

Sustainable and Environmental Catalysis

Edited by Raffaele Cucciniello, Daniele Cespi and Tommaso Tabanelli Printed Edition of the Special Issue Published in *Catalysts*



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Editorial Sustainable and Environmental Catalysis

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1. Introduction

Over the last few decades, an increasing amount of interest from academia and industry has been devoted to the application of the Twelve Principles of the Green Chemistry in order to pursue the Sustainable Development Goals (SDGs) recommended by the United Nations [1]. They are based on the fundamental idea of guiding research and innovation toward more environmental-friendly practices as well as socioeconomic sustainable solutions. Among them, catalysis plays a pivotal role able to address some important needs: (i) avoiding the use of stoichiometric amount of chemicals; (ii) increasing selectivity (i.e., decreasing the generation of waste), and (iii) decreasing energy demand. In this context, with the aim to eliminate environmental pollutants (NO_x , CO, SO_x , VOCs) and to design new catalytic routes for clean energy production, environmental and sustainable catalysis represents a noble and one of the most investigated research directions. Moreover, as recently suggested, sustainable and environmental catalysis allows for converting waste in value-added products, and the degradation of pollutants through catalytic combustion/photocatalysis are considered main topics in this context [2,3]. As a matter of fact, it is worth highlighting some recent research advances. The oxidation of chlorinated compounds by catalytic combustion on non-noble metals based oxides [4,5], NO_x reduction to nitrogen or by selective catalytic reduction (SCR) with ammonia in the presence of heterogeneous catalysts [6]; biofuel production from vegetable oils [7]; the development of new active catalysts for Fenton and photo-Fenton processes [8]; the development of supported nanoparticle catalysts for the treatment of the emission of harmful substances from automobiles, and the use of waste as source of metals for catalysts preparation [9]; the design of new active catalytic systems for the preparation of olefins from polyols [10]; the catalytic hydrotreatment in the valorization of bio-oils obtained from lignocellulosic biomass pyrolysis [11]; and the design of active catalysts for the preparation of organic carbonates from CO₂ or bio-based compounds are some examples in this framework [12,13].

This Special Issue aims to cover new and promising examples of sustainable and environmental catalysis with particular emphasis on the adoption of green chemistry principles at both a laboratory and industrial scale.

2. The Contents of the Special Issue

In this Special Issue, several fields of research on the sustainable catalytic valorization of biomasses are discussed. Therefore, we would like to sincerely thank all the authors who contributed with their excellent contributions to this Special Issue, which includes fourteen articles.

Cucciniello et al. investigated the use of iron-doped mayenite catalysts for trichloroethylene (TCE) oxidation in the gas phase. All the synthesized catalysts showed good performances for TCE oxidation, totally converted into CO₂, CO, and HCl. Mayenite loaded with 2% iron was found to be the best catalyst in terms of T₅₀ (300 °C). This result was correlated



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Copyright: © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). with an optimum combination of the oxidative properties of the mayenite active support with the redox properties of iron, as Temperature Programmed Reduction (TPR), X-ray photoelectron spectroscopy (XPS) and Raman results have shown [14].

Chevez Rivas et al. reported the preparation and characterization of natural purified mordenite treated with a hydrothermal ion exchange process in an acid medium with Fe^{2+} or Fe^{3+} salts. The set of samples was characterized regarding their textural properties, morphology, and crystallinity, and tested in the NO reduction with CO/C_3H_6 . The activity in hydrocarbons-selective catalytic reduction (HC–SCR) (used as a reaction test) was found to depend on the ion exchange process [15].

Husnain et al. discussed the selective catalytic reduction of NO with NH₃ at low temperatures with natural iron ore catalysts. The results showed that the sample based on α -Fe₂O₃ and γ -Fe₂O₃ calcined at 250 °C, achieved excellent selective catalytic reduction (SCR) activity (above 80% at 170–350 °C) and N₂ selectivity (above 90%, up to 250 °C) at low temperatures [16].

Ngoie et al. investigated the potential of a heterogeneous catalyst produced from mineral processing waste for biodiesel production. Tailings from the concentration of cupriferous minerals served as the starting material for synthesis of the catalyst. The nano-magnetic catalysts were prepared using coprecipitation and sol–gel methods, combined with zero-valent iron nanoparticles to form a hydride catalyst. Catalyst properties were assessed using SEM, TEM, BET, and EDX. The maximum yield obtained with this catalyst was 88% and an average of 27% decrease in biodiesel yield observed after four reaction cycles [17].

Muhammad Habib et al. discussed the preparation of two alternative catalysts $(Co_3O_4/TiO_2 \text{ and } 8 \text{ wt.}\% ZrO_2-Co_3O_4/TiO_2)$ for CO, HC, and NO_x conversions. These systems were produced along with a wire mesh-based substrate and tested by mounting them at the exhaust tailpipe of a motorcycle engine. Zirconia-promoted catalyst showed more promising towards NO_x conversion. The cobalt supported by the titania Co_3O_4/TiO_2 catalyst showed a performance towards conversion of carbon monoxide, nitrogen oxides, and unburnt hydrocarbons to values of 78.1%, 61.9%, and 82.6% efficiency, respectively, at 1500 RPM; whereas, the conversion efficiency of zirconia promoted $ZrO_2-Co_3O_4/TiO_2$ catalyst was 81.3%, 78.6%, and 55.1% towards HCs, CO, and NO_x, respectively, at 1500 RPM value. Due to small crystalline size, thermal stability, and fouling inhibition, the ZrO_2 -promoted Co_3O_4/TiO_2 catalyst showed better conversion efficiency towards CO and NO_x. The slightly lower efficiency of zirconia-promoted catalyst showed selectivity towards CO, NO_x, and HC, and had comparable performance with respect to the activity of a conventional catalyst [18].

Zhou et al. proposed a copper-based Fenton-like catalyst (Cu/Al₂O₃/g–C₃N₄) to achieve high degradation efficiencies for Rhodamine B (Rh B) in a wide range of pH (4.9–11.0). The Cu/Al₂O₃ composite was first prepared via a hydrothermal method followed by a calcination process. The composite was then stabilized on graphitic carbon nitride (g–C₃N₄). The characterizations show that Cu species were immobilized on the Al₂O₃ framework in the form of Cu²⁺ and Cu⁺, and the introduction of CN increased its specific surface area and adsorption capacity for Rh B. The Cu/Al₂O₃/CN composite showed an excellent catalytic performance in a wide range of pH (4.9–11.0). The specific reaction rate constant of Rh B degradation was calculated as (5.9 ± 0.07) × 10⁻⁹ m·s⁻¹, and the activation energy was calculated to be 71.0 kJ/mol. The recycling experiment demonstrated its durability for Rh B removal and proved that the degradation reaction was surface dominated, with a negligible leaching of copper species in solution [19].

A novel method for preparing highly efficient glass fiber-supported Pt nanoparticle catalysts for the treatment of the emission of harmful substances from automobiles was proposed by Sasaki et al. The Pt catalyst was prepared by depositing a reactive chemically adsorbed monomolecular film with a thiol group at the molecular terminal on the surface of a hydrophilized glass fiber. The monomolecular film enabled the uniform and dense grafting of Pt nanoparticles on the surface of the glass fiber as a single layer. Both catalysts exhibited catalytic performance at temperatures \geq 200 °C. At 300 °C, the octane combustion rates (index for evaluating performances of the Pt and commercially available catalysts) of the catalysts were \geq 80%. At 50–400 °C, the octane combustion rates of both catalysts were approximately the same. Pt catalysts were found to exhibit catalytic performance comparable to that of Pd catalysts under lean conditions, despite the lower price [20].

Research conducted by Villamarin-Barriga et al. showed that the residual sludge of galvanic industries can be used as catalytic materials (after thermal treatment) for the synthesis of materials. Researchers evaluated the sludge from three galvanic industries. Catalyst was obtained from a thermal process based on sludge dried between 100 and 120 °C, and calcination of sludges between 400 to 700 °C. Catalytic activity was analyzed by thermogravimetric analysis of a thermocatalytic decomposition of crude oil. The best conditions for catalyst synthesis were calcination between 400 and 500 °C, the temperature of reduction between 750 and 850 °C for 15 min. The catalytic material had mainly Fe as active phase and a specific surface between 17.68–96.15 m²·g⁻¹; the catalysts promoted around 6% more weight-loss of crude oil in the thermal decomposition compared with assays without the catalyst. To determinate the environmental sustainability of this process, the E-factor (mass of waste/mass of product) was calculated by obtaining values between 0.1 and 0.3; the ideal E-factor is zero [21].

In the manuscript of Klein Gebbink et al., two new tetradentate N-donor ligandsupported ReO_2^+ complexes (cis-[(BPMEN)ReO_2]PF₆ and cis-[(BmdmPMEN)ReO_2]PF₆) were synthesized and fully characterized. They were found to be active in deoxydehydration (DODH) reactions of diols, suggesting that Re(V) dioxo complexes can be involved in DODH catalysis. Treatment of (N₂Py₂) ReO₂⁺ with an excess amount of water generates an active species for DODH catalysis; use of the Re-product of this reaction shows a much shorter induction period compared to the pristine complex. No ligand is coordinated to the "water-treated" complex, indicating that the real catalyst is formed after ligand dissociation. IR analysis suggested this catalyst to be a rhenium-oxide/hydroxide oligomer. The monodentate pyridine ligand is much easier to dissociate from the metal center than a tetradentate N₂Py₂ ligand, which makes the Py₄ReO₂⁺-initiated DODH reaction more efficient. For the Py₄ReO₂⁺-initiated DODH of diols and biomass-based polyols, both PPh₃ and 3-pentanol could be used as a reductant. Excellent olefin yields are achieved [22].

The manuscript of Ray et al. reports on the photocatalytic and antibacterial activity of ZnO nanoparticles. This activity is strongly related to the amount of surficial reactive oxygen species (ROS) and metal ions (Zn^{2+}) which, in turn, is strictly dependent on the morphology of the nanomaterials. In this context, the authors managed to optimize the preparation of different ZnO nanospheres, nanopetals, and nanorods by varying the precipitation solvent ranging from PEG400, water, and toluene. These nanocatalysts (dimension ranging from 10 to few hundreds nanometers) were effective in killing 99% of bacteria at low concentrations in water while the photodegradation of caffeine using solar light was completed after 120 min using the optimized ZnO nanospheres. These results are promising; therefore, the mechanism of both the processes will be investigated in depth in future investigations [23].

The research work of Kaewkannetra and coworkers show the possibility to successfully valorize the triglyceride-rich palm-oil mill effluent (POME) through the combination of biological and thermochemical processes. In this complementary approach, the aqueous waste of the palm oil manufacture first undergoes an enzymatic hydrolysis with yield up to 90% in free fatty acids (FFA). Subsequently, FFA are efficiently converted into long chain hydrocarbon mixtures, suitable for jet fuel application, via the heterogeneously catalyzed hydrogenation reaction (Pd/Al₂O₃, 400 °C, 10 bar of H₂, 1 h). This innovative and complementary approach for the valorization of POME was never reported in literature and represents a new way to both alleviate the wastewater environmental issue and to obtain a high value-added product (jet fuels) for local biorefineries (e.g., Southeast Asia) [24].

Dutta et al. reported on the catalytic activity of Pd/SiO_2 for the selective oxidation of CO at low temperature. An extensive characterization of the catalytic materials (by FTIR, TGA–DSC, TEM, and XPS) allowed for investigating the influence of the thermal pretreatment on catalyst activity and stability. Interestingly, a structure–activity relationship was proposed, correlating the catalyst activation and CO oxidation hysteresis behavior with the information on both the palladium oxidation states and nanoparticle dispersion. In particular, the best low-temperature CO oxidation performance was achieved by calcining the catalyst at 450 °C [25].

In a comprehensive review, Paone et al. extensively discussed the potentials of catalytic hydrotreatment in the valorization of bio-oils obtained from either lignocellulosic biomass pyrolysis or by the physical pressing of oleaginous vegetable seeds. This treatment uses high-pressure hydrogen in order to both stabilize the bio-oil and decrease the amount of oxygenated compounds, in this way obtaining mixtures suitable for direct use as drop-in biofuels. In particular, the current state-of-the-art on the reaction pathways, catalyst formulations, and reactor technology (i.e., traditional vs. membrane) were analyzed indepth [26].

Zhang et al. proposed an innovative series of binuclear aluminum complexes as highly active and selective homogeneous catalysts for the cycloaddition reaction of epoxides and carbon dioxide. The reaction is of interest because the market for organic carbonates is steadily increasing due to their utilization as solvents, electrolytes, and monomers for high-performance polymers (i.e., polycarbonates, polyurethane, and polyureas), as well as a way to valorize CO_2 as a feedstock. Interestingly, the bifunctional tridentate tetrammino phenoxyimino-phenoxy aluminum complex is also active in very mild conditions, i.e., 100 °C and low CO_2 pressure (≤ 2 atm), which allows for obtaining good to excellent conversions of the parental epoxides. Kinetic investigations showed a first-order dependence on the concentration of the epoxide for the target reaction [27].

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Communication Base-Free Synthesis of Furfurylamines from Biomass Furans Using Ru Pincer Complexes

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Abstract: We report the first example of employing homogeneous organometal-catalyzed transfer hydrogenation for the selective reductive amination of furfurals to furfurylamines. An efficient, chemoselective, and base-free method is described using Ru-MACHO-BH as catalyst and *i*PrOH as H donor. The method tolerates a range of substituents affording moderate to excellent yields.

