

Fundamental Parameters of Antennas

- The time average Poynting vector (average power density) does not depend on time, and can be written as

$$\mathbf{W}_{\text{av}}(x, y, z) = [\mathcal{W}(x, y, z; t)]_{\text{av}} = \frac{1}{2} \text{Re}[\mathbf{E} \times \mathbf{H}^*] \quad (\text{W/m}^2)$$

Where, average power density is obtained by integrating the instantaneous Poynting vector over one period and dividing by the period.

\mathbf{E} and \mathbf{H} fields represent peak values, complex fields

Instantaneous Poynting vector represents the energy transfer per unit area per unit time of an electromagnetic field.

$$\mathcal{W} = \mathcal{E} \times \mathcal{H} = \frac{1}{2} \text{Re}[\mathbf{E} \times \mathbf{H}^*] + \frac{1}{2} \text{Re}[\mathbf{E} \times \mathbf{H} e^{j2\omega t}]$$

→ Avg=0

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Average power radiated by an antenna (radiated power)

$$P_{rad} = \iint W_{rad} ds$$

$$P_{rad} = P_{ave} = \int_0^{2\pi} \int_0^{\pi} \left(\frac{1}{2} \text{Re} [\underline{E} \times \underline{H}^*] \right) \cdot \hat{\mathbf{a}}_r r^2 \sin \theta d\theta d\phi \quad (2-9)$$

For Isotropic radiator which radiates equally in all directions(not exist but used as reference to compared with other antenna), the power density equal to

$$\mathbf{W}_0 = \hat{\mathbf{a}}_r W_0 = \hat{\mathbf{a}}_r \left(\frac{P_{rad}}{4\pi r^2} \right) \quad (\text{W/m}^2)$$

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Example 1

A **hypothetical isotropic antenna** is radiating in free space. At a distance of 100 m from the antenna, the total electric field (E_θ) is measured to be 5 V/m. Find the

(a) Power density (W_{rad})

(b) Power radiated (P_{rad})

$$(a) \quad \underline{W}_{\text{rad}} = \frac{1}{2} [\underline{E} \times \underline{H}^*] = \frac{E^2}{2\eta} \hat{a}_r = \frac{5^2 \hat{a}_r}{2(120\pi)} = 0.03315 \hat{a}_r \text{ Watts/m}^2$$

(b) Since isotropic:

$$P_{\text{rad}} = w_{\text{rad}} * 4\pi r^2$$

$$= 0.03315 * 4\pi * 100^2 = 4165.75 \text{ watts}$$

Note E depend on r so prad always const and wrad decrease as r increase

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Example 2

Example 2.2

$$\underline{W}_{ave} = \underline{W}_{rad} = \hat{a}_r A_0 \frac{\sin \theta}{r^2}$$

$$P_{ave} = P_{rad} = \oiint_S \underline{W}_{ave} \cdot d\underline{s}$$

$$= \int_0^{2\pi} \int_0^{\pi} \left[\hat{a}_r A_0 \frac{\sin \theta}{r^2} \right] \cdot \left[\hat{a}_r r^2 \sin \theta d\theta d\phi \right]$$

$$P_{ave} = P_{rad} = A_0 \int_0^{2\pi} \int_0^{\pi} \sin^2 \theta d\theta d\phi = 2\pi A_0 \int_0^{\pi} \sin^2 \theta d\theta$$

$$P_{rad} = A_0 \pi^2$$

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Radiation intensity: defined as

The power radiated from antenna per unit solid angle $U(\theta, \phi)$

$$U(\theta, \phi) = \frac{r^2}{2\eta} |\mathbf{E}(r, \theta, \phi)|^2 \simeq \frac{r^2}{2\eta} [|E_\theta(r, \theta, \phi)|^2 + |E_\phi(r, \theta, \phi)|^2] \quad (2-12a)$$

where

$\mathbf{E}(r, \theta, \phi)$ = far-zone electric-field intensity of the antenna

E_θ, E_ϕ = far-zone electric-field components of the antenna

η = intrinsic impedance of the medium

U = radiation intensity (W/unit solid angle)

The total power is obtained by integrating the radiation intensity, as given by (2-12), over the entire solid angle of 4π . Thus

$$P_{\text{rad}} = \oint_{\Omega} U d\Omega = \int_0^{2\pi} \int_0^\pi U \sin\theta d\theta d\phi \quad (2-13)$$

$$\text{radiation intensity of an isotropic source } U_0 = \frac{P_{\text{rad}}}{4\pi}$$

$$W_{\text{rad}} \Rightarrow \text{watt/m}^2$$

$$U \Rightarrow \text{watt/solid angle} = \text{watt/m}^2/\text{r}^2$$

$$U = \text{r}^2 W_{\text{rad}}$$

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Example 3

Compute Beam width, Beam solid angle and the power radiated through HPBW for normalized field pattern $F_n = \sin\theta$

