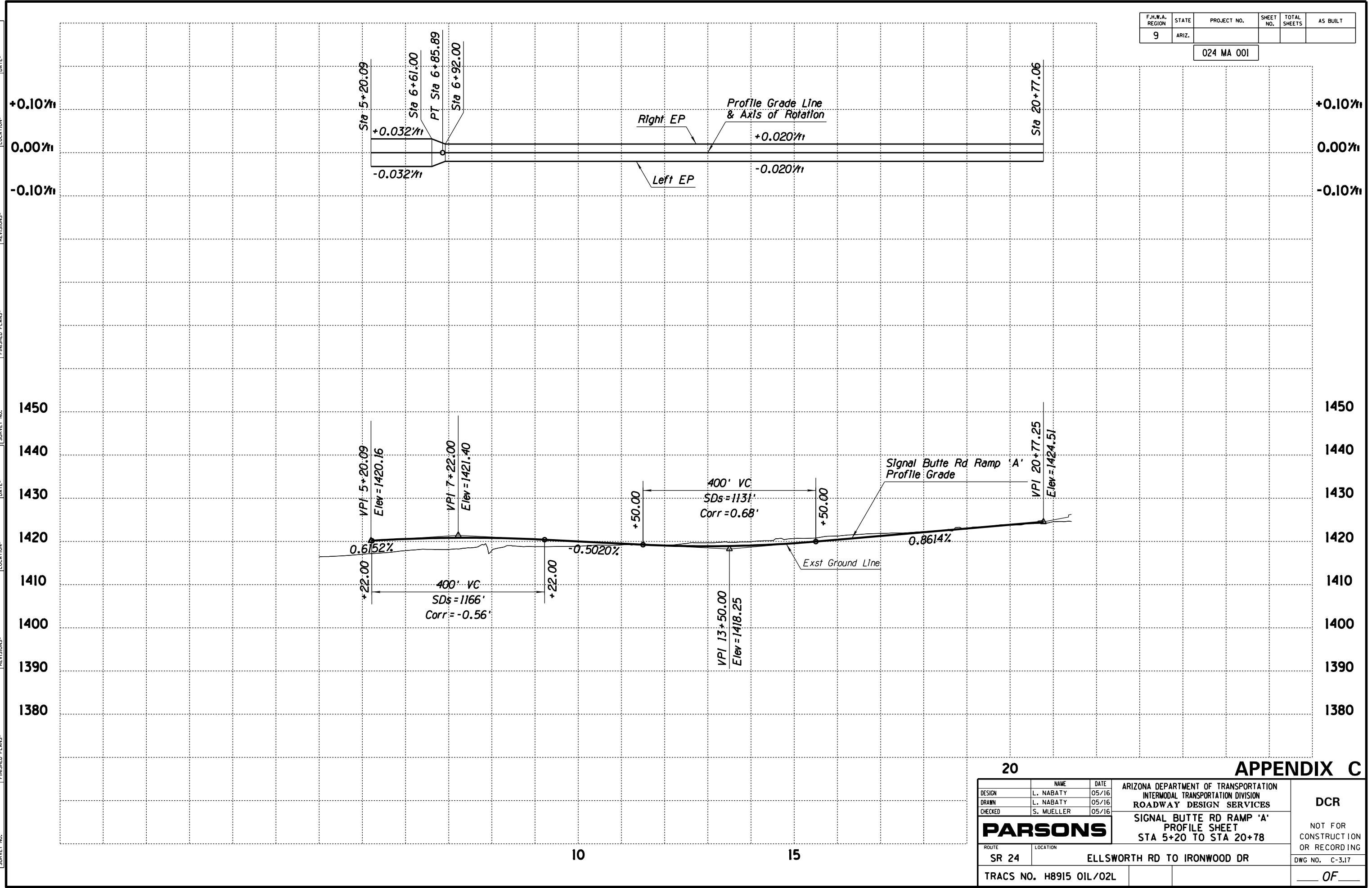


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DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SR 24 PROFILE SHEET STA 160+00 TO STA 188+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.16
TRACS NO. H8915 OIL/02L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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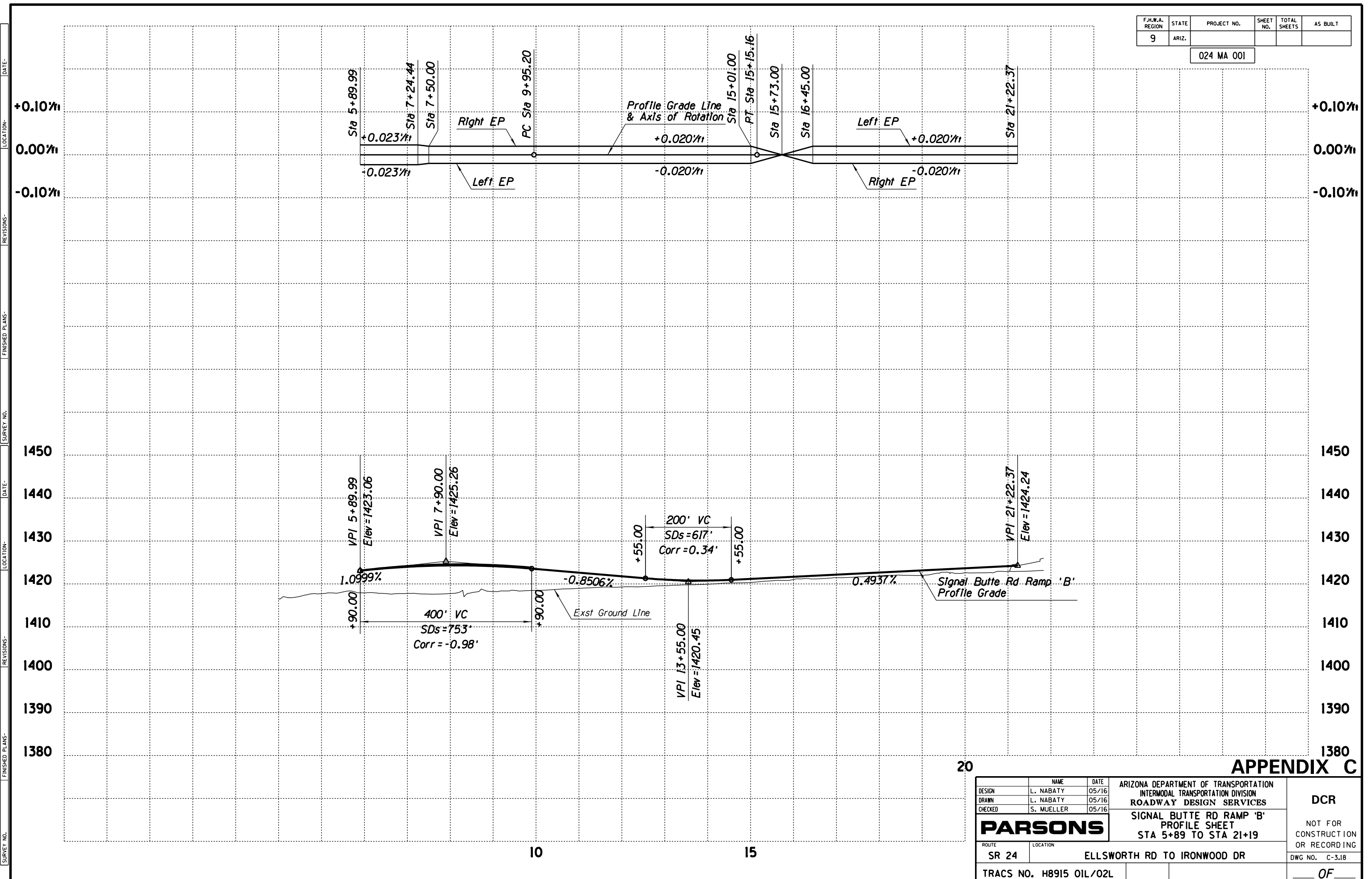
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APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SIGNAL BUTTE RD RAMP 'A' PROFILE SHEET STA 5+20 TO STA 20+78	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.17
TRACS NO. H8915 OIL/02L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SIGNAL BUTTE RD RAMP 'B' PROFILE SHEET STA 5+89 TO STA 21+19	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.18
TRACS NO. H8915 OIL/02L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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Interim WB Roadway Section

12' Outside Shldr (2' at Ramps)
 12' Lane
 12' Lane
 6' Inside Shldr (2' at Ramps)

End Signal Butte Rd Ramp 'C' Cst & PT Sta 18+78.48 =
 73.00' Lt SR24 Med Cst & Sta 213+00.00

Signal Butte Rd Ramp 'C' Cst & Sta 12+78.10 =
 95.53' Lt SR24 Cst & Sta 207+00.19

Nose of Gore Control Point

End Signal Butte Rd Ramp 'D' Cst & PT Sta 18+21.95 =
 73.00' Rt SR24 Med Cst & Sta 212+50.00

Signal Butte Rd Ramp 'D'
 Cst & Sta 13+30.89 =
 90.53' Rt SR24 Med
 Cst & Sta 207+59.35

Nose of Gore Control Point

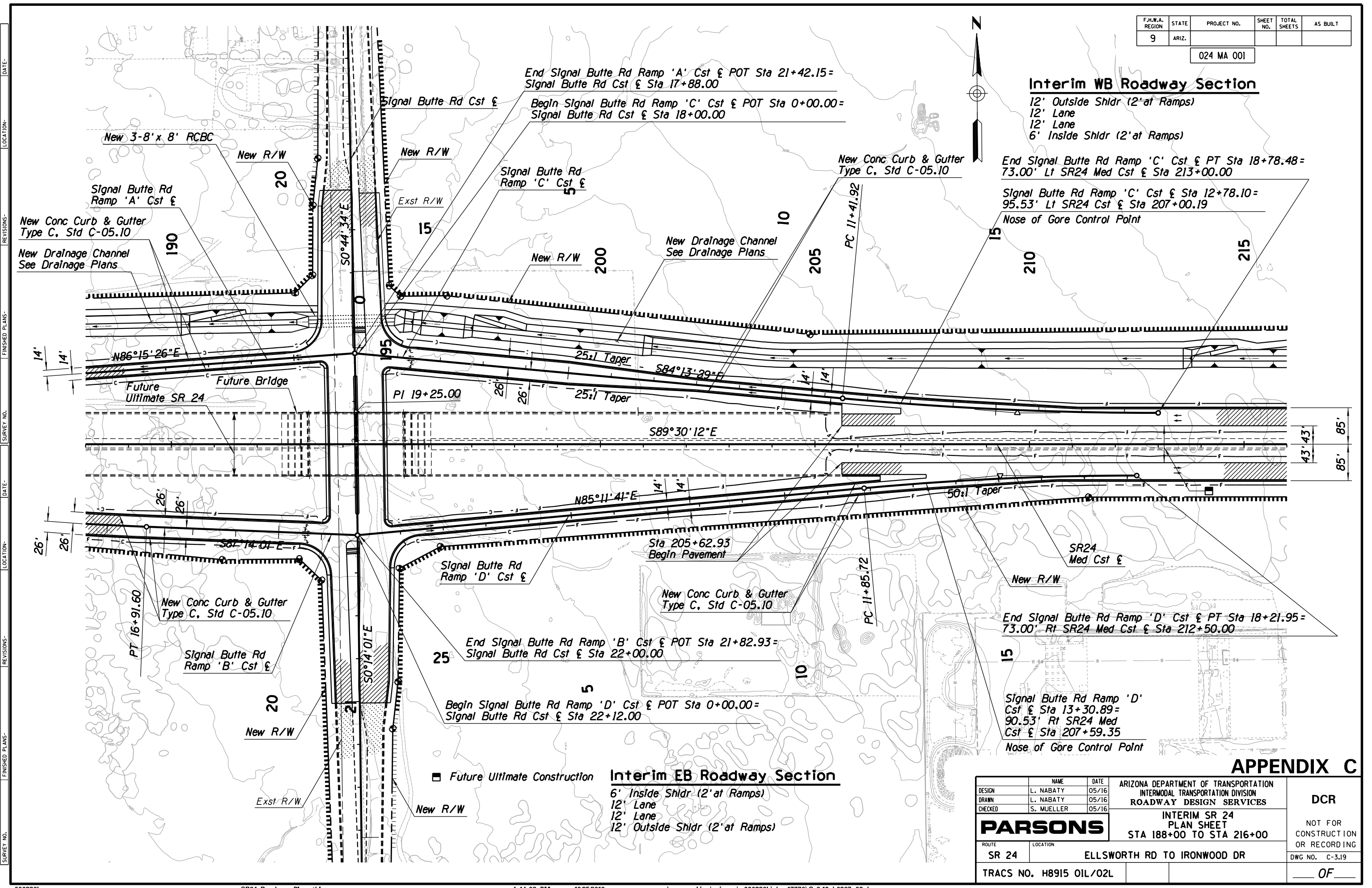
Interim EB Roadway Section

6' Inside Shldr (2' at Ramps)
 12' Lane
 12' Lane
 12' Outside Shldr (2' at Ramps)

Future Ultimate Construction

APPENDIX C

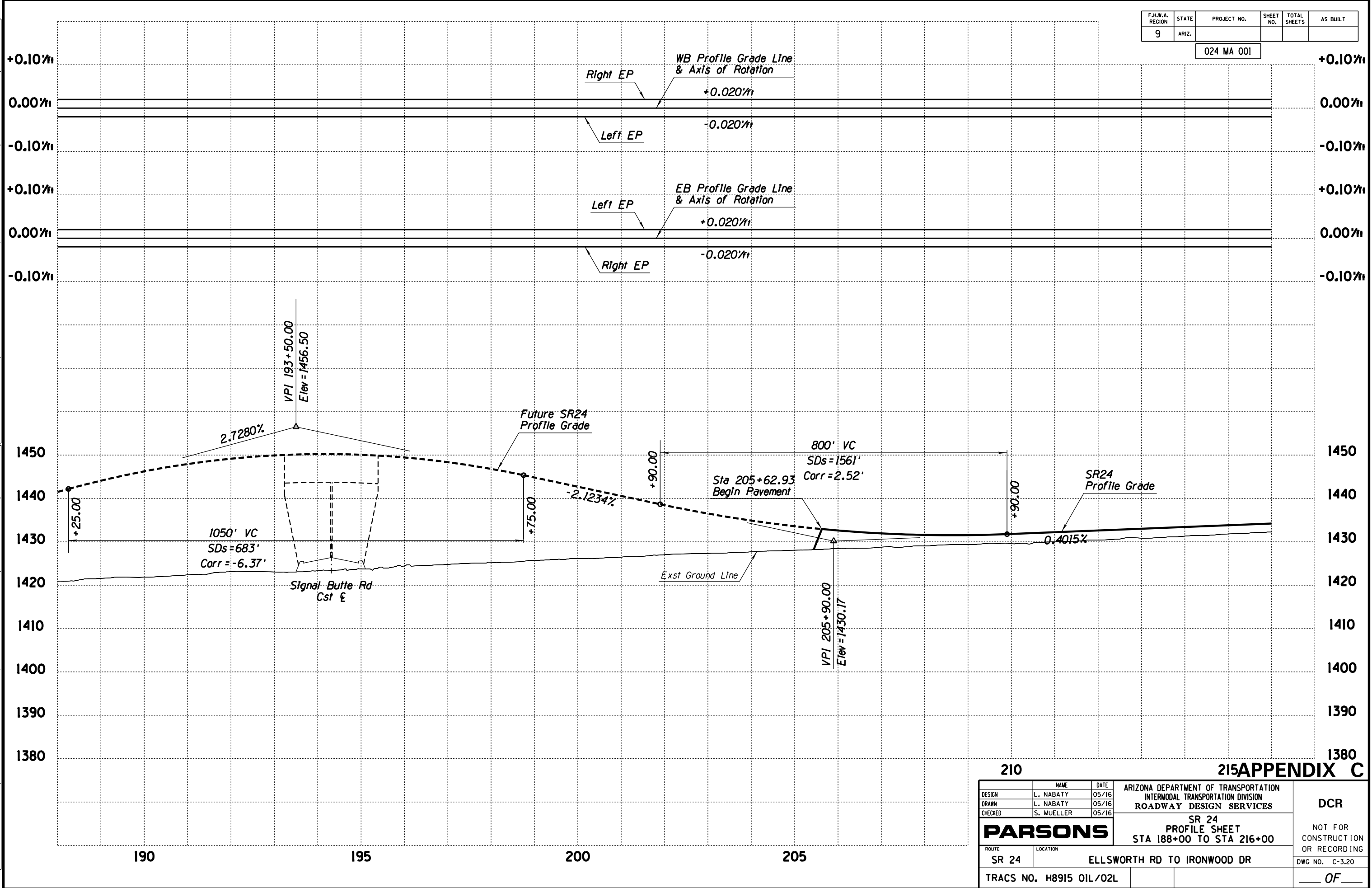
DESIGN	NAME	DATE	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR		
DRAWN	L. NABATY	05/16			INTERIM SR 24 PLAN SHEET STA 188+00 TO STA 216+00	NOT FOR CONSTRUCTION OR RECORDING
CHECKED	S. MUELLER	05/16				
ROUTE LOCATION			ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.19		
TRACS NO. H8915 OIL/O2L				OF		



SURVEY NO. LOCATION DATE FINISHED PLANS REVISIONS DATE SURVEY NO. LOCATION DATE FINISHED PLANS REVISIONS DATE SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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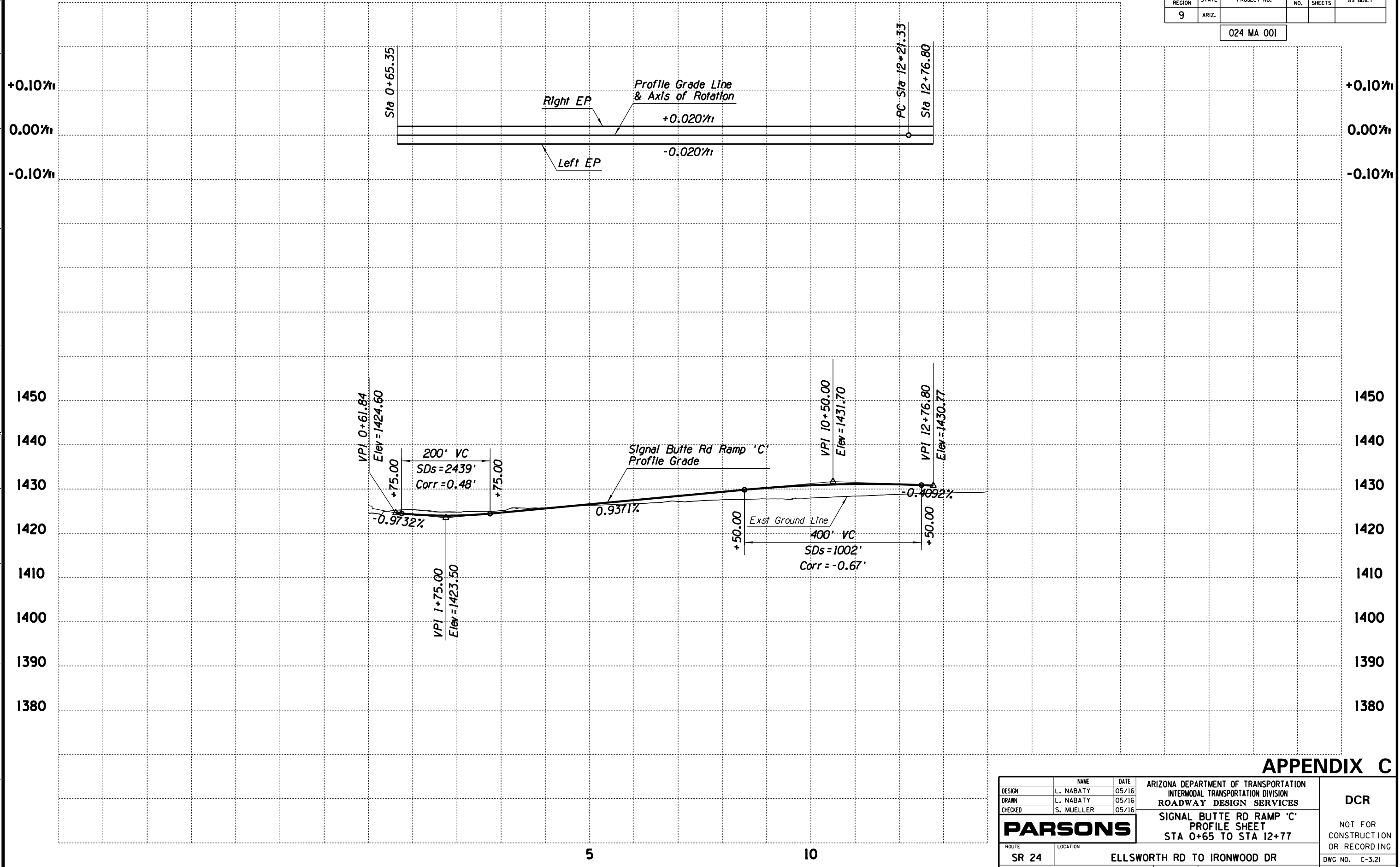


210 215 APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SR 24 PROFILE SHEET STA 188+00 TO STA 216+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.20
TRACS NO. H8915 OIL/O2L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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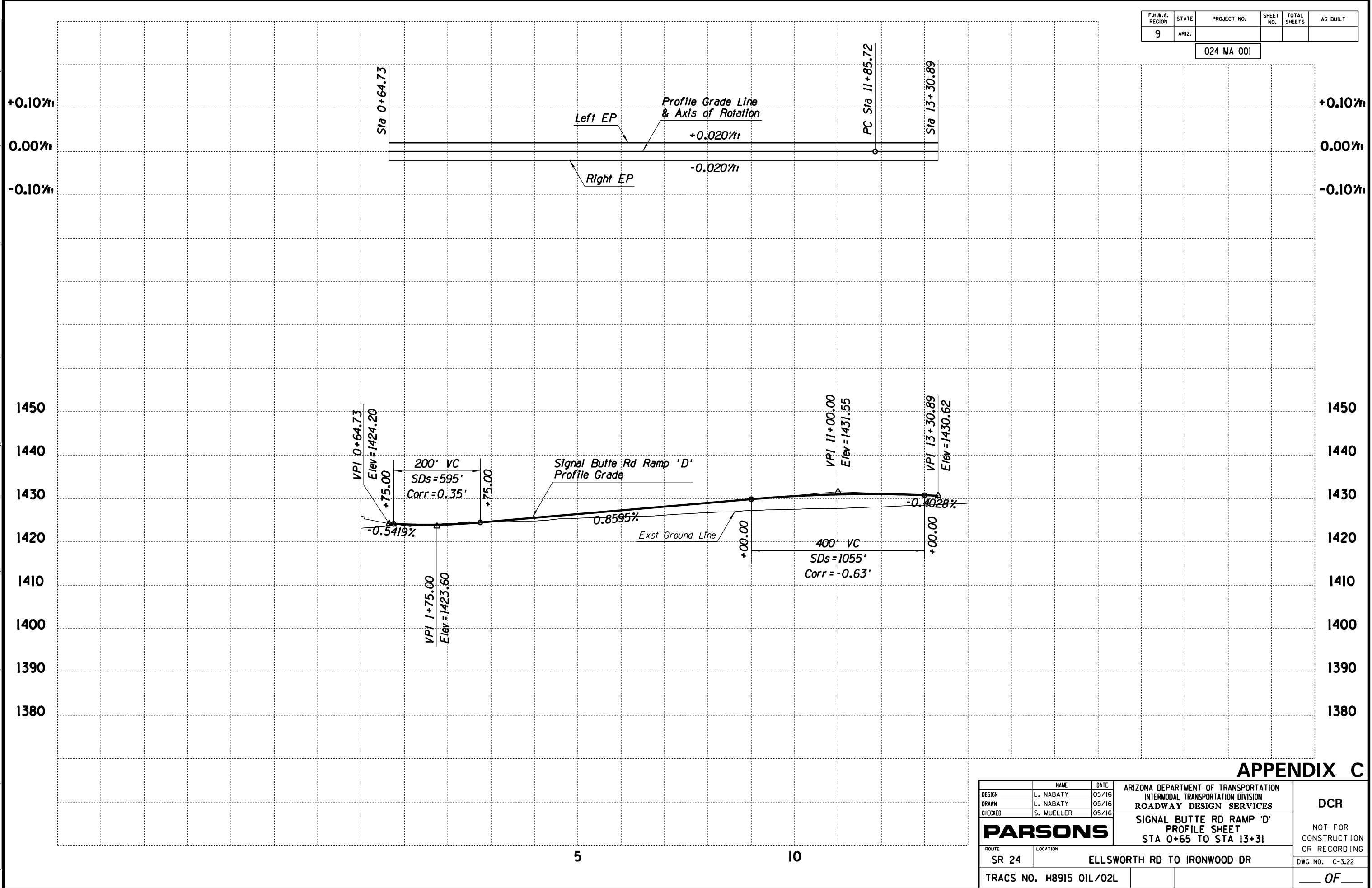
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DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SIGNAL BUTTE RD RAMP 'C' PROFILE SHEET STA 0+65 TO STA 12+77	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.21
TRACS NO. H8915 OIL/02L				OF

DATE: LOCATION: REVISIONS: FINISHED PLANS: SURVEY NO. DATE: LOCATION: REVISIONS: FINISHED PLANS: SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SIGNAL BUTTE RD RAMP 'D' PROFILE SHEET STA 0+65 TO STA 13+31	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.22
TRACS NO. H8915 OIL/02L				OF

SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE FINISHED PLANS SURVEY NO. DATE FINISHED PLANS SURVEY NO. DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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Interim WB Roadway Section

12' Outside Shldr (2' at Ramps)
 12' Lane
 12' Lane
 6' Inside Shldr (2' at Ramps)

Meridian Rd Ramp 'A' Cst & Sta 4+91.07 =
 90.53' Lt SR24 Med Cst & Sta 232+90.65
 Nose of Gore Control Point

New Drainage Channel
 See Drainage Plans

New Conc Curb & Gutter
 Type C, Std C-05.10

New Conc Half Barrier
 Std

Meridian Rd
 Ramp 'A' Cst &

Begin Meridian Rd Ramp 'A' Cst & PC Sta 0+00.00 =
 73.00' Lt SR24 Med Cst & Sta 228+00.00

Sta 234+88.46
 End Pavement

50:1 Taper

N85°29'30"E

Future
 Ultimate SR 24

S89°30'12"E

S84°32'10"E

25:1 Taper

25:1 Taper

SR24
 Med Cst &

New Bridge

Begin Meridian Rd Ramp 'B' Cst & PC Sta 0+00.00 =
 73.00' Rt SR24 Med Cst & Sta 227+50.00

Mountain Rd Cst &

New R/W

Meridian Rd Ramp 'B' Cst & Sta 6+00.38 =
 95.53' Rt SR24 Med Cst & Sta 233+49.81
 Nose of Gore Control Point

New Conc Curb & Gutter
 Type C, Std C-05.10

Meridian Rd
 Ramp 'B' Cst &

Future Ultimate Construction

Interim EB Roadway Section

6' Inside Shldr (2' at Ramps)
 12' Lane
 12' Lane
 12' Outside Shldr (2' at Ramps)

POE 28+87.90

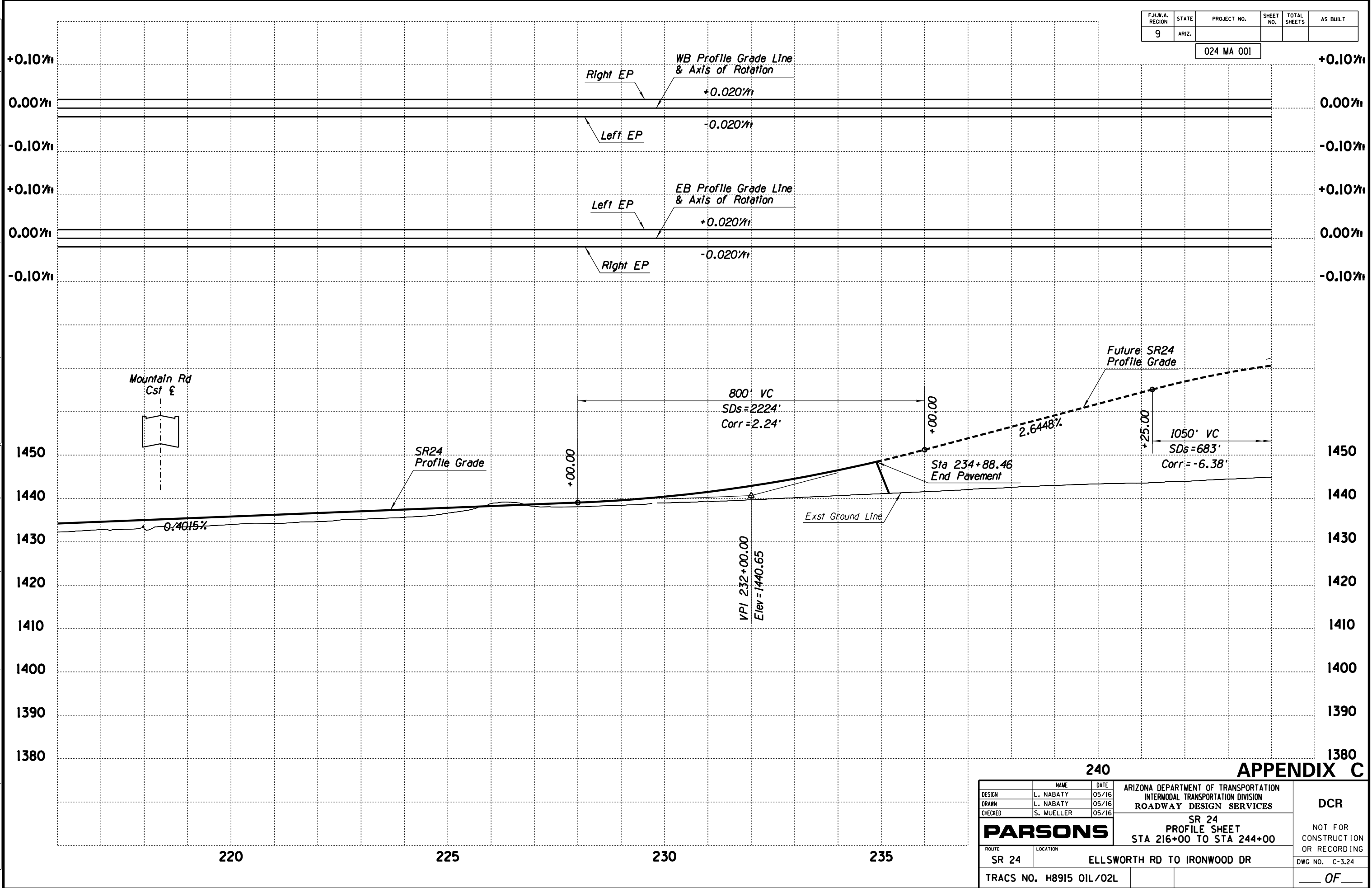
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			INTERIM SR 24 PLAN SHEET STA 216+00 TO STA 244+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.23
TRACS NO. H8915 OIL/02L				OF

SURVEY NO. FINISHED PLANS DATE LOCATION REVISIONS FINISHED PLANS DATE SURVEY NO. FINISHED PLANS DATE LOCATION REVISIONS FINISHED PLANS DATE SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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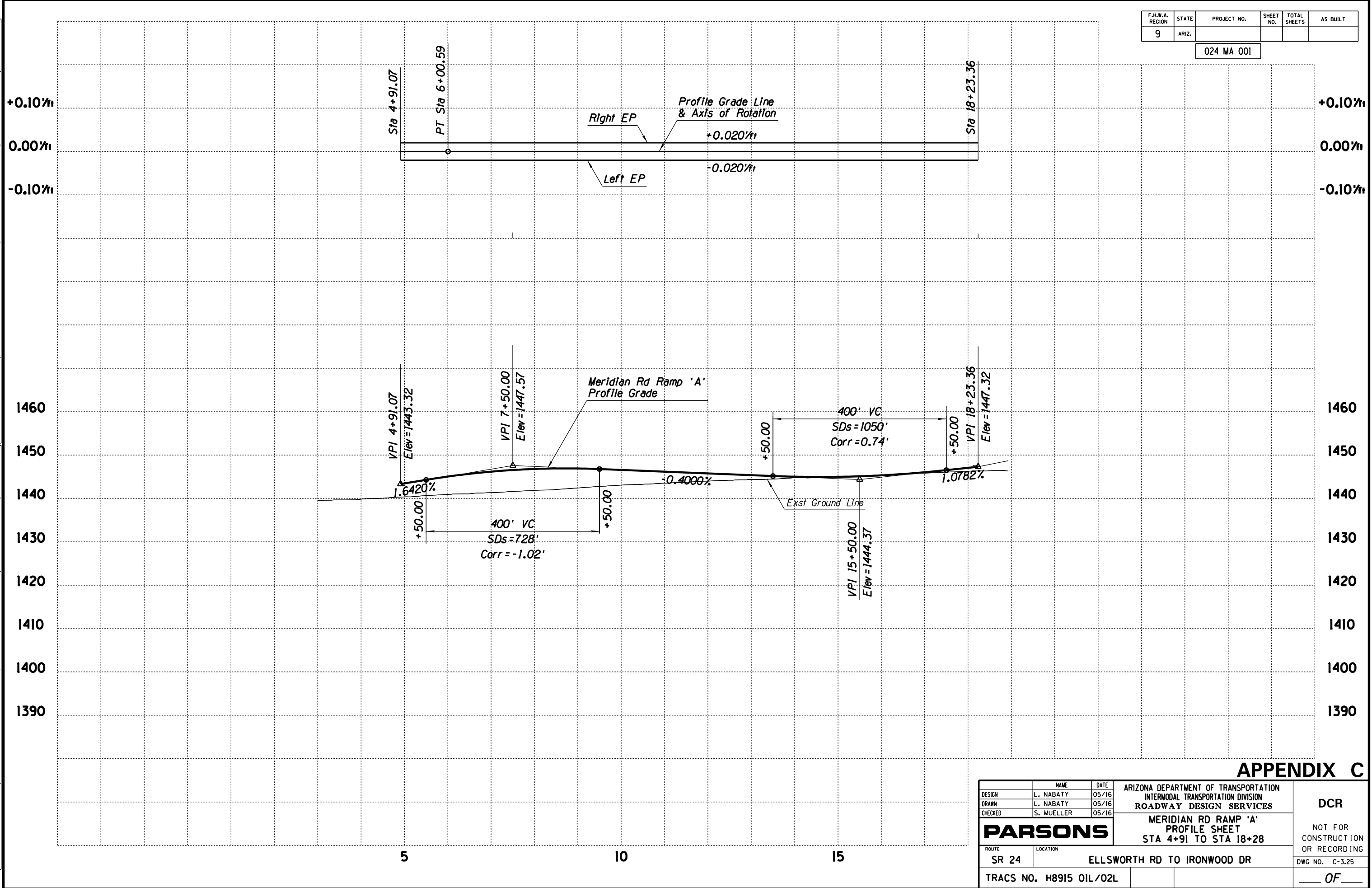
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DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SR 24 PROFILE SHEET STA 216+00 TO STA 244+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.24
TRACS NO. H8915 OIL/O2L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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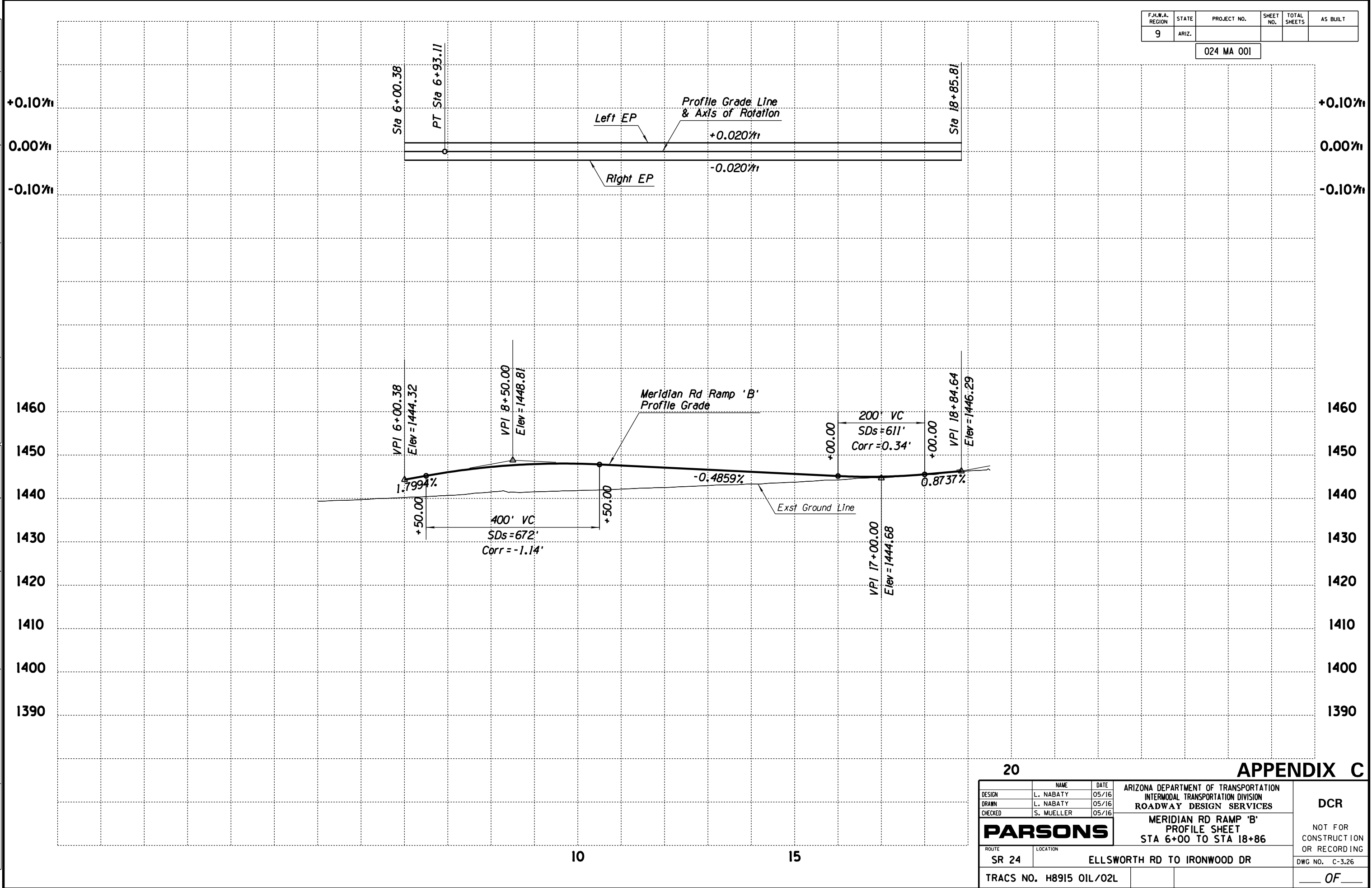
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			MERIDIAN RD RAMP 'A' PROFILE SHEET STA 4+91 TO STA 18+28	
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.25
TRACS NO. H8915 OIL/02L				OF

SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE
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F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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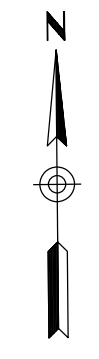
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APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			MERIDIAN RD RAMP 'B' PROFILE SHEET STA 6+00 TO STA 18+86	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.26
TRACS NO. H8915 OIL/O2L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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Interim WB Roadway Section

12' Outside Shldr (2' at Ramps)
 12' Lane
 12' Lane
 6' Inside Shldr (2' at Ramps)

End Meridian Rd Ramp 'C' Cst & PT Sta 22+16.48 =
 73.00' Lt SR24 Med Cst & Sta 269+00.00

Meridian Rd Ramp 'C' Cst & Sta 16+09.86 =
 95.52' Lt SR24 Med Cst & Sta 262+93.93

Nose of Gore Control Point

New Drainage Channel
 See Drainage Plans

New Conc Curb & Gutter
 Type C, Std C-05.10

Interim EB Roadway Section

6' Inside Shldr (2' at Ramps)
 12' Lane
 12' Lane
 12' Outside Shldr (2' at Ramps)

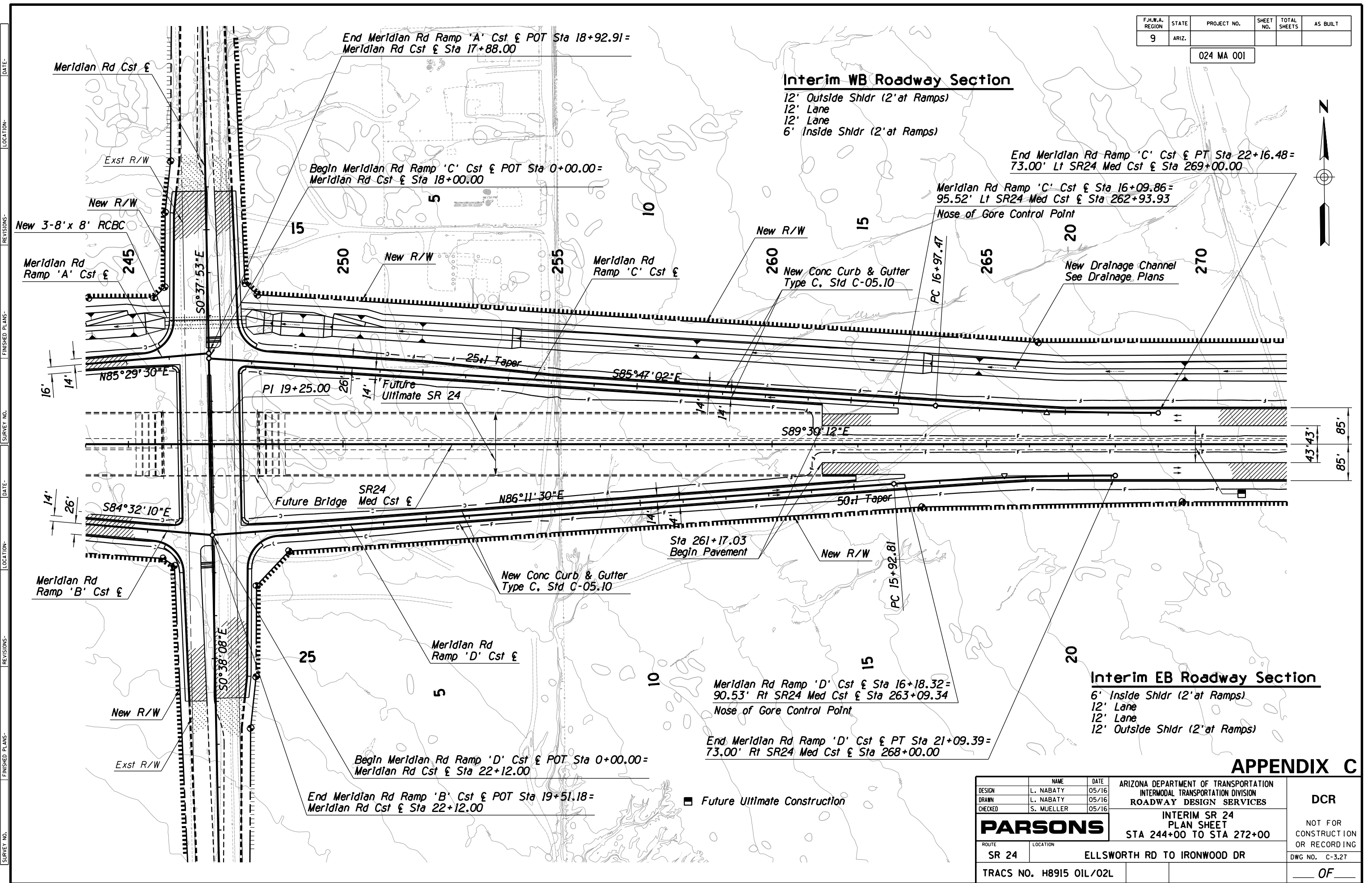
Meridian Rd Ramp 'D' Cst & Sta 16+18.32 =
 90.53' Rt SR24 Med Cst & Sta 263+09.34

Nose of Gore Control Point

End Meridian Rd Ramp 'D' Cst & PT Sta 21+09.39 =
 73.00' Rt SR24 Med Cst & Sta 268+00.00

APPENDIX C

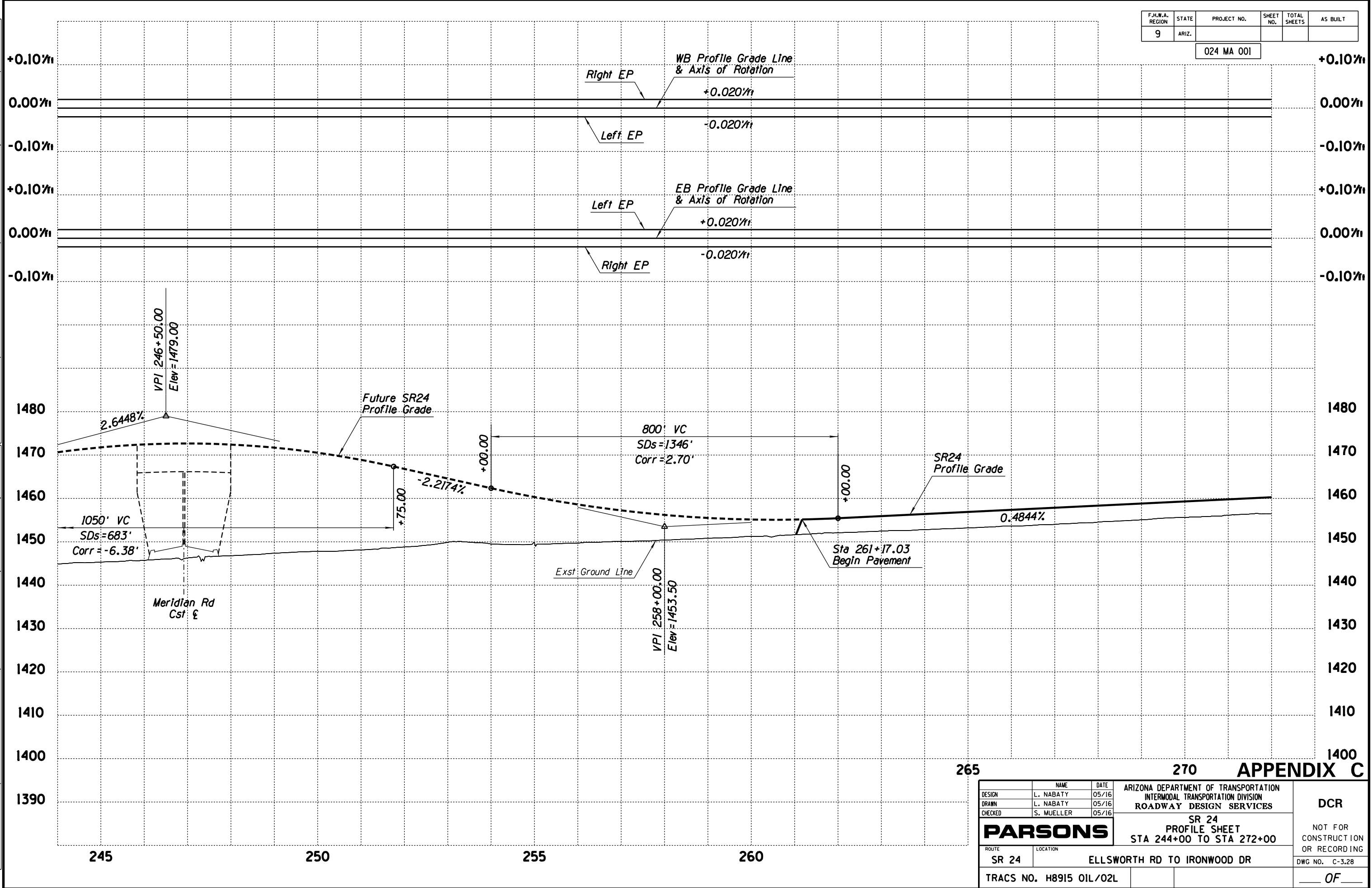
DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			INTERIM SR 24 PLAN SHEET STA 244+00 TO STA 272+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.27
TRACS NO. H8915 OIL/02L				OF



SURVEY NO. LOCATION DATE FINISHED PLANS REVISIONS LOCATION DATE FINISHED PLANS SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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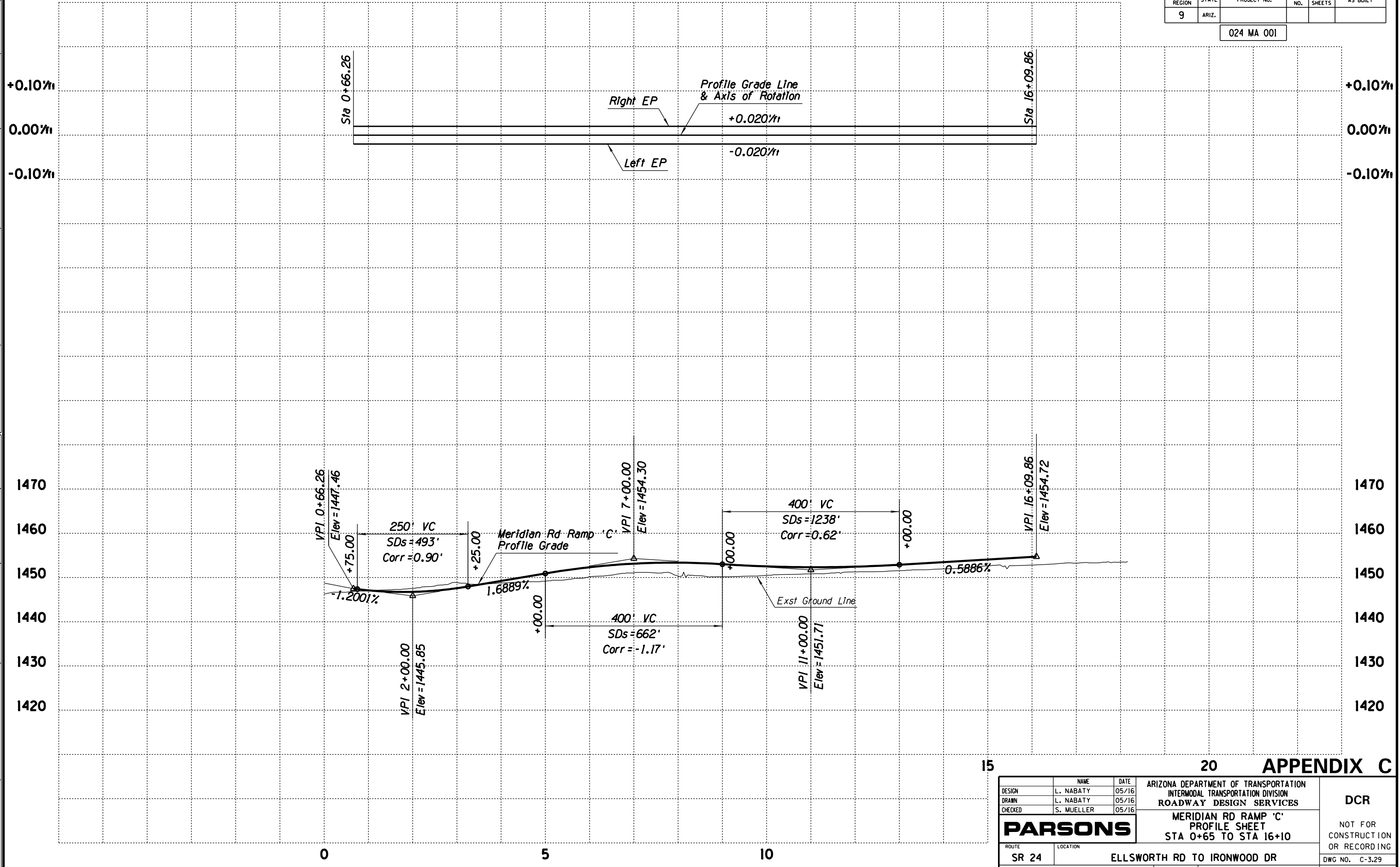
265 270 APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SR 24 PROFILE SHEET STA 244+00 TO STA 272+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.28
TRACS NO. H8915 OIL/O2L				OF

SURVEY NO. FINISHED PLANS DATE LOCATION REVISIONS FINISHED PLANS DATE SURVEY NO. FINISHED PLANS DATE LOCATION REVISIONS FINISHED PLANS DATE SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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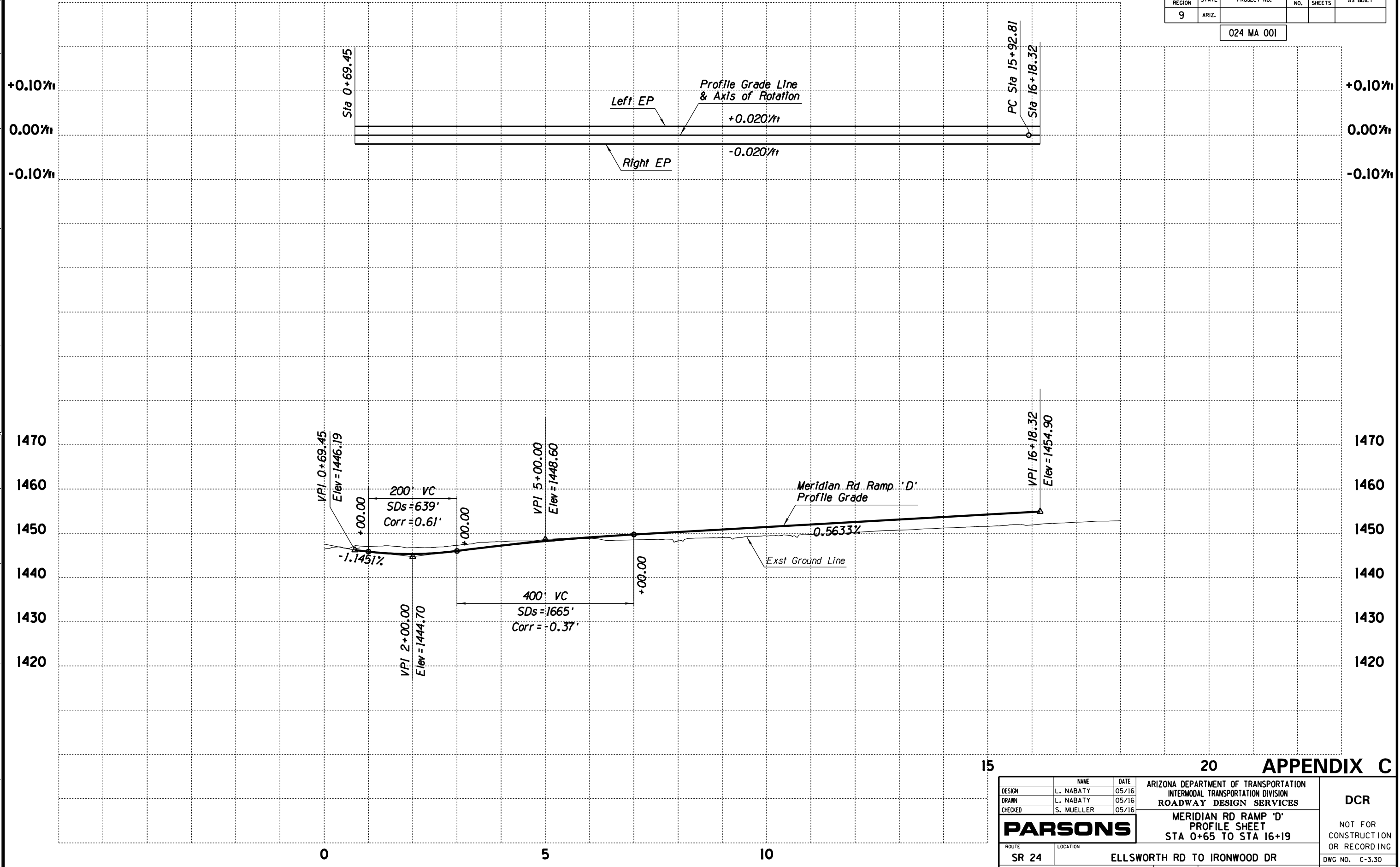
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DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			MERIDIAN RD RAMP 'C' PROFILE SHEET STA 0+65 TO STA 16+10	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.29
TRACS NO. H8915 OIL/O2L				OF

DATE LOCATION REVISIONS SURVEY NO. DATE LOCATION REVISIONS SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE
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DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			MERIDIAN RD RAMP 'D' PROFILE SHEET STA 0+65 TO STA 16+19	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.30
TRACS NO. H8915 OIL/O2L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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Interim WB Roadway Section

12' Outside Shldr (2' at Ramps)
 12' Lane
 12' Lane
 6' Inside Shldr (2' at Ramps)

Ironwood Dr Ramp 'A' Cst & Sta 4+91.07 =
 90.53' Lt SR24 Med Cst & Sta 291+40.65
 Nose of Gore Control Point

New Conc Curb & Gutter
 Type C, Std C-05.10

Begin Ironwood Dr Ramp 'A' Cst & PC Sta 0+00.00 =
 73.00' Lt SR24 Med Cst & Sta 286+50.00

STA 293+57.55
 END PAVEMENT

275

280

285

290

295

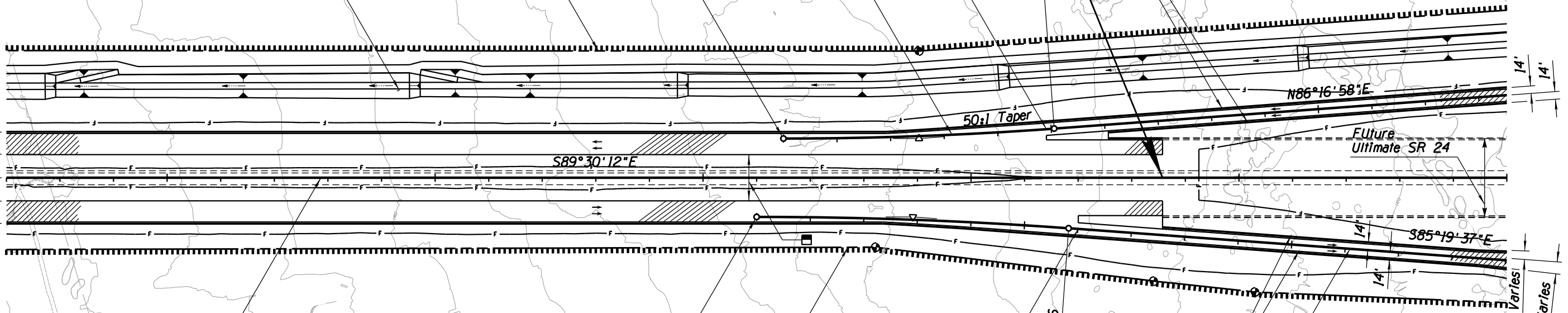
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New Drainage Channel
 See Drainage Plans

New R/W

Ironwood Dr
 Ramp 'A' Cst &

PT 5+05.65
 5



SR24
 Med Cst &

Begin Ironwood Dr Ramp 'B' Cst & PC Sta 0+00.00 =
 73.00' Rt SR24 Med Cst & Sta 286+00.00

New R/W

Ironwood Dr Ramp 'B' Cst & Sta 6+00.62 =
 95.53' Rt SR24 Med Cst & Sta 292+00.05
 Nose of Gore Control Point

New Conc Curb & Gutter
 Type C, Std C-05.10

PT 5+82.76
 5

Ironwood Dr
 Ramp 'B' Cst &

APPENDIX C

■ Future Ultimate Construction

Interim EB Roadway Section

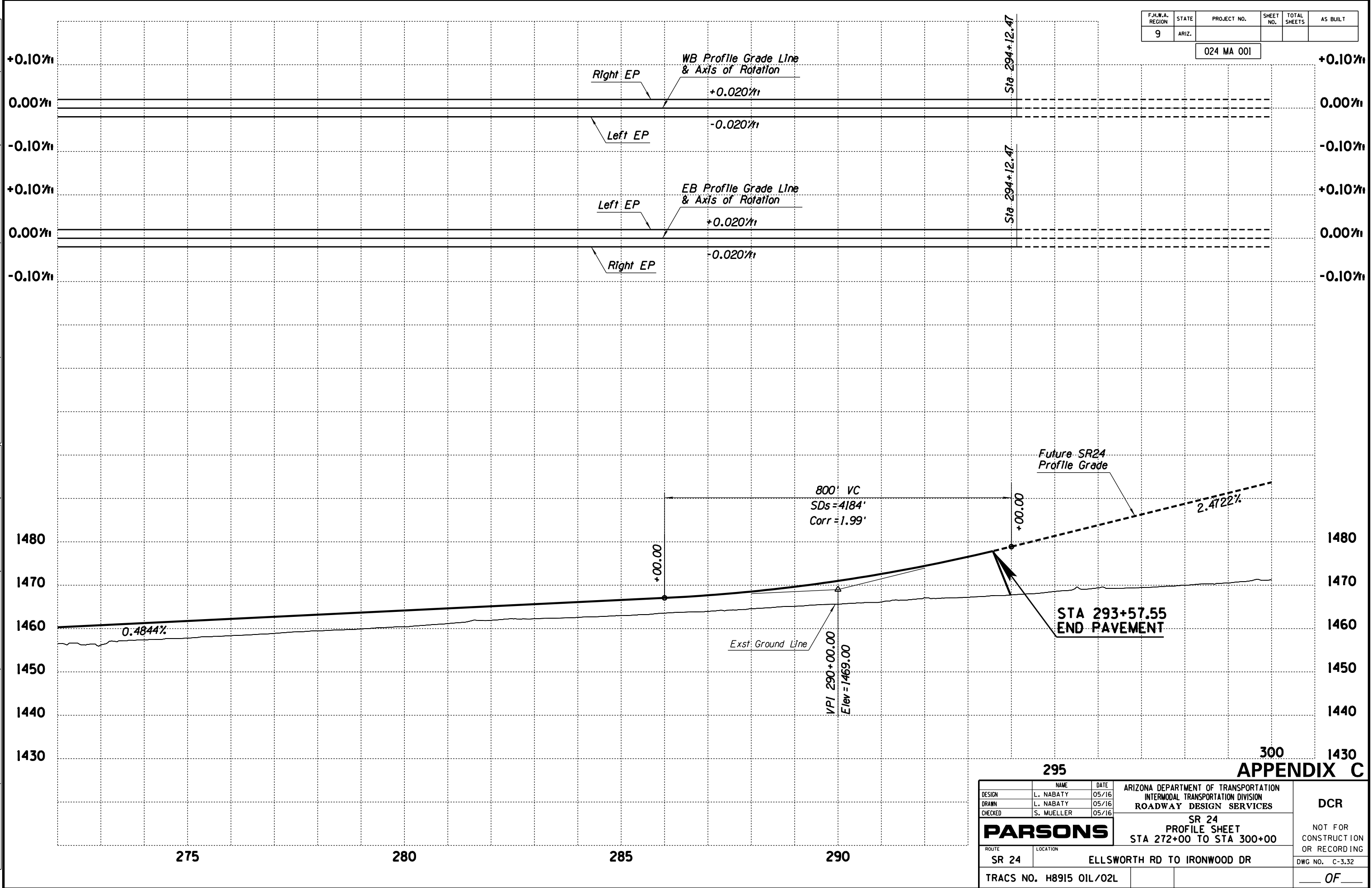
6' Inside Shldr (2' at Ramps)
 12' Lane
 12' Lane
 12' Outside Shldr (2' at Ramps)

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			INTERIM SR 24 PLAN SHEET STA 272+00 TO STA 300+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.31
TRACS NO. H8915 OIL/O2L				OF

SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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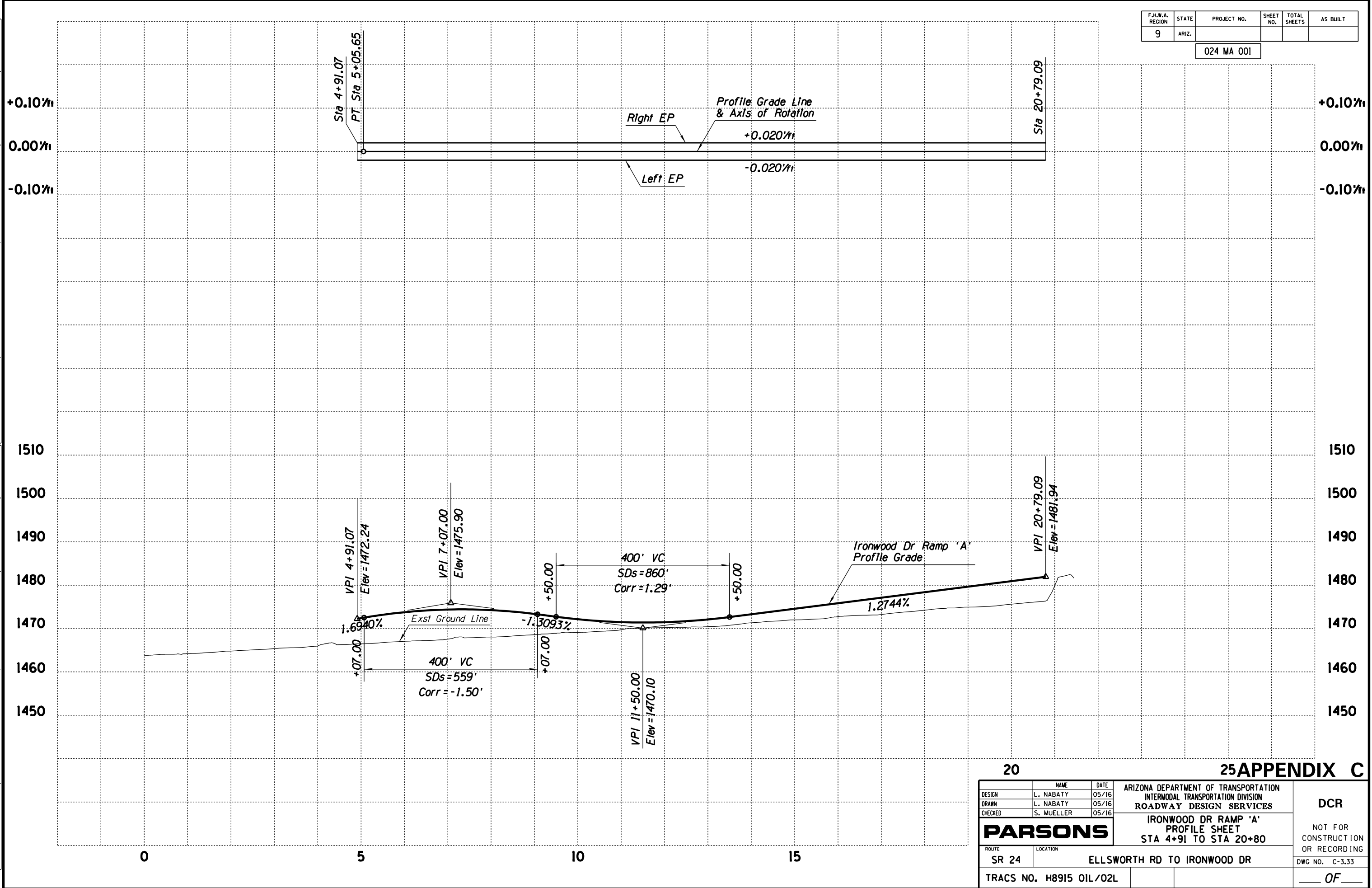


DESIGN		L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN		L. NABATY	05/16		
CHECKED		S. MUELLER	05/16		
PARSONS		SR 24 PROFILE SHEET STA 272+00 TO STA 300+00		NOT FOR CONSTRUCTION OR RECORDING	
ROUTE	LOCATION	ELLSWORTH RD TO IRONWOOD DR			DWG NO. C-3.32
TRACS NO. H8915 OIL/02L					OF

SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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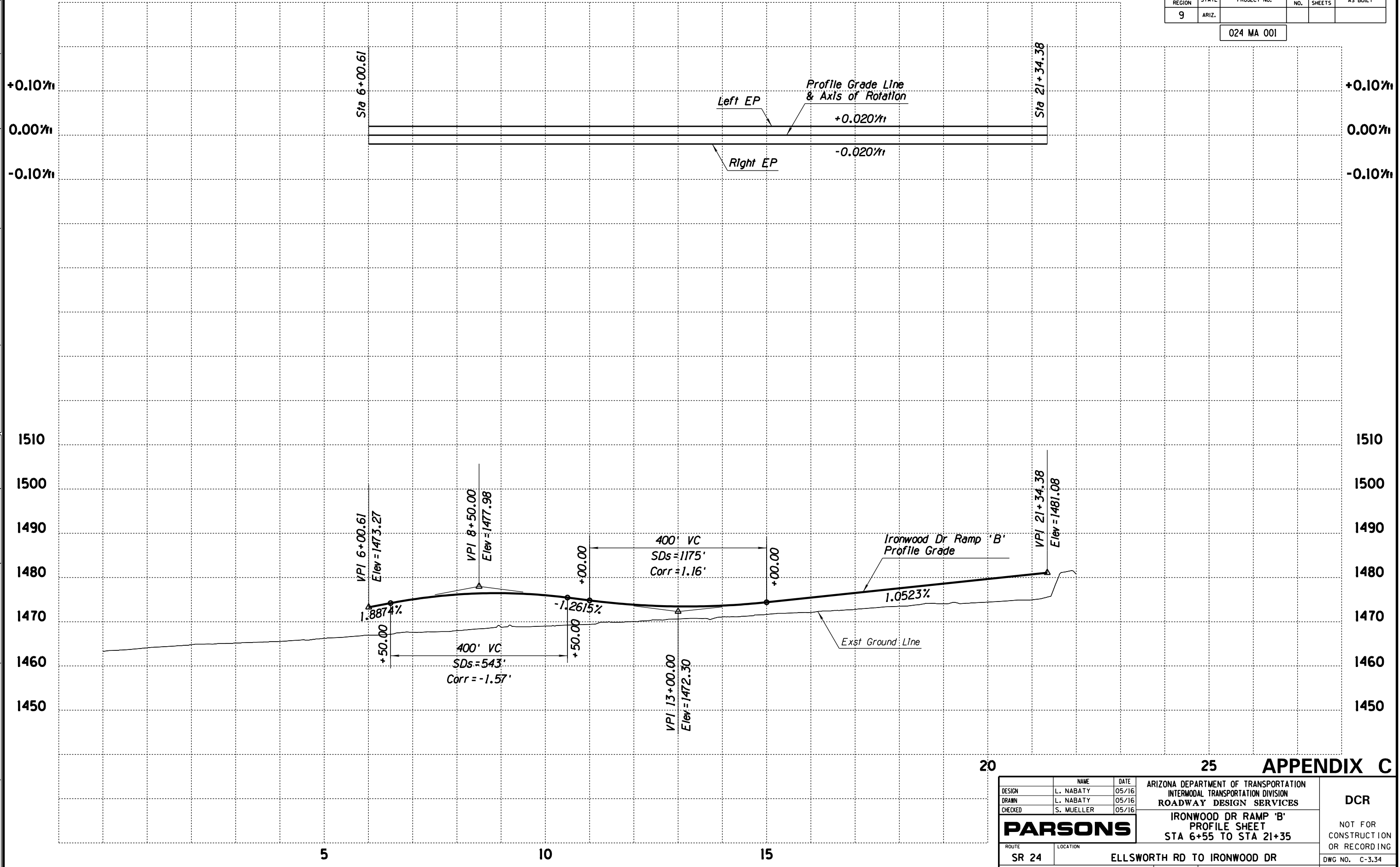
SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE

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DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			IRONWOOD DR RAMP 'A' PROFILE SHEET STA 4+91 TO STA 20+80	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.33
TRACS NO. H8915 OIL/O2L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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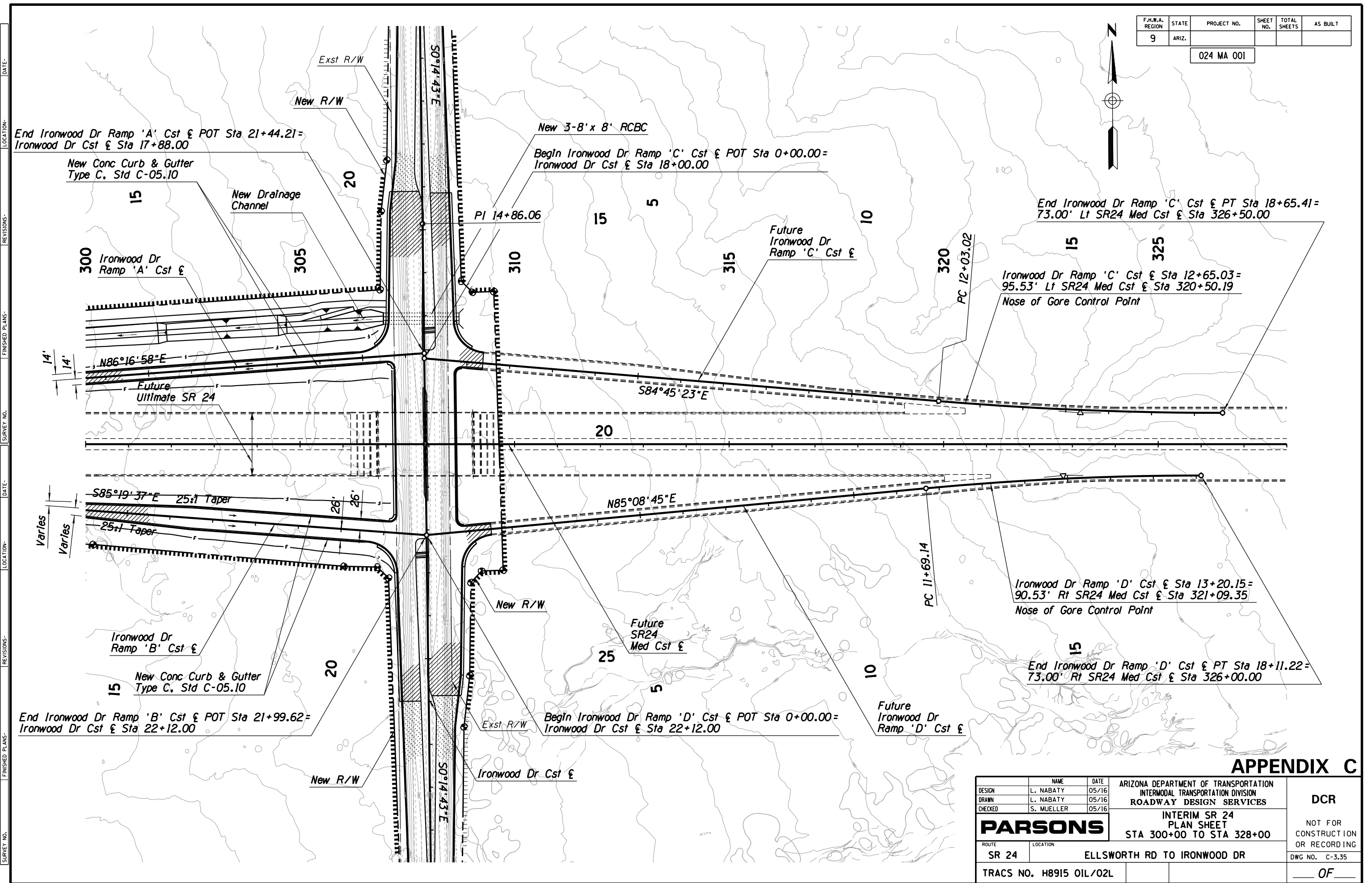
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DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			IRONWOOD DR RAMP 'B' PROFILE SHEET STA 6+55 TO STA 21+35	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.34
TRACS NO. H8915 OIL/O2L				OF

SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE FINISHED PLANS SURVEY NO. DATE REVISIONS LOCATION DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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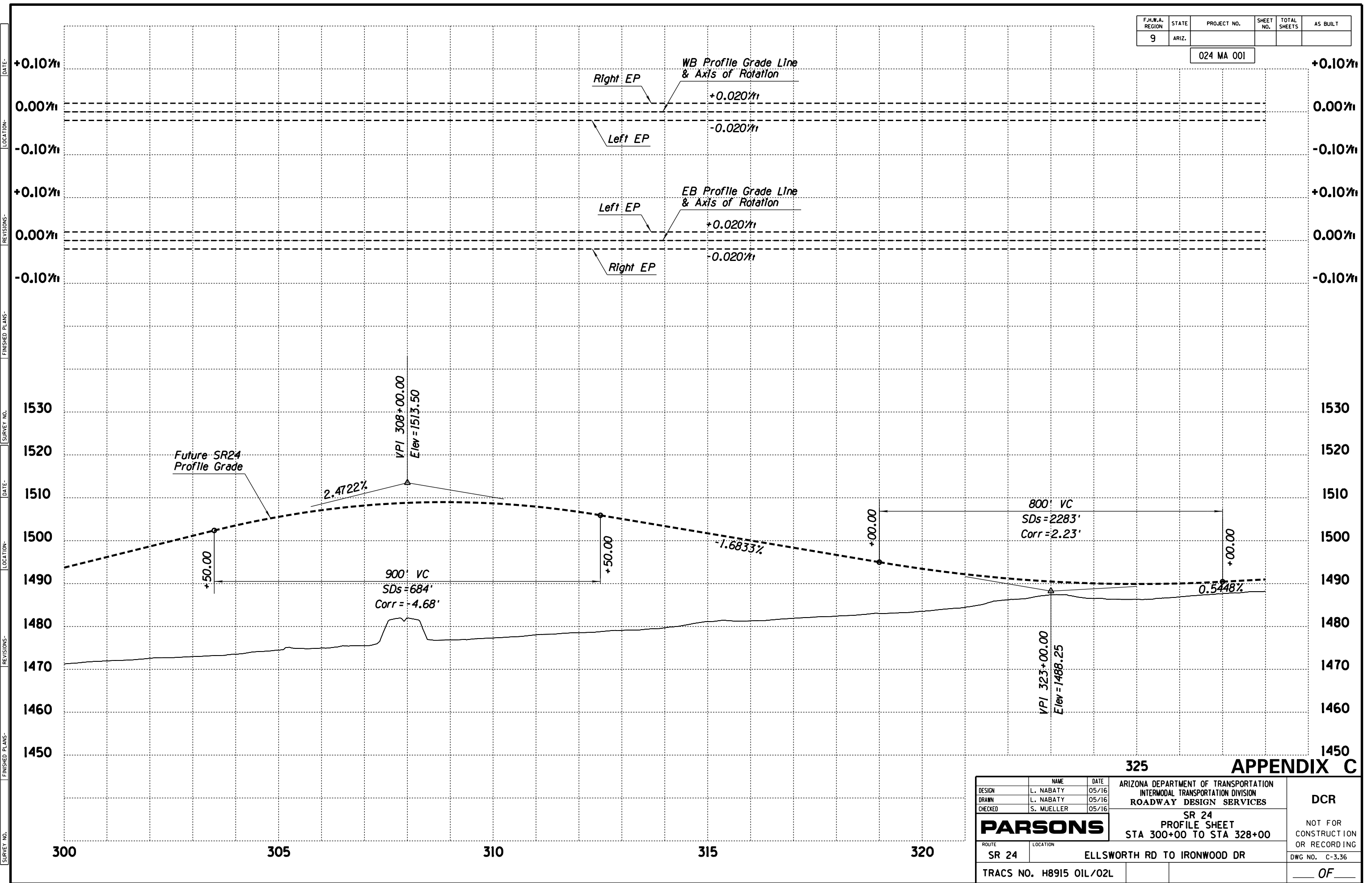


APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			INTERIM SR 24 PLAN SHEET STA 300+00 TO STA 328+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.35
TRACS NO. H8915 OIL/02L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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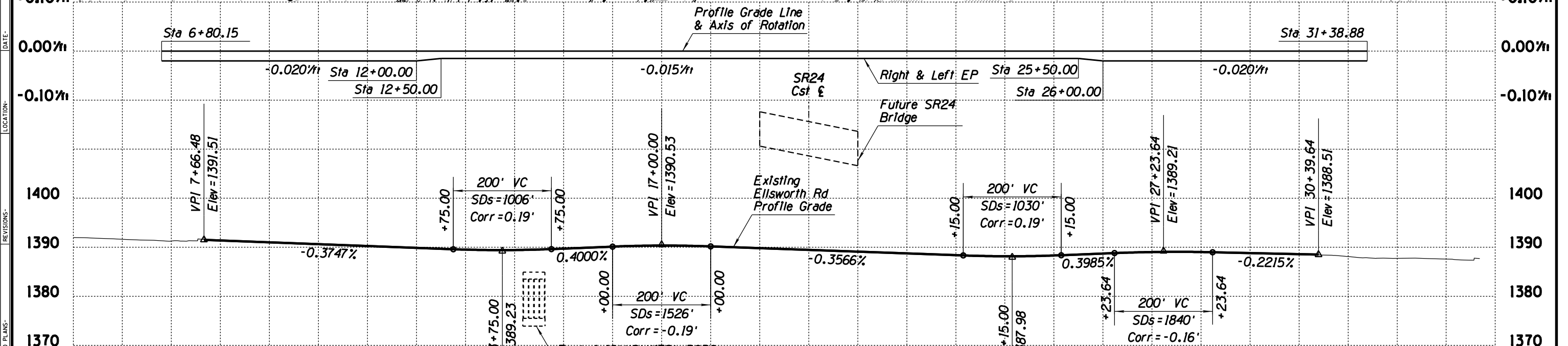
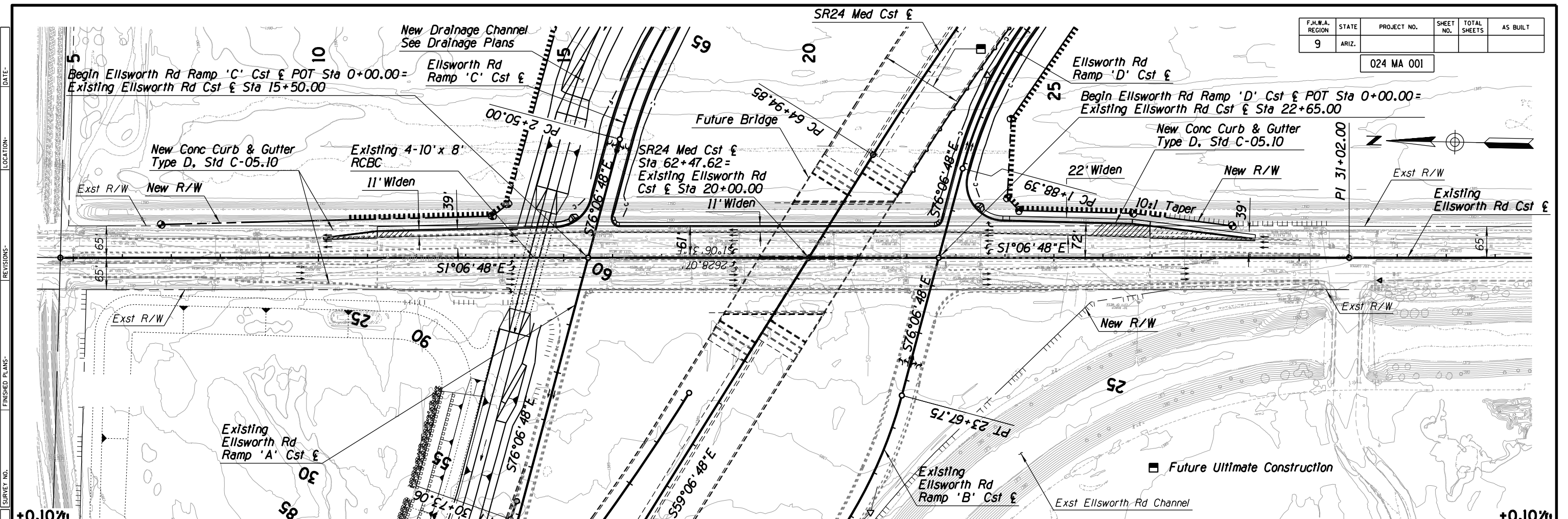


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DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SR 24 PROFILE SHEET STA 300+00 TO STA 328+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-3.36
TRACS NO. H8915 OIL/O2L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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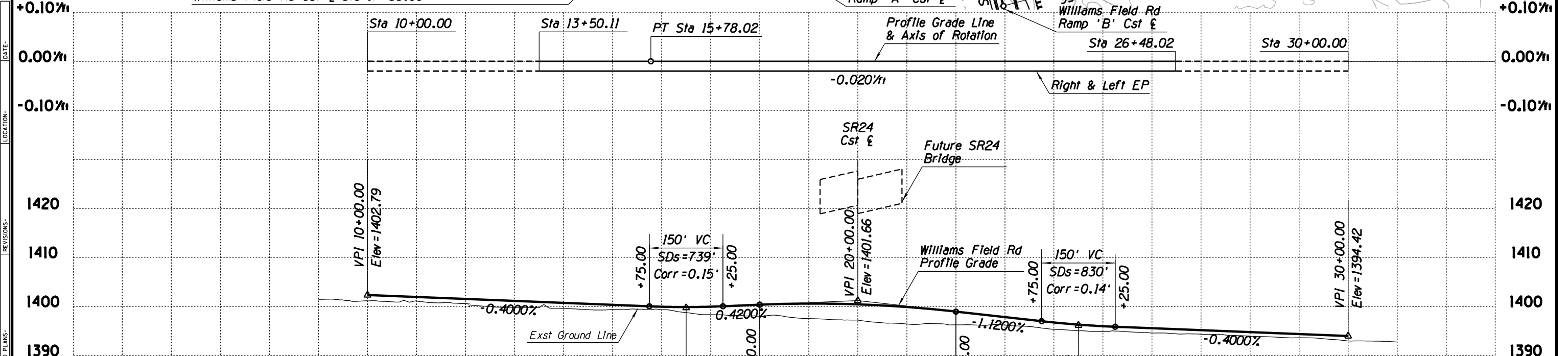
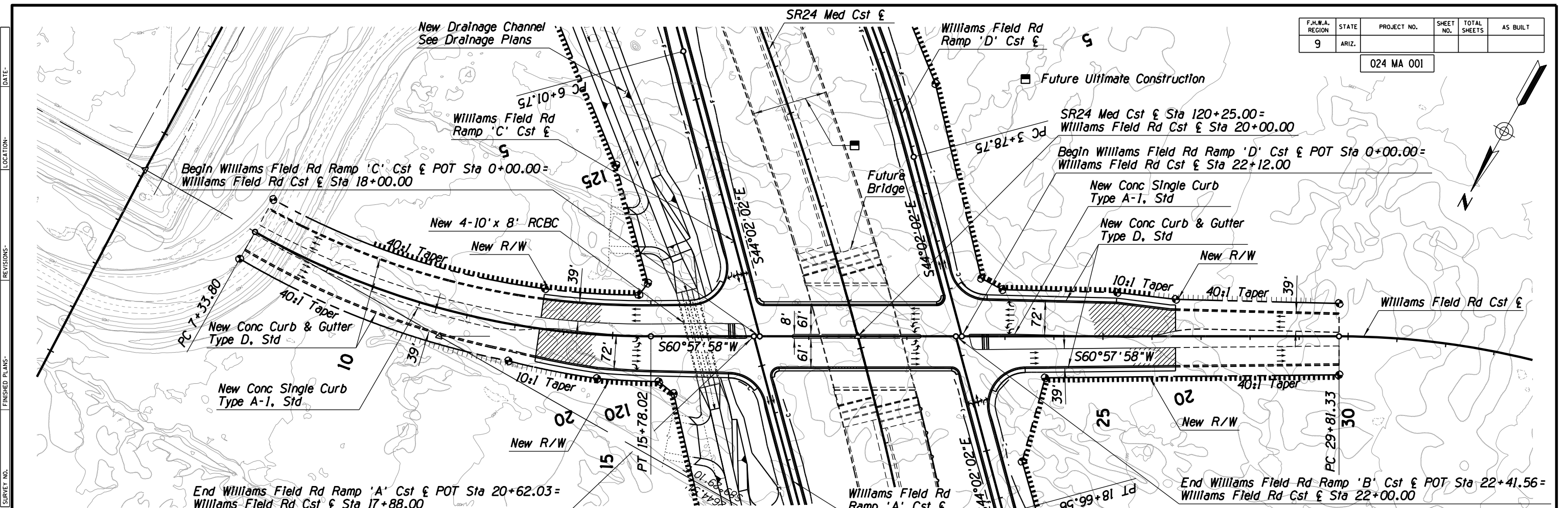


APPENDIX C

DESIGN	NAME	DATE	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			ELLSWORTH ROAD PLAN AND PROFILE SHEET	
ROUTE	LOCATION	NOT FOR CONSTRUCTION OR RECORDING		
SR 24	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-4.01		
TRACS NO. H8915 OIL/O2L		OF		

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

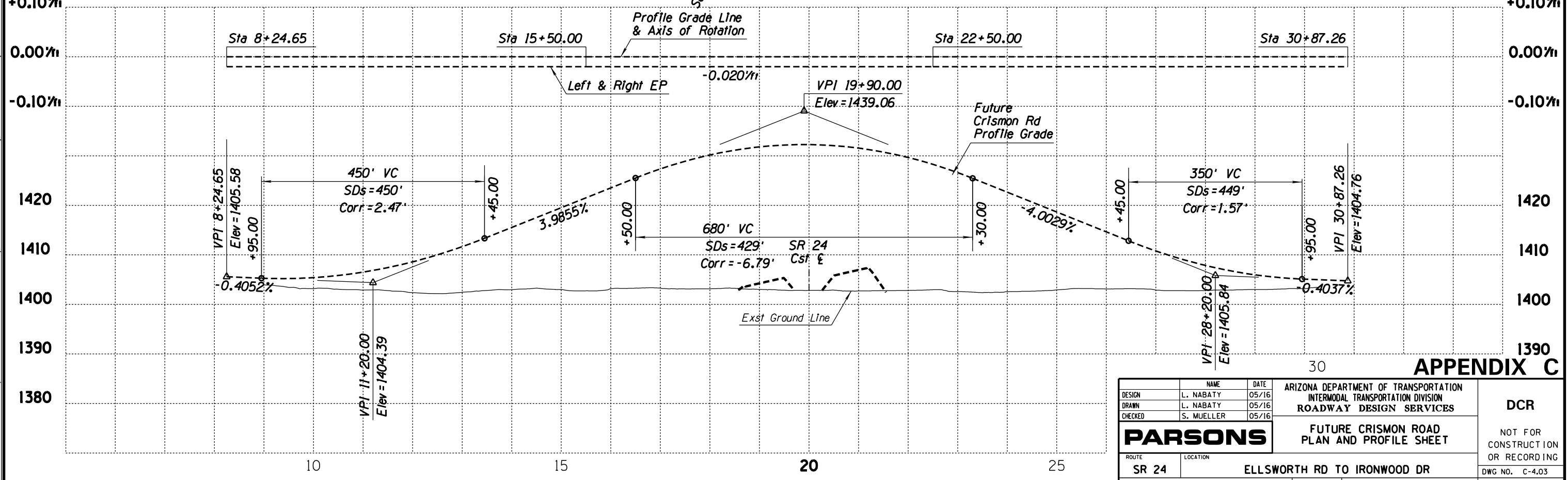
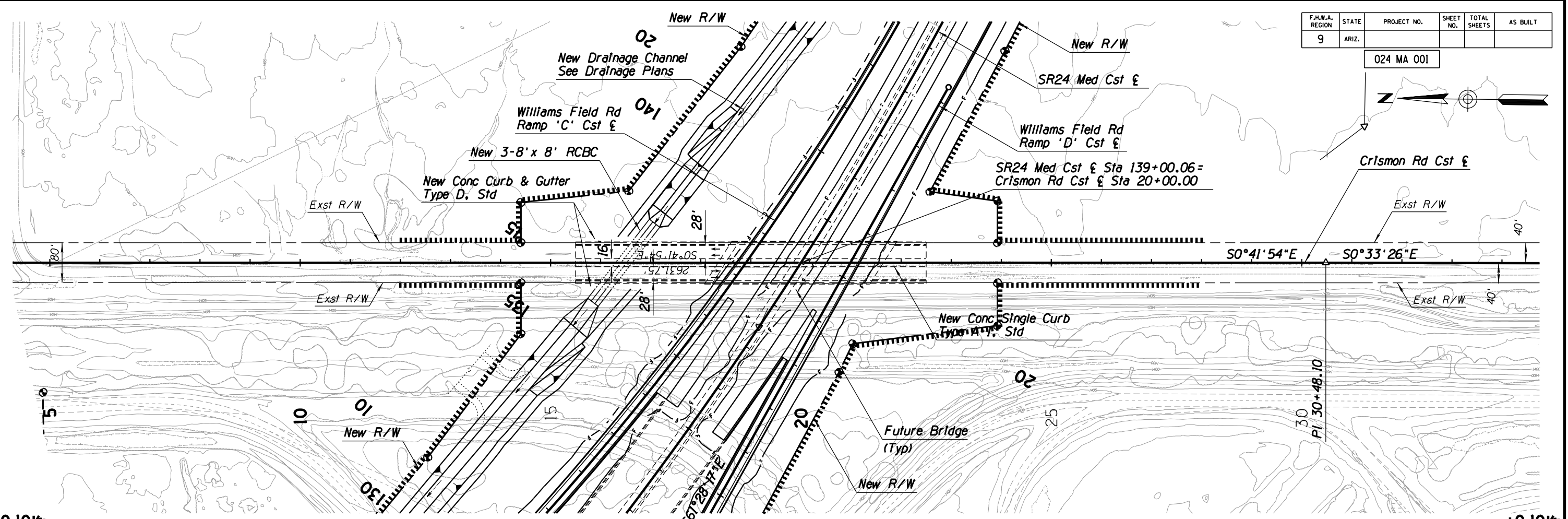
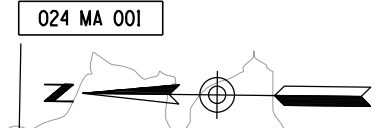
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APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			WILLIAMS FIELD ROAD PLAN AND PROFILE SHEET	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-4.02
TRACS NO. H8915 OIL/02L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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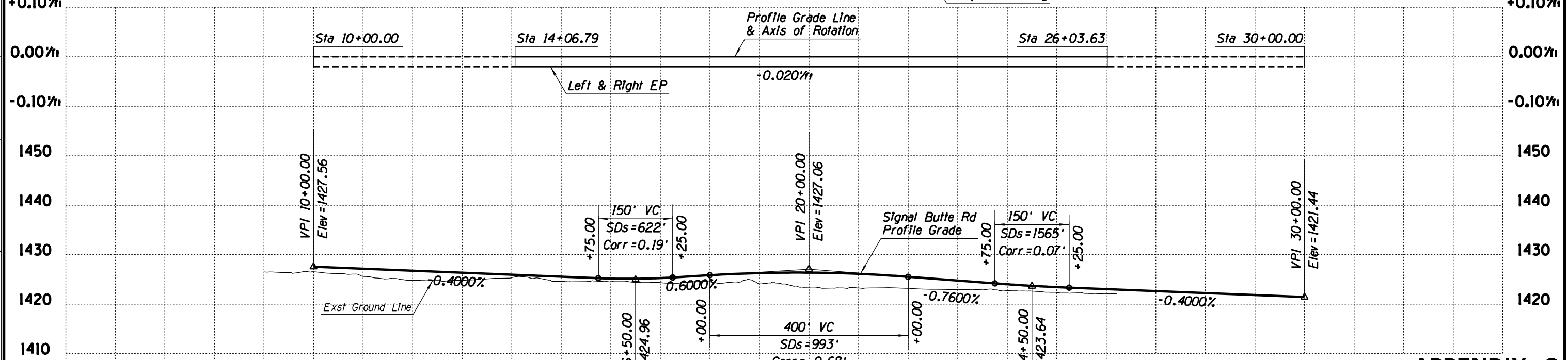
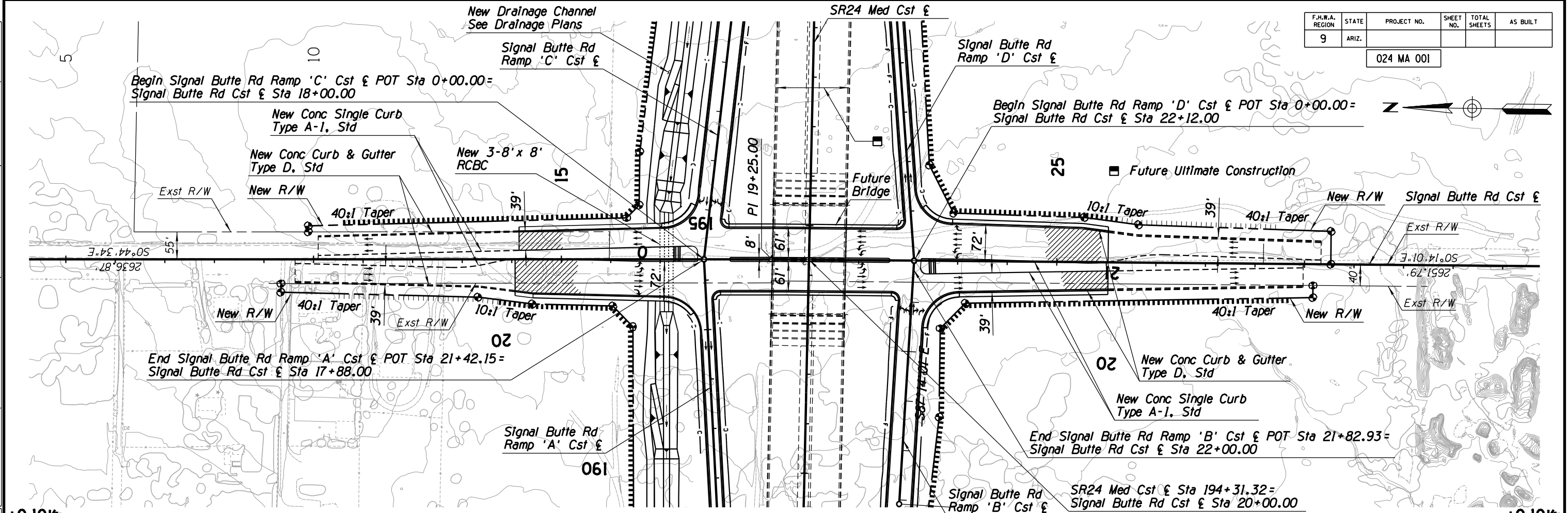
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			FUTURE CRISMON ROAD PLAN AND PROFILE SHEET	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-4.03
TRACS NO. H8915 OIL/O2L				OF

SURVEY NO. FINISHED PLANS DATE REVISIONS LOCATION DATE FINISHED PLANS SURVEY NO. REVISIONS LOCATION DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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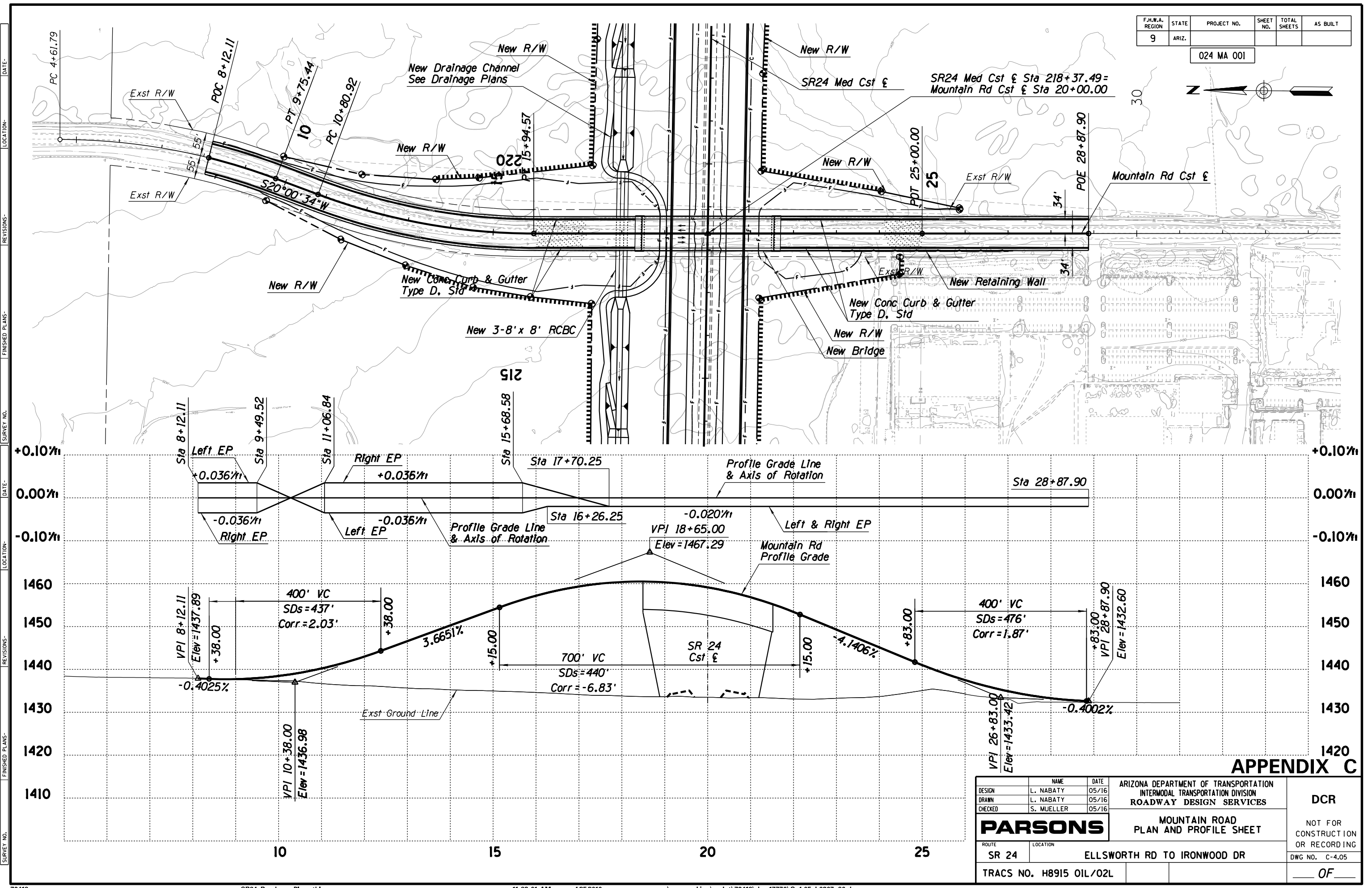
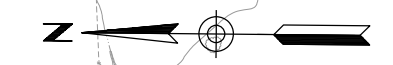
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			SIGNAL BUTTE ROAD PLAN AND PROFILE SHEET	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-4.04
TRACS NO. H8915 OIL/02L				OF

DATE: LOCATION: REVISIONS: FINISHED PLANS: SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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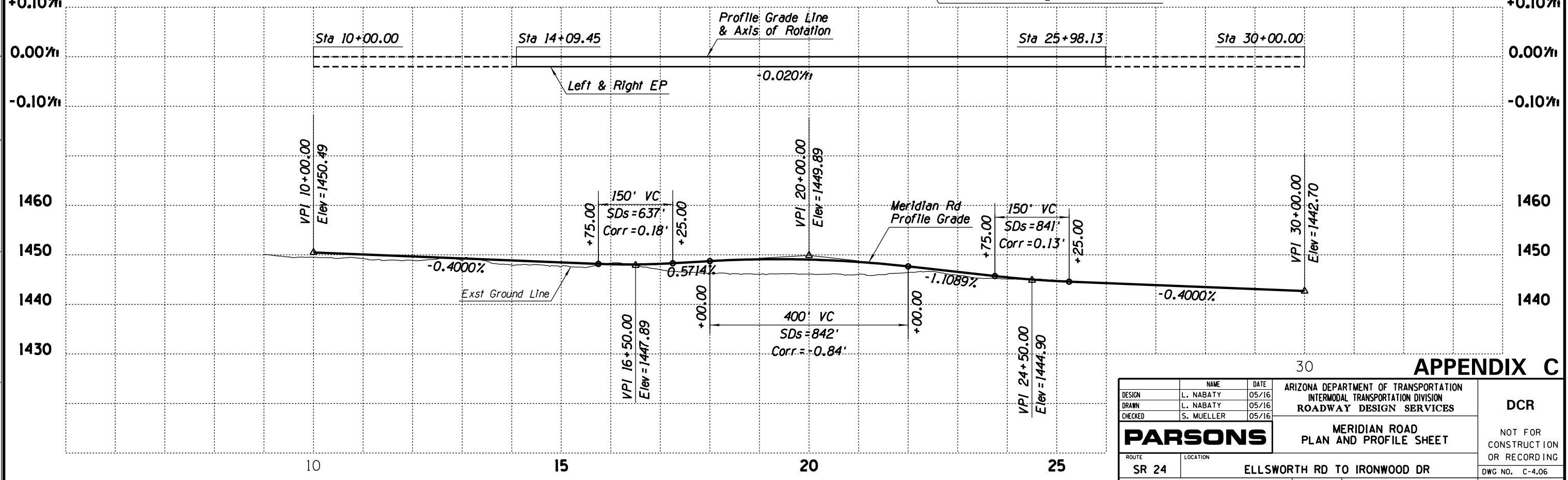
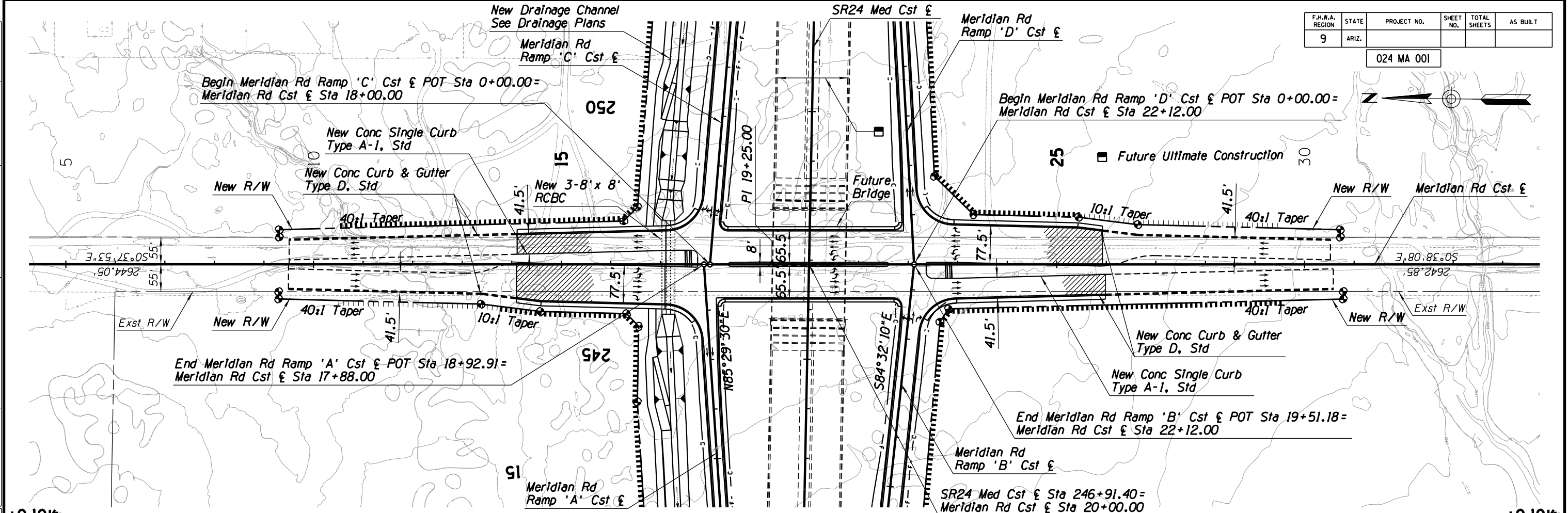


APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			MOUNTAIN ROAD PLAN AND PROFILE SHEET	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-4.05
TRACS NO. H8915 OIL/02L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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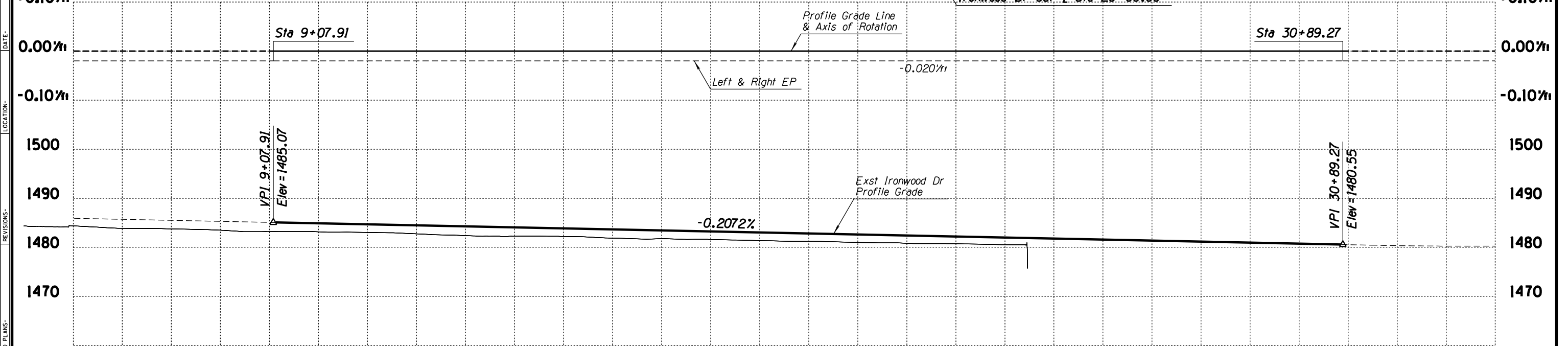
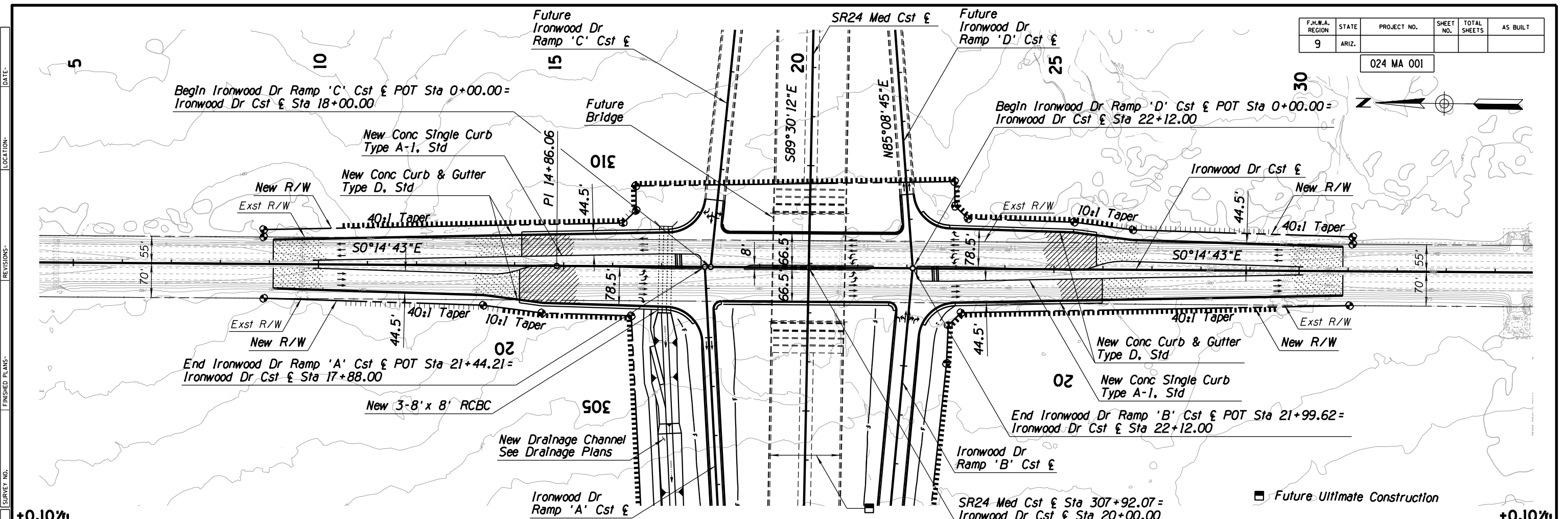
APPENDIX C

DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			MERIDIAN ROAD PLAN AND PROFILE SHEET	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-4.06
TRACS NO. H8915 OIL/O2L				OF

DATE: _____ LOCATION: _____ REVISIONS: _____ FINISHED PLANS: _____ SURVEY NO. _____

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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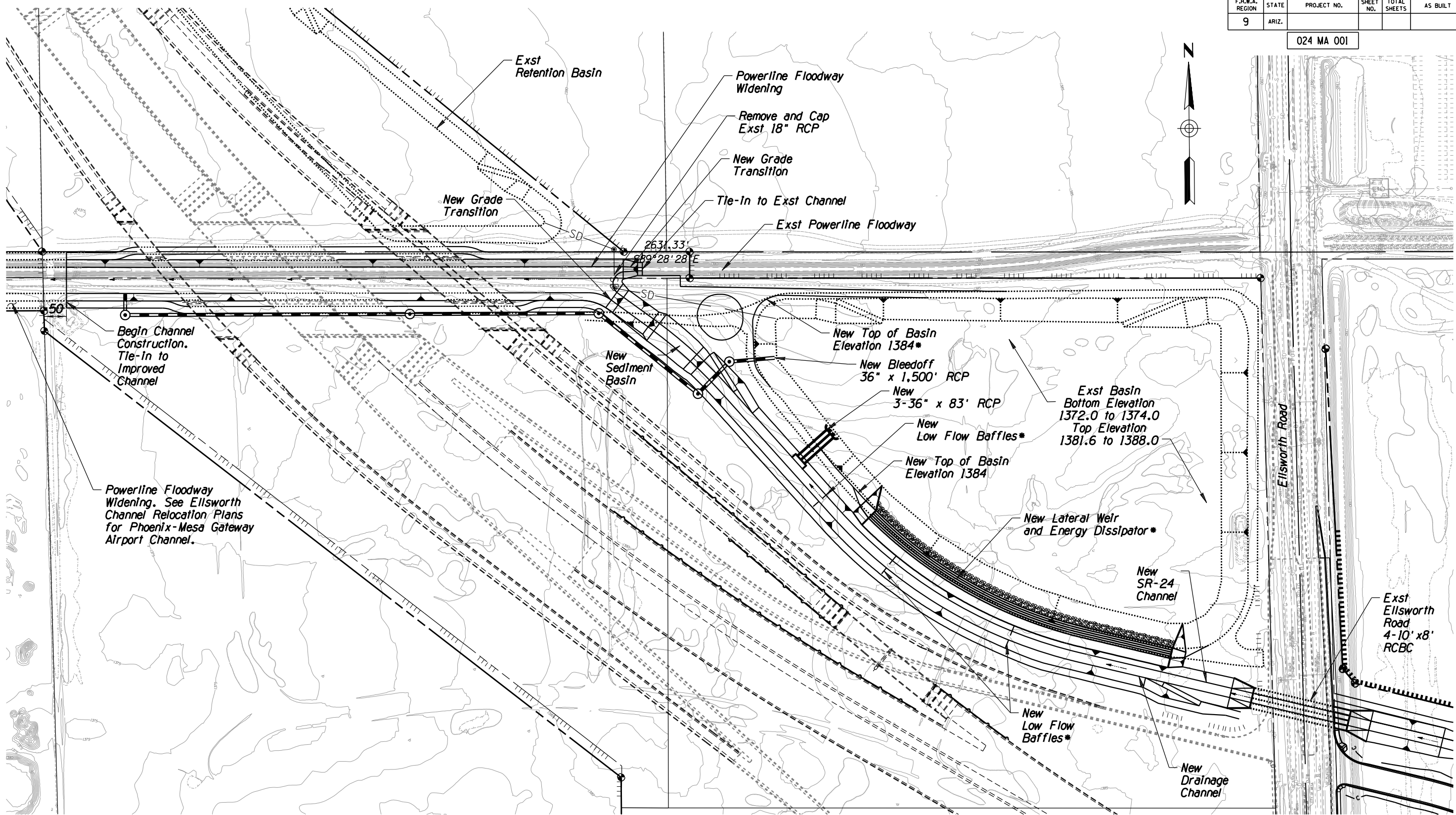


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DESIGN	L. NABATY	05/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	L. NABATY	05/16		
CHECKED	S. MUELLER	05/16		
PARSONS			IRONWOOD DRIVE PLAN AND PROFILE SHEET	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. C-4.07
TRACS NO. H8915 OIL/O2L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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Begin Channel Construction. Tie-In to Improved Channel

Powerline Floodway Widening. See Ellsworth Channel Relocation Plans for Phoenix-Mesa Gateway Airport Channel.

DESIGN NOTE:

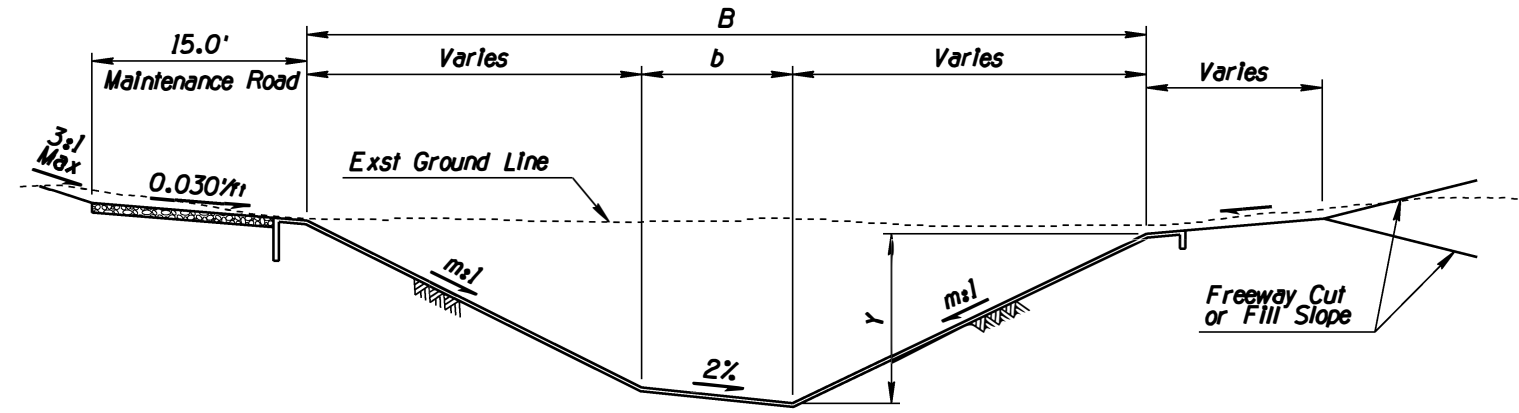
* The Lateral Weir (740 LF), Low Flow Baffles and elevated top of basin as shown are conceptual and will be refined in final design to reduce the estimated maximum 100-year, 24-hour channel peak flow discharging to Powerline Floodway to approximately 1,650 cfs. The maximum channel peak flow is estimated based on hydrology illustrating the January 2016 development conditions, and assuming that the SR-24 alignment extends to Central Arizona Project Canal intercepting all flows approaching from the north and the northeast. As development progress, peak flows reduce. The SR-24 Interim Phase II off-site channel will collect flows only to Ironwood Drive. The length and operation of the lateral weir and of the Ellsworth Road Basin should be revised based on the magnitude of the peak flow at the time of construction.

DESIGN	L. FERRERAS	07/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	A. ISLAM	07/16		
CHECKED	F. BRAILEANU	07/16		
PARSONS			ELLSWORTH BASIN LAYOUT PLAN	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. D-1.01
TRACS NO. H8915 OIL/02L				OF

SURVEY NO. FINISHED PLANS DATE LOCATION REVISIONS DATE FINISHED PLANS SURVEY NO. DATE LOCATION REVISIONS DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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TYPICAL SECTION

Stationing	From Station	To Station	Bottom Width (b) 1	Side Slope (m:1)	Depth (Y) 1	Top Width (T) 1,2
Ellsworth, Ramp A	9+21	26+01	20	2	9.25	56.5
SR 24	60+44	120+04	20	2	9.25	55.2
	122+13	135+97	12-20 ³	2	7.75	42.5-50.5
	138+06	193+20	12	2	7.75	42.5-50.5
	195+21	216+85	12	2	7.25	40.5-48.5
	219+79	245+85	12	2	7.25	40.5-48.5
	247+75	306+94	12	2	7.25	40.5-48.5

Notes:

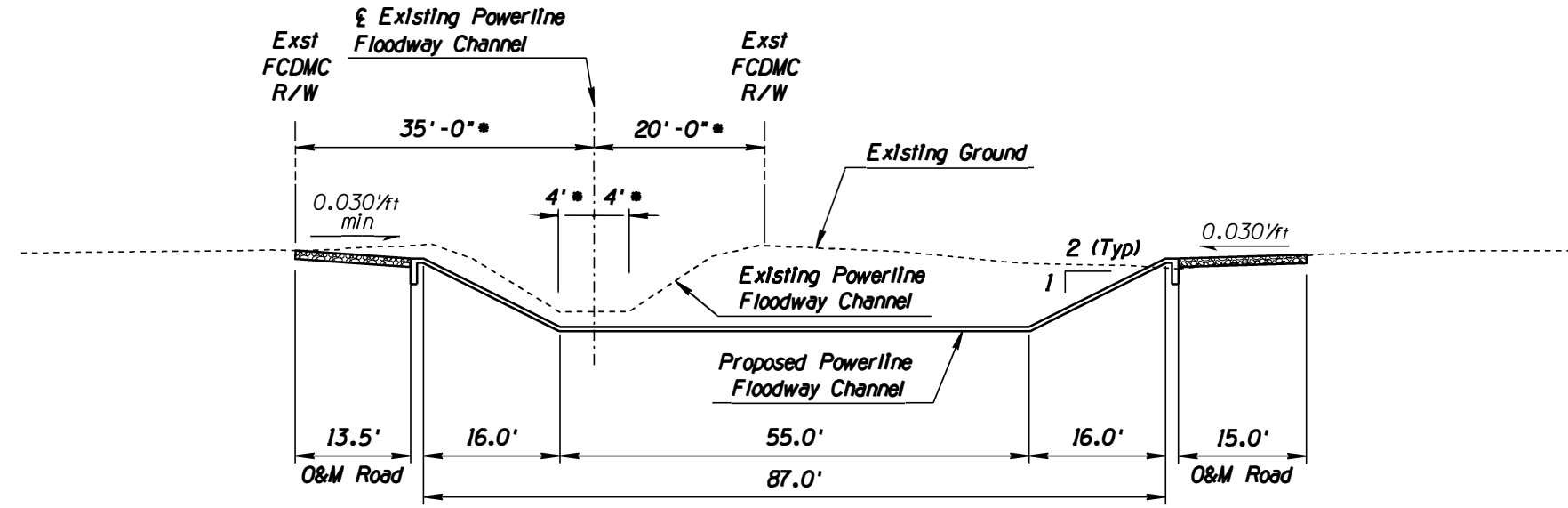
1. All Dimensions are in feet
2. Stepped Channel maximum top width accounts for a 2ft step.
3. Larger bottom width downstream of confluence with offsite channel from Pacific Proving Grounds North Development west of Crismon Rd.

DESIGN		L. FERRERAS	02/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN		A. ISLAM	02/16		
CHECKED		F. BRALEMANU	02/16		
PARSONS			OFFSITE CHANNEL TYPICAL SECTION		NOT FOR CONSTRUCTION OR RECORDING
ROUTE	LOCATION			DWG NO. D-1.02	
SR 24	ELLSWORTH RD TO IRONWOOD RD				
TRACS NO. H8915 OIL/02L				OF	

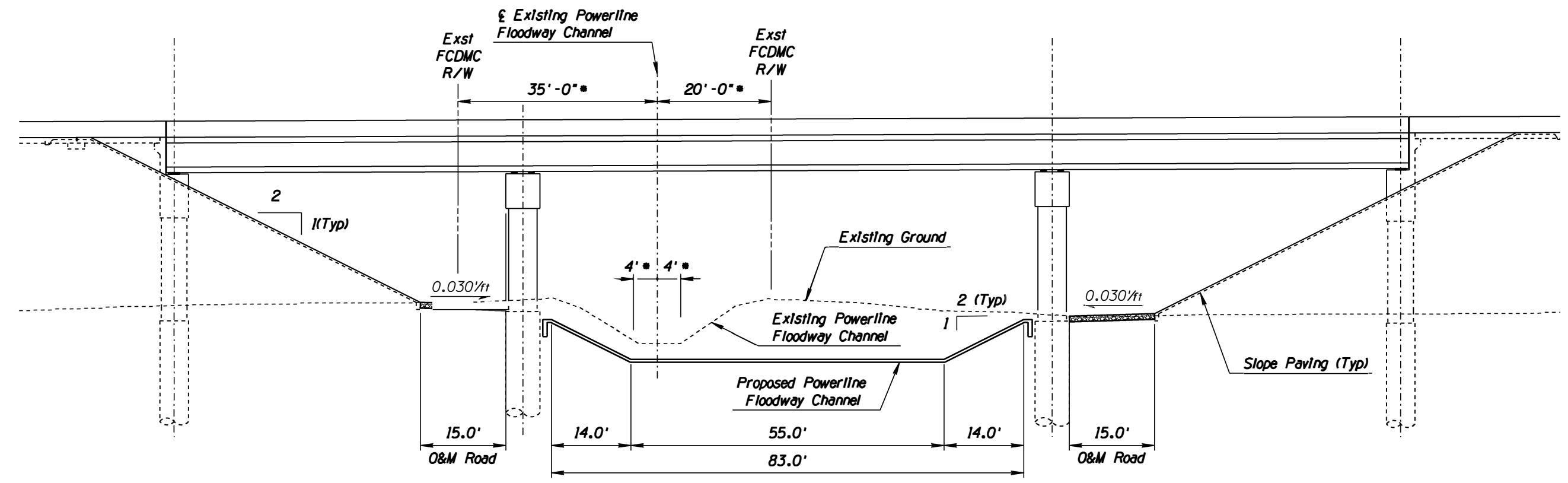
SURVEY NO. DATE FINISHED PLANS REVISIONS LOCATION DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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TYPICAL SECTION - POWERLINE FLOODWAY WIDENING
OUTSIDE OF SR 24 MAINLINE AND RAMP STRUCTURES



TYPICAL SECTION - POWERLINE FLOODWAY WIDENING
AT SR 24 MAINLINE AND RAMP STRUCTURES

* R/W Data Based on Powerline Floodway As-Built Plans.

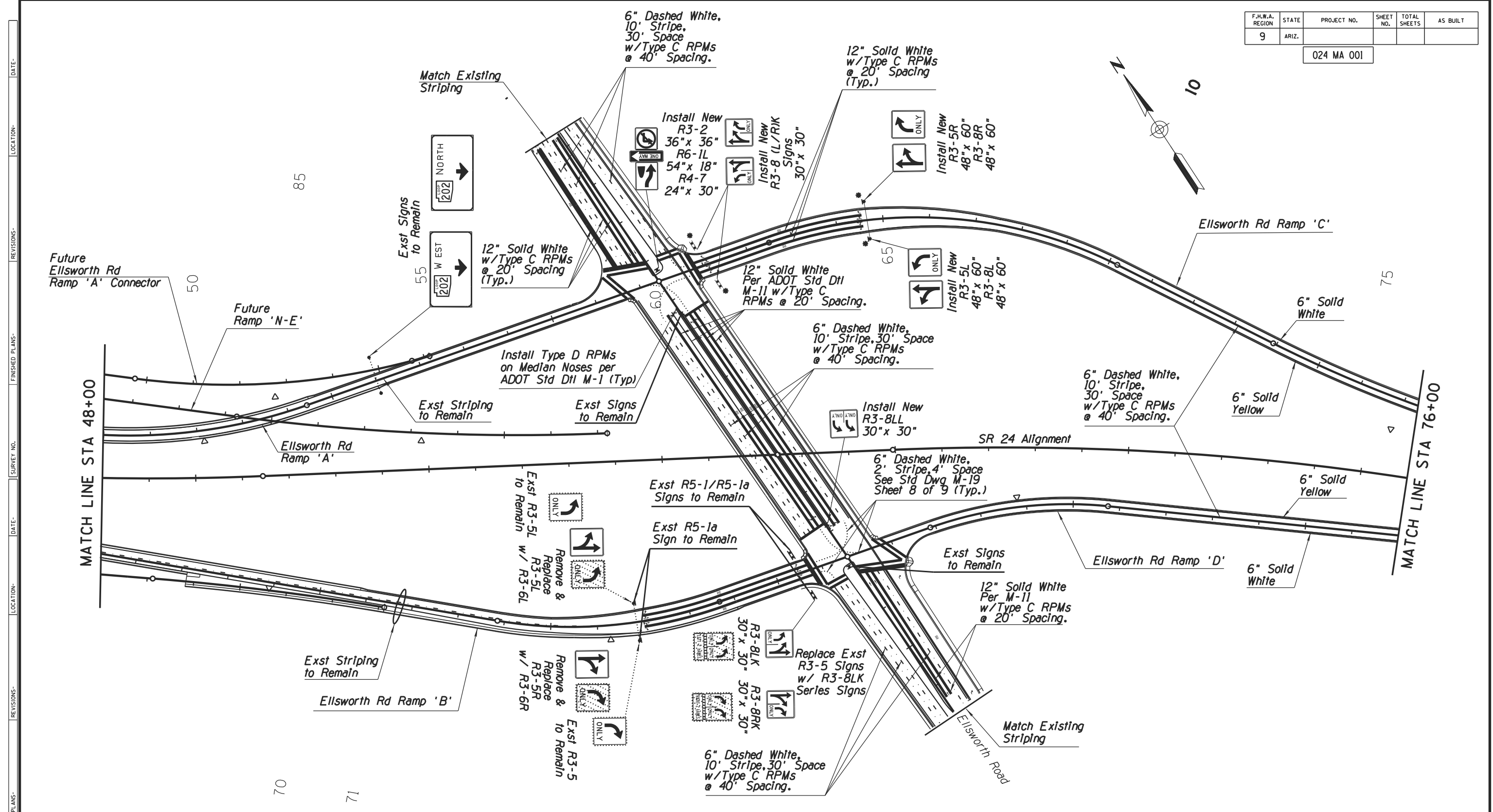
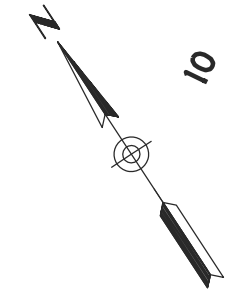
Note: Dimensions are Normal to Channel.

DESIGN	L. FERRERAS	DATE	07/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION ROADWAY DESIGN SERVICES	DCR
DRAWN	A. ISLAM	DATE	07/16		
CHECKED	F. BRAILEANU	DATE	07/16		
PARSONS		POWERLINE FLOODWAY TYPICAL SECTIONS		NOT FOR CONSTRUCTION OR RECORDING	
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. D-1.03	
TRACS NO. H8915 OIL/02L				OF	

DATE: _____ LOCATION: _____ REVISIONS: _____ FINISHED PLANS: _____ SURVEY NO. _____ DATE: _____ LOCATION: _____ REVISIONS: _____ FINISHED PLANS: _____ SURVEY NO. _____

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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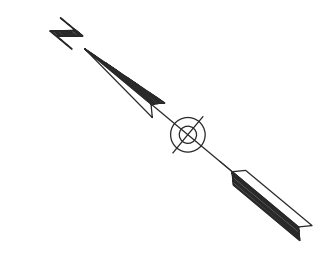
Notes:
 1. Install R5-1a and R5-1 (Wrong Way/Do Not Enter) Signage Per ADOT Latest Standards for Off Ramp Intersections
 2. Install R5-1a (Wrong Way) Signs On Sign Structure Poles and Mast Arm Per ADOT Latest Standards

APPENDIX C

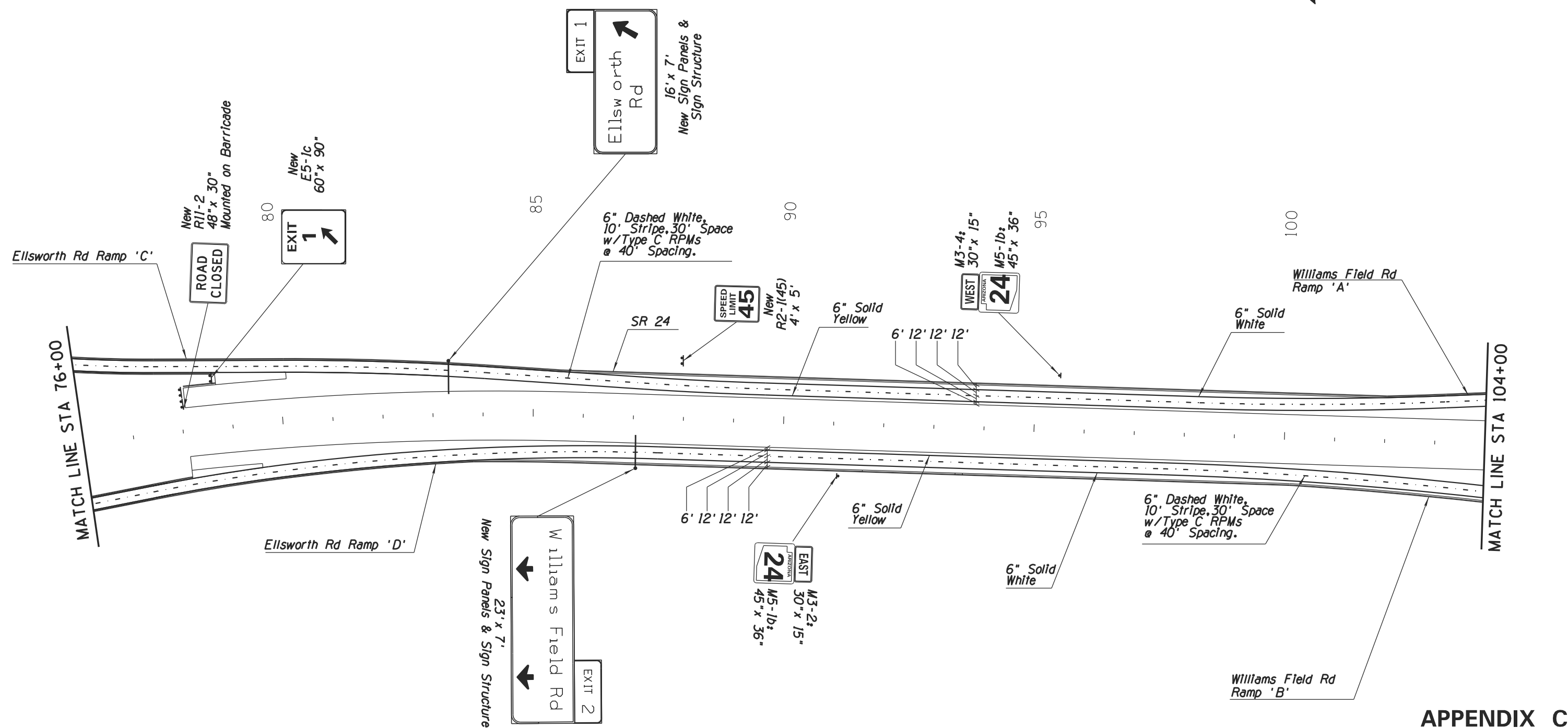
DESIGN	A. IBEJI	DATE	12/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION TRAFFIC DESIGN SERVICES	DCR
DRAWN	K. ABARIKWU	DATE	12/16		
CHECKED	J. SCHUMANN	DATE	12/16		
the CK Group, Inc.			SIGNING & MARKING PLANS INTERIM SR 24 STA 48+00 TO STA 76+00		NOT FOR CONSTRUCTION OR RECORDING
ROUTE	LOCATION		SR 24 ELLSWORTH RD TO IRONWOOD DR		DWG NO. T-1.01
TRACS NO. H8915 OIL/02L					OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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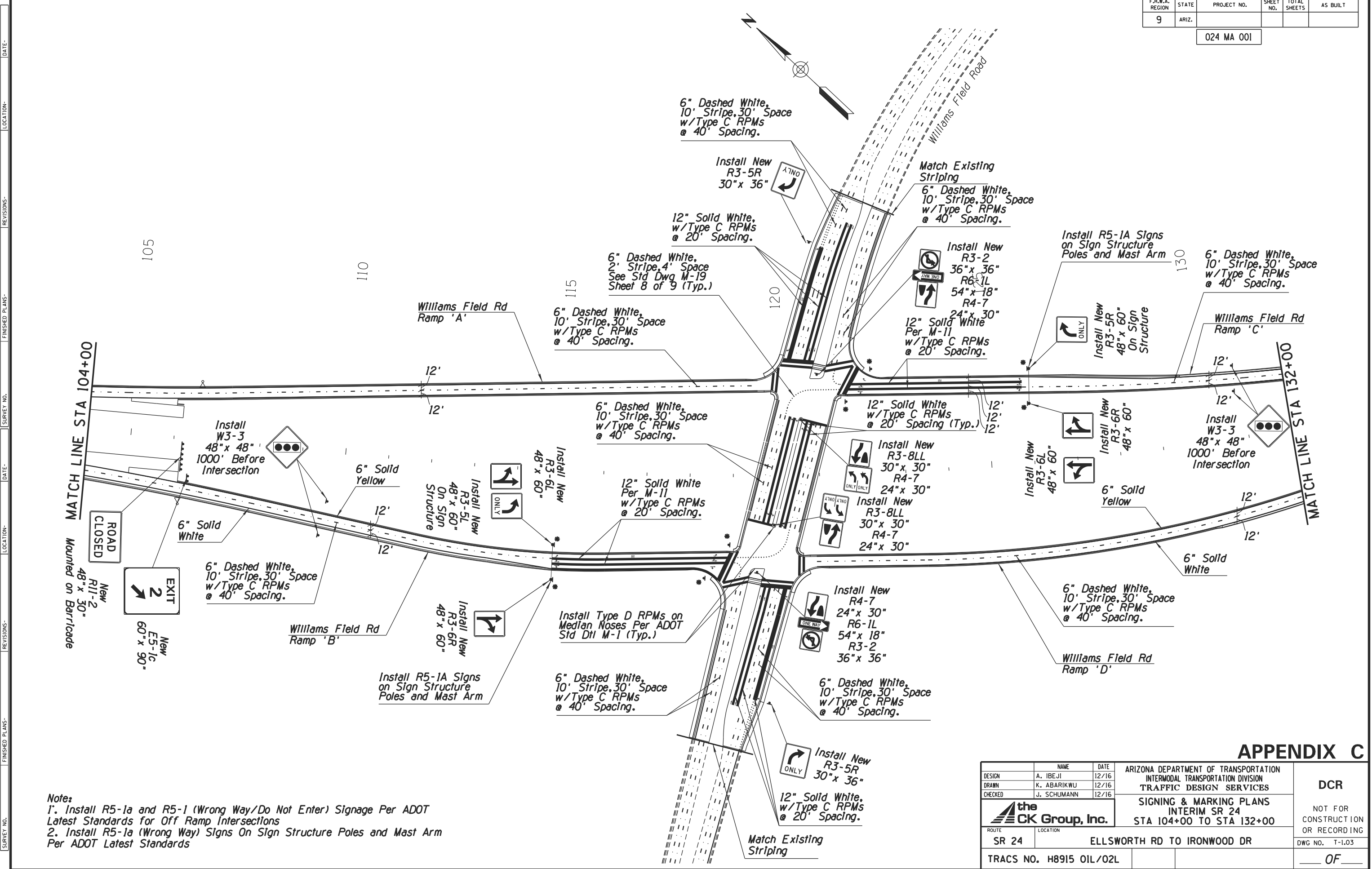
DATE: LOCATION: REVISIONS: FINISHED PLANS: SURVEY NO. DATE: LOCATION: REVISIONS: FINISHED PLANS: SURVEY NO.



APPENDIX C

DESIGN	A. IBEJI	DATE	12/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING
DRAWN	K. ABARIKWU	DATE	12/16		
CHECKED	J. SCHUMANN	DATE	12/16		
		SIGNING & MARKING PLANS INTERIM SR 24 STA 76+00 TO STA 104+00		DWG NO. T-1.02	
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR		
TRACS NO. H8915 OIL/02L			OF		

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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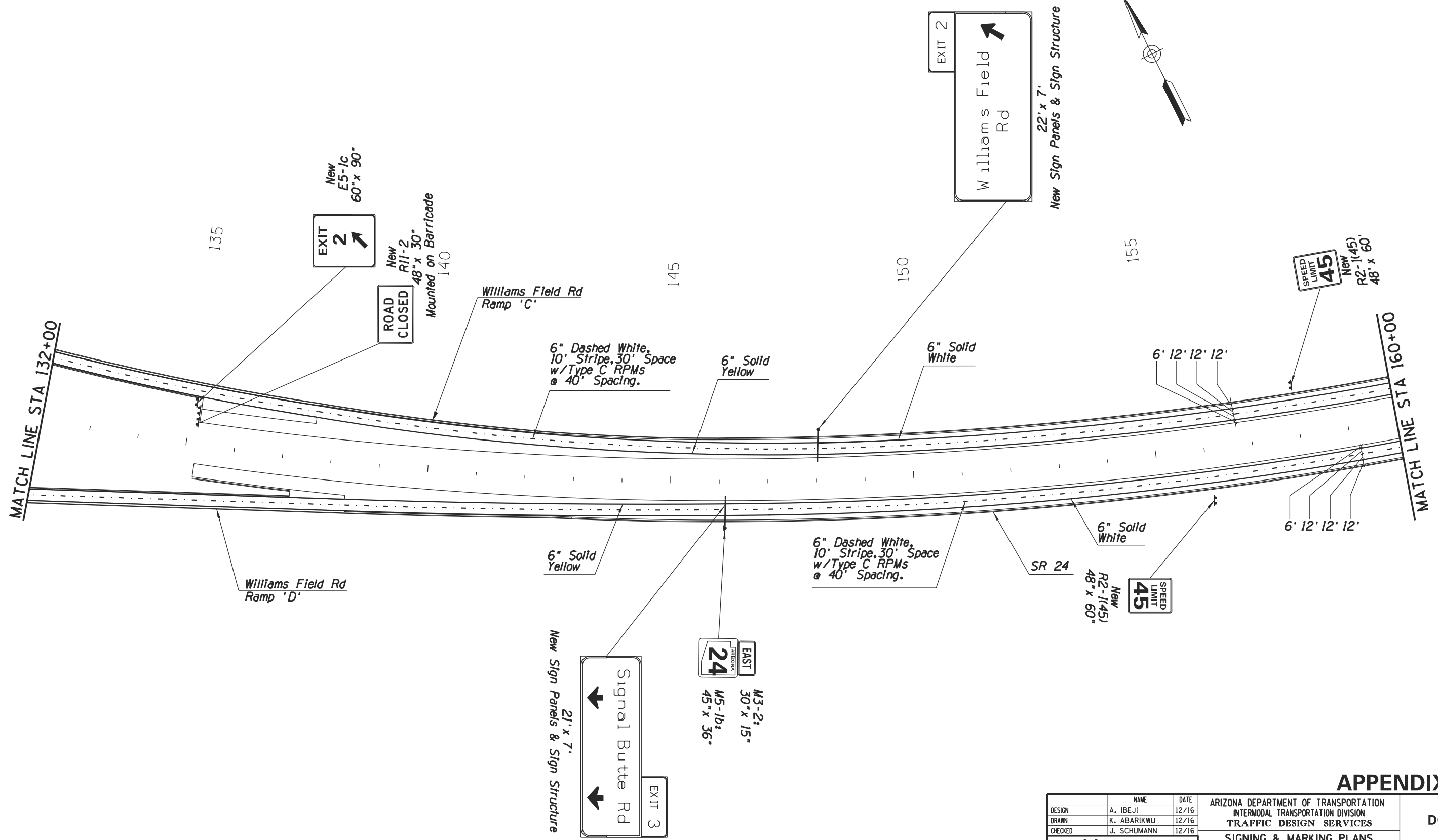
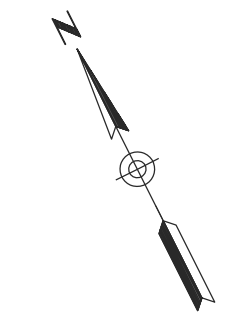
Notes:
 1. Install R5-1a and R5-1 (Wrong Way/Do Not Enter) Signage Per ADOT Latest Standards for Off Ramp Intersections
 2. Install R5-1a (Wrong Way) Signs On Sign Structure Poles and Mast Arm Per ADOT Latest Standards

APPENDIX C

DESIGN	A. IBEJI	12/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION TRAFFIC DESIGN SERVICES	DCR
DRAWN	K. ABARIKWU	12/16		
CHECKED	J. SCHUMANN	12/16		
			SIGNING & MARKING PLANS INTERIM SR 24 STA 104+00 TO STA 132+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. T-1.03
TRACS NO. H8915 OIL/O2L				OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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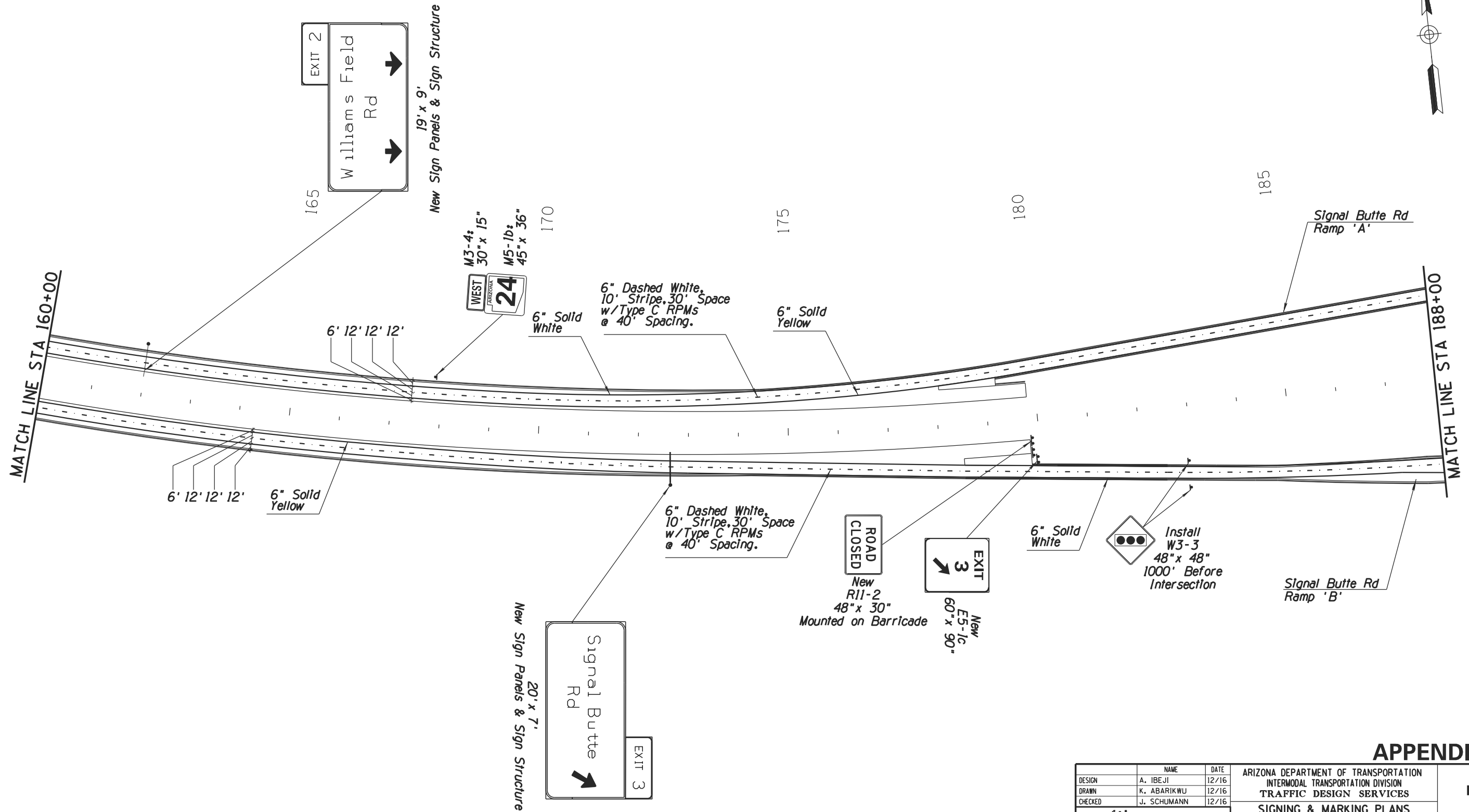
APPENDIX C

DESIGN	A. IBEJI	DATE	12/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING
DRAWN	K. ABARIKWU	DATE	12/16		
CHECKED	J. SCHUMANN	DATE	12/16		
		SIGNING & MARKING PLANS INTERIM SR 24 STA 132+00 TO STA 160+00		DWG NO. T-1.04	
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR		
TRACS NO. H8915 OIL/O2L			OF		

SURVEY NO. FINISHED PLANS. LOCATION. DATE. REVISIONS. FINISHED PLANS. SURVEY NO. DATE. REVISIONS. FINISHED PLANS. LOCATION. DATE.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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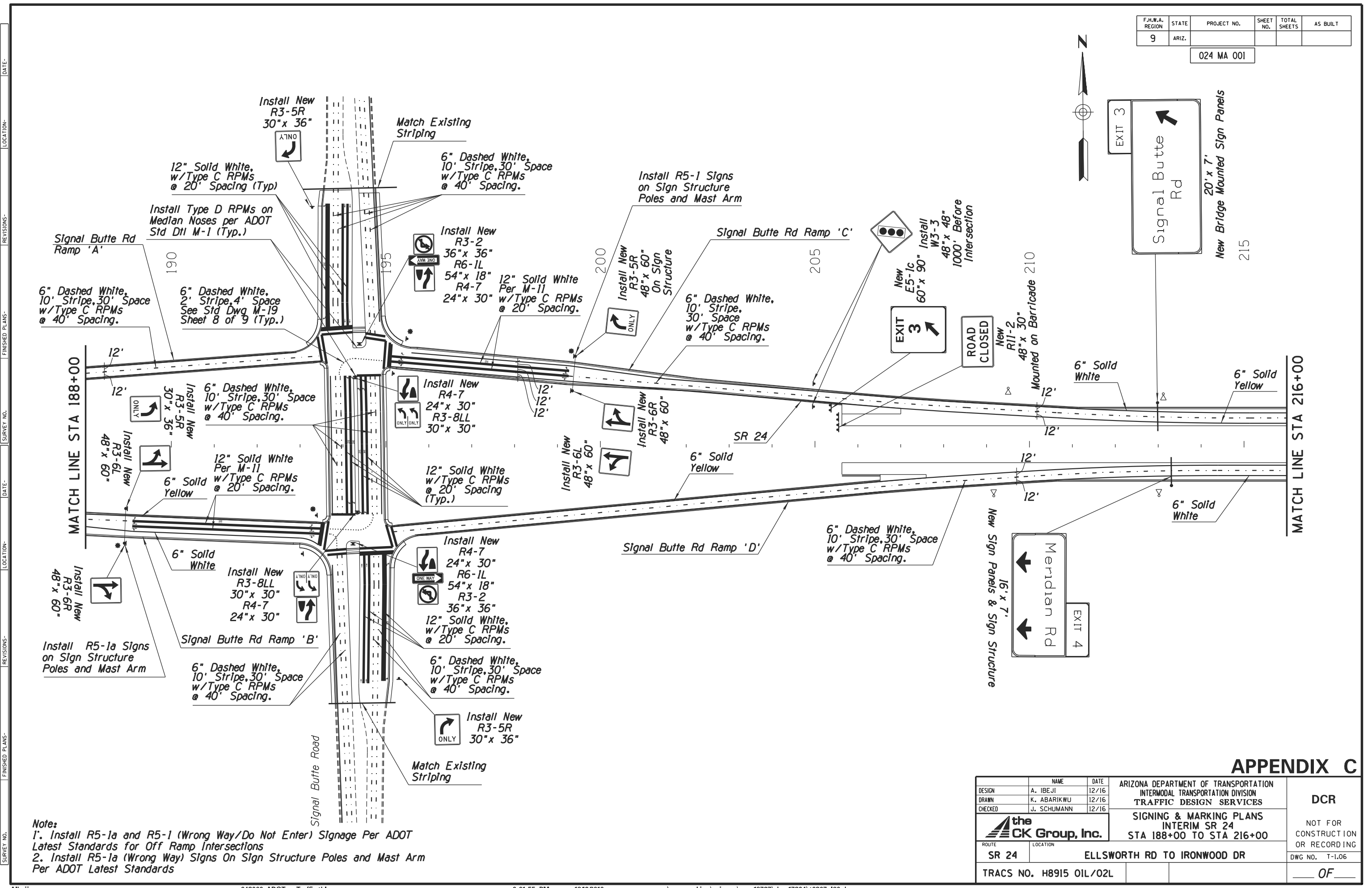
APPENDIX C

DESIGN	A. IBEJI	DATE	12/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING
DRAWN	K. ABARIKWU	DATE	12/16		
CHECKED	J. SCHUMANN	DATE	12/16		
		SIGNING & MARKING PLANS INTERIM SR 24 STA 160+00 TO STA 188+00		DWG NO. T-1.05	
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR		
TRACS NO. H8915 OIL/02L			OF		

SURVEY NO. DATE FINISHED PLANS LOCATION DATE REVISIONS DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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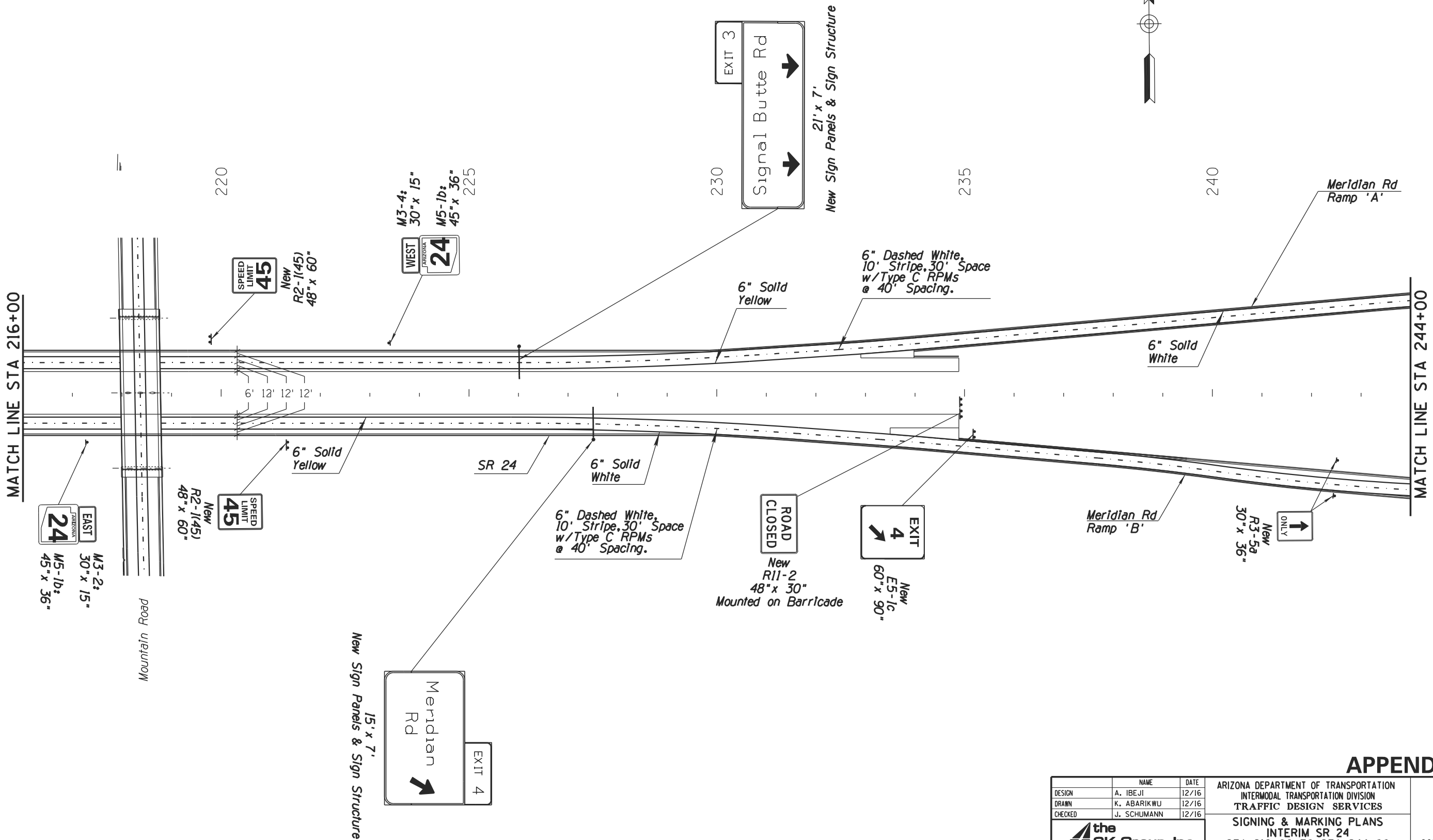
Note:
 1. Install R5-1a and R5-1 (Wrong Way/Do Not Enter) Signage Per ADOT Latest Standards for Off Ramp Intersections
 2. Install R5-1a (Wrong Way) Signs On Sign Structure Poles and Mast Arm Per ADOT Latest Standards

APPENDIX C

DESIGN	A. IBEJI	12/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION TRAFFIC DESIGN SERVICES	DCR
DRAWN	K. ABARIKWU	12/16		
CHECKED	J. SCHUMANN	12/16		
			SIGNING & MARKING PLANS INTERIM SR 24 STA 188+00 TO STA 216+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. T-1.06
TRACS NO. H8915 OIL/O2L				OF

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APPENDIX C

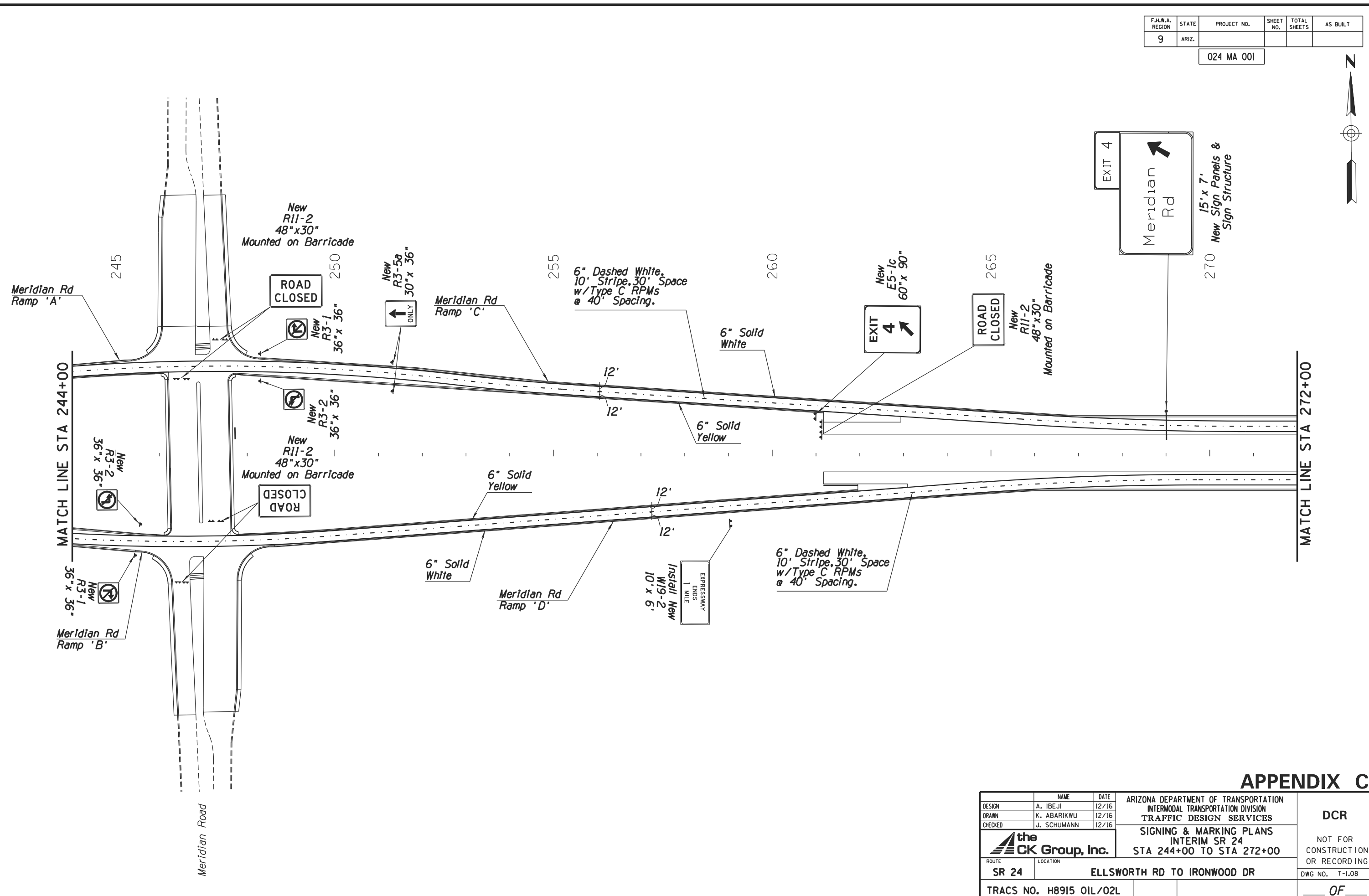
DESIGN	A. IBEJI	DATE	12/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING
DRAWN	K. ABARIKWU	DATE	12/16		
CHECKED	J. SCHUMANN	DATE	12/16		
		SIGNING & MARKING PLANS INTERIM SR 24 STA 216+00 TO STA 244+00		DWG NO. T-1.07	
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR		
TRACS NO. H8915 OIL/O2L					OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
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SURVEY NO. FINISHED PLANS REVISIONS LOCATION DATE
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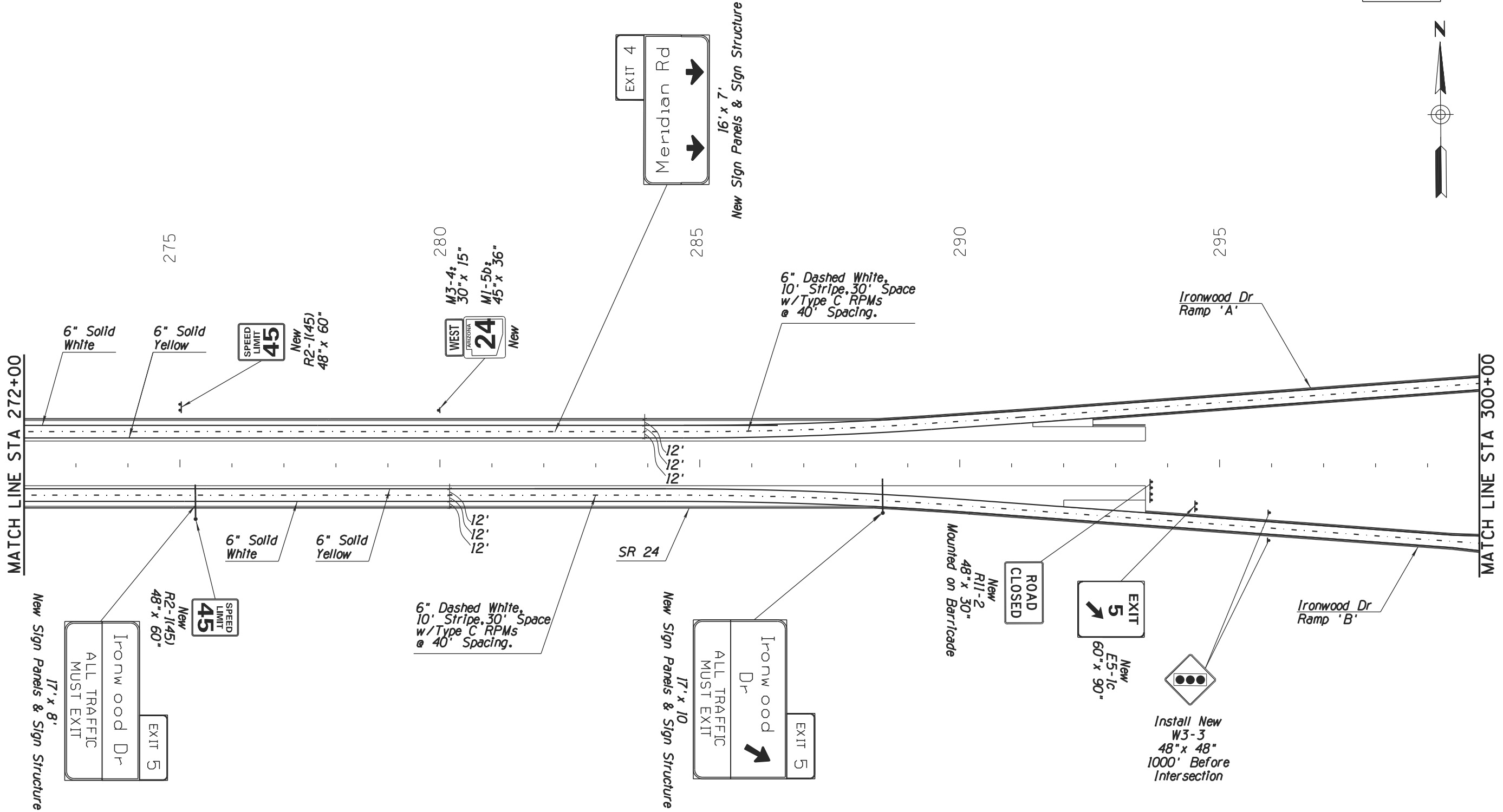


APPENDIX C

DESIGN	A. IBEJI	DATE	12/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING
DRAWN	K. ABARIKWU	DATE	12/16		
CHECKED	J. SCHUMANN	DATE	12/16		
		SIGNING & MARKING PLANS INTERIM SR 24 STA 244+00 TO STA 272+00		DWG NO. T-1.08	
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR		TRACS NO. H8915 OIL/02L

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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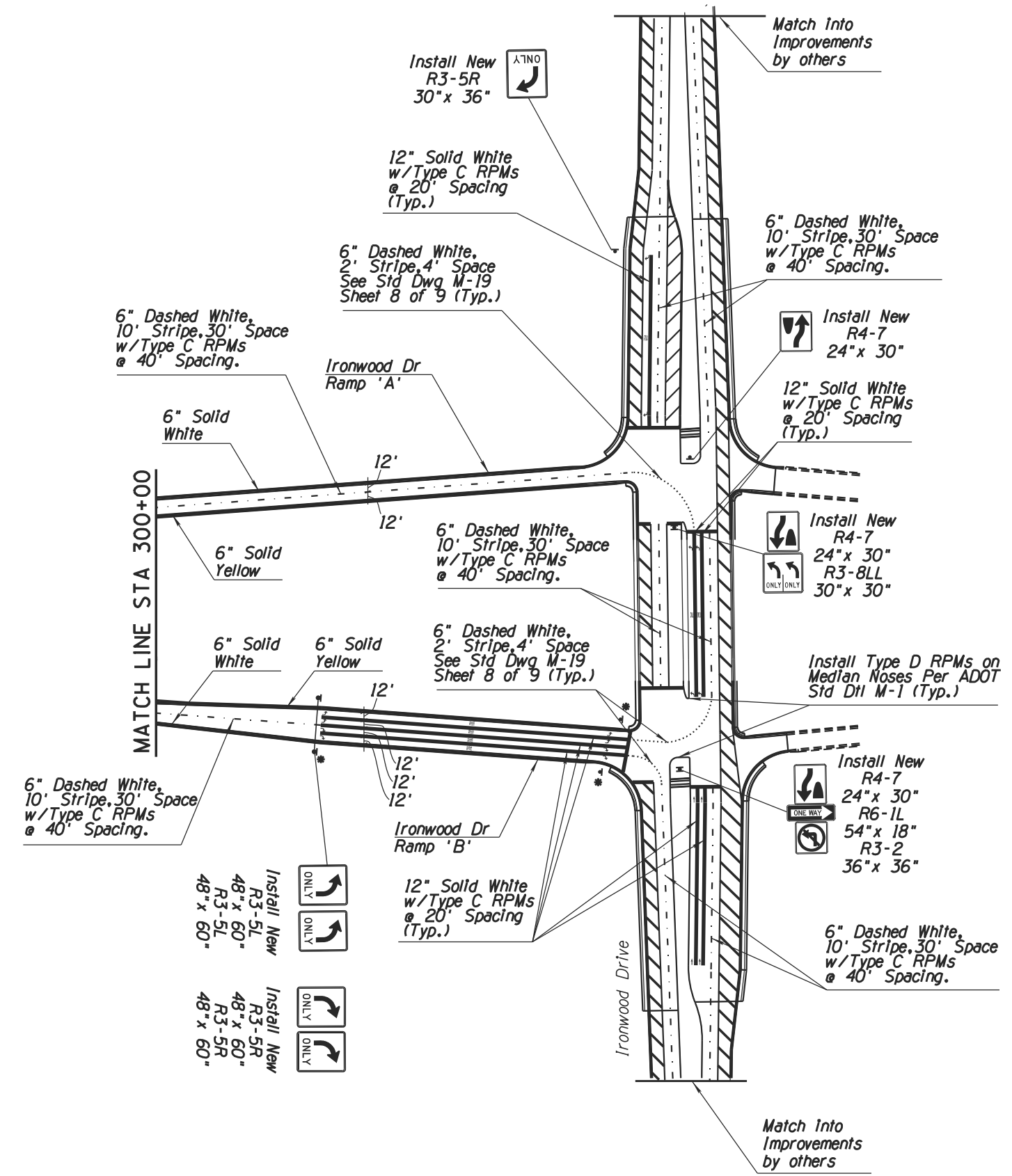
APPENDIX C

DESIGN	A. IBEJI	DATE	12/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING
DRAWN	K. ABARIKWU	DATE	12/16		
CHECKED	J. SCHUMANN	DATE	12/16		
		SIGNING & MARKING PLANS INTERIM SR 24 STA 272+00 TO STA 300+00		DWG NO. T-1.09	
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR		
TRACS NO. H8915 OIL/02L			OF		

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F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	ARIZ.				