Keywords: transfer hydrogenation; furfurals; furfurylamine; reductive amination; Ru-MACHO

1. Introduction

The development of sustainable techniques to transform biomass into useful compounds is one of the biggest challenges of modern chemistry [1]. The introduction of nitrogen in biomass-derived compounds adds value and expands their industry applicability [2]. Furfurals are aldehydes derived from biomass and are identified as one of the key chemicals produced by the lignocellulosic biorefineries. Around 280 kTon are produced globally per year [3]. Furfurylamines (amines derived from furfurals) present diverse applications in the industry, including the preparation of pharmaceutical compounds such as Furesomide, Furtrethonium, an anti-hepatitis-B, and Barmastine (Figure 1), as well as polymers, antiseptic agents, agrochemicals, pesticides, and synthetic resins [1,2,4].



Figure 1. Pharmaceutical compounds containing furfurylamines.

The synthesis of furfurylamines from furfurals by reductive amination has been investigated using diverse reducing agents and catalysts. Studies involving hydrogen gas, silanes, borohydrides, and formic acid as reductants have been reported in the literature. Hydrogen gas as reductant is an interesting green tool; however, the method needs to operate under pressure of a highly flammable gas, increasing the operating cost. Nevertheless, there are many examples in the literature using H₂ as reductant for reductive amination with noble and non-noble metal catalysts such as Ru, Au, Ir, Pt, Ni, Co and Fe [5–11]. Although silane is obtained from waste residues of the silicon industry, their use is still in stoichiometric amounts, generating excessive amounts of waste [12–14]. The use of formic acid as H donor for the reductive amination of furfural was demonstrated as well. Cao and co-workers synthesized N-(furan-2-ylmethyl)aniline in 93% yield from nitrobenzene and furfural using Au/TiO₂-R as catalyst at 80 °C for 4 h [15]. Smith Jr and co-workers also employed formic acid as H donor, but used formamide as N source [16]. To the best of our



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Copyright: © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). knowledge, the only work involving an alcohol as H donor (*i*PrOH) for the synthesis of furfurylamines from furfural was reported by Yus [17]. In this work, the reaction between furfural and heptylamine using 20 mol% of NiNPs at 76 °C for 48 h afforded 30% yield of the furfurylamine.

One of the most powerful and robust methods for effective C–N bond formation of amines is the reductive amination of carbonyl compounds. [4,18–30]. This transformation features compelling advantages, such as simple operating setups, mild reaction conditions, direct use of available substrates, and inexpensive reagents [31]. The reductive amination using transfer hydrogenation for the synthesis of furfurylamines from furfurals is limited, even though this transformation as a synthetic tool is non-toxic, environmentally friendly, does not require flammable gasses, and employs a stable, easy to handle, and inexpensive source of hydrogen [4,32–37]. However, transfer hydrogenation catalysts typically require strong bases to be active, which can be detrimental for substrates that are base-sensitive [38]. Therefore, studies applying base-free conditions must be developed to avoid this drawback.

The use of homogenous metal catalysis has demonstrated great reactivity for transfer hydrogenation of carbonyl compounds and has been proven to hold many advantages [38–41]. In 2018, De Vries reported a base-free transfer hydrogenation of α , β unsaturated ketones and aldehydes using the PNP pincer complex carbonylhydrido (tetrahydroborato)[bis(2-diphenylphosphinoethyl)amino]ruthenium(II) (Ru-MACHO-BH) as catalyst, in the presence of EtOH or *i*PrOH as H source and showed high activity and selectivity [42]. The amino-based Ru-PNP complexes are also very efficient catalysts for hydrogenation [43–49] and dehydrogenation [50–57] reactions. The high activity of these Ru PNP complexes in hydrogenations is often attributed to the presence of the Ru–H unit and N–H group [58].

Inspired by these works, we investigated the use of Ru-MACHO [59] (carbonylhydrido (tetrahydroborato)[bis(2-diphenylphosphinoethyl)amino]ruthenium(II)) and Ru-MACHO-BH complexes as potential catalysts for the transfer hydrogenation of the reductive amination in this work.

2. Results and Discussion

Our studies commenced with testing Ru-MACHO (1 mol%) as the catalyst for the transfer hydrogenation of the aldimine **1a** (Figure S1) in the presence of *i*PrOH (0.2 M of **1a**) as hydrogen source and KOtBu (20 mol%) as additive at 90 °Cfor 3 h (Scheme 1). To our delight, the reaction afforded >99% conversion to furfurylamine **2a**. We then set out to evaluate the transfer hydrogenation of **1a** using varying catalyst loading, additives, temperatures, and reaction times with the aim of developing a mild protocol for this reaction.



Scheme 1. (a) Ru-PNP catalysts used in this work. (b) Transfer hydrogenation of aldimine using Ru-MACHO. ^[a] Measured by ¹H NMR spectroscopy analysis of the crude reaction mixture.

Reducing the reaction time to 15 min, the catalyst loading of Ru-MACHO to 0.5 mol%, and the KOtBu loading to 10 mol% still led to full conversion (Table 1, Entry 3). In fact, after 5 min, 51% was already converted (Entry 4). Changing the additive to NaOH had

a detrimental effect, and only 18% conversion was observed. Likewise, lowering the catalyst loading to 0.1 mol% afforded less than 5% conversion. Changing the catalyst to Ru-MACHO-BH showed very low activity within 15 min, both with and without additive (Entries 6 and 7, respectively).

Entry ^a	Catalyst (mol%)	Additive ^b	Time	Conv. ^c (%)
1	Ru-MACHO (0.5)	KOtBu	1 h	>99
2	Ru-MACHO (0.5)	KOtBu	30 min	>99
3	Ru-MACHO (0.5)	KOtBu	15 min	>99
4	Ru-MACHO (0.5)	KOtBu	5 min	51
5	Ru-MACHO (0.5)	NaOH	15 min	18
6	Ru-MACHO (0.1)	KOtBu	15 min	<5
7	Ru-MACHO-BH (0.5)	-	15 min	<5

Table 1. Transfer hydrogenation of aldimines: Initial studies.

^a Reactions were carried out using 1.3 mmol of furfural and aniline in 7 mL *i*PrOH at 90 °C. ^b 10 mol% additive used. ^c Measured by ¹H NMR spectroscopy analysis of the crude reaction mixture.

Motivated by these initial positive results, the reductive amination of furfural with aniline was further investigated. Thus, in the presence of 10 mol% KOtBu, 0.5 mol% of Ru-MACHO afforded >99% conversion after 18 h at 90 °C. However, the furfuryl alcohol (FA, 3) appeared as a significant side product in a proportion of 7:3 (2a/3) (Scheme 2). Fortunately, introducing MgSO₄ as drying agent led to >99% conversion selectively to the desired product in 3 h (Table 2, Entry 2). Reducing the reaction time to 1 h decreased the selectivity to 93:7. Using Ru-MACHO-BH (0.5 mol%) and MgSO₄ but without the basic additive still resulted in 93% conversion after 1 h and with 2a as the sole product by ¹H NMR analysis (Entry 3). Increasing the amount of aniline from 1.0 to 1.2 equivalent afforded >99% 2a under otherwise identical conditions (Entry 5). Unfortunately, it was not possible to further reduce the reaction time without compromising the conversion and selectivity (Entries 6-8). Decreasing the amount of Ru-MACHO-BH to 0.25 mol% also led to a low conversion of 11% (Entry 9). Lowering the temperature to 70 $^{\circ}$ C resulted in practically no conversion (<5%, Entry 10). However, by increasing the temperature to 120 °C, it was possible to achieve exclusively 2a with >99% conversion within 30 min (Entry 11).

A number of drying agents were then tested. Using Na₂SO₄ at 90 °C afforded >99% conversion in 1 h. However, the selectivity decreased to 97:3 (**2a**/**3**) (Entry 12). Decreasing the time further to 15 min maintained the full conversion but led to even lower selectivity, down to 57:42 (**2a**/**3**) (Entries 13–15). These observations suggest that the formation of **3** is highly reversible, and that **1a** is regenerated from **3** throughout the course of the reaction. Moreover, decreasing the reaction temperature to 70 °C led to merely 17% conversion (Entry 16). Molecular sieves (4 Å) were also evaluated and showed full conversion after 1 h, albeit with slightly lower selectivity (94:6 **2a**/**3**) (Entry 17). Decreasing the time further to 15 min maintained the full conversion but also led to lower selectivity, (71:29 **2a**/**3**) (Entry 18). The temperature was evaluated, and carrying out the reaction at 70 °C led to 71% conversion and 96:4 (**2a**/**3**) of selectivity (Entry 19).



Scheme 2. Reductive amination between furfural and aniline.

Entry ^a	Catalyst (mol%)	Additive ^b	Temperature (°C)	Time	Conversion ^c (%)	2a ^c (%)	3 ^c (%)
1	Ru-MACHO (0.5)	KOtBu	90	18 h	>99	70	30
2	Ru-MACHO (0.5)	$KOtBu + MgSO_4$	90	3 h	>99	>99	-
3	Ru-MACHO (0.5)	$KOtBu + MgSO_4$	90	1 h	>99	93	7
4	Ru-MACHO-BH (0.5)	$MgSO_4$	90	1 h	93	>99	-
5 d	Ru-MACHO-BH (0.5)	MgSO ₄	90	1 h	>99	>99	-
6 ^d	Ru-MACHO-BH (0.5)	MgSO ₄	90	45 min	75	86	14
7 ^d	Ru-MACHO-BH (0.5)	MgSO ₄	90	30 min	30	73	27
8 d	Ru-MACHO-BH (0.5)	-	90	30 min	15	52	48
9 d	Ru-MACHO-BH (0.25)	$MgSO_4$	90	1 h	11	-	>99
10 ^d	Ru-MACHO-BH (0.5)	MgSO ₄	70	1 h	<5	-	-
11 ^d	Ru-MACHO-BH (0.5)	MgSO ₄	120	30 min	>99	>99	-
12 ^d	Ru-MACHO-BH (0.5)	Na ₂ SO ₄	90	1 h	>99	97	3
13 ^d	Ru-MACHO-BH (0.5)	Na_2SO_4	90	45 min	>99	90	10
14 ^d	Ru-MACHO-BH (0.5)	Na_2SO_4	90	30 min	>99	76	24
15 ^d	Ru-MACHO-BH (0.5)	Na_2SO_4	90	15 min	>99	57	42
16 ^d	Ru-MACHO-BH (0.5)	Na ₂ SO ₄	70	1 h	17	72	28
17 ^d	Ru-MACHO-BH (0.5)	MS 4 Å	90	1 h	>99	94	6
18 ^d	Ru-MACHO-BH (0.5)	MS 4 Å	90	15 min	>99	71	29
19 ^d	Ru-MACHO-BH (0.5)	MS 4 Å	70	1 h	71	96	4

Table 2. One-pot synthesis of furfurylamines: Optimization.

^a Reactions were carried out using 1.3 mmol of furfural, aniline, and 1.3 mmol of drying agent in 7 mL *i*PrOH. ^b 10 mol% of KOtBu used. ^c Measured by ¹H NMR spectroscopy analysis of the crude reaction mixture. ^d Reactions were carried out using 1.2 equivalent of aniline. MS = Molecular sieves.

As seen in Figure 2, the levels of 1–3 differed significantly throughout the course of the reaction, depending on whether Na_2SO_4 or $MgSO_4$ was employed. Within 15 min, almost all 1a had disappeared and 60% of 2a had already been generated when using Na_2SO_4 . Surprisingly, 35% of 3 was observed at this point. Hereafter, the reaction slowed significantly, and after 30 min, merely 70% of 2a had been produced and 3 had only dropped

to 22%. By contrast, with MgSO₄ the level of **3** did not exceed 15% throughout the entire course of the reaction, and after 30 min, it was 12%. At this time, there was still an ample amount of **1a** (45%) to undergo hydrogenation, and 43% of **2a** had been produced. This difference in amount of **1a** present during the course of the reaction might explain the superiority of MgSO₄ as drying agent after 60 min.



Figure 2. Monitoring the reaction of furfural with aniline using either MgSO₄ as drying agent (**a**) or Na_2SO_4 as drying agent (**b**). Reactions were carried out using 1.3 mmol of furfural, 1.2 equivalent aniline, and 1.3 mmol of drying agent in 7 mL *i*PrOH.

Therefore, although Na₂SO₄ and molecular sieves demonstrate higher conversion rates than MgSO₄, the latter drying agent was chosen due to the higher yield provided

after 1 h of reaction time. Therefore, the conditions described in the Entry 5 in Table 2 were defined as standard conditions for the scope.

To assess the general applicability of the Ru-MACHO-BH as a catalyst for the one-pot synthesis of furfurylamines from furfurals and amines, various anilines were evaluated using the standard conditions (Scheme 3). Generally, moderate to excellent yields were obtained. The parent aniline afforded an excellent 93% of isolated product. Comparing the anilines containing either electron-donating or -withdrawing substituents, the latter group showed superior yield. As such, 4-F-C₆H₄NH₂, 4-CF₃-C₆H₄NH₂, and 4-aminopyridine generated the best yields of the substituted anilines with 74-95% of isolated products 2h-j. The product **2j** is analogous to the anti-hepatitis-B compound shown in Figure 1, which demonstrates the direct applicability of the method for the synthesis of pharmacological activity compounds. On the other hand, a donating group (4-CH₃-C₆H₄NH₂) afforded lower yield of 61% of 2d. This observation can perhaps be explained by the increased electronic deficiency of the imines when employing $4-CF_3-C_6H_4NH_2$ as reagent [1]. Various halogens were tested as well and showed moderate to good yields (2b, 2e, 2h). Compounds with substituent in different positions, such as $3-Cl-C_6H_4NH_2$ and $2-F-C_6H_4NH_2$, showed good tolerance, yielding 60% and 56% of 2c and 2f, respectively. The method was also tested with the secondary amine N-methylaniline, which afforded the tertiary amine 2g in high yield (89%). Unfortunately, no products were observed when employing various primary and secondary alkyl amines (tBuNH₂, nHepNH₂, Me₂NH, morpholine).



