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SATELLITE SYSTEMS

ESA study: System impacts of Propulsion passivation OHB Sweden - OHB System - FOI - Etamax

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- 1. What is Propulsion Passivation?
- 2. What are the Space Debris Mitigation requirements for Propulsion Passivation?
- 3. What does a "Safe configuration" mean for a Propulsion system at EoL?
- 4. How do we further reduce the risks in the future?



Prisma mission – Flight configuration and the 3 Propulsion systems passivated in 2015



In-orbit break-up history

- 233 break-up events in orbit since 1958 (including all known and unknown causes):
 Source: NASA Orbital Debris Program Office (ODPO). The "History of On-Orbit Satellite Fragmentations" and "Orbital Debris Quarterly News" (ODQN)
- The Two Main Sources for Propulsion:

54 Deliberate Satellite Break-ups

 \rightarrow 52 x COSMOS APO System

98 Propulsion Break-ups → 97 Rocket Upper Stage







→Only one case of propulsion induced SAT break-up known (USA-68: Solid Rocket Motor)

→USA-73 break-up in 2004:
 Propulsion S/S is most likely not the break-up cause
 (Battery failure instead, as for USA-109)



Passivation operations – Residual energy in current missions

LEO reference case

- Passivation limited by diaphragm tank
 N2: ~5.5bar at EoL
 N2H4: ~5.5bar, 2% residuals
- Depletion down to the min qualified thruster feed pressure.



GEO reference case

- Passivation limited by isolation of Gas side after LEOP: Helium: ~50bar after LEOP MON-MMH: ~9bar, 1.8 to 2.6% residuals
- Depletion down to the min qualified thruster feed pressure
- MTG: Additional passivation line downstream MPR





Passivation operations – PRISMA Hydrazine system

Attitude control

- AOCS mode: Normal Mode to reduce operational risks
- Last operations in visibility of ground only
- Last burn with SA to the sun and Antenna to Earth
 → Safest configuration (NLLP mode)





Propulsion monitoring and controls

- P_drop during burns increases quickly at EoL (Bladder reaches tank wall)
- Critical pressure predicted with a ±0.1 bar accuracy
- Thrusters temperatures (Catbed, FCV) monitored at 1Hz, although no attitude divergence due to bubbles is expected
- Duty cycles with reduced ON time are used

Results:

Passivation down to ~5 bar. Is this safe? Which risks remain?



Passivation operations – Recommendations for LEO missions

Propulsion:

- Detect bubbles: PT noise + FCV/Cat bed temperatures monitoring
- Predict Critical pressure by analysis (±0.1bar accuracy)
- Safe duty cycles: Reduced T_ON
- Maintain RCT feed pressure: Increase tank temperature
- Maintain Hydrazine liquid: Decrease tank temperature
- Stop passivation when/if attitude is no longer controlable

Attitude and orbit:

- Ensure telemetry access: Attitude and operation time selection
- Limit aerodynamic perturbations
 Adapt attitude at low altitudes (SPOT-1)



TM/TC:

- Detect bubbles: Monitor angular velocities (risk of attitude divergence)
- Detect bubbles: PT and TT acquisition rate: >1Hz to detect bubbles

→ Propulsion passivation should not put at risk the other Passivation operations (E.g. Battery)

→No generic passivation sequence or strategy since it depends on S/C design, Telemetry access...

 \rightarrow A full list of recommendations has been issued in the Study



Passivation operations – Recommendations for GEO missions

Propulsion:

- Detect bubbles: PT noise + FCV/Cat bed temperatures monitoring
- Safe duty cycles: Reduced T_ON
- Maintain RCT feed pressure: Increase tank temperature
- Maintain MON/MMH liquid: Decrease tank temperature
- Stop passivation when/if attitude is no longer controlable
- Avoid freezing of lines: Monitor shadowed RCT flow valves
- Avoid bubble contamination: Optimize thruster selection, Use bubble migration models

Attitude and orbit:

- Earth Pointing Mode:
- + Good telemetry access
- + Predictable Forces
- Usually less robust than Sun Pointing
- Sun Pointing mode:
- Usually poor telemetry access
- + Preferred mode directly after 1st bubble appears



TM/TC:

- Detect bubbles: Monitor angular velocities if assymetrical Thrust is expected
- Detect bubbles: Use high PT / TT acquisition rate

- → Propulsion passivation should not put at risk the other Passivation operations (E.g. Power S/S passivation)
- →No generic passivation sequence or strategy since it depends on S/C design, Telemetry access...
- \rightarrow A full list of recommendations has been issued in the Study



ISO 24113: Adopted in ECSS-U-AS-10C

- "What to do?" International high-level debris mitigation requirements
- "...permanently deplete or make safe all remaining on-board sources of stored energy..."