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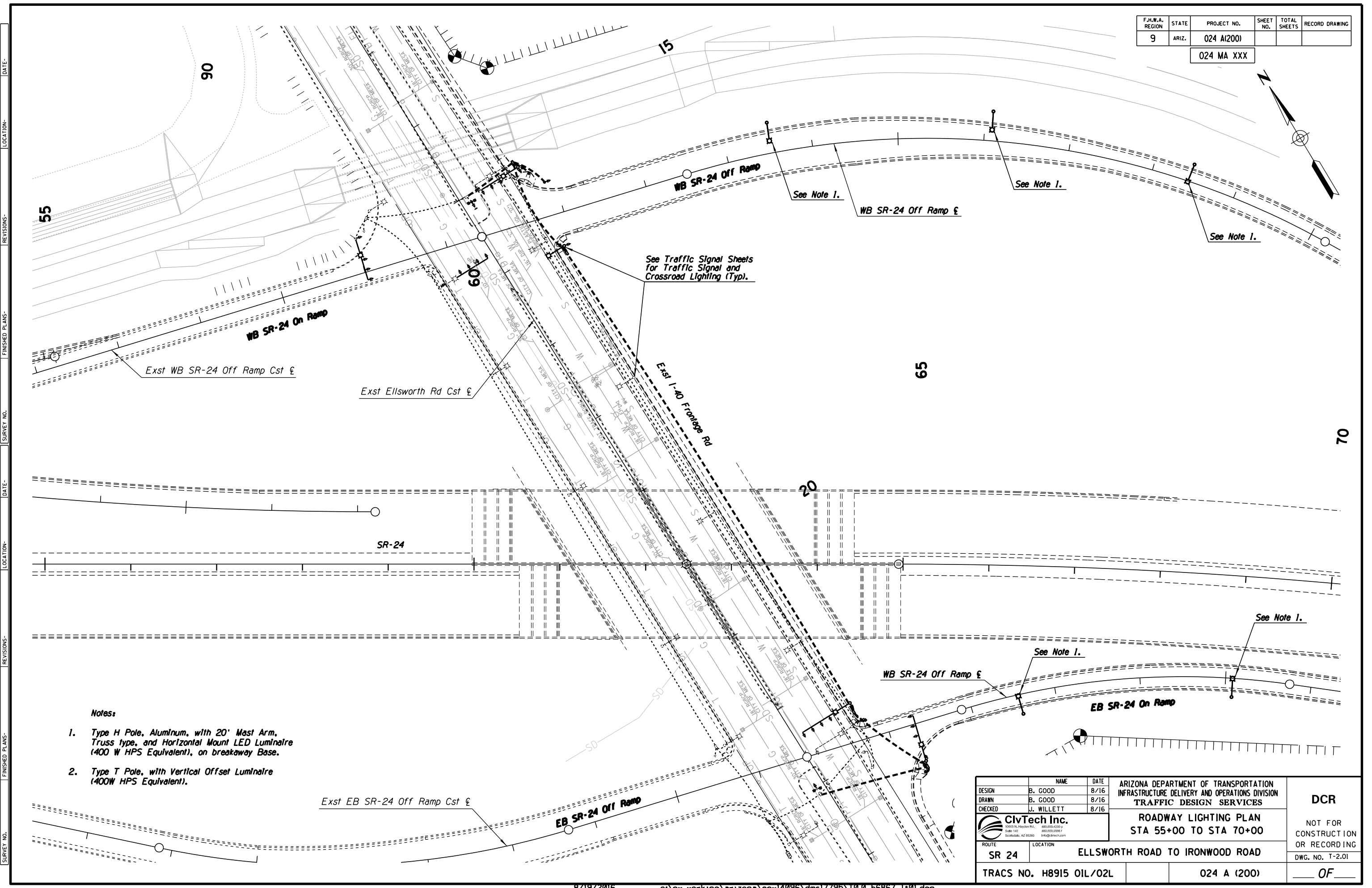
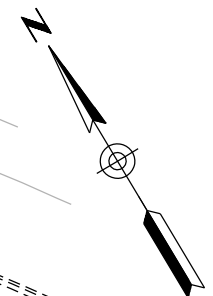
Note:
 1. Install R5-1a and R5-1 (Wrong Way/Do Not Enter) Signage Per ADOT Latest Standards for Off Ramp Intersections
 2. Install R5-1a (Wrong Way) Signs On Sign Structure Poles and Mast Arm Per ADOT Latest Standards

APPENDIX C

DESIGN	A. IBEJI	DATE	12/16	ARIZONA DEPARTMENT OF TRANSPORTATION INTERMODAL TRANSPORTATION DIVISION TRAFFIC DESIGN SERVICES	DCR
DRAWN	K. ABARIKWU	DATE	12/16		
CHECKED	J. SCHUMANN	DATE	12/16		
		SIGNING & MARKING PLANS INTERIM SR 24 STA 300+00 TO STA 328+00		NOT FOR CONSTRUCTION OR RECORDING	
ROUTE	SR 24	LOCATION	ELLSWORTH RD TO IRONWOOD DR	DWG NO. T-1.10	
TRACS NO. H8915 OIL/02L				OF	

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	RECORD DRAWING
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Notes:

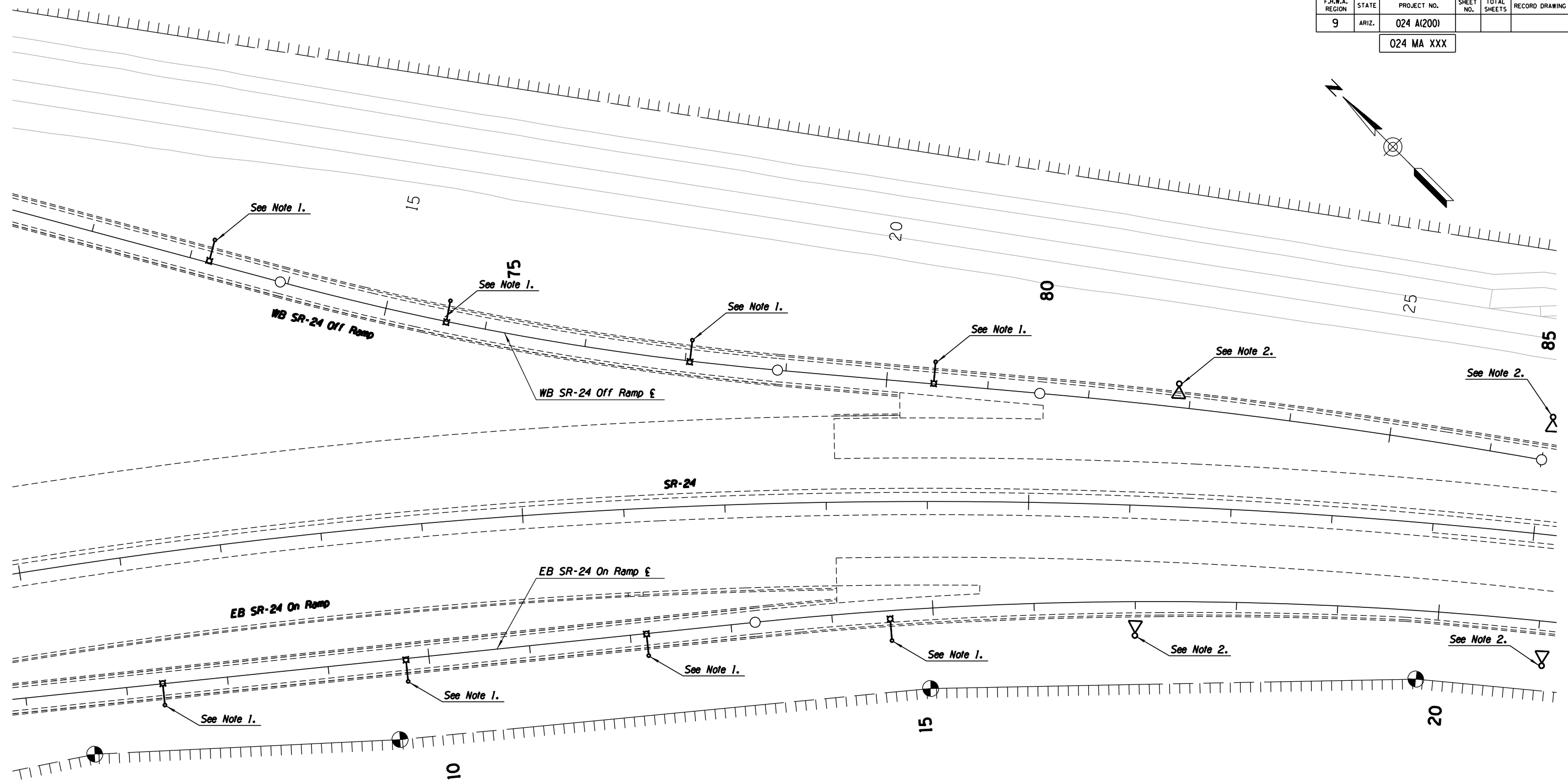
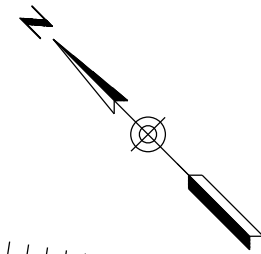
1. Type H Pole, Aluminum, with 20' Mast Arm, Truss type, and Horizontal Mount LED Luminaire (400 W HPS Equivalent), on breakaway Base.
2. Type T Pole, with Vertical Offset Luminaire (400W HPS Equivalent).

DESIGN	B. GOOD	8/16	ARIZONA DEPARTMENT OF TRANSPORTATION INFRASTRUCTURE DELIVERY AND OPERATIONS DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING DWG. NO. T-2.01
DRAWN	B. GOOD	8/16		
CHECKED	J. WILLETT	8/16		
		ROADWAY LIGHTING PLAN STA 55+00 TO STA 70+00		
ROUTE	SR 24	LOCATION	ELLSWORTH ROAD TO IRONWOOD ROAD	
TRACS NO.	H8915 OIL/O2L		024 A (200)	OF

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F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	RECORD DRAWING
9	ARIZ.	024 A(200)			

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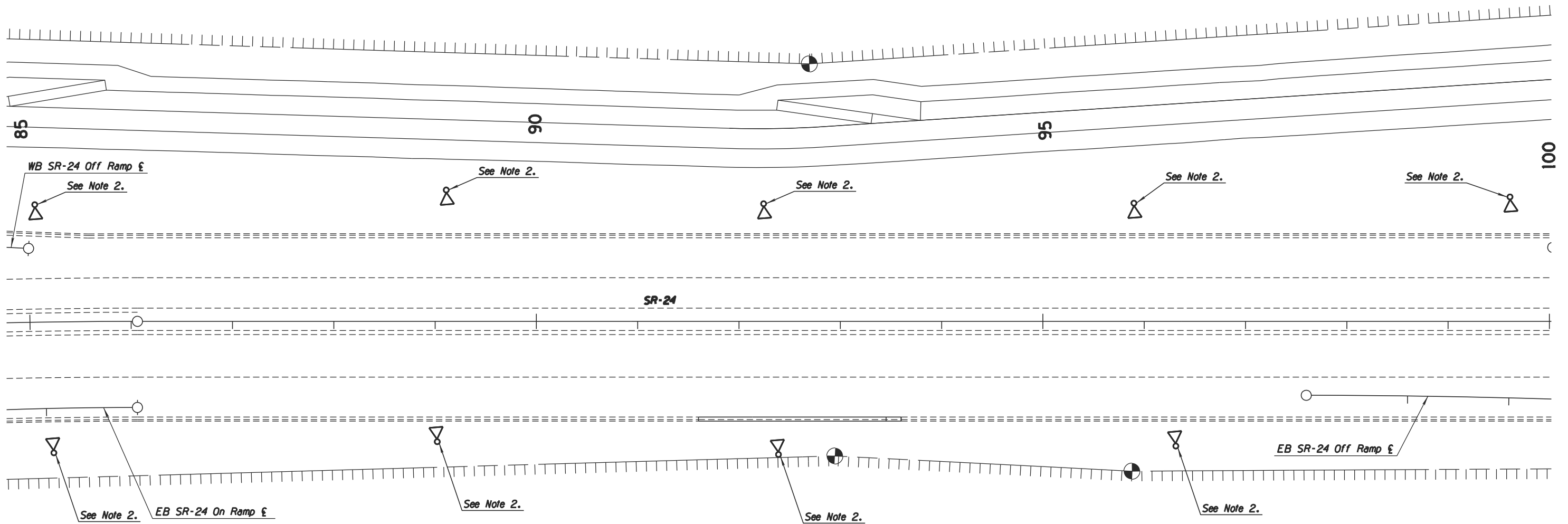
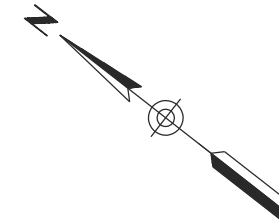
1. Type H Pole, Aluminum, with 20' Mast Arm, Truss type, and Horizontal Mount LED Luminaire (400 W HPS Equivalent), on breakaway Base.
2. Type T Pole, with Vertical Offset Luminaire (400W HPS Equivalent).

DESIGN	B. GOOD	8/16	ARIZONA DEPARTMENT OF TRANSPORTATION INFRASTRUCTURE DELIVERY AND OPERATIONS DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING	
DRAWN	B. GOOD	8/16			
CHECKED	J. WILLETT	8/16			
			ROADWAY LIGHTING PLAN STA 70+00 TO STA 85+00		
ROUTE	SR 24	LOCATION	ELLSWORTH ROAD TO IRONWOOD ROAD		
TRACS NO. H8915 OIL/O2L			024 A (200)		OF

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Notes:

1. Type H Pole, Aluminum, with 20' Mast Arm, Truss type, and Horizontal Mount LED Luminaire (400 W HPS Equivalent), on breakaway Base.
2. Type T Pole, with Vertical Offset Luminaire (400W HPS Equivalent).

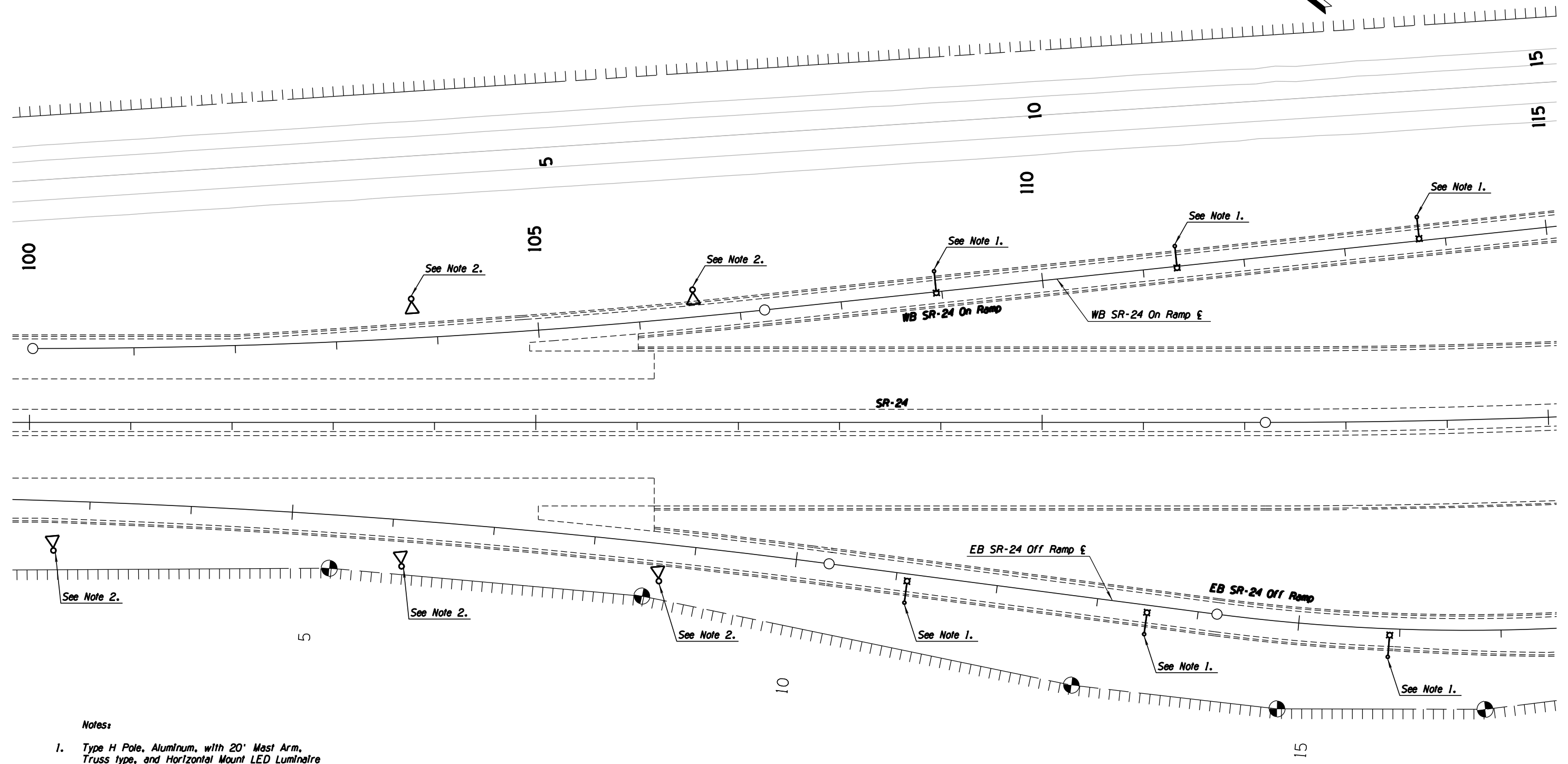
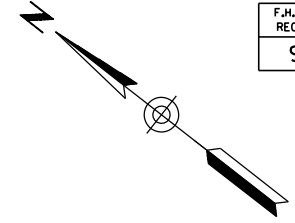
DESIGN	B. GOOD	8/16	ARIZONA DEPARTMENT OF TRANSPORTATION INFRASTRUCTURE DELIVERY AND OPERATIONS DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING
DRAWN	B. GOOD	8/16		
CHECKED	J. WILLETT	8/16		
			ROADWAY LIGHTING PLAN STA 85+00 TO STA 100+00	DWG. NO. T-2.03 OF
ROUTE	SR 24	LOCATION		
TRACS NO. H8915 OIL/O2L		024 A (200)		

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F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	RECORD DRAWING
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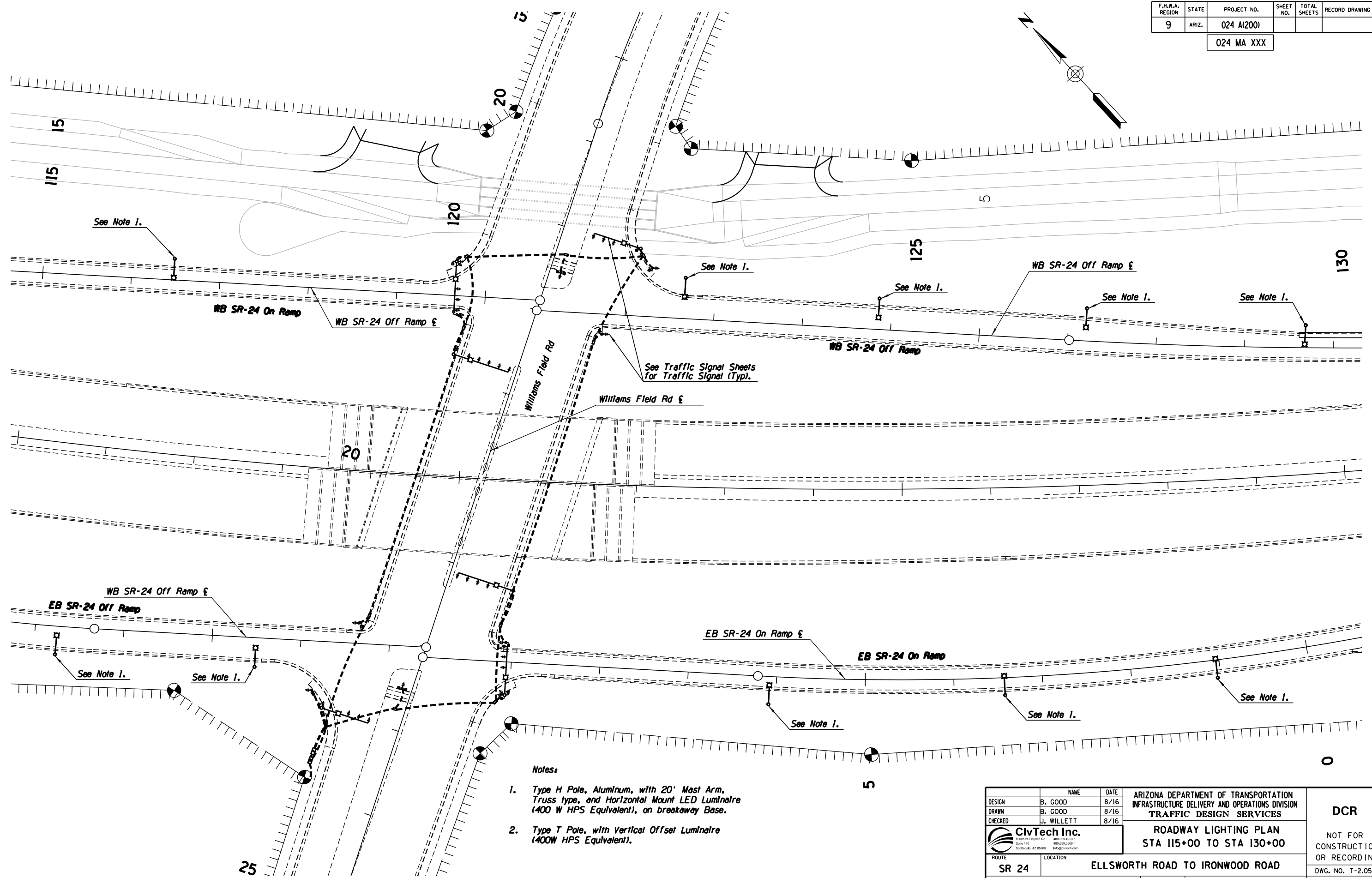
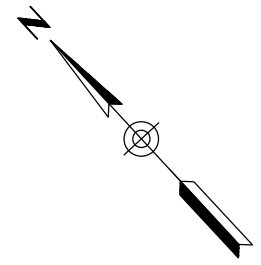
Notes:

1. Type H Pole, Aluminum, with 20' Mast Arm, Truss type, and Horizontal Mount LED Luminaire (400 W HPS Equivalent), on breakaway Base.
2. Type T Pole, with Vertical Offset Luminaire (400W HPS Equivalent).

DESIGN	B. GOOD	DATE	8/16	ARIZONA DEPARTMENT OF TRANSPORTATION INFRASTRUCTURE DELIVERY AND OPERATIONS DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING
DRAWN	B. GOOD	DATE	8/16		
CHECKED	J. WILLETT	DATE	8/16		
		10800 N. Hayden Rd., Suite 100, Scottsdale, AZ 85250 480.255.8222 480.255.0161 info@civtech.com		ROADWAY LIGHTING PLAN STA 100+00 TO STA 115+00	
ROUTE	SR 24	LOCATION	ELLSWORTH ROAD TO IRONWOOD ROAD		
TRACS NO. H8915 01L/02L			024 A (200)		DWG. NO. T-2.04 OF

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	RECORD DRAWING
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Notes:

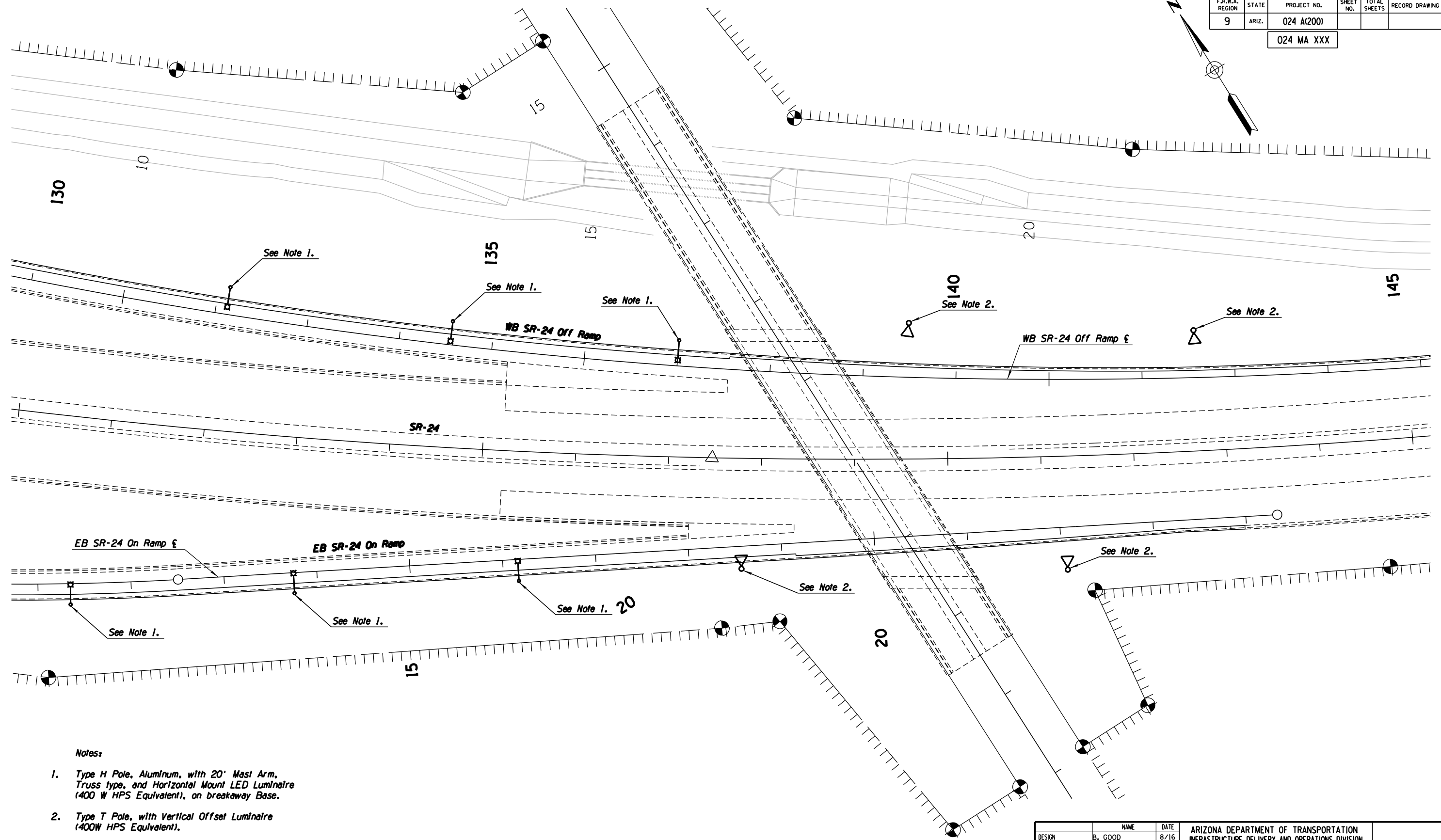
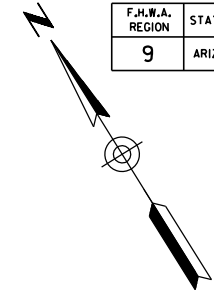
1. Type H Pole, Aluminum, with 20' Mast Arm, Truss type, and Horizontal Mount LED Luminaire (400 W HPS Equivalent), on breakaway Base.
2. Type T Pole, with Vertical Offset Luminaire (400W HPS Equivalent).

DESIGN	B. GOOD	8/16	ARIZONA DEPARTMENT OF TRANSPORTATION INFRASTRUCTURE DELIVERY AND OPERATIONS DIVISION TRAFFIC DESIGN SERVICES	DCR
DRAWN	B. GOOD	8/16		
CHECKED	J. WILLETT	8/16		
			ROADWAY LIGHTING PLAN STA 115+00 TO STA 130+00	NOT FOR CONSTRUCTION OR RECORDING
ROUTE	SR 24	LOCATION		
TRACS NO. H8915 OIL/O2L			024 A (200)	DWG. NO. T-2.05

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F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	RECORD DRAWING
9	ARIZ.	024 A(200)			
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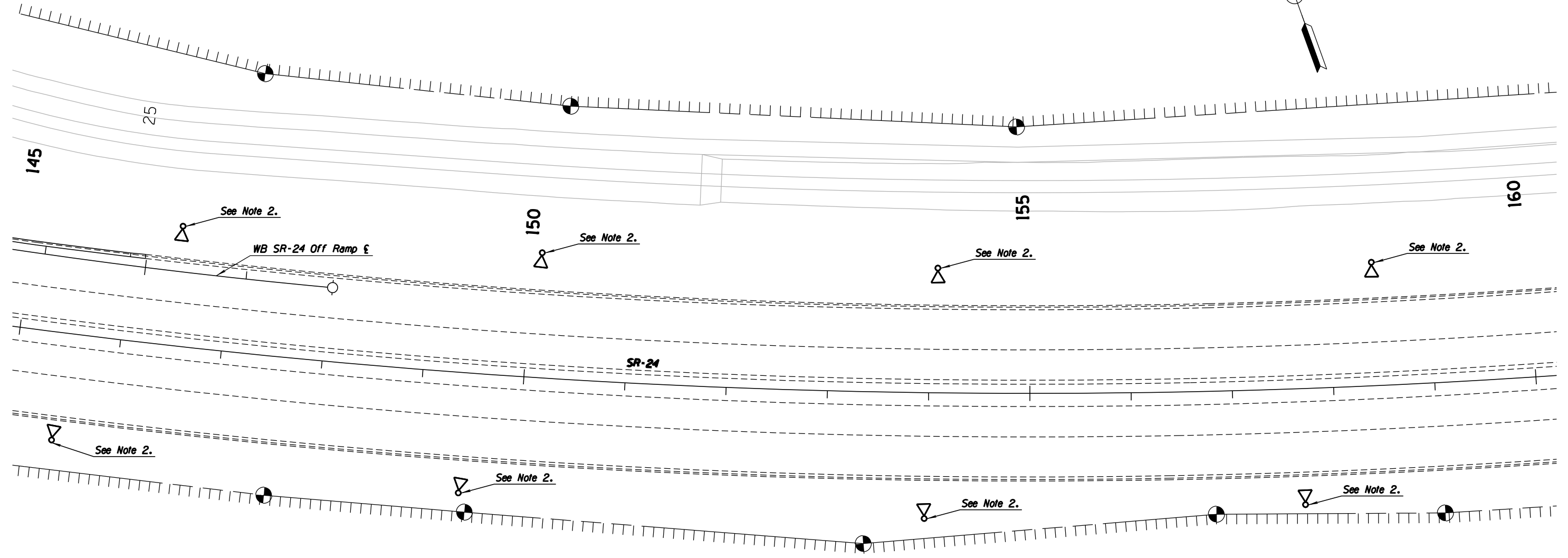
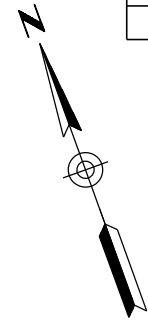
- Notes:**
1. Type H Pole, Aluminum, with 20' Mast Arm, Truss type, and Horizontal Mount LED Luminaire (400 W HPS Equivalent), on breakaway Base.
 2. Type T Pole, with Vertical Offset Luminaire (400W HPS Equivalent).

DESIGN	B. GOOD	DATE	8/16	ARIZONA DEPARTMENT OF TRANSPORTATION INFRASTRUCTURE DELIVERY AND OPERATIONS DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING	
DRAWN	B. GOOD	DATE	8/16			
CHECKED	J. WILLETT	DATE	8/16			
		ROADWAY LIGHTING PLAN STA 130+00 TO STA 145+00		DWG. NO. T-2.06 OF		
ROUTE	SR 24	LOCATION	ELLSWORTH ROAD TO IRONWOOD ROAD			
TRACS NO. H8915 OIL/O2L		024 A (200)				

SURVEY NO. FINISHED PLANS DATE LOCATION REVISIONS DATE SURVEY NO. FINISHED PLANS DATE LOCATION REVISIONS DATE SURVEY NO. FINISHED PLANS DATE

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	RECORD DRAWING
9	ARIZ.	024 A(200)			

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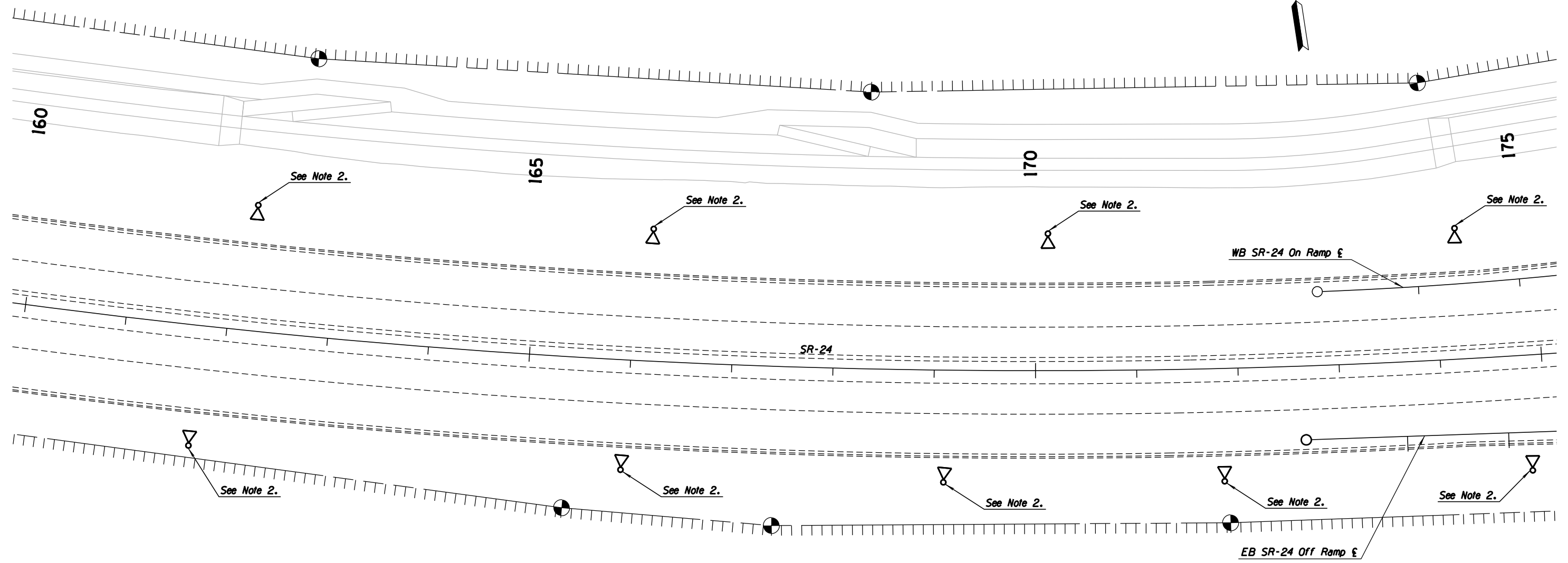
1. Type H Pole, Aluminum, with 20' Mast Arm, Truss type, and Horizontal Mount LED Luminaire (400 W HPS Equivalent), on breakaway Base.
2. Type T Pole, with Vertical Offset Luminaire (400W HPS Equivalent).

DESIGN	B. GOOD	8/16	ARIZONA DEPARTMENT OF TRANSPORTATION INFRASTRUCTURE DELIVERY AND OPERATIONS DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING DWG. NO. T-2.07
DRAWN	B. GOOD	8/16		
CHECKED	J. WILLETT	8/16		
		ROADWAY LIGHTING PLAN STA 145+00 TO STA 160+00		
ROUTE	SR 24	LOCATION	ELLSWORTH ROAD TO IRONWOOD ROAD	
TRACS NO.	H8915 OIL/O2L		024 A (200)	OF

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F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	RECORD DRAWING
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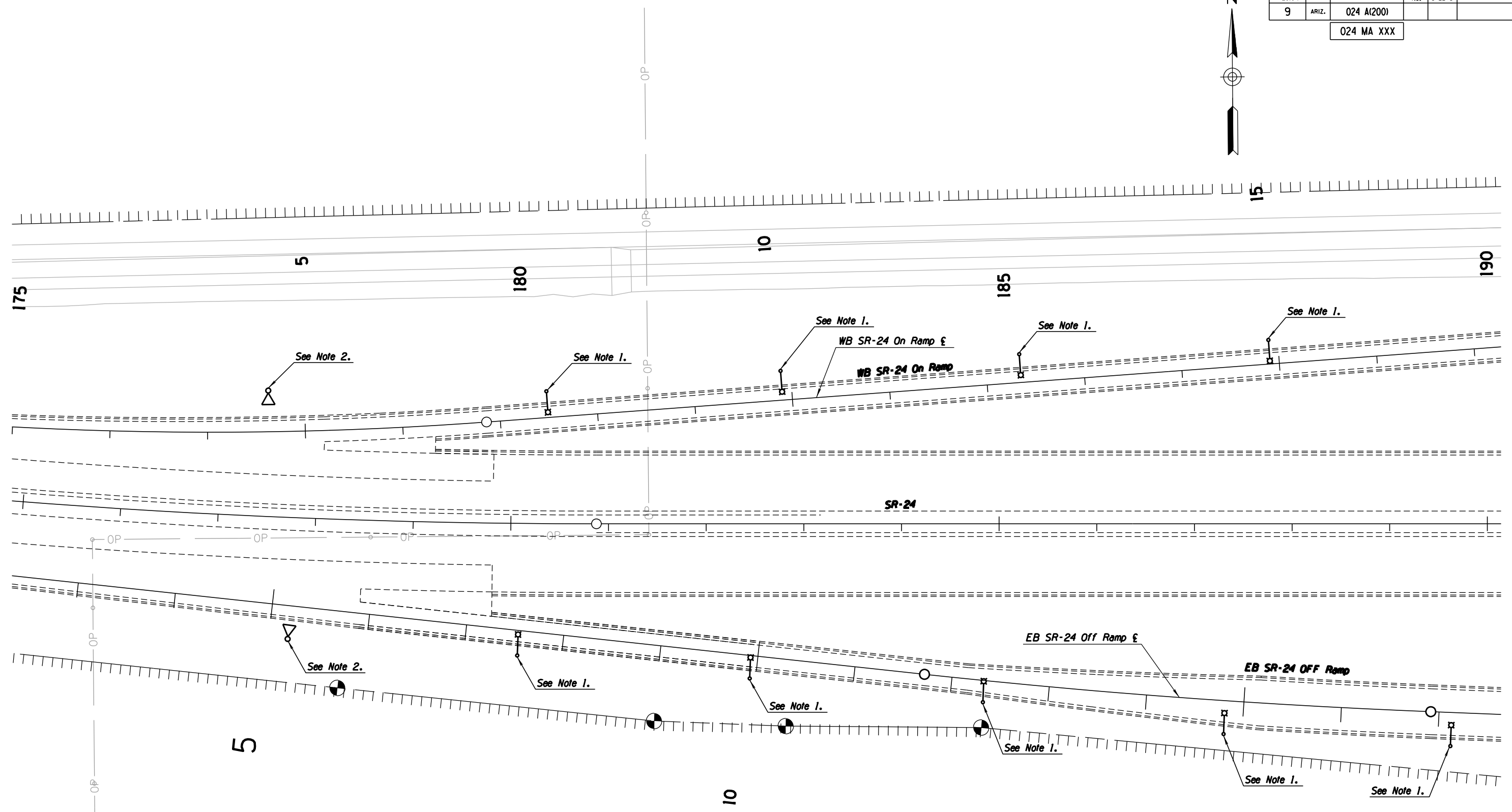
1. Type H Pole, Aluminum, with 20' Mast Arm, Truss type, and Horizontal Mount LED Luminaire (400 W HPS Equivalent), on breakaway Base.
2. Type T Pole, with Vertical Offset Luminaire (400W HPS Equivalent).

DESIGN	B. GOOD	8/16	ARIZONA DEPARTMENT OF TRANSPORTATION INFRASTRUCTURE DELIVERY AND OPERATIONS DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING DWG. NO. T-2.08
DRAWN	B. GOOD	8/16		
CHECKED	J. WILLETT	8/16		
		ROADWAY LIGHTING PLAN STA 160+00 TO STA 175+00		
ROUTE	SR 24	LOCATION	ELLSWORTH ROAD TO IRONWOOD ROAD	
TRACS NO.	H8915 OIL/O2L		024 A (200)	OF

DATE- LOCATION- REVISIONS- FINISHED PLANS- SURVEY NO. DATE- LOCATION- REVISIONS- FINISHED PLANS- SURVEY NO.

F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	RECORD DRAWING
9	ARIZ.	024 A(200)			

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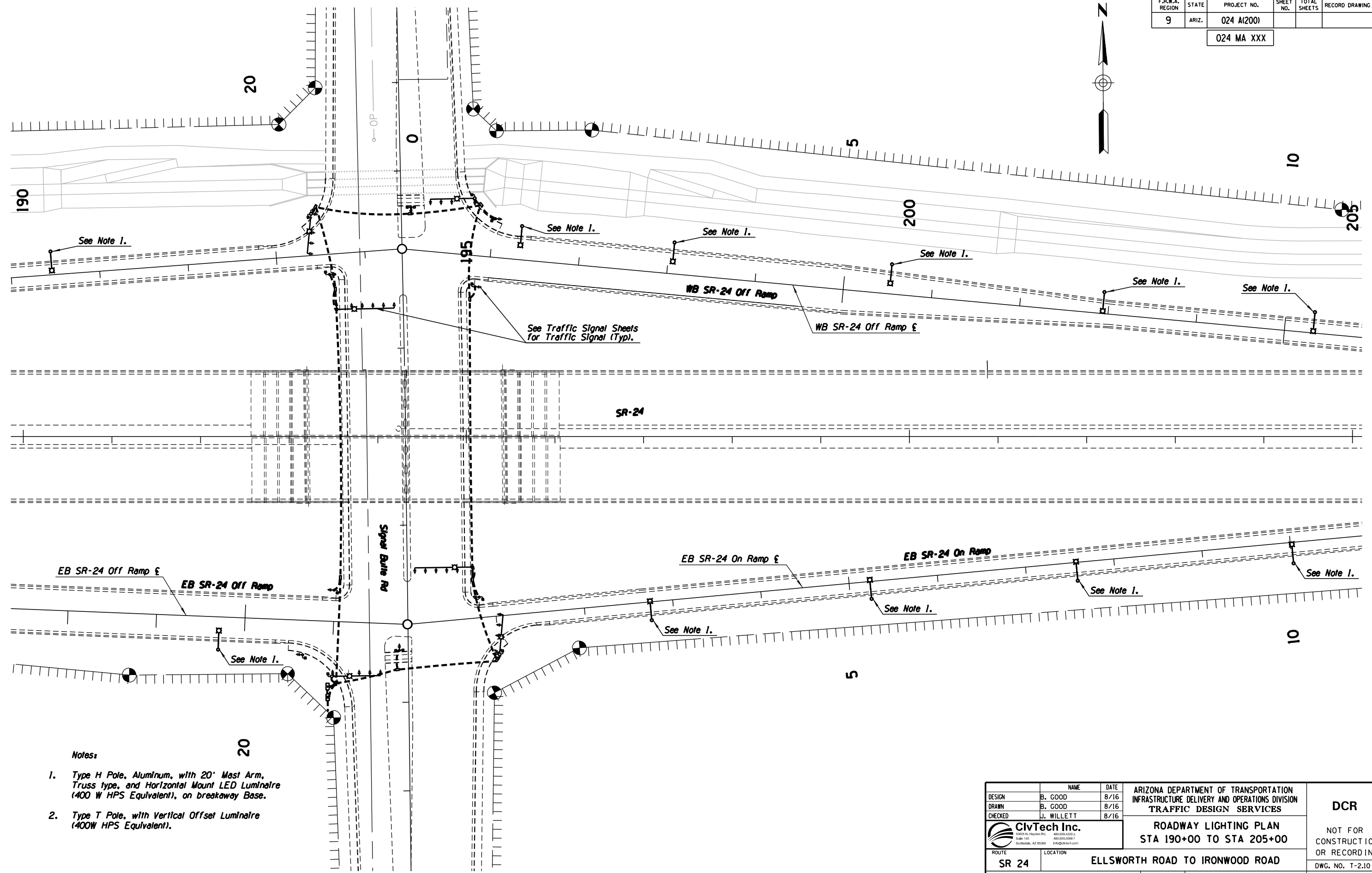
- Notes:**
1. Type H Pole, Aluminum, with 20' Mast Arm, Truss type, and Horizontal Mount LED Luminaire (400 W HPS Equivalent), on breakaway Base.
 2. Type T Pole, with Vertical Offset Luminaire (400W HPS Equivalent).

DESIGN	B. GOOD	8/16	ARIZONA DEPARTMENT OF TRANSPORTATION INFRASTRUCTURE DELIVERY AND OPERATIONS DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING DWG. NO. T-2.09
DRAWN	B. GOOD	8/16		
CHECKED	J. WILLETT	8/16		
		ROADWAY LIGHTING PLAN STA 175+00 TO STA 190+00		
ROUTE	SR 24	LOCATION	ELLSWORTH ROAD TO IRONWOOD ROAD	
TRACS NO. H8915 OIL/O2L		024 A (200)		OF

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F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	RECORD DRAWING
9	ARIZ.	024 A(200)			

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Notes:

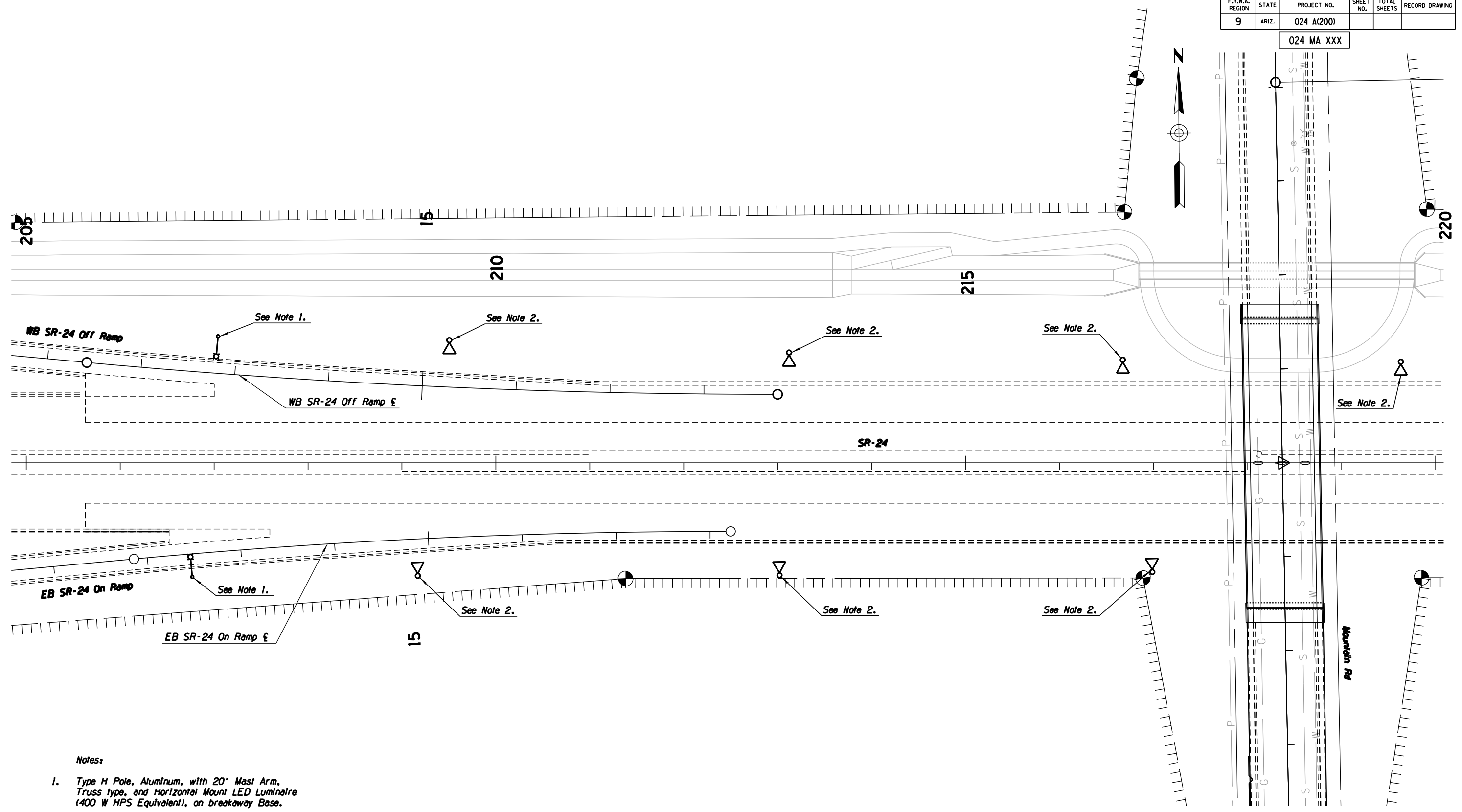
1. Type H Pole, Aluminum, with 20' Mast Arm, Truss type, and Horizontal Mount LED Luminaire (400 W HPS Equivalent), on breakaway Base.
2. Type T Pole, with Vertical Offset Luminaire (400W HPS Equivalent).

DESIGN	B. GOOD	DATE	8/16	ARIZONA DEPARTMENT OF TRANSPORTATION INFRASTRUCTURE DELIVERY AND OPERATIONS DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING
DRAWN	B. GOOD	DATE	8/16		
CHECKED	J. WILLETT	DATE	8/16		
		10000 N. Hayden Rd., Suite 100, Scottsdale, AZ 85250 480.355.0200 480.699.0909 info@civtech.com		ROADWAY LIGHTING PLAN STA 190+00 TO STA 205+00	
ROUTE	SR 24	LOCATION	ELLSWORTH ROAD TO IRONWOOD ROAD		
TRACS NO. H8915 OIL/O2L			024 A (200)		DWG. NO. T-2.10 OF

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F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	RECORD DRAWING
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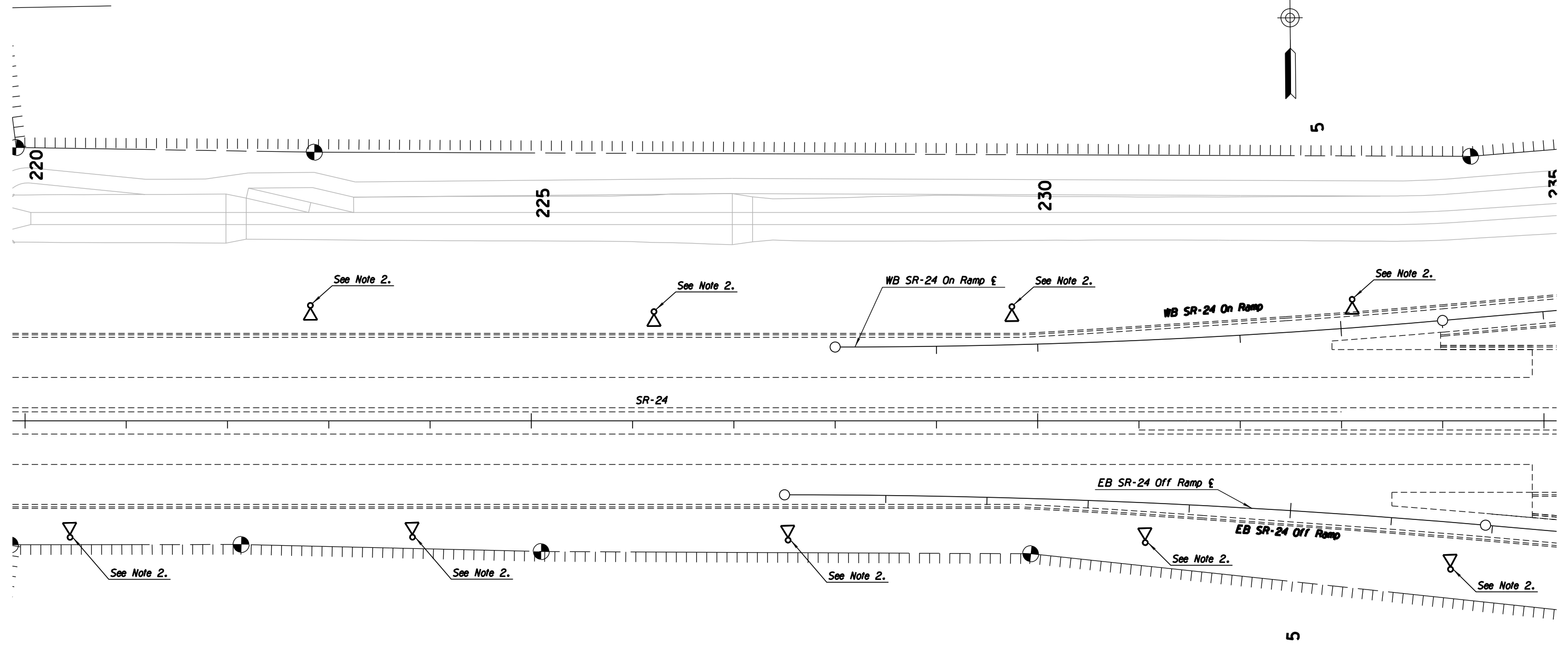
1. Type H Pole, Aluminum, with 20' Mast Arm, Truss type, and Horizontal Mount LED Luminaire (400 W HPS Equivalent), on breakaway Base.
2. Type T Pole, with Vertical Offset Luminaire (400W HPS Equivalent).

DESIGN	B. GOOD	DATE	8/16	ARIZONA DEPARTMENT OF TRANSPORTATION INFRASTRUCTURE DELIVERY AND OPERATIONS DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING
DRAWN	B. GOOD	DATE	8/16		
CHECKED	J. WILLETT	DATE	8/16		
		10800 N. Hayden Rd., Suite 100, Scottsdale, AZ 85250 480.255.0200 info@civtech.com		ROADWAY LIGHTING PLAN STA 205+00 TO STA 220+00	
ROUTE	SR 24	LOCATION	ELLSWORTH ROAD TO IRONWOOD ROAD		
TRACS NO. H8915 OIL/O2L			024 A (200)		DWG. NO. T-2.11 OF

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F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	RECORD DRAWING
9	ARIZ.	024 A(200)			

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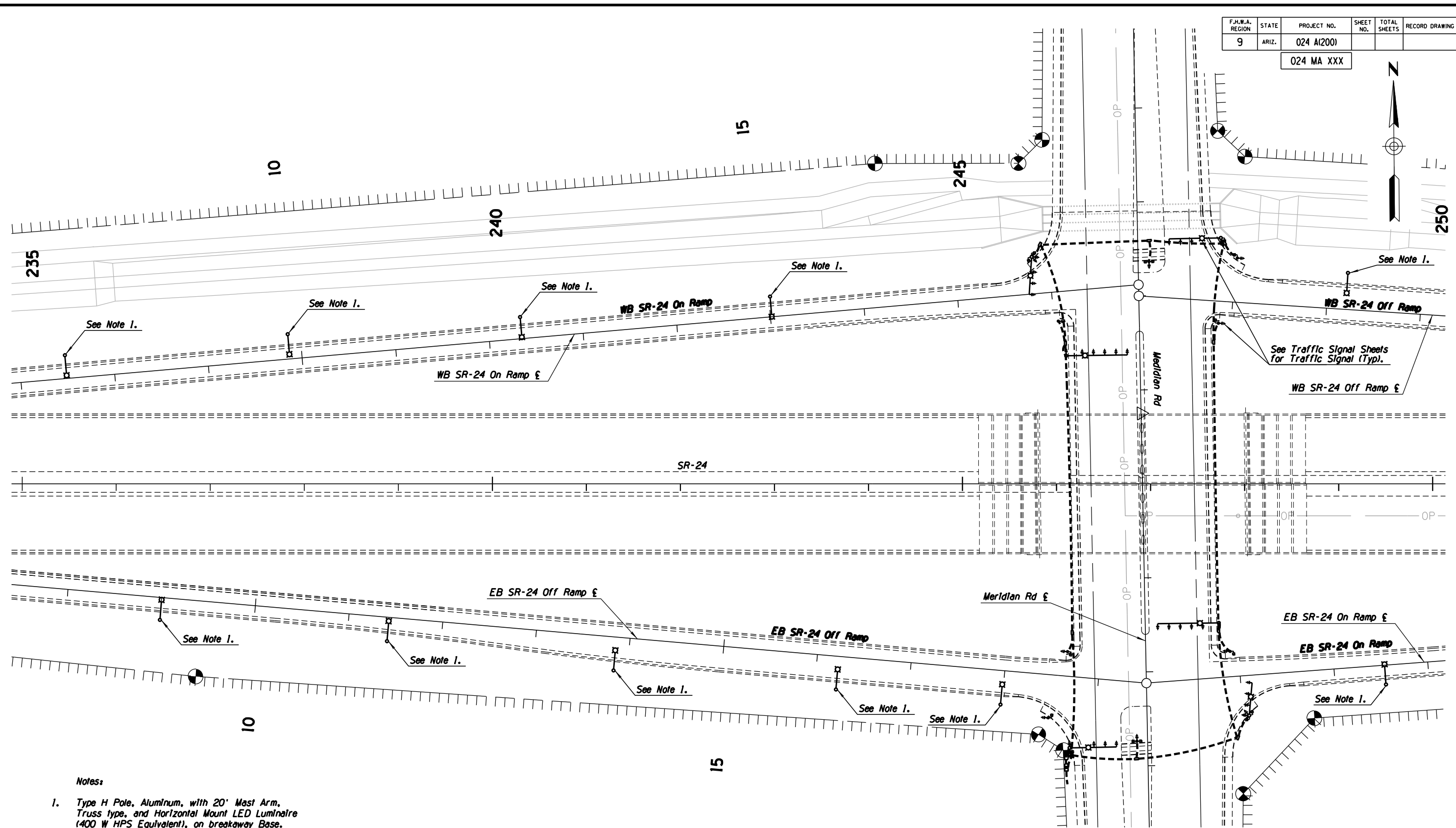
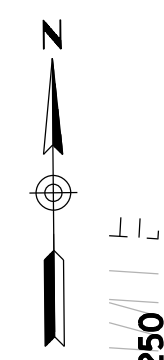
Notes:

1. Type H Pole, Aluminum, with 20' Mast Arm, Truss type, and Horizontal Mount LED Luminaire (400 W HPS Equivalent), on breakaway Base.
2. Type T Pole, with Vertical Offset Luminaire (400W HPS Equivalent).

DESIGN	B. GOOD	8/16	ARIZONA DEPARTMENT OF TRANSPORTATION INFRASTRUCTURE DELIVERY AND OPERATIONS DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING
DRAWN	B. GOOD	8/16		
CHECKED	J. WILLETT	8/16		
			ROADWAY LIGHTING PLAN STA 220+00 TO STA 235+00	DWG. NO. T-2.12
ROUTE	LOCATION			
SR 24	ELLSWORTH ROAD TO IRONWOOD ROAD			OF
TRACS NO. H8915 01L/02L			024 A (200)	

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Notes:

1. Type H Pole, Aluminum, with 20' Mast Arm, Truss type, and Horizontal Mount LED Luminaire (400 W HPS Equivalent), on breakaway Base.
2. Type T Pole, with Vertical Offset Luminaire (400W HPS Equivalent).

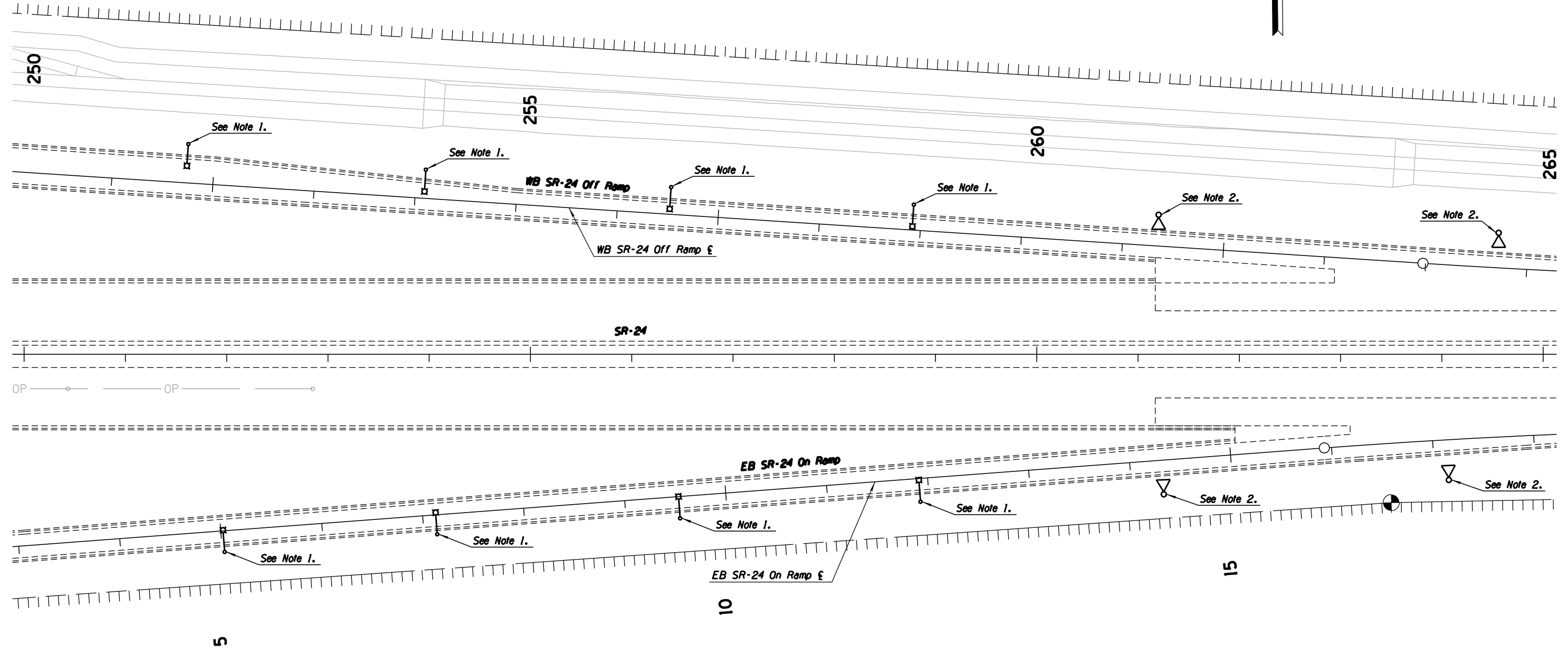
DESIGN	B. GOOD	8/16	ARIZONA DEPARTMENT OF TRANSPORTATION INFRASTRUCTURE DELIVERY AND OPERATIONS DIVISION TRAFFIC DESIGN SERVICES	DCR NOT FOR CONSTRUCTION OR RECORDING	
DRAWN	B. GOOD	8/16			
CHECKED	J. WILLETT	8/16			
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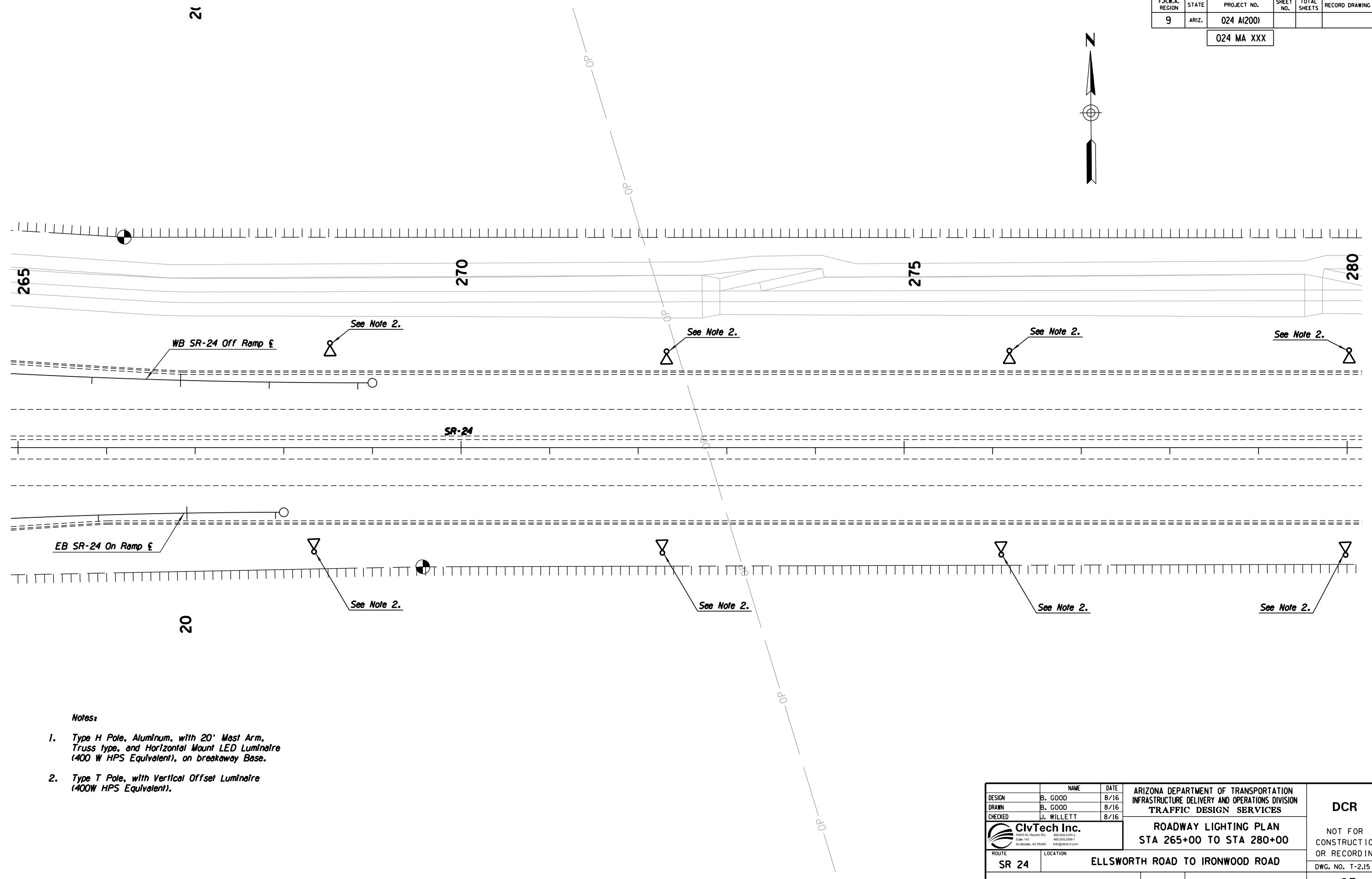
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		<small>10800 N. Hayden Rd., Suite 100, Scottsdale, AZ 85250</small> <small>480.999.0000</small> <small>info@civtech.com</small>		ROADWAY LIGHTING PLAN STA 250+00 TO STA 265+00	
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		10000 N. Hayden Rd., Suite 100, Scottsdale, AZ 85250 480.350.0200 info@civtech.com		ROADWAY LIGHTING PLAN STA 265+00 TO STA 280+00	
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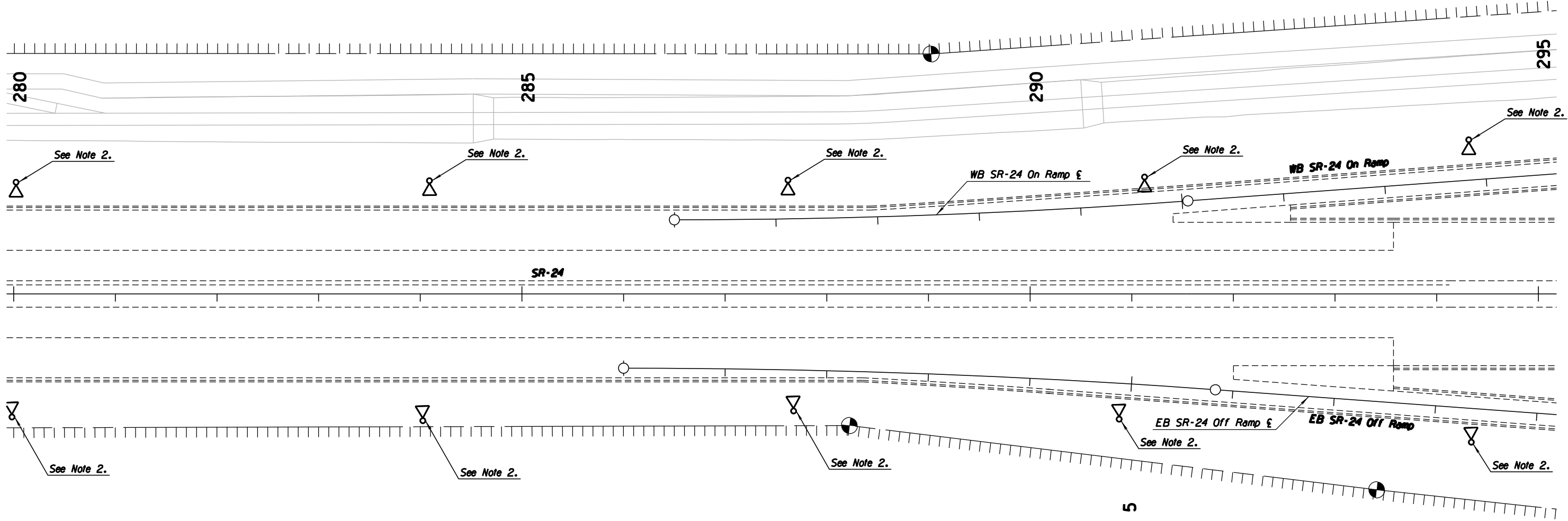
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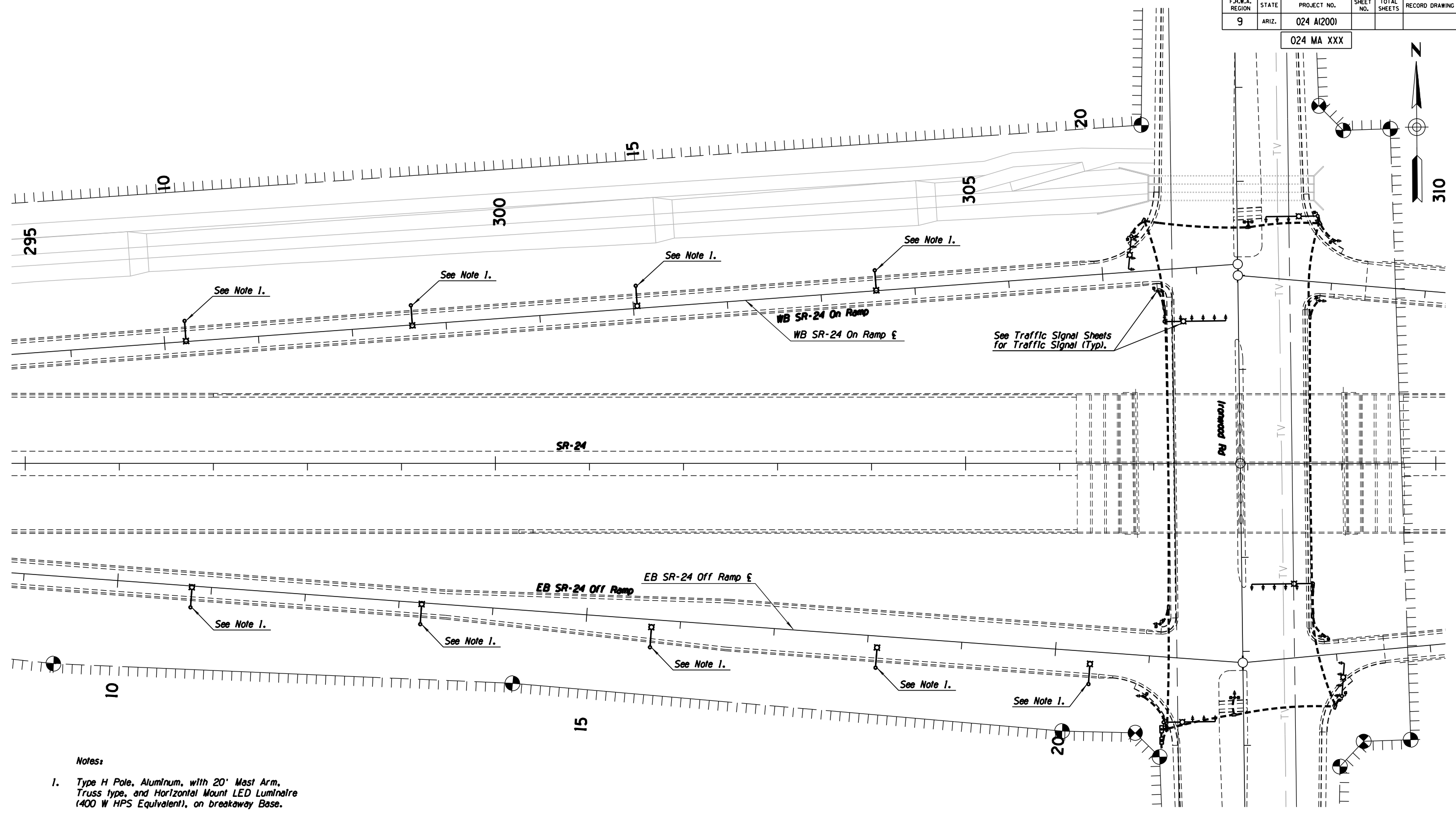
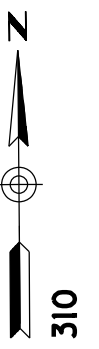
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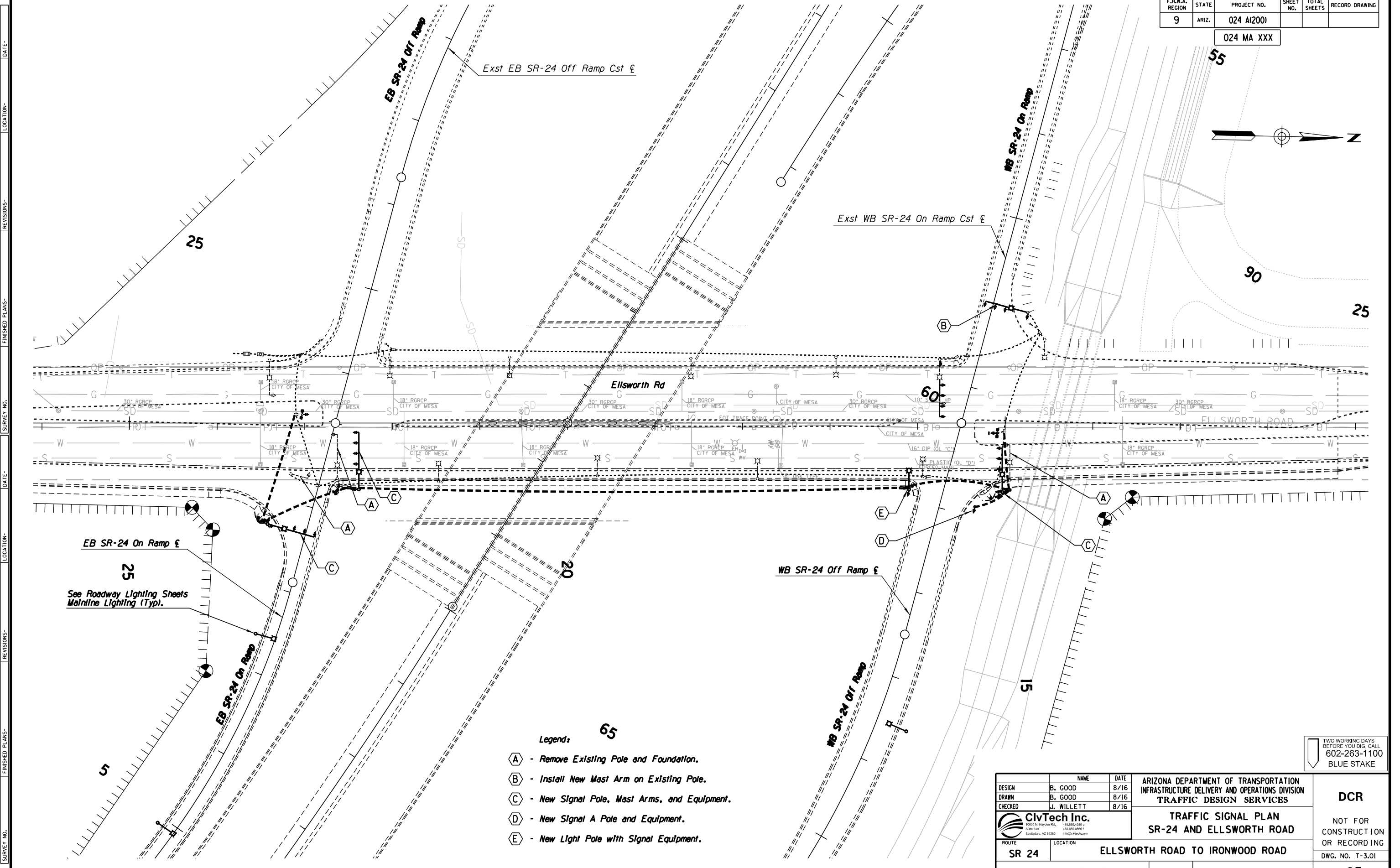
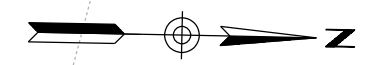


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Legends:

- (A) - Remove Existing Pole and Foundation.
- (B) - Install New Mast Arm on Existing Pole.
- (C) - New Signal Pole, Mast Arms, and Equipment.
- (D) - New Signal A Pole and Equipment.
- (E) - New Light Pole with Signal Equipment.

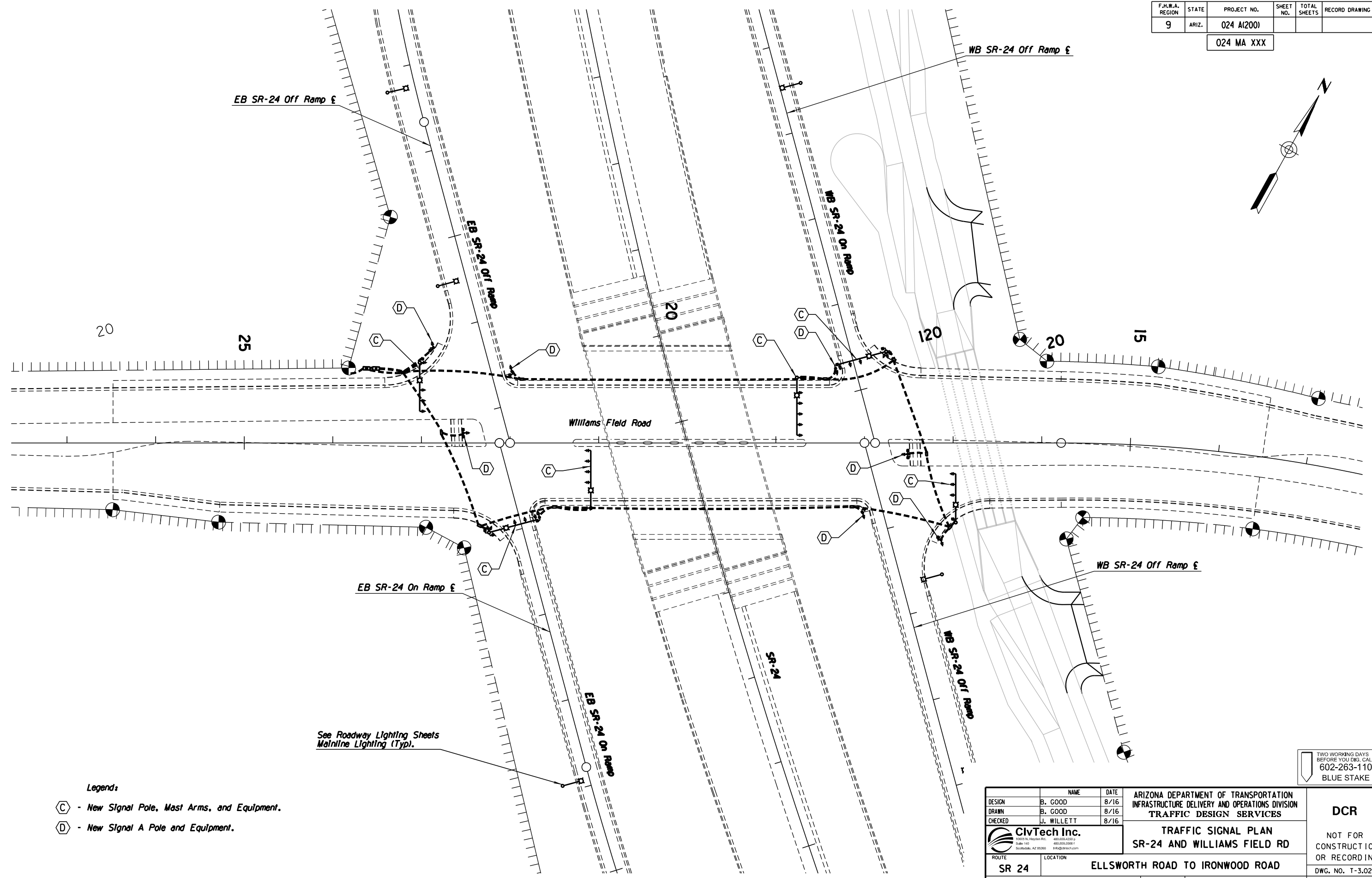
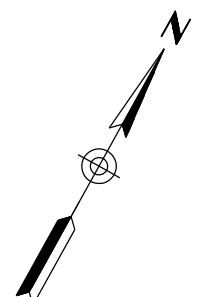
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See Roadway Lighting Sheets
Mainline Lighting (Typ).

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TWO WORKING DAYS
BEFORE YOU DIG. CALL
602-263-1100
BLUE STAKE

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See Roadway Lighting Sheets
Mainline Lighting (Typ).

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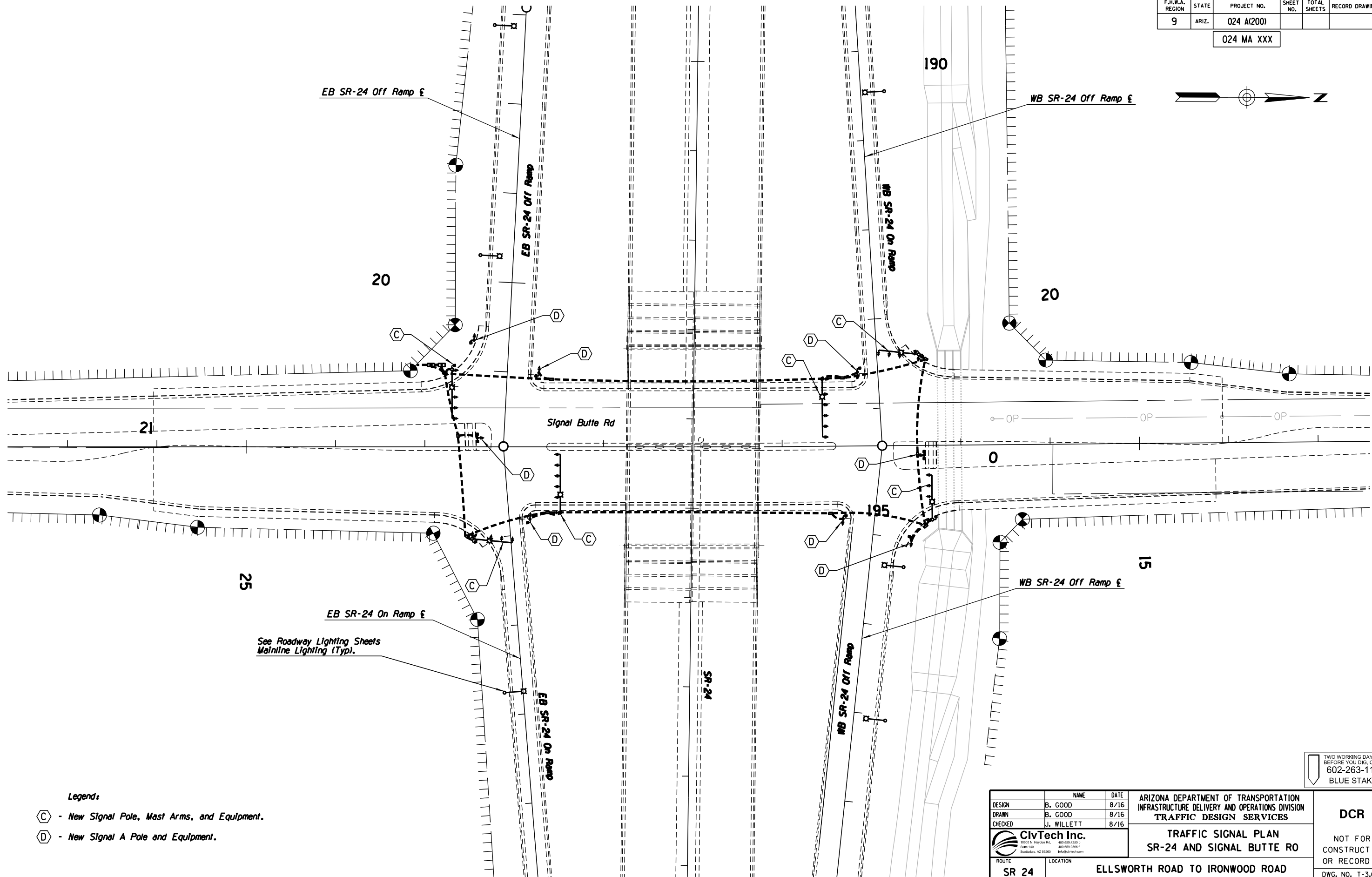
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 - (D) - New Signal A Pole and Equipment.

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See Roadway Lighting Sheets
Mainline Lighting (Typ).

- Legend:**
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 - (D) - New Signal A Pole and Equipment.

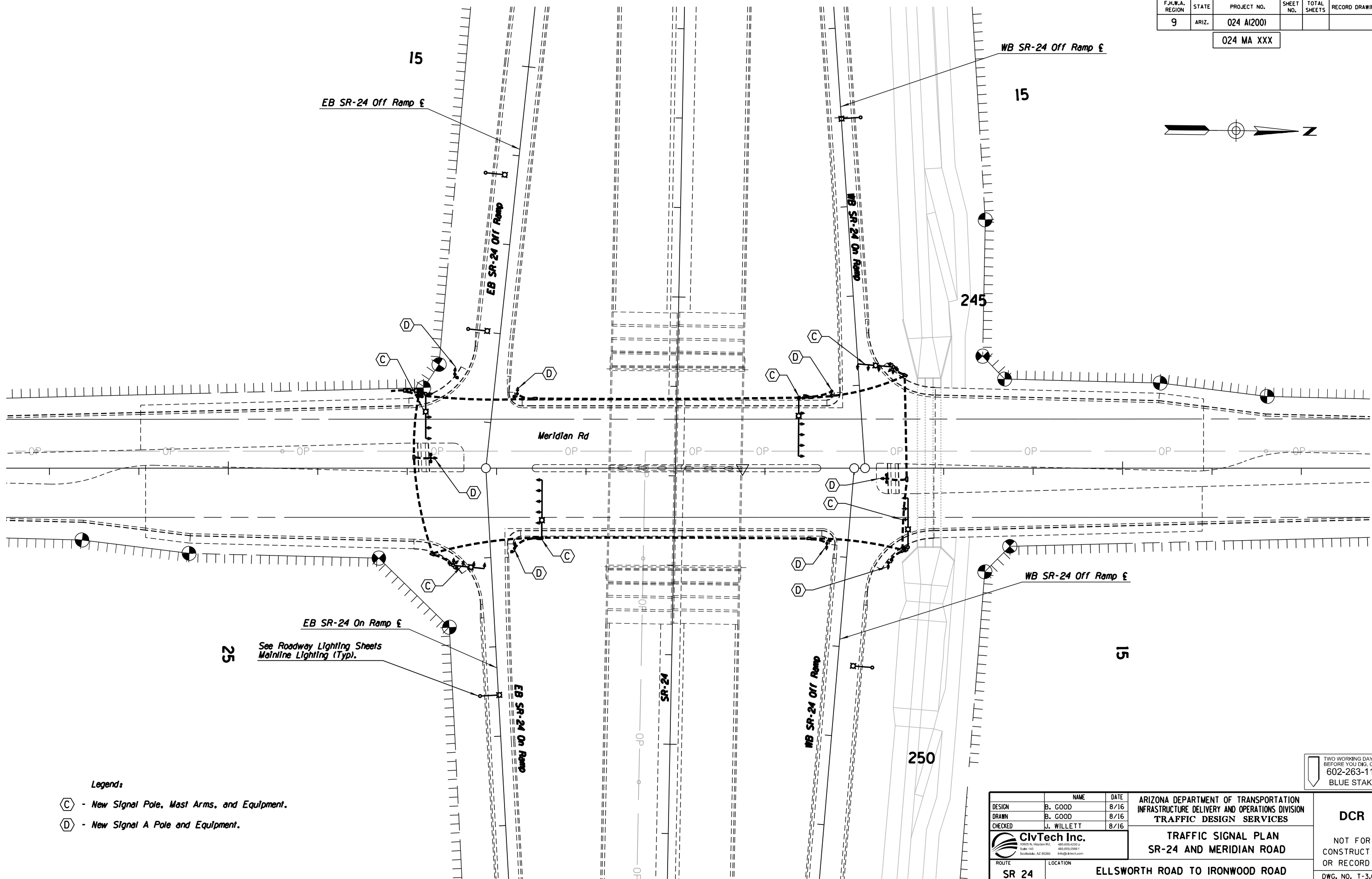
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Legends:

- (C) - New Signal Pole, Mast Arms, and Equipment.
- (D) - New Signal A Pole and Equipment.

TWO WORKING DAYS
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BLUE STAKE

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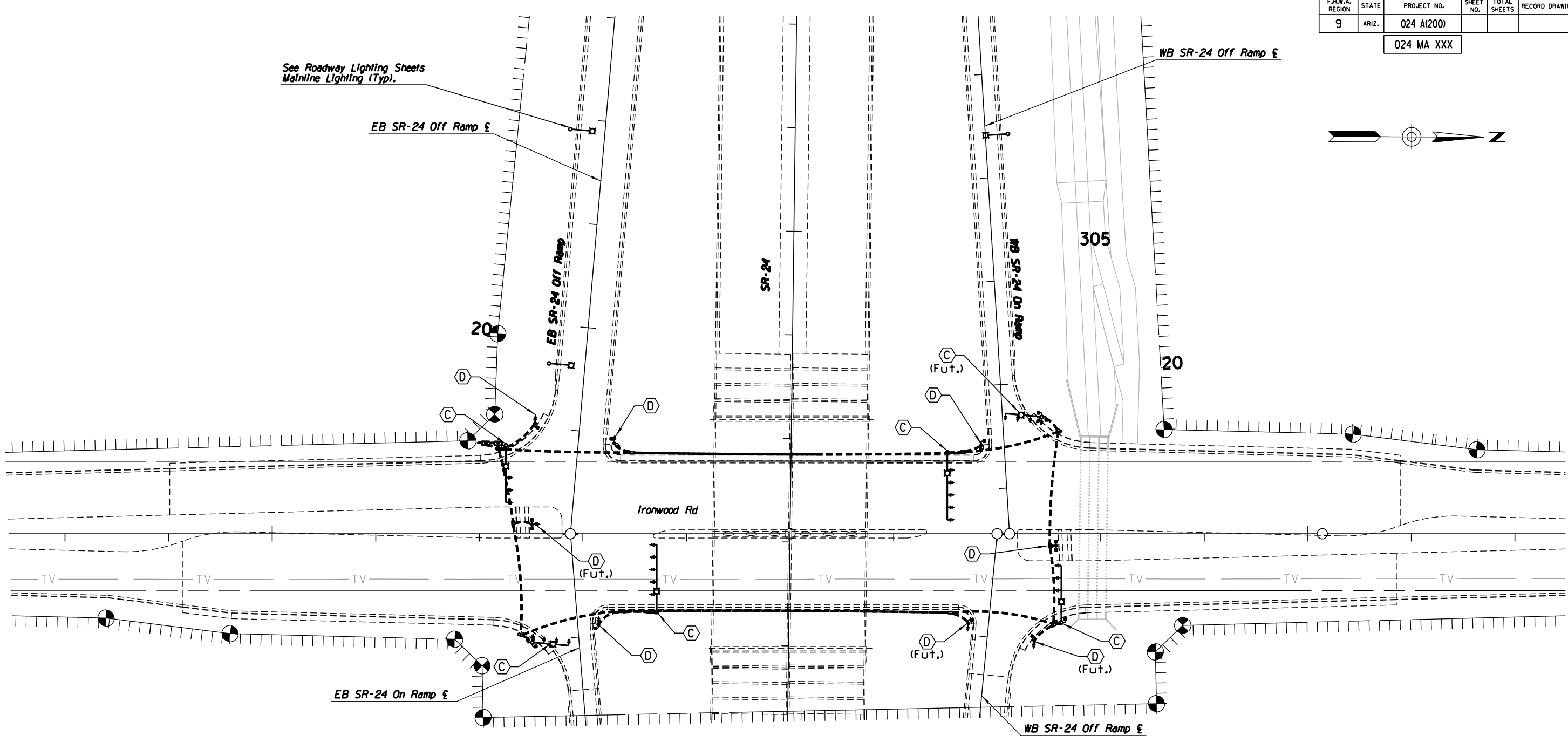
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See Roadway Lighting Sheets
Mainline Lighting (Typ).

EB SR-24 Off Ramp £

WB SR-24 Off Ramp £



EB SR-24 On Ramp £

WB SR-24 Off Ramp £

TWO WORKING DAYS
BEFORE YOU DIG. CALL
602-263-1100
BLUE STAKE

Legends:

- (C) - New Signal Pole, Mast Arms, and Equipment.
- (D) - New Signal A Pole and Equipment.

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**FINAL DESIGN CONCEPT REPORT
SR-24, Ellsworth Road to Ironwood Drive
Interim Phase II**

APPENDIX D – INITIAL DRAINAGE REPORT

Initial Drainage Report

in support of the
Interim Phase II DCR Plans

**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Drive,
in Maricopa County and Pinal County, Arizona**

ADOT TRACS No. H8915 01L/02L
FHWA Federal Aid Project No. 024 A (200)

Prepared For:



Arizona Department of Transportation

July 2016

Prepared by:

PARSONS
Parsons Transportation Group



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- B. Floodplain Maps
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- D. Off-site Hydrology
- E. Off-site Channel Hydraulics
- F. Retention Basin Calculations
- G. Draft Initial DCR Review Comments and Resolutions



Expires 6/30/18

1.0 BACKGROUND

State Route 24 (SR 24) (Gateway Freeway) is an important element of the Maricopa Association of Governments (MAG) (which is a Council of Governments that serves as the regional planning and policy agency for the metropolitan Phoenix area) adopted Regional Freeway System in the southeast portion of Maricopa County and extending into Pinal County. This area southeast of State Route 202 Loop (SR 202L) Santan Freeway within the City of Mesa and unincorporated areas of Maricopa County has been under development, the primary drivers being the improvements at the Phoenix-Mesa Gateway Airport (Airport), and the residential and commercial developments within the area of the former General Motors Proving Grounds. The regional traffic is projected to increase as development and its supporting arterial transportation systems are being expanded and improved. When fully completed, the SR 24 project will connect the existing and future arterial streets to the SR 202L to the west, and into Pinal County, to the east.

As a transportation corridor, the purpose of SR 24 is to provide regional connectivity to the residential and commercial centers by enhancing regional mobility of goods and services between Maricopa County and Pinal County, and to enhance access to the Airport. The MAG 2035 Regional Transportation Plan (RTP) (MAG, 2014) incorporated the SR 24 project under two segments:

- Segment I, between SR 202L and Ellsworth Road was constructed in 2014 as an interim project, including a full freeway-to-freeway interchange with the Santan Fwy and at-grade roadway improvements at Ellsworth Road. Two major drainage components were also constructed with Segment I: the Ellsworth Basin located north of SR 24 and west of Ellsworth Road, and the reinforced concrete box culvert (RCBC) under Ellsworth Road.
- Segment II, from Ellsworth Road to Ironwood Drive is part of Group 3 (MAG, 2014) projects scheduled between Fiscal Year (FY) 2027 and FY 2035, and was identified for final construction to be a six-lane freeway from Ellsworth Road to Meridian Road.

A timeline of events is summarized in *SR-24 Williams Gateway Freeway, Ellsworth Road - Ironwood Drive Interim Phase II Feasibility Study* (MAG, 2015).

With the increased development in the area, MAG and the City of Mesa are considering an interim project for Segment II ahead of the FY 2027 - FY 2035 construction window, which is the subject of the present analysis. The improvements will extend Segment I of SR 24 by approximately 4.6 miles east of Ellsworth Road (See Figure 1 for the project location). The proposed work would include two general purpose travel lanes in each direction separated by median, from Ellsworth Road to Ironwood Drive. The project would follow the alignment approved for the ultimate facility presented in the *SR 24, Gateway Freeway Final Design Concept Report* (FDCR) (ADOT 2011), but on a modified profile that maintains the roadway closely above existing ground for most of its extent and eliminates the need for a pump station to handle on-site drainage.

The major roadway work during the interim project would comprise:

- Constructing pavement for the outer two lanes of the ultimate facility between on- and off-ramps,
- Building one bridge structure to ultimate width,

- Constructing entrance and exit ramps that carry mainline traffic during the interim project, and improvements on surface streets within the Access Control limits.

The major drainage items of work would include:

- Constructing a concrete-lined drainage channel with in-line sedimentation basins along the entire project, including the portion of Segment I between Powerline Floodway and Ellsworth Road;
- Enlarging the Powerline Floodway to the west limits of the ADOT right-of-way and constructing the confluence with the SR 24 channel;
- Building a concrete-lined lateral weir, emergency spillway and a RCBC to connect the SR 24 channel to the Ellsworth Basin,
- Extending the existing RCBC at Ellsworth Road and building six RCBC structures under existing and future surface streets.

1.1 Project Location

The drainage project begins at SR 24 Station 32+23, approximately 50 feet east of the western limit of the ADOT right-of-way where a new confluence with Powerline Floodway. Here the enlarged Powerline Floodway would extend west and tie into an improved channel section developed as part of the Ellsworth Channel. The Ellsworth Channel Relocation work is done by the Airport as a separate project in conjunction with their improvements.

The drainage project ends at SR 24 Station 308+71, which is approximately the eastern end of the RCBC under Ironwood Drive.

Drainage improvements west of Meridian Road will be within the City of Mesa or Maricopa County Unincorporated Area situated within the City of Mesa planning area. Drainage improvements east of Meridian Road will be located within unincorporated Pinal County. (Figure 1 and Figure 2)

1.2 Description

This Draft Initial Drainage Report is a supporting document for the Interim Phase II DCR design submittal to the Arizona Department of Transportation (ADOT) made in February 2016. This report summarizes the design recommendations for the off-site drainage systems for the SR 24 Gateway Freeway, Ellsworth Road to Ironwood Drive, TRACS No. H8915 01L/02L, ADOT.

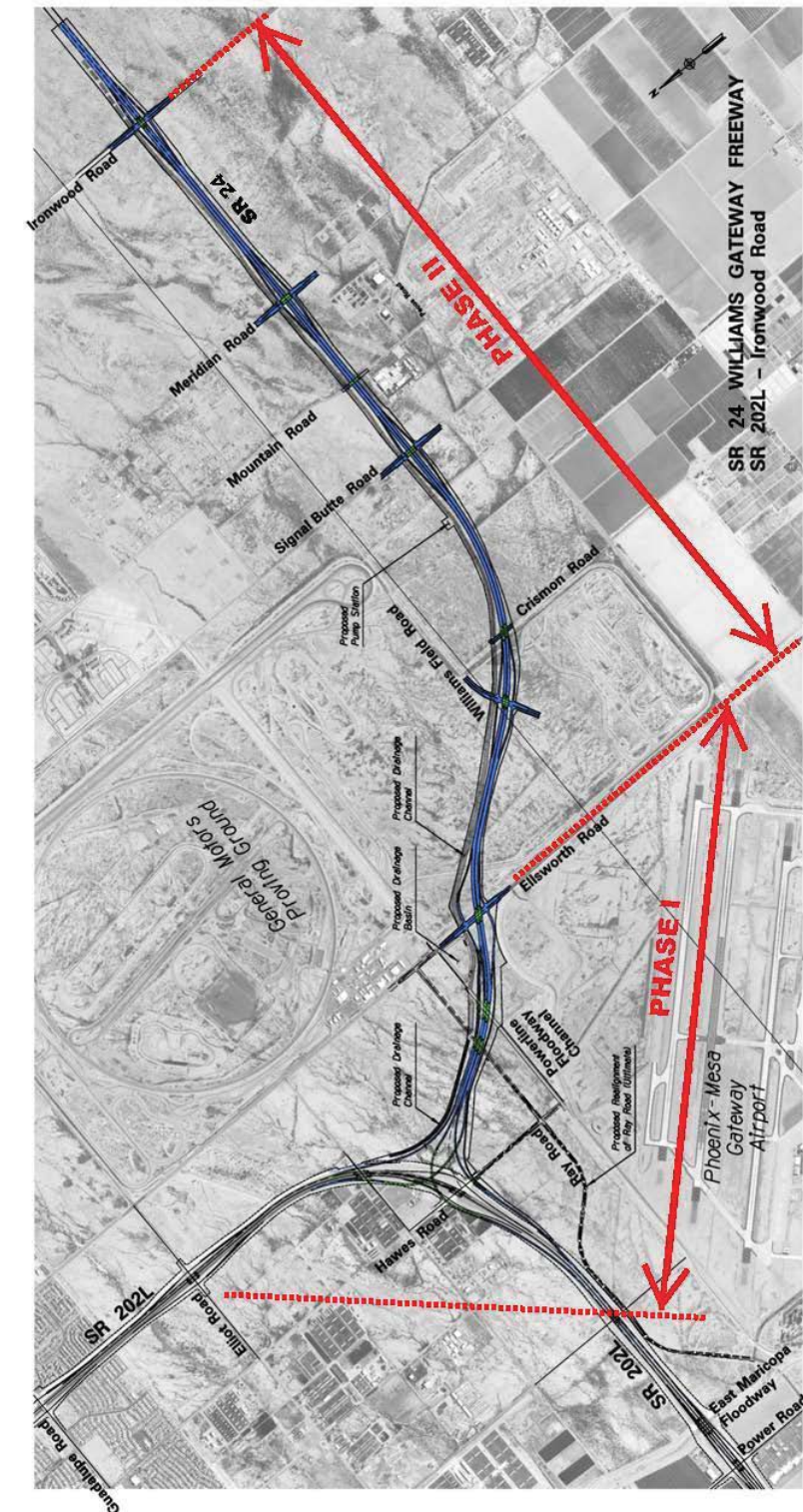
The hydrologic and hydraulic concepts for this project were prepared in accordance with current ADOT and FHWA design criteria, using hydrologic models developed by the Flood Control District of Maricopa County (FCDMC).

A set of DCR Civil Plans are included in Appendix A. The plans show the best available information for ADOT-owned facilities and private utilities. The existing utilities shown are in conformance with the utility designation survey performed for the *SR 24 Gateway Freeway FDCR*, (ADOT, 2011).

Figure 1 – Location Map (Based on State Highway System, 2014 ADOT Map Book)



Figure 2 – Vicinity Map



2.0 CONCEPT PLAN DEVELOPMENT

This interim project is an extension of the interim Phase I project completed in March 2014. It is a green-field project extending from Ellsworth Road east to Ironwood Drive for approximately 4.6 miles. At the time this report is released, the proposed roadway passes through a predominantly undeveloped, or suburban environment, but master planned residential and commercial developments are being planned particularly north of the roadway.

There are no existing grade separation bridge structures east of Ellsworth Road within this project corridor, as major arterial streets that cross SR 24 (Signal Butte Road and Meridian Road) have not been developed/improved yet.

Transportation improvements are being discussed for simultaneous implementation with the SR 24 interim project to provide regional north-south connectivity within the project limits. The City of Mesa has expressed a willingness to accelerate the improvements for Signal Butte Road, from Williams Field Road to Pecos Road. Also, the segment of Signal Butte Road north of Williams Field Road, and the north side of Williams Field Road east of Signal Butte Road, are currently being constructed/improved by developers.

The roadway improvements that are being, or will be, constructed with the project and adjacent to the project constitute the existing condition and basis of design for the interim SR 24 Ellsworth Road to Ironwood Drive project.

2.1 Local Watershed

The general topography north of SR 24 and east of SR 202L slopes from the north and northeast to the south and southwest. Storm water runoff is conveyed to a slight depression located between SR 24 and Pecos Road (See Figure 2, where washes are indicated by darker vegetated areas). This depression concentrates flows approaching from northeast, and from the east and southeast. In the proposed condition SR 24 will form a barrier prohibiting flow across the freeway from the north and northeast. For a detailed description of the watershed see SR 24 Gateway Freeway FDCR (ADOT, 2011), and East Mesa ADMPU (FCDMC, 2013a).

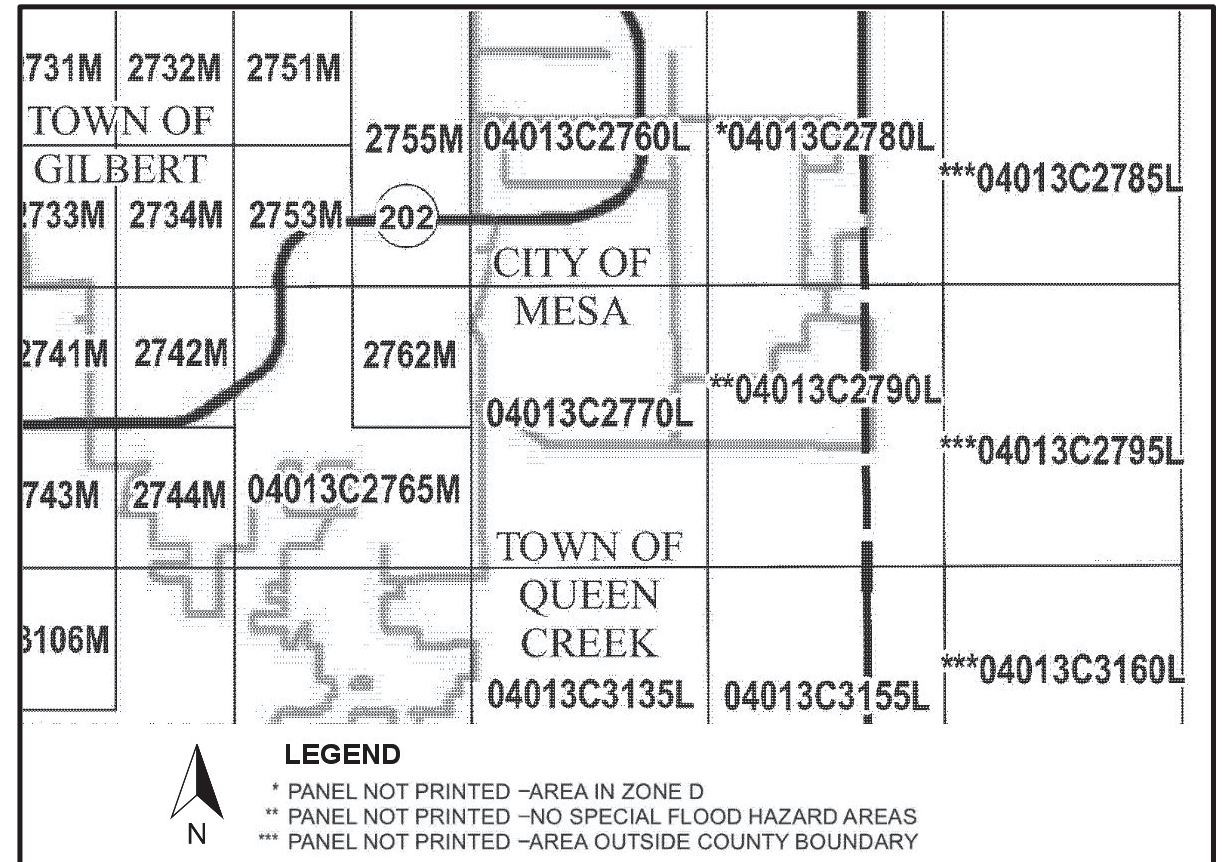
2.2 Floodplain Locations

A review of the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Maps (FIRM) for the project area indicates that this project is located within portions of a 100-year floodplain. Figure 3 shows an excerpt of the FIRM Map index (04013CIND0C) for Maricopa County, AZ, but flood hazards have either been listed as Zone D (04013C2780L) or have not been mapped (04013C2760L, 04013C2770L and 04013C2790L) in the project area located within Maricopa County. According to FEMA, the Zone D designation is used for areas where there are possible but undetermined flood hazards, as no analysis of flood hazards has been conducted (FEMA, 2011).

However, the FIRM maps within Pinal County identify flood hazards north of and crossing the SR 24 corridor. These areas identified as floodplains include a crossing of SR 24 at Meridian Road (Zone A and Zone X in map panel 04021C0200E, December 4, 2007); this hazard would extend into Maricopa County west of Meridian Road to Signal Butte Road, but it is not mapped as such. It is also noted that the effective FIRM was not revised subsequent to the Ironwood Drive Improvements.

Copies of the floodplain maps within the project area are included in Appendix B.

Figure 3 – FIRM Map Index (04013CIND0C) for Maricopa County, AZ (November 4, 2015) - Excerpt



This project would intercept the flows approaching the transportation corridor from the northeast between Signal Butte Road and Meridian Road and divert them to the west. Future floodplains would be revised by the project, but at the moment no flooding hazard is mapped in this area.

2.3 Review of Previous Studies, Reports and Design/As-Built Plans

Several existing studies have been performed in the project area. A list and description (where applicable) of each study is presented below.

- *East Mesa Area Drainage Master Plan Update, Arizona, November 2013 by Entellus for FCDMC.* The Flood Control District of Maricopa County requested an update of the East Mesa Area Drainage Master Plan (ADMP) dating back to 1998. East Mesa Area Drainage Master Plan Update (ADMPU) developed and recommended strategies to reduce flood hazards and protect public safety in a 58-square-mile portion of southeastern Maricopa County. The study area includes portions of Mesa, Queen Creek, Gilbert, and unincorporated Maricopa and Pinal counties. Multiple hydrologic models were developed for

existing and ultimate-development conditions using a range of storm frequency events (FCDMC, 2013a).

- *Powerline Floodway Hydraulic Analysis Technical Memorandum, East Mesa Area Drainage Master Plan Update, Arizona, November 2013 by Entellus for FCDMC.* This memorandum focused on a capacity analysis for Powerline Floodway, which is a concrete-lined channel draining the Powerline, Vineyard Road, and Rittenhouse Flood Retarding Structures (FCDMC, 2013b).
- *City of Mesa Storm Drain Master Plan (SDMP), Arizona, January 2010 by Entellus for City of Mesa.* The SDMP studied the current City Storm Drain System and identified necessary improvements. The system was evaluated against the latest City drainage criteria and hydrologic modeling results developed by the City and the Flood Control District of Maricopa County. The recommended changes included revisions to the City Drainage Regulations for retention design, minimum storm drain sizes, manhole spacing, and first flush requirements for AZPDES, including recommendations for inclusion of green drainage solutions (Entellus, 2010).
- *Bella Via Mountain Road, Mesa, Arizona, Final Drainage Report, February 2014 by HilgartWilson for Pulte Group.* The report documented the drainage analysis and improvements of the Mountain Road alignment as part of the Bella Via (formerly known as Mountain Horizons) master planned development (HilgartWilson, 2014).
- *Master Drainage Report Update for Eastmark, Revised April 24, 2014, by Wood Patel and Associates for DMB Mesa Proving Grounds, LLC.* This document incorporated proposed land use for Eastmark (previously known as Mesa Proving Grounds) Development. The report updated the hydrologic modeling as well as the hydraulic analysis and design within the Development, including that of the off-site channel that runs along the southeast corner of the property (Wood Patel, 2014).
- *Final Drainage Report for Gila River Ranches, Warner and Meridian, Mesa, Arizona, Second Revision January 25, 2005 by CMX for Gila River Ranches LLC.* The report documented on-site and off-site pre- and post-development hydrologic estimates, calculated street, ditch and storm drain flows as well as the volumes necessary to meet retention requirements. To protect the east boundary of the property from the off-site 100-year flows, Meridian Drive was elevated. Off-site runoff north of the Powerline Floodway was directed south along Meridian Road. South of the Powerline Floodway off-site runoff transitioned back into sheet flow conditions and drain southwesterly in historic flow patterns (CMX, 2005a).
- *Off-site Flow Management for Gila River Ranches 4625 S Mountain Road at Warner and Meridian, Mesa, Arizona Revised June 15, 2005 by CMX for Meritage Homes.* The report addresses the drainage management plan for the off-site flows that impact the east boundary of the Gila River Ranches. The plan proposed to direct the off-site flows along the east side of Meridian Road, which will be elevated above natural ground, toward the Powerline Floodway Channel. Also, the capacity of Powerline Floodway was improved to Signal Butte Road (CMX, 2005b).
- *Final Drainage Report Ironwood Drive Ocotillo Road – US 60 – Phase B, April 2007, by Kimley-Horn and Associates for Pinal County Department of Public Works.* The report identified drainage improvements for the Ironwood Drive/Gantzel Road Project, that

extended between Ocotillo Road and the intersection of US 60 and Ironwood Drive. This report documents the methodology and results of the hydrologic analysis as well as the existing and proposed drainage conditions along the approximately 9.5 mile-long project. Existing type, size, and location of cross drainage structures were documented and recommendations were made for improvements to the drainage infrastructure. Analysis of the off-site hydrology, existing cross culverts, and roadway drainage was performed in accordance with Pinal County Drainage Standards and the Draft Drainage Design Manual (Drainage Manual). The analysis was supplemented by ADOT hydrologic design criteria. This design was implemented with the Ironwood Drive roadway improvements and the results of the analysis were later used for a split flow calculation that was incorporated in the East Mesa ADMPU (Kimley-Horn, 2007).

- *Preliminary Drainage Report for Keighley Place, August 2, 2005, by LandAide Inc. for Providence Homes.* The report documents on-site and off-site hydrology estimates for the Keighley Place Development located at the northwest corner of Meridian Road and Ray Road. The subdivision layout indicated that off-site runoff approaching from northeast and moving to southwest crosses the site within the pre-development drainage corridor (LandAide, 2005)
- *Final Drainage Report for Mountain Horizons South of the Powerline Floodway 5210 South Mountain Road, Mesa, AZ by CMX LLC for Pulte Homes, August 2006.* The report detailed the pre- and post-development on-site and off-site drainage analysis. It included hydrology estimates and hydraulic calculations for storm drains and retention capacities. The off-site drainage analysis was based on regional hydrology developed for the East Mesa Area Drainage Master Plan prior to its 2013 update. (CMX, 2006)
- *Addendum to Final Drainage Report for Mountain Horizons South of the Powerline Floodway 5210 South Mountain Road, Mesa, AZ (August 2006) by CMX LLC for Pulte Homes, January 2008.* The addendum incorporated revisions due to modifications of the Mountain Horizons grading plans. It included updated post-development hydraulic calculations for storm drains and retention capacities. (CMX, 2008)
- *Master Drainage Report for Harvard Investments Pacific Proving Grounds North (PPGN), City of Mesa, Arizona, March 2013, by EPS Group for Harvard Investments.* The report focused on the existing surrounding regional conditions, the proposed regional conditions with the development of PPGN among other planned regional improvements, and it presented the results of a broad analysis of the PPGN drainage areas, runoff, retention, storage, and drainage management strategy in compliance with City of Mesa standards. The report discussed the management of off-site flows, particularly of those approaching from the east at the south boundary of the development. These flows would be conveyed through an extension of the channel departing the Eastmark development by heading west along future Williams Field Road, and then turning south after crossings the Crismon Road alignment. This channel would ultimately outfall into the SR 24 channel once the latter is constructed (EPG, 2013).

The following As-Built and Final Design plans have been reviewed:

- *024 MA 000 H6867 01 C, SR 24: SR 202L to Ellsworth Road, March 5, 2015.*

2.4 Design Constraints and Opportunities

According to the ADOT *SR 24 Gateway Freeway Final Design Concept Report, April 2011* the recommended alternative for the ultimate project profile consists of a four-lane mainline with grade-separated intersections. The cross streets are maintained at or just above existing grade. The intersections at Ellsworth Road, Williams Field Road and Crismon Road are overpasses. Provisions are made for the Ironwood Drive intersection to be a proposed overpass, as well. Between approximate Station 156+50 to approximate Station 275+20 the mainline profile is depressed below existing ground, hence the intersections at Signal Butte Road, Mountain Road and Meridian Road are underpasses. The depressed profile requires a deep on-site drainage system serviced by a pump station that would outfall into the SR 24 channel proposed on the north side of the roadway.

The phased development of SR 24 involving an interim facility to Ironwood Drive presents an opportunity for a revised roadway profile, which keeps the proposed grade slightly above existing ground. This opportunity is also justified by the elimination of a costly pump station and deep storm drain trunk line that would be required for a depressed mainline profile. Furthermore, some of the major roads do not exist yet or are at a very incipient stage; it would be more cost effective for the crossings at Crismon Road and Mountain Road, for instance, to go over SR 24 through a bridge structure either by being constructed at a later date, or with the interim SR 24 project.

A coherent drainage design concept could be implemented for both on-site and off-site by using elements of the recommended ultimate project. The off-site channel would be maintained on the north side of the project to intercept overland runoff through sheet flow as well as concentrated input. The flow approaching from the north is a major design constraint that dictates the size and the capacity of the channel along the project. Provisions would be made for the channel to be concrete-lined and provide sufficient flow capacity to accommodate existing 100-year flows within the freeboard. The channel could also be relocated closer to the roadway taking advantage of the smaller roadway footprint and reducing the need for right-of-way.

The on-site drainage elements of the interim project would be greatly simplified by maximizing the use of sheet flow and surface conveyance in ditches. Water quality treatment would be provided in shallow linear basins located on both sides of the roadway within the existing right-of-way. These basins would be located in cascading sequence and sized for handling the ultimate water quality volume. The medians would require minimal grading and runoff collected within would flow overland downstream to the next cross road where the flow would be collected and transferred to the infield areas.

3.0 ON-SITE DRAINAGE DESIGN

SR 24 is discussed in this section as an interim project between Ellsworth Road and Ironwood Drive, but provisions are made for the ultimate configurations and runoff flows. The pavement will be normal crowned at most locations to allow for continued drainage to the outside shoulder and to roadside ditches. The proposed interim two lanes of traffic would be located at the outside limit of the ultimate section. In super-elevated sections, catch basins would be placed along the median barrier rail to collect runoff.

3.1 On-Site Existing Conditions

The existing drainage improvements on the corridor are related to Segment I of the project finalized in May 2014 between SR 202L and Ellsworth Road, and the improved Ellsworth Road and Ironwood Drive. At Mountain Road the on-site drainage is limited to roadside ditches.

Currently, on-site freeway drainage is collected in catch basins and conveyed through lateral pipes into existing off-site drainage systems. Runoff is also collected by catch basin inlets within the limits of the Ellsworth Road improvements. Ironwood Drive is a median-separated facility and runoff sheet flows off the edge of the pavement to the outside ditches; median flows are intercepted at the culverts crossing the road.

The existing on-site drainage system would see minor modifications including:

- Several cross pipes that currently discharge into the Ellsworth Basin across the future SR 24 channel would be cut short and discharge into the SR 24 channel once that is built.
- Should the need for a grade-separated crossing at Ellsworth Road be justified by the traffic analysis, the footprint of the temporary basin between the existing on- and off-ramps at Ellsworth Road would be reduced to construct the mainline embankment.
- At Mountain Road a grade-separated crossing is proposed. Mountain Road would cross above SR 24 through a bridge and the roadway section would be improved. Existing roadway side ditches north of the project would be intercepted by the SR 24 channel.
- Ironwood Drive would be improved within the access control limits. Curb and gutter and catch basins would direct and intercept the on-site runoff on each side of the road. Storm drain pipes would convey the flow to the SR 24 channel or the RCBC crossing Ironwood Drive.

In areas of super-elevation, catch basins along the concrete median half barrier are provided to intercept and remove drainage flows from the roadway.

3.2 Design Criteria

The on-site hydrology has not been analyzed as part of this study, and such an analysis is deferred to a later design stage. In the meantime, the on-site hydrologic analysis done for the *SR 24 Gateway Freeway Final Design Concept Report*, April 2011 (ADOT, 2011) is referenced herein.

The procedures described in the *ADOT Roadway Design Guidelines* (RDG) (ADOT, 2014a), *ADOT Highway Drainage Design Manual, Volume 2, Hydrology* (HDDM2) (ADOT, 2014b) and *ADOT Highway Drainage Design Manual, Volume 3, Hydraulics* (HDDM3) (ADOT, 2014c), are applicable.

The Rational Method is used to develop the 10-year and 50-year peak runoffs based on a site-specific Intensity-Duration Frequency (I-D-F) (ADOT, 2011).

The Rational Formula is:

$$Q = C i A$$

where:

Q = the peak discharge in cfs

C = runoff coefficient

i = the average rainfall intensity, in inches/hour (in/hr) for the selected rainfall return period

A = the contributing drainage area in acres

The following values of "C" are used:

- Paved surfaces – 0.95
- Highway landscaped slopes – 0.70

The rainfall intensity is estimated based upon the time of concentration at the point being analyzed. A site-specific I-D-F Graph, developed from the procedures in the HDDM2, is used to estimate the average rainfall intensity. The initial time of concentration is calculated from Equation 2-2 of the HDDM2 as follows:

$$T_c = 11.4 L^{0.5} K_b^{0.52} S^{-0.31} I^{-0.38}$$

where:

T_c = time of concentration in hours

L = the length of the longest flow path in miles

K_b = the watershed resistance coefficient from Table 2-1, HDDM2

S = the slope of the longest flow path in ft/mile

I = the average rainfall intensity in in/hr (same as Equation 2-1, HDDM2)

The minimum T_c , and therefore the minimum rainfall duration, is ten (10) minutes. For Stage II design, all on-site drainage areas have been assumed to have a 10 minute time of concentration.

The following drainage criteria will be applied to the on-site hydrology design and are found in Chapter 600, of the *ADOT Roadway Design Guidelines* (ADOT, 2014a):

- Storm Drain Design Storm Frequency is 10 years for at grade/elevated mainline, ramps and crossroads and 50 years for depressed areas per Section 603.2.
- Hydraulic grade line shall be at least 6 inches below the top of the catch basin grate for the Storm Drainage System per Section 603.2.
- For the 10-year storm, the allowable spread (ponding width) shall not exceed the width of the roadway gutter, shoulder, parking lane and/or distress lane and one-half of the adjacent lane (for roadways with more than one lane) per Section 603.2.
- Inlet Capture Ratios shall conform to Table 606.2 of RDG.
- Restrictions on types of inlets are found in subsection 606.2.B of RDG.
- Minimum pipe size for storm drains shall be 24 inches except those pipes connecting catch basins to trunk lines may not be less than 18 inches per Section 607.1.
- Desirable "self cleaning" velocity is 3 feet per sec (fps) flowing full. The minimum velocity flowing full is 2 fps per Section 607.1. Some exceptions occur due to catch basins requirements at transitions and end of barriers and short pipe connections of flanking inlets.
- Allowable ponding depth on highways shall not exceed the height of the curb for a 10-year storm frequency per Section 603.2.
- The capacity of ditches that are parallel to the roadway and serve to convey on-site roadway drainage shall be designed to meet the requirements of the 10-year storm frequency and the Hydraulic Grade Line must be below the subgrade, (or 3" below pavement elevation for the 50-year storm) per Section 603.2. In addition, the ditches that drain sag points must be checked for the 50-year storm peak flow.
- Storm drain lengths are limited to the desirable maximum distance between manholes per Table 607.2.

Pipes under 33 inches in diameter – 330 feet
 Pipes 36 and 39 inches in diameter – 440 feet
 Pipes from 42 to 69 inches in diameter – 660 feet
 Pipes 72 inches in diameter and larger – 1,200 feet

The following pipe design criteria will be used on this project and are found in the *ADOT Pipe Selection Guidelines and Procedures* (ADOT, 1996).

- Approved pipe types are reinforced concrete pipe (RCP), non-reinforced concrete pipe (NRCP), and corrugated high density polyethylene plastic pipe (CHDPEPP) Class S up to

42 inches in diameter in fills less than 10 feet. No corrugated pipe is allowed in closed systems.

- Pipe roughness values of 0.012 shall be used for all pipes except for non-reinforced cast-in-place concrete pipe (NRCIPCP) which has a pipe roughness value of 0.014.

Drainage areas, which include shoulders, median and side slopes, are identified by examination of the roadway plan and profile. New inlet catch basins that are to be placed along the median barrier are sized for the ultimate freeway section.

3.3 Inlet Design

The standard catch basin inlets used for the project are ADOT Standards C-15.91 and C-15.92. Slotted drains (ADOT Standard C-13.60) supplement catch basins; they have been used extensively to minimize the number of inlets in the system and to control runoff spread. These inlets would be used at the superelevated or grade-elevated sections of the project (approaches to grade-separated crossings) where curb and gutter is used, or to improved surface streets with curb and gutter. For the rest of the interim project, as the finished grade profile is only slightly elevated above the existing grade and the pavement width is limited to two lanes of traffic plus shoulders, the curb and gutter could be eliminated leaving the on-site runoff to sheetflow over the edge of pavement.

New C-15.90 area catch basins are considered for the future infield areas at Ellsworth Road, future William Field Road, Signal Butte Road, Meridian Road and Ironwood Drive. For the interim project these inlets would bleed-off the areas between on- and off-ramps that would be used for water quality treatment. Median inlets are not anticipated with the interim project.

Grate inlets are designed with a 50% clogging factor except when flanking catch basins are provided at sag locations. The flanking inlets would be placed with a 0.1-foot vertical difference in grate elevation where possible.

Slotted drains are designed with a capture ratio 67% when on grade and 50% when located in a sump.

Deck drains are not anticipated.

Pavement Inlet Design Procedure

The following steps are used to locate and size the mainline catch basins on curb and gutter or concrete barrier sections:

- a. Assume a length of pavement for the initial inlet based upon the ultimate pavement width, and using the Rational Formula, calculate the 10-year peak and 50-year peak discharge value (Q) in cfs.
- b. Utilizing HEC – 22 design procedures, calculate the spread for the 10-year (50-year if in a sag location) return storm and RDG inlet capture ratios. Check spread and depth at curb against design criteria. Add slotted drain if necessary. Calculate bypass flow.

- c. Continue steps "a" and "b" until all mainline inlets have been located. Include bypass flow from previous inlet when analyzing the next inlet.

In addition to the procedure outlined above, catch basin inlets should be located at critical points as recommended by the ADOT RDG (ADOT, 2014a), Chapter 600.

The inlet analysis was not done as part of this study, and such an analysis is deferred to a later design stage. Until then, the inlet analysis done for the SR 24 Gateway Freeway Final Design Concept Report, April 2011 (ADOT, 2011) is referenced herein.

3.4 Storm Drain Design & Analysis

Based upon inlet locations, design the storm drain trunk line and catch basin laterals as follows:

1. Size the storm drain trunk line.
2. Define the maximum hydraulic grade line (HGL) at the end of the pipe run.
3. Calculate the HGL for the pipe network using ADOT accepted design procedures.
4. Review the HGL to determine if pipe size reductions are possible and confirm that the HGL is not higher than allowable at catch basins.
5. Iterate steps 3 and 4 as necessary to optimize the pipe network.

The on-site storm drain network was not analyzed as part of this study, and such an analysis is deferred to a later design stage. Until then, the on-site storm drain analysis done for the SR 24 Gateway Freeway Final Design Concept Report, April 2011 (ADOT, 2011) is referenced herein.

3.5 Outlet Design

Outlets from the elevated roadway into the existing channel are designed for the 10-year frequency storm in the outlet pipe and minimal flow (crown elevation tailwater) in the channel, but no less than 6" above the channel invert. The catch basin grates should be checked with existing 100-year frequency storm hydraulic grade line in the off-site channel. The outlet design was not analyzed for this study,

3.6 Proposed On-Site Drainage Features

Due to the mix of developed (developing) urban, suburban and undeveloped landscape within the project area, the recommended alternative for pavement drainage is sheet flow over the edge of pavement to adjacent roadway ditches. Concrete half barrier or curb and gutter is recommended adjacent to the outside shoulder of the roadway for superelevated or grade-elevated roadway segments (approaches to grade-separated crossings).

The pavement will have a 2% cross grade draining to the outside for a majority of the project, except for the superelevated sections.

The proposed drainage system would include installation of shallow linear detention basins for water quality treatment, roadside ditches, catch basins and storm drain pipes. Such features are

only loosely indicated on the plans and calculations were not done at this design stage; this work is deferred to a later design phase.

ADOT C-15.91 catch basins would be installed along curb and gutter sections to collect the pavement runoff. Similarly, ADOT C-15.92 catch basins would be installed in locations with concrete half barrier. Additional catch basins (flanking inlets) would be added at sag curves and superelevation transitions to reduce bypass flows. Flanking inlets could be supplemented by slotted drains.

Runoff collected in the catch basins will be conveyed to cut ditches or storm drains. New storm drain would be installed to convey flows to a discharge point, or a connection between the new catch basins and existing storm drain laterals is made, where possible.

The on- and off- ramps would not include catch basins unless curb and gutter is required.

The areas between on- and off- ramps at Ellsworth Road, Williams Field Road, Signal Butte Road, Meridian Road and Ironwood Drive would be used for water quality retention basins. These areas would be regraded to a more traditional infield configuration when the ultimate project is constructed.

Several existing pipes would be shortened to discharge into the SR 24 channel (between Powerline Floodway and Ellsworth Road). The remaining pipes not being used would be abandoned in place, capped and filled with sand/cement slurry.

In addition to the general approach described above, Table 1 summarizes the future on-site drainage features by segment.

Table 1 – Future On-Site Drainage Features and Runoff Flow Patterns

Begin Approach	End Approach	Northern Runoff	Southern Runoff
East of Powerline Floodway	West of Ellsworth Road	- Several on-site retention bleed-off and pavement runoff pipes that discharge to the northeast into the Ellsworth Basin would be shortened to discharge into the SR 24 channel.	-- The temporary infield basin between the on- and off- ramps west of Ellsworth Road would be re-graded to accommodate the mainline embankment, should a grade-separated intersection at Ellsworth Road be needed; - the regrading would result into two distinct infield basins that would be connected by an equalization/ bleedoff pipe.

Begin Approach	End Approach	Northern Runoff	Southern Runoff
East of Ellsworth Road	West of Williams Field Road	- Runoff on the mainline will sheetflow or be collected by catch basin and conveyed to a side ditch located between the WB lanes and the SR 24 channel; - The side ditch would convey the flow to the northwest and cross the WB lanes east of Ellsworth Road to a water quality basin located at the northeast infield of the intersection. This basin would provide water quality treatment for the entire segment. - The water quality retention basin would bleed-off to the SR 24 channel.	- Runoff on mainline will sheetflow or be collected by catch basins and be conveyed to a side ditch; - the side ditch would convey the flow to the west and cross the EB lane east of Ellsworth Road to a water quality retention basin in the northeast infield of the intersection.
East of Williams Field Road	West of Crismon Road	- Runoff on the mainline will sheetflow or be collected by catch basins and conveyed to a linear water quality basins located between the WB lanes and the SR 24 channel; - The shallow linear water quality retention basin would bleed-off to the SR 24 channel.	- Runoff on mainline will sheetflow or be collected by catch basins and conveyed to a side ditch; - the side ditch would convey the flow to the northwest and cross the EB lanes east of Williams Field Road to a water quality retention basin in the infield; - The water quality retention basin would bleed-off to the SR 24 channel.
East of Crismon Road	West of Signal Butte Road	- Runoff on mainline will sheetflow or be collected by catch basins and be conveyed to linear water quality basins located between the WB lanes and the SR 24 channel; - The water quality retention basins would be separated by check dams and bleed-off to the SR 24 channel.	- Runoff on mainline will sheetflow or be collected by catch basins and conveyed to a side ditch; - the side ditch would convey the flow to the west and cross the EB and WB lanes east of Crismon Road to a water quality retention basin; - The water quality retention basin would bleed-off to the SR 24 channel.

Begin Approach	End Approach	Northern Runoff	Southern Runoff
East of Signal Butte Road	West of Meridian Road	- Runoff on the mainline will sheetflow or be collected by catch basins and conveyed to linear water quality basins located between the WB lanes and the SR 24 channel; - The water quality retention basins would be separated by check dams and bleed-off to the SR 24 channel.	- Runoff on mainline will sheetflow or be collected by catch basins and conveyed to a side ditch; - the side ditch would convey the flow to the west and cross both EB and WB lanes east of Mountain Road to a water quality retention basin; - west of Mountain Road the side ditch would continue to the west and cross the EB lanes east of Signal Butte Road to a water quality retention basin in the infield; - The water quality retention basins would bleed-off to the SR 24 channel.
East of Meridian Road	West of Ironwood Drive	- Runoff on mainline will sheetflow or be collected by catch basins and conveyed to linear water quality basins located between the WB lanes and the SR 24 channel; - The water quality retention basins would be separated by check dams and bleed-off to the SR 24 channel.	- Runoff on mainline will sheetflow or be collected by catch basins and conveyed to a side ditch; - the side ditch would convey the flow to the west and cross the EB lanes west of Ironwood Drive and east of Meridian Road to water quality retention basins; - The water quality retention basins would bleed-off to the SR 24 channel.

Proposed on-site drainage features are shown in Figure 4 and on the plan sheets included in Appendix A. Supporting documentation for the design of various drainage components are included in Appendices D and F.

The bridge anticipated with the project is the Mountain Road Overpass. Drainage calculations have not been done at this design stage, but both structures are relatively short and have sufficient longitudinal grade to ensure positive drainage and contain the runoff spread within design. Deck drains are not anticipated, but spillway embankments will be designed as needed in later design phases.

3.8 Final Design Issues

Several issues will need to be considered with the final design of the drainage features.

Runoff spread, interception and conveyance of pavement runoff generated throughout the interim project was not evaluated.

- Consideration of the effect of the time of concentration on the rainfall intensity for peak flow calculations. Most of pavement drainage areas are likely to generate a time of concentration of 10 minutes, but that was not calculated for this study.
- For curb and gutter sections, slotted drain could be considered to supplement the interception capacity at most catch basin inlets. Based on current construction costs, it makes economic sense to use a slotted drain up to 60-65 ft in length instead of a new catch basin inlet with the same length of discharge pipe. However, this concept will need to be revised based on capital and maintenance costs at the time the final design is performed.
- Roadside ditches were not analyzed with this study. They will require analysis for transport of drainage flows to water quality basins at all locations within the right-of-way.
- Available retention capacity for water quality treatment shall be analyzed and sized to contain the first flush volume (equivalent to that generated by the first 0.5 inches of rainfall on impervious surfaces) at the minimum as indicated in FCDMC *Drainage Policies and Standards for Maricopa County, Arizona*, (FCDMC, 2007).

4.0 OFF-SITE DRAINAGE DESIGN

This section is intended as an update to the analysis performed by ADOT for the project area as part of the *SR 24 Gateway Freeway FDCR* (ADOT, 2011), and extensive references will be made to the ADOT, 2011 report and its accompanying Initial Drainage Report. The update relies heavily on the extensive regional evaluation done by FCDMC for the East Mesa ADMPU (FCDMC 2013a, FCDMC 2013b) using hydrologic models modified for the purpose of the SR 24 interim project.

4.1 Existing Conditions

Several existing or proposed regional drainage facilities in the project area will have an influence upon or be affected by the project. They are:

- Powerline Flood Retarding Structure (FRS) and Vineyard FRS in Pinal County, designed to provide flood protection to Central Arizona Project (CAP) Canal and to downstream areas in Pinal County and Maricopa County;
- Powerline Floodway, a concrete-lined channel that extends from the Powerline FRS to the East Maricopa Floodway; it is primarily designed to drain the FRS structures;
- Ellsworth Channel, which runs along the east and west sides of Ellsworth Road between Pecos Road and the Powerline Floodway;
- Former General Motors Proving Grounds perimeter channel, which will be improved by developers;
- East Maricopa Floodway, which serves as a regional outfall for eastern Maricopa County;
- Pecos Road Channel is one of the proposed drainage improvements in the East Mesa ADMPU, it is intended to run along Pecos Road and to discharge into Ellsworth Channel.

The SR 202L Santan drainage channel is not affected by this project.

The ADOT, 2011 accompanying Initial Drainage Report provides a list of design flows in the major existing facilities in the area. These flows are presented in Table 2:

Table 2 – Existing Drainage Facility Design Flows (from ADOT, 2011 Initial Drainage Report)

Drainage Facility	Design Flow (cfs)
SR 202L Santan Channel	2,200
Powerline Floodway at confluence with Ellsworth Channel	3,935
Ellsworth Channel	3,500
East Maricopa Floodway at confluence with Powerline Floodway	8,460

An extensive description of these drainage facilities is provided in the ADOT, 2011 and its accompanying Initial Drainage Report. See Figure 4 for an illustration of existing drainage facilities in the project area.

Figure 4 – Existing Regional Drainage Facilities (Excerpt from ADOT, 2011 Initial Drainage Report, Figure 2)



4.2 Existing (Pre-project) Hydrology

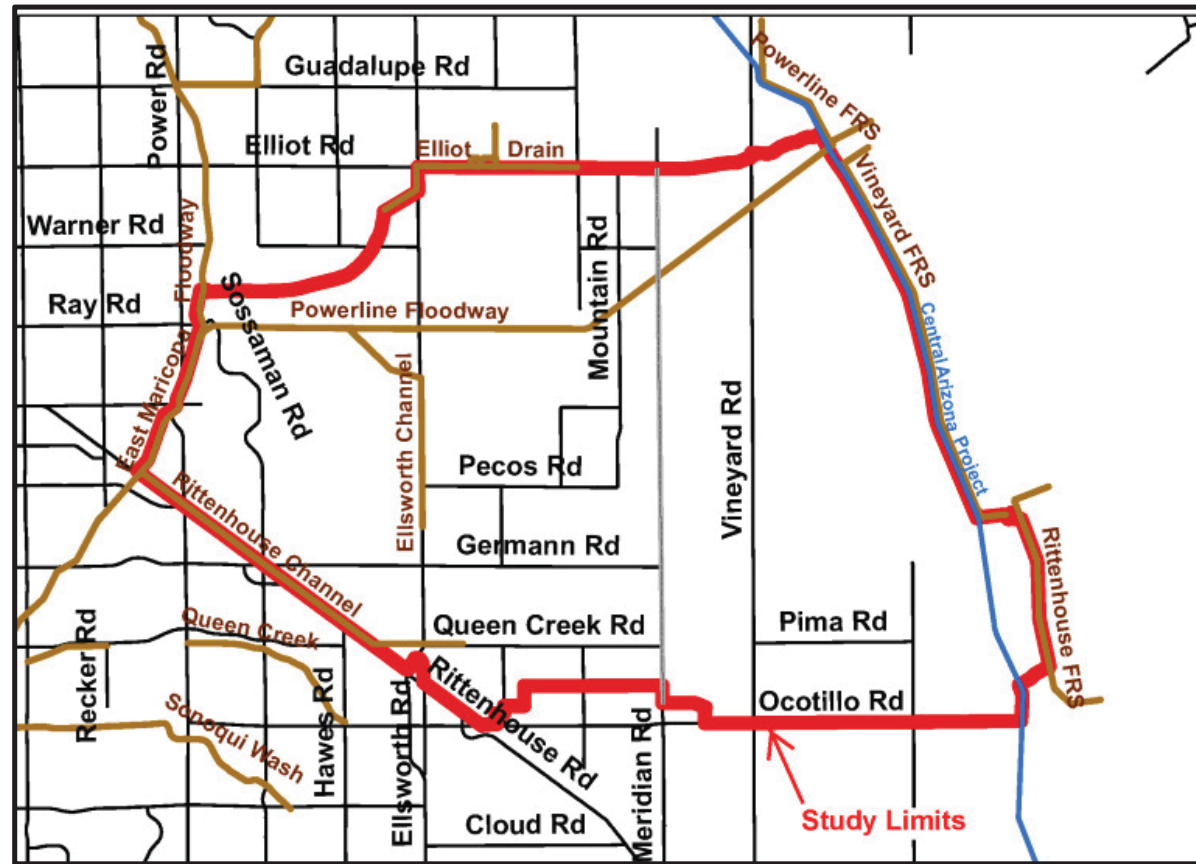
Pertinent pre- and post-project hydrology was developed by ADOT for the *SR 24 Gateway Freeway FDCR* (ADOT, 2011) Initial Drainage Report. The most current hydrologic analysis in the project watershed was performed by FCDMC in the *East Mesa ADMPU* (FCDMC, 2013a and FCDMC, 2013b). The latter study updated the existing condition regional hydrology to reflect major infrastructure improvements in the area (Ironwood Drive Improvement, FCDMC 2013b).

Both ADOT and FCDMC hydrology indicated that the existing condition flows within the SR 24 project area are higher in most cases than the ultimate development flows. This is justified by the existing undeveloped or suburban areas and the lack of regional retention facilities. With development extending in the region, drainage regulations require implementation of the 100-year, 2-hour retention capacity for new areas to be developed, which leads to an attenuation of peak flows and reduction of runoff volume.

The East Mesa ADMPU covered an extensive area (see Figure 5) and developed hydrology and HEC-1 models for existing (2013) and ultimate development conditions in the watershed for several storm frequencies and durations. The hydrology was based on National Oceanic and

Atmospheric Agency (NOAA) Atlas 14 and implemented specific requirements by both Maricopa County and Pinal County.

Figure 5 – Mesa ADMPU Study Limits (From FCDMC, 2013a, Figure 1-1)



See ADOT 2011, FCDMC 2013a and FCDMC 2013b for extensive details regarding the hydrologic procedures applied by the ADOT and FCDMC studies.

4.3 Proposed Options

According to ADOT, the interim SR 24 project could be constructed in the next 3- to 10 years. The proposed off-site drainage system would be based on the default conceptual drainage design provided with the *SR 24 Gateway Freeway DCR* (ADOT, 2011), but sized for a revised hydrology that accounts for development likely to occur in the watershed within this time frame. This concept shows an off-site channel on the north side of SR 24 that is sized for the larger existing (pre-project) condition design flows (Figure 6). The SR 24 channel outfalls into the Powerline Floodway, which would be widened to the confluence with Ellsworth Channel. A detention/retention basin at Ellsworth Road (Ellsworth Basin) would regulate the SR 24 channel peak flow before the outfall into Powerline Floodway. This concept represents the baseline approach to off-site drainage design.

The interim SR 24 project would contribute additional flows to the existing off-site runoff due to the new pavement surface. Although on-site runoff will increase, the proposed off-site collection

infrastructure would not be affected as the on-site and off-site peak flows are far apart. The peak flows approaching the SR 24 alignment would only be affected by the development in the upstream watershed.

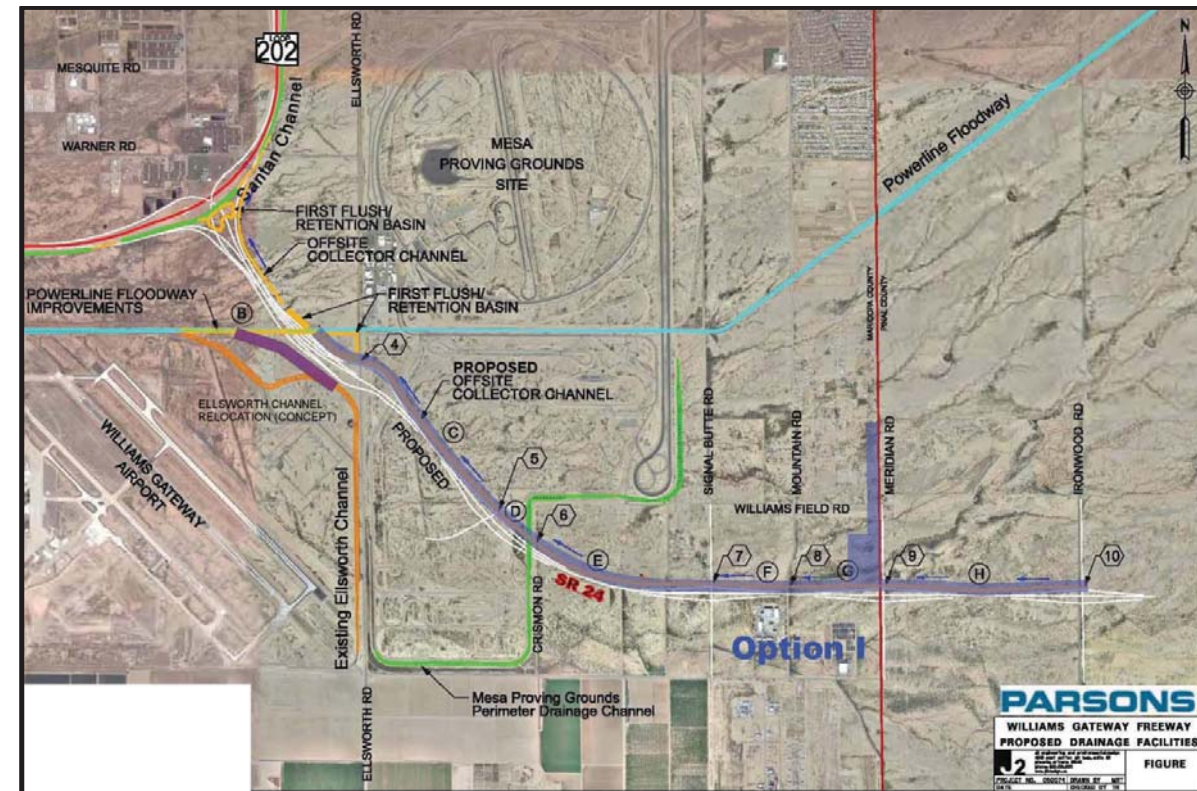
Figure 6 – Baseline SR 24 Off-site Drainage Improvements for the Ultimate Project (From ADOT, 2011, Figure 25, Modified)



With the projected reduction in flows as development occurs in the watershed, the off-site drainage would need to be reassessed for opportunities of peak flow and runoff volume reduction. For that purpose, three possible options for the proposed off-site drainage infrastructure were presented to the stakeholders, and examined. These options were in addition to the baseline design, and were all inspired by alternatives presented and discussed in East Mesa ADMPU (FCDMC, 2013a), and in the City of Mesa SDMP (Entellus, 2010):

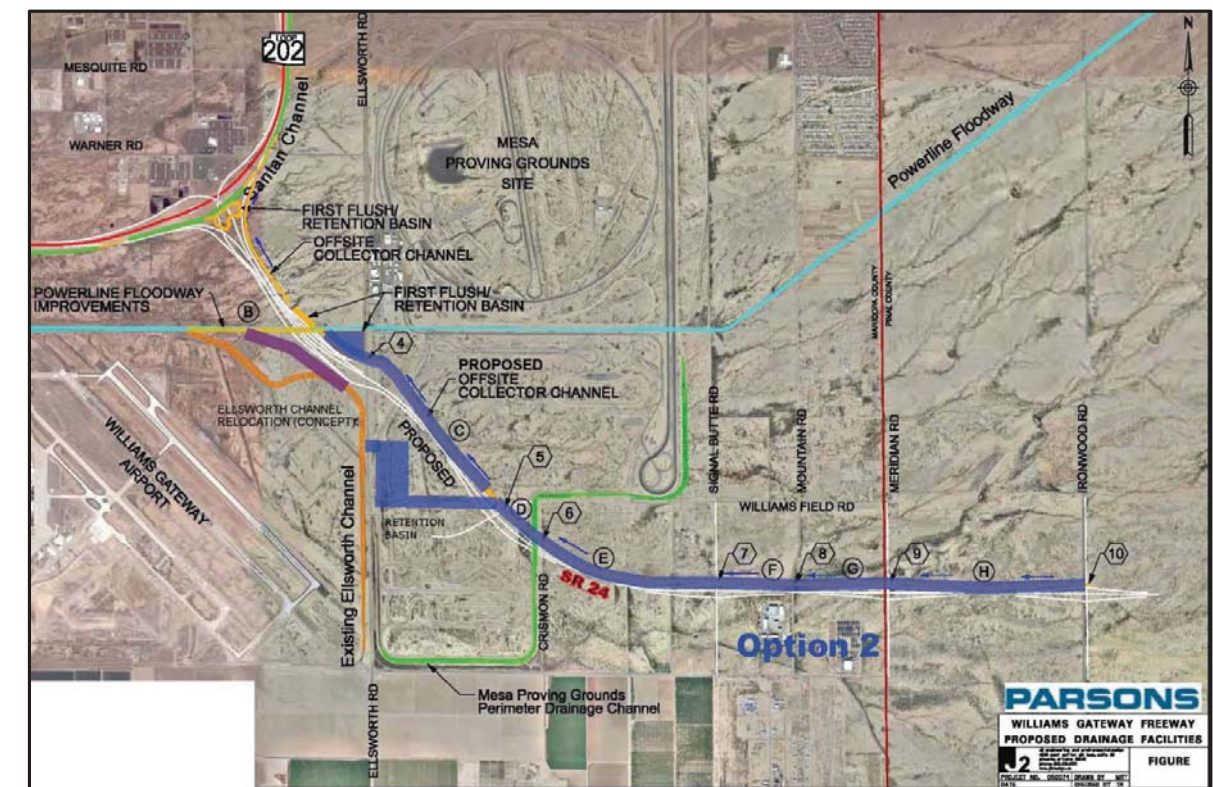
- Option 1 – Baseline design, with a detention basin at Meridian Road and an approximately one mile long channel running north-south along Meridian Road (Figure 7). The detention basin would be sized according to Pinal County development requirements, reduce the peak flow in the SR 24 system and protect an area west of Meridian Road from flooding. The planned relocation of the Ellsworth Channel at the Airport is also indicated in the figure.

Figure 7 – Option 1 - SR 24 Off-site Drainage Improvements for the Interim Project (Based on ADOT, 2011, Figure 25, Modified)



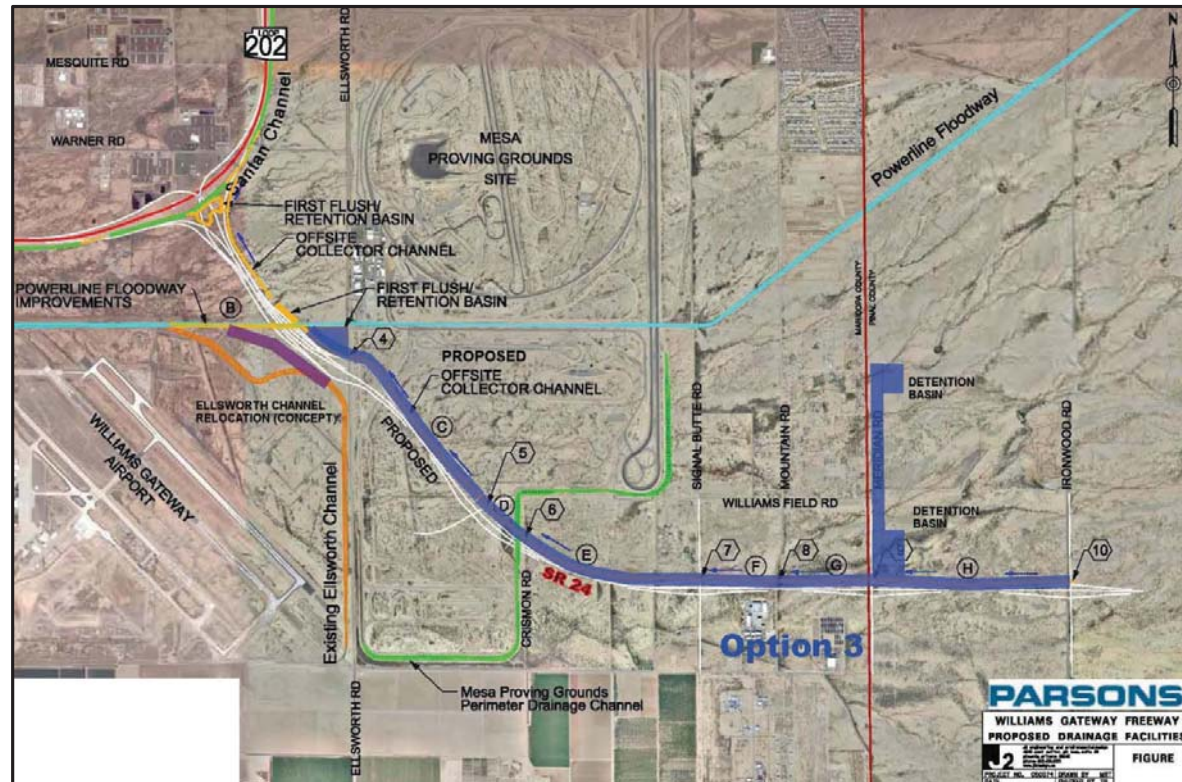
- Option 2 – Off-site channel from Ironwood Drive to Williams Field Road following the baseline design, but continuing west to Ellsworth Road; a detention basin would be located east of Ellsworth with an outfall connection to Ellsworth Channel. A smaller SR 24 channel would begin north of Williams Field Road following the baseline design. Powerline Floodway would be widened downstream of the confluence to the relocated confluence of Ellsworth Channel. (Figure 8).

Figure 8 – Option 2 - SR 24 Off-site Drainage Improvements for the Interim Project (Based on ADOT, 2011, Figure 25, Modified)



- Option 3 – Baseline design, with two detention basins at Meridian Road and an approximately one mile long channel running north-south connecting the basins. (Figure 9). The detention basins would be sized according to Pinal County development requirements, reduce the peak flow in the SR 24 system and protect an area west of Meridian Road from flooding.

Figure 9 – Option 3 - SR 24 Off-site Drainage Improvements for the Interim Project (Based on ADOT, 2011, Figure 25, Modified)



The three options were discussed with ADOT, MAG, State Land Department, Pinal County, City of Mesa and FCDMC. All options were eventually eliminated from consideration in relation to the Interim SR 24 project because they would require facilities located outside of the current environmentally-cleared footprint.

Therefore, the baseline SR 24 off-site drainage configuration, amended with the relocation of Ellsworth Channel at the Airport, was selected to be applied for further hydrologic analysis and conceptual hydraulic design.

4.4 Proposed Conditions for the Interim Project

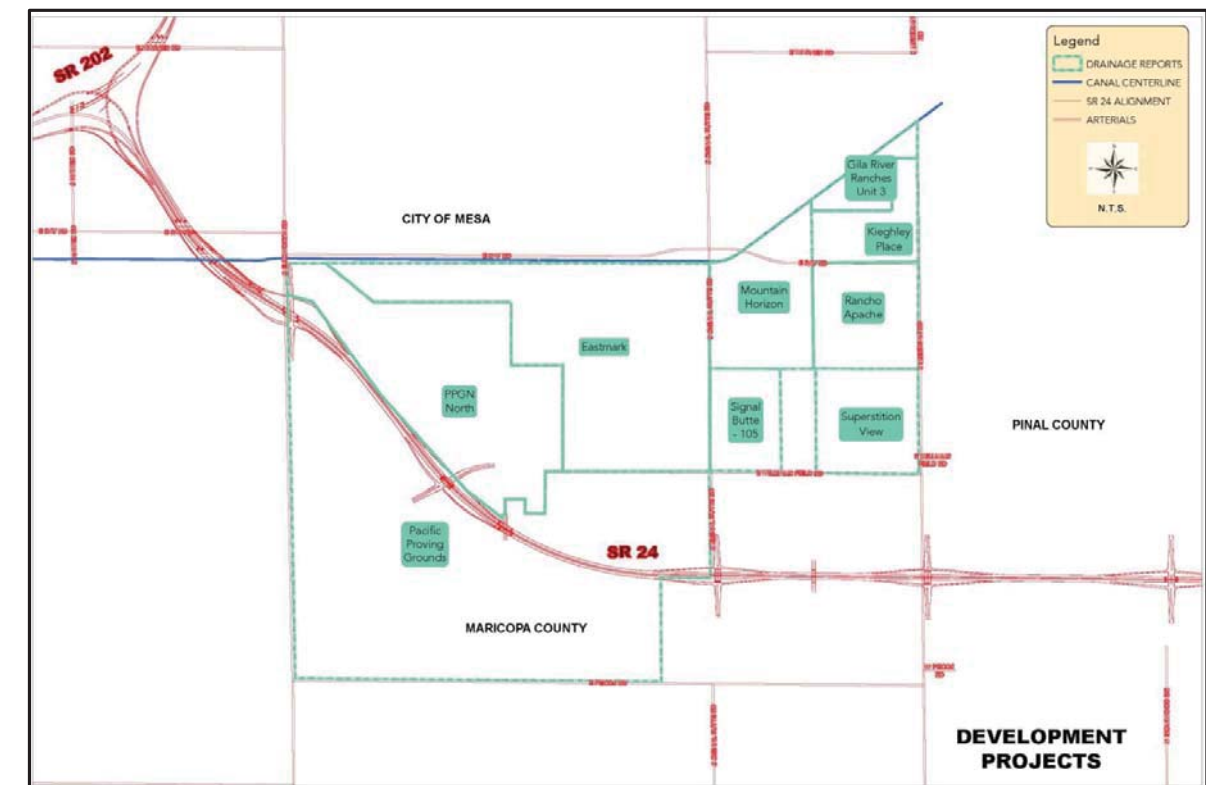
The East Mesa ADMPU existing condition and ultimate development condition hydrologic models for 50-year, 24-hour and 100-year, 24-hour were of particular interest for the Interim SR 24 analysis. The ultimate condition models were well updated by the ADMPU to reflect proposed residential and commercial development in the watershed, and included the SR 24

off-site channel. Hence, the ultimate development condition models were taken and revised for the hydrologic analysis of the Interim SR 24 Project.

The revisions consisted of:

- Reverting the watershed area within Pinal County to undeveloped hydrologic conditions. This was achieved by replacing the sub-basin modules from the ultimate development models with corresponding ones from the existing condition models, and by removing the retention volumes at the sub-basins. These changes are documented in the HEC-1 models included in Appendix D;
- Evaluating the rate of development within Maricopa County and City of Mesa portion of the watershed, based on site development documentation provided by City of Mesa. Figure 10 presents a schematic of the developments that were reviewed and their location in relation to the project. The evaluation considered the rate of development and construction, and looked at whether the required retention volume was or is in the process of being constructed. From the hydrologic stand point, developments that are fully mass graded but only partially constructed were considered at ultimate development. These changes are documented in the HEC-1 models included in Appendix D;

Figure 10 – Development Projects within Maricopa County and City of Mesa



- Changing some of the routing parameters to reflect channel conditions presented in the development plans, as well as modifications of the SR 24 off-site channel. These changes are documented in the HEC-1 models included in Appendix D, which includes a schematic of the components of the hydrologic model that were revised.

Three materials were considered for the off-site channel lining: grass, gravel and concrete. Two lining materials (gravel and concrete) were used in the hydrologic models for comparison. Minor revisions of routing parameters were required to accommodate the two materials.

4.5 Design Criteria

The procedures described in the *ADOT Roadway Design Guidelines* (RDG) (ADOT, 2014a), *ADOT Highway Drainage Design Manual, Volume 2, Hydrology* (HDDM2) (ADOT, 2014b) and *ADOT Highway Drainage Design Manual, Volume 3, Hydraulics* (HDDM3) (ADOT, 2014c), are applicable.

The channel design was based on 50-year, 24-hour peak flows with freeboard. It is desirable to adjust the channel longitudinal slope to maintain a subcritical flow regime with a maximum Froude number below 0.86; as such, the channel freeboard would be 1 foot. Flow regimes with Froude numbers between 0.86 and 1.1 create flow instability and should be avoided.

The channel should convey the 100-year, 24-hour flow with no freeboard and the flow should be contained within the ADOT right-of-way.

A trapezoidal channel section is typical, with the bottom sloping 2% to one side when concrete lining is used. The minimum width of the channel bottom must accommodate maintenance access. The side slopes are no steeper than 2 to 1 horizontal to vertical for concrete lining, and no steeper than 3 to 1 horizontal to vertical for gravel lining.

Important feedback was received from the ADOT Maintenance and Construction Districts. Concrete-lined channels are preferred because of ease of maintenance, and the conceptual design and the cost estimates were developed for such a facility. In addition, multiple access ramps are desired at the channel with spacing no larger than one half-mile, and a 15-foot wide Operation and Maintenance Road provided on the north side of the channel.

4.6 Proposed Conceptual Design – SR 24 Channel

The channel design was optimized to maintain hydraulic conditions within the design parameters described above. In addition, several factors specific to the project were considered:

- The Ellsworth Basin was constructed with Interim Phase I of SR 24 as a future off-line detention basin designed to control the outfall rate of flows exiting the SR 24 drainage channel into Powerline Floodway. The basin would divert channel flows through a lateral weir and therefore trim the peak of the flow hydrograph. The *SR 24 Gateway Freeway DCR* (ADOT, 2011) assumed a controlled flow of 1,650 cfs at the channel outfall. As constructed, the basin has a limited operational volume, which is estimated to approximately 100 acre-feet;
- The Ellsworth Basin may not require a lateral weir during SR 24 Interim Phase II. Under this phase, the SR 24 Channel collects only a limited amount of runoff originating from south of Powerline Floodway to east of Ironwood Drive, and the 100-year, 24-hour peak flow at Ellsworth Road is 1754 cfs (Appendix D). Unsteady flow hydraulic modeling of this scenario (Appendix F) shows that the Ellsworth Basin could successfully attenuate the flow below

1650 cfs by using 3-36" pipe culverts that operate unrestricted. The culverts could operate in conjunction with a future lateral weir that would be required to attenuate the larger peak flow when SR 24 and its channel extend east of Ironwood Drive;

- According to development plans for PPGN (Wood Patel, 2014), flow in excess of the 100-year, 24-hour storm event would cross Ellsworth Road and discharge into the Ellsworth Basin. This would limit the volume available for channel peak flow attenuation;
- An efficient concrete lined channel would convey flow at high velocities accelerating the hydrograph. The Ellsworth Basin would fill too quickly and become less effective for peak flow attenuation. This condition reinforced the argument of designing the channel for a subcritical flow regime, operating at a lower design velocity;
- Reducing the design velocity in the channel would require a mild longitudinal grade (in the range of 0.15% to 0.17%) which would increase the channel cross section, as well as the cost of excavation and concrete lining;
- The natural terrain along the channel is several times steeper (up to 0.0049 ft/ft) than the mild longitudinal channel slope, which would require a deep channel unless channel steps are provided. The stepped channel approach was used, and 2- or 3-foot vertical transitions were placed where necessary using 10 to 1 horizontal to vertical slopes at each transition;
- The Ellsworth Road RCBC was constructed with the Interim Phase I project and it restricts the channel slope to the Powerline Floodway outfall to approximately 0.069%. This slope is difficult to construct, but it provides an opportunity for a sediment basin downstream of the RCBC;
- Provisions were made for in-line sediment basins upstream of the Meridian Road and Signal Butte Road culvert crossings, and upstream of the Powerline Floodway confluence. They are approximately 60 to 100 feet long, and are created through a 2-foot depression at the bottom of the channel; the upstream end of the transition is sloping 10 to 1 to allow access and maintenance, while the downstream end is vertical.
- The widening of Powerline Floodway was coordinated with the improvements and widening due to the relocation of Ellsworth Channel at the Airport. The channel cross-section is similar to that presented in the *SR 24 Gateway Freeway DCR* (ADOT, 2011) (See drainage plans in Appendix A), but it is shallower with 2 to 1 side slopes instead of 1.5 to 1. This cross section was designed based on FCDMC design peak flow frequency and magnitude requirements and it is identical to the section downstream of the new Ellsworth Channel confluence at the Airport.

Typical sections and a summary of SR 24 channel dimensions are presented in Appendix A. Table 3 provides a summary of channel dimensions and design flow versus capacity. The design is documented in the drainage plans in Appendix A, and in the calculations included in Appendix E.

Table 3 – Proposed SR 24 Concrete-lined Channel Dimensions and Flows

Channel Reach	Channel ID	Design/Check Flows Q ₅₀ /Q ₁₀₀ ¹ (cfs)	Bottom Width (ft)	Depth ² (ft)	Top of Channel Flow Capacity (cfs)
Powerline Floodway Widening	B	4400/4400 ³	55	8.0 ⁴	-
Ellsworth Road to Powerline Floodway	C	2002/2479	20	9.0	2670
Williams Field Road to Ellsworth Road	C	1977/2452	20	7.5	2725
Crismon Road to Williams Field Road	D	1329/1630	12 to 20	7.5	2097
Signal Butte Road to Crismon Road	E	1335/1637	12	7.5	2097
Mountain Road to Signal Butte Road	F	1173/1440	12	7.0	1815
Meridian Road to Mountain Road	G	1176/1445	12	7.0	1815
Ironwood Drive to Meridian Road	H	1166/1432	12	7.0	1815

The cross culverts were not revised from the dimensions provided in the *SR 24 Gateway Freeway DCR* (ADOT, 2011).

4.7 Final Design Considerations

Integrating the operation of the SR 24 channel with the Ellsworth Basin and the widened section of Powerline Floodway will require modifications to the Basin and the on-site drainage infrastructure constructed west of Ellsworth Road. Also, the operation of the Ellsworth Basin will change from a water quality treatment basin to a detention basin with a water quality treatment component. The following aspects must be considered during final design:

- A new 36" bleed-off line to drain Ellsworth Basin to the widened Powerline Floodway. The new bleed-off line would run along the south bank of the widened Powerline Floodway and take the role of draining the Basin within 36 hours from the existing 18-inch line that drains to the retention basin located north of the existing Powerline Floodway. The existing bleed-off line cannot be maintained because it is in conflict with the proposed SR 24 - Powerline Floodway confluence. The confluence requires a deeper cross section than that of the current concrete-lined channel. In addition, the capacity of the existing bleed-off line is not

¹ Powerline Floodway is a facility operated by FCDMC. The design flow frequency for flood control facilities is the 100-year event.

² Average depth along the reach.

³ The design flow magnitude requested by FCDMC for the Powerline Floodway Widening is 4,400 cfs.

⁴ Channel is supercritical; depth of channel was selected to contain most of the velocity head.

sufficient to drain the larger storm water volumes that Ellsworth Basin would handle under its detention role.

- Storm drain collector lines that outfall to the Ellsworth Basin from the south and southwest must be modified in order to provide water quality treatment. These storm drains are in conflict with, and cannot outfall directly to the SR 24 Channel without prior water quality treatment. Either the pipes are lowered and use inverted siphons to continue discharge into the Ellsworth Basin, or the storm drain system is reconfigured to use hydrodynamic separator devices that would be placed before the storm drains outfall to the SR 24 Channel. The storm drains that outfall to Ellsworth Channel from the east do not require modifications;
- Depending on the final thalweg elevation and profile of the widened Powerline Floodway, a control structure and energy dissipater will be required downstream of SR 24 Channel at the confluence with Powerline Floodway.