Scheme 3. One-pot synthesis of furfurylamines catalyzed by Ru-MACHO-BH. Reactions were carried out using 1.3 mmol of furfural, 1.56 mmol of aniline, and 1.3 mmol of MgSO₄ in 7 mL *i*PrOH. All yields are isolated.

5-(hydroxymethyl)furfural (HMF) and 5-methylfurfural are other important biomassderived furans with industrial applications [60,61]. The furfurylamines derived from HMF are used in the synthesis of biopolymers (polyamides) and pharmaceuticals [4]. The *N*-(5-methylfurfuryl)aniline is a very important compound used in the synthesis of epoxyisonindoles and bioactive compounds such as anti-bacterial, anti-tuberculosis, antitumor, and anti-inflammatory entities [62–70]. Therefore, the method is an interesting alternative for the production of these valuable compounds. Hence, we also evaluated this compound as a potential substrate (Scheme 4). The reactions afforded a high yield of **4** (87%) and a moderate yield of **5** (54%).



Scheme 4. One-pot synthesis of furfurylamines catalyzed by Ru-MACHO-BH. Reactions were carried out using 1.3 mmol of furfural, 1.56 mmol of aniline and 1.3 mmol of MgSO₄ in 7 mL of *i*PrOH. ^[a] Isolated yield.

3. Materials and Methods

3.1. Materials

Most chemicals were purchased from commercial suppliers and used without further purification unless otherwise stated. Hydroxymethylfurfural (HMF, 99%) (Sigma-Aldrich, St. Louis, MO, USA), furfural (99%) (Sigma-Aldrich, St. Louis, MO, USA), formethylfurfural (99%, Sigma-Aldrich, St. Louis, MO, USA), KotBu (99%, Sigma-Aldrich, St. Louis, MO, USA), *i*PrOH (anhydrous, 99.5%, Sigma-Aldrich, St. Louis, MO, USA), Ru-MACHO (Sigma-Aldrich, St. Louis, MO, USA), and Ru-MACHO-BH (Strem Chemicals, Newburyport, MA, USA) are commercially available and were used without further purification. All reactions dealing with air or moisture-sensitive compounds were performed using standard Schlenk techniques or in an argon-filled glovebox. The ¹H and ¹³C NMR spectra were recorded on a Bruker Avance III 400 MHz spectrometer (Bruker, Billerica, MA, USA) and were referenced to the solvent peak. The software MestReNova version 11.0.0-17609 (Mestrelab, Escondido, CA, USA, 2016) was used for NMR analysis. The software OriginPro 2019 9.6.0.172 (Academic) (OriginLab, Northampton, MA, USA, 2019) was used for graphic plot. All the products are literature known compounds, and the experimental data (¹H and ¹³C{¹H} NMR spectra) fit those reported.

3.2. Methods

3.2.1. Preparation of Aldimine 1a

A mixture of furfural (54 mmol), aniline (54 mmol) and methanol (0.5 M) in the presence of MS (4 Å) was stirred at room temperature for 3 h. After completion of the reaction, the crude mixture was filtered off and evaporated under reduced pressure. The product **1a** was obtained as a brown oil, 7.83 g, 85%.

3.2.2. General Procedure for Transfer Hydrogenation of Aldimine 1a Catalyzed by Ru-PNP Complexes

A Schlenk pressure vessel containing catalyst, additive and magnetic bar was sealed and flushed with argon (three times). The solvent and H-donor (*i*-PrOH) was introduced by a needle and stirred at 90 °C. After 10 min, the aldimine **1a** was added to the solution. After a certain reaction time (5–18 h), the reaction was stopped, and the crude was analyzed. The conversion was determined by spectroscopy ¹H NMR.

3.2.3. General Procedure for One-Pot Reductive Amination of Furfural

In a Schlenk pressure vessel containing Ru-MACHO-BH (0.5 mol %) and MgSO₄ (1.3 mmol), a magnetic stirring bar was added and the vessel was sealed and flushed with argon (three times). During argon flow, 4.5 mL of *i*PrOH was introduced by a needle and the solution was heated at 90 °C and stirred for 10 min. In a flame-dried screw-cap vial, aniline (1.56 mmol) and furfural (1.3 mmol) were mixed with 2.5 mL of *i*PrOH (to provide a solution with furfural concentration of 0.18 M) under argon flow. The atmosphere was replaced with argon and the solution was introduced to the Schlenk pressure vessel. The reaction mixture was kept at 90 °C for 1 h. The crude reaction mixture was evaporated under reduced pressure, and the product was obtained after purification through chromatography column (Ethyl acetate/pentane, 90:10). For the optimization process, the method of employing relative conversions as measured by NMR was confirmed with respect to absolute values by a single duplicate test reaction using mesitylene as internal standard.

4. Conclusions

In conclusion, we report the first example of an efficient base free one-pot transfer hydrogenative reductive amination of furfural for the synthesis of furfurylamines under mild conditions, employing low amounts of the commercially available catalyst Ru-MACHO-BH and *i*PrOH as H donor. The general applicability of the method is demonstrated by the use of furfural and various anilines with different substituents, which afforded yields that varied from moderate to excellent (56–93%). Furthermore, this chemoselective methodology established a high yield (83%) in the synthesis of the furfurylamine derived from HMF and a moderate yield (54%) from *N*-(5-methylfurfuryl)aniline.

Supplementary Materials: The following are available online at https://www.mdpi.com/article/ 10.3390/catal11050558/s1, Table S1: Monitoring the reaction of furfural and aniline using MgSO₄ as drying agent. Table S2: Monitoring the reaction of furfural and aniline using Na₂SO₄ as drying agent. Figure S1: ¹H NMR spectrum of 1a (400 MHz, CDCl₃), Figure S2: ¹³C NMR spectrum of 1a (100 MHz, CDCl₃), Figure S3: ¹H NMR spectrum of **2a** (400 MHz, CDCl₃), Figure S4: ¹³C NMR spectrum of 2a (100 MHz, CDCl₃), Figure S5: ¹H NMR spectrum of 2b (400 MHz, CDCl₃), Figure S6: ¹³C NMR spectrum of **2b** (100 MHz, CDCl₃), Figure S7: ¹H NMR spectrum of **2c** (400 MHz, CDCl₃), Figure S8: ¹³C NMR spectrum of 2c (100 MHz, CDCl₃), Figure S9: ¹H NMR spectrum of 2d (400 MHz, CDCl₃), Figure S10: ¹³C NMR spectrum of 2d (100 MHz, CDCl₃), Figure S11: ¹H NMR spectrum of 2e (400 MHz, CDCl₃), Figure S12: ¹³C NMR spectrum of 2e (100 MHz, CDCl₃), Figure S13: ¹H NMR spectrum of 2f (400 MHz, CDCl₃), Figure S14: ¹³C NMR spectrum of 2f (100 MHz, CDCl₃), Figure S15: ¹H NMR spectrum of **2g** (400 MHz, CDCl₃), Figure S16: ¹³C NMR spectrum of **2g** (100 MHz, CDCl₃), Figure S17: ¹H NMR spectrum of **2h** (400 MHz, CD₃OD), Figure S18: ¹³C NMR spectrum of **2h** (100 MHz, CDCl₃), Figure S19: ¹H NMR spectrum of **2i** (400 MHz, CDCl₃), Figure S20: ¹³C NMR spectrum of 2i (100 MHz, CDCl₃), Figure S21: ¹H NMR spectrum of 2j (400 MHz, CDCl₃), Figure S22: ¹³C NMR spectrum of **2***j* (100 MHz, CDCl₃), Figure S23: ¹H NMR spectrum of **4** (400 MHz, CDCl₃), Figure S24: ¹³C NMR spectrum of 4 (100 MHz, CDCl₃), Figure S25: ¹H NMR spectrum of 5 (400 MHz, CDCl₃), Figure S26: ¹³C NMR spectrum of 5 (100 MHz, CDCl₃).

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Recent Catalytic Advances in Hydrotreatment Processes of Pyrolysis Bio-Oil

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Abstract: Catalytic hydrotreatment (HT) is one of the most important refining steps in the actual petroleum-based refineries for the production of fuels and chemicals, and it will play also a crucial role for the development of biomass-based refineries. In fact, the utilization of HT processes for the upgrading of biomass and/or lignocellulosic residues aimed to the production of synthetic fuels and chemical intermediates represents a reliable strategy to reduce both carbon dioxide emissions and fossil fuels dependence. At this regard, the catalytic hydrotreatment of oils obtained from either thermochemical (e.g., pyrolysis) or physical (e.g., vegetable seeds pressing) processes allows to convert biomass-derived oils into a biofuel with properties very similar to conventional ones (so-called drop-in biofuels). Similarly, catalytic hydro-processing also may have a key role in the valorization of other biorefinery streams, such as lignocellulose, for the production of high-added value chemicals. This review is focused on recent hydrotreatment developments aimed to stabilizing the pyrolytic oil from biomasses. A particular emphasis is devoted on the catalyst formulation, reaction pathways, and technologies.

Keywords: pyrolysis oils; catalytic hydrotreatment; heterogeneous catalysis; hydrogenation; biorefinery; green chemistry

1. Introduction

In a green and sustainable perspective, the world is moving from a strong fossil fuels' dependence to a consistent use of renewable feedstocks. In this view, Anastas and Green proposed in 1998 "the 12 principles of green chemistry" [1], where a particular attention was also given to (second and third generation) transportation biofuels, chemicals, commodities, and pharmaceuticals directly produced from biomass in modern biorefineries [2–6]. This transition is given not only by the matured awareness that fossil resources are running out, but it is mostly accelerated by the United Nation decision to adopt the 2030 Agenda for Sustainable Development, a program action of 17 ambitious goals (SDGs) and 169 targets aimed to eradicate the poverty, to protect the planet, and to ensure the prosperity for all [7]. Biomasses, that currently supply about 80% of global renewable energy and a low-emissions character, represent a unique sustainable pathway to successfully address SDGs [1,7,8]. Among several technologies that can use biomass waste as the feedstock to produce energy fuels, power, heat, and various high value-added chemicals [9–14], an interesting example is the use of lignocellulose (plant based biomasses mainly composed of cellulose, hemicellulose, and lignin) and microalgae (biomasses with high protein and carbohydrate content characterized by the absence of lignin) for the production of bio-oil



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Copyright: © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). that can be used as intermediate for the production of liquid bio-fuels [15]. Bio-oil is a dark brown-red colored liquid, with a characteristic smell of smoke and a chemical composition strictly related to the biomass feedstocks containing a wide number of unique compounds generated from the rapid quenching of pyrolytic fragments of lignocellulose [16]. Figure 1 shows the main compounds present in the bio-oil: an aqueous solution of several products derived from the fragmentation of cellulose and hemicellulose and from the depolymerization of lignin. The mixture consists of various organic compounds (20–30 wt%), water (19–20 wt%), water-soluble oligomers (WS, also known as pyrolityc humin), and waterinsoluble oligomers (WIS, also known as pyrolityc lignin) (43–59 wt%) that can be efficiently used for several applications, such as drop-in fuel, production of chemicals, and various carbon-based materials [17–22].



Figure 1. A simplified chemical composition of bio-oil: main lignocellulose-derived compounds.

Conventionally, bio-oil is produced by using a high energy demanding multistep process, such as pyrolysis (fast or slow, thermal or thermo-catalytic) and hydrothermal liquefaction (HTL). These thermochemical processes are conducted in the absence of oxygen and at high reaction temperature with the aim to allow the decomposition/depolymerisation of lignocellulose and microalgae into a bio-oil liquid (the major product), solid (bio-char), and gaseous products (CO₂, CO, CH₄, H₂) (bio-syngas [15,23,24]. Bio-char can access applications in several fields (e.g., soil amendment in agriculture, chemical sensing, adsorbent material in wastewater remediation) or combusted to recover energy for the pyrolysis stage [25], while bio-syngas may be directly utilized for many energy uses (e.g., electricity generation, fuel for transport, cooking fuel, feedstock for fuel cells) [26]. HTL processes were developed to improve the efficiency of direct thermal decomposition methods and differ from the pyrolysis for the adoption of lower reaction temperatures and for the presence of a homogeneous or heterogeneous catalyst by applying water and simple aliphatic (e.g., methanol, ethanol, and 2-propanol) alcohols used as such or in combination as reaction solvents. However, bio-oils arising from these two processes cannot be directly used as drop-in fuels in conventional engines due to problems related to the presence of a common limiting feature, the high oxygen content of biomass otherwise responsible of chemical unfavorable properties of bio-oil (high acidity, high viscosity, thermal and chemical instability) [16].

Thus, a biorefinery process in which biomass is first converted in bio-oil by pyrolytic or HTL step followed by an oxygen removal stage represents a most promising approach for the production of biofuels and chemicals.

To this regard, in order to mitigate the oxygen content and to improve the bio-oil properties for practical use, some catalytic approach (catalytic cracking, hydrodeoxygenation HDO, etc.), based on a thermal-catalytic treatment of biomass (hydrotreatment or hydrotreating process), come to help. Among them, one of the most promising strategies is the catalytic hydrodeoxygenation (HDO) that allows the reduction of oxygen content providing, at the same time, the highest C-atom efficiency.

Although this process allows to obtain bio-oil in a high yield, the formation of a variable quantity of coke remains a problem to be solved. In this context, it was reported that the presence of a suitable catalyst in a two-step biorefinery process can reduce the formation of coke by improving, at the same time, the bio-oil properties [27,28]. The first step (or stabilization step) permits the transformation of carbonyl and carboxyl functional groups into alcohols promoted by noble metals catalysts (Pt, Ru, and Pd) in a temperature range between 100 and 300 °C. The second step is conducted between 350 and 400 °C and is driven by sulphide conventional catalysts that allows to completely remove oxygen species.