Beam Width

$$P_n(\theta, \phi) = \sin^2 \theta \implies \frac{1}{2} = \sin^2 \theta_{HP} \quad \sin \theta_{HP} = \pm \frac{1}{\sqrt{2}}$$

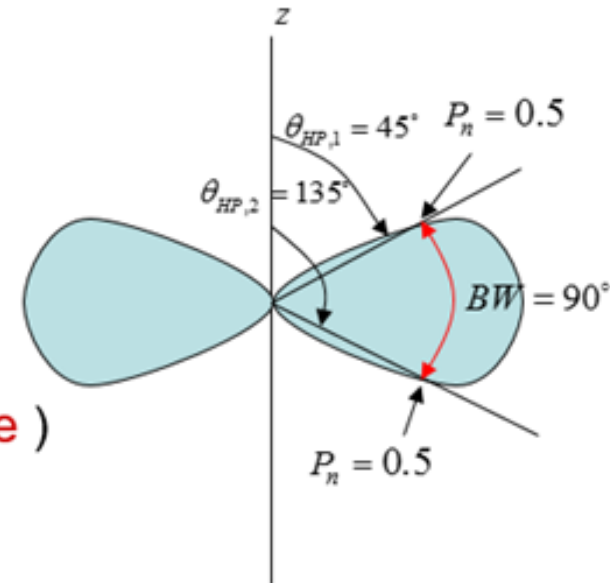
$$\sin \theta_{HP} = + \frac{1}{\sqrt{2}}$$

A

$$\theta_{HP,1} = 45^\circ \text{ and } \theta_{HP,2} = 135^\circ$$

$$\text{Beamwidth}(BW) = 135^\circ - 45^\circ = 90^\circ$$

*Approximation can not be used here
As it is not one main lobe*



Pattern Solid Angle Ω_A (Integrate over the entire sphere)

$$\Omega_A = \iint P_n(\theta, \phi) d\Omega$$

$$\Omega_A = \iint \sin^2 \theta \sin \theta d\theta d\phi = \int_0^{2\pi} \int_0^\pi \sin^3 \theta d\theta d\phi = \left(\int_0^\pi \sin^3 \theta d\theta \right) \left(\int_0^{2\pi} d\phi \right) = \left(\frac{4}{3} \right) (2\pi) = \frac{8\pi}{3}$$

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Half-power Pattern Solid Angle $\Omega_{A,HP}$ (*integrate over half power Beam width*)

$$\Omega_{A,HP} = \iint P_n(\theta, \phi) d\Omega$$

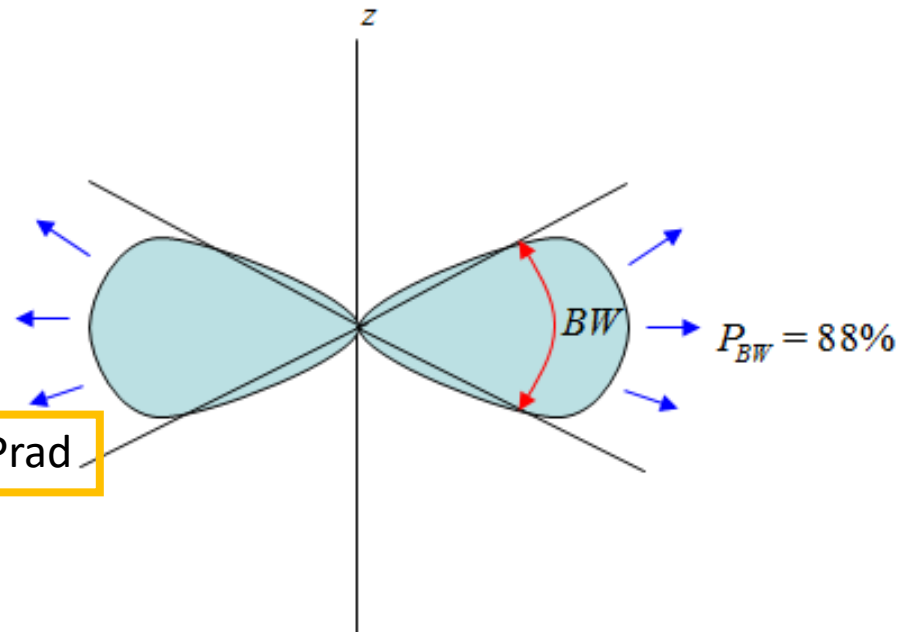
$$\Omega_{A,HP} = \iint \sin^2 \theta \sin \theta d\theta d\phi = \int_0^{2\pi} \int_{45^\circ}^{135^\circ} \sin^3 \theta d\theta d\phi = \left(\int_{45^\circ}^{135^\circ} \sin^3 \theta d\theta \right) \left(\int_0^{2\pi} d\phi \right) = \left(\frac{5}{3\sqrt{2}} \right) (2\pi) = \frac{5\pi\sqrt{2}}{3}$$