5.0 REFERENCES

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APPENDIX A

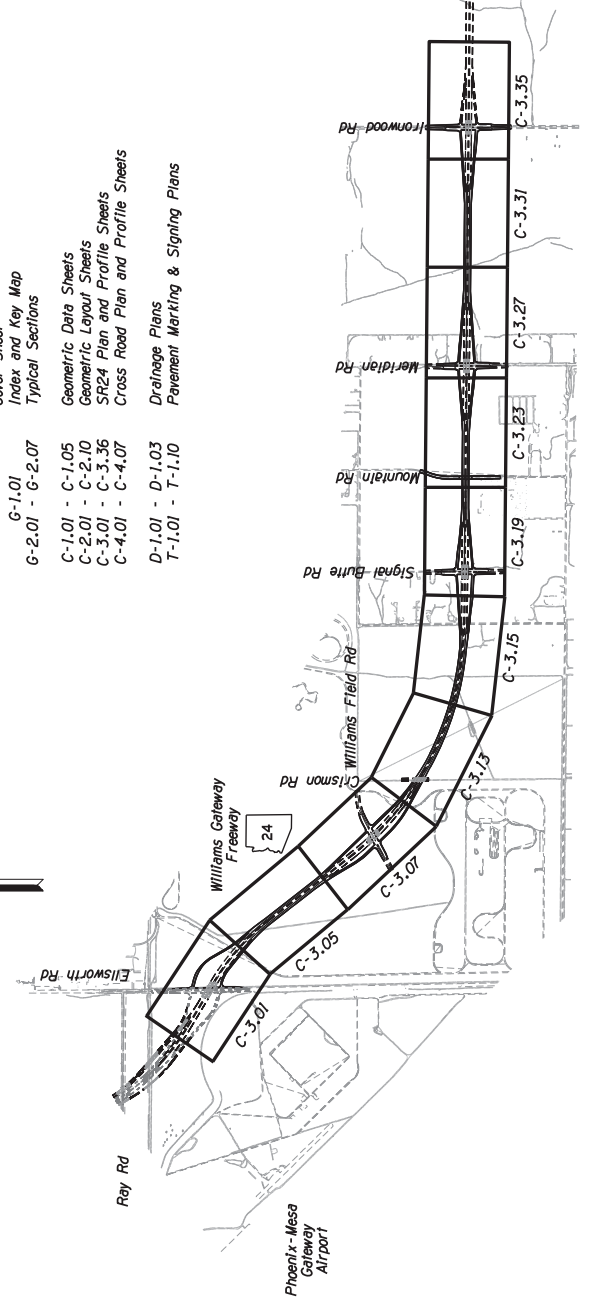
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- Sheet No. Sheet Type
- Cover Sheet
Index and Key Map
Typical Sections
- G-1.01 - G-2.07
- C-1.01 - C-1.05
C-2.01 - C-2.10
C-3.01 - C-3.36
C-4.01 - C-4.07
- D-1.01 - D-1.03
T-1.01 - T-1.10
- Geometric Data Sheets
Geometric Layout Sheets
SR24 Plan and Profile Sheets
Cross Road Plan and Profile Sheets
- Drainage Plans
Pavement Marking & Signing Plans

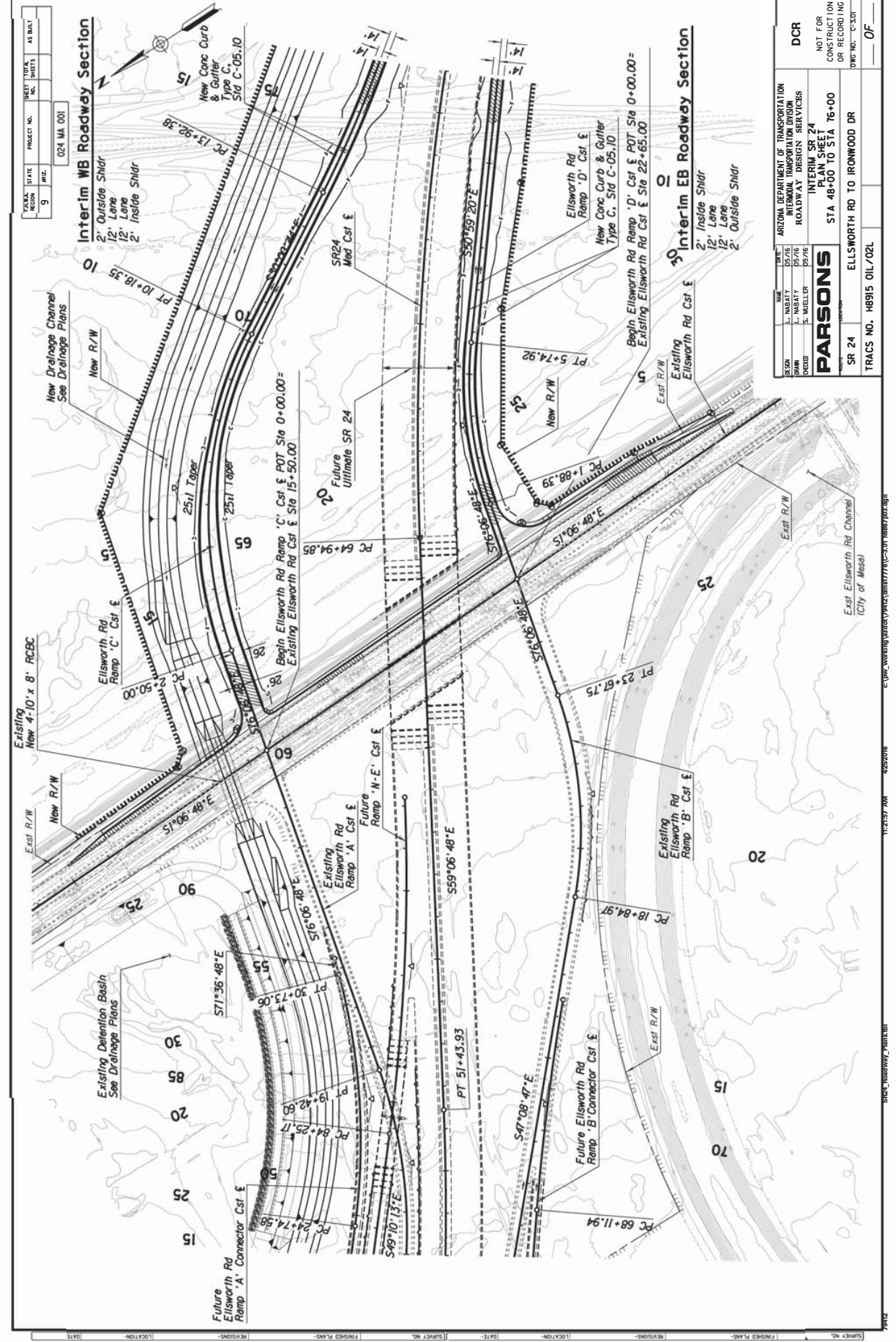


Access Control Legend (See Roadway Plans for Location)

- Right-in-Right-out Access Control only
- Full Access Control

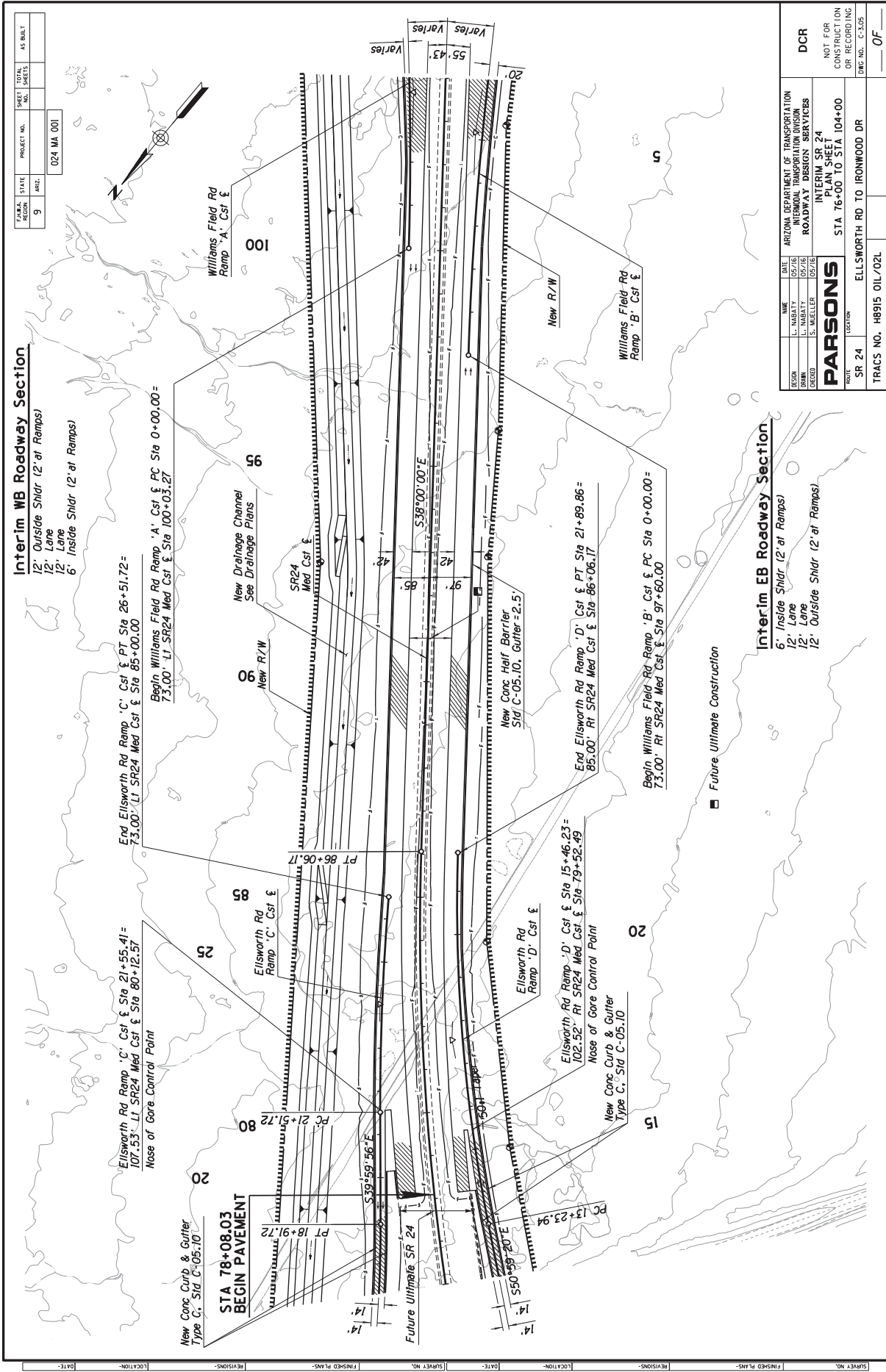
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SR 24	ELLSWORTH RD TO IRONWOOD DR	SR 24 SHEET INDEX AND KEY MAP					
TRACS NO.	H8915 OIL/02L	DCR NOT FOR CONSTRUCTION OR RECORDING DWG NO.: C-3.01					
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 12' Lane
 12' Lane
 6' Inside Shldr (2' at Ramps)

Interim EB Roadway Section
 6' Inside Shldr (2' at Ramps)
 12' Lane
 12' Lane
 12' Outside Shldr (2' at Ramps)

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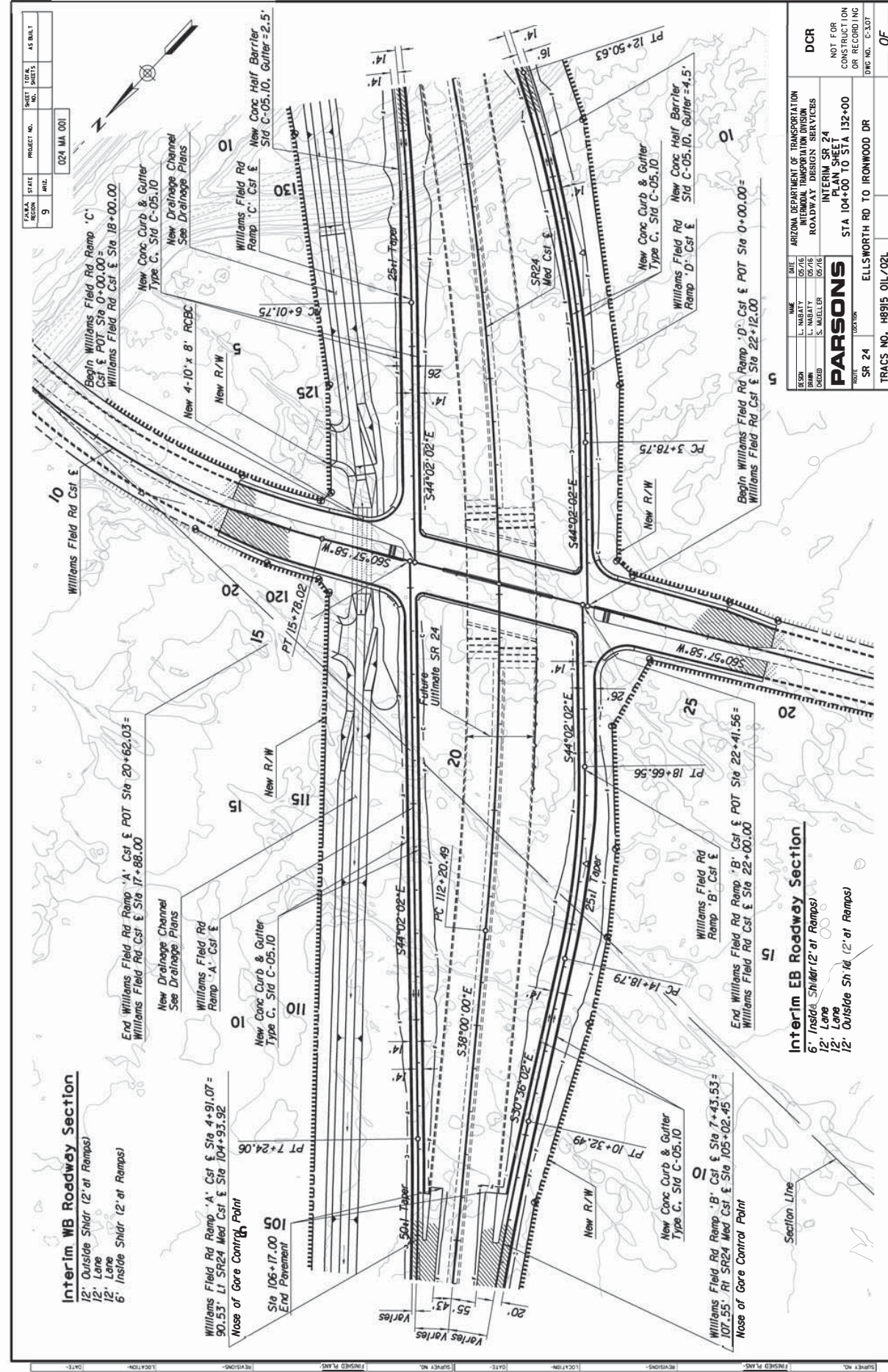
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 12' Lane
 12' Outside Shldr (2' at Ramps)

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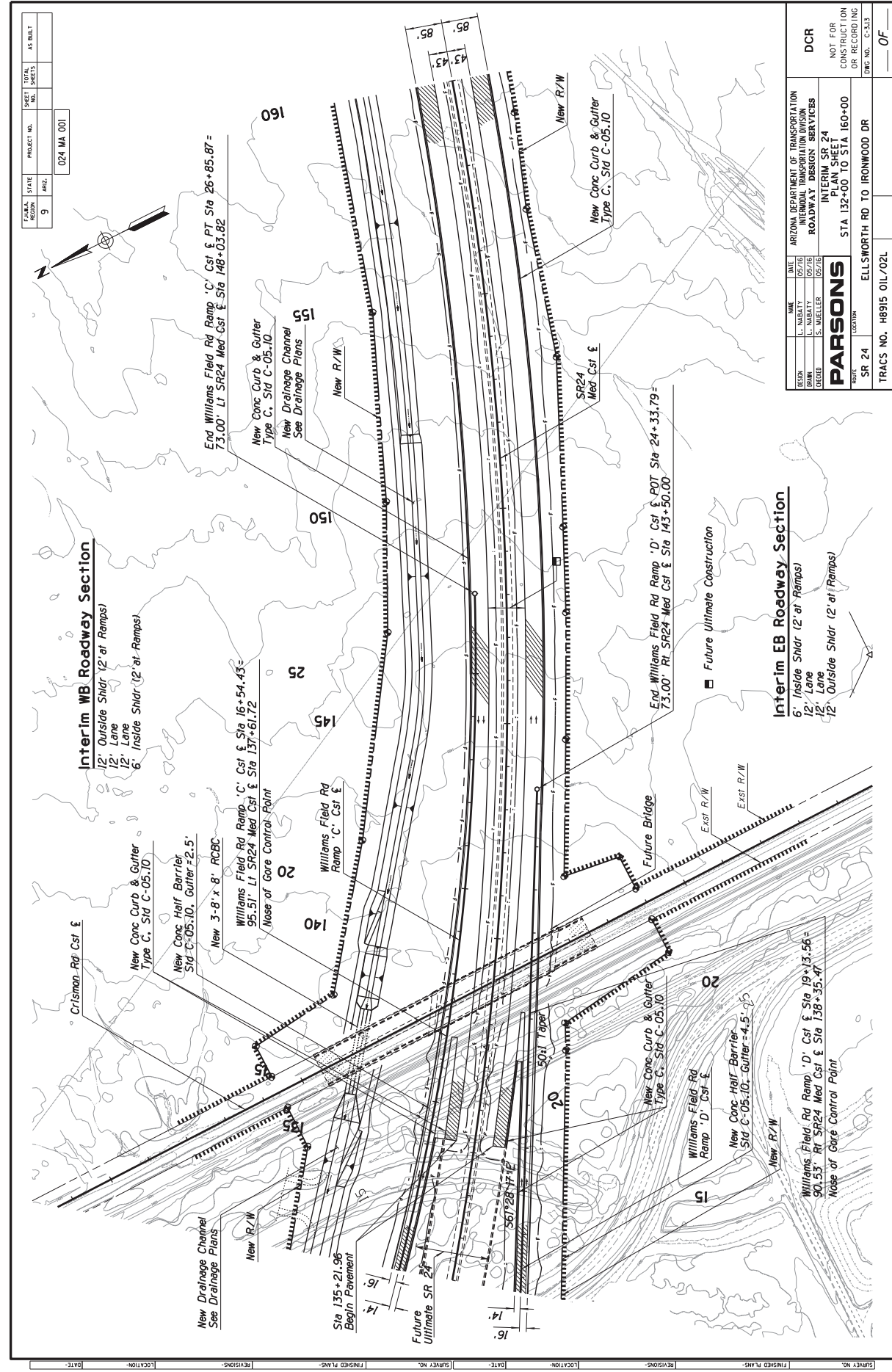
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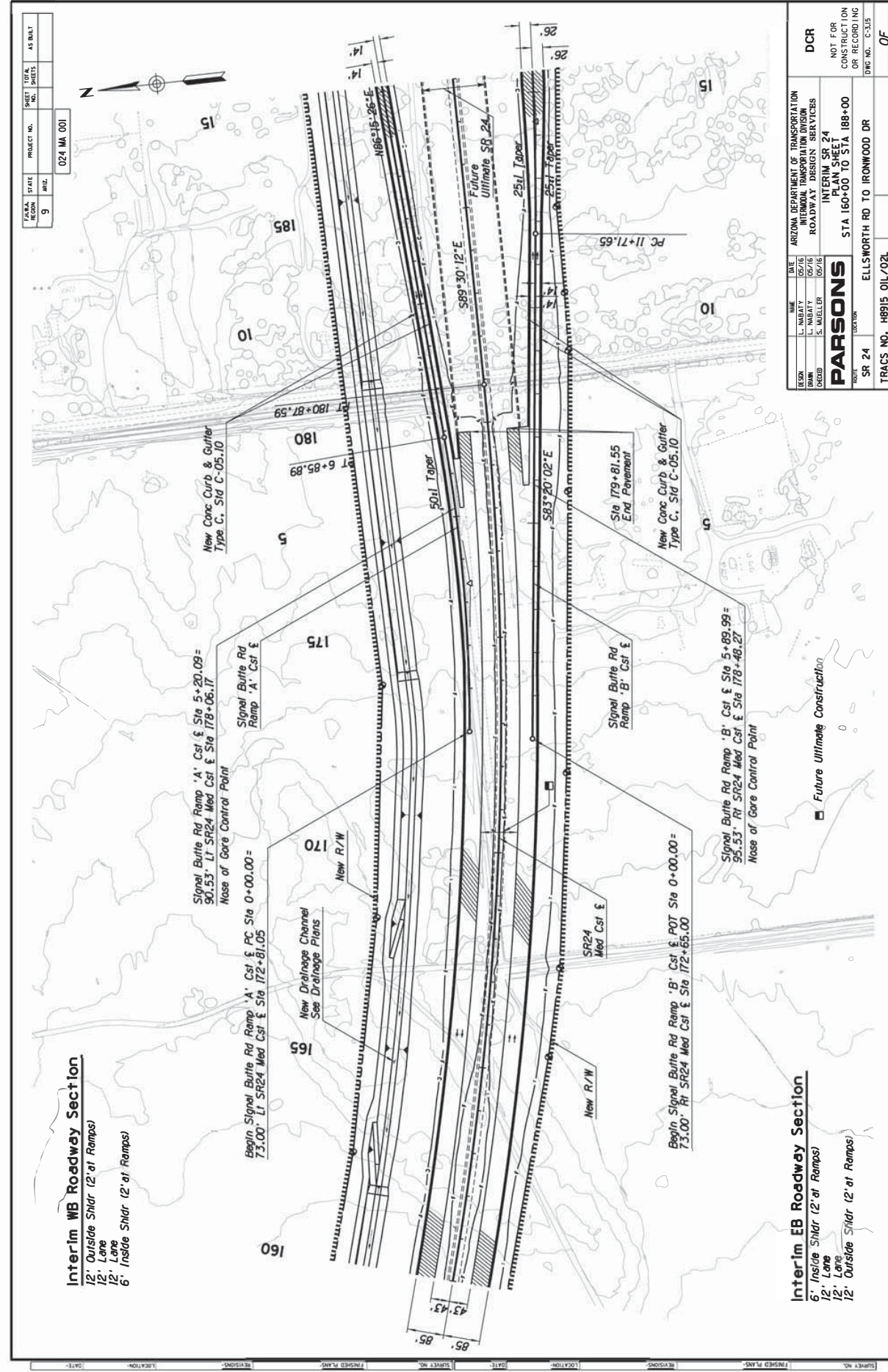
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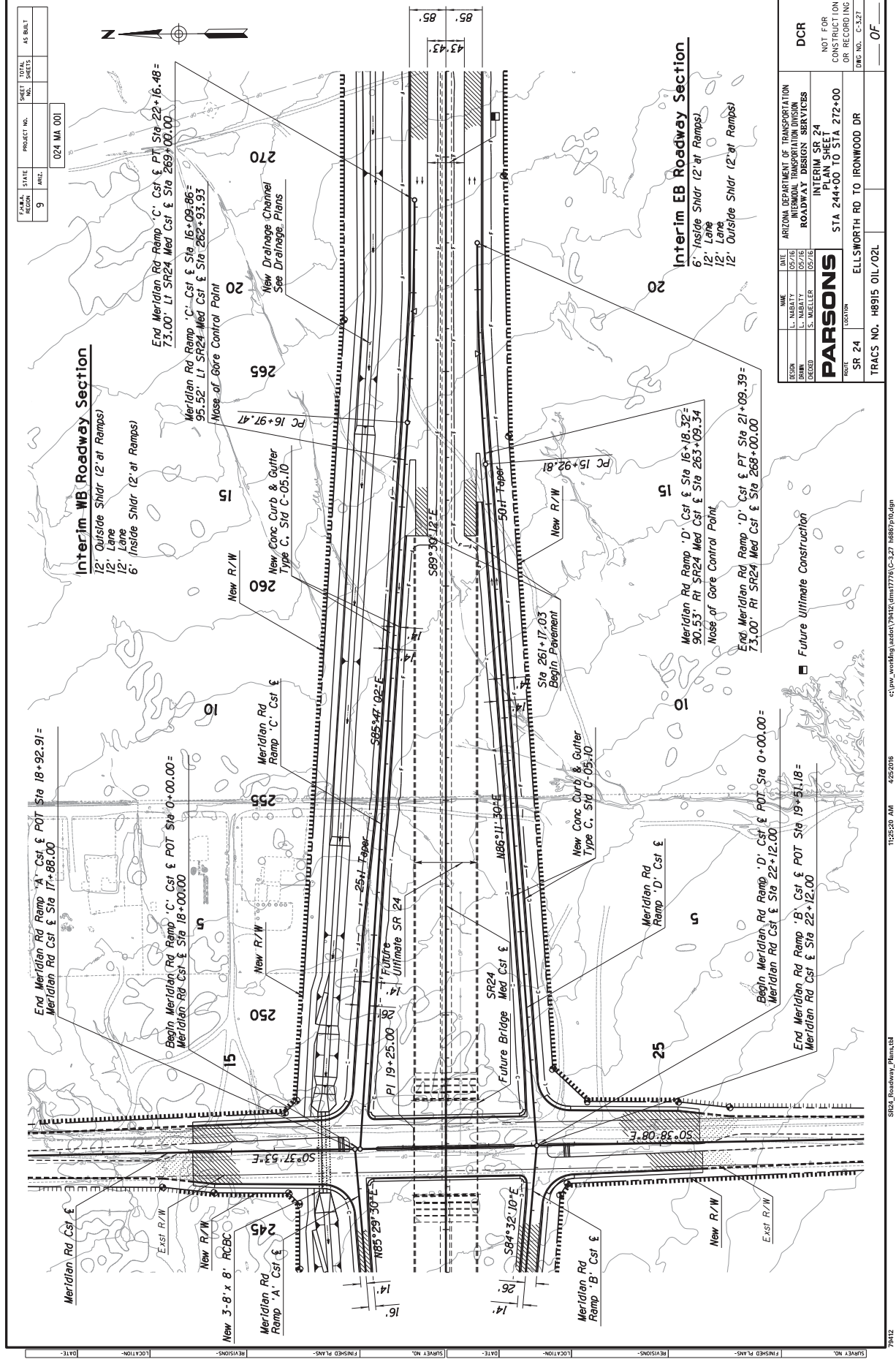
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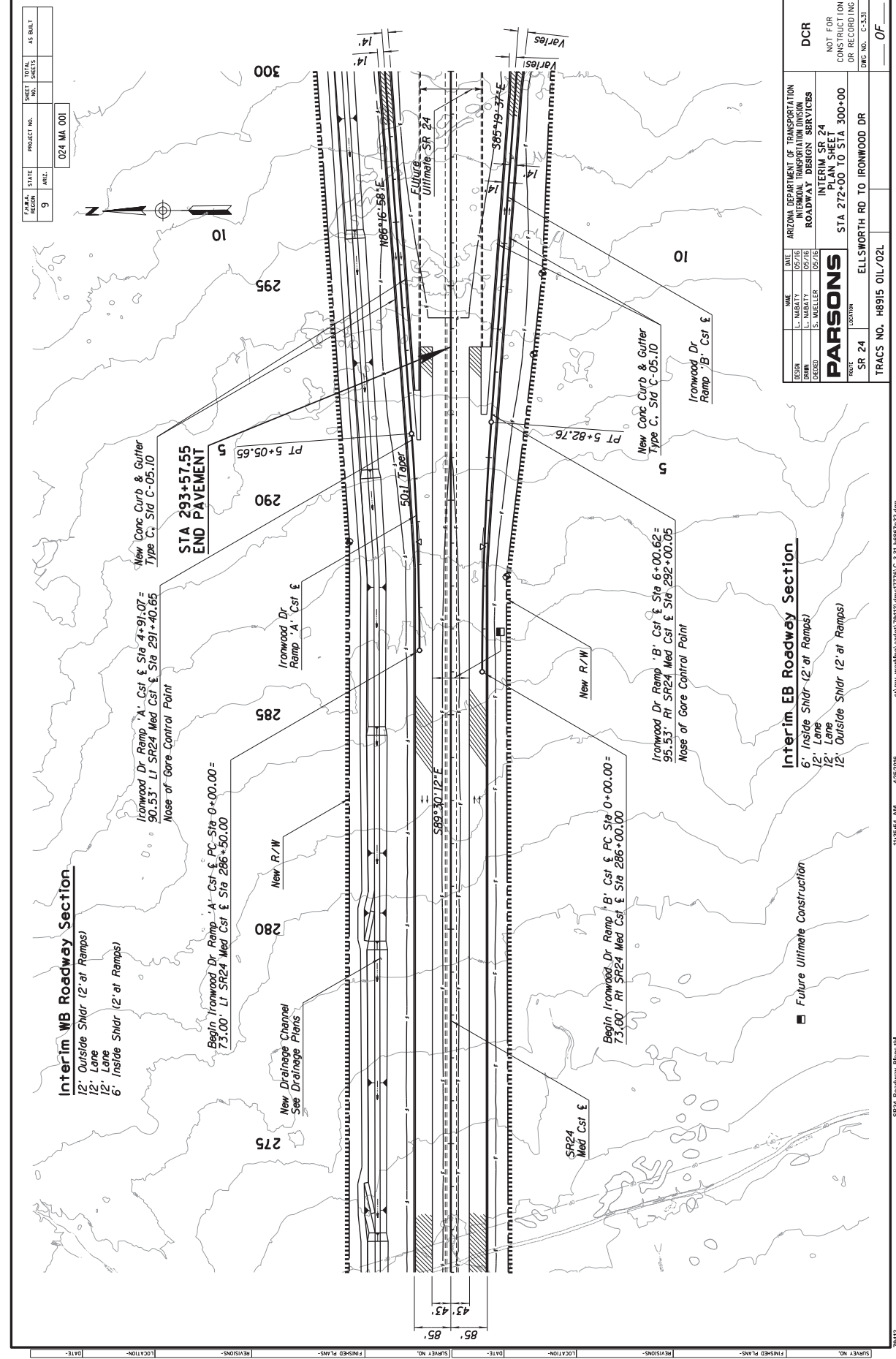
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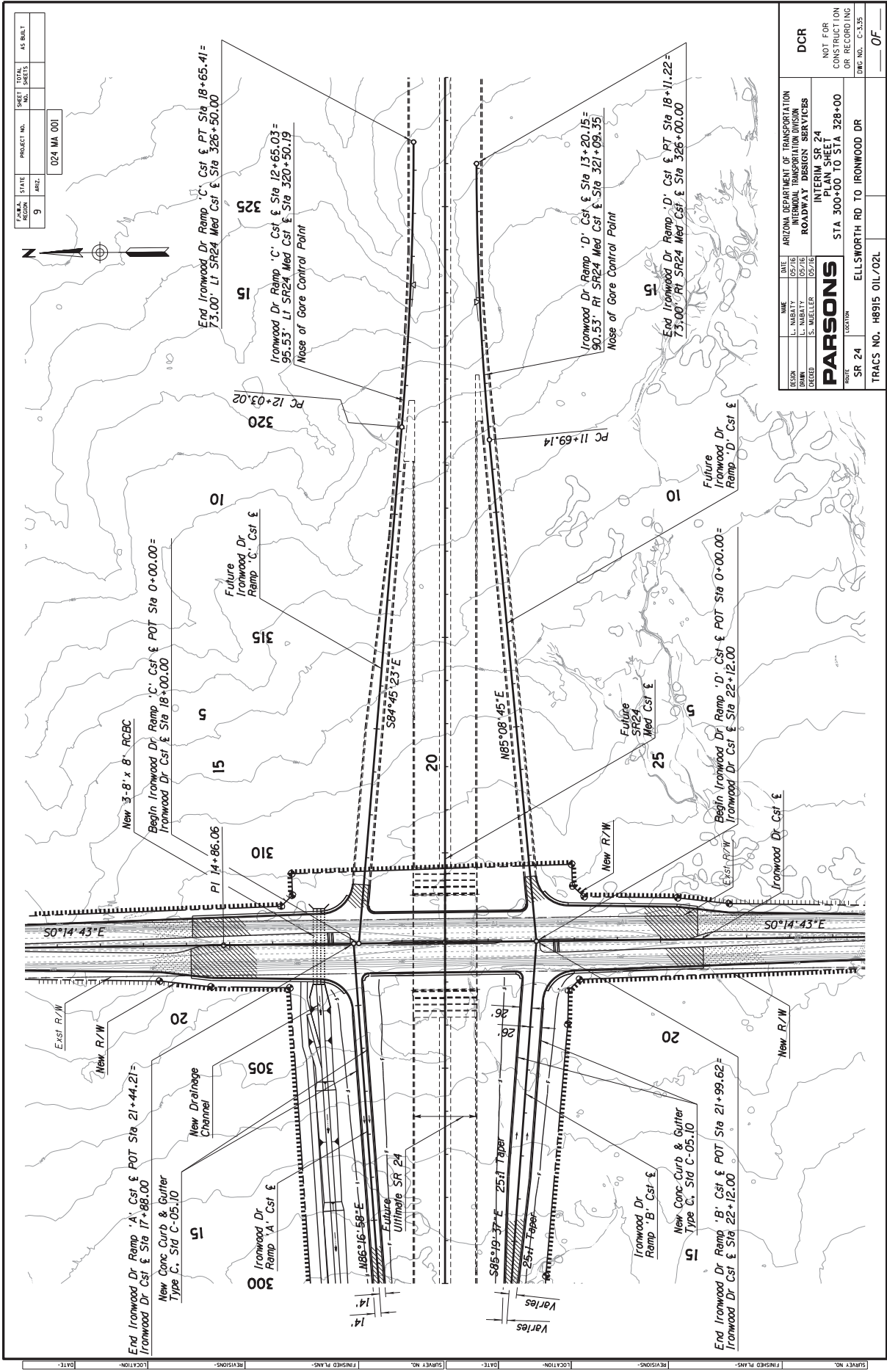
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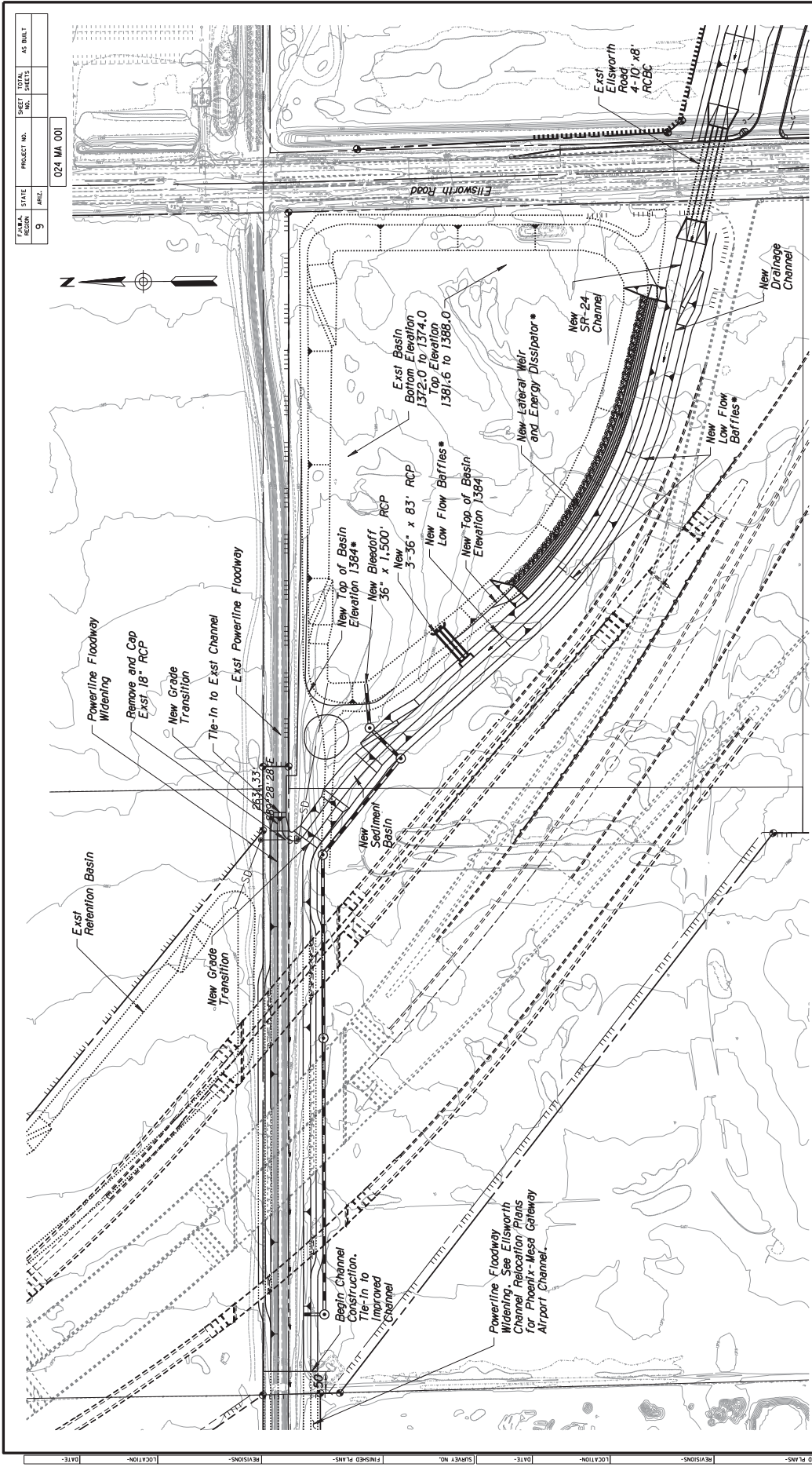
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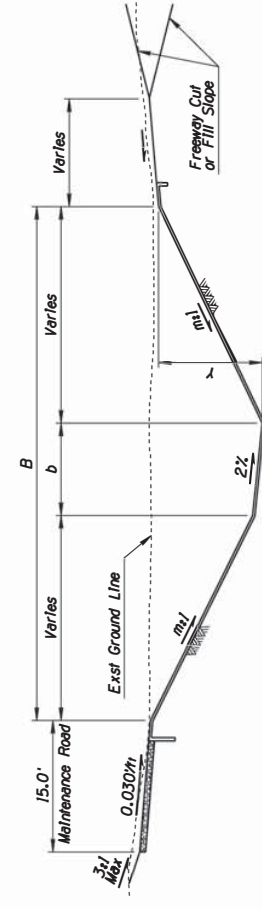
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DESIGN NOTE:
 • The Lateral Weir (740 L.F.), Low Flow Barfltes and elevated top of basin as shown are conceptual and will be refined in final design to reduce the estimated maximum 100-year, 24-hour channel peak flow discharging to Powerline Floodway to approximately 1,650 cfs. The maximum channel peak flow is estimated based on hydrology illustrating the January 2016 development conditions, and assuming that the SR-24 alignment extends to Central Arizona Project Canal Intersecting all flows discharging from the north and the northeast. As development progresses, peak flow reduces. The design of the Lateral Weir and the Lateral Weir Basin should be revised based on the magnitude of the peak flow at the line of construction.

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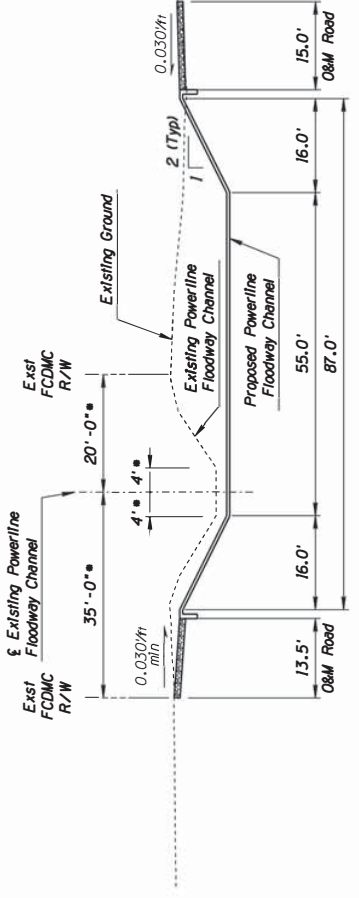
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Ellsworth, Ramp A	9+21	26+01	20 2	9.25 56.5
SR 24	60+44	120+04	20 2	9.25 55.2
	122+13	135+97	12-20.3 2	7.75 42.5-50.5
	138+06	193+20	12 2	7.75 42.5-50.5
	195+21	216+85	12 2	7.25 40.5-48.5
	219+79	245+85	12 2	7.25 40.5-48.5
	247+75	306+94	12 2	7.25 40.5-48.5

- Notes:
- All Dimensions are In feet
 - Stepped Channel maximum top width accounts for a 2ft step.
 - Larger bottom width downstream of confluences with offsite channel from Pacific Praying Grounds North Development west of Crisman Rd.

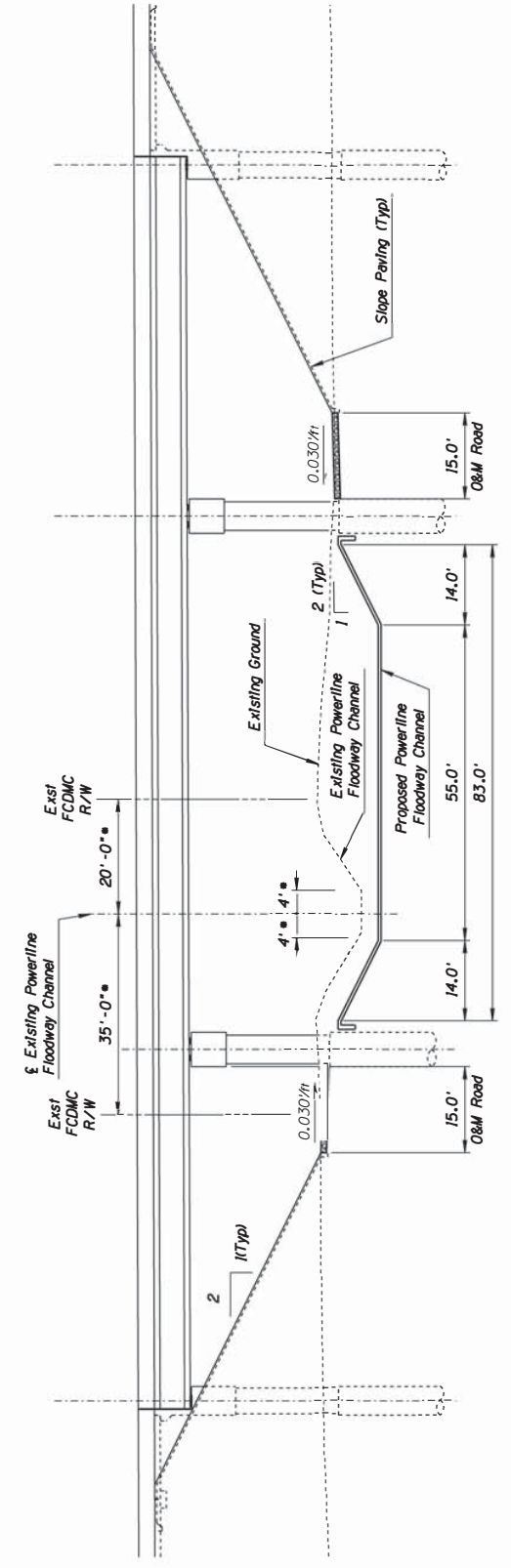
DATE	DATE	DATE	DATE
11/15/2018	11/15/2018	11/15/2018	11/15/2018
DESIGNED	CHECKED	IN CHARGE	DATE
PARSONS			
PROJECT	LOCATION	DRAWING NO.	
SR 24	ELLSWORTH RD TO IRONWOOD RD	D-102	
TRACS NO. H8915 OIL/O2L		OF	

SR24_Roadway_Plan.dwg 3:10:48 PM 24/09/18 c:\pwworking\arcan\p003024\sm1778\0-102_H8915.dwg

STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	AS BUILT
9	024 MA 001			



TYPICAL SECTION - POWERLINE FLOODWAY WIDENING OUTSIDE OF SR 24 MAINLINE AND RAMP STRUCTURES



TYPICAL SECTION - POWERLINE FLOODWAY WIDENING AT SR 24 MAINLINE AND RAMP STRUCTURES

- R/W Data Based on Powerline Floodway As-Built Plans.
- Note: Dimensions are Normal to Channel.

DATE	DATE	DATE	DATE
11/15/2018	11/15/2018	11/15/2018	11/15/2018
DESIGNED	CHECKED	IN CHARGE	DATE
PARSONS			
PROJECT	LOCATION	DRAWING NO.	
SR 24	ELLSWORTH RD TO IRONWOOD DR	D-102	
TRACS NO. H8915 OIL/O2L		OF	

SR24_Roadway_Plan.dwg 8:54:22 AM 2/17/2018 c:\pwworking\arcan\p003024\sm1778\0-103_H8915.dwg

APPENDIX B
FLOODPLAIN MAPS

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APPENDIX C

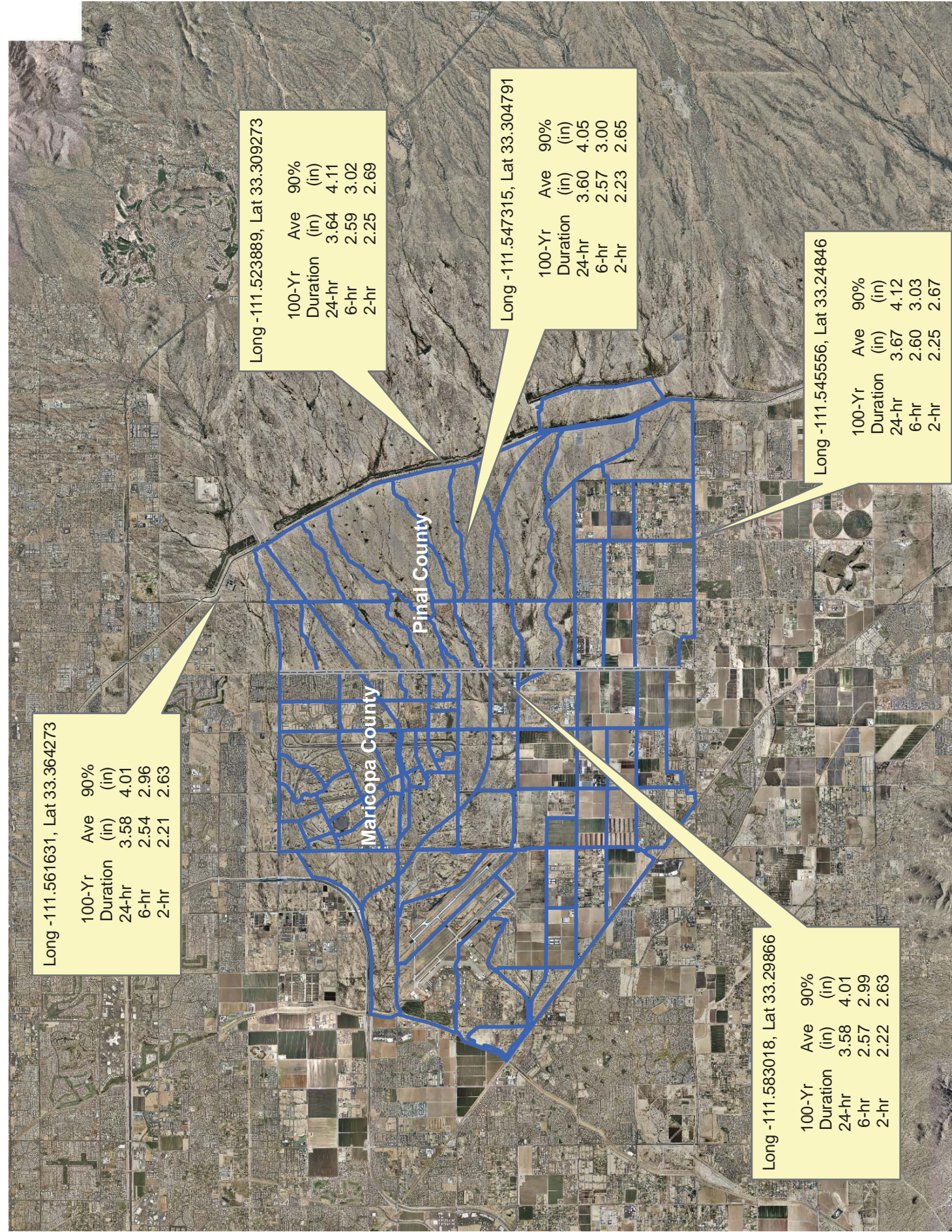
RAINFALL INTENSITY CALCULATIONS (FROM EAST MESA ADMPU)

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NOAA 14 Point Precipitation Values (in inches) for overall EMADMPU study watershed
(Maricopa and Pinal Counties combined)

Duration	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
5 MIN	0.251	0.340	0.408	0.500	0.572	0.645
10 MIN	0.383	0.518	0.621	0.762	0.871	0.981
15 MIN	0.474	0.642	0.770	0.944	1.079	1.216
30 MIN	0.639	0.865	1.037	1.272	1.453	1.638
1 HOUR	0.791	1.070	1.283	1.574	1.799	2.027
2 HOUR	0.897	1.193	1.422	1.731	1.971	2.219
3 HOUR	0.944	1.239	1.472	1.797	2.055	2.324
6 HOUR	1.126	1.438	1.686	2.025	2.293	2.572
12 HOUR	1.278	1.611	1.874	2.231	2.505	2.785
24 HOUR	1.547	1.982	2.330	2.809	3.184	3.579

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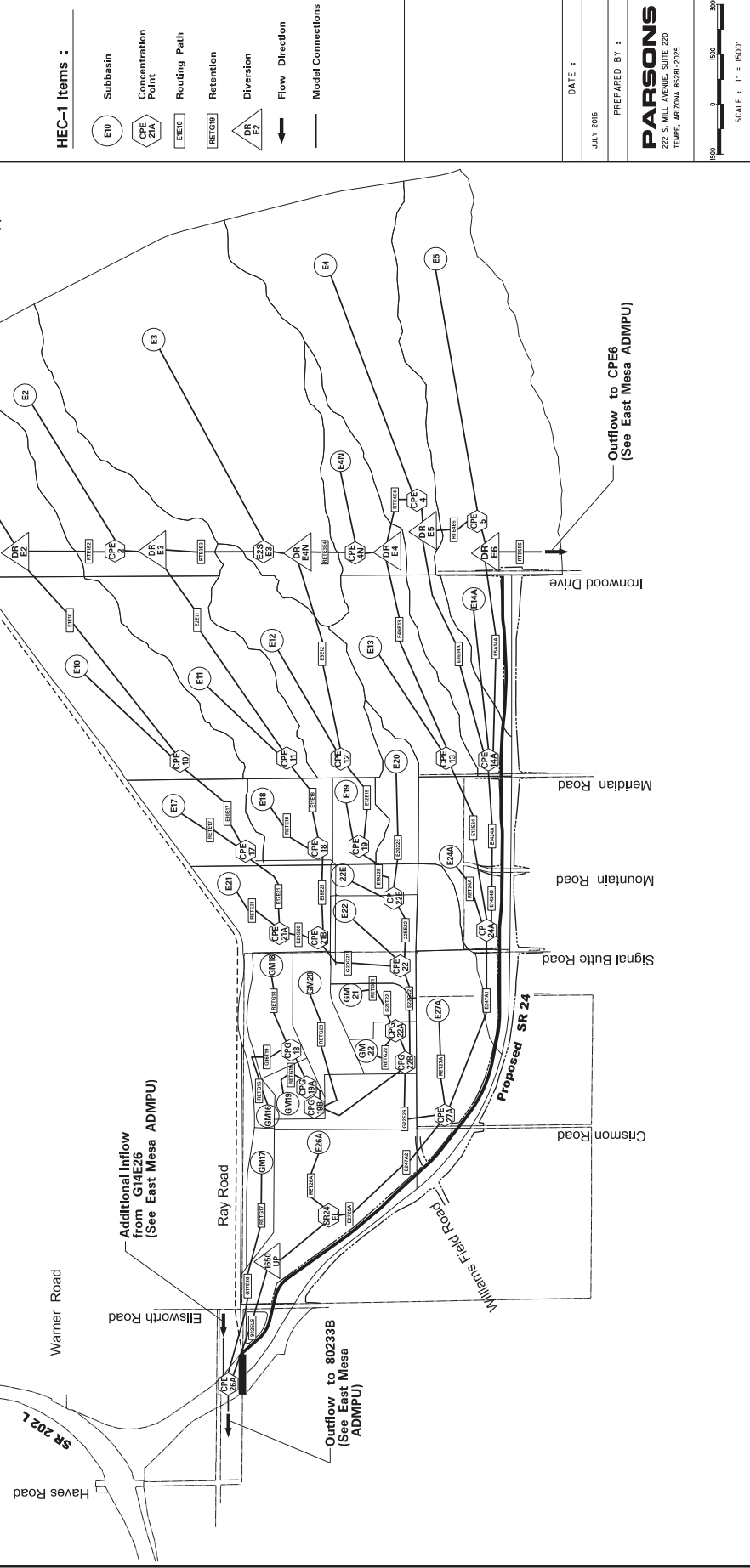


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APPENDIX D
OFF-SITE HYDROLOGY

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**SR 24 GATEWAY FREEWAY ELLSWORTH ROAD TO IRONWOOD DRIVE
INTERIM PHASE II
HEC-1 Schematic
Ironwood Dr. Terminus
(24INT0501C and 24INT1001C)**



Reference Items :
 East Mesa ADMP Subbasin Boundary
 Right of Way
 Major Arterials
 SR 24 Channel
 Powerline Floodway (Existing)
 Powerline Floodway (Proposed/Widened)

HEC-1 Items :

- Subbasin
- Concentration Point
- Routing Path
- Retention
- Diversions
- Flow Direction
- Model Connections

DATE :
 JULY 2006
 PREPARED BY :
PARSONS
 225 S. MILL AVENUE, SUITE 270
 TEMPE, ARIZONA 85281-2025
 SCALE : 1" = 1500'

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Date:
Prepared by: F. Braileanu 12/22/2015
Checked by: L. Ferreras 1/11/2016

SR 24 - Revised Routes for the INT models using concrete lining

ROUTE	FROM	TO	TIME STEP (sec)	LENGTH (ft)	VELOCITY (ft/s)	Time Steps
			300			
E2726A	Williams Field Road	Ellsworth Road	300	6350	10.72	4
E247A2	Ellsworth Road	Crismon Road	300	1528	10.35	1
E247A1	Crismon Road	Signal Butte Road	300	5594	10.35	4
E1424B	Signal Butte Road	Mountain Road	300	2461	9.97	2
E1424A	Mountain Road	Meridian Road	300	2808	9.97	2
E5A14A	Meridian Road	Ironwood Road	300	6121	9.97	4

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```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 04JUL16 TIME 13:51:13
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

```

```

X X XXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID 24INT050IC 100-YEAR, 24-hr Interim Phase II Conditions 2016-07-04
2 ID Assuming concrete-lined channel for the following routes:
3 ID E5A14A, E1424A, E1424B, E247A1, E247A2 and E2726A.
4 ID by Parsons Corporation
5 ID
6 ID The model reflects interim drainage conditions for SR 24 and it is based
7 ID on Mesa ADMPU with revisions reflecting development work around the
8 ID corridor.
9 ID This model simulates that the SR 24 corridor extends to Ironwood Dr,
10 ID which would eliminate the need to intercept runoff from subbasins
11 ID E5A, E6A and RTE4E5.
12 ID Therefore, subbasins E5A and E5B, and E6A and E6B were reconfigured to
13 ID match the layout, characteristics and hydrologic connectivity of
14 ID subbasins E5 and E6 in the existing condition model (24EX100). Also,
15 ID diversion DRE6 was reintroduced to simulate the cascading flows
16 ID east of Ironwood Dr.
17 ID
18 ID *****
19 ID FUTEMADMP24 20110519 - EMADMPU 24-hr Future Conditions 20110519
20 ID Flood Control District of Maricopa County
21 ID 50 YEAR
22 ID 24 Hour Storm
23 ID Unit Hydrograph: S-Graph
24 ID 08/05/2011
25 IT 5 0 0 2000
26 IN 15
27 IO 5
28 *DIAGRAM
29 *
30 JD 3.184 0.0001
31 PC 0.000 0.002 0.005 0.008 0.011 0.014 0.017 0.020 0.023 0.026
32 PC 0.029 0.032 0.035 0.038 0.041 0.044 0.048 0.052 0.056 0.060
33 PC 0.064 0.068 0.072 0.076 0.080 0.085 0.090 0.095 0.100 0.105
34 PC 0.110 0.115 0.120 0.126 0.133 0.140 0.147 0.155 0.163 0.172
35 PC 0.181 0.191 0.203 0.218 0.236 0.257 0.283 0.307 0.337 0.370
36 PC 0.735 0.758 0.776 0.791 0.804 0.815 0.825 0.834 0.842 0.849
37 PC 0.856 0.863 0.869 0.875 0.881 0.887 0.893 0.898 0.903 0.908
38 PC 0.913 0.918 0.922 0.926 0.930 0.934 0.938 0.942 0.946 0.950
39 PC 0.953 0.956 0.959 0.962 0.965 0.968 0.971 0.974 0.977 0.980
40 PC 0.983 0.986 0.989 0.992 0.995 0.998 1.000
41 JD 3.168 1.0
42 JD 3.104 5.0
43 JD 3.025 10.0
44 JD 2.923 20.0
45 JD 2.866 30.0
46 JD 2.824 40.0
47 JD 2.792 50.0
48 JD 2.770 60.0
49 *

```

1 HEC-1 INPUT PAGE 2

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
47 KK P1 BASIN
48 KM
49 KM Used the unit hydrograph for undeveloped conditions
50 KM by Parsons Corporation 2015-11
51 BA 0.387
52 LG 0.35 0.35 3.95 0.47 0
53 UI 0 29 29 99 134 162 189 226 301 369
54 UI 298 248 210 175 144 108 65 50 45 29
55 UI 26 9 9 9 9 9 9 0 0 0
56 UI 0 0 0 0 0 0 0 0 0 0
57 UI 0 0 0 0 0 0 0 0 0 0

```

```

58 *
59 KM KK DIVP1 DIVERT
60 KM Revised by removing the retention to account for undeveloped conditions
61 KM by Parsons Corporation 2015-11
62 *DT RETP1 29.5 0.0
63 *DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
64 *DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
65 *

```

```

62 KK DP1PFW DIVERT
63 KM
64 DT DRPFW 0.0 0.0
65 DI 0.0 50.0 100.0 150.0 200.0 250.0 300.0 400.0 500.0 600.0
66 DQ 0.0 10.0 42.0 81.0 123.0 166.0 211.0 301.0 392.0 485.0
67 *

```

```

67 KK P1P2 ROUTE
68 KM
69 KM Revised by using routing for undeveloped conditions
70 KM by Parsons Corporation 2015-11
71 RS 22 FLOW
72 RC 0.045 0.040 0.045 6529 0.0061 5.50
73 RX 0.00 500.00 1000.00 1005.00 1006.00 1010.00 1510.00 2010.00
74 RY 2.50 2.00 1.50 1.00 1.00 1.50 2.00 2.50
75 *

```

```

75 KK P2 BASIN
76 KM
77 KM Used the unit hydrograph for undeveloped conditions
78 KM by Parsons Corporation 2015-11
79 BA 0.577
80 LG 0.35 0.35 4.10 0.44 0
81 UI 0 38 38 92 151 187 214 247 287 357
82 UI 476 428 352 306 263 226 190 158 108 67
83 UI 63 55 38 38 14 12 12 12 12 12
84 UI 12 0 0 0 0 0 0 0 0 0
85 UI 0 0 0 0 0 0 0 0 0 0
86 *

```

```

86 KM KK DIVP2 DIVERT
87 KM
88 KM Revised by removing the retention to account for undeveloped conditions
89 KM by Parsons Corporation 2015-11
90 *DT RETP2 44.3 0.0
91 *DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
92 *DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
93 *

```

1 HEC-1 INPUT PAGE 3

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
90 KK CPP2 COMBINE
91 KM Combine Sub-basin P2 and routed flows from sub-basin P1
92 HC 2
93 *

```

```

93 KK P2P4 ROUTE
94 KM
95 RS 5 FLOW
96 RC 0.060 0.050 0.060 2856 0.0063 5.00
97 RX 0.00 100.00 110.00 145.00 150.00 200.00 210.00 325.00
98 RY 5.00 5.00 3.00 1.00 1.00 3.00 5.00 5.00
99 *

```

```

99 KK P4 BASIN
100 KM
101 BA 0.497
102 LG 0.25 0.25 5.40 0.27 30
103 UI 0 49 94 206 267 331 431 603 478 383
104 UI 303 239 159 85 75 49 29 15 15 15
105 UI 15 0 0 0 0 0 0 0 0 0
106 UI 0 0 0 0 0 0 0 0 0 0
107 UI 0 0 0 0 0 0 0 0 0 0
108 *

```

```

108 KK DIVP4 DIVERT
109 KM
110 DT RETP4 50.8 0.0
111 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
112 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
113 *

```

```

113 KK CPP4 COMBINE
114 KM
115 HC 2
116 *
116 KK P4P6 ROUTE
117 KM
118 RS 6 FLOW
119 RC 0.035 0.050 0.045 3423 0.0053 7.00
120 RX 0.00 10.00 35.00 100.00 105.00 120.00 125.00 140.00
121 RY 5.00 5.00 3.00 1.00 1.00 3.00 5.00 7.00
122 *

```

```

122 KK P6 BASIN
123 KM
124 BA 0.504
125 LG 0.25 0.25 5.20 0.31 31
126 UI 0 39 39 137 182 219 258 310 423 485
127 UI 379 319 266 221 180 126 72 65 49 39
128 UI 23 12 12 12 12 12 0 0 0 0

```

129 UI 0 0 0 0 0 0 0 0 0 0
130 UI 0 0 0 0 0 0 0 0 0 0
*

HEC-1 INPUT PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

131 KK DIVP6 DIVERT
132 KM
133 DT RETP6 50.4 0.0
134 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
135 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

136 KK CPP6 COMBINE
137 KM
138 HC 2
*

139 KK P6GM8 ROUTE
140 KM
141 RS 3 FLOW
142 RC 0.035 0.030 0.035 2432 0.0019 5.00
143 RX 950.00 989.00 991.00 1003.00 1007.00 1019.00 1021.00 1050.00
144 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
*

145 KK GM8G10 ROUTE
146 KM
147 RS 3 FLOW
148 RC 0.035 0.035 0.035 2628 0.0051 5.00
149 RX 0.00 500.00 980.00 1003.00 1007.00 1031.00 1511.00 2011.00
150 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.00
*

151 KK DRPFWRETRIEVE
152 KM
153 DR DRPFW
*

154 KK P1PFW ROUTE
155 KM
156 KM Revised by using routing for undeveloped conditions
157 KM by Parsons Corporation 2015-11
158 RS 2 FLOW
159 RC 0.030 0.016 0.030 8110 0.0062 8.00
160 RX 0.00 10.00 11.00 21.00 27.00 37.00 40.00 50.00
161 RY 8.00 8.00 7.50 1.00 1.00 7.50 8.00 8.00
*

162 KK P3 BASIN
163 KM
164 KM Used the unit hydrograph for undeveloped conditions
165 KM by Parsons Corporation 2015-11
166 BA 0.522
167 LG 0.35 0.35 3.95 0.47 0
168 UI 0 27 27 29 91 112 132 149 165 187
169 UI 209 250 317 349 290 251 224 201 175 156
170 UI 136 117 89 61 48 45 43 27 27 25
171 UI 8 8 8 8 8 8 8 8 8 0
172 UI 0 0 0 0 0 0 0 0 0 0
*

HEC-1 INPUT PAGE 5

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

173 KM KK DIVP3 DIVERT
174 KM
175 KM Revised by removing the retention to account for undeveloped conditions
176 KM by Parsons Corporation 2015-11
*DT RETP3 39.9 0.0
*DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
*DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
*

177 KK CPP3 COMBINE
178 KM
179 HC 2 0.91
*

180 KK P3P5 ROUTE
181 KM
182 RS 1 FLOW
183 RC 0.030 0.016 0.030 2889 0.0062 8.00
184 RX 0.00 10.00 11.00 21.00 27.00 37.00 40.00 50.00
185 RY 8.00 8.00 7.50 1.00 1.00 7.50 8.00 8.00
*

186 KK P5 BASIN
187 KM
188 BA 0.254
189 LG 0.25 0.25 6.00 0.22 30
190 UI 0 23 40 93 123 149 186 269 264 204
191 UI 167 134 104 64 40 34 23 14 7 7
192 UI 7 7 0 0 0 0 0 0 0 0
193 UI 0 0 0 0 0 0 0 0 0 0
194 UI 0 0 0 0 0 0 0 0 0 0
*

195 KK DIVP5 DIVERT
196 KM
197 DT RETP5 17.4 0.0

198 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
199 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

200 KK CPP5 COMBINE
201 KM
202 HC 2
*

203 KK P5P7 ROUTE
204 KM Powerline Floodway
205 RS 1 FLOW
206 RC 0.030 0.016 0.030 3146 0.0057 8.00
207 RX 0.00 10.00 11.00 21.00 27.00 37.00 40.00 50.00
208 RY 8.00 8.00 7.50 1.00 1.00 7.50 8.00 8.00
*

HEC-1 INPUT PAGE 6

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

209 KK P7 BASIN
210 KM
211 BA 0.429
212 LG 0.25 0.19 6.60 0.17 30
213 UI 0 40 71 163 214 260 328 478 436 341
214 UI 276 220 170 94 68 52 40 16 12 12
215 UI 12 12 0 0 0 0 0 0 0 0
216 UI 0 0 0 0 0 0 0 0 0 0
217 UI 0 0 0 0 0 0 0 0 0 0
*

218 KK DIVP7 DIVERT
219 KM
220 DT RETP7 31.0 0.0
221 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
222 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

223 KK CPP7 COMBINE
224 KM
225 HC 3 3.17
*

226 KK P7GM14 ROUTE
227 KM
228 RS 9 FLOW
229 RC 0.025 0.016 0.025 10659 0.0036 7.00
230 RX 0.00 14.50 16.00 24.60 32.60 41.20 42.70 57.20
231 RY 7.00 7.00 6.00 0.25 0.25 6.00 7.00 7.00
*

232 KK GM1 BASIN
233 KM
234 BA 0.345
235 LG 0.10 0.15 8.00 0.13 5
236 UI 0 38 93 178 228 297 447 394 303 232
237 UI 175 98 64 45 30 12 12 12 12 0
238 UI 0 0 0 0 0 0 0 0 0 0
239 UI 0 0 0 0 0 0 0 0 0 0
240 UI 0 0 0 0 0 0 0 0 0 0
*

241 KK GM2 BASIN
242 KM
243 BA 0.683
244 LG 0.20 0.25 6.00 0.23 48
245 UI 0 104 415 625 942 1178 805 560 298 165
246 UI 96 32 32 32 0 0 0 0 0 0
247 UI 0 0 0 0 0 0 0 0 0 0
248 UI 0 0 0 0 0 0 0 0 0 0
249 UI 0 0 0 0 0 0 0 0 0 0
*

HEC-1 INPUT PAGE 7

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

250 KK GM3 BASIN
251 KM
252 BA 0.288
253 LG 0.13 0.15 8.80 0.08 71
254 UI 0 279 882 743 244 57 0 0 0 0
255 UI 0 0 0 0 0 0 0 0 0 0
256 UI 0 0 0 0 0 0 0 0 0 0
257 UI 0 0 0 0 0 0 0 0 0 0
258 UI 0 0 0 0 0 0 0 0 0 0
*

259 KK CPG123 COMBINE
260 KM
261 HC 3
*

262 KK DIVG1 DIVERT
263 KM
264 DT RETG1 102.1 0.0
265 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
266 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

267 KK GM1T5 ROUTE
268 KM

269 RS 1 FLOW
 270 RC 0.040 0.035 0.040 2680 0.0050 5.00
 271 RX 0.00 5.00 10.00 22.00 33.00 45.00 50.00 55.00
 272 RY 5.00 4.50 4.00 1.00 1.00 4.00 4.50 5.00
 *

273 KK GM5 BASIN
 274 KM
 275 BA 0.176
 276 LG 0.11 0.13 10.10 0.05 60
 277 UI 0 68 210 385 353 206 81 36 12 12
 278 UI 0 0 0 0 0 0 0 0 0 0
 279 UI 0 0 0 0 0 0 0 0 0 0
 280 UI 0 0 0 0 0 0 0 0 0 0
 281 UI 0 0 0 0 0 0 0 0 0 0
 *

282 KK DIVG5 DIVERT
 283 KM
 284 DT RETG5 13.6 0.0
 285 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 286 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

HEC-1 INPUT PAGE 8

1 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

287 KK CPG5 COMBINE
 288 KM
 289 HC 2
 *

290 KK GM5T7 ROUTE
 291 KM
 292 RS 3 FLOW
 293 RC 0.032 0.032 0.032 3745 0.0020 5.50
 294 RX 0.00 5.00 10.00 24.00 44.00 58.00 63.00 68.00
 295 RY 5.50 5.00 4.50 1.00 1.00 4.50 5.00 5.50
 *

296 KK GM6 BASIN
 297 KM
 298 BA 0.368
 299 LG 0.25 0.15 8.00 0.10 38
 300 UI 0 240 705 1079 558 177 55 32 0 0
 301 UI 0 0 0 0 0 0 0 0 0 0
 302 UI 0 0 0 0 0 0 0 0 0 0
 303 UI 0 0 0 0 0 0 0 0 0 0
 304 UI 0 0 0 0 0 0 0 0 0 0
 *

305 KK DIVG6 DIVERT
 306 KM
 307 DT RETG6 26.8 0.0
 308 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 309 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

310 KK GM7 BASIN
 311 KM
 312 BA 0.216
 313 LG 0.14 0.19 6.60 0.21 16
 314 UI 0 29 95 155 208 328 286 209 152 88
 315 UI 49 32 15 9 9 0 0 0 0 0
 316 UI 0 0 0 0 0 0 0 0 0 0
 317 UI 0 0 0 0 0 0 0 0 0 0
 318 UI 0 0 0 0 0 0 0 0 0 0
 *

319 KK DIVG7 DIVERT
 320 KM
 321 DT RETG7 14.6 0.0
 322 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 323 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

HEC-1 INPUT PAGE 9

1 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

324 KK CPG7A COMBINE
 325 KM
 326 HC 2
 *

327 KK CPG7B COMBINE
 328 KM
 329 HC 2
 *

330 KK GM7T9 ROUTE
 331 KM
 332 RS 1 FLOW
 333 RC 0.032 0.032 0.032 2140 0.0020 5.50
 334 RX 0.00 5.00 10.00 24.00 44.00 58.00 63.00 68.00
 335 RY 5.50 5.00 4.50 1.00 1.00 4.50 5.00 5.50
 *

336 KK GM8 BASIN
 337 KM
 338 BA 0.558
 339 LG 0.24 0.25 5.60 0.27 43

340 UI 0 82 310 473 681 964 681 481 306 140
 341 UI 94 41 25 25 0 0 0 0 0 0
 342 UI 0 0 0 0 0 0 0 0 0 0
 343 UI 0 0 0 0 0 0 0 0 0 0
 344 UI 0 0 0 0 0 0 0 0 0 0
 *

345 KK DIVG8 DIVERT
 346 KM
 347 DT RETG8 40.1 0.0
 348 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 349 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

350 KK GM9 BASIN
 351 KM
 352 BA 0.095
 353 LG 0.16 0.25 5.40 0.32 22
 354 UI 0 69 206 278 127 39 10 0 0 0
 355 UI 0 0 0 0 0 0 0 0 0 0
 356 UI 0 0 0 0 0 0 0 0 0 0
 357 UI 0 0 0 0 0 0 0 0 0 0
 358 UI 0 0 0 0 0 0 0 0 0 0
 *

359 KK DIVG9 DIVERT
 360 KM
 361 DT RETG9 6.7 0.0
 362 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 363 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

HEC-1 INPUT PAGE 10

1 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

364 KK CPG9A COMBINE
 365 KM
 366 HC 2
 *

367 KK GM10 BASIN
 368 KM
 369 BA 0.280
 370 LG 0.23 0.17 6.80 0.17 40
 371 UI 0 38 131 210 285 447 362 265 188 98
 372 UI 62 38 13 12 12 0 0 0 0 0
 373 UI 0 0 0 0 0 0 0 0 0 0
 374 UI 0 0 0 0 0 0 0 0 0 0
 375 UI 0 0 0 0 0 0 0 0 0 0
 *

376 KK DIVG10 DIVERT
 377 KM
 378 DT RETG10 17.5 0.0
 379 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 380 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

381 KK GM11 BASIN
 382 KM
 383 BA 0.075
 384 LG 0.19 0.25 4.00 0.63 30
 385 UI 0 23 75 125 162 101 54 23 10 5
 386 UI 5 0 0 0 0 0 0 0 0 0
 387 UI 0 0 0 0 0 0 0 0 0 0
 388 UI 0 0 0 0 0 0 0 0 0 0
 389 UI 0 0 0 0 0 0 0 0 0 0
 *

390 KK DIVG11 DIVERT
 391 KM
 392 DT RETG11 5.4 0.0
 393 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 394 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

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1 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

395 KK CPG11 COMBINE
 396 KM
 397 HC 2
 *

398 KK CPG9B COMBINE
 399 KM
 400 HC 3
 *

401 KK GM9T14 ROUTE
 402 KM
 403 RS 3 FLOW
 404 RC 0.032 0.032 0.032 3560 0.0020 6.00
 405 RX 0.00 5.00 10.00 24.00 46.00 60.00 65.00 80.00
 406 RY 6.00 5.00 4.50 1.00 1.00 4.50 5.00 6.00
 *

407 KK GM12 BASIN
 408 KM
 409 BA 0.118
 410 LG 0.10 0.15 8.80 0.09 78

558 KM
 559 HC 2
 *
 560 KK E17E21 ROUTE
 561 KM
 562 KM Buildout routing steps kept at 4
 563 KM by Parsons Corporation 2015-11
 564 RS 4 FLOW
 565 RC 0.030 0.045 0.030 2832 0.0042 1440.20
 HEC-1 INPUT

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1
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

566 RX 0.00 90.00 100.00 115.00 180.00 195.00 255.00 260.00
 567 RY 1440.0 1439.90 1439.80 1438.00 1438.00 1440.00 1440.10 1440.20
 *

568 KK E21 BASIN
 569 KM
 570 KM Mountain Horizons
 571 KM Buildout conditions assumed through the interim condition
 572 KM by Parsons Corporation 2015-11
 573 BA 0.311
 574 LG 0.25 0.25 6.00 0.22 30
 575 UI 0 30 56 125 162 199 257 368 305 243
 576 UI 193 153 108 59 49 31 24 9 9 9
 577 UI 9 0 0 0 0 0 0 0 0 0
 578 UI 0 0 0 0 0 0 0 0 0 0
 579 UI 0 0 0 0 0 0 0 0 0 0
 *

580 KK DIVE21 DIVERT
 581 KM
 582 KM Buildout retention in place through the interim condition
 583 KM by Parsons Corporation 2015-11
 584 DT RETE21 20.3 0.0
 585 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 586 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

587 KK CPE21A COMBINE
 588 KM
 589 HC 2
 *

590 KK E21G20 ROUTE
 591 KM
 592 RS 1 FLOW
 593 RC 0.032 0.032 0.032 1655 0.0036 5.50
 594 RX 0.00 5.00 10.00 24.00 34.00 48.00 53.00 58.00
 595 RY 5.50 5.00 4.50 1.00 1.00 4.50 5.00 5.50
 *

596 KM
 597 KK DRE2RETRIEVE
 598 KM
 599 DR DRE2
 *

600 KK RTE1E2 ROUTE
 601 KM
 602 KM Revised by using routing for undeveloped conditions
 603 KM by Parsons Corporation 2015-11
 604 RS 4 FLOW
 605 RC 0.035 0.030 0.025 4100 0.0035 6.00
 606 RX 0.00 100.00 700.00 1050.00 1090.00 1110.00 1140.00 1240.00
 607 RY 6.00 6.00 4.00 1.00 1.00 5.00 6.00 6.00
 *

HEC-1 INPUT PAGE 16

1
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

608 KK E2 BASIN
 609 KM
 610 KM Used the unit hydrograph for undeveloped conditions
 611 KM by Parsons Corporation 2015-11
 612 BA 0.779
 613 LG 0.35 0.35 4.25 0.41 0
 614 UI 0 45 45 77 159 202 234 263 298 342
 615 UI 412 536 556 456 394 352 304 267 228 196
 616 UI 145 95 78 74 58 45 45 19 14 14
 617 UI 14 14 14 14 14 0 0 0 0 0
 618 UI 0 0 0 0 0 0 0 0 0 0
 *

619 KM KK DIVE2 DIVERT
 620 KM
 621 KM Revised by removing the retention to account for undeveloped conditions
 622 KM by Parsons Corporation 2015-11
 *DT RETE2 60.4 0.0
 *DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

623 KK CPE2 COMBINE
 624 KM
 625 HC 2 1.67
 *

626 KK DE2S DIVERT
 627 KM
 628 DT DRE3 0.0 0.0

629 DI 0.0 135.0 279.0 431.0 583.0 738.0 894.0 0.0 0.0 0.0
 630 DQ 0.0 15.0 121.0 243.0 370.0 504.0 636.0 0.0 0.0 0.0
 *

631 KK E2E11 ROUTE
 632 KM
 633 KM Revised by using routing for undeveloped conditions
 634 KM by Parsons Corporation 2015-11
 635 RS 34 FLOW
 636 RC 0.055 0.045 0.055 9374 0.0052 5.00
 637 RX 0.00 500.00 1000.00 1005.00 1006.00 1010.00 1510.00 2010.00
 638 RY 2.50 2.00 1.50 1.00 1.00 1.50 2.00 2.50
 *

639 KK E11 BASIN
 640 KM
 641 KM Used the unit hydrograph for undeveloped conditions
 642 KM by Parsons Corporation 2015-11
 643 BA 0.600
 644 LG 0.35 0.35 3.95 0.47 0
 645 UI 0 37 37 76 135 174 201 226 261 303
 646 UI 394 472 392 332 293 252 220 186 157 114
 647 UI 70 63 60 39 37 28 11 11 11 11
 648 UI 11 11 11 0 0 0 0 0 0 0
 649 UI 0 0 0 0 0 0 0 0 0 0
 *

HEC-1 INPUT PAGE 17

1
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

650 KM KK DIVE11 DIVERT
 651 KM
 652 KM Revised by removing the retention to account for undeveloped conditions
 653 KM by Parsons Corporation 2015-11
 654 KM DT RETE11 45.8 0.0
 655 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 656 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

657 KK CPE11 COMBINE
 658 KM
 659 HC 2
 *

660 KK E11E18 ROUTE
 661 KM
 662 KM Buildout routing steps reduced from 22 to 9 through the interim condition
 663 KM by Parsons Corporation 2015-11
 664 RS 9 FLOW
 665 RC 0.045 0.040 0.045 3164 0.0044 5.50
 666 RX 0.00 500.00 1000.00 1005.00 1006.00 1010.00 1510.00 2010.00
 667 RY 2.50 2.00 1.50 1.00 1.00 1.50 2.00 2.50
 *

668 KK E18 BASIN
 669 KM
 670 KM Rancho Apache
 671 KM Existing and Buildout conditions are the same
 672 KM by Parsons Corporation 2015-11
 673 BA 0.224
 674 LG 0.30 0.15 7.00 0.14 16
 675 UI 0 30 103 166 224 352 291 213 153 82
 676 UI 51 30 12 9 9 0 0 0 0 0
 677 UI 0 0 0 0 0 0 0 0 0 0
 678 UI 0 0 0 0 0 0 0 0 0 0
 679 UI 0 0 0 0 0 0 0 0 0 0
 *

680 KK DIVE18 DIVERT
 681 KM
 682 DT RETE18 0.3 0.0
 683 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 684 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

685 KK CPE18 COMBINE
 686 KM
 687 HC 2
 *

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1
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

688 KK E18E21 ROUTE
 689 KM
 690 KM Buildout routing steps unchanged
 691 KM by Parsons Corporation 2015-11
 692 RS 2 FLOW
 693 RC 0.035 0.040 0.045 2664 0.0053 5.00
 694 RX 0.00 15.00 50.00 60.00 100.00 110.00 290.00 300.00
 695 RY 3.50 3.00 3.00 1.00 1.00 3.00 3.00 5.00
 *

696 KK CPE21B COMBINE
 697 KM
 698 HC 2 3.90
 *

699 KK G20G21 ROUTE
 700 KM
 701 KM
 702 RS 2 FLOW

703 RC 0.032 0.032 0.032 1901 0.0021 5.50
 704 RX 0.00 1.00 5.00 24.00 124.00 138.00 143.00 148.00
 705 RY 5.50 5.00 4.50 1.00 1.00 4.50 5.00 5.50
 *
 706 KM

707 KK DRE3RETRIEVE
 708 KM
 709 DR DRE3
 *
 710 KK RTE2E3 ROUTE
 711 KM
 712 KM Revised by using routing for undeveloped conditions
 713 KM by Parsons Corporation 2015-11
 714 RS 4 FLOW
 715 RC 0.035 0.030 0.025 3678 0.0035 6.00
 716 RX 0.00 100.00 700.00 1050.00 1090.00 1110.00 1140.00 1240.00
 717 RY 6.00 6.00 4.00 1.00 1.00 5.00 6.00 6.00
 *

718 KK E3 BASIN
 719 KM
 720 KM Used the unit hydrograph for undeveloped conditions
 721 KM by Parsons Corporation 2015-11
 722 BA 2.234
 723 LG 0.35 0.35 4.60 0.33 0
 724 UI 0 91 91 91 136 303 356 427 467 510
 725 UI 552 605 672 731 857 1035 1206 1075 936 840
 726 UI 769 712 638 576 531 468 432 369 285 220
 727 UI 162 158 150 150 92 91 91 79 28 28
 728 UI 28 28 28 28 28 28 28 28 28 28
 729 UI 0 0 0 0 0 0 0 0 0 0
 *

730 KM KK DIVE3 DIVERT
 *
 734 KK E2SE3 COMBINE
 735 KM
 736 HC 2 3.9
 *

737 KK DE3S DIVERT
 738 KM
 739 DT DRE4N 0.0 0.0
 740 DI 0.0 192.0 476.0 774.0 1079.0 1390.0 1699.0 0.0 0.0 0.0
 741 DQ 0.0 5.0 197.0 415.0 656.0 912.0 1175.0 0.0 0.0 0.0
 *

742 KK E3E12 ROUTE
 743 KM
 744 KM Revised by using routing for undeveloped conditions
 745 KM by Parsons Corporation 2015-11
 746 RS 15 FLOW
 747 RC 0.060 0.050 0.060 4852 0.0054 5.50
 748 RX 0.00 500.00 980.00 1003.00 1007.00 1031.00 1511.00 2011.00
 749 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

750 KK E12 BASIN
 751 KM
 752 KM Used the unit hydrograph for undeveloped conditions.
 753 KM by Parsons Corporation 2015-11
 754 BA 0.573
 755 LG 0.35 0.35 4.60 0.33 0
 756 UI 0 32 32 49 112 140 164 184 208 237
 757 UI 275 354 415 346 296 263 232 202 177 154
 758 UI 126 89 57 55 53 35 32 30 10 10
 759 UI 10 10 10 10 10 10 10 0 0 0
 760 UI 0 0 0 0 0 0 0 0 0 0
 *

761 KM KKDIVE12 DIVERT
 762 KM
 763 KM Revised by removing the retention to account for undeveloped conditions
 764 KM by Parsons Corporation 2015-11
 765 KM DTRETE12 43.7 0.0
 766 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 767 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 *
 HEC-1 INPUT
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
 768 KK CPE12 COMBINE
 769 KM
 770 HC 2
 *
 771 KK E12E19 ROUTE
 772 KM
 773 KM Buildout routing steps kept at 9 through the interim condition
 774 KM by Parsons Corporation 2015-11

775 RS 9 FLOW
 776 RX 0.060 0.055 0.060 2707 0.0052 5.50
 777 RX 0.00 500.00 980.00 1003.00 1007.00 1031.00 1511.00 2011.00
 778 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *
 779 KK E19 BASIN
 780 KM
 781 KM Part of Superstition View
 782 KM Existing conditions assumed through the interim condition
 783 KM by Parsons Corporation 2015-11
 784 BA 0.135
 785 LG 0.30 0.15 8.00 0.10 15
 786 UI 0 35 119 186 288 194 122 51 29 9
 787 UI 8 0 0 0 0 0 0 0 0 0
 788 UI 0 0 0 0 0 0 0 0 0 0
 789 UI 0 0 0 0 0 0 0 0 0 0
 790 UI 0 0 0 0 0 0 0 0 0 0
 *

791 KM KKDIVE19 DIVERT
 792 KM
 793 KM Revised by removing the retention to account for undeveloped conditions
 794 KM by Parsons Corporation 2015-11
 795 KM DTRETE19 0.2 0.0
 796 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 797 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 *

798 KK CPE19 COMBINE
 799 KM
 800 HC 2
 *

801 KK E1922E ROUTE
 802 KM
 803 KM No change between existing (pre-buildup) and buildup conditions
 804 KM by Parsons Corporation 2015-11
 805 RS 4 FLOW
 806 RC 0.050 0.040 0.050 1912 0.0042 10.00
 807 RX 0.00 500.00 980.00 1003.00 1007.00 1031.00 1511.00 2011.00
 808 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

1 HEC-1 INPUT PAGE 21

809 KK 22E BASIN
 810 KM
 811 KM Used the unit hydrograph for existing (partially developed) conditions.
 812 KM by Parsons Corporation 2015-11
 813 BA 0.089
 814 LG 0.31 0.19 8.40 0.08 11
 815 UI 0 19 69 104 173 137 91 48 24 12
 816 UI 5 5 0 0 0 0 0 0 0 0
 817 UI 0 0 0 0 0 0 0 0 0 0
 818 UI 0 0 0 0 0 0 0 0 0 0
 819 UI 0 0 0 0 0 0 0 0 0 0
 *

820 KM KKDIV22E DIVERT
 821 KM
 822 KM Revised by removing the retention to account for undeveloped conditions
 823 KM by Parsons Corporation 2015-11
 824 KM DTRETE22E 7.8 0.0
 825 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 826 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 *

827 KK E20 BASIN
 828 KM
 829 KM Used the unit hydrograph for existing (partially developed) conditions.
 830 KM by Parsons Corporation 2015-11
 831 BA 0.169
 832 LG 0.32 0.28 4.50 0.35 10
 833 UI 0 17 33 72 93 115 153 206 161 129
 834 UI 102 79 50 29 24 17 8 5 5 5
 835 UI 5 0 0 0 0 0 0 0 0 0
 836 UI 0 0 0 0 0 0 0 0 0 0
 837 UI 0 0 0 0 0 0 0 0 0 0
 *

838 KM KKDIVE20 DIVERT
 839 KM
 840 KM Revised by removing the retention to account for existing (pre-buildout)
 841 KM conditions
 842 KM by Parsons Corporation 2015-11
 843 KM DTRETE20 3.2 0.0
 844 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 845 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 *

846 KK E2022E ROUTE
 847 KM
 848 KM Revised by using routing for existing (pre-buildout) conditions
 849 KM by Parsons Corporation 2015-11
 850 RS 3 FLOW
 851 RC 0.045 0.035 0.045 1115 0.0054 10.00
 852 RX 0.00 500.00 1000.00 1005.00 1007.00 1010.00 1511.00 2011.00
 853 RY 2.50 2.00 1.50 1.00 1.00 1.50 2.00 2.50
 *

1 HEC-1 INPUT PAGE 22

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

854 KK CP22E COMBINE
855 KM
856 HC 3
*

857 KK 22EE22 ROUTE
858 KM
859 RS 1 FLOW
860 RC 0.045 0.040 0.045 1740 0.0046 10.00
861 RX 950.00 973.00 993.00 1005.00 1013.00 1025.00 1045.00 1055.00
862 RY 5.00 4.50 4.00 1.00 1.00 4.00 4.50 5.00
*

863 KK E22 BASIN
864 KM
865 KM Revised by using the unit hydrograph for undeveloped conditions
866 KM by Parsons Corporation 2015-11
867 BA 0.158
868 LG 0.35 0.32 7.60 0.10 1
869 UI 0 18 18 58 81 99 114 136 171 232
870 UI 200 164 141 117 98 80 55 32 30 23
871 UI 18 12 6 6 6 6 6 6 0 0
872 UI 0 0 0 0 0 0 0 0 0 0
873 UI 0 0 0 0 0 0 0 0 0 0
*

874 KM KKDIVE22 DIVERT
875 KM
876 KM Revised by removing the retention to account for undeveloped conditions
877 KM by Parsons Corporation 2015-11
878 KM DTRETE22 13.8 0.0
879 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
880 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
*

881 KK CPE22 COMBINE
882 KM
883 HC 3 7.25
*

884 KK E22G22 ROUTE
885 KM
886 RS 3 FLOW
887 RC 0.040 0.050 0.040 4418 0.0043 8.00
888 RX 720.00 750.00 785.00 805.00 845.00 865.00 880.00 910.00
889 RY 8.00 7.00 6.00 1.00 1.00 6.00 7.00 8.00
*

890 KK GM21 BASIN
891 KM
892 BA 0.210
893 LG 0.10 0.15 7.30 0.14 75
894 UI 0 51 176 272 437 309 200 90 49 19
895 UI 12 12 0 0 0 0 0 0 0 0
896 UI 0 0 0 0 0 0 0 0 0 0
*

1 HEC-1 INPUT PAGE 23
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
897 UI 0 0 0 0 0 0 0 0 0 0
898 UI 0 0 0 0 0 0 0 0 0 0
*

899 KK DIVG21 DIVERT
900 KM
901 DT RETG21 17.3 0.0
902 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
903 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

904 KK G21T22 ROUTE
905 KM
906 RS 1 FLOW
907 RC 0.032 0.008 0.032 1500 0.0020 3.00
908 RX 0.00 2.00 4.00 6.00 60.00 62.00 64.00 66.00
909 RY 3.00 2.50 2.00 1.00 1.00 2.00 2.50 3.00
*

910 KK GM22 BASIN
911 KM
912 BA 0.095
913 LG 0.10 0.15 8.80 0.08 79
914 UI 0 67 197 280 134 40 11 0 0 0
915 UI 0 0 0 0 0 0 0 0 0 0
916 UI 0 0 0 0 0 0 0 0 0 0
917 UI 0 0 0 0 0 0 0 0 0 0
918 UI 0 0 0 0 0 0 0 0 0 0
*

919 KK DIVG22 DIVERT
920 KM
921 DT RETG22 8.0 0.0
922 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
923 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

924 KK CPG22A COMBINE
925 KM
926 HC 2
*

927 KK GM16 BASIN
928 KM

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```

929 BA 0.069
930 LG 0.26 0.25 4.50 0.48 44
931 UI 0 10 38 59 84 119 84 59 38 17
932 UI 12 5 3 3 0 0 0 0 0 0
933 UI 0 0 0 0 0 0 0 0 0 0
934 UI 0 0 0 0 0 0 0 0 0 0
935 UI 0 0 0 0 0 0 0 0 0 0
*

1 HEC-1 INPUT PAGE 24
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
936 KK DIVG16 DIVERT
937 KM
938 DT RETG16 4.9 0.0
939 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
940 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

941 KK G16T19 ROUTE
942 KM
943 RS 2 FLOW
944 RC 0.032 0.016 0.032 1200 0.0020 3.00
945 RX 0.00 2.00 4.00 6.00 60.00 62.00 64.00 66.00
946 RY 3.00 2.50 2.00 1.00 1.00 2.00 2.50 3.00
*

947 KK GM18 BASIN
948 KM
949 BA 0.173
950 LG 0.25 0.25 5.30 0.29 44
951 UI 0 39 137 209 346 262 172 87 44 21
952 UI 9 9 0 0 0 0 0 0 0 0
953 UI 0 0 0 0 0 0 0 0 0 0
954 UI 0 0 0 0 0 0 0 0 0 0
955 UI 0 0 0 0 0 0 0 0 0 0
*

956 KK DIVG18 DIVERT
957 KM
958 DT RETG18 12.4 0.0
959 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
960 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

961 KK CPG18 COMBINE
962 KM
963 HC 2
*

964 KK GM19 BASIN
965 KM
966 BA 0.085
967 LG 0.17 0.15 7.60 0.14 22
968 UI 0 52 152 246 137 48 15 7 0 0
969 UI 0 0 0 0 0 0 0 0 0 0
970 UI 0 0 0 0 0 0 0 0 0 0
971 UI 0 0 0 0 0 0 0 0 0 0
972 UI 0 0 0 0 0 0 0 0 0 0
*

1 HEC-1 INPUT PAGE 25
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
973 KK DIVG19 DIVERT
974 KM
975 DT RETG19 5.5 0.0
976 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
977 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

978 KK CPG19A COMBINE
979 KM
980 HC 2
*

981 KK GM20 BASIN
982 KM
983 BA 0.183
984 LG 0.25 0.15 8.80 0.07 44
985 UI 0 72 224 413 362 209 80 33 13 0
986 UI 0 0 0 0 0 0 0 0 0 0
987 UI 0 0 0 0 0 0 0 0 0 0
988 UI 0 0 0 0 0 0 0 0 0 0
989 UI 0 0 0 0 0 0 0 0 0 0
*

990 KK DIVG20 DIVERT
991 KM
992 DT RETG20 14.5 0.0
993 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
994 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

995 KK CPG19B COMBINE
996 KM
997 HC 2
*

998 KK CPG22B COMBINE
999 KM

```

1000 KM Modified to combining 3 hydrographs instead of 2 due to adding CPG19B
 1001 KM by Parsons Corporation 2015-02
 1002 HC 3
 *

1003 KK G22E26 ROUTE
 1004 KM
 1005 RS 2 FLOW
 1006 RC 0.040 0.030 0.040 2939 0.0031 8.00
 1007 RX 0.00 500.00 800.00 805.00 820.00 825.00 1125.00 1625.00
 1008 RY 8.00 7.00 6.00 1.00 1.00 6.00 7.00 8.00
 *

1009 KM

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1010 KK DRE4NRETRIEVE
 1011 KM
 1012 DR DRE4N
 *

1013 KK RTE3E4 ROUTE
 1014 KM
 1015 KM Revised by using routing for undeveloped conditions
 1016 KM by Parsons Corporation 2015-11
 1017 RS 2 FLOW
 1018 RC 0.035 0.030 0.025 2000 0.0035 6.00
 1019 RX 0.00 100.00 700.00 1050.00 1090.00 1110.00 1140.00 1240.00
 1020 RY 0.00 6.00 4.00 1.00 1.00 5.00 6.00 6.00
 *

1021 KK E4N BASIN
 1022 KM
 1023 KM Used the unit hydrograph for undeveloped conditions
 1024 KM by Parsons Corporation 2015-11
 1025 BA 0.307
 1026 LG 0.35 0.35 3.95 0.47 0 63 80 93 104 118 135
 1027 UI 0 18 18 30 63 80 93 104 118 135
 1028 UI 163 213 219 179 155 138 119 105 90 77
 1029 UI 57 37 31 29 23 18 18 7 5 5
 1030 UI 5 5 5 5 5 0 0 0 0 0
 1031 UI 0 0 0 0 0 0 0 0 0 0
 *

1032 KM KKDIVE4N DIVERT
 1033 KM
 1034 KM Revised by removing the retention to account for undeveloped conditions
 1035 KM by Parsons Corporation 2015-11
 *DTRETE4N 23.4 0.0
 *DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
 *DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
 *

1036 KK CPE4N COMBINE
 1037 KM
 1038 HC 2 4.21
 *

1039 KK DE4NS DIVERT
 1040 KM
 1041 DT DRE4 0.0 0.0
 1042 DI 0.0 34.0 255.0 502.0 772.0 1056.0 1348.0 0.0 0.0 0.0
 1043 DQ 0.0 11.0 171.0 378.0 614.0 868.0 1133.0 0.0 0.0 0.0
 *

1044 KK E4NE13 ROUTE
 1045 KM
 1046 KM Revised by using routing for undeveloped conditions
 1047 KM by Parsons Corporation 2015-11
 1048 RS 23 FLOW
 1049 RC 0.055 0.045 0.055 6955 0.0046 5.50
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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1050 RX 0.00 500.00 980.00 1003.00 1010.00 1050.00 1511.00 2011.00
 1051 RY 3.00 2.50 2.00 1.00 1.00 2.00 2.50 3.00
 *

1052 KK E13 BASIN
 1053 KM
 1054 BA 0.477
 1055 LG 0.35 0.36 5.00 0.27 0 127 147 165 188 215
 1056 UI 0 28 28 50 100 127 147 165 188 215
 1057 UI 264 345 334 274 239 213 183 160 138 116
 1058 UI 83 50 48 46 31 28 24 9 9 9
 1059 UI 9 9 9 9 9 0 0 0 0 0
 1060 UI 0 0 0 0 0 0 0 0 0 0
 *

1061 KM KKDIVE13 DIVERT
 1062 KM
 1063 KM Revised by removing the retention to account for undeveloped conditions
 1064 KM by Parsons Corporation 2015-11
 1065 KM DTRETE13 38.8 0.0
 1066 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 1067 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 *

1068 KK CPE13 COMBINE
 1069 KM
 1070 HC 2
 *

1071 KK E13E24 ROUTE
 1072 KM
 1073 RS 8 FLOW
 1074 RC 0.035 0.030 0.035 5921 0.0042 6.00
 1075 RX 980.00 990.00 995.00 1003.00 1007.00 1015.00 1520.00 1530.00
 1076 RY 4.00 3.50 3.00 1.00 1.00 3.00 3.50 4.00
 *

1077 KM
 1078 KK DRE4RETRIEVE
 1079 KM
 1080 DR DRE4
 *

1081 KK RTE4E4 ROUTE
 1082 KM
 1083 KM Revised by using routing for undeveloped conditions
 1084 KM by Parsons Corporation 2015-11
 1085 RS 10 FLOW
 1086 RC 0.035 0.030 0.025 9400 0.0035 6.00
 1087 RX 0.00 100.00 700.00 1050.00 1090.00 1110.00 1140.00 1240.00
 1088 RY 0.00 6.00 4.00 1.00 1.00 5.00 6.00 6.00
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1089 KK E4 BASIN
 1090 KM
 1091 KM Used the unit hydrograph for undeveloped conditions
 1092 KM by Parsons Corporation 2015-11
 1093 BA 1.200
 1094 LG 0.35 0.35 4.15 0.43 0 71 162 189 228 249 271
 1095 UI 0 49 49 49 71 162 189 228 249 271
 1096 UI 294 322 357 388 453 550 639 582 506 452
 1097 UI 414 384 345 312 287 254 233 202 159 125
 1098 UI 86 86 80 80 54 49 48 15 15
 1099 UI 15 15 15 15 15 15 15 15 15 15
 1100 UI 0 0 0 0 0 0 0 0 0 0
 *

1101 KM KK DIVE4 DIVERT
 1102 KM
 1103 KM Revised by removing the retention to account for undeveloped conditions
 1104 KM by Parsons Corporation 2015-11
 *DT RETE4 92.6 0.0
 *DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
 *DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
 *

1105 KK CPE4 COMBINE
 1106 KM
 1107 HC 2 5.41
 *

1108 KK DE4S DIVERT
 1109 KM
 1110 DT DRE5 0.0 0.0
 1111 DI 0.0 97.0 343.0 637.0 959.0 1299.0 1650.0 0.0 0.0 0.0
 1112 DQ 0.0 89.0 330.0 622.0 943.0 1283.0 1633.0 0.0 0.0 0.0
 *

1113 KK E4E14A ROUTE
 1114 KM
 1115 KM Revised by using routing for undeveloped conditions (E4E14N) from
 1116 KM existing condition (pre-SR 24) model
 1117 KM by Parsons Corporation 2015-11
 1118 RS 12 FLOW
 1119 RC 0.060 0.050 0.060 6921 0.0049 5.50
 1120 RX 0.00 500.00 980.00 1003.00 1007.00 1031.00 1511.00 2011.00
 1121 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

1122 KK E14A BASIN
 1123 KM
 1124 KM Used the unit hydrograph for undeveloped conditions for Basin E14N from
 1125 KM existing condition model (pre-SR 24)
 1126 KM by Parsons Corporation 2015-11
 1127 BA 0.481
 1128 LG 0.35 0.35 4.10 0.44 0 112 129 150 185
 1129 UI 0 20 20 47 78 97 112 129 150 185
 1130 UI 247 226 185 161 139 119 101 84 59 35
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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1131 UI 33 30 20 20 8 6 6 6 6 6
 1132 UI 6 0 0 0 0 0 0 0 0 0
 1133 UI 0 0 0 0 0 0 0 0 0 0
 *

1134 KM KKDIV14A DIVERT
 1135 KM
 1136 KM Revised by removing the retention to account for undeveloped conditions
 1137 KM by Parsons Corporation 2015-11
 1138 KM DTRET14A 38.6 0.0
 1139 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 1140 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 *

1141 KM KK E6A BASIN
 1142 KM
 1143 KM Revised to replace subbasins E6A and E6B with subbasin E6 under existing
 1144 KM (pre-development) conditions as SR 24 does not continue beyond Ironwood Dr.

1145 KM by Parsons Corporation 2015-11
1146 KM BA 0.581
1147 KM LG 0.16 0.25 5.70 0.27 59
1148 KM UI 0 46 46 46 77 155 183 217 238 2
1149 KM UI 282 311 346 381 455 556 598 511 450 4
1150 KM UI 374 343 305 278 251 226 201 161 130
1151 KM UI 81 76 76 55 46 46 46 14 14
1152 KM UI 14 14 14 14 14 14 14 14 14
*

1153 KM KKDIVE6A DIVERT
1154 KM
1155 KM Revised by removing the retention to account for undeveloped conditions
1156 KM by Parsons Corporation 2015-11
1157 KM DTRETE6A 53.1 0.0
1158 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
1159 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
*

1160 KM KKE6AE5A ROUTE
1161 KM
1162 KM Revised by removing the route to account for undeveloped conditions as SR 2
1163 KM does not continue beyond Ironwood Dr.
1164 KM by Parsons Corporation 2015-11
1165 KM RS 6 FLOW
1166 KM RC 0.020 0.020 0.020 7264 0.0010 100.00
1167 KM RX 0.00 1.00 2.00 20.00 30.00 48.00 49.00 50.00
1168 KM RY100.00 99.00 99.00 90.00 90.00 99.00 99.00 100.00
*

1169 KK DRE5RETRIEVE
1170 KM
1171 DR DRE5
*

1172 KK RTE4E5 ROUTE
1173 KM
1174 KM Revised by using routing for undeveloped conditions as SR24 does not extend
1175 KM beyond Ironwood Dr.
1176 KM by Parsons Corporation 2015-11
1177 RS 3 FLOW

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1178 RC 0.035 0.030 0.025 3700 0.0035 6.00
1179 RX 0.00 100.00 700.00 1050.00 1090.00 1110.00 1140.00 1240.00
1180 RY 0.00 6.00 4.00 1.00 1.00 5.00 6.00 6.00
*

1181 KK E5 BASIN
1182 KM
1183 KM Used the footprint, unit hydrograph and LG for undeveloped conditions
1184 KM by Parsons Corporation 2015-11
1185 BA 1.426
1186 LG 0.35 0.35 3.95 0.47 0
1187 UI 0 59 59 59 89 195 229 274 300 328
1188 UI 354 389 432 471 555 670 773 682 595 535
1189 UI 489 453 407 366 336 298 275 232 177 134
1190 UI 104 101 96 92 59 59 59 45 18 18
1191 UI 18 18 18 18 18 18 18 18 18 0
*

1192 KM KKDIVE5A DIVERT
1193 KM
1194 KM Revised by removing the retention to account for undeveloped conditions
1195 KM by Parsons Corporation 2015-11
*DTRETE5A 89.1 0.0
*DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
*DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
*

1196 KK CPE5 COMBINE
1197 KM
1198 KM Used the hydrograph combine from existing condition model as SR24 does not
1199 KM extend beyond Ironwood Dr.
1200 KM by Parsons Corporation 2015-11
1201 HC 2 6.84
*

1202 KM KKCPESA2 COMBINE
1203 KM
1204 KM Revised by replacing CPE5A2 combine with DE55 diversion
1205 KM by Parsons Corporation 2015-11
1206 KM HC 2
*

1207 KK DE55 DIVERT
1208 KM Revised by replacing CPE5A2 combine with DE55 diversion
1209 KM by Parsons Corporation 2015-11
1210 DT DRE6 0.0 0.0
1211 DI 0.0 212.0 527.0 921.0 1342.0 1783.0 2234.0 0.0 0.0 0.0
1212 DQ 0.0 1.0 206.0 431.0 723.0 1076.0 1460.0 0.0 0.0 0.0
*

1213 KK E5A14A ROUTE
1214 KM
1215 KM Revised for channel length/time steps and cross section between
1216 KM Ironwood Dr. and Meridian Rd. to account for concrete-lined channel.
1217 KM by Parsons Corporation 2015-12
1218 RS 4 FLOW

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1219 RC 0.016 0.016 0.016 6121 0.0017 97.00

1220 RX 0.00 7.50 15.00 29.00 41.00 55.00 62.50 70.00
1221 RY 97.45 97.23 97.00 90.00 90.00 97.00 97.23 97.45
*

1222 KK CPE14A COMBINE
1223 KM ***** PARSONS 10/30/2015 *****
1224 KO 1
1225 HC 3 7.61
*

1226 KK E1424A ROUTE
1227 KM
1228 KM Revised for channel length and time steps between Mountain Rd
1229 KM and Meridian Rd to account for concrete lining.
1230 KM by Parsons Corporation 2016-03
1231 RS 2 FLOW
1232 RC 0.016 0.016 0.016 2808 0.0017 97.00
1233 RX 0.00 7.50 15.00 29.00 41.00 55.00 62.50 70.00
1234 RY 97.45 97.23 97.00 90.00 90.00 97.00 97.23 97.45
*

1235 KK E1424B ROUTE
1236 KM
1237 KM Introduced for channel length and time steps between
1238 KM Signal Bute Rd. and Mountain Rd. to account for concrete lining.
1239 KM by Parsons Corporation 2015-12
1240 RS 2 FLOW
1241 RC 0.016 0.016 0.016 2461 0.0017 97.00
1242 RX 0.00 7.50 15.00 29.00 41.00 55.00 62.50 70.00
1243 RY 97.45 97.23 97.00 90.00 90.00 97.00 97.23 97.45
*

1244 KK E24A BASIN
1245 KM
1246 BA 0.528
1247 LG 0.14 0.25 6.00 0.24 59
1248 UI 0 81 324 487 736 911 620 431 224 126
1249 UI 72 25 25 25 0 0 0 0 0 0
1250 UI 0 0 0 0 0 0 0 0 0 0
1251 UI 0 0 0 0 0 0 0 0 0 0
1252 UI 0 0 0 0 0 0 0 0 0 0
*

1253 KK DIV24A DIVERT
1254 KM
1255 DT RET24A 39.6 0.0
1256 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1257 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1258 KK CP24A COMBINE
1259 KM
1260 HC 3 8.62
*

1261 KK E247A1 ROUTE
1262 KM
1263 KM Revised for channel length/routing steps and cross section between
1264 KM Signal Butte Rd. and Crismon Rd. to account for concrete lining.
1265 KM by Parsons Corporation 2015-12
1266 RS 4 FLOW
1267 RC 0.016 0.016 0.016 5594 0.0017 97.50
1268 RX 0.00 7.50 15.00 30.00 42.00 57.00 64.50 72.00
1269 RY 97.95 97.73 97.50 90.00 90.00 97.50 97.73 97.95
*

1270 KK E27A BASIN
1271 KM
1272 BA 0.544
1273 LG 0.20 0.15 7.00 0.15 54
1274 UI 0 50 84 198 261 316 393 565 570 439
1275 UI 360 288 227 143 86 75 50 32 15 15
1276 UI 15 15 15 0 0 0 0 0 0 0
1277 UI 0 0 0 0 0 0 0 0 0 0
1278 UI 0 0 0 0 0 0 0 0 0 0
*

1279 KK DIV27A DIVERT
1280 KM
1281 DT RET27A 42.0 0.0
1282 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1283 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

1284 KK CPE27A COMBINE
1285 KM
1286 KM Confluence of channel south of Eastmark/southeast of PPG North and portion
1287 KM of PPG with SR 24 offsite channel.
1288 KM by Parsons Corporation 2015-11
1289 HC 3 12.81
*

1290 KK E247A2 ROUTE
1291 KM
1292 KM Revised for channel length/routing steps and cross section between
1293 KM Signal Butte Rd. and Crismon Rd. to account for concrete lining.
1294 KM by Parsons Corporation 2015-12
1295 RS 1 FLOW
1296 RC 0.016 0.016 0.016 1528 0.0017 97.50

1297 RX 0.00 7.50 15.00 30.00 42.00 57.00 64.50 72.00
1298 RY 97.95 97.73 97.50 90.00 90.00 97.50 97.73 97.95
*

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1299 KK E2726A ROUTE
1300 KO 1
1301 KM
1302 KM Revised for channel length/routing steps and cross section between
1303 Signal Butte Rd. and Crismon Rd. to account for concrete lining.
1304 KM by Parsons Corporation 2015-12
1305 RS 4 FLOW
1306 RC 0.016 0.016 0.016 6350 0.0016 97.50
1307 RX 0.00 7.50 15.00 30.00 42.00 57.00 64.50 72.00
1308 RY 97.95 97.73 97.50 90.00 90.00 97.50 97.73 97.95
*

1309 KK E26A BASIN
1310 KM
1311 BA 0.865
1312 LG 0.22 0.15 7.30 0.14 52
1313 UI 0 86 172 370 479 596 804 1055 818 656
1314 UI 516 400 244 148 119 86 36 26 26 26
1315 UI 26 0 0 0 0 0 0 0 0 0
1316 UI 0 0 0 0 0 0 0 0 0 0
1317 UI 0 0 0 0 0 0 0 0 0 0
*

1318 KK DIV26A DIVERT
1319 KM
1320 DT RET26A 66.0 0.0
1321 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1322 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

1323 KK SR24EL COMBINE
1324 KO 1
1325 KM
1326 KM Combine hydrographs from E2726A and RET26A prior to routing through.
1327 KM SR 24 offline detention basin at Ellsworth Rd. and Powerline Floodway
1328 KM by Parsons Corporation 2015-11
1329 HC 2 13.68
*

1330 KM KKELSRC1 DIVERT
1331 KM KO 1
1332 KM
1333 KM Diversion to SR 24 ramp C offline detention basin at Ellsworth Rd.
1334 KM Basin capacity estimated at 10 ac-ft. Diversion for 80% as effective volume
1335 KM (8 ac-ft as 0.8*10 ac-ft).
1336 KM by Parsons Corporation 2016-03
1337 KM
1338 KM Diversion deactivated as not needed with the SR-24 alignment extending to
1339 KM Ironwood Drive
1340 KM by Parsons Corporation 2016-07
1341 KM DTRC1DIV 8.0 0.0
1342 KM DI 0.0 1650.0 5000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1343 KM DQ 0.0 0.0 3350.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1344 KK 802ELS DIVERT
1345 KO 1
1346 KM
1347 KM Diversion to SR 24 offline detention basin at Ellsworth Rd. and Powerline
1348 KM Floodway. Basin capacity estimated at 100 ac-ft. Diversion modified to
1349 KM include finite detention volume (80 ac-ft as 0.8*100 ac-ft).
1350 KM by Parsons Corporation 2016-07
1351 KM
1352 DT 1650UP 100.0 0.0
1353 DI 0.0 1650.0 5000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1354 DQ 0.0 0.0 3350.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

1355 KM KKG19E26 ROUTE
1356 KM
1357 KM Revised by removing the Routing to Powerline Floodway as result of
1358 KM the Eastmark Development
1359 KM by Parsons Corporation 2016-11
1360 KM RS 4 FLOW
1361 KM RC 0.020 0.020 0.020 9348 0.0038 100.00
1362 KM RX 0.00 1.00 2.00 20.00 45.00 63.00 64.00 65.00
1363 KM RY100.00 99.00 99.00 90.00 90.00 99.00 99.00 100.00
*

1364 KK GM17 BASIN
1365 KO 1
1366 KM
1367 KM Part of Eastmark
1368 KM by Parsons Corporation 2015-11
1369 BA 0.104
1370 LG 0.25 0.25 4.10 0.55 45
1371 UI 0 42 129 238 205 117 44 18 7 0
1372 UI 0 0 0 0 0 0 0 0 0 0
1373 UI 0 0 0 0 0 0 0 0 0 0
1374 UI 0 0 0 0 0 0 0 0 0 0
1375 UI 0 0 0 0 0 0 0 0 0 0
*

1376 KK DIVG17 DIVERT
1377 KM
1378 KM Revised by retaining the entire volume from GM17,
1379 KM per Master Drainage Report Update for Eastmark (Wood-Patel, Rev. 10-24-14)
1380 KM by Parsons Corporation 2015-11
1381 DT RETG17 0.0 0.0
1382 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1383 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

1384 KK G17E26 ROUTE
1385 KM
1386 RS 4 FLOW
1387 RC 0.020 0.020 0.020 3933 0.0063 100.00
1388 RX 0.00 1.00 2.00 20.00 45.00 63.00 64.00 65.00
1389 RY 100.00 99.00 99.00 90.00 90.00 99.00 99.00 100.00
*

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1390 KK CPE26A COMBINE
1391 KO 1
1392 KM
1393 KM Modified to combining 4 hydrographs instead of 5
1394 KM by Parsons Corporation 2015-11
1395 KM Modified to combining 3 hydrographs instead of 4 due to removing G19E26
1396 KM by Parsons Corporation 2015-02
1397 HC 3
*

1398 KK 80233B ROUTE
1399 KM
1400 KM
1401 KM
1402 KM
1403 KM
1404 RS 1 FLOW
1405 RC 0.025 0.029 0.025 4205 0.0045 9.00
1406 RX 0.00 13.00 15.30 25.00 33.00 42.70 45.00 58.00
1407 RY 9.00 9.00 7.50 1.00 1.00 7.50 9.00 9.00
*

1408 KK E7 BASIN
1409 KM
1410 BA 1.124
1411 LG 0.24 0.26 5.10 0.32 35
1412 UI 0 64 64 102 224 281 328 369 416 477
1413 UI 561 725 814 670 575 512 449 390 339 300
1414 UI 226 159 113 106 99 64 64 46 20 20
1415 UI 20 20 20 20 20 20 0 0 0 0
1416 UI 0 0 0 0 0 0 0 0 0 0
*

1417 KK DIVE7 DIVERT
1418 KM
1419 DT RETE7 85.5 0.0
1420 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1421 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

1422 KK E7STOR STORAGE
1423 KM
1424 KO
1425 RS 1 STOR
1426 SV 22.82 34.23 45.64 78.34 111.03 143.72 176.42 230.23 284.04
1427 SQ 1.75 5.50 11.00 17.70 25.70 34.20 43.00 51.70
1428 SE 1566.0 1567.00 1567.50 1568.00 1568.50 1569.00 1569.50 1570.00 1570.50 1571.00
1429 ST 1574.0 10000.0 3.0 1.5
*

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1430 KK E7E6 ROUTE
1431 KM
1432 KM
1433 KM
1434 RS 23 FLOW
1435 RC 0.035 0.030 0.030 16362 0.0062 5.50
1436 RX 0.00 500.00 980.00 1003.00 1007.00 1031.00 1511.00 2011.00
1437 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
*

1438 KK DRE6RETRIEVE
1439 KM
1440 KM Revised to retrieve diversion to south along Ironwood Dr. when SR 24 does
1441 KM not extend beyond Ironwood Dr. This diversion is identical with that in
1442 KM the existing condition model (24EX100).
1443 KM by Parsons Corporation 2015-11
1444 DR DRE6
*

1445 KK RTE5E6 ROUTE
1446 KM
1447 KM Revised to route diversion to south along Ironwood Dr. when SR 24 does
1448 KM not extend beyond Ironwood Dr. This route is identical with that in
1449 KM the existing condition model (24EX100).
1450 RS 5 FLOW
1451 RC 0.035 0.030 0.025 3700 0.0035 6.00
1452 RX 0.00 100.00 700.00 1050.00 1090.00 1110.00 1140.00 1240.00

1596 UI 0 0 0 0 0 0 0 0 0 0 0
 1597 UI 0 0 0 0 0 0 0 0 0 0 0
 *

1598 KK DIVE5B DIVERT
 1599 KM
 1600 DT RETE5B 25.0 0.0
 1601 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1602 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1603 KK E5E14B ROUTE
 1604 KM
 1605 RS 5 FLOW
 1606 RC 0.035 0.030 0.035 6256 0.0054 5.50
 1607 RX 950.00 985.00 991.00 1003.00 1007.00 1019.00 1025.00 1050.00
 1608 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

1609 KK E14B BASIN
 1610 KM
 1611 BA 0.528
 1612 LG 0.14 0.25 5.60 0.29 60
 1613 UI 0 125 435 667 1086 785 512 237 126 53
 1614 UI 29 29 0 0 0 0 0 0 0 0
 1615 UI 0 0 0 0 0 0 0 0 0 0
 1616 UI 0 0 0 0 0 0 0 0 0 0
 1617 UI 0 0 0 0 0 0 0 0 0 0
 *

1618 KK DIV14B DIVERT
 1619 KM
 1620 DT RET14B 48.4 0.0
 1621 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1622 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1623 KK CP14B COMBINE
 1624 KM
 1625 HC 2
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1626 KK E14E24 ROUTE
 1627 KM
 1628 RS 5 FLOW
 1629 RC 0.030 0.030 0.030 6080 0.0032 9.00
 1630 RX 970.00 990.00 1001.00 1010.00 1014.00 1023.00 1034.00 1054.00
 1631 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

1632 KK E24B BASIN
 1633 KM
 1634 BA 0.464
 1635 LG 0.15 0.15 7.30 0.14 57
 1636 UI 0 92 339 513 852 731 493 294 133 76
 1637 UI 24 24 0 0 0 0 0 0 0 0
 1638 UI 0 0 0 0 0 0 0 0 0 0
 1639 UI 0 0 0 0 0 0 0 0 0 0
 1640 UI 0 0 0 0 0 0 0 0 0 0
 *

1641 KK DIV24B DIVERT
 1642 KM
 1643 DT RET24B 38.7 0.0
 1644 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1645 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1646 KK CPE24B COMBINE
 1647 KM
 1648 HC 3
 *

1649 KK E24E28 ROUTE
 1650 KM
 1651 RS 4 FLOW
 1652 RC 0.035 0.035 0.035 6172 0.0036 10.00
 1653 RX 940.00 960.00 980.00 1000.00 1010.00 1030.00 1050.00 1070.00
 1654 RY 7.00 6.00 5.00 1.00 1.00 5.00 6.00 7.00
 *

1655 KK E28B BASIN
 1656 KM
 1657 BA 0.539
 1658 LG 0.20 0.15 8.40 0.09 51
 1659 UI 0 65 183 329 427 606 772 566 430 318
 1660 UI 179 110 73 41 20 20 0 0 0 0
 1661 UI 0 0 0 0 0 0 0 0 0 0
 1662 UI 0 0 0 0 0 0 0 0 0 0
 1663 UI 0 0 0 0 0 0 0 0 0 0
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1664 KK DIV28B DIVERT
 1665 KM
 1666 DT RET28B 42.0 0.0

1667 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1668 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1669 KK CPE28B COMBINE
 1670 KM
 1671 HC 2
 *

1672 KK E28E31 ROUTE
 1673 KM
 1674 RS 3 FLOW
 1675 RC 0.040 0.040 0.040 5081 0.0036 10.00
 1676 RX 950.00 975.00 985.00 1005.00 1010.00 1030.00 1040.00 1065.00
 1677 RY 7.00 6.50 6.00 1.00 1.00 6.00 6.50 7.00
 *

1678 KK E25 BASIN
 1679 KM
 1680 BA 0.932
 1681 LG 0.15 0.25 5.40 0.30 55
 1682 UI 0 86 146 342 451 546 683 986 969 749
 1683 UI 613 490 383 234 148 125 86 51 26 26
 1684 UI 26 26 0 0 0 0 0 0 0 0
 1685 UI 0 0 0 0 0 0 0 0 0 0
 1686 UI 0 0 0 0 0 0 0 0 0 0
 *

1687 KK DIVE25 DIVERT
 1688 KM
 1689 DT RETE25 110.7 0.0
 1690 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1691 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1692 KK E25E29 ROUTE
 1693 KM
 1694 RS 20 FLOW
 1695 RC 0.030 0.030 0.030 7016 0.0022 2.50
 1696 RX 976.00 996.00 1003.00 1005.00 1006.00 1008.00 1015.00 1025.00
 1697 RY 2.50 2.00 1.50 1.00 1.00 1.50 2.00 2.50
 *

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1698 KK E29 BASIN
 1699 KM
 1700 BA 1.002
 1701 LG 0.15 0.23 6.20 0.22 55
 1702 UI 0 103 218 452 586 733 1019 1240 924 737
 1703 UI 574 428 229 172 116 82 31 31 31 31
 1704 UI 0 0 0 0 0 0 0 0 0 0
 1705 UI 0 0 0 0 0 0 0 0 0 0
 *

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1706 UI 0 0 0 0 0 0 0 0 0 0
 *

1707 KK DIVE29 DIVERT
 1708 KM
 1709 DT RETE29 73.9 0.0
 1710 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1711 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1712 KK CPE29 COMBINE
 1713 KM
 1714 HC 2
 *

1715 KK E29E31 ROUTE
 1716 KM
 1717 RS 4 FLOW
 1718 RC 0.030 0.030 0.030 7025 0.0034 10.00
 1719 RX 950.00 975.00 985.00 1005.00 1006.00 1026.00 1036.00 1070.00
 1720 RY 8.00 7.00 6.00 1.00 1.00 6.00 7.00 8.00
 *

1721 KK E32 BASIN
 1722 KM
 1723 BA 0.246
 1724 LG 0.14 0.25 4.25 0.55 58
 1725 UI 0 72 238 387 535 337 190 78 37 15
 1726 UI 15 0 0 0 0 0 0 0 0 0
 1727 UI 0 0 0 0 0 0 0 0 0 0
 1728 UI 0 0 0 0 0 0 0 0 0 0
 1729 UI 0 0 0 0 0 0 0 0 0 0
 *

1730 KK DIVE32 DIVERT
 1731 KM
 1732 DT RETE32 17.2 0.0
 1733 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1734 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1735 KK E32E31 ROUTE
 1736 KM
 1737 RS 5 FLOW
 1738 RC 0.025 0.060 0.025 3272 0.0028 1388.60
 1739 RX 100.00 110.00 128.00 149.80 160.00 191.50 209.20 210.00
 1740 RY 1388.3 1388.32 1388.32 1380.37 1380.17 1388.04 1388.39 1388.60
 *

1741 KK E31 BASIN
 1742 KM
 1743 BA 0.810
 1744 LG 0.15 0.25 4.80 0.39 55
 1745 UI 0 86 197 391 504 641 943 970 728 571
 1746 UI 441 296 151 126 86 37 26 26 26 0

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
 1747 UI 0 0 0 0 0 0 0 0 0 0
 1748 UI 0 0 0 0 0 0 0 0 0 0
 1749 UI 0 0 0 0 0 0 0 0 0 0
 *

1750 KK DIVE31 DIVERT
 1751 KM
 1752 DT RETE31 56.5 0.0
 1753 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1754 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1755 KK CPE31 COMBINE
 1756 KM
 1757 HC 4
 *

1758 KK E31E30 ROUTE
 1759 KM
 1760 RS 5 FLOW
 1761 RC 0.025 0.045 0.025 4404 0.0008 1387.00
 1762 RX 100.00 107.00 112.50 144.90 175.10 201.50 225.90 244.00
 1763 RY 1386.1 1386.09 1386.09 1377.99 1377.99 1384.59 1385.08 1387.00
 *

1764 KK E30B BASIN
 1765 KM
 1766 BA 0.882
 1767 LG 0.24 0.15 8.40 0.09 47
 1768 UI 0 56 56 128 217 272 314 357 416 500
 1769 UI 668 683 552 475 416 355 303 261 191 124
 1770 UI 98 92 66 56 44 17 17 17 17 17
 1771 UI 17 17 0 0 0 0 0 0 0 0
 1772 UI 0 0 0 0 0 0 0 0 0 0
 *

1773 KK DIV30B DIVERT
 1774 KM
 1775 DT RET30B 67.1 0.0
 1776 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1777 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1778 KK CPE30 COMBINE
 1779 KM
 1780 HC 2
 *

1781 KK E30E26 ROUTE
 1782 KM
 1783 RS 1 FLOW
 1784 RC 0.025 0.035 0.025 822 0.0005 1387.00
 1785 RX 100.00 105.00 108.50 149.90 220.10 251.30 279.10 285.10
 1786 RY 1387.0 1387.00 1386.66 1376.31 1376.31 1384.11 1384.66 1386.00
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1787 KK E26B BASIN
 1788 KM
 1789 BA 0.259
 1790 LG 0.24 0.15 8.80 0.07 48
 1791 UI 0 38 145 222 320 448 315 222 139 65
 1792 UI 43 18 12 12 0 0 0 0 0 0
 1793 UI 0 0 0 0 0 0 0 0 0 0
 1794 UI 0 0 0 0 0 0 0 0 0 0
 1795 UI 0 0 0 0 0 0 0 0 0 0
 *

1796 KK DIV26B DIVERT
 1797 KM
 1798 DT RET26B 20.1 0.0
 1799 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1800 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1801 KK CPE26 COMBINE
 1802 KM
 1803 HC 2
 *

1804 KK E26E33 ROUTE
 1805 KM
 1806 RS 5 FLOW
 1807 RC 0.025 0.030 0.025 8929 0.0028 1379.67
 1808 RX 100.00 100.50 102.50 134.90 205.10 237.50 253.50 255.00
 1809 RY 1379.1 1379.12 1379.35 1371.25 1371.25 1379.35 1379.67 1379.67
 *

1810 KK E33B BASIN

1811 KM
 1812 BA 0.851
 1813 LG 0.15 0.15 7.30 0.14 56
 1814 UI 0 117 409 651 892 1385 1087 793 558 278
 1815 UI 179 110 36 36 0 0 0 0 0
 1816 UI 0 0 0 0 0 0 0 0 0
 1817 UI 0 0 0 0 0 0 0 0 0
 1818 UI 0 0 0 0 0 0 0 0 0
 *

1819 KK DIV33B DIVERT
 1820 KM
 1821 DT RET33B 66.8 0.0
 1822 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1823 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1824 KK CPE33B COMBINE
 1825 KM
 1826 HC 3
 *

1827 KK E33P9A ROUTE
 1828 KM
 1829 RS 1 FLOW
 1830 RC 0.025 0.060 0.025 2115 0.0039 8.00
 1831 RX 0.00 18.00 21.00 33.00 93.00 105.00 108.00 129.00
 1832 RY 8.00 8.00 6.50 0.50 0.50 6.50 8.00 8.00
 *

1833 KK E33P9B ROUTE
 1834 KM
 1835 RS 1 FLOW
 1836 RC 0.025 0.060 0.025 2299 0.0029 8.20
 1837 RX 0.00 18.00 21.00 33.00 93.00 105.00 108.00 129.00
 1838 RY 8.20 8.00 6.50 0.50 0.50 6.50 8.00 8.20
 *

1839 KK P9 BASIN
 1840 KM
 1841 BA 1.122
 1842 LG 0.11 0.15 8.00 0.12 74
 1843 UI 0 119 271 539 695 881 1292 1349 1011 795
 1844 UI 612 416 214 177 119 55 36 36 0
 1845 UI 0 0 0 0 0 0 0 0 0
 1846 UI 0 0 0 0 0 0 0 0 0
 1847 UI 0 0 0 0 0 0 0 0 0
 *

1848 KK DIVP9 DIVERT
 1849 KM
 1850 DT RETP9 36.4 0.0
 1851 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1852 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1853 KK CPP9 COMBINE
 1854 KM
 1855 HC 2
 *

1856 KK P9EMF1 ROUTE
 1857 KM
 1858 RS 1 FLOW
 1859 RC 0.025 0.029 0.025 4403 0.0029 8.00
 1860 RX 0.00 18.00 21.00 33.00 93.00 105.00 108.00 129.00
 1861 RY 8.00 8.00 6.50 0.50 0.50 6.50 8.00 8.00
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1862 KK EMF1B BASIN
 1863 KM
 1864 BA 1.036
 1865 LG 0.12 0.14 7.60 0.13 63
 1866 UI 0 117 296 556 717 944 1407 1153 891 677
 1867 UI 493 256 194 117 66 36 36 0 0
 1868 UI 0 0 0 0 0 0 0 0 0
 1869 UI 0 0 0 0 0 0 0 0 0
 1870 UI 0 0 0 0 0 0 0 0 0
 *

1871 KK DEMF1B DIVERT
 1872 KM
 1873 DT REMF1B 85.0 0.0
 1874 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1875 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1876 KK CPEM1 COMBINE
 1877 KM
 1878 HC 2
 *

1879 KK EM1EM2 ROUTE
 1880 KM
 1881 RS 19 FLOW

1882 RC 0.030 0.015 0.030 5153 0.0012 1326.70
 1883 RX 4931.0 4943.00 4952.00 4974.00 5022.00 5047.00 5058.00 5064.00
 1884 RY 1324.0 1323.90 1323.80 1312.60 1312.70 1323.30 1324.30 1326.70
 *

1885 KK EMF2 BASIN
 1886 KM
 1887 BA 1.850
 1888 LG 0.13 0.21 6.40 0.22 62
 1889 UI 0 108 108 195 388 494 572 641 733 839
 1890 UI 1028 1347 1292 1063 927 823 707 618 533 447
 1891 UI 319 191 184 178 116 108 90 33 33 33
 1892 UI 33 33 33 33 33 0 0 0 0 0
 1893 UI 0 0 0 0 0 0 0 0 0 0
 *

1894 KK DIVEM2 DIVERT
 1895 KM
 1896 DT RETEM2 96.9 0.0
 1897 DI 0.0 78.0 79.0 10079.0 0.0 0.0 0.0 0.0 0.0 0.0
 1898 DQ 0.0 0.0 1.0 10001.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1899 KK CPEMF2 COMBINE
 1900 KM
 1901 HC 2
 *

1902 KK EM2M3A ROUTE
 1903 KM
 1904 RS 1 FLOW
 1905 RC 0.030 0.030 0.030 1085 0.0002 1326.40
 1906 RX 4945.0 4946.00 4947.00 4976.00 5027.00 5057.00 5109.00 5120.00
 1907 RY 1324.1 1324.10 1324.10 1311.10 1311.10 1325.20 1325.30 1326.40
 *

1908 KK EM2M3B ROUTE
 1909 KM
 1910 RS 1 FLOW
 1911 RC 0.030 0.020 0.030 972 0.0002 1324.10
 1912 RX 4829.0 4848.00 4879.00 4912.00 5087.00 5120.00 5163.00 5172.00
 1913 RY 1324.1 1322.00 1321.30 1310.50 1309.80 1321.00 1322.70 1324.10
 *

1914 KK EMF3 BASIN
 1915 KM
 1916 BA 1.489
 1917 LG 0.21 0.24 4.80 0.42 52
 1918 UI 0 104 104 298 444 544 625 737 879 1196
 1919 UI 1278 1014 866 740 627 521 421 265 184 171
 1920 UI 124 104 69 32 32 32 32 32 32 0
 1921 UI 0 0 0 0 0 0 0 0 0 0
 1922 UI 0 0 0 0 0 0 0 0 0 0
 *

1923 KK DIVEM3 DIVERT
 1924 KM
 1925 DT RETEM3 59.1 0.0
 1926 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1927 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1928 KK CPEMF3 COMBINE
 1929 KM
 1930 HC 2
 *

1931 KK EMF3RB ROUTE
 1932 KM
 1933 RS 1 FLOW
 1934 RC 0.030 0.025 0.030 939 0.0007 1324.10
 1935 RX 4829.0 4848.00 4879.00 4912.00 5087.00 5120.00 5163.00 5172.00
 1936 RY 1324.1 1322.00 1321.30 1310.50 1309.80 1321.00 1322.70 1324.10
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1937 KK RITBAS BASIN
 1938 KM
 1939 BA 0.294
 1940 LG 0.01 0.02 4.80 0.25 0
 1941 UI 0 1043 1115 112 0 0 0 0 0 0
 1942 UI 0 0 0 0 0 0 0 0 0 0
 1943 UI 0 0 0 0 0 0 0 0 0 0
 1944 UI 0 0 0 0 0 0 0 0 0 0
 1945 UI 0 0 0 0 0 0 0 0 0 0
 *

1946 KK RITBAS STORAGE
 1947 KM
 1948 KO
 1949 RS 1 STOR
 1950 SV 22.00 99.00 213.00 331.00 451.00 571.00 693.00
 1951 SQ 1.00 2.00 3.00 4.00 5.00 6.00 7.00
 1952 SE 1311.0 1312.00 1313.00 1314.00 1315.00 1316.00 1317.00 1318.00
 1953 ST 1318.0 900.0 3.0 1.5
 *

1954 KK CPRITB COMBINE
 1955 KM
 1956 HC 2
 *

1957 KK RBEMF4 ROUTE
 1958 KM
 1959 RS 3 FLOW
 1960 RC 0.030 0.030 0.030 2391 0.0001 1324.10
 1961 RX 4829.0 4848.00 4879.00 4912.00 5087.00 5120.00 5163.00 5172.00
 1962 RY 1324.1 1322.00 1321.30 1310.50 1309.80 1321.00 1322.70 1324.10
 *

1963 KM

1964 KK R2 BASIN
 1965 KM
 1966 BA 0.677
 1967 LG 0.28 0.25 5.80 0.23 22
 1968 UI 0 52 52 176 237 287 335 402 537 651
 1969 UI 517 432 364 303 251 182 109 88 75 52
 1970 UI 42 16 16 16 16 16 16 0 0 0
 1971 UI 0 0 0 0 0 0 0 0 0 0
 1972 UI 0 0 0 0 0 0 0 0 0 0
 *

1973 KK DIVR2 DIVERT
 1974 KM
 1975 DT RETR2 18.5 0.0
 1976 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1977 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1978 KK R3 BASIN
 1979 KM
 1980 BA 0.413
 1981 LG 0.27 0.25 4.65 0.36 19
 1982 UI 0 34 42 122 165 196 235 293 413 372
 1983 UI 298 250 205 167 122 71 57 45 34 20
 1984 UI 10 10 10 10 10 0 0 0 0 0
 1985 UI 0 0 0 0 0 0 0 0 0 0
 1986 UI 0 0 0 0 0 0 0 0 0 0
 *

1987 KK DIVR3 DIVERT
 1988 KM
 1989 DT RETR3 15.6 0.0
 1990 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1991 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1992 KK CPR2R3 COMBINE
 1993 KM
 1994 HC 2
 *

1995 KK R2R3R6 ROUTE
 1996 KM
 1997 RS 18 FLOW
 1998 RC 0.045 0.040 0.045 7280 0.0033 2.50
 1999 RX 0.00 500.00 1000.00 1001.00 1002.00 1500.00 2000.00 2500.00
 2000 RY 2.50 2.00 1.50 1.00 1.00 1.50 2.00 2.50
 *

2001 KK R6 BASIN
 2002 KM
 2003 BA 0.504
 2004 LG 0.30 0.25 4.65 0.39 15
 2005 UI 0 40 46 143 194 231 274 336 472 469
 2006 UI 369 312 255 211 166 99 70 63 40 35
 2007 UI 12 12 12 12 12 12 0 0 0 0
 2008 UI 0 0 0 0 0 0 0 0 0 0
 2009 UI 0 0 0 0 0 0 0 0 0 0
 *

2010 KK CPR6 COMBINE
 2011 KM
 2012 HC 2
 *

2013 KK R6R9 ROUTE
 2014 KM
 2015 RS 4 FLOW
 2016 RC 0.035 0.035 0.035 6687 0.0040 6.00
 2017 RX 961.00 981.00 989.00 1001.00 1005.00 1017.00 1025.00 1045.00
 2018 RY 6.00 5.00 4.00 1.00 1.00 4.00 5.00 6.00
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2019 KK R9 BASIN
 2020 KM
 2021 BA 0.592
 2022 LG 0.16 0.25 4.80 0.40 64
 2023 UI 0 80 269 435 585 924 773 566 409 222
 2024 UI 134 81 34 24 24 0 0 0 0 0
 2025 UI 0 0 0 0 0 0 0 0 0 0
 *

2026 UI 0 0 0 0 0 0 0 0 0 0 0
2027 UI 0 0 0 0 0 0 0 0 0 0 0
*
2028 KK DIVR9 DIVERT
2029 KM
2030 DT RETR9 54.2 0.0
2031 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
2032 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*
2033 KK CPR9 COMBINE
2034 KM
2035 HC 2
*
2036 KK R9R11 ROUTE
2037 KM
2038 RS 7 FLOW
2039 RC 0.035 0.035 0.035 7667 0.0030 6.00
2040 RX 950.00 977.00 989.00 1001.00 1006.00 1018.00 1030.00 1050.00
2041 RY 6.00 5.00 4.00 1.00 1.00 4.00 5.00 6.00
*
2042 KK R11 BASIN
2043 KM
2044 BA 0.986
2045 LG 0.14 0.23 6.20 0.23 45
2046 UI 0 101 213 442 574 717 994 1219 912 728
2047 UI 567 426 229 169 116 84 31 31 31 31
2048 UI 0 0 0 0 0 0 0 0 0 0
2049 UI 0 0 0 0 0 0 0 0 0 0
2050 UI 0 0 0 0 0 0 0 0 0 0
*
2051 KK DIVR11 DIVERT
2052 KM
2053 DT RETR11 67.9 0.0
2054 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
2055 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2056 KK DRRSRETRIEVE
2057 KM
2058 DR DRR5
*
2059 KK R5 BASIN
2060 KM
2061 BA 0.504
2062 LG 0.29 0.25 5.40 0.27 21
2063 UI 0 53 120 241 310 393 574 608 455 358
2064 UI 277 189 98 80 53 26 16 16 16 16
2065 UI 0 0 0 0 0 0 0 0 0 0
2066 UI 0 0 0 0 0 0 0 0 0 0
2067 UI 0 0 0 0 0 0 0 0 0 0
*
2068 KK DIVR5 DIVERT
2069 KM
2070 DT RETR5 1.0 0.0
2071 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
2072 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

2073 KK CPR5 COMBINE
2074 KM
2075 HC 2 1.22
*
2076 KK R5R8 ROUTE
2077 KM
2078 RS 5 FLOW
2079 RC 0.040 0.035 0.040 6587 0.0043 5.00
2080 RX 966.00 986.00 994.00 1006.00 1012.00 1024.00 1032.00 1052.00
2081 RY 5.00 4.50 4.00 1.00 1.00 4.00 4.50 5.00
*

2082 KK R8 BASIN
2083 KM
2084 BA 0.554
2085 LG 0.16 0.25 4.60 0.45 64
2086 UI 0 69 208 360 471 695 788 567 421 299
2087 UI 149 105 69 23 21 21 21 0 0 0
2088 UI 0 0 0 0 0 0 0 0 0 0
2089 UI 0 0 0 0 0 0 0 0 0 0
2090 UI 0 0 0 0 0 0 0 0 0 0
*

2091 KK DIVR8 DIVERT
2092 KM
2093 DT RETR8 50.5 0.0
2094 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
2095 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2096 KK CPR8 COMBINE
2097 KM
2098 HC 2
*
2099 KK R8R11 ROUTE
2100 KM
2101 RS 7 FLOW
2102 RC 0.070 0.030 0.040 5355 0.0037 15.00
2103 RX 0.00 1000.00 1005.00 1010.00 1050.00 1060.00 1560.00 2060.00
2104 RY 15.00 14.50 13.00 12.00 11.00 13.00 14.50 15.00
*
2105 KK CPR11 COMBINE
2106 KM
2107 HC 3
*
2108 KK R11R13 ROUTE
2109 KM
2110 RS 6 FLOW
2111 RC 0.040 0.025 0.040 5263 0.0027 15.00
2112 RX 0.00 1000.00 1005.00 1010.00 1050.00 1060.00 1560.00 2060.00
2113 RY 15.00 14.50 13.00 12.00 11.00 13.00 14.50 15.00
*
2114 KK R13 BASIN
2115 KM
2116 BA 0.501
2117 LG 0.15 0.25 3.95 0.63 56
2118 UI 0 80 322 483 750 853 575 392 188 110
2119 UI 58 24 24 0 0 0 0 0 0 0
2120 UI 0 0 0 0 0 0 0 0 0 0
2121 UI 0 0 0 0 0 0 0 0 0 0
2122 UI 0 0 0 0 0 0 0 0 0 0
*
2123 KK DIVR13 DIVERT
2124 KM
2125 DT RETR13 33.8 0.0
2126 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
2127 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

2128 KK CPR13 COMBINE
2129 KM
2130 HC 2
*

HEC-1 INPUT PAGE 54

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2131 KK R13R16 ROUTE
2132 KM
2133 RS 7 FLOW
2134 RC 0.070 0.025 0.045 5239 0.0031 15.00
2135 RX 0.00 1000.00 1005.00 1010.00 1050.00 1060.00 1560.00 2060.00
2136 RY 15.00 14.50 13.00 12.00 11.00 13.00 14.50 15.00
*
2137 KK R16 BASIN
2138 KM
2139 BA 0.498
2140 LG 0.13 0.25 4.25 0.57 67
2141 UI 0 90 343 515 840 812 552 353 157 97
2142 UI 39 25 25 0 0 0 0 0 0 0
2143 UI 0 0 0 0 0 0 0 0 0 0
2144 UI 0 0 0 0 0 0 0 0 0 0
2145 UI 0 0 0 0 0 0 0 0 0 0
*

2146 KK DIVR16 DIVERT
2147 KM
2148 DT RETR16 37.2 0.0
2149 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
2150 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

2151 KK CPR16 COMBINE
2152 KM
2153 HC 2
*

2154 KK R16R21 ROUTE
2155 KM
2156 RS 12 FLOW
2157 RC 0.070 0.035 0.045 10034 0.0042 15.00
2158 RX 0.00 1000.00 1005.00 1010.00 1050.00 1060.00 1560.00 2060.00
2159 RY 15.00 14.50 13.00 12.00 11.00 13.00 14.50 15.00
*

2160 KK R21 BASIN
2161 KM
2162 BA 0.836
2163 LG 0.22 0.24 4.80 0.35 33
2164 UI 0 65 65 227 302 364 428 515 701 804
2165 UI 628 529 440 366 299 210 120 108 82 65
2166 UI 38 20 20 20 20 20 0 0 0 0
2167 UI 0 0 0 0 0 0 0 0 0 0
2168 UI 0 0 0 0 0 0 0 0 0 0
*

2312 UI 0 0 0 0 0 0 0 0 0 0 0
 2313 UI 0 0 0 0 0 0 0 0 0 0 0
 *

2314 KK DIVR18 DIVERT
 2315 KM
 2316 DT RETR18 50.8 0.0
 2317 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 2318 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

HEC-1 INPUT

1 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2319 KK CPR18 COMBINE
 2320 KM
 2321 HC 2
 *

2322 KK R18R22 ROUTE
 2323 KM
 2324 RS 5 FLOW
 2325 RC 0.025 0.050 0.025 7103 0.0031 1374.50
 2326 RX 947.00 954.00 966.00 995.00 1005.00 1034.00 1038.00 1053.00
 2327 RY 1374.5 1374.20 1373.70 1366.50 1366.50 1373.70 1373.70 1374.50
 *

2328 KK R22 BASIN
 2329 KM
 2330 BA 0.574
 2331 LG 0.17 0.24 4.65 0.41 53
 2332 UI 0 79 273 436 596 929 736 538 380 192
 2333 UI 122 76 24 24 24 0 0 0 0 0
 2334 UI 0 0 0 0 0 0 0 0 0 0
 2335 UI 0 0 0 0 0 0 0 0 0 0
 2336 UI 0 0 0 0 0 0 0 0 0 0
 *

2337 KK DIVR22 DIVERT
 2338 KM
 2339 DT RETR22 37.6 0.0
 2340 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 2341 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

2342 KK R14 BASIN
 2343 KM
 2344 BA 0.497
 2345 LG 0.14 0.25 4.55 0.46 61
 2346 UI 0 117 405 621 1015 742 487 229 120 52
 2347 UI 27 27 0 0 0 0 0 0 0 0
 2348 UI 0 0 0 0 0 0 0 0 0 0
 2349 UI 0 0 0 0 0 0 0 0 0 0
 2350 UI 0 0 0 0 0 0 0 0 0 0
 *

2351 KK DIVR14 DIVERT
 2352 KM
 2353 DT RETR14 33.9 0.0
 2354 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 2355 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

HEC-1 INPUT

1 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2356 KK R14R17 ROUTE
 2357 KM
 2358 RS 5 FLOW
 2359 RC 0.035 0.030 0.035 6503 0.0031 10.00
 2360 RX 950.00 960.00 980.00 1000.00 1005.00 1025.00 1045.00 1055.00
 2361 RY 7.00 6.00 5.00 1.00 1.00 5.00 6.00 7.00
 *

2362 KK R17 BASIN
 2363 KM
 2364 BA 0.491
 2365 LG 0.22 0.25 4.55 0.43 43
 2366 UI 0 45 75 177 234 284 352 505 516 397
 2367 UI 325 261 206 132 78 69 45 31 14 14
 2368 UI 14 14 14 0 0 0 0 0 0 0
 2369 UI 0 0 0 0 0 0 0 0 0 0
 2370 UI 0 0 0 0 0 0 0 0 0 0
 *

2371 KK DIVR17 DIVERT
 2372 KM
 2373 DT RETR17 30.4 0.0
 2374 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 2375 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

2376 KK CPR17 COMBINE
 2377 KM
 2378 HC 2
 *

2379 KK R17R22 ROUTE
 2380 KM
 2381 RS 4 FLOW
 2382 RC 0.045 0.035 0.045 6645 0.0048 15.00

2383 RX 0.00 1000.00 1005.00 1010.00 1050.00 1060.00 1560.00 2060.00
 2384 RY 15.00 14.50 14.00 12.00 11.00 14.00 14.50 15.00
 *

2385 KK CPR22 COMBINE
 2386 KM
 2387 HC 3
 *

2388 KK R22R21 ROUTE
 2389 KM
 2390 RS 3 FLOW
 2391 RC 0.025 0.050 0.025 4455 0.0022 1363.30
 2392 RX 947.00 954.00 966.00 995.00 1005.00 1034.00 1038.00 1053.00
 2393 RY 1363.3 1363.00 1362.50 1355.30 1355.30 1362.50 1362.50 1363.30
 *

HEC-1 INPUT

1 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2394 KK CPR21 COMBINE
 2395 KM
 2396 HC 3
 *

2397 KK R21R25 ROUTE
 2398 KM
 2399 RS 3 FLOW
 2400 RC 0.025 0.050 0.025 6771 0.0032 1342.30
 2401 RX 941.00 947.00 959.00 984.00 1012.00 1042.00 1046.00 1061.00
 2402 RY 1342.3 1341.50 1341.00 1334.60 1333.60 1341.00 1341.00 1341.30
 *

2403 KK R25 BASIN
 2404 KM
 2405 BA 0.279
 2406 LG 0.15 0.23 4.80 0.36 43
 2407 UI 0 62 219 334 553 424 280 144 72 35
 2408 UI 15 15 0 0 0 0 0 0 0 0
 2409 UI 0 0 0 0 0 0 0 0 0 0
 2410 UI 0 0 0 0 0 0 0 0 0 0
 2411 UI 0 0 0 0 0 0 0 0 0 0
 *

2412 KK DIVR25 DIVERT
 2413 KM
 2414 DT RETR25 14.2 0.0
 2415 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 2416 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

2417 KK R20 BASIN
 2418 KM
 2419 BA 0.503
 2420 LG 0.17 0.26 3.45 0.85 47
 2421 UI 0 61 176 313 407 582 724 524 396 290
 2422 UI 156 103 64 33 19 19 0 0 0 0
 2423 UI 0 0 0 0 0 0 0 0 0 0
 2424 UI 0 0 0 0 0 0 0 0 0 0
 2425 UI 0 0 0 0 0 0 0 0 0 0
 *

2426 KK DIVR20 DIVERT
 2427 KM
 2428 DT RETR20 34.4 0.0
 2429 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 2430 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

HEC-1 INPUT

1 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2431 KK R20R23 ROUTE
 2432 KM
 2433 RS 6 FLOW
 2434 RC 0.050 0.040 0.050 5267 0.0040 15.00
 2435 RX 0.00 1000.00 1005.00 1010.00 1050.00 1060.00 1560.00 2060.00
 2436 RY 15.00 14.00 13.00 12.00 11.00 14.00 14.50 15.00
 *

2437 KK R23 BASIN
 2438 KM
 2439 BA 0.496
 2440 LG 0.15 0.25 4.65 0.42 55
 2441 UI 0 70 254 397 553 833 621 448 304 144
 2442 UI 95 53 22 22 22 0 0 0 0 0
 2443 UI 0 0 0 0 0 0 0 0 0 0
 2444 UI 0 0 0 0 0 0 0 0 0 0
 2445 UI 0 0 0 0 0 0 0 0 0 0
 *

2446 KK DIVR23 DIVERT
 2447 KM
 2448 DT RETR23 35.2 0.0
 2449 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 2450 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

2451 KK CPR23 COMBINE
 2452 KM
 2453 HC 2

```

*
2454 KK R23R25 ROUTE
2455 KM
2456 RS 3 FLOW
2457 RC 0.035 0.030 0.035 5186 0.0044 15.00
2458 RX 960.00 980.00 1004.00 1010.00 1050.00 1052.00 1070.00 1090.00
2459 RY 15.00 13.00 12.50 11.00 11.00 14.00 14.50 15.00
*

```

```

2460 KK CPR25 COMBINE
2461 KM
2462 HC 3
*

```

```

2463 KK R25R24 ROUTE
2464 KM
2465 RS 22 FLOW
2466 RC 0.100 0.010 0.100 454 0.0044 1336.30
2467 RX 847.00 857.00 939.00 940.00 1031.00 1033.00 1109.00 1137.00
2468 RY 1333.6 1333.50 1333.40 1326.90 1326.90 1333.40 1334.10 1336.30
*

```

1 HEC-1 INPUT PAGE 63

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

2469 KK R19 BASIN
2470 KM
2471 BA 1.533
2472 LG 0.14 0.25 4.35 0.52 60
2473 UI 0 164 380 749 965 1230 1825 1821 1373 1071
2474 UI 828 534 285 231 164 60 50 50 0
2475 UI 0 0 0 0 0 0 0 0 0 0
2476 UI 0 0 0 0 0 0 0 0 0 0
2477 UI 0 0 0 0 0 0 0 0 0 0
*

```

```

2478 KK DIVR19 DIVERT
2479 KM
2480 DT RETR19 108.8 0.0
2481 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
2482 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

```

```

2483 KK DIV19R DIVERT
2484 KM
2485 DT DETR19 35.2 0.0
2486 DI 0.0 171.0 172.0 10172.0 0.0 0.0 0.0 0.0 0.0
2487 DQ 0.0 0.0 1.0 10001.0 0.0 0.0 0.0 0.0 0.0
*

```

```

2488 KK R19R24 ROUTE
2489 KM
2490 RS 8 FLOW
2491 RC 0.040 0.020 0.040 5577 0.0038 2.50
2492 RX 0.00 500.00 1000.00 1001.00 1002.00 1500.00 2000.00 2500.00
2493 RY 2.50 2.00 1.50 1.00 1.00 1.50 2.00 2.50
*

```

```

2494 KK R24 BASIN
2495 KM
2496 BA 0.294
2497 LG 0.18 0.25 4.80 0.40 52
2498 UI 0 40 133 216 291 459 384 281 203 110
2499 UI 67 40 17 12 12 0 0 0 0 0
2500 UI 0 0 0 0 0 0 0 0 0 0
2501 UI 0 0 0 0 0 0 0 0 0 0
2502 UI 0 0 0 0 0 0 0 0 0 0
*

```

```

2503 KK DIVR24 DIVERT
2504 KM
2505 DT RETR24 19.7 0.0
2506 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
2507 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

```

1 HEC-1 INPUT PAGE 64

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

2508 KK CPR24 COMBINE
2509 KM
2510 HC 3
*

```

```

2511 KK R24EM4 ROUTE
2512 KM
2513 RS 1 FLOW
2514 RC 0.025 0.025 0.025 3679 0.0044 1325.00
2515 RX 933.00 939.00 951.00 977.00 1019.00 1049.00 1053.00 1069.00
2516 RY 1325.0 1323.60 1323.10 1316.70 1315.70 1323.10 1323.10 1325.00
*

```

```

2517 KK EMF4 BASIN
2518 KM
2519 BA 0.060
2520 LG 0.08 0.08 4.80 0.25 0
2521 UI 0 102 258 87 14 0 0 0 0 0
2522 UI 0 0 0 0 0 0 0 0 0 0
2523 UI 0 0 0 0 0 0 0 0 0 0
2524 UI 0 0 0 0 0 0 0 0 0 0

```

```

2525 UI 0 0 0 0 0 0 0 0 0 0
*

```

```

2526 KK CPEMF4 COMBINE
2527 HC 3 55.93
*

```

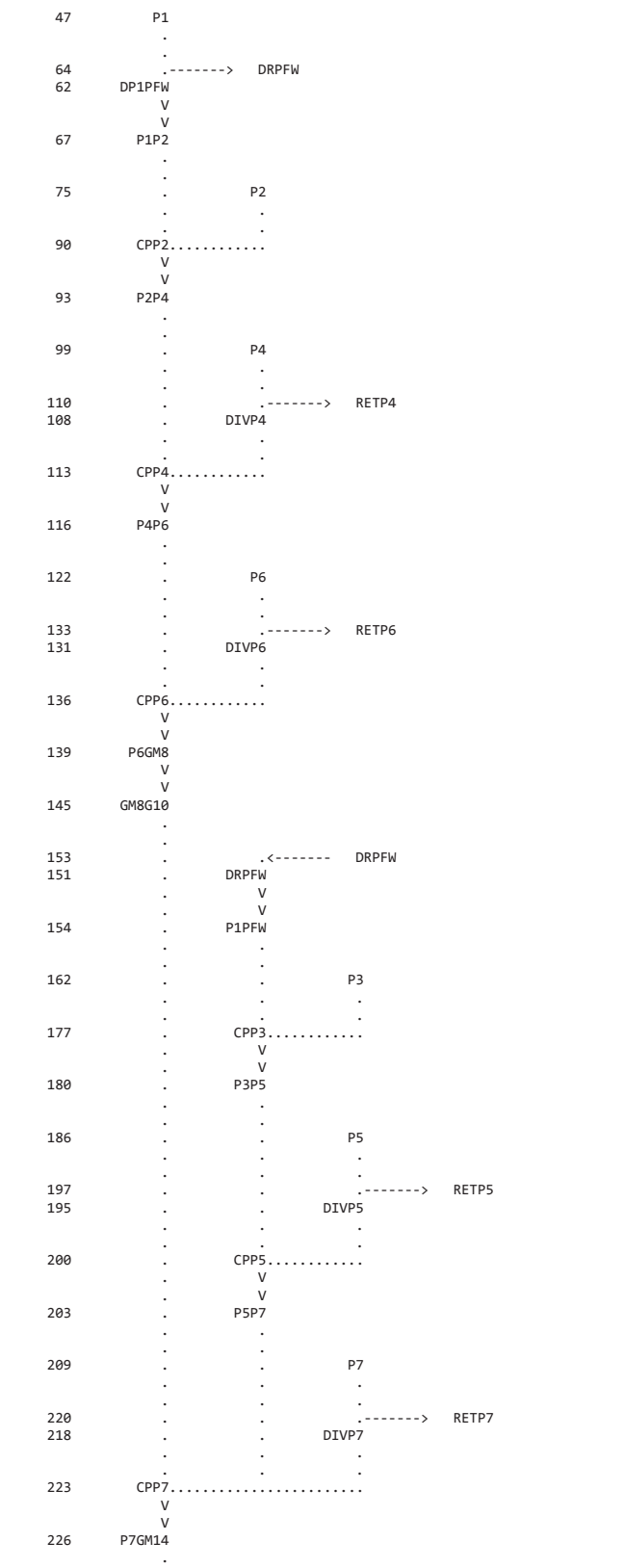
```

2528 ZZ

```

1 SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW



```

232 . GM1
241 . GM2
250 . GM3
259 . CPG123
264 .-----> RETG1
262 . DIVG1
. V
. V
267 . GM1T5
273 . GM5
284 .-----> RETG5
282 . DIVG5
287 . CPG5
. V
. V
290 . GM5T7
296 . GM6
307 .-----> RETG6
305 . DIVG6
310 . GM7
321 .-----> RETG7
319 . DIVG7
324 . CPG7A
327 . CPG7B
. V
. V
330 . GM7T9
336 . GM8
347 .-----> RETG8
345 . DIVG8
350 . GM9
361 .-----> RETG9
359 . DIVG9
364 . CPG9A
367 . GM10
378 .-----> RETG10
376 . DIVG10
381 . GM11
392 .-----> RETG11
390 . DIVG11
395 . CPG11
398 . CPG9B
. V
. V
401 . GM9T14
407 . GM12
418 .-----> RETG12
416 . DIVG12
. V
. V

```

```

421 . G12T13
427 . GM13
438 .-----> RETG13
436 . DIVG13
441 . CPG13
. V
. V
444 . G13T14
450 . GM14
461 .-----> RETG14
459 . DIVG14
464 . CPG14A
467 . CPG14B
470 . CPG14C
. V
. V
473 . G14E26
480 . E1
495 .-----> DRE2
493 . DE15
. V
. V
498 . E1E10
506 . E10
524 . CPE10
. V
. V
527 . E10E17
535 . E17
554 .-----> RETE17
550 . DIVE17
557 . CPE17
. V
. V
560 . E17E21
568 . E21
584 .-----> RETE21
580 . DIVE21
587 . CPE21A
. V
. V
590 . E21G20
599 . <----- DRE2
597 . DRE2
. V
. V
600 . RTE1E2
608 . E2
623 . CPE2
628 .-----> DRE3
626 . DE2S
. V
. V
631 . E2E11
639 . E11

```

```

657 . . . . . CPE11.....
. . . . . V
. . . . . V
660 . . . . . E11E18
. . . . .
. . . . . E18
. . . . .
. . . . . DIVE18-----> RETE18
682 . . . . .
680 . . . . .
. . . . .
685 . . . . . CPE18.....
. . . . . V
. . . . . V
688 . . . . . E18E21
. . . . .
. . . . .
696 . . . . . CPE21B.....
. . . . . V
. . . . . V
699 . . . . . G20G21
. . . . .
. . . . .
709 . . . . . <----- DRE3
707 . . . . . DRE3
. . . . . V
. . . . . V
710 . . . . . RTE2E3
. . . . .
. . . . . E3
. . . . .
718 . . . . .
. . . . .
734 . . . . . E2SE3.....
. . . . .
. . . . .
739 . . . . . -----> DRE4N
737 . . . . . DE3S
. . . . . V
. . . . . V
742 . . . . . E3E12
. . . . .
. . . . . E12
. . . . .
750 . . . . .
. . . . .
768 . . . . . CPE12.....
. . . . . V
. . . . . V
771 . . . . . E12E19
. . . . .
. . . . . E19
. . . . .
779 . . . . .
. . . . .
798 . . . . . CPE19.....
. . . . . V
. . . . . V
801 . . . . . E1922E
. . . . .
. . . . .
809 . . . . . 22E
. . . . .
. . . . . E20
. . . . . V
. . . . . V
827 . . . . .
. . . . . E2022E
. . . . .
. . . . .
846 . . . . .
. . . . .
854 . . . . . CP22E.....
. . . . . V
. . . . . V
857 . . . . . 22EE22
. . . . .
. . . . . E22
. . . . .
863 . . . . .
. . . . .
881 . . . . . CPE22.....
. . . . . V
. . . . . V
884 . . . . . E22G22
. . . . .
. . . . .
890 . . . . . GM21
. . . . .
. . . . . -----> RETG21
901 . . . . .
899 . . . . . DIVG21
. . . . . V
. . . . . V
904 . . . . . G21T22
. . . . .
. . . . .
910 . . . . . GM22
. . . . .
. . . . .
921 . . . . . -----> RETG22
919 . . . . . DIVG22
. . . . .