This review aims to provide a brief overview on recent advances in the catalytic hydrogenation process of bio-oil arising from thermal treatment of lignocellulosic biomass and microalgae, highlighting progresses made in terms of enhancing catalyst efficient activity for upgrade bio-oil HDO.

2. Bio-Oil Proprieties

Bio-oil is the main product of biomass pyrolysis. Historical documents report that this process was already used in ancient Egypt to prepare sealants for boats and ointments. In the 18th century, wood distillation provided compounds such as soluble tar, pitch, creosote oil, as well as chemical and non-condensable gases. Interest in biomass pyrolysis was revived in the 1980s, when the process was perfected to have a high yield of liquid compound [29]. The pyrolysis process carried out with a temperature between 400 °C and 600 °C and varying the residence time and heating rate, the product distribution changes. To maximize the process in term of liquid yield, the fast pyrolysis at ~500 °C is usually preferred, advantageously producing a liquid yield up to three times larger than the conventional and slow pyrolysis [30].

As an example, Figure 2 shows the flow diagram of the BTG Bi-oliquids BV pyrolysis plant [31]. The first part of the plant consists in a drying unit where biomass from different origin (for example, wood, rice husk, bagasse, sludge, tobacco, energy crops, palm-oil residues, straw, olive stone residues, chicken manure) is dried to decrease the water content. The dry biomass, in presence of a hot carrier (sand), is then converted in a fluidized bed reactor into pyrolysis oil, gas, and char. After that, the products and the sand are separated from the vapor/gas phase by a series of cyclones. Then, the char and sand fraction is moved to a fluid bed combustor, where the char is used to heat the sand recycled in the fluidized bed. The vapor/gas phase is instead quenched by re-circulated oil to divide the bio-oil from the incondensable gases, where the latter are captured as high-pressure steam and utilized in a steam turbine system.



Figure 2. Pyrolysis plant. With permission from BTG Bioliquids BTG bioliquids BV [31].

Furthermore, recent researchers are focusing their attention to microalgae as feedstock for fast pyrolytic reaction [32]. Microalgae are classified as third-generation biofuel due to their fast growth cycle and high lipid content (~50%), easily converted in fuels. Moreover, microalgae do not require arable land and are adaptable at different water sources, including wastewater. The pyrolysis of microalgae is usually carried out in presence of a catalyst, such as zeolites, aluminosilicates, transitional metal-loaded zeolites, MOFs, silica gel [33–35]. The pyrolysis process for microalgae may be performed as (i) one-pot step process, where microalgae and catalyst are mixed together (ii) or a double-step process, the pyrolysis vapors from microalgae are swept over a catalyst at a specific temperature [36,37].

The fast pyrolysis of biomass produces hundreds of different compounds (Table 1), where their composition depends of the cellulose, hemicellulose, lignin, and extractive content in the respective feedstock. The influence of biomass composition on bio-oils composition can be appreciated from the variability of the bio-oils elemental composition reported in Table 2, where the C content can vary from 39% (pine sawdust) to about 60% (beech wood) under the same pyrolysis conditions. Furthermore, the operating conditions of the fast pyrolysis influence the bio-oil composition [38–40].

Fraction/Chemical Groups	tion/Chemical Groups Compound Types		wt% (Wet Basis) [39]	wt% [40]
	Water solubles 75–85%			
Acids alcohols	Small acids, small alcohols	5-10	6.5	8.5
Ether-solubles	Catechols, syringols, guaiacols, aldehydes, ketones, furans, and pyrans	5–15	15.4	20.3
Ether-insolubles	Sugars	30-40	34.4	45.3
Water	Water	20-30	23.9	-
	Water insoluble 15–25%			
Hexane-solubles	Extractives (High MW compounds with functional groups such as acids, alcohols)	2–6	4.35	5.7
DCM solubles	Stilbenes, Low MW lignin degraded compounds	5–10	13.4	17.7
DCM insolubles	High MW lignin degraded compounds	2-10	1.95	2.6

Table 1. Bio-oil composition.

Table 2. Feedstock composition updated from [35].

Feedstock for Bio-Oil	С	н	0	Ν	S	Ref.
Beechwood	51.1	7.3	41.6			[41]
Pine wood	40.1	7.6	52.1	0.1		[42]
Rice husk	39.92	8.15	51.29	0.61	0.03	[43]
Beech wood	58.6	6.2	35.2			[44]
Pine sawdust	38.8	7.7	53.4	0.09	0.02	[45]
Eucalyptus	44.8	7.2	48.1	0.2		[46]
White spruce	49.6	6.4	43.1	0.2		[47]
Poplar	49.5	6.05	44.4	0.07		[47]
Sawdust	60.4	6.9	31.8	0.9		[48]
Microalgae	54.8	7.6	28.7	8.5	0.4	[49]
Scenedesmus	44.6	6.1	40.8	4.8	3.6	[50]
Nannochloropsis gaditana	40.3	5.97	14.5	6.3	0.37	[51]
Chlorella protothecoides	62.1	8.7	11.2	9.7	n/a	[52]
Spirulina	67.5	9.8	11.3	10.7	n/a	[53]
Nannochloropsis sp.	80.2	6.2	5.8	6.2	n/a	[54]

3. Catalytic Hydrogenation of BIO-Oil

In refineries, the hydrogenation reactions are common operations to limit the presence of oxygen, nitrogen, sulphur, olefins, and aromatics. The reaction is generally catalyzed by molybdenum together with Ni or Co supported by γ Al₂O₃. The operating conditions depend on the type of feed: LHSV 0.2 to 8.0, H₂ circulation from 50 to 675 Nm³/m³, H₂ pressure between 14 and 138 bar, and temperatures between 290 and 470 °C [55]. Actually, there are not industrial processes for HDO of bio-oil, but several catalysts have been tested from noble metals to Ni and Co, in presence of acid supports such as Al₂O₃ and SiO₂, or C, in the temperature range 150–500 °C, pressure range between 2 and 200 bar [47]. In this section, recent advances on catalysts for HDO of bio-oil are summarized. Furthermore, technical aspects of emergent technologies (e.g., membrane reactors) for hydroprocessing are also discussed.

3.1. Catalysts

Hydro-processing is conventionally catalyzed in presence of metals from group VIII, such as nickel, palladium, and platinum [56]. Furthermore, group VIB metals (tungsten and molybdenum) have also been used for oxygen removal, since they are resistant to attack by oxygen, acids, and alkalis [57,58]. According to Masel [59], hydrogen is reactive in the surfaces of Co, Ni, Ru, Rh, Pd, Os, Ir, Pt as well as on Sc, Ti, V, Y, Zr, Nb, Mo, La, Hf, Ta, W, Cr, Mn, Fe, Tc, and Re. A slower uptake of hydrogen was observed with Cu [59]. Some authors increased the catalyst activity adding a second metal in order to promote an efficient adsorption of hydrogen at low temperature [60,61]. The most used supports were alumina-silica, carbon, titania (rutile), and zirconia (monoclinic form). Activated carbon is a well-known high-surface area (typically ~1000 m²/g) support material, which has been shown to be stable in hot water processing environments; rutile titania and monoclinic zirconia have lesser surface area (typically $30-80 \text{ m}^2/\text{g}$) but have also demonstrated their utility as catalytic metal support and have been used in the hot water processing environment [62–64]. A possible pathway for upgrading bio-oils is represented by hydrogenation reactions in liquid phase, with the conversion of aldehydes, ketones, sugars, phenols, etc., in more stable alcohols. In order to improve the conversion of the bio-oils compounds and enhance the selectivity on desired products, several catalysts have been studied (Table 3). Interesting is the work of Wei et al. [65], where Pt over different ceria-zirconia supports were evaluated for the hydrogenation of cinnamaldehyde at 10 bar and 60 °C, obtaining a conversion in the range of 60–95%.

Catalyst	Reactant	Pressure (bar)	Temperature (°C)	Time (h)	Conversion (%)	Note	Ref.
30% Ni/CNT	acetic acid	40	150	4	5.8	2 wt% cat	[66]
30% Cu/CNT	acetic acid	40	150	4	3.5	2 wt% cat	[66]
Ru/C	acetic acid	40	150	4	4.7	2 wt% cat	[66]
20% Mo/CNT	acetic acid	40	150	4	<2	2 wt% cat	[66]
10/10 wt% NiMo/CNT	acetic acid	40	150	4	14.8	2 wt% cat	[66]
3 wt% Ru/TiO ₂	acetic acid	62	120	33 *	37.5	* time on stream	[67]
3 wt% Ru/TiO ₂	Acetol	62	70	14 *	93.6	* time on stream	[67]

Table 3. Hydrogenation reaction.

Catalyst	Reactant	Pressure (bar)	Temperature (°C)	Time (h)	Conversion (%)	Note	Ref.
3 wt% Ru/TiO ₂	Bio-oil	62	120	21	27/38/79 **	** acetic acid/acetol/formic	[67]
3 wt% Ru/C	Bio-oil	52	120	6	33/99/97 **	acid	[67]
Ru/Zr-MOFs	Furfural	5	20	5	20–95	TOF: 2–11 Selectivity to Furfuryl alcohol: 20–95	[68]
AuNCs/CNTs membrane	4-nitro-phenol				53/100	5/10 µmol Au/17 cm ²	[69]
Au/SiO ₂	25 compounds	80	6	5–24	40–99	1 mmol of alkyne, 0.01 mmol of Au, and 1 mmol of piperazine	[70]
Re-Pd/SiO ₂	Stearic acid	80	140	1	15	$D_{r}/D_{r} = 1/0$	[71]
Re-Pd/SiO ₂	Stearic acid	80	140	4	13	- Ke/ru = 1/8	[71]
Ni/rutile	Crotonaldehyde	10	70		60		[72]
Pd-Cu/MgO	Furfural	6–8	80–130	0.5	100	98.7% selectivity of Furfuryl alcohol	[73]
Pt/MWNT	Furfural	20	150	5	75–100	Max Furfuryl alcohol selectivity: 79%	[74]
ReOx-Pd/CeO ₂	16 compounds	80	140	4	1–60	substrate 0.5 g, 1,4 dioxane 4 g, Wcat = 150 mg (2 wt% Re, 0.3 wt% Pd)	[75]
Rh- MoOx/SiO ₂ + CeO ₂	cyclohexanecarboxamide	80	140	4	89		[76]

Table 3. Cont.

Liao et al. [77] used CeO as support with different metals (Ni, Co, and Cu) for the hydrogenation in liquid phase of maleic anhydride at 50 bar and 210 °C, converting all the reactant after 60, 180, and 420 min, for Ni, Co, and Cu, respectively. Elliott al. [78] elaborated a reactivity scale of hydrogenation of different organic compounds in presence of CoMo and NiMo sulphided catalysts (see Figure 3) based on literature work [79]. Olefins, aldehydes, and ketones were hydrogenated at low temperatures as low as 150–200 °C, while the alcohols at 250–300 °C. Carboxylic and phenolic ethers reacted at around 300 °C.

Recently, copper catalysts have attracted much attention for the conversion of glycerol to propylene glycol because of their intrinsic ability to selectively cleave the C-O bonds in glycerol rather than the C-C bonds. To increase the activity of Cu metal, Cu-based catalysts such as Cu-Cr, Cu-Al, and Cu-Mg have been developed to promote the hydrogenolysis reaction. Bienholz et al. prepared a highly dispersed silica-supported copper catalyst (Cu/SiO₂) using an ion-exchange method and achieved 100% glycerol conversion with 87% propylene glycol selectivity at optimum conditions of 5 mL/h of 40 wt% aqueous glycerol solution, 255 °C, and 300 mL/min of H₂ at 15 bar [80]. Liu's group studied the glycerol hydrogenolysis over Ru-Cu catalysts supported on different support materials including SiO₂, Al₂O₃, NaY zeolite, TiO₂, ZrO₂, and HY zeolite. The best activity was observed for Ru-Cu/ZrO₂ with 100% glycerol conversion and 78.5% propylene glycol selectivity. The high activity of this catalyst was attributed to the synergistic effect of Ru in the catalyst related to hydrogen spill-over, while the high selectivity was attributed mainly to the low acidity of the support and the Cu amount [81]. The HDO of the Water soluble fraction of Bio-Oil (WBO) at different temperatures (220, 270, and 310 °C) at 190 bar, using 5 wt% Ru/C catalyst, was studied by de Miguel Mercader et al. [82], where the recovery of carbon in oil phase increased from 16.3 wt% to 38.5 wt%, when the temperature was increased from 220 to 310 °C. In another study, several lignin model compounds (phenol, m-cresol, anisole, guaiacol, and diphenyl ether) were tested for HDO reactions in presence of MoO₃ at atmospheric pressure and temperature between 150 and 250 °C [83]. The authors noted that, according to the bond dissociation energy, the highest catalytic reactivity was obtained 400 °C dibenzofuran diphenyl ethers 350 °C phenols phenolic ethers 300 °C carboxylic group dehydratation > olefins aliphatic alcohols 250 °C aliphatic esters 200 °C aldehydes and alcohols ketones olefins 150 °C

with diphenyl ether, but important carburization phenomena have been noted onto the catalyst surface.

Figure 3. Reactivity scale of organic compounds under hydrotreatment conditions. Adapted with permission from [78].

Bagnato et al. [84] prepared by impregnation technique a series of monometallic and bimetallic metal catalysts in which the zirconia was doped with Pd and not noble metals (Cu and Fe), characterized, and their performances studied in term of conversion and selectivity for key bio-compounds. Vanillin was completely converted after 80 min at 100 °C and 50 bar, in presence of PdFe/ZrO₂. Meanwhile, the PdFe reached the conversion of 65.5% and 20% for furfural to furfuryl alcohol and glucose to sorbitol (74% selectivity), respectively.