$$\int_{45^\circ}^{135^\circ} \sin^3 \theta d\theta = \left[-\cos \theta + \frac{\cos^3 \theta}{3} \right]_{45^\circ}^{135^\circ} = \left[\left(-\cos(135^\circ) + \frac{\cos^3(135^\circ)}{3} \right) - \left(-\cos(45^\circ) + \frac{\cos^3(45^\circ)}{3} \right) \right]$$

$$= \left[\left(\frac{1}{\sqrt{2}} - \frac{1}{6\sqrt{2}} \right) - \left(-\frac{1}{\sqrt{2}} + \frac{1}{6\sqrt{2}} \right) \right] = \frac{2}{\sqrt{2}} - \frac{2}{6\sqrt{2}} = \frac{10}{6\sqrt{2}} = \frac{5}{3\sqrt{2}}$$

Power radiated through the beam width

$$P_{BW} = \frac{\Omega_{A,HP}}{\Omega_A} = \frac{\frac{5\pi\sqrt{2}}{3}}{\frac{8\pi}{3}} = \frac{5\sqrt{2}}{8} \cong 0.88 \text{ (or) } 88\% \text{ of Prad}$$



Directivity

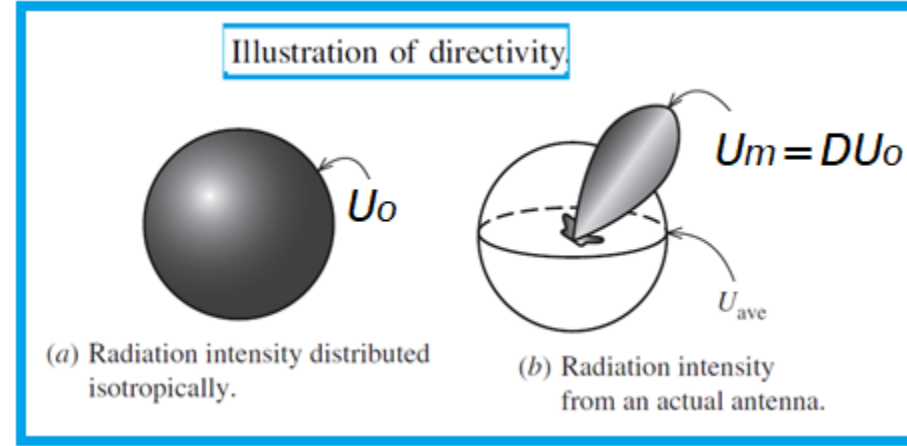
is the ratio of radiation intensity in a given direction to isotropic radiation intensity

$$D = \frac{U}{U_0} = \frac{4\pi U}{P_{\text{rad}}}$$

If the direction is not specified \rightarrow (maximum directivity)

$$D_{\text{max}} = D_0 = \frac{U|_{\text{max}}}{U_0} = \frac{U_{\text{max}}}{U_0} = \frac{4\pi U_{\text{max}}}{P_{\text{rad}}}$$

Example 4



Example 2.5

find the maximum directivity of the antenna whose radiation intensity is $U = A_0 \sin \theta$. Write an expression for the directivity as a function of the directional angles θ and ϕ .

$$P_{\text{rad}} = \int_0^{2\pi} \int_0^\pi U \sin \theta \, d\theta \, d\phi = A_0 \int_0^{2\pi} \int_0^\pi \sin^2 \theta \, d\theta \, d\phi = \pi^2 A_0$$

Using (2-16a), we find that the maximum directivity is equal to

$$D_0 = \frac{4\pi U_{\text{max}}}{P_{\text{rad}}} = \frac{4}{\pi} = 1.27$$

Since the radiation intensity is only a function of θ , the directivity as a function of the directional angles is represented by

$$D = D_0 \sin \theta = 1.27 \sin \theta$$

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Approximated Directivity (by Kraus)

For antennas with **one narrow major lobe** and very negligible minor lobes, the **beam solid angle is approximately equal to the product of the half-power beam widths in two perpendicular planes**