```

```

924 . . . . . CPG22A.....
. . . . .
. . . . . GM16
. . . . .
. . . . . -----> RETG16
938 . . . . .
936 . . . . . DIVG16
. . . . . V
. . . . . V
941 . . . . . G16T19
. . . . .
. . . . .
947 . . . . . GM18
. . . . .
. . . . . -----> RETG18
958 . . . . .
956 . . . . . DIVG18
. . . . .
. . . . .
961 . . . . . CPG18.....
. . . . .
. . . . . GM19
. . . . .
975 . . . . . -----> RETG19
973 . . . . . DIVG19
. . . . .
. . . . .
978 . . . . . CPG19A.....
. . . . .
. . . . . GM20
. . . . .
981 . . . . .
. . . . . -----> RETG20
992 . . . . .
990 . . . . . DIVG20
. . . . .
. . . . .
995 . . . . . CPG19B.....
. . . . .
. . . . .
998 . . . . . CPG22B.....
. . . . . V
. . . . . V
1003 . . . . . G22E26
. . . . .
. . . . .
1012 . . . . . <----- DRE4N
1010 . . . . . DRE4N
. . . . . V
. . . . . V
1013 . . . . . RTE3E4
. . . . .
. . . . . E4N
. . . . .
1021 . . . . .
. . . . .
1036 . . . . . CPE4N.....
. . . . .
. . . . .
1041 . . . . . -----> DRE4
1039 . . . . . DE4NS
. . . . . V
. . . . . V
1044 . . . . . E4NE13
. . . . .
. . . . . E13
. . . . .
1052 . . . . .
. . . . .
1068 . . . . . CPE13.....
. . . . . V
. . . . . V
1071 . . . . . E13E24
. . . . .
. . . . .
1080 . . . . . <----- DRE4
1078 . . . . . DRE4
. . . . . V
. . . . . V
1081 . . . . . RTE4E4
. . . . .
. . . . . E4
. . . . .
1089 . . . . .
. . . . .
1105 . . . . . CPE4.....
. . . . .
. . . . .
1110 . . . . . -----> DRE5
1108 . . . . . DE4S
. . . . . V
. . . . . V
1113 . . . . . E4E14A
. . . . .
. . . . .
1122 . . . . . E14A
. . . . .
. . . . .
1171 . . . . . <----- DRE5

```

```

1169 . . . . . DRE5
. . . . . V
1172 . . . . . RTE4E5
. . . . .
. . . . . E5
1181 . . . . .
. . . . .
1196 . . . . . CPE5.....
. . . . .
1210 . . . . . -----> DRE6
1207 . . . . . DE5S
. . . . . V
1213 . . . . . E5A14A
. . . . .
1222 . . . . . CPE14A.....
. . . . . V
1226 . . . . . E1424A
. . . . . V
1235 . . . . . E1424B
. . . . .
1244 . . . . . E24A
. . . . .
1255 . . . . . -----> RET24A
1253 . . . . . DIV24A
. . . . .
1258 . . . . . CP24A.....
. . . . . V
1261 . . . . . E247A1
. . . . .
1270 . . . . . E27A
. . . . .
1281 . . . . . -----> RET27A
1279 . . . . . DIV27A
. . . . .
1284 . . . . . CPE27A.....
. . . . . V
1290 . . . . . E247A2
. . . . . V
1299 . . . . . E2726A
. . . . .
1309 . . . . . E26A
. . . . .
1320 . . . . . -----> RET26A
1318 . . . . . DIV26A
. . . . .
1323 . . . . . SR24EL.....
. . . . .
1352 . . . . . -----> 1650UP
1344 . . . . . 802ELS
. . . . .
1364 . . . . . GM17
. . . . .
1381 . . . . . -----> RETG17
1376 . . . . . DIVG17
. . . . . V
1384 . . . . . G17E26
. . . . .
1390 . . . . . CPE26A.....
. . . . . V
1398 . . . . . 80233B
. . . . .
1408 . . . . . E7
. . . . .
1419 . . . . . -----> RETE7
1417 . . . . . DIVE7
. . . . . V
1422 . . . . . E7STOR
. . . . . V
1430 . . . . . E7E6
. . . . .
1444 . . . . . <----- DRE6
1438 . . . . . DRE6
. . . . . V

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```

1445 . . . . . V
. . . . . RTE5E6
. . . . .
1454 . . . . . E6
. . . . .
1472 . . . . . E8
. . . . .
1483 . . . . . -----> RETE8
1481 . . . . . DIVE8
. . . . . V
1486 . . . . . E8E6
. . . . .
1492 . . . . . CPE6.....
. . . . .
1497 . . . . . -----> DRE9
1495 . . . . . DE6S
. . . . . V
1500 . . . . . E6E15
. . . . .
1506 . . . . . E15
. . . . .
1517 . . . . . -----> RETE15
1515 . . . . . DIVE15
. . . . .
1522 . . . . . <----- DRE9
1520 . . . . . DRE9
. . . . . V
1523 . . . . . RTE6E9
. . . . .
1529 . . . . . E9
. . . . .
1540 . . . . . -----> RETE9
1538 . . . . . DIVE9
. . . . .
1543 . . . . . CPE9.....
. . . . .
1548 . . . . . -----> DRR5
1546 . . . . . DE9S
. . . . . V
1551 . . . . . E9E16
. . . . .
1557 . . . . . E16
. . . . .
1568 . . . . . -----> RETE16
1566 . . . . . DIVE16
. . . . .
1571 . . . . . CPE16.....
. . . . . V
1574 . . . . . E16E15
. . . . .
1580 . . . . . CPE15.....
. . . . . V
1583 . . . . . E1524B
. . . . .
1589 . . . . . E5B
. . . . .
1600 . . . . . -----> RETE5B
1598 . . . . . DIVE5B
. . . . . V
1603 . . . . . E5E14B
. . . . .
1609 . . . . . E14B
. . . . .
1620 . . . . . -----> RET14B
1618 . . . . . DIV14B
. . . . .
1623 . . . . . CP14B.....
. . . . . V
1626 . . . . . E14E24
. . . . .
1632 . . . . . E24B
. . . . .

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1643 . . . . .
1641 . . . . . DIV24B -----> RET24B
1646 . . . . . CPE24B -----
      . . . . . V
      . . . . . V
1649 . . . . . E24E28
      . . . . .
      . . . . . E28B
      . . . . .
      . . . . . DIV28B -----> RET28B
1666 . . . . .
1664 . . . . . CPE28B -----
      . . . . . V
      . . . . . V
1672 . . . . . E28E31
      . . . . .
      . . . . . E25
      . . . . .
      . . . . . DIVE25 -----> RETE25
1689 . . . . .
1687 . . . . . DIVE25
      . . . . . V
      . . . . . V
1692 . . . . . E25E29
      . . . . .
      . . . . . E29
      . . . . .
      . . . . . DIVE29 -----> RETE29
1709 . . . . .
1707 . . . . . CPE29 -----
      . . . . . V
      . . . . . V
1715 . . . . . E29E31
      . . . . .
      . . . . . E32
      . . . . .
      . . . . . DIVE32 -----> RETE32
1732 . . . . .
1730 . . . . . DIVE32
      . . . . . V
      . . . . . V
1735 . . . . . E32E31
      . . . . .
      . . . . . E31
      . . . . .
      . . . . . DIVE31 -----> RETE31
1752 . . . . .
1750 . . . . . CPE31 -----
      . . . . . V
      . . . . . V
1758 . . . . . E31E30
      . . . . .
      . . . . . E30B
      . . . . .
      . . . . . DIV30B -----> RET30B
1775 . . . . .
1773 . . . . . CPE30 -----
      . . . . . V
      . . . . . V
1781 . . . . . E30E26
      . . . . .
      . . . . . E26B
      . . . . .
      . . . . . DIV26B -----> RET26B
1798 . . . . .
1796 . . . . . CPE26 -----
      . . . . . V
      . . . . . V
1804 . . . . . E26E33
      . . . . .
      . . . . . E33B
      . . . . .
      . . . . . DIV33B -----> RET33B
1821 . . . . .
1819 . . . . . CPE33B -----
1824 . . . . .

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```

      . . . . . V
      . . . . . V
1827 . . . . . E33P9A
      . . . . . V
      . . . . . V
1833 . . . . . E33P9B
      . . . . .
      . . . . . P9
      . . . . .
      . . . . . DIVP9 -----> RETP9
1850 . . . . .
1848 . . . . . CPP9 -----
      . . . . . V
      . . . . . V
1856 . . . . . P9EMF1
      . . . . .
      . . . . . EMF1B
      . . . . .
      . . . . . DEMF1B -----> REMF1B
1873 . . . . .
1871 . . . . . CPEMF1 -----
      . . . . . V
      . . . . . V
1876 . . . . . EM1EM2
      . . . . .
      . . . . . EMF2
      . . . . .
      . . . . . DIVEM2 -----> RETEM2
1896 . . . . .
1894 . . . . . CPEMF2 -----
      . . . . . V
      . . . . . V
1902 . . . . . EM2M3A
      . . . . . V
      . . . . . V
1908 . . . . . EM2M3B
      . . . . .
      . . . . . EMF3
      . . . . .
      . . . . . DIVEM3 -----> RETEM3
1925 . . . . .
1923 . . . . . CPEMF3 -----
      . . . . . V
      . . . . . V
1931 . . . . . EMF3RB
      . . . . .
      . . . . . RITBAS
      . . . . . V
      . . . . . V
1946 . . . . . RITBAS
      . . . . .
      . . . . . CPRITB -----
      . . . . . V
      . . . . . V
1954 . . . . . RBEMF4
1957 . . . . .
      . . . . . R2
      . . . . .
      . . . . . DIVR2 -----> RETR2
1975 . . . . .
1973 . . . . . R3
      . . . . .
      . . . . . DIVR3 -----> RETR3
1989 . . . . .
1987 . . . . . CPR2R3 -----
      . . . . . V
      . . . . . V
1992 . . . . . R2R3R6
1995 . . . . .
      . . . . . R6
2001 . . . . .
      . . . . . CPR6 -----
      . . . . . V
      . . . . . V
2010 . . . . . R6R9
2013 . . . . .

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```
2019 . . . . . R9
. . . . .
2030 . . . . . DIVR9-----> RETR9
2028 . . . . .
. . . . .
2033 . . . . . CPR9-----
. . . . . V
. . . . . V
2036 . . . . . R9R11
. . . . .
. . . . .
2042 . . . . . R11
. . . . .
2053 . . . . . DIVR11-----> RETR11
2051 . . . . .
. . . . .
2058 . . . . . <----- DRR5
2056 . . . . . DRR5
. . . . .
. . . . . R5
2059 . . . . .
. . . . . DIVR5-----> RETR5
2070 . . . . .
2068 . . . . .
. . . . .
2073 . . . . . CPR5-----
. . . . . V
. . . . . V
2076 . . . . . R5R8
. . . . .
. . . . . R8
2082 . . . . .
. . . . . DIVR8-----> RETR8
2093 . . . . .
2091 . . . . .
. . . . .
2096 . . . . . CPR8-----
. . . . . V
. . . . . V
2099 . . . . . R8R11
. . . . .
. . . . .
2105 . . . . . CPR11-----
. . . . . V
. . . . . V
2108 . . . . . R11R13
. . . . .
. . . . . R13
2114 . . . . .
. . . . . DIVR13-----> RETR13
2125 . . . . .
2123 . . . . .
. . . . .
2128 . . . . . CPR13-----
. . . . . V
. . . . . V
2131 . . . . . R13R16
. . . . .
. . . . . R16
2137 . . . . .
. . . . . DIVR16-----> RETR16
2148 . . . . .
2146 . . . . .
. . . . .
2151 . . . . . CPR16-----
. . . . . V
. . . . . V
2154 . . . . . R16R21
. . . . .
. . . . . R21
2160 . . . . .
. . . . . DIVR21-----> RETR21
2171 . . . . .
2169 . . . . .
. . . . .
2175 . . . . . R1
. . . . .
. . . . . DIVR1-----> RETR1
2186 . . . . .
2184 . . . . .
. . . . . V
. . . . . V
2189 . . . . . R1R4
. . . . .
. . . . . R4
2195 . . . . .
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```
2204 . . . . . CPR4-----
. . . . . V
. . . . . V
2207 . . . . . R4R7
. . . . .
. . . . . R7
2213 . . . . .
. . . . .
2224 . . . . . DIVR7-----> RETR7
2222 . . . . .
. . . . .
2227 . . . . . CPR7-----
. . . . . V
. . . . . V
2230 . . . . . R7R10
. . . . .
. . . . . R10
2236 . . . . .
. . . . . DIVR10-----> RETR10
2247 . . . . .
2245 . . . . .
. . . . .
2250 . . . . . CPR10-----
. . . . . V
. . . . . V
2253 . . . . . R10R12
. . . . .
. . . . . R12
2259 . . . . .
. . . . . DIVR12-----> RETR12
2270 . . . . .
2268 . . . . .
. . . . .
2273 . . . . . CPR12-----
. . . . . V
. . . . . V
2276 . . . . . R12R15
. . . . .
. . . . . R15
2282 . . . . .
. . . . . DIVR15-----> RETR15
2293 . . . . .
2291 . . . . .
. . . . .
2296 . . . . . CPR15-----
. . . . . V
. . . . . V
2299 . . . . . R15R18
. . . . .
. . . . . R18
2305 . . . . .
. . . . . DIVR18-----> RETR18
2316 . . . . .
2314 . . . . .
. . . . .
2319 . . . . . CPR18-----
. . . . . V
. . . . . V
2322 . . . . . R18R22
. . . . .
. . . . . R22
2328 . . . . .
. . . . . DIVR22-----> RETR22
2339 . . . . .
2337 . . . . .
. . . . .
2342 . . . . . R14
. . . . .
. . . . . DIVR14-----> RETR14
2353 . . . . .
2351 . . . . .
. . . . . V
. . . . . V
2356 . . . . . R14R17
. . . . .
. . . . . R17
2362 . . . . .
. . . . . DIVR17-----> RETR17
2373 . . . . .
2371 . . . . .
. . . . .
2376 . . . . . CPR17-----
. . . . . V
. . . . . V
2379 . . . . . R17R22
. . . . .
. . . . .
2385 . . . . . CPR22-----
. . . . . V
```

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2388 . . . . . V
. . . . . R22R21
. . . . .
2394 . . . . . CPR21-----
. . . . . V
. . . . . V
2397 . . . . . R21R25
. . . . .
. . . . . R25
. . . . .
2403 . . . . .
. . . . .
2414 . . . . . -----> RETR25
2412 . . . . . DIVR25
. . . . .
. . . . . R20
. . . . .
2417 . . . . .
. . . . .
2428 . . . . . -----> RETR20
2426 . . . . . DIVR20
. . . . . V
. . . . . V
2431 . . . . . R20R23
. . . . .
. . . . . R23
. . . . .
2437 . . . . .
. . . . .
2448 . . . . . -----> RETR23
2446 . . . . . DIVR23
. . . . .
. . . . . CPR23-----
2451 . . . . . V
. . . . . V
2454 . . . . . R23R25
. . . . .
. . . . . CPR25-----
2460 . . . . . V
. . . . . V
2463 . . . . . R25R24
. . . . .
. . . . . R19
. . . . .
2469 . . . . .
. . . . .
2480 . . . . . -----> RETR19
2478 . . . . . DIVR19
. . . . .
. . . . . -----> DETR19
2485 . . . . . DIV19R
2483 . . . . . V
. . . . . V
2488 . . . . . R19R24
. . . . .
. . . . . R24
. . . . .
2494 . . . . .
. . . . .
2505 . . . . . -----> RETR24
2503 . . . . . DIVR24
. . . . .
. . . . . CPR24-----
2508 . . . . . V
. . . . . V
2511 . . . . . R24EM4
. . . . .
. . . . . EMF4
. . . . .
2517 . . . . .
. . . . .
2526 . . . . . CPEMF4-----

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(***) RUNOFF ALSO COMPUTED AT THIS LOCATION
1*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 04JUL16 TIME 13:51:13 *
*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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24INT050IC 100-YEAR, 24-hr Interim Phase II Conditions 2016-07-04
Assuming concrete-lined channel for the following routes:
E5A14A, E1424A, E1424B, E247A1, E247A2 and E2726A.
by Parsons Corporation

The model reflects interim drainage conditions for SR 24 and it is based
on Mesa ADMPU with revisions reflecting development work around the
corridor.
This model simulates that the SR 24 corridor extends to Ironwood Dr,
which would eliminate the need to intercept runoff from subbasins

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WARNING --- ROUTED OUTFLOW ( 899.) IS GREATER THAN MAXIMUM OUTFLOW ( 873.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 909.) IS GREATER THAN MAXIMUM OUTFLOW ( 873.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 905.) IS GREATER THAN MAXIMUM OUTFLOW ( 873.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 889.) IS GREATER THAN MAXIMUM OUTFLOW ( 873.) IN STORAGE-OUTFLOW TABLE

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*****
* RITBAS * STORAGE
*
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1948 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

```

1

RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT								
+	P1	194.	12.67	25.	6.	2.	0.39		
+	DIVERSION TO								
+	DRPFW	118.	12.67	12.	3.	1.	0.39		
+	HYDROGRAPH AT								
+	DP1PFW	76.	12.67	13.	3.	1.	0.39		
+	ROUTED TO								
+	P1P2	49.	14.58	13.	3.	1.	0.39		
+	HYDROGRAPH AT								
+	P2	258.	12.75	38.	10.	3.	0.58		
+	2 COMBINED AT								
+	CPP2	258.	12.75	52.	13.	4.	0.96		
+	ROUTED TO								
+	P2P4	242.	13.00	52.	13.	4.	0.96		
+	HYDROGRAPH AT								
+	P4	459.	12.50	68.	21.	7.	0.50		
+	DIVERSION TO								
+	RETP4	459.	12.50	68.	21.	7.	0.50		
+	HYDROGRAPH AT								
+	DIVP4	0.	0.00	0.	0.	0.	0.50		
+	2 COMBINED AT								
+	CPP4	242.	13.00	52.	13.	4.	1.46		
+	ROUTED TO								
+	P4P6	220.	13.33	51.	13.	4.	1.46		
+	HYDROGRAPH AT								
+	P6	390.	12.67	68.	21.	7.	0.50		
+	DIVERSION TO								
+	RETP6	390.	12.67	68.	21.	7.	0.50		
+	HYDROGRAPH AT								
+	DIVP6	0.	0.00	0.	0.	0.	0.50		
+	2 COMBINED AT								
+	CPP6	220.	13.33	51.	13.	4.	1.96		
+	ROUTED TO								
+	P6GM8	210.	13.50	50.	13.	4.	1.96		
+	ROUTED TO								
+	GM8G10	201.	13.67	50.	13.	4.	1.96		
+	HYDROGRAPH AT								
+	DRPFW	118.	12.67	12.	3.	1.	0.39		
+	ROUTED TO								
+	P1PFW	92.	12.83	12.	3.	1.	0.39		
+	HYDROGRAPH AT								
+	P3	191.	13.00	34.	8.	3.	0.52		
+	2 COMBINED AT								
+	CPP3	275.	12.92	45.	11.	4.	0.91		
+	ROUTED TO								
+	P3P5	271.	13.00	45.	11.	4.	0.91		
+	HYDROGRAPH AT								

+		P5	229.	12.50	35.	11.	4.	0.25
+	DIVERSION TO	RETP5	229.	12.50	33.	9.	3.	0.25
+	HYDROGRAPH AT	DIVP5	34.	13.25	6.	2.	1.	0.25
+	2 COMBINED AT	CPP5	271.	13.00	50.	13.	4.	1.16
+	ROUTED TO	P5P7	263.	13.08	50.	13.	4.	1.16
+	HYDROGRAPH AT	P7	419.	12.50	64.	19.	6.	0.43
+	DIVERSION TO	RETP7	419.	12.50	59.	16.	5.	0.43
+	HYDROGRAPH AT	DIVP7	60.	13.17	11.	4.	1.	0.43
+	3 COMBINED AT	CPP7	360.	13.58	106.	28.	9.	3.17
+	ROUTED TO	P7GM14	348.	13.83	105.	28.	9.	3.17
+	HYDROGRAPH AT	GM1	377.	12.42	44.	12.	4.	0.34
+	HYDROGRAPH AT	GM2	888.	12.33	113.	36.	12.	0.68
+	HYDROGRAPH AT	GM3	577.	12.08	60.	20.	7.	0.29
+	3 COMBINED AT	CPG123	1521.	12.17	217.	68.	23.	1.32
+	DIVERSION TO	RETG1	1521.	12.17	189.	51.	17.	1.32
+	HYDROGRAPH AT	DIVG1	354.	12.75	51.	16.	5.	1.32
+	ROUTED TO	GM1T5	223.	12.92	50.	16.	5.	1.32
+	HYDROGRAPH AT	GM5	310.	12.17	37.	12.	4.	0.18
+	DIVERSION TO	RETG5	310.	12.17	25.	7.	2.	0.18
+	HYDROGRAPH AT	DIVG5	218.	12.33	17.	5.	2.	0.18
+	2 COMBINED AT	CPG5	246.	12.92	65.	21.	7.	1.49
+	ROUTED TO	GM5T7	206.	13.25	63.	21.	7.	1.49
+	HYDROGRAPH AT	GM6	685.	12.17	63.	19.	6.	0.37
+	DIVERSION TO	RETG6	685.	12.17	50.	14.	5.	0.37
+	HYDROGRAPH AT	DIVG6	282.	12.33	19.	6.	2.	0.37
+	HYDROGRAPH AT	GM7	249.	12.33	27.	8.	3.	0.22
+	DIVERSION TO	RETG7	249.	12.33	27.	7.	2.	0.22
+	HYDROGRAPH AT	DIVG7	2.	16.75	1.	0.	0.	0.22
+	2 COMBINED AT	CPG7A	282.	12.33	20.	6.	2.	0.58
+	2 COMBINED AT	CPG7B	236.	12.33	79.	26.	9.	2.08
+	ROUTED TO	GM7T9	200.	13.42	78.	26.	9.	2.08
+	HYDROGRAPH AT	GM8	692.	12.33	86.	28.	9.	0.56
+	DIVERSION TO	RETG8	692.	12.33	74.	20.	7.	0.56
+	HYDROGRAPH AT	DIVG8	192.	12.67	23.	7.	2.	0.56
+	HYDROGRAPH AT	GM9	153.	12.17	11.	3.	1.	0.09

+	DIVERSION TO	RETG9	153.	12.17	11.	3.	1.	0.09
+	HYDROGRAPH AT	DIVG9	0.	23.83	0.	0.	0.	0.09
+	2 COMBINED AT	CPG9A	192.	12.67	23.	7.	2.	0.65
+	HYDROGRAPH AT	GM10	357.	12.33	46.	14.	5.	0.28
+	DIVERSION TO	RETG10	357.	12.33	32.	9.	3.	0.28
+	HYDROGRAPH AT	DIVG10	236.	12.50	18.	5.	2.	0.28
+	HYDROGRAPH AT	GM11	91.	12.25	9.	3.	1.	0.08
+	DIVERSION TO	RETG11	91.	12.25	9.	3.	1.	0.08
+	HYDROGRAPH AT	DIVG11	1.	23.00	0.	0.	0.	0.08
+	2 COMBINED AT	CPG11	236.	12.50	18.	5.	2.	0.36
+	3 COMBINED AT	CPG9B	344.	12.75	114.	38.	13.	3.08
+	ROUTED TO	GM9T14	299.	12.92	112.	38.	13.	3.08
+	HYDROGRAPH AT	GM12	244.	12.08	26.	9.	3.	0.12
+	DIVERSION TO	RETG12	244.	12.08	16.	5.	2.	0.12
+	HYDROGRAPH AT	DIVG12	212.	12.17	13.	4.	1.	0.12
+	ROUTED TO	G12T13	82.	12.42	13.	4.	1.	0.12
+	HYDROGRAPH AT	GM13	519.	12.08	48.	16.	5.	0.29
+	DIVERSION TO	RETG13	519.	12.08	42.	11.	4.	0.29
+	HYDROGRAPH AT	DIVG13	75.	12.42	13.	4.	1.	0.29
+	2 COMBINED AT	CPG13	156.	12.42	26.	8.	3.	0.41
+	ROUTED TO	G13T14	132.	12.50	25.	8.	3.	0.41
+	HYDROGRAPH AT	GM14	591.	12.17	59.	19.	6.	0.35
+	DIVERSION TO	RETG14	591.	12.17	46.	13.	4.	0.35
+	HYDROGRAPH AT	DIVG14	254.	12.33	21.	7.	2.	0.35
+	2 COMBINED AT	CPG14A	292.	12.33	46.	15.	5.	0.76
+	2 COMBINED AT	CPG14B	386.	12.92	151.	51.	17.	3.84
+	2 COMBINED AT	CPG14C	540.	13.83	236.	75.	25.	7.01
+	ROUTED TO	G14E26	537.	13.83	235.	75.	25.	7.01
+	HYDROGRAPH AT	E1	374.	12.83	57.	14.	5.	0.89
+	DIVERSION TO	DRE2	296.	12.83	42.	11.	4.	0.89
+	HYDROGRAPH AT	DE15	77.	12.83	15.	4.	1.	0.89
+	ROUTED TO	E1E10	48.	14.83	15.	4.	1.	0.89
+	HYDROGRAPH AT	E10	326.	12.92	53.	13.	4.	0.82
+	2 COMBINED AT	CPE10	340.	12.92	67.	17.	6.	1.71

+	ROUTED TO	E10E17	308.	13.17	67.	17.	6.	1.71
+	HYDROGRAPH AT	E17	245.	12.50	35.	11.	4.	0.27
+	DIVERSION TO	RETE17	245.	12.50	34.	9.	3.	0.27
+	HYDROGRAPH AT	DIVE17	18.	13.50	5.	2.	1.	0.27
+	2 COMBINED AT	CPE17	308.	13.17	71.	18.	6.	1.98
+	ROUTED TO	E17E21	291.	13.33	70.	18.	6.	1.98
+	HYDROGRAPH AT	E21	291.	12.50	43.	13.	4.	0.31
+	DIVERSION TO	RETE21	291.	12.50	38.	10.	3.	0.31
+	HYDROGRAPH AT	DIVE21	63.	13.00	9.	3.	1.	0.31
+	2 COMBINED AT	CPE21A	319.	13.33	78.	21.	7.	2.29
+	ROUTED TO	E21G20	311.	13.42	78.	21.	7.	2.29
+	HYDROGRAPH AT	DRE2	296.	12.83	42.	11.	4.	0.89
+	ROUTED TO	RTE1E2	234.	13.25	42.	11.	4.	0.89
+	HYDROGRAPH AT	E2	325.	12.92	53.	13.	4.	0.78
+	2 COMBINED AT	CPE2	472.	13.00	94.	24.	8.	1.67
+	DIVERSION TO	DRE3	277.	13.00	39.	10.	3.	1.67
+	HYDROGRAPH AT	DE2S	195.	13.00	55.	14.	5.	1.67
+	ROUTED TO	E2E11	151.	15.92	54.	14.	5.	1.67
+	HYDROGRAPH AT	E11	251.	12.83	39.	10.	3.	0.60
+	2 COMBINED AT	CPE11	246.	12.83	83.	23.	8.	2.27
+	ROUTED TO	E11E18	173.	13.75	80.	23.	8.	2.27
+	HYDROGRAPH AT	E18	278.	12.33	31.	9.	3.	0.22
+	DIVERSION TO	RETE18	1.	4.50	1.	0.	0.	0.22
+	HYDROGRAPH AT	DIVE18	278.	12.33	31.	8.	3.	0.22
+	2 COMBINED AT	CPE18	274.	12.33	96.	31.	10.	2.49
+	ROUTED TO	E18E21	247.	12.50	95.	31.	10.	2.49
+	2 COMBINED AT	CPE21B	417.	13.67	169.	52.	17.	3.90
+	ROUTED TO	G20G21	413.	13.75	168.	52.	17.	3.90
+	HYDROGRAPH AT	DRE3	277.	13.00	39.	10.	3.	1.67
+	ROUTED TO	RTE2E3	241.	13.42	39.	10.	3.	1.67
+	HYDROGRAPH AT	E3	748.	13.25	165.	41.	14.	2.23
+	2 COMBINED AT	E25E3	938.	13.25	200.	50.	17.	3.90
+	DIVERSION TO	DRE4N	545.	13.25	81.	20.	7.	3.90
+	HYDROGRAPH AT	DE3S	394.	13.25	119.	30.	10.	3.90
+	ROUTED TO							

+		E3E12	347.	14.50	119.	30.	10.	3.90
+	HYDROGRAPH AT	E12	256.	12.92	43.	11.	4.	0.57
+	2 COMBINED AT	CPE12	468.	12.92	160.	40.	13.	4.47
+	ROUTED TO	E12E19	416.	13.75	160.	40.	13.	4.47
+	HYDROGRAPH AT	E19	205.	12.25	19.	5.	2.	0.14
+	2 COMBINED AT	CPE19	418.	13.75	178.	45.	15.	4.61
+	ROUTED TO	E1922E	404.	14.08	178.	45.	15.	4.61
+	HYDROGRAPH AT	22E	130.	12.25	13.	3.	1.	0.09
+	HYDROGRAPH AT	E20	133.	12.50	16.	5.	2.	0.17
+	ROUTED TO	E2022E	107.	12.75	16.	5.	2.	0.17
+	3 COMBINED AT	CP22E	407.	14.08	205.	53.	18.	4.87
+	ROUTED TO	22EE22	402.	14.25	205.	53.	18.	4.87
+	HYDROGRAPH AT	E22	188.	12.67	28.	7.	2.	0.16
+	3 COMBINED AT	CPE22	756.	14.00	381.	108.	36.	7.25
+	ROUTED TO	E22G22	747.	14.17	377.	108.	36.	7.25
+	HYDROGRAPH AT	GM21	335.	12.25	45.	15.	5.	0.21
+	DIVERSION TO	RETG21	335.	12.25	31.	9.	3.	0.21
+	HYDROGRAPH AT	DIVG21	216.	12.42	21.	6.	2.	0.21
+	ROUTED TO	G21T22	180.	12.50	21.	6.	2.	0.21
+	HYDROGRAPH AT	GM22	184.	12.17	21.	7.	2.	0.09
+	DIVERSION TO	RETG22	176.	12.08	14.	4.	1.	0.09
+	HYDROGRAPH AT	DIVG22	143.	12.25	10.	3.	1.	0.09
+	2 COMBINED AT	CPG22A	210.	12.50	30.	9.	3.	0.31
+	HYDROGRAPH AT	GM16	79.	12.33	10.	3.	1.	0.07
+	DIVERSION TO	RETG16	79.	12.33	9.	2.	1.	0.07
+	HYDROGRAPH AT	DIVG16	12.	12.83	2.	1.	0.	0.07
+	ROUTED TO	G16T19	7.	13.17	2.	1.	0.	0.07
+	HYDROGRAPH AT	GM18	238.	12.25	27.	9.	3.	0.17
+	DIVERSION TO	RETG18	238.	12.25	23.	6.	2.	0.17
+	HYDROGRAPH AT	DIVG18	62.	12.58	7.	2.	1.	0.17
+	2 COMBINED AT	CPG18	62.	12.58	10.	3.	1.	0.24
+	HYDROGRAPH AT	GM19	152.	12.17	12.	4.	1.	0.09
+	DIVERSION TO	RETG19	152.	12.17	11.	3.	1.	0.09
+	HYDROGRAPH AT	DIVG19	34.	12.42	3.	1.	0.	0.09
+	2 COMBINED AT	CPG19A	73.	12.58	12.	4.	1.	0.33

+		E8E6	43.	15.25	23.	8.	3.	1.10
+	3 COMBINED AT	CPE6	1001.	13.50	291.	77.	26.	3.05
+	DIVERSION TO	DRE9	151.	13.50	15.	4.	1.	3.05
+	HYDROGRAPH AT	DE6S	850.	13.50	276.	74.	25.	3.05
+	ROUTED TO	E6E15	800.	14.00	275.	74.	25.	3.05
+	HYDROGRAPH AT	E15	955.	12.33	135.	45.	15.	0.78
+	DIVERSION TO	RETE15	955.	12.33	123.	34.	11.	0.78
+	HYDROGRAPH AT	DIVE15	120.	13.00	31.	11.	4.	0.78
+	HYDROGRAPH AT	DRE9	151.	13.50	15.	4.	1.	3.05
+	ROUTED TO	RTE6E9	126.	13.83	15.	4.	1.	3.05
+	HYDROGRAPH AT	E9	846.	12.42	128.	42.	14.	0.72
+	DIVERSION TO	RETE9	846.	12.42	119.	33.	11.	0.72
+	HYDROGRAPH AT	DIVE9	102.	13.17	28.	9.	3.	0.72
+	2 COMBINED AT	CPE9	193.	13.75	45.	14.	5.	0.72
+	DIVERSION TO	DRR5	65.	13.75	6.	1.	0.	0.72
+	HYDROGRAPH AT	DE9S	128.	13.75	39.	12.	4.	0.72
+	ROUTED TO	E9E16	119.	14.17	38.	12.	4.	0.72
+	HYDROGRAPH AT	E16	508.	12.33	69.	23.	8.	0.40
+	DIVERSION TO	RETE16	508.	12.33	64.	18.	6.	0.40
+	HYDROGRAPH AT	DIVE16	48.	13.08	15.	5.	2.	0.40
+	2 COMBINED AT	CPE16	138.	14.17	52.	17.	6.	1.12
+	ROUTED TO	E16E15	138.	14.33	51.	17.	6.	1.12
+	3 COMBINED AT	CPE15	923.	14.17	338.	97.	32.	4.95
+	ROUTED TO	E1524B	909.	14.33	337.	97.	32.	4.95
+	HYDROGRAPH AT	E5B	387.	12.25	50.	17.	6.	0.29
+	DIVERSION TO	RETE5B	387.	12.25	45.	13.	4.	0.29
+	HYDROGRAPH AT	DIVE5B	41.	12.92	12.	4.	1.	0.29
+	ROUTED TO	E5E14B	27.	13.58	12.	4.	1.	0.29
+	HYDROGRAPH AT	E14B	774.	12.25	96.	32.	11.	0.53
+	DIVERSION TO	RET14B	774.	12.25	88.	24.	8.	0.53
+	HYDROGRAPH AT	DIV14B	74.	12.92	22.	7.	2.	0.53
+	2 COMBINED AT	CP14B	74.	12.92	33.	12.	4.	0.81
+	ROUTED TO	E14E24	63.	13.92	32.	12.	4.	0.81
+	HYDROGRAPH AT	E24B	695.	12.25	88.	28.	9.	0.46
+	DIVERSION TO	RET24B	695.	12.25	71.	20.	7.	0.46

+	HYDROGRAPH AT	DIV24B	238.	12.58	29.	9.	3.	0.46
+	3 COMBINED AT	CPE24B	948.	14.33	372.	113.	38.	6.23
+	ROUTED TO	E24E28	933.	14.58	370.	113.	38.	6.23
+	HYDROGRAPH AT	E28B	681.	12.42	101.	32.	11.	0.54
+	DIVERSION TO	RET28B	681.	12.42	77.	21.	7.	0.54
+	HYDROGRAPH AT	DIV28B	377.	12.67	36.	11.	4.	0.54
+	2 COMBINED AT	CPE28B	942.	14.58	392.	121.	40.	6.77
+	ROUTED TO	E28E31	922.	14.92	388.	121.	40.	6.77
+	HYDROGRAPH AT	E25	903.	12.50	161.	53.	18.	0.93
+	DIVERSION TO	RETE25	903.	12.50	161.	53.	18.	0.93
+	HYDROGRAPH AT	DIVE25	0.	0.00	0.	0.	0.	0.93
+	ROUTED TO	E25E29	0.	0.00	0.	0.	0.	0.93
+	HYDROGRAPH AT	E29	1079.	12.50	178.	58.	19.	1.00
+	DIVERSION TO	RETE29	1079.	12.50	134.	37.	12.	1.00
+	HYDROGRAPH AT	DIVE29	640.	12.75	68.	21.	7.	1.00
+	2 COMBINED AT	CPE29	577.	12.75	66.	20.	7.	1.93
+	ROUTED TO	E29E31	303.	13.17	64.	20.	7.	1.93
+	HYDROGRAPH AT	E32	351.	12.25	42.	14.	5.	0.25
+	DIVERSION TO	RETE32	351.	12.25	31.	9.	3.	0.25
+	HYDROGRAPH AT	DIVE32	192.	12.42	17.	5.	2.	0.25
+	ROUTED TO	E32E31	79.	12.83	16.	5.	2.	0.25
+	HYDROGRAPH AT	E31	838.	12.50	137.	45.	15.	0.81
+	DIVERSION TO	RETE31	838.	12.50	101.	28.	9.	0.81
+	HYDROGRAPH AT	DIVE31	466.	12.75	55.	17.	6.	0.81
+	4 COMBINED AT	CPE31	961.	14.92	476.	152.	51.	9.76
+	ROUTED TO	E31E30	947.	15.25	468.	152.	51.	9.76
+	HYDROGRAPH AT	E30B	739.	12.83	162.	51.	17.	0.88
+	DIVERSION TO	RET30B	739.	12.83	123.	34.	11.	0.88
+	HYDROGRAPH AT	DIV30B	415.	13.25	57.	17.	6.	0.88
+	2 COMBINED AT	CPE30	960.	15.25	505.	164.	55.	10.64
+	ROUTED TO	E30E26	958.	15.33	503.	164.	55.	10.64
+	HYDROGRAPH AT	E26B	366.	12.33	49.	15.	5.	0.26
+	DIVERSION TO	RET26B	366.	12.33	37.	10.	3.	0.26
+	HYDROGRAPH AT	DIV26B	178.	12.58	17.	5.	2.	0.26

+		R23R25	135.	13.00	47.	16.	5.	1.00
+	3 COMBINED AT	CPR25	828.	15.83	591.	222.	75.	15.93
+	ROUTED TO	R25R24	828.	15.92	591.	222.	75.	15.93
+	HYDROGRAPH AT	R19	1566.	12.50	263.	88.	29.	1.53
+	DIVERSION TO	RETR19	1566.	12.50	194.	55.	18.	1.53
+	HYDROGRAPH AT	DIVR19	875.	12.75	110.	34.	11.	1.53
+	DIVERSION TO	DETR19	704.	12.75	36.	9.	3.	1.53
+	HYDROGRAPH AT	DIV19R	171.	12.67	74.	25.	8.	1.53
+	ROUTED TO	R19R24	160.	13.92	70.	25.	8.	1.53
+	HYDROGRAPH AT	R24	346.	12.33	48.	16.	5.	0.29
+	DIVERSION TO	RETR24	346.	12.33	36.	10.	3.	0.29
+	HYDROGRAPH AT	DIVR24	196.	12.58	19.	6.	2.	0.29
+	3 COMBINED AT	CPR24	865.	15.75	649.	245.	82.	17.75
+	ROUTED TO	R24EM4	860.	15.92	647.	245.	82.	17.75
+	HYDROGRAPH AT	EMF4	119.	12.08	7.	2.	1.	0.06
+	3 COMBINED AT	CPEMF4	1800.	13.42	1207.	475.	164.	55.93

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION E7STOR
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
PLAN 1	1566.00	1574.00	1574.00	1.00	1566.55	0.00	12.	0.	0.00	0.00	0.00
PLAN 2	1566.00	1574.00	1574.00	1.00	1566.52	0.00	12.	0.	0.00	0.00	0.00
PLAN 3	1566.00	1574.00	1574.00	1.00	1566.41	0.00	9.	0.	0.00	0.00	0.00
PLAN 4	1566.00	1574.00	1574.00	1.00	1566.28	0.00	6.	0.	0.00	0.00	0.00
PLAN 5	1566.00	1574.00	1574.00	1.00	1566.28	0.00	6.	0.	0.00	0.00	0.00

PLAN	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
PLAN 6	1566.00	1574.00	1574.00	1.00	1566.10	0.00	2.	0.	0.00	0.00	0.00
PLAN 7	1566.00	1574.00	1574.00	1.00	1566.01	0.00	0.	0.	0.00	0.00	0.00
PLAN 8	1566.00	1574.00	1574.00	1.00	1566.00	0.00	0.	0.	0.00	0.00	0.00
PLAN 9	1566.00	1574.00	1574.00	1.00	1566.00	0.00	0.	0.	0.00	0.00	0.00
1	1311.00	1318.00	1318.00	1.00	1566.00	0.00	0.	0.	0.00	0.00	0.00
PLAN 1	1311.00	1318.00	1318.00	1.00	1311.84	0.00	18.	1.	0.00	12.92	0.00
PLAN 2	1311.00	1318.00	1318.00	1.00	1311.83	0.00	18.	1.	0.00	12.92	0.00
PLAN 3	1311.00	1318.00	1318.00	1.00	1311.81	0.00	18.	1.	0.00	12.92	0.00

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION RITBAS
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 4		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1311.00	1318.00	1318.00				
	STORAGE	0.	693.	693.				
	OUTFLOW	0.	7.	7.				
	RATIO	MAXIMUM	MAXIMUM	MAXIMUM	MAXIMUM	DURATION	TIME OF	TIME OF
	OF	RESERVOIR	DEPTH	STORAGE	OUTFLOW	OVER TOP	MAX OUTFLOW	FAILURE
	PMF	W.S.ELEV	OVER DAM	AC-FT	CFS	HOURS	HOURS	HOURS
	1.00	1311.78	0.00	17.	1.	0.00	12.83	0.00

PLAN 5		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1311.00	1318.00	1318.00				
	STORAGE	0.	693.	693.				
	OUTFLOW	0.	7.	7.				
	RATIO	MAXIMUM	MAXIMUM	MAXIMUM	MAXIMUM	DURATION	TIME OF	TIME OF
	OF	RESERVOIR	DEPTH	STORAGE	OUTFLOW	OVER TOP	MAX OUTFLOW	FAILURE
	PMF	W.S.ELEV	OVER DAM	AC-FT	CFS	HOURS	HOURS	HOURS
	1.00	1311.74	0.00	16.	1.	0.00	12.75	0.00

PLAN 6		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1311.00	1318.00	1318.00				
	STORAGE	0.	693.	693.				
	OUTFLOW	0.	7.	7.				
	RATIO	MAXIMUM	MAXIMUM	MAXIMUM	MAXIMUM	DURATION	TIME OF	TIME OF
	OF	RESERVOIR	DEPTH	STORAGE	OUTFLOW	OVER TOP	MAX OUTFLOW	FAILURE
	PMF	W.S.ELEV	OVER DAM	AC-FT	CFS	HOURS	HOURS	HOURS
	1.00	1311.72	0.00	16.	1.	0.00	12.75	0.00

PLAN 7		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1311.00	1318.00	1318.00				
	STORAGE	0.	693.	693.				
	OUTFLOW	0.	7.	7.				
	RATIO	MAXIMUM	MAXIMUM	MAXIMUM	MAXIMUM	DURATION	TIME OF	TIME OF
	OF	RESERVOIR	DEPTH	STORAGE	OUTFLOW	OVER TOP	MAX OUTFLOW	FAILURE
	PMF	W.S.ELEV	OVER DAM	AC-FT	CFS	HOURS	HOURS	HOURS
	1.00	1311.71	0.00	16.	1.	0.00	12.75	0.00

PLAN 8		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1311.00	1318.00	1318.00				
	STORAGE	0.	693.	693.				
	OUTFLOW	0.	7.	7.				
	RATIO	MAXIMUM	MAXIMUM	MAXIMUM	MAXIMUM	DURATION	TIME OF	TIME OF
	OF	RESERVOIR	DEPTH	STORAGE	OUTFLOW	OVER TOP	MAX OUTFLOW	FAILURE
	PMF	W.S.ELEV	OVER DAM	AC-FT	CFS	HOURS	HOURS	HOURS
	1.00	1311.70	0.00	15.	1.	0.00	12.75	0.00

PLAN 9		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1311.00	1318.00	1318.00				
	STORAGE	0.	693.	693.				
	OUTFLOW	0.	7.	7.				
	RATIO	MAXIMUM	MAXIMUM	MAXIMUM	MAXIMUM	DURATION	TIME OF	TIME OF
	OF	RESERVOIR	DEPTH	STORAGE	OUTFLOW	OVER TOP	MAX OUTFLOW	FAILURE
	PMF	W.S.ELEV	OVER DAM	AC-FT	CFS	HOURS	HOURS	HOURS
	1.00	1311.69	0.00	15.	1.	0.00	12.75	0.00

*** NORMAL END OF HEC-1 ***

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 * FLOOD HYDROGRAPH PACKAGE (HEC-1) *
 * JUN 1998 *
 * VERSION 4.1 *
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 * RUN DATE 04JUL16 TIME 13:39:43 *
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 * U.S. ARMY CORPS OF ENGINEERS *
 * HYDROLOGIC ENGINEERING CENTER *
 * 609 SECOND STREET *
 * DAVIS, CALIFORNIA 95616 *
 * (916) 756-1104 *
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID 24INT100IC 100-YEAR, 24-hr Interim Phase II Conditions 2016-07-04
2 ID Assuming concrete-lined channel for the following routes:
3 ID E5A14A, E1424A, E1424B, E247A1, E247A2 and E2726A.
4 ID by Parsons Corporation
5 ID
6 ID The model reflects interim drainage conditions for SR 24 and it is based
7 ID on Mesa ADMPU with revisions reflecting development work around the
8 ID corridor.
9 ID This model simulates that the SR 24 corridor extends to Ironwood Dr,
10 ID which would eliminate the need to intercept runoff from subbasins
11 ID E5A, E6A and RTE4E5.
12 ID Therefore, subbasins E5A and E5B, and E6A and E6B were reconfigured to
13 ID match the layout, characteristics and hydrologic connectivity of
14 ID subbasins E5 and E6 in the existing condition model (24EX100). Also,
15 ID diversion DRE6 was reintroduced to simulate the cascading flows
16 ID east of Ironwood Dr.
17 ID *****
18 ID FUTEMADMP24 20110519 - EMADMPU 24-hr Future Conditions 20110519
19 ID Flood Control District of Maricopa County
20 ID 100 YEAR
21 ID 24 Hour Storm
22 ID Unit Hydrograph: S-Graph
23 ID 08/05/2011
24 ID
25 IT 5 0 0 2000
26 IN 15
27 IO 5
*DIAGRAM
*
28 JD 3.579 0.0001
29 PC 0.000 0.002 0.005 0.008 0.011 0.014 0.017 0.020 0.023 0.026
30 PC 0.029 0.032 0.035 0.038 0.041 0.044 0.048 0.052 0.056 0.060
31 PC 0.064 0.068 0.072 0.076 0.080 0.085 0.090 0.095 0.100 0.105
32 PC 0.110 0.115 0.120 0.126 0.133 0.140 0.147 0.155 0.163 0.172
33 PC 0.181 0.191 0.203 0.218 0.236 0.257 0.283 0.307 0.337 0.370
34 PC 0.735 0.758 0.776 0.791 0.804 0.815 0.825 0.834 0.842 0.849
35 PC 0.856 0.863 0.869 0.875 0.881 0.887 0.893 0.898 0.903 0.908
36 PC 0.913 0.918 0.922 0.926 0.930 0.934 0.938 0.942 0.946 0.950
37 PC 0.953 0.956 0.959 0.962 0.965 0.968 0.971 0.974 0.977 0.980
38 PC 0.983 0.986 0.989 0.992 0.995 0.998 1.000
39 JD 3.561 1.0
40 JD 3.490 5.0
41 JD 3.400 10.0
42 JD 3.286 20.0
43 JD 3.221 30.0
44 JD 3.175 40.0
45 JD 3.139 50.0
46 JD 3.114 60.0
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1 HEC-1 INPUT PAGE 2

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
47 KK P1 BASIN
48 KM
49 KM Used the unit hydrograph for undeveloped conditions
50 KM by Parsons Corporation 2015-11
51 BA 0.387
52 LG 0.35 0.35 3.95 0.47 0
53 UI 0 29 29 99 134 162 189 226 301 369
54 UI 298 248 210 175 144 108 65 50 45 29
55 UI 26 9 9 9 9 9 9 0 0 0
56 UI 0 0 0 0 0 0 0 0 0 0
57 UI 0 0 0 0 0 0 0 0 0 0
  
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WARNING --- ROUTED OUTFLOW (489.) IS GREATER THAN MAXIMUM OUTFLOW (487.) IN STORAGE-OUTFLOW TABLE
 WARNING --- ROUTED OUTFLOW (491.) IS GREATER THAN MAXIMUM OUTFLOW (487.) IN STORAGE-OUTFLOW TABLE
 WARNING --- ROUTED OUTFLOW (523.) IS GREATER THAN MAXIMUM OUTFLOW (487.) IN STORAGE-OUTFLOW TABLE
 WARNING --- ROUTED OUTFLOW (513.) IS GREATER THAN MAXIMUM OUTFLOW (487.) IN STORAGE-OUTFLOW TABLE
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 WARNING EXCESS AT PONDING LESS THAN ZERO PERIOD. EXCESS SET TO ZERO

1
 RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

+	OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
					6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT	P1	244.	12.67	32.	8.	3.	0.39		
+	DIVERSION TO	DRPFW	161.	12.67	17.	4.	1.	0.39		
+	HYDROGRAPH AT	DP1PFW	83.	12.67	15.	4.	1.	0.39		
+	ROUTED TO	P1P2	58.	14.50	15.	4.	1.	0.39		
+	HYDROGRAPH AT	P2	326.	12.75	49.	12.	4.	0.58		
+	2 COMBINED AT	CPP2	326.	12.75	65.	16.	5.	0.96		
+	ROUTED TO	P2P4	310.	13.00	64.	16.	5.	0.96		
+	HYDROGRAPH AT	P4	536.	12.50	79.	24.	8.	0.50		
+	DIVERSION TO	RETP4	536.	12.50	79.	24.	8.	0.50		
+	HYDROGRAPH AT	DIVP4	0.	0.00	0.	0.	0.	0.50		
+	2 COMBINED AT	CPP4	310.	13.00	64.	16.	5.	1.46		
+	ROUTED TO	P4P6	289.	13.25	64.	16.	5.	1.46		
+	HYDROGRAPH AT	P6	456.	12.67	79.	24.	8.	0.50		
+	DIVERSION TO	RETP6	456.	12.67	79.	24.	8.	0.50		
+	HYDROGRAPH AT	DIVP6	0.	0.00	0.	0.	0.	0.50		
+	2 COMBINED AT	CPP6	289.	13.25	64.	16.	5.	1.96		
+	ROUTED TO	P6GM8	273.	13.42	63.	16.	5.	1.96		
+	ROUTED TO	GM8G10	265.	13.58	63.	16.	5.	1.96		
+	HYDROGRAPH AT	DRPFW	161.	12.67	17.	4.	1.	0.39		
+	ROUTED TO	P1PFW	135.	12.83	17.	4.	1.	0.39		
+	HYDROGRAPH AT	P3	242.	13.00	43.	11.	4.	0.52		
+	2 COMBINED AT	CPP3	363.	12.92	60.	15.	5.	0.91		
+	ROUTED TO	P3P5	358.	13.00	60.	15.	5.	0.91		
+	HYDROGRAPH AT									

+		P5	268.	12.50	41.	12.	4.	0.25
+	DIVERSION TO	RETP5	268.	12.50	33.	9.	3.	0.25
+	HYDROGRAPH AT	DIVP5	121.	12.92	12.	4.	1.	0.25
+	2 COMBINED AT	CPP5	463.	12.92	71.	19.	6.	1.16
+	ROUTED TO	P5P7	447.	13.00	71.	19.	6.	1.16
+	HYDROGRAPH AT	P7	485.	12.50	74.	22.	7.	0.43
+	DIVERSION TO	RETP7	485.	12.50	58.	16.	5.	0.43
+	HYDROGRAPH AT	DIVP7	212.	12.92	22.	6.	2.	0.43
+	3 COMBINED AT	CPP7	586.	13.00	150.	40.	13.	3.17
+	ROUTED TO	P7GM14	569.	13.25	149.	40.	13.	3.17
+	HYDROGRAPH AT	GM1	435.	12.42	53.	14.	5.	0.34
+	HYDROGRAPH AT	GM2	1023.	12.33	130.	42.	14.	0.68
+	HYDROGRAPH AT	GM3	651.	12.08	69.	23.	8.	0.29
+	3 COMBINED AT	CPG123	1747.	12.17	250.	78.	26.	1.32
+	DIVERSION TO	RETG1	1747.	12.17	188.	51.	17.	1.32
+	HYDROGRAPH AT	DIVG1	847.	12.58	89.	26.	9.	1.32
+	ROUTED TO	GM1T5	640.	12.67	88.	26.	9.	1.32
+	HYDROGRAPH AT	GM5	349.	12.17	42.	13.	4.	0.18
+	DIVERSION TO	RETG5	325.	12.17	24.	7.	2.	0.18
+	HYDROGRAPH AT	DIVG5	334.	12.25	23.	7.	2.	0.18
+	2 COMBINED AT	CPG5	686.	12.67	109.	33.	11.	1.49
+	ROUTED TO	GM5T7	571.	12.92	107.	33.	11.	1.49
+	HYDROGRAPH AT	GM6	777.	12.17	73.	22.	7.	0.37
+	DIVERSION TO	RETG6	777.	12.17	50.	14.	5.	0.37
+	HYDROGRAPH AT	DIVG6	552.	12.25	30.	9.	3.	0.37
+	HYDROGRAPH AT	GM7	290.	12.33	32.	9.	3.	0.22
+	DIVERSION TO	RETG7	290.	12.33	28.	7.	2.	0.22
+	HYDROGRAPH AT	DIVG7	71.	12.75	5.	2.	1.	0.22
+	2 COMBINED AT	CPG7A	552.	12.25	36.	10.	3.	0.58
+	2 COMBINED AT	CPG7B	633.	12.92	139.	42.	14.	2.08
+	ROUTED TO	GM7T9	585.	13.00	137.	42.	14.	2.08
+	HYDROGRAPH AT	GM8	798.	12.33	100.	32.	11.	0.56
+	DIVERSION TO	RETG8	798.	12.33	73.	20.	7.	0.56
+	HYDROGRAPH AT	DIVG8	516.	12.50	38.	11.	4.	0.56
+	HYDROGRAPH AT	GM9	177.	12.17	13.	4.	1.	0.09

+	DIVERSION TO	RETG9	177.	12.17	13.	3.	1.	0.09
+	HYDROGRAPH AT	DIVG9	5.	12.75	2.	1.	0.	0.09
+	2 COMBINED AT	CPG9A	516.	12.50	40.	12.	4.	0.65
+	HYDROGRAPH AT	GM10	409.	12.33	53.	16.	5.	0.28
+	DIVERSION TO	RETG10	409.	12.33	32.	9.	3.	0.28
+	HYDROGRAPH AT	DIVG10	329.	12.42	26.	7.	2.	0.28
+	HYDROGRAPH AT	GM11	108.	12.25	10.	3.	1.	0.08
+	DIVERSION TO	RETG11	108.	12.25	10.	3.	1.	0.08
+	HYDROGRAPH AT	DIVG11	4.	13.33	1.	1.	0.	0.08
+	2 COMBINED AT	CPG11	329.	12.42	28.	8.	3.	0.36
+	3 COMBINED AT	CPG9B	946.	12.50	198.	60.	20.	3.08
+	ROUTED TO	GM9T14	723.	12.75	195.	60.	20.	3.08
+	HYDROGRAPH AT	GM12	275.	12.08	29.	10.	3.	0.12
+	DIVERSION TO	RETG12	217.	12.00	16.	5.	2.	0.12
+	HYDROGRAPH AT	DIVG12	255.	12.17	17.	5.	2.	0.12
+	ROUTED TO	G12T13	130.	12.33	17.	5.	2.	0.12
+	HYDROGRAPH AT	GM13	596.	12.08	55.	18.	6.	0.29
+	DIVERSION TO	RETG13	596.	12.08	41.	11.	4.	0.29
+	HYDROGRAPH AT	DIVG13	376.	12.25	21.	6.	2.	0.29
+	2 COMBINED AT	CPG13	471.	12.25	38.	11.	4.	0.41
+	ROUTED TO	G13T14	366.	12.33	38.	11.	4.	0.41
+	HYDROGRAPH AT	GM14	678.	12.17	67.	22.	7.	0.35
+	DIVERSION TO	RETG14	676.	12.17	46.	13.	4.	0.35
+	HYDROGRAPH AT	DIVG14	546.	12.25	31.	9.	3.	0.35
+	2 COMBINED AT	CPG14A	708.	12.25	69.	21.	7.	0.76
+	2 COMBINED AT	CPG14B	849.	12.75	256.	80.	27.	3.84
+	2 COMBINED AT	CPG14C	1156.	13.25	379.	113.	38.	7.01
+	ROUTED TO	G14E26	1151.	13.25	379.	113.	38.	7.01
+	HYDROGRAPH AT	E1	472.	12.83	73.	18.	6.	0.89
+	DIVERSION TO	DRE2	383.	12.83	56.	14.	5.	0.89
+	HYDROGRAPH AT	DE15	88.	12.83	18.	4.	1.	0.89
+	ROUTED TO	E1E10	55.	15.00	18.	4.	1.	0.89
+	HYDROGRAPH AT	E10	411.	12.92	68.	17.	6.	0.82
+	2 COMBINED AT	CPE10	435.	12.92	85.	21.	7.	1.71

+	ROUTED TO	E10E17	402.	13.08	84.	21.	7.	1.71
+	HYDROGRAPH AT	E17	287.	12.50	41.	13.	4.	0.27
+	DIVERSION TO	RETE17	287.	12.50	34.	9.	3.	0.27
+	HYDROGRAPH AT	DIVE17	123.	12.83	11.	3.	1.	0.27
+	2 COMBINED AT	CPE17	452.	13.08	95.	24.	8.	1.98
+	ROUTED TO	E17E21	433.	13.25	94.	24.	8.	1.98
+	HYDROGRAPH AT	E21	341.	12.50	51.	15.	5.	0.31
+	DIVERSION TO	RETE21	341.	12.50	38.	10.	3.	0.31
+	HYDROGRAPH AT	DIVE21	175.	12.83	17.	5.	2.	0.31
+	2 COMBINED AT	CPE21A	474.	13.25	110.	29.	10.	2.29
+	ROUTED TO	E21G20	465.	13.25	110.	29.	10.	2.29
+	HYDROGRAPH AT	DRE2	383.	12.83	56.	14.	5.	0.89
+	ROUTED TO	RTE1E2	316.	13.17	56.	14.	5.	0.89
+	HYDROGRAPH AT	E2	409.	12.92	68.	17.	6.	0.78
+	2 COMBINED AT	CPE2	627.	13.00	122.	31.	10.	1.67
+	DIVERSION TO	DRE3	408.	13.00	60.	15.	5.	1.67
+	HYDROGRAPH AT	DE2S	219.	13.00	62.	16.	5.	1.67
+	ROUTED TO	E2E11	173.	15.83	62.	16.	5.	1.67
+	HYDROGRAPH AT	E11	318.	12.83	50.	12.	4.	0.60
+	2 COMBINED AT	CPE11	311.	12.83	100.	28.	9.	2.27
+	ROUTED TO	E11E18	236.	13.58	97.	28.	9.	2.27
+	HYDROGRAPH AT	E18	320.	12.33	36.	10.	3.	0.22
+	DIVERSION TO	RETE18	1.	4.17	1.	0.	0.	0.22
+	HYDROGRAPH AT	DIVE18	320.	12.33	36.	10.	3.	0.22
+	2 COMBINED AT	CPE18	316.	12.33	118.	37.	12.	2.49
+	ROUTED TO	E18E21	287.	12.50	117.	37.	12.	2.49
+	2 COMBINED AT	CPE21B	576.	13.50	223.	66.	22.	3.90
+	ROUTED TO	G20G21	573.	13.58	221.	66.	22.	3.90
+	HYDROGRAPH AT	DRE3	408.	13.00	60.	15.	5.	1.67
+	ROUTED TO	RTE2E3	365.	13.33	60.	15.	5.	1.67
+	HYDROGRAPH AT	E3	935.	13.25	209.	52.	17.	2.23
+	2 COMBINED AT	E25E3	1259.	13.25	264.	66.	22.	3.90
+	DIVERSION TO	DRE4N	804.	13.25	125.	31.	10.	3.90
+	HYDROGRAPH AT	DE3S	455.	13.25	139.	35.	12.	3.90
+	ROUTED TO							

+		E3E12	401.	14.50	139.	35.	12.	3.90
+	HYDROGRAPH AT	E12	318.	12.92	55.	14.	5.	0.57
+	2 COMBINED AT	CPE12	546.	12.92	191.	48.	16.	4.47
+	ROUTED TO	E12E19	486.	13.67	191.	48.	16.	4.47
+	HYDROGRAPH AT	E19	234.	12.25	23.	6.	2.	0.14
+	2 COMBINED AT	CPE19	488.	13.67	212.	54.	18.	4.61
+	ROUTED TO	E1922E	467.	14.00	212.	54.	18.	4.61
+	HYDROGRAPH AT	22E	149.	12.25	15.	4.	1.	0.09
+	HYDROGRAPH AT	E20	159.	12.50	20.	5.	2.	0.17
+	ROUTED TO	E2022E	129.	12.75	20.	5.	2.	0.17
+	3 COMBINED AT	CP22E	472.	14.00	245.	63.	21.	4.87
+	ROUTED TO	22EE22	465.	14.17	245.	63.	21.	4.87
+	HYDROGRAPH AT	E22	223.	12.67	33.	8.	3.	0.16
+	3 COMBINED AT	CPE22	940.	13.83	477.	133.	44.	7.25
+	ROUTED TO	E22G22	931.	14.00	473.	133.	44.	7.25
+	HYDROGRAPH AT	GM21	379.	12.25	50.	17.	6.	0.21
+	DIVERSION TO	RETG21	360.	12.17	30.	9.	3.	0.21
+	HYDROGRAPH AT	DIVG21	347.	12.33	28.	8.	3.	0.21
+	ROUTED TO	G21T22	298.	12.42	28.	8.	3.	0.21
+	HYDROGRAPH AT	GM22	208.	12.17	24.	8.	3.	0.09
+	DIVERSION TO	RETG22	199.	12.08	14.	4.	1.	0.09
+	HYDROGRAPH AT	DIVG22	177.	12.17	13.	4.	1.	0.09
+	2 COMBINED AT	CPG22A	347.	12.42	41.	12.	4.	0.31
+	HYDROGRAPH AT	GM16	93.	12.33	12.	4.	1.	0.07
+	DIVERSION TO	RETG16	93.	12.33	9.	2.	1.	0.07
+	HYDROGRAPH AT	DIVG16	42.	12.58	4.	1.	0.	0.07
+	ROUTED TO	G16T19	29.	12.75	4.	1.	0.	0.07
+	HYDROGRAPH AT	GM18	274.	12.25	31.	10.	3.	0.17
+	DIVERSION TO	RETG18	274.	12.25	23.	6.	2.	0.17
+	HYDROGRAPH AT	DIVG18	178.	12.42	12.	4.	1.	0.17
+	2 COMBINED AT	CPG18	178.	12.42	16.	5.	2.	0.24
+	HYDROGRAPH AT	GM19	174.	12.17	15.	4.	1.	0.09
+	DIVERSION TO	RETG19	174.	12.17	11.	3.	1.	0.09
+	HYDROGRAPH AT	DIVG19	77.	12.33	5.	1.	0.	0.09
+	2 COMBINED AT	CPG19A	218.	12.42	21.	6.	2.	0.33

+	HYDROGRAPH AT	GM20	359.	12.17	39.	12.	4.	0.18
+	DIVERSION TO	RETG20	359.	12.17	27.	7.	2.	0.18
+	HYDROGRAPH AT	DIVG20	244.	12.33	16.	5.	2.	0.18
+	2 COMBINED AT	CPG19B	368.	12.42	37.	11.	4.	0.51
+	3 COMBINED AT	CPG22B	970.	14.00	536.	153.	51.	8.06
+	ROUTED TO	G22E26	940.	14.33	534.	153.	51.	8.06
+	HYDROGRAPH AT	DRE4N	804.	13.25	125.	31.	10.	3.90
+	ROUTED TO	RTE3E4	750.	13.42	125.	31.	10.	3.90
+	HYDROGRAPH AT	E4N	154.	12.92	25.	6.	2.	0.31
+	2 COMBINED AT	CPE4N	813.	13.42	149.	37.	12.	4.21
+	DIVERSION TO	DRE4	651.	13.42	110.	27.	9.	4.21
+	HYDROGRAPH AT	DE4NS	162.	13.42	40.	10.	3.	4.21
+	ROUTED TO	E4NE13	131.	15.33	40.	10.	3.	4.21
+	HYDROGRAPH AT	E13	284.	12.83	48.	12.	4.	0.48
+	2 COMBINED AT	CPE13	275.	12.83	86.	22.	7.	4.69
+	ROUTED TO	E13E24	190.	13.92	85.	22.	7.	4.69
+	HYDROGRAPH AT	DRE4	651.	13.42	110.	27.	9.	4.21
+	ROUTED TO	RTE4E4	515.	14.25	109.	27.	9.	4.21
+	HYDROGRAPH AT	E4	462.	13.25	103.	26.	9.	1.20
+	2 COMBINED AT	CPE4	645.	14.17	205.	51.	17.	5.41
+	DIVERSION TO	DRE5	630.	14.17	198.	49.	16.	5.41
+	HYDROGRAPH AT	DE4S	15.	14.17	8.	2.	1.	5.41
+	ROUTED TO	E4E14A	14.	15.17	8.	2.	1.	5.41
+	HYDROGRAPH AT	E14A	170.	12.75	26.	6.	2.	0.48
+	HYDROGRAPH AT	DRE5	630.	14.17	198.	49.	16.	5.41
+	ROUTED TO	RTE4E5	583.	14.42	197.	49.	16.	5.41
+	HYDROGRAPH AT	E5	534.	13.25	117.	29.	10.	1.43
+	2 COMBINED AT	CPE5	789.	13.33	302.	76.	25.	6.84
+	DIVERSION TO	DRE6	356.	13.33	102.	25.	8.	6.84
+	HYDROGRAPH AT	DE5S	433.	13.33	200.	50.	17.	6.84
+	ROUTED TO	ESA14A	423.	13.58	199.	50.	17.	6.84
+	3 COMBINED AT	CPE14A	453.	13.50	228.	58.	19.	7.61
+	ROUTED TO	E1424A	451.	13.58	228.	58.	19.	7.61
+	ROUTED TO	E1424B	449.	13.67	228.	58.	19.	7.61

+	HYDROGRAPH AT	E24A	812.	12.33	110.	36.	12.	0.53
+	DIVERSION TO	RET24A	807.	12.25	70.	20.	7.	0.53
+	HYDROGRAPH AT	DIV24A	704.	12.42	55.	16.	5.	0.53
+	3 COMBINED AT	CP24A	655.	13.75	356.	93.	31.	8.62
+	ROUTED TO	E247A1	652.	13.92	354.	93.	31.	8.62
+	HYDROGRAPH AT	E27A	647.	12.50	115.	37.	12.	0.54
+	DIVERSION TO	RET27A	647.	12.50	76.	21.	7.	0.54
+	HYDROGRAPH AT	DIV27A	478.	12.75	54.	16.	5.	0.54
+	3 COMBINED AT	CPE27A	1549.	12.83	898.	250.	83.	12.81
+	ROUTED TO	E247A2	1561.	12.83	897.	250.	83.	12.81
+	ROUTED TO	E2726A	1522.	13.08	894.	250.	83.	12.81
+	HYDROGRAPH AT	E26A	1093.	12.50	181.	58.	19.	0.87
+	DIVERSION TO	RET26A	1093.	12.50	119.	33.	11.	0.87
+	HYDROGRAPH AT	DIV26A	843.	12.67	84.	24.	8.	0.87
+	2 COMBINED AT	SR24EL	1788.	13.00	957.	269.	90.	13.68
+	DIVERSION TO	1650UP	138.	13.00	5.	1.	0.	13.68
+	HYDROGRAPH AT	802ELS	1650.	13.00	952.	267.	89.	13.68
+	HYDROGRAPH AT	GM17	174.	12.17	18.	6.	2.	0.10
+	DIVERSION TO	RETG17	174.	12.17	18.	6.	2.	0.10
+	HYDROGRAPH AT	DIVG17	0.	0.00	0.	0.	0.	0.10
+	ROUTED TO	G17E26	0.	0.00	0.	0.	0.	0.10
+	3 COMBINED AT	CPE26A	2364.	13.33	1215.	353.	118.	20.80
+	ROUTED TO	80233B	2350.	13.42	1214.	353.	118.	20.80
+	HYDROGRAPH AT	E7	820.	12.92	182.	56.	19.	1.12
+	DIVERSION TO	RETE7	820.	12.92	159.	43.	14.	1.12
+	HYDROGRAPH AT	DIVE7	234.	13.67	43.	13.	4.	1.12
+	ROUTED TO	E75TOR	1.	25.67	1.	1.	0.	1.12
+	ROUTED TO	E7E6	1.	30.00	1.	1.	0.	1.12
+	HYDROGRAPH AT	DRE6	356.	13.33	102.	25.	8.	6.84
+	ROUTED TO	RTE5E6	329.	13.75	102.	25.	8.	6.84
+	HYDROGRAPH AT	E6	1053.	13.42	270.	68.	23.	2.53
+	HYDROGRAPH AT	E8	901.	12.75	180.	57.	19.	1.10
+	DIVERSION TO	RETE8	901.	12.75	149.	41.	14.	1.10
+	HYDROGRAPH AT	DIVE8	378.	13.25	52.	16.	5.	1.10
+	ROUTED TO							

+		E8E6	191.	14.00	50.	16.	5.	1.10
+	3 COMBINED AT	CPE6	1318.	13.50	419.	110.	37.	3.05
+	DIVERSION TO	DRE9	353.	13.50	47.	12.	4.	3.05
+	HYDROGRAPH AT	DE6S	965.	13.50	372.	98.	33.	3.05
+	ROUTED TO	E6E15	935.	14.08	371.	98.	33.	3.05
+	HYDROGRAPH AT	E15	1096.	12.33	154.	51.	17.	0.78
+	DIVERSION TO	RETE15	1096.	12.33	122.	34.	11.	0.78
+	HYDROGRAPH AT	DIVE15	431.	12.67	54.	17.	6.	0.78
+	HYDROGRAPH AT	DRE9	353.	13.50	47.	12.	4.	3.05
+	ROUTED TO	RTE6E9	316.	13.75	47.	12.	4.	3.05
+	HYDROGRAPH AT	E9	968.	12.42	147.	48.	16.	0.72
+	DIVERSION TO	RETE9	968.	12.42	118.	33.	11.	0.72
+	HYDROGRAPH AT	DIVE9	372.	12.75	49.	15.	5.	0.72
+	2 COMBINED AT	CPE9	408.	13.67	103.	29.	10.	0.72
+	DIVERSION TO	DRR5	221.	13.67	36.	9.	3.	0.72
+	HYDROGRAPH AT	DE9S	186.	13.67	67.	20.	7.	0.72
+	ROUTED TO	E9E16	175.	14.08	65.	20.	7.	0.72
+	HYDROGRAPH AT	E16	582.	12.33	79.	26.	9.	0.40
+	DIVERSION TO	RETE16	582.	12.33	64.	18.	6.	0.40
+	HYDROGRAPH AT	DIVE16	213.	12.58	26.	8.	3.	0.40
+	2 COMBINED AT	CPE16	201.	12.58	90.	28.	9.	1.12
+	ROUTED TO	E16E15	197.	14.25	89.	28.	9.	1.12
+	3 COMBINED AT	CPE15	1147.	14.08	497.	139.	46.	4.95
+	ROUTED TO	E1524B	1137.	14.33	494.	139.	46.	4.95
+	HYDROGRAPH AT	E5B	447.	12.25	57.	19.	6.	0.29
+	DIVERSION TO	RETE5B	447.	12.25	45.	13.	4.	0.29
+	HYDROGRAPH AT	DIVE5B	204.	12.50	21.	7.	2.	0.29
+	ROUTED TO	E5E14B	89.	12.92	20.	7.	2.	0.29
+	HYDROGRAPH AT	E14B	884.	12.25	109.	36.	12.	0.53
+	DIVERSION TO	RET14B	884.	12.25	88.	24.	8.	0.53
+	HYDROGRAPH AT	DIV14B	372.	12.50	37.	12.	4.	0.53
+	2 COMBINED AT	CP14B	371.	12.50	57.	18.	6.	0.81
+	ROUTED TO	E14E24	180.	13.00	55.	18.	6.	0.81
+	HYDROGRAPH AT	E24B	788.	12.25	100.	32.	11.	0.46
+	DIVERSION TO	RET24B	788.	12.25	70.	20.	7.	0.46

+	HYDROGRAPH AT	DIV24B	572.	12.42	43.	13.	4.	0.46
+	3 COMBINED AT	CPE24B	1205.	14.25	567.	164.	55.	6.23
+	ROUTED TO	E24E28	1192.	14.58	562.	164.	55.	6.23
+	HYDROGRAPH AT	E28B	773.	12.42	116.	37.	12.	0.54
+	DIVERSION TO	RET28B	773.	12.42	76.	21.	7.	0.54
+	HYDROGRAPH AT	DIV28B	555.	12.58	54.	16.	5.	0.54
+	2 COMBINED AT	CPE28B	1209.	14.50	602.	177.	59.	6.77
+	ROUTED TO	E28E31	1195.	14.83	597.	177.	59.	6.77
+	HYDROGRAPH AT	E25	1038.	12.50	184.	60.	20.	0.93
+	DIVERSION TO	RETE25	1038.	12.50	184.	56.	19.	0.93
+	HYDROGRAPH AT	DIVE25	23.	18.08	16.	4.	1.	0.93
+	ROUTED TO	E25E29	20.	19.75	16.	4.	1.	0.93
+	HYDROGRAPH AT	E29	1237.	12.50	203.	66.	22.	1.00
+	DIVERSION TO	RETE29	1237.	12.50	132.	37.	12.	1.00
+	HYDROGRAPH AT	DIVE29	906.	12.67	99.	29.	10.	1.00
+	2 COMBINED AT	CPE29	897.	12.67	96.	32.	11.	1.93
+	ROUTED TO	E29E31	573.	13.00	94.	32.	11.	1.93
+	HYDROGRAPH AT	E32	404.	12.25	48.	16.	5.	0.25
+	DIVERSION TO	RETE32	394.	12.17	30.	9.	3.	0.25
+	HYDROGRAPH AT	DIVE32	344.	12.33	25.	7.	2.	0.25
+	ROUTED TO	E32E31	155.	12.75	24.	7.	2.	0.25
+	HYDROGRAPH AT	E31	964.	12.42	157.	52.	17.	0.81
+	DIVERSION TO	RETE31	964.	12.42	100.	28.	9.	0.81
+	HYDROGRAPH AT	DIVE31	835.	12.58	79.	23.	8.	0.81
+	4 COMBINED AT	CPE31	1272.	14.75	741.	225.	75.	9.76
+	ROUTED TO	E31E30	1257.	15.08	730.	225.	75.	9.76
+	HYDROGRAPH AT	E30B	844.	12.83	186.	58.	19.	0.88
+	DIVERSION TO	RET30B	844.	12.83	122.	34.	11.	0.88
+	HYDROGRAPH AT	DIV30B	619.	13.08	84.	24.	8.	0.88
+	2 COMBINED AT	CPE30	1316.	13.33	793.	243.	81.	10.64
+	ROUTED TO	E30E26	1294.	13.42	789.	243.	81.	10.64
+	HYDROGRAPH AT	E26B	415.	12.33	56.	18.	6.	0.26
+	DIVERSION TO	RET26B	415.	12.33	37.	10.	3.	0.26
+	HYDROGRAPH AT	DIV26B	280.	12.50	26.	7.	2.	0.26

+	2 COMBINED AT	CPE26	1311.	13.42	796.	248.	83.	10.90
	ROUTED TO	E26E33	1274.	15.50	787.	248.	83.	10.90
+	HYDROGRAPH AT	E33B	1304.	12.33	183.	59.	20.	0.85
+	DIVERSION TO	RET33B	1304.	12.33	120.	34.	11.	0.85
+	HYDROGRAPH AT	DIV33B	972.	12.50	86.	25.	8.	0.85
+	3 COMBINED AT	CPE33B	1284.	15.50	797.	264.	88.	12.87
+	ROUTED TO	E33P9A	1279.	15.58	793.	264.	88.	12.87
+	ROUTED TO	E33P9B	1272.	15.67	791.	263.	88.	12.87
+	HYDROGRAPH AT	P9	1513.	12.42	268.	90.	30.	1.12
+	DIVERSION TO	RETP9	137.	11.50	53.	18.	6.	1.12
+	HYDROGRAPH AT	DIVP9	1513.	12.42	255.	72.	24.	1.12
+	2 COMBINED AT	CPP9	1421.	12.50	947.	326.	109.	13.99
+	ROUTED TO	P9EMF1	1302.	15.83	939.	326.	109.	13.99
+	HYDROGRAPH AT	EMF1B	1442.	12.42	233.	76.	25.	1.04
+	DIVERSION TO	REMF1B	1442.	12.42	152.	43.	14.	1.04
+	HYDROGRAPH AT	DEMF1B	1142.	12.58	114.	34.	11.	1.04
+	2 COMBINED AT	CPEMF1	2089.	12.67	1022.	351.	117.	15.03
+	ROUTED TO	EM1EM2	2055.	12.83	1021.	351.	117.	15.03
+	HYDROGRAPH AT	EMF2	1610.	12.83	393.	130.	43.	1.85
+	DIVERSION TO	RETEM2	1532.	12.83	195.	49.	16.	1.85
+	HYDROGRAPH AT	DIVEM2	1181.	13.17	198.	81.	27.	1.85
+	2 COMBINED AT	CPEMF2	2098.	12.83	1165.	406.	140.	16.88
+	ROUTED TO	EM2M3A	1916.	12.92	1160.	406.	140.	16.88
+	ROUTED TO	EM2M3B	1812.	13.00	1156.	406.	140.	16.88
+	HYDROGRAPH AT	EMF3	1324.	12.75	277.	91.	30.	1.49
+	DIVERSION TO	RETEM3	812.	12.33	98.	30.	10.	1.49
+	HYDROGRAPH AT	DIVEM3	1324.	12.75	218.	61.	20.	1.49
+	2 COMBINED AT	CPEMF3	2728.	12.92	1325.	455.	156.	18.37
+	ROUTED TO	EMF3RB	2683.	13.00	1321.	455.	156.	18.37
+	HYDROGRAPH AT	RITBAS	693.	12.08	44.	11.	4.	0.29
+	ROUTED TO	RITBAS	1.	12.92	1.	1.	1.	0.29
+	2 COMBINED AT	CPRITB	2683.	13.00	1320.	455.	157.	18.66
+	ROUTED TO	RBEMF4	2395.	13.25	1295.	455.	156.	18.66
+	HYDROGRAPH AT	R2	612.	12.67	101.	29.	10.	0.68
	DIVERSION TO							

+		RETR2	398.	12.33	33.	9.	3.	0.68
	HYDROGRAPH AT	DIVR2	612.	12.67	76.	20.	7.	0.68
+	HYDROGRAPH AT	R3	358.	12.58	55.	16.	5.	0.41
+	DIVERSION TO	RETR3	330.	12.50	29.	8.	3.	0.41
+	HYDROGRAPH AT	DIVR3	352.	12.67	30.	8.	3.	0.41
+	2 COMBINED AT	CPR2R3	962.	12.67	105.	28.	9.	1.09
	ROUTED TO	R2R3R6	467.	14.17	100.	28.	9.	1.09
+	HYDROGRAPH AT	R6	409.	12.67	62.	18.	6.	0.50
+	2 COMBINED AT	CPR6	470.	14.25	155.	45.	15.	1.59
	ROUTED TO	R6R9	434.	14.58	154.	45.	15.	1.59
+	HYDROGRAPH AT	R9	840.	12.33	123.	41.	14.	0.59
+	DIVERSION TO	RETR9	840.	12.33	97.	27.	9.	0.59
+	HYDROGRAPH AT	DIVR9	351.	12.67	45.	14.	5.	0.59
+	2 COMBINED AT	CPR9	609.	12.67	195.	58.	20.	2.19
	ROUTED TO	R9R11	476.	13.25	194.	58.	20.	2.19
+	HYDROGRAPH AT	R11	1179.	12.50	184.	58.	19.	0.99
+	DIVERSION TO	RETR11	1179.	12.50	123.	34.	11.	0.99
+	HYDROGRAPH AT	DIVR11	859.	12.67	83.	24.	8.	0.99
+	HYDROGRAPH AT	DRR5	221.	13.67	36.	9.	3.	0.72
+	HYDROGRAPH AT	R5	546.	12.50	72.	21.	7.	0.50
+	DIVERSION TO	RETR5	4.	4.67	2.	1.	0.	0.50
+	HYDROGRAPH AT	DIVR5	546.	12.50	72.	21.	7.	0.50
+	2 COMBINED AT	CPR5	544.	12.50	107.	29.	10.	1.22
	ROUTED TO	R5R8	470.	12.92	107.	29.	10.	1.22
+	HYDROGRAPH AT	R8	741.	12.42	115.	39.	13.	0.55
+	DIVERSION TO	RETR8	741.	12.42	91.	25.	8.	0.55
+	HYDROGRAPH AT	DIVR8	366.	12.67	42.	13.	4.	0.55
+	2 COMBINED AT	CPR8	721.	12.67	143.	42.	14.	1.77
	ROUTED TO	R8R11	582.	13.33	143.	42.	14.	1.77
+	3 COMBINED AT	CPR11	1147.	13.25	400.	119.	40.	4.95
	ROUTED TO	R11R13	1049.	13.75	396.	119.	40.	4.95
+	HYDROGRAPH AT	R13	708.	12.33	94.	31.	10.	0.50
+	DIVERSION TO	RETR13	705.	12.25	60.	17.	6.	0.50
+	HYDROGRAPH AT	DIVR13	599.	12.42	48.	14.	5.	0.50
+	2 COMBINED AT	CPR13	1071.	13.75	431.	131.	44.	5.45

+	ROUTED TO	R13R16	1005.	14.25	428.	131.	44.	5.45
+	HYDROGRAPH AT	R16	765.	12.25	105.	35.	12.	0.50
+	DIVERSION TO	RETR16	765.	12.25	65.	19.	6.	0.50
+	HYDROGRAPH AT	DIVR16	604.	12.42	56.	17.	6.	0.50
+	2 COMBINED AT	CPR16	1025.	14.25	470.	145.	49.	5.95
+	ROUTED TO	R16R21	928.	15.33	464.	145.	49.	5.95
+	HYDROGRAPH AT	R21	757.	12.67	133.	41.	14.	0.84
+	DIVERSION TO	RETR21	305.	12.17	30.	9.	3.	0.84
+	HYDROGRAPH AT	DIVR21	757.	12.67	117.	32.	11.	0.84
+	HYDROGRAPH AT	R1	1372.	12.58	214.	66.	22.	1.45
+	DIVERSION TO	RETR1	1372.	12.58	187.	51.	17.	1.45
+	HYDROGRAPH AT	DIVR1	308.	13.08	48.	15.	5.	1.45
+	ROUTED TO	R1R4	108.	15.25	42.	15.	5.	1.45
+	HYDROGRAPH AT	R4	817.	12.58	106.	28.	9.	1.00
+	2 COMBINED AT	CPR4	802.	12.58	131.	41.	14.	2.45
+	ROUTED TO	R4R7	621.	13.08	130.	41.	14.	2.45
+	HYDROGRAPH AT	R7	965.	12.58	157.	49.	16.	1.00
+	DIVERSION TO	RETR7	938.	12.50	85.	24.	8.	1.00
+	HYDROGRAPH AT	DIVR7	890.	12.67	89.	25.	8.	1.00
+	2 COMBINED AT	CPR7	1259.	12.67	213.	65.	22.	3.45
+	ROUTED TO	R7R10	1040.	13.33	209.	65.	22.	3.45
+	HYDROGRAPH AT	R10	781.	12.83	161.	50.	17.	1.01
+	DIVERSION TO	RETR10	781.	12.83	129.	35.	12.	1.01
+	HYDROGRAPH AT	DIVR10	358.	13.33	50.	15.	5.	1.01
+	2 COMBINED AT	CPR10	1384.	13.33	252.	78.	26.	4.46
+	ROUTED TO	R10R12	1124.	13.67	247.	78.	26.	4.46
+	HYDROGRAPH AT	R12	939.	12.17	114.	39.	13.	0.49
+	DIVERSION TO	RETR12	850.	12.17	70.	20.	7.	0.49
+	HYDROGRAPH AT	DIVR12	887.	12.25	64.	19.	6.	0.49
+	2 COMBINED AT	CPR12	1165.	13.67	297.	96.	32.	4.95
+	ROUTED TO	R12R15	949.	14.58	284.	96.	32.	4.95
+	HYDROGRAPH AT	R15	616.	12.50	90.	28.	9.	0.56
+	DIVERSION TO	RETR15	537.	12.33	40.	12.	4.	0.56
+	HYDROGRAPH AT	DIVR15	616.	12.50	60.	17.	6.	0.56

+	2 COMBINED AT	CPR15	953.	14.58	323.	111.	37.	5.51
+	ROUTED TO	R15R18	901.	15.00	315.	110.	37.	5.51
+	HYDROGRAPH AT	R18	661.	12.67	122.	38.	13.	0.80
+	DIVERSION TO	RETR18	661.	12.67	94.	26.	9.	0.80
+	HYDROGRAPH AT	DIVR18	354.	13.08	40.	12.	4.	0.80
+	2 COMBINED AT	CPR18	907.	15.00	344.	119.	40.	6.30
+	ROUTED TO	R18R22	852.	15.42	338.	119.	40.	6.30
+	HYDROGRAPH AT	R22	794.	12.33	109.	36.	12.	0.57
+	DIVERSION TO	RETR22	794.	12.33	67.	19.	6.	0.57
+	HYDROGRAPH AT	DIVR22	723.	12.42	58.	17.	6.	0.57
+	HYDROGRAPH AT	R14	806.	12.25	101.	34.	11.	0.50
+	DIVERSION TO	RETR14	751.	12.17	59.	17.	6.	0.50
+	HYDROGRAPH AT	DIVR14	746.	12.33	56.	17.	6.	0.50
+	ROUTED TO	R14R17	370.	12.75	55.	17.	6.	0.50
+	HYDROGRAPH AT	R17	497.	12.58	84.	27.	9.	0.49
+	DIVERSION TO	RETR17	497.	12.58	55.	15.	5.	0.49
+	HYDROGRAPH AT	DIVR17	360.	12.75	40.	12.	4.	0.49
+	2 COMBINED AT	CPR17	729.	12.75	94.	28.	9.	0.99
+	ROUTED TO	R17R22	519.	13.08	91.	28.	9.	0.99
+	3 COMBINED AT	CPR22	893.	15.42	444.	157.	53.	7.87
+	ROUTED TO	R22R21	857.	15.67	436.	156.	53.	7.87
+	3 COMBINED AT	CPR21	1527.	15.58	881.	302.	101.	14.65
+	ROUTED TO	R21R25	1477.	15.92	870.	301.	101.	14.65
+	HYDROGRAPH AT	R25	436.	12.25	49.	16.	5.	0.28
+	DIVERSION TO	RETR25	402.	12.17	25.	7.	2.	0.28
+	HYDROGRAPH AT	DIVR25	406.	12.33	30.	8.	3.	0.28
+	HYDROGRAPH AT	R20	562.	12.42	82.	27.	9.	0.50
+	DIVERSION TO	RETR20	562.	12.42	62.	17.	6.	0.50
+	HYDROGRAPH AT	DIVR20	296.	12.67	32.	10.	3.	0.50
+	ROUTED TO	R20R23	141.	13.17	30.	10.	3.	0.50
+	HYDROGRAPH AT	R23	700.	12.33	96.	32.	11.	0.50
+	DIVERSION TO	RETR23	700.	12.33	63.	18.	6.	0.50
+	HYDROGRAPH AT	DIVR23	492.	12.50	47.	14.	5.	0.50
+	2 COMBINED AT	CPR23	492.	12.50	76.	24.	8.	1.00
+	ROUTED TO							

+		R23R25	282.	12.75	73.	24.	8.	1.00
+	3 COMBINED AT	CPR25	1495.	15.92	923.	324.	109.	15.93
+	ROUTED TO	R25R24	1495.	15.92	923.	324.	109.	15.93
+	HYDROGRAPH AT	R19	1808.	12.42	302.	101.	34.	1.53
+	DIVERSION TO	RETR19	1808.	12.42	192.	55.	18.	1.53
+	HYDROGRAPH AT	DIVR19	1558.	12.58	156.	46.	15.	1.53
+	DIVERSION TO	DETR19	1387.	12.58	70.	18.	6.	1.53
+	HYDROGRAPH AT	DIV19R	229.	13.17	86.	29.	10.	1.53
+	ROUTED TO	R19R24	191.	13.83	82.	29.	10.	1.53
+	HYDROGRAPH AT	R24	400.	12.33	55.	18.	6.	0.29
+	DIVERSION TO	RETR24	400.	12.33	35.	10.	3.	0.29
+	HYDROGRAPH AT	DIVR24	305.	12.50	28.	8.	3.	0.29
+	3 COMBINED AT	CPR24	1536.	15.92	991.	351.	118.	17.75
+	ROUTED TO	R24EM4	1526.	16.00	990.	351.	118.	17.75
+	HYDROGRAPH AT	EMF4	135.	12.08	8.	2.	1.	0.06
+	3 COMBINED AT	CPEMF4	2722.	13.33	1899.	690.	237.	55.93

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION E7STOR
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
PLAN 1	1.00	1567.20	0.00	27.	1.	0.00	25.75	0.00
PLAN 2	1.00	1567.17	0.00	27.	1.	0.00	25.75	0.00
PLAN 3	1.00	1567.06	0.00	24.	0.	0.00	26.00	0.00
PLAN 4	1.00	1566.91	0.00	21.	0.	0.00	0.00	0.00
PLAN 5								

PLAN	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
PLAN 6	1.00	1566.72	0.00	16.	0.	0.00	0.00	0.00
PLAN 7	1.00	1566.61	0.00	14.	0.	0.00	0.00	0.00
PLAN 8	1.00	1566.53	0.00	12.	0.	0.00	0.00	0.00
PLAN 9	1.00	1566.47	0.00	11.	0.	0.00	0.00	0.00
PLAN 1	1.00	1566.43	0.00	10.	0.	0.00	0.00	0.00
PLAN 1	1.00	1311.98	0.00	22.	1.	0.00	13.00	0.00
PLAN 2	1.00	1311.98	0.00	21.	1.	0.00	13.00	0.00
PLAN 3	1.00	1311.95	0.00	21.	1.	0.00	13.00	0.00

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION RITBAS
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

1

PLAN 4		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1311.00	1318.00	1318.00				
	STORAGE	0.	693.	693.				
	OUTFLOW	0.	7.	7.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1311.92	0.00	20.	1.	0.00	13.00	0.00

PLAN 5		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1311.00	1318.00	1318.00				
	STORAGE	0.	693.	693.				
	OUTFLOW	0.	7.	7.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1311.87	0.00	19.	1.	0.00	13.00	0.00

PLAN 6		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1311.00	1318.00	1318.00				
	STORAGE	0.	693.	693.				
	OUTFLOW	0.	7.	7.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1311.85	0.00	19.	1.	0.00	13.00	0.00

PLAN 7		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1311.00	1318.00	1318.00				
	STORAGE	0.	693.	693.				
	OUTFLOW	0.	7.	7.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1311.83	0.00	18.	1.	0.00	12.92	0.00

PLAN 8		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1311.00	1318.00	1318.00				
	STORAGE	0.	693.	693.				
	OUTFLOW	0.	7.	7.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1311.82	0.00	18.	1.	0.00	12.92	0.00

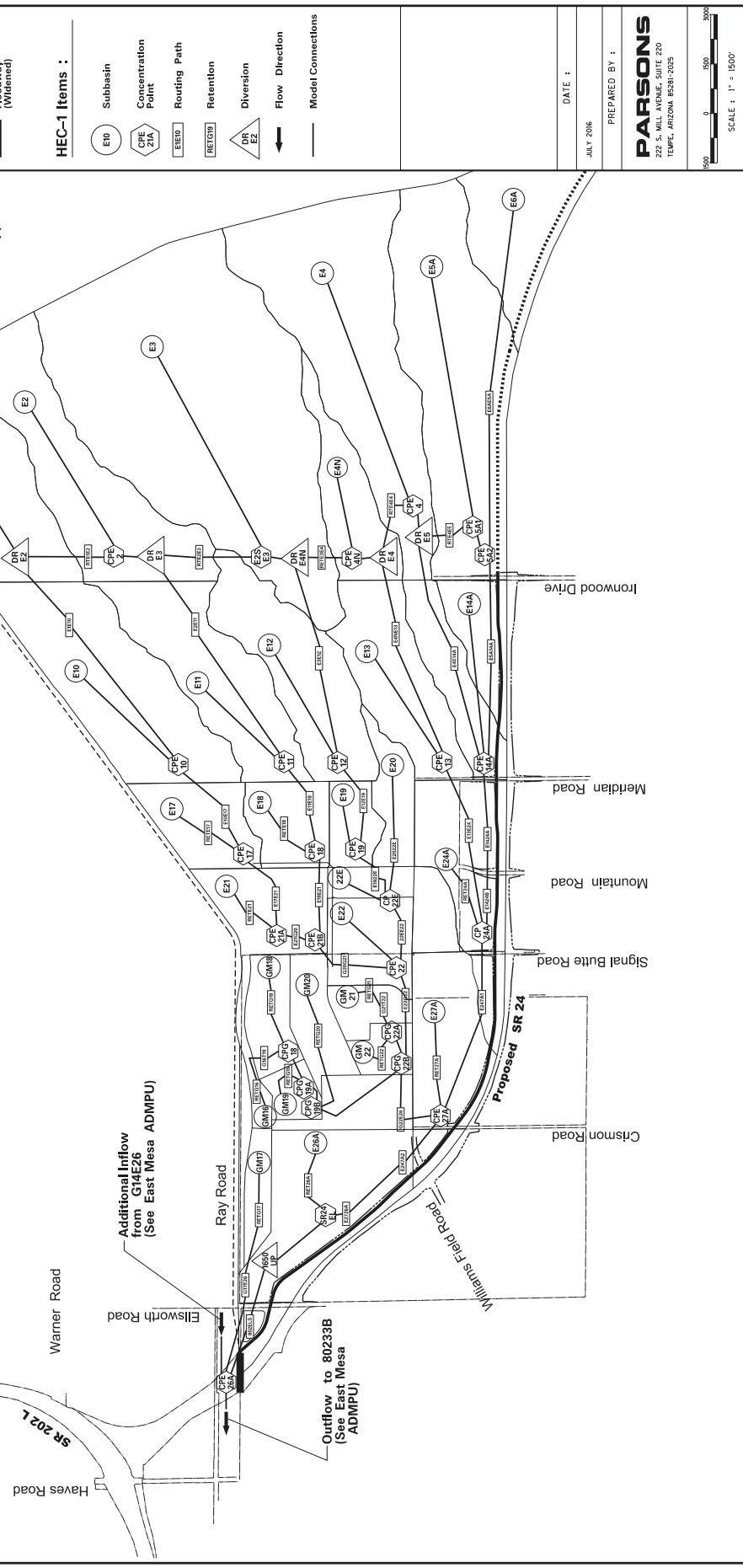
PLAN 9		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1311.00	1318.00	1318.00				
	STORAGE	0.	693.	693.				
	OUTFLOW	0.	7.	7.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1311.81	0.00	18.	1.	0.00	12.92	0.00

*** NORMAL END OF HEC-1 ***

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**SR 24 GATEWAY FREEWAY ELLSWORTH ROAD TO IRONWOOD DRIVE
INTERIM PHASE II**

**HEC-1 Schematic
Future Extension East
(24INT050C and 24INT100C)**



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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 04JUL16 TIME 08:39:40
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID 24INT050C 50-YEAR, 24-hr Interim Conditions 2016-03-02
2 ID Copy of 24INT100 assuming concrete-lined channel for the following routes
3 ID E5A14A, E1424A, E1424B, E247A1, E247A2 and E2726A.
4 ID by Parsons Corporation
5 ID
6 ID 2015-12-22 The model reflects interim drainage conditions for SR 24
7 ID and it is based on Mesa ADMPU with revisions reflecting development work
8 ID around the corridor.
9 ID
10 ID 2016-03-02 Modified to combine CPG19B to CPG22B as result of the Eastmar
11 ID Development. G19E26 was subsequently removed.
12 ID
13 ID 2016-07-04 Modified to include concrete lining for the SR 24 Channel.
14 ID
15 ID
16 ID *****
17 ID FUTEMADMP24 20110519 - EMADMPU 24-hr Future Conditions 20110519
18 ID Flood Control District of Maricopa County
19 ID 50 YEAR
20 ID 24 Hour Storm
21 ID Unit Hydrograph: S-Graph
22 ID 08/05/2011
23 IT 5 0 0 2000
24 IN 15
25 IO 5
*DIAGRAM
*
26 JD 3.184 0.0001
27 PC 0.000 0.002 0.005 0.008 0.011 0.014 0.017 0.020 0.023 0.026
28 PC 0.029 0.032 0.035 0.038 0.041 0.044 0.048 0.052 0.056 0.060
29 PC 0.064 0.068 0.072 0.076 0.080 0.085 0.090 0.095 0.100 0.105
30 PC 0.110 0.115 0.120 0.126 0.133 0.140 0.147 0.155 0.163 0.172
31 PC 0.181 0.191 0.203 0.218 0.236 0.257 0.283 0.387 0.663 0.707
32 PC 0.735 0.758 0.776 0.791 0.804 0.815 0.825 0.834 0.842 0.849
33 PC 0.856 0.863 0.869 0.875 0.881 0.887 0.893 0.898 0.903 0.908
34 PC 0.913 0.918 0.922 0.926 0.930 0.934 0.938 0.942 0.946 0.950
35 PC 0.953 0.956 0.959 0.962 0.965 0.968 0.971 0.974 0.977 0.980
36 PC 0.983 0.986 0.989 0.992 0.995 0.998 1.000
37 JD 3.168 1.0
38 JD 3.104 5.0
39 JD 3.025 10.0
40 JD 2.923 20.0
41 JD 2.866 30.0
42 JD 2.824 40.0
43 JD 2.792 50.0
44 JD 2.770 60.0
*
45 KK P1 BASIN
46 KM
47 KM Used the unit hydrograph for undeveloped conditions
48 KM by Parsons Corporation 2015-11
49 BA 0.387
50 LG 0.35 0.35 3.95 0.47 0
51 UI 0 29 29 99 134 162 189 226 301 369

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1 HEC-1 INPUT PAGE 2

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
52 UI 298 248 210 175 144 108 65 50 45 29
53 UI 26 9 9 9 9 9 9 9 9 9
54 UI 0 0 0 0 0 0 0 0 0 0
55 UI 0 0 0 0 0 0 0 0 0 0
*
56 KM KK DIVP1 DIVERT

```

```

57 KM
58 KM Revised by removing the retention to account for undeveloped conditions
59 KM by Parsons Corporation 2015-11
*DI RETP1 29.5 0.0
*DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

```

```

60 KK DP1PFW DIVERT
61 KM
62 DT DRPFW 0.0 0.0
63 DI 0.0 50.0 100.0 150.0 200.0 250.0 300.0 400.0 500.0 600.0
64 DQ 0.0 10.0 42.0 81.0 123.0 166.0 211.0 301.0 392.0 485.0
*

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```

65 KK P1P2 ROUTE
66 KM
67 KM Revised by using routing for undeveloped conditions
68 KM by Parsons Corporation 2015-11
69 RS 22 FLOW
70 RC 0.045 0.040 0.045 6529 0.0061 5.50
71 RX 0.00 500.00 1000.00 1005.00 1006.00 1010.00 1510.00 2010.00
72 RY 2.50 2.00 1.50 1.00 1.00 1.50 2.00 2.50
*

```

```

73 KK P2 BASIN
74 KM
75 KM Used the unit hydrograph for undeveloped conditions
76 KM by Parsons Corporation 2015-11
77 BA 0.577
78 LG 0.35 0.35 4.10 0.44 0
79 UI 0 38 38 92 151 187 214 247 287 357
80 UI 476 428 352 306 263 226 190 158 108 67
81 UI 63 55 38 38 14 12 12 12 12 12
82 UI 12 0 0 0 0 0 0 0 0 0
83 UI 0 0 0 0 0 0 0 0 0 0
*

```

```

84 KM KK DIVP2 DIVERT
85 KM
86 KM Revised by removing the retention to account for undeveloped conditions
87 KM by Parsons Corporation 2015-11
*DI RETP2 44.3 0.0
*DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

```

1 HEC-1 INPUT PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

88 KK CPP2 COMBINE
89 KM Combine Sub-basin P2 and routed flows from sub-basin P1
90 HC 2
*
91 KK P2P4 ROUTE
92 KM
93 RS 5 FLOW
94 RC 0.060 0.050 0.060 2856 0.0063 5.00
95 RX 0.00 100.00 110.00 145.00 150.00 200.00 210.00 325.00
96 RY 5.00 5.00 3.00 1.00 1.00 3.00 5.00 5.00
*

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97 KK P4 BASIN
98 KM
99 BA 0.497
100 LG 0.25 0.25 5.40 0.27 30
101 UI 0 49 94 206 267 331 431 603 478 383
102 UI 303 239 159 85 75 49 29 15 15 15
103 UI 15 0 0 0 0 0 0 0 0 0
104 UI 0 0 0 0 0 0 0 0 0 0
105 UI 0 0 0 0 0 0 0 0 0 0
*

```

```

106 KK DIVP4 DIVERT
107 KM
108 DT RETP4 50.8 0.0
109 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
110 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

```

```

111 KK CPP4 COMBINE
112 KM
113 HC 2
*

```

```

114 KK P4P6 ROUTE
115 KM
116 RS 6 FLOW
117 RC 0.035 0.050 0.045 3423 0.0053 7.00
118 RX 0.00 10.00 35.00 100.00 105.00 120.00 125.00 140.00
119 RY 5.00 5.00 3.00 1.00 1.00 3.00 5.00 7.00
*

```

```

120 KK P6 BASIN
121 KM
122 BA 0.504
123 LG 0.25 0.25 5.20 0.31 31
124 UI 0 39 39 137 182 219 258 310 423 485
125 UI 379 319 266 221 180 126 72 65 49 39
126 UI 23 12 12 12 12 12 0 0 0 0
127 UI 0 0 0 0 0 0 0 0 0 0
128 UI 0 0 0 0 0 0 0 0 0 0

```

HEC-1 INPUT PAGE 4

LINE	ID	1	2	3	4	5	6	7	8	9	10
129	KK	DIVP6 DIVERT									
130	KM										
131	DT	RETP6	50.4	0.0							
132	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
133	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
134	KK	CPP6 COMBINE									
135	KM										
136	HC	2									
137	KK	P6GM8	ROUTE								
138	KM										
139	RS	3	FLOW								
140	RC	0.035	0.030	0.035	2432	0.0019	5.00				
141	RX	950.00	989.00	991.00	1003.00	1007.00	1019.00	1021.00	1050.00		
142	RY	5.50	4.50	4.00	1.00	1.00	4.00	4.50	5.50		
143	KK	GMBG10	ROUTE								
144	KM										
145	RS	3	FLOW								
146	RC	0.035	0.035	0.035	2628	0.0051	5.00				
147	RX	0.00	500.00	980.00	1003.00	1007.00	1031.00	1511.00	2011.00		
148	RY	5.50	4.50	4.00	1.00	1.00	4.00	4.50	5.00		
149	KK	DRPFWRRETRIEVE									
150	KM										
151	DR	DRPFW									
152	KK	P1PFW	ROUTE								
153	KM										
154	KM	Revised by using routing for undeveloped conditions									
155	KM	by Parsons Corporation 2015-11									
156	RS	2	FLOW								
157	RC	0.030	0.016	0.030	8110	0.0062	8.00				
158	RX	0.00	10.00	11.00	21.00	27.00	37.00	40.00	50.00		
159	RY	8.00	8.00	7.50	1.00	1.00	7.50	8.00	8.00		
160	KK	P3 BASIN									
161	KM										
162	KM	Used the unit hydrograph for undeveloped conditions									
163	KM	by Parsons Corporation 2015-11									
164	BA	0.522									
165	LG	0.35	0.35	3.95	0.47	0					
166	UI	0	27	27	29	91	112	132	149	165	187
167	UI	209	250	317	349	290	251	224	201	175	156
168	UI	136	117	89	61	48	45	43	27	27	25
169	UI	8	8	8	8	8	8	8	8	8	0
170	UI	0	0	0	0	0	0	0	0	0	0

HEC-1 INPUT PAGE 5

LINE	ID	1	2	3	4	5	6	7	8	9	10
171	KK	DIVP3 DIVERT									
172	KM										
173	KM	Revised by removing the retention to account for undeveloped conditions									
174	KM	by Parsons Corporation 2015-11									
	*DT	RETP3	39.9	0.0							
	*DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	*DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
175	KK	CPP3 COMBINE									
176	KM										
177	HC	2	0.91								
178	KK	P3P5	ROUTE								
179	KM										
180	RS	1	FLOW								
181	RC	0.030	0.016	0.030	2889	0.0062	8.00				
182	RX	0.00	10.00	11.00	21.00	27.00	37.00	40.00	50.00		
183	RY	8.00	8.00	7.50	1.00	1.00	7.50	8.00	8.00		
184	KK	P5 BASIN									
185	KM										
186	BA	0.254									
187	LG	0.25	0.25	6.00	0.22	30					
188	UI	0	23	40	93	123	149	186	269	264	204
189	UI	167	134	104	64	40	34	23	14	7	7
190	UI	7	7	0	0	0	0	0	0	0	0
191	UI	0	0	0	0	0	0	0	0	0	0
192	UI	0	0	0	0	0	0	0	0	0	0
193	KK	DIVP5 DIVERT									
194	KM										
195	DT	RETP5	17.4	0.0							
196	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
197	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

HEC-1 INPUT PAGE 6

LINE	ID	1	2	3	4	5	6	7	8	9	10
198	KK	CPPS COMBINE									
199	KM										
200	HC	2									
201	KK	P5P7	ROUTE								
202	KM										
203	RS	1	FLOW								
204	RC	0.030	0.016	0.030	3146	0.0057	8.00				
205	RX	0.00	10.00	11.00	21.00	27.00	37.00	40.00	50.00		
206	RY	8.00	8.00	7.50	1.00	1.00	7.50	8.00	8.00		
207	KK	P7	BASIN								
208	KM										
209	BA	0.429									
210	LG	0.25	0.19	6.60	0.17	30					
211	UI	0	40	71	163	214	260	328	478	436	341
212	UI	276	220	170	94	68	52	40	16	12	12
213	UI	12	12	0	0	0	0	0	0	0	0
214	UI	0	0	0	0	0	0	0	0	0	0
215	UI	0	0	0	0	0	0	0	0	0	0
216	KK	DIVP7 DIVERT									
217	KM										
218	DT	RETP7	31.0	0.0							
219	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
220	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
221	KK	CPP7 COMBINE									
222	KM										
223	HC	3	3.17								
224	KK	P7GM14	ROUTE								
225	KM										
226	RS	9	FLOW								
227	RC	0.025	0.016	0.025	10659	0.0036	7.00				
228	RX	0.00	14.50	16.00	24.60	32.60	41.20	42.70	57.20		
229	RY	7.00	7.00	6.00	0.25	0.25	6.00	7.00	7.00		
230	KK	GM1 BASIN									
231	KM										
232	BA	0.345									
233	LG	0.10	0.15	8.00	0.13	5					
234	UI	0	38	93	178	228	297	447	394	303	232
235	UI	175	98	64	45	30	12	12	12	12	0
236	UI	0	0	0	0	0	0	0	0	0	0
237	UI	0	0	0	0	0	0	0	0	0	0
238	UI	0	0	0	0	0	0	0	0	0	0
239	KK	GM2 BASIN									
240	KM										
241	BA	0.683									
242	LG	0.20	0.25	6.00	0.23	48					
243	UI	0	104	415	625	942	1178	805	560	298	165
244	UI	96	32	32	32	0	0	0	0	0	0
245	UI	0	0	0	0	0	0	0	0	0	0
246	UI	0	0	0	0	0	0	0	0	0	0
247	UI	0	0	0	0	0	0	0	0	0	0

HEC-1 INPUT PAGE 7

LINE	ID	1	2	3	4	5	6	7	8	9	10
248	KK	GM3 BASIN									
249	KM										
250	BA	0.288									
251	LG	0.13	0.15	8.80	0.08	71					
252	UI	0	279	882	743	244	57	0	0	0	0
253	UI	0	0	0	0	0	0	0	0	0	0
254	UI	0	0	0	0	0	0	0	0	0	0
255	UI	0	0	0	0	0	0	0	0	0	0
256	UI	0	0	0	0	0	0	0	0	0	0
257	KK	CPG123 COMBINE									
258	KM										
259	HC	3									
260	KK	DIVG1 DIVERT									
261	KM										
262	DT	RETG1	102.1	0.0							
263	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
264	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
265	KK	GM1T5 ROUTE									
266	KM										
267	RS	1	FLOW								
268	RC	0.040	0.035	0.040	2680	0.0050	5.00				

411 UI 0 0 0 0 0 0 0 0 0 0 0
 412 UI 0 0 0 0 0 0 0 0 0 0 0
 413 UI 0 0 0 0 0 0 0 0 0 0 0
 *

414 KK DIVG12 DIVERT
 415 KM
 416 DT RETG12 9.4 0.0
 417 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 418 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

419 KK G12T13 ROUTE
 420 KM
 421 RS 2 FLOW
 422 RC 0.032 0.032 0.032 4000 0.0042 6.00
 423 RX 950.00 985.00 995.00 1003.00 1005.00 1013.00 1023.00 1068.00
 424 RY 6.00 5.50 5.00 1.00 1.00 5.00 5.50 6.00
 *

425 KK GM13 BASIN
 426 KM
 427 BA 0.292
 428 LG 0.23 0.25 5.60 0.27 49
 429 UI 0 256 804 796 294 78 29 0 0 0
 430 UI 0 0 0 0 0 0 0 0 0 0
 431 UI 0 0 0 0 0 0 0 0 0 0
 432 UI 0 0 0 0 0 0 0 0 0 0
 433 UI 0 0 0 0 0 0 0 0 0 0
 *

434 KK DIVG13 DIVERT
 435 KM
 436 DT RETG13 22.6 0.0
 437 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 438 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

439 KK CPG13 COMBINE
 440 KM
 441 HC 2
 *

442 KK G13T14 ROUTE
 443 KM
 444 RS 1 FLOW
 445 RC 0.032 0.018 0.032 1320 0.0030 3.50
 446 RX 0.00 5.00 12.00 15.00 65.00 68.00 135.00 140.00
 447 RY 3.50 3.00 2.50 1.00 1.00 2.50 3.00 3.50
 *

448 KK GM14 BASIN
 449 KM
 450 BA 0.347
 451 LG 0.17 0.25 4.55 0.44 56
 452 UI 0 211 619 1004 558 194 62 29 0 0
 453 UI 0 0 0 0 0 0 0 0 0 0
 454 UI 0 0 0 0 0 0 0 0 0 0
 455 UI 0 0 0 0 0 0 0 0 0 0
 456 UI 0 0 0 0 0 0 0 0 0 0
 *

457 KK DIVG14 DIVERT
 458 KM
 459 DT RETG14 25.6 0.0
 460 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 461 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

462 KK CPG14A COMBINE
 463 KM
 464 HC 2
 *

465 KK CPG14B COMBINE
 466 KM
 467 HC 2
 *

468 KK CPG14C COMBINE
 469 KM
 470 HC 2
 *

471 KK G14E26 ROUTE
 472 KM
 473 RS 1 FLOW
 474 RC 0.025 0.015 0.025 1450 0.0045 9.00
 475 RX 0.00 13.00 15.30 25.00 33.00 42.70 45.00 58.00
 476 RY 9.00 9.00 7.50 1.00 1.00 7.50 9.00 9.00
 *

1

HEC-1 INPUT PAGE 13

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

478 KK E1 BASIN
 479 KM

480 BA 0.886
 481 LG 0.35 0.35 3.95 0.47 0
 482 UI 0 55 55 115 203 259 301 338 392 455
 483 UI 596 700 574 488 430 369 320 273 228 162
 484 UI 96 92 88 55 55 34 17 17 17 17
 485 UI 17 17 17 0 0 0 0 0 0 0
 486 UI 0 0 0 0 0 0 0 0 0 0
 *

487 KM KK DIVE1 DIVERT
 488 KM
 489 KM Revised by removing the retention to account for undeveloped conditions
 490 KM by Parsons Corporation 2015-11
 *DT RETE1 67.6 0.0
 *DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

491 KK DE1S DIVERT
 492 KM
 493 DT DRE2 0.0 0.0
 494 DI 0.0 88.0 176.0 264.0 352.0 440.0 528.0 0.0 0.0 0.0
 495 DQ 0.0 58.0 126.0 201.0 277.0 355.0 434.0 0.0 0.0 0.0
 *

496 KK E1E10 ROUTE
 497 KM
 498 KM Revised by using routing for undeveloped conditions
 499 KM by Parsons Corporation 2015-11
 500 RS 26 FLOW
 501 RC 0.060 0.050 0.060 7806 0.0063 5.00
 502 RX 0.00 500.00 1000.00 1003.00 1007.00 1011.00 1511.00 2011.00
 503 RY 5.00 4.50 4.00 1.00 1.00 3.00 3.50 4.00
 *

504 KK E10 BASIN
 505 KM
 506 KM Used the unit hydrograph for undeveloped conditions
 507 KM by Parsons Corporation 2015-11
 508 BA 0.823
 509 LG 0.35 0.35 3.95 0.47 0
 510 UI 0 47 47 79 167 211 246 276 312 358
 511 UI 427 556 592 483 418 373 322 283 243 211
 512 UI 157 105 83 77 65 47 24 14 14
 513 UI 14 14 14 14 14 14 0 0 0 0
 514 UI 0 0 0 0 0 0 0 0 0 0
 *

515 KM KK DIVE10 DIVERT
 516 KM
 517 KM Revised by removing the retention to account for undeveloped conditions
 518 KM by Parsons Corporation 2015-11
 519 KM DT RETE10 62.9 0.0
 520 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

521 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

522 KK CPE10 COMBINE
 523 KM
 524 HC 2
 *

525 KK E10E17 ROUTE
 526 KM
 527 KM Buildout routing steps reduced from 5 to 3 through the interim condition
 528 KM by Parsons Corporation 2015-11
 529 RS 3 FLOW
 530 RC 0.045 0.035 0.045 3407 0.0048 5.00
 531 RX 0.00 100.00 110.00 145.00 150.00 200.00 210.00 325.00
 532 RY 5.00 5.00 3.00 1.00 1.00 3.00 5.00 5.00
 *

533 KK E17 BASIN
 534 KM
 535 KM Gila River Ranches Unit 3
 536 KM Buildout conditions existent through the interim condition
 537 KM
 538 KM Kieghley Place
 539 KM Buildout conditions assumed through the interim condition
 540 KM by Parsons Corporation 2015-11
 541 BA 0.271
 542 LG 0.26 0.25 5.00 0.33 29
 543 UI 0 27 55 118 153 190 260 331 254 204
 544 UI 160 123 71 46 36 27 9 8 8 8
 545 UI 8 0 0 0 0 0 0 0 0 0
 546 UI 0 0 0 0 0 0 0 0 0 0
 547 UI 0 0 0 0 0 0 0 0 0 0
 *

548 KK DIVE17 DIVERT
 549 KM
 550 KM Buildout retention in place through the interim condition
 551 KM by Parsons Corporation 2015-11
 552 DT RETE17 18.0 0.0
 553 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 554 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

555 KK CPE17 COMBINE
 556 KM
 557 HC 2

*
 558 KK E17E21 ROUTE
 559 KM
 560 KM Buildout routing steps kept at 4
 561 KM by Parsons Corporation 2015-11
 562 RS 4 FLOW
 563 RC 0.030 0.045 0.030 2832 0.0042 1440.20
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1
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

564 RX 0.00 90.00 100.00 115.00 180.00 195.00 255.00 260.00
 565 RY 1440.0 1439.90 1439.80 1438.00 1438.00 1440.00 1440.10 1440.20
 *

566 KK E21 BASIN
 567 KM
 568 KM Mountain Horizons
 569 KM Buildout conditions assumed through the interim condition
 570 KM by Parsons Corporation 2015-11
 571 BA 0.311
 572 LG 0.25 0.25 6.00 0.22 30
 573 UI 0 30 56 125 162 199 257 368 305 243
 574 UI 193 153 108 59 49 31 24 9 9 9
 575 UI 9 0 0 0 0 0 0 0 0 0
 576 UI 0 0 0 0 0 0 0 0 0 0
 577 UI 0 0 0 0 0 0 0 0 0 0
 *

578 KK DIVE21 DIVERT
 579 KM
 580 KM Buildout retention in place through the interim condition
 581 KM by Parsons Corporation 2015-11
 582 DT RETE21 20.3 0.0
 583 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 584 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

585 KK CPE21A COMBINE
 586 KM
 587 HC 2
 *

588 KK E21G20 ROUTE
 589 KM
 590 RS 1 FLOW
 591 RC 0.032 0.032 0.032 1655 0.0036 5.50
 592 RX 0.00 5.00 10.00 24.00 34.00 48.00 53.00 58.00
 593 RY 5.50 5.00 4.50 1.00 1.00 4.50 5.00 5.50
 *

594 KM
 595 KK DRE2RETRIEVE
 596 KM
 597 DR DRE2
 *

598 KK RTE1E2 ROUTE
 599 KM
 600 KM Revised by using routing for undeveloped conditions
 601 KM by Parsons Corporation 2015-11
 602 RS 4 FLOW
 603 RC 0.035 0.030 0.025 4100 0.0035 6.00
 604 RX 0.00 100.00 700.00 1050.00 1090.00 1110.00 1140.00 1240.00
 605 RY 6.00 6.00 4.00 1.00 1.00 5.00 6.00 6.00
 *

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1
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

606 KK E2 BASIN
 607 KM
 608 KM Used the unit hydrograph for undeveloped conditions
 609 KM by Parsons Corporation 2015-11
 610 BA 0.779
 611 LG 0.35 0.35 4.25 0.41 0
 612 UI 0 45 45 77 159 202 234 263 298 342
 613 UI 412 536 556 456 394 352 304 267 228 196
 614 UI 145 95 78 74 58 45 45 19 14 14
 615 UI 14 14 14 14 14 0 0 0 0 0
 616 UI 0 0 0 0 0 0 0 0 0 0
 *

617 KM KK DIVE2 DIVERT
 618 KM
 619 KM Revised by removing the retention to account for undeveloped conditions
 620 KM by Parsons Corporation 2015-11
 *DT RETE2 60.4 0.0
 *DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

621 KK CPE2 COMBINE
 622 KM
 623 HC 2 1.67
 *

624 KK DE2S DIVERT
 625 KM
 626 DT DRE3 0.0 0.0
 627 DI 0.0 135.0 279.0 431.0 583.0 738.0 894.0 0.0 0.0 0.0
 628 DQ 0.0 15.0 121.0 243.0 370.0 504.0 636.0 0.0 0.0 0.0

*
 629 KK E2E11 ROUTE
 630 KM
 631 KM Revised by using routing for undeveloped conditions
 632 KM by Parsons Corporation 2015-11
 633 RS 34 FLOW
 634 RC 0.055 0.045 0.055 9374 0.0052 5.00
 635 RX 0.00 500.00 1000.00 1005.00 1006.00 1010.00 1510.00 2010.00
 636 RY 2.50 2.00 1.50 1.00 1.00 1.50 2.00 2.50
 *

1
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637 KK E11 BASIN
 638 KM
 639 KM Used the unit hydrograph for undeveloped conditions
 640 KM by Parsons Corporation 2015-11
 641 BA 0.600
 642 LG 0.35 0.35 3.95 0.47 0
 643 UI 0 37 37 76 135 174 201 226 261 303
 644 UI 394 472 392 332 293 252 220 186 157 114
 645 UI 70 63 60 39 37 28 11 11 11 11
 646 UI 11 11 11 0 0 0 0 0 0 0
 647 UI 0 0 0 0 0 0 0 0 0 0
 *

1
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

648 KM KKDIVE11 DIVERT
 649 KM
 650 KM Revised by removing the retention to account for undeveloped conditions
 651 KM by Parsons Corporation 2015-11
 652 KM DTRETE11 45.8 0.0
 653 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 654 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

655 KK CPE11 COMBINE
 656 KM
 657 HC 2
 *

658 KK E11E18 ROUTE
 659 KM
 660 KM Buildout routing steps reduced from 22 to 9 through the interim condition
 661 KM by Parsons Corporation 2015-11
 662 RS 9 FLOW
 663 RC 0.045 0.040 0.045 3164 0.0044 5.50
 664 RX 0.00 500.00 1000.00 1005.00 1006.00 1010.00 1510.00 2010.00
 665 RY 2.50 2.00 1.50 1.00 1.00 1.50 2.00 2.50
 *

666 KK E18 BASIN
 667 KM
 668 KM Rancho Apache
 669 KM Existing and Buildout conditions are the same
 670 KM by Parsons Corporation 2015-11
 671 BA 0.224
 672 LG 0.30 0.15 7.00 0.14 16
 673 UI 0 30 103 166 224 352 291 213 153 82
 674 UI 51 30 12 9 9 0 0 0 0 0
 675 UI 0 0 0 0 0 0 0 0 0 0
 676 UI 0 0 0 0 0 0 0 0 0 0
 677 UI 0 0 0 0 0 0 0 0 0 0
 *

678 KK DIVE18 DIVERT
 679 KM
 680 DT RETE18 0.3 0.0
 681 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 682 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

683 KK CPE18 COMBINE
 684 KM
 685 HC 2
 *

1
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1
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

686 KK E18E21 ROUTE
 687 KM
 688 KM Buildout routing steps unchanged
 689 KM by Parsons Corporation 2015-11
 690 RS 2 FLOW
 691 RC 0.035 0.040 0.045 2664 0.0053 5.00
 692 RX 0.00 15.00 50.00 60.00 100.00 110.00 290.00 300.00
 693 RY 3.50 3.00 3.00 1.00 1.00 3.00 3.00 5.00
 *

694 KK CPE21B COMBINE
 695 KM
 696 HC 2 3.90
 *

697 KK G20G21 ROUTE
 698 KM
 699 KM
 700 RS 2 FLOW
 701 RC 0.032 0.032 0.032 1901 0.0021 5.50
 702 RX 0.00 1.00 5.00 24.00 124.00 138.00 143.00 148.00

703 RY 5.50 5.00 4.50 1.00 1.00 4.50 5.00 5.50
 *
 704 KM
 705 KK DRE3RETRIEVE
 706 KM
 707 DR DRE3
 *
 708 KK RTE2E3 ROUTE
 709 KM
 710 KM Revised by using routing for undeveloped conditions
 711 KM by Parsons Corporation 2015-11
 712 RS 4 FLOW
 713 RC 0.035 0.030 0.025 3678 0.0035 6.00
 714 RX 0.00 100.00 700.00 1050.00 1090.00 1110.00 1140.00 1240.00
 715 RY 6.00 6.00 4.00 1.00 1.00 5.00 6.00 6.00
 *

716 KK E3 BASIN
 717 KM
 718 KM Used the unit hydrograph for undeveloped conditions
 719 KM by Parsons Corporation 2015-11
 720 BA 2.234
 721 LG 0.35 0.35 4.60 0.33 0
 722 UI 0 91 91 91 136 303 356 427 467 510
 723 UI 552 605 672 731 857 1035 1206 1075 936 840
 724 UI 769 712 638 576 531 468 432 369 285 220
 725 UI 162 158 150 150 92 91 91 79 28 28
 726 UI 28 28 28 28 28 28 28 28 28 28
 727 UI 0 0 0 0 0 0 0 0 0 0
 *

728 KM KK DIVE3 DIVERT HEC-1 INPUT PAGE 19

1
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
 729 KM
 730 KM Revised by removing the retention to account for undeveloped conditions
 731 KM by Parsons Corporation 2015-11
 *DT RETE3 178.6 0.0
 *DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
 *DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
 *

732 KK E2SE3 COMBINE
 733 KM
 734 HC 2 3.9
 *
 735 KK DE3S DIVERT
 736 KM
 737 DT DRE4N 0.0 0.0
 738 DI 0.0 192.0 476.0 774.0 1079.0 1390.0 1699.0 0.0 0.0 0.0
 739 DQ 0.0 5.0 197.0 415.0 656.0 912.0 1175.0 0.0 0.0 0.0
 *

740 KK E3E12 ROUTE
 741 KM
 742 KM Revised by using routing for undeveloped conditions
 743 KM by Parsons Corporation 2015-11
 744 RS 15 FLOW
 745 RC 0.060 0.050 0.060 4852 0.0054 5.50
 746 RX 0.00 500.00 980.00 1003.00 1007.00 1031.00 1511.00 2011.00
 747 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

748 KK E12 BASIN
 749 KM
 750 KM Used the unit hydrograph for undeveloped conditions.
 751 KM by Parsons Corporation 2015-11
 752 BA 0.573
 753 LG 0.35 0.35 4.60 0.33 0
 754 UI 0 32 32 49 112 140 164 184 208 237
 755 UI 275 354 415 346 296 263 232 202 177 154
 756 UI 126 89 57 55 53 35 32 30 10 10
 757 UI 10 10 10 10 10 10 0 0 0 0
 758 UI 0 0 0 0 0 0 0 0 0 0
 *

759 KM KKDIVE12 DIVERT
 760 KM
 761 KM Revised by removing the retention to account for undeveloped conditions
 762 KM by Parsons Corporation 2015-11
 763 KM DTRETE12 43.7 0.0
 764 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 765 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

766 KK CPE12 COMBINE
 767 KM
 768 HC 2
 *

769 KK E12E19 ROUTE
 770 KM
 771 KM Buildout routing steps kept at 9 through the interim condition
 772 KM by Parsons Corporation 2015-11
 773 RS 9 FLOW
 774 RC 0.060 0.055 0.060 2707 0.0052 5.50

775 RX 0.00 500.00 980.00 1003.00 1007.00 1031.00 1511.00 2011.00
 776 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

777 KK E19 BASIN
 778 KM
 779 KM Part of Superstition View
 780 KM Existing conditions assumed through the interim condition
 781 KM by Parsons Corporation 2015-11
 782 BA 0.135
 783 LG 0.30 0.15 8.00 0.10 15
 784 UI 0 35 119 186 288 194 122 51 29 9
 785 UI 8 0 0 0 0 0 0 0 0 0
 786 UI 0 0 0 0 0 0 0 0 0 0
 787 UI 0 0 0 0 0 0 0 0 0 0
 788 UI 0 0 0 0 0 0 0 0 0 0
 *

789 KM KKDIVE19 DIVERT
 790 KM
 791 KM Revised by removing the retention to account for undeveloped conditions
 792 KM by Parsons Corporation 2015-11
 793 KM DTRETE19 0.2 0.0
 794 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 795 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 *

796 KK CPE19 COMBINE
 797 KM
 798 HC 2
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

807 KK 22E BASIN
 808 KM
 809 KM Used the unit hydrograph for existing (partially developed) conditions.
 810 KM by Parsons Corporation 2015-11
 811 BA 0.089
 812 LG 0.31 0.19 8.40 0.08 11
 813 UI 0 19 69 104 173 137 91 48 24 12
 814 UI 5 5 0 0 0 0 0 0 0 0
 815 UI 0 0 0 0 0 0 0 0 0 0
 816 UI 0 0 0 0 0 0 0 0 0 0
 817 UI 0 0 0 0 0 0 0 0 0 0
 *

818 KM KKDIV22E DIVERT
 819 KM
 820 KM Revised by removing the retention to account for undeveloped conditions
 821 KM by Parsons Corporation 2015-11
 822 KM DTRET22E 7.8 0.0
 823 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 824 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 *

825 KK E20 BASIN
 826 KM
 827 KM Used the unit hydrograph for existing (partially developed) conditions.
 828 KM by Parsons Corporation 2015-11
 829 BA 0.169
 830 LG 0.32 0.28 4.50 0.35 10
 831 UI 0 17 33 72 93 115 153 206 161 129
 832 UI 102 79 50 29 24 17 8 5 5 5
 833 UI 5 0 0 0 0 0 0 0 0 0
 834 UI 0 0 0 0 0 0 0 0 0 0
 835 UI 0 0 0 0 0 0 0 0 0 0
 *

836 KM KKDIVE20 DIVERT
 837 KM
 838 KM Revised by removing the retention to account for existing (pre-buildout)
 839 KM conditions
 840 KM by Parsons Corporation 2015-11
 841 KM DTRETE20 3.2 0.0
 842 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 843 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 *

844 KK E2022E ROUTE
 845 KM
 846 KM Revised by using routing for existing (pre-buildout) conditions
 847 KM by Parsons Corporation 2015-11
 848 RS 3 FLOW
 849 RC 0.045 0.035 0.045 1115 0.0054 10.00
 850 RX 0.00 500.00 1000.00 1005.00 1007.00 1010.00 1511.00 2011.00
 851 RY 2.50 2.00 1.50 1.00 1.00 1.50 2.00 2.50
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

852 KK CP22E COMBINE


```

853 KM
854 HC 3
*

855 KK 22EE22 ROUTE
856 KM
857 RS 1 FLOW
858 RC 0.045 0.040 0.045 1740 0.0046 10.00
859 RX 950.00 973.00 993.00 1005.00 1013.00 1025.00 1045.00 1055.00
860 RY 5.00 4.50 4.00 1.00 1.00 4.00 4.50 5.00
*

861 KK E22 BASIN
862 KM
863 KM Revised by using the unit hydrograph for undeveloped conditions
864 KM by Parsons Corporation 2015-11
865 BA 0.158
866 LG 0.35 0.32 7.60 0.10 1
867 UI 0 18 18 58 81 99 114 136 171 232
868 UI 200 164 141 117 98 80 55 32 30 23
869 UI 18 12 6 6 6 6 6 6 0 0
870 UI 0 0 0 0 0 0 0 0 0 0
871 UI 0 0 0 0 0 0 0 0 0 0
*

872 KM KKDIVE22 DIVERT
873 KM
874 KM Revised by removing the retention to account for undeveloped conditions
875 KM by Parsons Corporation 2015-11
876 KM DTRETE22 13.8 0.0
877 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
878 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
*

879 KK CPE22 COMBINE
880 KM
881 HC 3 7.25
*

882 KK E22G22 ROUTE
883 KM
884 RS 3 FLOW
885 RC 0.040 0.050 0.040 4418 0.0043 8.00
886 RX 720.00 750.00 785.00 805.00 845.00 865.00 880.00 910.00
887 RY 8.00 7.00 6.00 1.00 1.00 6.00 7.00 8.00
*

888 KK GM21 BASIN
889 KM
890 BA 0.210
891 LG 0.10 0.15 7.30 0.14 75
892 UI 0 51 176 272 437 309 200 90 49 19
893 UI 12 12 0 0 0 0 0 0 0 0
894 UI 0 0 0 0 0 0 0 0 0 0
*

1 HEC-1 INPUT PAGE 23
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
895 UI 0 0 0 0 0 0 0 0 0 0
896 UI 0 0 0 0 0 0 0 0 0 0
*

897 KK DIVG21 DIVERT
898 KM
899 DT RETG21 17.3 0.0
900 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
901 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

902 KK G21T22 ROUTE
903 KM
904 RS 1 FLOW
905 RC 0.032 0.008 0.032 1500 0.0020 3.00
906 RX 0.00 2.00 4.00 6.00 60.00 62.00 64.00 66.00
907 RY 3.00 2.50 2.00 1.00 1.00 2.00 2.50 3.00
*

908 KK GM22 BASIN
909 KM
910 BA 0.095
911 LG 0.10 0.15 8.80 0.08 79
912 UI 0 67 197 280 134 40 11 0 0 0
913 UI 0 0 0 0 0 0 0 0 0 0
914 UI 0 0 0 0 0 0 0 0 0 0
915 UI 0 0 0 0 0 0 0 0 0 0
916 UI 0 0 0 0 0 0 0 0 0 0
*

917 KK DIVG22 DIVERT
918 KM
919 DT RETG22 8.0 0.0
920 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
921 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

922 KK CPG22A COMBINE
923 KM
924 HC 2
*

925 KK GM16 BASIN
926 KM
927 BA 0.069
928 LG 0.26 0.25 4.50 0.48 44

```

```

929 UI 0 10 38 59 84 119 84 59 38 17
930 UI 12 5 3 3 0 0 0 0 0 0
931 UI 0 0 0 0 0 0 0 0 0 0
932 UI 0 0 0 0 0 0 0 0 0 0
933 UI 0 0 0 0 0 0 0 0 0 0
*

1 HEC-1 INPUT PAGE 24
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
934 KK DIVG16 DIVERT
935 KM
936 DT RETG16 4.9 0.0
937 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
938 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

939 KK G16T19 ROUTE
940 KM
941 RS 2 FLOW
942 RC 0.032 0.016 0.032 1200 0.0020 3.00
943 RX 0.00 2.00 4.00 6.00 60.00 62.00 64.00 66.00
944 RY 3.00 2.50 2.00 1.00 1.00 2.00 2.50 3.00
*

945 KK GM18 BASIN
946 KM
947 BA 0.173
948 LG 0.25 0.25 5.30 0.29 44
949 UI 0 39 137 209 346 262 172 87 44 21
950 UI 9 9 0 0 0 0 0 0 0 0
951 UI 0 0 0 0 0 0 0 0 0 0
952 UI 0 0 0 0 0 0 0 0 0 0
953 UI 0 0 0 0 0 0 0 0 0 0
*

954 KK DIVG18 DIVERT
955 KM
956 DT RETG18 12.4 0.0
957 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
958 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

959 KK CPG18 COMBINE
960 KM
961 HC 2
*

962 KK GM19 BASIN
963 KM
964 BA 0.085
965 LG 0.17 0.15 7.60 0.14 22
966 UI 0 52 152 246 137 48 15 7 0 0
967 UI 0 0 0 0 0 0 0 0 0 0
968 UI 0 0 0 0 0 0 0 0 0 0
969 UI 0 0 0 0 0 0 0 0 0 0
970 UI 0 0 0 0 0 0 0 0 0 0
*

1 HEC-1 INPUT PAGE 25
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
971 KK DIVG19 DIVERT
972 KM
973 DT RETG19 5.5 0.0
974 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
975 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

976 KK CPG19A COMBINE
977 KM
978 HC 2
*

979 KK GM20 BASIN
980 KM
981 BA 0.183
982 LG 0.25 0.15 8.80 0.07 44
983 UI 0 72 224 413 362 209 80 33 13 0
984 UI 0 0 0 0 0 0 0 0 0 0
985 UI 0 0 0 0 0 0 0 0 0 0
986 UI 0 0 0 0 0 0 0 0 0 0
987 UI 0 0 0 0 0 0 0 0 0 0
*

988 KK DIVG20 DIVERT
989 KM
990 DT RETG20 14.5 0.0
991 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
992 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

993 KK CPG19B COMBINE
994 KM
995 HC 2
*

996 KK CPG22B COMBINE
997 KM
998 KM Modified to combining 3 hydrographs instead of 2 due to adding CPG19B
999 KM by Parsons Corporation 2015-02

```

1000 HC 3
 *
 1001 KK G22E26 ROUTE
 1002 KM
 1003 RS 2 FLOW
 1004 RC 0.040 0.030 0.040 2939 0.0031 8.00
 1005 RX 0.00 500.00 800.00 805.00 820.00 825.00 1125.00 1625.00
 1006 RY 8.00 7.00 6.00 1.00 1.00 6.00 7.00 8.00
 *

1 HEC-1 INPUT PAGE 26

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1008 KK DRE4NRETRIEVE
 1009 KM
 1010 DR DRE4N
 *
 1011 KK RTE3E4 ROUTE
 1012 KM
 1013 KM Revised by using routing for undeveloped conditions
 1014 KM by Parsons Corporation 2015-11
 1015 RS 2 FLOW
 1016 RC 0.035 0.030 0.025 2000 0.0035 6.00
 1017 RX 0.00 100.00 700.00 1050.00 1090.00 1110.00 1140.00 1240.00
 1018 RY 0.00 6.00 4.00 1.00 1.00 5.00 6.00 6.00
 *

1019 KK E4N BASIN
 1020 KM
 1021 KM Used the unit hydrograph for undeveloped conditions
 1022 KM by Parsons Corporation 2015-11
 1023 BA 0.307
 1024 LG 0.35 0.35 3.95 0.47 0
 1025 UI 0 18 18 30 63 80 93 104 118 135
 1026 UI 163 213 219 179 155 138 119 105 90 77
 1027 UI 57 37 31 29 23 18 18 7 5 5
 1028 UI 5 5 5 5 5 0 0 0 0 0
 1029 UI 0 0 0 0 0 0 0 0 0 0
 *

1030 KM KKDIVE4N DIVERT
 1031 KM
 1032 KM Revised by removing the retention to account for undeveloped conditions
 1033 KM by Parsons Corporation 2015-11
 *DTRETE4N 23.4 0.0
 *DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
 *DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
 *

1034 KK CPE4N COMBINE
 1035 KM
 1036 HC 2 4.21
 *

1037 KK DE4NS DIVERT
 1038 KM
 1039 DT DRE4 0.0 0.0
 1040 DI 0.0 34.0 255.0 502.0 772.0 1056.0 1348.0 0.0 0.0 0.0
 1041 DQ 0.0 11.0 171.0 378.0 614.0 868.0 1133.0 0.0 0.0 0.0
 *

1042 KK E4NE13 ROUTE
 1043 KM
 1044 KM Revised by using routing for undeveloped conditions
 1045 KM by Parsons Corporation 2015-11
 1046 RS 23 FLOW
 1047 RC 0.055 0.045 0.055 6955 0.0046 5.50
 HEC-1 INPUT PAGE 27

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1048 RX 0.00 500.00 980.00 1003.00 1010.00 1050.00 1511.00 2011.00
 1049 RY 3.00 2.50 2.00 1.00 1.00 2.00 2.50 3.00
 *

1050 KK E13 BASIN
 1051 KM
 1052 BA 0.477
 1053 LG 0.35 0.36 5.00 0.27 0
 1054 UI 0 28 28 50 100 127 147 165 188 215
 1055 UI 264 345 334 274 239 213 183 160 138 116
 1056 UI 83 50 48 46 31 28 24 9 9 9
 1057 UI 9 9 9 9 9 0 0 0 0 0
 1058 UI 0 0 0 0 0 0 0 0 0 0
 *

1059 KM KKDIVE13 DIVERT
 1060 KM
 1061 KM Revised by removing the retention to account for undeveloped conditions
 1062 KM by Parsons Corporation 2015-11
 1063 KM DTRETE13 38.8 0.0
 1064 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 1065 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 *

1066 KK CPE13 COMBINE
 1067 KM
 1068 HC 2
 *

1069 KK E13E24 ROUTE

1070 KM
 1071 RS 8 FLOW
 1072 RC 0.035 0.030 0.035 5921 0.0042 6.00
 1073 RX 980.00 990.00 995.00 1003.00 1007.00 1015.00 1520.00 1530.00
 1074 RY 4.00 3.50 3.00 1.00 1.00 3.00 3.50 4.00
 *

1075 KM
 1076 KK DRE4RETRIEVE
 1077 KM
 1078 DR DRE4
 *

1079 KK RTE4E4 ROUTE
 1080 KM
 1081 KM Revised by using routing for undeveloped conditions
 1082 KM by Parsons Corporation 2015-11
 1083 RS 10 FLOW
 1084 RC 0.035 0.030 0.025 9400 0.0035 6.00
 1085 RX 0.00 100.00 700.00 1050.00 1090.00 1110.00 1140.00 1240.00
 1086 RY 0.00 6.00 4.00 1.00 1.00 5.00 6.00 6.00
 *

1 HEC-1 INPUT PAGE 28

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1087 KK E4 BASIN
 1088 KM
 1089 KM Used the unit hydrograph for undeveloped conditions
 1090 KM by Parsons Corporation 2015-11
 1091 BA 1.200
 1092 LG 0.35 0.35 4.15 0.43 0
 1093 UI 0 49 49 49 71 162 189 228 249 271
 1094 UI 294 322 357 388 453 550 639 582 506 452
 1095 UI 414 384 345 312 287 254 233 202 159 125
 1096 UI 86 86 80 80 54 49 49 48 15 15
 1097 UI 15 15 15 15 15 15 15 15 15 15
 1098 UI 0 0 0 0 0 0 0 0 0 0
 *

1099 KM KK DIVE4 DIVERT
 1100 KM
 1101 KM Revised by removing the retention to account for undeveloped conditions
 1102 KM by Parsons Corporation 2015-11
 *DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
 *DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
 *

1103 KK CPE4 COMBINE
 1104 KM
 1105 HC 2 5.41
 *

1106 KK DE4S DIVERT
 1107 KM
 1108 DT DRE5 0.0 0.0
 1109 DI 0.0 97.0 343.0 637.0 959.0 1299.0 1650.0 0.0 0.0 0.0
 1110 DQ 0.0 89.0 330.0 622.0 943.0 1283.0 1633.0 0.0 0.0 0.0
 *

1111 KK E4E14A ROUTE
 1112 KM
 1113 KM Revised by using routing for undeveloped conditions (E4E14N) from
 1114 KM existing condition (pre-SR 24) model
 1115 KM by Parsons Corporation 2015-11
 1116 RS 12 FLOW
 1117 RC 0.060 0.050 0.060 6921 0.0049 5.50
 1118 RX 0.00 500.00 980.00 1003.00 1007.00 1031.00 1511.00 2011.00
 1119 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

1120 KK E14A BASIN
 1121 KM
 1122 KM Used the unit hydrograph for undeveloped conditions for Basin E14N from
 1123 KM existing condition model (pre-SR 24)
 1124 KM by Parsons Corporation 2015-11
 1125 BA 0.481
 1126 LG 0.35 0.35 4.10 0.44 0
 1127 UI 0 20 20 47 78 97 112 129 150 185
 1128 UI 247 226 185 161 139 119 101 84 59 35
 HEC-1 INPUT PAGE 29

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
 1129 UI 33 30 20 20 8 6 6 6 6 6
 1130 UI 6 0 0 0 0 0 0 0 0 0
 1131 UI 0 0 0 0 0 0 0 0 0 0
 *

1132 KM KKDIV14A DIVERT
 1133 KM
 1134 KM Revised by removing the retention to account for undeveloped conditions
 1135 KM by Parsons Corporation 2015-11
 1136 KM DTRETE14A 38.6 0.0
 1137 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 1138 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0
 *

1139 KK E6A BASIN
 1140 KM
 1141 KM Revised the unit hydrograph for undeveloped conditions
 1142 KM by Parsons Corporation 2015-11
 1143 BA 0.581

1144	LG	0.16	0.25	5.70	0.27	59														
1145	UI	0	46	46	46	77	155	183	217	238	261									
1146	UI	282	311	346	381	455	556	598	511	450	406									
1147	UI	374	343	305	278	251	226	201	161	130	81									
1148	UI	81	76	76	55	46	46	46	14	14	14									
1149	UI	14	14	14	14	14	14	14	14	14	0									

1150 KM KKDIVE6A DIVERT
 1151 KM
 1152 KM Revised by removing the retention to account for undeveloped conditions
 1153 KM by Parsons Corporation 2015-11
 1154 KM DTRETE6A 53.1 0.0
 1155 KM DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1156 KM DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

1157 KK E6AE5A ROUTE
 1158 KM
 1159 RS 6 FLOW
 1160 RC 0.020 0.020 0.020 7264 0.0010 100.00
 1161 RX 0.00 1.00 2.00 20.00 30.00 48.00 49.00 50.00
 1162 RY 100.00 99.00 99.00 90.00 90.00 99.00 99.00 100.00

1163 KK DRE5RETRIEVE
 1164 KM
 1165 DR DRE5

1166 KK RTE4E5 ROUTE
 1167 KM
 1168 KM Revised by using routing for undeveloped conditions
 1169 KM by Parsons Corporation 2015-11
 1170 RS 3 FLOW
 1171 RC 0.035 0.030 0.025 3700 0.0035 6.00
 1172 RX 0.00 100.00 700.00 1050.00 1090.00 1110.00 1140.00 1240.00
 1173 RY 0.00 6.00 4.00 1.00 1.00 5.00 6.00 6.00

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1174 KK E5A BASIN
 1175 KM
 1176 KM Revised the unit hydrograph and LG for undeveloped conditions (Basin E5)
 1177 KM by Parsons Corporation 2015-11
 1178 BA 1.140
 1179 LG 0.35 0.35 3.95 0.47 0
 1180 UI 0 59 59 59 89 195 229 274 300 328
 1181 UI 354 389 432 471 555 670 773 682 595 535
 1182 UI 489 453 407 366 336 298 275 232 177 134
 1183 UI 104 101 96 92 59 59 45 18 18
 1184 UI 18 18 18 18 18 18 18 18 18 0

1185 KM KKDIVE5A DIVERT
 1186 KM
 1187 KM Revised by removing the retention to account for undeveloped conditions
 1188 KM by Parsons Corporation 2015-11
 *DTRETE5A 89.1 0.0
 *DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

1189 KK CPE5A1 COMBINE
 1190 KM
 1191 HC 2 6.55

1192 KK CPE5A2 COMBINE
 1193 KO 1
 1194 KM
 1195 HC 2

1196 KK E5A14A ROUTE
 1197 KM
 1198 KM Revised for channel length/time steps and cross section between
 1199 KM Ironwood Dr. and Meridian Rd. to account for concrete-lined channel.
 1200 KM by Parsons Corporation 2015-12
 1201 RS 4 FLOW
 1202 RC 0.016 0.016 0.016 6121 0.0017 97.00
 1203 RX 0.00 7.50 15.00 29.00 41.00 55.00 62.50 70.00
 1204 RY 97.45 97.23 97.00 90.00 90.00 97.00 97.23 97.45

1205 KK CPE14A COMBINE
 1206 KM ***** PARSONS 10/30/2015 *****
 1207 KO 1
 1208 HC 3 7.61

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1209 KK E1424A ROUTE
 1210 KM
 1211 KM Revised for channel length and time steps between Mountain Rd
 1212 KM and Meridian Rd to account for concrete lining.
 1213 KM by Parsons Corporation 2016-03
 1214 RS 2 FLOW
 1215 RC 0.016 0.016 0.016 2808 0.0017 97.00

1216	RX	0.00	7.50	15.00	29.00	41.00	55.00	62.50	70.00												
1217	RY	97.45	97.23	97.00	90.00	90.00	97.00	97.23	97.45												

1218 KK E1424B ROUTE
 1219 KM
 1220 KM Introduced for channel length and time steps between
 1221 KM Signal Butte Rd. and Mountain Rd. to account for concrete lining.
 1222 KM by Parsons Corporation 2015-12
 1223 RS 2 FLOW
 1224 RC 0.016 0.016 0.016 2461 0.0017 97.00
 1225 RX 0.00 7.50 15.00 29.00 41.00 55.00 62.50 70.00
 1226 RY 97.45 97.23 97.00 90.00 90.00 97.00 97.23 97.45

1227 KK E24A BASIN
 1228 KM
 1229 BA 0.528
 1230 LG 0.14 0.25 6.00 0.24 59
 1231 UI 0 81 324 487 736 911 620 431 224 126
 1232 UI 72 25 25 25 0 0 0 0 0 0
 1233 UI 0 0 0 0 0 0 0 0 0 0
 1234 UI 0 0 0 0 0 0 0 0 0 0
 1235 UI 0 0 0 0 0 0 0 0 0 0

1236 KK DIV24A DIVERT
 1237 KM
 1238 DT RET24A 39.6 0.0
 1239 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1240 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

1241 KK CP24A COMBINE
 1242 KM
 1243 HC 3 8.62

1244 KK E247A1 ROUTE
 1245 KM
 1246 KM Revised for channel length/routing steps and cross section between
 1247 KM Signal Butte Rd. and Crimson Rd. to account for concrete lining.
 1248 KM by Parsons Corporation 2015-12
 1249 RS 4 FLOW
 1250 RC 0.016 0.016 0.016 5594 0.0017 97.50
 1251 RX 0.00 7.50 15.00 30.00 42.00 57.00 64.50 72.00
 1252 RY 97.95 97.73 97.50 90.00 90.00 97.50 97.73 97.95

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1253 KK E27A BASIN
 1254 KM
 1255 BA 0.544
 1256 LG 0.20 0.15 7.00 0.15 54
 1257 UI 0 50 84 198 261 316 393 565 570 439
 1258 UI 360 288 227 143 86 75 50 32 15 15
 1259 UI 15 15 15 0 0 0 0 0 0 0
 1260 UI 0 0 0 0 0 0 0 0 0 0
 1261 UI 0 0 0 0 0 0 0 0 0 0

1262 KK DIV27A DIVERT
 1263 KM
 1264 DT RET27A 42.0 0.0
 1265 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 1266 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

1267 KK CPE27A COMBINE
 1268 KM
 1269 KM Confluence of channel south of Eastmark/southeast of PPG North and portion
 1270 KM of PPG with SR 24 offsite channel.
 1271 KM by Parsons Corporation 2015-11
 1272 HC 3 12.81

1273 KK E247A2 ROUTE
 1274 KM
 1275 KM Revised for channel length/routing steps and cross section between
 1276 KM Signal Butte Rd. and Crismon Rd. to account for concrete lining.
 1277 KM by Parsons Corporation 2015-12
 1278 RS 1 FLOW
 1279 RC 0.016 0.016 0.016 1528 0.0017 97.50
 1280 RX 0.00 7.50 15.00 30.00 42.00 57.00 64.50 72.00
 1281 RY 97.95 97.73 97.50 90.00 90.00 97.50 97.73 97.95

1282 KK E2726A ROUTE
 1283 KO 1
 1284 KM

1285 KM Revised for channel length/routing steps and cross section between
 1286 KM Signal Butte Rd. and Crismon Rd. to account for concrete lining.
 1287 KM by Parsons Corporation 2015-12
 1288 RS 4 FLOW
 1289 RC 0.016 0.016 0.016 6350 0.0016 97.50
 1290 RX 0.00 7.50 15.00 30.00 42.00 57.00 64.50 72.00
 1291 RY 97.95 97.73 97.50 90.00 90.00 97.50 97.73 97.95

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1449 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1450 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*
1451 KK E8E6 ROUTE
1452 KM
1453 RS 9 FLOW
1454 RC 0.060 0.035 0.060 9833 0.0052 5.50
1455 RX 0.00 500.00 980.00 1003.00 1007.00 1031.00 1511.00 2011.00
1456 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
*
1457 KK CPE6 COMBINE
1458 KM
1459 HC 3 3.05

```

1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

1460 KK DE6S DIVERT
1461 KM
1462 DT DRE9 0.0 0.0
1463 DI 0.0 236.0 682.0 1141.0 1670.0 2261.0 2886.0 0.0 0.0 0.0
1464 DQ 0.0 1.0 13.0 212.0 633.0 1096.0 1568.0 0.0 0.0 0.0
*

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```

1465 KK E6E15 ROUTE
1466 KM
1467 RS 7 FLOW
1468 RC 0.035 0.030 0.035 8259 0.0042 5.50
1469 RX 950.00 975.00 991.00 1003.00 1007.00 1019.00 1030.00 1065.00
1470 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
*

```

```

1471 KK E15 BASIN
1472 KM
1473 BA 0.777
1474 LG 0.15 0.25 5.10 0.35 57
1475 UI 0 106 363 582 791 1239 1004 734 522 273
1476 UI 171 106 36 32 32 0 0 0 0 0
1477 UI 0 0 0 0 0 0 0 0 0 0
1478 UI 0 0 0 0 0 0 0 0 0 0
1479 UI 0 0 0 0 0 0 0 0 0 0
*

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```

1480 KK DIVE15 DIVERT
1481 KM
1482 DT RETE15 67.7 0.0
1483 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1484 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

```

```

1485 KK DRE9RETRIEVE
1486 KM
1487 DR DRE9
*

```

```

1488 KK RTE6E9 ROUTE
1489 KM
1490 RS 5 FLOW
1491 RC 0.035 0.030 0.025 2200 0.0035 6.00
1492 RX 0.00 100.00 700.00 1050.00 1090.00 1110.00 1140.00 1240.00
1493 RY 0.00 6.00 4.00 1.00 1.00 5.00 6.00 6.00
*

```

```

1494 KK E9 BASIN
1495 KM
1496 BA 0.723
1497 LG 0.14 0.25 5.40 0.30 58
1498 UI 0 88 253 450 585 836 1040 754 570 416
1499 UI 225 148 92 48 27 27 0 0 0 0
1500 UI 0 0 0 0 0 0 0 0 0 0
1501 UI 0 0 0 0 0 0 0 0 0 0
*

```

1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

1502 UI 0 0 0 0 0 0 0 0 0 0
*

```

```

1503 KK DIVE9 DIVERT
1504 KM
1505 DT RETE9 65.4 0.0
1506 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1507 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

```

```

1508 KK CPE9 COMBINE
1509 KM
1510 HC 2
*

```

```

1511 KK DE9S DIVERT
1512 KM
1513 DT DRR5 0.0 0.0
1514 DI 0.0 78.0 163.0 440.0 936.0 1475.0 2024.0 0.0 0.0 0.0
1515 DQ 0.0 1.0 43.0 245.0 670.0 1157.0 1661.0 0.0 0.0 0.0
*

```

```

1516 KK E9E16 ROUTE
1517 KM

```

```

1518 RS 6 FLOW
1519 RC 0.035 0.030 0.035 6751 0.0040 5.50
1520 RX 950.00 985.00 991.00 1003.00 1007.00 1019.00 1025.00 1060.00
1521 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
*

```

```

1522 KK E16 BASIN
1523 KM
1524 BA 0.396
1525 LG 0.15 0.25 5.10 0.35 57
1526 UI 0 58 224 342 497 684 480 338 207 100
1527 UI 64 26 18 18 0 0 0 0 0 0
1528 UI 0 0 0 0 0 0 0 0 0 0
1529 UI 0 0 0 0 0 0 0 0 0 0
1530 UI 0 0 0 0 0 0 0 0 0 0
*

```

```

1531 KK DIVE16 DIVERT
1532 KM
1533 DT RETE16 35.1 0.0
1534 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1535 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

```

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

1539 KK E16E15 ROUTE
1540 KM
1541 RS 10 FLOW
1542 RC 0.030 0.012 0.030 4112 0.0015 5.00
1543 RX 45.00 65.00 71.00 83.00 87.00 99.00 105.00 125.00
1544 RY 5.00 4.50 4.00 1.00 1.00 4.00 4.50 5.00
*

```

```

1545 KK CPE15 COMBINE
1546 KM
1547 HC 3 4.95
*

```

```

1548 KK E1524B ROUTE
1549 KM
1550 RS 3 FLOW
1551 RC 0.035 0.030 0.035 4705 0.0033 5.00
1552 RX 0.00 60.00 71.00 83.00 87.00 99.00 110.00 170.00
1553 RY 5.00 5.00 5.00 1.00 1.00 2.00 3.00 4.00
*

```

```

1554 KK E5B BASIN
1555 KM
1556 BA 0.286
1557 LG 0.14 0.25 3.95 0.64 62
1558 UI 0 64 225 342 567 435 287 148 74 36
1559 UI 15 15 0 0 0 0 0 0 0 0
1560 UI 0 0 0 0 0 0 0 0 0 0
1561 UI 0 0 0 0 0 0 0 0 0 0
1562 UI 0 0 0 0 0 0 0 0 0 0
*

```

```

1563 KK DIVE5B DIVERT
1564 KM
1565 DT RETE5B 25.0 0.0
1566 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1567 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

```

```

1568 KK E5E14B ROUTE
1569 KM
1570 RS 5 FLOW
1571 RC 0.035 0.030 0.035 6256 0.0054 5.50
1572 RX 950.00 985.00 991.00 1003.00 1007.00 1019.00 1025.00 1050.00
1573 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
*

```

```

1574 KK E14B BASIN
1575 KM
1576 BA 0.528
1577 LG 0.14 0.25 5.60 0.29 60
1578 UI 0 125 435 667 1086 785 512 237 126 53
1579 UI 29 29 0 0 0 0 0 0 0 0
1580 UI 0 0 0 0 0 0 0 0 0 0
*

```

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

1581 UI 0 0 0 0 0 0 0 0 0 0
1582 UI 0 0 0 0 0 0 0 0 0 0
*

```

```

1583 KK DIV14B DIVERT
1584 KM
1585 DT RET14B 48.4 0.0
1586 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1587 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

```

```

1588 KK CP14B COMBINE

```

1589 KM
1590 HC 2
*
1591 KK E14E24 ROUTE
1592 KM
1593 RS 5 FLOW
1594 RC 0.030 0.030 0.030 6080 0.0032 9.00
1595 RX 970.00 990.00 1001.00 1010.00 1014.00 1023.00 1034.00 1054.00
1596 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
*

1597 KK E24B BASIN
1598 KM
1599 BA 0.464
1600 LG 0.15 0.15 7.30 0.14 57
1601 UI 0 92 339 513 852 731 493 294 133 76
1602 UI 24 24 0 0 0 0 0 0 0 0
1603 UI 0 0 0 0 0 0 0 0 0 0
1604 UI 0 0 0 0 0 0 0 0 0 0
1605 UI 0 0 0 0 0 0 0 0 0 0
*

1606 KK DIV24B DIVERT
1607 KM
1608 DT RET24B 38.7 0.0
1609 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1610 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

1611 KK CPE24B COMBINE
1612 KM
1613 HC 3
*

1614 KK E24E28 ROUTE
1615 KM
1616 RS 4 FLOW
1617 RC 0.035 0.035 0.035 6172 0.0036 10.00
1618 RX 940.00 960.00 980.00 1000.00 1010.00 1030.00 1050.00 1070.00
1619 RY 7.00 6.00 5.00 1.00 1.00 5.00 6.00 7.00
*

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1620 KK E28B BASIN
1621 KM
1622 BA 0.539
1623 LG 0.20 0.15 8.40 0.09 51
1624 UI 0 65 183 329 427 606 772 566 430 318
1625 UI 179 110 73 41 20 20 20 0 0 0
1626 UI 0 0 0 0 0 0 0 0 0 0
1627 UI 0 0 0 0 0 0 0 0 0 0
1628 UI 0 0 0 0 0 0 0 0 0 0
*

1629 KK DIV28B DIVERT
1630 KM
1631 DT RET28B 42.0 0.0
1632 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1633 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

1634 KK CPE28B COMBINE
1635 KM
1636 HC 2
*

1637 KK E28E31 ROUTE
1638 KM
1639 RS 3 FLOW
1640 RC 0.040 0.040 0.040 5081 0.0036 10.00
1641 RX 950.00 975.00 985.00 1005.00 1010.00 1030.00 1040.00 1065.00
1642 RY 7.00 6.50 6.00 1.00 1.00 6.00 6.50 7.00
*

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1657 KK E25E29 ROUTE
1658 KM
1659 RS 20 FLOW

1660 RC 0.030 0.030 0.030 7016 0.0022 2.50
1661 RX 976.00 996.00 1003.00 1005.00 1006.00 1008.00 1015.00 1025.00
1662 RY 2.50 2.00 1.50 1.00 1.00 1.50 2.00 2.50
*

1663 KK E29 BASIN
1664 KM
1665 BA 1.002
1666 LG 0.15 0.23 6.20 0.22 55
1667 UI 0 103 218 452 586 733 1019 1240 924 737
1668 UI 574 428 229 172 116 82 31 31 31 31
1669 UI 0 0 0 0 0 0 0 0 0 0
1670 UI 0 0 0 0 0 0 0 0 0 0
1671 UI 0 0 0 0 0 0 0 0 0 0
*

1672 KK DIVE29 DIVERT
1673 KM
1674 DT RETE29 73.9 0.0
1675 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1676 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

1677 KK CPE29 COMBINE
1678 KM
1679 HC 2
*

1680 KK E29E31 ROUTE
1681 KM
1682 RS 4 FLOW
1683 RC 0.030 0.030 0.030 7025 0.0034 10.00
1684 RX 950.00 975.00 985.00 1005.00 1006.00 1026.00 1036.00 1070.00
1685 RY 8.00 7.00 6.00 1.00 1.00 6.00 7.00 8.00
*

1686 KK E32 BASIN
1687 KM
1688 BA 0.246
1689 LG 0.14 0.25 4.25 0.55 58
1690 UI 0 72 238 387 535 337 190 78 37 15
1691 UI 15 0 0 0 0 0 0 0 0 0
1692 UI 0 0 0 0 0 0 0 0 0 0
1693 UI 0 0 0 0 0 0 0 0 0 0
1694 UI 0 0 0 0 0 0 0 0 0 0
*

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1695 KK DIVE32 DIVERT
1696 KM
1697 DT RETE32 17.2 0.0
1698 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1699 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

1700 KK E32E31 ROUTE
1701 KM
1702 RS 5 FLOW
1703 RC 0.025 0.060 0.025 3272 0.0028 1388.60
1704 RX 100.00 110.00 128.00 149.80 160.00 191.50 209.20 210.00
1705 RY 1388.3 1388.32 1388.32 1380.37 1380.17 1388.04 1388.39 1388.60
*

1706 KK E31 BASIN
1707 KM
1708 BA 0.810
1709 LG 0.15 0.25 4.80 0.39 55
1710 UI 0 86 197 391 504 641 943 970 728 571
1711 UI 441 296 151 126 86 37 26 26 26 0
1712 UI 0 0 0 0 0 0 0 0 0 0
1713 UI 0 0 0 0 0 0 0 0 0 0
1714 UI 0 0 0 0 0 0 0 0 0 0
*

1715 KK DIVE31 DIVERT
1716 KM
1717 DT RETE31 56.5 0.0
1718 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1719 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

1720 KK CPE31 COMBINE
1721 KM
1722 HC 4
*

1723 KK E31E30 ROUTE
1724 KM
1725 RS 5 FLOW
1726 RC 0.025 0.045 0.025 4404 0.0008 1387.00
1727 RX 100.00 107.00 112.50 144.90 175.10 201.50 225.90 244.00
1728 RY 1386.1 1386.09 1386.09 1377.99 1377.99 1384.59 1385.08 1387.00
*

1729 KK E30B BASIN
1730 KM
1731 BA 0.882
1732 LG 0.24 0.15 8.40 0.09 47
1733 UI 0 56 56 128 217 272 314 357 416 500
1734 UI 668 683 552 475 416 355 303 261 191 124

1735 UI 98 92 66 56 44 17 17 17 17 17
1736 UI 17 17 0 0 0 0 0 0 0 0
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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1737 UI 0 0 0 0 0 0 0 0 0 0
*

1738 KK DIV30B DIVERT
1739 KM
1740 DT RET30B 67.1 0.0
1741 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1742 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

1743 KK CPE30 COMBINE
1744 KM
1745 HC 2
*

1746 KK E30E26 ROUTE
1747 KM
1748 RS 1 FLOW
1749 RC 0.025 0.035 0.025 822 0.0005 1387.00
1750 RX 100.00 105.00 108.50 149.90 220.10 251.30 279.10 285.10
1751 RY 1387.0 1387.00 1386.66 1376.31 1376.31 1384.11 1384.66 1386.00
*

1752 KK E26B BASIN
1753 KM
1754 BA 0.259
1755 LG 0.24 0.15 8.80 0.07 48
1756 UI 0 38 145 222 320 448 315 222 139 65
1757 UI 43 18 12 12 0 0 0 0 0 0
1758 UI 0 0 0 0 0 0 0 0 0 0
1759 UI 0 0 0 0 0 0 0 0 0 0
1760 UI 0 0 0 0 0 0 0 0 0 0
*

1761 KK DIV26B DIVERT
1762 KM
1763 DT RET26B 20.1 0.0
1764 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1765 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

1766 KK CPE26 COMBINE
1767 KM
1768 HC 2
*

1769 KK E26E33 ROUTE
1770 KM
1771 RS 5 FLOW
1772 RC 0.025 0.030 0.025 8929 0.0028 1379.67
1773 RX 100.00 100.50 102.50 134.90 205.10 237.50 253.50 255.00
1774 RY 1379.1 1379.12 1379.35 1371.25 1371.25 1379.35 1379.67 1379.67
*

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1775 KK E33B BASIN
1776 KM
1777 BA 0.851
1778 LG 0.15 0.15 7.30 0.14 56
1779 UI 0 117 409 651 892 1385 1087 793 558 278
1780 UI 179 110 36 36 0 0 0 0 0 0
1781 UI 0 0 0 0 0 0 0 0 0 0
1782 UI 0 0 0 0 0 0 0 0 0 0
1783 UI 0 0 0 0 0 0 0 0 0 0
*

1784 KK DIV33B DIVERT
1785 KM
1786 DT RET33B 66.8 0.0
1787 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1788 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

1789 KK CPE33B COMBINE
1790 KM
1791 HC 3
*

1792 KK E33P9A ROUTE
1793 KM
1794 RS 1 FLOW
1795 RC 0.025 0.060 0.025 2115 0.0039 8.00
1796 RX 0.00 18.00 21.00 33.00 93.00 105.00 108.00 129.00
1797 RY 8.00 8.00 6.50 0.50 0.50 6.50 8.00 8.00
*

1798 KK E33P9B ROUTE
1799 KM
1800 RS 1 FLOW
1801 RC 0.025 0.060 0.025 2299 0.0029 8.20
1802 RX 0.00 18.00 21.00 33.00 93.00 105.00 108.00 129.00
1803 RY 8.20 8.00 6.50 0.50 0.50 6.50 8.00 8.20
*

1804 KK P9 BASIN
1805 KM
1806 BA 1.122
1807 LG 0.11 0.15 8.00 0.12 74
1808 UI 0 119 271 539 695 881 1292 1349 1011 795
1809 UI 612 416 214 177 119 55 36 36 36 0
1810 UI 0 0 0 0 0 0 0 0 0 0
1811 UI 0 0 0 0 0 0 0 0 0 0
1812 UI 0 0 0 0 0 0 0 0 0 0
*

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1813 KK DIVP9 DIVERT
1814 KM
1815 DT RETP9 36.4 0.0
1816 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1817 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

1818 KK CPP9 COMBINE
1819 KM
1820 HC 2
*

1821 KK P9EMF1 ROUTE
1822 KM
1823 RS 1 FLOW
1824 RC 0.025 0.029 0.025 4403 0.0029 8.00
1825 RX 0.00 18.00 21.00 33.00 93.00 105.00 108.00 129.00
1826 RY 8.00 8.00 6.50 0.50 0.50 6.50 8.00 8.00
*

1827 KK EMF1B BASIN
1828 KM
1829 BA 1.036
1830 LG 0.12 0.14 7.60 0.13 63
1831 UI 0 117 296 556 717 944 1407 1153 891 677
1832 UI 493 256 194 117 66 36 36 0 0
1833 UI 0 0 0 0 0 0 0 0 0
1834 UI 0 0 0 0 0 0 0 0 0
1835 UI 0 0 0 0 0 0 0 0 0
*

1836 KK DEMF1B DIVERT
1837 KM
1838 DT REMF1B 85.0 0.0
1839 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1840 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

1841 KK CPEMF1 COMBINE
1842 KM
1843 HC 2
*

1844 KK EM1EM2 ROUTE
1845 KM
1846 RS 19 FLOW
1847 RC 0.030 0.015 0.030 5153 0.0012 1326.70
1848 RX 4931.0 4943.00 4952.00 4974.00 5022.00 5047.00 5058.00 5064.00
1849 RY 1324.0 1323.90 1323.80 1312.60 1312.70 1323.30 1324.30 1326.70
*

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1850 KK EMF2 BASIN
1851 KM
1852 BA 1.850
1853 LG 0.13 0.21 6.40 0.22 62
1854 UI 0 108 108 195 388 494 572 641 733 839
1855 UI 1028 1347 1292 1063 927 823 707 618 533 447
1856 UI 319 191 184 178 116 108 90 33 33 33
1857 UI 33 33 33 33 33 0 0 0 0 0
1858 UI 0 0 0 0 0 0 0 0 0 0
*

1859 KK DIVEM2 DIVERT
1860 KM
1861 DT RETEM2 96.9 0.0
1862 DI 0.0 78.0 79.0 10079.0 0.0 0.0 0.0 0.0 0.0 0.0
1863 DQ 0.0 0.0 1.0 10001.0 0.0 0.0 0.0 0.0 0.0 0.0
*

1864 KK CPEMF2 COMBINE
1865 KM
1866 HC 2
*

1867 KK EM2M3A ROUTE
1868 KM
1869 RS 1 FLOW
1870 RC 0.030 0.030 0.030 1085 0.0002 1326.40
1871 RX 4945.0 4946.00 4947.00 4976.00 5027.00 5057.00 5109.00 5120.00
1872 RY 1324.1 1324.10 1324.10 1311.10 1311.10 1325.20 1325.30 1326.40
*

1873 KK EM2M3B ROUTE
1874 KM

```

1875 RS 1 FLOW
1876 RC 0.030 0.020 0.030 972 0.0002 1324.10
1877 RX 4829.0 4848.00 4879.00 4912.00 5087.00 5120.00 5163.00 5172.00
1878 RY 1324.1 1322.00 1321.30 1310.50 1309.80 1321.00 1322.70 1324.10
*
1879 KK EMF3 BASIN
1880 KM
1881 BA 1.489
1882 LG 0.21 0.24 4.80 0.42 52
1883 UI 0 104 104 298 444 544 625 737 879 1196
1884 UI 1278 1014 866 740 627 521 421 265 184 171
1885 UI 124 104 69 32 32 32 32 32 32 0
1886 UI 0 0 0 0 0 0 0 0 0 0
1887 UI 0 0 0 0 0 0 0 0 0 0
*

```

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

1888 KK DIVEM3 DIVERT
1889 KM
1890 DT RETEM3 59.1 0.0
1891 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1892 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

```

```

1893 KK CPEMF3 COMBINE
1894 KM
1895 HC 2
*

```

```

1896 KK EMF3RB ROUTE
1897 KM
1898 RS 1 FLOW
1899 RC 0.030 0.025 0.030 939 0.0007 1324.10
1900 RX 4829.0 4848.00 4879.00 4912.00 5087.00 5120.00 5163.00 5172.00
1901 RY 1324.1 1322.00 1321.30 1310.50 1309.80 1321.00 1322.70 1324.10
*

```

```

1902 KK RITBAS BASIN
1903 KM
1904 BA 0.294
1905 LG 0.01 0.02 4.80 0.25 0
1906 UI 0 1043 1115 112 0 0 0 0 0 0
1907 UI 0 0 0 0 0 0 0 0 0 0
1908 UI 0 0 0 0 0 0 0 0 0 0
1909 UI 0 0 0 0 0 0 0 0 0 0
1910 UI 0 0 0 0 0 0 0 0 0 0
*

```

```

1911 KK RITBAS STORAGE
1912 KM
1913 KO
1914 RS 1 STOR
1915 SV 22.00 99.00 213.00 331.00 451.00 571.00 693.00
1916 SQ 1.00 2.00 3.00 4.00 5.00 6.00 7.00
1917 SE 1311.0 1312.00 1313.00 1314.00 1315.00 1316.00 1317.00 1318.00
1918 ST 1318.0 900.0 3.0 1.5
*

```

```

1919 KK CPRITB COMBINE
1920 KM
1921 HC 2
*

```

```

1922 KK RBEMF4 ROUTE
1923 KM
1924 RS 3 FLOW
1925 RC 0.030 0.030 0.030 2391 0.0001 1324.10
1926 RX 4829.0 4848.00 4879.00 4912.00 5087.00 5120.00 5163.00 5172.00
1927 RY 1324.1 1322.00 1321.30 1310.50 1309.80 1321.00 1322.70 1324.10
*

```

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

1929 KK R2 BASIN
1930 KM
1931 BA 0.677
1932 LG 0.28 0.25 5.80 0.23 22
1933 UI 0 52 52 176 237 335 402 537 651
1934 UI 517 432 364 303 251 182 109 88 75 52
1935 UI 42 16 16 16 16 16 0 0 0 0
1936 UI 0 0 0 0 0 0 0 0 0 0
1937 UI 0 0 0 0 0 0 0 0 0 0
*

```

```

1938 KK DIVR2 DIVERT
1939 KM
1940 DT RETR2 18.5 0.0
1941 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1942 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

```

```

1943 KK R3 BASIN
1944 KM
1945 BA 0.413
1946 LG 0.27 0.25 4.65 0.36 19
1947 UI 0 34 42 122 165 196 235 293 413 372

```

```

1948 UI 298 250 205 167 122 71 57 45 34 20
1949 UI 10 10 10 10 10 0 0 0 0 0
1950 UI 0 0 0 0 0 0 0 0 0 0
1951 UI 0 0 0 0 0 0 0 0 0 0
*
1952 KK DIVR3 DIVERT
1953 KM
1954 DT RETR3 15.6 0.0
1955 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1956 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

```

```

1957 KK CPR2R3 COMBINE
1958 KM
1959 HC 2
*

```

```

1960 KK R2R3R6 ROUTE
1961 KM
1962 RS 18 FLOW
1963 RC 0.045 0.040 0.045 7280 0.0033 2.50
1964 RX 0.00 500.00 1000.00 1001.00 1002.00 1500.00 2000.00 2500.00
1965 RY 2.50 2.00 1.50 1.00 1.00 1.50 2.00 2.50
*

```

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

1966 KK R6 BASIN
1967 KM
1968 BA 0.504
1969 LG 0.30 0.25 4.65 0.39 15
1970 UI 0 40 46 143 194 231 274 336 472 469
1971 UI 369 312 255 211 166 99 70 63 40 35
1972 UI 12 12 12 12 12 12 0 0 0 0
1973 UI 0 0 0 0 0 0 0 0 0 0
1974 UI 0 0 0 0 0 0 0 0 0 0
*

```

```

1975 KK CPR6 COMBINE
1976 KM
1977 HC 2
*

```

```

1978 KK R6R9 ROUTE
1979 KM
1980 RS 4 FLOW
1981 RC 0.035 0.035 0.035 6687 0.0040 6.00
1982 RX 961.00 981.00 989.00 1001.00 1005.00 1017.00 1025.00 1045.00
1983 RY 6.00 5.00 4.00 1.00 1.00 4.00 5.00 6.00
*

```

```

1984 KK R9 BASIN
1985 KM
1986 BA 0.592
1987 LG 0.16 0.25 4.80 0.40 64
1988 UI 0 80 269 435 585 924 773 566 409 222
1989 UI 134 81 34 24 24 0 0 0 0 0
1990 UI 0 0 0 0 0 0 0 0 0 0
1991 UI 0 0 0 0 0 0 0 0 0 0
1992 UI 0 0 0 0 0 0 0 0 0 0
*

```

```

1993 KK DIVR9 DIVERT
1994 KM
1995 DT RETR9 54.2 0.0
1996 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
1997 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*

```

```

1998 KK CPR9 COMBINE
1999 KM
2000 HC 2
*

```

```

2001 KK R9R11 ROUTE
2002 KM
2003 RS 7 FLOW
2004 RC 0.035 0.035 0.035 7667 0.0030 6.00
2005 RX 950.00 977.00 989.00 1001.00 1006.00 1018.00 1030.00 1050.00
2006 RY 6.00 5.00 4.00 1.00 1.00 4.00 5.00 6.00
*

```

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

2007 KK R11 BASIN
2008 KM
2009 BA 0.986
2010 LG 0.14 0.23 6.20 0.23 45
2011 UI 0 101 213 442 574 717 994 1219 912 728
2012 UI 567 426 229 169 116 84 31 31 31 31
2013 UI 0 0 0 0 0 0 0 0 0 0
2014 UI 0 0 0 0 0 0 0 0 0 0
2015 UI 0 0 0 0 0 0 0 0 0 0
*

```

```

2016 KK DIVR11 DIVERT
2017 KM
2018 DT RETR11 67.9 0.0

```


2019 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 2020 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

2021 KK DRR5RETRIEVE
 2022 KM
 2023 DR DRR5
 *

2024 KK R5 BASIN
 2025 KM
 2026 BA 0.504
 2027 LG 0.29 0.25 5.40 0.27 21
 2028 UI 0 53 120 241 310 393 574 608 455 358
 2029 UI 277 189 98 80 53 26 16 16 16 16
 2030 UI 0 0 0 0 0 0 0 0 0 0
 2031 UI 0 0 0 0 0 0 0 0 0 0
 2032 UI 0 0 0 0 0 0 0 0 0 0
 *

2033 KK DIVR5 DIVERT
 2034 KM
 2035 DT RETR5 1.0 0.0
 2036 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 2037 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

2038 KK CPR5 COMBINE
 2039 KM
 2040 HC 2 1.22
 *

2041 KK R5R8 ROUTE
 2042 KM
 2043 RS 5 FLOW
 2044 RC 0.040 0.035 0.040 6587 0.0043 5.00
 2045 RX 966.00 986.00 994.00 1006.00 1012.00 1024.00 1032.00 1052.00
 2046 RY 5.00 4.50 4.00 1.00 1.00 4.00 4.50 5.00
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2047 KK R8 BASIN
 2048 KM
 2049 BA 0.554
 2050 LG 0.16 0.25 4.60 0.45 64
 2051 UI 0 69 208 360 471 695 788 567 421 299
 2052 UI 149 105 69 23 21 21 0 0 0
 2053 UI 0 0 0 0 0 0 0 0 0
 2054 UI 0 0 0 0 0 0 0 0 0
 2055 UI 0 0 0 0 0 0 0 0 0
 *

2056 KK DIVR8 DIVERT
 2057 KM
 2058 DT RETR8 50.5 0.0
 2059 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 2060 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

2061 KK CPR8 COMBINE
 2062 KM
 2063 HC 2
 *

2064 KK R8R11 ROUTE
 2065 KM
 2066 RS 7 FLOW
 2067 RC 0.070 0.030 0.040 5355 0.0037 15.00
 2068 RX 0.00 1000.00 1005.00 1010.00 1050.00 1060.00 1560.00 2060.00
 2069 RY 15.00 14.50 13.00 12.00 11.00 13.00 14.50 15.00
 *

2070 KK CPR11 COMBINE
 2071 KM
 2072 HC 3
 *

2073 KK R11R13 ROUTE
 2074 KM
 2075 RS 6 FLOW
 2076 RC 0.040 0.025 0.040 5263 0.0027 15.00
 2077 RX 0.00 1000.00 1005.00 1010.00 1050.00 1060.00 1560.00 2060.00
 2078 RY 15.00 14.50 13.00 12.00 11.00 13.00 14.50 15.00
 *

2079 KK R13 BASIN
 2080 KM
 2081 BA 0.501
 2082 LG 0.15 0.25 3.95 0.63 56
 2083 UI 0 80 322 483 750 853 575 392 188 110
 2084 UI 58 24 24 0 0 0 0 0 0 0
 2085 UI 0 0 0 0 0 0 0 0 0 0
 2086 UI 0 0 0 0 0 0 0 0 0 0
 2087 UI 0 0 0 0 0 0 0 0 0 0
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1

2088 KK DIVR13 DIVERT
 2089 KM
 2090 DT RETR13 33.8 0.0
 2091 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 2092 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

2093 KK CPR13 COMBINE
 2094 KM
 2095 HC 2
 *

2096 KK R13R16 ROUTE
 2097 KM
 2098 RS 7 FLOW
 2099 RC 0.070 0.025 0.045 5239 0.0031 15.00
 2100 RX 0.00 1000.00 1005.00 1010.00 1050.00 1060.00 1560.00 2060.00
 2101 RY 15.00 14.50 13.00 12.00 11.00 13.00 14.50 15.00
 *

2102 KK R16 BASIN
 2103 KM
 2104 BA 0.498
 2105 LG 0.13 0.25 4.25 0.57 67
 2106 UI 0 90 343 515 840 812 552 353 157 97
 2107 UI 39 25 25 0 0 0 0 0 0 0
 2108 UI 0 0 0 0 0 0 0 0 0 0
 2109 UI 0 0 0 0 0 0 0 0 0 0
 2110 UI 0 0 0 0 0 0 0 0 0 0
 *

2111 KK DIVR16 DIVERT
 2112 KM
 2113 DT RETR16 37.2 0.0
 2114 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 2115 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

2116 KK CPR16 COMBINE
 2117 KM
 2118 HC 2
 *

2119 KK R16R21 ROUTE
 2120 KM
 2121 RS 12 FLOW
 2122 RC 0.070 0.035 0.045 10034 0.0042 15.00
 2123 RX 0.00 1000.00 1005.00 1010.00 1050.00 1060.00 1560.00 2060.00
 2124 RY 15.00 14.50 13.00 12.00 11.00 13.00 14.50 15.00
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2125 KK R21 BASIN
 2126 KM
 2127 BA 0.836
 2128 LG 0.22 0.24 4.80 0.35 33
 2129 UI 0 65 65 227 302 364 428 515 701 804
 2130 UI 628 529 440 366 299 210 120 108 82 65
 2131 UI 38 20 20 20 20 20 0 0 0 0
 2132 UI 0 0 0 0 0 0 0 0 0 0
 2133 UI 0 0 0 0 0 0 0 0 0 0
 *

2134 KK DIVR21 DIVERT
 2135 KM
 2136 DT RETR21 18.4 0.0
 2137 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 2138 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

2139 KM
 2140 KK R1 BASIN
 2141 KM
 2142 BA 1.448
 2143 LG 0.25 0.25 4.55 0.42 30
 2144 UI 0 132 222 523 691 836 1039 1490 1523 1171
 2145 UI 960 769 608 389 230 203 132 90 40 40
 2146 UI 40 40 40 40 0 0 0 0 0 0
 2147 UI 0 0 0 0 0 0 0 0 0 0
 2148 UI 0 0 0 0 0 0 0 0 0 0
 *

2149 KK DIVR1 DIVERT
 2150 KM
 2151 DT RETR1 100.2 0.0
 2152 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 2153 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

2154 KK R1R4 ROUTE
 2155 KM
 2156 RS 26 FLOW
 2157 RC 0.070 0.070 0.070 5946 0.0054 2.50
 2158 RX 0.00 500.00 1000.00 1001.00 1002.00 1500.00 2000.00 2500.00
 2159 RY 2.50 2.00 1.50 1.00 1.00 1.50 2.00 2.50
 *

2160 KK R4 BASIN
 2161 KM
 2162 BA 0.998

1

2163	LG	0.30	0.25	4.60	0.40	5														
2164	UI	0	87	129	330	440	526	643	871	1074	840									
2165	UI	691	562	455	345	198	148	118	87	48	27									
2166	UI	27	27	27	27	0	0	0	0	0	0									
2167	UI	0	0	0	0	0	0	0	0	0	0									
2168	UI	0	0	0	0	0	0	0	0	0	0									

1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2169	KK	CPR4	COMBINE																	
2170	KM																			
2171	HC	2																		
	*																			
2172	KK	R4R7	ROUTE																	
2173	KM																			
2174	RS	6	FLOW																	
2175	RC	0.050	0.025	0.070	5336	0.0052	15.00													
2176	RX	0.00	10.00	20.00	25.00	65.00	75.00	575.00	1075.00											
2177	RY	15.00	14.50	14.00	12.00	11.00	12.50	14.00	15.00											
	*																			

2178	KK	R7	BASIN																		
2179	KM																				
2180	BA	1.003																			
2181	LG	0.25	0.25	4.65	0.40	34															
2182	UI	0	88	135	338	450	538	662	900	1088	835										
2183	UI	690	557	450	331	188	148	111	88	37	27										
2184	UI	27	27	27	0	0	0	0	0	0	0										
2185	UI	0	0	0	0	0	0	0	0	0	0										
2186	UI	0	0	0	0	0	0	0	0	0	0										
	*																				

2187	KK	DIVR7	DIVERT																		
2188	KM																				
2189	DT	RETR7	47.2	0.0																	
2190	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0										
2191	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0										
	*																				

2192	KK	CPR7	COMBINE																		
2193	KM																				
2194	HC	2																			
	*																				

2195	KK	R7R10	ROUTE																		
2196	KM																				
2197	RS	8	FLOW																		
2198	RC	0.025	0.040	0.035	6813	0.0029	9.00														
2199	RX	75.00	78.00	88.00	100.00	130.00	145.00	155.00	500.00												
2200	RY	9.00	4.00	4.00	1.00	1.00	4.00	5.00	6.00												
	*																				

2201	KK	R10	BASIN																		
2202	KM																				
2203	BA	1.010																			
2204	LG	0.23	0.25	4.70	0.38	35															
2205	UI	0	64	64	142	244	307	355	401	468	556										
2206	UI	737	791	638	548	482	409	354	303	230	153										
2207	UI	112	104	83	64	60	19	19	19	19	19										
2208	UI	19	19	0	0	0	0	0	0	0	0										
2209	UI	0	0	0	0	0	0	0	0	0	0										
	*																				

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2210	KK	DIVR10	DIVERT																		
2211	KM																				
2212	DT	RETR10	69.7	0.0																	
2213	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0										
2214	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0										
	*																				

2215	KK	CPR10	COMBINE																		
2216	KM																				
2217	HC	2																			
	*																				

2218	KK	R10R12	ROUTE																		
2219	KM																				
2220	RS	4	FLOW																		
2221	RC	0.035	0.030	0.035	7002	0.0026	10.00														
2222	RX	940.00	961.00	981.00	1001.00	1005.00	1025.00	1050.00	1075.00												
2223	RY	7.00	6.00	5.00	1.00	1.00	5.00	6.00	7.00												
	*																				

2224	KK	R12	BASIN																		
2225	KM																				
2226	BA	0.486																			
2227	LG	0.10	0.25	4.80	0.43	80															
2228	UI	0	198	609	1126	949	536	201	81	34	0										
2229	UI	0	0	0	0	0	0	0	0	0	0										
2230	UI	0	0	0	0	0	0	0	0	0	0										
2231	UI	0	0	0	0	0	0	0	0	0	0										
2232	UI	0	0	0	0	0	0	0	0	0	0										
	*																				

2233	KK	DIVR12	DIVERT																	
------	----	--------	--------	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--

2234	KM																				
2235	DT	RETR12	40.3	0.0																	
2236	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0										
2237	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0										
	*																				

1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2241	KK	R12R15	ROUTE																		
2242	KM																				
2243	RS	11	FLOW																		
2244	RC	0.045	0.040	0.045	5352	0.0035	2.50														
2245	RX	0.00	500.00	1000.00	1001.00	1002.00	1500.00	2000.00	2500.00												
2246	RY	2.50	2.00	1.50	1.00	1.00	1.50	2.00	2.50												
	*																				

2247	KK	R15	BASIN																	
2248	KM																			
2249	BA	0.562																		
2250	LG	0.24	0.25	4.80	0.37	35														
2251	UI	0	59	132	265	342	432	626	684	510	4									

2305	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2306	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
*													
2307	KK	R14	BASIN										
2308	KM												
2309	BA	0.497											
2310	LG	0.14	0.25	4.55	0.46	61							
2311	UI	0	117	405	621	1015	742	487	229	120	52		
2312	UI	27	27	0	0	0	0	0	0	0	0		
2313	UI	0	0	0	0	0	0	0	0	0	0		
2314	UI	0	0	0	0	0	0	0	0	0	0		
2315	UI	0	0	0	0	0	0	0	0	0	0		
*													
2316	KK	DIVR14	DIVERT										
2317	KM												
2318	DT	RETR14	33.9	0.0									
2319	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2320	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
*													

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2321	KK	R14R17	ROUTE										
2322	KM												
2323	RS	5	FLOW										
2324	RC	0.035	0.030	0.035	6503	0.0031	10.00						
2325	RX	950.00	960.00	980.00	1000.00	1005.00	1025.00	1045.00	1055.00				
2326	RY	7.00	6.00	5.00	1.00	1.00	5.00	6.00	7.00				
*													
2327	KK	R17	BASIN										
2328	KM												
2329	BA	0.491											
2330	LG	0.22	0.25	4.55	0.43	43							
2331	UI	0	45	75	177	234	284	352	505	516	397		
2332	UI	325	261	206	132	78	69	45	31	14	14		
2333	UI	14	14	14	0	0	0	0	0	0	0		
2334	UI	0	0	0	0	0	0	0	0	0	0		
2335	UI	0	0	0	0	0	0	0	0	0	0		
*													

2336	KK	DIVR17	DIVERT										
2337	KM												
2338	DT	RETR17	30.4	0.0									
2339	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2340	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
*													

2341	KK	CPR17	COMBINE										
2342	KM												
2343	HC	2											
*													

2344	KK	R17R22	ROUTE										
2345	KM												
2346	RS	4	FLOW										
2347	RC	0.045	0.035	0.045	6645	0.0048	15.00						
2348	RX	0.00	1000.00	1005.00	1010.00	1050.00	1060.00	1560.00	2060.00				
2349	RY	15.00	14.50	14.00	12.00	11.00	14.00	14.50	15.00				
*													

2350	KK	CPR22	COMBINE										
2351	KM												
2352	HC	3											
*													

2353	KK	R22R21	ROUTE										
2354	KM												
2355	RS	3	FLOW										
2356	RC	0.025	0.050	0.025	4455	0.0022	1363.30						
2357	RX	947.00	954.00	966.00	995.00	1005.00	1034.00	1038.00	1053.00				
2358	RY	1363.3	1363.00	1362.50	1355.30	1355.30	1362.50	1362.50	1363.30				
*													

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2359	KK	CPR21	COMBINE										
2360	KM												
2361	HC	3											
*													

2362	KK	R21R25	ROUTE										
2363	KM												
2364	RS	3	FLOW										
2365	RC	0.025	0.050	0.025	6771	0.0032	1342.30						
2366	RX	941.00	947.00	959.00	984.00	1012.00	1042.00	1046.00	1061.00				
2367	RY	1342.3	1341.50	1341.00	1334.60	1333.60	1341.00	1341.00	1341.30				
*													

2368	KK	R25	BASIN										
2369	KM												
2370	BA	0.279											
2371	LG	0.15	0.23	4.80	0.36	43							
2372	UI	0	62	219	334	553	424	280	144	72	35		
2373	UI	15	15	0	0	0	0	0	0	0	0		
2374	UI	0	0	0	0	0	0	0	0	0	0		
2375	UI	0	0	0	0	0	0	0	0	0	0		
*													

2376	UI	0	0	0	0	0	0	0	0	0	0	0	0
*													
2377	KK	DIVR25	DIVERT										
2378	KM												
2379	DT	RETR25	14.2	0.0									
2380	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2381	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
*													
2382	KK	R20	BASIN										
2383	KM												
2384	BA	0.503											
2385	LG	0.17	0.26	3.45	0.85	47							
2386	UI	0	61	176	313	407	582	724	524	396	290		
2387	UI	156	103	64	33	19	19	19	0	0	0		
2388	UI	0	0	0	0	0	0	0	0	0	0		
2389	UI	0	0	0	0	0	0	0	0	0	0		
2390	UI	0	0	0	0	0	0	0	0	0	0		
*													

2391	KK	DIVR20	DIVERT										
2392	KM												
2393	DT	RETR20	34.4	0.0									
2394	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2395	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
*													

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2396	KK	R20R23	ROUTE										
2397	KM												
2398	RS	6	FLOW										
2399	RC	0.050	0.040	0.050	5267	0.0040	15.00						
2400	RX	0.00	1000.00	1005.00	1010.00	1050.00	1060.00	1560.00	2060.00				
2401	RY	15.00	14.00	13.00	12.00	11.00	14.00	14.50	15.00				
*													
2402	KK	R23	BASIN										
2403	KM												
2404	BA	0.496											
2405	LG	0.15	0.25	4.65	0.42	55							
2406	UI	0	70	254	397	553	833	621	448	304	144		
2407	UI	95	53	22	22	22	0	0	0	0	0		
2408	UI	0	0	0	0	0	0	0	0	0	0		
2409	UI	0	0	0	0	0	0	0	0	0	0		
2410	UI	0	0	0	0	0	0	0	0	0	0		
*													

2411	KK	DIVR23	DIVERT										
2412	KM												
2413	DT	RETR23	35.2	0.0									
2414	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2415	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
*													

2416	KK	CPR23	COMBINE										
2417	KM												
2418	HC	2											
*													

2419	KK	R23R25	ROUTE										
2420	KM												
2421	RS	3	FLOW										
2422	RC	0.035	0.030	0.035	5186	0.0044	15.00						
2423	RX	960.00	980.00	1004.00	1010.00	1050.00	1052.00	1070.00	1090.00				
2424	RY	15.00	13.00	12.50	11.00	11.00	14.00	14.50	15.00				
*													

2425	KK	CPR25	COMBINE										
2426	KM												
2427	HC	3											
*													

2428	KK	R25R24	ROUTE										
2429	KM												
2430	RS	22	FLOW										
2431	RC	0.100	0.010	0.100	454	0.0044	1336.30						
2432	RX	847.00	857.00	939.00	940.00	1031.00	1033.00	1109.00	1137.00				
2433	RY	1333.6	1333.50	1333.40	1326.90	1326.90	1333.40	1334.10	1336.30				
*													

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2434	KK	R19	BASIN										
2435	KM												
2436	BA	1.533											
2437	LG	0.14	0.25	4.35	0.52	60							
2438	UI	0	164	380	749	965	1230	1825	1821	1373	1071		
2439	UI	828	534	285	231	164	60	50	50	50	0		
2440	UI	0	0	0	0	0	0	0	0	0	0		
2441	UI	0	0	0	0	0	0	0	0	0	0		
2442	UI	0	0	0	0	0	0	0	0	0	0		
*													

2443	KK	DIVR19	DIVERT										
2444	KM												
2445	DT	RETR19	108.8	0.0									
2446	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

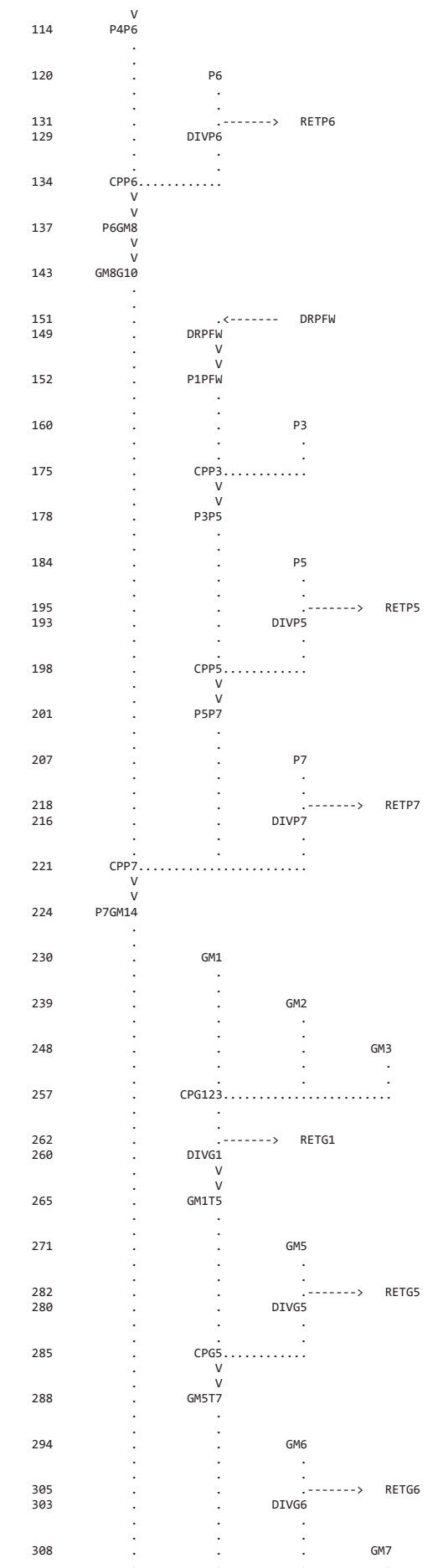
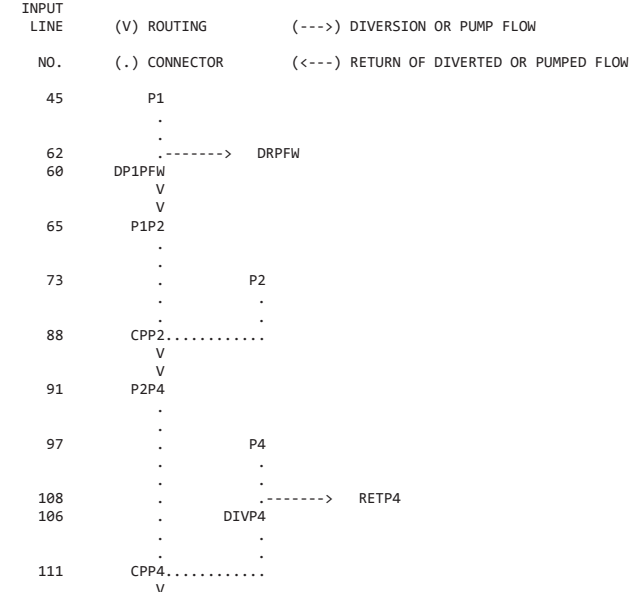
2447	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2448	KK	DIV19R	DIVERT								
2449	KM										
2450	DT	DETR19	35.2	0.0							
2451	DI	0.0	171.0	172.0	10172.0	0.0	0.0	0.0	0.0	0.0	0.0
2452	DQ	0.0	0.0	1.0	10001.0	0.0	0.0	0.0	0.0	0.0	0.0
2453	KK	R19R24	ROUTE								
2454	KM										
2455	RS	8	FLOW								
2456	RC	0.040	0.020	0.040	5577	0.0038	2.50				
2457	RX	0.00	500.00	1000.00	1001.00	1002.00	1500.00	2000.00	2500.00		
2458	RY	2.50	2.00	1.50	1.00	1.00	1.50	2.00	2.50		
2459	KK	R24	BASIN								
2460	KM										
2461	BA	0.294									
2462	LG	0.18	0.25	4.80	0.40	52					
2463	UI	0	40	133	216	291	459	384	281	203	110
2464	UI	67	40	17	12	12	0	0	0	0	0
2465	UI	0	0	0	0	0	0	0	0	0	0
2466	UI	0	0	0	0	0	0	0	0	0	0
2467	UI	0	0	0	0	0	0	0	0	0	0
2468	KK	DIVR24	DIVERT								
2469	KM										
2470	DT	RETR24	19.7	0.0							
2471	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2472	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

1 HEC-1 INPUT PAGE 63

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2473	KK	CPR24	COMBINE								
2474	KM										
2475	HC	3									
2476	KK	R24EM4	ROUTE								
2477	KM										
2478	RS	1	FLOW								
2479	RC	0.025	0.025	0.025	3679	0.0044	1325.00				
2480	RX	933.00	939.00	951.00	977.00	1019.00	1049.00	1053.00	1069.00		
2481	RY	1325.0	1323.60	1323.10	1316.70	1315.70	1323.10	1323.10	1325.00		
2482	KK	EMF4	BASIN								
2483	KM										
2484	BA	0.060									
2485	LG	0.08	0.08	4.80	0.25	0					
2486	UI	0	102	258	87	14	0	0	0	0	0
2487	UI	0	0	0	0	0	0	0	0	0	0
2488	UI	0	0	0	0	0	0	0	0	0	0
2489	UI	0	0	0	0	0	0	0	0	0	0
2490	UI	0	0	0	0	0	0	0	0	0	0
2491	KK	CPEMF4	COMBINE								
2492	HC	3	55.93								
2493	ZZ										

1 SCHEMATIC DIAGRAM OF STREAM NETWORK



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319 . . . . .
317 . . . . . DIVG7 -----> RETG7
322 . . . . . CPG7A.....
325 . . . . . CPG7B.....
. . . . . V
. . . . . V
328 . . . . . GM7T9
334 . . . . . GM8
345 . . . . . DIVG8 -----> RETG8
343 . . . . .
348 . . . . . GM9
. . . . .
359 . . . . . DIVG9 -----> RETG9
357 . . . . .
362 . . . . . CPG9A.....
365 . . . . . GM10
376 . . . . . DIVG10 -----> RETG10
374 . . . . .
379 . . . . . GM11
. . . . .
390 . . . . . DIVG11 -----> RETG11
388 . . . . .
393 . . . . . CPG11.....
396 . . . . . CPG9B.....
. . . . . V
. . . . . V
399 . . . . . GM9T14
405 . . . . . GM12
416 . . . . . DIVG12 -----> RETG12
414 . . . . .
. . . . . V
. . . . . V
419 . . . . . G12T13
425 . . . . . GM13
436 . . . . . DIVG13 -----> RETG13
434 . . . . .
439 . . . . . CPG13.....
. . . . . V
. . . . . V
442 . . . . . G13T14
448 . . . . . GM14
459 . . . . . DIVG14 -----> RETG14
457 . . . . .
462 . . . . . CPG14A.....
465 . . . . . CPG14B.....
468 . . . . . CPG14C.....
. . . . . V
. . . . . V
471 . . . . . G14E26
478 . . . . . E1
. . . . .
493 . . . . . DE1S -----> DRE2
491 . . . . .
. . . . . V

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496 . . . . . E1E10
504 . . . . . E10
522 . . . . . CPE10.....
. . . . . V
. . . . . V
525 . . . . . E10E17
533 . . . . . E17
552 . . . . . DIVE17 -----> RETE17
548 . . . . .
555 . . . . . CPE17.....
. . . . . V
. . . . . V
558 . . . . . E17E21
566 . . . . . E21
582 . . . . . DIVE21 -----> RETE21
578 . . . . .
585 . . . . . CPE21A.....
. . . . . V
. . . . . V
588 . . . . . E21G20
597 . . . . . DRE2 <----- DRE2
595 . . . . .
. . . . . V
. . . . . V
598 . . . . . RTE1E2
606 . . . . . E2
621 . . . . . CPE2.....
626 . . . . . DE2S -----> DRE3
624 . . . . .
. . . . . V
. . . . . V
629 . . . . . E2E11
637 . . . . . E11
655 . . . . . CPE11.....
. . . . . V
. . . . . V
658 . . . . . E11E18
666 . . . . . E18
680 . . . . . DIVE18 -----> RETE18
678 . . . . .
683 . . . . . CPE18.....
. . . . . V
. . . . . V
686 . . . . . E18E21
694 . . . . . CPE21B.....
. . . . . V
. . . . . V
697 . . . . . G20G21
707 . . . . . DRE3 <----- DRE3
705 . . . . .
. . . . . V
. . . . . V
708 . . . . . RTE2E3
716 . . . . . E3
732 . . . . . E2SE3.....
737 . . . . . DRE4N -----> DRE4N
735 . . . . .
. . . . . V
. . . . . V

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```

740 . . . E3E12
. . . . .
748 . . . . . E12
. . . . .
766 . . . CPE12.....
. . . V
. . . V
769 . . . E12E19
. . . . .
777 . . . . . E19
. . . . .
796 . . . CPE19.....
. . . V
. . . V
799 . . . E1922E
. . . . .
807 . . . . . 22E
. . . . .
825 . . . . . E20
. . . V
. . . V
844 . . . . . E2022E
. . . . .
852 . . . CP22E.....
. . . V
. . . V
855 . . . 22EE22
. . . . .
861 . . . . . E22
. . . . .
879 . . . CPE22.....
. . . V
. . . V
882 . . . E22G22
. . . . .
888 . . . GM21
. . . . .
899 . . . . .-> RETG21
897 . . . DIVG21
. . . V
. . . V
902 . . . G21T22
. . . . .
908 . . . . . GM22
. . . . .
919 . . . . .-> RETG22
917 . . . DIVG22
. . . . .
922 . . . CPG22A.....
. . . . .
925 . . . . . GM16
. . . . .
936 . . . . .-> RETG16
934 . . . DIVG16
. . . V
. . . V
939 . . . G16T19
. . . . .
945 . . . . . GM18
. . . . .
956 . . . . .-> RETG18
954 . . . DIVG18
. . . . .
959 . . . CPG18.....
. . . . .
962 . . . . . GM19
. . . . .
973 . . . . .-> RETG19
971 . . . DIVG19
. . . . .
976 . . . CPG19A.....
. . . . .
979 . . . . . GM20
. . . . .
990 . . . . .-> RETG20
988 . . . DIVG20
. . . . .
993 . . . CPG19B.....