The authors noted that the bimetallic catalyst was able to improve the conversion than the monometallic, mainly due the adsorption mechanism onto the catalytic surface: the not noble metal favoured the bonding to the aldehyde group, while the noble metal favoured the hydrogen molecule adsorption.

Bergem et al. [67] investigated the HDO of a model WBO using Ru/TiO₂ and Ru/C catalysts in a packet bed reactor (PBR) at a temperature between 100 and 140 $^{\circ}$ C, ~62 bar. A completed conversion was noted already a 100 °C for compounds such as acetone, acetaldehyde, propionaldehyde, 2-propen-1-ol, 1-hydroxy-2-butanone, 3-hydroxy-2-butanone, 2hexanone, and 2-furanone. Other compounds such as furfural and hydroxyacetaldehyde required elevate temperature (>140 °C) for converting completely. Furthermore, the authors observed a decrement of catalyst activity, about 25% after 90 h, due at acid leaching. Sanna et al. [85] studied the HDO of a real WBO in presence of Ru/C and Pt/C catalysts in a two-stage continuous reactor. In the first stage, the reaction was carried out in presence of Ru/C catalyst at 125 °C, while in the second stage, it was carried out at a temperature between 200 and 250 °C with Pt/C, at 50 and 100 bar, and different weight hourly space velocities from 0.75 to $6 h^{-1}$. During the first low temperature stage, the unstable bio-oil functionalities were stabilized into alcohols, where the main products were ethylene glycol, propylene glycol, and sorbitol, losing 7% of carbon as gas and solid phase. Furthermore, the catalyst showed a constant activity for about 80 h. In the second-high temperature stage, 45% of the carbon was converted in gasoline blend stocks and C_2 to C_6 diols.

3.2. Kinetic Mechanism

The reactions involved during the hydrotreating of bio-oil have been widely studied [86–88], as shown below:

Hydrodeoxygenation	(HDO):	R - OH +	$H_2 \rightarrow I$	R - H +	$H_2O;$	(1)
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Hydrodesulphurisation (HDS): $R - SH + H_2 \rightarrow R - H + H_2S$; (2)

Hydrodenitrogenation (HDN) : $Pyridine + H_2 \rightarrow Pentane + NH_3;$ (3)

Hydrodealkylation :
$$R - C_6H_5 + H_2 \rightarrow C_6H_6 + R - H;$$
 (4)

Hydrocracking:
$$R_1 - CH_2CH_2 - R_2 + H_2 \rightarrow R_1 - CH_3 + R_2 - CH_3$$
; (5)

- Isomerisation of alkanes : $n alkane \rightarrow i alkane;$ (6)
 - Decarboxylation : $R CO OH \rightarrow R H + CO_2$; (7)
 - Decarbonilation : $R CHO \rightarrow R H + CO$; (8)
 - Water gas shift reaction : $CO_2 + H_2 \leftrightarrow CO + H_2O$; (9)

Coke formation :
$$polyaromatic \rightarrow coke$$
. (10)

In the following section, the reaction mechanisms of some of the most representative bio-oil compounds will be discussed.

3.2.1. Phenol

The phenol hydrogenation has been widely studied [89–93]. The reaction pathways are shown in Figure 4, where hydrogen reacts with the phenol (PHE) attacking the hydroxyl group to produce benzene with subsequent production of cyclohexene (CHE) and cyclohexane (CHO). Another reaction pathway of the aromatic ring is the formation of cyclohexanol (CXO) with consecutive hydrogenation in cyclohexene and cyclohexane. A further reaction pathway is represented by the formation of cyclohexanoe (COL) with subsequent cyclohexano in cyclohexene and cyclohexane. Finally, methylcyclopentane (MCP) can be produced by isomerization reaction.



Figure 4. Phenol hydrogenation pathways.

3.2.2. Guaiacol

Another representative compound in bio-oil is guaiacol that reacts forming phenol [39–43] via two paths: (1) direct demethoxylation; and (2) indirect reaction through demethylation to catechol with subsequent hydrogenation of the latter compound. The undesired polymerisation of guaiacol (GCL) (Figure 5) leads to coke formation.



Figure 5. Guaiacol reaction path.

Bindwal et al. [94] proposed a kinetic rate for the hydrogenation of guaiacol in 1,2 cycloexanediol in presence of 5% Ru/C catalyst according to the Langmuir–Hinshe–wood–Hougen–Watson (LHHW) model. The authors, according to the experimental data obtained, identified the limitation step for the reaction taking place on the catalyst surface, assuming the dissociative adsorption of H_2 . The reaction rate was described by the following equation:

$$r = \frac{k_{3,a}K_BC_B\sqrt{K_{H_2}C_{H_2}}}{\left(1 + \sqrt{K_{H_2}C_{H_2}} + K_BC_B\right)^2},$$
(11)

where $C_B C_{H2}$ are the molar concentration of guaiacol and hydrogen, respectively, $k_{3,a}$ the kinetic constant, K_B and K_{H2} are the adsorption constant of guaiacol and hydrogen.

3.2.3. Levoglucosan

The hydrolysis of levoglucosan has been studied in a solution of water and in the presence of Ru/C [95]. The path involves the production of glucose (hydrolysis reaction) with subsequent hydrogenation into sorbitol. Finally, ethylene glycol, 1,2-Propanediol, and 1,4-Butanediol are produced by the hydrogenation of sorbitol (Figure 6).



Figure 6. Levoglucosan reaction path.

Bindwal et al. [95] proposed a kinetic rate for the hydrogenation in presence of Ru/C, where the H_2 and levoglucosan (LG) chemisorbed and dissociated on the surface catalyst are as follows:

$$H_2 + X \leftrightarrow 2HX,$$
 (12)

$$LG + X \leftrightarrow LGX$$
, (13)

$$2HX + LGX \leftrightarrow products,$$
 (14)

represented by the following equation:

$$r = \frac{k_3 K_{H2} K_{LG} C_{H2} C_{LG}}{\left(1 + \sqrt{K_{H2} C_{H2}} + K_{LG} C_{LG}\right)^3}.$$
(15)

3.2.4. Other Compounds

Bindwal et al. [94] studied the kinetics rate of other compounds using 5% Ru/C catalyst to convert hydroxycetone, hydroxyacetaldehyde and 2-furanone in 1,2 propanediol, ethylene glycol and γ -butyrolactone, according to the reactions in Figure 7.



Figure 7. Hydrogenation of hydroxyacetone, hydroxyacetaldehyde, and 2-furanone.

The authors proposed different kinetics rates varying the limitation step and the possibility to have an atomic or molecular H_2 adsorption.

The kinetics rates hypothesized were validated experimentally confirming that the reactions are surface-reaction limited in presence of dissociative adsorption of H_2 . The equation for the kinetics rate were

$$r = \frac{k_3 \sqrt{K_{H_2} C_{H_2}} K_B C_B}{\left(1 + \sqrt{K_{H_2} C_{H_2}} + K_B C_B\right)^2},\tag{16}$$

$$r = \frac{k_3 K_{H_2} K_B C_{H_2} C_B}{\left(1 + \sqrt{K_{H_2} C_{H_2}} + K_B C_B\right)^3}.$$
(17)

Zhang et al. [96,97] described the reaction kinetics by dividing the products as Light oil ranged from 36 °C to 250 °C, heavy oil from 250 °C to 450 °C, vapors, water, and

coke. They assumed a series of parallel reactions with a first-order kinetics in presence of $CoMo/\gamma Al_2O_3$ catalyst.

$$Bio-oil \xrightarrow{k_1} light fraction oil,$$
(18)

$$Bio - oil \xrightarrow{k_2} heavy \ fraction \ oil \xrightarrow{k_4} light \ fraction \ oil, \tag{19}$$

$$Bio-oil \xrightarrow{k_2} heavy \ fraction \ oil \xrightarrow{k_5} gas + water + char,$$
(20)

$$Bio - oil \xrightarrow{k_3} gas + water + char.$$
 (21)

Furthermore, Sheu et al. [98] divided the bio-oil into six groups (heavy non-volatiles, light non-volatile, phenols, aromatics, alkanes, Coke + H_2O + Outlet Gases) and used three different catalysts (Pt/Al₂O₃/SiO₂, CoMo/ γ -Al₂O₃, and Ni-W/ γ -Al₂O₃) to study the hydrogenation of bio-oil. Moreover, the authors proposed a reaction pathway by series-parallels of first-order reactions.

heavy nonvolatiles
$$\underset{k_1}{\rightarrow}$$
 light nonvolatiles $\underset{k_2}{\rightarrow}$ phenols, (22)

heavy nonvolatiles
$$\underset{k_2}{\rightarrow} aromatics + alkanes,$$
 (23)

$$phenols \xrightarrow{k_4} aromatics + alkanes \xrightarrow{k_5} Coke + H_2O + outlet gases.$$
(24)

 k_i is a kinetic constant and depend of the temperature and pressure by

$$k_i = k_{i0} P^{n_i} \exp\left(-\frac{Ea}{RT}\right),\tag{25}$$

where k_{i0} and n_i are the parameters of the reaction and the catalysts used.

3.3. Reactor Technologies

3.3.1. Conventional Reactors

The hydrogenation reaction is largely used in refinery to convert the heavy oil fraction into light hydrocarbons. The existing process have been based on the following reactors: fixed beds (FBRs), moving beds (MBRs), and expanded or ebullated beds (EBRs). The main difference among the reactors involves the transport phenomena and some technical details.

The FBRs are the main reactor systems used commercially and used for hydrogenating light hydrocarbon mixture such as naphtha and middle distillate. The FBRs are designed for operating in an adiabatic condition. The reactor is divided into three catalytic zones separated to an inert material (ceramic balls), the liquid and gas stream through the first catalytic bed. The output fed exchange heat by the inert bed and subsequently quenched adding fresh gas reactant and then fed inlet of the second catalytic bed. The output of the second reactor is cooled again by the inert bed and by quenching. EBR reactors have been also used to hydrogenate feeds such as vacuum residue.

The EBRs are used for heavy feeds with a large amount of metals and asphaltenes, where the liquid and gas streams are fed from bottom expanding and mixing the catalyst bed, reducing the pressure drop effect. In the output of the catalytic bed the hydrogen not reacted is recycled, while the liquid products are recovered by a flash unit.

3.3.2. Membrane Reactor

The main disadvantage of hydrogenation reaction is represented by mass transport limitation, because the reaction takes place in contact with the gaseous, liquid, and solid phase. The system has to have a high operating pressure, improving the gas solubility into the liquid system and high temperature to advantage the kinetic, but at the same time, the H₂ solubility decreases under those conditions. A membrane reactor (MR) is an operation unit to produce new species by chemical reaction and separation process in a single equipment [99]. The use of MRs can reduce the process footprint, since the plant will be more compact and can result in lower investment costs, improving the economics of the process [100,101].

In a MBR, the fresh catalyst is fed from the top and trough the reactor, while the reactant stream is fed from the bottom. Afterthought, the products leave the MBR and the deactivated catalyst is sent to the regenerator reactor, where the coke deposition is burned and the activated catalyst returns to MBR.

One of the features of the MRs is to act as a contactor between the three phases during HDO reaction. Furthermore, the membrane can have catalytic activity chancing the product distribution as reported by Liu et al. [102], who compared packed bed MR and catalytic MR for the hydrogenation of nitrobenzene in presence of Pd/ γ -Al₂O₃ catalyst. The CMMR showed best performance in term of conversion and catalytic stability (~85% for 10 h) as shown in Figure 8.



Figure 8. Comparison between catalytic membrane reactor (CMR) and packed bed membrane reactor (PBMR) [102].

Liu et al. [103] studied the selectivity hydrogenation of butadiene in butene at 40 °C and 10 bar by catalytic membrane reactors (CMRs), obtaining a butene selectivity higher than 99% and butadiene concentration in the output stream lower than 10 ppm. Another example of hydrogenation reaction is reported in Table 4. Despite the increasing interest in catalytic membranes, the HDO of bio-oil in MR is a novelty, since in literature there is only one article [104] available on the topic, where the authors used a MR for the hydrogenation of levulinic acid (compound present in bio-oils) by a porous expanded polytetrafluoroethylene (ePTFE) membrane with Ru catalyst particles. Moreover, the same membranes were coated only in one side with a dense Matrimid layer, which was used to control the hydrogen flux through the membrane. The reaction was studied in a temperature and reaction pressure between 40 and 90 °C and 0.7 and 5.6 bar, respectively. Furthermore, the authors compared the result obtained with a PBR as shown in Figure 9, where the kinetic rate is presented as ratio of gamma-valerolactone product (g/h) over grams of Ru. In particular, the MR without the Matrimid layer obtained the best performance (four times more than PBR) with a conversion of 0.0065%, while the MR with the control layer (Matrimid) showed a kinetic rate two times less than the PBR.

Recent studies have emphasized the functionality of MR to be able to achieve a TOF equal to 48,000 h^{-1} for the partial hydrogenation of furfural in presence of Ru–polyethersulfone (PES) catalytic membrane at 70 °C and 7 bar [105].



Figure 9. Kinetic rate of hydrogenation of levulonic acid using membrane reactors (MRs) and a packet bed reactor (PBR) [104].