ESSB-HB-U-002 SDM Compliance Verification Guidelines - ESA handbook

- "How to do it?" Aims of providing compliance verification methods
- Problem: It remains at the same level of ISO 24113
- → Risk of contradicting requirements (E.g. Risk of HyperVelocity Impact excluded from ISO 24113)

Compliance status:

- LEO ref: Residuals in the Diaphragm tank, by design
- GEO ref: Residuals in the Pressurant side + Propellant PMD tank, by design
- \rightarrow Full depletion not achievable, not required, and not needed if S/C is already safe.
- \rightarrow In any case, we need to fill the knowledge gaps to define what a "Safe state" is.





Risk assessment - 1/ Tank burst due to thermal drift

Thermal analysis - Worst case assumptions in LEO:

- Single side radiator pointing to the Sun
- Equilibrium condition (t=∞)
- No cooling by structure
- No tumbling motion
- EOL material properties
- Conservative also for albedo/IR flux

→ Propellant Tank Temperature < 90°C at EOL</p>

Risk of burst (Assuming 200°C!)

LEO: Tank ~ 10bar << Burst (~50bar)
 →Low risk TBC (Hydrazine decomposition to be assessed)

■ GEO: MON/MMH Tanks ~ 15bar << Burst (~30bar) He Tank ~ 96bar << Burst (~620 bar) →Low risk



Note: VDA MLI and Titanium are typical materials



Risk assessment - 2/ Long term chemical effects

LEO - MEO: Hydrazine tanks

- Hydrazine dissociation → Exothermic reaction + Corrosion
- Long term compatibility test (US Air Force):
- \rightarrow < 5% N2H4 decomposed after 25 years (at 43°C)
- \rightarrow N2H4 decomposition <u>and</u> metal dissolution minimized with SS and Ti
- □ Effects of N2H4 decomposition on Tank Pressure to be assessed.
- Risk of Tank thermal fatigue to be assessed



GEO: MMH - MON tanks

- Low risk of corrosion with MON (NTO+NO). NO inhibits stress-corrosion cracking
- MON MMH known for their good storability but accelerated ageing tests are needed to justify their "safe state".



Risk assessment – 3/ Fragmentation due to Hypervelocity Impacts

Study case

Target: 50cm Titanium hydrazine tank - Externally mounted - 5bar residual Hydrazine **Orbit**: 800km, 98.6degrees inclination

Debris: 3.5 mm and 13mm Ø AI spheres. (Probability of impacting the target over 25 yrs is 10⁻² and 10⁻³ resp.)

- Hyper-velocity impact modelling
- 1. Debris penetration simulation (FEM-Exp)



3. Impact of a Shielding structure (FEM-SPH)



Simulation of a 13mm debris at 14km/s (relative velocity) hitting the S/C structure before impacting the tank wall (blue)

2. Propagation of the debris plume (FEM-SPH)



4. Detonation in the liquid phase? (RMD)



5. Detonation in the vapour phase? (Cheetah)





Conclusion – HyperVelocity Impact risk assessment

14 km/s impact with a non-shielded tank

13 mm particle, T>90 °C

EXP: rupture SPH: Violent interaction at rear wall RMD: Liquid detonation not ruled out FEM: Vapour det.: clear frag.

Rupture

13 mm particle, T<90 °C

EXP: rupture SPH: Violent interaction at rear wall RMD: Liquid detonation not ruled out FEM: vapour det: small contribution

Rupture

3.5 mm particle, T>150 °C

EXP: f/b performation, no rupture SPH: very dispersed plume RMD: liquid detonation unlikely FEM: vapour det.: clear frag.

Rupture

3.5 mm particle, 90°C<T<150 °C

EXP: f/b performation, no rupture SPH: very dispersed plume RMD: liquid detonation unlikely FEM: vapour det.: significant contrib.

Transition zone

3.5 mm particle, T<90 °C

EXP: f/b performation, no rupture SPH: very dispersed plume RMD: liquid detonation unlikely FEM: vapour det.: small contrib.

No rupture (Safe state)



Activities to improve passivation levels for LEO missions

1. Define what a safe state is

- Define a Safe Pressure at EoL (HVI models to be validated by tests, as done for Upper stages)
- Investigate EoL thermal configuration (200°C)
- Assess risks of pressure build-up in tanks

2. Future architectures minimizing System impacts - Trade-off conclusions

 Delta-qualification of RCTs to low inlet pressures is the preferred option



System impact of Propulsion Passivation – Clean Space Industrial Days- 2016-05-27

Develop a passivation valve (TBC if needed)



Activities to improve passivation levels for GEO missions

1. Define what a safe state is

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2. Future architectures minimizing System impacts - Trade-off conclusions

- Delta-qualification of bi-prop RCTs to low inlet pressures
- Develop a He Electronic Pressure Regulator
 → Increases system performances while permitting gas depletion !









Conclusions

- Propulsion systems need to be made safe at EoL
- Definition of a S/C Safe state is missing → Engineering activities are identified
- The risk reduction gained fron passivating a propulsion S/S is unclear
- Operational risks are on the other hand clearly identified

New passivation systems should:

- Be useful to the nominal mission phase when possible → E.g. He EPR, Low Power HET
- Limit System impact (Reliability, AIT, Cost) → Delta-qual of RCTs at low Pressures





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