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996 . . . CPG22B.....
. . . V
. . . V
1001 . . . G22E26
. . . . .
1010 . . . . .-<----- DRE4N
1008 . . . DRE4N
. . . V
. . . V
1011 . . . RTE3E4
. . . . .
1019 . . . . . E4N
. . . . .
1034 . . . CPE4N.....
. . . . .
1039 . . . . .->----- DRE4
1037 . . . DE4NS
. . . V
. . . V
1042 . . . E4NE13
. . . . .
1050 . . . . . E13
. . . . .
1066 . . . CPE13.....
. . . V
. . . V
1069 . . . E13E24
. . . . .
1078 . . . . .-<----- DRE4
1076 . . . DRE4
. . . V
. . . V
1079 . . . RTE4E4
. . . . .
1087 . . . . . E4
. . . . .
1103 . . . CPE4.....
. . . . .
1108 . . . . .->----- DRE5
1106 . . . DE4S
. . . V
. . . V
1111 . . . E4E14A
. . . . .
1120 . . . . . E14A
. . . . .
1139 . . . . . E6A
. . . V
. . . V
1157 . . . . . E6AE5A
. . . . .
1165 . . . . .-<----- DRE5
1163 . . . DRE5
. . . V
. . . V
1166 . . . RTE4E5
. . . . .
1174 . . . . . E5A
. . . . .
1189 . . . CPE5A1.....
. . . . .
1192 . . . CPE5A2.....
. . . V
. . . V
1196 . . . E5A14A
. . . . .
1205 . . . CPE14A.....
. . . V
. . . V
1209 . . . E1424A
. . . V
. . . V
1218 . . . E1424B
. . . . .
1227 . . . . . E24A
. . . . .
1238 . . . . .->----- RET24A
1236 . . . DIV24A
. . . . .
1241 . . . CP24A.....
. . . V

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1244 . . . . . V
      . . . . . E247A1
1253 . . . . . E27A
      . . . . .
1264 . . . . . -----> RET27A
1262 . . . . . DIV27A
      . . . . .
1267 . . . . . CPE27A-----
      . . . . . V
      . . . . . E247A2
      . . . . . V
      . . . . . E2726A
1282 . . . . .
      . . . . . E26A
1292 . . . . .
      . . . . . -----> RET26A
1303 . . . . . DIV26A
1301 . . . . .
      . . . . . SR24EL-----
1306 . . . . .
      . . . . . -----> 1650UP
1337 . . . . . 802ELS
1327 . . . . .
      . . . . . GM17
1349 . . . . .
      . . . . . -----> RETG17
1366 . . . . . DIVG17
1361 . . . . . V
      . . . . . G17E26
1369 . . . . .
      . . . . . CPE26A-----
      . . . . . V
      . . . . . 80233B
1383 . . . . .
      . . . . . E7
1393 . . . . . -----> RETE7
1404 . . . . . DIVE7
      . . . . . V
      . . . . . E7STOR
      . . . . . V
      . . . . . E7E6
1415 . . . . .
      . . . . . E6B
1423 . . . . .
      . . . . . -----> RETE6B
1434 . . . . . DIVE6B
1432 . . . . .
      . . . . . E8
1437 . . . . .
      . . . . . -----> RETE8
1448 . . . . . DIVE8
1446 . . . . . V
      . . . . . E8E6
1451 . . . . .
      . . . . . CPE6-----
1457 . . . . .
      . . . . . -----> DRE9
1462 . . . . . DRE9
1460 . . . . . DE6S
      . . . . . V
      . . . . . E6E15
1465 . . . . .
      . . . . . E15
1471 . . . . .
      . . . . . -----> RETE15
1482 . . . . . DIVE15
1480 . . . . .
      . . . . . <----- DRE9
1487 . . . . . DRE9
1485 . . . . . V
      . . . . . RTE6E9
1488 . . . . .

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1494 . . . . . E9
1505 . . . . . -----> RETE9
1503 . . . . . DIVE9
      . . . . .
1508 . . . . . CPE9-----
      . . . . .
1513 . . . . . -----> DRR5
1511 . . . . . DE9S
      . . . . . V
      . . . . . E9E16
1516 . . . . .
      . . . . . E16
1522 . . . . .
      . . . . . -----> RETE16
1533 . . . . . DIVE16
1531 . . . . .
      . . . . . CPE16-----
      . . . . . V
      . . . . . E16E15
1539 . . . . .
      . . . . . CPE15-----
      . . . . . V
      . . . . . E1524B
1548 . . . . .
      . . . . . E5B
1554 . . . . .
      . . . . . -----> RETE5B
1565 . . . . . DIVE5B
1563 . . . . . V
      . . . . . E5E14B
1568 . . . . .
      . . . . . E14B
1574 . . . . .
      . . . . . -----> RET14B
1585 . . . . . DIVE14B
1583 . . . . .
      . . . . . CP14B-----
      . . . . . V
      . . . . . E14E24
1591 . . . . .
      . . . . . E24B
1597 . . . . .
      . . . . . -----> RET24B
1608 . . . . . DIVE24B
1606 . . . . .
      . . . . . CPE24B-----
      . . . . . V
      . . . . . E24E28
1614 . . . . .
      . . . . . E28B
1620 . . . . .
      . . . . . -----> RET28B
1631 . . . . . DIVE28B
1629 . . . . .
      . . . . . CPE28B-----
      . . . . . V
      . . . . . E28E31
1637 . . . . .
      . . . . . E25
1643 . . . . .
      . . . . . -----> RETE25
1654 . . . . . DIVE25
1652 . . . . . V
      . . . . . E25E29
1657 . . . . .
      . . . . . E29
1663 . . . . .
      . . . . . -----> RETE29
1674 . . . . . DIVE29
1672 . . . . .

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1677 . . . CPE29.....
      . . . V
1680 . . . E29E31
      . . .
1686 . . . E32
      . . .
1697 . . . DIVE32-----> RETE32
1695 . . . V
      . . . V
1700 . . . E32E31
      . . .
1706 . . . E31
      . . .
1717 . . . DIVE31-----> RETE31
1715 . . .
      . . .
1720 . . . CPE31.....
      . . . V
1723 . . . E31E30
      . . .
1729 . . . E30B
      . . .
1740 . . . DIV30B-----> RET30B
1738 . . .
      . . .
1743 . . . CPE30.....
      . . . V
1746 . . . E30E26
      . . .
1752 . . . E26B
      . . .
1763 . . . DIV26B-----> RET26B
1761 . . .
      . . .
1766 . . . CPE26.....
      . . . V
1769 . . . E26E33
      . . .
1775 . . . E33B
      . . .
1786 . . . DIV33B-----> RET33B
1784 . . .
      . . .
1789 . . . CPE33B.....
      . . . V
1792 . . . E33P9A
      . . . V
1798 . . . E33P9B
      . . .
1804 . . . P9
      . . .
1815 . . . DIVP9-----> RETP9
1813 . . .
      . . .
1818 . . . CPP9.....
      . . . V
1821 . . . P9EMF1
      . . . V
1827 . . . EMF1B
      . . .
1838 . . . DEMF1B-----> REMF1B
1836 . . .
      . . .
1841 . . . CPEMF1.....
      . . . V
1844 . . . EM1EM2
      . . .
1850 . . . EMF2
      . . .
1861 . . . DIVEM2-----> RETEM2
1859 . . .

```

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1864 . . . CPEMF2.....
      . . . V
1867 . . . EM2M3A
      . . . V
1873 . . . EM2M3B
      . . .
1879 . . . EMF3
      . . .
1890 . . . DIVEM3-----> RETEM3
1888 . . .
      . . .
1893 . . . CPEMF3.....
      . . . V
1896 . . . EMF3RB
      . . .
1902 . . . RITBAS
      . . . V
1911 . . . RITBAS
      . . .
1919 . . . CPRITB.....
      . . . V
1922 . . . RBEMF4
      . . .
1929 . . . R2
      . . .
1940 . . . DIVR2-----> RETR2
1938 . . .
      . . .
1943 . . . R3
      . . .
1954 . . . DIVR3-----> RETR3
1952 . . .
      . . .
1957 . . . CPR2R3.....
      . . . V
1960 . . . R2R3R6
      . . .
1966 . . . R6
      . . .
1975 . . . CPR6.....
      . . . V
1978 . . . R6R9
      . . .
1984 . . . R9
      . . .
1995 . . . DIVR9-----> RETR9
1993 . . .
      . . .
1998 . . . CPR9.....
      . . . V
2001 . . . R9R11
      . . .
2007 . . . R11
      . . .
2018 . . . DIVR11-----> RETR11
2016 . . .
      . . .
2023 . . . DRR5-----> DRR5
2021 . . .
      . . .
2024 . . . R5
      . . .
2035 . . . DIVR5-----> RETR5
2033 . . .
      . . .
2038 . . . CPR5.....
      . . . V
2041 . . . R5R8
      . . .
2047 . . . R8

```



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2058 . . . . .
2056 . . . . . DIVR8 -----> RETR8

2061 . . . . . CPR8 ----->
      . . . . . V
2064 . . . . . R8R11
      . . . . .
2070 . . . . . CPR11 ----->
      . . . . . V
2073 . . . . . R11R13
      . . . . .
2079 . . . . . R13
      . . . . .
2090 . . . . . DIVR13 -----> RETR13
2088 . . . . .
      . . . . .
2093 . . . . . CPR13 ----->
      . . . . . V
2096 . . . . . R13R16
      . . . . .
2102 . . . . . R16
      . . . . .
2113 . . . . . DIVR16 -----> RETR16
2111 . . . . .
      . . . . .
2116 . . . . . CPR16 ----->
      . . . . . V
2119 . . . . . R16R21
      . . . . .
2125 . . . . . R21
      . . . . .
2136 . . . . . DIVR21 -----> RETR21
2134 . . . . .
      . . . . .
2140 . . . . . R1
      . . . . .
2151 . . . . . DIVR1 -----> RETR1
2149 . . . . .
      . . . . . V
2154 . . . . . R1R4
      . . . . .
2160 . . . . . R4
      . . . . .
2169 . . . . . CPR4 ----->
      . . . . . V
2172 . . . . . R4R7
      . . . . .
2178 . . . . . R7
      . . . . .
2189 . . . . . DIVR7 -----> RETR7
2187 . . . . .
      . . . . .
2192 . . . . . CPR7 ----->
      . . . . . V
2195 . . . . . R7R10
      . . . . .
2201 . . . . . R10
      . . . . .
2212 . . . . . DIVR10 -----> RETR10
2210 . . . . .
      . . . . .
2215 . . . . . CPR10 ----->
      . . . . . V
2218 . . . . . R10R12
      . . . . .
2224 . . . . . R12
      . . . . .
2235 . . . . . DIVR12 -----> RETR12
2233 . . . . .
      . . . . .
2238 . . . . . CPR12 ----->

```

```

2241 . . . . . V
      . . . . . R12R15
      . . . . .
2247 . . . . . R15
      . . . . .
2258 . . . . . DIVR15 -----> RETR15
2256 . . . . .
      . . . . .
2261 . . . . . CPR15 ----->
      . . . . . V
2264 . . . . . R15R18
      . . . . .
2270 . . . . . R18
      . . . . .
2281 . . . . . DIVR18 -----> RETR18
2279 . . . . .
      . . . . .
2284 . . . . . CPR18 ----->
      . . . . . V
2287 . . . . . R18R22
      . . . . .
2293 . . . . . R22
      . . . . .
2304 . . . . . DIVR22 -----> RETR22
2302 . . . . .
      . . . . .
2307 . . . . . R14
      . . . . .
2318 . . . . . DIVR14 -----> RETR14
2316 . . . . .
      . . . . . V
2321 . . . . . R14R17
      . . . . .
2327 . . . . . R17
      . . . . .
2338 . . . . . DIVR17 -----> RETR17
2336 . . . . .
      . . . . .
2341 . . . . . CPR17 ----->
      . . . . . V
2344 . . . . . R17R22
      . . . . .
2350 . . . . . CPR22 ----->
      . . . . . V
2353 . . . . . R22R21
      . . . . .
2359 . . . . . CPR21 ----->
      . . . . . V
2362 . . . . . R21R25
      . . . . .
2368 . . . . . R25
      . . . . .
2379 . . . . . DIVR25 -----> RETR25
2377 . . . . .
      . . . . .
2382 . . . . . R20
      . . . . .
2393 . . . . . DIVR20 -----> RETR20
2391 . . . . .
      . . . . . V
2396 . . . . . R20R23
      . . . . .
2402 . . . . . R23
      . . . . .
2413 . . . . . DIVR23 -----> RETR23
2411 . . . . .
      . . . . .
2416 . . . . . CPR23 ----->
      . . . . . V
2419 . . . . . R23R25
      . . . . .

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2425 . . . . . CPR25.....
. . . . . V
. . . . . V
2428 . . . . . R25R24
. . . . .
. . . . .
2434 . . . . . R19
. . . . .
. . . . .
2445 . . . . . -----> RETR19
2443 . . . . . DIVR19
. . . . .
. . . . .
2450 . . . . . -----> DETR19
2448 . . . . . DIV19R
. . . . . V
. . . . . V
2453 . . . . . R19R24
. . . . .
. . . . .
2459 . . . . . R24
. . . . .
. . . . .
2470 . . . . . -----> RETR24
2468 . . . . . DIVR24
. . . . .
. . . . .
2473 . . . . . CPR24.....
. . . . . V
. . . . . V
2476 . . . . . R24EM4
. . . . .
. . . . .
2482 . . . . . EMF4
. . . . .
. . . . .
2491 . . . . . CPEMF4.....

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(***) RUNOFF ALSO COMPUTED AT THIS LOCATION
1*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 04JUL16 TIME 08:39:40 *
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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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24INT100C 100-YEAR, 24-hr Interim Conditions 2016-03-02
Copy of 24INT100 assuming concrete-lined channel for the following routes
E5A14A, E1424A, E1424B, E247A1, E247A2 and E2726A.
by Parsons Corporation

2015-12-22 The model reflects interim drainage conditions for SR 24
and it is based on Mesa ADMPU with revisions reflecting development work
around the corridor.

2016-03-02 Modified to combine CPG19B to CPG22B as result of the Eastmar
Development. G19E26 was subsequently removed.

2016-07-04 Modified to include concrete lining for the SR 24 Channel.

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*****
FUTEMADMP24 20110519 - EMADMPU 24-hr Future Conditions 20110519
Flood Control District of Maricopa County
50 YEAR
24 Hour Storm
Unit Hydrograph: S-Graph
08/05/2011

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25 IO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

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IT HYDROGRAPH TIME DATA
NMIN 5 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 2000 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 7 0 ENDING DATE
NDTIME 2235 ENDING TIME
ICENT 19 CENTURY MARK

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COMPUTATION INTERVAL 0.08 HOURS
TOTAL TIME BASE 166.58 HOURS

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ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE- FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

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26 JD INDEX STORM NO. 1

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WARNING --- ROUTED OUTFLOW ( 3019.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2957.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2881.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2802.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2723.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2797.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2923.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2997.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 3016.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2990.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2934.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2863.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2786.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2785.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2844.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2857.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2832.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2783.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 2722.) IS GREATER THAN MAXIMUM OUTFLOW ( 2721.) IN STORAGE-OUTFLOW TABLE

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*****
1911 KK * RITBAS * STORAGE
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1913 KO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

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1
RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

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OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT								
	P1	194.	12.67	25.	6.	2.	0.39		
+	DIVERSION TO								
	DRPFW	118.	12.67	12.	3.	1.	0.39		
+	HYDROGRAPH AT								
	DP1PFW	76.	12.67	13.	3.	1.	0.39		
+	ROUTED TO								
	P1P2	49.	14.58	13.	3.	1.	0.39		
+	HYDROGRAPH AT								
	P2	258.	12.75	38.	10.	3.	0.58		
+	2 COMBINED AT								
	CPP2	258.	12.75	52.	13.	4.	0.96		
+	ROUTED TO								
	P2P4	242.	13.00	52.	13.	4.	0.96		
+	HYDROGRAPH AT								
	P4	459.	12.50	68.	21.	7.	0.50		
+	DIVERSION TO								
	RETP4	459.	12.50	68.	21.	7.	0.50		
+	HYDROGRAPH AT								
	DIVP4	0.	0.00	0.	0.	0.	0.50		
+	2 COMBINED AT								
	CPP4	242.	13.00	52.	13.	4.	1.46		
+	ROUTED TO								
	P4P6	220.	13.33	51.	13.	4.	1.46		
+	HYDROGRAPH AT								
	P6	390.	12.67	68.	21.	7.	0.50		
+	DIVERSION TO								
	RETP6	390.	12.67	68.	21.	7.	0.50		

+	HYDROGRAPH AT	DIVP6	0.	0.00	0.	0.	0.	0.50
+	2 COMBINED AT	CPP6	220.	13.33	51.	13.	4.	1.96
+	ROUTED TO	P6GM8	210.	13.50	50.	13.	4.	1.96
+	ROUTED TO	GM8G10	201.	13.67	50.	13.	4.	1.96
+	HYDROGRAPH AT	DRPFW	118.	12.67	12.	3.	1.	0.39
+	ROUTED TO	P1PFW	92.	12.83	12.	3.	1.	0.39
+	HYDROGRAPH AT	P3	191.	13.00	34.	8.	3.	0.52
+	2 COMBINED AT	CPP3	275.	12.92	45.	11.	4.	0.91
+	ROUTED TO	P3P5	271.	13.00	45.	11.	4.	0.91
+	HYDROGRAPH AT	P5	229.	12.50	35.	11.	4.	0.25
+	DIVERSION TO	RETP5	229.	12.50	33.	9.	3.	0.25
+	HYDROGRAPH AT	DIVP5	34.	13.25	6.	2.	1.	0.25
+	2 COMBINED AT	CPP5	271.	13.00	50.	13.	4.	1.16
+	ROUTED TO	P5P7	263.	13.08	50.	13.	4.	1.16
+	HYDROGRAPH AT	P7	419.	12.50	64.	19.	6.	0.43
+	DIVERSION TO	RETP7	419.	12.50	59.	16.	5.	0.43
+	HYDROGRAPH AT	DIVP7	60.	13.17	11.	4.	1.	0.43
+	3 COMBINED AT	CPP7	360.	13.58	106.	28.	9.	3.17
+	ROUTED TO	P7GM14	348.	13.83	105.	28.	9.	3.17
+	HYDROGRAPH AT	GM1	377.	12.42	44.	12.	4.	0.34
+	HYDROGRAPH AT	GM2	888.	12.33	113.	36.	12.	0.68
+	HYDROGRAPH AT	GM3	577.	12.08	60.	20.	7.	0.29
+	3 COMBINED AT	CPG123	1521.	12.17	217.	68.	23.	1.32
+	DIVERSION TO	RETG1	1521.	12.17	189.	51.	17.	1.32
+	HYDROGRAPH AT	DIVG1	354.	12.75	51.	16.	5.	1.32
+	ROUTED TO	GM1T5	223.	12.92	50.	16.	5.	1.32
+	HYDROGRAPH AT	GM5	310.	12.17	37.	12.	4.	0.18
+	DIVERSION TO	RETG5	310.	12.17	25.	7.	2.	0.18
+	HYDROGRAPH AT	DIVG5	218.	12.33	17.	5.	2.	0.18
+	2 COMBINED AT	CPG5	246.	12.92	65.	21.	7.	1.49
+	ROUTED TO	GM5T7	206.	13.25	63.	21.	7.	1.49
+	HYDROGRAPH AT	GM6	685.	12.17	63.	19.	6.	0.37
+	DIVERSION TO	RETG6	685.	12.17	50.	14.	5.	0.37
+	HYDROGRAPH AT	DIVG6	282.	12.33	19.	6.	2.	0.37

+	HYDROGRAPH AT	GM7	249.	12.33	27.	8.	3.	0.22
+	DIVERSION TO	RETG7	249.	12.33	27.	7.	2.	0.22
+	HYDROGRAPH AT	DIVG7	2.	16.75	1.	0.	0.	0.22
+	2 COMBINED AT	CPG7A	282.	12.33	20.	6.	2.	0.58
+	2 COMBINED AT	CPG7B	236.	12.33	79.	26.	9.	2.08
+	ROUTED TO	GM7T9	200.	13.42	78.	26.	9.	2.08
+	HYDROGRAPH AT	GM8	692.	12.33	86.	28.	9.	0.56
+	DIVERSION TO	RETG8	692.	12.33	74.	20.	7.	0.56
+	HYDROGRAPH AT	DIVG8	192.	12.67	23.	7.	2.	0.56
+	HYDROGRAPH AT	GM9	153.	12.17	11.	3.	1.	0.09
+	DIVERSION TO	RETG9	153.	12.17	11.	3.	1.	0.09
+	HYDROGRAPH AT	DIVG9	0.	23.83	0.	0.	0.	0.09
+	2 COMBINED AT	CPG9A	192.	12.67	23.	7.	2.	0.65
+	HYDROGRAPH AT	GM10	357.	12.33	46.	14.	5.	0.28
+	DIVERSION TO	RETG10	357.	12.33	32.	9.	3.	0.28
+	HYDROGRAPH AT	DIVG10	236.	12.50	18.	5.	2.	0.28
+	HYDROGRAPH AT	GM11	91.	12.25	9.	3.	1.	0.08
+	DIVERSION TO	RETG11	91.	12.25	9.	3.	1.	0.08
+	HYDROGRAPH AT	DIVG11	1.	23.00	0.	0.	0.	0.08
+	2 COMBINED AT	CPG11	236.	12.50	18.	5.	2.	0.36
+	3 COMBINED AT	CPG9B	344.	12.75	114.	38.	13.	3.08
+	ROUTED TO	GM9T14	299.	12.92	112.	38.	13.	3.08
+	HYDROGRAPH AT	GM12	244.	12.08	26.	9.	3.	0.12
+	DIVERSION TO	RETG12	244.	12.08	16.	5.	2.	0.12
+	HYDROGRAPH AT	DIVG12	212.	12.17	13.	4.	1.	0.12
+	ROUTED TO	G12T13	82.	12.42	13.	4.	1.	0.12
+	HYDROGRAPH AT	GM13	519.	12.08	48.	16.	5.	0.29
+	DIVERSION TO	RETG13	519.	12.08	42.	11.	4.	0.29
+	HYDROGRAPH AT	DIVG13	75.	12.42	13.	4.	1.	0.29
+	2 COMBINED AT	CPG13	156.	12.42	26.	8.	3.	0.41
+	ROUTED TO	G13T14	132.	12.50	25.	8.	3.	0.41
+	HYDROGRAPH AT	GM14	591.	12.17	59.	19.	6.	0.35
+	DIVERSION TO	RETG14	591.	12.17	46.	13.	4.	0.35
+	HYDROGRAPH AT	DIVG14	254.	12.33	21.	7.	2.	0.35
+	2 COMBINED AT							

+		CPG14A	292.	12.33	46.	15.	5.	0.76
+	2 COMBINED AT	CPG14B	386.	12.92	151.	51.	17.	3.84
+	2 COMBINED AT	CPG14C	540.	13.83	236.	75.	25.	7.01
+	ROUTED TO	G14E26	537.	13.83	235.	75.	25.	7.01
+	HYDROGRAPH AT	E1	374.	12.83	57.	14.	5.	0.89
+	DIVERSION TO	DRE2	296.	12.83	42.	11.	4.	0.89
+	HYDROGRAPH AT	DE15	77.	12.83	15.	4.	1.	0.89
+	ROUTED TO	E1E10	48.	14.83	15.	4.	1.	0.89
+	HYDROGRAPH AT	E10	326.	12.92	53.	13.	4.	0.82
+	2 COMBINED AT	CPE10	340.	12.92	67.	17.	6.	1.71
+	ROUTED TO	E10E17	308.	13.17	67.	17.	6.	1.71
+	HYDROGRAPH AT	E17	245.	12.50	35.	11.	4.	0.27
+	DIVERSION TO	RETE17	245.	12.50	34.	9.	3.	0.27
+	HYDROGRAPH AT	DIVE17	18.	13.50	5.	2.	1.	0.27
+	2 COMBINED AT	CPE17	308.	13.17	71.	18.	6.	1.98
+	ROUTED TO	E17E21	291.	13.33	70.	18.	6.	1.98
+	HYDROGRAPH AT	E21	291.	12.50	43.	13.	4.	0.31
+	DIVERSION TO	RETE21	291.	12.50	38.	10.	3.	0.31
+	HYDROGRAPH AT	DIVE21	63.	13.00	9.	3.	1.	0.31
+	2 COMBINED AT	CPE21A	319.	13.33	78.	21.	7.	2.29
+	ROUTED TO	E21G20	311.	13.42	78.	21.	7.	2.29
+	HYDROGRAPH AT	DRE2	296.	12.83	42.	11.	4.	0.89
+	ROUTED TO	RTE1E2	234.	13.25	42.	11.	4.	0.89
+	HYDROGRAPH AT	E2	325.	12.92	53.	13.	4.	0.78
+	2 COMBINED AT	CPE2	472.	13.00	94.	24.	8.	1.67
+	DIVERSION TO	DRE3	277.	13.00	39.	10.	3.	1.67
+	HYDROGRAPH AT	DE2S	195.	13.00	55.	14.	5.	1.67
+	ROUTED TO	E2E11	151.	15.92	54.	14.	5.	1.67
+	HYDROGRAPH AT	E11	251.	12.83	39.	10.	3.	0.60
+	2 COMBINED AT	CPE11	246.	12.83	83.	23.	8.	2.27
+	ROUTED TO	E11E18	173.	13.75	80.	23.	8.	2.27
+	HYDROGRAPH AT	E18	278.	12.33	31.	9.	3.	0.22
+	DIVERSION TO	RETE18	1.	4.50	1.	0.	0.	0.22
+	HYDROGRAPH AT	DIVE18	278.	12.33	31.	8.	3.	0.22
+	2 COMBINED AT	CPE18	274.	12.33	96.	31.	10.	2.49

+	ROUTED TO	E18E21	247.	12.50	95.	31.	10.	2.49
+	2 COMBINED AT	CPE21B	417.	13.67	169.	52.	17.	3.90
+	ROUTED TO	G20G21	413.	13.75	168.	52.	17.	3.90
+	HYDROGRAPH AT	DRE3	277.	13.00	39.	10.	3.	1.67
+	ROUTED TO	RTE2E3	241.	13.42	39.	10.	3.	1.67
+	HYDROGRAPH AT	E3	748.	13.25	165.	41.	14.	2.23
+	2 COMBINED AT	E2SE3	938.	13.25	200.	50.	17.	3.90
+	DIVERSION TO	DRE4N	545.	13.25	81.	20.	7.	3.90
+	HYDROGRAPH AT	DE3S	394.	13.25	119.	30.	10.	3.90
+	ROUTED TO	E3E12	347.	14.50	119.	30.	10.	3.90
+	HYDROGRAPH AT	E12	256.	12.92	43.	11.	4.	0.57
+	2 COMBINED AT	CPE12	468.	12.92	160.	40.	13.	4.47
+	ROUTED TO	E12E19	416.	13.75	160.	40.	13.	4.47
+	HYDROGRAPH AT	E19	205.	12.25	19.	5.	2.	0.14
+	2 COMBINED AT	CPE19	418.	13.75	178.	45.	15.	4.61
+	ROUTED TO	E1922E	404.	14.08	178.	45.	15.	4.61
+	HYDROGRAPH AT	22E	130.	12.25	13.	3.	1.	0.09
+	HYDROGRAPH AT	E20	133.	12.50	16.	5.	2.	0.17
+	ROUTED TO	E2022E	107.	12.75	16.	5.	2.	0.17
+	3 COMBINED AT	CP22E	407.	14.08	205.	53.	18.	4.87
+	ROUTED TO	22EE22	402.	14.25	205.	53.	18.	4.87
+	HYDROGRAPH AT	E22	188.	12.67	28.	7.	2.	0.16
+	3 COMBINED AT	CPE22	756.	14.00	381.	108.	36.	7.25
+	ROUTED TO	E22G22	747.	14.17	377.	108.	36.	7.25
+	HYDROGRAPH AT	GM21	335.	12.25	45.	15.	5.	0.21
+	DIVERSION TO	RETG21	335.	12.25	31.	9.	3.	0.21
+	HYDROGRAPH AT	DIVG21	216.	12.42	21.	6.	2.	0.21
+	ROUTED TO	G21T22	180.	12.50	21.	6.	2.	0.21
+	HYDROGRAPH AT	GM22	184.	12.17	21.	7.	2.	0.09
+	DIVERSION TO	RETG22	176.	12.08	14.	4.	1.	0.09
+	HYDROGRAPH AT	DIVG22	143.	12.25	10.	3.	1.	0.09
+	2 COMBINED AT	CPG22A	210.	12.50	30.	9.	3.	0.31
+	HYDROGRAPH AT	GM16	79.	12.33	10.	3.	1.	0.07
+	DIVERSION TO	RETG16	79.	12.33	9.	2.	1.	0.07

+	HYDROGRAPH AT	DIVG16	12.	12.83	2.	1.	0.	0.07
+	ROUTED TO	G16T19	7.	13.17	2.	1.	0.	0.07
+	HYDROGRAPH AT	GM18	238.	12.25	27.	9.	3.	0.17
+	DIVERSION TO	RETG18	238.	12.25	23.	6.	2.	0.17
+	HYDROGRAPH AT	DIVG18	62.	12.58	7.	2.	1.	0.17
+	2 COMBINED AT	CPG18	62.	12.58	10.	3.	1.	0.24
+	HYDROGRAPH AT	GM19	152.	12.17	12.	4.	1.	0.09
+	DIVERSION TO	RETG19	152.	12.17	11.	3.	1.	0.09
+	HYDROGRAPH AT	DIVG19	34.	12.42	3.	1.	0.	0.09
+	2 COMBINED AT	CPG19A	73.	12.58	12.	4.	1.	0.33
+	HYDROGRAPH AT	GM20	317.	12.17	34.	10.	3.	0.18
+	DIVERSION TO	RETG20	317.	12.17	27.	7.	2.	0.18
+	HYDROGRAPH AT	DIVG20	113.	12.42	10.	3.	1.	0.18
+	2 COMBINED AT	CPG19B	145.	12.42	22.	7.	2.	0.51
+	3 COMBINED AT	CPG22B	779.	14.17	417.	121.	40.	8.06
+	ROUTED TO	G22E26	751.	14.50	416.	121.	40.	8.06
+	HYDROGRAPH AT	DRE4N	545.	13.25	81.	20.	7.	3.90
+	ROUTED TO	RTE3E4	496.	13.50	81.	20.	7.	3.90
+	HYDROGRAPH AT	E4N	122.	12.92	20.	5.	2.	0.31
+	2 COMBINED AT	CPE4N	546.	13.42	100.	25.	8.	4.21
+	DIVERSION TO	DRE4	416.	13.42	69.	17.	6.	4.21
+	HYDROGRAPH AT	DE4NS	130.	13.42	31.	8.	3.	4.21
+	ROUTED TO	E4NE13	105.	15.17	31.	8.	3.	4.21
+	HYDROGRAPH AT	E13	231.	12.92	39.	10.	3.	0.48
+	2 COMBINED AT	CPE13	223.	12.92	68.	17.	6.	4.69
+	ROUTED TO	E13E24	154.	13.92	67.	17.	6.	4.69
+	HYDROGRAPH AT	DRE4	416.	13.42	69.	17.	6.	4.21
+	ROUTED TO	RTE4E4	312.	14.33	69.	17.	6.	4.21
+	HYDROGRAPH AT	E4	364.	13.25	80.	20.	7.	1.20
+	2 COMBINED AT	CPE4	385.	14.25	144.	36.	12.	5.41
+	DIVERSION TO	DRE5	372.	14.25	137.	34.	11.	5.41
+	HYDROGRAPH AT	DE4S	13.	14.25	7.	2.	1.	5.41
+	ROUTED TO	E4E14A	13.	15.33	7.	2.	1.	5.41
+	HYDROGRAPH AT	E14A	135.	12.83	20.	5.	2.	0.48
+	HYDROGRAPH AT							

+		E6A	646.	13.25	197.	65.	22.	0.58
+	ROUTED TO	E6AE5A	616.	13.50	197.	65.	22.	0.58
+	HYDROGRAPH AT	DRE5	372.	14.25	137.	34.	11.	5.41
+	ROUTED TO	RTE4E5	344.	14.58	137.	34.	11.	5.41
+	HYDROGRAPH AT	E5A	423.	13.25	92.	23.	8.	1.14
+	2 COMBINED AT	CPE5A1	606.	13.33	220.	55.	18.	6.55
+	2 COMBINED AT	CPE5A2	1166.	13.50	407.	118.	39.	7.13
+	ROUTED TO	E5A14A	1160.	13.58	407.	118.	39.	7.13
+	3 COMBINED AT	CPE14A	1176.	13.58	430.	123.	41.	7.61
+	ROUTED TO	E1424A	1173.	13.67	430.	123.	41.	7.61
+	ROUTED TO	E1424B	1168.	13.75	430.	123.	41.	7.61
+	HYDROGRAPH AT	E24A	710.	12.33	96.	32.	11.	0.53
+	DIVERSION TO	RET24A	710.	12.33	71.	20.	7.	0.53
+	HYDROGRAPH AT	DIV24A	432.	12.50	38.	12.	4.	0.53
+	3 COMBINED AT	CP24A	1335.	13.75	523.	149.	50.	8.62
+	ROUTED TO	E247A1	1329.	13.83	523.	149.	50.	8.62
+	HYDROGRAPH AT	E27A	568.	12.50	101.	32.	11.	0.54
+	DIVERSION TO	RET27A	568.	12.50	76.	21.	7.	0.54
+	HYDROGRAPH AT	DIV27A	310.	12.83	37.	11.	4.	0.54
+	3 COMBINED AT	CPE27A	1977.	13.92	931.	269.	90.	12.81
+	ROUTED TO	E247A2	1975.	13.92	931.	269.	90.	12.81
+	ROUTED TO	E2726A	1968.	14.08	929.	269.	90.	12.81
+	HYDROGRAPH AT	E26A	959.	12.50	158.	51.	17.	0.87
+	DIVERSION TO	RET26A	959.	12.50	120.	33.	11.	0.87
+	HYDROGRAPH AT	DIV26A	485.	12.83	57.	17.	6.	0.87
+	2 COMBINED AT	SR24EL	2002.	14.08	967.	282.	94.	13.68
+	DIVERSION TO	1650UP	352.	14.08	41.	10.	3.	13.68
+	HYDROGRAPH AT	802ELS	1650.	13.67	926.	271.	91.	13.68
+	HYDROGRAPH AT	GM17	150.	12.17	15.	5.	2.	0.10
+	DIVERSION TO	RETG17	150.	12.17	15.	5.	2.	0.10
+	HYDROGRAPH AT	DIVG17	0.	0.00	0.	0.	0.	0.10
+	ROUTED TO	G17E26	0.	0.00	0.	0.	0.	0.10
+	3 COMBINED AT	CPE26A	2035.	13.92	1077.	323.	108.	20.80
+	ROUTED TO	80233B	2031.	14.00	1075.	323.	108.	20.80
+	HYDROGRAPH AT	E7	702.	12.92	157.	49.	16.	1.12

+	DIVERSION TO	RETE7	702.	12.92	156.	43.	14.	1.12
+	HYDROGRAPH AT	DIVE7	29.	15.17	17.	6.	2.	1.12
+	ROUTED TO	E7STOR	0.	0.00	0.	0.	0.	1.12
+	ROUTED TO	E7E6	0.	0.00	0.	0.	0.	1.12
+	HYDROGRAPH AT	E6B	1907.	12.58	350.	116.	39.	1.95
+	DIVERSION TO	RETE6B	1907.	12.58	325.	91.	30.	1.95
+	HYDROGRAPH AT	DIVE6B	213.	13.58	73.	25.	8.	1.95
+	HYDROGRAPH AT	E8	770.	12.75	155.	49.	16.	1.10
+	DIVERSION TO	RETE8	770.	12.75	148.	41.	14.	1.10
+	HYDROGRAPH AT	DIVE8	70.	14.08	25.	8.	3.	1.10
+	ROUTED TO	E8E6	43.	15.25	23.	8.	3.	1.10
+	3 COMBINED AT	CPE6	210.	13.67	87.	32.	11.	3.05
+	DIVERSION TO	DRE9	1.	13.67	0.	0.	0.	3.05
+	HYDROGRAPH AT	DE6S	209.	13.67	87.	32.	11.	3.05
+	ROUTED TO	E6E15	153.	14.25	85.	32.	11.	3.05
+	HYDROGRAPH AT	E15	955.	12.33	135.	45.	15.	0.78
+	DIVERSION TO	RETE15	955.	12.33	123.	34.	11.	0.78
+	HYDROGRAPH AT	DIVE15	120.	13.00	31.	11.	4.	0.78
+	HYDROGRAPH AT	DRE9	1.	13.67	0.	0.	0.	3.05
+	ROUTED TO	RTE6E9	1.	14.67	0.	0.	0.	3.05
+	HYDROGRAPH AT	E9	846.	12.42	128.	42.	14.	0.72
+	DIVERSION TO	RETE9	846.	12.42	119.	33.	11.	0.72
+	HYDROGRAPH AT	DIVE9	102.	13.17	28.	9.	3.	0.72
+	2 COMBINED AT	CPE9	102.	13.17	28.	10.	3.	0.72
+	DIVERSION TO	DRR5	13.	13.17	1.	0.	0.	0.72
+	HYDROGRAPH AT	DE9S	89.	13.17	28.	9.	3.	0.72
+	ROUTED TO	E9E16	59.	13.83	27.	9.	3.	0.72
+	HYDROGRAPH AT	E16	508.	12.33	69.	23.	8.	0.40
+	DIVERSION TO	RETE16	508.	12.33	64.	18.	6.	0.40
+	HYDROGRAPH AT	DIVE16	48.	13.08	15.	5.	2.	0.40
+	2 COMBINED AT	CPE16	81.	13.83	40.	14.	5.	1.12
+	ROUTED TO	E16E15	80.	14.08	40.	14.	5.	1.12
+	3 COMBINED AT	CPE15	252.	14.25	138.	53.	18.	4.95
+	ROUTED TO	E1524B	222.	14.75	138.	53.	18.	4.95

+	HYDROGRAPH AT	E5B	387.	12.25	50.	17.	6.	0.29
+	DIVERSION TO	RETE5B	387.	12.25	45.	13.	4.	0.29
+	HYDROGRAPH AT	DIVE5B	41.	12.92	12.	4.	1.	0.29
+	ROUTED TO	E5E14B	27.	13.58	12.	4.	1.	0.29
+	HYDROGRAPH AT	E14B	774.	12.25	96.	32.	11.	0.53
+	DIVERSION TO	RET14B	774.	12.25	88.	24.	8.	0.53
+	HYDROGRAPH AT	DIV14B	74.	12.92	22.	7.	2.	0.53
+	2 COMBINED AT	CP14B	74.	12.92	33.	12.	4.	0.81
+	ROUTED TO	E14E24	63.	13.92	32.	12.	4.	0.81
+	HYDROGRAPH AT	E24B	695.	12.25	88.	28.	9.	0.46
+	DIVERSION TO	RET24B	695.	12.25	71.	20.	7.	0.46
+	HYDROGRAPH AT	DIV24B	238.	12.58	29.	9.	3.	0.46
+	3 COMBINED AT	CPE24B	252.	14.83	169.	69.	23.	6.23
+	ROUTED TO	E24E28	244.	15.25	168.	69.	23.	6.23
+	HYDROGRAPH AT	E28B	681.	12.42	101.	32.	11.	0.54
+	DIVERSION TO	RET28B	681.	12.42	77.	21.	7.	0.54
+	HYDROGRAPH AT	DIV28B	377.	12.67	36.	11.	4.	0.54
+	2 COMBINED AT	CPE28B	277.	12.75	177.	77.	26.	6.77
+	ROUTED TO	E28E31	246.	15.67	176.	77.	26.	6.77
+	HYDROGRAPH AT	E25	903.	12.50	161.	53.	18.	0.93
+	DIVERSION TO	RETE25	903.	12.50	161.	53.	18.	0.93
+	HYDROGRAPH AT	DIVE25	0.	0.00	0.	0.	0.	0.93
+	ROUTED TO	E25E29	0.	0.00	0.	0.	0.	0.93
+	HYDROGRAPH AT	E29	1079.	12.50	178.	58.	19.	1.00
+	DIVERSION TO	RETE29	1079.	12.50	134.	37.	12.	1.00
+	HYDROGRAPH AT	DIVE29	640.	12.75	68.	21.	7.	1.00
+	2 COMBINED AT	CPE29	577.	12.75	66.	20.	7.	1.93
+	ROUTED TO	E29E31	303.	13.17	64.	20.	7.	1.93
+	HYDROGRAPH AT	E32	351.	12.25	42.	14.	5.	0.25
+	DIVERSION TO	RETE32	351.	12.25	31.	9.	3.	0.25
+	HYDROGRAPH AT	DIVE32	192.	12.42	17.	5.	2.	0.25
+	ROUTED TO	E32E31	79.	12.83	16.	5.	2.	0.25
+	HYDROGRAPH AT	E31	838.	12.50	137.	45.	15.	0.81
+	DIVERSION TO	RETE31	838.	12.50	101.	28.	9.	0.81
+	HYDROGRAPH AT							

+		DIVE31	466.	12.75	55.	17.	6.	0.81
+	4 COMBINED AT	CPE31	521.	13.25	261.	109.	36.	9.76
+	ROUTED TO	E31E30	454.	13.75	254.	109.	36.	9.76
+	HYDROGRAPH AT	E30B	739.	12.83	162.	51.	17.	0.88
+	DIVERSION TO	RET30B	739.	12.83	123.	34.	11.	0.88
+	HYDROGRAPH AT	DIV30B	415.	13.25	57.	17.	6.	0.88
+	2 COMBINED AT	CPE30	605.	13.58	292.	121.	40.	10.64
+	ROUTED TO	E30E26	595.	13.67	289.	120.	40.	10.64
+	HYDROGRAPH AT	E26B	366.	12.33	49.	15.	5.	0.26
+	DIVERSION TO	RET26B	366.	12.33	37.	10.	3.	0.26
+	HYDROGRAPH AT	DIV26B	178.	12.58	17.	5.	2.	0.26
+	2 COMBINED AT	CPE26	603.	13.67	294.	124.	41.	10.90
+	ROUTED TO	E26E33	527.	14.25	285.	124.	41.	10.90
+	HYDROGRAPH AT	E33B	1148.	12.33	160.	52.	17.	0.85
+	DIVERSION TO	RET33B	1148.	12.33	121.	34.	11.	0.85
+	HYDROGRAPH AT	DIV33B	630.	12.58	59.	18.	6.	0.85
+	3 COMBINED AT	CPE33B	2247.	14.50	1200.	409.	137.	32.54
+	ROUTED TO	E33P9A	2238.	14.58	1197.	409.	137.	32.54
+	ROUTED TO	E33P9B	2226.	14.67	1191.	409.	137.	32.54
+	HYDROGRAPH AT	P9	1338.	12.42	236.	79.	26.	1.12
+	DIVERSION TO	RETP9	177.	11.75	54.	18.	6.	1.12
+	HYDROGRAPH AT	DIVP9	1338.	12.42	218.	61.	20.	1.12
+	2 COMBINED AT	CPP9	2271.	14.67	1295.	459.	154.	33.67
+	ROUTED TO	P9EMF1	2257.	14.75	1286.	459.	154.	33.67
+	HYDROGRAPH AT	EMF1B	1271.	12.42	205.	67.	22.	1.04
+	DIVERSION TO	REMF1B	1271.	12.42	153.	43.	14.	1.04
+	HYDROGRAPH AT	DEMFB	681.	12.67	80.	24.	8.	1.04
+	2 COMBINED AT	CPEMF1	2289.	14.75	1331.	474.	159.	34.70
+	ROUTED TO	EM1EM2	2288.	14.83	1331.	474.	159.	34.70
+	HYDROGRAPH AT	EMF2	1409.	12.83	345.	114.	38.	1.85
+	DIVERSION TO	RETEM2	1331.	12.83	195.	49.	16.	1.85
+	HYDROGRAPH AT	DIVEM2	814.	13.33	149.	65.	22.	1.85
+	2 COMBINED AT	CPEMF2	2375.	14.75	1420.	513.	175.	36.55
+	ROUTED TO	EM2M3A	2371.	14.83	1416.	513.	175.	36.55
+	ROUTED TO	EM2M3B	2367.	14.92	1413.	513.	175.	36.55

+	HYDROGRAPH AT	EMF3	1144.	12.75	241.	79.	26.	1.49
+	DIVERSION TO	RETEM3	801.	12.42	100.	30.	10.	1.49
+	HYDROGRAPH AT	DIVEM3	1144.	12.75	175.	50.	17.	1.49
+	2 COMBINED AT	CPEMF3	2407.	14.83	1541.	550.	188.	38.04
+	ROUTED TO	EMF3RB	2407.	14.92	1537.	550.	188.	38.04
+	HYDROGRAPH AT	RITBAS	610.	12.08	37.	9.	3.	0.29
+	ROUTED TO	RITBAS	1.	12.92	1.	1.	1.	0.29
+	2 COMBINED AT	CPRITB	2407.	14.92	1537.	551.	188.	38.33
+	ROUTED TO	RBEMF4	2392.	15.08	1516.	550.	188.	38.33
+	HYDROGRAPH AT	R2	519.	12.67	86.	25.	8.	0.68
+	DIVERSION TO	RETR2	383.	12.42	33.	9.	3.	0.68
+	HYDROGRAPH AT	DIVR2	519.	12.67	59.	16.	5.	0.68
+	HYDROGRAPH AT	R3	301.	12.58	47.	14.	5.	0.41
+	DIVERSION TO	RETR3	301.	12.58	29.	8.	3.	0.41
+	HYDROGRAPH AT	DIVR3	241.	12.75	21.	6.	2.	0.41
+	2 COMBINED AT	CPR2R3	718.	12.75	79.	21.	7.	1.09
+	ROUTED TO	R2R3R6	331.	14.33	74.	21.	7.	1.09
+	HYDROGRAPH AT	R6	342.	12.67	52.	15.	5.	0.50
+	2 COMBINED AT	CPR6	338.	12.67	119.	35.	12.	1.59
+	ROUTED TO	R6R9	305.	14.67	118.	35.	12.	1.59
+	HYDROGRAPH AT	R9	733.	12.33	108.	36.	12.	0.59
+	DIVERSION TO	RETR9	733.	12.33	98.	27.	9.	0.59
+	HYDROGRAPH AT	DIVR9	102.	13.00	27.	9.	3.	0.59
+	2 COMBINED AT	CPR9	337.	13.00	142.	44.	15.	2.19
+	ROUTED TO	R9R11	303.	15.17	140.	44.	15.	2.19
+	HYDROGRAPH AT	R11	1022.	12.50	160.	51.	17.	0.99
+	DIVERSION TO	RETR11	1022.	12.50	124.	34.	11.	0.99
+	HYDROGRAPH AT	DIVR11	460.	12.83	55.	17.	6.	0.99
+	HYDROGRAPH AT	DRR5	13.	13.17	1.	0.	0.	0.72
+	HYDROGRAPH AT	R5	465.	12.50	61.	18.	6.	0.50
+	DIVERSION TO	RETR5	3.	5.00	2.	1.	0.	0.50
+	HYDROGRAPH AT	DIVR5	465.	12.50	61.	17.	6.	0.50
+	2 COMBINED AT	CPR5	463.	12.50	62.	18.	6.	1.22
+	ROUTED TO	R5R8	392.	12.83	62.	18.	6.	1.22

+	HYDROGRAPH AT	R8	647.	12.42	101.	34.	11.	0.55
+	DIVERSION TO	RETR8	647.	12.42	91.	25.	8.	0.55
+	HYDROGRAPH AT	DIVR8	91.	13.08	25.	9.	3.	0.55
+	2 COMBINED AT	CPR8	392.	12.83	84.	26.	9.	1.77
+	ROUTED TO	R8R11	357.	13.25	82.	26.	9.	1.77
+	3 COMBINED AT	CPR11	714.	12.83	265.	83.	28.	4.95
+	ROUTED TO	R11R13	652.	13.75	262.	83.	28.	4.95
+	HYDROGRAPH AT	R13	612.	12.33	81.	27.	9.	0.50
+	DIVERSION TO	RETR13	612.	12.33	60.	17.	6.	0.50
+	HYDROGRAPH AT	DIVR13	362.	12.50	33.	10.	3.	0.50
+	2 COMBINED AT	CPR13	675.	13.75	285.	92.	31.	5.45
+	ROUTED TO	R13R16	640.	14.25	282.	92.	31.	5.45
+	HYDROGRAPH AT	R16	666.	12.25	92.	31.	10.	0.50
+	DIVERSION TO	RETR16	666.	12.25	66.	19.	6.	0.50
+	HYDROGRAPH AT	DIVR16	368.	12.50	40.	12.	4.	0.50
+	2 COMBINED AT	CPR16	661.	14.25	311.	102.	34.	5.95
+	ROUTED TO	R16R21	601.	15.25	306.	102.	34.	5.95
+	HYDROGRAPH AT	R21	649.	12.67	114.	35.	12.	0.84
+	DIVERSION TO	RETR21	333.	12.25	30.	9.	3.	0.84
+	HYDROGRAPH AT	DIVR21	649.	12.67	96.	26.	9.	0.84
+	HYDROGRAPH AT	R1	1164.	12.58	182.	56.	19.	1.45
+	DIVERSION TO	RETR1	1164.	12.58	182.	51.	17.	1.45
+	HYDROGRAPH AT	DIVR1	22.	15.08	17.	6.	2.	1.45
+	ROUTED TO	R1R4	18.	20.42	15.	6.	2.	1.45
+	HYDROGRAPH AT	R4	673.	12.58	86.	23.	8.	1.00
+	2 COMBINED AT	CPR4	660.	12.58	84.	27.	9.	2.45
+	ROUTED TO	R4R7	513.	13.08	84.	27.	9.	2.45
+	HYDROGRAPH AT	R7	823.	12.58	134.	42.	14.	1.00
+	DIVERSION TO	RETR7	823.	12.58	86.	24.	8.	1.00
+	HYDROGRAPH AT	DIVR7	624.	12.75	64.	18.	6.	1.00
+	2 COMBINED AT	CPR7	990.	12.75	142.	44.	15.	3.45
+	ROUTED TO	R7R10	853.	13.25	140.	44.	15.	3.45
+	HYDROGRAPH AT	R10	667.	12.83	139.	43.	14.	1.01
+	DIVERSION TO	RETR10	667.	12.83	129.	35.	12.	1.01
+	HYDROGRAPH AT							

+		DIVR10	110.	13.83	25.	8.	3.	1.01
+	2 COMBINED AT	CPR10	853.	13.25	160.	51.	17.	4.46
+	ROUTED TO	R10R12	725.	13.67	156.	51.	17.	4.46
+	HYDROGRAPH AT	R12	828.	12.17	101.	35.	12.	0.49
+	DIVERSION TO	RETR12	828.	12.17	71.	20.	7.	0.49
+	HYDROGRAPH AT	DIVR12	550.	12.33	47.	14.	5.	0.49
+	2 COMBINED AT	CPR12	764.	13.67	196.	64.	22.	4.95
+	ROUTED TO	R12R15	590.	14.67	188.	64.	22.	4.95
+	HYDROGRAPH AT	R15	528.	12.50	77.	24.	8.	0.56
+	DIVERSION TO	RETR15	477.	12.42	41.	12.	4.	0.56
+	HYDROGRAPH AT	DIVR15	528.	12.50	45.	13.	4.	0.56
+	2 COMBINED AT	CPR15	598.	14.67	220.	75.	25.	5.51
+	ROUTED TO	R15R18	564.	15.08	214.	75.	25.	5.51
+	HYDROGRAPH AT	R18	560.	12.67	104.	32.	11.	0.80
+	DIVERSION TO	RETR18	560.	12.67	94.	26.	9.	0.80
+	HYDROGRAPH AT	DIVR18	108.	13.50	21.	7.	2.	0.80
+	2 COMBINED AT	CPR18	572.	15.08	225.	79.	27.	6.30
+	ROUTED TO	R18R22	534.	15.58	221.	78.	27.	6.30
+	HYDROGRAPH AT	R22	689.	12.33	95.	31.	10.	0.57
+	DIVERSION TO	RETR22	689.	12.33	67.	19.	6.	0.57
+	HYDROGRAPH AT	DIVR22	432.	12.50	41.	12.	4.	0.57
+	HYDROGRAPH AT	R14	703.	12.25	88.	29.	10.	0.50
+	DIVERSION TO	RETR14	703.	12.25	60.	17.	6.	0.50
+	HYDROGRAPH AT	DIVR14	458.	12.42	41.	12.	4.	0.50
+	ROUTED TO	R14R17	220.	12.83	40.	12.	4.	0.50
+	HYDROGRAPH AT	R17	427.	12.58	73.	23.	8.	0.49
+	DIVERSION TO	RETR17	427.	12.58	55.	15.	5.	0.49
+	HYDROGRAPH AT	DIVR17	219.	12.83	27.	8.	3.	0.49
+	2 COMBINED AT	CPR17	436.	12.83	66.	20.	7.	0.99
+	ROUTED TO	R17R22	275.	13.25	63.	20.	7.	0.99
+	3 COMBINED AT	CPR22	575.	15.58	287.	105.	35.	7.87
+	ROUTED TO	R22R21	550.	15.92	283.	104.	35.	7.87
+	3 COMBINED AT	CPR21	838.	15.58	571.	208.	70.	14.65
+	ROUTED TO	R21R25	815.	15.83	559.	207.	70.	14.65
+	HYDROGRAPH AT	R25	378.	12.25	43.	14.	5.	0.28

+	DIVERSION TO	RETR25	346.	12.17	25.	7.	2.	0.28
+	HYDROGRAPH AT	DIVR25	353.	12.33	23.	6.	2.	0.28
+	HYDROGRAPH AT	R20	482.	12.42	72.	24.	8.	0.50
+	DIVERSION TO	RETR20	482.	12.42	62.	17.	6.	0.50
+	HYDROGRAPH AT	DIVR20	103.	12.92	20.	6.	2.	0.50
+	ROUTED TO	R20R23	47.	13.75	18.	6.	2.	0.50
+	HYDROGRAPH AT	R23	608.	12.33	84.	28.	9.	0.50
+	DIVERSION TO	RETR23	608.	12.33	63.	18.	6.	0.50
+	HYDROGRAPH AT	DIVR23	309.	12.58	32.	10.	3.	0.50
+	2 COMBINED AT	CPR23	309.	12.58	49.	16.	5.	1.00
+	ROUTED TO	R23R25	135.	13.00	47.	16.	5.	1.00
+	3 COMBINED AT	CPR25	828.	15.83	590.	222.	75.	15.93
+	ROUTED TO	R25R24	827.	15.92	590.	222.	75.	15.93
+	HYDROGRAPH AT	R19	1566.	12.50	263.	88.	29.	1.53
+	DIVERSION TO	RETR19	1566.	12.50	194.	55.	18.	1.53
+	HYDROGRAPH AT	DIVR19	875.	12.75	110.	34.	11.	1.53
+	DIVERSION TO	DETR19	704.	12.75	36.	9.	3.	1.53
+	HYDROGRAPH AT	DIV19R	171.	12.67	74.	25.	8.	1.53
+	ROUTED TO	R19R24	160.	13.92	70.	25.	8.	1.53
+	HYDROGRAPH AT	R24	346.	12.33	48.	16.	5.	0.29
+	DIVERSION TO	RETR24	346.	12.33	36.	10.	3.	0.29
+	HYDROGRAPH AT	DIVR24	196.	12.58	19.	6.	2.	0.29
+	3 COMBINED AT	CPR24	865.	15.75	648.	245.	82.	17.75
+	ROUTED TO	R24EM4	860.	15.83	647.	245.	82.	17.75
+	HYDROGRAPH AT	EMF4	119.	12.08	7.	2.	1.	0.06
+	3 COMBINED AT	CPEMF4	2926.	15.17	1939.	721.	246.	55.93

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION E7STOR
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	STORAGE	1566.00	1574.00	1574.00				
	OUTFLOW	0.	607.	607.				
		0.	104.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.55	0.00	12.	0.	0.00	0.00	0.00

PLAN 2	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	STORAGE	1566.00	1574.00	1574.00				
	OUTFLOW	0.	607.	607.				
		0.	104.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.55	0.00	12.	0.	0.00	0.00	0.00

	PMF	W.S.ELEV	OVER DAM	AC-FT	CFS	HOURS	HOURS	HOURS
	1.00	1566.52	0.00	12.	0.	0.00	0.00	0.00
PLAN 3		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1566.00	1574.00	1574.00				
	STORAGE	0.	607.	607.				
	OUTFLOW	0.	104.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.41	0.00	9.	0.	0.00	0.00	0.00
PLAN 4		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1566.00	1574.00	1574.00				
	STORAGE	0.	607.	607.				
	OUTFLOW	0.	104.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.28	0.00	6.	0.	0.00	0.00	0.00
PLAN 5		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1566.00	1574.00	1574.00				
	STORAGE	0.	607.	607.				
	OUTFLOW	0.	104.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.10	0.00	2.	0.	0.00	0.00	0.00
PLAN 6		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1566.00	1574.00	1574.00				
	STORAGE	0.	607.	607.				
	OUTFLOW	0.	104.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.01	0.00	0.	0.	0.00	0.00	0.00
PLAN 7		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1566.00	1574.00	1574.00				
	STORAGE	0.	607.	607.				
	OUTFLOW	0.	104.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.00	0.00	0.	0.	0.00	0.00	0.00
PLAN 8		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1566.00	1574.00	1574.00				
	STORAGE	0.	607.	607.				
	OUTFLOW	0.	104.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.00	0.00	0.	0.	0.00	0.00	0.00
PLAN 9		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	1566.00	1574.00	1574.00				
	STORAGE	0.	607.	607.				
	OUTFLOW	0.	104.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.00	0.00	0.	0.	0.00	0.00	0.00

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION RITBAS
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	STORAGE	1311.00	1318.00	1318.00				
	OUTFLOW	0.	693.	693.				
		0.	7.	7.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.00	0.00	0.	0.	0.00	0.00	0.00

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1.00	1311.84	0.00	18.	1.	0.00	12.92	0.00
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PLAN 2

ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
0.	1311.00	1318.00	1318.00
0.	0.	693.	693.
0.	0.	7.	7.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1.00	1311.83	0.00	18.	1.	0.00	12.92	0.00
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PLAN 3

ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
0.	1311.00	1318.00	1318.00
0.	0.	693.	693.
0.	0.	7.	7.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1.00	1311.81	0.00	18.	1.	0.00	12.92	0.00
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PLAN 4

ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
0.	1311.00	1318.00	1318.00
0.	0.	693.	693.
0.	0.	7.	7.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1.00	1311.78	0.00	17.	1.	0.00	12.83	0.00
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PLAN 5

ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
0.	1311.00	1318.00	1318.00
0.	0.	693.	693.
0.	0.	7.	7.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1.00	1311.74	0.00	16.	1.	0.00	12.75	0.00
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PLAN 6

ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
0.	1311.00	1318.00	1318.00
0.	0.	693.	693.
0.	0.	7.	7.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1.00	1311.72	0.00	16.	1.	0.00	12.75	0.00
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PLAN 7

ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
0.	1311.00	1318.00	1318.00
0.	0.	693.	693.
0.	0.	7.	7.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1.00	1311.71	0.00	16.	1.	0.00	12.75	0.00
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PLAN 8

ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
0.	1311.00	1318.00	1318.00
0.	0.	693.	693.
0.	0.	7.	7.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1.00	1311.70	0.00	15.	1.	0.00	12.75	0.00
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PLAN 9

ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
0.	1311.00	1318.00	1318.00
0.	0.	693.	693.
0.	0.	7.	7.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1.00	1311.69	0.00	15.	1.	0.00	12.75	0.00
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*** NORMAL END OF HEC-1 ***

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*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 04JUL16 TIME 08:42:05
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*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID 24INT100C 100-YEAR, 24-hr Interim Conditions 2016-03-02
2 ID Copy of 24INT100 assumng concrete-lined channel for the following routes
3 ID E5A14A, E1424A, E1424B, E247A1, E247A2 and E2726A.
4 ID by Parsons Corporation
5 ID
6 ID 2015-12-22 The model reflects interim drainage conditions for SR 24
7 ID and it is based on Mesa ADMPU with revisions reflecting development work
8 ID around the corridor.
9 ID
10 ID 2016-03-02 Modified to combine CPG19B to CPG22B as result of the Eastmark
11 ID Development. G19E26 was subsequently removed.
12 ID
13 ID 2016-07-04 Modified to include concrete lining for the SR 24 Channel.
14 ID
15 ID
16 ID *****
17 ID FUTEMADMP24 20110519 - EMADMPU 24-hr Future Conditions 20110519
18 ID Flood Control District of Maricopa County
19 ID 100 YEAR
20 ID 24 Hour Storm
21 ID Unit Hydrograph: S-Graph
22 ID 08/05/2011
23 IT 5 0 0 2000
24 IN 15
25 IO 5
*DIAGRAM
*
26 JD 3.579 0.0001
27 PC 0.000 0.002 0.005 0.008 0.011 0.014 0.017 0.020 0.023 0.026
28 PC 0.029 0.032 0.035 0.038 0.041 0.044 0.048 0.052 0.056 0.060
29 PC 0.064 0.068 0.072 0.076 0.080 0.085 0.090 0.095 0.100 0.105
30 PC 0.110 0.115 0.120 0.126 0.133 0.140 0.147 0.155 0.163 0.172
31 PC 0.181 0.191 0.203 0.218 0.236 0.257 0.283 0.387 0.663 0.707
32 PC 0.735 0.758 0.776 0.791 0.804 0.815 0.825 0.834 0.842 0.849
33 PC 0.856 0.863 0.869 0.875 0.881 0.887 0.893 0.898 0.903 0.908
34 PC 0.913 0.918 0.922 0.926 0.930 0.934 0.938 0.942 0.946 0.950
35 PC 0.953 0.956 0.959 0.962 0.965 0.968 0.971 0.974 0.977 0.980
36 PC 0.983 0.986 0.989 0.992 0.995 0.998 1.000
37 JD 3.561 1.0
38 JD 3.490 5.0
39 JD 3.400 10.0
40 JD 3.286 20.0
41 JD 3.221 30.0
42 JD 3.175 40.0
43 JD 3.139 50.0
44 JD 3.114 60.0
*
45 KK P1 BASIN
46 KM
47 KM Used the unit hydrograph for undeveloped conditions
48 KM by Parsons Corporation 2015-11
49 BA 0.387
50 LG 0.35 0.35 3.95 0.47 0
51 UI 0 29 29 99 134 162 189 226 301 369

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1 HEC-1 INPUT PAGE 2

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
52 UI 298 248 210 175 144 108 65 50 45 29
53 UI 26 9 9 9 9 9 9 0 0 0
54 UI 0 0 0 0 0 0 0 0 0 0
55 UI 0 0 0 0 0 0 0 0 0 0
*
56 KM KK DIVP1 DIVERT

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WARNING --- ROUTED OUTFLOW ( 494.) IS GREATER THAN MAXIMUM OUTFLOW ( 487.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 498.) IS GREATER THAN MAXIMUM OUTFLOW ( 487.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 489.) IS GREATER THAN MAXIMUM OUTFLOW ( 487.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 490.) IS GREATER THAN MAXIMUM OUTFLOW ( 487.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 523.) IS GREATER THAN MAXIMUM OUTFLOW ( 487.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 513.) IS GREATER THAN MAXIMUM OUTFLOW ( 487.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 503.) IS GREATER THAN MAXIMUM OUTFLOW ( 487.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 497.) IS GREATER THAN MAXIMUM OUTFLOW ( 487.) IN STORAGE-OUTFLOW TABLE
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WARNING --- ROUTED OUTFLOW ( 509.) IS GREATER THAN MAXIMUM OUTFLOW ( 487.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 499.) IS GREATER THAN MAXIMUM OUTFLOW ( 487.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 490.) IS GREATER THAN MAXIMUM OUTFLOW ( 487.) IN STORAGE-OUTFLOW TABLE
WARNING --- ROUTED OUTFLOW ( 491.) IS GREATER THAN MAXIMUM OUTFLOW ( 487.) IN STORAGE-OUTFLOW TABLE
WARNING EXCESS AT PONDING LESS THAN ZERO FOR PERIOD. EXCESS SET TO ZERO

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1 RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT								
+	P1	244.	12.67	32.	8.	3.	0.39		
+	DIVERSION TO								
+	DRPFW	161.	12.67	17.	4.	1.	0.39		
+	HYDROGRAPH AT								
+	DP1PFW	83.	12.67	15.	4.	1.	0.39		
+	ROUTED TO								
+	P1P2	58.	14.50	15.	4.	1.	0.39		
+	HYDROGRAPH AT								
+	P2	326.	12.75	49.	12.	4.	0.58		
+	2 COMBINED AT								
+	CPP2	326.	12.75	65.	16.	5.	0.96		
+	ROUTED TO								
+	P2P4	310.	13.00	64.	16.	5.	0.96		
+	HYDROGRAPH AT								
+	P4	536.	12.50	79.	24.	8.	0.50		
+	DIVERSION TO								
+	RETP4	536.	12.50	79.	24.	8.	0.50		
+	HYDROGRAPH AT								
+	DIVP4	0.	0.00	0.	0.	0.	0.50		
+	2 COMBINED AT								
+	CPP4	310.	13.00	64.	16.	5.	1.46		
+	ROUTED TO								
+	P4P6	289.	13.25	64.	16.	5.	1.46		
+	HYDROGRAPH AT								
+	P6	456.	12.67	79.	24.	8.	0.50		
+	DIVERSION TO								
+	RETP6	456.	12.67	79.	24.	8.	0.50		
+	HYDROGRAPH AT								
+	DIVP6	0.	0.00	0.	0.	0.	0.50		
+	2 COMBINED AT								
+	CPP6	289.	13.25	64.	16.	5.	1.96		
+	ROUTED TO								
+	P6GM8	273.	13.42	63.	16.	5.	1.96		
+	ROUTED TO								
+	GM8G10	265.	13.58	63.	16.	5.	1.96		
+	HYDROGRAPH AT								
+	DRPFW	161.	12.67	17.	4.	1.	0.39		
+	ROUTED TO								
+	P1PFW	135.	12.83	17.	4.	1.	0.39		
+	HYDROGRAPH AT								
+	P3	242.	13.00	43.	11.	4.	0.52		
+	2 COMBINED AT								
+	CPP3	363.	12.92	60.	15.	5.	0.91		

+	ROUTED TO	P3P5	358.	13.00	60.	15.	5.	0.91
+	HYDROGRAPH AT	P5	268.	12.50	41.	12.	4.	0.25
+	DIVERSION TO	RETP5	268.	12.50	33.	9.	3.	0.25
+	HYDROGRAPH AT	DIVP5	121.	12.92	12.	4.	1.	0.25
+	2 COMBINED AT	CPP5	463.	12.92	71.	19.	6.	1.16
+	ROUTED TO	P5P7	447.	13.00	71.	19.	6.	1.16
+	HYDROGRAPH AT	P7	485.	12.50	74.	22.	7.	0.43
+	DIVERSION TO	RETP7	485.	12.50	58.	16.	5.	0.43
+	HYDROGRAPH AT	DIVP7	212.	12.92	22.	6.	2.	0.43
+	3 COMBINED AT	CPP7	586.	13.00	150.	40.	13.	3.17
+	ROUTED TO	P7GM14	569.	13.25	149.	40.	13.	3.17
+	HYDROGRAPH AT	GM1	435.	12.42	53.	14.	5.	0.34
+	HYDROGRAPH AT	GM2	1023.	12.33	130.	42.	14.	0.68
+	HYDROGRAPH AT	GM3	651.	12.08	69.	23.	8.	0.29
+	3 COMBINED AT	CPG123	1747.	12.17	250.	78.	26.	1.32
+	DIVERSION TO	RETG1	1747.	12.17	188.	51.	17.	1.32
+	HYDROGRAPH AT	DIVG1	847.	12.58	89.	26.	9.	1.32
+	ROUTED TO	GM1T5	640.	12.67	88.	26.	9.	1.32
+	HYDROGRAPH AT	GM5	349.	12.17	42.	13.	4.	0.18
+	DIVERSION TO	RETG5	325.	12.17	24.	7.	2.	0.18
+	HYDROGRAPH AT	DIVG5	334.	12.25	23.	7.	2.	0.18
+	2 COMBINED AT	CPG5	686.	12.67	109.	33.	11.	1.49
+	ROUTED TO	GM5T7	571.	12.92	107.	33.	11.	1.49
+	HYDROGRAPH AT	GM6	777.	12.17	73.	22.	7.	0.37
+	DIVERSION TO	RETG6	777.	12.17	50.	14.	5.	0.37
+	HYDROGRAPH AT	DIVG6	552.	12.25	30.	9.	3.	0.37
+	HYDROGRAPH AT	GM7	290.	12.33	32.	9.	3.	0.22
+	DIVERSION TO	RETG7	290.	12.33	28.	7.	2.	0.22
+	HYDROGRAPH AT	DIVG7	71.	12.75	5.	2.	1.	0.22
+	2 COMBINED AT	CPG7A	552.	12.25	36.	10.	3.	0.58
+	2 COMBINED AT	CPG7B	633.	12.92	139.	42.	14.	2.08
+	ROUTED TO	GM7T9	585.	13.00	137.	42.	14.	2.08
+	HYDROGRAPH AT	GM8	798.	12.33	100.	32.	11.	0.56
+	DIVERSION TO	RETG8	798.	12.33	73.	20.	7.	0.56
+	HYDROGRAPH AT							

+		DIVG8	516.	12.50	38.	11.	4.	0.56
+	HYDROGRAPH AT	GM9	177.	12.17	13.	4.	1.	0.09
+	DIVERSION TO	RETG9	177.	12.17	13.	3.	1.	0.09
+	HYDROGRAPH AT	DIVG9	5.	12.75	2.	1.	0.	0.09
+	2 COMBINED AT	CPG9A	516.	12.50	40.	12.	4.	0.65
+	HYDROGRAPH AT	GM10	409.	12.33	53.	16.	5.	0.28
+	DIVERSION TO	RETG10	409.	12.33	32.	9.	3.	0.28
+	HYDROGRAPH AT	DIVG10	329.	12.42	26.	7.	2.	0.28
+	HYDROGRAPH AT	GM11	108.	12.25	10.	3.	1.	0.08
+	DIVERSION TO	RETG11	108.	12.25	10.	3.	1.	0.08
+	HYDROGRAPH AT	DIVG11	4.	13.33	1.	1.	0.	0.08
+	2 COMBINED AT	CPG11	329.	12.42	28.	8.	3.	0.36
+	3 COMBINED AT	CPG9B	946.	12.50	198.	60.	20.	3.08
+	ROUTED TO	GM9T14	723.	12.75	195.	60.	20.	3.08
+	HYDROGRAPH AT	GM12	275.	12.08	29.	10.	3.	0.12
+	DIVERSION TO	RETG12	217.	12.00	16.	5.	2.	0.12
+	HYDROGRAPH AT	DIVG12	255.	12.17	17.	5.	2.	0.12
+	ROUTED TO	G12T13	130.	12.33	17.	5.	2.	0.12
+	HYDROGRAPH AT	GM13	596.	12.08	55.	18.	6.	0.29
+	DIVERSION TO	RETG13	596.	12.08	41.	11.	4.	0.29
+	HYDROGRAPH AT	DIVG13	376.	12.25	21.	6.	2.	0.29
+	2 COMBINED AT	CPG13	471.	12.25	38.	11.	4.	0.41
+	ROUTED TO	G13T14	366.	12.33	38.	11.	4.	0.41
+	HYDROGRAPH AT	GM14	678.	12.17	67.	22.	7.	0.35
+	DIVERSION TO	RETG14	676.	12.17	46.	13.	4.	0.35
+	HYDROGRAPH AT	DIVG14	546.	12.25	31.	9.	3.	0.35
+	2 COMBINED AT	CPG14A	708.	12.25	69.	21.	7.	0.76
+	2 COMBINED AT	CPG14B	849.	12.75	256.	80.	27.	3.84
+	2 COMBINED AT	CPG14C	1156.	13.25	379.	113.	38.	7.01
+	ROUTED TO	G14E26	1151.	13.25	379.	113.	38.	7.01
+	HYDROGRAPH AT	E1	472.	12.83	73.	18.	6.	0.89
+	DIVERSION TO	DRE2	383.	12.83	56.	14.	5.	0.89
+	HYDROGRAPH AT	DE15	88.	12.83	18.	4.	1.	0.89
+	ROUTED TO	E1E10	55.	15.00	18.	4.	1.	0.89
+	HYDROGRAPH AT	E10	411.	12.92	68.	17.	6.	0.82

+	2 COMBINED AT	CPE10	435.	12.92	85.	21.	7.	1.71
	ROUTED TO	E10E17	402.	13.08	84.	21.	7.	1.71
+	HYDROGRAPH AT	E17	287.	12.50	41.	13.	4.	0.27
+	DIVERSION TO	RETE17	287.	12.50	34.	9.	3.	0.27
+	HYDROGRAPH AT	DIVE17	123.	12.83	11.	3.	1.	0.27
+	2 COMBINED AT	CPE17	452.	13.08	95.	24.	8.	1.98
+	ROUTED TO	E17E21	433.	13.25	94.	24.	8.	1.98
+	HYDROGRAPH AT	E21	341.	12.50	51.	15.	5.	0.31
+	DIVERSION TO	RETE21	341.	12.50	38.	10.	3.	0.31
+	HYDROGRAPH AT	DIVE21	175.	12.83	17.	5.	2.	0.31
+	2 COMBINED AT	CPE21A	474.	13.25	110.	29.	10.	2.29
+	ROUTED TO	E21G20	465.	13.25	110.	29.	10.	2.29
+	HYDROGRAPH AT	DRE2	383.	12.83	56.	14.	5.	0.89
+	ROUTED TO	RTE1E2	316.	13.17	56.	14.	5.	0.89
+	HYDROGRAPH AT	E2	409.	12.92	68.	17.	6.	0.78
+	2 COMBINED AT	CPE2	627.	13.00	122.	31.	10.	1.67
+	DIVERSION TO	DRE3	408.	13.00	60.	15.	5.	1.67
+	HYDROGRAPH AT	DE2S	219.	13.00	62.	16.	5.	1.67
+	ROUTED TO	E2E11	173.	15.83	62.	16.	5.	1.67
+	HYDROGRAPH AT	E11	318.	12.83	50.	12.	4.	0.60
+	2 COMBINED AT	CPE11	311.	12.83	100.	28.	9.	2.27
+	ROUTED TO	E11E18	236.	13.58	97.	28.	9.	2.27
+	HYDROGRAPH AT	E18	320.	12.33	36.	10.	3.	0.22
+	DIVERSION TO	RETE18	1.	4.17	1.	0.	0.	0.22
+	HYDROGRAPH AT	DIVE18	320.	12.33	36.	10.	3.	0.22
+	2 COMBINED AT	CPE18	316.	12.33	118.	37.	12.	2.49
+	ROUTED TO	E18E21	287.	12.50	117.	37.	12.	2.49
+	2 COMBINED AT	CPE21B	576.	13.50	223.	66.	22.	3.90
+	ROUTED TO	G20G21	573.	13.58	221.	66.	22.	3.90
+	HYDROGRAPH AT	DRE3	408.	13.00	60.	15.	5.	1.67
+	ROUTED TO	RTE2E3	365.	13.33	60.	15.	5.	1.67
+	HYDROGRAPH AT	E3	935.	13.25	209.	52.	17.	2.23
+	2 COMBINED AT	E2SE3	1259.	13.25	264.	66.	22.	3.90
+	DIVERSION TO	DRE4N	804.	13.25	125.	31.	10.	3.90

+	HYDROGRAPH AT	DE3S	455.	13.25	139.	35.	12.	3.90
+	ROUTED TO	E3E12	401.	14.50	139.	35.	12.	3.90
+	HYDROGRAPH AT	E12	318.	12.92	55.	14.	5.	0.57
+	2 COMBINED AT	CPE12	546.	12.92	191.	48.	16.	4.47
+	ROUTED TO	E12E19	486.	13.67	191.	48.	16.	4.47
+	HYDROGRAPH AT	E19	234.	12.25	23.	6.	2.	0.14
+	2 COMBINED AT	CPE19	488.	13.67	212.	54.	18.	4.61
+	ROUTED TO	E1922E	467.	14.00	212.	54.	18.	4.61
+	HYDROGRAPH AT	22E	149.	12.25	15.	4.	1.	0.09
+	HYDROGRAPH AT	E20	159.	12.50	20.	5.	2.	0.17
+	ROUTED TO	E2022E	129.	12.75	20.	5.	2.	0.17
+	3 COMBINED AT	CP22E	472.	14.00	245.	63.	21.	4.87
+	ROUTED TO	22EE22	465.	14.17	245.	63.	21.	4.87
+	HYDROGRAPH AT	E22	223.	12.67	33.	8.	3.	0.16
+	3 COMBINED AT	CPE22	940.	13.83	477.	133.	44.	7.25
+	ROUTED TO	E22G22	931.	14.00	473.	133.	44.	7.25
+	HYDROGRAPH AT	GM21	379.	12.25	50.	17.	6.	0.21
+	DIVERSION TO	RETG21	360.	12.17	30.	9.	3.	0.21
+	HYDROGRAPH AT	DIVG21	347.	12.33	28.	8.	3.	0.21
+	ROUTED TO	G21T22	298.	12.42	28.	8.	3.	0.21
+	HYDROGRAPH AT	GM22	208.	12.17	24.	8.	3.	0.09
+	DIVERSION TO	RETG22	199.	12.08	14.	4.	1.	0.09
+	HYDROGRAPH AT	DIVG22	177.	12.17	13.	4.	1.	0.09
+	2 COMBINED AT	CPG22A	347.	12.42	41.	12.	4.	0.31
+	HYDROGRAPH AT	GM16	93.	12.33	12.	4.	1.	0.07
+	DIVERSION TO	RETG16	93.	12.33	9.	2.	1.	0.07
+	HYDROGRAPH AT	DIVG16	42.	12.58	4.	1.	0.	0.07
+	ROUTED TO	G16T19	29.	12.75	4.	1.	0.	0.07
+	HYDROGRAPH AT	GM18	274.	12.25	31.	10.	3.	0.17
+	DIVERSION TO	RETG18	274.	12.25	23.	6.	2.	0.17
+	HYDROGRAPH AT	DIVG18	178.	12.42	12.	4.	1.	0.17
+	2 COMBINED AT	CPG18	178.	12.42	16.	5.	2.	0.24
+	HYDROGRAPH AT	GM19	174.	12.17	15.	4.	1.	0.09
+	DIVERSION TO	RETG19	174.	12.17	11.	3.	1.	0.09
+	HYDROGRAPH AT							

+		DIVG19	77.	12.33	5.	1.	0.	0.09
+	2 COMBINED AT	CPG19A	218.	12.42	21.	6.	2.	0.33
+	HYDROGRAPH AT	GM20	359.	12.17	39.	12.	4.	0.18
+	DIVERSION TO	RETG20	359.	12.17	27.	7.	2.	0.18
+	HYDROGRAPH AT	DIVG20	244.	12.33	16.	5.	2.	0.18
+	2 COMBINED AT	CPG19B	368.	12.42	37.	11.	4.	0.51
+	3 COMBINED AT	CPG22B	970.	14.00	536.	153.	51.	8.06
+	ROUTED TO	G22E26	940.	14.33	534.	153.	51.	8.06
+	HYDROGRAPH AT	DRE4N	804.	13.25	125.	31.	10.	3.90
+	ROUTED TO	RTE3E4	750.	13.42	125.	31.	10.	3.90
+	HYDROGRAPH AT	E4N	154.	12.92	25.	6.	2.	0.31
+	2 COMBINED AT	CPE4N	813.	13.42	149.	37.	12.	4.21
+	DIVERSION TO	DRE4	651.	13.42	110.	27.	9.	4.21
+	HYDROGRAPH AT	DE4NS	162.	13.42	40.	10.	3.	4.21
+	ROUTED TO	E4NE13	131.	15.33	40.	10.	3.	4.21
+	HYDROGRAPH AT	E13	284.	12.83	48.	12.	4.	0.48
+	2 COMBINED AT	CPE13	275.	12.83	86.	22.	7.	4.69
+	ROUTED TO	E13E24	190.	13.92	85.	22.	7.	4.69
+	HYDROGRAPH AT	DRE4	651.	13.42	110.	27.	9.	4.21
+	ROUTED TO	RTE4E4	515.	14.25	109.	27.	9.	4.21
+	HYDROGRAPH AT	E4	462.	13.25	103.	26.	9.	1.20
+	2 COMBINED AT	CPE4	645.	14.17	205.	51.	17.	5.41
+	DIVERSION TO	DRE5	630.	14.17	198.	49.	16.	5.41
+	HYDROGRAPH AT	DE4S	15.	14.17	8.	2.	1.	5.41
+	ROUTED TO	E4E14A	14.	15.17	8.	2.	1.	5.41
+	HYDROGRAPH AT	E14A	170.	12.75	26.	6.	2.	0.48
+	HYDROGRAPH AT	E6A	740.	13.25	226.	74.	25.	0.58
+	ROUTED TO	E6AE5A	709.	13.50	226.	74.	25.	0.58
+	HYDROGRAPH AT	DRE5	630.	14.17	198.	49.	16.	5.41
+	ROUTED TO	RTE4E5	583.	14.42	197.	49.	16.	5.41
+	HYDROGRAPH AT	E5A	537.	13.25	118.	29.	10.	1.14
+	2 COMBINED AT	CPE5A1	792.	13.33	303.	76.	25.	6.55
+	2 COMBINED AT	CPE5A2	1432.	13.42	516.	147.	49.	7.13
+	ROUTED TO	E5A14A	1424.	13.58	516.	147.	49.	7.13
+	3 COMBINED AT	CPE14A	1445.	13.58	545.	154.	52.	7.61

+	ROUTED TO	E1424A	1440.	13.58	545.	154.	52.	7.61
+	ROUTED TO	E1424B	1440.	13.67	544.	154.	52.	7.61
+	HYDROGRAPH AT	E24A	812.	12.33	110.	36.	12.	0.53
+	DIVERSION TO	RET24A	807.	12.25	70.	20.	7.	0.53
+	HYDROGRAPH AT	DIV24A	704.	12.42	55.	16.	5.	0.53
+	3 COMBINED AT	CP24A	1637.	13.67	670.	188.	63.	8.62
+	ROUTED TO	E247A1	1630.	13.83	669.	188.	63.	8.62
+	HYDROGRAPH AT	E27A	647.	12.50	115.	37.	12.	0.54
+	DIVERSION TO	RET27A	647.	12.50	76.	21.	7.	0.54
+	HYDROGRAPH AT	DIV27A	478.	12.75	54.	16.	5.	0.54
+	3 COMBINED AT	CPE27A	2452.	13.83	1202.	342.	114.	12.81
+	ROUTED TO	E247A2	2448.	13.92	1201.	342.	114.	12.81
+	ROUTED TO	E2726A	2442.	14.00	1199.	342.	114.	12.81
+	HYDROGRAPH AT	E26A	1093.	12.50	181.	58.	19.	0.87
+	DIVERSION TO	RET26A	1093.	12.50	119.	33.	11.	0.87
+	HYDROGRAPH AT	DIV26A	843.	12.67	84.	24.	8.	0.87
+	2 COMBINED AT	SR24EL	2479.	14.00	1260.	360.	120.	13.68
+	DIVERSION TO	1650UP	829.	14.00	190.	47.	16.	13.68
+	HYDROGRAPH AT	802ELS	1650.	12.92	1070.	312.	104.	13.68
+	HYDROGRAPH AT	GM17	174.	12.17	18.	6.	2.	0.10
+	DIVERSION TO	RETG17	174.	12.17	18.	6.	2.	0.10
+	HYDROGRAPH AT	DIVG17	0.	0.00	0.	0.	0.	0.10
+	ROUTED TO	G17E26	0.	0.00	0.	0.	0.	0.10
+	3 COMBINED AT	CPE26A	2483.	13.42	1355.	403.	134.	20.80
+	ROUTED TO	80233B	2464.	13.50	1353.	402.	134.	20.80
+	HYDROGRAPH AT	E7	820.	12.92	182.	56.	19.	1.12
+	DIVERSION TO	RETE7	820.	12.92	159.	43.	14.	1.12
+	HYDROGRAPH AT	DIVE7	234.	13.67	43.	13.	4.	1.12
+	ROUTED TO	E7STOR	1.	25.67	1.	1.	0.	1.12
+	ROUTED TO	E7E6	1.	30.00	1.	1.	0.	1.12
+	HYDROGRAPH AT	E6B	2187.	12.58	400.	132.	44.	1.95
+	DIVERSION TO	RETE6B	2187.	12.58	326.	91.	30.	1.95
+	HYDROGRAPH AT	DIVE6B	897.	13.00	131.	41.	14.	1.95
+	HYDROGRAPH AT	E8	901.	12.75	180.	57.	19.	1.10

+	DIVERSION TO	RETE8	901.	12.75	149.	41.	14.	1.10
+	HYDROGRAPH AT	DIVE8	378.	13.25	52.	16.	5.	1.10
+	ROUTED TO	E8E6	191.	14.00	50.	16.	5.	1.10
+	3 COMBINED AT	CPE6	897.	13.00	176.	57.	19.	3.05
+	DIVERSION TO	DRE9	104.	13.00	3.	1.	0.	3.05
+	HYDROGRAPH AT	DE6S	788.	13.00	169.	55.	18.	3.05
+	ROUTED TO	E6E15	497.	13.58	165.	55.	18.	3.05
+	HYDROGRAPH AT	E15	1096.	12.33	154.	51.	17.	0.78
+	DIVERSION TO	RETE15	1096.	12.33	122.	34.	11.	0.78
+	HYDROGRAPH AT	DIVE15	431.	12.67	54.	17.	6.	0.78
+	HYDROGRAPH AT	DRE9	104.	13.00	3.	1.	0.	3.05
+	ROUTED TO	RTE6E9	26.	13.42	3.	1.	0.	3.05
+	HYDROGRAPH AT	E9	968.	12.42	147.	48.	16.	0.72
+	DIVERSION TO	RETE9	968.	12.42	118.	33.	11.	0.72
+	HYDROGRAPH AT	DIVE9	372.	12.75	49.	15.	5.	0.72
+	2 COMBINED AT	CPE9	372.	12.75	52.	16.	5.	0.72
+	DIVERSION TO	DRR5	196.	12.75	9.	2.	1.	0.72
+	HYDROGRAPH AT	DE9S	177.	12.75	43.	14.	5.	0.72
+	ROUTED TO	E9E16	122.	13.25	42.	14.	5.	0.72
+	HYDROGRAPH AT	E16	582.	12.33	79.	26.	9.	0.40
+	DIVERSION TO	RETE16	582.	12.33	64.	18.	6.	0.40
+	HYDROGRAPH AT	DIVE16	213.	12.58	26.	8.	3.	0.40
+	2 COMBINED AT	CPE16	201.	12.58	66.	22.	7.	1.12
+	ROUTED TO	E16E15	189.	12.83	66.	22.	7.	1.12
+	3 COMBINED AT	CPE15	689.	13.58	263.	90.	30.	4.95
+	ROUTED TO	E1524B	621.	13.83	260.	90.	30.	4.95
+	HYDROGRAPH AT	E5B	447.	12.25	57.	19.	6.	0.29
+	DIVERSION TO	RETE5B	447.	12.25	45.	13.	4.	0.29
+	HYDROGRAPH AT	DIVE5B	204.	12.50	21.	7.	2.	0.29
+	ROUTED TO	E5E14B	89.	12.92	20.	7.	2.	0.29
+	HYDROGRAPH AT	E14B	884.	12.25	109.	36.	12.	0.53
+	DIVERSION TO	RET14B	884.	12.25	88.	24.	8.	0.53
+	HYDROGRAPH AT	DIV14B	372.	12.50	37.	12.	4.	0.53
+	2 COMBINED AT	CP14B	371.	12.50	57.	18.	6.	0.81
+	ROUTED TO							

+		E14E24	180.	13.00	55.	18.	6.	0.81
+	HYDROGRAPH AT	E24B	788.	12.25	100.	32.	11.	0.46
+	DIVERSION TO	RET24B	788.	12.25	70.	20.	7.	0.46
+	HYDROGRAPH AT	DIV24B	572.	12.42	43.	13.	4.	0.46
+	3 COMBINED AT	CPE24B	697.	13.83	328.	116.	39.	6.23
+	ROUTED TO	E24E28	660.	14.17	324.	116.	39.	6.23
+	HYDROGRAPH AT	E28B	773.	12.42	116.	37.	12.	0.54
+	DIVERSION TO	RET28B	773.	12.42	76.	21.	7.	0.54
+	HYDROGRAPH AT	DIV28B	555.	12.58	54.	16.	5.	0.54
+	2 COMBINED AT	CPE28B	676.	14.17	362.	129.	43.	6.77
+	ROUTED TO	E28E31	650.	14.42	356.	129.	43.	6.77
+	HYDROGRAPH AT	E25	1038.	12.50	184.	60.	20.	0.93
+	DIVERSION TO	RETE25	1038.	12.50	184.	56.	19.	0.93
+	HYDROGRAPH AT	DIVE25	23.	18.08	16.	4.	1.	0.93
+	ROUTED TO	E25E29	20.	19.75	16.	4.	1.	0.93
+	HYDROGRAPH AT	E29	1237.	12.50	203.	66.	22.	1.00
+	DIVERSION TO	RETE29	1237.	12.50	132.	37.	12.	1.00
+	HYDROGRAPH AT	DIVE29	906.	12.67	99.	29.	10.	1.00
+	2 COMBINED AT	CPE29	897.	12.67	96.	32.	11.	1.93
+	ROUTED TO	E29E31	573.	13.00	94.	32.	11.	1.93
+	HYDROGRAPH AT	E32	404.	12.25	48.	16.	5.	0.25
+	DIVERSION TO	RETE32	394.	12.17	30.	9.	3.	0.25
+	HYDROGRAPH AT	DIVE32	344.	12.33	25.	7.	2.	0.25
+	ROUTED TO	E32E31	155.	12.75	24.	7.	2.	0.25
+	HYDROGRAPH AT	E31	964.	12.42	157.	52.	17.	0.81
+	DIVERSION TO	RETE31	964.	12.42	100.	28.	9.	0.81
+	HYDROGRAPH AT	DIVE31	835.	12.58	79.	23.	8.	0.81
+	4 COMBINED AT	CPE31	1095.	13.00	501.	177.	59.	9.76
+	ROUTED TO	E31E30	963.	13.42	489.	177.	59.	9.76
+	HYDROGRAPH AT	E30B	844.	12.83	186.	58.	19.	0.88
+	DIVERSION TO	RET30B	844.	12.83	122.	34.	11.	0.88
+	HYDROGRAPH AT	DIV30B	619.	13.08	84.	24.	8.	0.88
+	2 COMBINED AT	CPE30	1307.	13.33	553.	195.	65.	10.64
+	ROUTED TO	E30E26	1282.	13.42	550.	195.	65.	10.64
+	HYDROGRAPH AT	E26B	415.	12.33	56.	18.	6.	0.26

+	DIVERSION TO	RET26B	415.	12.33	37.	10.	3.	0.26
+	HYDROGRAPH AT	DIV26B	280.	12.50	26.	7.	2.	0.26
+	2 COMBINED AT	CPE26	1299.	13.42	556.	201.	67.	10.90
+	ROUTED TO	E26E33	1157.	13.83	546.	200.	67.	10.90
+	HYDROGRAPH AT	E33B	1304.	12.33	183.	59.	20.	0.85
+	DIVERSION TO	RET33B	1304.	12.33	120.	34.	11.	0.85
+	HYDROGRAPH AT	DIV33B	972.	12.50	86.	25.	8.	0.85
+	3 COMBINED AT	CPE33B	3181.	13.92	1742.	569.	191.	32.54
+	ROUTED TO	E33P9A	3156.	14.00	1737.	568.	191.	32.54
+	ROUTED TO	E33P9B	3112.	14.08	1731.	568.	191.	32.54
+	HYDROGRAPH AT	P9	1513.	12.42	268.	90.	30.	1.12
+	DIVERSION TO	RETP9	137.	11.50	53.	18.	6.	1.12
+	HYDROGRAPH AT	DIVP9	1513.	12.42	255.	72.	24.	1.12
+	2 COMBINED AT	CPP9	3183.	14.08	1857.	628.	210.	33.67
+	ROUTED TO	P9EMF1	3146.	14.25	1850.	628.	210.	33.67
+	HYDROGRAPH AT	EMF1B	1442.	12.42	233.	76.	25.	1.04
+	DIVERSION TO	REMF1B	1442.	12.42	152.	43.	14.	1.04
+	HYDROGRAPH AT	DEMF1B	1142.	12.58	114.	34.	11.	1.04
+	2 COMBINED AT	CPEMF1	3195.	14.25	1925.	651.	218.	34.70
+	ROUTED TO	EM1EM2	3194.	14.33	1924.	651.	218.	34.70
+	HYDROGRAPH AT	EMF2	1610.	12.83	393.	130.	43.	1.85
+	DIVERSION TO	RETEM2	1532.	12.83	195.	49.	16.	1.85
+	HYDROGRAPH AT	DIVEM2	1181.	13.17	198.	81.	27.	1.85
+	2 COMBINED AT	CPEMF2	3350.	14.33	2056.	704.	239.	36.55
+	ROUTED TO	EM2M3A	3338.	14.42	2053.	704.	239.	36.55
+	ROUTED TO	EM2M3B	3329.	14.42	2050.	704.	239.	36.55
+	HYDROGRAPH AT	EMF3	1324.	12.75	277.	91.	30.	1.49
+	DIVERSION TO	RETEM3	812.	12.33	98.	30.	10.	1.49
+	HYDROGRAPH AT	DIVEM3	1324.	12.75	218.	61.	20.	1.49
+	2 COMBINED AT	CPEMF3	3391.	14.42	2207.	751.	255.	38.04
+	ROUTED TO	EMF3RB	3388.	14.50	2204.	751.	255.	38.04
+	HYDROGRAPH AT	RITBAS	693.	12.08	44.	11.	4.	0.29
+	ROUTED TO	RITBAS	1.	12.92	1.	1.	1.	0.29
+	2 COMBINED AT	CPRITB	3388.	14.50	2204.	751.	256.	38.33

+	ROUTED TO	RBEMF4	3352.	14.67	2179.	751.	255.	38.33
+	HYDROGRAPH AT	R2	612.	12.67	101.	29.	10.	0.68
+	DIVERSION TO	RETR2	398.	12.33	33.	9.	3.	0.68
+	HYDROGRAPH AT	DIVR2	612.	12.67	76.	20.	7.	0.68
+	HYDROGRAPH AT	R3	358.	12.58	55.	16.	5.	0.41
+	DIVERSION TO	RETR3	330.	12.50	29.	8.	3.	0.41
+	HYDROGRAPH AT	DIVR3	352.	12.67	30.	8.	3.	0.41
+	2 COMBINED AT	CPR2R3	962.	12.67	105.	28.	9.	1.09
+	ROUTED TO	R2R3R6	467.	14.17	100.	28.	9.	1.09
+	HYDROGRAPH AT	R6	409.	12.67	62.	18.	6.	0.50
+	2 COMBINED AT	CPR6	470.	14.25	155.	45.	15.	1.59
+	ROUTED TO	R6R9	434.	14.58	154.	45.	15.	1.59
+	HYDROGRAPH AT	R9	840.	12.33	123.	41.	14.	0.59
+	DIVERSION TO	RETR9	840.	12.33	97.	27.	9.	0.59
+	HYDROGRAPH AT	DIVR9	351.	12.67	45.	14.	5.	0.59
+	2 COMBINED AT	CPR9	609.	12.67	195.	58.	20.	2.19
+	ROUTED TO	R9R11	476.	13.25	194.	58.	20.	2.19
+	HYDROGRAPH AT	R11	1179.	12.50	184.	58.	19.	0.99
+	DIVERSION TO	RETR11	1179.	12.50	123.	34.	11.	0.99
+	HYDROGRAPH AT	DIVR11	859.	12.67	83.	24.	8.	0.99
+	HYDROGRAPH AT	DRR5	196.	12.75	9.	2.	1.	0.72
+	HYDROGRAPH AT	R5	546.	12.50	72.	21.	7.	0.50
+	DIVERSION TO	RETR5	4.	4.67	2.	1.	0.	0.50
+	HYDROGRAPH AT	DIVR5	546.	12.50	72.	21.	7.	0.50
+	2 COMBINED AT	CPR5	544.	12.50	81.	23.	8.	1.22
+	ROUTED TO	R5R8	470.	12.92	81.	23.	8.	1.22
+	HYDROGRAPH AT	R8	741.	12.42	115.	39.	13.	0.55
+	DIVERSION TO	RETR8	741.	12.42	91.	25.	8.	0.55
+	HYDROGRAPH AT	DIVR8	366.	12.67	42.	13.	4.	0.55
+	2 COMBINED AT	CPR8	721.	12.67	119.	35.	12.	1.77
+	ROUTED TO	R8R11	581.	13.33	118.	35.	12.	1.77
+	3 COMBINED AT	CPR11	1147.	13.25	379.	114.	38.	4.95
+	ROUTED TO	R11R13	1049.	13.75	376.	114.	38.	4.95
+	HYDROGRAPH AT	R13	708.	12.33	94.	31.	10.	0.50
+	DIVERSION TO							

+		RETR13	705.	12.25	60.	17.	6.	0.50
+	HYDROGRAPH AT	DIVR13	599.	12.42	48.	14.	5.	0.50
+	2 COMBINED AT	CPR13	1071.	13.75	412.	126.	42.	5.45
+	ROUTED TO	R13R16	1005.	14.25	409.	126.	42.	5.45
+	HYDROGRAPH AT	R16	765.	12.25	105.	35.	12.	0.50
+	DIVERSION TO	RETR16	765.	12.25	65.	19.	6.	0.50
+	HYDROGRAPH AT	DIVR16	604.	12.42	56.	17.	6.	0.50
+	2 COMBINED AT	CPR16	1024.	14.25	452.	141.	47.	5.95
+	ROUTED TO	R16R21	925.	15.33	445.	141.	47.	5.95
+	HYDROGRAPH AT	R21	757.	12.67	133.	41.	14.	0.84
+	DIVERSION TO	RETR21	305.	12.17	30.	9.	3.	0.84
+	HYDROGRAPH AT	DIVR21	757.	12.67	117.	32.	11.	0.84
+	HYDROGRAPH AT	R1	1372.	12.58	214.	66.	22.	1.45
+	DIVERSION TO	RETR1	1372.	12.58	187.	51.	17.	1.45
+	HYDROGRAPH AT	DIVR1	308.	13.08	48.	15.	5.	1.45
+	ROUTED TO	R1R4	108.	15.25	42.	15.	5.	1.45
+	HYDROGRAPH AT	R4	817.	12.58	106.	28.	9.	1.00
+	2 COMBINED AT	CPR4	802.	12.58	131.	41.	14.	2.45
+	ROUTED TO	R4R7	621.	13.08	130.	41.	14.	2.45
+	HYDROGRAPH AT	R7	965.	12.58	157.	49.	16.	1.00
+	DIVERSION TO	RETR7	938.	12.50	85.	24.	8.	1.00
+	HYDROGRAPH AT	DIVR7	890.	12.67	89.	25.	8.	1.00
+	2 COMBINED AT	CPR7	1259.	12.67	213.	65.	22.	3.45
+	ROUTED TO	R7R10	1040.	13.33	209.	65.	22.	3.45
+	HYDROGRAPH AT	R10	781.	12.83	161.	50.	17.	1.01
+	DIVERSION TO	RETR10	781.	12.83	129.	35.	12.	1.01
+	HYDROGRAPH AT	DIVR10	358.	13.33	50.	15.	5.	1.01
+	2 COMBINED AT	CPR10	1384.	13.33	252.	78.	26.	4.46
+	ROUTED TO	R10R12	1124.	13.67	247.	78.	26.	4.46
+	HYDROGRAPH AT	R12	939.	12.17	114.	39.	13.	0.49
+	DIVERSION TO	RETR12	850.	12.17	70.	20.	7.	0.49
+	HYDROGRAPH AT	DIVR12	887.	12.25	64.	19.	6.	0.49
+	2 COMBINED AT	CPR12	1165.	13.67	297.	96.	32.	4.95
+	ROUTED TO	R12R15	949.	14.58	284.	96.	32.	4.95
+	HYDROGRAPH AT	R15	616.	12.50	90.	28.	9.	0.56

+	DIVERSION TO	RETR15	537.	12.33	40.	12.	4.	0.56
+	HYDROGRAPH AT	DIVR15	616.	12.50	60.	17.	6.	0.56
+	2 COMBINED AT	CPR15	953.	14.58	323.	111.	37.	5.51
+	ROUTED TO	R15R18	901.	15.00	315.	110.	37.	5.51
+	HYDROGRAPH AT	R18	661.	12.67	122.	38.	13.	0.80
+	DIVERSION TO	RETR18	661.	12.67	94.	26.	9.	0.80
+	HYDROGRAPH AT	DIVR18	354.	13.08	40.	12.	4.	0.80
+	2 COMBINED AT	CPR18	907.	15.00	344.	119.	40.	6.30
+	ROUTED TO	R18R22	852.	15.42	338.	119.	40.	6.30
+	HYDROGRAPH AT	R22	794.	12.33	109.	36.	12.	0.57
+	DIVERSION TO	RETR22	794.	12.33	67.	19.	6.	0.57
+	HYDROGRAPH AT	DIVR22	723.	12.42	58.	17.	6.	0.57
+	HYDROGRAPH AT	R14	806.	12.25	101.	34.	11.	0.50
+	DIVERSION TO	RETR14	751.	12.17	59.	17.	6.	0.50
+	HYDROGRAPH AT	DIVR14	746.	12.33	56.	17.	6.	0.50
+	ROUTED TO	R14R17	370.	12.75	55.	17.	6.	0.50
+	HYDROGRAPH AT	R17	497.	12.58	84.	27.	9.	0.49
+	DIVERSION TO	RETR17	497.	12.58	55.	15.	5.	0.49
+	HYDROGRAPH AT	DIVR17	360.	12.75	40.	12.	4.	0.49
+	2 COMBINED AT	CPR17	729.	12.75	94.	28.	9.	0.99
+	ROUTED TO	R17R22	519.	13.08	91.	28.	9.	0.99
+	3 COMBINED AT	CPR22	893.	15.42	444.	157.	53.	7.87
+	ROUTED TO	R22R21	857.	15.67	436.	156.	53.	7.87
+	3 COMBINED AT	CPR21	1519.	15.58	870.	299.	101.	14.65
+	ROUTED TO	R21R25	1466.	15.92	859.	298.	101.	14.65
+	HYDROGRAPH AT	R25	436.	12.25	49.	16.	5.	0.28
+	DIVERSION TO	RETR25	402.	12.17	25.	7.	2.	0.28
+	HYDROGRAPH AT	DIVR25	406.	12.33	30.	8.	3.	0.28
+	HYDROGRAPH AT	R20	562.	12.42	82.	27.	9.	0.50
+	DIVERSION TO	RETR20	562.	12.42	62.	17.	6.	0.50
+	HYDROGRAPH AT	DIVR20	296.	12.67	32.	10.	3.	0.50
+	ROUTED TO	R20R23	141.	13.17	30.	10.	3.	0.50
+	HYDROGRAPH AT	R23	700.	12.33	96.	32.	11.	0.50
+	DIVERSION TO	RETR23	700.	12.33	63.	18.	6.	0.50

+	HYDROGRAPH AT	DIVR23	492.	12.50	47.	14.	5.	0.50
+	2 COMBINED AT	CPR23	492.	12.50	76.	24.	8.	1.00
	ROUTED TO							
+	R23R25	R23R25	282.	12.75	73.	24.	8.	1.00
+	3 COMBINED AT	CPR25	1484.	15.92	912.	321.	108.	15.93
	ROUTED TO							
+	R25R24	R25R24	1484.	15.92	912.	321.	108.	15.93
+	HYDROGRAPH AT	R19	1808.	12.42	302.	101.	34.	1.53
+	DIVERSION TO	RETR19	1808.	12.42	192.	55.	18.	1.53
+	HYDROGRAPH AT	DIVR19	1558.	12.58	156.	46.	15.	1.53
+	DIVERSION TO	DETR19	1387.	12.58	70.	18.	6.	1.53
+	HYDROGRAPH AT	DIV19R	229.	13.17	86.	29.	10.	1.53
	ROUTED TO							
+	R19R24	R19R24	191.	13.83	82.	29.	10.	1.53
+	HYDROGRAPH AT	R24	400.	12.33	55.	18.	6.	0.29
+	DIVERSION TO	RETR24	400.	12.33	35.	10.	3.	0.29
+	HYDROGRAPH AT	DIVR24	305.	12.50	28.	8.	3.	0.29
+	3 COMBINED AT	CPR24	1526.	15.92	982.	349.	117.	17.75
	ROUTED TO							
+	R24EM4	R24EM4	1516.	16.00	980.	349.	117.	17.75
+	HYDROGRAPH AT	EMF4	135.	12.08	8.	2.	1.	0.06
+	3 COMBINED AT	CPEMF4	4083.	14.83	2880.	1015.	345.	55.93

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION E7STOR
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	STORAGE	1566.00	1574.00	1574.00				
	OUTFLOW	0.	607.	607.				
		0.	104.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1567.20	0.00	27.	1.	0.00	25.75	0.00
PLAN 2	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	STORAGE	1566.00	1574.00	1574.00				
	OUTFLOW	0.	607.	607.				
		0.	104.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1567.17	0.00	27.	1.	0.00	25.75	0.00
PLAN 3	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	STORAGE	1566.00	1574.00	1574.00				
	OUTFLOW	0.	607.	607.				
		0.	104.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1567.06	0.00	24.	0.	0.00	26.00	0.00
PLAN 4	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	STORAGE	1566.00	1574.00	1574.00				
	OUTFLOW	0.	607.	607.				
		0.	104.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS

	OF PMF	RESERVOIR W.S.ELEV	DEPTH OVER DAM	STORAGE AC-FT	OUTFLOW CFS	OVER TOP HOURS	MAX OUTFLOW HOURS	FAILURE HOURS
	1.00	1566.91	0.00	21.	0.	0.00	0.00	0.00
PLAN 5		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
		ELEVATION	1566.00	1574.00				
		STORAGE	0.	607.				
		OUTFLOW	0.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.72	0.00	16.	0.	0.00	0.00	0.00
PLAN 6		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
		ELEVATION	1566.00	1574.00				
		STORAGE	0.	607.				
		OUTFLOW	0.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.61	0.00	14.	0.	0.00	0.00	0.00
PLAN 7		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
		ELEVATION	1566.00	1574.00				
		STORAGE	0.	607.				
		OUTFLOW	0.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.53	0.00	12.	0.	0.00	0.00	0.00
PLAN 8		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
		ELEVATION	1566.00	1574.00				
		STORAGE	0.	607.				
		OUTFLOW	0.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.47	0.00	11.	0.	0.00	0.00	0.00
PLAN 9		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
		ELEVATION	1566.00	1574.00				
		STORAGE	0.	607.				
		OUTFLOW	0.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.43	0.00	10.	0.	0.00	0.00	0.00
1		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION RITBAS (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)						
PLAN 1	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	STORAGE	1311.00	1318.00	1318.00				
	OUTFLOW	0.	693.	693.				
		0.	7.	7.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1311.98	0.00	22.	1.	0.00	13.00	0.00
PLAN 2	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	STORAGE	1311.00	1318.00	1318.00				
	OUTFLOW	0.	693.	693.				
		0.	7.	7.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1311.98	0.00	21.	1.	0.00	13.00	0.00
PLAN 3	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	STORAGE	1311.00	1318.00	1318.00				
	OUTFLOW	0.	693.	693.				
		0.	7.	7.				

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1311.95	0.00	21.	1.	0.00	13.00	0.00

PLAN 4	ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	1311.00	1311.00	1318.00	1318.00
	0.	0.	693.	693.
	0.	0.	7.	7.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1311.92	0.00	20.	1.	0.00	13.00	0.00

PLAN 5	ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	1311.00	1311.00	1318.00	1318.00
	0.	0.	693.	693.
	0.	0.	7.	7.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1311.87	0.00	19.	1.	0.00	13.00	0.00

PLAN 6	ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	1311.00	1311.00	1318.00	1318.00
	0.	0.	693.	693.
	0.	0.	7.	7.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1311.85	0.00	19.	1.	0.00	13.00	0.00

PLAN 7	ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	1311.00	1311.00	1318.00	1318.00
	0.	0.	693.	693.
	0.	0.	7.	7.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1311.83	0.00	18.	1.	0.00	12.92	0.00

PLAN 8	ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	1311.00	1311.00	1318.00	1318.00
	0.	0.	693.	693.
	0.	0.	7.	7.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1311.82	0.00	18.	1.	0.00	12.92	0.00

PLAN 9	ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	1311.00	1311.00	1318.00	1318.00
	0.	0.	693.	693.
	0.	0.	7.	7.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1311.81	0.00	18.	1.	0.00	12.92	0.00

*** NORMAL END OF HEC-1 ***

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APPENDIX E
OFF-SITE CHANNEL HYDRAULICS

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Date
 By: F Braileanu 07/04/16
 Checked: A. Islam 07/19/16

SR 24 - Comparison of Hydrology (HEC-1 models) using Concrete-lined Channel Routing

INT(ERIM)C

- SR 24 channel extending to Central Arizona Project (CAP) Canal; drainage condition assuming full interception of watershed runoff North of SR 24 under January 2016 development levels in Maricopa and Pinal Counties.

INT(ERIM) I(RONWOOD)

- SR 24 channel extending to Ironwood Drive; interim phase II drainage condition assuming full interception of the watershed runoff north of SR 24 to Ironwood Drive only, under January 2016 development levels in Maricopa and Pinal Counties.

Major Crossing	2011 DCR (EXST. W/ PROJ) BASELINE				100-YR, 24-HR INT(ERIM)C				INT(ERIM) I(RONWOOD)			
	NODE	Q (cfs)	TP (hrs)	TP (hrs)	NODE	Q (cfs)	TP (hrs)	TP (hrs)	NODE	Q (cfs)	TP (hrs)	TP (hrs)
Powerline Floodway	D79A1	1650	13.08	13.08	802ELS	1650	12.92	12.92	802ELS	1650	13.00	13.00
Ellsworth Road	C79A1	2513	14.58	14.58	SR24EL	2479	14.00	14.00	SR24EL	1788	13.00	13.00
Prop. Williams Field Road	C78E1A	2110	14.50	14.50	CPE27A	2452	13.83	13.83	CPE27A	1549	12.83	12.83
Crismon Road	C78E1	1461	14.33	14.33	E247A1	1630	13.83	13.83	E247A1	652	13.92	13.92
Signal Butte Road	C78D1	1421	14.17	14.17	CP24A	1637	13.67	13.67	CP24A	655	13.75	13.75
Mountain Road	R78F	1392	14.00	14.00	E1424A	1440	13.58	13.58	E1424A	451	13.58	13.58
Meridian Road	C78F	1436	14.00	14.00	CPE14A	1445	13.58	13.58	CPE14A	453	13.50	13.50
Ironwood Road	S78F2	338	13.75	13.75	CPE5A2	1432	13.42	13.42	DE5S	433	13.33	13.33

Required Retention/Detention Volume:
 - 122 ac-ft of effective detention volume at Ellsworth Basin (Ellsworth Road and Powerline Floodway).

Existing Retention/Detention Volume:
 - Approximately 100 ac-ft of detention volume is available (January 2016.) @ Ellsworth Basin (Ellsworth Road and Powerline Floodway) provided in SR 24 Interim Phase I



Date
 By: F Braileanu 07/04/16
 Checked: A. Islam 07/19/16

SR 24 - Comparison of Hydrology (HEC-1 models) using Concrete-lined Channel Routing

INT(ERIM)C

- SR 24 channel extending to Central Arizona Project (CAP) Canal; drainage condition assuming full interception of watershed runoff North of SR 24 under January 2016 development levels in Maricopa and Pinal Counties.

INT(ERIM) I(RONWOOD)

- SR 24 channel extending to Ironwood Drive; interim phase II drainage condition assuming full interception of the watershed runoff north of SR 24 to Ironwood Drive only, under January 2016 development levels in Maricopa and Pinal Counties.

Major Crossing	2011 DCR (EXST. W/ PROJ) BASELINE				50-YR, 24-HR INT(ERIM)C				INT(ERIM) I(RONWOOD)			
	NODE	Q (cfs)	TP (hrs)	TP (hrs)	NODE	Q (cfs)	TP (hrs)	TP (hrs)	NODE	Q (cfs)	TP (hrs)	TP (hrs)
Powerline Floodway	D79A1				802ELS	1650	13.67	13.67	802ELS	1348	13.25	13.25
Ellsworth Road	C79A1				SR24EL	2002	14.08	14.08	SR24EL	1348	13.25	13.25
Prop. Williams Field Road	C78E1A				CPE27A	1977	13.92	13.92	CPE27A	1244	13.00	13.00
Crismon Road	C78E1				E247A1	1329	13.83	13.83	E247A1	536	13.92	13.92
Signal Butte Road	C78D1				CP24A	1335	13.75	13.75	CP24A	538	13.75	13.75
Mountain Road	R78F				E1424A	1173	13.67	13.67	E1424A	367	13.58	13.58
Meridian Road	C78F				CPE14A	1176	13.58	13.58	CPE14A	369	13.50	13.50
Ironwood Road	S78F2				CPE5A2	1166	13.50	13.50	DE5S	354	13.33	13.33

Required Retention/Detention Volume:
 - 122 ac-ft of effective detention volume at Ellsworth Basin (Ellsworth Road and Powerline Floodway).

Existing Retention/Detention Volume:
 - Approximately 100 ac-ft of detention volume is available (January 2016.) @ Ellsworth Basin (Ellsworth Road and Powerline Floodway) provided in SR 24 Interim Phase I

Variables:

Q - Peak Flow
 Tc - Time of Peak



SR 24 - Offsite Channel Options Based on INT Hydrology and ADOT Design Criteria (Concrete-Lined Channel and Gravel Channel)

Date: 7/4/16
By: F Braileanu
Checked: A. Islam

Table with columns: Major Crossing, Ground Elev., Reach Length, Ground Slope, Channel ROW, HEC-1 NODE ID, Design Event, HEC-1 Node Peak Flow, Rounded Qp50, Channel Lining, Lining Thickness, Projected Lining, Slope, Bottom Width, Side Slope, Required Depth, Velocity Head, Froude.

Note 1: Data calculated using Flow Master
Note 1: Projected Lining (Horizontal), ft
Tp = T / sin [tan^-1(1/m)]

Note 2: Velocity Head, Velocity
Velocity Head = V^2 / 2g
V = sqrt(2g * Velocity Head)



SR 24 - Offsite Channel Options Based on INT Hydrology and ADOT Design Criteria (Concrete-Lined Channel and Gravel Channel) (Continue)

Date: 7/4/2016
By: F Braileanu
Checked: A. Islam

Table with columns: Major Crossing, Velocity, Freeboard, Depth + Freeboard, Effective Design Flow Depth, Top Width, Top Width + O&M, Slope Diff. Depth, Max Width from Slope Diff. Depth, ROW Savings, Rounded Qp50, Top of Channel Flow, HEC-1 Node Peak Flow, Flow Capacity Within Freeboard, Estimated Channel Excavation Volume.

Note 3: Freeboard
F = max [1, 0.2 * (v + zc)] if Fr < 0.86
F = 1 if Fr >= 0.86

Note 4: Total Depth, Top Width
Y = Y + F
B = b + 2 * m * Y

Note 6: Maximum Width from Slope Difference Depth
Ws = Z * m * abs[Ss - Sc] * L

Note 8: Estimated Concrete-lined Channel Excavation Volume, cu.yd.
Vexc = VFRISM * VTRIANGULAR PYRAMID + VTRIANGULAR PYRAMID

Note 5: Operation and Maintenance Road
OM = O&M Road Width (15 ft)

Note 7: Right-of-Way Savings
ROWSAVINGS = ROWCHANNEL - (B + OM)

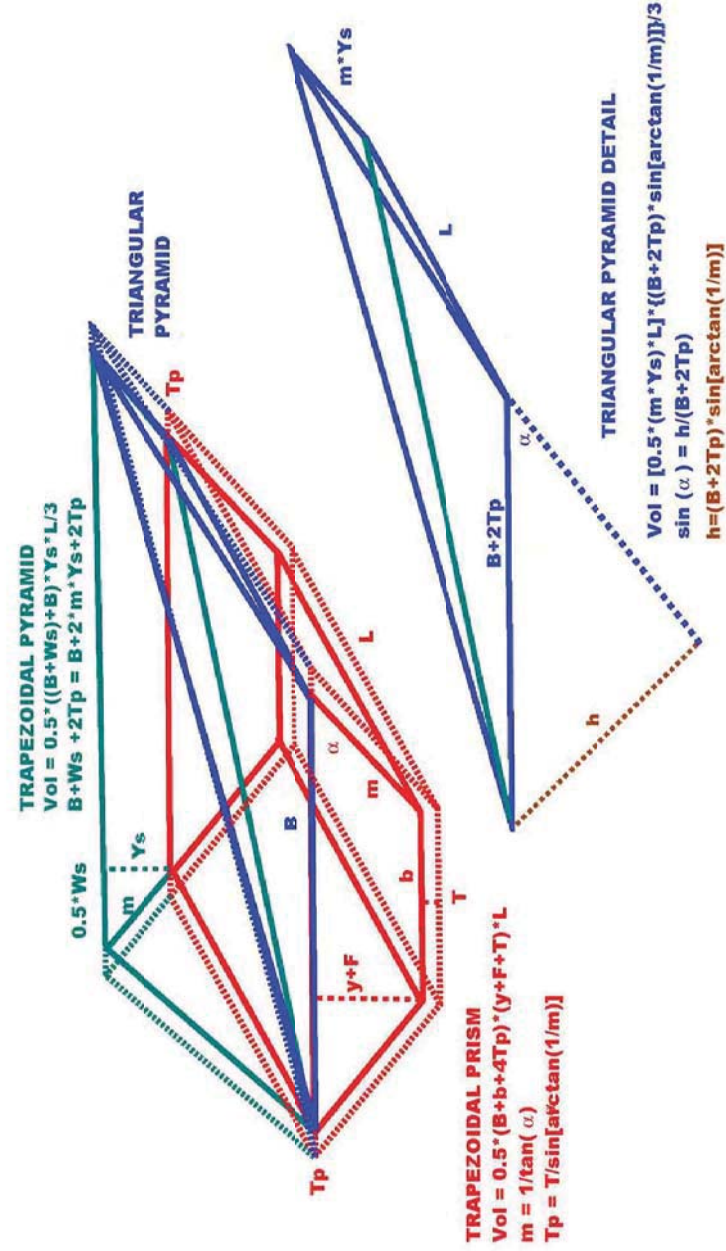
SR 24 - Offsite Channel Right-of-Way Savings, Quantity and Cost of Channel Lining (Concrete Lined Channel)

Date: 7/4/2016
 7/19/2016
 BY: F Bralleanu
 Checked: A. Islam

Major Crossing	Reach Length (ft)	ROW Savings			Gravel Channel (ac)
		Savings (North side) (ft)	Concrete Channel (ac)	Gravel Channel (ac)	
Powerline Floodway	1585	N/A		N/A	
Ellsworth Road	1585	N/A	N/A		
Prop. Williams Field Road	6172	18	7.38	2.55	
	6172	57.1			
Crismon Road	1328	33.9		1.03	
	1328	58	1.77		
Signal Butte Road	5394	35.6		4.41	
	5394	54.7	6.77		
Mountain Road	2261	32.3		1.68	
	2261	46.8	2.43		
Meridian Road	2696	27.7		1.71	
	2696	41	2.54		
Ironwood Road	5929	17.1		2.33	
	5929	36.5	4.97		
TOTAL			25.86	11.16	

Major Crossing	Lining Surface (sq.yd.)	Additional Lining Surface (No Steps) (sq.yd.)	Additional Lining Surface (Steps) (sq.yd.)	Total Lining Surface (No Steps) (sq.yd.)	Total Lining Surface (Steps) (sq.yd.)	Total Lining Cost (No Steps)	Total Lining Cost (Steps)
Powerline Floodway							
Ellsworth Road	10610.56	2284.45		12,900	12,900	\$645,000	\$645,000
Prop. Williams Field Road	36717.24	8328.70		45,050	45,050	\$2,252,500	\$2,252,500
Crismon Road	6719.83	823.75		7,540	7,540	\$377,000	\$377,000
Signal Butte Road	27294.25	33107.76		60,400	32,810	\$3,020,000	\$1,640,500
Mountain Road	10879.17	6909.43		17,790	13,180	\$889,500	\$659,000
Meridian Road	12872.24	11954.74		24,930	15,960	\$1,246,500	\$798,000
Ironwood Road	28528.34	55721.92		84,250	34,720	\$4,212,500	\$1,736,000
TOTAL				252,860	162,160	\$12,643,000	\$8,108,000

Calculation Support - Geometric Breakdown of Channel Volume



Worksheet for Ellsworth-Powerline INT Gravel Sizing S=0.0020

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient 0.035
Channel Slope 0.002000 ft/ft
Left Side Slope 3.00 ft/ft (H:V)
Right Side Slope 3.00 ft/ft (H:V)
Bottom Width 24.00 ft
Discharge 2000 ft³/s

Results

Normal Depth 7.68 ft
Flow Area 361.30 ft²
Wetted Perimeter 72.58 ft
Hydraulic Radius 4.98 ft
Top Width 70.08 ft
Critical Depth 4.86 ft
Critical Slope 0.01219 ft/ft
Velocity 5.54 ft/s
Velocity Head 0.48 ft
Specific Energy 8.16 ft
Froude Number 0.43
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 7.68 ft
Critical Depth 4.86 ft
Channel Slope 0.002000 ft/ft

Worksheet for Ellsworth-Powerline INT Gravel Sizing S=0.0020

GVF Output Data

Critical Slope 0.01219 ft/ft

Worksheet for Ellsworth-Powerline INT Gravel Check S=0.0020

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient 0.035
Channel Slope 0.002000 ft/ft
Normal Depth 8.75 ft
Left Side Slope 3.00 ft/ft (H:V)
Right Side Slope 3.00 ft/ft (H:V)
Bottom Width 24.00 ft

Results

Discharge 2614 ft³/s
Flow Area 439.69 ft²
Wetted Perimeter 79.34 ft
Hydraulic Radius 5.54 ft
Top Width 76.50 ft
Critical Depth 5.64 ft
Critical Slope 0.01173 ft/ft
Velocity 5.95 ft/s
Velocity Head 0.55 ft
Specific Energy 9.30 ft
Froude Number 0.44
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 8.75 ft
Critical Depth 5.64 ft
Channel Slope 0.002000 ft/ft

Worksheet for Ellsworth-Powerline INT Gravel Check S=0.0020

GVF Output Data

Critical Slope 0.01173 ft/ft

Worksheet for Ellsworth-Powerline INT Concrete Sizing S=0.00069

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient 0.016
Channel Slope 0.000698 ft/ft
Left Side Slope 2.00 ft/ft (H:V)
Right Side Slope 2.00 ft/ft (H:V)
Bottom Width 20.00 ft
Discharge 2000 ft³/s

Results

Normal Depth 7.78 ft
Flow Area 276.88 ft²
Wetted Perimeter 54.81 ft
Hydraulic Radius 5.05 ft
Top Width 51.14 ft
Critical Depth 5.58 ft
Critical Slope 0.00252 ft/ft
Velocity 7.22 ft/s
Velocity Head 0.81 ft
Specific Energy 8.60 ft
Froude Number 0.55
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 7.78 ft
Critical Depth 5.58 ft
Channel Slope 0.000698 ft/ft

Worksheet for Ellsworth-Powerline INT Concrete Sizing S=0.00069

GVF Output Data

Critical Slope 0.00252 ft/ft

Worksheet for Ellsworth-Powerline INT Concrete Check S=0.00069

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient 0.016
Channel Slope 0.000698 ft/ft
Normal Depth 9.00 ft
Left Side Slope 2.00 ft/ft (H:V)
Right Side Slope 2.00 ft/ft (H:V)
Bottom Width 20.00 ft

Results

Discharge 2670 ft³/s
Flow Area 342.00 ft²
Wetted Perimeter 60.25 ft
Hydraulic Radius 5.68 ft
Top Width 56.00 ft
Critical Depth 6.56 ft
Critical Slope 0.00243 ft/ft
Velocity 7.81 ft/s
Velocity Head 0.95 ft
Specific Energy 9.95 ft
Froude Number 0.56
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 9.00 ft
Critical Depth 6.56 ft
Channel Slope 0.000698 ft/ft

Worksheet for Ellsworth-Powerline INT Concrete Check S=0.00069

GVF Output Data

Critical Slope 0.00243 ft/ft

Worksheet for Williams Field-Ellsworth INT Gravel Sizing S=0.0020

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.035
Channel Slope	0.002000 ft/ft
Left Side Slope	4.00 ft/ft (H:V)
Right Side Slope	4.00 ft/ft (H:V)
Bottom Width	24.00 ft
Discharge	2000 ft ³ /s

Results

Normal Depth	7.23 ft
Flow Area	382.31 ft ²
Wetted Perimeter	83.59 ft
Hydraulic Radius	4.57 ft
Top Width	81.81 ft
Critical Depth	4.62 ft
Critical Slope	0.01239 ft/ft
Velocity	5.23 ft/s
Velocity Head	0.43 ft
Specific Energy	7.65 ft
Froude Number	0.43
Flow Type	Subcritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	7.23 ft
Critical Depth	4.62 ft
Channel Slope	0.002000 ft/ft

Worksheet for Williams Field-Ellsworth INT Gravel Sizing S=0.0020

GVF Output Data

Critical Slope	0.01239 ft/ft
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Worksheet for Williams Field-Ellsworth INT Gravel Check S=0.0020

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient 0.035
Channel Slope 0.002000 ft/ft
Normal Depth 8.25 ft
Left Side Slope 4.00 ft/ft (H:V)
Right Side Slope 4.00 ft/ft (H:V)
Bottom Width 24.00 ft

Results

Discharge 2649 ft³/s
Flow Area 470.25 ft²
Wetted Perimeter 92.03 ft
Hydraulic Radius 5.11 ft
Top Width 90.00 ft
Critical Depth 5.37 ft
Critical Slope 0.01190 ft/ft
Velocity 5.63 ft/s
Velocity Head 0.49 ft
Specific Energy 8.74 ft
Froude Number 0.43
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 8.25 ft
Critical Depth 5.37 ft
Channel Slope 0.002000 ft/ft

Worksheet for Williams Field-Ellsworth INT Gravel Check S=0.0020

GVF Output Data

Critical Slope 0.01190 ft/ft

Worksheet for Williams Field-Ellsworth INT Concrete Sizing S=0.0015

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient 0.016
Channel Slope 0.001500 ft/ft
Left Side Slope 2.00 ft/ft (H:V)
Right Side Slope 2.00 ft/ft (H:V)
Bottom Width 20.00 ft
Discharge 2000 ft³/s

Results

Normal Depth 6.40 ft
Flow Area 209.77 ft²
Wetted Perimeter 48.61 ft
Hydraulic Radius 4.32 ft
Top Width 45.59 ft
Critical Depth 5.58 ft
Critical Slope 0.00252 ft/ft
Velocity 9.53 ft/s
Velocity Head 1.41 ft
Specific Energy 7.81 ft
Froude Number 0.78
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 6.40 ft
Critical Depth 5.58 ft
Channel Slope 0.001500 ft/ft

Worksheet for Williams Field-Ellsworth INT Concrete Sizing S=0.0015

GVF Output Data

Critical Slope 0.00252 ft/ft

Worksheet for Williams Field-Ellsworth INT Concrete Check S=0.0015

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient 0.016
Channel Slope 0.001500 ft/ft
Normal Depth 7.50 ft
Left Side Slope 2.00 ft/ft (H:V)
Right Side Slope 2.00 ft/ft (H:V)
Bottom Width 20.00 ft

Results

Discharge 2725 ft³/s
Flow Area 262.50 ft²
Wetted Perimeter 53.54 ft
Hydraulic Radius 4.90 ft
Top Width 50.00 ft
Critical Depth 6.63 ft
Critical Slope 0.00242 ft/ft
Velocity 10.38 ft/s
Velocity Head 1.67 ft
Specific Energy 9.17 ft
Froude Number 0.80
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 7.50 ft
Critical Depth 6.63 ft
Channel Slope 0.001500 ft/ft

Worksheet for Williams Field-Ellsworth INT Concrete Check S=0.0015

GVF Output Data

Critical Slope 0.00242 ft/ft

Worksheet for Crimson-Williams Field INT Gravel Sizing S=0.0020

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient 0.035
Channel Slope 0.002000 ft/ft
Left Side Slope 3.00 ft/ft (H:V)
Right Side Slope 3.00 ft/ft (H:V)
Bottom Width 12.00 ft
Discharge 1350 ft³/s

Results

Normal Depth 7.60 ft
Flow Area 264.62 ft²
Wetted Perimeter 60.08 ft
Hydraulic Radius 4.40 ft
Top Width 57.61 ft
Critical Depth 4.96 ft
Critical Slope 0.01275 ft/ft
Velocity 5.10 ft/s
Velocity Head 0.40 ft
Specific Energy 8.01 ft
Froude Number 0.42
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 7.60 ft
Critical Depth 4.96 ft
Channel Slope 0.002000 ft/ft

Worksheet for Crimson-Williams Field INT Gravel Sizing S=0.0020

GVF Output Data

Critical Slope 0.01275 ft/ft

Worksheet for Crimson-Williams Field INT Gravel Check S=0.0020

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient 0.035
Channel Slope 0.002000 ft/ft
Normal Depth 8.75 ft
Left Side Slope 3.00 ft/ft (H:V)
Right Side Slope 3.00 ft/ft (H:V)
Bottom Width 12.00 ft

Results

Discharge 1851 ft³/s
Flow Area 334.69 ft²
Wetted Perimeter 67.34 ft
Hydraulic Radius 4.97 ft
Top Width 64.50 ft
Critical Depth 5.81 ft
Critical Slope 0.01222 ft/ft
Velocity 5.53 ft/s
Velocity Head 0.48 ft
Specific Energy 9.23 ft
Froude Number 0.43
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 8.75 ft
Critical Depth 5.81 ft
Channel Slope 0.002000 ft/ft

Worksheet for Crimson-Williams Field INT Gravel Check S=0.0020

GVF Output Data

Critical Slope 0.01222 ft/ft

Worksheet for Crismon-Williams Field INT Concrete Sizing S=0.0017

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.016
Channel Slope	0.001700 ft/ft
Left Side Slope	2.00 ft/ft (H:V)
Right Side Slope	2.00 ft/ft (H:V)
Bottom Width	12.00 ft
Discharge	1350 ft ³ /s

Results

Normal Depth	6.06 ft
Flow Area	146.32 ft ²
Wetted Perimeter	39.12 ft
Hydraulic Radius	3.74 ft
Top Width	36.26 ft
Critical Depth	5.43 ft
Critical Slope	0.00266 ft/ft
Velocity	9.23 ft/s
Velocity Head	1.32 ft
Specific Energy	7.39 ft
Froude Number	0.81
Flow Type	Subcritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	6.06 ft
Critical Depth	5.43 ft
Channel Slope	0.001700 ft/ft

Worksheet for Crismon-Williams Field INT Concrete Sizing S=0.0017

GVF Output Data

Critical Slope 0.00266 ft/ft

Worksheet for Crismon-Williams Field INT Concrete Check S=0.0017

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient 0.016
Channel Slope 0.001700 ft/ft
Normal Depth 7.50 ft
Left Side Slope 2.00 ft/ft (H:V)
Right Side Slope 2.00 ft/ft (H:V)
Bottom Width 12.00 ft

Results

Discharge 2097 ft³/s
Flow Area 202.50 ft²
Wetted Perimeter 45.54 ft
Hydraulic Radius 4.45 ft
Top Width 42.00 ft
Critical Depth 6.83 ft
Critical Slope 0.00252 ft/ft
Velocity 10.35 ft/s
Velocity Head 1.67 ft
Specific Energy 9.17 ft
Froude Number 0.83
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 7.50 ft
Critical Depth 6.83 ft
Channel Slope 0.001700 ft/ft

Worksheet for Crismon-Williams Field INT Concrete Check S=0.0017

GVF Output Data

Critical Slope 0.00252 ft/ft

Worksheet for Signal Butte-Crimson INT Gravel Sizing S=0.0037

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient 0.035
Channel Slope 0.003700 ft/ft
Left Side Slope 3.00 ft/ft (H:V)
Right Side Slope 3.00 ft/ft (H:V)
Bottom Width 12.00 ft
Discharge 1350 ft³/s

Results

Normal Depth 6.61 ft
Flow Area 210.56 ft²
Wetted Perimeter 53.83 ft
Hydraulic Radius 3.91 ft
Top Width 51.68 ft
Critical Depth 4.96 ft
Critical Slope 0.01275 ft/ft
Velocity 6.41 ft/s
Velocity Head 0.64 ft
Specific Energy 7.25 ft
Froude Number 0.56
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 6.61 ft
Critical Depth 4.96 ft
Channel Slope 0.003700 ft/ft

Worksheet for Signal Butte-Crimson INT Gravel Sizing S=0.0037

GVF Output Data

Critical Slope 0.01275 ft/ft

Worksheet for Signal Butte-Crimson INT Gravel Check S=0.0037

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient 0.035
Channel Slope 0.003700 ft/ft
Normal Depth 7.75 ft
Left Side Slope 3.00 ft/ft (H:V)
Right Side Slope 3.00 ft/ft (H:V)
Bottom Width 12.00 ft

Results

Discharge 1916 ft³/s
Flow Area 273.19 ft²
Wetted Perimeter 61.02 ft
Hydraulic Radius 4.48 ft
Top Width 58.50 ft
Critical Depth 5.91 ft
Critical Slope 0.01217 ft/ft
Velocity 7.02 ft/s
Velocity Head 0.76 ft
Specific Energy 8.51 ft
Froude Number 0.57
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 7.75 ft
Critical Depth 5.91 ft
Channel Slope 0.003700 ft/ft

Worksheet for Signal Butte-Crimson INT Gravel Check S=0.0037

GVF Output Data

Critical Slope 0.01217 ft/ft

Worksheet for Signal Butte-Crismon INT Concrete Sizing S=0.0017

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient 0.016
Channel Slope 0.001700 ft/ft
Left Side Slope 2.00 ft/ft (H:V)
Right Side Slope 2.00 ft/ft (H:V)
Bottom Width 12.00 ft
Discharge 1350 ft³/s

Results

Normal Depth 6.06 ft
Flow Area 146.32 ft²
Wetted Perimeter 39.12 ft
Hydraulic Radius 3.74 ft
Top Width 36.26 ft
Critical Depth 5.43 ft
Critical Slope 0.00266 ft/ft
Velocity 9.23 ft/s
Velocity Head 1.32 ft
Specific Energy 7.39 ft
Froude Number 0.81
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 6.06 ft
Critical Depth 5.43 ft
Channel Slope 0.001700 ft/ft

Worksheet for Signal Butte-Crismon INT Concrete Sizing S=0.0017

GVF Output Data

Critical Slope 0.00266 ft/ft

Worksheet for Mountain-Signal Butte INT Gravel Sizing S=0.0040

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient 0.035
Channel Slope 0.004000 ft/ft
Left Side Slope 3.00 ft/ft (H:V)
Right Side Slope 3.00 ft/ft (H:V)
Bottom Width 12.00 ft
Discharge 1200 ft³/s

Results

Normal Depth 6.15 ft
Flow Area 187.46 ft²
Wetted Perimeter 50.92 ft
Hydraulic Radius 3.68 ft
Top Width 48.92 ft
Critical Depth 4.67 ft
Critical Slope 0.01296 ft/ft
Velocity 6.40 ft/s
Velocity Head 0.64 ft
Specific Energy 6.79 ft
Froude Number 0.58
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 6.15 ft
Critical Depth 4.67 ft
Channel Slope 0.004000 ft/ft

Worksheet for Mountain-Signal Butte INT Gravel Sizing S=0.0040

GVF Output Data

Critical Slope 0.01296 ft/ft

Worksheet for Mountain-Signal Butte INT Gravel Check S=0.0040

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient 0.035
Channel Slope 0.004000 ft/ft
Normal Depth 7.25 ft
Left Side Slope 3.00 ft/ft (H:V)
Right Side Slope 3.00 ft/ft (H:V)
Bottom Width 12.00 ft

Results

Discharge 1718 ft³/s
Flow Area 244.69 ft²
Wetted Perimeter 57.85 ft
Hydraulic Radius 4.23 ft
Top Width 55.50 ft
Critical Depth 5.60 ft
Critical Slope 0.01234 ft/ft
Velocity 7.02 ft/s
Velocity Head 0.77 ft
Specific Energy 8.02 ft
Froude Number 0.59
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 7.25 ft
Critical Depth 5.60 ft
Channel Slope 0.004000 ft/ft

Worksheet for Mountain-Signal Butte INT Gravel Check S=0.0040

GVF Output Data

Critical Slope 0.01234 ft/ft

Worksheet for Mountain-Signal Butte INT Concrete Sizing S=0.0017

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient 0.016
Channel Slope 0.001700 ft/ft
Left Side Slope 2.00 ft/ft (H:V)
Right Side Slope 2.00 ft/ft (H:V)
Bottom Width 12.00 ft
Discharge 1200 ft³/s

Results

Normal Depth 5.72 ft
Flow Area 134.18 ft²
Wetted Perimeter 37.59 ft
Hydraulic Radius 3.57 ft
Top Width 34.89 ft
Critical Depth 5.10 ft
Critical Slope 0.00270 ft/ft
Velocity 8.94 ft/s
Velocity Head 1.24 ft
Specific Energy 6.97 ft
Froude Number 0.80
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 5.72 ft
Critical Depth 5.10 ft
Channel Slope 0.001700 ft/ft

Worksheet for Mountain-Signal Butte INT Concrete Sizing S=0.0017

GVF Output Data

Critical Slope 0.00270 ft/ft

Worksheet for Mountain-Signal Butte INT Concrete Check S=0.0017

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient 0.016
Channel Slope 0.001700 ft/ft
Normal Depth 7.00 ft
Left Side Slope 2.00 ft/ft (H:V)
Right Side Slope 2.00 ft/ft (H:V)
Bottom Width 12.00 ft

Results

Discharge 1815 ft³/s
Flow Area 182.00 ft²
Wetted Perimeter 43.30 ft
Hydraulic Radius 4.20 ft
Top Width 40.00 ft
Critical Depth 6.34 ft
Critical Slope 0.00256 ft/ft
Velocity 9.97 ft/s
Velocity Head 1.55 ft
Specific Energy 8.55 ft
Froude Number 0.82
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 7.00 ft
Critical Depth 6.34 ft
Channel Slope 0.001700 ft/ft

Worksheet for Mountain-Signal Butte INT Concrete Check S=0.0017

GVF Output Data

Critical Slope 0.00256 ft/ft

Worksheet for Meridian-Mountain INT Gravel Sizing S=0.0045

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient 0.035
Channel Slope 0.004500 ft/ft
Left Side Slope 3.00 ft/ft (H:V)
Right Side Slope 3.00 ft/ft (H:V)
Bottom Width 12.00 ft
Discharge 1200 ft³/s

Results

Normal Depth 5.99 ft
Flow Area 179.45 ft²
Wetted Perimeter 49.87 ft
Hydraulic Radius 3.60 ft
Top Width 47.93 ft
Critical Depth 4.67 ft
Critical Slope 0.01296 ft/ft
Velocity 6.69 ft/s
Velocity Head 0.69 ft
Specific Energy 6.68 ft
Froude Number 0.61
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 5.99 ft
Critical Depth 4.67 ft
Channel Slope 0.004500 ft/ft

Worksheet for Meridian-Mountain INT Gravel Sizing S=0.0045

GVF Output Data

Critical Slope 0.01296 ft/ft

Worksheet for Meridian-Mountain INT Gravel Check S=0.0045

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient 0.035
Channel Slope 0.004500 ft/ft
Normal Depth 7.00 ft
Left Side Slope 3.00 ft/ft (H:V)
Right Side Slope 3.00 ft/ft (H:V)
Bottom Width 12.00 ft

Results

Discharge 1687 ft³/s
Flow Area 231.00 ft²
Wetted Perimeter 56.27 ft
Hydraulic Radius 4.11 ft
Top Width 54.00 ft
Critical Depth 5.54 ft
Critical Slope 0.01238 ft/ft
Velocity 7.30 ft/s
Velocity Head 0.83 ft
Specific Energy 7.83 ft
Froude Number 0.62
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 7.00 ft
Critical Depth 5.54 ft
Channel Slope 0.004500 ft/ft

Worksheet for Meridian-Mountain INT Gravel Check S=0.0045

GVF Output Data

Critical Slope 0.01238 ft/ft

Worksheet for Meridian-Mountain INT Concrete Sizing S=0.0017

Project Description

Friction Method Manning Formula
 Solve For Normal Depth

Input Data

Roughness Coefficient 0.016
 Channel Slope 0.001700 ft/ft
 Left Side Slope 2.00 ft/ft (H:V)
 Right Side Slope 2.00 ft/ft (H:V)
 Bottom Width 12.00 ft
 Discharge 1200 ft³/s

Results

Normal Depth 5.72 ft
 Flow Area 134.18 ft²
 Wetted Perimeter 37.59 ft
 Hydraulic Radius 3.57 ft
 Top Width 34.89 ft
 Critical Depth 5.10 ft
 Critical Slope 0.00270 ft/ft
 Velocity 8.94 ft/s
 Velocity Head 1.24 ft
 Specific Energy 6.97 ft
 Froude Number 0.80
 Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
 Length 0.00 ft
 Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
 Profile Description
 Profile Headloss 0.00 ft
 Downstream Velocity Infinity ft/s
 Upstream Velocity Infinity ft/s
 Normal Depth 5.72 ft
 Critical Depth 5.10 ft
 Channel Slope 0.001700 ft/ft

Worksheet for Meridian-Mountain INT Concrete Sizing S=0.0017

GVF Output Data

Critical Slope 0.00270 ft/ft

Worksheet for Meridian-Mountain INT Concrete Check S=0.0017

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient	0.016	
Channel Slope	0.001700	ft/ft
Normal Depth	7.00	ft
Left Side Slope	2.00	ft/ft (H:V)
Right Side Slope	2.00	ft/ft (H:V)
Bottom Width	12.00	ft

Results

Discharge	1815	ft³/s
Flow Area	182.00	ft²
Wetted Perimeter	43.30	ft
Hydraulic Radius	4.20	ft
Top Width	40.00	ft
Critical Depth	6.34	ft
Critical Slope	0.00256	ft/ft
Velocity	9.97	ft/s
Velocity Head	1.55	ft
Specific Energy	8.55	ft
Froude Number	0.82	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	7.00	ft
Critical Depth	6.34	ft
Channel Slope	0.001700	ft/ft

Worksheet for Meridian-Mountain INT Concrete Check S=0.0017

GVF Output Data

Critical Slope 0.00256 ft/ft

Worksheet for Ironwood-Meridian INT Gravel Sizing S=0.0045

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient 0.035
Channel Slope 0.004500 ft/ft
Left Side Slope 3.00 ft/ft (H:V)
Right Side Slope 3.00 ft/ft (H:V)
Bottom Width 12.00 ft
Discharge 1200 ft³/s

Results

Normal Depth 5.99 ft
Flow Area 179.45 ft²
Wetted Perimeter 49.87 ft
Hydraulic Radius 3.60 ft
Top Width 47.93 ft
Critical Depth 4.67 ft
Critical Slope 0.01296 ft/ft
Velocity 6.69 ft/s
Velocity Head 0.69 ft
Specific Energy 6.68 ft
Froude Number 0.61
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 5.99 ft
Critical Depth 4.67 ft
Channel Slope 0.004500 ft/ft

Worksheet for Ironwood-Meridian INT Gravel Sizing S=0.0045

GVF Output Data

Critical Slope 0.01296 ft/ft

Worksheet for Ironwood-Meridian INT Gravel Check S=0.0045

Project Description

Friction Method	Manning Formula
Solve For	Discharge

Input Data

Roughness Coefficient	0.035
Channel Slope	0.004500 ft/ft
Normal Depth	7.00 ft
Left Side Slope	3.00 ft/ft (H:V)
Right Side Slope	3.00 ft/ft (H:V)
Bottom Width	12.00 ft

Results

Discharge	1687 ft ³ /s
Flow Area	231.00 ft ²
Wetted Perimeter	56.27 ft
Hydraulic Radius	4.11 ft
Top Width	54.00 ft
Critical Depth	5.54 ft
Critical Slope	0.01238 ft/ft
Velocity	7.30 ft/s
Velocity Head	0.83 ft
Specific Energy	7.83 ft
Froude Number	0.62
Flow Type	Subcritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	7.00 ft
Critical Depth	5.54 ft
Channel Slope	0.004500 ft/ft

Worksheet for Ironwood-Meridian INT Gravel Check S=0.0045

GVF Output Data

Critical Slope	0.01238 ft/ft
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Worksheet for Ironwood-Meridian INT Concrete Sizing S=0.0017

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.016
Channel Slope	0.001700 ft/ft
Left Side Slope	2.00 ft/ft (H:V)
Right Side Slope	2.00 ft/ft (H:V)
Bottom Width	12.00 ft
Discharge	1200 ft ³ /s

Results

Normal Depth	5.72 ft
Flow Area	134.18 ft ²
Wetted Perimeter	37.59 ft
Hydraulic Radius	3.57 ft
Top Width	34.89 ft
Critical Depth	5.10 ft
Critical Slope	0.00270 ft/ft
Velocity	8.94 ft/s
Velocity Head	1.24 ft
Specific Energy	6.97 ft
Froude Number	0.80
Flow Type	Subcritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	5.72 ft
Critical Depth	5.10 ft
Channel Slope	0.001700 ft/ft

Worksheet for Ironwood-Meridian INT Concrete Sizing S=0.0017

GVF Output Data

Critical Slope	0.00270 ft/ft
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Worksheet for Ironwood-Meridian INT Concrete Check S=0.0017

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient 0.016
Channel Slope 0.001700 ft/ft
Normal Depth 7.00 ft
Left Side Slope 2.00 ft/ft (H:V)
Right Side Slope 2.00 ft/ft (H:V)
Bottom Width 12.00 ft

Results

Discharge 1815 ft³/s
Flow Area 182.00 ft²
Wetted Perimeter 43.30 ft
Hydraulic Radius 4.20 ft
Top Width 40.00 ft
Critical Depth 6.34 ft
Critical Slope 0.00256 ft/ft
Velocity 9.97 ft/s
Velocity Head 1.55 ft
Specific Energy 8.55 ft
Froude Number 0.82
Flow Type Subcritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 7.00 ft
Critical Depth 6.34 ft
Channel Slope 0.001700 ft/ft

Worksheet for Ironwood-Meridian INT Concrete Check S=0.0017

GVF Output Data

Critical Slope 0.00256 ft/ft

Worksheet for Powerline Floodway INT Concrete Sizing S=0.00456

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient 0.016
Channel Slope 0.00450 ft/ft
Left Side Slope 2.00 ft/ft (H:V)
Right Side Slope 2.00 ft/ft (H:V)
Bottom Width 55.00 ft
Discharge 4400.00 ft³/s

Results

Normal Depth 4.50 ft
Flow Area 288.22 ft²
Wetted Perimeter 75.14 ft
Hydraulic Radius 3.84 ft
Top Width 73.01 ft
Critical Depth 5.45 ft
Critical Slope 0.00233 ft/ft
Velocity 15.27 ft/s
Velocity Head 3.62 ft
Specific Energy 8.12 ft
Froude Number 1.35
Flow Type Supercritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 4.50 ft
Critical Depth 5.45 ft
Channel Slope 0.00450 ft/ft

Worksheet for Powerline Floodway INT Concrete Sizing S=0.00456

GVF Output Data

Critical Slope 0.00233 ft/ft

Worksheet for Powerline Floodway INT Concrete Check S=0.00456

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient 0.016
Channel Slope 0.00450 ft/ft
Normal Depth 8.00 ft
Left Side Slope 2.00 ft/ft (H:V)
Right Side Slope 2.00 ft/ft (H:V)
Bottom Width 55.00 ft

Results

Discharge 12015.57 ft³/s
Flow Area 568.00 ft²
Wetted Perimeter 90.78 ft
Hydraulic Radius 6.26 ft
Top Width 87.00 ft
Critical Depth 10.03 ft
Critical Slope 0.00200 ft/ft
Velocity 21.15 ft/s
Velocity Head 6.95 ft
Specific Energy 14.95 ft
Froude Number 1.46
Flow Type Supercritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Downstream Velocity Infinity ft/s
Upstream Velocity Infinity ft/s
Normal Depth 8.00 ft
Critical Depth 10.03 ft
Channel Slope 0.00450 ft/ft

Worksheet for Powerline Floodway INT Concrete Check S=0.00456

GVF Output Data

Critical Slope 0.00200 ft/ft

Rating Curve for Powerline Floodway INT Concrete Check S=0.00456

Project Description

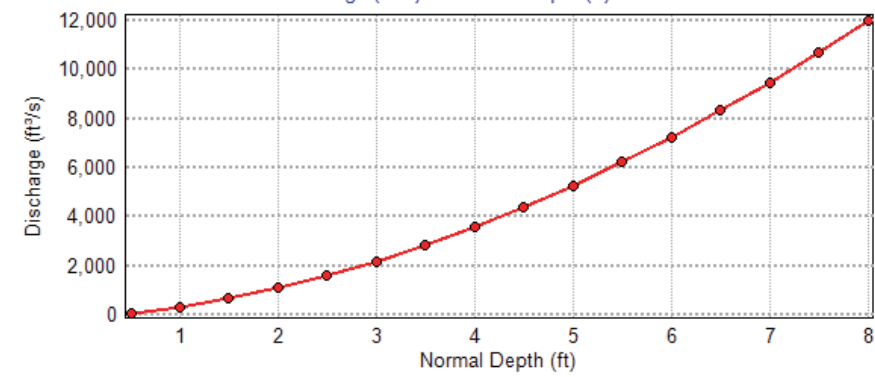
Friction Method Manning Formula
Solve For Discharge

Input Data

Roughness Coefficient 0.016
Channel Slope 0.00450 ft/ft
Normal Depth 8.00 ft
Left Side Slope 2.00 ft/ft (H:V)
Right Side Slope 2.00 ft/ft (H:V)
Bottom Width 55.00 ft

Rating Curve Plot

Worksheet: Powerline Floodway INT Concrete Check S=0.00456
Discharge (ft³/s) vs Normal Depth (ft)

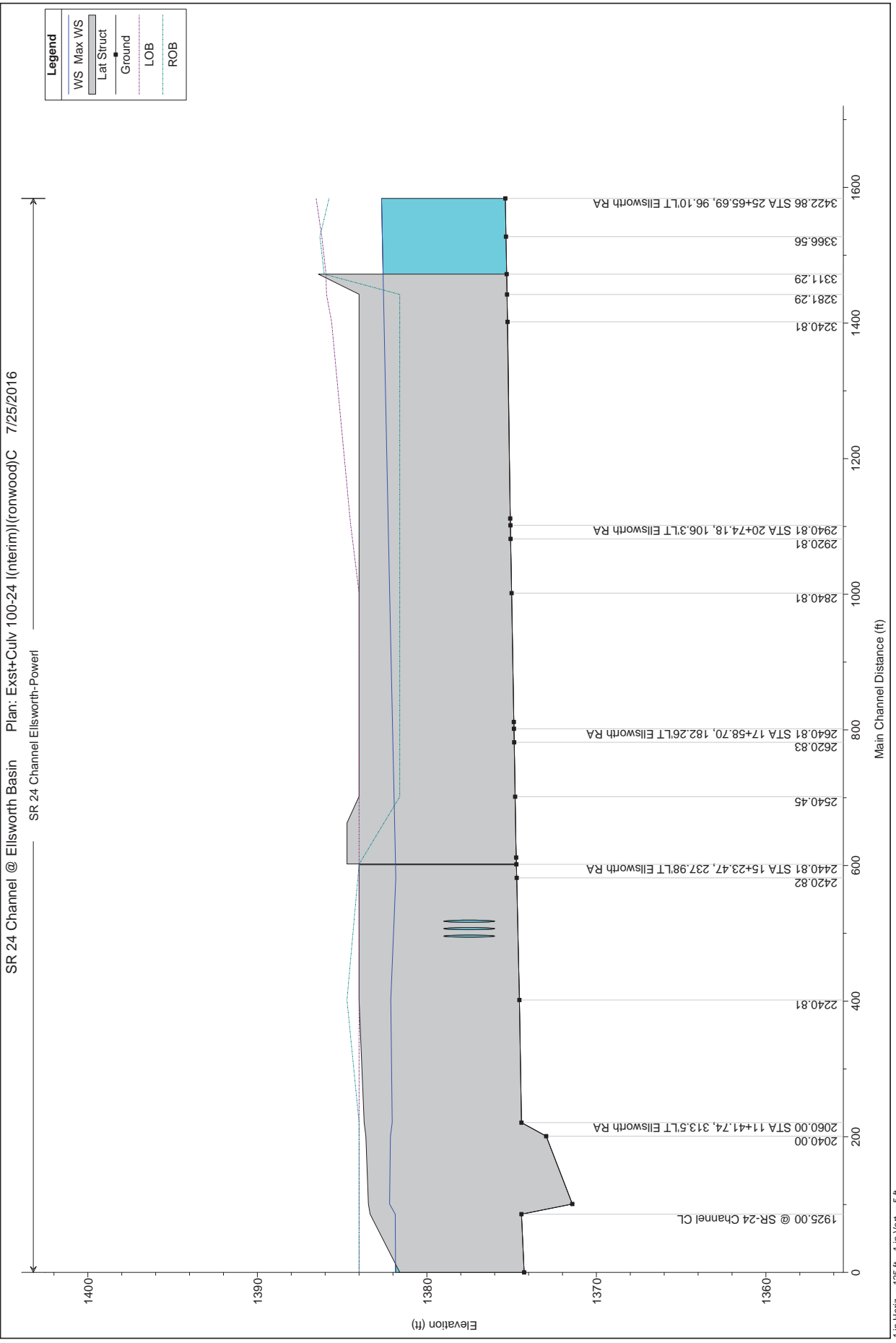
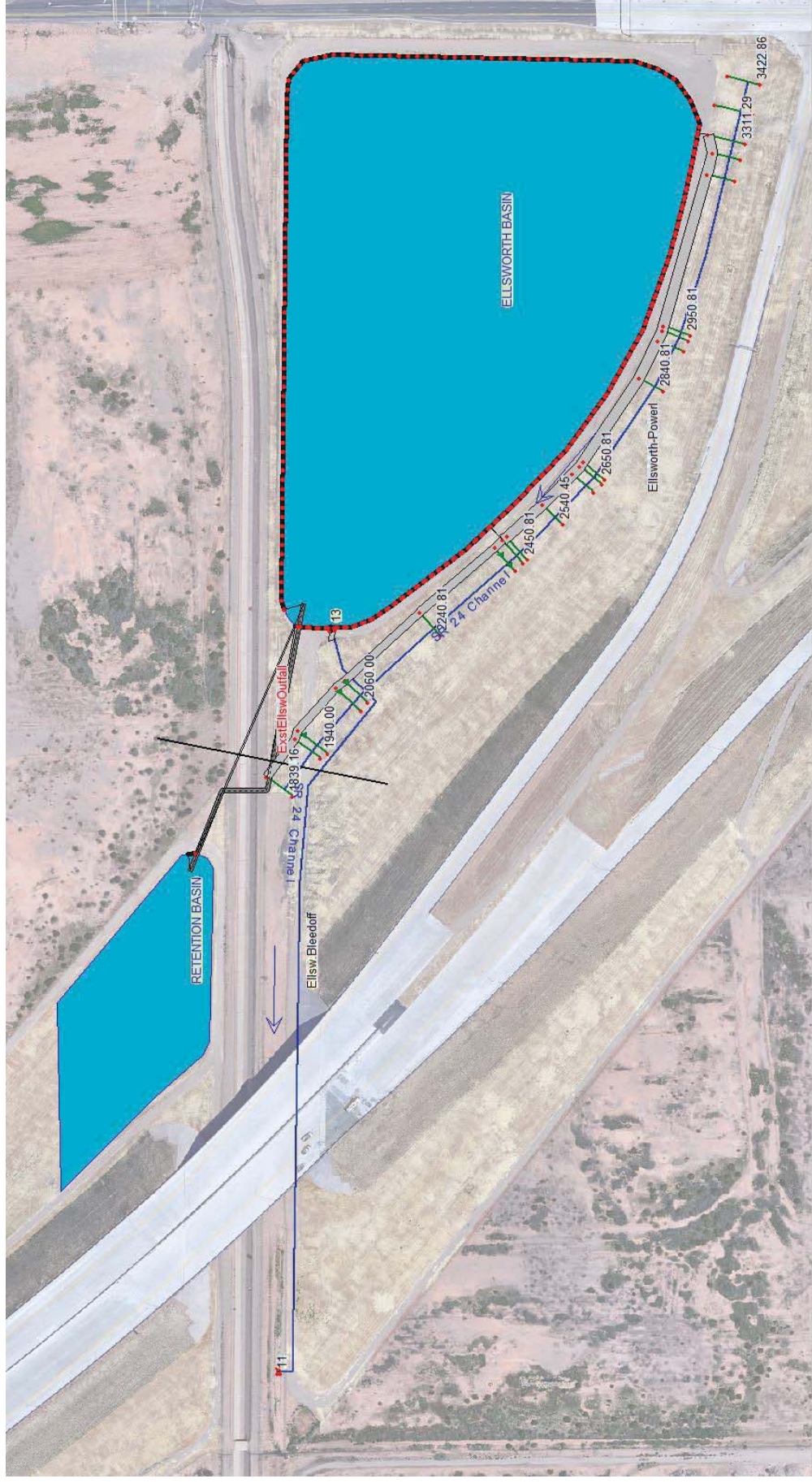


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APPENDIX F
RETENTION BASIN CALCULATIONS

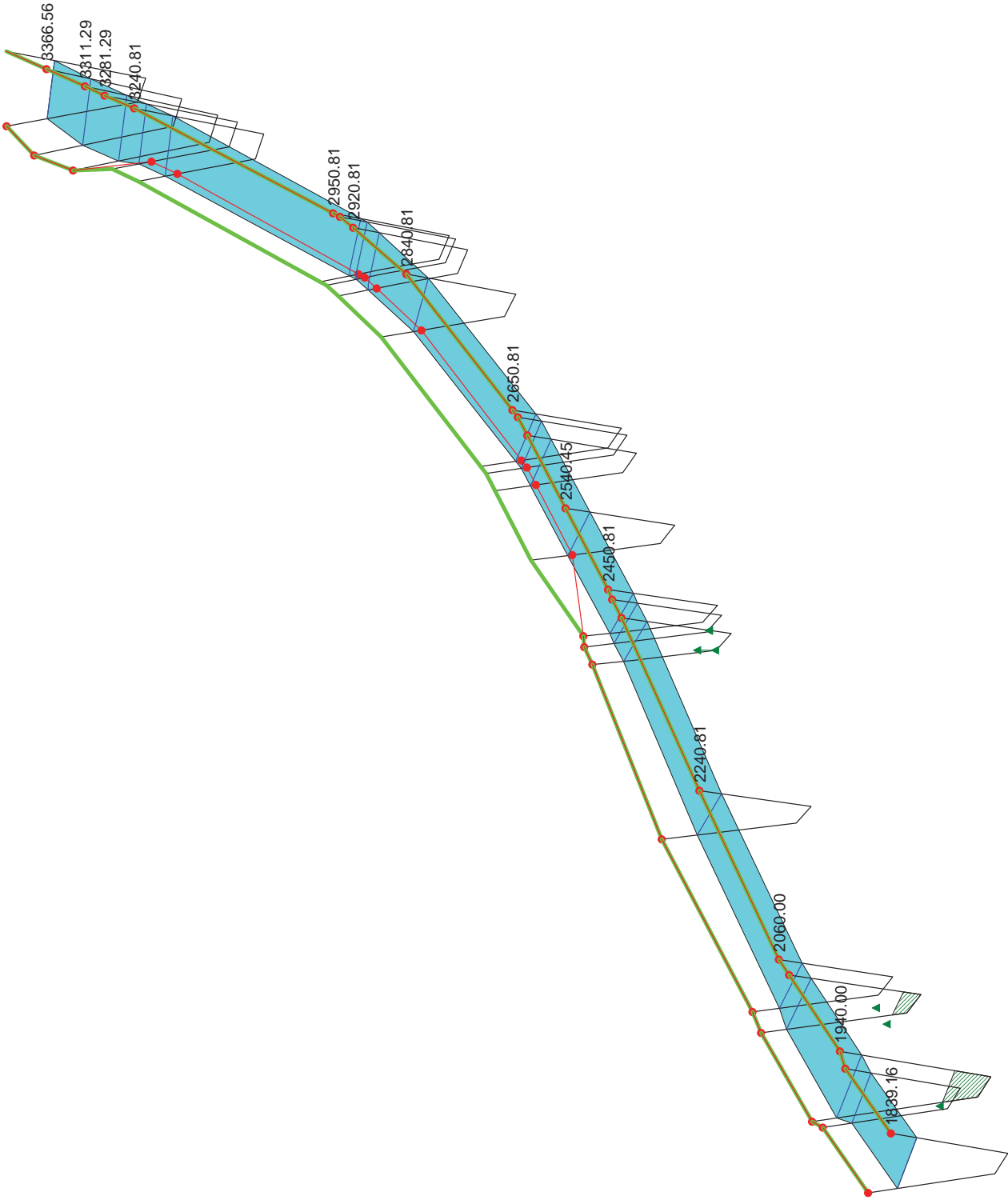
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GEOMETRY LAYOUT: EXST Basin+Culvert+LowFlow