Hydrogenation of	Catalyst	Support		Pressure (bar)	Temperature (°C)	Ref.
3-hexyn-1-ol	Pd nanoparticles (4.6 nm)	zirconia/polyvinyl alcohol	Batch	5-10	25	[106]
Nitrite	Pd	γ -Al ₂ O ₃	Continuous	1	25	[107]
Methylenecyclohexane (and isomerization)	Pt, Pd, Ru in γ -Al ₂ O ₃	macroporous α -Al ₂ O ₃	Continuous	1.5 liquid 2 gas	15-70	[108]
Methylenecyclohexane	Pd-PVDS PVP	macroporous α-Al ₂ O ₃	Continuous		25-50	[109] *
Edible oil	Pd, Pt	porous polyamideimide (PAI)	Continuous	4	100	[110]
Nitrobenzene	Pd	zirconia/polyvinyl alcohol	Continuous	1–2	25	[111]
Nitrobenzene	Pd/γ - Al_2O_3	PDMS	Continuous	1–2	20	[102]
Butadiene	PVP-Pd, PVP-Pd, EC-Pd, AR-Pd, AR-Pd, PVP-Pd, PVP-Pd-0.5 Co(OAc) ₂ , PVP-Pd-0.5 Co(OAc) ₂	CA, PSF, CA, CA, PSF, CA, CA, CA	Continuous	10	40	[103] **
Furfural	Ru	PES	Continous	7	70	[105]

Table 4. MR for hydrogenation reaction.

* Ceramic membrane showed a higher selectivity toward the hydrogenated product than the polymeric membrane but exhibited a lower TON (= converted moles in a second per gram of Pd) value. ** PVP-Pd-0.5 Co(OAc)₂ showed best performance. The presence of Co inhibited isomerization reaction.

4. Concluding Remarks and Future Outlook

The valorization of biomass and residues for the production of liquid fuels by both thermochemical (e.g., pyrolysis) or physical (e.g., pressing) methods has attracted a great attention from both scientific and technological point of view. In fact, the utilization of vegetable raw materials for the production of synthetic chemical intermediates and hydrocarbons is considered one of the most investigated strategies aimed at reducing both the carbon dioxide emissions and the dependence on fossils fuels.

In this review, we summarize the main aspects related to pyrolysis and to the properties of the obtained bio-oils, focusing great attention to the hydrotreatment process alternatives for converting the pyrolysis bio-oil into drop-in fuel.

Research studies usually are focused on the pyrolysis of a well-defined biomass, while a limited number of papers are devoted to biomass residues with variable composition. The former approach is useful for understanding the complex mechanism involved during the pyrolysis and the effect of process parameters on reaction pathways, while the latter is
of paramount importance for developing the technology at a pilot and demonstrative scale. In fact, the compositional variations in the feedstock modify both yield and composition of bio-oil, and this aspect has a significant impact on the viability of the process. As previously mentioned, biomass availability at a low cost is one of the biggest challenges of biorefinery. Therefore, more effort should be put on the experimental investigation at a pilot and demonstrative scale on the production of bio-oil from biomass residues with a large compositional variability. The research is also focused on the role of biomass pre-treatment on bio-oil quality. In particular, physical, chemical, and thermal methods may be adopted. As an example, the modification of size and shape of biomass particles has an effect on heat transfer with an impact on bio-oil quality. Whereas, the reduction of hemicellulose by a thermal method, such as torrefaction, decreases the amount of organic acids, acetals, and water in the bio-oil, with a positive impact on bio-oil stability, but with a higher inorganics content. The amount of inorganics may be reduced by physical pre-treatment such as biomass washing with water or acids. Unfortunately, there is a lack of information and knowledge about the economic feasibility of the biomass pre-treatment methods. Another important aspect that should be investigated in more detail is the stability of produced bio-oil. In fact, the bio-oil is a complex mixture containing water and both polar and nonpolar organics that cause several reactions, e.g., oligomerization condensation and dehydration, with aging of the bio-oil and formation of a more complex multiphase systems. The addition of alcohols, such as methanol, usually improves stability, homogeneity, and viscosity of bio-oil. Further research on bio-oil stabilization is needed to address technical issues during bio-oil storage and processing.

This review aims to summarize recent advances on the conversion to pyrolysis bio-oil into drop-in fuels by catalytic hydrogenation. In this regard, the research efforts should be better focused on (i) catalytic assessment of novel catalysts, and (ii) experimental investigation at pilot and demonstrative scale of hydrotreatment of real bio-oil. Concerning the first point, several metals and metals supported over moderately acid solids have been investigated. Ni-Mo or Co-Mo bimetallic systems supported over gamma-alumina are the most investigated catalysts for hydrotreatment, since they are well-known catalysts for hydroprocessing oil-derived streams, i.e., hydrodesulphurization. In these systems, Mo represents the active phase for the removal of heteroatoms, while Ni or Co acts as promoters for the hydrogenation step. Several alternative catalysts have been studied mostly for the hydrogenation of model compounds, whose catalytic behavior is in part discussed in this review. For instance, different metals and different supports have been studied, while a less attention was paid to the design of innovative hybrid systems, where the catalytic functionalities requested by the process, e.g., redox, acids, are carefully tuned with the aim to improve catalyst effectiveness. In this regard, research should be also devoted to the study of reaction mechanism as a function of surface properties of the catalysts. This approach has brought advances in other fields, such as hydrogenation of carbon dioxide to synthetic fuels, and it may be useful for a better understanding of catalysis of hydrogenation of bio-oils.

Nevertheless, bio-oil strongly differs from typical crude oil derived streams, due to the presence of a large amount of oxygenated compounds, e.g., carboxylic acids, phenols, aldehydes, ketones, sugars, and water. For this reason, the physic-chemical features of the catalyst for hydrotreatment of bio-oil should be carefully tuned as a function of biooil composition. On the contrary, a limited number of studies were carried out on the hydrotreatment of real pyrolysis bio-oil. In that case, the number of variables and the issues strongly increase. As an example, the presence of unsaturated oligomers in real bio-oil may lead to the formation of coke with deactivation of the catalyst. Therefore, future focus should be on the separation of bio-oil fractions in order to assess the most suitable bio-oil cut for hydroprocessing. In fact, the presence of oligomers inevitably causes a large amount of coke formation with catalyst deactivation. Of course, the presence of an additional step between pyrolysis and hydrotreatment has a significant effect on the process costs. The experimental investigation of hydrotreatment of bio-oil fractions at an either pilot or demonstrative scale may push towards more research in the field of bio-oil pre-treatments, as well as address also challenges, such as hydrogen consumption. In fact, most of the papers on hydrotreatment of bio-oil or bio-oil models are focused on product yield and quality, but it is difficult to find quantitative information on hydrogen consumption, which is usually used in large excess. As in the case of pyrolysis step, investigations at scales larger than laboratory of hydrogenation steps may surely provide quantitative data useful for viability studies on the production of drop-in fuels from biomass via pyrolysis.

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Abbreviations

BNZ	Benzene
CHE	Cyclohexene
CHO	Cyclohexanol
CMR	Catalytic membrane reactor
COL	Cyclohexanone
CXO	Cyclohexanol
Ea	Activation energy
EBR	Ebullated bed reactor
EG	Ethylene glycol
γ-BCT	γ-Butyrolactone
GCL	Guaiacol
GCS	Glucose
HDO	Hydrodeoxygenation reaction
HD	Hydrotreating
HTL	Hydrothermal liquefaction
HXD	Hydroxyacetaldehyde
HXE	Hydroxyacetone
k	Kinetic rate
k0	Pre-exponential number
LG	Levoglucosan
LHHW	Langmuir-Hinshelwood-Hougen-Watson
LHSV	Liquid hourly space velocity
MR	Membrane reactor
MBR	Moving bed reactor
MCP	Methylcyclopentane
n	Kinetic order
PBR	Packet bed reactor
PBMR	Packed bed membrane reactor
PCL	Pyrocatechol
PHE	Phenol
SOB	Sorbitol
TEA	Techno-economical assessment
TOF	Turnover of frequency
WBO	Water soluble bio-oil fraction
1,2-PDO	1,2-Propanediol
1,4-BDO	1,4-Butanediol
2-FN	2-Furanone

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Article



Syntheses, Characterization, and Application of Tridentate Phenoxyimino-Phenoxy Aluminum Complexes for the Coupling of Terminal Epoxide with CO₂: From Binary System to Single Component Catalyst

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Abstract: A series of binuclear aluminum complexes **1–3** supported by tridentate phenoxyiminophenoxy ligands was synthesized and used as catalysts for the coupling reaction of terminal epoxide with carbon dioxide. The aluminum complex 1, which is catalytically inactive toward the coupling of epoxide with CO_2 by itself, shows moderate activity in the presence of excess nucleophiles or organic bases at high temperature. In sharp contrast to complex **1**, bifunctional complexes **2** and **3**, which incorporate tertiary amine groups as the built-in nucleophile, are able to efficiently transform terminal epoxide with CO_2 to corresponding cyclic carbonates as a sole product by themselves at 100 °C. The number of amine groups on the ligand skeleton and the reaction temperature exert a great influence on the catalytic activity. The bifunctional complexes **2** and **3** are also active at low carbon dioxide pressure such as 2 atm or atmospheric CO_2 pressure. Kinetic studies of the coupling reactions of chloropropylene oxide/ CO_2 and styrene oxide/ CO_2 using bifunctional catalysts under atmospheric pressure of CO_2 demonstrate that the coupling reaction has a first-order dependence on the concentration of the epoxide.

Keywords: aluminum complex; CO2 fixation; bifunctional catalyst; cyclic carbonate

1. Introduction

With the rapid development of the industry as well as the ever-growing human activity, a huge amount of CO_2 has been released to the air, which has caused severe environmental problems [1-4]. The utilization of CO₂ as feedstock to produce valuable chemicals is a promising way to solve this problem, but this conversion is limited due to the inertness of CO_2 [5]. The catalytic coupling reaction with epoxides represents one of the promising processes employing CO_2 to produce organic cyclic carbonate, which has found widespread applications in many respects [6–10]. Generally, the catalyst capable of achieving the transformation is comprised of nucleophile and Lewis acid. Thus, organic compounds and metal-based complexes have been employed as the Lewis acid for the coupling reaction, with the aid of nucleophiles to constitute the binary catalytic system. Usually, metal-based complexes display higher reactivity than organocatalysts for the coupling reaction. As a result of the diversity of the metal across the periodic table and the organic ligands of different structures, miscellaneous metal complexes based on aluminum [11–32], magnesium [33–36], chromium [37–42], cobalt [43–48], iron [49–53], and rare earth metals [54,55] have been innovated for the coupling reaction of CO₂ with epoxides. Of many metal complexes, aluminum complexes have been drawing attention due to their low price, easy availability, and the superior selectivity for the cyclic carbonate



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Copyright: © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). over polymeric products [56]. It is well established that the electronic effects and steric hindrance around the aluminum center that can be finely tuned are crucial for the catalytic activity and the product selectivity. For example, optically active carbonate can be produced from the coupling of racemic epoxide with CO₂ when the chiral complexes are employed [44,45,57].

In addition to binary catalytic system, there is a tendency to employ a bifunctional catalyst in which nucleophile and Lewis metal complexes are constructed into one molecule as the one-component catalyst for the coupling of CO_2 with epoxides in the past decade [58–68]. Quaternary ammonium halide as a nucleophile is usually integrated into the metal complex to construct an ionic bifunctional catalyst. The pre-association of the nucleophilic halide to the metal complex via electrostatic attraction would effectively reduce the translational entropy penalty at the ring-opening step and the cyclization step as compared with the binary catalytic system [69]. Thus, the bifunctional catalyst loading for the coupling reaction is significantly reduced, and usually, a higher catalytic reactivity is achieved than that with the corresponding binary catalytic system. However, the incorporation of the quaternary onium salts into the metal complex impairs the solubility of the bifunctional catalyst. Another drawback is the thermostability of the ammonium halide-functionalized catalyst at elevated temperature [59], which undergoes ammonium salt decomposition pathways, including Zaitsev and Hoffman type eliminations [70-72] and retro-Menschutkin reactions [73–76]. Hence, it is important and necessary to develop bifunctional catalyst of high efficiency and stability at elevated temperature.

In this work, we present the syntheses of a series of aluminum complexes supported by novel tridentate phenoxyimino-phenoxy ligands and their catalytic behaviors for the coupling of terminal epoxides with CO₂. Compared with tetradentate salen-type ligand stabilized metal complexes, which are extensively employed for the coupling of epoxide with CO₂, aluminum complexes supported by tridentate ligands for this transformation are rare. As a result of the low coordination number of tridentate ligands, the resultant complexes are expected to have a more acidic metal center, which is supposed to benefit the activation of the epoxide ring and to facilitate the ring-opening. Moreover, an amine group was incorporated onto the ligand framework as the built-in nucleophile to construct neutral bifunctional complexes **2** and **3**, in order to avoid the decomposition of ammonium halide moiety under elevated temperature. Systematic investigation of the catalytic behaviors of the aluminum complexes **2** and **3** reveals that the neutral and ionic bifunctional complexes are highly active toward the coupling of epoxide to CO₂, whereas the unfunctionalized aluminum complex 1 is catalytically inactive by itself.

2. Results and Discussion

2.1. Syntheses and Characterization of Complexes 1-3

The tridentate ligand precursors $H_2L^1-H_2L^3$ (see Scheme 1) were readily synthesized by reacting the substituted salicylaldehyde with substituted aminophenol in 1:1 molar ratio (see the experimental section in the supporting material). The three ligand precursors were identified by proton nuclear magnetic resonance (¹H NMR) and ¹³C-nuclear magnetic resonance (¹³C NMR) (Figures S1–S3 in the supporting material).



Scheme 1. The syntheses of complexes 1–3.