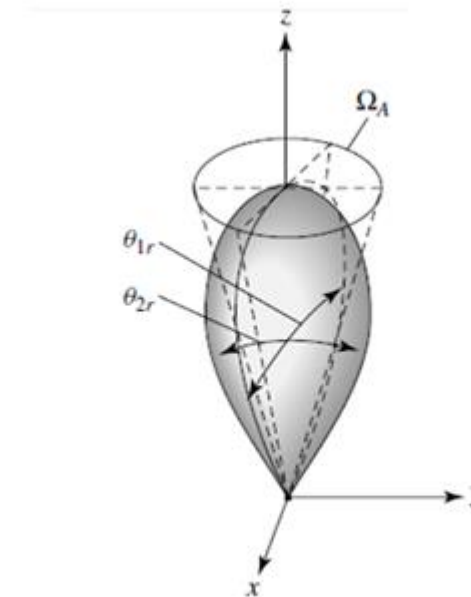
$$D_0 = \frac{4\pi}{\Omega_A} \simeq \frac{4\pi}{\theta_{1r} \cdot \theta_{2r}} \quad (\text{Kraus})$$

θ_{1r} = half-power beamwidth in one plane (rad)

θ_{2r} = half-power beamwidth in a plane at a right angle to the other (rad)

For radiation intensity

$$U(\theta, \phi) = B_0 \cos^n(\theta) \quad \text{at } 0 < \theta < \pi/2, 0 < \phi < 2\pi \text{ and } 0 \text{ elsewhere}$$



Beam solid angles $\Omega_A = \theta_{1r} \cdot \theta_{2r}$

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Example 5

The normalized field pattern of an antenna is given by $E_n = \sin \theta \sin \phi$, where θ = zenith angle (measured from z axis) and ϕ = azimuth angle (measured from x axis). E_n has a value only for $0 \leq \theta \leq \pi$ and $0 \leq \phi \leq \pi$ and is zero elsewhere (pattern is unidirectional with maximum in $+y$ direction). Find (a) the exact directivity, (b) the approximate directivity and (c) the decibel difference.

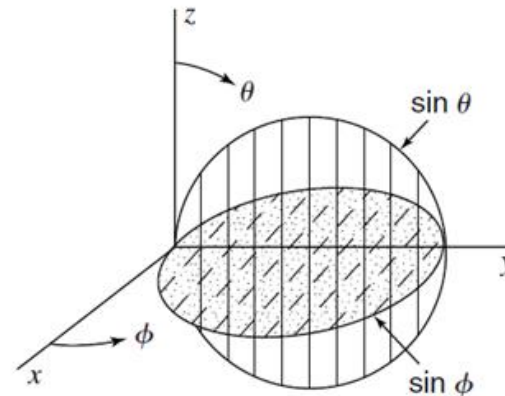
Solution

$$(a) G = \frac{4\pi}{\iint_{4\pi} P_n(\theta, \phi) d\Omega} = \frac{4\pi}{\int_0^\pi \int_0^\pi (\sin \theta \sin \phi)^2 \sin \theta d\theta d\phi}$$

$$G = \frac{4\pi}{\int_0^\pi \int_0^\pi \sin^3 \theta \sin^2 \phi d\theta d\phi} = \frac{4\pi}{2\pi/3} = 6$$

$$(b) D = \frac{41,253}{\theta_{HP}^\circ \phi_{HP}^\circ} = \frac{41,253}{(90^\circ)(90^\circ)} = 5.1$$

$$(c) \Delta D(dB) = 10 \log \frac{6}{5.1} = 0.7 dB$$



Unidirectional $\sin \theta$ and $\sin \phi$ field patterns.

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Example 6 Directivity of a Sector Omnidirectional Pattern

An ideal omnidirectional antenna would have constant radiation in the horizontal plane ($\theta = 90^\circ$) and would fall rapidly to zero outside that plane. If power pattern in the vertical plane is constant out to $\pm 30^\circ$ **from horizontal**. find Directivity.