1 in Horiz. = 125 ft 1 in Vert. = 5 ft

SR 24 Channel @ Ellsworth Basin Plan: Exst+Culv 100-24 (nterim)(ronwood)C 7/25/2016

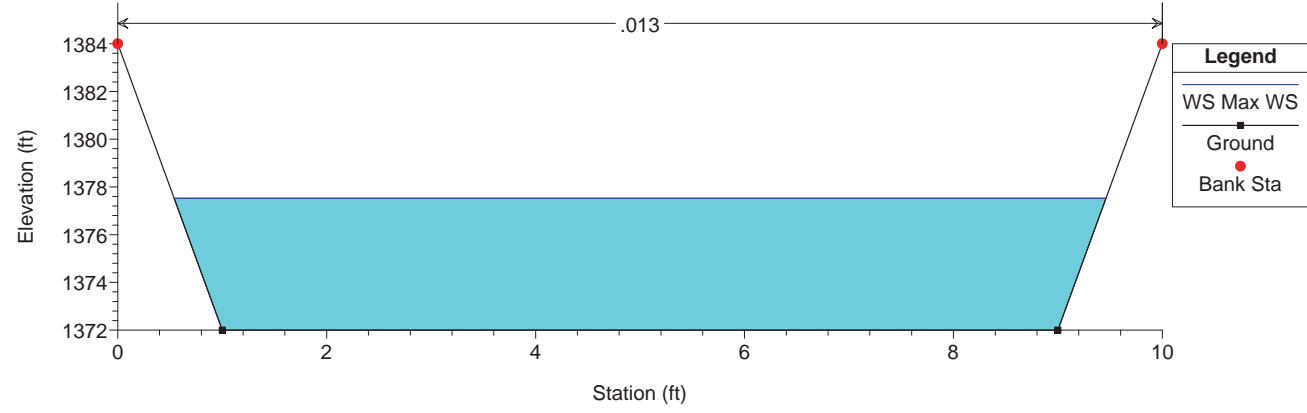


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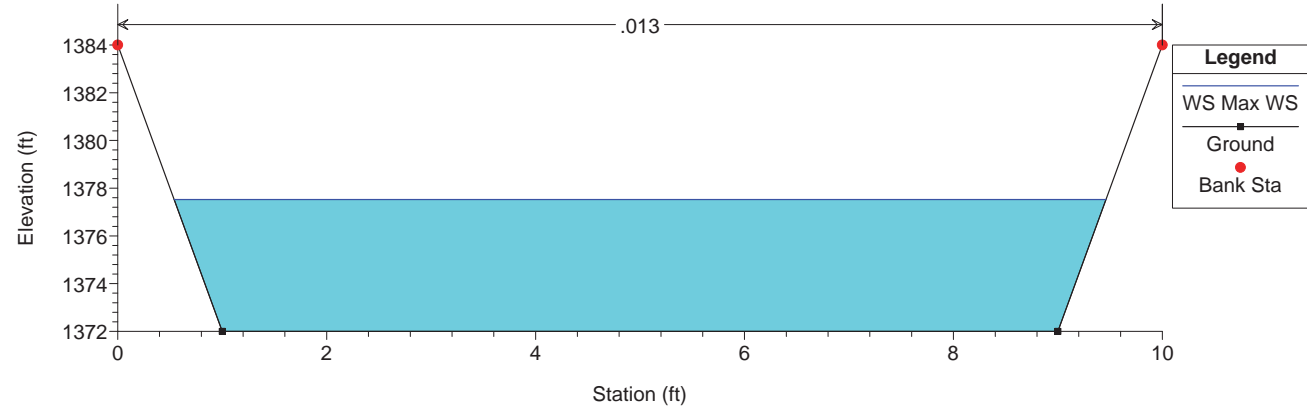
Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	F# Chl
Ellsw.Bleedoff	13	Max WS	39.06	1372.00	1377.53		1377.54	0.000016	0.84	46.74	8.92	0.06
Ellsw.Bleedoff	12	Max WS	39.06	1372.00	1377.53	1372.90	1377.54	0.000016	0.84	46.74	8.92	0.06
Ellsw.Bleedoff	12	Inl Struct										
Ellsw.Bleedoff	11	Max WS	20.07	1368.20	1372.71		1372.72	0.000008	0.53	37.55	8.64	0.05
Ellsw.Bleedoff	10	Max WS	6.07	1368.20	1372.70	1368.46	1372.70	0.000001	0.16	37.45	8.64	0.01
Ellsworth-Powerl	3423	Max WS	1752.00	1375.37	1382.67		1383.48	0.000767	7.21	243.00	48.41	0.57
Ellsworth-Powerl	3367	Max WS	1751.29	1375.33	1382.63		1383.44	0.000767	7.21	242.85	48.40	0.57
Ellsworth-Powerl	3311	Max WS	1750.72	1375.29	1382.59		1383.40	0.000767	7.21	242.80	48.39	0.57
Ellsworth-Powerl	3311	Lat Struct										
Ellsworth-Powerl	3281	Max WS	1750.83	1375.27	1382.56		1383.37	0.000737	7.25	242.37	48.36	0.56
Ellsworth-Powerl	3241	Max WS	1750.60	1375.24	1382.53		1383.35	0.000737	7.24	242.42	48.36	0.56
Ellsworth-Powerl	2951	Max WS	1749.88	1375.08	1382.28		1383.12	0.000781	7.36	238.16	48.01	0.57
Ellsworth-Powerl	2941	Max WS	1749.76	1375.07	1382.27		1383.11	0.000781	7.36	238.22	48.01	0.57
Ellsworth-Powerl	2921	Max WS	1749.81	1375.06	1382.26		1383.10	0.000783	7.36	238.01	47.99	0.58
Ellsworth-Powerl	2841	Max WS	1755.04	1375.00	1382.19		1383.04	0.000793	7.39	237.74	47.97	0.58
Ellsworth-Powerl	2651	Max WS	1754.72	1374.87	1382.03		1382.89	0.000812	7.43	236.31	47.85	0.58
Ellsworth-Powerl	2641	Max WS	1754.69	1374.86	1382.02		1382.88	0.000812	7.43	236.30	47.85	0.58
Ellsworth-Powerl	2621	Max WS	1754.75	1374.85	1382.01		1382.87	0.000816	7.44	236.00	47.85	0.59
Ellsworth-Powerl	2540	Max WS	1755.01	1374.79	1381.94		1382.80	0.000824	7.45	235.53	47.80	0.59
Ellsworth-Powerl	2451	Max WS	1755.01	1374.73	1381.86		1382.73	0.000849	7.48	234.52	47.70	0.60
Ellsworth-Powerl	2441	Max WS	1755.42	1374.72	1381.85		1382.72	0.000848	7.48	234.59	47.71	0.59
Ellsworth-Powerl	2440	Lat Struct										
Ellsworth-Powerl	2421	Max WS	1755.26	1374.70	1381.83		1382.70	0.000846	7.48	234.72	47.69	0.59
Ellsworth-Powerl	2241	Max WS	1527.89	1374.54	1382.13		1382.68	0.000501	5.95	256.59	49.43	0.46
Ellsworth-Powerl	2060	Max WS	1528.01	1374.42	1382.04		1382.59	0.000492	5.92	258.21	49.54	0.46
Ellsworth-Powerl	2040	Max WS	1527.99	1372.96	1382.15		1382.53	0.000315	4.95	308.83	55.02	0.37
Ellsworth-Powerl	1940	Max WS	1527.98	1371.42	1382.20		1382.47	0.000216	4.20	363.55	62.30	0.31
Ellsworth-Powerl	1925	Max WS	1528.00	1374.42	1381.86		1382.45	0.000540	6.12	249.88	48.97	0.48
Ellsworth-Powerl	1839	Max WS	1526.78	1374.26	1381.84	1379.23	1382.39	0.000500	5.95	256.76	49.53	0.46

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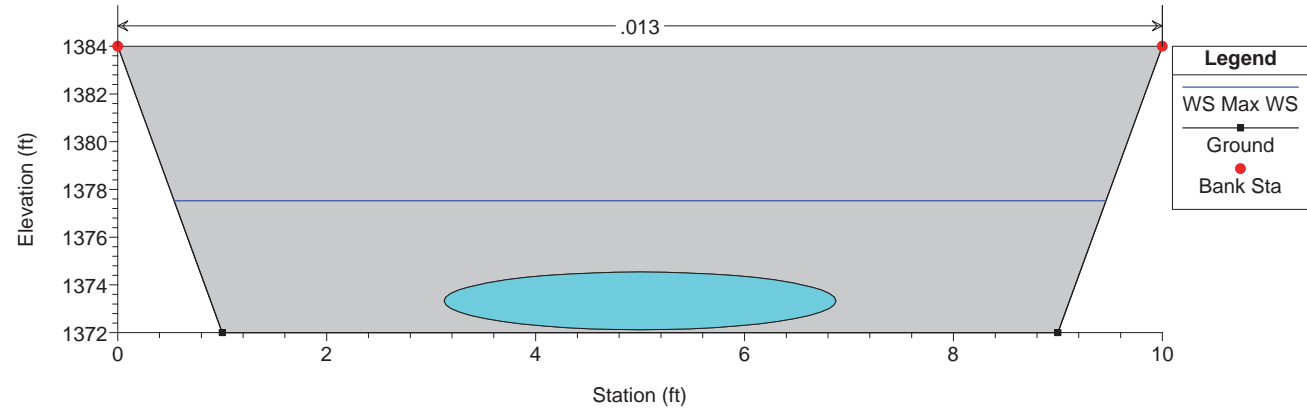
SR 24 Channel @ Ellsworth Basin Plan: Exst+Culv 100-24 I(nterim)I(ronwood)C 7/25/2016
 River = SR 24 Channel Reach = Ellsw.Bleedoff RS = 13 Dummy cross section to simulate the 36" bleedoff line outfall to



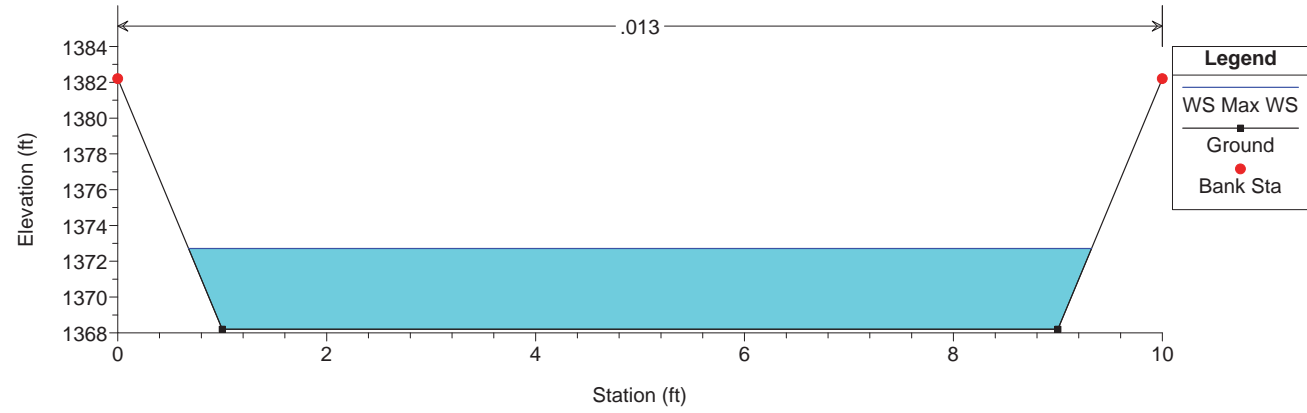
SR 24 Channel @ Ellsworth Basin Plan: Exst+Culv 100-24 I(nterim)I(ronwood)C 7/25/2016
 River = SR 24 Channel Reach = Ellsw.Bleedoff RS = 12 Dummy cross section to simulate the 36" bleedoff line outfall to



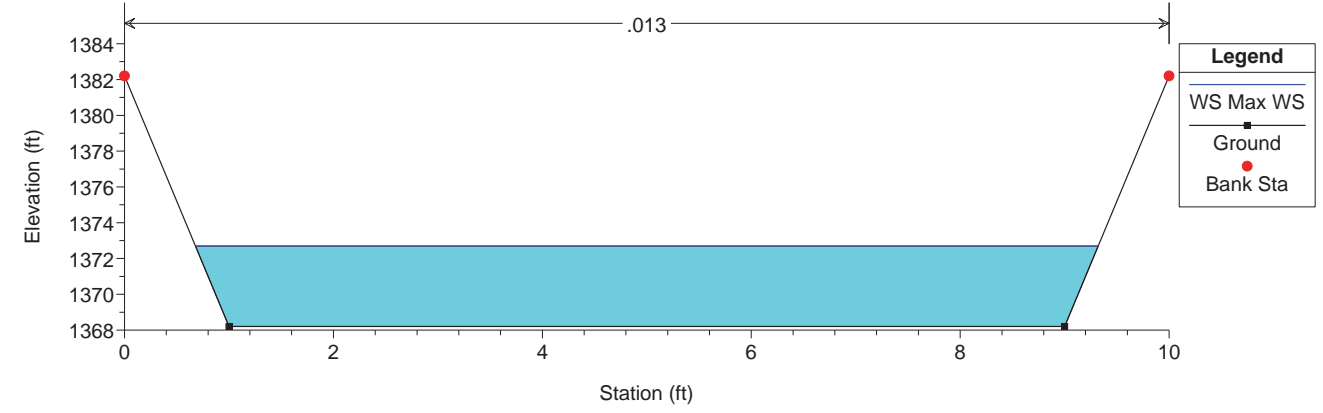
SR 24 Channel @ Ellsworth Basin Plan: Exst+Culv 100-24 I(nterim)I(ronwood)C 7/25/2016
 River = SR 24 Channel Reach = Ellsw.Bleedoff RS = 11.999 IS Proposed 36" RCP bleedoff pipe for the Ellsworth Basin that cross



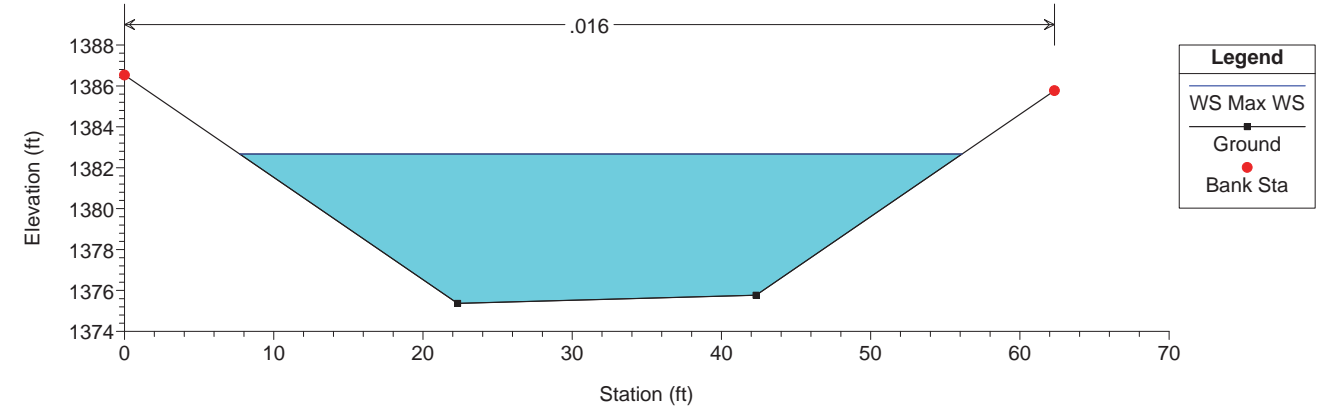
SR 24 Channel @ Ellsworth Basin Plan: Exst+Culv 100-24 I(nterim)I(ronwood)C 7/25/2016
 River = SR 24 Channel Reach = Ellsw.Bleedoff RS = 11 Dummy cross section to simulate the 36" bleedoff line outfall to



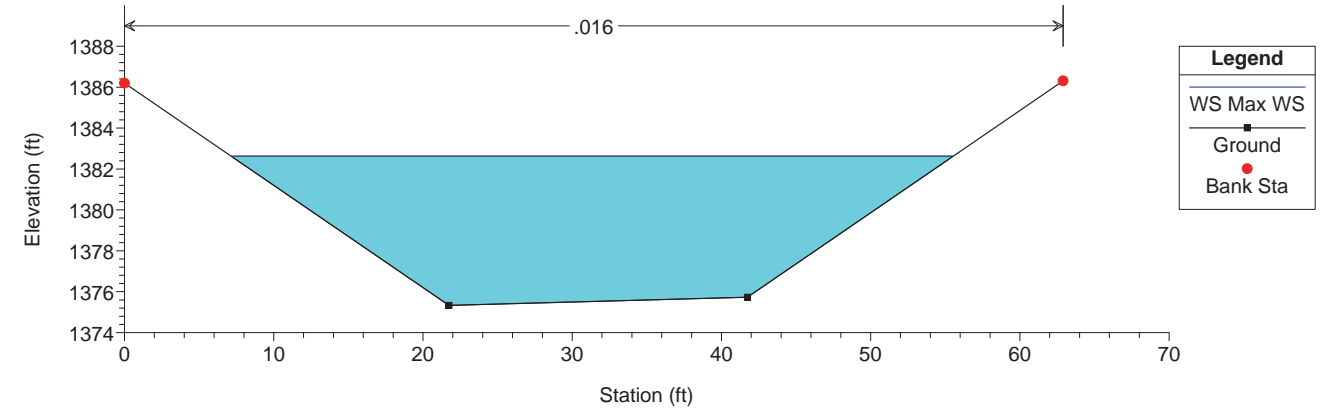
SR 24 Channel @ Ellsworth Basin Plan: Exst+Culv 100-24 I(nterim)I(ronwood)C 7/25/2016
 River = SR 24 Channel Reach = Ellsw.Bleedoff RS = 10 Dummy cross section to simulate the 36" bleedoff line outfall to



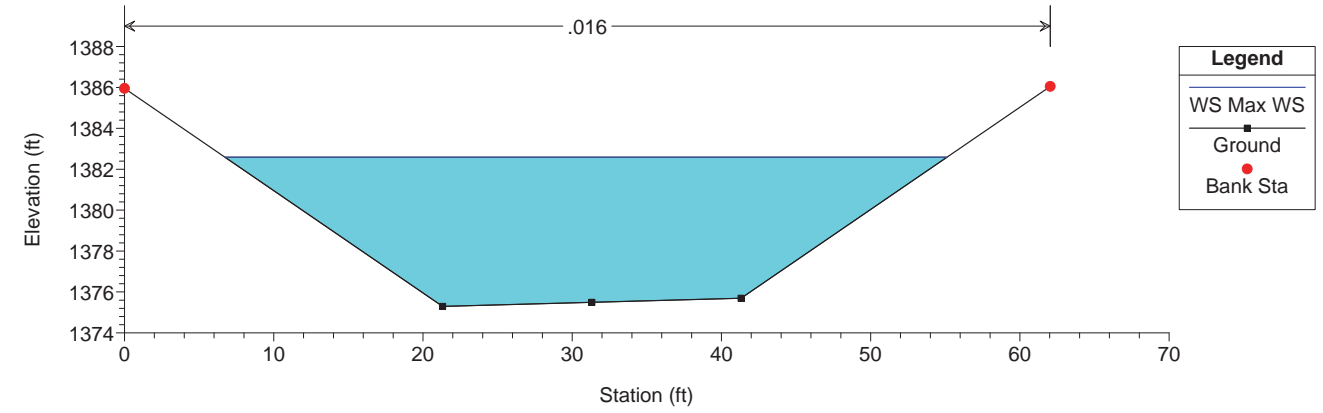
SR 24 Channel @ Ellsworth Basin Plan: Exst+Culv 100-24 I(nterim)I(ronwood)C 7/25/2016
 River = SR 24 Channel Reach = Ellsworth-Powerl RS = 3422.86 STA 25+65.69, 96.10'LT Ellsworth RA

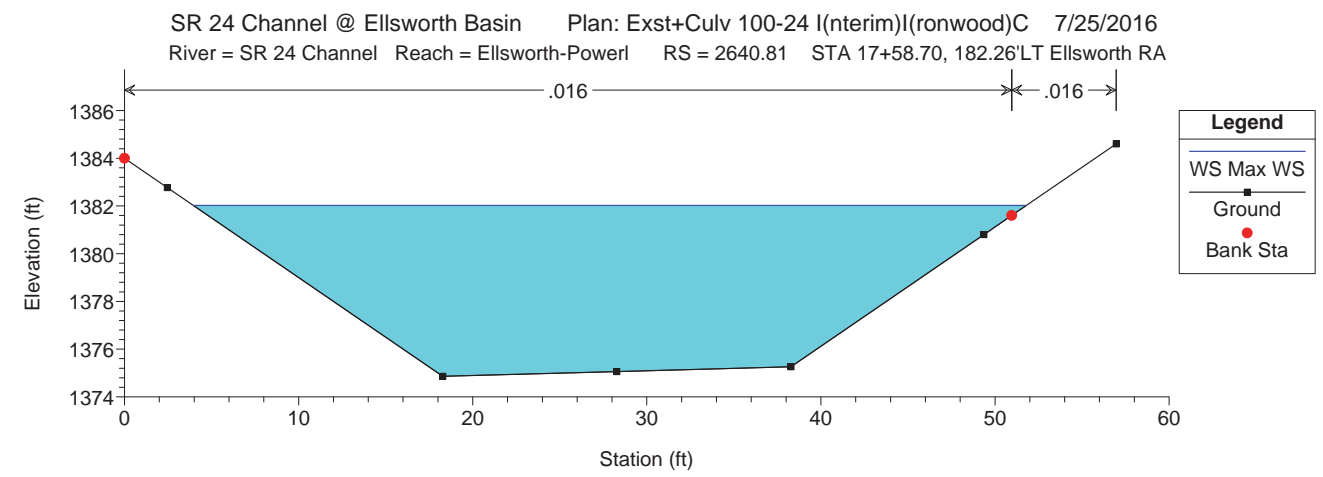
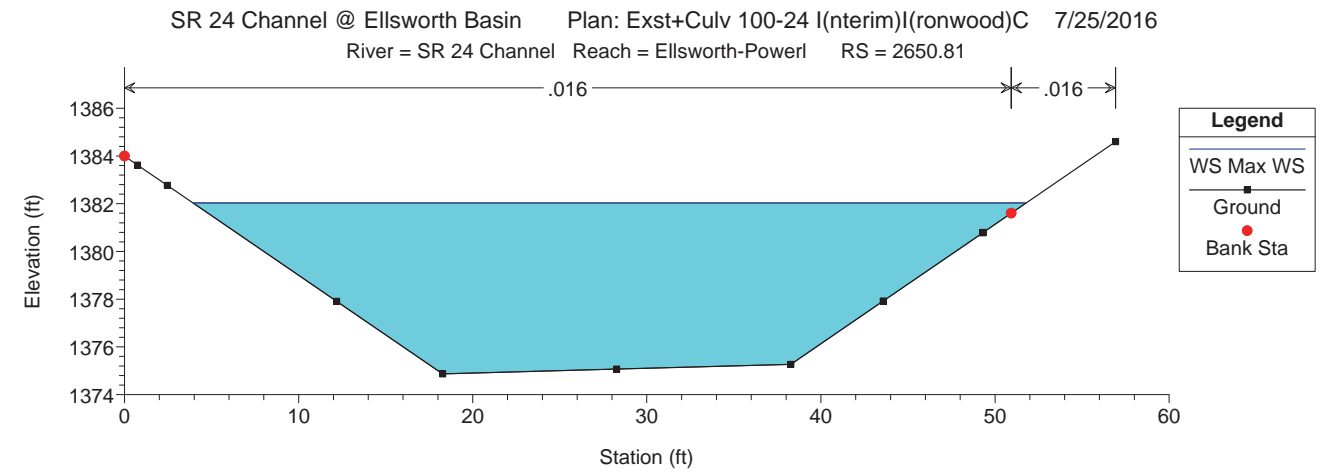
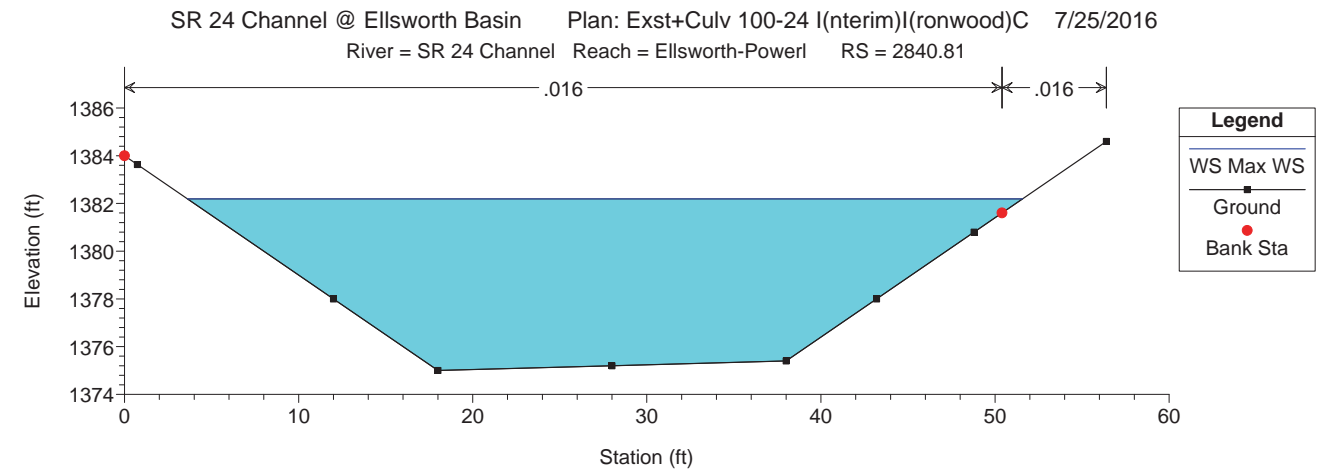
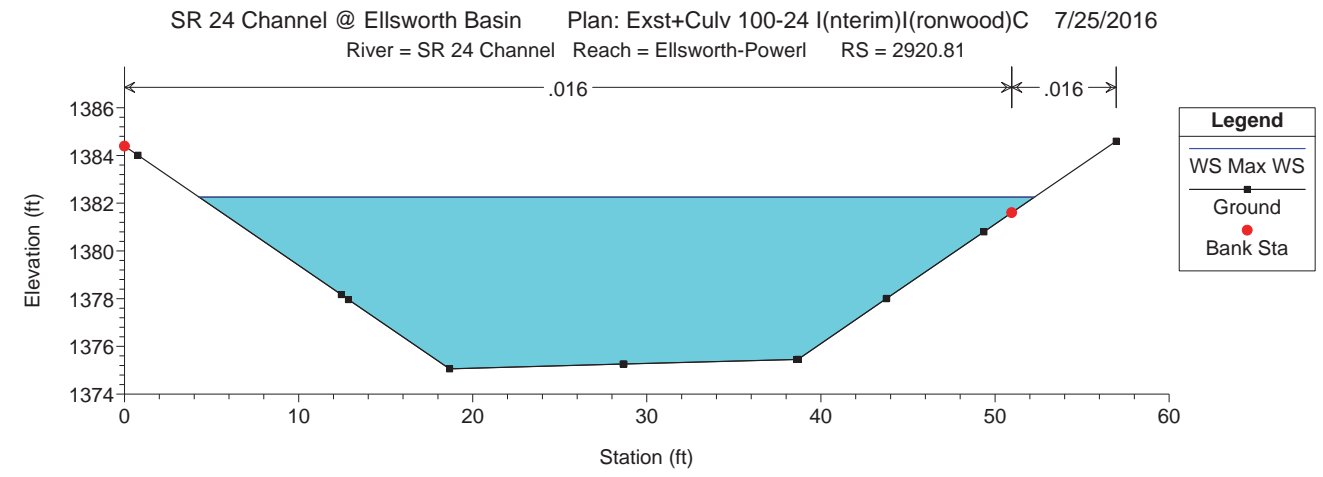
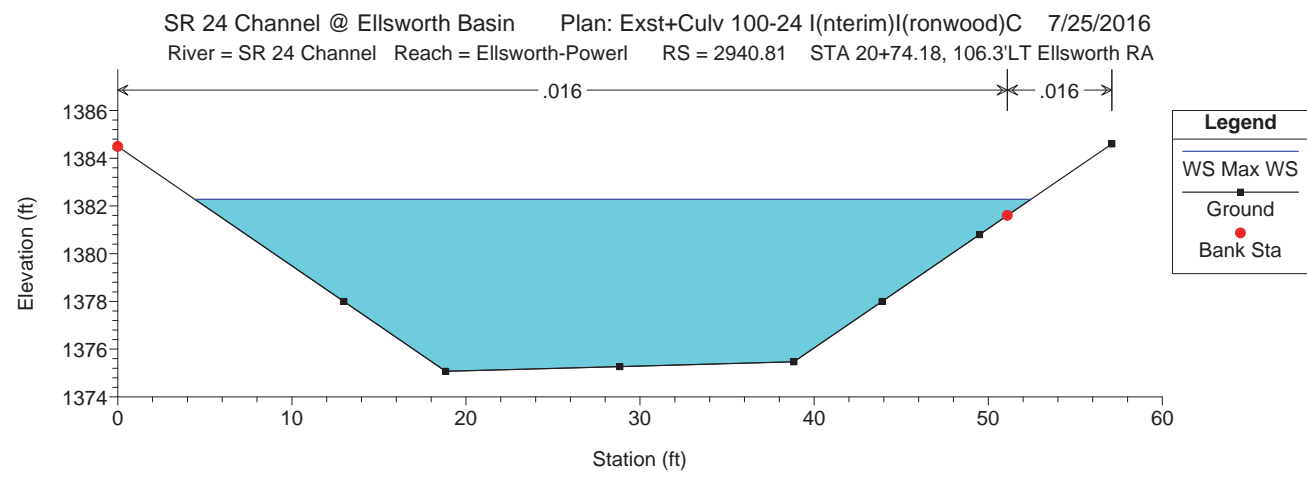
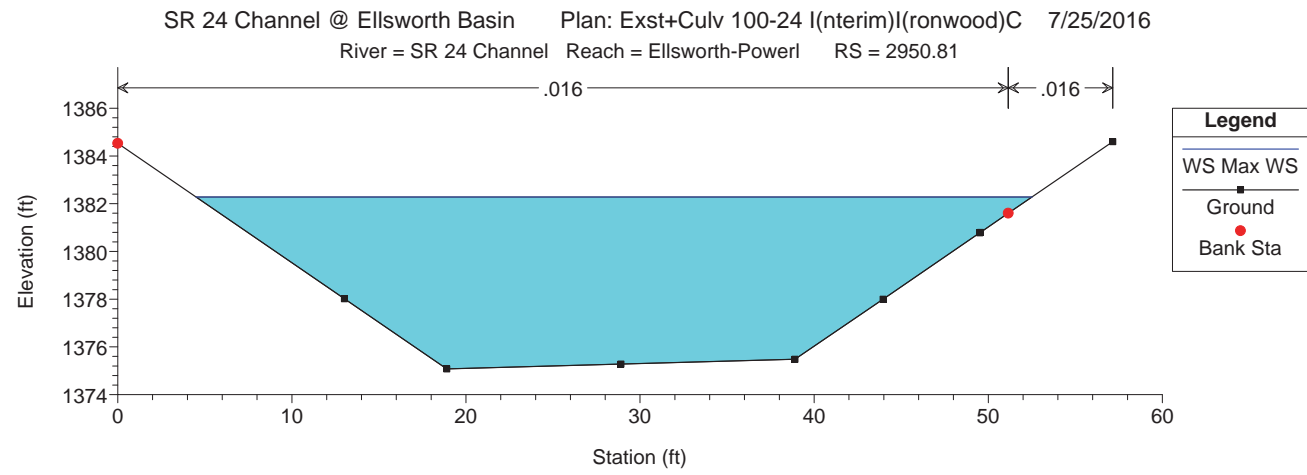
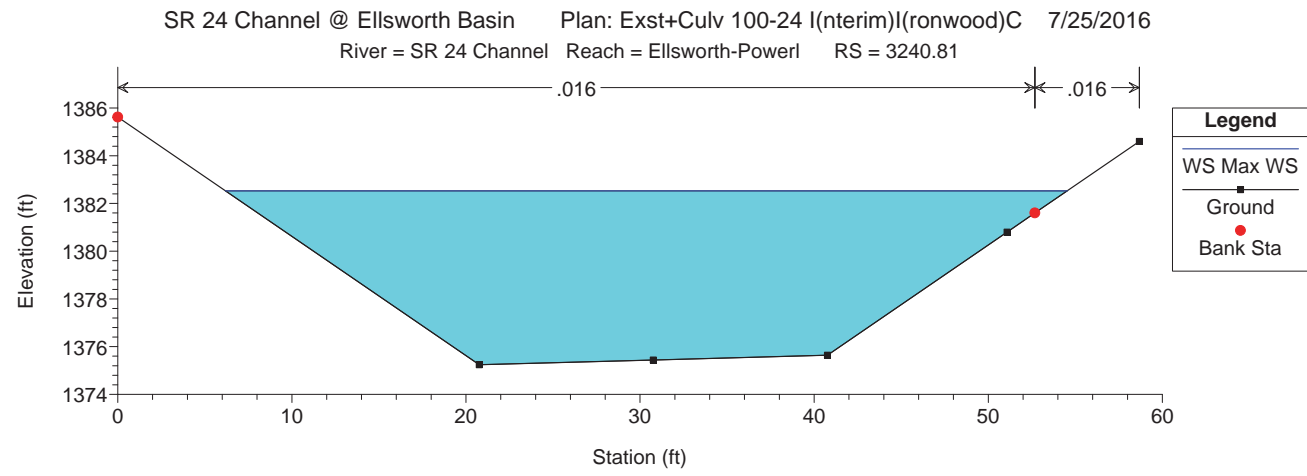
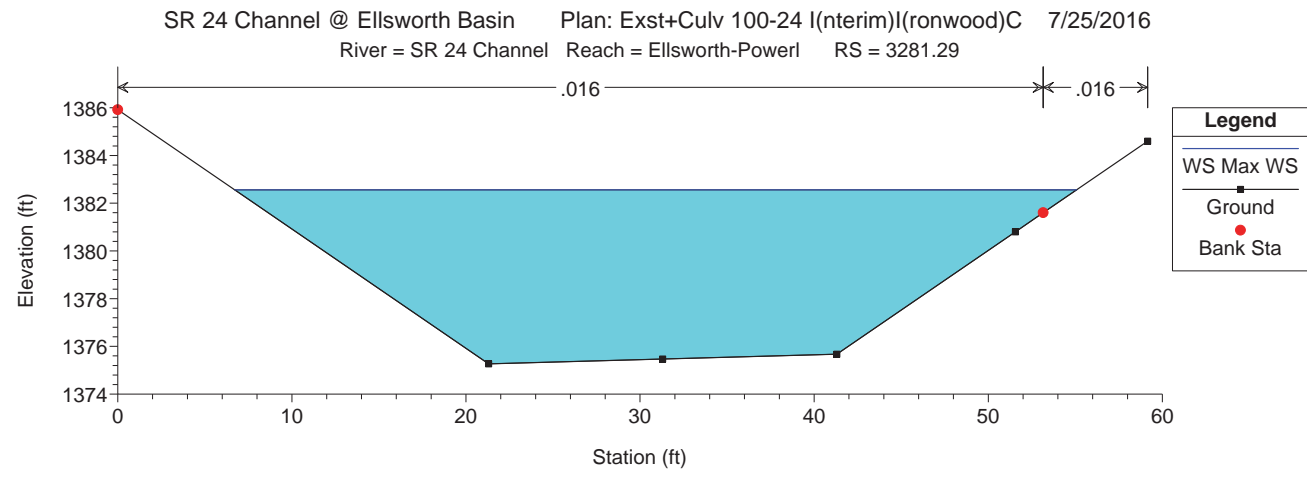


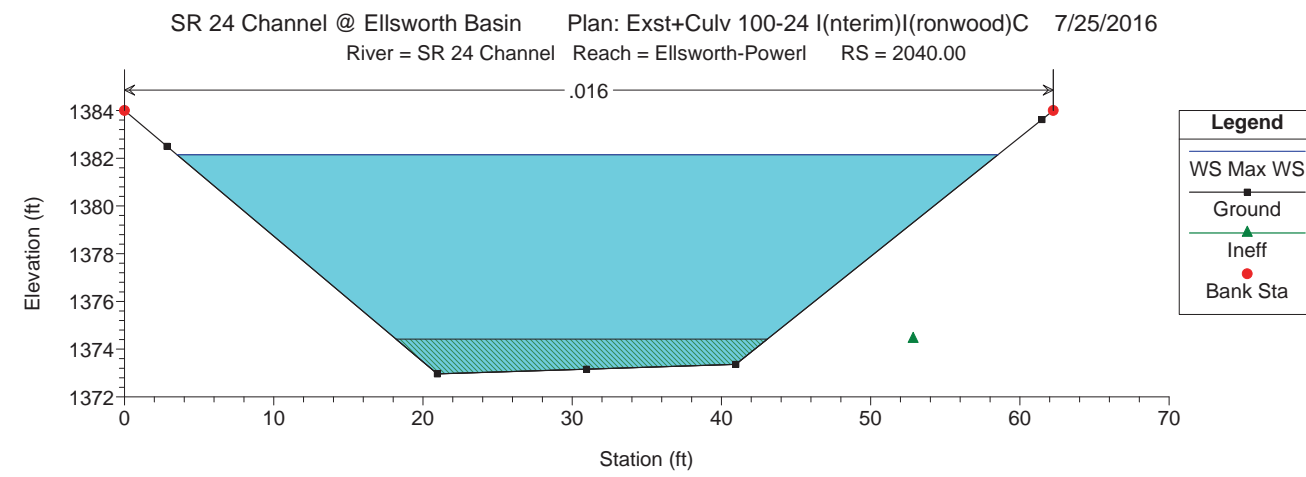
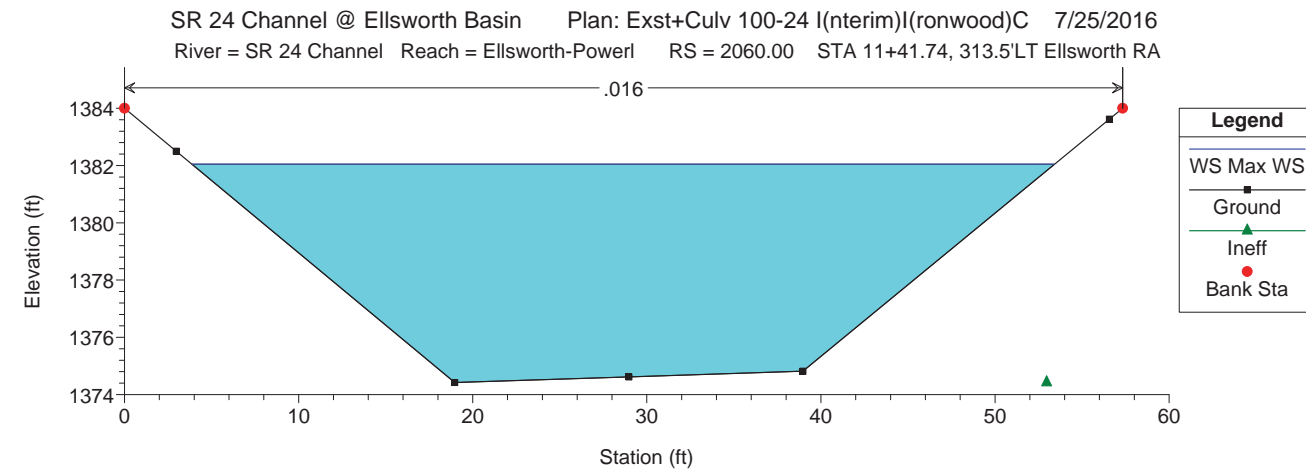
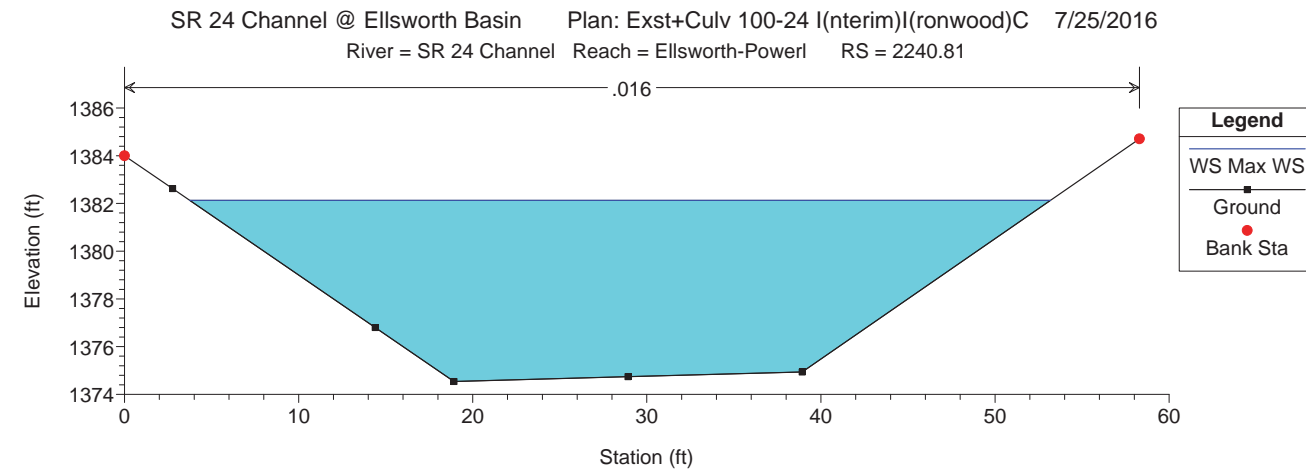
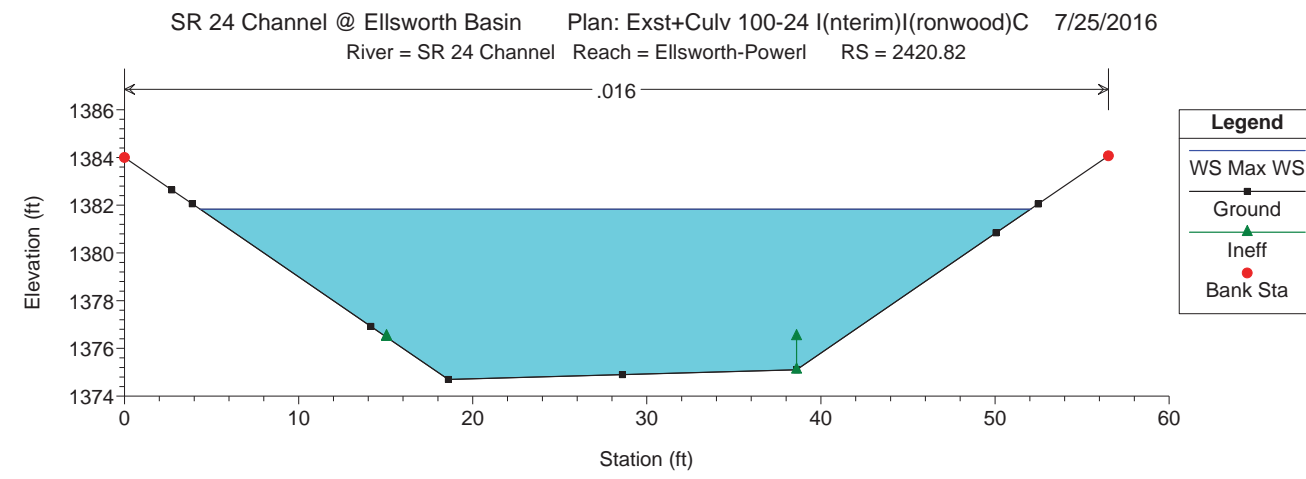
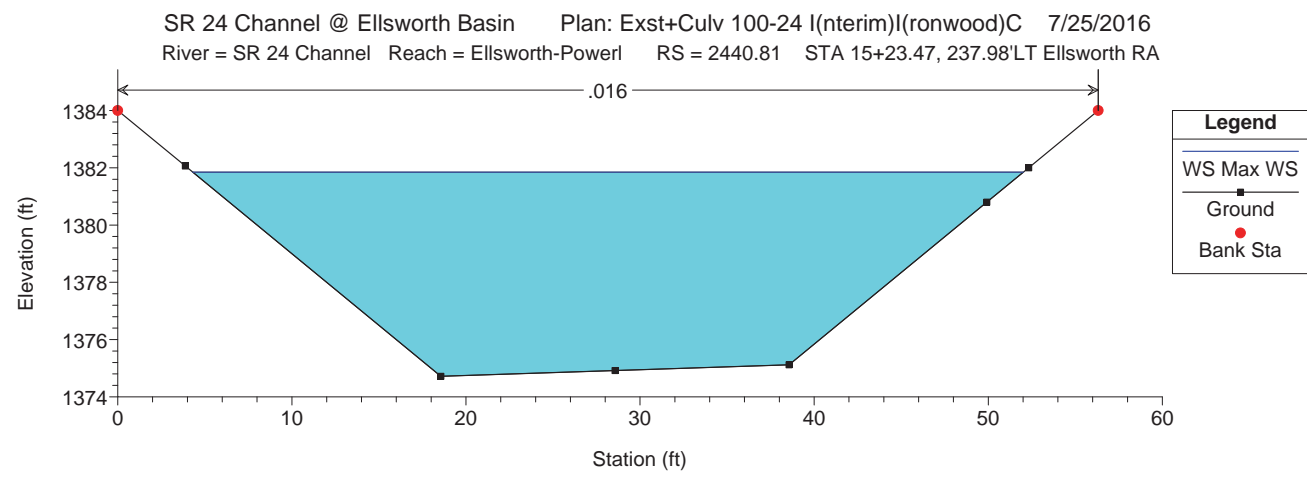
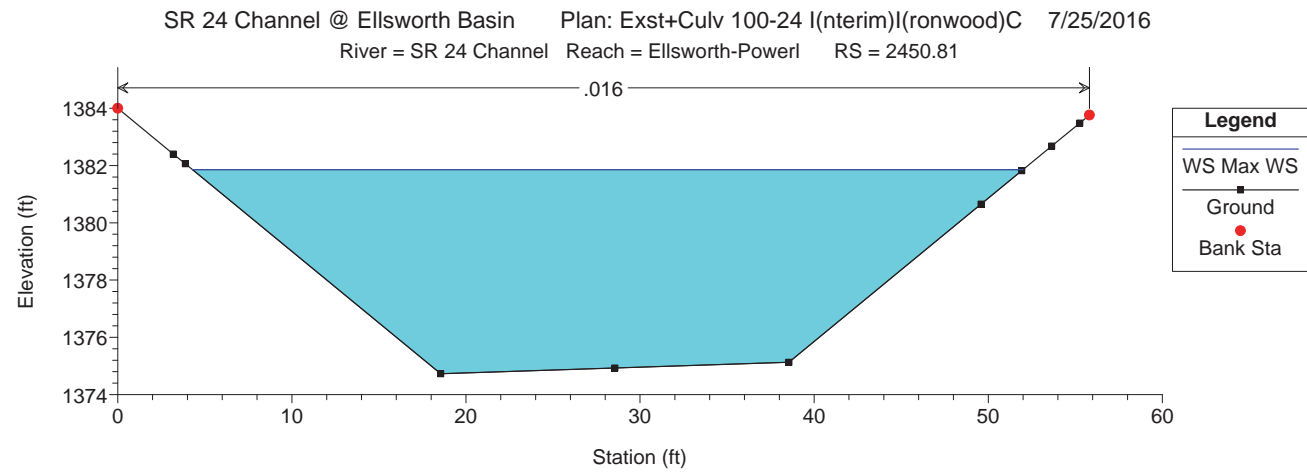
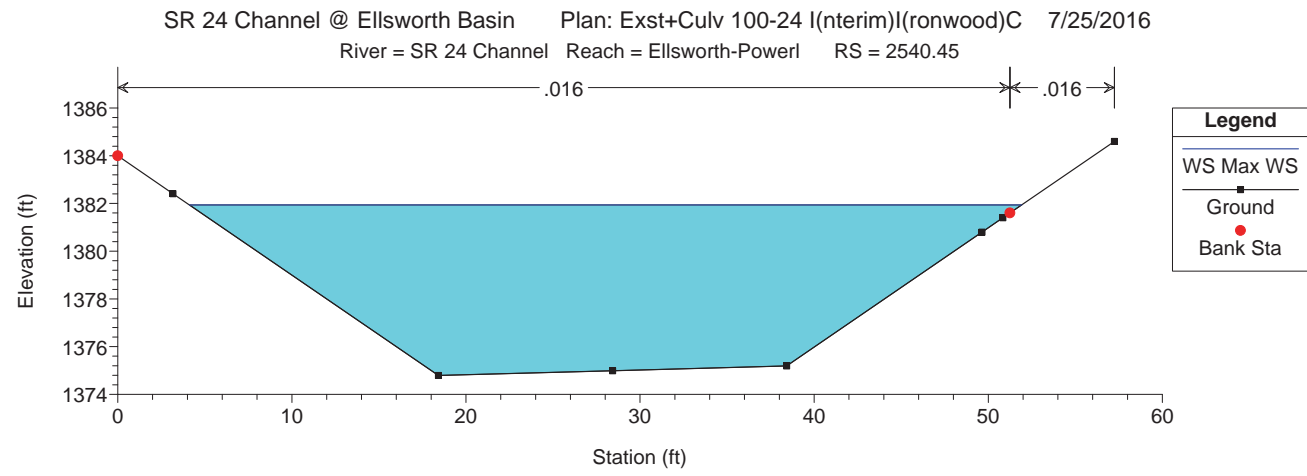
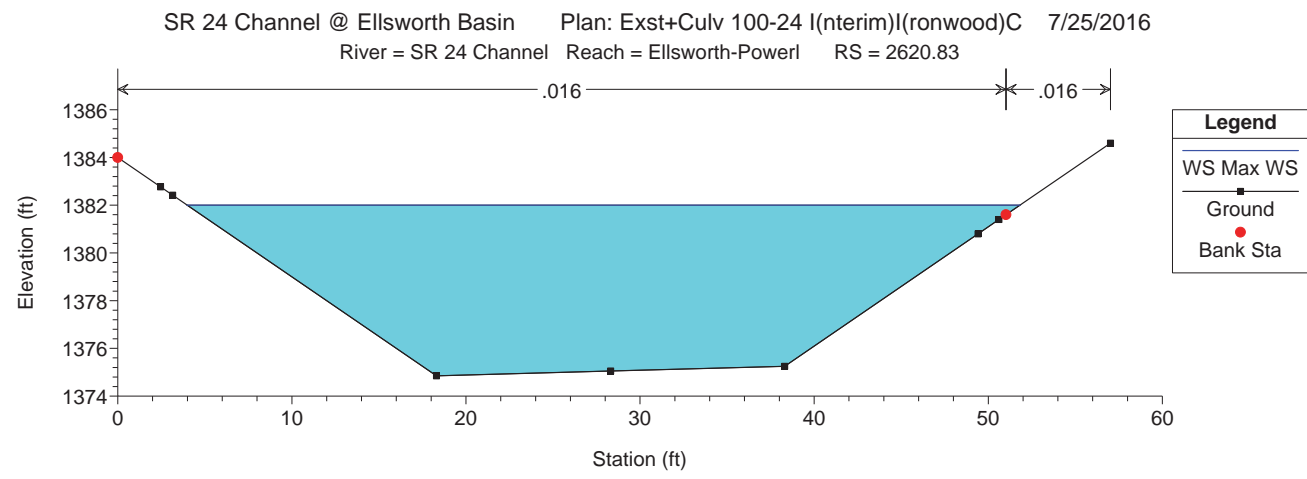
SR 24 Channel @ Ellsworth Basin Plan: Exst+Culv 100-24 I(nterim)I(ronwood)C 7/25/2016
 River = SR 24 Channel Reach = Ellsworth-Powerl RS = 3366.56



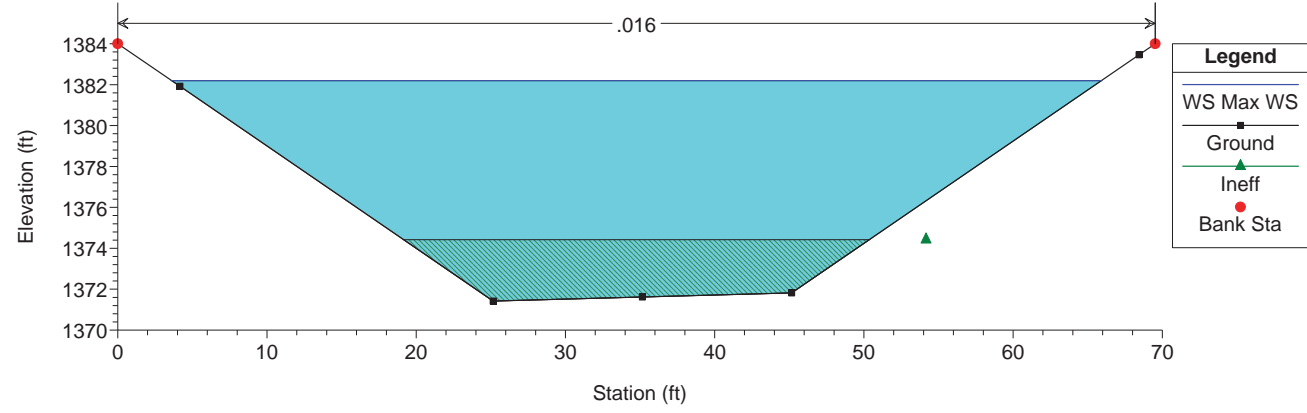
SR 24 Channel @ Ellsworth Basin Plan: Exst+Culv 100-24 I(nterim)I(ronwood)C 7/25/2016
 River = SR 24 Channel Reach = Ellsworth-Powerl RS = 3311.29



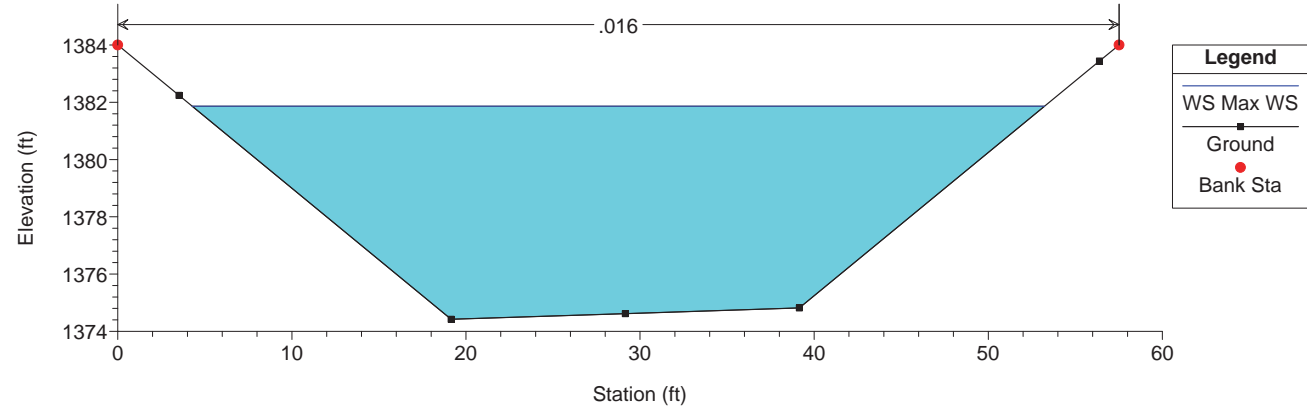




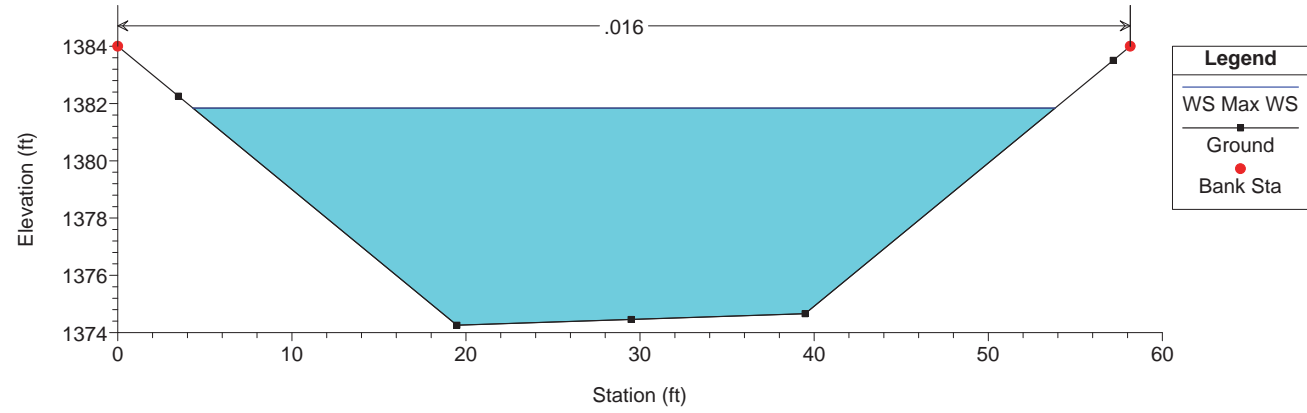
SR 24 Channel @ Ellsworth Basin Plan: Exst+Culv 100-24 I(nterim)I(ronwood)C 7/25/2016
 River = SR 24 Channel Reach = Ellsworth-Powerl RS = 1940.00 @ SR-24 Channel CL



SR 24 Channel @ Ellsworth Basin Plan: Exst+Culv 100-24 I(nterim)I(ronwood)C 7/25/2016
 River = SR 24 Channel Reach = Ellsworth-Powerl RS = 1925.00 @ SR-24 Channel CL

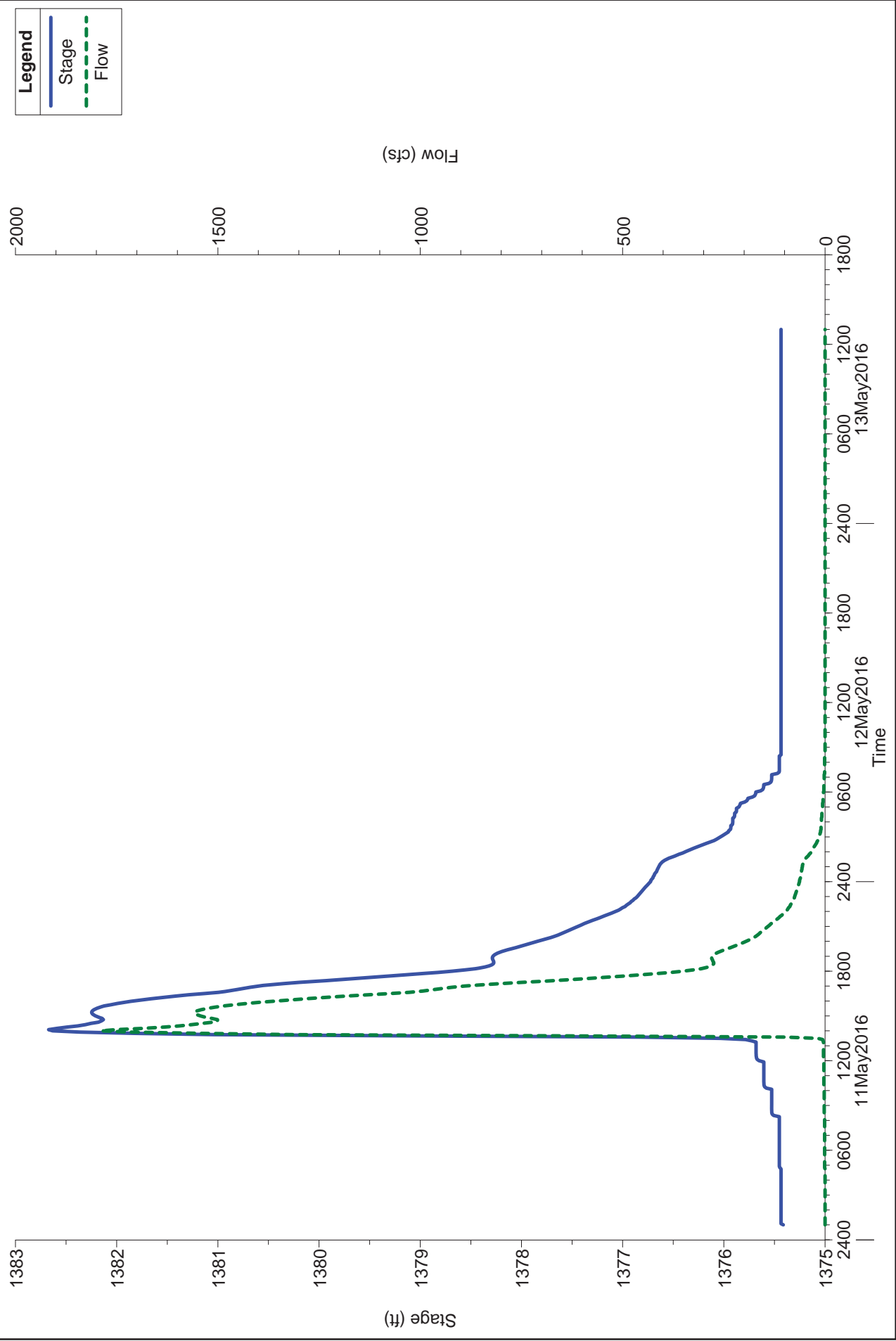


SR 24 Channel @ Ellsworth Basin Plan: Exst+Culv 100-24 I(nterim)I(ronwood)C 7/25/2016
 River = SR 24 Channel Reach = Ellsworth-Powerl RS = 1839.16 STA 9+21.21, 321.32'LT Ellsworth RA

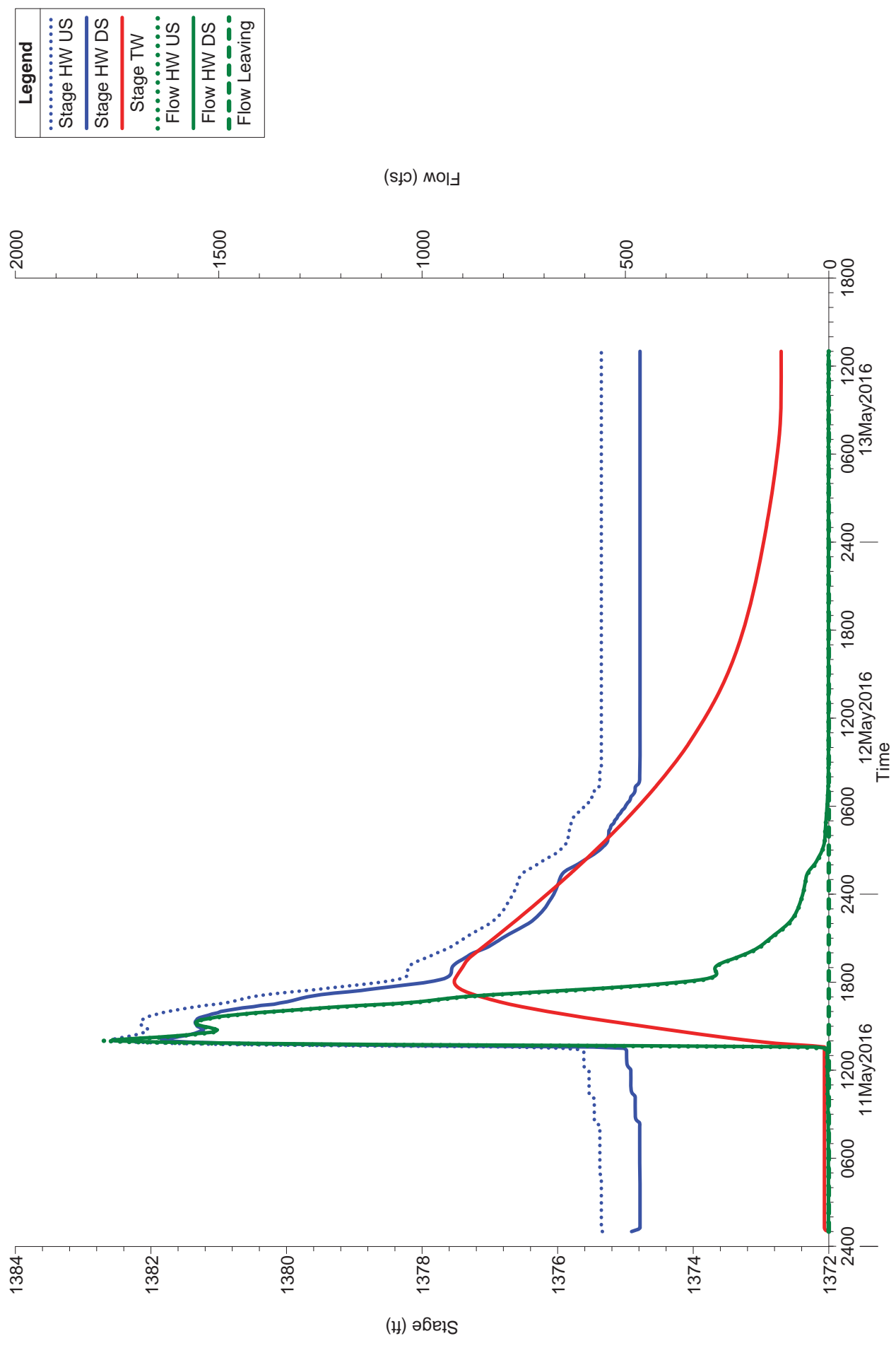


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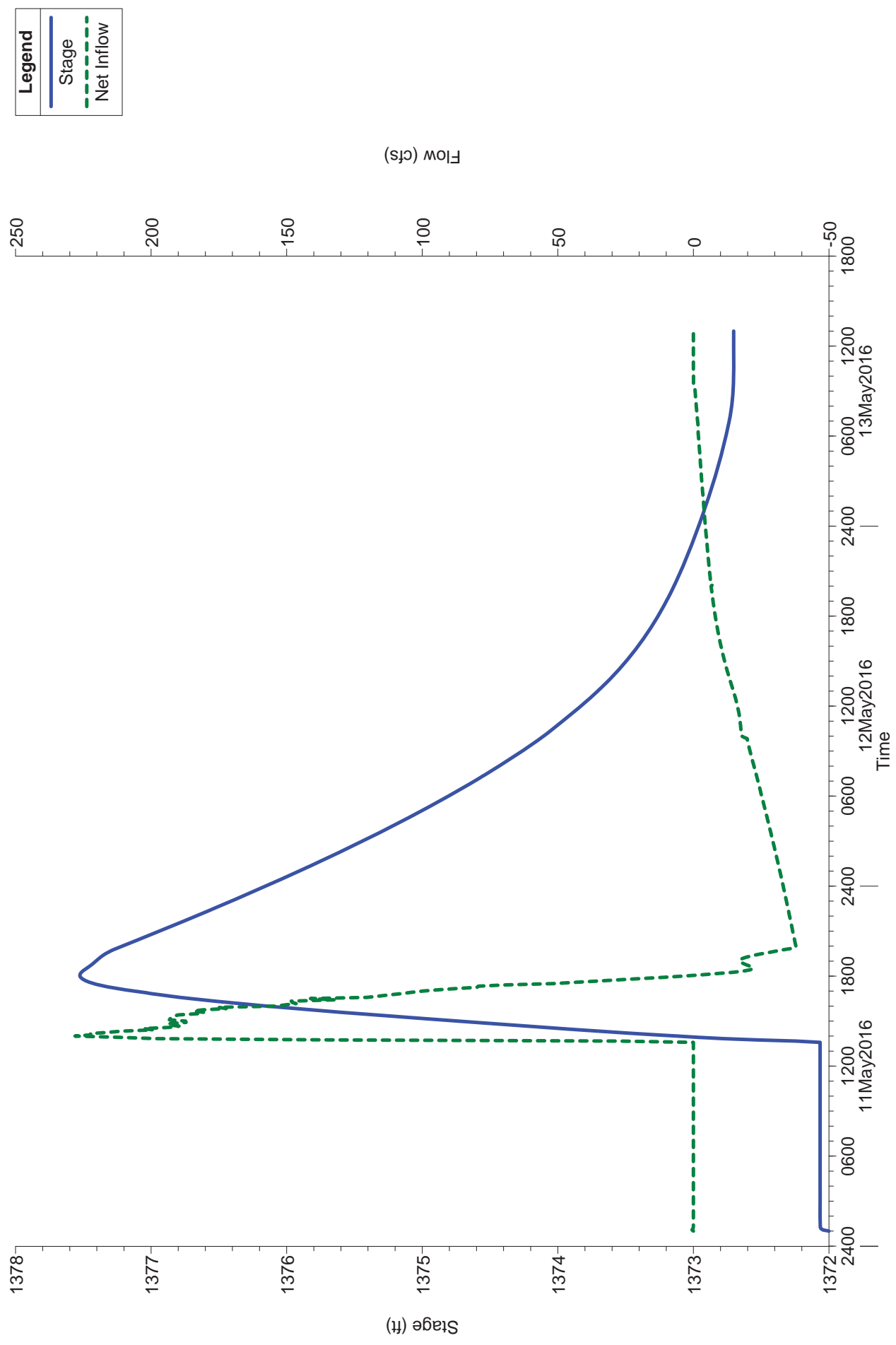
Plan: 10024INTIC River: SR 24 Channel Reach: Ellsworth-Powerl RS: 3422.86



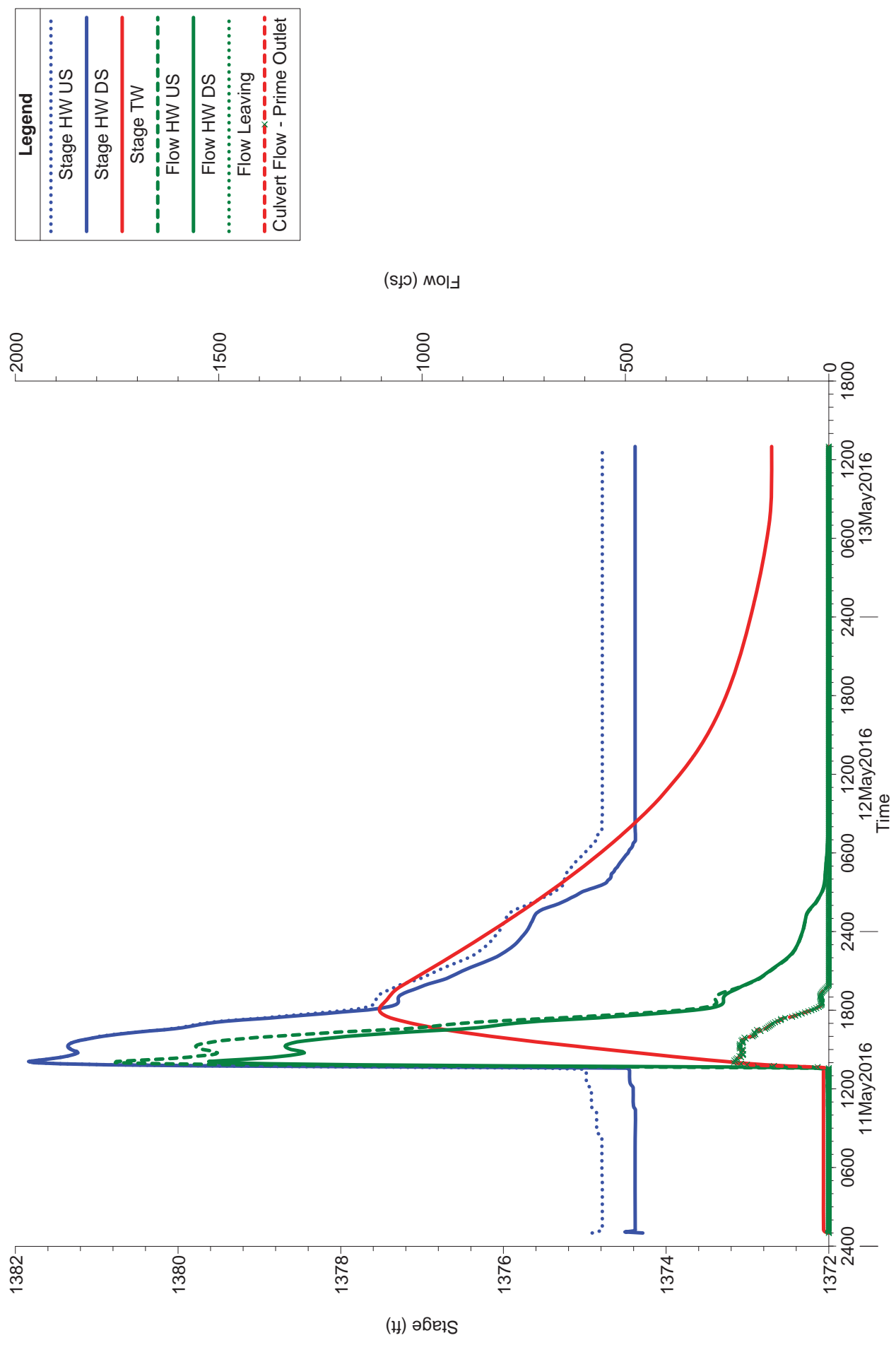
Plan: 10024INTIC River: SR 24 Channel Reach: Ellsworth-Powerl RS: 3311.



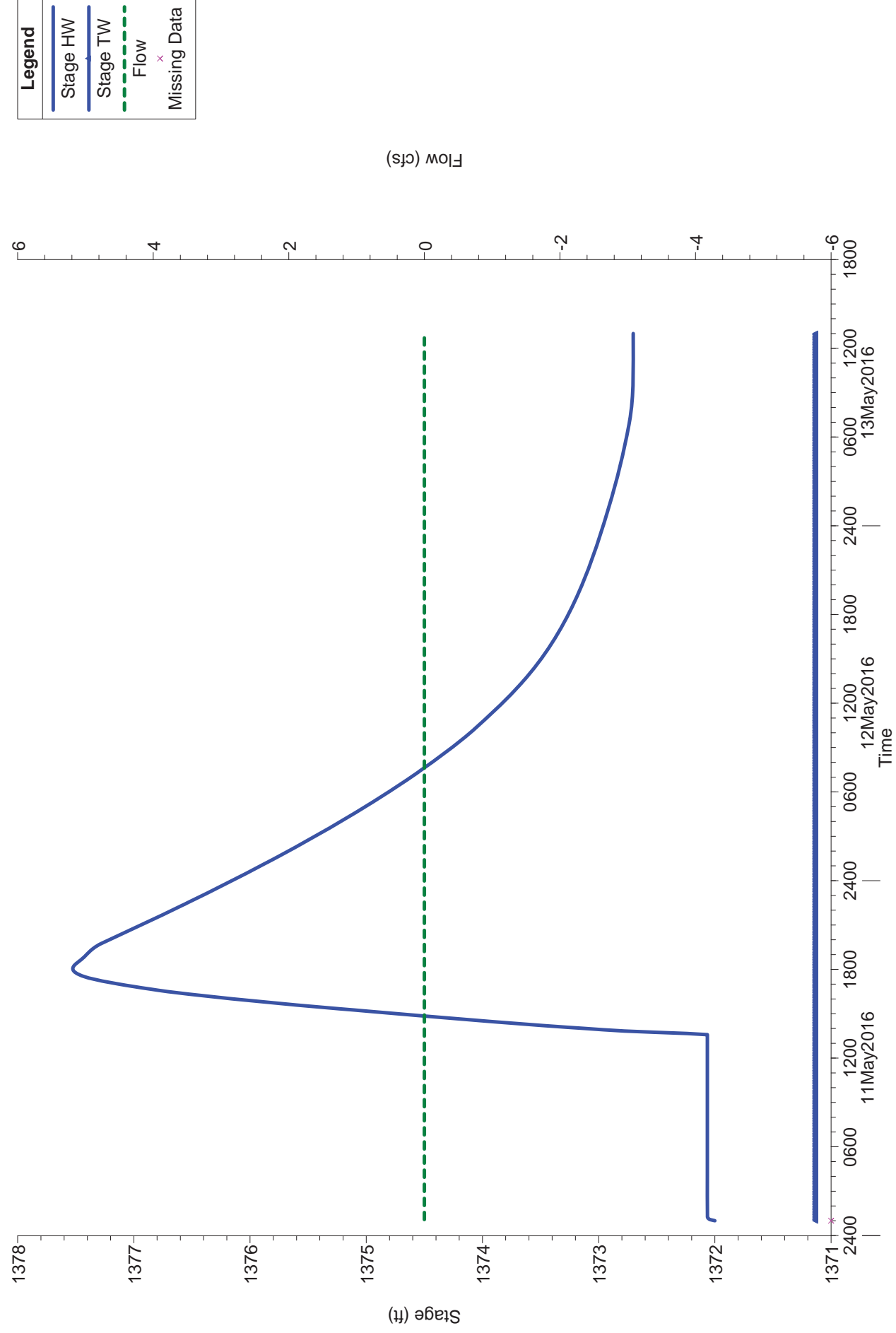
Plan: 10024INTIC Storage Area: ELLSWORTH BASIN



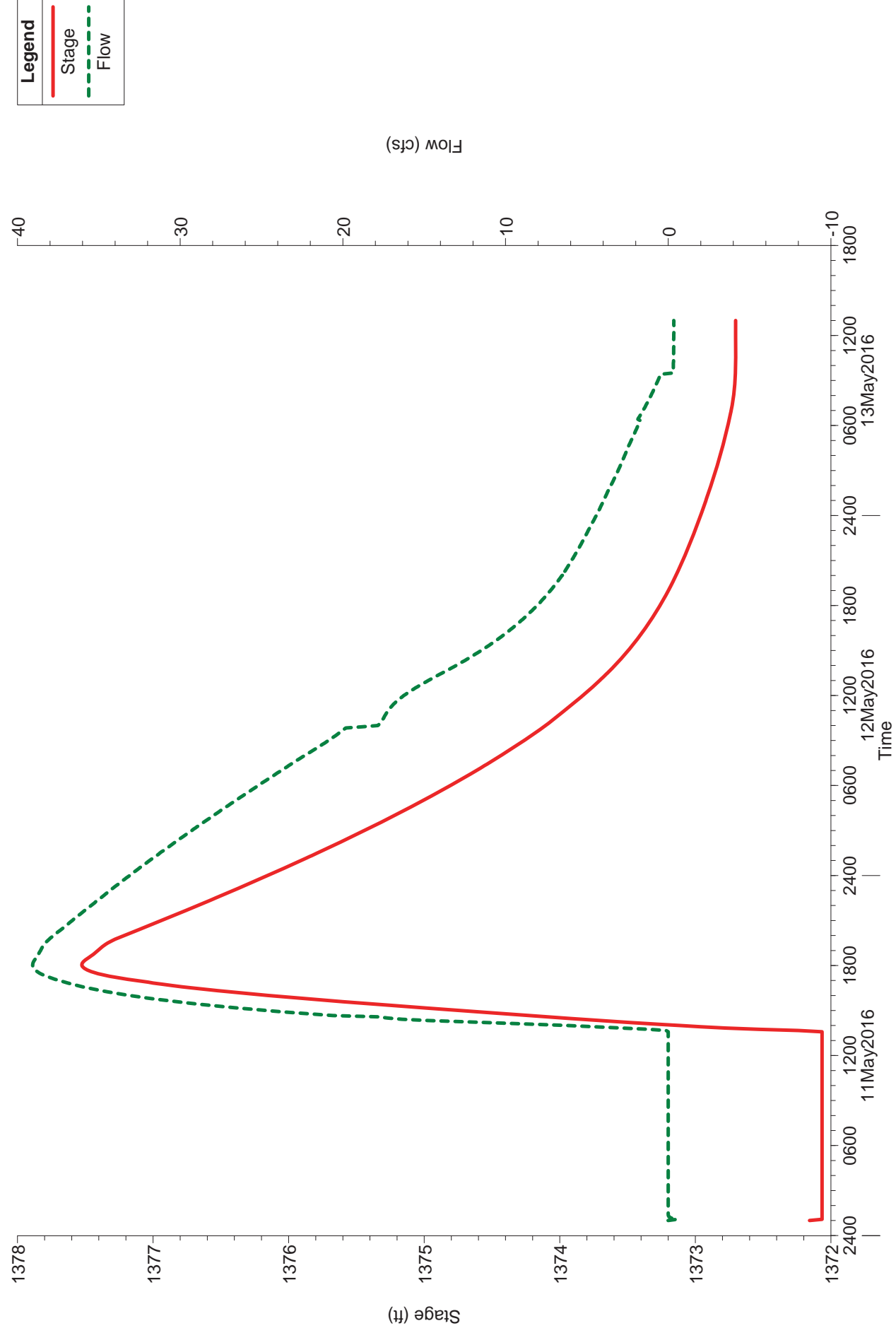
Plan: 10024INTIC River: SR 24 Channel Reach: Ellsworth-Power! RS: 2440



Plan: 10024INTIC SA Connection: ExstEliswOutfall



Plan: 10024INTIC River: SR 24 Channel Reach: Elisw.Bleedoff RS: 13



COMPUTATION OPTIONS AND TOLERANCES

HEC-RAS Unsteady Computation Options and Tolerances

General (1D Options) | 2D Flow Options | 1D/2D Options

Unsteady Flow Options

Theta [implicit weighting factor] (0.6-1.0):	<input type="text" value="0.83"/>	Number of warm up time steps (0 - 100,000):	<input type="text" value="0"/>
Theta for warm up [implicit weighting factor] (0.6-1.0):	<input type="text" value="1"/>	Time step during warm up period (hrs):	<input type="text" value="0"/>
Water surface calculation tolerance (ft):	<input type="text" value="0.075"/>	Minimum time step for time slicing (hrs):	<input type="text" value="0"/>
Storage Area elevation tolerance (ft):	<input type="text" value="0.1"/>	Maximum number of time slices:	<input type="text" value="40"/>
Flow calculation tolerance [optional] (cfs):	<input type="text"/>	Lateral Structure flow stability factor (1.0-3.0):	<input type="text" value="2"/>
Max error in water surface solution (Abort Tolerance)(ft):	<input type="text" value="100"/>	Inline Structure flow stability factor (1.0-3.0):	<input type="text" value="1"/>
Maximum number of iterations (0-40):	<input type="text" value="40"/>	Weir flow submergence decay exponent (1.0-3.0):	<input type="text" value="1"/>
Maximum iterations without improvement (0-40):	<input type="text"/>	Gate flow submergence decay exponent (1.0-3.0):	<input type="text" value="1"/>
<input checked="" type="checkbox"/> Compute energy losses over junctions		DSS Messaging Level (1 to 10, Default = 4)	<input type="text" value="4"/>

Geometry Preprocessor Options

Family of Rating Curves for Internal Boundaries

Use existing internal boundary tables when possible.

Recompute at all internal boundaries

1D Equation Solver

Skyline/Gaussian (Default: Faster for dendritic systems)

Pardiso (Optional: May be faster for large interconnected systems)

Number of cores to use with Pardiso solver:

OK Cancel Defaults ...

UNSTEADY FLOW ANALYSIS SUMMARY (EXCERPT)

PLAN Exst+Culv 100-24 I(nterim)I(ronwood)C

Unsteady Flow Analysis

File Options Help

Plan : Short ID

Geometry File :

Unsteady Flow File :

Plan Description :

The 2016 stage-volume curve of the Ellsworth Basin is simulated.
The maximum volume is 100.3 ac-ft at elevation 1381.6 before the water leaves the basin at its northwest extremity.

Programs to Run

Geometry Preprocessor

Unsteady Flow Simulation

Sediment

Post Processor

Floodplain Mapping

Simulation Time Window

Starting Date: Starting Time:

Ending Date: Ending Time:

Computation Settings

Computation Interval: Hydrograph Output Interval:

Mapping Output Interval: Detailed Output Interval:

Computation Level Output

DSS Output Filename:

Mixed Flow Regime (see menu: "Options/Mixed Flow Options ...")

Compute

HEC-RAS Finished Computations

Write Geometry Information
Layer: Complete

Geometry Processor
River: SR 24 Channel RS: 1839.16
Reach: Ellsworth-Powerl Node Type: Cross Section
IB Curve:

Unsteady Flow Simulation
Simulation:
Time: 60.0000 13MAY2016 13:00:00 Iteration (1D): 0 Iteration (2D):
Writing Profiles 2900

Post Process
River: SR 24 Channel RS: 13
Reach: Ellsw.Bleedoff Node Type: Cross Section
Profile: 13MAY2016 1300
Simulation: 722/722

Computation Messages

Plan: 'Exst+Culv 100-24 I(nterim)I(ronwood)C' (EllsworthChan.p02)
Simulation started at: 25Jul2016 10:03:03 AM
Using 64 Bit Computation Engines

Writing Geometry
Computing XS Interpolation Surfaces
XS Interpolation Surfaces generated in 102 ms
Completed Writing Geometry

Geometric Preprocessor HEC-RAS 5.0.1 April 2016
1 Internal Boundary curve(s) have been read in

Finished Processing Geometry

Writing Event Conditions
Event Conditions Complete

Performing Unsteady Flow Simulation HEC-RAS 5.0.1 April 2016

Maximum iterations of 40			RS	WSEL	ERROR
11MAY2016 01:00:01	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.168
11MAY2016 01:00:02	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.129
11MAY2016 01:00:03	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.128
11MAY2016 01:00:04	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.128
11MAY2016 01:00:05	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.127
11MAY2016 01:00:06	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.126
11MAY2016 01:00:07	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.126
11MAY2016 01:00:08	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.125
11MAY2016 01:00:09	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.125
11MAY2016 01:00:10	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.124
11MAY2016 01:00:11	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.124
11MAY2016 01:00:12	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.123
11MAY2016 01:00:13	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.123

Pause Take Snapshot of Results Close

HEC-RAS Finished Computations

Write Geometry Information
Layer: Complete

Geometry Processor
River: SR 24 Channel RS: 1839.16
Reach: Ellsworth-Powerl Node Type: Cross Section
IB Curve:

Unsteady Flow Simulation
Simulation:
Time: 60.0000 13MAY2016 13:00:00 Iteration (1D): 0 Iteration (2D):
Writing Profiles 2900

Post Process
River: SR 24 Channel RS: 13
Reach: Ellsw.Bleedoff Node Type: Cross Section
Profile: 13MAY2016 1300
Simulation: 722/722

Computation Messages

11MAY2016 01:01:14	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.056
11MAY2016 01:01:15	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.056
11MAY2016 01:01:16	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.055
11MAY2016 01:01:17	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.055
11MAY2016 01:01:18	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.055
11MAY2016 01:01:19	SR 24 Channel	Ellsw.Bleedoff	13	1372.07	0.055

The maximum xsec wsel error was 0.168
SR 24 Channel Ellsw.Bleedoff 13 at 11MAY2016 01:00:01

Finished Unsteady Flow Simulation

Writing Results to DSS
Finished Writing Results to DSS

Reading Data for Post Process

Running Post Processor HEC-RAS 5.0.1 April 2016

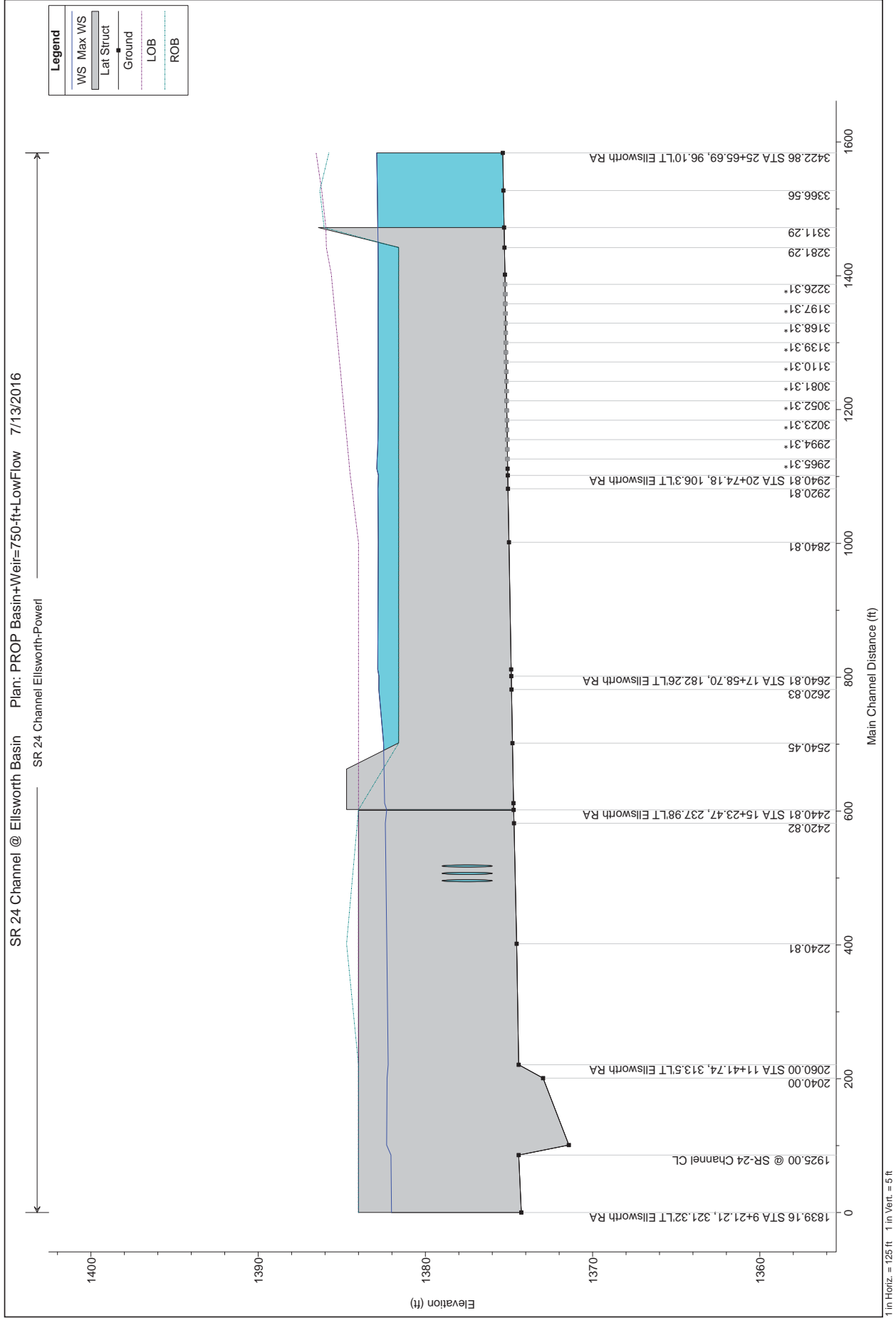
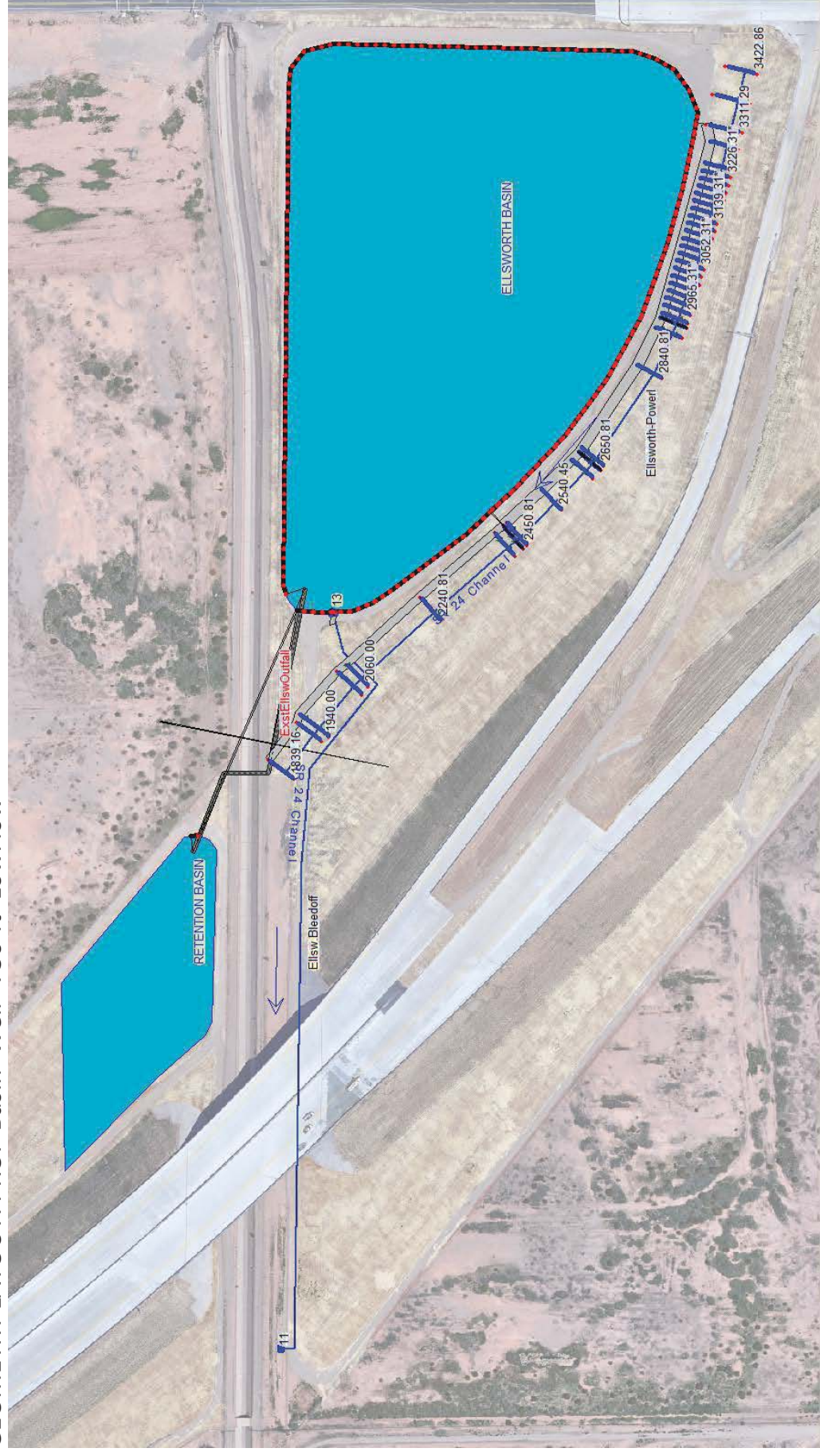
Finished Post Processing

Computations Summary

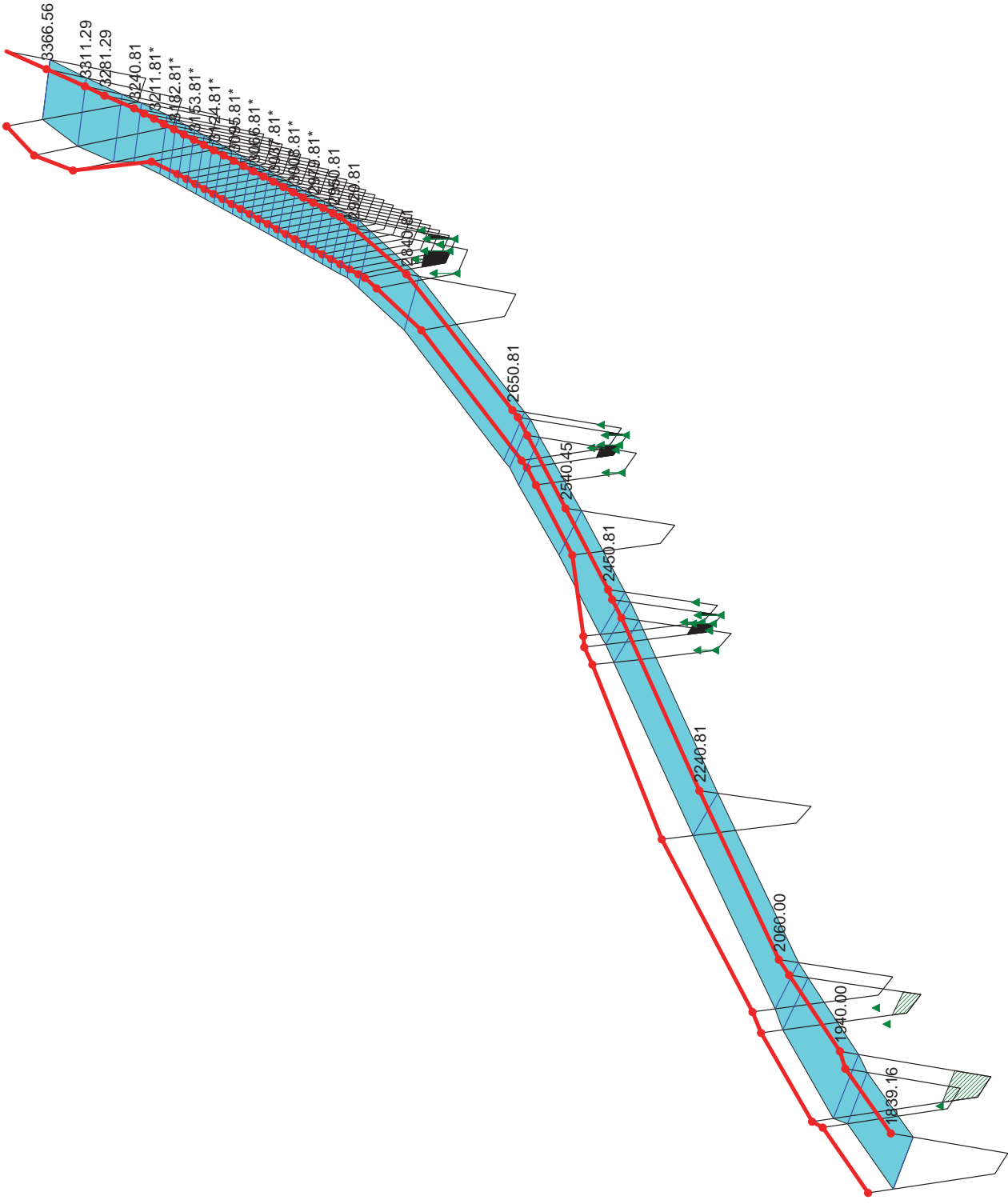
Computation Task	Time(hh:mm:ss)
Completing Geometry	<1
Preprocessing Geometry(64)	<1
Unsteady Flow Computations(64)	45
Writing to DSS(64)	<1
Post-Processing(64)	8
Complete Process	55

Pause Take Snapshot of Results Close

GEOMETRY LAYOUT: PROP Basin+Weir=750-ft+LowFlow



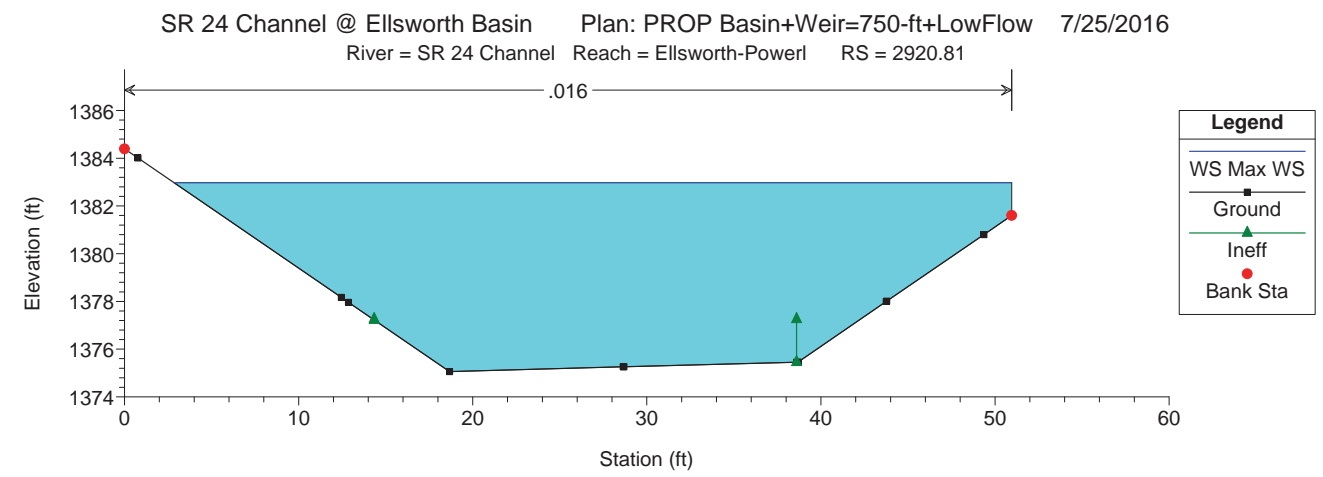
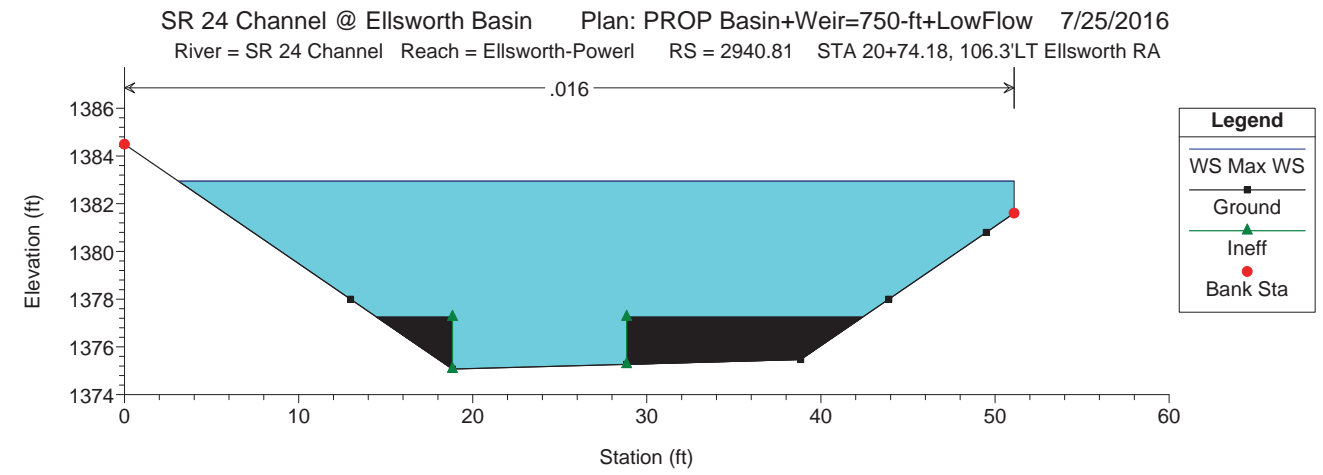
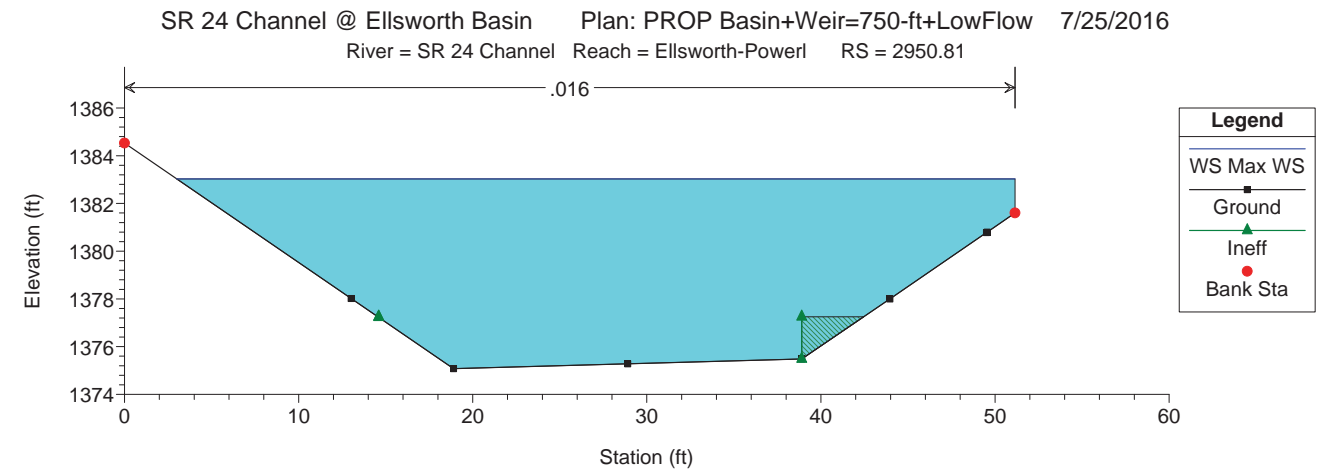
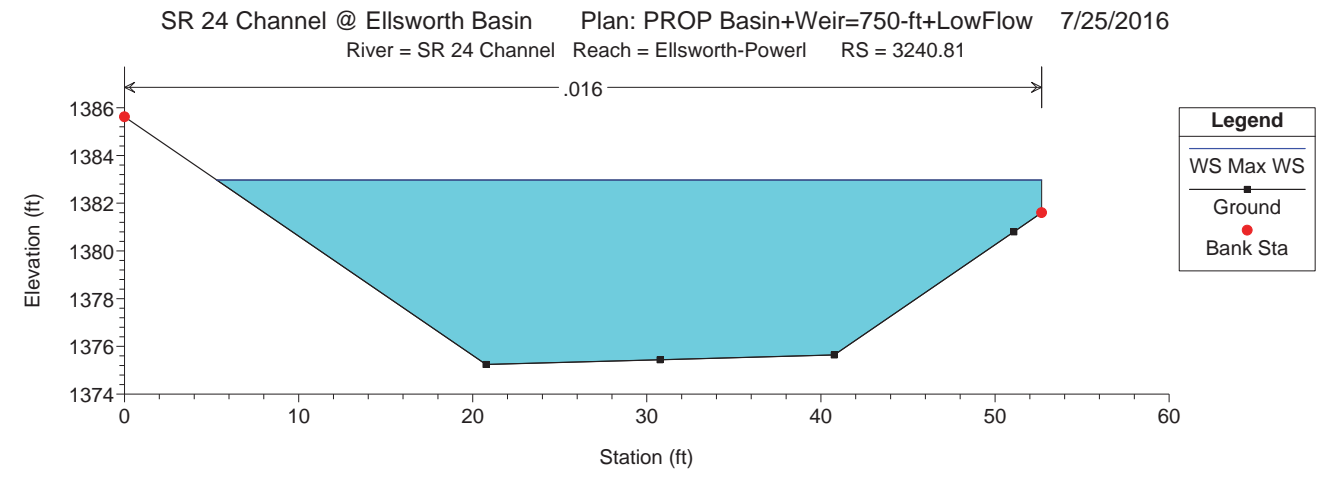
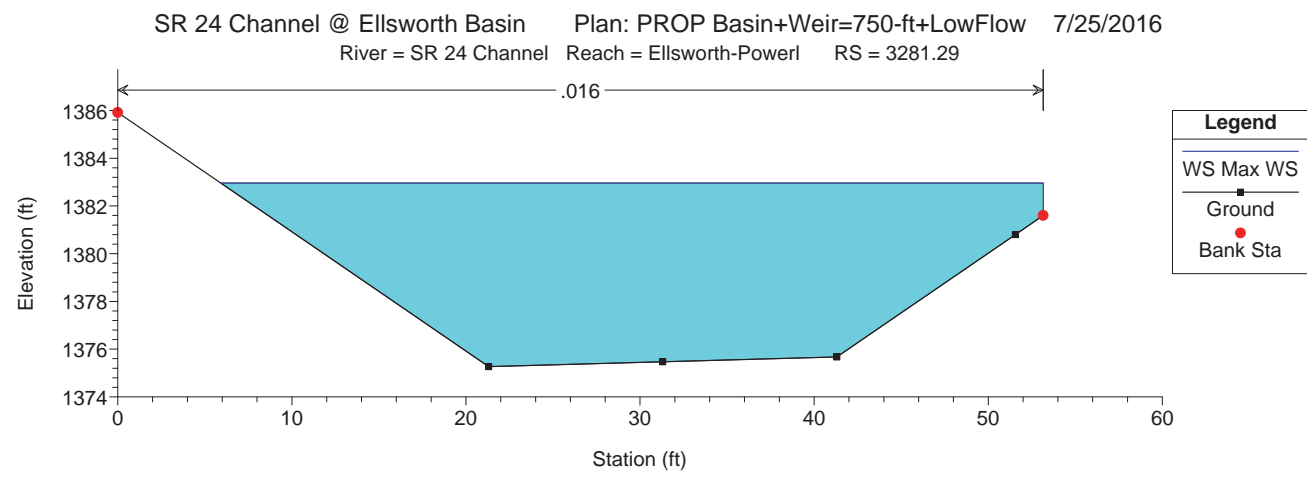
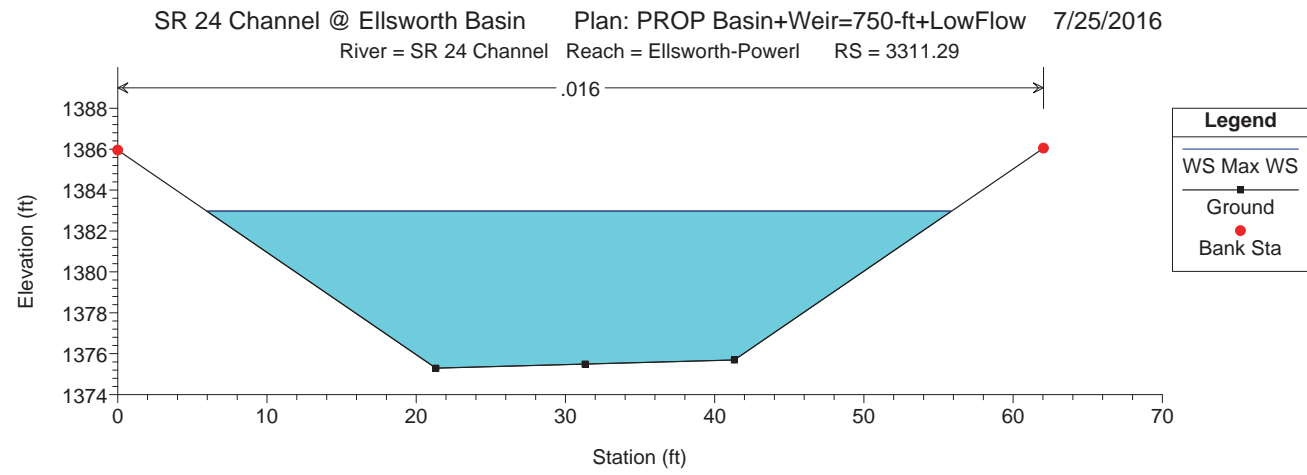
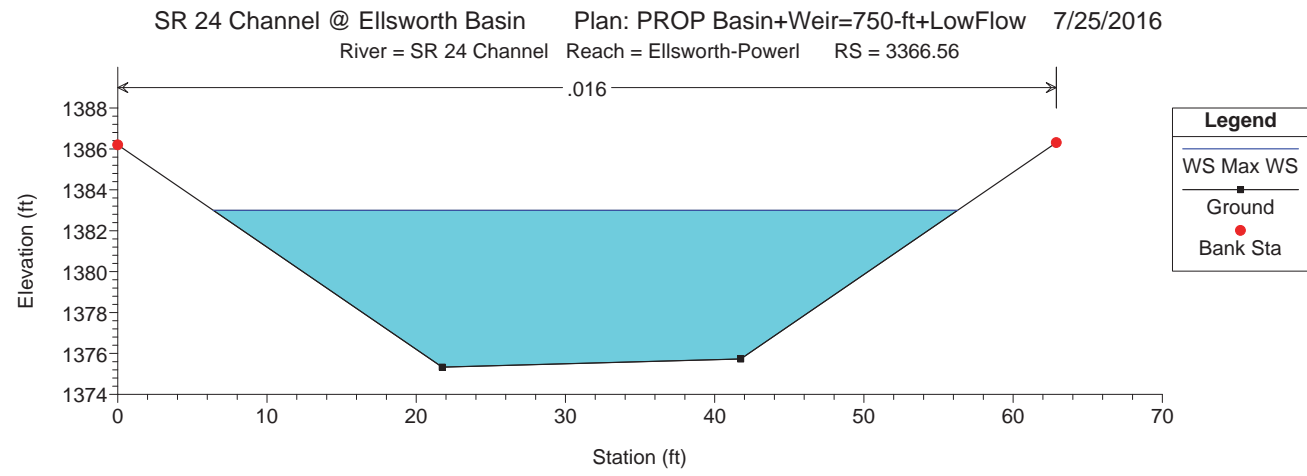
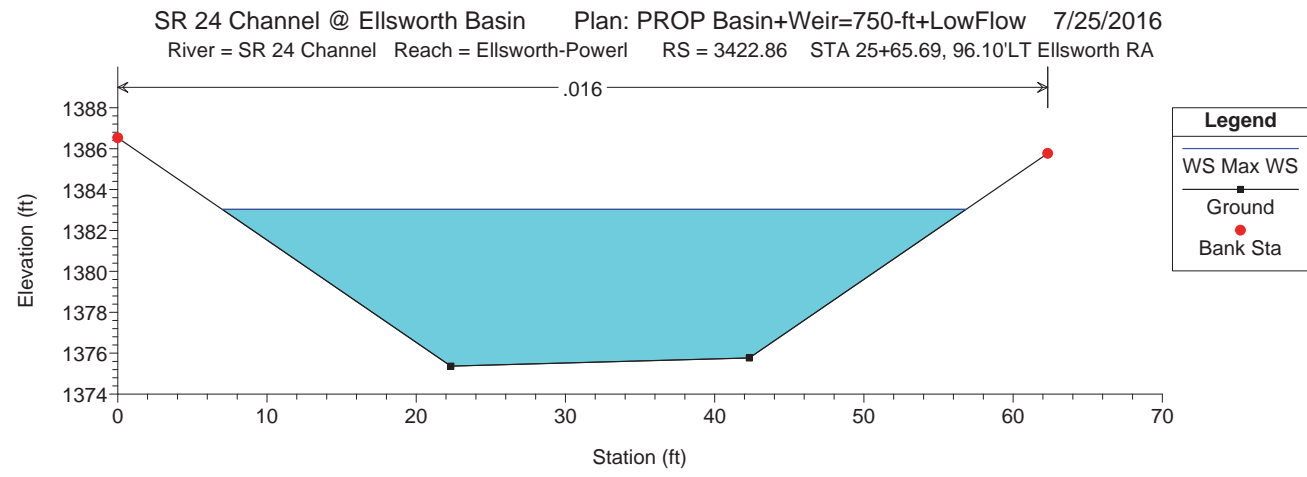
SR 24 Channel @ Ellsworth Basin Plan: PROP Basin+Weir=750-ft+LowFlow 7/25/2016

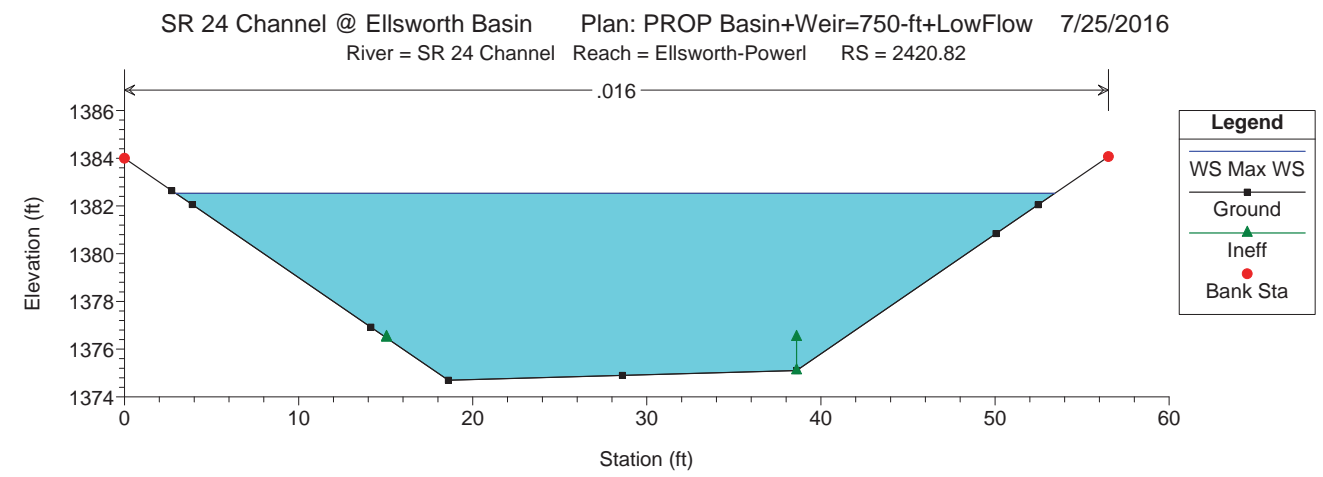
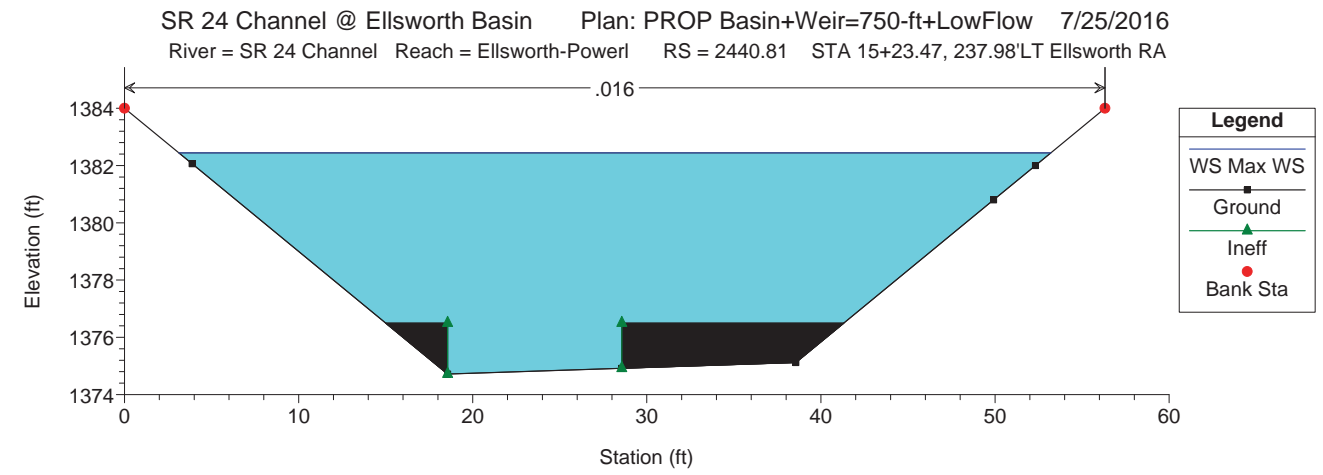
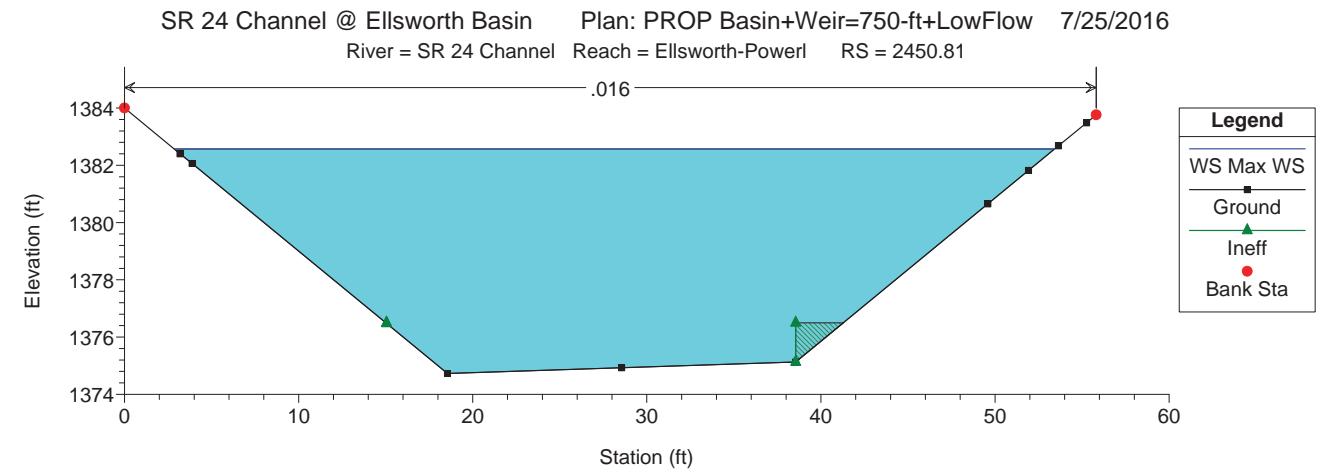
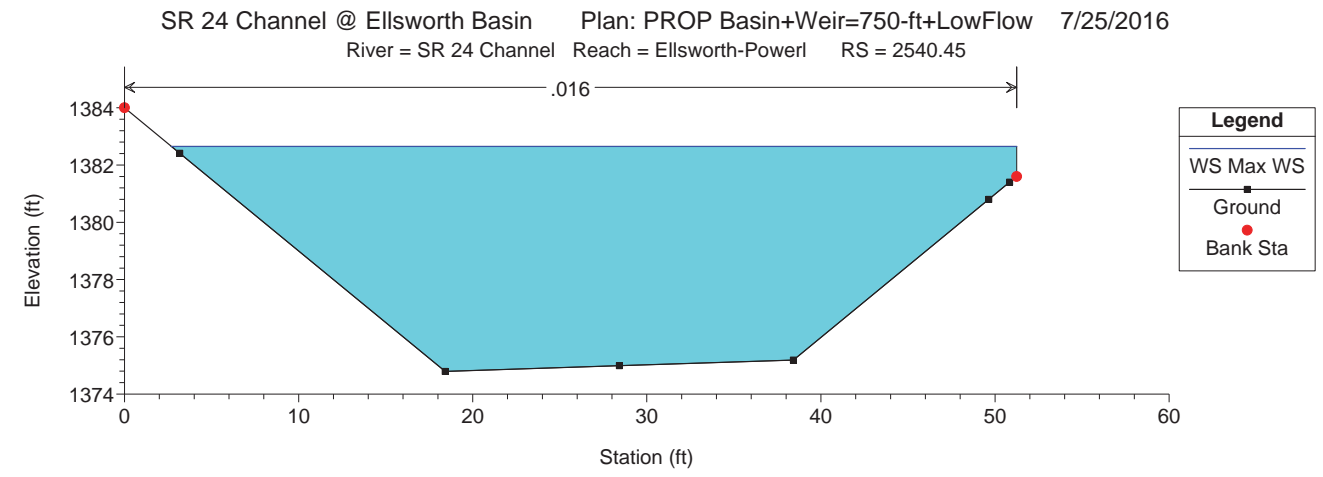
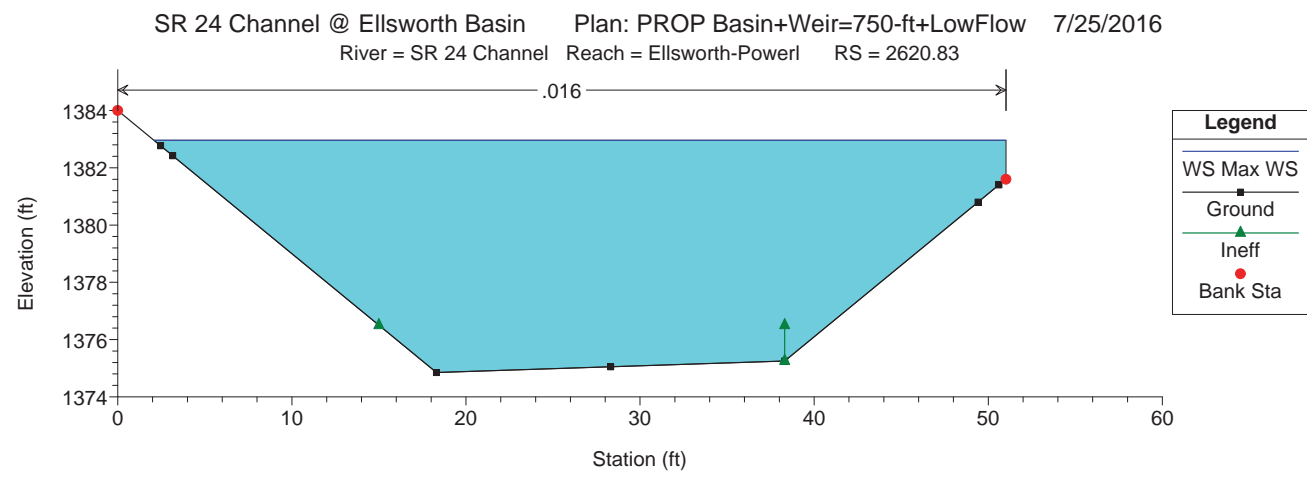
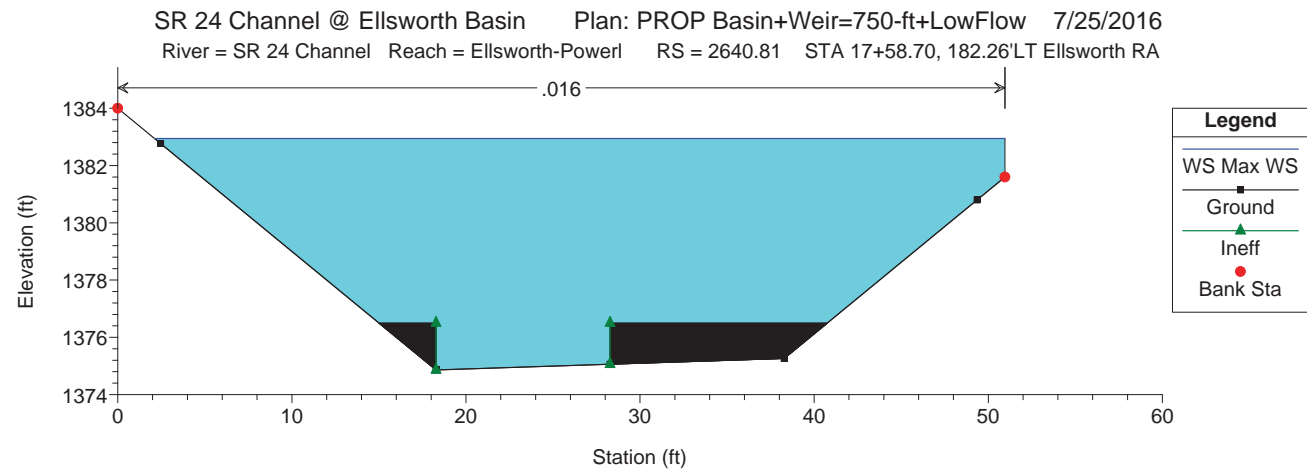
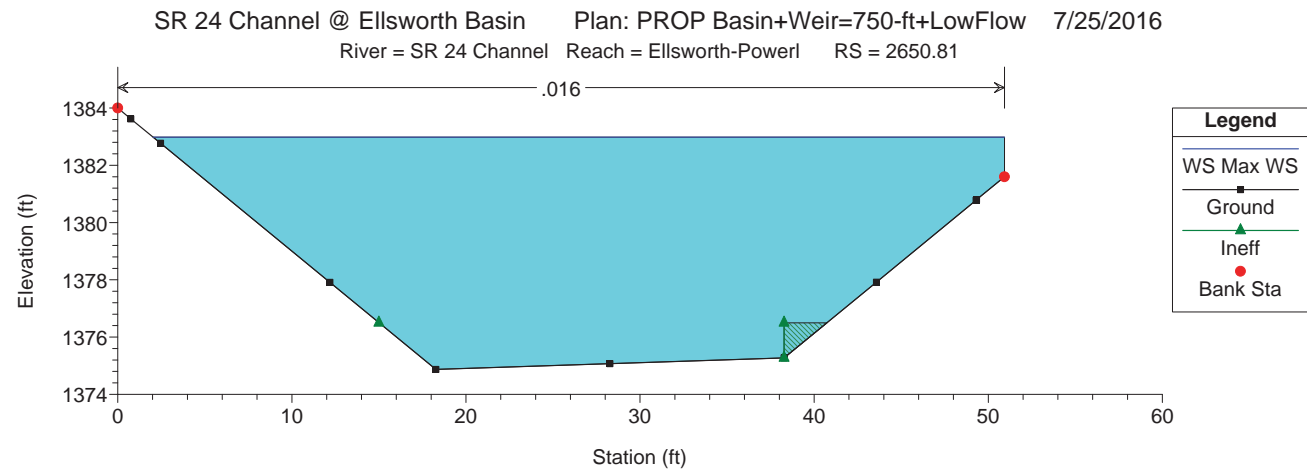
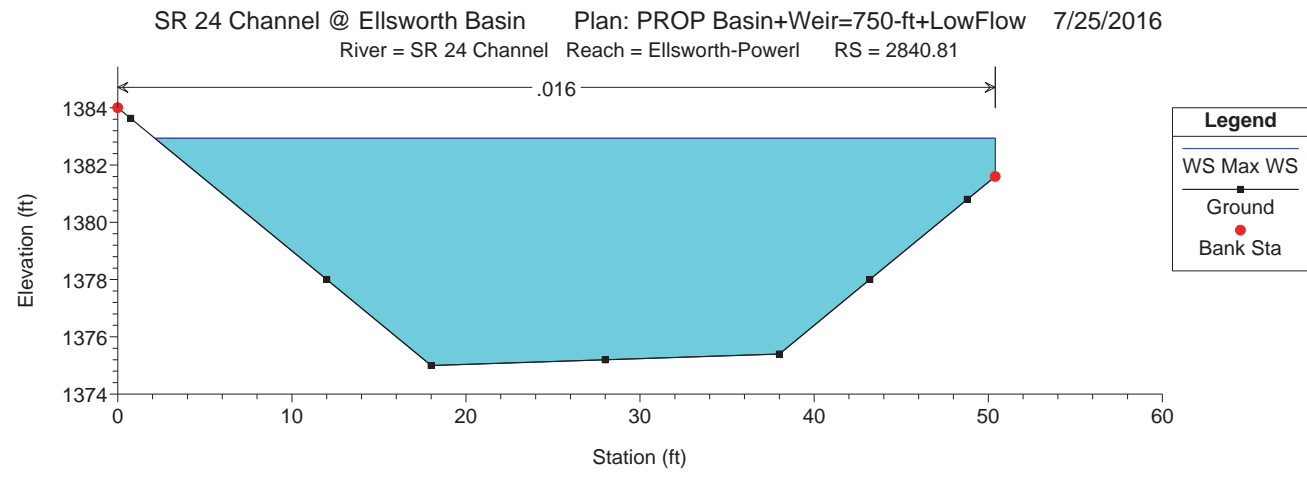


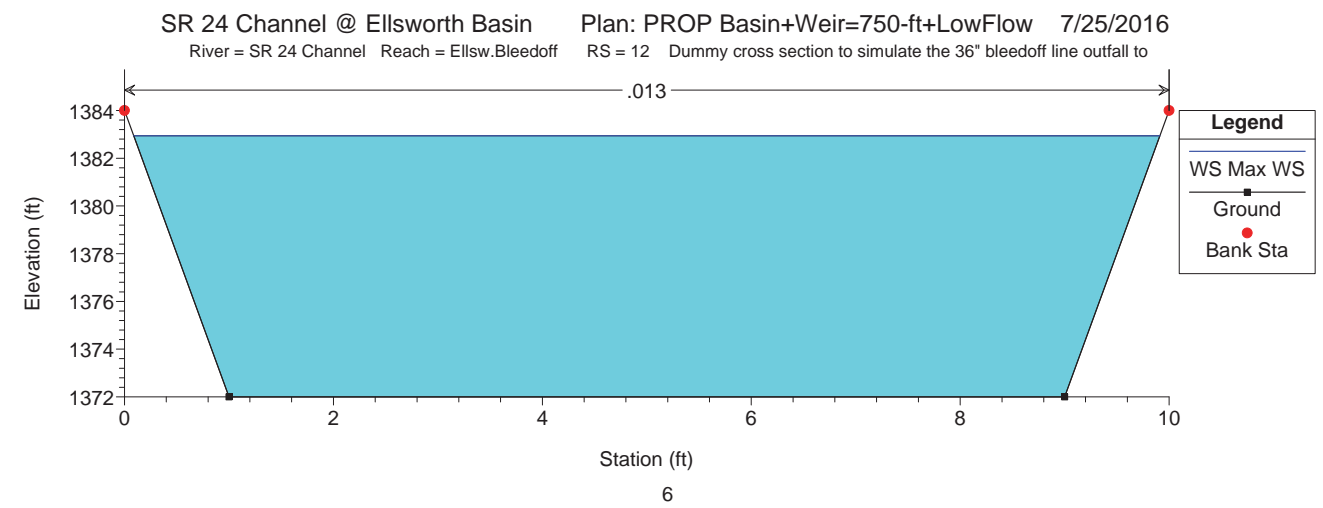
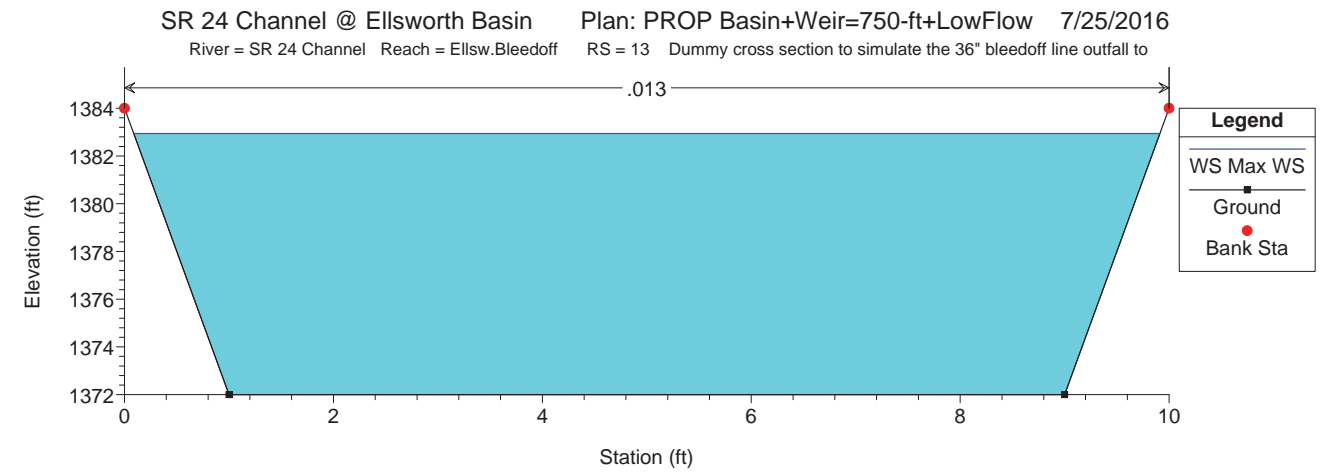
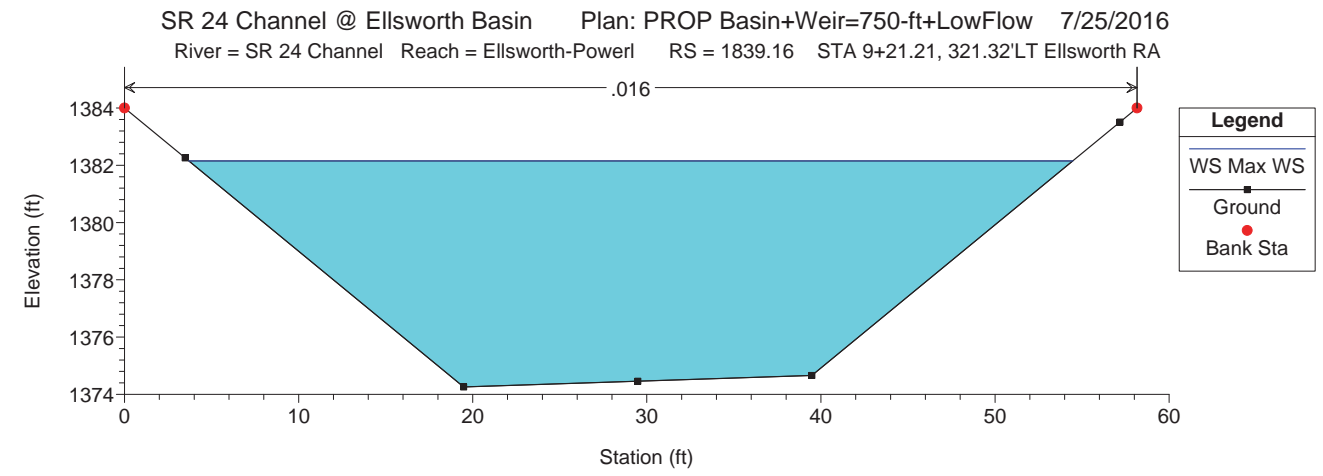
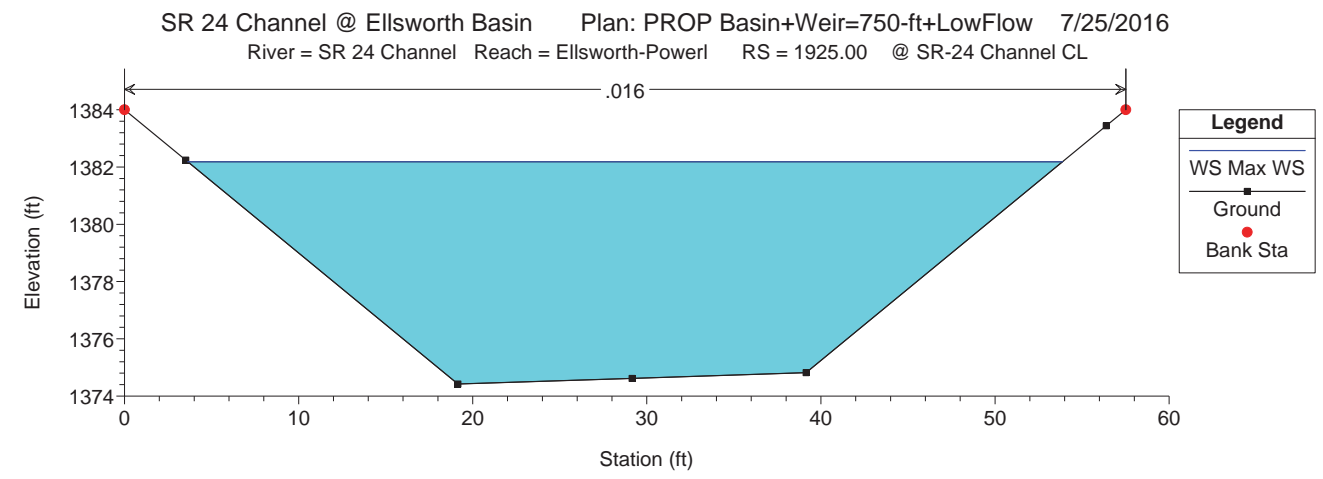
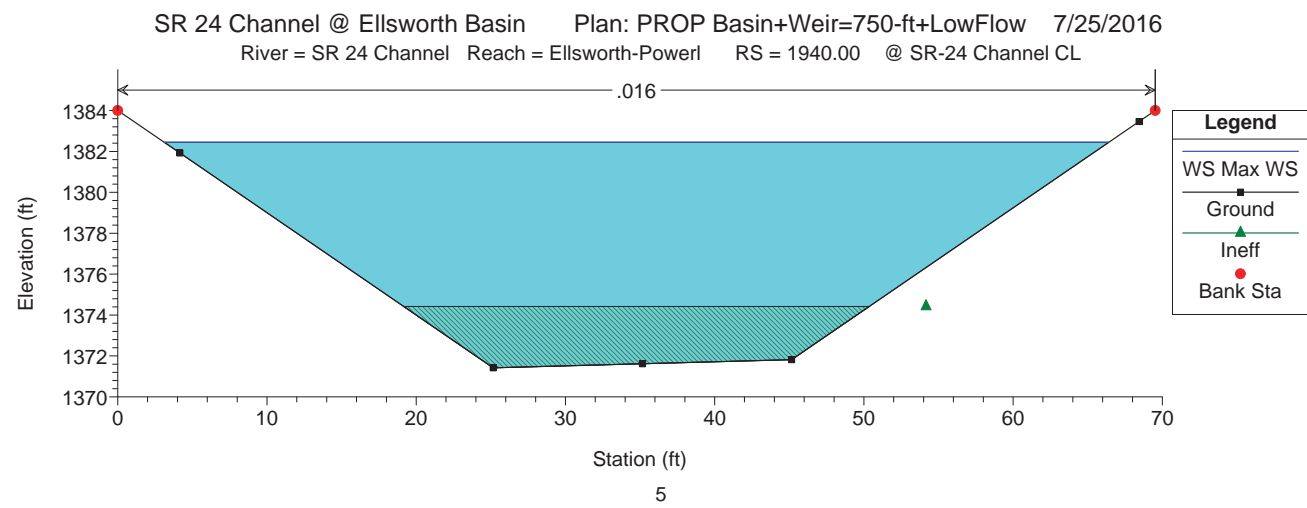
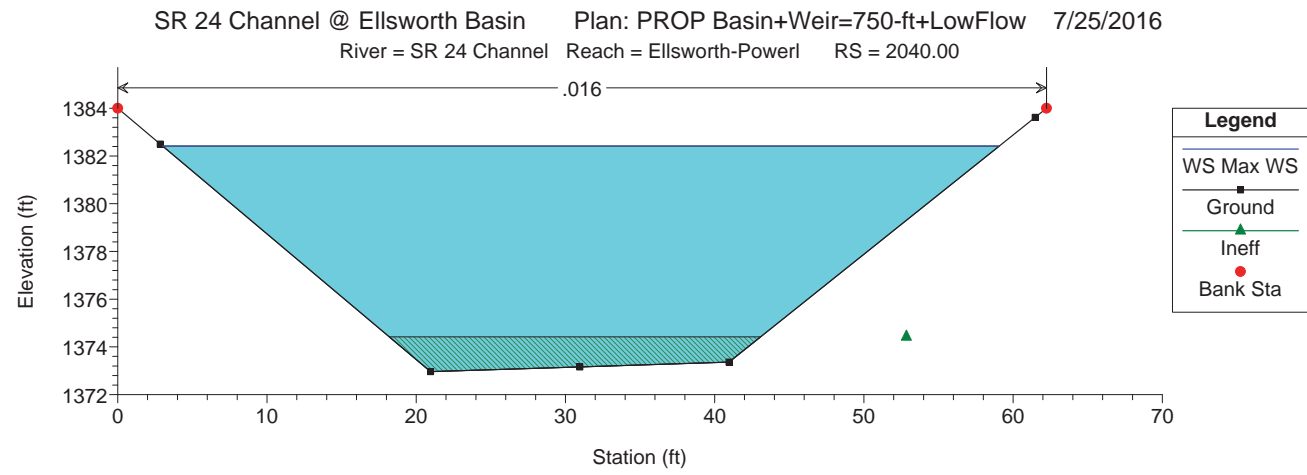
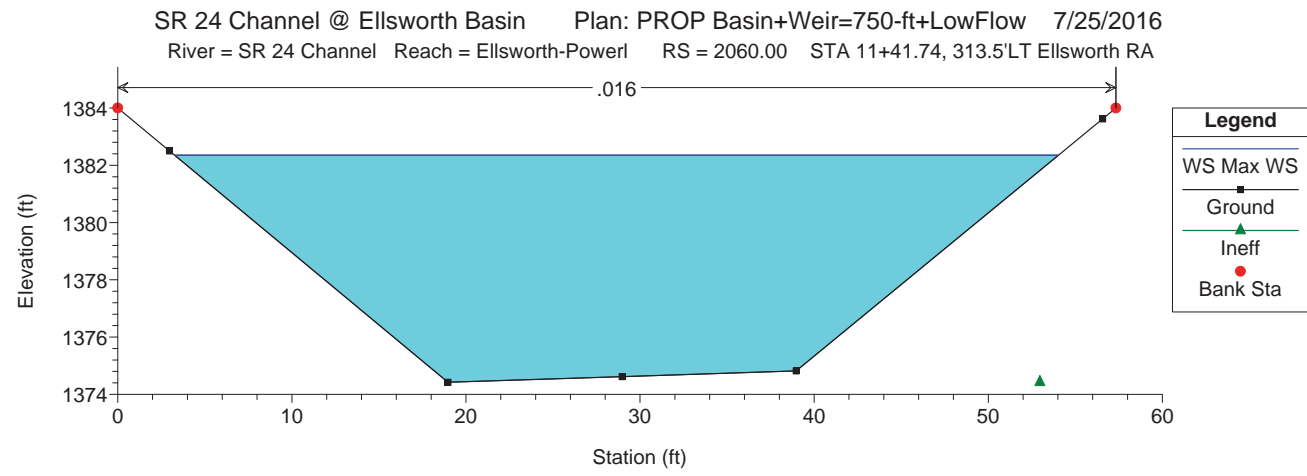
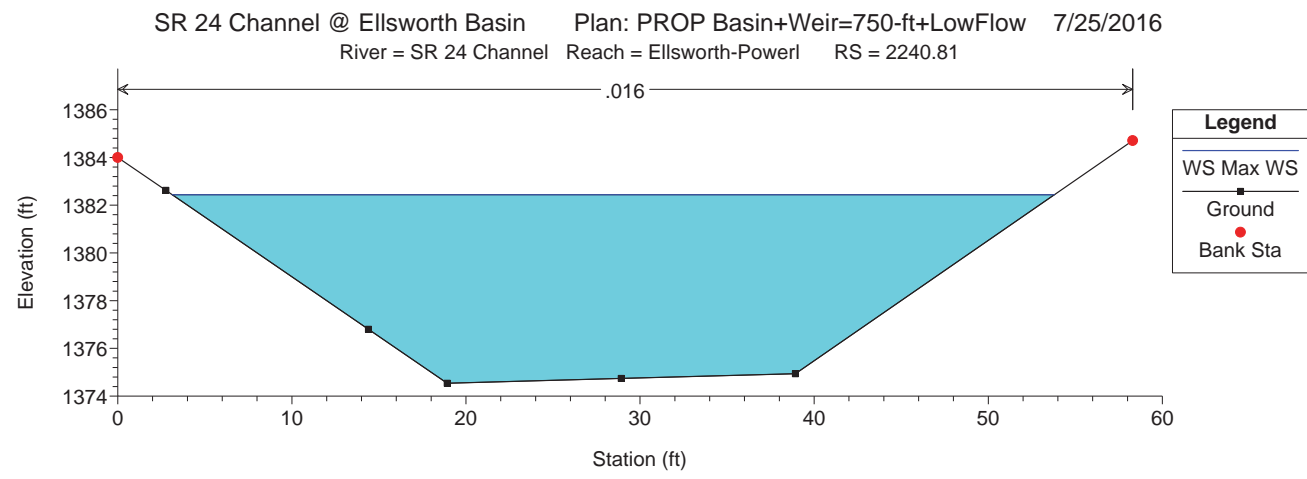
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Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Fr# Chl
Ellsworth-Powerl	3423	Max WS	1665.50	1375.37	1382.91		1383.57	0.000611	6.55	254.43	49.34	0.51
Ellsworth-Powerl	3367	Max WS	1659.00	1375.33	1382.88		1383.53	0.000603	6.51	254.88	49.38	0.51
Ellsworth-Powerl	3311	Max WS	1651.19	1375.29	1382.84		1383.49	0.000594	6.47	255.32	49.42	0.50
Ellsworth-Powerl	3311	Lat Struct										
Ellsworth-Powerl	3281	Max WS	1636.86	1375.27	1382.83		1383.47	0.000572	6.45	253.92	46.97	0.49
Ellsworth-Powerl	3241	Max WS	1622.50	1375.24	1382.83		1383.45	0.000554	6.35	255.35	47.09	0.48
Ellsworth-Powerl	3226.31*	Max WS	1620.16	1375.23	1382.82		1383.45	0.000550	6.34	255.68	47.11	0.48
Ellsworth-Powerl	3211.81*	Max WS	1615.91	1375.22	1382.83		1383.44	0.000544	6.30	256.32	47.16	0.48
Ellsworth-Powerl	3197.31*	Max WS	1608.87	1375.22	1382.82		1383.44	0.000539	6.28	256.39	47.18	0.47
Ellsworth-Powerl	3182.81*	Max WS	1602.68	1375.21	1382.82		1383.43	0.000532	6.24	256.84	47.21	0.47
Ellsworth-Powerl	3168.31*	Max WS	1596.74	1375.20	1382.82		1383.42	0.000526	6.21	257.26	47.25	0.47
Ellsworth-Powerl	3153.81*	Max WS	1586.92	1375.19	1382.82		1383.41	0.000516	6.15	257.83	47.29	0.46
Ellsworth-Powerl	3139.31*	Max WS	1585.49	1375.18	1382.83		1383.41	0.000513	6.14	258.28	47.31	0.46
Ellsworth-Powerl	3124.81*	Max WS	1577.41	1375.18	1382.82		1383.40	0.000507	6.10	258.42	47.35	0.46
Ellsworth-Powerl	3110.31*	Max WS	1574.11	1375.17	1382.82		1383.40	0.000502	6.08	258.85	47.38	0.46
Ellsworth-Powerl	3095.81*	Max WS	1570.51	1375.16	1382.82		1383.39	0.000497	6.05	259.39	47.43	0.46
Ellsworth-Powerl	3081.31*	Max WS	1562.19	1375.15	1382.82		1383.39	0.000490	6.01	259.77	47.45	0.45
Ellsworth-Powerl	3066.81*	Max WS	1562.99	1375.14	1382.83		1383.39	0.000488	6.01	260.28	47.47	0.45
Ellsworth-Powerl	3052.31*	Max WS	1556.77	1375.14	1382.82		1383.38	0.000484	5.98	260.37	47.51	0.45
Ellsworth-Powerl	3037.81*	Max WS	1555.86	1375.13	1382.82		1383.38	0.000480	5.96	260.97	47.54	0.45
Ellsworth-Powerl	3023.31*	Max WS	1544.96	1375.12	1382.83		1383.37	0.000471	5.91	261.41	47.58	0.44
Ellsworth-Powerl	3008.81*	Max WS	1542.83	1375.11	1382.82		1383.36	0.000468	5.89	261.73	47.61	0.44
Ellsworth-Powerl	2994.31*	Max WS	1534.51	1375.10	1382.83		1383.36	0.000458	5.84	262.67	47.66	0.44
Ellsworth-Powerl	2979.81*	Max WS	1517.50	1375.10	1382.85		1383.37	0.000442	5.75	263.91	47.73	0.43
Ellsworth-Powerl	2965.31*	Max WS	1497.19	1375.09	1382.88		1383.38	0.000422	5.63	265.82	47.84	0.42
Ellsworth-Powerl	2951	Max WS	1463.10	1375.08	1382.90		1383.38	0.000413	5.54	263.96	47.89	0.42
Ellsworth-Powerl	2941	Max WS	1423.13	1375.07	1382.81		1383.37	0.000609	6.02	236.26	47.73	0.48
Ellsworth-Powerl	2921	Max WS	1451.39	1375.06	1382.84		1383.30	0.000400	5.48	265.00	47.84	0.41
Ellsworth-Powerl	2841	Max WS	1389.33	1375.00	1382.81		1383.23	0.000360	5.21	266.78	48.03	0.39
Ellsworth-Powerl	2651	Max WS	1322.27	1374.87	1382.85		1383.21	0.000305	4.83	273.62	48.62	0.36
Ellsworth-Powerl	2641	Max WS	1337.98	1374.86	1382.78		1383.21	0.000420	5.26	254.46	48.51	0.40

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Fr# Chl
Ellsworth-Powerl	2621	Max WS	1379.98	1374.85	1382.78		1383.18	0.000334	5.05	273.03	48.59	0.38
Ellsworth-Powerl	2540	Max WS	1589.05	1374.79	1382.50		1383.07	0.000498	6.06	262.27	48.26	0.46
Ellsworth-Powerl	2451	Max WS	1602.69	1374.73	1382.43		1383.02	0.000530	6.14	260.93	50.03	0.47
Ellsworth-Powerl	2441	Max WS	1602.69	1374.72	1382.31		1383.02	0.000765	6.75	237.28	49.56	0.54
Ellsworth-Powerl	2440	Lat Struct										
Ellsworth-Powerl	2421	Max WS	1602.68	1374.70	1382.39		1382.98	0.000520	6.11	262.20	49.96	0.47
Ellsworth-Powerl	2241	Max WS	1602.59	1374.54	1382.31		1382.88	0.000502	6.03	265.59	50.16	0.46
Ellsworth-Powerl	2060	Max WS	1602.55	1374.42	1382.22		1382.78	0.000494	6.00	267.10	50.25	0.46
Ellsworth-Powerl	2040	Max WS	1602.64	1372.96	1382.29		1382.69	0.000324	5.06	316.51	55.56	0.37
Ellsworth-Powerl	1940	Max WS	1602.60	1371.42	1382.32		1382.61	0.000224	4.32	371.05	62.78	0.31
Ellsworth-Powerl	1925	Max WS	1602.59	1374.42	1382.06		1382.65	0.000536	6.18	259.40	49.74	0.48
Ellsworth-Powerl	1839	Max WS	1602.55	1374.26	1382.03	1379.38	1382.59	0.000501	6.03	265.84	50.26	0.46

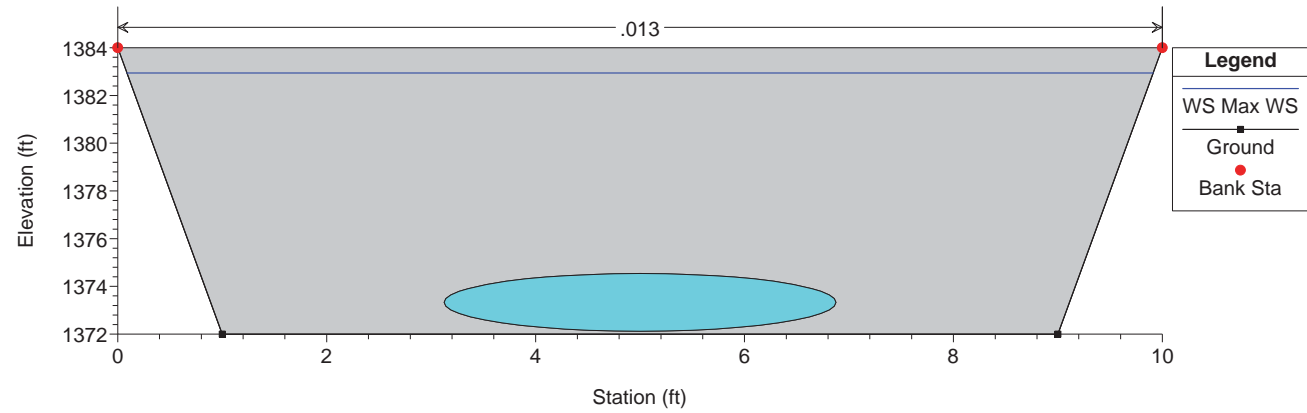






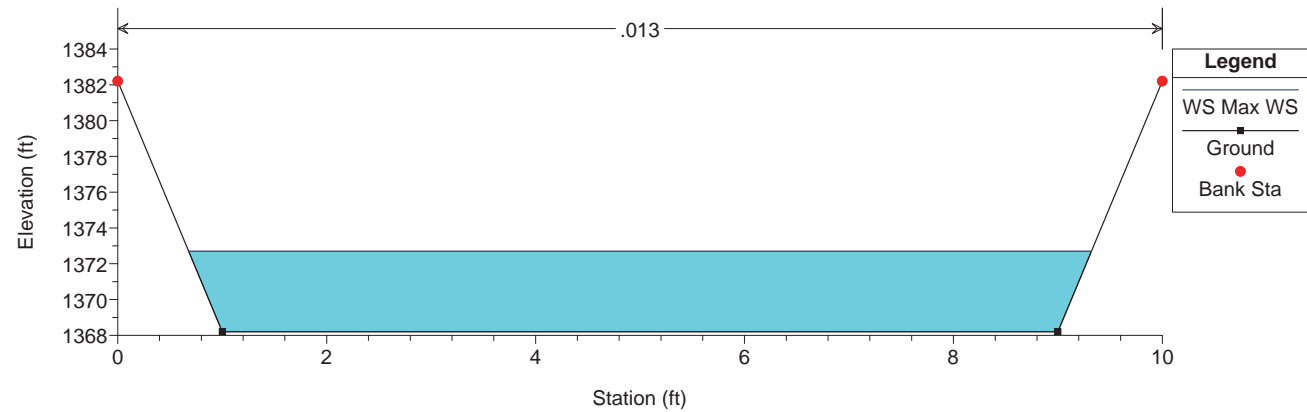
SR 24 Channel @ Ellsworth Basin Plan: PROP Basin+Weir=750-ft+LowFlow 7/25/2016

River = SR 24 Channel Reach = Ellsw.Bleedoff RS = 11.999 IS Proposed 36" RCP bleedoff pipe for the Ellsworth Basin that crosses



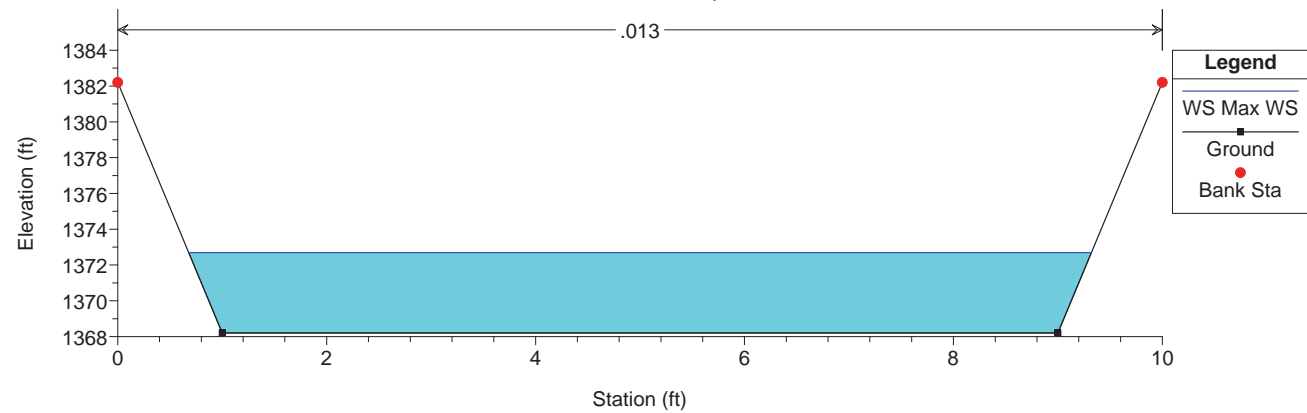
SR 24 Channel @ Ellsworth Basin Plan: PROP Basin+Weir=750-ft+LowFlow 7/25/2016

River = SR 24 Channel Reach = Ellsw.Bleedoff RS = 11 Dummy cross section to simulate the 36" bleedoff line outfall to



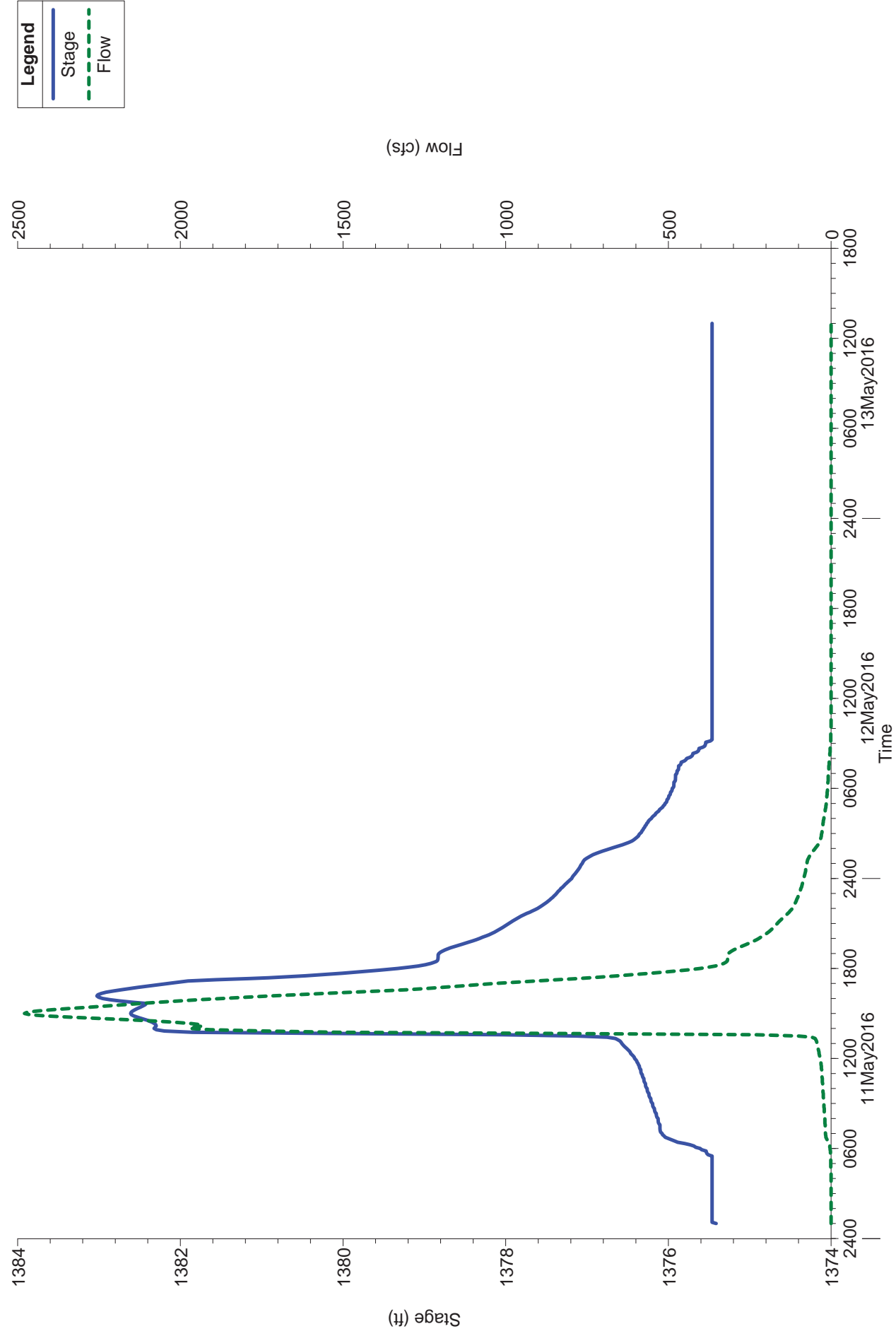
SR 24 Channel @ Ellsworth Basin Plan: PROP Basin+Weir=750-ft+LowFlow 7/25/2016

River = SR 24 Channel Reach = Ellsw.Bleedoff RS = 10 Dummy cross section to simulate the 36" bleedoff line outfall to

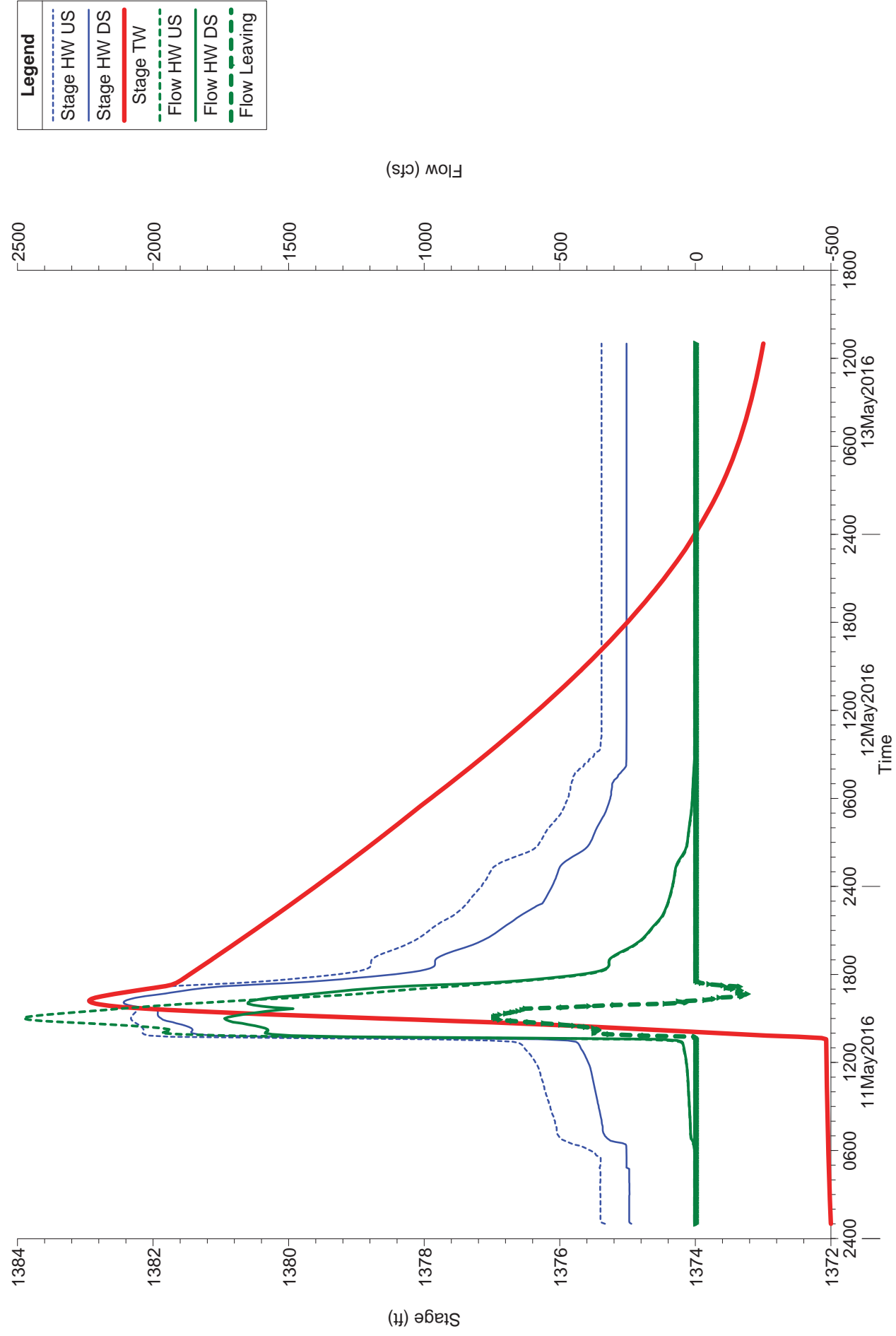


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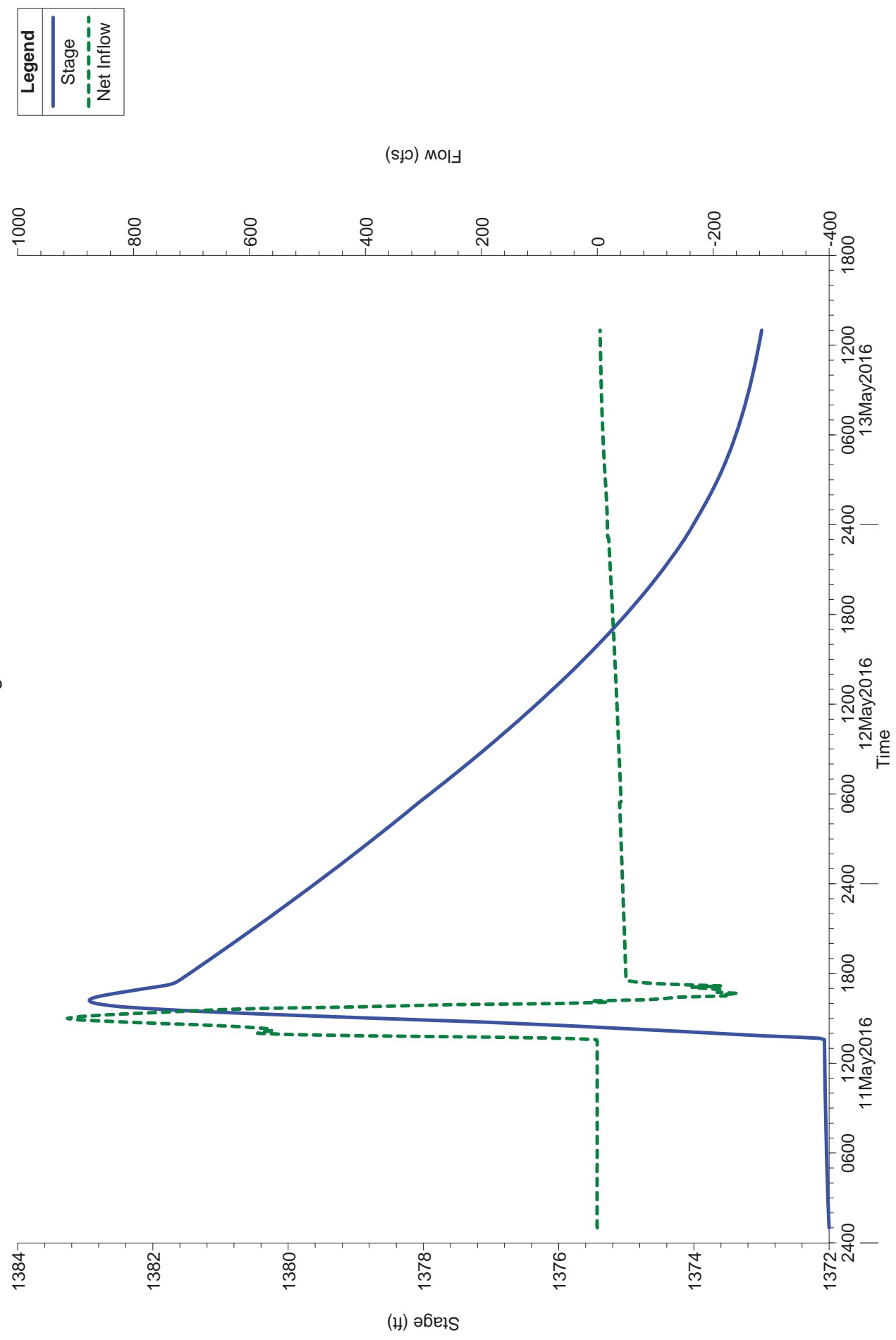
Plan: PB+750W+LF River: SR 24 Channel Reach: Ellsworth-Powerl RS: 3422.86



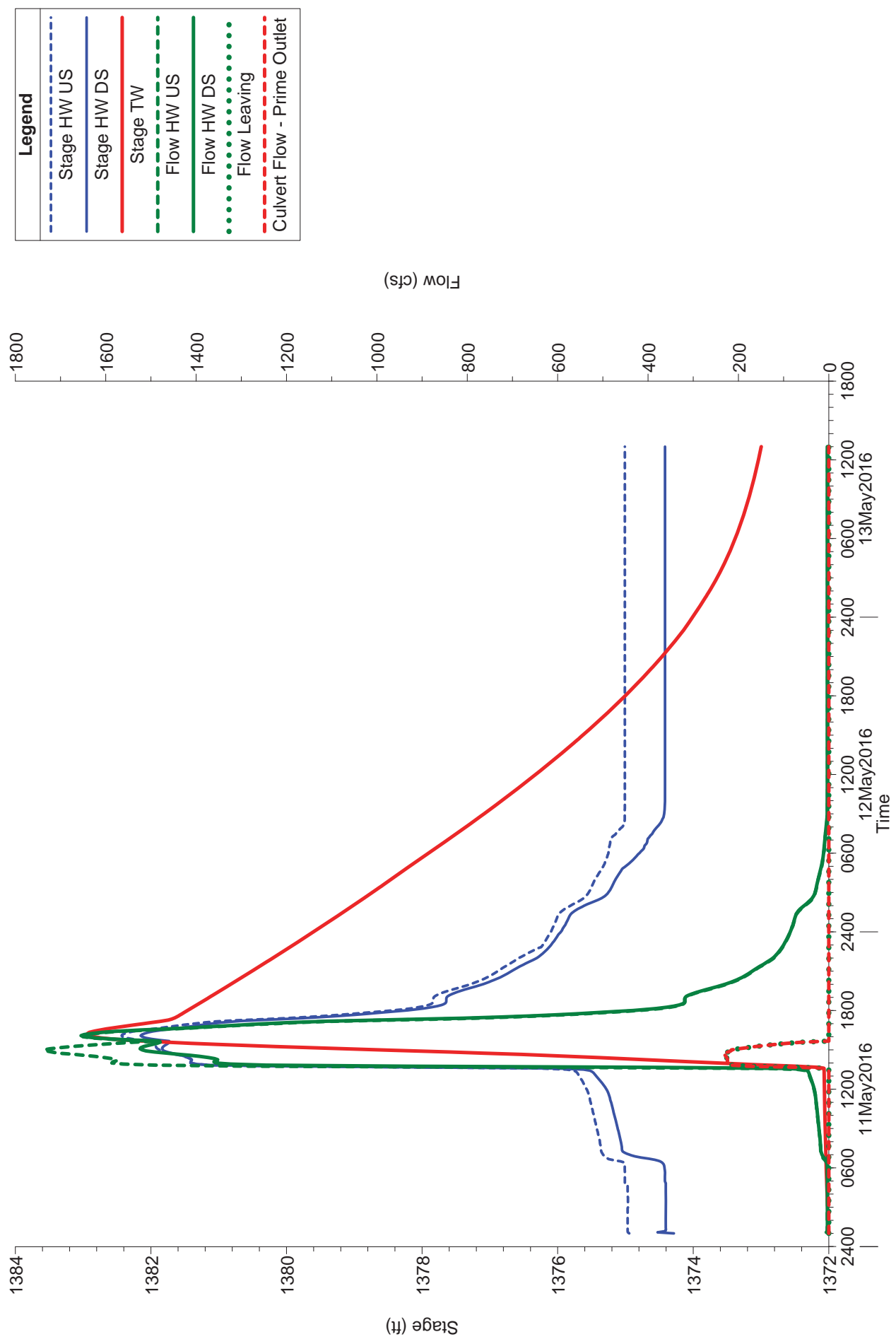
Plan: PB+750W+LF River: SR 24 Channel Reach: Ellsworth-Powerl RS: 3311.