Subsequent syntheses of complexes 1-3 were conducted by the alkyl-elimination reaction of Et₂AlCl with the corresponding ligand precursors at low temperature, as illustrated in Scheme 1. In a typical procedure, a tetrahydrofuran (THF) solution of H_2L^1 was added dropwise to a stirred hexane solution of AlEt₂Cl at -30 °C to afford a yellow solution. The reaction was slowly warmed up to room temperature and stirred for another 4 h. After the removal of all the volatiles under reduced pressure, yellow solids were separated, which was followed by washing with cold hexane three times and drying to constant weight under vacuum. The structure of the isolated solids was characterized by the NMR technique with CDCl₃ as the solvent. The ¹H NMR spectrum shows no resonances of hydroxy groups or ethyl groups bound to aluminum. In the low field, the resonance of 8.06 ppm assignable to the imino moiety was observed, which slightly shifted to the low field when compared with that in free ligand precursor H_2L^1 (see Figure S4 in the supporting material). Two distinct resonances of 1.32 ppm and 0.84 ppm for the tBu groups were found (1.49 and 1.35 ppm in the H_2L^1), indicating chelation of the tridentate ligand to aluminum. Moreover, the upfield shift of the imino group in the H_2L^1 from 8.72 to 8.06 ppm in the isolated complex suggested the coordination of nitrogen of the imino group to the aluminum center. Remarkably, no solvent molecules were detected in the ¹H NMR spectrum, suggesting that the isolated complex is THF-free.

In addition to the characterization by NMR, mass spectrometry (MS) was employed to characterize the isolated complex. A very weak peak at m/z = 350.1566 was detected, which corresponds to the cationic species **1a** having the formula of C₂₁H₂₅O₂NAl, as shown in Scheme 2. Interestingly, a strong signal was observed at m/z = 414.2219, which was assigned to the cationic species 1b with the formula of C₂₃H₃₃O₄NAl. We supposed that the species **1b** was generated by the coordination of two methanol molecules to the cationic species **1a**. Thus, it is reasonable to interpret the weak signal of **1a** and the strong peak of **1b** on the mass spectrum. In the light of the strong signal of **1b** on the MS, no solvent detection on the ¹H NMR spectrum, and the coordination number of 5 usually adopted by aluminum complex, we expected that complex **1** should be a binuclear structure, with each aluminum center being surrounded by a phenoxyimino-phenoxy ligand and two chlorides, as presented in Scheme 2.



Scheme 2. Possible pathway for the formation of cationic species 1a and 1b.

Similarly, treatment of the ligand precursors H_2L^2 and H_2L^3 with AlEt₂Cl under low temperature resulted in the formation of bifunctional complexes **2** and **3**. The characterization of complex **2** by ¹H NMR showed the successful alkyl elimination between AlEt₂Cl and H_2L^2 . Moreover, there are no THF molecules detected on the ¹H NMR spectrum, suggesting that complex **2** is THF-free. The MS spectrum of complex **2** shows a *m*/*z* peak positioning at 397.1085. We tentatively ascribed this signal to the structure **2a**, which probably is an ethanol coordinated species, as illustrated in Figure 1. Meanwhile, a peak

at m/z = 783.3226 was detected, which is ascribed to the cationic species **2b**. Although a tertiary amine group is introduced into the molecule, the inner coordination of the amine group to the Al center is impossible because of the orientation of the tertiary amine group. Taking into account the coordination saturation of the aluminum, it is reasonable to assume the complex **2** adopts binuclear structure with dangling tertiary amine groups. Similar results were also observed for complex **3**, as indicated by the ¹H NMR and MS, which should also adopt a binuclear structure with dangling amine groups via chloride bridges.



Figure 1. Possible structures of cationic species of 2a and 2b found in the MS of complex 2.

2.2. Catalytic Performance of Complexes 1-3 in the Coupling Reactions of Terminal Epoxide with CO_2

To begin with, we examined the catalytic performance of complex 1 for the coupling of propylene oxide (PO) with CO₂ (see Scheme 3). Unfortunately, complex 1 was catalytically inactive by itself, which was in agreement with the previous literature reports [21,22]. When it was paired with a nucleophile or organic base, complex 1 showed moderate activity for the PO/CO_2 coupling (see Tables S1–S4 in the supporting information). For instance, complex 1 in combination with tetrabutylammonium bromide (TBAB, 40 eq) catalyzed the PO/CO2 coupling to produce propylene carbonate (PC) as the sole product at 80 °C under 20 atm CO₂ in 10 h with 91% PO conversion (see entry 8 in Table S1). There was no detection of any polymeric products as evidenced by the ¹H NMR spectrum of the reaction mixtures. It was also interesting to find that the complex 1/TBAB (40 eq) system displayed a zeroth-order dependence on the PO throughout the coupling (see Table S2 and Figure S7, in the supporting material). This result is analogous to Han's report in which polymeric ionic liquid was employed as the catalyst for the PO/CO_2 coupling reaction [77]. When other organobases such as 4-dimethylaminopyridine (DMAP) or 1-methylimidazole (1-MeIm) were employed as the cocatalysts, high cocatalyst loading was required for effective transformation (see Tables S3 and S4 in the supporting material). For instance, the binary system composed of complex 1/DMAP (1/20) displayed lower catalytic activity than complex 1/TBAB (1/20) at 60 °C.



Scheme 3. This is a figure. Schemes follow the same formatting.

It has been reported by North and Pasquale that quaternary ammonium halide would decompose at high temperature to generate tertiary amine and halohydrocarbon [78]. The in situ generated tertiary amine, together with the remaining ammonium halide salts, assists the metal complex to convert propylene oxide and CO₂ to cyclic carbonate. Recently, Kim and his coworkers reported the coupling of epoxide with CO2 catalyzed by a series of tertiary amines with moderate catalytic activity [79]. These results enlightened us to design amine-functionalized complex 2 as the single-component catalyst for the coupling of epoxide with CO₂. The catalytic results were compiled in Table 1. It was satisfying that the bifunctional complex 2 by itself succeeded in transforming the CO₂ and PO to PC. Analysis of the reaction mixture showed that PC was exclusively produced without the formation of any polymeric products as evidenced by ¹H NMR spectrum. Although complex 2 displayed very low activity at 80 $^{\circ}$ C (entries 1 and 2, in Table 1), however, the catalytic activity was considerably enhanced when the reaction was conducted at 100 °C. For instance, 68% of PO was converted to PC under 10 atm CO₂ in 10 h (entry 3, Table 1). In addition to the reaction temperature, increasing the CO₂ pressure accelerates the coupling reaction. Then, 94% of PO was transformed to PC at 20 atm CO₂ pressure within 10 h (entry 4, Table 1), suggesting that high CO₂ pressure, namely, the high CO₂ concentration facilitated the coupling reaction.

Table 1.	The coupling	reaction of termi	nal epoxide wit	th CO ₂ by the s	ole complex 2 ¹ .
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Entry	Epoxide	P(CO ₂) (atm)	Temperature (°C)	Time (h)	Conversion ² (%)
1	PO	10	80	10	7
2	PO	20	80	10	8
3	PO	10	100	10	68
4	PO	20	100	10	94
5	BO	10	80	10	7
6	BO	20	100	10	49
7	CPO	10	80	10	12
8	CPO	20	80	10	26
9	CPO	10	100	5	36
10	CPO	10	100	10	52
11	CPO	10	100	24	90
12	CPO	20	100	5	40
13	CPO	20	100	10	62
14	SO	10	100	5	5
15	SO	10	100	10	11
16	SO	10	100	18	32
17	SO	10	100	24	75
18	SO	20	100	5	7
19	SO	20	100	10	15

 $\overline{1}$ Conditions: Complex 2 (38.7 mg, 50 μ mol), $n_{(2)}/n_{(epoxide)} = 1/1000$. ² Determined by ¹H NMR; No polymeric products were discovered as evidenced by ¹H NMR.

Subsequent examination of the catalytic performance of complex **2** in other terminal epoxides/CO₂ coupling reactions confirmed again the significance of the reaction temperature and CO₂ pressure. The 1,2-butylene oxide (BO) conversion of 7% at 80 °C under 10 atm CO₂ was improved to 49% when the reaction was performed at 100 °C under 20 atm of CO₂ pressure (entries 5 and 6, Table 1). Similar trends were also observed for the coupling of CO₂ with epichlorohydrin (or chloropropylene oxide, abbreviated as CPO) or styrene oxide (SO). The CPO conversion of 12% at 80 °C under 10 atm of CO₂ in 10 h was enhanced to 36%, 52%, and 90% within 5, 10, and 24 h, respectively, when the reaction temperature was simply increased to 100 °C (entries 7, 9–11, Table 1). As the CO₂ pressure was increased to 20 atm, the conversion of CPO rose to 40% in 5 h and 62% in 10 h under 20 atm CO₂ (entries 12 and 13, Table 1). As for the SO/CO₂ coupling, the reaction was quite sluggish

(entries 14–19, Table 1). High SO conversion can only be achieved after a long reaction time (entry 17, Table 1).

Complex 2 was capable of transforming CPO/CO₂ and SO/CO₂ to cyclic carbonate under atmospheric CO₂ pressure. The results were collected in Table 2, and the kinetic curves (conversion vs. reaction time) were depicted in Figure 2. As expected, the rate of the coupling of CO₂ with either CPO or SO under 1 atm CO₂ was extremely slow, which was partly due to the low CO₂ pressure. As can be seen from Figure 2, there is a surge in the CPO conversion after 36 h (the blue curve). This might be interpreted by the poor solubility of complex 2 in CPO. Therefore, the metal complex 2 was not well dispersed in the epoxide, leading to a heterogeneous system. Thus, the effective concentration of complex 2 was lower than the theoretical value at the beginning. With the proceeding of the coupling reaction, highly polar cyclic carbonate was generated, which in turn acted as solvent to dissolve complex 2. Thus, the effective concentration of complex 2. This would accelerate the coupling, as is shown in Figure 2 (the blue curve). A similar situation took place in the case of SO/CO₂ coupling as well, where the reaction rate gradually increased with the reaction time, as indicated by the kinetic curve (the red curves in Figure 2).

Table 2. Complex **2** catalyzed chloropropylene oxide (CPO)/CO₂ and styrene oxide (SO)/CO₂ coupling under atmospheric CO₂¹.

Entry	Epoxide	Time (h)	Conversion (%)
1	СРО	5	6
2	CPO	10	11
3	CPO	24	28
4	CPO	36	35
5	CPO	48	68
6	SO	5	0.7
7	SO	10	2
8	SO	24	9
9	SO	36	17
10	SO	48	30
11	SO	60	42

 $\frac{1}{1}$ Conditions: Complex 2 (38.7 mg, 50 µmol), $n_{(2)}/n_{(epoxide)} = 1/1000$, $P(CO_2) = 1$ atm, temperature is 100 °C. Other notes are the same as those in Table 1.



Figure 2. Kinetic curves (substrate conversion vs reaction time) of the coupling of CPO/CO₂ and SO/CO₂ by complex **2** under atmospheric CO₂ pressure at 100 °C.

The success of complex **2** as a single-component catalyst motivated us to examine the catalytic performance of complex **3**, which has more tertiary amine groups on the ligand skeleton for the coupling of epoxides toward CO_2 . The catalytic results were collected in Table 3. As anticipated, complex **3** displayed higher activity than complex **2** did under the

same conditions, which was tentatively attributed to the incorporation of one more amine group. Similar to complex **2**, complex **3** exhibited low activity at 80 °C. For example, 14% of PO was transformed to PC under 20 atm CO_2 in 10 h (entry 1, Table 3). However, the catalytic activity was dramatically improved by increasing the temperature to 100 °C, with the 64% conversion of PO in 5 h, and 99% in 10 h (entries 2 and 3, Table 3). The significance of reaction temperature was also observed in the BO/CO₂ coupling. The BO conversion of 5% at 80 °C was dramatically increased to 76% when the reaction temperature was increased to 100 °C at 10 atm CO₂ pressure (entries 4 and 5, Table 3). Similarly, enhancing the CO₂ pressure to 20 atm gave rise to 95% of BO conversion in 10 h (entry 6, Table 3), which was much higher than that of the coupling reaction catalyzed by complex 2 (entry 6, Table 1).

Entry	Epoxide	P(CO ₂) (atm)	Temperature (°C)	Time (h)	Conversion (%)
1	PO	20	80	10	14
2	PO	20	100	5	64
3	PO	20	100	10	99
4	BO	10	80	10	5
5	BO	10	100	10	76
6	BO	20	100	10	95
7	CPO	20	100	5	92
8	CPO	20	100	10	98
9	SO	20	100	10	50
10	SO	20	100	24	99

Table 3. The coupling reaction of terminal epoxide with CO_2 by the sole complex **3**¹.

¹ Conditions: Complex 3 (44.4 mg, 50 μ mol), $n_{(3)}/n_{(epoxide)} = 1/1000$. Other notes are the same as those in Table 1.

Complex **3** displayed high catalytic activity for the CPO/CO₂ and SO/CO₂ coupling. Taking the CPO/CO₂ coupling as an example, complex **3** converted 92% of CPO in 5 h at 100 °C under 20 atm of CO₂ to produce the corresponding carbonate (entry 7, Table 3), and a higher conversion rate of 98% was achieved in 10 h (entry 8, Table 3). When SO was used as the substrate, 50% of the SO was converted to the corresponding cyclic carbonate in 10 h at 100 °C under 20 atm of CO₂ (entry 9, Table 3). Nearly complete conversion of SO was achieved by extension of the reaction time to 24 h (entry 10, Table 3).

Complex 3 also displayed high activity toward CPO/CO₂ coupling under low CO₂ pressure. For example, 85% of CPO was converted to cyclic carbonate at 100 °C within 5 h under constant 2 atm CO₂ pressure (entry 1, Table 4). Prolonging the reaction time to 10 h gave rise to the nearly complete conversion of CPO (entry 2, Table 4). Complex 3 was still active under atmospheric CO₂ pressure, but the activity dropped sharply. For example, the conversion of CPO was only 28% in 5 h and 55% in 10 h (entries 1 and 2, Table 4), owing to the low concentration of CO₂ dissolved in CPO. By further extending the reaction time, high conversion of CPO was achieved (entries 3–6, Table 4). However, for SO/CO₂ coupling, complex 3 displayed very low activity. The conversion of SO was only 26% in 10 h when the reaction was performed at 100 °C, maintaining the CO₂ pressure at constant 2 atm (entry 7, Table 4). Lower SO conversion was expected, as the reaction was carried out at atmospheric CO₂ pressure. Analogous to CPO/CO₂ coupling, a high conversion of SO can be achieved by extending the reaction time (entries 8–14, Table 4).