The power pattern expression is then written as:

$$F(\theta) = \begin{cases} 1 & \frac{1}{3}\pi < \theta < \frac{2}{3}\pi \\ 0 & \text{elsewhere} \end{cases}$$

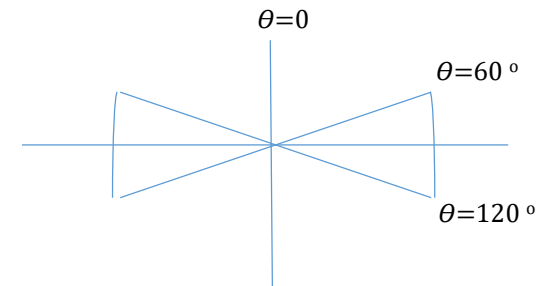
Solution:

The solid angle of the pattern is

$$\begin{aligned} \Omega_A &= \int \int |F(\theta, \phi)| d\Omega = \int_0^{2\pi} \int_{\pi/3}^{2\pi/3} \sin \theta d\theta d\phi \\ &= (2\pi) [-\cos \theta]_{\pi/3}^{2\pi/3} = (2\pi)(0.5 + 0.5) = 2\pi \end{aligned}$$

The directivity is

$$D = \frac{4\pi}{\Omega_A} = \frac{4\pi}{2\pi} = 2.$$



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Example 7

Example 2.8

Design an antenna with omnidirectional amplitude pattern with a half-power beamwidth of 90° . Express its radiation intensity by $U = \sin^n \theta$. Determine the value of n , max directivity

Solution: Since the half-power beamwidth is 90° , the angle at which the half-power point occurs is $\theta = 45^\circ$. Thus

$$U(\theta = 45^\circ) = 0.5 = \sin^n(45^\circ) = (0.707)^n$$

or

$$n = 2$$

Therefore, the radiation intensity of the omnidirectional antenna is represented by $U = \sin^2 \theta$. An infinitesimal dipole (see Chapter 4) or a small circular loop (see Chapter 5) are two antennas which possess such a pattern.

Using the definition of (2-16a), the exact directivity is

$$U_{\max} = 1$$

$$P_{\text{rad}} = \int_0^{2\pi} \int_0^\pi \sin^2 \theta \sin \theta d\theta d\phi = \frac{8\pi}{3}$$

$$D_0 = \frac{4\pi}{8\pi/3} = \frac{3}{2} = 1.761 \text{ dB}$$

$$\int_0^\pi \sin^3 \theta d\theta = \frac{4}{3}$$

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Example 8

The antenna is a lossless end-fire array of 10 isotropic point sources spaced $\lambda/4$ and operating with increased directivity. The normalized field pattern is

$$E_n = \sin\left(\frac{\pi}{2n}\right) \frac{\sin(n\psi/2)}{\sin(\psi/2)}$$

where

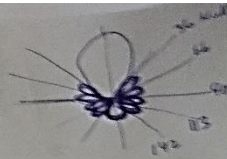
$$\psi = d_r (\cos \phi - 1) - \frac{\pi}{n} \quad d_r = \pi/2 \quad n = 10$$

Since the antenna is lossless, gain = directivity.

- (a) Calculate the gain G .
- (b) Calculate the approximate gain
- (c) What is the difference?

Solution

$$E_n = \sin\left(\frac{\pi}{20}\right) \frac{\sin(2.5\pi \cos(\theta-1) - 0.5\pi)}{\sin(0.25\pi \cos(\theta-1) - 0.05\pi)}$$



To Find HPBW Use Table

θ°	0	10	20	30	40	50	60	70	80	90
E_n	1	0.92	0.68	0.29	-0.12	-0.34	-0.21	0.11	0.2	0
	100	110	120	130	140	150	160	170	180	
E_n	-0.17	-0.07	0.11	0.14	0.04	-0.07	-0.14	-0.15	-0.15	

So θ_h between 10° and 20° and $\theta_{max} = 0^\circ$

Try and Error [or table between $10^\circ \rightarrow 20^\circ$ step 1°]

$$\theta_h = 19.3^\circ$$

$$\therefore \text{HPBW} = 2|\theta_{max} - \theta_h| = 2 \times 19.3^\circ = 38.6^\circ$$

Approximate Directivity:

$$D_{app} = \frac{4\pi}{(\text{HPBW})^2} = \frac{4\pi}{\left(\frac{38.6}{180}\pi\right)^2} = 27.7 \text{ or } 14.4 \text{ dB}$$

Exact Directivity:

$$D = \frac{4\pi}{\int_0^\pi \int_0^{2\pi} \left[0.1564 \frac{(\sin(2.5\pi(\cos\theta-1) - 0.5\pi))^2}{(\sin(0.25\pi(\cos\theta-1) - 0.05\pi))^2} \right] \sin\theta d\theta d\phi}$$

$$= \frac{4\pi}{(2\pi) \int_0^\pi \left[\dots \right]^2 \sin\theta d\theta} = \frac{4\pi}{2\pi \times (0.1564)^2 \times 4.59}$$

$$D_{\text{exact}} = 17.8 \text{ or } 12.5 \text{ dB} \quad \therefore \Delta D = 1.89 \text{ dB}$$