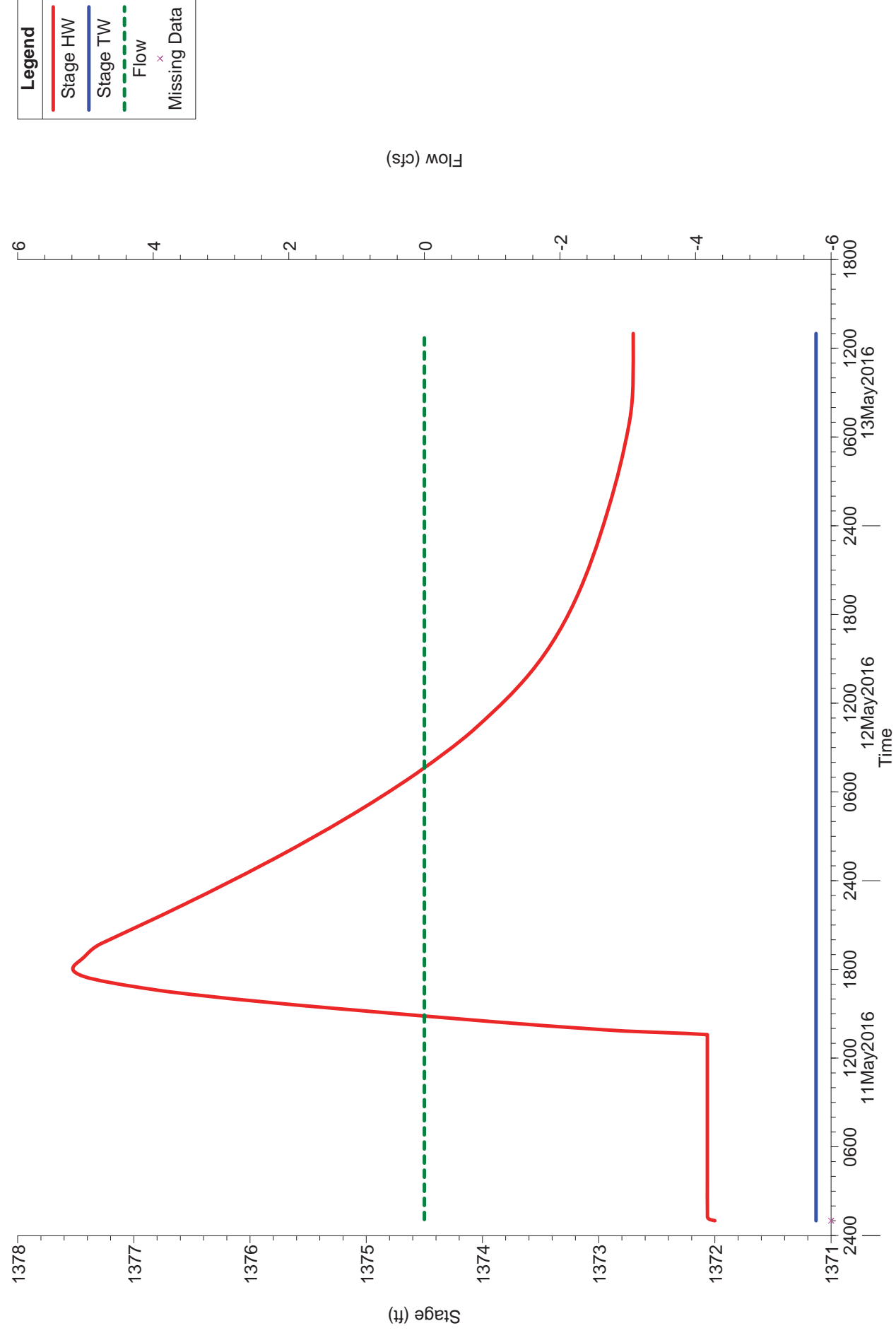
Plan: PB+750W+LF Storage Area: ELLSWORTH BASIN



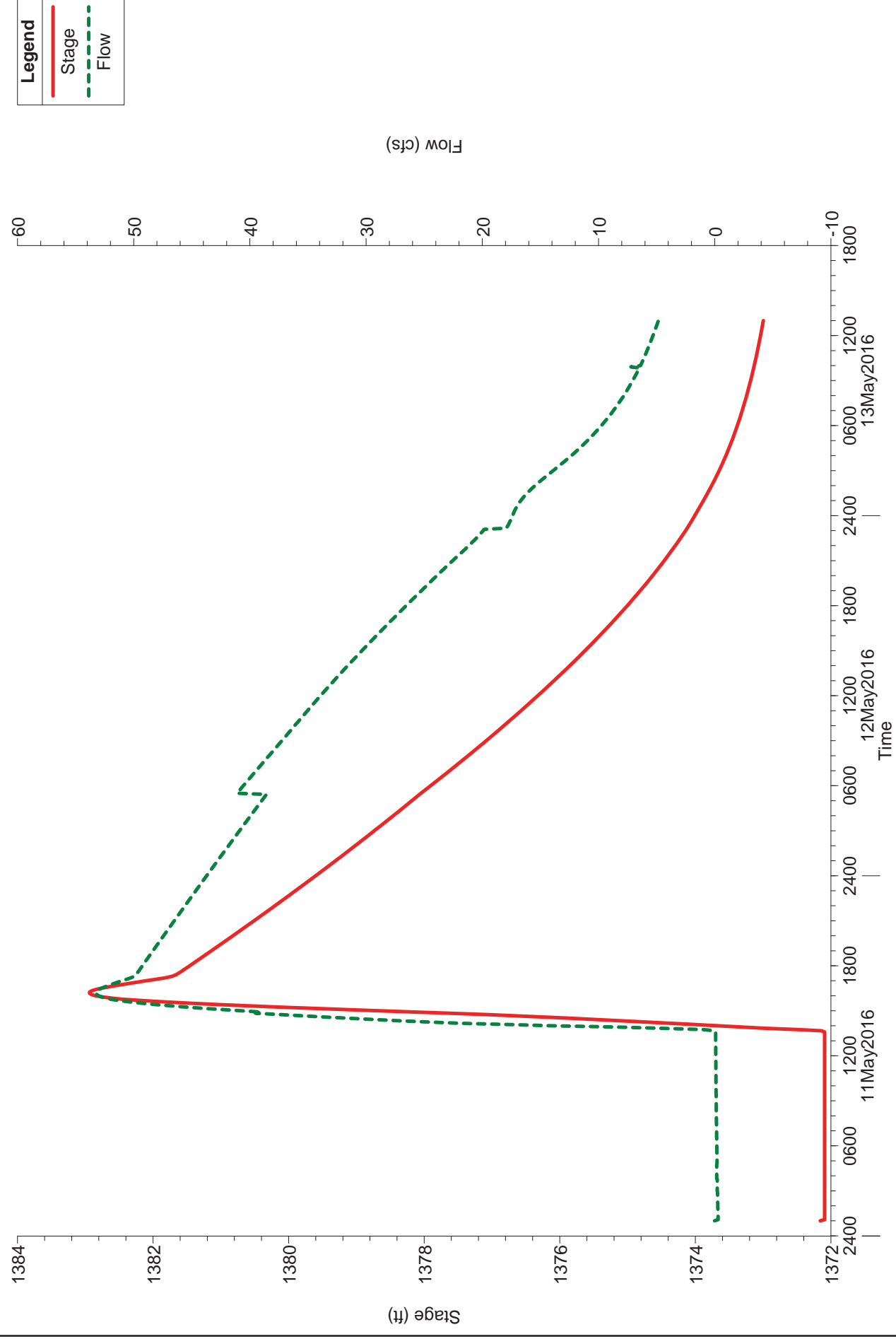
Plan: PB+750W+LF River: SR 24 Channel Reach: Ellsworth-Powerl RS: 2440



Plan: 10024INTIC SA Connection: ExstEliswOutfall



Plan: PB+750W+LF River: SR 24 Channel Reach: Elisw.Bleedoff RS: 13



COMPUTATION OPTIONS AND TOLERANCES

HEC-RAS Unsteady Computation Options and Tolerances

General (1D Options) | 2D Flow Options | 1D/2D Options

Unsteady Flow Options

Theta [implicit weighting factor] (0.6-1.0):	0.83	Number of warm up time steps (0 - 100,000):	0
Theta for warm up [implicit weighting factor] (0.6-1.0):	1	Time step during warm up period (hrs):	0
Water surface calculation tolerance (ft):	0.075	Minimum time step for time slicing (hrs):	0
Storage Area elevation tolerance (ft):	0.1	Maximum number of time slices:	40
Flow calculation tolerance [optional] (cfs):		Lateral Structure flow stability factor (1.0-3.0):	2
Max error in water surface solution (Abort Tolerance)(ft):	100	Inline Structure flow stability factor (1.0-3.0):	1
Maximum number of iterations (0-40):	40	Weir flow submergence decay exponent (1.0-3.0):	1
Maximum iterations without improvement (0-40):		Gate flow submergence decay exponent (1.0-3.0):	1
<input checked="" type="checkbox"/> Compute energy losses over junctions		DSS Messaging Level (1 to 10, Default = 4)	4

Geometry Preprocessor Options

Family of Rating Curves for Internal Boundaries

Use existing internal boundary tables when possible.

Recompute at all internal boundaries

1D Equation Solver

Skyline/Gaussian (Default: Faster for dendritic systems)

Pardiso (Optional: May be faster for large interconnected systems)

Number of cores to use with Pardiso solver: All Available

OK Cancel Defaults ...

UNSTEADY FLOW ANALYSIS SUMMARY (EXCERPT)

PLAN PROP Basin+Weir=750-ft+LowFlow

Unsteady Flow Analysis

File Options Help

Plan : PROP Basin+Weir=750-ft+LowFlow Short ID PB+750W+LF

Geometry File : PROP Basin+Weir=750-ft+LowFlow

Unsteady Flow File : 100-yr, 24-hr I(nterim)C(oncrete)

Plan Description :

A revised stage-volume curve of the Ellsworth Basin is simulated. The following assumptions are made:
 - The top of basin is raised to a minimum of 1384.00, as opposed to a minimum elevation of 1381.6 as existing in 2016. The maximum calculated volume is 135.1 ac-ft at elevation 1384.00.

Programs to Run

Geometry Preprocessor

Unsteady Flow Simulation

Sediment

Post Processor

Floodplain Mapping

Simulation Time Window

Starting Date: 11MAY2016 Starting Time: 0100

Ending Date: 13MAY2016 Ending Time: 1300

Computation Settings

Computation Interval: 15 Second Hydrograph Output Interval: 5 Minute

Mapping Output Interval: 1 Hour Detailed Output Interval: 5 Minute

Computation Level Output

DSS Output Filename: c:\Users\p004524B\Documents_PARSONS\PROJECTS\SR 24\HE

Mixed Flow Regime (see menu: "Options/Mixed Flow Options ...")

Compute

HEC-RAS Finished Computations

Write Geometry Information
Layer: Complete

Geometry Processor
River: SR 24 Channel RS: 1839.16
Reach: Ellsworth-Powerl Node Type: Cross Section
IB Curve:

Unsteady Flow Simulation
Simulation:
Time: 60.0000 13MAY2016 13:00:00 Iteration (1D): 0 Iteration (2D):
Writing Profiles 2900

Post Process
River: SR 24 Channel RS: 13
Reach: Ellsw.Bleedoff Node Type: Cross Section
Profile: 13MAY2016 1300
Simulation: 722/722

Computation Messages

Notes generated when writing the computation files:
User has selected to recompute all internal boundaries.

Plan: 'PROP Basin+Weir=750-ft+LowFlow' (EllsworthChan.p08)
Simulation started at: 13Jul2016 01:07:33 PM
Using 64 Bit Computation Engines

Writing Geometry
Computing XS Interpolation Surfaces
XS Interpolation Surfaces generated in 144 ms
Completed Writing Geometry

Geometric Preprocessor HEC-RAS 5.0.1 April 2016

Finished Processing Geometry

Writing Event Conditions
Event Conditions Complete

Performing Unsteady Flow Simulation HEC-RAS 5.0.1 April 2016

Initial Backwater, Split flow optimization, iteration 1
Maximum iterations of 40

	RS	WSEL	ERROR
11MAY2016 01:00:05 SR 24 Channel Ellsw.Bleedoff	13	1372.09	0.199
11MAY2016 01:00:10 SR 24 Channel Ellsw.Bleedoff	13	1372.09	0.104
11MAY2016 01:00:15 SR 24 Channel Ellsw.Bleedoff	13	1372.09	0.104
11MAY2016 01:00:20 SR 24 Channel Ellsw.Bleedoff	13	1372.09	0.104
11MAY2016 01:00:25 SR 24 Channel Ellsw.Bleedoff	13	1372.09	0.104
11MAY2016 01:00:30 SR 24 Channel Ellsw.Bleedoff	13	1372.09	0.104
11MAY2016 01:00:35 SR 24 Channel Ellsw.Bleedoff	13	1372.09	0.104
11MAY2016 01:00:40 SR 24 Channel Ellsw.Bleedoff	13	1372.09	0.104
11MAY2016 01:00:45 SR 24 Channel Ellsw.Bleedoff	13	1372.09	0.104

Pause Take Snapshot of Results Close

HEC-RAS Finished Computations

Write Geometry Information
Layer: Complete

Geometry Processor
River: SR 24 Channel RS: 10
Reach: Ellsw.Bleedoff Node Type: Cross Section
IB Curve:

Unsteady Flow Simulation
Simulation:
Time: 60.0000 13MAY2016 13:00:00 Iteration (1D): 0 Iteration (2D):
Writing Profiles 2900

Post Process
River: SR 24 Channel RS: 3422.86
Reach: Ellsworth-Powerl Node Type: Cross Section
Profile: 13MAY2016 1300
Simulation: 722/722

Computation Messages

****** Warning! Extrapolated above Cross Section Table at: ******

SR 24 Channel Ellsworth-Powerl from R.S. 2650.81 to 2640.81
SR 24 Channel Ellsworth-Powerl R.S. 2440.81

The maximum xsec wsel error was 0.199
SR 24 Channel Ellsw.Bleedoff 13 at 11MAY2016 01:00:05

**** The Model Has One Or More Warning(s) ****

Finished Unsteady Flow Simulation

Writing Results to DSS
Finished Writing Results to DSS

Reading Data for Post Process

Running Post Processor HEC-RAS 5.0.1 April 2016

Finished Post Processing

Computations Summary

Computation Task	Time(hh:mm:ss)
Completing Geometry	<1
Preprocessing Geometry(64)	<1
Unsteady Flow Computations(64)	16
Writing to DSS(64)	<1
Post-Processing(64)	10
Complete Process	28

Pause Take Snapshot of Results Close

Worksheet for New Bleedoff Line at Ellsworth Basin (Surcharged)

Project Description

Friction Method Manning Formula
Solve For Discharge

Input Data

Pressure 1 10.50 feet H2O
Pressure 2 4.50 feet H2O
Elevation 1 1372.12 ft
Elevation 2 1368.72 ft
Length 1500.00 ft
Roughness Coefficient 0.013
Diameter 36.00 in

Results

Discharge 52.80 ft³/s
Headloss 9.40 ft
Energy Grade 1 1383.49 ft
Energy Grade 2 1374.09 ft
Hydraulic Grade 1 1382.62 ft
Hydraulic Grade 2 1373.22 ft
Flow Area 7.07 ft²
Wetted Perimeter 9.42 ft
Velocity 7.47 ft/s
Velocity Head 0.87 ft
Friction Slope 0.00627 ft/ft

Worksheet for New Bleedoff Line at Ellsworth Basin (Gravity)

Project Description

Friction Method Manning Formula
Solve For Full Flow Capacity

Input Data

Roughness Coefficient 0.013
Channel Slope 0.00130 ft/ft
Normal Depth 3.00 ft
Diameter 36.00 in
Discharge 24.05 ft³/s

Results

Discharge 24.05 ft³/s
Normal Depth 3.00 ft
Flow Area 7.07 ft²
Wetted Perimeter 9.42 ft
Hydraulic Radius 0.75 ft
Top Width 0.00 ft
Critical Depth 1.58 ft
Percent Full 100.0 %
Critical Slope 0.00436 ft/ft
Velocity 3.40 ft/s
Velocity Head 0.18 ft
Specific Energy 3.18 ft
Froude Number 0.00
Maximum Discharge 25.87 ft³/s
Discharge Full 24.05 ft³/s
Slope Full 0.00130 ft/ft
Flow Type SubCritical

GVF Input Data

Downstream Depth 0.00 ft
Length 0.00 ft
Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 ft
Profile Description
Profile Headloss 0.00 ft
Average End Depth Over Rise 0.00 %

Worksheet for New Bleedoff Line at Ellsworth Basin (Gravity)

GVF Output Data

Normal Depth Over Rise	100.00	%
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	3.00	ft
Critical Depth	1.58	ft
Channel Slope	0.00130	ft/ft
Critical Slope	0.00436	ft/ft

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APPENDIX G
DRAFT INITIAL DCR REVIEW COMMENTS
AND RESOLUTIONS

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**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
in Maricopa County and Pinal County, Arizona**

TRACS No. H8915 01L/02L
Federal Project No. 024 A (200)

Draft IDCR Comment Response Document

ADOT Project Manager: Ronald McCally
Consultant: PARSONS

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			JOHN WENNES, ADOT ENVIRONMENTAL			
1	1	Pg. 1-1 Draft IDCR	MITIGATION MEASURES – Replace paragraph with the following text: “No updates at this time. As part of the Environmental Assessment Re-evaluation currently being prepared for this study, Mitigation Measures will be updated.”.	A	A	Will revise
2	2	Pg. 1-4 Draft IDCR	Section 1.3.3, <i>Second paragraph, second row</i> – include “of” after “the area north”	A	A	Will revise
3	3	Pg. 4-2 Draft IDCR	Section 4.4.1, <i>First paragraph, second row</i> – include “roads” after “planned”.	A	A	Will revise
4	4	Pg. 8-1 Draft IDCR	Section 8, <i>First paragraph</i> – replace all text with “Updates for the current study are in process.”	A	A	Will revise
			TED LEHMAN, JE FULLER - HYDROLOGY			
5	1	App. D, Draft Initial Drain. Report	Sub-basin E6a appears to have been left developed, while the report suggests it should have been reverted to undeveloped conditions	A	A	Will revise. The basin unit hydrograph was revised to reflect undeveloped conditions, but tests indicate further revisions are needed to simulate that condition appropriately

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6	2	App. D, Draft Initial Drain. Report	Sub-basins GM16-GM20 are combined downstream of the SR24 channel and detention basin. Review of the development plans, topography, and discussions between the Premier (working on the Ellsworth Channel realignment) and Parsons team members suggest that any outflow from these sub-basins is more likely to be collected by the new SR24 channel, probably near its intersection with Crismon Road.	A	A	Model has been revised
			TAMMY MIVSHEK, ADOT TRAFFIC ENGINEERING			
7	1	IDCR 4-4	4.4.2 Ellsworth Road Interim TI, it states "The traffic operational analysis indicates the intersections will operate at adequate capacity for the Interim Design Year 2025." In the Traffic Analysis Report on page 17, Table 5 it shows that the overall operation of the NB and WB approach the overall LOS for AM and PM Peak hours are at F(E) for NB and F(F) for WB for the SR 24/Ellsworth WB Ramp under Option A. Under Option B, the LOS during AM and PM Peak Hours is F(F) for the NB approach and F(F) for the WB approach at the WB Ramp per Table 7 on Page 19 of the Traffic Analysis Report. At present the intersection is operating under acceptable conditions with some delays in the turning movement.	B	A	The overall level of service is acceptable with the mitigated lane configurations shown in figures 6 and 7 of the report.

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8	2	IDCR 4-8	4.12 Freeway Signing and Pavement Marking, it states "A signing concept plan was developed to ensure an effective signing plan should be developed for the Preferred Interim Alternative." The Interim concept appears to be directed at the Ultimate condition and not the Interim. It doesn't make sense to sign for roads that don't exist yet. Also, would we want to have sign structures sitting out there without signs on them and to be sitting there for however long in between the interim and ultimate? What if during the Ultimate Design the structures are in the way of future sound walls, etc.	B	D	Even though some of the roads do not exist today, we are assuming they will be there at time of construction or soon after. For the DCR we will depict the striping as if the roads existing other than at Meridian.
9	3	IDCR 4-8	4.12 Freeway Signing and Pavement Marking. These are going to be at-grade intersections but I don't see any signing pertaining to the x-roads at the TIs. Only Ellsworth, Mountain and Ironwood are open but there is nothing showing what will be used in order to guide or control traffic on these roadways. The other roads for the x-roads may be used as turn around points for the Interim condition but again there is no traffic control or guide signing. For the roads that lead to nowhere it would also be a good idea for barricades to be placed at the end of the roadway.	B	D	We are updating the original DCR. The traffic plans were at the same level of detail. Intersections to be signalized except Meridian Road

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10	4	IDCR 4-8	4.13 Lighting and Traffic Signals. There were no comments made pertaining to the Interim condition. Is there lighting going to be placed on the Interim condition. It appears that the mainline will be divided without barrier put in place but lighting is not going to be placed on the ramps? Also, no mention of any signals in the Interim. The Ellsworth signal would need to be updated because of the new ramps. The end of roadway, whether it be Signal Butte, if that option is selected and the roadway built, or Ironwood, will lead into a roadway that will have traffic on it. Will traffic control be set up utilizing a signal light at that location? What about Mountain Road. What type of traffic control will be used on this roadway, a stop condition or a signal light. SR 24 will not be able to move freely through these locations.	A	A	We are adding Signals and Lighting. All cross roads will have signals with the ramps for the interim condition except for Meridian.
11	5	IDCR 4-8	4.14 Construction Phasing and Traffic Control. It may be advisable that an Emergency Management Plan be put into effect as well with the traffic control in order for emergency vehicles and personnel to enter into the construction area since there will be limited points in which to enter in case of an emergency. It probably would be helpful for emergency personnel to know where the access points would be to the project if something were to happen during construction of SR 24.	D	A	This appears to be a final design issue. Text will be included indicating an Emergency Management Plan needs to be prepared during final design.

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12	6	IDCR, App. C T-1.01	The raised pavement markers should all be Type C since there are median islands separating the traffic lanes on the x-roads. Type C should be used on all the lane lines. The spacing for the RPM's on the broken white should be at 40 ft. spacing and not 20 ft. spacing and on the turn lane lines they should be spaced at 20 ft. Also, Type D RPMs should also be used on the median island noses as per Std. Dwg. M-1 as well as the yellow paint.	A	A	Will revise.
13	7	IDCR, App. C T-1.01 - T-1.10	Ellsworth Rd Ramp "A" Connector is listed as "Future" per C-3.01. As far as the DCR is concerned all of the work will be done on the East of Ellsworth Rd. Why is there new sign panels and sign structure being placed for Ramp A depicting two lanes for WB L202 and one lane for NB L202. There is nothing in the DCR that states that this ramp will be widened to two lanes for WB direction during the Interim.	A	D	The connector ramp will not be constructed with interim project
14	8	IDCR, App. C T-1.01	Per the 1st paragraph under 4.4.2 Ellsworth Road Interim TI on Page 4-4 of the DCR it states, "For the interim condition, NB Ellsworth Road will be widened to add additional pavement for the future third through lane northbound." This 3rd lane in the NB direction was also depicted in Appendix C on sheet C-4.01 but is not shown on the pavement marking sheet T-1.01.	B	A	Discussion needed based on Traffic Operations at Ellsworth Road. The project team will meet with the City of Mesa to discuss the third left turn lane. The results of this meeting will impact the report. Meeting resulted in 2 Lt turn lanes at this location based on operations and maintenance preferred by the City of Mesa. Updates will reflect this.

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15	9	IDCR, App. C T-1.01 - T-1.10	Again many of the signs on here are more representative of the Ultimate condition and not of the Interim condition. We shouldn't be signing for roadways that do not exist at this time nor should we have signing such as "Right Lane Exit Only" signs in the interim. Some of the signs on these pages do not comply with the 2009 MUTCD or the current MOAS as shown.	A	A	Even though some of the roads do not exist today, we are assuming they will be there at time of construction or soon after. For the DCR we will depict the striping as if the roads existing other than at Meridian
16	10	IDCR, App. C T-1.01 - T-1.10	On the x-roads there is no signing shown or barriers for end of roadway conditions on the non-existent roads. On all of the x-roads, with the exception of Meridian Rd, it shows that the striping will match existing striping regardless of whether the road exists or not. At Meridian no striping is shown on T-1.08 even though on C-4.06 it shows a portion of the x-road will be built. In the interim the only roads in existence will be Ellsworth, Mountain, and Ironwood. The x-road sheets should be more representative of the conditions that will exist when the Interim project is completed. If the Interim conditions do include x-roads around SR 24 even though the roadways are not in place is beneficial to traffic who can use them to make turn around. It does not show on the x-roads if it will be free flow through them, stop condition, or signal light.	B	A	Even though some of the roads do not exist today, we are assuming they will be there at time of construction or soon after. For the DCR we will depict the striping as if the roads existing other than at Meridian. At the time of final design it will be determined which cross roads will be developed. We will add a discussion to the DCR.
17	11	IDCR, App. C T-1.01 - T-1.10	Why isn't there a W10-2 Expressway Ends XX Miles located on EB SR 24 before Ironwood?	B	A	Warning and regulatory signs will be freeway size and not expressway size.

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18	12	Traffic Analysis Report	On Page 6, 1st Paragraph under Existing Intersection Configuration it states that the NB approach on Ellsworth consists of four through lanes at the EB off-ramp. Technically there are four lanes going through this intersection but in reality there are only two through lanes. The other two lanes are actually two left turn storage lanes for the WB on-ramp.	A	A	The text of the report will be updated to clarify that two left turn lanes are queue storage for the northbound left turn lanes at the intersection of Ellsworth Road and SR 24 EB Ramps.
19	13	Traffic Analysis Report	On Page 8 the left turn arrow in Figure 1A is missing.	A	A	The figure will be corrected.
20	14	Traffic Analysis Report	On Page 9, it appears that the data in Table 2 is backwards for 1A and 1B.	A	A	The figure will be corrected.
21	15	Traffic Analysis Report	On Page 9 in the first sentence of the 2nd paragraph under Crash Analysis it states, " identified a one-year total of 24 crashes (without any fatalities) on 24 from Loop 202 . . ." Should it not say " identified a one-year total of 24 crashes (without any fatalities on SR 24 from Loop 202. . ."	A	A	The table will be corrected.
22	16	Traffic Analysis Report	On Page 11 under Projected Segment Traffic Volumes, it states an "end of freeway" condition. Ellsworth is the "end of freeway" condition and Signal Butte in Option B or Ironwood in Option A would be an "end of expressway" condition. Per the ADOT Roadway Design Guide (2012), "Full access control gives preference to through traffic by providing access only through selected public roads and by prohibiting at-grade crossings or direct access from abutting property. Partial access control still gives preference to through traffic but permits some crossings at grade	B	A	The report will be updated to state that Ellsworth Road is an end of expressway condition in Option A.

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23	17	Traffic Analysis Report	and some private driveway connections." The 2009 MUTCD defines a Freeway as a divided highway with full access control and an Expressway as a divided highway with partial control of access. "End of freeway" exists at Ellsworth Rd with the at-grade signalized intersection. In the Interim SR 24 could only be labeled as an Expressway with the at-grade intersections with partial controlled access from Ellsworth Rd to Signal Butte Rd/Ironwood Rd, depending on the Option selected.	B	A	The project team will evaluate the recommended intersection geometry at the intersection of Ellsworth Road and SR 24 WB Ramp due to the impact to the SR 24 EB on ramps and Ellsworth Road. Pavement widening on Ellsworth Road is to accommodate the 12-foot lane shift of the existing NB through lanes. The additional pavement width will be used for the third northbound left turn lane.
24	18	Traffic Analysis Report	Currently Signal Butte Rd does not exist in the area of SR 24. From what I understand in the DCR under Option A that this road will not be built by 2025. Under Option B it would become the logical terminus but would still have to be built. Why is it under Option A that you are showing through movements NB and SB through the intersections to a nonexistent road?	B	D	Signal Butte Road is expected to be built at time of construction or soon after. We are showing the ultimate striping, Final Designer will provide appropriate striping at time of construction. City of Mesa is planning to construct Signal Butte Road from Ray Road to Pecos Road.
25	19	Traffic Analysis Report	In Figure 4 and Figure 5, on the diagram you are showing Meridian Rd as Moeur Rd.	A	A	Will change

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26	20	Traffic Analysis Report	On Page 18, 20, Figure 6, and Figure 7 for the Mitigated intersections, adding a third left turn lane for the WB on ramp at Ellsworth would improve the level of service for Option A and Option B but there are other factors that also need to be considered. By adding the third left turn lane this would mean widening Ellsworth Rd with another lane on top of the third NB through lane. Also, the WB on-ramp would need to be widened to three lanes from the existing two in order to accommodate the third left turn lane. By adding the third lane on the ramp there would need to be enough room in order to merge that third lane prior to Ramp A or leaving the third lane as the Ramp A lane from the Ellsworth intersection.	B	A	The project team will evaluate the recommended intersection geometry at the intersection of Ellsworth Road and SR 24 WB Ramp due to the impact to the SR 24 EB on ramps and Ellsworth Road. Pavement widening on Ellsworth Road is to accommodate the 12-foot lane shift of the existing NB through lanes. The additional pavement width will be used for the third northbound left turn lane. Ellsworth Road will not be widened to three through lanes. The WB on ramp would need to be widened to add an additional lane.
27	21	Traffic Analysis Report	Figure 7, the proposed lane configuration diagrams label 3A and 3B as Ironwood Dr when they should be Signal Butte Rd.	A	A	The figure will be corrected.
28	22	Traffic Analysis Report	Page 26 under 2025 Option A Scenario, 1st paragraph Ironwood Rd would not be an "end of freeway" but an "end of expressway" condition. Also it states that Mountain Rd would be "grade separated" over SR 24 but in the next paragraph it states, "Grade separation of interchanges is not recommended in the 2025 Option A scenario." Maybe it should be re-stated that all other interchanges besides Mountain Rd will not be grade separated.	D	A	Mountain Road will not be an interchange. It will just be a grade separated crossing. It will not have direct access to SR-24 The text will be clarified to better explain why Mountain Road isn't a TI.
29	23	Traffic Analysis Report	Page 27, third paragraph under 2025 Option A Mitigated Analysis, third line states, "...ramp through movement During AM both peak hour." Please clarify.	A	A	The report will be updated to state that the northbound left turn turning movement conflicts with the westbound ramp movements. The word "through" will be deleted.

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30	24	Traffic Analysis Report	Page 27 under 2025 Option B Scenario, 1st paragraph, Signal Butte would be "end of expressway" condition and not "end of freeway."	B/C	A	The report will be updated to designate that Signal Butte Road will be an "end of expressway" condition.
			EUNICE CHAN, FHWA			
31	1	Pg 3, Traffic Analysis Report	2025 Opt A Mitigated Analysis references expected delays for the NB left turn movement at the intersection of Ellsworth Rd and WB SR24 Ramps and no further mitigation is recommended. a. Include discussion of the severity of the impact to justify the recommendation for no mitigation. Appendix H seems to indicate that even with the mitigation measures, there will be a 76.8 s/veh delay for the NBL movement on Ellsworth and SR 24 WB Ramps, and a 102.9 s/veh delay for the EBT movement on Ellsworth Rd and SR 24 EB Ramps.	B	A	The predicted overall level of service for the 2025 Option A mitigated condition is level of service D or better. The predicted delay for northbound left turning vehicles is in the AM peak hour only. For intersection with heavy through movements, turning movement delays in the peak hour are not uncommon.
32	2	Pg 4, Traffic Analysis Report	2035 Horizon Year – mentions that vehicles are expected to queue on the westbound on ramp and northbound left turn lane at the intersection of Meridian Rd and SR 24 WB Ramps and no mitigation is recommended. a. Include discussion of the severity of the impact to justify the recommendation for no mitigation. For example, Appendix K indicates LOS F during peak hours for the NBL in 2035, but the delay is only 58.1 s/veh.	B	A	The predicted overall level of service for the 2035 horizon year is level of service D or better. The predicted delay for northbound and westbound turning vehicles is in the AM peak hour only. For intersection with heavy through movements, turning movement delays in the peak hour are not uncommon.

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33	3	Pg 6, Traffic Analysis Report	Existing Roadway Network – Include sentence on posted speed limit for Meridian Road.	A	A	The report will be updated.
34	4	Pg 11, Traffic Analysis Report	Design Concept Report Alternatives and Projected Segment Traffic Volumes discussions appear to be the same?	A	A	The report will be updated.
35	5	Pg 17, Traffic Analysis Report	Table 5: a. Clarify "recommended lane configurations" in the first sentence. Figure 6 only labels the "Mitigated" configurations. Are the recommended lane configurations the ones that are unlabeled? b. Include discussion of the severity of unmitigated peak hour delays (Appendix G). For example, not incorporating the recommended mitigation would result in LOS F with a delay of 137.2 s/veh for the NBL and 564.1 veh/s for WBT at the intersection of Ellsworth Rd and SR 24 WB Ramps.	A B	A A	a. Table 5 refers to the unmitigated lane configurations. The text and figures will be updated. b. Table 5 refers to the unmitigated lane configurations. An alternative analysis is shown in Table 6 with the mitigated levels of service. Discussion referring to Table 6 and the mitigated analysis will be added to this section.
36	6	Pg 18, Traffic Analysis Report	Table 6 – See comment 1. Table shows LOS C for EB through movements at Ellsworth Rd and EB SR 24 Ramps. But Appendix H shows LOS F?	A	A	Table will be updated.
37	7	Pg 19, Traffic Analysis Report	Table 7 – See comment 5.a.	A	A	Table 7 refers to the unmitigated lane configurations. The text and figures will be updated.

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38	8	Pg 21, Traffic Analysis Report	Table 9 – See comment 2.a.	A	A	Table 9 refers to the unmitigated lane configurations. The text and figures will be updated.
39	9	Traffic Analysis Report	Figure 6 - Didn't see a difference between the original and the mitigated configuration for 3A or 3B? What was the mitigation?	A	A	The mitigated lane configuration at Signal Butte Road and SR 24 WB off ramps is three (3) northbound left turn lanes. The figure will be updated.
40	10	Traffic Analysis Report	Figure 8 – Reason for calling out the lane configurations on Meridian Rd and not for the other crossroads?	D	D	The lane configuration was shown on Meridian Road to clarify a six lane cross section north of SR 24 and a four lane cross section south of SR 24.
41	11	Pg 3-1, Draft IDCR	a. Provide description of Tier 1 analysis and background on why it was not used for evaluating the four alternatives. b. Section 3.3.2 Description of Alternatives should reference or include typical sections of each alternative.	D	D	a. Tier 1 analysis was used for determining the SR 24 Corridor Alignment in the original DCR. b. Will include typical sections of each
42	12	Pg 3-2, Draft IDCR	a. Was Alternative B removed from consideration for reasons other than the feasibility of the traffic operation analysis? b. Clarify last sentence under subheading, "Compatibility with Ultimate."	D	D	a. That and the compatibility with the ultimate. b. Will clarify

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OVERALL COMMENT NO.	REVIEWER COMMENT NO.	DWG, SHT, PAGE NO.	COMMENT	INITIAL CODE	FINAL CODE	DESIGNER RESPONSE
43	13	Pg 3-3, Draft IDCR	a. Traffic Analysis – All alternatives would operate at a similar Level of Service, which is -? Provide additional discussion. b. Suggest including a table that shows how each of the four alternatives quantitatively addresses the primary objectives of the evaluation criteria as part of the Tier 2 evaluation process. While this is generally discussed per alternative, it is not presented in a way that allows comparison of similarities and differences between the alternatives and the extent to which they meet (or don't meet) the primary objectives. c. Second sentence under "Development Impacts" should include "of" between "amount" and "area" d. Under "Estimated Construction Cost" subheading, the Alternatives in the second paragraph should be capitalized for uniformity (see also para 4.5 on pg 4-5). • What were the costs for each alternative? It appears that only the estimated cost for the preferred alternative is given (pg. 5-1).	D	D	a. Our scope was to update the existing DCR therefore was structured to provide a traffic analysis on the selected alternative. b. Will add table c. Will revise d. Will revise • Our scope was to update the existing DCR therefore was structured to provide a traffic analysis on the selected alternative.
44	14	Pg 4-2, Draft IDCR	Include discussion of number of GP lanes in the WB direction under subheading, "SR 24 Interim Westbound Mainline."	A	A	Will add two GP lanes

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**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
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TRACS No. H8915 01L/02L
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Consultant: **PARSONS**

OVERALL COMMENT NO.	REVIEWER COMMENT NO.	DWG, SHT, PAGE NO.	COMMENT	INITIAL CODE	FINAL CODE	DESIGNER RESPONSE
45	15	Pg. 4-4, Draft IDCR	4.4.5 Signal Butte Road Full Diamond TI 1. General note: in order for Signal Butte to be the logical terminus, City of Mesa needs to include improvements in the STIP (to the north and south) to ensure Signal Butte can handle the end of freeway traffic	A	A	Text will be added to denote the City of Mesa needs to include improvements.
46	16	Pg. 4-7, Draft IDCR	Section 4.8.4 Noise Walls notes no updates. Verify if any updates/additional mitigation measures are needed to reflect the change from a depressed freeway to an at grade or above grade freeway between Williams Field Rd and Ironwood and the change from at grade to above grade bridges at Crimson and Mountain.	B	C	Decision from FHWA pending. Depending on outcome ADOT would prepare a Hot Spot or noise wall Analysis if needed.
47	17	Pg. 5-2, Draft IDCR	a. Does the project wide erosion control (1%) cover permanent erosion control measures or just BMPs during construction? Verify whether permanent seeding for all disturbed areas is included within this 1% or include a line item in the cost estimate as there will be no landscaping under the interim condition. b. Ensure all existing pedestrian features within the interim scope of work/project limits are upgraded, if needed, and any new features designed to meet ADA/PROWAG.	B A	A A	a. Will add seeding item b. Will add a statement regarding upgrading existing facilities to meet ADA/Prowag

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KEN AKOH-ARREY, ADOT DRAINAGE						
OVERALL COMMENT NO.	REVIEWER COMMENT NO.	DWG, SHT, PAGE NO.	COMMENT	INITIAL CODE	FINAL CODE	DESIGNER RESPONSE
48	1	App. D, Draft Initial Drain. Report	Existing condition HEC-1 Schematic is not matching the input in HEC-1 output. Sub-basin labels such as P1, P2, etc., are not on the schematic. Is there another schematic which should have been included? In fact, the labels on this schematic map are only of the E-series.	A	A	The ADMPU schematic will be included for reference. The project Schematic represents only the watershed pertaining to SR 24, which was revised for the project (see Section 4.4, Draft Initial Drainage Report). The Hydrologic model includes the entire East Mesa ADMPU area, incorporating E, P and R sub-basin groups. The ADMPU model was maintained intact in its coverage to ensure that the revised information is available to FCDMC and City of Mesa for further updates as a comprehensive regional tool.
49	2	Pgs 21-22, Draft Initial Drain. Report	The Interim option – the Baseline option, modeled with existing condition will convey more flow than any of the three ultimate condition options that were eliminated from consideration. However, Figure 6 is not showing a pump station as shown for those three options. Will this option get by without a pump station? How so? What is different?	A	A	The interim and revised ultimate roadway profiles are fully above ground and the pump station is not needed in any of the options that were analyzed. The reference to a pump station in the exhibits is incorrect and it was removed.
50	3	Pg 27, Draft Initial Drain. Report	Section 4.6 - This section should include discussion on the pump station as a conceptual design appurtenant that supplements the performance of the channel, if there is going to be one.	D	D	The pump station is not needed.
51	4	Pg 27, Draft Initial Drain. Report	Section 4.6 - The second bullet states that flow from PPGN (Wood Patel, 2014) in excess of the 100-year, 24-hr storm would flow across Ellsworth Rd. to the Ellsworth Retention Basin and fill it up limiting the flow that can be clipped from the channel's hydrograph for attenuation. Is this a potential problem? What is the recommended solution so that more discharge is not sent downstream than is being intended?	D	D	Note that the statement refers to "flows in excess of the 100-year, 24-hour event", which is a condition in excess of the design and is applicable for extreme events only. At the moment this is an assumption, as the PPGN development is in very early stages of planning and a detailed grading plan is not available to indicate the location where emergency flows would leave the development.

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		MIKE DUNCAN, FLOOD CONTROL DISTRICT OF MARICOPA COUNTY			
52	1	App. D - Draft Initial Drain. Report HEC-1 model output, for run of 01DEC15 14:28 The flows from the SR24 channel and the Ellsworth Basin area are: "802ELS", "G19E26", and "G17E26", which are 1,876 cfs + 182 cfs + 0 cfs = 2,058 cfs, which exceeds the 1,650 cfs criteria of Section 4.6, page 27 of the report.	A	A	The analysis in the Draft Initial Drainage Report was done for a detention volume of 96 ac-ft. Approximately 109 ac-ft of detention volume is needed to attenuate the peak flow to 1,650 cfs. An area suitable for detention has been identified at Ellsworth Rd, Ramp C, which could provide the additional volume.
53	2	App. D - Draft Initial Drain. Report Line 1242, page 29, of the HEC-1 output has: DT 1650UP 96.0 0.0 Which means that the diversion is limited to 96 acre-feet, but section 4.6 of the report mentions 100 acre-feet.	A	A	See response to Comment 52/1
54	3	Draft Initial Drain. Report The report does not address or show that the Powerline Floodway (and downstream East Maricopa Floodway) is not negatively impacted by the drainage system that encompasses the SR24 channel and the Ellsworth Basin.	B	A	The impact is being assessed based on the hydrology and the conceptual design work for the Ellsworth Channel Relocation, which followed the SR 24 hydrology.
55	4	App. D - Draft Initial Drain. Report HEC-1 Schematic - At the upper left there are two concentration points shown with the same label CPE26A	A	A	Duplicate label was deleted
56	5	Sht. D-1.03, Plans The bottom width for the proposed, modified Powerline Floodway channel is 55 feet. What is the design basis for this?	B	A	The impact is being assessed based on the hydrology and the conceptual design work for the Ellsworth Channel Relocation, which followed the SR 24 hydrology.

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57	6	Sht. C-4.07, Plans The box culvert under Ironwood Dr is shown as 2 @ 8' x 6'. This should be 3 @ 8' x 8' to match the same culvert shown on sht. C-3.35.	A	A	Will adjust
58	7	Sht. D-1.01, Plans Are there any supporting analyses to show that the approx. 750 ft. long lateral weir and 4 barrel box culvert will function as expected to meet the overall peak outflow criteria?	B	A	Analysis is in progress and will be made available with the Initial Drainage Report. Analysis included in drainage report.
59	8	Sht. D-1.02, Plans The typical section uses B for top width while the table below uses T.	A	A	Will adjust
60	9	All sheets, Plans Refer to Ironwood Road but it should be Ironwood Drive.	A	A	Will adjust
61	10	Sht. D-1.03 The channel side slopes are shown as 1.5:1. For the subject major re-construction of the Powerline Floodway, side slopes of 2:1 would be the steepest allowed by FCDMC.	A	A	Will adjust

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		JEFF SHELTON, FLOOD CONTROL DISTRICT OF MARICOPA COUNTY				
62	1	App. D, Draft Initial Drain. Report	HEC-1 model 24INT100C.dat. Comparison of EMADMPU hydrology to SR-24 hydrology and the effect on the EMF. The hydrograph at CPEMF1 from model 24INT100C.dat was added to a hydrograph from PVR with peak of 600 cfs. This was then input into an unsteady EMF HEC-RAS model that was developed by the FCD to evaluate the levee status of the channel. The hydrographs for CPEMF1 and PVR were added together for the existing and future EMADMPU models and input into the unsteady EMF model for comparison to 24INT100C.dat. The results indicate that your current plan would produce water surfaces 1.37 feet higher than the future EMADMPU model in the EMF at the Powerline Floodway. Average increases of approximately 0.5 feet occur for miles up and down stream of the confluence. The results also indicate that your current plan would produce water surfaces 0.16 feet higher than the existing EMADMPU model in the EMF at the Powerline Floodway. Your model also produces reductions in the water surface for miles downstream of the confluence (see attached spreadsheets). The EMF HEC-RAS model and other supporting calculations will be provided upon request.	A	A	FCDMC provided the regional model. The material will be referenced and the effects of the added SR 24 flows described in the Initial Drainage Report.
63	2	App. D, Draft Initial Drain. Report	HEC-1 model 24INT100C.dat. Function of basin at Ellsworth Road and SR-24. The calculations in HEC-1 (802ELS) that represent the offline basin at Ellsworth are so basic that they might not adequately give a rough estimation of the effect the SR-24 drainage system has on the Powerline Floodway and EMF.	B	A	The level of hydraulic modeling involved is complex and is dependent of an advanced design stage that was not scoped for the IDCR phase of the project. The detention basin operation is being refined, but at a simplified level.

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		MARIA DEEB, CITY OF MESA				
64	1	Pg. 1-1 Draft IDCR	Programming, Paragraph two - Define acronym: Regional Transportation Plan Freeway Program	A	A	Will define
65	2	Pg. 1-1 Draft IDCR	Mitigation Measures, Paragraph one - I will suggest not using the words: "no updates" The mitigation language currently used by ADOT has changed since 2010. Also, the concept includes updated locations for drainage structures, therefore related mitigations be required? these might affect level of impact and impact locations. And have the noise and air quality conformity runs been completed? HPT completed? Will updates only occur during design and not at this DCR stage? Suggest text with clarification if not updates are to be done at this time but will during the design phase.	A	A	Will provide updates if available at time of final DCR submittal or provide statement regarding the update to the Environmental Evaluation and mitigations
66	3	Pg. 1-3 Draft IDCR	Provide a color label that explains the pink vs. blue colors.	A	A	Will add
67	4	Pg. 1-4 Draft IDCR	Section 1.3.1, Paragraph one - Within Mesa: per the Mesa 2040 Transportation Master Plan (page 81) it is a 6L arterial separated by raised medians from Southern Avenue to Pecos Road, then a 4L with raised medians to Germann Road (medians page 77)	A	A	Will update to further extents
68	5	Pg. 1-4 Draft IDCR	Section 1.3.1, Paragraph two - Within Mesa: per the Mesa 2040 Transportation Master Plan (page 81) it is a 6L arterial separated by raised medians from Ellsworth Road to Crismon, then a 4L with raised medians to Meridian Road (medians page 77)	A	A	Will update to further extents

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69	6	Pg. 1-4 Draft IDCR	Section 1.3.1, Paragraph three - 4 lane per the 2040 plan	A	A	Will adjust Crismon Rd to 4 lanes with raised median
70	7	Pg. 1-4 Draft IDCR	Section 1.3.1, Paragraph four - medians are required on all legs of arterials to arterials, raised medians are proposed for SB from north of Williams Field to Pecos Roads	A	A	Will update to further extents (Comment 67)
71	8	Pg. 1-4 Draft IDCR	Section 1.3.1, Paragraph six - classified as 6L except in segment from south of Guadalupe Road to Williams Field Road where it is a 4L	A	A	Will update to further extents (Comment 67)
72	9	Pg. 1-4 Draft IDCR	Section 1.3.1, Paragraph six - medians are required on all legs of arterials to arterials, raised medians are proposed for Meridian from north of Williams Field to Pecos Roads	A	A	Will update to further extents (Comment 67)
73	10	Pg. 1-5 Draft IDCR	Section 1.3.6, Drainage - suggest including comment: "see detailed drainage report".	A	A	Will add
74	11	Pg. 4-1 Draft IDCR	Section 4.2, Table 1 - typo	A	A	Will fix spelling of Clearance
75	12	Pg. 4-1 Draft IDCR	Section 4.2, Table 2 - typo	A	A	Will fix spelling of Clearance
76	13	Pg. 4-2 Draft IDCR	Section 4.3, SR 24 Interim Freeway Concept - Can we add language in the introduction section that references: The interim concept will include accommodation for a trail; the City may open it prior to the freeway's ultimate construction.	A	A	Will add

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77	14	Pg. 4-8 Draft IDCR	Section 4.11.3, Landscaping - The interim landscape should support the construction of a shared use pathway.	B/C	A	We will reference seeding on the trail
78	15	Pg. 4-9 Draft IDCR	Section 4.15.1, FMS Communications and Trunk Line - Should the foundation/infrastructure be constructed with interim and at ultimate pull wire, etc. as desired/needed?	D	A	DISCUSSION NEEDED We received comment from ADOT Central Phoenix Construction District during our CRA meeting to not include FMS infrastructure as it gets damaged prior to fiber being pulled. Text to be added to DCR Update to reflect that conduit should be included along the corridor for signal use.
79	16	Pg. 4-9 Draft IDCR	Section 4.15.1, FMS Communications and Trunk Line - Per Avery R. If signals are to be operated by COM we desire to get fiber to them sooner rather than later. I would recommend that conduit be added to any bridge structures; if the freeway crosses any canals, drainage areas, etc. it would be a good idea to get a conduit crossing in those structures if they are built now. COM wants to know which traffic signals we were going to have in this interim condition so we recommend some conduit that could help us right away	B/C	A	DISCUSSION NEEDED Text to be added to DCR Update to reflect that conduit should be included along the corridor for signal use.
ERIK GUDERIAN, CITY OF MESA						
80	1	Pg. 4-4 Draft IDCR	Section 4.4.3, Paragraph one - It should be assumed that Williams Field could be open during the interim condition. Most likely not at opening day, but at some point.	A	A	Will assume it is open.

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81	2	Pg. 4-4 Draft IDCR	Section 4.4.6, Paragraph one - Has this been proposed to Fuji in previous meetings with them? There is a new development plan for the north section of their property.	D	D	Yes, we have provided our design and have met with Fuji Film on 3/3/16. There are benefits to Fuji Film as well by reducing the R/W impacts along SR-24
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			MARC AHLSTROM, CITY OF MESA			
82	1	Pg. 1-5 Draft IDCR	Table 1, Ellsworth Cross Street - There is also a 20" water line in Ellsworth. Both water lines are DIP.	A	A	Will add
83	2	Pg. 4-4 Draft IDCR	Section 4.4.4, Crismon Road Grade Separation - This should be included in the cost of the freeway.	A	A	Portion inside ADOT R/W to be included in the ultimate SR 24 project.
			AL ZUBI, CITY OF MESA			
84	1	Pg. 4-4 Draft IDCR	Section 4.4.4, Crismon Road Grade Separation - Same comment on the economic impact on adjacent properties as Mountain Rd.	A	A	Portion inside ADOT R/W to be included in the ultimate SR 24 project.
85	2	Pg. 4-4 Draft IDCR	Section 4.4.4, Paragraph one - How will that be funded if not by the SR24 project?	A	A	It will be funded by SR-24 just not the interim project.
86	3	Pg. 4-4 Draft IDCR	Section 4.4.6, Mountain Road Grade Separation - Raising Mountain Rd will also have an economic impact on the other three corners/properties, by limiting access. Would ADOT take that in consideration, and not just discuss the impact with just Fuji, but the other property owners?	A	A	A statement will be added to the document about ADOT R/W acquisition process and Final Design.
87	4	Pg. 4-4 Draft IDCR	Section 4.4.6, Paragraph one - Remove reference to 2011 DCR as the nature of the grade separation changed (<i>Parsons interpretation of the highlighted text</i>)	A	A	It will be removed.

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		CHAUN HILL, MARICOPA ASSOCIATION OF GOVERNMENTS				
88	1	General, Draft IDCR	Please correct references to read "SR-24"	A	A	Will update
89	2	Pg. 1-1 Draft IDCR	<i>Executive Summary</i> - When referencing "Group 3" of the RTPFP, should this be "Phase 3"?	D	D	Latest RTPFP describes "Groups" rather than "Phases"
90	3	Pg. 1-1 Draft IDCR	<i>Section 1.3.3, Paragraph two</i> – "City of Mesa has requested that the new right-of-way accommodate a future multi-use path that may follow the SR-24 alignment." Is this request accommodated within the currently identified right-of-way footprint, or will additional right-of way be necessary?	A	A	The proposed R/W accommodates the trail.
91	4	Pg. 3-1 Draft IDCR	<i>Section 3.3, Paragraph one</i> – "Connectivity of Mountain Road between Williams Field Road and Pecos Road must not be removed in the interim alternatives." This again brings up the concern of interim and ultimate access. If interim access is provided at Mountain Road, does this provide the expectation that access will be provided in the ultimate condition? Is this the intent of the ultimate project?	A	A	Will clarify, Mountain Road is only a Grade Separated Crossing; it is not an interchange and will not have direct access to SR-24. Intent was to not cut off Mountain road with SR 24 (ie a grade separation is needed)
92	5	Pg. 5-1 Draft IDCR	QUINN CASTRO, MARICOPA ASSOCIATION OF GOVERNMENTS <i>Section 5.0,</i> – Present this section as the total corridor costs only, with a breakout of a combined segment 1 and 2 together (all within Maricopa County) and only one separate segment from Meridian to Ironwood (because it's within Pinal County). This seems to	A	A	The reason for the breakout into 3 segments was if the project was only constructed to Signal Butte (based on funding) then the costs are broken out. If funding allows project to be constructed to Ironwood, then the Signal Butte to Meridian Road estimate was

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93	6	Pg. 6-1 Draft IDCR	<i>Section 6.2,</i> – The last paragraph needs to be revised to reflect the changes above related to the estimate.	A	A	It will be revised.
94	1	General	CHUCK CHRISTIANSEN, PREMIER ENGINEERING CORP FOR PHX-MESA GATEWAY AIRPORT The PMGAA led Ellsworth Channel Relocation project recently completed a coordinated effort to obtain existing condition (without future SR-24 extension) hydrology and future condition (with future SR-24 extension) hydrology models. The results show an increase of approximately 1200 cfs in the Powerline Floodway in the future conditions model with the future SR-24 extension constructed. The increased flows affect the channel relocation. Please provide a coordinated solution to the increase with project stakeholders and/or mitigate the increase.	C	D	The interim condition will collect flows only to Ironwood Road. However, the peak flow will be in excess of the 1,200 cfs. Attenuation can not happen without an additional detention basin. The original DCR regulated the outflow to the Powerline Floodway to 1,650 cfs. The current project follows the same conditions.

the remaining portion within Maricopa County. We can combine the estimates.

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		LANCE WEBB, CITY OF MESA			
95	1	App. E - Draft Initial Drain. Report	For the offsite channel options, Parsons has only provided adequate freeboard for the Powerline Floodway for the dirt lined, not concrete lined. The concrete lined channel will require a greater freeboard since the hydraulics of the channel at this location is supercritical and 1-ft of freeboard is not adequate. This alternative needs to be modified to meet hydraulics requirements for channel design.	B	A
96	2	App. F - Draft Initial Drain. Report	Should the concrete lined option be pursued, more volume will be required to attenuate flows within the outfall basin prior to passing under the existing (already constructed) crossing under the SR 24	B	A
97	3	App. D - Draft Initial Drain. Report	(PARSONS Note - Repeat of Comment 93/1 by Chuck Christiansen): The PMGAA project for the relocation of the Ellsworth Channel project has been coordinating with ADOT as far as the flows to expect. The results from this report for the future conditions (with future SR-24 extension) show an increase of ~1200 CFS in the Powerline Floodway for future conditions with future SR -24 extension constructed. The increased flows for the model affect how the channel can and will be relocated. Please provide a coordinated solution to mitigate this increase in flows by likely upsizing the outfall basin to accommodate this additional flow	C	D

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		GLENN GAELICK, ADOT ROADWAY DESIGN SUPPORT			
98	1	G-2.06	Why is there 17.5 outside lane widths here vs 17' on previous crossroads?	B	D
99	2	G-2.07	Please clarify the need for 18.5' outside lane width vs previous 17' dimension for same on other crossroads.	B	D
100	3	C-1.01	1) Tangent Length for Curve Ref No. 800 seems excessive. Please check. 2) POT's 49 & 50 for Exst Ellsworth Cst CL do not show up on Geometric layout sheets although they seem to be called out as Pt. No's 20899 & 20909. Please clarify. 3) L & T shown for curve Ref No. 813 do not substantiate data shown on Geo Layout sheet C-2.01. Please check.	A A A	A A A
101	4	C-1.03	POT 2094 (Signal Butte) seems to be shown as 20943 of Sht C-2.06. Please clarify.	A	A
102	5	C-2.03	Suggest value in showing SR24 Med. Cst CL Sta where Section 27's south section line crosses.	A	A

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103	6	C-3.01	<p>1) Recommend acquisition of access control per ADOT RDG Fig 506A on both ends of Ellsworth.</p> <p>2) Suggest some investigation as to feasibility of either false work or soffit fill for construction of the SR24 overpass structure. Downside of soffit fill could be differential settlement of the exst. PCCP. False work construction would need to be accommodated in proposed clearance over Ellsworth.</p> <p>3) Proximity of proposed retaining wall adjacent to Ellsworth Ramp D Lt could pose construction problems. Please investigate.</p>	C	A	<p>1) Discussion has occurred on this subject with ADOT RW. Some development planning has occurred based on the pre-2014 RDG Access Control Requirements. We are showing the "Full Access Control" limits in the plans per ADOT R/W request. Ellsworth Rd will require a variance at the NE Quadrant, based on approved Development Plat Plans for Cadence Parkway.</p> <p>2) Soffit Fill will probably not be feasible here because the interim interchange will need to remain open. False work should work, but will confirm clearances</p> <p>3) Retaining wall is approx 15' at its closest point.</p>
104	7	C-3.05	Based on plans data there may be an excessive grade difference across the gore nose at Ellsworth Ramp D. Please check.	B	A	Profile to be revised.
105	8	C-3.07	Recommend acquisition of access control per ADOT RDG Fig 506A on both ends of Williams Field.	B	A	Discussion has occurred on this subject with ADOT R/W. Some development planning has occurred based on the pre-2014 RDG Access Control Requirements. We will show Access Control (Full & Right in Right Out per the RDG Fig 506A
106	9	C-3.09 & C-03.10	Beginning profile grade seems to be missing for Ramps A & B.	A	A	Will add
107	10	C-3.11	Ramp terminus station seems to be at odds with callouts on Sht C-3.13. Please check.	A	A	Will revise

**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
in Maricopa County and Pinal County, Arizona**

TRACS No. H8915 01L/02L
Federal Project No. 024 A (200)

Draft IDCR Comment Response Document

Client Project Manager: Ronald McCally
Consultant: **PARSONS**

108	11	C-3.13	Would there be value in extending access control north and south of Crismon per RDG due to the likelihood that the approach embankments would limit access anyway?	B/C	A	Will show access control
109	12	C-3.19	<p>1) Recommend acquisition of access control per ADOT RDG Fig 506A on both ends of Signal Butte.</p> <p>2) Based on plans data there may be an excessive grade difference across the gore nose at Signal Butte Ramp C. Please check.</p>	C	A	<p>1) Discussion has occurred on this subject with ADOT RW. Some development planning has occurred based on the pre-2014 RDG Access Control Requirements. We will show Access Control (Full & Right in Right Out per the RDG Fig 506A</p> <p>2) Profile to be revised.</p>
110	13	C-3.23	Recommend acquisition of access control per ADOT RDG Fig 506A on both ends of Mountain to encompass embankment prism and to limit access to points far enough away from the crest VC to provide reasonable decision sight distance.	B/C	A	Will show access control
111	14	C-3.24	Mainline VC data is obscured on Rt end.	A	A	Will revise
112	15	C-3.27	<p>1) Recommend extending access ctrl to comply with ADOT RDG Fig 506A on both ends of Meridian.</p> <p>2) Do proposed clearances over Meridian provided by mainline profile accommodate false work construction for the SR24 overpass structure?</p>	C	A	<p>1) Discussion has occurred on this subject with ADOT RW. Some development planning has occurred based on the pre-2014 RDG Access Control Requirements. We will show Access Control (Full & Right in Right Out per the RDG Fig 506A.</p> <p>2) Will confirm</p>
113	16	C-3.31	Graphic location of Ironwood Ramp B Gore is at odds with Gore Ctrl Point callout. Please check.	A	A	Will update the plan call out.

**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
in Maricopa County and Pinal County, Arizona**

TRACS No. H8915 01L/02L
Federal Project No. 024 A (200)

Draft IDCR Comment Response Document

Client Project Manager: Ronald McCally
Consultant: **PARSONS**

114	17	C-4.07	<p>1) Recommend extending access ctrl to comply with ADOT RDG Fig 506A.</p> <p>2) Do proposed clearances over Ironwood provided by mainline profile accommodate false work construction for the SR24 overpass structure?</p>	A	A	<p>1) Discussion has occurred on this subject with ADOT RW. Some development planning has occurred based on the pre-2014 RDG Access Control Requirements. We will show Access Control (Full & Right in Right Out per the RDG Fig 506A.</p> <p>2) Will revise.</p>
115	18	General	<p>Juxtaposition of interim ramps and mainline with future mainline and/or crossroad structures raises questions about construction compatibility. Cross sections would be of value in determining any serious conflicts.</p>	B/C	D	<p>The interim design will allow for the future ultimate construction to be compatible.</p>

A-Will Comply
B-Consultant To Evaluate
C-ADOT To Evaluate
D-No Further Action Required

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**FINAL DESIGN CONCEPT REPORT
SR-24, Ellsworth Road to Ironwood Drive
Interim Phase II**

APPENDIX E – TRAFFIC ANALYSIS REPORT

SR-24

Design Concept Report

Traffic Analysis Report

SR-24: Ellsworth Road to
Ironwood Road - ADOT Central District

December 2016
Project No. 14-670A

Prepared For:

Parsons Corporation
222 South Mill Avenue, Suite 220
Tempe, AZ 85208

For Submittal to:

Arizona Department of Transportation

Prepared By:



10605 North Hayden Road
Suite 140
Scottsdale, Arizona 85260
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SR 24 INTERIM PHASE II DCR TRAFFIC ANALYSIS REPORT

SR 24: Ellsworth Road to Ironwood Road ADOT Central District

Prepared for:

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Expires 12-31-16

December 2016
CivTech Project # 14-670A

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EXECUTIVE SUMMARY

State Route (SR) 24 is currently a 1.3-mile freeway segment connecting Loop 202 to Ellsworth Road. The Arizona Department of Transportation (ADOT) has retained Parsons Transportation Group (Parsons) to complete an Interim Phase II Design Concept Report (DCR) and Environmental Evaluation to evaluate the interim and buildout alternatives of SR 24. CivTech Inc. has been retained by Parsons to evaluate the operation of the existing conditions and the proposed alternatives detailed in the Interim Phase II DCR.

CivTech evaluated two interim alternatives for SR 24 in 2025. Option A proposes extending SR 24 from Ellsworth Road to Ironwood Drive as an at grade arterial roadway with an at grade intersection at Signal Butte Road. The existing at grade intersection with Ellsworth Road would remain if possible and an “end of expressway” condition would occur at Ironwood Road. Mountain Road would be “grade separated” over SR 24. Option B is an at grade arterial roadway extension from Ellsworth Road to Signal Butte Road with no additional access. The existing at grade intersection with Ellsworth Road would remain if possible and an “end of expressway” condition would occur at Signal Butte Road. In 2035, SR 24 is considered to be a controlled access freeway extending the existing freeway from Ellsworth Road to Ironwood Drive. Freeway interchanges will be provided at Ellsworth Road, Williams Field Road, Signal Butte Road, Meridian Road, and Ironwood Drive.

This report documents the traffic analysis and recommendations of the alternatives provided in the SR 24 Interim Phase II DCR. The specific objectives of the study are:

1. To determine existing level of service for the SR 24 interchange at Ellsworth Road.
2. To evaluate the crash experience and patterns at the existing SR 24 interchange at Ellsworth Road.
3. To determine future Levels of Service (LOS) for all proposed interchanges and study alternatives within the study area.
4. To determine necessary lane configurations at all proposed traffic interchanges and freeway segments within the study area.

The following findings, conclusions, and recommendations have been documented in this study:

Existing Conditions

- ◆ All existing intersection approaches operate at an acceptable level of service (LOS D) with the existing lane configurations and stop control except for select turning movements during the AM and PM peak hours. The northbound left turn movement experiences delays in the AM peak hour due to a combination of the high left turn volume and southbound volumes and the limited green time for the northbound left turn movement. The eastbound right turn movement experiences

delay in the PM peak hour due to the limited green time for the eastbound approach as a result of the high demand of vehicles on Ellsworth Road.

- ◆ The segment of SR 24 from Loop 202 to Ellsworth Road experienced 24 crashes in 2014 and 2015. The data provided does not seem to indicate any unusual crash pattern.
- ◆ The intersections of SR 24 at Ellsworth Road experienced 27 crashes in 2014 and 2015. The data provided does not seem to indicate any unusual crash patterns.

2025 Option A Scenario

- ◆ Option A proposes extending SR 24 from Ellsworth Road to Ironwood Drive as an at grade arterial roadway with an at grade intersection at Signal Butte Road. The existing at grade intersection with Ellsworth Road would remain if possible and an “end of expressway” condition would occur at Ironwood Road. Mountain Road would be “grade separated” over SR 24.
- ◆ Grade separation of interchanges is not recommended in the 2025 Option A scenario.
- ◆ The 2025 Option A intersection capacity analysis was performed using the recommended lane configurations and stop control as shown in **Figure 6**.
- ◆ The results of the intersection capacity analysis in **Table 5** indicate that the SR 24 intersections at Ellsworth Road and Signal Butte Road are expected to experience delays during the peak hours.
 - The intersection of **Ellsworth Road and WB SR 24 Ramps** is predicted to experience delays during the AM and PM peak hours. During both peak hours, the demand of northbound left turning movement conflicts with the demand of the westbound off ramp through movement. Vehicles are expected to experience delays for the westbound approach movements and northbound left turning movement. An alternate mitigation analysis is included in this report.
 - The intersection of **Ellsworth Road and EB SR 24 Ramps** is predicted to experience delays during the AM and PM peak hours. During the AM peak hour, the heavy northbound through volumes on Ellsworth Road require the majority of green time which minimizes the green time available for other movements. During the PM peak hour, the heavy through volumes on the SR 24 eastbound off ramp conflict with southbound traffic on Ellsworth Road. Southbound left turning vehicles and the eastbound ramp approach vehicles are expected to experience delays during the PM peak hour. An alternate mitigation analysis is also included in this report.
 - The intersection of **Signal Butte Road and WB SR 24 Ramps** is predicted to experience delays in the AM peak hour. The high volumes of

through vehicles on westbound SR 24 conflict with the NB left turning vehicles travelling to westbound SR 24. An alternate mitigation analysis is also included in this report.

- The intersection of **Signal Butte Road and EB SR 24 Ramps** is predicted to experience delays in the PM peak hour. The high volumes of through vehicles on eastbound SR 24 conflict with the SB left turning vehicles travelling to eastbound SR 24. An alternate mitigation analysis is also included in this report.

2025 Option A Mitigated Analysis

- ◆ A mitigation analysis was performed for the 2025 Option A scenario at intersections that experience delays in the AM and PM peak hours. ADOT may consider the mitigated lane configurations shown in **Figure 6** to improve levels of service.
- ◆ The results of the intersection capacity analysis in **Table 6** indicate that the SR 24 intersections at Ellsworth Road are expected to experience delays during the peak hours.
 - The intersection of **Ellsworth Road and WB SR 24 Ramps** is predicted to experience delays during the AM peak hour. The demand of northbound left turning movement conflicts with the demand of the westbound off ramp through movement. Vehicles are expected to experience delays for the westbound approach movements and northbound left turning movement.
 - The intersection of **Ellsworth Road and EB SR 24 Ramps** is predicted to experience delays during the AM and PM peak hours. During the AM peak hour, the heavy northbound through volumes on Ellsworth Road require the majority of green time which minimizes the green time available for other movements. During the PM peak hour, the heavy through volumes on the SR 24 eastbound off ramp conflict with southbound traffic on Ellsworth Road. Southbound left turning vehicles and the eastbound ramp approach vehicles are expected to experience delays during the PM peak hour.

2025 Option B Scenario

- ◆ Option B is an at grade arterial roadway extension from Ellsworth Road to Signal Butte Road with no additional access. The existing at grade intersection with Ellsworth Road would remain if possible and an “end of expressway” condition would occur at Signal Butte Road.
- ◆ Grade separation of interchanges is not recommended in the 2025 Option B scenario.

- ◆ The 2025 Option B intersection capacity analysis was performed using the recommended lane configurations and stop control as shown in **Figure 7**.
- ◆ The results of the intersection capacity analysis in **Table 7** indicate that the SR 24 intersections at Ellsworth Road are expected to experience delays during the peak hours.
 - The intersection of **Ellsworth Road and WB SR 24 Ramps** is predicted to experience delays during the AM and PM peak hours. During both peak hours, the demand of northbound left turning movement conflicts with the demand of the westbound off ramp through movement. Vehicles are expected to experience delays for the westbound approach movements and northbound left turning movement. An alternate mitigation analysis is included in this report.
 - The intersection of **Ellsworth Road and EB SR 24 Ramps** is predicted to experience delays during the AM and PM peak hours. During the AM peak hour, the heavy northbound through volumes on Ellsworth Road require the majority of green time which minimizes the green time available for other movements. An alternate mitigation analysis is also included in this report.

2025 Option B Mitigated Analysis

- ◆ A mitigation analysis was performed for the 2025 Option B scenario at intersections that experience delays in the AM and PM peak hours. ADOT may consider the mitigated lane configurations shown in **Figure 7** to improve levels of service.
- ◆ The results of the intersection capacity analysis in **Table 8** indicate that the SR 24 intersections at Ellsworth Road are expected to experience delays during the peak hours. The proposed mitigation measures are not predicted to improve the level of service at the intersections of Ellsworth Road and SR 24 in 2025.

2035 Horizon Year

- ◆ In 2035, SR 24 is considered to be a controlled access freeway, extending the existing freeway from Ellsworth Road to Ironwood Drive. Freeway interchanges will be provided at Ellsworth Road, Williams Field Road, Signal Butte Road, Meridian Road, and Ironwood Drive.
- ◆ The 2035 intersection capacity analysis was performed using the recommended lane configurations and stop control as shown in **Figure 8**.
- ◆ The results of the intersection capacity analysis indicate that all study intersection approaches and movements are predicted to operate at LOS D or better during the peak hours except for select movements at the intersection of **Meridian Road and SR 24 WB Ramps**.

- ◆ The northbound left turning vehicles and westbound left turning vehicles conflict at the intersection of **Meridian Road and SR 24 WB Ramps** and are expected to experience delays in the AM peak hour. Vehicles are expected to queue on the westbound on ramp and northbound left turn lane. It is not uncommon for heavy turning movements at freeway interchanges to experience delays in the peak hour. No mitigation is recommended.

INTRODUCTION

State Route (SR) 24 is currently a 1.3-mile freeway segment connecting Loop 202 to Ellsworth Road. The Arizona Department of Transportation (ADOT) has retained Parsons Transportation Group (Parsons) to complete an Interim Phase II Design Concept Report (DCR) and Environmental Evaluation to evaluate the interim and buildout alternatives of SR 24. CivTech Inc. has been retained by Parsons to evaluate the operation of the existing conditions and the proposed alternatives detailed in the Interim Phase II DCR.

ADOT previously completed a DCR for SR 24 between SR 202L and Ironwood Road in April 2011. Since then MAG authorized a study “SR 24 Williams Gateway Freeway, Ellsworth Road – Ironwood Road Interim Phase II Feasibility Study (600-0110-14)” to be completed by Parsons. As a result of the Feasibility Study, ADOT has decided that an interim condition for SR 24 between Ellsworth Road and Ironwood Drive should be evaluated and has requested Parsons to complete an Interim Phase II DCR and Environmental Evaluation of the project limits. The DCR will evaluate several interim condition alternatives and provide a recommended interim alternative.

Study Area

The study area includes the proposed interim and final configuration of SR 24 in 2025 and 2035. The following intersections were analyzed in this study:

- Ellsworth Road/SR 24 EB Ramps
- Ellsworth Road/SR 24 WB Ramps
- Williams Field Road/SR 24 EB Ramps
- Williams Field Road/SR 24 WB Ramps
- Signal Butte Road/SR 24 EB Ramps
- Signal Butte Road/SR 24 WB Ramps
- Meridian Road/SR 24 EB Ramps
- Meridian Road/SR 24 WB Ramps
- Ironwood Drive/SR 24 EB Ramps
- Ironwood Drive/SR 24 WB Ramps

Horizon Years

CivTech evaluated two interim alternatives for SR 24 in 2025. Option A proposes extending SR 24 from Ellsworth Road to Ironwood Drive as an at grade arterial roadway with an at grade intersection at Signal Butte Road. The existing at grade intersection with Ellsworth Road would remain if possible and an “end of expressway” condition would occur at Ironwood Road. Mountain Road would be “grade separated” over SR 24. Option B is an at grade arterial roadway extension from Ellsworth Road to Signal Butte Road with no additional access. The existing at grade intersection with Ellsworth Road would remain if possible and an “end of expressway” condition would occur at Signal Butte Road. In 2035, SR 24 is considered to be a controlled access freeway extending

the existing freeway from Ellsworth Road to Ironwood Drive. Freeway interchanges will be provided at Ellsworth Road, Williams Field Road, Signal Butte Road, Meridian Road, and Ironwood Drive.

EXISTING CONDITIONS

EXISTING ROADWAY NETWORK

The existing roadway network within the study area includes State Route (SR) 24, Ellsworth Road, Williams Field Road, Crismon Road, Signal Butte Road, Meridian Road, and Ironwood Drive.

SR 24 is a freeway segment connecting Loop 202 to Ellsworth Road. It consists of two (2) lanes in each direction of travel. SR 24 was opened on May 4, 2014. It currently does not have a posted speed limit.

Ellsworth Road is a north-south five-lane arterial roadway with two (2) lanes in the northbound movement and three (3) lanes in the southbound movement. Ellsworth Road begins just south of Empire Boulevard, continuing north for about 18 miles before terminating at McDowell Road. Within the vicinity of the study area, the posted speed limit on Ellsworth Road is 50 miles per hour (mph).

Williams Field Road is an east-west two-lane roadway with one (1) lane in each direction of travel. Within the vicinity of the site, Williams Field Road begins to the east at Meridian Road and continues west for about 1.25 miles terminating at 222nd Street. The posted speed limit on Williams Field Road is 35 mph.

Crismon Road would be a north-south section line roadway. Currently it is an unimproved dirt road serving farm fields in the area.

Signal Butte Road is a north-south section line roadway. It begins to the north at Jensen Street, continuing south for about 8.4 miles before terminating just south of Ray Road. It provides at least one (1) lane in each direction and in some locations two (2) lanes in each direction. The posted speed limit on Signal Butte Road is 45-mph.

Meridian Road is a north-south 2-lane roadway with one (1) lane in the northbound movement and one (1) lane in the southbound movement. Meridian Road begins approximately ½ mile north of Elliot Road and continues south for about 2.5-miles before terminating at Ray Road. The posted speed limit on Meridian Road is 35-mph.

Ironwood Drive is a north-south 4-lane divided roadway with two (2) lanes in each direction separated by a median. Ironwood Drive begins to the north at McDowell Boulevard, continuing south for about 21.1 miles before terminating at Bella Vista Road. The posted speed limit on Ironwood Drive is 45-mph.

EXISTING INTERSECTION CONFIGURATION

The intersection of **Ellsworth Road and Eastbound SR 24 Off-Ramp** operates as a three-legged signalized intersection with protective/permissive right-turn phasing in the eastbound approach. The northbound approach consists of four (4) lanes – two (2) through lanes and two (2) left turn storage lanes. The southbound approach consists of three (3) through lanes. The eastbound approach consists of dual left-turn lanes as well as dual right-turn lanes.

The intersection of **Ellsworth Road and Westbound SR 24 On-Ramp** operates as a three-legged signalized intersection with protective left-turn phasing in the northbound approach. The northbound approach consists of dual left-turn lanes and two (2) through lanes. The southbound approach consists of three (3) through lanes and a dedicated right-turn lane.

Figure 1 depicts existing lane geometry and traffic controls for the project study area.

EXISTING TRAFFIC VOLUMES

Field Data Services of Arizona (FDS) conducted turning movement counts at the intersection of Ellsworth Road and State Route 24 between 7:00 AM and 9:00 AM and 4:00 PM and 6:00 PM on January 5, 2016. Existing peak hour traffic count data is shown on **Figure 1** and provided within **Appendix B**.

EXISTING LEVELS OF SERVICE ANALYSIS

Peak hour capacity analyses have been conducted for the study intersections based on existing conditions and traffic volumes. All intersections have been analyzed using the methodologies presented in the *Highway Capacity Manual (HCM), Special Report 209*, Updated 2010 and using Synchro Software version 9.0 under the HCM 2010 methodology.

The concept of level-of-service (LOS) uses qualitative measures that characterize operational conditions within the traffic stream. The individual levels-of-service are described by factors that include speed, travel time, freedom to maneuver, traffic interruptions, and comfort and convenience. Six levels of service are defined for each type of facility for which analysis procedures are available. They are given letter designations A through F, with LOS A representing the best operating conditions and LOS F the worst. Each level of service represents a range of operating conditions. **Table 1** lists the level of service criteria for signalized intersections.

Table 1 – Level-of-Service Criteria for Signalized Intersections

Level-of-Service	Signalized Control Delay (sec/veh)
A	≤ 10
B	> 10-20
C	> 20-35
D	> 35-55
E	> 55-80
F	> 80

Source: Exhibit 18-4 Highway Capacity Manual 2010

Results of the existing level-of-service analyses are shown in **Table 2** for both the AM and PM peak hours. Analysis worksheets for the existing conditions have been included in **Appendix C**. The traffic signals to the EB and WB Loop 202 ramps at Ellsworth Road were analyzed using a 120-second traffic cycle length.

Table 2 – Existing Level of Service Summary

ID	Intersection	Stop Control	Approach	AM (PM) Peak Hour			
				Left	Thru	Right	Overall
1A	Ellsworth Road & WB SR 24 Ramps	Signalized	NB	F(D)	A(A)	--(--)	D(C)
			SB	--(--)	C(A)	D(B)	C(B)
			Overall	D(C)			
1B	Ellsworth Road & EB SR 24 Ramps	Signalized	NB	--(--)	C(D)	--(--)	C(D)
			SB	--(--)	A(C)	--(--)	A(C)
			EB	C(A)	--(--)	D(F)	C(E)
			Overall	C(E)			

All existing intersection approaches operate at an acceptable level of service (LOS D) with the existing lane configurations and stop control except for select turning movements during the AM and PM peak hours. The northbound left turn movement experiences delays in the AM peak hour due to a combination of the high left turn volume and southbound volumes and the limited green time for the northbound left turn movement. The eastbound right turn movement experiences delay in the PM peak hour due to the limited green time for the eastbound approach as a result of the high demand of vehicles on Ellsworth Road.

CRASH ANALYSIS

The following crash analysis was developed from historical data obtained by CivTech from the Arizona Department of Transportation. Construction on SR 24 was completed in May 2014. The Arizona Department of Transportation collects crash data annually, reporting the data in July. Therefore, the crash history data represents the periods available, May 2014 through July 2015.¹ For the purposes of this analysis, CivTech has organized the data in intervals by calendar year 2014, reporting from May 2014 to December 2014, and calendar year 2015, representing January 2015 through July 2015.

CivTech identified a one-year total of 24 crashes (without any fatalities) on SR 24 from Loop 202 to Ellsworth Road and 27 crashes (without any fatalities on SR 24 from Loop 202) at the intersection of SR 24 and Ellsworth Road. The results are summarized in **Table 3** and **Table 4**, respectively. The crash data provided by the Arizona Department of Transportation can be found in **Appendix D**.

¹ ADOT is charged by statute with the responsibility of tracking all incidents involving motor vehicles occurring, reported, and investigated in the State. ADOT has neither the mandate nor the staff to fulfill requests for crash data for specific locations (as they generously had in previous years), only providing crash data for the entire State on an annual basis.

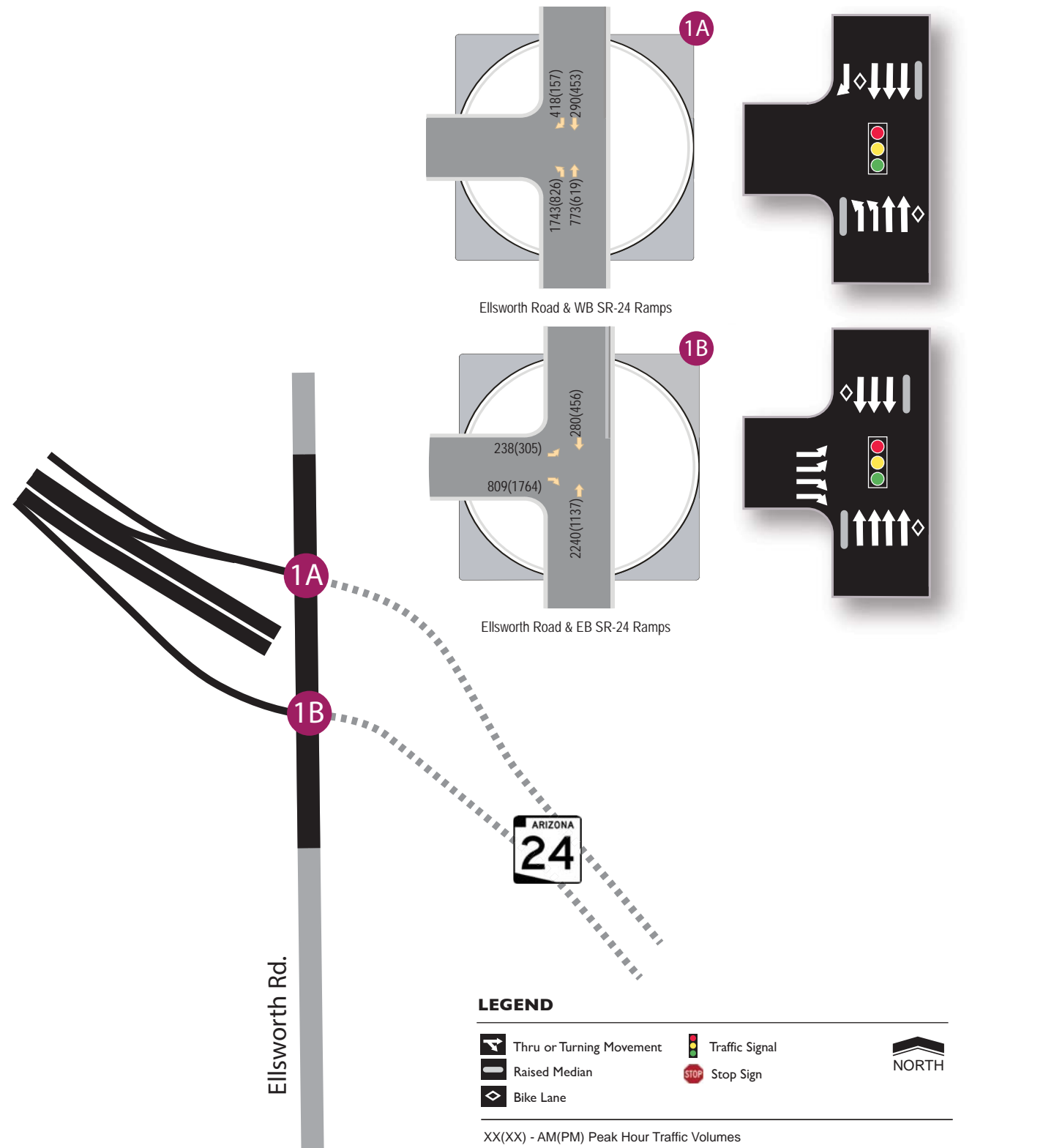


Figure 1: Existing Lane Configurations and Traffic Volumes

Table 3 - Crash Experience on SR 24 from Loop 202 to Ellsworth Road

Crash Severity	2014	2015	Total
Fatality Crashes	-	-	-
Injury Crashes	1	1	2
Non-Injury, Property Damage Only	10	12	22
TOTAL	11	13	24
Crash Type	2014	2015	Total
Rear End	10	11	21
Sideswipe Same Direction	-	2	2
Other	1	-	1
TOTAL	11	13	24

The segment of SR 24 from Loop 202 to Ellsworth Road experienced 24 crashes in 2014 and 2015. Of these crashes, 2 (8%) caused injuries (no fatalities) and the remaining did not cause any injuries. Regarding crash types, 21 (88%) were rear end, 2 (8%) were sideswipe, and 1 (4%) was classified as “other”. The data provided does not seem to indicate any unusual crash patterns.

Table 4 - Crash Experience at the Intersection of SR 24 and Ellsworth Road

Crash Severity	2014	2015	TOTAL
Fatality Crashes	-	-	-
Injury Crashes	2	1	3
Non-Injury, Property Damage Only	13	11	24
TOTAL	15	12	27
Crash Type	2014	2015	TOTAL
Angle	-	2	2
Head On	-	1	1
Left Turn	2	1	3
Rear End	4	5	9
Sideswipe Same Direction	7	2	9
Other	2	1	3
TOTAL	15	12	27

The intersections of SR 24 at Ellsworth Road experienced 27 crashes in 2014 and 2015. Of these crashes, 3 (11%) caused injuries (no fatalities) and the remaining did not cause any injuries. Regarding crash types, 9 (33%) were rear end, 9 (33%) were sideswipe (same direction), 3 (11%) were left-turn, 2 (7%) were angle, 1 (4%) was head on, and the remaining 3 (11%) were classified as “other”. The data provided does not seem to indicate any unusual crash patterns.

FUTURE PROJECTED TRAFFIC VOLUMES

DESIGN CONCEPT REPORT ALTERNATIVES

The DCR evaluates SR 24 in the interim condition in 2025 and as a controlled access freeway in 2035. Two interim alternatives for SR 24 are evaluated in 2025. Option A proposes extending SR 24 from Ellsworth Road to Ironwood Drive as an at grade arterial roadway with an at grade intersection at Signal Butte Road. The existing at grade intersection with Ellsworth Road would remain if possible and an “end of expressway” condition would occur at Ironwood Road. Mountain Road would be “grade separated” over SR 24. Option B is an at grade arterial roadway extension from Ellsworth Road to Signal Butte Road with no additional access. The existing at grade intersection with Ellsworth Road would remain if possible and an “end of expressway” condition would occur at Signal Butte Road.

In 2035, SR 24 is considered to be a controlled access freeway, extending the existing freeway from Ellsworth Road to Ironwood Drive. Freeway interchanges will be provided at Ellsworth Road, Williams Field Road, Signal Butte Road, Meridian Road, and Ironwood Drive.

PROJECTED SEGMENT TRAFFIC VOLUMES

CivTech received information from the Maricopa Association of Governments (MAG) Travel Demand Model on January 13, 2016 for the 2025 and 2035 horizon years. CivTech proposed two interim traffic scenarios for the 2025 horizon year. The first scenario, referred to as Option A, proposes extending SR 24 from Ellsworth Road to Ironwood Drive as an at grade arterial roadway with an at grade intersection at Signal Butte Road. The existing at grade intersection with Ellsworth Road would remain if possible and an “end of expressway” condition would occur at Ironwood Road. Mountain Road would be “grade separated” over SR 24. Option B is an at grade arterial roadway extension from Ellsworth Road to Signal Butte Road with no additional access. The existing at grade intersection with Ellsworth Road would remain if possible and an “end of expressway” condition would occur at Signal Butte Road.

The 2035 analysis studied the construction of SR 24 from Ellsworth Road to Ironwood Drive with full access interchanges at Ellsworth Road, Williams Field Road, Signal Butte Road, Meridian Road and Ironwood Drive. The requested MAG regional travel demand model data is included in **Appendix E**.

PROJECTED TURNING MOVEMENT VOLUMES

CivTech developed the turning movements for all of the study intersections based on the total average daily volumes from the MAG Travel Demand Model. NCHRP methodologies were evaluated but found to produce abnormal results due the smaller volume from the daily ramp volumes compared to the large through volumes predicted by the MAG model.

A smoothing technique was utilized to better distribute the ramp volumes during the peak hour and develop turning movements for each intersection. Peak hour values of eight percent (8%) and nine percent (9%) were applied to the daily volumes to calculate the AM and PM peak hour volumes, respectively. North-south directional splits were determined from the existing traffic counts. These volumes indicated a prevailing travel pattern to the north and west in the AM peak hour and south and east in the PM peak hour. Initial directional assumptions were assumed and then adjusted to balance the approach and departure volumes at each interchange. Turning percentages were initially assumed and adjusted to balance the calculated directional departure volume against the resulting sum of the appropriate turning volumes assigning vehicles to that departure.

Calculations used to determine the AM and PM peak hour turning movement volumes at each study location are included in **Appendix F**.

The 2025 Option A turning movements are shown in **Figure 2**, the 2025 Option B turning movements are shown in **Figure 3** and the 2035 turning movements are shown in **Figure 4**. Average Annual Daily Traffic Volumes are depicted in **Figure 5** for 2025 Option A, 2025 Option B and 2035.

TRAFFIC AND IMPROVEMENT ANALYSIS

Peak hour capacity analyses have been conducted for the study intersections. All intersections have been analyzed using the methodologies as described previously and presented in the *Highway Capacity Manual (HCM), Special Report 209*, updated 2010 and using Synchro Software version 9.0 under the HCM 2010 methodology.

Results of the analysis for the 2025 Option A and 2025 Option B scenarios, and the 2035 horizon year conditions have been included in **Appendices G, I and K** respectively.

A mitigation analysis was performed for the 2025 Option A and B scenarios at intersections that are predicted to experience delays in the AM and PM peak hours. Results of the 2025 Option A Mitigated Analysis and 2025 Option B Mitigated Analysis have been included in **Appendices H and J** respectively.

2025 OPTION A INTERSECTION LEVEL OF SERVICE ANALYSIS

The 2025 Option A intersection capacity analysis was performed using the unmitigated lane configurations and stop control as shown in **Figure 6**. The resulting intersection movement level of service is shown in **Table 5**. An alternate mitigated intersection movement level of service analysis is shown in **Table 6**.

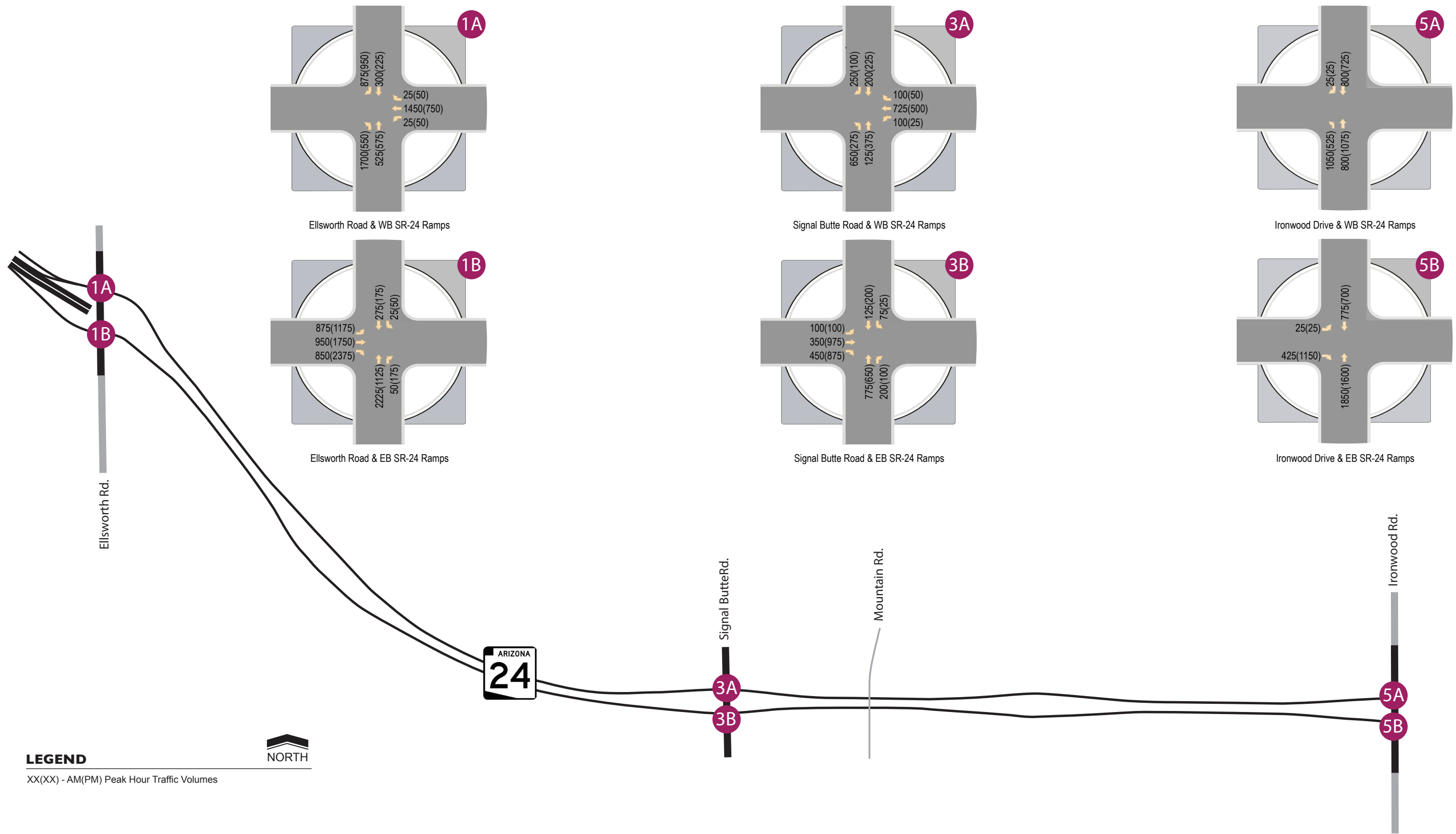


Figure 2: 2025 Option A - Peak Hour Volumes

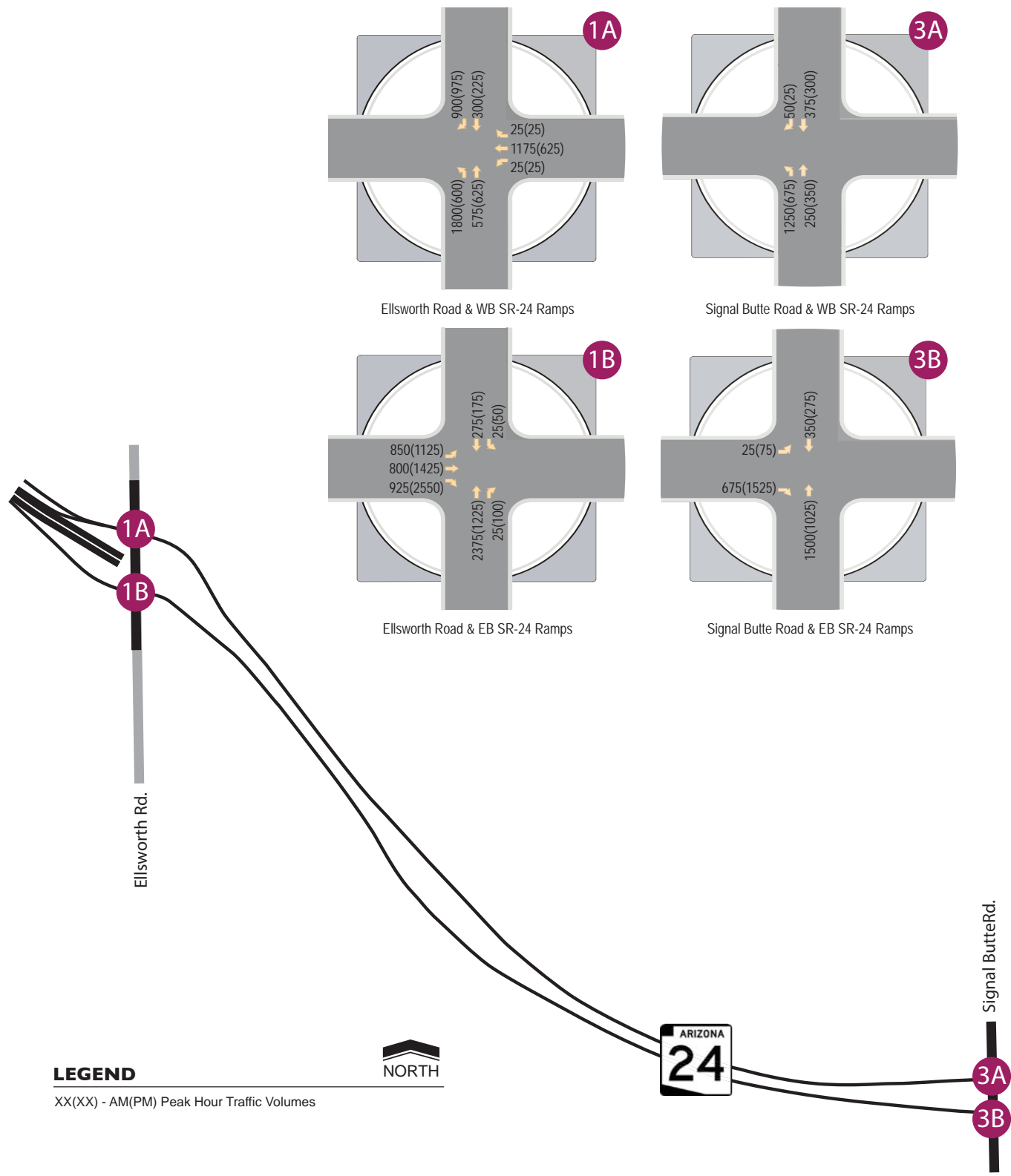


Figure 3: 2025 Option B - Peak Hour Volumes

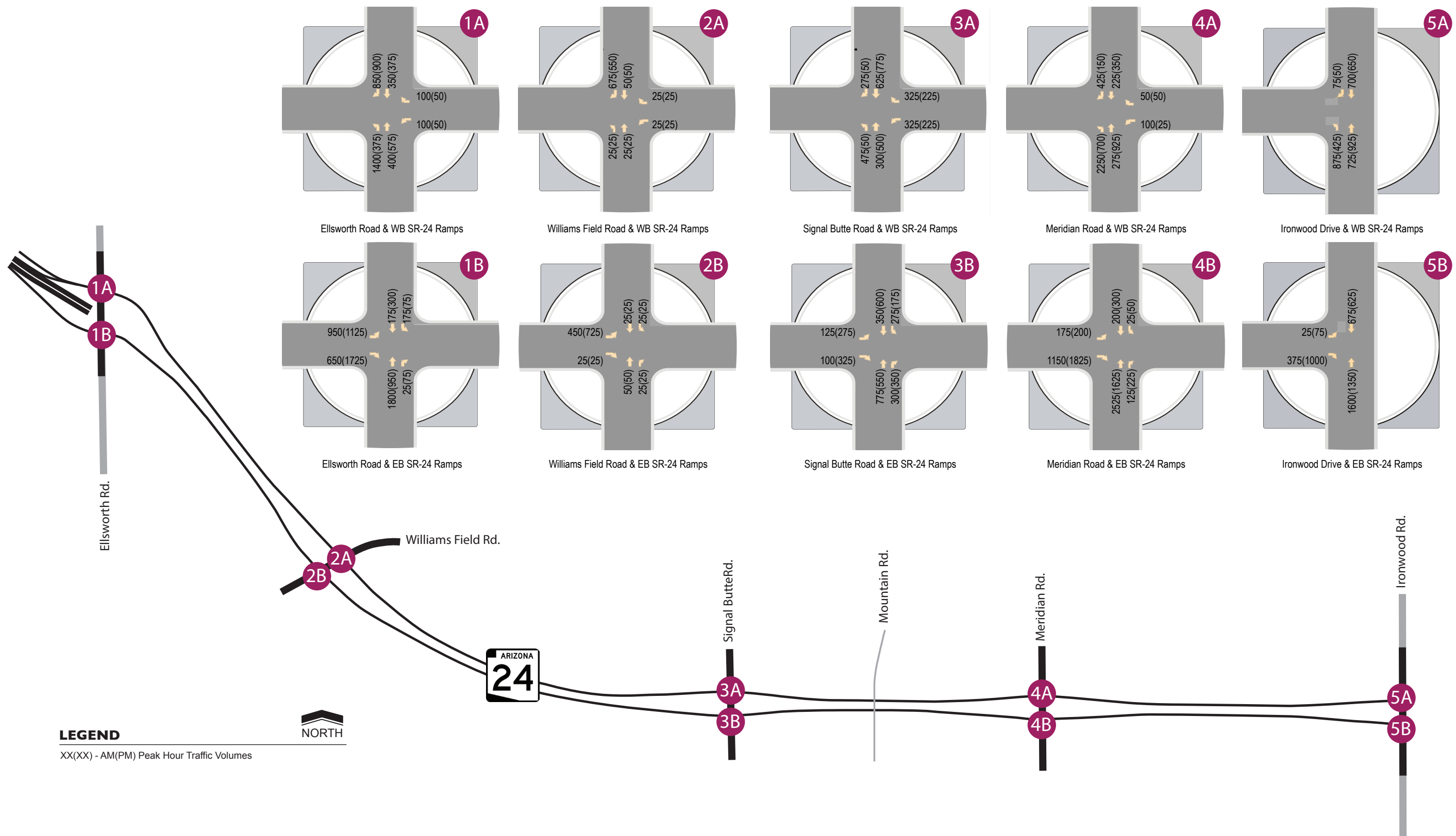


Figure 4: 2035 Peak Hour Volumes

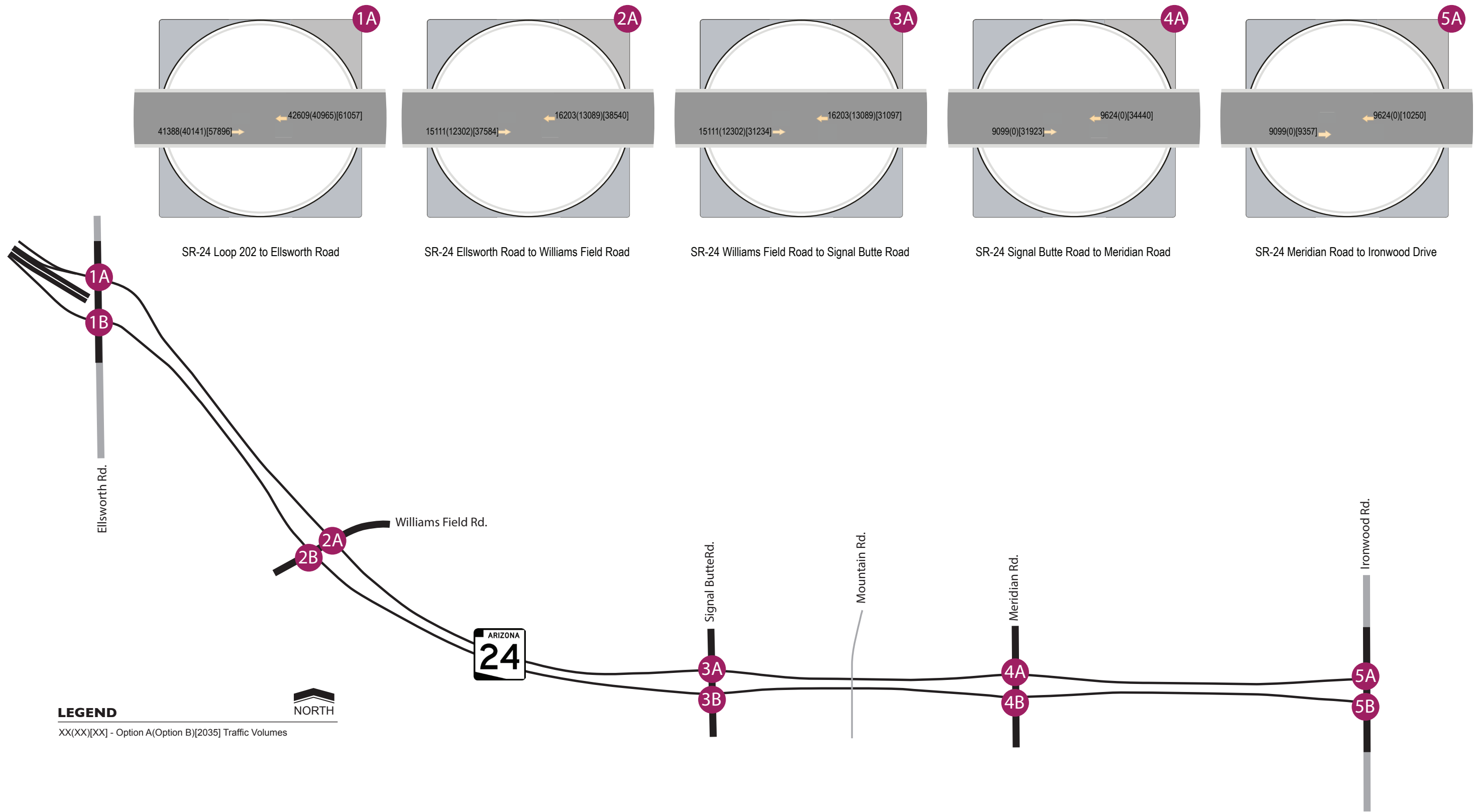


Figure 5: 2025 and 2035 AADT Volumes

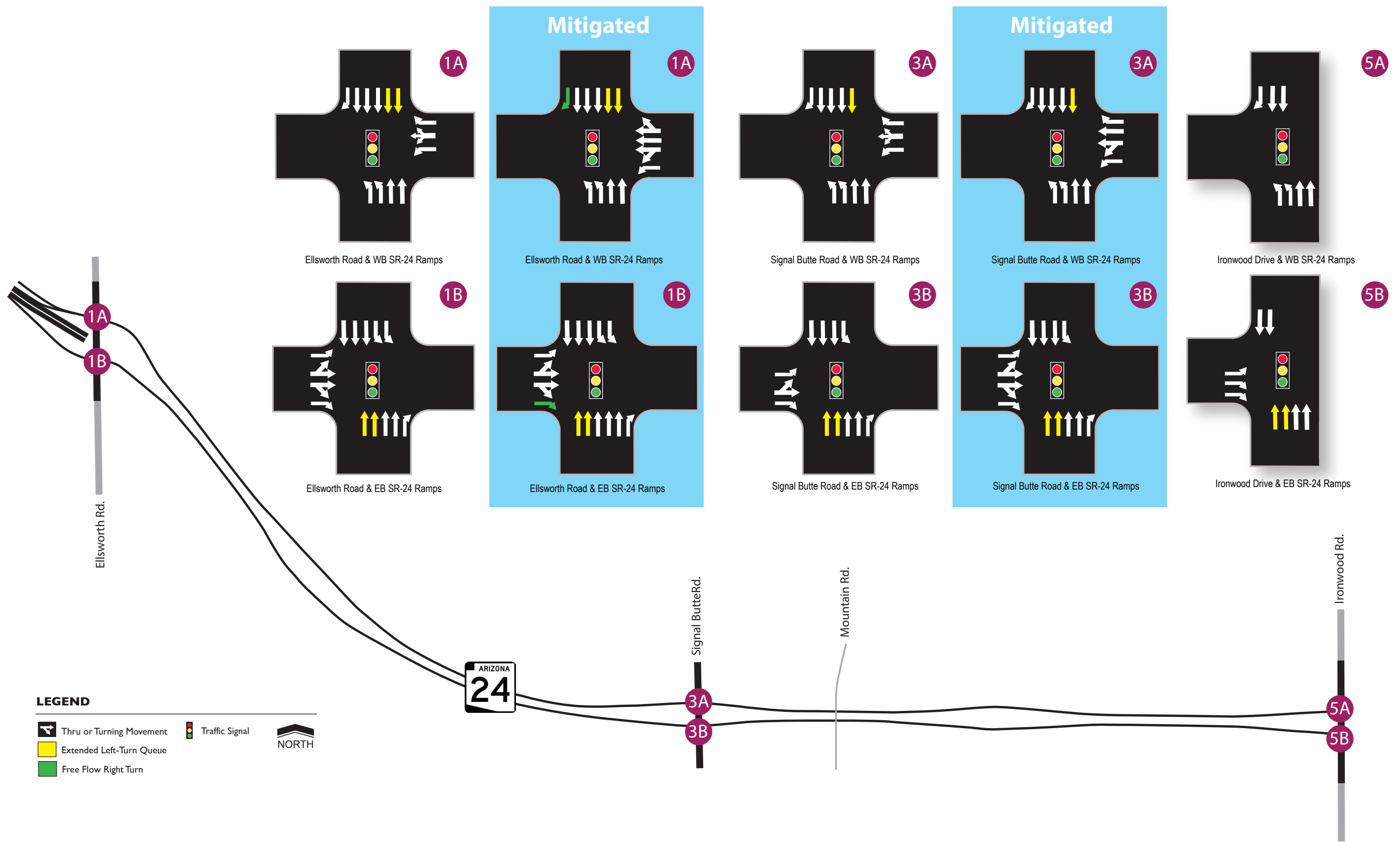


Figure 6: 2025 Option A - Proposed Lane Configurations and Stop Controls

Table 5 – 2025 Option A Peak Hour Levels of Service

ID	Intersection	Stop Control	Approach	AM (PM) Peak Hour			
				Left	Thru	Right	Overall
1A	Ellsworth Road & WB SR 24 Ramps ⁽¹⁾	Signalized	NB	F(F)	A(A)	--(--)	F(E)
			SB	--(--)	D(B)	A(A)	D(B)
			WB	C(D)	F(F)	C(D)	F(F)
			Overall	F(F)			
1B	Ellsworth Road & EB SR 24 Ramps ⁽¹⁾	Signalized	NB	--(--)	F(D)	C(D)	F(D)
			SB	D(D)	A(B)	--(--)	A(C)
			EB	D(C)	D(F)	A(A)	D(F)
			Overall	F(E)			
3A	Signal Butte Road & WB SR 24 Ramps ⁽¹⁾	Signalized	NB	C(D)	A(A)	--(--)	C(C)
			SB	--(--)	C(C)	D(D)	C(C)
			WB	C(B)	F(C)	C(B)	E(C)
			Overall	F(C)			
3B	Signal Butte Road & EB SR 24 Ramps ⁽¹⁾	Signalized	NB	--(--)	D(D)	D(D)	D(D)
			SB	D(D)	A(B)	--(--)	C(B)
			EB	B(B)	C(F)	C(F)	C(E)
			Overall	C(E)			
5A	Ironwood Drive & WB SR 24 Ramps	Signalized	NB	A(A)	A(A)	--(--)	A(A)
			SB	--(--)	C(B)	C(B)	C(B)
5B	Ironwood Drive & EB SR 24 Ramps	Signalized	NB	--(--)	C(D)	--(--)	B(D)
			SB	--(--)	A(B)	--(--)	A(B)
			Overall	B(C)			

(1) An alternate mitigation analysis has been performed for the intersections of the SR 24 Ramps and Ellsworth Road and the intersections of the SR 24 Ramps and Signal Butte Road and included in this report.

The results of the intersection capacity analysis in **Table 5** indicate that the SR 24 intersections at Ellsworth Road and Signal Butte Road are expected to experience delays during the peak hours.

The intersection of **Ellsworth Road and WB SR 24 Ramps** is predicted to experience delays during the AM and PM peak hours. During both peak hours, the demand of northbound left turning movement conflicts with the demand of the westbound off ramp through movement. Vehicles are expected to experience delays for the westbound approach movements and northbound left turning movement. An alternate mitigation analysis is included in this report.

The intersection of **Ellsworth Road and EB SR 24 Ramps** is predicted to experience delays during the AM and PM peak hours. During the AM peak hour, the heavy northbound through volumes on Ellsworth Road require the majority of green time which minimizes the green time available for other movements. During the PM peak hour, the heavy through volumes on the SR 24 eastbound off ramp conflict with southbound traffic on Ellsworth Road. Southbound left turning vehicles and the eastbound ramp approach vehicles are expected to experience delays during the PM peak hour. An alternate mitigation analysis is also included in this report.

The intersection of **Signal Butte Road and WB SR 24 Ramps** is predicted to experience delays in the AM peak hour. The high volumes of through vehicles on westbound SR 24 conflict with the NB left turning vehicles travelling to westbound SR 24. An alternate mitigation analysis is also included in this report.

The intersection of **Signal Butte Road and EB SR 24 Ramps** is predicted to experience delays in the PM peak hour. The high volumes of through vehicles on eastbound SR 24 conflict with the SB left turning vehicles travelling to eastbound SR 24. An alternate mitigation analysis is also included in this report.

2025 OPTION A MITIGATED INTERSECTION LEVEL OF SERVICE ANALYSIS

A mitigation analysis was performed for the 2025 Option A scenario at intersections that experience delays in the AM and PM peak hours. ADOT may consider the mitigated lane configurations shown in **Figure 6** to improve levels of service. The resulting intersection movement level of service is shown in **Table 6**. Grade separation of interchanges is not recommended in the 2025 Option A Mitigated Scenario.

Table 6 – 2025 Option A Mitigated Analysis Peak Hour Levels of Service

ID	Intersection	Stop Control	Approach	AM (PM) Peak Hour			
				Left	Thru	Right	Overall
1A	Ellsworth Road & WB SR 24 Ramps	Signalized	NB	F(F)	A(A)	--(--)	F(E)
			SB	--(--)	D(B)	A(A)	D(B)
			WB	C(D)	D(D)	D(D)	D(D)
			Overall	F(D)			
1B	Ellsworth Road & EB SR 24 Ramps	Signalized	NB	--(--)	F(D)	C(D)	F(D)
			SB	D(D)	A(B)	--(--)	A(C)
			EB	D(C)	D(F)	A(A)	D(F)
			Overall	F(E)			
3A	Signal Butte Road & WB SR 24 Ramps	Signalized	NB	C(D)	A(A)	--(--)	C(C)
			SB	--(--)	C(C)	D(D)	D(C)
			WB	C(B)	D(C)	C(B)	D(C)
			Overall	D(C)			
3B	Signal Butte Road & EB SR 24 Ramps	Signalized	NB	--(--)	D(D)	D(D)	D(D)
			SB	D(D)	A(B)	--(--)	C(B)
			EB	B(B)	C(C)	C(C)	C(C)
			Overall	C(C)			

The results of the intersection capacity analysis in **Table 6** indicate that the SR 24 intersections at Ellsworth Road are expected to experience delays during the peak hours.

The intersection of **Ellsworth Road and WB SR 24 Ramps** is predicted to experience delays during the AM peak hour. The demand of northbound left turning movement conflicts with the demand of the westbound off ramp through movement. Vehicles are expected to experience delays for the westbound approach movements and northbound left turning movement.

The intersection of **Ellsworth Road and EB SR 24 Ramps** is predicted to experience delays during the AM and PM peak hours. During the AM peak hour, the heavy northbound through volumes on Ellsworth Road require the majority of green time which minimizes the green time available for other movements. During the PM peak hour, the heavy through volumes on the SR 24 eastbound off ramp conflict with southbound traffic on Ellsworth Road. Southbound left turning vehicles and the eastbound ramp approach vehicles are expected to experience delays during the PM peak hour.

2025 OPTION B INTERSECTION LEVEL OF SERVICE ANALYSIS

The 2025 Option B mitigated intersection capacity analysis was performed using the unmitigated lane configurations and stop control as shown in **Figure 7**. The resulting intersection movement level of service is shown in **Table 7**. An alternate mitigated intersection movement level of service analysis is shown in **Table 8**.

Table 7 – 2025 Option B Peak Hour Levels of Service

ID	Intersection	Stop Control	Approach	AM (PM) Peak Hour			
				Left	Thru	Right	Overall
1A	Ellsworth Road & WB SR 24 Ramps ⁽¹⁾	Signalized	NB	F(F)	A(A)	--(--)	F(F)
			SB	--(--)	D(C)	A(A)	D(C)
			WB	C(C)	D(C)	D(C)	D(C)
			Overall	F(E)			
1B	Ellsworth Road & EB SR 24 Ramps ⁽¹⁾	Signalized	NB	--(--)	F(D)	C(D)	F(D)
			SB	D(D)	A(B)	--(--)	A(C)
			EB	C(C)	C(D)	A(A)	C(D)
			Overall	E(D)			
3A	Signal Butte Road & WB SR 24 Ramps	Signalized	NB	B(A)	A(A)	--(--)	A(A)
			SB	--(--)	B(C)	B(C)	B(C)
			Overall	B(A)			
3B	Signal Butte Road & EB SR 24 Ramps	Signalized	NB	--(--)	C(D)	--(--)	C(D)
			SB	--(--)	A(C)	--(--)	A(C)
			EB	B(A)	--(--)	A(A)	B(A)
			Overall	C(D)			

(1) An alternate mitigation analysis has been performed for the intersections of the SR 24 Ramps and Ellsworth Road and included in this report.

The results of the intersection capacity analysis in **Table 7** indicate that the SR 24 intersections at Ellsworth Road are expected to experience delays during the peak hours.

The intersection of **Ellsworth Road and WB SR 24 Ramps** is predicted to experience delays during the AM and PM peak hours. During both peak hours, the demand of northbound left turning movement conflicts with the demand of the westbound off ramp through movement. Vehicles are expected to experience delays for the westbound approach movements and northbound left turning movement. An alternate mitigation analysis is included in this report.

The intersection of **Ellsworth Road and EB SR 24 Ramps** is predicted to experience delays during the AM and PM peak hours. During the AM peak hour, the heavy northbound through volumes on Ellsworth Road require the majority of green time which minimizes the green time available for other movements. An alternate mitigation analysis is also included in this report.

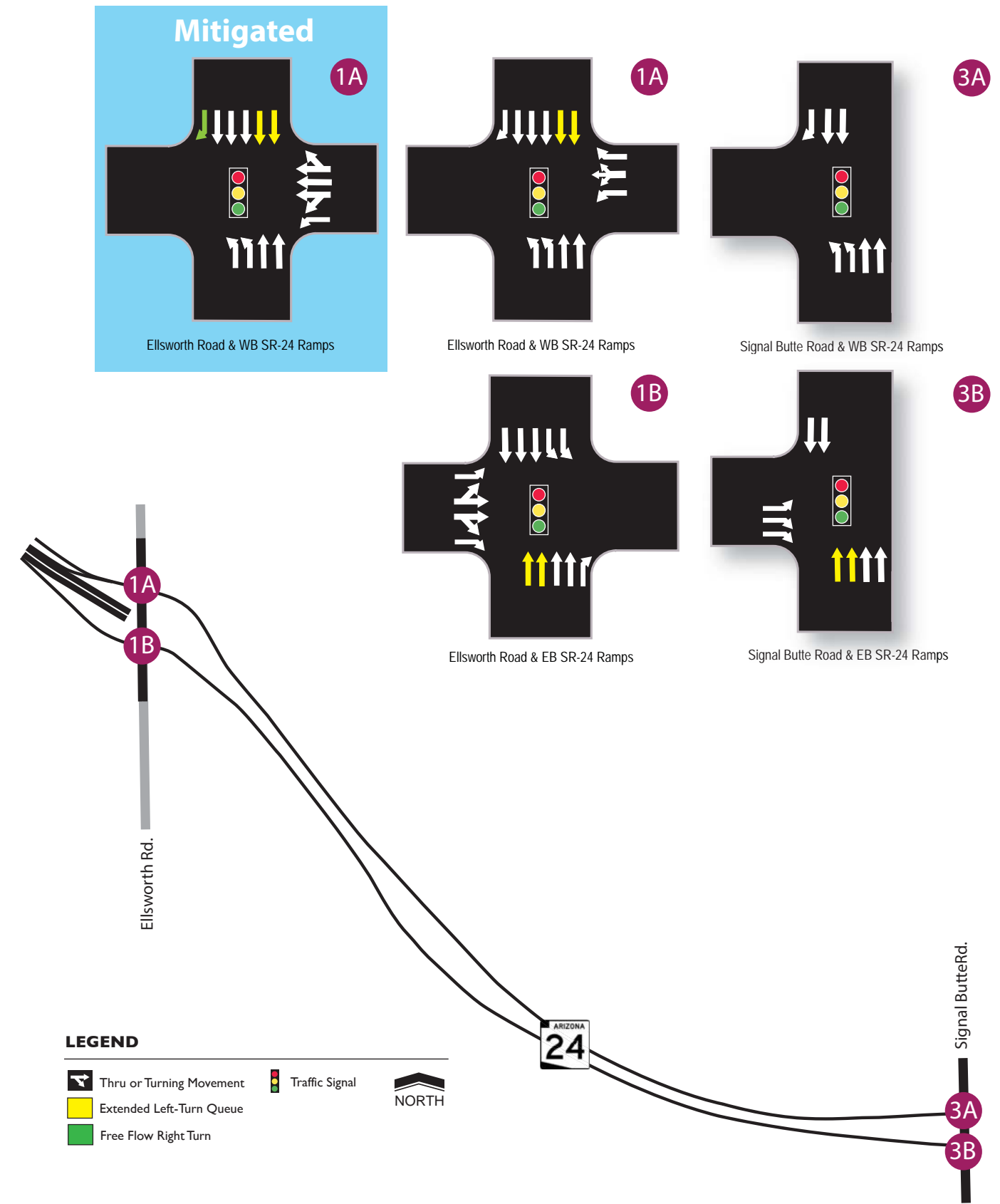


Figure 7: 2025 Option B - Proposed Lane Configurations and Stop Controls

2025 OPTION B MITIGATED INTERSECTION LEVEL OF SERVICE ANALYSIS

A mitigation analysis was performed for the 2025 Option B scenario at intersections that experience delays in the AM and PM peak hours. ADOT may consider the mitigated lane configurations shown in **Figure 7** to improve levels of service. Grade separation of interchanges is not recommended in the 2025 Option B Mitigated Scenario.

The 2025 Option B mitigated intersection capacity analysis was performed using the recommended lane configurations as shown in **Figure 7**. The resulting intersection movement level of service is shown in **Table 8**.

Table 8 – 2025 Option B Mitigated Analysis Peak Hour Levels of Service

ID	Intersection	Stop Control	Approach	AM (PM) Peak Hour			
				Left	Thru	Right	Overall
1A	Ellsworth Road & WB SR 24 Ramps	Signalized	NB	F(F)	A(A)	--(--)	F(F)
			SB	--(--)	D(C)	A(A)	D(C)
			WB	C(C)	D(C)	D(C)	D(C)
			Overall	F(E)			
1B	Ellsworth Road & EB SR 24 Ramps	Signalized	NB	--(--)	F(D)	C(D)	F(D)
			SB	D(D)	A(B)	--(--)	A(C)
			EB	C(C)	C(D)	A(A)	C(D)
			Overall	E(D)			

The results of the intersection capacity analysis in **Table 8** indicate that the SR 24 intersections at Ellsworth Road are expected to experience delays during the peak hours. The proposed mitigation measures are not predicted to improve the level of service at the intersections of Ellsworth Road and SR 24 in 2025.

2035 INTERSECTION LEVEL OF SERVICE ANALYSIS

The 2035 intersection capacity analysis was performed using the recommended lane configurations as shown in **Figure 8**. The resulting intersection movement level of service is shown in **Table 9**.

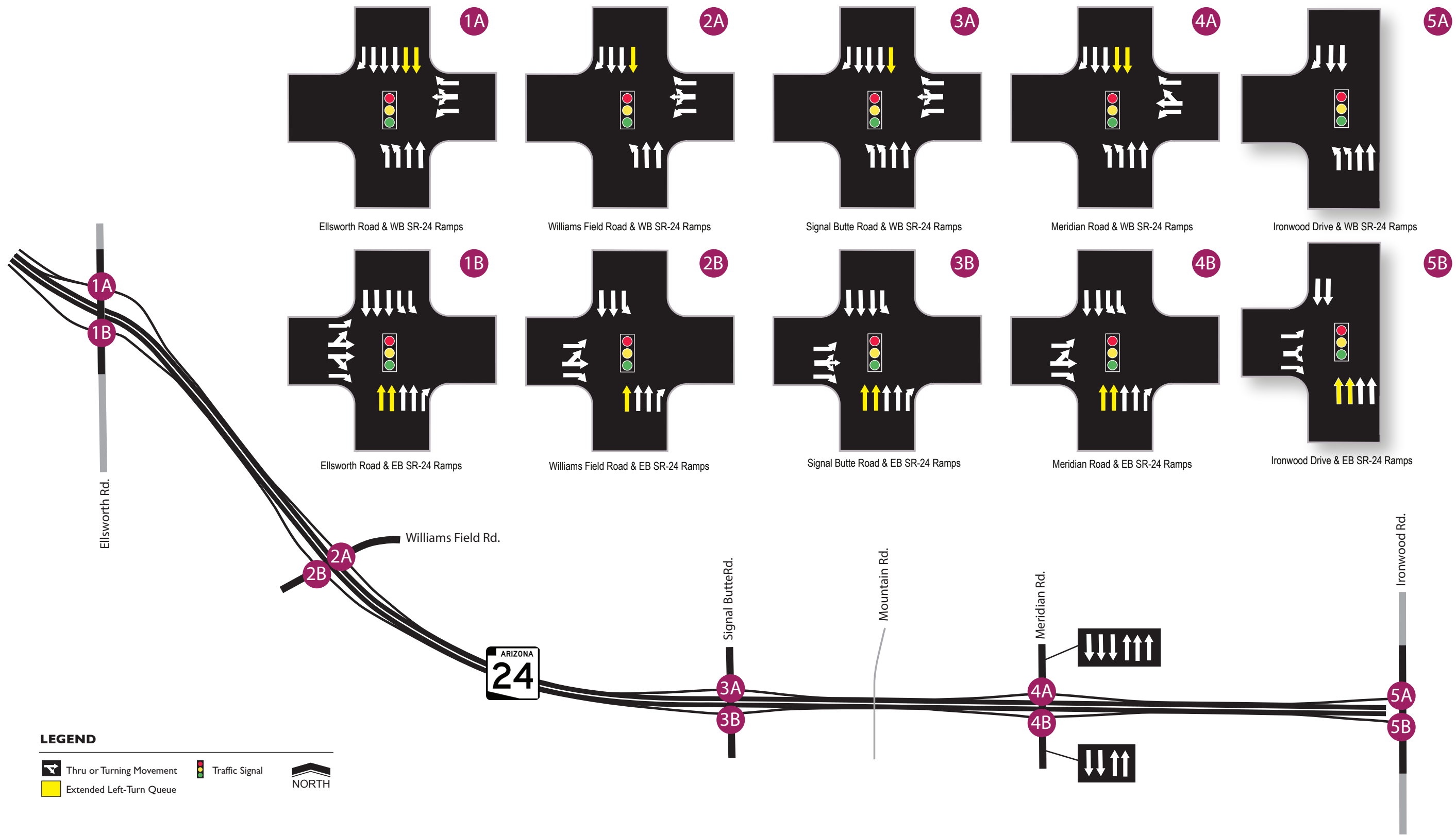


Figure 8: 2035 Proposed Lane Configurations and Stop Controls

Table 9 – 2035 Peak Hour Levels of Service

ID	Intersection	Stop Control	Approach	AM (PM) Peak Hour			
				Left	Thru	Right	Overall
1A	Ellsworth Road & WB SR 24 Ramps	Signalized	NB	C(D)	A(A)	--(--)	C(B)
			SB	--(--)	D(B)	A(A)	D(B)
			WB	D(C)	--(--)	D(C)	D(C)
			Overall	C(C)			
1B	Ellsworth Road & EB SR 24 Ramps	Signalized	NB	--(--)	D(D)	C(D)	D(D)
			SB	D(D)	A(A)	--(--)	C(B)
			EB	D(C)	--(--)	A(A)	D(C)
			Overall	C(C)			
2A	Williams Field Road & WB SR 24 Ramps	Signalized	NB	B(B)	A(A)	--(--)	A(A)
			SB	--(--)	B(B)	C(C)	C(C)
			EB	C(C)	--(--)	C(C)	C(C)
			Overall	C(C)			
2B	Williams Field Road & EB SR 24 Ramps	Signalized	NB	--(--)	C(C)	C(C)	C(C)
			SB	C(C)	A(A)	--(--)	B(B)
			WB	B(B)	--(--)	B(B)	B(B)
			Overall	C(C)			
3A	Signal Butte Road & WB SR 24 Ramps	Signalized	NB	B(D)	A(A)	--(--)	A(A)
			SB	--(--)	D(C)	D(C)	D(C)
			EB	D(C)	--(--)	D(C)	D(C)
			Overall	C(B)			
3B	Signal Butte Road & EB SR 24 Ramps	Signalized	NB	--(--)	C(C)	D(C)	C(C)
			SB	C(D)	A(A)	--(--)	B(A)
			WB	D(D)	--(--)	D(D)	D(D)
			Overall	C(C)			
4A	Meridian Road & WB SR 24 Ramps	Signalized	NB	F(A)	A(A)	--(--)	D(A)
			SB	--(--)	D(D)	A(A)	D(D)
			WB	E(D)	--(--)	D(D)	D(D)
			Overall	D(B)			
4B	Meridian Road & EB SR 24 Ramps	Signalized	NB	--(--)	D(D)	C(C)	D(D)
			SB	C(C)	A(A)	--(--)	A(A)
			EB	D(C)	--(--)	A(A)	D(C)
			Overall	D(C)			
5A	Ironwood Drive & WB SR 24 Ramps	Signalized	NB	A(A)	A(A)	--(--)	A(A)
			SB	--(--)	C(B)	B(A)	C(B)
			Overall	A(A)			
5B	Ironwood Drive & EB SR 24 Ramps	Signalized	NB	--(--)	B(D)	--(--)	B(D)
			SB	--(--)	A(B)	--(--)	A(B)
			EB	C(B)	--(--)	C(B)	C(B)
			Overall	B(C)			

The results of the intersection capacity analysis indicate that all study intersection approaches and movements are predicted to operate at LOS D or better during the peak hours except for select movements at the intersection of **Meridian Road and SR 24 WB Ramps**.

The northbound left turning vehicles and westbound left turning vehicles conflict at the intersection of **Meridian Road and SR 24 WB Ramps** and are expected to experience delays in the AM peak hour. Vehicles are expected to queue on the westbound on ramp and northbound left turn lane. It is not uncommon for heavy turning movements at

freeway interchanges to experience delays in the peak hour. No mitigation is recommended.

INTERSECTION AND FREEWAY SEGMENT LANE REQUIREMENTS

As a result of the intersection capacity analyses and the projected AADT's, the proposed intersection approach lane configurations are depicted in **Figure 6**, **Figure 7** and **Figure 8** for the 2025 Option A, 2025 Option B and 2035 scenarios.

CONCLUSIONS AND RECOMMENDATIONS

The following findings, conclusions, and recommendations have been documented in this study:

Existing Conditions

- ♦ All existing intersection approaches operate at an acceptable level of service (LOS D) with the existing lane configurations and stop control except for select turning movements during the AM and PM peak hours. The northbound left turn movement experiences delays in the AM peak hour due to a combination of the high left turn volume and southbound volumes and the limited green time for the northbound left turn movement. The eastbound right turn movement experiences delay in the PM peak hour due to the limited green time for the eastbound approach as a result of the high demand of vehicles on Ellsworth Road.
- ♦ The segment of SR 24 from Loop 202 to Ellsworth Road experienced 24 crashes in 2014 and 2015. The data provided does not seem to indicate any unusual crash pattern.
- ♦ The intersections of SR 24 at Ellsworth Road experienced 27 crashes in 2014 and 2015. The data provided does not seem to indicate any unusual crash patterns.

2025 Option A Scenario

- ♦ Option A proposes extending SR 24 from Ellsworth Road to Ironwood Drive as an at grade arterial roadway with an at grade intersection at Signal Butte Road. The existing at grade intersection with Ellsworth Road would remain if possible and an "end of expressway" condition would occur at Ironwood Road. Mountain Road would be "grade separated" over SR 24.
- ♦ Grade separation of interchanges is not recommended in the 2025 Option A scenario.
- ♦ The 2025 Option A intersection capacity analysis was performed using the recommended lane configurations and stop control as shown in **Figure 6**.

- ◆ The results of the intersection capacity analysis in **Table 5** indicate that the SR 24 intersections at Ellsworth Road and Signal Butte Road are expected to experience delays during the peak hours.
 - The intersection of **Ellsworth Road and WB SR 24 Ramps** is predicted to experience delays during the AM and PM peak hours. During both peak hours, the demand of northbound left turning movement conflicts with the demand of the westbound off ramp through movement. Vehicles are expected to experience delays for the westbound approach movements and northbound left turning movement. An alternate mitigation analysis is included in this report.
 - The intersection of **Ellsworth Road and EB SR 24 Ramps** is predicted to experience delays during the AM and PM peak hours. During the AM peak hour, the heavy northbound through volumes on Ellsworth Road require the majority of green time which minimizes the green time available for other movements. During the PM peak hour, the heavy through volumes on the SR 24 eastbound off ramp conflict with southbound traffic on Ellsworth Road. Southbound left turning vehicles and the eastbound ramp approach vehicles are expected to experience delays during the PM peak hour. An alternate mitigation analysis is also included in this report.
 - The intersection of **Signal Butte Road and WB SR 24 Ramps** is predicted to experience delays in the AM peak hour. The high volumes of through vehicles on westbound SR 24 conflict with the NB left turning vehicles travelling to westbound SR 24. An alternate mitigation analysis is also included in this report.
 - The intersection of **Signal Butte Road and EB SR 24 Ramps** is predicted to experience delays in the PM peak hour. The high volumes of through vehicles on eastbound SR 24 conflict with the SB left turning vehicles travelling to eastbound SR 24. An alternate mitigation analysis is also included in this report.

2025 Option A Mitigated Analysis

- ◆ A mitigation analysis was performed for the 2025 Option A scenario at intersections that experience delays in the AM and PM peak hours. ADOT may consider the mitigated lane configurations shown in **Figure 6** to improve levels of service.
- ◆ The results of the intersection capacity analysis in **Table 6** indicate that the SR 24 intersections at Ellsworth Road are expected to experience delays during the peak hours.
 - The intersection of **Ellsworth Road and WB SR 24 Ramps** is predicted to experience delays during the AM peak hour. The demand of northbound left turning movement conflicts with the demand of the westbound off ramp through movement. Vehicles are expected to experience delays for the westbound approach movements and northbound left turning movement.

- The intersection of **Ellsworth Road and EB SR 24 Ramps** is predicted to experience delays during the AM and PM peak hours. During the AM peak hour, the heavy northbound through volumes on Ellsworth Road require the majority of green time which minimizes the green time available for other movements. During the PM peak hour, the heavy through volumes on the SR 24 eastbound off ramp conflict with southbound traffic on Ellsworth Road. Southbound left turning vehicles and the eastbound ramp approach vehicles are expected to experience delays during the PM peak hour.

2025 Option B Scenario

- ◆ Option B is an at grade arterial roadway extension from Ellsworth Road to Signal Butte Road with no additional access. The existing at grade intersection with Ellsworth Road would remain if possible and an “end of expressway” condition would occur at Signal Butte Road.
- ◆ Grade separation of interchanges is not recommended in the 2025 Option B scenario.
- ◆ The 2025 Option B intersection capacity analysis was performed using the recommended lane configurations and stop control as shown in **Figure 7**.
- ◆ The results of the intersection capacity analysis in **Table 7** indicate that the SR 24 intersections at Ellsworth Road are expected to experience delays during the peak hours.
 - The intersection of **Ellsworth Road and WB SR 24 Ramps** is predicted to experience delays during the AM and PM peak hours. During both peak hours, the demand of northbound left turning movement conflicts with the demand of the westbound off ramp through movement. Vehicles are expected to experience delays for the westbound approach movements and northbound left turning movement. An alternate mitigation analysis is included in this report.
 - The intersection of **Ellsworth Road and EB SR 24 Ramps** is predicted to experience delays during the AM and PM peak hours. During the AM peak hour, the heavy northbound through volumes on Ellsworth Road require the majority of green time which minimizes the green time available for other movements. An alternate mitigation analysis is also included in this report.

2025 Option B Mitigated Analysis

- ◆ A mitigation analysis was performed for the 2025 Option B scenario at intersections that experience delays in the AM and PM peak hours. ADOT may

consider the mitigated lane configurations shown in **Figure 7** to improve levels of service.

- ◆ The results of the intersection capacity analysis in **Table 8** indicate that the SR 24 intersections at Ellsworth Road are expected to experience delays during the peak hours. The proposed mitigation measures are not predicted to improve the level of service at the intersections of Ellsworth Road and SR 24 in 2025.

2035 Horizon Year

- ◆ In 2035, SR 24 is considered to be a controlled access freeway, extending the existing freeway from Ellsworth Road to Ironwood Drive. Freeway interchanges will be provided at Ellsworth Road, Williams Field Road, Signal Butte Road, Meridian Road, and Ironwood Drive.
- ◆ The 2035 intersection capacity analysis was performed using the recommended lane configurations and stop control as shown in **Figure 8**.
- ◆ The results of the intersection capacity analysis indicate that all study intersection approaches and movements are predicted to operate at LOS D or better during the peak hours except for select movements at the intersection of **Meridian Road and SR 24 WB Ramps**.
- ◆ The northbound left turning vehicles and westbound left turning vehicles conflict at the intersection of **Meridian Road and SR 24 WB Ramps** and are expected to experience delays in the AM peak hour. Vehicles are expected to queue on the westbound on ramp and northbound left turn lane. It is not uncommon for heavy turning movements at freeway interchanges to experience delays in the peak hour. No mitigation is recommended.

LIST OF REFERENCES

A Policy on Geometric Design (Green Book). American Association of State and Highway Transportation Officials, Washington D.C., 2011.

Highway Capacity Manual. Transportation Research Board, National Research Council, Washington D.C., 2010.

Manual of Uniform Traffic Control Devices, U.S. Department of Transportation, Federal Highways Administration, Washington D.C., 2009.

Maricopa Association of Governments Regional Demand Model

Arizona Department of Transportation Traffic Safety Crash Data (2014 and 2015)

NCHRP Report 765, National Cooperative Highway Research Program, 2014

TECHNICAL APPENDIX

- APPENDIX A: ADOT REVIEW COMMENTS**
- APPENDIX B: EXISTING PEAK HOUR TRAFFIC COUNTS**
- APPENDIX C: EXISTING PEAK HOUR ANALYSIS**
- APPENDIX D: ADOT 2014 AND 2015 CRASH DATA**
- APPENDIX E: MAG TRAVEL DEMAND MODEL DATA**
- APPENDIX F: PEAK HOUR TURNING MOVEMENT CALCULATIONS**
- APPENDIX G: 2025 OPTION A PEAK HOUR ANALYSIS**
- APPENDIX H: 2025 OPTION A MITIGATED PEAK HOUR ANALYSIS**
- APPENDIX I: 2025 OPTION B PEAK HOUR ANALYSIS**
- APPENDIX J: 2025 OPTION B MITIGATED PEAK HOUR ANALYSIS**
- APPENDIX K: 2035 PEAK HOUR ANALYSIS**



ADOT REVIEW COMMENTS

APPENDIX A

SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road in Maricopa County and Pinal County, Arizona

Draft IDCR Comment Response Document

Client Project Manager: Ronald McCally

Consultant: **PARSONS**

OVERALL COMMENT NO.	REVIEWER COMMENT NO.	DWG, SHT, PAGE NO.	COMMENT	INITIAL CODE	FINAL CODE	DESIGNER RESPONSE
18	12	Traffic Analysis Report	On Page 6, 1st Paragraph under Existing Intersection Configuration it states that the NB approach on Ellsworth consists of four through lanes at the EB off-ramp. Technically there are four lanes going through this intersection but in reality there are only two through lanes. The other two lanes are actually two left turn storage lanes for the WB on-ramp.	A		The text of the report will be updated to clarify that two left turn lanes are queue storage for the northbound left turn lanes at the intersection of Ellsworth Road and SR 24 EB Ramps.
19	13	Traffic Analysis Report	On Page 8 the left turn arrow in Figure 1A is missing.	A		The figure will be corrected.
20	14	Traffic Analysis Report	On Page 9, it appears that the data in Table 2 is backwards for 1A and 1B.	A		
21	15	Traffic Analysis Report	On Page 9 in the first sentence of the 2nd paragraph under Crash Analysis it states, " identified a one-year total of 24 crashes (without any fatalities) on 24 from Loop 202 . . ." Should it not say " identified a one-year total of 24 crashes (without any fatalities on SR 24 from Loop 202 . . ."	A		The table will be corrected.

**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
in Maricopa County and Pinal County, Arizona**

Draft IDCR Comment Response Document

Client Project Manager: Ronald McCally
Consultant: **PARSONS**

OVERALL COMMENT NO.	REVIEWER COMMENT NO.	DWG, SHT, PAGE NO.	COMMENT	INITIAL CODE	FINAL CODE	DESIGNER RESPONSE
22	16	Traffic Analysis Report	On Page 11 under Projected Segment Traffic Volumes, it states an "end of freeway" condition. Ellsworth is the "end of freeway" condition and Signal Butte in Option B or Ironwood in Option A would be an "end of expressway" condition. Per the ADOT Roadway Design Guide (2012), "Full access control gives preference to through traffic by providing access only through selected public roads and by prohibiting at-grade crossings or direct access from abutting property. Partial access control still gives preference to through traffic but permits some crossings at grade and some private driveway connections." The 2009 MUTCD defines a Freeway as a divided highway with full access control and an Expressway as a divided highway with partial control of access. "End of freeway" exists at Ellsworth Rd with the at-grade signalized intersection. In the Interim SR 24 could only be labeled as an Expressway with the at-grade intersections with partial controlled access from Ellsworth Rd to Signal Butte Rd/Ironwood Rd, depending on the Option selected.	B	A	The report will be updated to state that Ellsworth Road is an end of expressway condition in Option A.
23	17	Traffic Analysis Report	On Page 4-4 of the DCR, 1st paragraph under 4.4.2 Ellsworth Road Interim TI it states, "For the interim condition, NB Ellsworth Road will be widened to add additional pavement for the future third through lane northbound." The DCR does not state that the third lane would be opened to traffic but is shown as a possibility in Appendix C C-4.01. The projected traffic volumes do not show any projections with the possibility of this third NB through lane	B	A	Pavement widening on Ellsworth Road is to accommodate the 12-foot lane shift of the existing NB through lanes. The additional pavement width will be used for the third northbound left turn lane.

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2016-07-18 H8915 01L_02L_SR 24 Draft IDCR Comments

A-Will Comply
B-Consultant To Evaluate
C-ADOT To Evaluate
D-No Further Action Required
Page 10 of 33

**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
in Maricopa County and Pinal County, Arizona**

Draft IDCR Comment Response Document

Client Project Manager: Ronald McCally
Consultant: **PARSONS**

OVERALL COMMENT NO.	REVIEWER COMMENT NO.	DWG, SHT, PAGE NO.	COMMENT	INITIAL CODE	FINAL CODE	DESIGNER RESPONSE
24	18	Traffic Analysis Report	Currently Signal Butte Rd does not exist in the area of SR 24. From what I understand in the DCR under Option A that this road will not be built by 2025. Under Option B it would become the logical terminus but would still have to be built. Why is it under Option A that you are showing through movements NB and SB through the intersections to a nonexistent road?	B	D	City of Mesa is planning to construct Signal Butte Road from Ray Road to Pecos Road.
25	19	Traffic Analysis Report	In Figure 4 and Figure 5, on the diagram you are showing Meridian Rd as Moeur Rd.	A	A	Will change
26	20	Traffic Analysis Report	On Page 18, 20, Figure 6, and Figure 7 for the Mitigated intersections, adding a third left turn lane for the WB on ramp at Ellsworth would improve the level of service for Option A and Option B but there are other factors that also need to be considered. By adding the third left turn lane this would mean widening Ellsworth Rd with another lane on top of the third NB through lane. Also, the WB on-ramp would need to be widened to three lanes from the existing two in order to accommodate the third left turn lane. By adding the third lane on the ramp there would need to be enough room in order to merge that third lane prior to Ramp A or leaving the third lane as the Ramp A lane from the Ellsworth intersection.	B	D	The third left turn lane has been deleted.
27	21	Traffic Analysis Report	Figure 7, the proposed lane configuration diagrams label 3A and 3B as Ironwood Dr when they should be Signal Butte Rd.	A		The figure will be corrected.

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2016-07-18 H8915 01L_02L_SR 24 Draft IDCR Comments

A-Will Comply
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D-No Further Action Required
Page 11 of 33

**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
in Maricopa County and Pinal County, Arizona**

Draft IDCR Comment Response Document

Client Project Manager: Ronald McCally
Consultant: **PARSONS**

OVERALL COMMENT NO.	REVIEWER COMMENT NO.	DWG, SHT, PAGE NO.	COMMENT	INITIAL CODE	FINAL CODE	DESIGNER RESPONSE
28	22	Traffic Analysis Report	Page 26 under 2025 Option A Scenario, 1st paragraph Ironwood Rd would not be an "end of freeway" but an "end of expressway" condition. Also it states that Mountain Rd would be "grade separated" over SR 24 but in the next paragraph it states, "Grade separation of interchanges is not recommended in the 2025 Option A scenario." Maybe it should be re-stated that all other interchanges besides Mountain Rd will not be grade separated.	D	D	Mountain Road will not be an interchange. It will just be a grade separated crossing. It will not have direct access to SR-24.
29	23	Traffic Analysis Report	Page 27, third paragraph under 2025 Option A Mitigated Analysis, third line states, ". . ."ramp through movement During AM both peak hour." Please clarify.	A	A	The report will be updated to state that the northbound left turn turning movement conflicts with the westbound ramp movements. The word "through" will be deleted.
30	24	Traffic Analysis Report	Page 27 under 2025 Option B Scenario, 1st paragraph, Signal Butte would be "end of expressway" condition and not "end of freeway."	B/C	A	The report will be updated to designate that Signal Butte Road will be an "end of expressway" condition.
			EUNICE CHAN, FHWA			

A-Will Comply
B-Consultant To Evaluate
C-ADOT To Evaluate
D-No Further Action Required

**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
in Maricopa County and Pinal County, Arizona**

Draft IDCR Comment Response Document

Client Project Manager: Ronald McCally
Consultant: **PARSONS**

OVERALL COMMENT NO.	REVIEWER COMMENT NO.	DWG, SHT, PAGE NO.	COMMENT	INITIAL CODE	FINAL CODE	DESIGNER RESPONSE
31	1	Pg 3, Traffic Analysis Report	2025 Opt A Mitigated Analysis references expected delays for the NB left turn movement at the intersection of Ellsworth Rd and WB SR24 Ramps and no further mitigation is recommended. a. Include discussion of the severity of the impact to justify the recommendation for no mitigation. Appendix H seems to indicate that even with the mitigation measures, there will be a 76.8 s/veh delay for the NBL movement on Ellsworth and SR 24 WB Ramps, and a 102.9 s/veh delay for the EBT movement on Ellsworth Rd and SR 24 EB Ramps.	B	A	The predicted overall level of service for the 2025 Option A mitigated condition is level of service D or better. The predicted delay for northbound left turning vehicles is in the AM peak hour only. For intersection with heavy through movements, turning movement delays in the peak hour are not uncommon.
32	2	Pg 4, Traffic Analysis Report	2035 Horizon Year – mentions that vehicles are expected to queue on the westbound on ramp and northbound left turn lane at the intersection of Meridian Rd and SR 24 WB Ramps and no mitigation is recommended. a. Include discussion of the severity of the impact to justify the recommendation for no mitigation. For example, Appendix K indicates LOS F during peak hours for the NBL in 2035, but the delay is only 58.1 s/veh.	B	A	The predicted overall level of service for the 2035 horizon year is level of service D or better. The predicted delay for northbound and westbound turning vehicles is in the AM peak hour only. For intersection with heavy through movements, turning movement delays in the peak hour are not uncommon.
33	3	Pg 6, Traffic Analysis Report	Existing Roadway Network – Include sentence on posted speed limit for Meridian Road.	A	A	
34	4	Pg 11, Traffic Analysis Report	Design Concept Report Alternatives and Projected Segment Traffic Volumes discussions appear to be the same?	A	A	The report will be updated.

A-Will Comply
B-Consultant To Evaluate
C-ADOT To Evaluate
D-No Further Action Required

**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
in Maricopa County and Pinal County, Arizona**

Draft IDCR Comment Response Document

Client Project Manager: Ronald McCally
Consultant: **PARSONS**

OVERALL COMMENT NO.	REVIEWER COMMENT NO.	DWG, SHT, PAGE NO.	COMMENT	INITIAL CODE	FINAL CODE	DESIGNER RESPONSE
35	5	Pg 17, Traffic Analysis Report	Table 5: a. Clarify "recommended lane configurations" in the first sentence. Figure 6 only labels the "Mitigated" configurations. Are the recommended lane configurations the ones that are unlabeled? b. Include discussion of the severity of unmitigated peak hour delays (Appendix G). For example, not incorporating the recommended mitigation would result in LOS F with a delay of 1373.2 s/veh for the NBL and 564.1 veh/s for WBT at the intersection of Ellsworth Rd and SR 24 WB Ramps.	A B	A	a. Table 5 refers to the unmitigated lane configurations. The text and figures will be updated. b. Table 5 refers to the unmitigated lane configurations. An alternative analysis is shown in Table 6 with the mitigated levels of service. Discussion referring to Table 6 and the mitigated analysis will be added to this section.
36	6	Pg 18, Traffic Analysis Report	Table 6 – See comment 1. Table shows LOS C for EB through movements at Ellsworth Rd and EB SR 24 Ramps. But Appendix H shows LOS F?	A		Table will be updated.
37	7	Pg 19, Traffic Analysis Report	Table 7 – See comment 5.a.	A		Table 7 refers to the unmitigated lane configurations. The text and figures will be updated.
38	8	Pg 21, Traffic Analysis Report	Table 9 – See comment 2.a.	A		Table 9 refers to the unmitigated lane configurations. The text and figures will be updated.
39	9	Traffic Analysis Report	Figure 6 - Didn't see a difference between the original and the mitigated configuration for 3A or 3B? What was the mitigation?	A		An additional lane was added to the WB and EB approaches of the off ramp intersections.

A-Will Comply
B-Consultant To Evaluate
C-ADOT To Evaluate
D-No Further Action Required

**SR 24 (Gateway Freeway) Ellsworth Road to Ironwood Road
in Maricopa County and Pinal County, Arizona**

Draft IDCR Comment Response Document

Client Project Manager: Ronald McCally
Consultant: **PARSONS**

OVERALL COMMENT NO.	REVIEWER COMMENT NO.	DWG, SHT, PAGE NO.	COMMENT	INITIAL CODE	FINAL CODE	DESIGNER RESPONSE
40	10	Traffic Analysis Report	Figure 8 – Reason for calling out the lane configurations on Meridian Rd and not for the other crossroads?	D		The lane configuration was shown on Meridian Road to clarify a six lane cross section north of SR 24 and a four lane cross section south of SR 24.
41	11	Pg. 3-1, Draft IDCR	a. Provide description of Tier 1 analysis and background on why it was not used for evaluating the four alternatives. b. Section 3.3.2 Description of Alternatives should reference or include typical sections of each alternative.	D A		a. Tier 1 analysis was used for determining the SR 24 Corridor Alignment in the original DCR. b. Will include typical sections of each
42	12	Pg. 3-2, Draft IDCR	a. Was Alternative B removed from consideration for reasons other than the feasibility of the traffic operation analysis? b. Clarify last sentence under subheading, "Compatibility with Ultimate."	D A		a. That and the compatibility with the ultimate. b. Will clarify

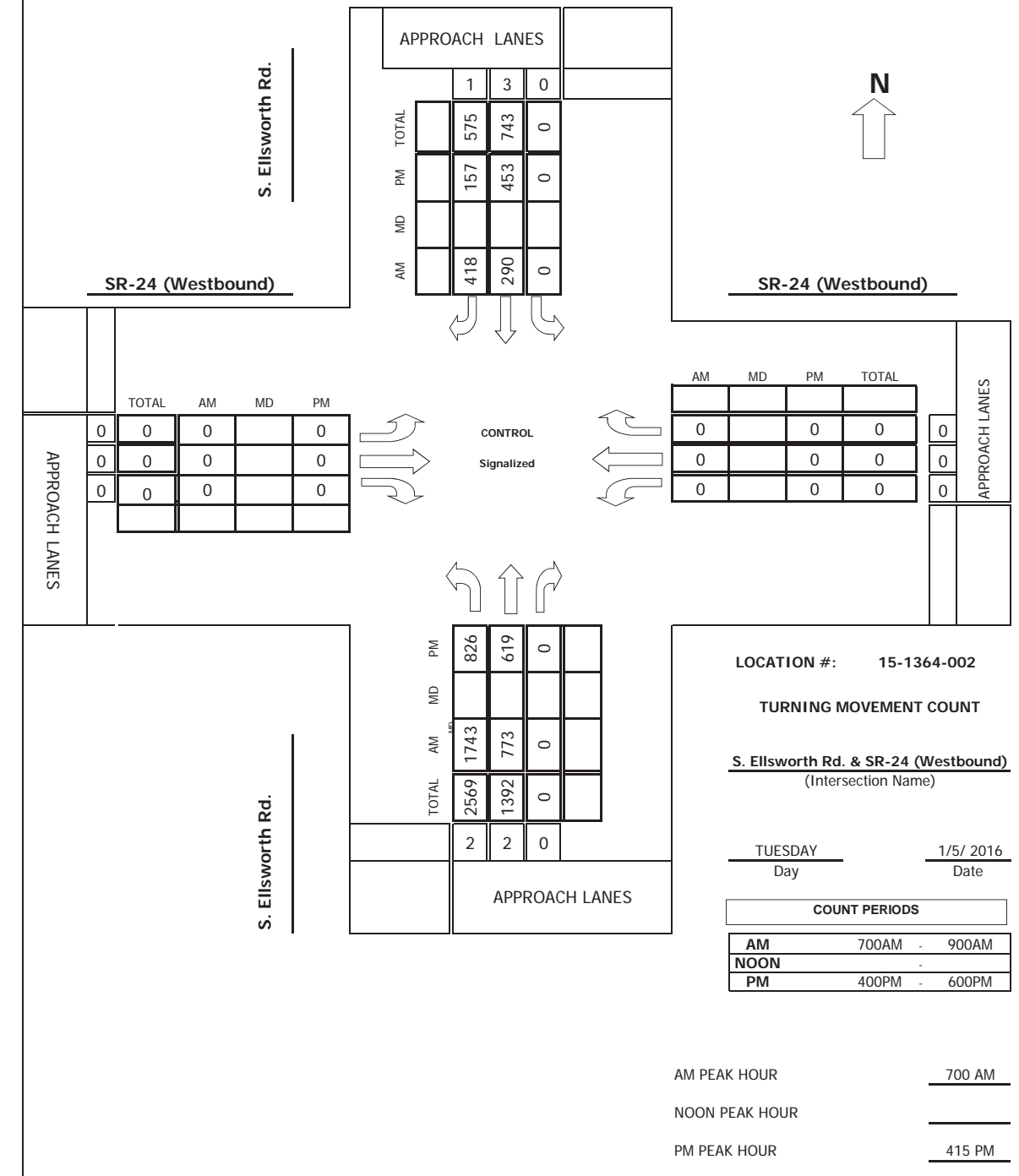
A-Will Comply
B-Consultant To Evaluate
C-ADOT To Evaluate
D-No Further Action Required

APPENDIX B

EXISTING PEAK HOUR TRAFFIC COUNTS

Project #: 15-1364-002

TMC SUMMARY OF S. Ellsworth Rd. & SR-24 (Westbound)



Intersection Turning Movement
Prepared by:



N-S STREET: S. Ellsworth Rd. DATE: 1/5/ 2016 LOCATION: Mesa
E-W STREET: SR-24 (Westbound) DAY: TUESDAY PROJECT#: 15-1364-002

	NORTHBOUND			SOUTHBOUND			EASTBOUND			WESTBOUND			
LANES:	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
	2	2	0	0	3	1	0	0	0	0	0	0	

6:00 AM													
6:15 AM													
6:30 AM													
6:45 AM													
7:00 AM	451	226	0	0	56	132	0	0	0	0	0	0	865
7:15 AM	444	161	0	0	88	91	0	0	0	0	0	0	784
7:30 AM	445	189	0	0	64	97	0	0	0	0	0	0	795
7:45 AM	403	197	0	0	82	98	0	0	0	0	0	0	780
8:00 AM	454	159	0	0	71	69	0	0	0	0	0	0	753
8:15 AM	368	180	0	0	52	44	0	0	0	0	0	0	644
8:30 AM	366	162	0	0	58	48	0	0	0	0	0	0	634
8:45 AM	286	108	0	0	51	45	0	0	0	0	0	0	490
9:00 AM													
9:15 AM													
9:30 AM													
9:45 AM													
10:00 AM													
10:15 AM													
10:30 AM													
10:45 AM													
11:00 AM													
11:15 AM													
11:30 AM													
11:45 AM													

TOTAL	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
Volumes	3217	1382	0	0	522	624	0	0	0	0	0	0	5745
Approach %	69.95	30.05	0.00	0.00	45.55	54.45	####	####	####	####	####	####	
App/Depart	4599	/	1382	1146	/	522	0	/	0	0	/	3841	

AM Peak Hr Begins at: 700 AM

PEAK	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
Volumes	1743	773	0	0	290	418	0	0	0	0	0	0	3224
Approach %	69.28	30.72	0.00	0.00	40.96	59.04	####	####	####	####	####	####	

PEAK HR. FACTOR:	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
	0.929			0.941			0.000			0.000			0.932

CONTROL: Signalized
COMMENT 1:
GPS: 33.318251, -111.635702

Intersection Turning Movement



N-S STREET: S. Ellsworth Rd. DATE: 1/5/ 2016 LOCATION: Mesa
E-W STREET: SR-24 (Westbound) DAY: TUESDAY PROJECT#: 15-1364-002

	NORTHBOUND			SOUTHBOUND			EASTBOUND			WESTBOUND			
LANES:	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
	2	2	0	0	3	1	0	0	0	0	0	0	

1:00 PM													
1:15 PM													
1:30 PM													
1:45 PM													
2:00 PM													
2:15 PM													
2:30 PM													
2:45 PM													
3:00 PM													
3:15 PM													
3:30 PM													
3:45 PM													
4:00 PM	237	163	0	0	89	57	0	0	0	0	0	0	546
4:15 PM	219	141	0	0	114	25	0	0	0	0	0	0	499
4:30 PM	183	159	0	0	100	54	0	0	0	0	0	0	496
4:45 PM	195	146	0	0	120	31	0	0	0	0	0	0	492
5:00 PM	229	173	0	0	119	47	0	0	0	0	0	0	568
5:15 PM	189	124	0	0	99	30	0	0	0	0	0	0	442
5:30 PM	188	147	0	0	97	36	0	0	0	0	0	0	468
5:45 PM	174	140	0	0	55	42	0	0	0	0	0	0	411
6:00 PM													
6:15 PM													
6:30 PM													
6:45 PM													

TOTAL	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
Volumes	1614	1193	0	0	793	322	0	0	0	0	0	0	3922
Approach %	57.50	42.50	0.00	0.00	71.12	28.88	####	####	####	####	####	####	
App/Depart	2807	/	1193	1115	/	793	0	/	0	0	/	1936	

PM Peak Hr Begins at: 415 PM

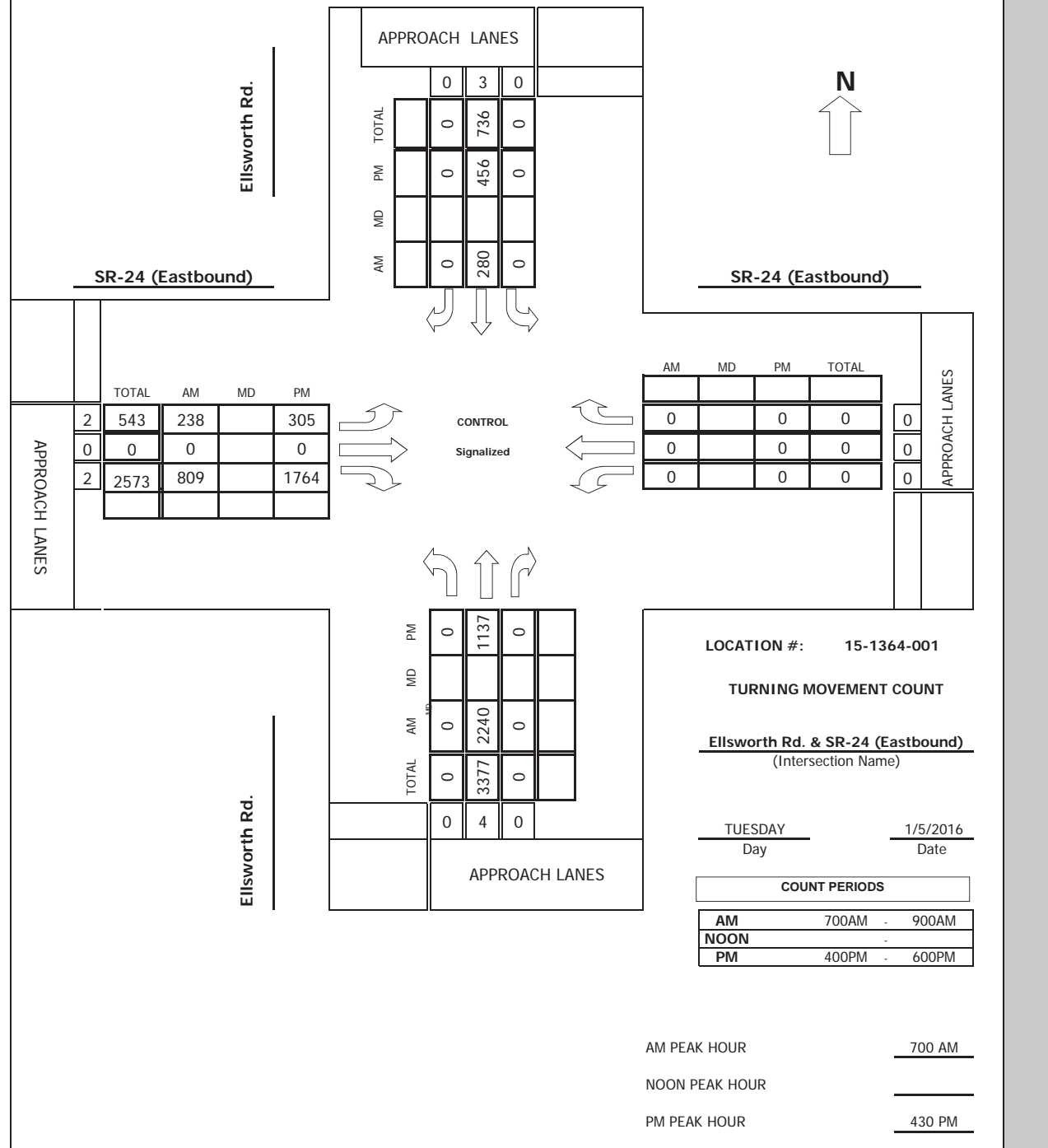
PEAK	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
Volumes	826	619	0	0	453	157	0	0	0	0	0	0	2055
Approach %	57.16	42.84	0.00	0.00	74.26	25.74	####	####	####	####	####	####	

PEAK HR. FACTOR:	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
	0.899			0.919			0.000			0.000			0.904

CONTROL: Signalized
COMMENT 1:
GPS: 33.318251, -111.635702

Project #: 15-1364-001

TMC SUMMARY OF Ellsworth Rd. & SR-24 (Eastbound)



N-S STREET: Ellsworth Rd. DATE: 1/5/2016 LOCATION: Mesa
E-W STREET: SR-24 (Eastbound) DAY: TUESDAY PROJECT#: 15-1364-001

	NORTHBOUND			SOUTHBOUND			EASTBOUND			WESTBOUND			
LANES:	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
	0	4	0	0	3	0	2	0	2	0	0	0	

Time	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
6:00 AM													
6:15 AM													
6:30 AM													
6:45 AM													
7:00 AM	0	569	0	0	57	0	102	0	193	0	0	0	921
7:15 AM	0	569	0	0	76	0	33	0	192	0	0	0	870
7:30 AM	0	557	0	0	68	0	55	0	240	0	0	0	920
7:45 AM	0	545	0	0	79	0	48	0	184	0	0	0	856
8:00 AM	0	527	0	0	89	0	37	0	181	0	0	0	834
8:15 AM	0	555	0	0	46	0	29	0	153	0	0	0	783
8:30 AM	0	506	0	0	62	0	53	0	147	0	0	0	768
8:45 AM	0	392	0	0	46	0	34	0	143	0	0	0	615
9:00 AM													
9:15 AM													
9:30 AM													
9:45 AM													
10:00 AM													
10:15 AM													
10:30 AM													
10:45 AM													
11:00 AM													
11:15 AM													
11:30 AM													
11:45 AM													

TOTAL	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
Volumes	0	4220	0	0	523	0	391	0	1433	0	0	0	6567
Approach %	0.00	100.00	0.00	0.00	100.00	0.00	21.44	0.00	78.56	####	####	####	
App/Depart	4220	/	4611	523	/	1956	1824	/	0	0	/	0	

AM Peak Hr Begins at: 700 AM

PEAK	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
Volumes	0	2240	0	0	280	0	238	0	809	0	0	0	3567
Approach %	0.00	100.00	0.00	0.00	100.00	0.00	22.73	0.00	77.27	####	####	####	

PEAK HR. FACTOR:	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
		0.984			0.886		0.887		0.000				0.968

CONTROL: Signalized
COMMENT 1:
GPS: 33.316576, -111.635321

Intersection Turning Movement



FIELD DATA SERVICES OF ARIZONA, INC.
520.316.6745



N-S STREET: Ellsworth Rd. DATE: 1/5/2016 LOCATION: Mesa
 E-W STREET: SR-24 (Eastbound) DAY: TUESDAY PROJECT#: 15-1364-001

LANES:	NORTHBOUND			SOUTHBOUND			EASTBOUND			WESTBOUND			TOTAL
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	
	0	4	0	0	3	0	2	0	2	0	0	0	
1:00 PM													
1:15 PM													
1:30 PM													
1:45 PM													
2:00 PM													
2:15 PM													
2:30 PM													
2:45 PM													
3:00 PM													
3:15 PM													
3:30 PM													
3:45 PM													
4:00 PM	0	348	0	0	85	0	83	0	396	0	0	0	912
4:15 PM	0	292	0	0	106	0	68	0	439	0	0	0	905
4:30 PM	0	291	0	0	118	0	79	0	451	0	0	0	939
4:45 PM	0	242	0	0	110	0	66	0	439	0	0	0	857
5:00 PM	0	286	0	0	108	0	93	0	433	0	0	0	920
5:15 PM	0	318	0	0	120	0	67	0	441	0	0	0	946
5:30 PM	0	220	0	0	85	0	79	0	419	0	0	0	803
5:45 PM	0	196	0	0	67	0	83	0	358	0	0	0	704
6:00 PM													
6:15 PM													
6:30 PM													
6:45 PM													

TOTAL	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
Volumes	0	2193	0	0	799	0	618	0	3376	0	0	0	6986
Approach %	0.00	100.00	0.00	0.00	100.00	0.00	15.47	0.00	84.53	####	####	####	
App/Depart	2193	/	2811	799	/	4175	3994	/	0	0	/	0	

PM Peak Hr Begins at: 430 PM

PEAK

Volumes	0	1137	0	0	456	0	305	0	1764	0	0	0	3662
Approach %	0.00	100.00	0.00	0.00	100.00	0.00	14.74	0.00	85.26	####	####	####	

PEAK HR. FACTOR:

	0.894	0.950	0.976	0.000	0.968
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CONTROL: Signalized
 COMMENT 1: 0
 GPS: 33.316576, -111.635321

EXISTING PEAK HOUR ANALYSIS

APPENDIX C

HCM 2010 Signalized Intersection Summary
1: Ellsworth Road & SR 24 EB Ramp(s)

1/20/2016

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔	↔	↔	↔	↔	↔
Volume (veh/h)	238	809	0	2240	280	0
Number	7	14	1	6	2	12
Initial Q (Obs) veh	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow, veh/h/ln	1810	1810	0	1810	1810	0
Adj Flow Rate, veh/h	264	899	0	2489	311	0
Adj No. of Lanes	2	2	0	4	3	0
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90
Percent Heavy Veh. %	5	5	0	5	5	0
Cap. veh/h	1393	1128	0	3009	2388	0
Arrive On Green	0.42	0.42	0.00	0.48	0.97	0.00
Sat Flow, veh/h	3343	2707	0	6731	5266	0
Grp Volume(V), veh/h	264	899	0	2489	311	0
Grp Sat Flow(s), veh/h/ln	1672	1354	0	1556	1647	0
O.Serve(g.s), s	6.0	34.8	0.0	41.3	0.3	0.0
Cycle Q Clear(g.c), s	6.0	34.8	0.0	41.3	0.3	0.0
Prop In Lane	1.00	1.00	0.00	0.00	0.00	0.00
Lane Grp Cap(c), veh/h	1393	1128	0	3009	2388	0
V/C Ratio(X)	0.19	0.80	0.00	0.83	0.13	0.00
Avail Cap(c.a), veh/h	1393	1128	0	3009	2388	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	2.00	1.00
Upstream Filter(I)	1.00	1.00	0.00	1.00	1.00	0.00
Uniform Delay (d), s/veh	22.2	30.6	0.0	26.7	1.0	0.0
Incr Delay (d2), s/veh	0.3	5.9	0.0	2.8	0.1	0.0
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOf(50%),veh/h	2.8	13.9	0.0	18.2	0.1	0.0
LnGrp Delay(d),s/veh	22.5	36.5	0.0	29.5	1.2	0.0
LnGrp LOS	C	D	C	C	A	A
Approach Vol, veh/h	1163			2489	311	
Approach Delay, s/veh	33.3			29.5	1.2	
Approach LOS	C			C	A	
Timer	1	2	3	4	5	6 7 8
Assigned Phs	2			4		6
Phs Duration (G+Y+Rc), s	64.0			56.0		64.0
Change Period (Y+Rc), s	6.0			6.0		6.0
Max Green Setting (Gmax), s	58.0			50.0		58.0
Max Q Clear Time (g_c+H1), s	2.3			36.8		43.3
Green Ext Time (p_c), s	40.4			4.2		13.2
Intersection Summary						
HCM 2010 Ctrl Delay	28.4					
HCM 2010 LOS	C					

HCM 2010 Signalized Intersection Summary
2: Ellsworth Road & SR 24 WB Ramp(s)

1/20/2016

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔	↔	↔	↔	↔	↔
Volume (veh/h)	0	0	1743	773	290	418
Number			5	2	6	16
Initial Q (Obs) veh			0	0	0	0
Ped-Bike Adj(A_pbT)			1.00	1.00	1.00	1.00
Parking Bus, Adj			1.00	1.00	1.00	1.00
Adj Sat Flow, veh/h/ln			1810	1810	1810	1810
Adj Flow Rate, veh/h			1937	859	322	464
Adj No. of Lanes			2	2	3	1
Peak Hour Factor			0.90	0.90	0.90	0.90
Percent Heavy Veh. %			5	5	5	5
Cap. veh/h			1672	3266	1976	615
Arrive On Green			1.00	1.00	0.40	0.40
Sat Flow, veh/h			3343	3529	5103	1538
Grp Volume(V), veh/h			1937	859	322	464
Grp Sat Flow(s), veh/h/ln			1672	1719	1647	1538
O.Serve(g.s), s			0.0	0.0	5.0	31.1
Cycle Q Clear(g.c), s			0.0	0.0	5.0	31.1
Prop In Lane			1.00	1.00	1.00	1.00
Lane Grp Cap(c), veh/h			1672	3266	1976	615
V/C Ratio(X)			1.76	0.26	0.16	0.75
Avail Cap(c.a), veh/h			1672	3266	1976	615
HCM Platoon Ratio			2.00	2.00	1.00	1.00
Upstream Filter(I)			1.00	1.00	1.00	1.00
Uniform Delay (d), s/veh			0.0	0.0	23.1	30.9
Incr Delay (d2), s/veh			78.6	0.2	0.2	8.3
Initial Q Delay(d3), s/veh			0.0	0.0	0.0	0.0
%ile BackOf(50%),veh/h			18.2	0.1	2.3	14.6
LnGrp Delay(d),s/veh			78.6	0.2	23.3	39.3
LnGrp LOS			F	A	C	D
Approach Vol, veh/h			2796	786		
Approach Delay, s/veh			54.5	32.7		
Approach LOS			D	C		
Timer	1	2	3	4	5	6 7 8
Assigned Phs		2				5
Phs Duration (G+Y+Rc), s		120.0				66.0
Change Period (Y+Rc), s		6.0				6.0
Max Green Setting (Gmax), s		114.0				60.0
Max Q Clear Time (g_c+H1), s		2.0				2.0
Green Ext Time (p_c), s		33.7				28.0
Intersection Summary						
HCM 2010 Ctrl Delay	49.7					
HCM 2010 LOS	D					

Timing Report, Sorted By Phase
1: Ellsworth Road & SR 24 EB Ramp(s)

1/20/2016

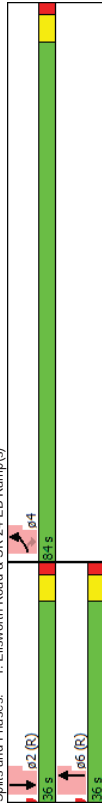


Phase Number	2	4	6
Movement	SBT	EBL	NBT
Lead/Lag			
Lead-Lag Optimize			
Recall Mode	Max	Max	Max
Maximum Spill (s)	36	84	36
Maximum Spill (%)	30.0%	70.0%	30.0%
Minimum Spill (s)	36	36	36
Yellow Time (s)	4	4	4
All-Red Time (s)	2	2	2
Minimum Initial (s)	4	4	4
Vehicle Extension (s)	3	3	3
Minimum Gap (s)	3	3	3
Time Before Reduce (s)	0	0	0
Time To Reduce (s)	5	5	5
Walk Time (s)	25	25	25
Flash Dont Walk (s)	Yes	Yes	Yes
Inhibit Max	Yes	Yes	Yes
Start Time (s)	0	36	0
End Time (s)	36	0	36
Yield/Force Off (s)	30	114	30
Yield/Force Off 170(s)	5	89	5
Local Start Time (s)	0	36	0
Local Yield (s)	30	114	30
Local Yield 170(s)	5	89	5

Intersection Summary

Cycle Length	120
Control Type	Prelimed
Natural Cycle	140
Offset: 0 (0%), Referenced to phase 2:SBT and 6:NBT, Start of Green	

Splits and Phases: 1: Ellsworth Road & SR 24 EB Ramp(s)



Timing Report, Sorted By Phase
2: Ellsworth Road & SR 24 WB Ramp(s)

1/20/2016



Phase Number	2	5	6
Movement	NBT	NBL	SBT
Lead/Lag		Lag	Lead
Lead-Lag Optimize			
Recall Mode	Max	Max	Max
Maximum Spill (s)	120	40	80
Maximum Spill (%)	100.0%	33.3%	66.7%
Minimum Spill (s)	36	10	36
Yellow Time (s)	4	4	4
All-Red Time (s)	2	2	2
Minimum Initial (s)	4	4	4
Vehicle Extension (s)	3	3	3
Minimum Gap (s)	3	3	3
Time Before Reduce (s)	0	0	0
Time To Reduce (s)	5	5	5
Walk Time (s)	25	25	25
Flash Dont Walk (s)	Yes	No	Yes
Inhibit Max	Yes	Yes	Yes
Start Time (s)	0	80	0
End Time (s)	0	0	80
Yield/Force Off (s)	114	114	74
Yield/Force Off 170(s)	89	114	49
Local Start Time (s)	0	80	0
Local Yield (s)	114	114	74
Local Yield 170(s)	89	114	49

Intersection Summary

Cycle Length	120
Control Type	Prelimed
Natural Cycle	60
Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBT, Start of Green	

Splits and Phases: 2: Ellsworth Road & SR 24 WB Ramp(s)



ADOT 2014 AND 2015 CRASH DATA

APPENDIX D

Arizona Department of Transportation
Traffic Records Section
Standard Detailed Report

IncidentDate	IncidentTime	IncidentOnroad	IncidentCrossing	IncidentSeverityDesc	IncidentHarmfulDesc	IncidentCollisionMannerDesc	IncidentLightConditionDesc	IncidentIntersectionTypeDesc	PersonViolationDesc1
4/7/2015	19:48 S 024	M000	M000	0.13 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	SIDESWIPE_SAME_DIRECTION	DARK_LIGHTED	T_INTERSECTION	FAILED_TO_YIELD_RIGHT_OF_WAY
6/20/2014	10:54 S 024	M000	M000	0.55 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
12/3/2014	11:54 S 024	M000	M000	0.97 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	UNKNOWN
7/28/2014	17:15 S 024	M001	M001	0 NON_INCAPACITATING_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
7/28/2014	16:30 S 024	M001	M001	0.19 NO_INJURY	OTHER_NON_FIXED_OBJECT	OTHER	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
6/26/2014	16:34 S 024	M001	M001	0.4 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	INTERSECTION_AS_PART_OF_INTERCHANGE	SPEED_TO_FAST_FOR_CONDITION
1/7/2015	17:38 S 024	M001	M001	0.01 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
5/9/2015	15:24 S 024	M001	M001	0 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
6/8/2015	16:56 S 024	M001	M001	0 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
8/19/2014	17:39 S 024	M001	M001	0.4 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
10/30/2014	7:37 S 024	M001	M001	0.39 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
10/30/2014	7:37 S 024	M001	M001	0.39 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
11/17/2014	16:35 S 024	M001	M001	0.4 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	Not Reported	SPEED_TO_FAST_FOR_CONDITION
11/24/2014	13:36 S 024	M001	M001	0.4 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
12/29/2014	18:23 S 024	M001	M001	0.19 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DARK_LIGHTED	NOT_AT_AN_INTERSECTION	UNKNOWN
3/16/2015	16:36 S 024	M001	M001	0.33 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	SIDESWIPE_SAME_DIRECTION	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
10/15/2014	19:16 S 024	M001	07 ELLSWORTH RD	0 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
6/17/2015	18:37 S 024	M001	M001	0 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
7/24/2015	17:22 S 024	M001	M001	0 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
7/28/2014	17:15 S 024	M001	M001	0 NON_INCAPACITATING_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
7/28/2014	16:30 S 024	M001	M001	0.19 NO_INJURY	OTHER_NON_FIXED_OBJECT	OTHER	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
6/26/2014	16:34 S 024	M001	M001	0.4 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	INTERSECTION_AS_PART_OF_INTERCHANGE	SPEED_TO_FAST_FOR_CONDITION
8/19/2014	17:39 S 024	M001	M001	0.4 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
10/30/2014	7:37 S 024	M001	M001	0.39 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
10/30/2014	7:37 S 024	M001	M001	0.39 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
12/29/2014	18:23 S 024	M001	M001	0.19 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DARK_LIGHTED	NOT_AT_AN_INTERSECTION	UNKNOWN
1/7/2015	17:38 S 024	M001	M001	0.01 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
3/19/2015	16:36 S 024	M001	M001	0.33 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	SIDESWIPE_SAME_DIRECTION	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
4/7/2015	16:17 S 024	M001	M001	0.4 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	FOUR_WAY_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
4/7/2015	18:13 S 024	M001	M001	0.18 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
3/30/2015	16:34 S 024	M001	M001	0.38 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	FOLLOWED_TOO_CLOSELY
3/30/2015	16:34 S 024	M001	M001	0.38 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	FOLLOWED_TOO_CLOSELY
3/19/2015	14:10 S 024	M001	M001	0.35 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
3/19/2015	14:10 S 024	M001	M001	0.35 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
4/8/2015	6:35 S 024	M001	07 ELLSWORTH RD	0.1894 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
5/9/2015	15:24 S 024	M001	M001	0 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
6/8/2015	16:56 S 024	M001	M001	0 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
6/17/2015	18:37 S 024	M001	M001	0 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
6/22/2015	11:31 S 024	M001	07 ELLSWORTH RD	0.0095 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
7/10/2015	17:58 S 024	M001	M001	0.3 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION
5/30/2014	11:51 07 ELLSWORTH RD	S 024	M000	0.0047 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	SIDESWIPE_SAME_DIRECTION	DAYLIGHT	FOUR_WAY_INTERSECTION	UNSAFE_LANE_CHANGE
6/20/2014	10:54 S 024	M000	M000	0.55 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	SPEED_TO_FAST_FOR_CONDITION

Arizona Department of Transportation
Traffic Records Section
Standard Detailed Report

IncidentDate/Time	IncidentOnroad	IncidentCrossing/Feature	IncidentOffset	IncidentInjurySeverityDesc	IncidentFirstHarmfulDesc	IncidentCollisionMannerDesc	IncidentLightConditionDesc	IncidentIntersectionTypeDesc	PersonViolationDesc1
4/8/2015 6:35 S 024	M001	07 ELLSWORTH RD	0	0.1894 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
4/7/2015 18:13 S 024	M001		0	0.18 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
4/7/2015 18:13 S 024	M001		0	0.18 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
3/16/2015 16:36 S 024	M001		0	0.33 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	SIDESWIPE_SAME_DIRECTION	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
3/19/2015 14:10 S 024	M001		0	0.35 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
3/19/2015 14:10 S 024	M001		0	0.35 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
1/7/2015 17:38 S 024	M001		0	0.01 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
10/30/2014 7:37 S 024	M001		0	0.39 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
8/19/2014 17:39 S 024	M001		0	0.4 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
7/28/2014 16:30 S 024	M001		0	0.19 NO_INJURY	OTHER_NON_FIXED_OBJECT	OTHER	DAYLIGHT	T_INTERSECTION	NO_IMPROPER_ACTION
6/26/2014 16:34 S 024	M001		0	0.4 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
12/29/2014 18:23 S 024	M001		0	0.19 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DARK_LIGHTED	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
7/28/2014 17:15 S 024	M001		0	0 NON_INCAPACITATING_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	NO_IMPROPER_ACTION
7/24/2015 17:22 S 024	M001		0	0 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	NO_IMPROPER_ACTION
11/17/2014 16:35 S 024	M001		0	0.4 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	Not Reported	NO_IMPROPER_ACTION
3/16/2015 16:36 S 024	M001		0	0.33 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	SIDESWIPE_SAME_DIRECTION	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
6/17/2015 18:37 S 024	M001		0	0 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	NO_IMPROPER_ACTION
1/12/2014 13:36 S 024	M001		0	0.4 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	NO_IMPROPER_ACTION
10/19/2014 19:16 S 024	M001	07 ELLSWORTH RD	0	0 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	NO_IMPROPER_ACTION
10/30/2014 7:37 S 024	M001		0	0.39 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
10/30/2014 7:37 S 024	M001		0	0.39 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
8/19/2014 17:39 S 024	M001		0	0.4 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	NO_IMPROPER_ACTION
4/17/2015 19:48 S 024	M000		0	0.13 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	SIDESWIPE_SAME_DIRECTION	DARK_LIGHTED	T_INTERSECTION	NO_IMPROPER_ACTION
6/26/2014 16:34 S 024	M001		0	0.4 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
6/9/2015 16:56 S 024	M001		0	0 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
5/9/2015 15:24 S 024	M001		0	0 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
1/7/2015 17:38 S 024	M001		0	0.01 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
7/28/2014 16:30 S 024	M001		0	0.19 NO_INJURY	OTHER_NON_FIXED_OBJECT	OTHER	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
7/28/2014 17:15 S 024	M001		0	0 NON_INCAPACITATING_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	T_INTERSECTION	NO_IMPROPER_ACTION
12/2/2014 11:54 S 024	M000		0	0.97 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
6/20/2014 10:54 S 024	M000		0	0.55 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
1/7/2015 17:38 S 024	M001		0	0.01 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
12/29/2014 18:23 S 024	M001		0	0.19 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DARK_LIGHTED	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
1/7/2015 17:38 S 024	M001		0	0.01 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
12/29/2014 18:23 S 024	M001		0	0.19 NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DARK_LIGHTED	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
4/8/2015 6:35 S 024	M001	07 ELLSWORTH RD	0	0.1894 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
7/10/2015 17:58 S 024	M001		0	0.3 POSSIBLE_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	REAR_END	DAYLIGHT	NOT_AT_AN_INTERSECTION	NO_IMPROPER_ACTION
5/27/2015 9:46 07 ELLSWORTH RD S 024	M001	S 024	-0.0047	NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	HEAD_ON	DAYLIGHT	T_INTERSECTION	NO_IMPROPER_ACTION
6/13/2011 13:50 07 FRYE RD	M001	GALLERIA WAY		NON_INCAPACITATING_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	ANGLE (front to side)(other than left turn)	DAYLIGHT	UNKNOWN	DISREGARDED_TRAFFIC_SIGNAL
6/13/2011 13:50 07 FRYE RD	M001	GALLERIA WAY		NON_INCAPACITATING_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	ANGLE (front to side)(other than left turn)	DAYLIGHT	UNKNOWN	NO_IMPROPER_ACTION
6/13/2011 13:50 07 FRYE RD	M001	GALLERIA WAY		NON_INCAPACITATING_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	ANGLE (front to side)(other than left turn)	DAYLIGHT	UNKNOWN	NO_IMPROPER_ACTION

Report Generated on:
Report ID : 06c8d86a-
Report Date : 5/27/2015
Report Route : State Route 2
PersonTypeDesc : DR

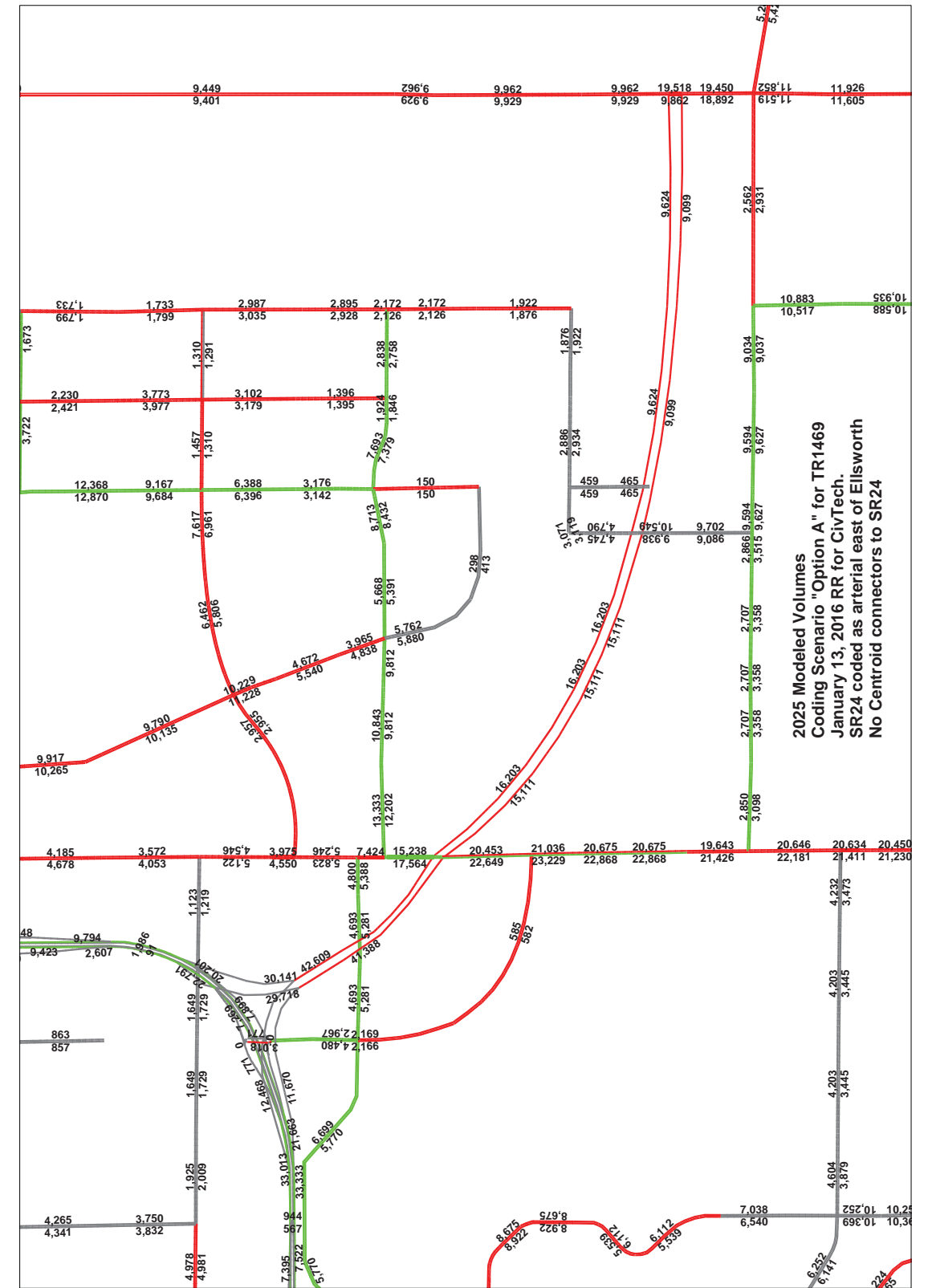
Arizona Department of Transportation
Traffic Records Section
Standard Detailed Report

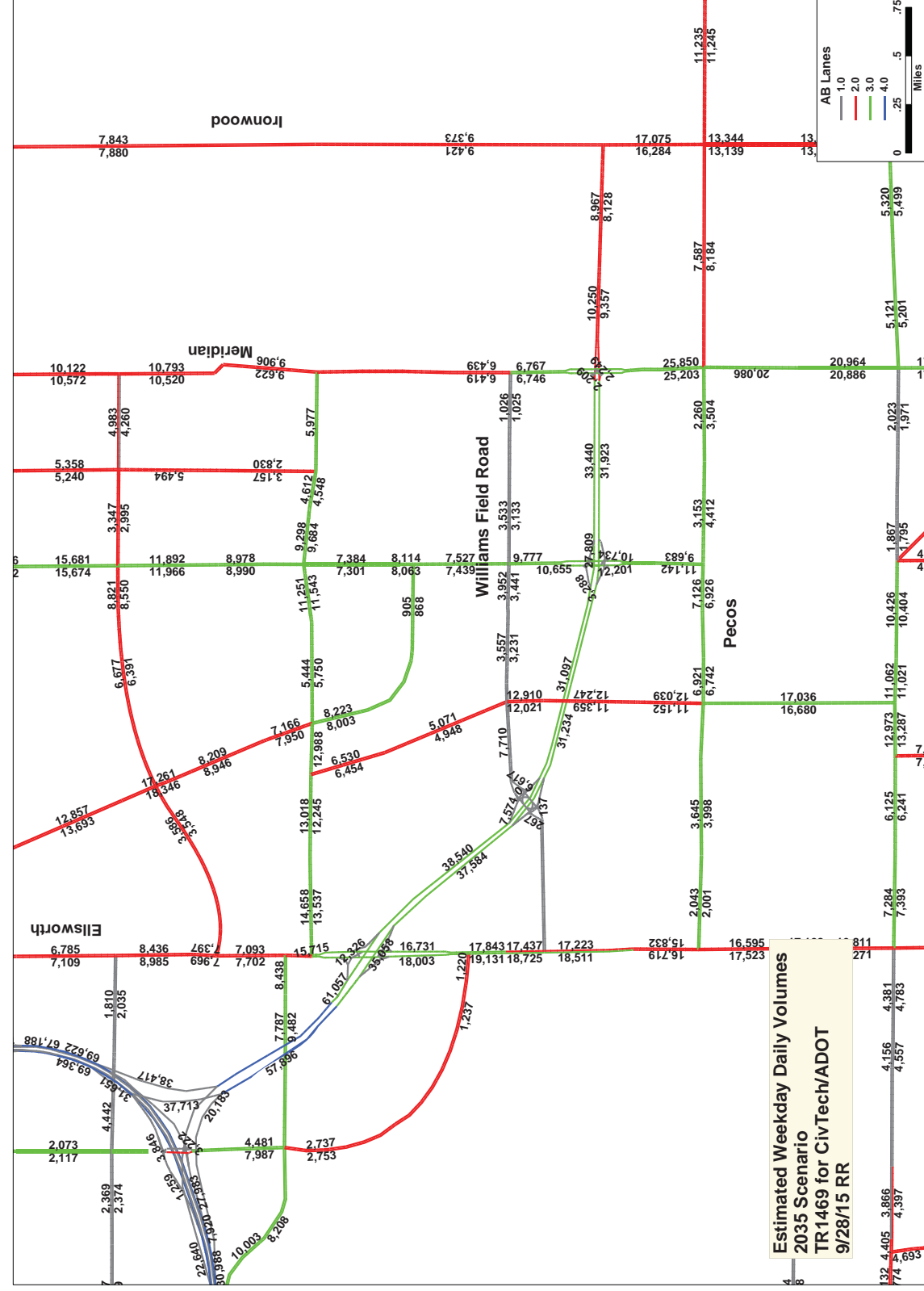
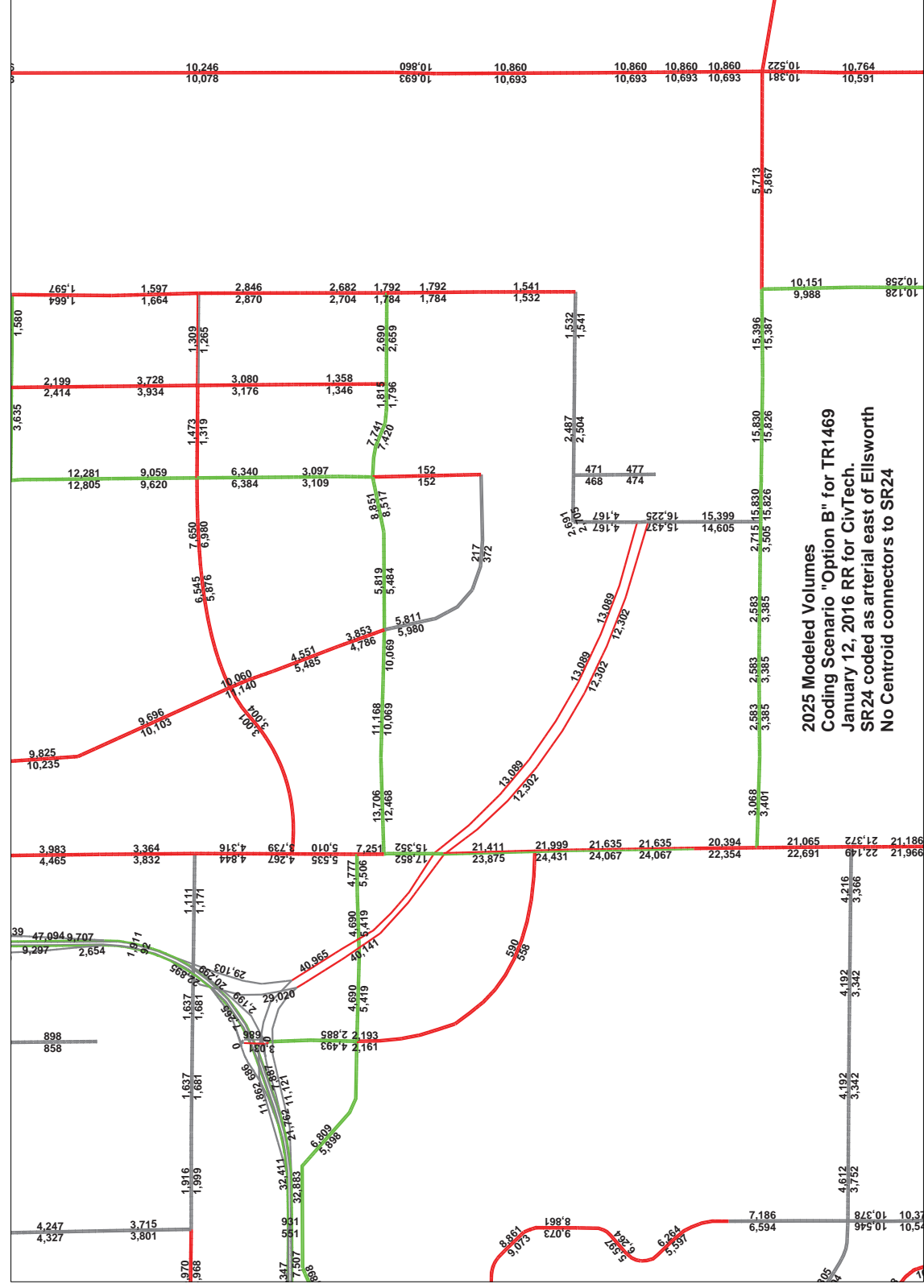
IncidentDate/Time	IncidentOnroad	IncidentCrossing/Feature	IncidentOffset	IncidentInjurySeverityDesc	IncidentFirstHarmfulDesc	IncidentCollisionMannerDesc	IncidentLightConditionDesc	IncidentIntersectionTypeDesc	PersonViolationDesc1
5/27/2015 9:46 07 ELLSWORTH RD S 024	M001	S 024	-0.0047	NO_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	HEAD_ON	DAYLIGHT	T_INTERSECTION	NO_IMPROPER_ACTION
6/13/2011 13:50 07 FRYE RD	M001	GALLERIA WAY		NON_INCAPACITATING_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	ANGLE (front to side)(other than left turn)	DAYLIGHT	UNKNOWN	DISREGARDED_TRAFFIC_SIGNAL
6/13/2011 13:50 07 FRYE RD	M001	GALLERIA WAY		NON_INCAPACITATING_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	ANGLE (front to side)(other than left turn)	DAYLIGHT	UNKNOWN	NO_IMPROPER_ACTION
6/13/2011 13:50 07 FRYE RD	M001	GALLERIA WAY		NON_INCAPACITATING_INJURY	MOTOR_VEHICLE_IN_TRANSPORT	ANGLE (front to side)(other than left turn)	DAYLIGHT	UNKNOWN	NO_IMPROPER_ACTION

Report Generated on:
Report ID : 06c8d86a-
Report Date : 5/27/2015
Report Route : State Route 2
PersonTypeDesc : DR

APPENDIX E

MAG TRAVEL DEMAND MODEL DATA





APPENDIX F

PEAK HOUR TURNING MOVEMENT CALCULATIONS

Intersection Elsworth Road and SR 24 Ramps

Turning Movement Calculations

2025 Option A



Intersection
Signal Butte Road and SR 24 Ramps

Turning Movement Calculations

2025 Option A



Appendix E

Intersection
Ironwood Drive and SR 24 Ramps

Turning Movement Calculations

2025 Option A



Appendix E



Intersection
Elsworth Road and SR 24 Ramps

Turning Movement Calculations

2035



Appendix E

Intersection
Williams Field Road and SR 24 Ramps

Turning Movement Calculations

2035



Appendix E

Intersection

Signal Butte Road and SR 24 Ramps

Turning Movement Calculations

2035



Appendix E

Intersection

Meridian Road and SR 24 Ramps

Turning Movement Calculations

2035



Appendix E

AM
Assumptions Provided data
Daily Average Directional AM
Departure 8967
Approach 8328

Calculated Check
Daily Average Directional AM
Daily Average Directional AM 70%
Daily Average Directional AM 957
Approach 410

Departures 2777
Approaches 34624

Approach 9421
Daily Average Directional AM
Daily Average Directional AM 50%
Daily Average Directional AM 752

Right Thru Left
Right 10%
Thru 90%
Left 0%

Check 1
Departure 956

Left Thru Right
Left 7%
Thru 0%
Right 93%

2 Check
Departure 749

2% Right
90% Thru
2% Left
Departure 0

AM
Directional Average
Directional Average 60%
Daily Approach 0
Daily Departure 0

881 721 0
Left Through Right
55% 45% 0%

Check 9
Departure 1088

Approach 1601
Daily Average Directional AM
Daily Average Directional AM 40%
Daily Average Directional AM 16384

AM
Daily Average Directional AM
Daily Average Directional AM 40%
Daily Average Directional AM 33359

Approach 17075
Departure 16384

PM
Assumptions Provided data
Daily Average Directional PM
Departure 8967
Approach 8328

Calculated Check
Daily Average Directional PM
Daily Average Directional PM 30%
Daily Average Directional PM 462
Approach 1077

Departures 3128
Approaches 3105

Approach 9421
Daily Average Directional PM
Daily Average Directional PM 60%
Daily Average Directional PM 1015

Right Thru Left
Right 6%
Thru 94%
Left 0%

Check 2
Departure 459

Left Thru Right
Left 7%
Thru 0%
Right 93%

7 Check
Departure 1008

5% Right
90% Thru
5% Left
Departure 0

PM
Directional Average
Directional Average 30%
Daily Approach 0
Daily Departure 0

419 932 0
Left Through Right
31% 69% 0%

Check 14
Departure 1651

Approach 1351
Daily Average Directional PM
Daily Average Directional PM 55%
Daily Average Directional PM 17075

PM
Daily Average Directional PM
Daily Average Directional PM 55%
Daily Average Directional PM 33359

Approach 17075
Departure 16384

2025 Option A AM

SR 24 Interchanges - 2025 Option A AM

2: Ellsworth Road & SR 24 WB Ramp(s)

Table with 15 columns (EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR) and rows for Movement, Lane Configurations, Traffic Volume, Future Volume, Number, etc.

Table with 15 columns (EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR) and rows for Approach Vol, Approach Delay, Approach LOS, Timer, Assigned Phs, etc.

Table with 15 columns (EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR) and rows for HCM 2010 Ch Delay, HCM 2010 LOS, Notes.

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2025 Option A AM

SR 24 Interchanges - 2025 Option A AM

2: Ellsworth Road & SR 24 WB Ramp(s)

Table with 15 columns (EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR) and rows for Movement, Lane Configurations, Traffic Volume, Future Volume, Number, etc.

Table with 15 columns (EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR) and rows for Approach Vol, Approach Delay, Approach LOS, Timer, Assigned Phs, etc.

Table with 15 columns (EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR) and rows for HCM 2010 Ch Delay, HCM 2010 LOS, Notes.

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2025 Option A AM

SR 24 Interchanges - 2025 Option A AM

7: Signal Butte Road & SR 24 EB Ramp(s)

Table with 15 columns (EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR) and rows for Movement, Lane Configurations, Traffic Volume, Future Volume, Number, etc.

Table with 15 columns (EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR) and rows for Approach Vol, Approach Delay, Approach LOS, Timer, Assigned Phs, etc.

Table with 15 columns (EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR) and rows for HCM 2010 Ch Delay, HCM 2010 LOS, Notes.

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2025 Option A AM

SR 24 Interchanges - 2025 Option A AM

7: Signal Butte Road & SR 24 EB Ramp(s)

Table with 15 columns (EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR) and rows for Movement, Lane Configurations, Traffic Volume, Future Volume, Number, etc.

Table with 15 columns (EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR) and rows for Approach Vol, Approach Delay, Approach LOS, Timer, Assigned Phs, etc.

Table with 15 columns (EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR) and rows for HCM 2010 Ch Delay, HCM 2010 LOS, Notes.

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2025 Option A PM
12: Ironwood Road & SR 24 WB Ramp(s)

SR 24 Interchanges - 2025 Option A PM
HCM 2010 Signalized Intersection Summary

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	0	0	525	1075	725	25
Future Volume (veh/h)	0	0	525	1075	725	25
Number			5	2	6	16
Initial Q (Cb), veh			0	0	0	0
PeakBikeAdj(A_pb1)			1.00	1.00	1.00	1.00
Parking Bus, Adj			1.00	1.00	1.00	1.00
Adj Sat Flow, veh/h/h			1863	1863	1863	1863
Adj Flow Rate, veh/h			559	1144	771	27
Adj No. of Lanes			2	2	2	1
Peak Hour Factor			0.94	0.94	0.94	0.94
Percent Heavy Veh, %			2	2	2	2
Cap, veh/h			1348	3362	1799	805
Arrive On Green			0.78	1.00	0.51	0.51
Sat Flow, veh/h			3442	3632	3632	1583
Grp Volume(V), veh/h			559	1144	771	27
Grp Sat Flow(S), veh/h/h			1721	1770	1770	1583
Q Serve(Q_s), s			6.3	0.0	16.4	1.0
Cycle O Clear(q_c), s			6.3	0.0	16.4	1.0
Prop In Lane			1.00			1.00
Lane Grp Cap(c), veh/h			1348	3362	1799	805
V/C Ratio(X)			0.41	0.34	0.43	0.03
Avail Cap(c_a), veh/h			1348	3362	1799	805
HCM Platoon Ratio			2.00	2.00	1.00	1.00
Upstream Filter(I)			1.00	1.00	1.00	1.00
Uniform Delay (d), s/veh			8.6	0.0	18.5	14.8
Incr Delay (d2), s/veh			0.9	0.3	0.7	0.1
Initial Q Delay(d3), s/veh			0.0	0.0	0.0	0.0
%ile BackOfQ(50%), veh/h			3.0	0.1	8.2	0.5
LnGrp Delay(d), s/veh			9.5	0.3	19.3	14.8
LnGrp LOS			A	A	B	B
Approach Vol, veh/h				1703	798	
Approach Delay, s/veh				3.3	19.1	
Approach LOS				A	B	
Timer	1	2	3	4	5	6
Assigned Phs	2					
Phs Duration (G+Y+Rc), s	120.0				53.0	67.0
Change Period (Y+Rc), s	6.0				6.0	6.0
Max Green Scaling (Gmax), s	114.0				47.0	61.0
Max O Clear Time (Q_c+H), s	2.0				8.3	18.4
Green Ext Time (p_c), s	14.6				13.0	5.7
Intersection Summary	8.4					
HCM 2010 Ctrl Delay	A					
HCM 2010 LOS	A					

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2025 Option A PM
12: Ironwood Road & SR 24 WB Ramp(s)

SR 24 Interchanges - 2025 Option A PM
Timing Report, Sorted By Phase

Phase Number	2	5	6
Movement	NBT	NBL	SBT
Lead/Lag		Lag	Lead
Recall Mode	Max	Max	Max
Maximum Split (s)	120	53	67
Maximum Split (%)	100.0%	44.2%	55.8%
Minimum Split (s)	36	10	36
Yellow Time (s)	4	4	4
All Red Time (s)	2	2	2
Minimum Initial (s)	4	4	4
Vehicle Extension (s)	3	3	3
Minimum Gap (s)	0	0	0
Time Before Reduce (s)	0	0	0
Walk Time (s)	5	0	5
Flash Don't Walk (s)	25	0	25
Dual Entry	Yes	No	Yes
Inhibit Max	Yes	Yes	Yes
Start Time (s)	0	67	0
End Time (s)	0	0	67
Yield/Force Off (s)	114	114	61
Yield/Force Off 170(s)	89	114	36
Local Start Time (s)	0	67	0
Local Yield (s)	114	114	61
Local Yield 170(s)	89	114	36
Intersection Summary	120		
Cycle Length	Prelimined		
Control Type	55		
Natural Cycle	55		
Offset: 0 (0%), Referenced to phase 2(NBT) and 6(SBT), Start of Green			
Spills and Phases: 12: Ironwood Road & SR 24 WB Ramp(s)			
↑ G2 (R)	↑ G2 (R)	↑ G2 (R)	
↓ G2 (R)	↓ G2 (R)	↓ G2 (R)	
↓ G6 (R)	↓ G6 (R)	↓ G6 (R)	
↓ G5 (R)	↓ G5 (R)	↓ G5 (R)	
67 s	53 s	67 s	

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HCM 2010 Signalized Intersection Summary
2: Ellsworth Road & SR 24 WB Ramp(s)

2025 Option A Mitigated AM, Syn

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBR
Lane Configurations		←	←	←	←	←	←	←	←	←	←
Traffic Volume (veh/h)	0	0	0	25	1450	25	1700	525	0	0	300
Future Volume (veh/h)	0	0	0	25	1450	25	1700	525	0	0	300
Number	0	0	0	3	8	18	5	2	12	1	6
Initial Q (Cb), veh	0	0	0	0	0	0	0	0	0	0	0
Peak-Bike Adj(A _{bkt})	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow, veh/h	1810	1810	1810	1810	1810	1810	1810	1810	1810	1810	1810
Adj Flow Rate, veh/h	28	1611	28	1889	583	0	0	333	0	0	333
Adj No. of Lanes	1	3	0	2	2	0	0	5	1	0	5
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Percent Heavy Veh, %	5	5	5	5	5	5	5	5	5	5	5
Cap, veh/h	618	1906	33	1226	1862	0	0	916	192	0	916
Arrive On Green	0.36	0.36	0.36	0.73	1.00	0.00	0.00	0.13	0.00	0.00	0.13
Sat Flow, veh/h	1723	5320	92	3343	3529	0	0	7672	1538	0	7672
Grp Volume(V), veh/h	28	1096	543	1889	583	0	0	333	0	0	333
Grp Sat Flow(S), veh/h	1723	1810	1783	1672	1719	0	0	1466	1538	0	1466
Q Serve(Q _s), s	1.3	33.4	33.5	44.0	0.0	0.0	0.0	5.0	0.0	0.0	5.0
Cycle O Clear(c ₁), s	1.3	33.4	33.5	44.0	0.0	0.0	0.0	5.0	0.0	0.0	5.0
Prop In Lane	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Lane Grp Cap(C), veh/h	618	1297	643	1226	1862	0	0	916	192	0	916
V/C Ratio(X)	0.05	0.85	0.85	1.54	0.31	0.00	0.00	0.36	0.00	0.00	0.36
Avail Cap(C _{av}), veh/h	618	1297	643	1226	1862	0	0	916	192	0	916
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Uniform Delay (d), s/veh	25.1	35.4	35.4	16.0	0.0	0.0	0.0	48.1	0.0	0.0	48.1
Incr Delay (d ₂), s/veh	0.1	6.9	12.9	247.5	0.4	0.0	0.0	1.1	0.0	0.0	1.1
Initial Q Delay(d ₃), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%), veh/h	0.6	18.0	18.9	61.6	0.1	0.0	0.0	2.1	0.0	0.0	2.1
LnGrp Delay(d _l), s/veh	25.3	42.3	48.3	263.5	0.4	0.0	0.0	49.2	0.0	0.0	49.2
LnGrp LOS	C	D	D	F	A			D		D	D
Approach Vol, veh/h		1667		2472				333			333
Approach Delay, s/veh		44.0		201.5				49.2			49.2
Approach LOS		D		F				D			D
Timer	1	2	3	4	5	6	7	8			
Assigned Phs	2			5	6			8			
Phs Duration (G+Y+Rc), s	71.0			50.0	21.0			49.0			
Change Period (Y+Rc), s	6.0			6.0	6.0			6.0			
Max Green Setting (G _{max}), s	65.0			44.0	15.0			43.0			
Max O Clear Time (G _o +H ₁), s	2.0			46.0	7.0			35.5			
Green Ext Time (G _o -C), s	22.0			0.0	1.2			5.4			
Intersection Summary											
HCM 2010 Ctrl Delay				131.4							
HCM 2010 LOS				F							
Notes											

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Timing Report, Sorted By Phase
2: Ellsworth Road & SR 24 WB Ramp(s)

2025 Option A Mitigated AM, Syn

Phase Number	2	5	6	8
Movement	NBT	SBT	WBTL	
Lead/Lag	Lag	Lead		
Recall Mode	Max	Max	Max	Max
Maximum Split (s)	71	50	21	49
Maximum Split (%)	59.2%	41.7%	17.5%	40.8%
Minimum Split (s)	36	10	36	36
Yellow Time (s)	4	4	4	4
All-Red Time (s)	2	2	2	2
Minimum Initial (s)	4	4	4	4
Vehicle Extension (s)	3	3	3	3
Minimum Gap (s)	3	3	3	3
Time Before Reduce (s)	0	0	0	0
Time To Reduce (s)	5	5	5	5
Walk Time (s)	0	0	0	0
Flash Dont Walk (s)	25	25	25	25
Dual Entry	Yes	No	Yes	Yes
Inhibit Max	Yes	Yes	Yes	Yes
Start Time (s)	50	71	50	1
End Time (s)	1	1	71	50
Yield/Force Off (s)	115	115	65	44
Yield/Force Off 170(s)	90	115	40	19
Local Start Time (s)	0	21	0	71
Local Yield (s)	65	65	15	114
Local Yield 170(s)	40	65	110	89
Intersection Summary				
Cycle Length		120		
Control Type		Prelim		
Natural Cycle		145		
Offset: 50 (42%), Referenced to phase 2:NBT and 6:SBT, Start of Green				
Spills and Phases: 2: Ellsworth Road & SR 24 WB Ramp(s)				
	↑ 02 (R)			
	71 s			
	↓ 05 (R)			
	24 s			
				↑ 05
				50 s
				↓ 05
				49 s
				↑ 08

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HCM 2010 Signalized Intersection Summary
7: Signal Butte Road & SR 24 EB Ramp(s)

2025 Option A Mitigated AM, Syn

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBR
Lane Configurations		←	←	←	←	←	←	←	←	←	←
Traffic Volume (veh/h)	100	350	450	0	0	0	0	775	200	75	125
Future Volume (veh/h)	100	350	450	0	0	0	0	775	200	75	125
Number	7	4	14	0	0	0	1	6	16	5	2
Initial Q (Cb), veh	0	0	0	0	0	0	0	0	0	0	0
Peak-Bike Adj(A _{bkt})	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow, veh/h	1810	1810	1810	1810	1810	1810	1810	1810	1810	1810	1810
Adj Flow Rate, veh/h	111	639	333	0	0	0	0	861	222	83	139
Adj No. of Lanes	1	2	1	0	0	0	0	4	1	1	3
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Percent Heavy Veh, %	5	5	5	5	5	5	5	5	5	5	5
Cap, veh/h	819	1719	731	0	0	0	0	1712	423	172	2100
Arrive On Green	0.47	0.47	0.47	0.00	0.00	0.00	0.00	0.28	0.20	0.85	0.00
Sat Flow, veh/h	1723	3619	1538	0	0	0	0	6478	1538	1723	5103
Grp Volume(V), veh/h	111	639	333	0	0	0	0	861	222	83	139
Grp Sat Flow(S), veh/h	1723	1810	1538	0	0	0	0	1556	1538	1723	1647
Q Serve(Q _s), s	4.3	13.5	17.4	0.0	0.0	0.0	0.0	14.0	14.7	5.1	0.5
Cycle O Clear(c ₁), s	4.3	13.5	17.4	0.0	0.0	0.0	0.0	14.0	14.7	5.1	0.5
Prop In Lane	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Lane Grp Cap(C), veh/h	819	1719	731	0	0	0	0	1712	423	172	2100
V/C Ratio(X)	0.14	0.37	0.46	0.00	0.00	0.00	0.00	0.50	0.52	0.48	0.07
Avail Cap(C _{av}), veh/h	819	1719	731	0	0	0	0	1712	423	172	2100
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Uniform Delay (d), s/veh	17.7	20.1	21.1	0.0	0.0	0.0	0.0	36.6	36.9	45.2	5.2
Incr Delay (d ₂), s/veh	0.3	0.6	2.0	0.0	0.0	0.0	0.0	1.1	4.6	9.3	0.1
Initial Q Delay(d ₃), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%), veh/h	2.1	6.9	17.3	0.0	0.0	0.0	0.0	6.1	6.8	2.9	0.2
LnGrp Delay(d _l), s/veh	18.0	20.7	23.2	0.0	0.0	0.0	0.0	37.7	41.5	54.6	5.3
LnGrp LOS	B	C	C					D	D	D	A
Approach Vol, veh/h	1083			1083				222			222
Approach Delay, s/veh	21.2			38.4				23.7			23.7
Approach LOS	C			D				C			C
Timer	1	2	3	4	5	6	7	8			
Assigned Phs	2			4	5	6		8			
Phs Duration (G+Y+Rc), s	57.0			63.0	18.0	39.0		49.0			
Change Period (Y+Rc), s	6.0			6.0	6.0	6.0		6.0			
Max Green Setting (G _{max}), s	51.0			57.0	12.0	33.0		43.0			
Max O Clear Time (G _o +H ₁), s	2.5			19.4	7.1	16.7		16.7			
Green Ext Time (G _o -C), s	1.1			6.2	0.4	5.7		5.7			
Intersection Summary											
HCM 2010 Ctrl Delay				29.2							
HCM 2010 LOS				C							
Notes											

HCM 2010 Signalized Intersection Summary
 8: Signal Butte Road & SR 24 WB Ramp(s)

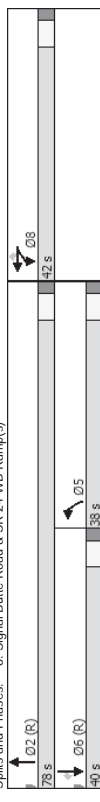
2025 Option A Mitigated AM, Syn

	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBR	
Lane Configurations			4↑	4↑	4↑	4↑	4↑	4↑	4↑	4↑	4↑	↑↑↑↑
Traffic Volume (veh/h)	0	0	0	100	725	100	650	125	0	0	200	250
Future Volume (veh/h)	0	0	0	100	725	100	650	125	0	0	200	250
Number				3	8	18	5	2	12	1	6	16
Initial Q (Ob), veh				0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A, pbT)				1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus, Adj				1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow, veh/hln				1810	1810	1810	1810	1810	1810	1810	1810	1810
Adj Flow Rate, veh/h				111	806	111	722	139	0	0	222	278
Adj No. of Lanes				1	2	1	2	2	0	0	4	1
Peak Hour Factor				0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Percent Heavy Veh, %				5	5	5	5	5	5	5	5	5
Cap, veh/h				517	1086	461	892	2063	0	0	1764	436
Arrive On Green				0.30	0.30	0.30	0.53	1.00	0.00	0.00	0.28	0.28
Sat Flow, veh/h				1723	3619	1538	3343	3529	0	0	6478	1538
Grip Volume(s), veh/h				111	806	111	722	139	0	0	222	278
Grip Sat Flow(s), veh/hln				1723	1810	1538	1672	1719	0	0	1556	1538
Q Serve(Q, s), s				5.8	24.1	6.5	21.3	0.0	0.0	0.0	3.2	19.0
Cycle Q Clear(q, c), s				5.8	24.1	6.5	21.3	0.0	0.0	0.0	3.2	19.0
Prop In Lane				1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Lane Grp Cap(c), veh/h				517	1086	461	892	2063	0	0	1764	436
V/C Ratio(X)				0.21	0.74	0.24	0.81	0.07	0.00	0.00	0.13	0.64
Avail Cap(c-a), veh/h				517	1086	461	892	2063	0	0	1764	436
HCM Platoon Ratio				1.00	1.00	1.00	2.00	2.00	1.00	1.00	1.00	1.00
Upstream Filter(i)				1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Incr Delay (d2), s/veh				0.9	4.6	1.2	7.9	0.1	0.0	0.0	0.1	7.0
Initial Q Delay(d3), s/veh				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%), veh/hln				2.9	12.7	2.9	10.6	0.0	0.0	0.0	1.4	8.9
LnGrp Delay(d), s/veh				32.4	42.4	32.9	33.4	0.1	0.0	0.0	32.1	44.6
LnGrp LOS				C	D	C	C	A			C	D
Approach Vol, veh/h				1028				861			500	
Approach Delay, s/veh				40.3				28.0			39.0	
Approach LOS				D				C			D	
Timer		1	2	3	4	5	6	7	8			
Assigned Phs		2			5	6		8				
Phs Duration (G+Y+Rc), s		78.0			38.0	40.0		42.0				
Change Period (Y+Rc), s		6.0			6.0	6.0		6.0				
Max Green Sealing (Gmax), s		72.0			32.0	34.0		36.0				
Max Q Clear Time (Qc+H1), s		2.0			23.3	21.0		26.1				
Green Ext Time (g-c), s		3.7			2.5	1.9		4.1				
Intersection Summary												
HCM 2010 Ctrl Delay												35.6
HCM 2010 LOS												D
Notes												

Timing Report, Sorted By Phase
 8: Signal Butte Road & SR 24 WB Ramp(s)

2025 Option A Mitigated AM, Syn

Phase Number	2	5	6	8
Movement	NBT	NBL	SBT	WBTL
Lead/Lag			Lag	Lead
Recall Mode	Max	Max	Max	Max
Maximum Spill (%)	78	38	40	42
Minimum Spill (%)	65.0%	31.7%	33.3%	35.0%
Yellow Time (s)	36	10	36	36
All-Red Time (s)	4	4	4	4
Minimum Initial (s)	2	2	2	2
Minimum Extension (s)	4	4	4	4
Vehicle Extension (s)	3	3	3	3
Minimum Gap (s)	3	3	3	3
Time Before Reduce (s)	0	0	0	0
Walk Time (s)	5	0	0	0
Flash Dont Walk (s)	25	25	25	25
Inhibit Max	Yes	No	Yes	Yes
Start Time (s)	0	40	0	78
End Time (s)	78	78	40	0
Yield/Force Off (s)	72	72	34	114
Yield/Force Off 170(s)	47	72	9	89
Local Start Time (s)	0	40	0	78
Local Yield (s)	72	72	34	114
Local Yield 170(s)	47	72	9	89
Intersection Summary				
Cycle Length	120			
Control Type	Prelimf			
Natural Cycle	95			
Offset: 0 (0%), Referenced to phase 2/NBT and 6/SBT, Start of Green				



HCM 2010 Signalized Intersection Summary
 1: Ellsworth Road & SR 24 EB Ramp(s)

2025 Option A Mitigated PM, Syn

	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBR	
Lane Configurations			4↑	4↑	4↑	4↑	4↑	4↑	4↑	4↑	4↑	↑↑↑↑
Traffic Volume (veh/h)	1175	1750	2375	0	0	0	0	1125	175	50	175	0
Future Volume (veh/h)	1175	1750	2375	0	0	0	0	1125	175	50	175	0
Number	7	4	14	0	0	0	1	6	16	5	2	12
Initial Q (Ob), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A, pbT)	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow, veh/hln	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863
Adj Flow Rate, veh/h	833	2445	0	0	0	0	0	1197	186	53	186	0
Adj No. of Lanes	1	2	1	0	0	0	0	4	1	2	3	0
Peak Hour Factor	0.94	0.94	0.94	0.90	0.94	0.94	0.94	0.94	0.94	0.94	0.90	0.90
Percent Heavy Veh, %	1005	2111	897	0	0	0	0	1388	343	229	1695	0
Cap, veh/h	1005	2111	897	0	0	0	0	1388	343	229	1695	0
Arrive On Green	0.57	0.57	0.57	0.00	0.00	0.00	0.22	0.22	0.13	0.67	0.00	0.00
Sat Flow, veh/h	1774	3725	1583	0	0	0	6669	1583	3442	5253	0	0
Grip Volume(s), veh/h	833	2445	0	0	0	0	1197	186	53	186	0	0
Grip Sat Flow(s), veh/hln	1774	1863	1583	0	0	0	1602	1583	1721	1695	0	0
Q Serve(Q, s), s	46.0	68.0	0.0	0.0	0.0	0.0	21.6	125	1.7	1.6	0.0	0.0
Cycle Q Clear(q, c), s	46.0	68.0	0.0	0.0	0.0	0.0	21.6	125	1.7	1.6	0.0	0.0
Prop In Lane	1.00	1.00	1.00	0.00	0.00	0.00	1.00	1.00	1.00	1.00	0.00	0.00
Lane Grp Cap(c), veh/h	1005	2111	897	0	0	0	1388	343	229	1695	0	0
V/C Ratio(X)	0.83	1.16	0.00	0.00	0.86	0.54	0.23	0.11	0.00	0.00	0.00	0.00
Avail Cap(c-a), veh/h	1005	2111	897	0	0	0	1388	343	229	1695	0	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	2.00	2.00	1.00	1.00	1.00	1.00
Upstream Filter(i)	1.00	1.00	0.00	0.00	0.00	0.00	1.00	1.00	1.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	21.2	26.0	0.0	0.0	45.3	41.7	49.2	13.6	0.0	0.0	0.0	0.0
Incr Delay (d2), s/veh	7.9	76.9	0.0	0.0	7.3	6.0	2.3	0.1	0.0	0.0	0.0	0.0
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%), veh/hln	24.6	57.2	0.0	0.0	10.3	6.1	0.9	0.7	0.0	0.0	0.0	0.0
LnGrp Delay(d), s/veh	29.1	102.9	0.0	0.0	52.5	47.8	51.6	13.7	0.0	0.0	0.0	0.0
LnGrp LOS	C	F			D	D	D	B				
Approach Vol, veh/h	3278						1383				239	
Approach Delay, s/veh	84.2						51.9				22.1	
Approach LOS	F						D				C	
Timer		1	2	3	4	5	6	7	8			
Assigned Phs		2			4	5	6					
Phs Duration (G+Y+Rc), s		46.0			74.0	14.0	32.0					
Change Period (Y+Rc), s		6.0			6.0	6.0	6.0					
Max Green Sealing (Gmax), s		40.0			68.0	8.0	26.0					
Max Q Clear Time (Qc+H1), s		3.6			70.0	3.7	23.6					
Green Ext Time (g-c), s		1.3			0.0	0.4	1.7					
Intersection Summary												
HCM 2010 Ctrl Delay												72.0
HCM 2010 LOS												E
Notes												

Timing Report, Sorted By Phase
 1: Ellsworth Road & SR 24 EB Ramp(s)

2025 Option A Mitigated PM, Syn

Phase Number	2	4	5	6
Movement	SBT	EBTL	SBL	NBT
Lead/Lag			Lag	Lead
Recall Mode	Max	Max	Max	Max
Maximum Spill (%)	46	74	14	32
Minimum Spill (%)	38.3%	61.7%	11.7%	26.7%
Yellow Time (s)	36	36	10	3

HCM 2010 Signalized Intersection Summary
 2: Ellsworth Road & SR 24 WB Ramp(s)

2025 Option A Mitigated PM, syn

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBR	
Lane Configurations		4↑		4↑	4↑		4↑	4↑		4↑	4↑	
Traffic Volume (veh/h)	0	0	0	50	750	50	550	575	0	0	225	
Future Volume (veh/h)	0	0	0	50	750	50	550	575	0	0	225	
Number	0	0	0	3	8	18	5	2	12	1	6	
Initial Q (Cb), veh	0	0	0	0	0	0	0	0	0	0	0	
Peak BkUp Adj(A _{pb})	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Adj Sat Flow, veh/hln	1863	1863	1863	1900	1863	1863	0	0	1863	1863	1863	
Adj Flow Rate, veh/h	53	798	53	585	612	0	0	0	239	0	1	
Adj No. of Lanes	1	3	0	2	2	0	2	0	0	5	1	
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.90	0.90	0.94	0.94	0.94	0.94	
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	
Cap, veh/h	444	1296	86	516	2300	0	0	3395	712	0	0	
Arrive On Green	0.25	0.25	0.25	0.30	1.00	0.00	0.00	0.00	0.45	0.00	0.00	
Sat Flow, veh/h	1774	5185	343	3442	3632	0	0	7898	1583	0	0	
Grp Volume(V), veh/h	53	572	279	585	612	0	0	239	0	0	0	
Grp Sat Flow(S), veh/hln	1774	1863	1802	1721	1770	0	0	1509	1583	0	0	
Q Serve(Q _s), s	2.8	16.3	16.5	18.0	0.0	0.0	0.0	2.2	0.0	0.0	2.2	
Cycle O Clear(c), s	2.8	16.3	16.5	18.0	0.0	0.0	0.0	2.2	0.0	0.0	2.2	
Prop In Lane	1.00	1.00	0.19	1.00	0.00	0.00	0.00	0.00	1.00	0.00	1.00	
Lane Grp Cap(C), veh/h	444	931	451	516	2300	0	0	3395	712	0	0	
V/C Ratio(X)	0.12	0.61	0.62	1.13	0.27	0.00	0.00	0.07	0.00	0.00	0.00	
Avail Cap(C _a), veh/h	444	931	451	516	2300	0	0	3395	712	0	0	
HCM Platoon Ratio	1.00	1.00	1.00	2.00	2.00	1.00	1.00	1.00	1.00	1.00	1.00	
Upstream Filter(I)	1.00	1.00	1.00	1.00	1.00	0.00	0.00	0.00	1.00	0.00	1.00	
Uniform Delay (d), s/veh	34.8	39.9	39.9	42.0	0.0	0.0	0.0	18.7	0.0	0.0	18.7	
Incr Delay (d2), s/veh	0.6	3.0	6.2	81.7	0.3	0.0	0.0	0.0	0.0	0.0	0.0	
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
%ile Back(Q _{50%}), veh/ln	1.4	8.8	9.0	14.3	0.1	0.0	0.0	0.9	0.0	0.0	0.9	
LnGrp Delay(d), s/veh	35.3	42.9	46.2	123.7	0.3	0.0	0.0	18.8	0.0	0.0	18.8	
LnGrp LOS	D	D	D	F	A	A	A	B	D	D	B	
Approach Vol, veh/h				904				1197				239
Approach Delay, s/veh				43.5				60.6				18.8
Approach LOS				D				E				B
Timer	1	2	3	4	5	6	7	8				
Assigned Phs	2			5	6			8				
Phs Duration (G+Y+R), s	84.0			24.0	60.0			36.0				
Change Period (Y+R), s	6.0			6.0	6.0			6.0				
Max Green Setting (G _{max}), s	78.0			18.0	54.0			30.0				
Max O Clear Time (G+C+H), s	2.0			20.0	4.2			18.5				
Green Ext Time (G _{ext}), s	7.0			0.0	1.5			4.0				
Intersection Summary												
HCM 2010 Ctrl Delay	49.7											
HCM 2010 LOS	D											
Notes												

Timing Report, Sorted By Phase
 2: Ellsworth Road & SR 24 WB Ramp(s)

2025 Option A Mitigated PM, syn

Phase Number	2	5	6	8
Movement	NBT	NBL	SBT	WBTL
Lead/Lag			Lag	Lead
Lead/Lag Optimize				
Recall Mode	Max	Max	Max	Max
Maximum Split (s)	84	24	60	36
Maximum Split (%)	70.0%	20.0%	50.0%	30.0%
Minimum Split (s)	36	10	36	36
Yellow Time (s)	4	4	4	4
All-Red Time (s)	2	2	2	2
Minimum Initial (s)	4	4	4	4
Minimum Extension (s)	3	3	3	3
Minimum Gap (s)	3	3	3	3
Time Before Reduce (s)	0	0	0	0
Time To Reduce (s)	5	0	0	0
Walk Time (s)	0	0	0	0
Flash Dont Walk (s)	25	25	25	25
Dual Entry	Yes	No	Yes	Yes
Inhibit Max	Yes	Yes	Yes	Yes
Start Time (s)	50	110	50	14
End Time (s)	14	14	110	50
Yield/Force Off (s)	8	8	104	44
Yield/Force Off 170(s)	103	8	79	19
Local Start Time (s)	0	60	0	84
Local Yield (s)	78	78	54	114
Local Yield 170(s)	53	78	29	89
Intersection Summary				
Cycle Length	120			
Control Type	Prelimed			
Natural Cycle	145			
Offset: 50 (42%), Referenced to phase 2:NBT and 6:SBT, Start of Green				



HCM 2010 Signalized Intersection Summary
 7: Signal Butte Road & SR 24 EB Ramp(s)

2025 Option A Mitigated PM, syn

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBR
Lane Configurations		4↑		4↑	4↑		4↑	4↑		4↑	4↑
Traffic Volume (veh/h)	100	975	875	0	0	0	650	100	25	200	0
Future Volume (veh/h)	100	975	875	0	0	0	650	100	25	200	0
Number	7	4	14	0	0	0	6	16	5	2	12
Initial Q (Cb), veh	0	0	0	0	0	0	0	0	0	0	0
Peak BkUp Adj(A _{pb})	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow, veh/hln	1863	1863	1863	1863	1863	1863	0	1863	1863	1863	1863
Adj Flow Rate, veh/h	106	1503	621	0	0	0	691	106	27	213	0
Adj No. of Lanes	1	2	1	1	1	0	4	1	1	3	0
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2
Cap, veh/h	961	2018	858	0	0	0	1549	383	118	1822	0
Arrive On Green	0.54	0.54	0.54	0.00	0.24	0.24	0.13	0.72	0.00	0.00	0.00
Sat Flow, veh/h	1774	3725	1583	0	0	0	6669	1583	1774	5253	0
Grp Volume(V), veh/h	106	1503	621	0	0	0	691	106	27	213	0
Grp Sat Flow(S), veh/hln	1774	1863	1583	0	0	0	1602	1583	1774	1695	0
Q Serve(Q _s), s	3.5	37.2	35.5	0.0	11.0	6.5	1.6	1.6	0.0	0.0	0.0
Cycle O Clear(c), s	3.5	37.2	35.5	0.0	11.0	6.5	1.6	1.6	0.0	0.0	0.0
Prop In Lane	1.00	1.00	1.00	0.00	1.00	1.00	1.00	1.00	0.00	0.00	0.00
Lane Grp Cap(C), veh/h	961	2018	858	0	1549	383	118	1822	0	0	0
V/C Ratio(X)	0.11	0.74	0.72	0.00	0.45	0.28	0.23	0.12	0.00	0.00	0.00
Avail Cap(C _a), veh/h	961	2018	858	0	1549	383	118	1822	0	0	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	2.00	2.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	1.00	0.00	1.00	1.00	1.00	1.00	0.00	0.00	0.00
Uniform Delay (d), s/veh	13.4	21.1	20.7	0.0	38.7	37.0	49.2	11.1	0.0	0.0	0.0
Incr Delay (d2), s/veh	0.2	2.5	5.3	0.0	0.9	1.8	4.4	0.1	0.0	0.0	0.0
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile Back(Q _{50%}), veh/ln	1.8	19.7	31.3	0.0	4.9	3.0	0.9	0.7	0.0	0.0	0.0
LnGrp Delay(d), s/veh	13.6	23.7	26.0	0.0	39.6	38.8	53.7	11.3	0.0	0.0	0.0
LnGrp LOS	B	C	C	D	D	D	D	D	D	D	B
Approach Vol, veh/h	2230			797			16.0			240	
Approach Delay, s/veh	23.9			39.5			16.0			B	
Approach LOS	C			D			D			B	
Timer	1	2	3	4	5	6	7	8			
Assigned Phs	2			4	5	6					
Phs Duration (G+Y+R), s	49.0			71.0	14.0	35.0					
Change Period (Y+R), s	6.0			6.0	6.0	6.0					
Max Green Setting (G _{max}), s	43.0			65.0	8.0	29.0					
Max O Clear Time (G+C+H), s	3.6			39.2	3.6	13.0					
Green Ext Time (G _{ext}), s	1.4			15.8	0.5	4.2					
Intersection Summary											
HCM 2010 Ctrl Delay	27.1										
HCM 2010 LOS	C										
Notes											

Timing Report, Sorted By Phase
 7: Signal Butte Road & SR 24 EB Ramp(s)

2025 Option A Mitigated PM, syn

Phase Number	2	4	5	6
Movement	SBT	EBTL	SBL	NBT
Lead/Lag			Lag	Lead
Lead/Lag Optimize				
Recall Mode	Max	Max	Max	Max
Maximum Split (s)	49	71	14	35
Maximum Split (%)	40.8%	59.2%	11.7%	29.2%
Minimum Split (s)	36	36	10	36
Yellow Time (s)	4	4	4	4
All-Red Time (s)	2	2	2	2
Minimum Initial (s)	4	4	4	4
Minimum Extension (s)	3	3	3	3
Minimum Gap (s)	3	3	3	3
Time Before Reduce (s)	0	0	0	0
Time To Reduce (s)	5	5	0	0
Walk Time (s)	25	25	25	25
Flash Dont Walk (s)	Yes	Yes	No	Yes
Inhibit Max	Yes	Yes	Yes	Yes
Start Time (s)	0	49	35	0
End Time (s)	43	114	43	

HCM 2010 Signalized Intersection Summary
 8: Signal Butte Road & SR 24 WB Ramp(s)

2025 Option A Mitigated PM.syn

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBR
Lane Configurations				←↑	←↑	←↑	←↑	←↑	←↑	←↑	←↑
Traffic Volume (veh/h)	0	0	0	25	500	50	275	375	0	0	225
Future Volume (veh/h)	0	0	0	25	500	50	275	375	0	0	225
Number				3	8	18	5	2	12	1	6
Initial Q (Cb), veh				0	0	0	0	0	0	0	0
Ped/Bike Adj(A_pb1)				1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus. Adj				1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow (veh/h)				1863	1863	1863	1863	1863	0	0	1863
Adj Sat Flow Rate (veh/h)				27	532	53	293	399	0	0	239
Adj No. of Lanes				1	2	1	2	2	0	0	4
Peak Hour Factor				0.94	0.94	0.94	0.94	0.90	0.90	0.94	0.94
Percent Heavy Veh. %				2	2	2	2	2	0	0	2
Cap. veh/h				798	1676	712	459	1593	0	0	1709
Arrive On Green				0.45	0.45	0.45	0.27	0.90	0.00	0.00	0.27
Sat Flow (veh/h)				1774	3725	1583	3442	3632	0	0	6669
Grp Volume(i), veh/h				27	532	53	293	399	0	0	239
Grp Sat Flow(i), veh/h/m				1774	1863	1583	1721	1770	0	0	1602
Q Serve(Q_s), s				1.0	11.0	2.3	9.0	1.7	0.0	0.0	3.4
Cycle Q Clear(q_c), s				1.0	11.0	2.3	9.0	1.7	0.0	0.0	3.4
Prop In Lane				1.00	1.00	1.00	1.00	0.00	0.00	0.00	1.00
Lane Grp Cap(c), veh/h				798	1676	712	459	1593	0	0	1709
%ile Retail(X)				0.03	0.32	0.07	0.64	0.25	0.00	0.00	0.14
Avail Cap(c-a), veh/h				798	1676	712	459	1593	0	0	1709
HCM Platoon Ratio				1.00	1.00	1.00	2.00	2.00	1.00	1.00	1.00
Upstream Filter(i)				1.00	1.00	1.00	1.00	1.00	0.00	0.00	1.00
Uniform Delay (d), s/veh				18.4	21.2	18.8	41.4	3.4	0.0	0.0	33.5
Incr Delay (d2), s/veh				0.1	0.5	0.2	6.7	0.4	0.0	0.0	0.2
Initial Q Delay(d3), s/veh				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%), veh/m				0.5	5.7	1.0	4.7	0.9	0.0	0.0	1.5
LnGrp Delay(d), s/veh				18.5	21.7	19.0	48.1	3.8	0.0	0.0	33.7
LnGrp LOS				B	C	B	D	A			C
Approach Vol, veh/h				612				692			345
Approach Delay, s/veh				21.3				22.5			34.4
Approach LOS				C				C			C
Timer				1	2	3	4	5	6	7	8
Assigned Phs				2							
Phs Duration (G+Y+Rc), s				60.0							
Change Period (Y+Rc), s				6.0							
Max Green Scalling (Gmax), s				54.0							
Max Q Clear Time (Q_c+1), s				3.7							
Green Ext Time (q_c), s				3.7							

Intersection Summary
 HCM 2010 Ctrl Delay 24.6
 HCM 2010 LOS C

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Timing Report, Sorted By Phase
 8: Signal Butte Road & SR 24 WB Ramp(s)

2025 Option A Mitigated PM.syn

Phase Number	2	5	6	8
Movement	NBT	NBL	SBT	WBTL
Lead/Lag		Lag	Lead	
Recall Mode	Max	Max	Max	Max
Maximum Split (s)	60	22	38	60
Maximum Split (%)	50.0%	18.3%	31.7%	50.0%
Minimum Split (s)	36	10	36	36
Yellow Time (s)	4	4	4	4
All-Red Time (s)	2	2	2	2
Minimum Initial (s)	4	4	4	4
Vehicle Extension (s)	3	3	3	3
Minimum Gap (s)	3	3	3	3
Time Before Reduce (s)	0	0	0	0
Walk Time (s)	5	0	0	0
Flash Dont Walk (s)	25	25	25	25
Dual Entry	Yes	No	Yes	Yes
Inhibit Max	Yes	Yes	Yes	Yes
Start Time (s)	0	38	0	60
End Time (s)	60	60	38	0
Yield/Force Off (s)	54	54	32	114
Yield/Force Off T70(s)	29	54	7	89
Local Start Time (s)	0	38	0	60
Local Yield (s)	54	54	32	114
Local Yield T70(s)	29	54	7	89
Intersection Summary				
Cycle Length	120			
Control Type	Pretimed			
Natural Cycle	85			
Offset: 0 (0%), Referenced to Phase 2/NBT and 6/SBT, Start of Green				
Spills and Phases:	8: Signal Butte Road & SR 24 WB Ramp(s)			
	↑ 02 (R)	↑ 03	↑ 05	↑ 08
	60 s	60 s	60 s	60 s
	↓ 06 (R)	↓ 07	↓ 09	↓ 12
	38 s	22 s	38 s	36 s

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2025 OPTION B PEAK HOUR ANALYSIS

APPENDIX I

2025 Option B AM
1: Ellsworth Road & SR 24 EB Ramp(s)

HCM 2010 Signalized Intersection Summary

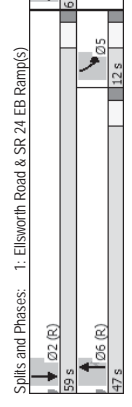
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	4T	4T	T	4T	T	T	T	T	T	T	T	T
Traffic Volume (veh/h)	850	800	925	0	0	0	0	2375	25	25	275	0
Future Volume (veh/h)	850	800	925	0	0	0	0	2375	25	25	275	0
Number	7	4	14	0	0	0	1	6	16	5	2	12
Initial Q (OB), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A, pbT)	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow, veh/hln	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863
Adj Flow Rate, veh/h	603	1273	0	0	0	0	2527	27	27	293	0	0
Adj No. of Lanes	1	2	1	0	0	0	4	1	2	3	0	0
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Percent Heavy Veh, %	813	1708	726	0	0	0	2189	541	172	2246	0	0
Cap, veh/h	0.46	0.46	0.46	0.00	0.34	0.34	0.10	0.88	0.00	0.00	0.00	0.00
Arrive On Green	1774	3725	1583	0	6669	1583	3442	5253	0	0	0	0
Sat Flow, veh/h	603	1273	0	0	2527	27	27	293	0	0	0	0
Grp Volume(s), veh/h	1774	1863	1583	0	1602	1583	1721	1695	0	0	0	0
Q Sat Flow(s), veh/hln	335	337	0	0	410	14	0.9	0.9	0.0	0.0	0.0	0.0
Q Served(s), s	335	337	0	0	410	14	0.9	0.9	0.0	0.0	0.0	0.0
Cycle Q Clear(Q_c), s	1.00	1.00	1.00	0.00	0.00	1.00	1.00	1.00	0.00	0.00	0.00	0.00
Prop In Lane	813	1708	726	0	2189	541	172	2246	0	0	0	0
Lane Cap Cap(C), veh/h	0.74	0.75	0.00	0.00	1.15	0.05	0.16	0.13	0.00	0.00	0.00	0.00
W/C Ratio(X)	813	1708	726	0	2189	541	172	2246	0	0	0	0
Avail Cap(C-a), veh/h	1.00	1.00	1.00	1.00	1.00	1.00	2.00	2.00	1.00	1.00	1.00	1.00
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(i)	267	267	0	0	39.5	26.5	51.7	4.0	0.0	0.0	0.0	0.0
Uniform Delay (d), s/veh	6.0	3.0	0.0	0.0	0.0	75.1	0.2	1.9	0.1	0.1	0.0	0.0
Incr Delay (d2), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Initial Q Delay(Q0), s/veh	17.6	18.0	0.0	0.0	29.5	0.6	0.5	0.4	0.0	0.0	0.0	0.0
%ile BackOfQ(50%), veh/h	32.7	29.8	0.0	0.0	114.6	26.6	53.6	4.1	0.0	0.0	0.0	0.0
LnGrp Delay(d), s/veh	C	C	C	F	C	D	A	A	A	A	A	A
LnGrp LOS	C	C	C	F	C	D	A	A	A	A	A	A
Approach Vol, veh/h	1876	307	0	2554	113.7	0	8.3	0	0	0	0	0
Approach Delay, s/veh	30.7	30.7	0	113.7	113.7	0	8.3	0	0	0	0	0
Approach LOS	C	C	C	F	F	A	A	A	A	A	A	A
Timer	1	2	3	4	5	6	7	8				
Assigned Phs	2	4	5	6								
Phs Duration (G+Y+R), s	59.0	61.0	12.0	47.0								
Change Period (Y+R), s	6.0	6.0	6.0	6.0								
Max Green Setting (Gmax), s	53.0	55.0	6.0	41.0								
Max Q Clear Time (Q_c+H), s	2.9	35.7	2.9	43.0								
Green EXT Time (G_c), s	2.0	10.7	0.5	0.0								
Intersection Summary												
HCM 2010 Ctrl Delay	73.8											
HCM 2010 LOS	E											
Notes												

2025 Option B AM
1: Ellsworth Road & SR 24 EB Ramp(s)

Timing Report, Sorted By Phase

Phase Number	2	4	5	6
Movement	SBT	EBTL	SBL	NBT
Lead/Lag	Lag	Lag	Lead	
Recall Mode	Max	Max	Max	Max
Maximum Spill (s)	59	61	12	47
Maximum Spill (%)	49.2%	50.8%	10.0%	39.2%
Minimum Spill (s)	36	36	10	36
Yellow Time (s)	4	4	4	4
All-Red Time (s)	2	2	2	2
Minimum Initial (s)	4	4	4	4
Vehicle Extension (s)	3	3	3	3
Minimum Gap (s)	3	3	3	3
Time Before Reduce (s)	0	0	0	0
Time To Reduce (s)	0	0	0	0
Walk Time (s)	5	5	5	5
Flash Don't Walk (s)	25	25	10	25
Dual Entry	Yes	Yes	No	Yes
Inhibit Max	Yes	Yes	Yes	Yes
Start Time (s)	0	59	47	0
End Time (s)	59	0	59	47
Yield/Force Off (s)	53	114	53	41
Yield/Force Off (170)(s)	28	89	53	16
Local Start Time (s)	0	59	47	0
Local Yield (s)	53	114	53	41
Local Yield 170(s)	28	89	53	16

Intersection Summary	120
Cycle Length	Prelim
Control Type	135
Natural Cycle	135
Offset: 0 (0%), Referenced to phase 2, SBT and 6, NBT, Start of Green	



Spills and Phases: 1: Ellsworth Road & SR 24 EB Ramp(s)

2025 Option B AM

2: Ellsworth Road & SR 24 WB Ramp(s)

SR 24 Interchanges - 2025 Option B AM

HCM 2010 Signalized Intersection Summary

Table with 16 columns: Movement, EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR. Rows include Lane Configurations, Traffic Volume, Future Volume, Number, Ped-Bike Adj, Parking Bus, Adj Sat Flow, Adj Flow Rate, Adj No. of Lanes, Peak Hour Factor, Percent Heavy Veh, Cap, Arrive On Green, Sat Flow, Grp Volume, Pkts Duration, Cycle O Clear, Prop In Lane, Lane Grp Cap, V/C Ratio, Avail Cap, HCM Platoon Ratio, Upstream Delay, Incr Delay, Initial O Delay, %ile BackOf, LnGrp Delay, LnGrp LOS, Approach Vol, Approach Delay, Approach LOS, Timer, Assigned Pkts, Pkts Duration, Change Period, Max Green, Max O Clear, Green Ext Time.

Intersection Summary

HCM 2010 CRT Delay 1212

HCM 2010 LOS F

Notes

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2025 Option B AM

2: Ellsworth Road & SR 24 WB Ramp(s)

SR 24 Interchanges - 2025 Option B AM

Timing Report, Sorted By Phase

Table with 8 columns: Phase Number, Movement, NBT, SBT, WBT, SBR, EBL, EBR. Rows include Lead-Lag, Recall Mode, Maximum Split, Minimum Split, Yellow Time, All-Red Time, Minimum Initial, Vehicle Extension, Minimum Gap, Time Before Reduce, Walk Time, Flash Dont Walk, Inhibit Max, Start Time, End Time, Yield/Force Off, Local Start, Local Yield, Local Yield 170s.

Intersection Summary

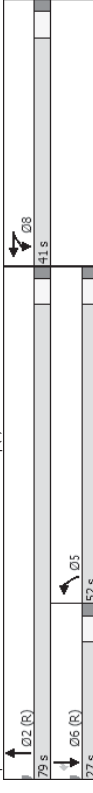
Cycle Length 120

Control Type Prelimed

Natural Cycle 145

Offset: 50 (42%), Referenced to phase 2:NBT and 6:SBT, Start of Green

Splits and Phases: 2: Ellsworth Road & SR 24 WB Ramp(s)



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SR 24 Interchanges - 2025 Option B AM

HCM 2010 Signalized Intersection Summary

Table with 16 columns: Movement, EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR. Rows include Lane Configurations, Traffic Volume, Future Volume, Number, Ped-Bike Adj, Parking Bus, Adj Sat Flow, Adj Flow Rate, Adj No. of Lanes, Peak Hour Factor, Percent Heavy Veh, Cap, Arrive On Green, Sat Flow, Grp Volume, Pkts Duration, Cycle O Clear, Prop In Lane, Lane Grp Cap, V/C Ratio, Avail Cap, HCM Platoon Ratio, Upstream Delay, Incr Delay, Initial O Delay, %ile BackOf, LnGrp Delay, LnGrp LOS, Approach Vol, Approach Delay, Approach LOS, Timer, Assigned Pkts, Pkts Duration, Change Period, Max Green, Max O Clear, Green Ext Time.

Intersection Summary

HCM 2010 CRT Delay 1212

HCM 2010 LOS F

Notes

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2025 Option B AM

7: Signal Butte Road & SR 24 EB Ramp(s)

SR 24 Interchanges - 2025 Option B AM

HCM 2010 Signalized Intersection Summary

Table with 16 columns: Movement, EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR. Rows include Lane Configurations, Traffic Volume, Future Volume, Number, Initial O, Parking Bus, Adj Sat Flow, Adj Flow Rate, Adj No. of Lanes, Peak Hour Factor, Percent Heavy Veh, Arrive On Green, Sat Flow, Grp Volume, Pkts Duration, Cycle O Clear, Prop In Lane, Lane Grp Cap, V/C Ratio, Avail Cap, HCM Platoon Ratio, Upstream Delay, Incr Delay, Initial O Delay, %ile BackOf, LnGrp Delay, LnGrp LOS, Approach Vol, Approach Delay, Approach LOS, Timer, Assigned Pkts, Pkts Duration, Change Period, Max Green, Max O Clear, Green Ext Time.

Intersection Summary

HCM 2010 CRT Delay 22.4

HCM 2010 LOS C

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2025 Option B AM

7: Signal Butte Road & SR 24 EB Ramp(s)

SR 24 Interchanges - 2025 Option B AM

Timing Report, Sorted By Phase

Table with 6 columns: Phase Number, Movement, SBT, EBL, NBT. Rows include Lead-Lag, Recall Mode, Maximum Split, Minimum Split, Yellow Time, All-Red Time, Minimum Initial, Vehicle Extension, Minimum Gap, Time Before Reduce, Walk Time, Flash Dont Walk, Inhibit Max, Start Time, End Time, Yield/Force Off, Local Start, Local Yield, Local Yield 170s.

Intersection Summary

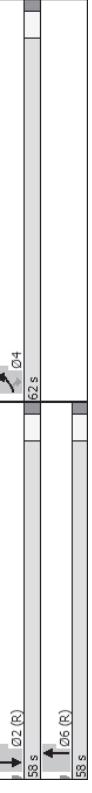
Cycle Length 120

Control Type Prelimed

Natural Cycle 75

Offset: 0 (0%), Referenced to phase 2:SBT and 6:NBT, Start of Green

Splits and Phases: 7: Signal Butte Road & SR 24 EB Ramp(s)



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2025 Option B AM

SR 24 Interchanges - 2025 Option B AM
HCM 2010 Signalized Intersection Summary

8: Signal Butte Road & SR 24 WB Ramp(s)

	EBL	EBT	EBR	NBL	NBT	SBT	SBR
Movement	↔	↔	↔	↔	↔	↔	↔
Lane Configurations							
Traffic Volume (veh/h)	0	0	1250	250	375	50	50
Future Volume (veh/h)	0	0	1250	250	375	50	50
Number			5	2	6	16	
Initial Q (Cb) veh			0	0	0	0	
Ped/Bike Adj(A _{pb})			1.00	1.00	1.00	1.00	
Parking Bus Adj			1.00	1.00	1.00	1.00	
Adj Sat Flow (veh/h)	1863	1863	1863	1863	1863	1863	
Adj Flow Rate (veh/h)	1330	266	399	53	53	53	
Adj No. of Lanes	2	2	2	2	1	1	
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	
Percent Heavy Veh. %			2	2	2	2	
Cap. veh/h	1514	3256	1416	633	633	633	
Arrive On Green	0.88	1.00	0.40	0.40	0.40	0.40	
Sat Flow (veh/h)	3442	3632	3632	1583	1583	1583	
Grip Volume(v), veh/h	1330	266	399	53	53	53	
Grip Sat Flow(s), veh/h/m	1721	1770	1770	1583	1583	1583	
Q Serve(Q _s), s	15.3	0.0	5.7	1.6	1.6	1.6	
Cycle O Clear(q _c), s	55.3	0.0	5.7	1.6	1.6	1.6	
Prop In Lane	1.00			1.00			
Lane Grp Cap(c), veh/h	1514	3256	1416	633	633	633	
V/C Ratio(X)	0.88	0.08	0.28	0.08	0.08	0.08	
Avail Cap(c _a), veh/h	1514	3256	1416	633	633	633	
HCM Platoon Ratio	2.00	2.00	1.00	1.00	1.00	1.00	
Upstream Filter(f)	1.00	1.00	1.00	1.00	1.00	1.00	
Uniform Delay (d), s/veh	3.4	0.0	15.2	14.0	14.0	14.0	
Incr Delay (d ₂), s/veh	7.5	0.0	0.5	0.3	0.3	0.3	
Initial Q Delay(d ₃), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	
%ile Back(Q ₅₀), veh/m	7.3	0.0	2.9	0.7	0.7	0.7	
LnGrp Delay(d ₄), s/veh	11.0	0.0	15.7	14.2	14.2	14.2	
LnGrp LOS	B	A	B	B	B	B	
Approach Vol, veh/h			1596	452	452	452	
Approach Delay, s/veh			9.2	15.5	15.5	15.5	
Approach LOS			A	B	B	B	
Timer	1	2	3	4	5	6	7
Assigned Phs	2						
Phs Duration (G+Y+Rc), s	75.0						
Change Period (Y+Rc), s	6.0						
Max Green Setting (G _{max}), s	69.0						
Max O Clear Time (Q _{c+H}), s	2.0						
Green Ext Time (q _c), s	9.0						
Intersection Summary							
HCM 2010 Ctrl Delay	10.6						
HCM 2010 LOS	B						

2025 Option B AM
8: Signal Butte Road & SR 24 WB Ramp(s)

SR 24 Interchanges - 2025 Option B AM
Timing Report, Sorted By Phase

	2	5	6				
Phase Number	NBT	SBL	NBT				
Movement	↔	↔	↔				
Lead/Lag	Lag	Lead	Lead				
Recall Mode	Max	Max	Max				
Maximum Split (s)	75	39	36				
Maximum Split (%)	100.0%	52.0%	48.0%				
Minimum Split (s)	36	10	36				
Yellow Time (s)	4	4	4				
All-Red Time (s)	2	2	2				
Minimum Initial (s)	4	4	4				
Vehicle Extension (s)	3	3	3				
Minimum Gap (s)	3	3	3				
Time Before Reduce (s)	0	0	0				
Time To Reduce (s)	0	0	0				
Walk Time (s)	5	5	5				
Flash Dont Walk (s)	25	No	25				
Dual Entry	Yes	No	Yes				
Inhibit Max	Yes	Yes	Yes				
Start Time (s)	0	36	0				
End Time (s)	0	0	36				
Yield/Force Off (s)	69	69	30				
Yield/Force Off 170(s)	44	69	5				
Local Start Time (s)	0	36	0				
Local Yield (s)	69	69	30				
Local Yield 170(s)	44	69	5				
Intersection Summary							
Cycle Length	75						
Control Type	Prelimined						
Natural Cycle	70						
Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBT, Start of Green							
Splits and Phases: 8: Signal Butte Road & SR 24 WB Ramp(s)							
	↑ 02 R						
	↓ 05 R	↑ 05					
	↓ 05 R		↓ 39 R				

2025 Option B PM

SR 24 Interchanges - 2025 Option B PM
HCM 2010 Signalized Intersection Summary

1: Ellisoroth Road & SR 24 EB Ramp(s)

	EBL	EBT	EBR	WBL	WBR	NBL	NBT	SBL	SBT	SBR
Movement	↔	↔	↔	↔	↔	↔	↔	↔	↔	↔
Lane Configurations										
Traffic Volume (veh/h)	1125	1425	2550	0	0	0	1225	100	50	175
Future Volume (veh/h)	1125	1425	2550	0	0	0	1225	100	50	175
Number	7	4	14	0	0	1	6	16	5	2
Initial Q (Cb) veh	0	0	0	0	0	0	0	0	0	0
Ped/Bike Adj(A _{pb})	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow (veh/h)	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863
Adj Flow Rate (veh/h)	798	2074	0	0	0	1303	106	53	186	0
Adj No. of Lanes	1	2	1	0	0	4	1	2	3	0
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Percent Heavy Veh. %	991	2080	884	0	0	1495	369	201	1737	0
Cap. veh/h	991	2080	884	0	0	1495	369	201	1737	0
Arrive On Green	0.56	0.56	0.00	0.00	0.00	0.23	0.23	0.12	0.68	0.00
Sat Flow (veh/h)	1774	3725	1583	0	0	6669	1583	3442	5253	0
Grip Volume(v), veh/h	798	2074	0	0	0	1303	106	53	186	0
Grip Sat Flow(s), veh/h/m	1774	1863	1583	0	0	1602	1583	1721	1695	0
Q Serve(Q _s), s	43.3	66.6	0.0	0.0	0.0	23.5	6.6	1.7	1.5	0.0
Cycle O Clear(q _c), s	43.3	66.6	0.0	0.0	0.0	23.5	6.6	1.7	1.5	0.0
Prop In Lane	1.00	1.00	1.00	0.00	0.00	1.00	1.00	1.00	1.00	0.00
Lane Grp Cap(c), veh/h	991	2080	884	0	0	1495	369	201	1737	0
V/C Ratio(X)	0.81	1.00	0.00	0.00	0.00	0.87	0.29	0.26	0.11	0.00
Avail Cap(c _a), veh/h	991	2080	884	0	0	1495	369	201	1737	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	2.00	2.00	1.00	0.00
Upstream Filter(f)	1.00	1.00	0.00	0.00	0.00	1.00	1.00	1.00	1.00	0.00
Uniform Delay (d), s/veh	21.3	26.4	0.0	0.0	0.0	44.3	37.8	50.7	12.7	0.0
Incr Delay (d ₂), s/veh	7.0	19.1	0.0	0.0	0.0	7.3	1.9	3.2	0.1	0.0
Initial Q Delay(d ₃), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile Back(Q ₅₀), veh/m	23.0	39.5	0.0	0.0	0.0	11.2	3.1	0.9	0.7	0.0
LnGrp Delay(d ₄), s/veh	28.2	45.5	0.0	0.0	0.0	51.5	39.7	53.8	12.9	0.0
LnGrp LOS	C	D	D	D	D	D	D	D	B	B
Approach Vol, veh/h			2872			1409			239	
Approach Delay, s/veh			40.7			50.6			22.0	
Approach LOS			D			D			C	
Timer	1	2	3	4	5	6	7	8		
Assigned Phs	2									
Phs Duration (G+Y+Rc), s	47.0									
Change Period (Y+Rc), s	6.0									
Max Green Setting (G _{max}), s	41.0									
Max O Clear Time (Q _{c+H}), s	3.5									
Green Ext Time (q _c), s	1.3									
Intersection Summary										
HCM 2010 Ctrl Delay	42.8									
HCM 2010 LOS	D									
Notes										

2025 Option B PM

SR 24 Interchanges - 2025 Option B PM
Timing Report, Sorted By Phase

1: Ellisoroth Road & SR 24 EB Ramp(s)

	2	4	5	6
Phase Number	SBT	EBTL	SBL	NBT
Movement	↔	↔	↔	↔
Lead/Lag	Lag	Lead	Lead	Lead
Recall Mode	Max	Max	Max	Max
Maximum Split (s)	47	73	13	34
Maximum Split (%)	39.2%	60.8%	10.8%	28.3%
Minimum Split (s)	36	36	10	36
Yellow Time (s)	4	4	4	4
All-Red Time (s)	2	2	2	2
Minimum Initial (s)	4	4	4	4
Vehicle Extension (s)	3	3	3	3
Minimum Gap (s)	3	3	3	3
Time Before Reduce (s)	0	0	0	0
Time To Reduce (s)	0	0	0	0
Walk Time (s)	5	5	5	5
Flash Dont Walk (s)	25	25	No	25
Dual Entry	Yes	Yes	Yes	Yes
Inhibit Max	Yes	Yes	Yes	Yes
Start Time (s)	0	47	34	0
End Time (s)	47	0	47	34
Yield/Force Off (s)	41	114	41	28
Yield/Force Off 170(s)	16	89	41	3
Local Start Time (s)	0	47	34	0
Local Yield (s)	41	114	41	28
Local Yield 170(s)	16	89	41	3
Intersection Summary				
Cycle Length	120			
Control Type	Prelimined			
Natural Cycle	145			
Offset: 0 (0%), Referenced to phase 2:SBT and 6:NBT, Start of Green				
Splits and Phases: 1: Ellisoroth Road & SR 24 EB Ramp(s)				
	↑ 02 R			
	↓ 47 R	↑ 05 R	↓ 04	
	↓ 47 R		↓ 13 R	↓ 34 R

2025 Option B PM
8: Signal Butte Road & SR 24 WB Ramp(s)

SR 24 Interchanges - 2025 Option B PM
HCM 2010 Signalized Intersection Summary

Movement	EBL	EBR	NBL	NBT	SBT	SBR		
Lane Configurations								
Traffic Volume (veh/h)	0	0	675	350	300	25		
Ped/Bike Adj (A _{pbT})								
Future Volume (veh/h)	0	0	675	350	300	25		
Number			5	2	6	16		
Initial Q (Cb), veh			0	0	0	0		
Parking Bus. Adj			1.00	1.00	1.00	1.00		
Adj Sat Flow, veh/hln			1863	1863	1863	1863		
Adj Flow Rate, veh/h			718	372	319	27		
Adj No. of Lanes			2	2	2	1		
Peak Hour Factor			0.94	0.94	0.94	0.94		
Percent Heavy Veh. %			2	2	2	2		
Cap. veh/h			1836	3362	1298	581		
Arrive On Green			1.00	1.00	0.37	0.37		
Sat Flow, veh/h			3442	3632	3632	1583		
Grp Volume(v), veh/h			718	372	319	27		
Grp Sat Flow(s), veh/hln			1721	1770	1770	1583		
Q Serve(q_s), s			0.0	0.0	7.5	1.3		
Cycle Q Clear(q_c), s			0.0	0.0	7.5	1.3		
Prop In Lane			1.00			1.00		
Lane Grp Cap(c), veh/h			1836	3362	1298	581		
V/C Ratio(X)			0.39	0.11	0.25	0.05		
Avail Cap(c_a), veh/h			1836	3362	1298	581		
HCM Platoon Ratio			2.00	2.00	1.00	1.00		
Upstream Filter(f)			1.00	1.00	1.00	1.00		
Uniform Delay (d), s/veh			0.0	0.0	26.5	24.5		
Incr Delay (d2), s/veh			0.6	0.1	0.5	0.2		
Initial Q Delay(d3), s/veh			0.0	0.0	0.0	0.0		
%ile BackOfQ(50%), veh/ln			0.2	0.0	3.8	0.6		
LnGrp Delay(d), s/veh			0.6	0.1	26.9	24.6		
LnGrp LOS			A	A	C	C		
Approach Vol, veh/h			1090	346				
Approach Delay, s/veh			0.4	26.7				
Approach LOS			A	C				
Timer	1	2	3	4	5	6	7	8
Assigned Phs	2				5	6		
Phs Duration (G+Y+Rc), s	120.0				70.0	50.0		
Change Period (Y+Rc), s	6.0				6.0	6.0		
Max Green Scalling (Gmax), s	114.0				64.0	44.0		
Max Q Clear Time (Q_c+H1), s	2.0				2.0	9.5		
Green Ext Time (g_c), s	5.5				5.5	2.0		

Intersection Summary
HCM 2010 Ctrl Delay
HCM 2010 LOS

2025 Option B PM
8: Signal Butte Road & SR 24 WB Ramp(s)

SR 24 Interchanges - 2025 Option B PM
Timing Report, Sorted By Phase

Phase Number	2	5	6
Movement	NBT	NBL	SBT
Lead/Lag		Lag	Lead
Recall Lag Optimize			
Lead/Lag			
Recall Mode	Max	Max	Max
Maximum Split (s)	120	70	50
Maximum Split (%)	100.0%	58.3%	41.7%
Minimum Split (s)	36	10	36
Yellow Time (s)	4	4	4
All-Red Time (s)	2	2	2
Minimum Initial (s)	4	4	4
Vehicle Extension (s)	3	3	3
Minimum Gap (s)	0	0	0
Time Before Reduce (s)	0	0	0
Walk Time (s)	5		5
Flash Dont Walk (s)	25	25	25
Dual Entry	Yes	No	Yes
Inhibit Max	Yes	Yes	Yes
Start Time (s)	0	50	0
End Time (s)	0	0	50
Yield/Force Off (s)	114	114	44
Yield/Force Off 170(s)	89	114	19
Local Start Time (s)	0	50	0
Local Yield (s)	114	114	44
Local Yield 170(s)	89	114	19

Intersection Summary
Cycle Length
Control Type
Natural Cycle
Offset: 0 (0%), Referenced to phase 2/NBT and 6/GBT, Start of Green

Spills and Phases: 8: Signal Butte Road & SR 24 WB Ramp(s)

↑ 0.2 (R)			
↓ 0.2 (R)			
↑ 0.5 (R)			
↓ 0.5 (R)			
50 s			
70 s			

HCM 2010 Signalized Intersection Summary

2035 AM.Syn

Timing Report, Sorted By Phase

2035 AM.Syn

2: Ellsworth Road & SR 24 WB Ramp(s)

Table showing traffic flow, delay, and timing parameters for the intersection. Columns include EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR. Rows include Traffic Volume, Number of Lanes, Peak Hour Factor, Cycle Length, and various delay metrics.

Intersection Summary HCM 2010 CRT Delay

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Phase timing report for Ellsworth Road & SR 24 WB Ramp(s). Shows 8 phases with columns for NBT, SBT, WBT, NBL, SBL, WBL. Includes metrics like Max, Lag, and Min.



Spills and Phases: 2: Ellsworth Road & SR 24 WB Ramp(s)

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HCM 2010 Signalized Intersection Summary

2035 AM.Syn

Timing Report, Sorted By Phase

2035 AM.Syn

3: Williams Field Road & SR 24 EB Ramp(s)

Table showing traffic flow, delay, and timing parameters for the intersection. Columns include EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR. Rows include Traffic Volume, Number of Lanes, Peak Hour Factor, Cycle Length, and various delay metrics.

Intersection Summary HCM 2010 CRT Delay

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Phase timing report for Williams Field Road & SR 24 EB Ramp(s). Shows 6 phases with columns for EBTL, EBTR, EBL, EBT, EBR, EBTL. Includes metrics like Max, Lag, and Min.



Spills and Phases: 3: Williams Field Road & SR 24 EB Ramp(s)

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HCM 2010 Signalized Intersection Summary

2035 AM.Syn

Timing Report, Sorted By Phase

2035 AM.Syn

3: Williams Field Road & SR 24 EB Ramp(s)

Table showing traffic flow, delay, and timing parameters for the intersection. Columns include EBL, EBT, EBR, WBL, WBT, WBR, NBL, NBT, SBL, SBR. Rows include Traffic Volume, Number of Lanes, Peak Hour Factor, Cycle Length, and various delay metrics.

Intersection Summary HCM 2010 CRT Delay

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Phase timing report for Williams Field Road & SR 24 EB Ramp(s). Shows 6 phases with columns for EBTL, EBTR, EBL, EBT, EBR, EBTL. Includes metrics like Max, Lag, and Min.



Spills and Phases: 3: Williams Field Road & SR 24 EB Ramp(s)

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HCM 2010 Signalized Intersection Summary
10: Meridian Road & SR 24 WB Ramp(s)

2035 AM.Syn

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBR
Lane Configurations											
Traffic Volume (veh/h)	0	0	0	100	0	50	2250	275	0	0	225
Future Volume (veh/h)	0	0	0	100	0	50	2250	275	0	0	225
Number				3	8	18	5	2	12	1	6
Initial Q (Cb), veh				0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)				1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus. Adj				1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow (veh/h)	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863
Adj Sat Flow (veh/h)	106	0	53	2394	293	0	0	239	0	0	
Adj No. of Lanes	1	0	2	2	2	2	2	2	0	0	
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	
Percent Heavy Veh. %	2	2	2	2	2	2	2	2	2	2	
Cap. veh/h	222	0	396	2151	2743	0	0	641	158	0	
Arrive On Green	0.13	0.00	0.13	1.00	1.00	1.00	0.00	0.00	0.10	0.00	
Sat Flow (veh/h)	1774	0	3167	3442	3632	0	0	6669	1583	0	
Grip Volume(V), veh/h	106	0	53	2394	293	0	0	239	0	0	
Grip Sat Flow(S), veh/h/h	1774	0	1583	1721	1770	0	0	1602	1583	0	
Q Serve(Q_s), s	6.7	0.0	1.8	75.0	0.0	0.0	0.0	4.2	0.0	0.0	
Cycle O Clear(q_c), s	6.7	0.0	1.8	75.0	0.0	0.0	0.0	4.2	0.0	0.0	
Prop In Lane	1.00	1.00	1.00	1.00	1.00	0.00	0.00	1.00	1.00	0.00	
Lane Grp Cap(C), veh/h	222	0	396	2151	2743	0	0	641	158	0	
V/C Ratio(X)	0.48	0.00	0.13	1.11	0.11	0.00	0.00	0.37	0.00	0.00	
Avail Cap(C-a), veh/h	222	0	396	2151	2743	0	0	641	158	0	
HCM Platoon Ratio	1.00	1.00	1.00	2.00	2.00	1.00	1.00	1.00	1.00	1.00	
Upstream Filter(I)	1.00	0.00	1.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00	
Uniform Delay (d), s/veh	48.9	0.00	46.7	0.00	0.00	0.00	0.00	50.5	0.00	0.00	
Incr Delay (d2), s/veh	7.2	0.00	0.7	58.1	0.11	0.00	0.00	1.7	0.00	0.00	
Initial Q Delay(d3), s/veh	0.0	0.00	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
%ile BackOfQ(50%), veh/h	3.7	0.00	0.8	17.3	0.00	0.00	0.00	1.9	0.00	0.00	
LnGrp Delay(d), s/veh	56.1	0.00	47.4	58.1	0.11	0.00	0.00	52.1	0.00	0.00	
LnGrp LOS	E		D	F	A			D		D	
Approach Vol, veh/h	159			2887			239			0	
Approach Delay, s/veh	53.2			51.7			52.1			0	
Approach LOS	D			D			D			D	
Timer	1	2	3	4	5	6	7	8			
Assigned Phs	2			5	6			8			
Phs Duration (G+Y+Rc), s	99.0			81.0	18.0			21.0			
Change Period (Y+Rc), s	6.0			6.0	6.0			6.0			
Max Green Setting (Gmax), s	93.0			75.0	12.0			15.0			
Max O Clear Time (q_c+H1), s	2.0			77.0	6.2			8.7			
Green Ext Time (g_c), s	29.8			0.0	0.6			0.2			

Intersection Summary
HCM 2010 Ctrl Delay 51.8
HCM 2010 LOS D

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Timing Report, Sorted By Phase
10: Meridian Road & SR 24 WB Ramp(s)

2035 AM.Syn

Phase Number	2	5	6	8
Movement	NBT	NBL	SBT	WBTL
Lead/Lag	Lag	Lead		
Recall Mode	Max	Max	Max	Max
Maximum Split (s)	99	81	18	21
Maximum Split (%)	82.5%	67.5%	15.0%	17.5%
Minimum Split (s)	36	10	27	13
Yellow Time (s)	4	4	4	4
All-Red Time (s)	2	2	2	2
Minimum Initial (s)	4	4	4	4
Vehicle Extension (s)	3	3	3	3
Minimum Gap (s)	3	3	3	3
Time Before Reduce (s)	0	0	0	0
Time To Reduce (s)	0	0	0	0
Walk Time (s)	5	5	5	5
Flash Dont Walk (s)	15	No	Yes	Yes
Inhibit Max	Yes	Yes	Yes	Yes
Start Time (s)	0	18	0	99
End Time (s)	99	99	18	0
Yield/Force Off (s)	93	93	12	114
Yield/Force Off 170(s)	78	93	117	114
Local Start Time (s)	0	18	0	99
Local Yield (s)	93	93	12	114
Local Yield 170(s)	78	93	117	114

Intersection Summary
Cycle Length 120
Control Type Prelimined
Natural Cycle 150
Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBT, Start of Green

Splits and Phases: 10: Meridian Road & SR 24 WB Ramp(s)

02 (R)	05	08
59 s	81 s	21 s

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HCM 2010 Signalized Intersection Summary
11: Ironwood Road & SR 24 EB Ramp(s)

2035 AM.Syn

Movement	EBL	EBR	NBL	NBR	SBL	SBR
Lane Configurations						
Traffic Volume (veh/h)	25	375	0	1600	675	0
Future Volume (veh/h)	25	375	0	1600	675	0
Number	7	14	1	6	2	12
Initial Q (Cb), veh	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus. Adj	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow (veh/h)	1863	1863	0	1863	1863	0
Adj Sat Flow (veh/h)	27	399	0	1702	718	0
Adj No. of Lanes	1	2	0	4	2	0
Peak Hour Factor	0.94	0.94	0.90	0.94	0.94	0.90
Percent Heavy Veh. %	2	2	2	2	2	2
Cap. veh/h	680	1214	0	3311	1829	0
Arrive On Green	0.38	0.38	0.00	0.52	1.00	0.00
Sat Flow (veh/h)	1774	3167	0	6929	3725	0
Grip Volume(V), veh/h	27	399	0	1702	718	0
Grip Sat Flow(S), veh/h/h	1774	1583	0	1602	1770	0
Q Serve(Q_s), s	11.1	10.7	0.0	21.0	0.0	0.0
Cycle O Clear(q_c), s	1.1	10.7	0.0	21.0	0.0	0.0
Prop In Lane	1.00	1.00	0.00	1.00	0.00	0.00
Lane Grp Cap(C), veh/h	680	1214	0	3311	1829	0
V/C Ratio(X)	0.04	0.33	0.00	0.51	0.39	0.00
HCM Platoon Ratio	1.00	1.00	1.00	2.00	1.00	1.00
Upstream Filter(I)	1.00	1.00	0.00	1.00	1.00	0.00
Uniform Delay (d), s/veh	23.2	26.1	0.00	19.1	0.00	0.00
Incr Delay (d2), s/veh	0.1	0.7	0.00	0.6	0.00	0.00
Initial Q Delay(d3), s/veh	0.0	0.0	0.00	0.00	0.00	0.00
%ile BackOfQ(50%), veh/h	0.6	4.8	0.00	9.4	0.2	0.00
LnGrp Delay(d), s/veh	23.3	26.8	0.00	19.7	0.00	0.00
LnGrp LOS	C	C		B	A	
Approach Vol, veh/h	426		1702		718	
Approach Delay, s/veh	26.6		19.7		0.6	
Approach LOS	C		B		A	
Timer	1	2	3	4	5	6
Assigned Phs	2			4		6
Phs Duration (G+Y+Rc), s	68.0			52.0		68.0
Change Period (Y+Rc), s	6.0			6.0		6.0
Max Green Setting (Gmax), s	62.0			46.0		62.0
Max O Clear Time (q_c+H1), s	2.0			12.7		23.0
Green Ext Time (g_c), s	31.5			1.7		24.8

Intersection Summary
HCM 2010 Ctrl Delay 15.9
HCM 2010 LOS B

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Timing Report, Sorted By Phase
11: Ironwood Road & SR 24 EB Ramp(s)

2035 AM.Syn

Phase Number	2	4	6
Movement	SBT	EBL	NBT
Lead/Lag			
Recall Mode	Max	Max	Max
Maximum Split (s)	68	52	68
Maximum Split (%)	56.7%	43.3%	56.7%
Minimum Split (s)	36	36	36
Yellow Time (s)	4	4	4
All-Red Time (s)	2	2	2
Minimum Initial (s)	4	4	4
Vehicle Extension (s)	3	3	3
Minimum Gap (s)	3	3	3
Time Before Reduce (s)	0	0	0
Time To Reduce (s)	5	5	5
Walk Time (s)	25	25	25
Flash Dont Walk (s)	Yes	Yes	Yes
Inhibit Max	Yes	Yes	Yes
Start Time (s)	0	68	0
End Time (s)	68	0	68
Yield/Force Off (s)	62	114	62
Yield/Force Off 170(s)	37	89	37
Local Start Time (s)	0	68	0
Local Yield (s)	62	114	62
Local Yield 170(s)	37	89	37

Intersection Summary
Cycle Length 120
Control Type Prelimined
Natural Cycle 75
Offset: 0 (0%), Referenced to phase 2:SBT and 6:NBT, Start of Green

Splits and Phases: 11: Ironwood Road & SR 24 EB Ramp(s)

02 (R)	04	06
68 s	52 s	68 s

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HCM 2010 Signalized Intersection Summary
12: Ironwood Road & SR 24 WB Ramp(s)

2035 AM.Syn

	EBL	EBR	NBL	NBT	SBT	SBR	
Movement							
Lane Configurations							
Traffic Volume (veh/h)	0	0	875	725	700	75	
Future Volume (veh/h)	0	0	875	725	700	75	
Number			5	2	6	16	
Initial Q (Ob), veh			0	0	0	0	
Ped-Bike Adj(A_pbT)			1.00	1.00	1.00	1.00	
Parking Bus, Adj			1.00	1.00	1.00	1.00	
Adj Sat Flow, veh/hln			1863	1863	1863	1863	
Adj Flow Rate, veh/h			931	771	745	80	
Adj No. of Lanes			2	2	2	1	
Peak Hour Factor			0.94	0.94	0.94	0.94	
Percent Heavy Veh, %			2	2	2	2	
Cap, veh/h			1991	3362	1681	752	
Arrive On Green			0.85	1.00	0.97	0.47	
Sat Flow, veh/h			3442	3632	3632	1583	
Grip Volume(V), veh/h			931	771	745	80	
Grip Sat Flow(S), veh/hln			1721	1770	1770	1583	
Q Serve(Q_s), s			0.0	0.0	16.8	3.4	
Cycle Q Clear(q_c), s			0.0	0.0	16.8	3.4	
Prop In Lane			1.00	1.00	1.00	1.00	
Lane Grp Cap(C), veh/h			1991	3362	1681	752	
V/C Ratio(X)			0.47	0.23	0.44	0.11	
Avail Cap(C_a), veh/h			1991	3362	1681	752	
HCM Platoon Ratio			2.00	2.00	1.00	1.00	
Upstream Filter(I)			1.00	1.00	1.00	1.00	
Uniform Delay (d), s/veh			1.3	0.0	20.9	17.4	
Incr Delay (d2), s/veh			0.8	0.2	0.8	0.3	
Initial Q Delay(d3), s/veh			0.0	0.0	0.0	0.0	
%ile BackOfQ(50%), veh/ln			1.5	0.1	8.4	1.5	
LnGrp Delay(d), s/veh			2.1	0.2	21.8	17.7	
LnGrp LOS			A	A	C	B	
Approach Vol, veh/h			1702	825			
Approach Delay, s/veh			1.2	21.4			
Approach LOS			A	C			
Timer	1	2	3	4	5	6	7
Assigned Phs	2			5	6		
Phs Duration (G+Y+Rc), s	120.0			57.0	63.0		
Change Period (Y+Rc), s	6.0			6.0	6.0		
Max Green Setting (Gmax), s	114.0			51.0	57.0		
Max Q Clear Time (Q_c+H1), s	2.0			2.0	18.8		
Green Ext Time (g_e), s	11.8			11.4	5.6		
Intersection Summary							
HCM 2010 Ctrl Delay	7.8						
HCM 2010 LOS	A						

Timing Report, Sorted By Phase
12: Ironwood Road & SR 24 WB Ramp(s)

2035 AM.Syn

	2	5	6
Movement	NBTL	SBL	NBT
Lead/Lag	Lag	Lead	Lead
Recall Mode	Max	Max	Max
Maximum Split (s)	120	57	63
Maximum Split (%)	100.0%	47.5%	52.5%
Minimum Split (s)	36	10	36
Yellow Time (s)	4	4	4
All-Red Time (s)	2	2	2
Minimum Initial (s)	4	4	4
Vehicle Extension (s)	3	3	3
Minimum Gap (s)	3	3	3
Time Before Reduce (s)	0	0	0
Time To Reduce (s)	5	0	5
Walk Time (s)	5	0	5
Flash Dont Walk (s)	25	No	25
Inhibit Max	Yes	Yes	Yes
Start Time (s)	0	63	0
End Time (s)	0	0	63
Yield/Force Off (s)	114	114	57
Yield/Force Off 170(s)	89	114	32
Local Start Time (s)	0	63	0
Local Yield (s)	114	114	57
Local Yield 170(s)	89	114	32
Intersection Summary			
Cycle Length	120		
Control Type	Prelimined		
Natural Cycle	50		
Offset: 0 (0%), Referenced to phase 2/NBTL and 6/SBT, Start of Green			
Splits and Phases: 12: Ironwood Road & SR 24 WB Ramp(s)			
	02 (R)		05
	53 s		157 s

HCM 2010 Signalized Intersection Summary
1: Ellsworth Road & SR 24 EB Ramp(s)

2035 PM.Syn

	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (veh/h)	1125	0	1725	0	0	0	0	950	75	75	300	0
Future Volume (veh/h)	1125	0	1725	0	0	0	0	950	75	75	300	0
Number	7	4	14	0	0	0	1	6	16	5	2	12
Initial Q (Ob), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow, veh/hln	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863
Adj Flow Rate, veh/h	1197	0	0	0	0	0	0	1011	80	80	319	0
Adj No. of Lanes	2	1	1	0	0	0	0	4	1	2	3	0
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	2
Cap, veh/h	1863	978	831	0	0	0	0	1602	396	258	1907	0
Arrive On Green	0.52	0.00	0.00	0.00	0.00	0.00	0.25	0.25	0.15	0.75	0.00	0.00
Sat Flow, veh/h	3548	1863	1583	0	0	0	6669	1583	3442	5253	0	0
Grip Volume(V), veh/h	1197	0	0	0	0	0	1011	80	80	319	0	0
Grip Sat Flow(S), veh/hln	1774	1863	1583	0	0	0	1602	1583	1721	1695	0	0
Q Serve(Q_s), s	29.0	0.0	0.0	0.0	0.0	0.0	16.9	4.8	2.5	2.2	0.0	0.0
Cycle Q Clear(q_c), s	29.0	0.0	0.0	0.0	0.0	0.0	16.9	4.8	2.5	2.2	0.0	0.0
Prop In Lane	1.00	1.00	1.00	0.00	0.00	0.00	1.00	1.00	1.00	1.00	0.00	0.00
Lane Grp Cap(C), veh/h	1863	978	831	0	0	0	1602	396	258	1907	0	0
V/C Ratio(X)	0.64	0.00	0.00	0.00	0.00	0.00	0.63	0.20	0.31	0.17	0.00	0.00
Avail Cap(C_a), veh/h	1863	978	831	0	0	0	1602	396	258	1907	0	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	2.00	2.00	1.00	1.00
Upstream Filter(I)	1.00	0.00	0.00	0.00	0.00	0.00	1.00	1.00	1.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	20.4	0.0	0.0	0.0	0.0	0.0	40.1	35.5	48.2	9.6	0.0	0.0
Incr Delay (d2), s/veh	1.7	0.0	0.0	0.0	0.0	0.0	1.9	1.1	3.1	0.2	0.0	0.0
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%), veh/ln	14.6	0.0	0.0	0.0	0.0	0.0	7.7	2.2	1.3	1.0	0.0	0.0
LnGrp Delay(d), s/veh	22.1	0.0	0.0	0.0	0.0	0.0	42.0	36.7	51.3	9.8	0.0	0.0
LnGrp LOS	C			D	D	D	D	D	D	D	A	A
Approach Vol, veh/h	1197			1091			1091			399		
Approach Delay, s/veh	22.1			41.6			41.6			18.2		
Approach LOS	C			D			D			B		
Timer	1	2	3	4	5	6	7	8				
Assigned Phs	2			4	5	6						
Phs Duration (G+Y+Rc), s	51.0			69.0	15.0	36.0						
Change Period (Y+Rc), s	6.0			6.0	6.0	6.0						
Max Green Setting (Gmax), s	45.0			63.0	9.0	30.0						
Max Q Clear Time (Q_c+H1), s	4.2			31.0	4.5	18.9						
Green Ext Time (g_e), s	2.3			5.3	0.9	5.0						
Intersection Summary												
HCM 2010 Ctrl Delay	29.4											
HCM 2010 LOS	C											

Timing Report, Sorted By Phase
1: Ellsworth Road & SR 24 EB Ramp(s)

2035 PM.Syn

	2	4	5	6
Movement	SBT	EBTL	SBL	NBT
Lead/Lag	Lag	Lead	Lead	Lead
Recall Mode	Max	Max	Max	Max
Maximum Split (s)	51	69	15	36
Maximum Split (%)	42.5%	57.5%	12.5%	30.0%
Minimum Split (s)	36	36	10	36
Yellow Time (s)	4	4	4	4
All-Red Time (s)	2	2	2	2
Minimum Initial (s)	4	4	4	4
Vehicle Extension (s)	3	3	3	3
Minimum Gap (s)	3	3	3	3
Time Before Reduce (s)	0	0	0	0
Time To Reduce (s)	5	5	0	5
Walk Time (s)	5	5	0	5
Flash Dont Walk (s)	25	25	No	25
Inhibit Max	Yes	Yes	Yes	Yes
Start Time (s)	0	51	36	0
End Time (s)	51	0	51	36
Yield/Force Off (s)	45	114	45	30
Yield/Force Off 170(s)	20	89	45	5
Local Start Time (s)	0	51	36	0
Local Yield (s)	45	114	45	30
Local Yield 170(s)	20	89	45	5
Intersection Summary				
Cycle Length	120			
Control Type	Prelimined			
Natural Cycle	135			
Offset: 0 (0%), Referenced to phase 2/SBT and 6/NBT, Start of Green				
Splits and Phases: 1: Ellsworth Road & SR 24 EB Ramp(s)				
	02 (R)		04	
	51 s		59 s	
	106 (R)		15 s	

HCM 2010 Signalized Intersection Summary

2035 PM.Syn

2035 PM.Syn

Timing Report, Sorted By Phase

2: Ellsworth Road & SR 24 WB Ramp(s)

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	0	0	0	50	0	50	375	575	0	0	375	900
Traffic Volume (veh/h)	0	0	0	50	0	50	375	575	0	0	375	900
Future Volume (veh/h)	0	0	0	50	0	50	375	575	0	0	375	900
Number	0	0	0	3	8	18	5	2	12	1	6	16
Initial Q (Obt.) veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pb1)	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus. Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow, veh/h/ln	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863
Adj Flow Rate, veh/h	69	0	35	399	612	0	0	399	0	0	399	0
Adj No. of Lanes	2	0	1	2	2	0	2	0	0	5	1	1
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.90	0.90	0.94	0.94	0.94	0.94
Percent Heavy Veh. %	2	2	2	2	2	2	2	2	2	2	2	2
Cap. veh/h	887	0	396	545	2300	0	0	3332	699	0	3332	699
Arrive On Green	0.25	0.00	0.25	0.32	1.00	0.00	0.00	0.44	0.00	0.00	0.44	0.00
Sat Flow, veh/h	3548	0	1583	3442	3632	0	0	7898	1583	0	7898	1583
Grp Volume(V), veh/h	69	0	35	399	612	0	0	399	0	0	399	0
Grp Sat Flow(S), veh/h/ln	1774	0	1583	1721	1770	0	0	1509	1583	0	1509	1583
Q Serve(Q_s), s	1.8	0.0	2.0	12.4	0.0	0.0	0.0	3.7	0.0	0.0	3.7	0.0
Cycle O Clear(c), s	1.8	0.0	2.0	12.4	0.0	0.0	0.0	3.7	0.0	0.0	3.7	0.0
Prop In Lane	1.00	1.00	1.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Lane Grp Cap(C), veh/h	887	0	396	545	2300	0	0	3332	699	0	3332	699
V/C Ratio(X)	0.08	0.00	0.09	0.73	0.27	0.00	0.00	0.12	0.00	0.00	0.12	0.00
Avail Cap(C-a), veh/h	887	0	396	545	2300	0	0	3332	699	0	3332	699
HCM Platoon Ratio	1.00	1.00	1.00	2.00	2.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	0.00	1.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Uniform Delay (d), s/veh	34.4	0.0	34.5	38.7	0.0	0.0	0.0	19.7	0.0	0.0	19.7	0.0
Incr Delay (d2), s/veh	0.2	0.0	0.4	8.4	0.3	0.0	0.0	0.1	0.0	0.0	0.1	0.0
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	0.9	0.0	0.9	6.5	0.1	0.0	0.0	1.6	0.0	0.0	1.6	0.0
LnGrp Delay(d),s/veh	34.6	0.0	35.0	47.2	0.3	0.0	0.0	19.8	0.0	0.0	19.8	0.0
LnGrp LOS	C		C	D	A		A	B			B	A
Approach Vol, veh/h			104				1011				399	
Approach Delay, s/veh			34.7				18.8				19.8	
Approach LOS			C				B				B	
Timer	1	2	3	4	5	6	7	8				
Assigned Phs	2			5	6		8					
Phs Duration (G+Y+Rc), s	84.0			25.0	59.0		36.0					
Change Period (Y+Rc), s	6.0			6.0	6.0		6.0					
Max Green Setting (Gmax), s	78.0			19.0	53.0		30.0					
Max O Clear Time (G_c+H1), s	2.0			14.4	5.7		4.0					
Green Ext Time (G_c), s	6.0			2.2	2.7		0.3					

Intersection Summary	202	
HCM 2010 CRT Delay	C	
HCM 2010 LOS	C	

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Synchro 9 Report
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Synchro 9 Report
Page 6

Phase Number	2	5	6	8
Movement	NBT	NBL	SBT	WBTL
Lead/Lag				
Lead/Lag Optimize				
Recall Mode	Max	Max	Max	Max
Maximum Spill (s)	84	25	59	36
Maximum Spill (%)	70.0%	20.8%	49.2%	30.0%
Minimum Spill (s)	36	10	36	36
Yellow Time (s)	4	4	4	4
All-Red Time (s)	2	2	2	2
Minimum Initial (s)	4	4	4	4
Minimum Extension (s)	3	3	3	3
Vehicle Extension (s)	3	3	3	3
Time Before Reduce (s)	0	0	0	0
Time To Reduce (s)	0	0	0	0
Walk Time (s)	5	5	5	5
Flash Dont Walk (s)	25	25	25	25
Dual Entry	Yes	No	Yes	Yes
Inhibit Max	Yes	Yes	Yes	Yes
Start Time (s)	50	109	50	14
End Time (s)	14	14	109	50
Yield/Force Off (s)	8	8	103	44
Yield/Force Off 170(s)	103	8	78	19
Local Start Time (s)	0	59	0	84
Local Yield 170(s)	78	78	53	114
Local Yield 170(s)	53	78	28	89

Intersection Summary	120	
Cycle Length	Prelim	
Natural Cycle	145	
Offset: 50 (42%), Referenced to phase 2:NBT and 6:SBT, Start of Green		

Spills and Phases:	2: Ellsworth Road & SR 24 WB Ramp(s)	
	84 s	36 s
	25 s	36 s
	59 s	25 s

HCM 2010 Signalized Intersection Summary

2035 PM.Syn

2035 PM.Syn

Timing Report, Sorted By Phase

3: Williams Field Road & SR 24 EB Ramp(s)

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	725	0	25	0	0	0	0	50	25	25	25	0
Traffic Volume (veh/h)	725	0	25	0	0	0	0	50	25	25	25	0
Future Volume (veh/h)	725	0	25	0	0	0	0	50	25	25	25	0
Number	7	4	14	0	0	0	1	6	16	5	2	12
Initial Q (Obt.) veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pb1)	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus. Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow, veh/h/ln	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863
Adj Flow Rate, veh/h	771	0	27	0	0	0	53	27	27	27	27	0
Adj No. of Lanes	2	0	1	0	0	0	3	1	1	1	2	0
Peak Hour Factor	0.94	0.94	0.94	0.90	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.90
Cap. veh/h	1804	0	805	0	1398	435	507	1386	0	0	1386	0
Arrive On Green	0.51	0.00	0.51	0.00	0.28	0.28	0.13	0.78	0.00	0.00	0.78	0.00
Sat Flow, veh/h	3548	0	1583	0	5253	1583	1774	3632	0	0	3632	0
Grp Volume(V), veh/h	771	0	27	0	0	53	27	27	27	27	27	0
Grp Sat Flow(S), veh/h/ln	1774	0	1583	0	1695	1583	1774	1770	0	0	1770	0
Q Serve(Q_s), s	16.4	0.0	1.0	0.0	0.9	1.5	0.0	0.2	0.0	0.0	0.2	0.0
Cycle O Clear(c), s	16.4	0.0	1.0	0.0	0.9	1.5	0.0	0.2	0.0	0.0	0.2	0.0
Prop In Lane	1.00	1.00	1.00	0.00	1.00	1.00	1.00	1.00	0.00	0.00	1.00	0.00
Lane Grp Cap(C), veh/h	1804	0	805	0	1398	435	507	1386	0	0	1386	0
V/C Ratio(X)	0.43	0.00	0.03	0.00	0.04	0.06	0.05	0.02	0.00	0.00	0.02	0.00
Avail Cap(C-a), veh/h	1804	0	805	0	1398	435	507	1386	0	0	1386	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	2.00	2.00	1.00	1.00	2.00	1.00
Upstream Filter(I)	1.00	0.00	1.00	0.00	1.00	1.00	1.00	1.00	0.00	0.00	1.00	0.00
Uniform Delay (d), s/veh	18.5	0.0	14.8	0.0	31.9	32.1	26.5	7.9	0.0	0.0	26.5	0.0
Incr Delay (d2), s/veh	0.7	0.0	0.1	0.0	0.1	0.3	0.2	0.0	0.0	0.0	0.2	0.0
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%),veh/ln	8.2	0.0	1.4	0.0	0.4	0.7	0.6	0.1	0.0	0.0	0.6	0.0
LnGrp Delay(d),s/veh	19.3	0.0	14.8	0.0	31.9	32.4	26.7	8.0	0.0	0.0	26.7	0.0
LnGrp LOS	B		B		C	C	C	A			C	A
Approach Vol, veh/h	798		19.1		80		80				54	
Approach Delay, s/veh	19.1		17.3		32.1		17.3				17.3	
Approach LOS	B		C		C		B				B	
Timer	1	2	3	4	5	6	7	8				
Assigned Phs	2			4	5	6						
Phs Duration (G+Y+Rc), s	53.0			67.0	14.0	39.0						
Change Period (Y+Rc), s	6.0			6.0	6.0	6.0						
Max Green Setting (Gmax), s	47.0			61.0	8.0	33.0						
Max O Clear Time (G_c+H1), s	2.2			18.4	2.0	3.5						
Green Ext Time (G_c), s	0.2			3.1	0.1	0.3						

Intersection Summary	201	
HCM 2010 CRT Delay	C	
HCM 2010 LOS	C	

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HCM 2010 Signalized Intersection Summary
4: Williams Field Road & SR 24 WB Ramp(s)

2035 PM.syn

	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	0	0	0	25	0	25	25	25	0	0	50	550
Traffic Volume (veh/h)	0	0	0	25	0	25	25	25	0	0	50	550
Future Volume (veh/h)	0	0	0	25	0	25	25	25	0	0	50	550
Number	0	0	0	3	8	18	5	2	12	1	6	16
Initial Q (Cb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A, pbT)	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow, veh/hln	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863
Adj Flow Rate, veh/h	35	0	18	27	2	0	0	0	53	585		
Adj No. of Lanes	2	0	1	1	2	0	0	0	3	1		
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Percent Heavy Veh, %	2	2	5	2	2	2	2	2	0	2	2	2
Cap, veh/h	887	0	385	548	2300	0	0	2882	897	897		
Arrive On Green	0.25	0.00	0.25	0.07	1.00	0.00	0.00	0.57	0.57	0.57		
Sat Flow, veh/h	3548	0	1538	1774	3632	0	0	5253	1583			
Grip Volume(V), veh/h	35	0	18	27	27	0	0	53	585			
Grip Sat Flow(S), veh/hln	1774	0	1538	1774	1770	0	0	1695	1583			
Q Serve(Q, s), s	0.9	0.0	1.1	0.0	0.0	0.0	0.0	0.5	30.5			
Cycle O Clear(q, c), s	0.9	0.0	1.1	0.0	0.0	0.0	0.0	0.5	30.5			
Prop In Lane	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
Lane Grp Cap(C), veh/h	887	0	385	548	2300	0	0	2882	897			
V/C Ratio(X)	0.04	0.00	0.05	0.05	0.01	0.00	0.00	0.02	0.65			
Avail Cap(C-a), veh/h	887	0	385	548	2300	0	0	2882	897			
HCM Platoon Ratio	1.00	1.00	1.00	1.00	2.00	1.00	1.00	1.00	1.00			
Upstream Filter(I)	1.00	0.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00			
Uniform Delay (d), s/veh	34.1	0.0	34.1	10.6	0.0	0.0	0.0	11.4	17.9			
Incr Delay (d2), s/veh	0.1	0.0	0.2	0.2	0.0	0.0	0.0	0.0	0.0	3.7		
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
%ile BackOfQ(50%), veh/ln	0.4	0.0	0.5	0.4	0.0	0.0	0.0	0.3	14.1			
LnGrp Delay(d), s/veh	34.2	0.0	34.4	10.8	0.0	0.0	0.0	11.4	21.5			
LnGrp LOS	C	C	C	B	A	A	A	B	C			
Approach Vol, veh/h				53			54		638			
Approach Delay, s/veh				34.2			5.4		20.7			
Approach LOS				C			A		C			
Timer	1	2	3	4	5	6	7	8				
Assigned Phs	2			5	6		8					
Phs Duration (G+Y+Rc), s	84.0			10.0	74.0		36.0					
Change Period (Y+Rc), s	6.0			6.0	6.0		6.0					
Max Green Setting (Gmax), s	78.0			4.0	68.0		30.0					
Max O Clear Time (Q_c+H1), s	2.0			2.0	32.5		3.1					
Green Ext Time (q_c), s	0.2			0.0	2.6		0.1					

Intersection Summary
HCM 2010 Ctrl Delay
HCM 2010 LOS

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Synchro 9 Report
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Timing Report, Sorted By Phase
4: Williams Field Road & SR 24 WB Ramp(s)

2035 PM.syn

Phase Number	2	5	6	8
Movement	NBTL	NBL	SBT	WBTL
Lead/Lag		Lag	Lead	
Recall Mode	Max	Max	Max	Max
Maximum Split (s)	84	10	74	36
Maximum Split (%)	70.0%	8.3%	61.7%	30.0%
Minimum Split (s)	36	10	36	36
Yellow Time (s)	4	4	4	4
All-Red Time (s)	2	2	2	2
Minimum Initial (s)	4	4	4	4
Vehicle Extension (s)	3	3	3	3
Minimum Gap (s)	3	3	3	3
Time Before Reduce (s)	0	0	0	0
Time To Reduce (s)	5	5	5	5
Walk Time (s)	5	5	5	5
Flash Dont Walk (s)	25	25	25	25
Dual Entry	Yes	No	Yes	Yes
Inhibit Max	Yes	Yes	Yes	Yes
Start Time (s)	0	74	0	84
End Time (s)	84	84	74	0
Yield/Force Off (s)	78	78	68	114
Yield/Force Off 170(s)	53	78	43	89
Local Start Time (s)	0	74	0	84
Local Yield (s)	78	78	68	114
Local Yield 170(s)	53	78	43	89



Intersection Summary
Cycle Length: 120
Control Type: Prelim
Natural Cycle: 85
Offset: 0 (0%), Referenced to phase 2/NBTL and 6/GBT, Start of Green

Spills and Phases: 4: Williams Field Road & SR 24 WB Ramp(s)
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HCM 2010 Signalized Intersection Summary
7: Signal Butte Road & SR 24 EB Ramp(s)

2035 PM.syn

	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	2	2	2	2	2	2	2	2	2	2	2	2
Traffic Volume (veh/h)	275	0	325	0	0	0	550	350	175	600	0	0
Future Volume (veh/h)	275	0	325	0	0	0	550	350	175	600	0	0
Number	7	4	14	0	0	0	6	16	5	2	12	0
Initial Q (Cb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A, pbT)	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow, veh/hln	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863
Adj Flow Rate, veh/h	409	0	222	0	0	0	585	372	186	638	0	0
Adj No. of Lanes	2	0	1	0	0	0	4	1	1	3	0	0
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Percent Heavy Veh, %	2	2	2	2	2	2	2	2	2	2	2	2
Cap, veh/h	946	0	422	0	0	0	2510	620	340	3221	0	0
Arrive On Green	0.27	0.00	0.27	0.00	0.00	0.39	0.39	0.38	1.00	0.00	0.00	0.00
Sat Flow, veh/h	3548	0	1583	0	0	6669	1583	1774	5253	0	0	0
Grip Volume(V), veh/h	409	0	222	0	0	585	372	186	638	0	0	0
Grip Sat Flow(S), veh/hln	1774	0	1583	0	0	1602	1583	1774	1695	0	0	0
Q Serve(Q, s), s	11.5	0.0	14.4	0.0	0.0	7.3	22.4	9.8	0.0	0.0	0.0	0.0
Cycle O Clear(q, c), s	11.5	0.0	14.4	0.0	0.0	7.3	22.4	9.8	0.0	0.0	0.0	0.0
Prop In Lane	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Lane Grp Cap(C), veh/h	946	0	422	0	0	2510	620	340	3221	0	0	0
V/C Ratio(X)	0.43	0.00	0.53	0.00	0.00	0.23	0.60	0.55	0.20	0.00	0.00	0.00
Avail Cap(C-a), veh/h	946	0	422	0	0	2510	620	340	3221	0	0	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	0.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Uniform Delay (d), s/veh	36.5	0.0	37.5	0.0	0.0	24.4	29.0	32.9	0.0	0.0	0.0	0.0
Incr Delay (d2), s/veh	1.4	0.0	4.6	0.0	0.0	0.2	4.3	6.2	0.1	0.0	0.0	0.0
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%), veh/ln	5.8	0.0	13.3	0.0	0.0	3.3	10.5	5.3	0.0	0.0	0.0	0.0
LnGrp Delay(d), s/veh	37.9	0.0	42.2	0.0	0.0	24.7	33.3	39.1	0.1	0.0	0.0	0.0
LnGrp LOS	D	D	D	C	C	C	D	A	C	D	A	A
Approach Vol, veh/h	631			957			824					
Approach Delay, s/veh	39.4			28.0			8.9					
Approach LOS	D			C			A					
Timer	1	2	3	4	5	6	7	8				
Assigned Phs	2			4	5	6						
Phs Duration (G+Y+Rc), s	82.0			38.0	29.0	53.0						
Change Period (Y+Rc), s	6.0			6.0	6.0	6.0						
Max Green Setting (Gmax), s	76.0			32.0	23.0	47.0						
Max O Clear Time (Q_c+H1), s	2.0			16.4	11.8	24.4						
Green Ext Time (q_c), s	5.1			2.0	3.4	5.1						

Intersection Summary
HCM 2010 Ctrl Delay
HCM 2010 LOS

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Timing Report, Sorted By Phase
7: Signal Butte Road & SR 24 EB Ramp(s)

2035 PM.syn

Phase Number	2	4	5	6
Movement	SBT	EBTL	SBL	NBT
Lead/Lag		Lag	Lead	
Recall Mode	Max	Max	Max	Max
Maximum Split (s)	82	38	29	53
Maximum Split (%)	68.3%	31.7%	24.2%	44.2%
Minimum Split (s)	36	36	10	36
Yellow Time (s)	4	4		

HCM 2010 Signalized Intersection Summary

2035 PM.Syn

Timing Report, Sorted By Phase
8: Signal Butte Road & SR 24 WB Ramp(s)

2035 PM.Syn

Movement	EBL	EBT	EBr	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBR
Lane Configurations											
Traffic Volume (veh/h)	0	0	0	225	0	225	50	500	0	0	775
Future Volume (veh/h)	0	0	0	225	0	225	50	500	0	0	775
Number				3	8	18	5	2	12	1	6
Initial Q (Cb) veh				0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)				1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus. Adj				1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow (veh/h)	1863	1863	1863	1863	1863	1863	0	0	1863	1863	
Adj Flow Rate, veh/h	313	0	159	53	532	0	0	824	53		
Adj No. of Lanes	2	0	1	2	2	0	0	4	1		
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.90	0.90	0.94	0.94	
Percent Heavy Veh. %				2	2	2	2	2	0	2	
Cap. veh/h	1331	0	594	315	1868	0	0	2456	607		
Arrive On Green	0.38	0.00	0.38	0.18	1.00	0.00	0.00	0.38	0.38		
Sat Flow, veh/h	3548	0	1583	3442	3632	0	0	6669	1583		
Grp Volume(V), veh/h	313	0	159	53	532	0	0	824	53		
Grp Sat Flow(S), veh/h/m	1774	0	1583	1721	1770	0	0	1602	1583		
Q Serve(Q_s), s	7.3	0.0	8.4	1.6	0.0	0.0	0.0	10.9	2.6		
Cycle Q Clear(q_c), s	7.3	0.0	8.4	1.6	0.0	0.0	0.0	10.9	2.6		
Prop In Lane	1.00	1.00	1.00	1.00	1.00	0.00	0.00	1.00	1.00		
Lane Grp Cap(c), veh/h	1331	0	594	315	1868	0	0	2456	607		
V/C Ratio(X)	0.24	0.00	0.27	0.17	0.29	0.00	0.00	0.34	0.09		
Avail Cap(c_a), veh/h	1331	0	594	315	1868	0	0	2456	607		
HCM Platoon Ratio	1.00	1.00	1.00	2.00	2.00	1.00	1.00	1.00	1.00		
Upstream Filter(i)	1.00	0.00	1.00	1.00	1.00	0.00	0.00	1.00	1.00		
Uniform Delay (d), s/veh	25.7	0.0	26.1	45.1	0.0	0.0	0.0	26.2	23.6		
Incr Delay (d2), s/veh	0.4	0.0	1.1	1.1	0.4	0.0	0.0	0.4	0.3		
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
%ile BackOfQ(50%), veh/in	3.6	0.0	3.8	0.8	0.1	0.0	0.0	4.9	1.2		
LnGrp Delay(d), s/veh	26.1	0.0	27.2	46.3	0.4	0.0	0.0	26.6	23.9		
LnGrp LOS	C	C	C	D	A	A	C	C	C	C	

Approach Vol, veh/h	472	585	877
Approach Delay, s/veh	26.5	4.5	26.4
Approach LOS	C	A	C
Timer	1	2	3
Assigned Phs	2	5	6
Phs Duration (G+Y+Rc), s	69.0	17.0	52.0
Change Period (Y+Rc), s	6.0	6.0	6.0
Max Green Setting (Gmax), s	63.0	11.0	46.0
Max Q Clear. Time (Q_c+H1), s	2.0	3.6	12.9
Green Ext Time (g_e), s	3.8	2.0	6.1

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Phase Number	2	5	6	8
Movement	NBT	SBT	WBTL	
Lead/Lag		Lag	Lead	
Recall Mode	Max	Max	Max	Max
Maximum Split (%)	69	17	52	51
Minimum Split (%)	57.5%	14.2%	43.3%	42.5%
Yellow Time (s)	3.6	10	3.6	3.6
All-Red Time (s)	4	4	4	4
Minimum Initial (s)	4	4	4	4
Vehicle Extension (s)	3	3	3	3
Minimum Gap (s)	3	3	3	3
Time Before Reduce (s)	0	0	0	0
Time To Reduce (s)	5	0	0	0
Walk Time (s)	5	5	5	5
Flash Dont Walk (s)	25	25	25	25
Inhibit Max	Yes	No	Yes	Yes
Start Time (s)	0	52	0	69
End Time (s)	69	69	52	0
Yield/Force Off (s)	63	63	46	114
Yield/Force Off 170(s)	38	63	21	89
Local Start Time (s)	0	52	0	69
Local Yield 170(s)	63	63	46	114
Local Yield 170(s)	38	63	21	89

Spills and Phases: 8: Signal Butte Road & SR 24 WB Ramp(s)

02 (R)	59 s
05 (R)	52 s
05 (R)	17 s

CivTech
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Intersection Summary

Cycle Length	120
Control Type	Prelimed
Natural Cycle	85
Offset: 0 (0%), Referenced to phase 2/NBT and 6/SBT, Start of Green	

Spills and Phases: 9: Meridian Road & SR 24 EB Ramp(s)

02 (R)	70 s
05 (R)	50 s
05 (R)	24 s

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HCM 2010 Signalized Intersection Summary

2035 PM.Syn

Timing Report, Sorted By Phase
9: Meridian Road & SR 24 EB Ramp(s)

2035 PM.Syn

Movement	EBL	EBT	EBr	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBR
Lane Configurations											
Traffic Volume (veh/h)	200	0	1825	0	0	0	0	1625	225	50	300
Future Volume (veh/h)	200	0	1825	0	0	0	0	1625	225	50	300
Number	7	4	14	0	0	0	1	6	16	5	2
Initial Q (Cb) veh	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus. Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow (veh/h)	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863	1863
Adj Flow Rate, veh/h	213	0	0	0	0	1729	239	53	319	0	
Adj No. of Lanes	2	0	1	0	0	4	1	2	2	0	
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.90
Percent Heavy Veh. %											
Cap. veh/h	1301	0	581	0	0	2296	567	595	1888	0	
Arrive On Green	0.37	0.00	0.00	0.00	0.36	0.36	0.25	1.00	0.00	0.00	
Sat Flow, veh/h	3548	0	1583	0	0	6669	1583	3442	3632	0	
Grp Volume(V), veh/h	213	0	0	0	1729	239	53	319	0		
Grp Sat Flow(S), veh/h/m	1774	0	1583	0	0	1602	1583	1721	1770	0	
Q Serve(Q_s), s	4.9	0.0	0.0	0.0	28.5	13.7	0.0	0.0	0.0	0.0	
Cycle Q Clear(q_c), s	4.9	0.0	0.0	0.0	28.5	13.7	0.0	0.0	0.0	0.0	
Prop In Lane	1.00	1.00	1.00	0.00	1.00	1.00	1.00	1.00	1.00	0.00	
Lane Grp Cap(c), veh/h	1301	0	581	0	2296	567	595	1888	0		
V/C Ratio(X)	0.16	0.00	0.00	0.00	0.75	0.42	0.09	0.17	0.00		
Avail Cap(c_a), veh/h	1301	0	581	0	2296	567	595	1888	0		
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	2.00	2.00	2.00	1.00		
Upstream Filter(i)	1.00	0.00	0.00	0.00	1.00	1.00	1.00	1.00	1.00	0.00	
Uniform Delay (d), s/veh	25.6	0.0	0.0	0.0	33.8	29.1	34.1	0.0	0.0		
Incr Delay (d2), s/veh	0.3	0.0	0.0	0.0	2.3	2.3	0.3	0.2	0.0		
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
%ile BackOfQ(50%), veh/in	2.4	0.0	0.0	0.0	13.0	6.3	0.7	0.1	0.0		
LnGrp Delay(d), s/veh	25.9	0.0	0.0	0.0	36.2	31.4	34.4	0.2	0.0		
LnGrp LOS	C	C	C	D	C	C	C	A	A		

Approach Vol, veh/h	213	1968	372
Approach Delay, s/veh	25.9	35.6	5.1
Approach LOS	C	D	A
Timer	1	2	3
Assigned Phs	2	4	5
Phs Duration (G+Y+Rc), s	70.0	50.0	21.0
Change Period (Y+Rc), s	6.0	6.0	6.0
Max Green Setting (Gmax), s	64.0	44.0	15.0
Max Q Clear. Time (Q_c+H1), s	2.0	6.9	2.0
Green Ext Time (g_e), s	2.2	0.7	1.6

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Intersection Summary

Cycle Length	120
Control Type	Prelimed
Natural Cycle	145
Offset: 0 (0%), Referenced to phase 2/SBT and 6/NBT, Start of Green	

Spills and Phases: 9: Meridian Road & SR 24 EB Ramp(s)

02 (R)	70 s
05 (R)	50 s
05 (R)	24 s

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HCM 2010 Signalized Intersection Summary
 10: Meridian Road & SR 24 WB Ramp(s)

2035 PM.Syn

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBR
Lane Configurations											
Traffic Volume (veh/h)	0	0	0	25	0	50	700	925	0	0	350
Future Volume (veh/h)	0	0	0	25	0	50	700	925	0	0	350
Number				3	8	18	5	2	12	1	6
Initial Q (Ob), veh				0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pb1)				1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus, Adj				1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow, veh/h	1863	1863	1863	1863	1863	1863	0	0	1863	1863	
Adj Flow Rate, veh/h	27	0	53	745	984	0	0	372	0	4	
Adj No. of Lanes	1	0	2	2	2	2	0	0	0	4	
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.90	0.90	0.94	0.94	
Percent Heavy Veh. %	2	2	2	2	2	2	0	0	0	2	
Cap. veh/h	384	0	686	1463	2418	0	0	1335	330	0	
Arrive On Green	0.22	0.00	0.22	0.85	1.00	0.00	0.00	0.21	0.00	0.00	
Sat Flow, veh/h	1774	0	3167	3442	3632	0	0	6669	1583	0	
Grip Volume(v), veh/h	27	0	53	745	984	0	0	372	0	4	
Grip Sat Flow(s), veh/h	1774	0	1583	1721	1770	0	0	1602	1583	0	
Q Serve(Q_s), s	1.5	0.0	1.6	6.9	0.0	0.0	0.0	5.9	0.0	0.0	
Cycle O Clear(q_c), s	1.5	0.0	1.6	6.9	0.0	0.0	0.0	5.9	0.0	0.0	
Prop In Lane	1.00	1.00	1.00	1.00	1.00	0.00	0.00	1.00	1.00	1.00	
Lane Grp Cap(c), veh/h	384	0	686	1463	2418	0	0	1335	330	0	
V/C Ratio(X)	0.07	0.00	0.08	0.51	0.41	0.00	0.00	0.28	0.00	0.00	
Avail Cap(c-a), veh/h	384	0	686	1463	2418	0	0	1335	330	0	
HCM Platoon Ratio	1.00	1.00	1.00	2.00	2.00	1.00	1.00	1.00	1.00	1.00	
Upstream Filter(i)	1.00	0.00	1.00	1.00	1.00	0.00	0.00	1.00	0.00	1.00	
Uniform Delay (d), s/veh	37.4	0.0	37.4	5.7	0.0	0.0	0.0	39.9	0.0	0.0	
Incr Delay (d2), s/veh	0.4	0.0	0.2	1.3	0.5	0.0	0.0	0.5	0.0	0.0	
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
%ile BackOfQ(50%), veh/h	0.8	0.0	0.7	3.4	0.2	0.0	0.0	2.6	0.0	0.0	
LnGrip Delay(d), s/veh	37.7	0.0	37.7	7.0	0.5	0.0	0.0	40.4	0.0	0.0	
LnGrip LOS	D	D	D	A	A	A	A	D	D	D	
Approach Vol, veh/h	80			1779			372			40.4	
Approach Delay, s/veh	37.7			3.3			A			D	
Approach LOS	D			A			A			D	
Timer	1	2	3	4	5	6	7	8			
Assigned Phs	2			5	6			8			
Phs Duration (G+Y+Rc), s	88.0			57.0	31.0			32.0			
Change Period (Y+Rc), s	6.0			6.0	6.0			6.0			
Max Green Setting (Gmax), s	82.0			51.0	25.0			26.0			
Max O Clear Time (q_c+H), s	2.0			8.9	7.9			3.6			
Green Ext Time (q_c), s	13.4			12.5	2.0			0.2			

Intersection Summary
 HCM 2010 Ctrl Delay 10.9
 HCM 2010 LOS B

Notes:
 10: Meridian Road & SR 24 WB Ramp(s)

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Timing Report, Sorted By Phase
 10: Meridian Road & SR 24 WB Ramp(s)

2035 PM.Syn

Phase Number	2	5	6	8
Movement	NBT	NBL	SBT	WBTL
Lead/Lag	Lag	Lead		
Recall Mode	Max	Max	Max	Max
Maximum Split (s)	88	57	31	32
Maximum Split (%)	73.3%	47.5%	25.8%	26.7%
Minimum Split (s)	36	10	36	36
Yellow Time (s)	4	4	4	4
All-Red Time (s)	2	2	2	2
Minimum Initial (s)	4	4	4	4
Vehicle Extension (s)	3	3	3	3
Minimum Gap (s)	3	3	3	3
Time Before Reduce (s)	0	0	0	0
Time To Reduce (s)	5	0	0	0
Walk Time (s)	5	5	5	5
Flash Dont Walk (s)	25	25	25	25
Inhibit Max	Yes	No	Yes	Yes
Inhibit Min	Yes	Yes	Yes	Yes
Start Time (s)	0	31	0	88
End Time (s)	88	88	31	0
Yield/Force Off (s)	82	82	25	114
Yield/Force Off 170(s)	57	82	0	89
Local Start Time (s)	0	31	0	88
Local Yield (s)	82	82	25	114
Local Yield 170(s)	57	82	0	89

Intersection Summary
 Cycle Length 120
 Control Type Prelimined
 Natural Cycle 95
 Offset: 0 (0%), Referenced to phase 2:NBT and 6:SBT, Start of Green

Splits and Phases: 10: Meridian Road & SR 24 WB Ramp(s)

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HCM 2010 Signalized Intersection Summary
 11: Ironwood Road & SR 24 EB Ramp(s)

2035 PM.Syn

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Volume (veh/h)	75	1000	0	1350	625	0
Future Volume (veh/h)	75	1000	0	1350	625	0
Number	7	14	1	6	2	12
Initial Q (Ob), veh	0	0	0	0	0	0
Ped-Bike Adj(A_pb1)	1.00	1.00	1.00	1.00	1.00	1.00
Parking Bus, Adj	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow, veh/h	1863	1863	0	1863	1863	0
Adj Flow Rate, veh/h	80	1064	0	1436	665	0
Adj No. of Lanes	1	2	0	4	2	0
Peak Hour Factor	0.94	0.94	0.94	0.94	0.90	0.90
Percent Heavy Veh. %	10.20	18.21	0	20.83	11.50	0
Cap. veh/h	0.57	0.57	0.00	0.32	0.65	0.00
Arrive On Green	1774	3167	0	6929	3725	0
Sat Flow, veh/h	80	1064	0	1436	665	0
Grip Volume(v), veh/h	1774	1583	0	1602	1770	0
Grip Sat Flow(s), veh/h	2.4	25.8	0.0	23.4	12.6	0.0
Q Serve(Q_s), s	2.4	25.8	0.0	23.4	12.6	0.0
Cycle O Clear(q_c), s	1.00	1.00	0.00	2.083	11.50	0.00
Prop In Lane	1.00	1.00	0.00	1.00	1.00	1.00
Lane Grp Cap(c), veh/h	1020	1821	0	2083	1150	0
V/C Ratio(X)	0.08	0.58	0.00	0.69	0.58	0.00
Avail Cap(c-a), veh/h	1020	1821	0	2083	1150	0
HCM Platoon Ratio	1.00	1.00	1.00	2.00	2.00	1.00
Upstream Filter(i)	1.00	1.00	0.00	1.00	1.00	0.00
Uniform Delay (d), s/veh	11.3	16.3	0.0	35.2	16.4	0.0
Incr Delay (d2), s/veh	0.2	1.4	0.0	1.9	2.1	0.0
Initial Q Delay(d3), s/veh	0.0	0.0	0.0	0.0	0.0	0.0
%ile BackOfQ(50%), veh/h	1.2	11.6	0.0	10.6	6.4	0.0
LnGrip Delay(d), s/veh	11.5	17.7	0.0	37.1	18.5	0.0
LnGrip LOS	B	B	D	B	B	B
Approach Vol, veh/h	1144		1436		665	
Approach Delay, s/veh	17.3		37.1		18.5	
Approach LOS	B		D		B	
Timer	1	2	3	4	5	6
Assigned Phs	2			4		6
Phs Duration (G+Y+Rc), s	45.0			75.0		45.0
Change Period (Y+Rc), s	6.0			6.0		6.0
Max Green Setting (Gmax), s	39.0			69.0		39.0
Max O Clear Time (q_c+H), s	14.6			27.8		25.4
Green Ext Time (q_c), s	15.6			5.5		10.2

Intersection Summary
 HCM 2010 Ctrl Delay 26.3
 HCM 2010 LOS C

Notes:
 11: Ironwood Road & SR 24 EB Ramp(s)

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Timing Report, Sorted By Phase
 11: Ironwood Road & SR 24 EB Ramp(s)

2035 PM.Syn

Phase Number	2	4	6
Movement	SBT	EBL	NBT
Lead/Lag			
Recall Mode	Max	Max	Max
Maximum Split (s)	45	75	45
Maximum Split (%)	37.5%	62.5%	37.5%
Minimum Split (s)	36	36	36
Yellow Time (s)	4	4	4
All-Red Time (s)	2	2	2
Minimum Initial (s)	4	4	4
Vehicle Extension (s)	3	3	3
Minimum Gap (s)	3	3	3
Time Before Reduce (s)	0	0	0
Time To Reduce (s)	5	5	5
Walk Time (s)	5	5	5
Flash Dont Walk (s)	25	25	25
Dual Entry	Yes	Yes	Yes
Inhibit Max	Yes	Yes	Yes
Start Time (s)	0	45	0
End Time (s)	45	0	45
Yield/Force Off (s)	39	114	39
Yield/Force Off 170(s)	14	89	14
Local Start Time (s)	0	45	0
Local Yield (s)	39	114	39
Local Yield 170(s)	14	89	14

Intersection Summary
 Cycle Length 120
 Control Type Prelimined
 Natural Cycle 75
 Offset: 0 (0%), Referenced to phase 2:SBT and 6:NBT, Start of Green

Splits and Phases: 11: Ironwood Road & SR 24 EB Ramp(s)

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**FINAL DESIGN CONCEPT REPORT
SR-24, Ellsworth Road to Ironwood Drive
Interim Phase II**

APPENDIX F – PAVEMENT MEMO



MEMORANDUM

TO: Sam Elters, Parsons

DATE: 02/09/16

FROM: Sohila Bemanian, Parsons

PHONE: (775) 297-6515

SUBJECT: **State Route 24 Interim- Pavement Design –Rev.1**

This intent of this memorandum is to provide recommendations on the selection of the preferred alternative based on the life cycle cost analysis (LCCA) for State Route (SR) 24 Interim Project.

1) Introduction

The pavement design for SR 24 Interim Project used the following information for the analysis:

- Final Design Concept Report (DCR) Vol. 1 (April 2011)
- Traffic Analysis Report dated January 2016 provided by CivTech
- ADOT’s Preliminary Engineering and Design Manual (Third Edition 1989)
- Development of a Traffic Data Input System in Arizona for the MEPDG (October 2013)
- The American Association of State Highway and Transportation Officials (AASHTO) 93 Design Guide
- DARWin 3.1 Software

2) Pavement Design

The design inputs used to calculate pavement thicknesses are presented in Table1.

Table 1: Pavement Design Inputs for DARWin 3.1

Design Input	Flexible Pavement	Rigid Pavement
Initial Serviceability	4.2	4.2
Terminal Serviceability	2.8	2.8
Reliability	99%	99%
Overall Standard Deviation	0.35	0.25
Roadbed Resilient Modulus	13,000 psi	-
Structural Coefficients and Moduli	HMA- 0.44 (450,000 psi) AB- 0.14 (28,000 psi)	-
Drainage Coefficient	1.00	1.1
28-day Mean PCC Modulus of Rupture	-	670 psi
28-day Mean Elastic Modulus of Slab	-	4,000,000 psi
Mean Effective k-value	-	613 psi/in
Load Transfer Coefficient, J	-	2.8

3) Subgrade

Based on the review of DCR report, the subgrade materials along the project alignment generally consist of predominantly finer-grained, moderately firm to hard, lenticular alluvial deposits containing varying proportions of sand, silt, clay, and gravel. The finer grained silty and clayey deposits vary from low to medium in plasticity whereas the cleaner sand with gravel layers is typically non-plastic.

It is assumed that an average of 24” of embankment fill will be used throughout the project. The embankment fill is assumed to be classified as Soil A7-6 with modulus value of 13,000 psi.

4) Traffic Loading-18-kip Equivalent Single Axle Loading (ESALs)

The traffic information provided by CivTech is presented in Table 2. Since Option A has higher traffic than Option B, this option was used to calculate the 10-year, 20-year, and 30-year ESALs.

The design ESALs was based on traffic from SR 24 Ellsworth Road to Signal Butte Road.

ID	SR 24 Segment	2025 Option A		Total ADT
		EB AADT	WB AADT	
1	SR 24 Loop 202 to Ellsworth Road	41388	42609	
2	SR 24 Ellsworth Road to Williams Field Road	15111	16203	31,314
3	SR 24 Williams Field Road to Signal Butte Road	15111	16203	31,314
4	SR 24 Signal Butte Road to Meridian Road	9099	9624	18,723
5	SR 24 Meridian Road to Ironwood Drive	9099	9624	18,723

The following assumptions were used to calculate the 10-yr., 20-yr., and 30-yr. ESALs.

Parameters	Value	Additional Input
Growth Factor	4.60%	
%Truck	7%	
Light Truck	5%	0.8 (ESAL/ Truck)
Heavy Truck	2%	1.2 (ESAL/ Truck)

The calculated 10, 20, and 30 year ESALs are 4,394,712, 11,38349, and 21,583,996 respectively. See Attachment A for ESALs Calculations.

5) New Pavement Thickness Design

The following alternatives were analyzed for the project and life-cycle cost analysis (LCCA).

- 10-year Flexible Pavement followed by 30-yr. JPCP for the Ultimate Configurations
- 20-year Flexible Pavement followed by 30-yr. JPCP for the Ultimate Configurations
- 30-year Rigid Pavement

Pavement sections were designed using DARWin software and design input values from Table 1 (See Attachment A for design outputs). Table 3 present the calculated thicknesses.

Table 3: Pavement Thickness for Alternatives

	Alternative I	Alternative II	Alternative III
	10-year Flexible	20-year Flexible	30-year Rigid
Pavement Structural Section	1.0" AR-ACFC 6" HMA 8" AB	1.0" AR-ACFC 7.5" HMA 9" AB	1" AR-ACFC 11" JPCP 4" AB

AR-ACFC (Asphalt rubber –asphalt friction course)
HMA-Hotmix asphalt
AB-Aggregate Base-Class II

6) Life Cycle Cost Analysis

A LCCA was conducted to determine the preferred pavement alternative based on the lowest LCCA. The LCCA analyses are in Attachment B. A summary of LCCA results are presented in Table 4.

Table 4: Summary of Pavement Alternative Initial Costs and LCCA

	Initial Cost (per lane-mile)	LCCA (per lane-mile)	Preferred Option based on LCCA
Option1: 30-year JPCP	\$337,660.55	\$386,179.40	#1
Option 2: 10-year HMA	\$243,078.99	\$497,622.20	#3
Option 3: 20-year HMA	\$289,833.59	\$494,909.50	#2

A ten year flexible pavement section provides the lowest initial construction cost, however it has the highest LCCA. The 30-year JPCP provides the lowest LCCA and has the highest initial cost.

7) Recommendations

Due to uncertainty about the construction timing of Ultimate Configurations, it is recommended to use a 30-year JPCP that will optimize available agency resources, while minimizing user cost.

The following considerations are suggested to reduce initial cost to allow for use of 30-yr. JPCP:

- 1) Use MEPDG for pavement design analysis to reduce JPCP thickness design. Based on our experience with running this program, the proposed thickness can be reduced by 1.5" to 2".
- 2) Place reduced HMA shoulder for the interim project
- 3) Use reduced HMA for cross roads and ramps
- 4) Consider not using AR-ACFC on the HMA section

Attachment A: Design Output

DARWin Pavement Design and Analysis System

A Proprietary AASHTOWare
Computer Software Product
Parsons

Flexible Structural Design Module SR

24 from Ellsworth to Signal Butte Road -10 Year Design

Flexible Structural Design

18-kip ESALs Over Initial Performance Period	4,684,105
Initial Serviceability	4.2
Terminal Serviceability	2.8
Reliability Level	99 %
Overall Standard Deviation	0.35
Roadbed Soil Resilient Modulus	13,000 psi
Stage Construction	1
Calculated Design Structural Number	4.16 in

Simple ESAL Calculation

Performance Period (years)	10
Two-Way Traffic (ADT)	31,314
Number of Lanes in Design Direction	2
Percent of All Trucks in Design Lane	100 %
Percent Trucks in Design Direction	50 %
Percent Heavy Trucks (of ADT) FHWA Class 5 or Greater	- %
Average Initial Truck Factor (ESALs/truck)	-
Annual Truck Factor Growth Rate	- %
Annual Truck Volume Growth Rate	- %
Growth	Simple
Total Calculated Cumulative ESALs	- *

*Note: This value is not represented by the inputs or an error occurred in calculation.

Rigorous ESAL Calculation

Performance Period (years)	10
Two-Way Traffic (ADT)	31,314
Number of Lanes in Design Direction	2
Percent of All Trucks in Design Lane	100 %
Percent Trucks in Design Direction	50 %

Vehicle Class	Percent of ADT	Annual % Growth	Average Initial Truck Factor (ESALs/Truck)	Annual % Growth in Truck Factor	Accumulated 18-kip ESALs over Performance Period
1	93	4.6	0.0008	1	53,827

Vehicle Class	Percent of ADT	Annual % Growth	Average Initial Truck Factor (ESALs/Truck)	Annual % Growth in Truck Factor	Accumulated 18-kip ESALs over Performance Period
5	5	4.6	0.8	1	2,893,924
7	2	4.6	1.2	1	1,736,354
Total	100	-	-	-	4,684,105

Growth Simple
Total Calculated Cumulative ESALs 4,684,105

Layered Thickness Design

Thickness precision Nearest 0.5 in

Layer	Material Description	Struct Coef. (Ai)	Drain Coef. (Mi)	Spec Thickness (Di)(in)	Min Thickness (Di)(in)	Elastic Modulus (psi)	Width (ft)	Calculated Thickness (in)	Calculated SN (in)
1	HMA	0.44	1	-	-	400,000	-	7.00	3.08
2	GBC	0.14	1	-	-	28,000	-	8.00	1.12
Total	-	-	-	-	-	-	-	15.00	4.20

1993 AASHTO Pavement Design DARWin Pavement Design and Analysis System

A Proprietary AASHTOWare
Computer Software Product
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Flexible Structural Design Module

SR 24 from Ellsworth to Signal Butte Road -20 Year Design

Flexible Structural Design

18-kip ESALs Over Initial Performance Period	11,765,226
Initial Serviceability	4.2
Terminal Serviceability	2.8
Reliability Level	99 %
Overall Standard Deviation	0.35
Roadbed Soil Resilient Modulus	13,000 psi
Stage Construction	1
Calculated Design Structural Number	4.82 in

Simple ESAL Calculation

Performance Period (years)	20
Two-Way Traffic (ADT)	31,314
Number of Lanes in Design Direction	2
Percent of All Trucks in Design Lane	100 %
Percent Trucks in Design Direction	50 %
Percent Heavy Trucks (of ADT) FHWA Class 5 or Greater	- %
Average Initial Truck Factor (ESALs/truck)	-
Annual Truck Factor Growth Rate	- %
Annual Truck Volume Growth Rate	- %
Growth	Simple
Total Calculated Cumulative ESALs	- *

*Note: This value is not represented by the inputs or an error occurred in calculation.

Rigorous ESAL Calculation

Performance Period (years)	20
Two-Way Traffic (ADT)	31,314
Number of Lanes in Design Direction	2
Percent of All Trucks in Design Lane	100 %
Percent Trucks in Design Direction	50 %

Vehicle Class	Percent of ADT	Annual % Growth	Average Initial Truck Factor (ESALs/Truck)	Annual % Growth in Truck Factor	Accumulated 18-kip ESALs over Performance Period
1	93	4.6	0.0008	1	135,199

APPENDIX F
PAVEMENT MEMO

Vehicle Class	Percent of ADT	Annual % Growth	Average Initial Truck Factor (ESALs/Truck)	Annual % Growth in Truck Factor	18-kip ESALs over Performance Period
5	5	4.6	0.8	1	7,268,767
7	2	4.6	1.2	1	4,361,260
Total	100	-	-	-	11,765,226

Growth Simple
Total Calculated Cumulative ESALs 11,765,226

Layered Thickness Design

Thickness precision Nearest 0.5 in

Layer	Material Description	Struct Coef. (Ai)	Drain Coef. (Mi)	Spec Thickness (Di)(in)	Min Thickness (Di)(in)	Elastic Modulus (psi)	Width (ft)	Calculated Thickness (in)	Calculated SN (in)
1	HMA	0.44	1	-	-	400,000	-	8.50	3.74
2	GBC	0.14	1	-	-	28,000	-	9.00	1.26
Total	-	-	-	-	-	-	-	17.50	5.00

APPENDIX F
PAVEMENT MEMO

1993 AASHTO Pavement Design DARWin Pavement Design and Analysis System

A Proprietary AASHTOWare
Computer Software Product
Parsons

Rigid Structural Design Module

SR-24 from Ellsworth to Signal Butte Road 30-yr. Design

Rigid Structural Design

Pavement Type	JPCP
18-kip ESALs Over Initial Performance Period	21,583,996
Initial Serviceability	4.2
Terminal Serviceability	2.8
28-day Mean PCC Modulus of Rupture	670 psi
28-day Mean Elastic Modulus of Slab	4,000,000 psi
Mean Effective k-value	613 psi/in
Reliability Level	99 %
Overall Standard Deviation	0.25
Load Transfer Coefficient, J	2.8
Overall Drainage Coefficient, Cd	1
Calculated Design Thickness	10.67 in

Effective Modulus of Subgrade Reaction

Period	Description	Roadbed Soil Resilient Modulus (psi)	Base Elastic Modulus (psi)
1	-	13,000	28,000
Base Type	Agg. Base		
Base Thickness	4 in		
Depth to Bedrock	20 ft		
Projected Slab Thickness	9 in		
Loss of Support Category	0		
Effective Modulus of Subgrade Reaction	613 psi/in		

Simple ESAL Calculation

Performance Period (years)	30
Two-Way Traffic (ADT)	31,314
Number of Lanes in Design Direction	2
Percent of All Trucks in Design Lane	100 %
Percent Trucks in Design Direction	50 %
Percent Heavy Trucks (of ADT) FHWA Class 5 or Greater	- %
Average Initial Truck Factor (ESALs/truck)	-
Annual Truck Factor Growth Rate	- %
Annual Truck Volume Growth Rate	- %

Growth Simple

Total Calculated Cumulative ESALs - *

*Note: This value is not represented by the inputs or an error occurred in calculation.

Rigorous ESAL Calculation

Performance Period (years) 30
 Two-Way Traffic (ADT) 31,314
 Number of Lanes in Design Direction 2
 Percent of All Trucks in Design Lane 100 %
 Percent Trucks in Design Direction 50 %

Vehicle Class	Percent of ADT	Annual % Growth	Average Initial Truck Factor (ESALs/Truck)	Annual % Growth in Truck Factor	Accumulated 18-kip ESALs over Performance Period
1	93	4.6	0.0008	1	248,031
5	5	4.6	0.8	1	13,334,978
9	2	4.6	1.2	1	8,000,987
Total	100	-	-	-	21,583,996

Growth Simple

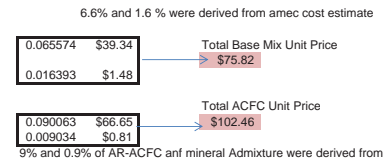
Total Calculated Cumulative ESALs 21,583,996

Attachment B: Life Cycle Cost Analysis

APPENDIX F
PAVEMENT MEMO

PAVEMENT STRUCTURE COST ESTIMATE
SR 24 - SR 202L to Ellsworth Road
TRACS No. MA 024 000 H6867 01C

ITEM NO	ITEM DESCRIPTION	UNIT MEASURE	UNIT PRICE
2020029	REMOVAL OF ASPHALTIC CONCRETE PAVEMENT	SQ.YD.	\$4.00
2020081	REMOVAL OF BITUMINOUS PAVEMENT (MILLING)(1")	SQ.YD.	\$2.00
3030022	AGGREGATE BASE, CLASS 2	CU.YD.	\$23.00
4010010	PORTLAND CEMENT CONCRETE PAVEMENT(10")	SQ.YD.	\$39.00
4010011	PORTLAND CEMENT CONCRETE PAVEMENT(11")	SQ.YD.	\$40.00
4010013	PORTLAND CEMENT CONCRETE PAVEMENT(13")	SQ.YD.	\$43.00
4010040	PORTLAND CEMENT CONCRETE PAVEMENT (REINFORCED) (10")	SQ.YD.	\$100.00
4040111	BITUMINOUS TACK COAT	TON	\$500.00
4040116	APPLY BITUMINOUS TACK COAT	TON	\$160.00
4040125	FOG COAT	TON	\$600.00
4040163	BLOTTER MATERIAL	TON	\$21.00
4040262	ASPHALT BINDER (PG64-16)	TON	\$600.00
4060021	ASPHALTIC CONCRETE (BASEMIX)	TON	\$35.00
4060027	MINERAL ADMIXTURE (FOR BASEMIX)	TON	\$90.00
4090006	ASPHALTIC CONCRETE (MISCELLANEOUS STRUCTURAL - SPECIAL MIX)	TON	\$65.00
4140040	ASPHALT CONCRETE FRICTION COURSE (ASPHALT-RUBBER)	TON	\$35.00
4140042	ASPHALT RUBBER MATERIAL (FOR AR-ACFC)	TON	\$740.00
4140044	MINERAL ADMIXTURE (FOR AR-ACFC)	TON	\$90.00



APPENDIX F
PAVEMENT MEMO

1 Cubic yard	1.9	Tons.
LCCA done for One lane Mile	7040	SQ.YD.
Discount rate	4	%

Option 1 - 10-yrs. (HMA with Agg. Base)

Years	Discount Rate	ITEM DESCRIPTION	COST	PW COST
		1.0" AR-ACFC	\$38,069.44	
		6" Asphalt Concrete (Base Mix) (Includes binder & mineral filler)	\$169,027.32	
		8.0" Aggregate Base, Class 2	\$35,982.22	
0	1.0000	Total	\$243,078.99	\$243,078.99
10	0.6756	Remove existing HMA	\$28,160.00	\$19,023.89
10	0.6756	Reconst. with New JPCP	\$319,669.44	\$215,957.22
15	0.5553			
15	0.5553			
15	0.5553			
20	0.4564			
20	0.4564			
20	0.4564			
25	0.3751	1" Mill AR-ACFC	\$14,080.00	\$5,281.64
25	0.3751	1" Placement AR-ACFC	\$38,069.44	\$14,280.49
25	0.3751			
30	0.3083			
Net Present Worth (NPW)				\$497,622.2

Strategy	Initial Cost	LCCA	Preferred Option
Option 1	\$243,079	\$497,622	#2
Option 2	\$289,834	\$494,910	#3
Option 3	\$337,661	\$386,179	#1

1) Use Option 3 - lowest Life cycle cost

1 Cubic yard	1.9	Tons.
LCCA done for One lane Mile	7040	SQ.YD.
Discount rate	4	%

Option 2 - 20yrs. (HMA with Agg. Base)

Years	Discount Rate	ITEM DESCRIPTION	COST	PW COST
		1.0" AR-ACFC	\$38,069.44	
		7.5" Asphalt Concrete (Base Mix) (Includes binder & mineral filler)	\$211,284.15	
		9.0" Aggregate Base, Class 2	\$40,480.00	
0	1.0000	Total	\$289,833.59	\$289,833.59
10	0.6756			
10	0.6756			
15	0.5553			
15	0.5553	1" Mill AR-ACFC	\$14,080.00	\$7,818.12
15	0.5553	1" Placement AR-ACFC	\$38,069.44	\$21,138.61
20	0.4564	Remove existing HMA	\$28,160.00	\$12,851.86
20	0.4564	Reconst. with New JPCP	\$319,669.44	\$145,892.96
20	0.4564	1" Placement AR-ACFC	\$38,069.44	\$17,374.40
25	0.3751			
25	0.3751			
25	0.3751			
30	0.3083			
Net Present Worth (NPW)				\$494,909.5

Strategy	Initial Cost
Option 1	\$243,079
Option 2	\$289,834
Option 3	\$337,661

1) Use Option 3 - lowest Life cycle cost

1 Cubic yard	1.9	Tons.
LCCA done for One lane Mile	7040	SQ.YD.
Discount rate	4	%

Option 3 - 30yrs. (JPCP with Agg. Base)

Years	Discount Rate	ITEM DESCRIPTION	COST	PW COST
		1.0" AR-ACFC	\$38,069.44	
		11" JPCP	\$281,600.00	
		4.0" Aggregate Base, Class 2	\$17,991.11	
0	1.0000	Total	\$337,660.55	\$337,660.55
10	0.6756			
10	0.6756			
15	0.5553	1" Mill AR-ACFC	\$14,080.00	\$7,818.12
15	0.5553	1" Placement AR-ACFC	\$38,069.44	\$21,138.61
15	0.5553			
20	0.4564			
20	0.4564			
20	0.4564			
25	0.3751	1" Mill AR-ACFC	\$14,080.00	\$5,281.64
25	0.3751	1" Placement AR-ACFC	\$38,069.44	\$14,280.49
25	0.3751			
30	0.3083			
Net Present Worth (NPW)				\$386,179.4

Strategy	Initial Cost
Option 1	\$243,079
Option 2	\$289,834
Option 3	\$337,661

1) Use Option 3 - lowest Life cycle cost