Entry	Epoxide	P(CO ₂) (atm)	Time (h)	Conversion (%)
1	CPO	2	5	85
2	CPO	2	10	98
3	CPO	1	5	28
4	CPO	1	10	55
5	CPO	1	24	83
6	CPO	1	36	91
7	SO	2	10	26
8	SO	1	5	10
9	SO	1	10	19
10	SO	1	24	50
11	SO	1	36	82
12	SO	1	48	92
13	SO	1	60	96

[ab]	e 4.	The co	upling o	f epoxide/	$'CO_2$	under	low	CO_2	pressure	by comp	olex 3	T
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¹ Conditions: Complex 3 (44.4 mg, 50 μ mol), $n_{(3)}/n_{(epoxide)} = 1/1000$, the temperature is 100 °C. Other notes are the same as those in Table 1.

Kinetic studies of the coupling reactions of CPO/CO_2 and SO/CO_2 at atmospheric CO_2 pressure by complex 3 are plotted in Figure 3. It is clear that the CPO/CO₂ coupling is faster than the SO/CO₂ coupling under the same conditions (the blue curves in Figure 3). It is worth noting that the coupling of CPO/CO_2 has a first-order dependence on CPO concentration throughout the coupling reaction, as illustrated in Figure 3 (the red dash line, -ln(1-Conversion) vs. time). This may indicate a better solubility of complex 3 in CPO than that of complex 2, which was tentatively ascribed to the incorporation of more amine groups on the ligand framework. Differing from CPO/CO_2 coupling, the kinetic curve (-ln(1-Conversion) vs. time) of SO/CO₂ coupling shows an increase in the slope during the early stage of the reaction (the red dot curve in Figure 3), reflecting the heterogeneous nature of the system owing to the poor solubility of complex 3 in SO. As the reaction proceeded, more SC was produced, which in turn helped to dissolve complex 3, increasing the catalyst concentration and speeding up the coupling reaction. After some time, complex 3 was totally dissolved, forming a homogeneous system and maintaining constant concentration. Thus, a linear relationship was observed at the late stage of the coupling reaction, demonstrating a first-order dependence on SO concentration. The linear relation at the late stage also suggested the high stability of complex 3 under elevated temperature such as 100 °C.



Figure 3. Kinetic curves of CPO/CO₂ and SO/SO₂ coupling catalyzed by complex 3 at 100 $^{\circ}$ C at atmospheric CO₂ pressure.

3. Materials and Methods

2-aminophenol (99%), 4-tertbutylphenol, aqueous dimethylamine solution (40 wt%), 3,5-ditertbutylsalicyaldehyde (98%), and diethyl aluminum chloride (1 mol/L, in hexane) were purchased from Energy Chemical (Anqing, China) and used as received. Propylene oxide, 1,2-butylene oxide, epichlorohydrin, and styrene oxide obtained from Energy Chemical (Anqing, China) were distilled over CaH₂ before use. THF and hexane were pre-dried over 4 Å molecular sieves before distillation over sodium with benzophenone as the indicator under an argon atmosphere and stored over freshly cut sodium in a glovebox. CO₂ (99.999% purity) was purchased from Shenyang Hongsheng Gas Limited Corporation, Suzhou, China. Ethanol and formic acid were used as received without further handling.

General procedures: All reactions sensitive to air and moisture were carried out in a glovebox filled with dry argon. Proligands $H_2L^{1-}H_2L^{3}$ were synthesized according to the literature methods and structurally identified by ¹H NMR and ¹³C NMR [24]. The aluminum complexes 1–3 were prepared by equimolar reaction of the proligands with AlEt₂Cl in a glovebox filled with argon. The structures of complexes 1–3 were characterized by ¹H NMR, ¹³C NMR, and MS. The coupling of epoxide with CO₂ was carried in a stainless-steel autoclave equipped with a magnetic stirring bar. The reaction mixture was analyzed by the ¹H NMR spectra with CDCl₃ as a solvent. The ¹H and ¹³C NMR spectra were recorded using Bruker AVANCE III 500 MHz spectrometer (Billerica, MA, USA). Mass spectra of complexes 1–3 were obtained in the electrospray positive mode (ESI+) on Thermo LTQ Orbitrap XL spectrometer (Waltham, MA, USA), samples were diluted in methanol or ethanol, at DUT Chemistry Analysis & Research Centre, Dalian University of Technology (Dalian, China).

3.1. Coupling Reaction of Epoxide with CO₂ by Aluminum Complex 1

The typical procedure for the coupling of PO with CO_2 by complex 1 under elevated pressure is as follows. Complex 1 and cocatalyst were dissolved in PO in a Schlenk tube. Then, the solution was transferred via syringe into the pre-dried autoclave under CO_2 atmosphere. Then, the autoclave was pressurized with CO_2 and heated. After the designated time, the autoclave was cooled in an ice bath. The excess of the CO_2 was vented out. The conversion of PO was determined by GC analysis and ¹H NMR of the reaction mixture, and the yield was calculated based on isolated propylene carbonate. The results showed that the GC result was consistent with that by weight analysis of the PC.

3.2. Coupling Reaction of Epoxide with CO₂ by Bifunctional Aluminum Complexes

The typical procedure for the coupling of PO with CO₂ by complex **2** or **3** under elevated pressure is as follows. Complex **2** (38.7 mg, 50 μ mol) was first placed in the predried autoclave. After the internal atmosphere of the autoclave was displaced by CO₂ three times, PO was injected, which was followed by charging CO₂ to 20 atm. Then, the autoclave was heated for the designated time. The analysis was the same as the above method.

The typical procedure for the coupling of CO_2 with CPO by complex **2** or **3** at atmospheric CO_2 pressure is as follows. Complex **2** (38.7 mg, 50 µmol) was placed in a 10 mL round-bottom flask in a glovebox. The flask was taken out, which was equipped with a balloon. The flask was vacuumed and recharged with CO_2 . After the injection of a prescribed amount of CPO, the flask was heated and maintained at 100 °C. The samples were taken out periodically and analyzed by Agilent GC to determine the conversion of CPO.

4. Conclusions

We have demonstrated the synthesis of a series of aluminum complexes 1–3. Structural characterization by NMR and MS suggested the formation of binuclear structures via the chloride. Although complex 1 can be activated by either a nucleophile or an organic base to enable the coupling of terminal epoxide with CO_2 , the excess use of cocatalyst unambiguously hampers its practical application. In contrast, the bifunctional complexes 2

and **3** containing tertiary amine as the built-in nucleophile are highly active catalysts by their own for the coupling of CO_2 with terminal epoxides. For bifunctional complexes **2** and **3**, high temperature facilitates the rapid transformation. It is found that the incorporation of more amine groups in the metal complex greatly enhances the catalytic activity. The bifunctional complexes are even active under low CO_2 pressure at the expense of catalystic activity to some extent. This work may shed light on the design of metal-based catalyst of high activity for the coupling of terminal epoxide with CO_2 .

Supplementary Materials: The following are available online at https://www.mdpi.com/2073-4 344/11/2/145/s1, Figure S1: ¹H NMR spectrum of proligand H_2L^1 in CDCl₃, Figure S1: ¹H NMR spectrum of proligand H_2L^2 in DMSO-d₆, Figure S3: ¹H NMR spectrum of proligand H_2L^3 in DMSO-d₆, Figure S3: ¹H NMR spectrum of the complex **1** in CDCl₃, Figure S5: ¹H NMR spectrum of the complex **2** in DMSO-d₆, Figure S6: ¹H NMR spectrum of the complex **3** in DMSO-d₆, Figure S7: Kinetic study of coupling of PO/CO₂ mediated by **1**/TBAB (1:40 molar ratio), PO conversion vs. reaction time, Table S1: Cycloaddition of CO₂ to PO mediated by complex **1** and TBAB, Table S2: Effect of reaction time on the PO conversion, Table S3: Coupling of CO₂/PO catalyzed by **1**/1-MeIm.

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Article CO Oxidation Efficiency and Hysteresis Behavior over Mesoporous Pd/SiO₂ Catalyst

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Abstract: Carbon monoxide (CO) oxidation is considered an important reaction in heterogeneous industrial catalysis and has been extensively studied. Pd supported on SiO₂ aerogel catalysts exhibit good catalytic activity toward this reaction owing to their CO bond activation capability and thermal stability. Pd/SiO₂ catalysts were investigated using carbon monoxide (CO) oxidation as a model reaction. The catalyst becomes active, and the conversion increases after the temperature reaches the ignition temperature (T_{ig}). A normal hysteresis in carbon monoxide (CO) oxidation has been observed, where the catalysts continue to exhibit high catalytic activity (CO conversion remains at 100%) during the extinction even at temperatures lower than T_{ig}. The catalyst was characterized using BET, TEM, XPS, TGA-DSC, and FTIR. In this work, the influence of pretreatment conditions and stability of the active sites on the catalytic activity and hysteresis is presented. The CO oxidation on the Pd/SiO₂ catalyst has been attributed to the dissociative adsorption of molecular oxygen and the activation of the C-O bond, followed by diffusion of adsorbates at T_{ig} to form CO₂. Whereas, the hysteresis has been explained by the enhanced stability of the active site caused by thermal effects, pretreatment conditions, Pd-SiO₂ support interaction, and PdO formation and decomposition.

Keywords: CO oxidation; hysteresis; thermal stability; pretreatment; structure-activity

1. Introduction

Low-temperature carbon monoxide (CO) oxidation is considered a prototype reaction for heterogeneous catalysis. It has garnered attention in recent years due to its interesting catalytic behavior and the screening of new heterogeneous catalysts [1]. In recent years, "metal oxide supported palladium catalysts" have been studied in detail due to their high intrinsic activity, lower cost, metal-support interaction, and other non-linear dynamic behaviors, which are beneficial for CO oxidation [2,3]. The properties of Pd catalysts are affected by types of support, preparation conditions, and the dispersion of the Pd particles [4]. Support materials are a crucial factor in the catalytic behavior of Pd toward CO oxidation where the synergistic effect between Pd and the support depends on the nature of support (i.e., reducible vs. non-reducible) [5]. Stabilization of the catalyst can be attained by anchoring Pd particles on the surface of the support to resist sintering at high temperatures and dispersion in metal oxides, such as silica (SiO₂) [6]. Silica materials have been widely explored as catalyst support owing to their unique morphologies, narrow pore sizes, large surface areas, and thermal stability [6]. Despite being inert and irreducible, SiO₂ can exhibit a metal–support interaction with Pd, that affects the morphology, wetting,



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Copyright: © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). and interdiffusion in the Pd/SiO₂ catalyst, which is known to improve catalytic properties and stability [7]. The heat treatment under oxidation and reduction conditions is crucial for the preparation of supported Pd/SiO₂ catalysts. Such treatment can induce morphological changes and affect the dispersion of Pd particles resulting from the sintering of the Pd particles. Therefore, it is crucial to study the optimal preparation and pretreatment conditions and activation of the Pd catalysts. Morphological changes due to sintering have been reported wherein encapsulation, inter-diffusion, and alloy formation are found to be highly dependent on heating conditions [8]. The thermal treatment can cause deactivation of catalysts impacting the support, oxidation state, particle size, and the surface area of the catalyst due to sintering at high temperatures, which can directly influence the catalytic activity [2]. Palladium nanoparticles dispersion within a narrow pore size distribution and high surface area mesoporous silica (SiO₂) aerogel increases the catalytic activity of supported Pd catalysts. Moreover, the formation of Pd intermediate has been reported to influence the catalytic behavior and stability during ignition/extinction cycles [9]. The Pd catalyst has a wide operating temperature range during CO oxidation and can exist in two thermodynamically stable phases depending on the partial pressure of oxygen and the reaction temperature, either as palladium oxide (PdO) or in its metallic form (Pd) [10]. Therefore, the Pd catalyst exhibits nonlinear dynamics such as hysteresis effects and selfsustained oscillations due to the PdO decomposition and re-formation. This behavior could be crucial for the future development of heterogeneous catalysts for a range of reactions in addition to CO oxidation reactions [11].

Hysteresis is a complex phenomenon attributed to many factors such as surface coverage, multiplicity, thermal inertia, exotherm, and catalyst oxidation states. The effects of CO conversion hysteresis over supported and unsupported palladium catalysts were investigated and reported by researchers, including our group [2,12]. Hysteresis loops arise from the difference between the activity during the heating and cooling processes [13]. The reversible oxidation of Pd due to the dissociative adsorption of oxygen on the subsurface layer of the catalyst to form a surface layer of PdO leads to the hysteresis and self-sustained oscillations in CO oxidation [12]. This phenomenon was observed in many exothermic oxidation reactions in addition to CO oxidation and has been attributed to the heat released at the surface of the catalyst during the exothermic oxidation, wherein the surface temperature exceeds the reactor temperature [14]. "Normal" hysteresis observed in CO oxidation when the catalytic activity during CO ignition takes place at a higher temperature than the temperature during extinction, while inverse hysteresis is observed for some gas mixtures, where the catalytic activity during ignition exceeds the activity during extinction [15]. This behavior has been realized and plays a crucial role in many applications, including long-life carbon dioxide (CO2) lasers, partial oxidation in chemical synthesis, and removal of pollutants in catalytic converters during prototype exothermic reactions including CO oxidation [16]. Most of the reports in the literature focus on the CO hysteresis as a function of inlet temperatures [15]. Although reasons for the hysteresis phenomena are still unclear, some researchers associate its rise with the multiplicity of steady states, oxidation of the catalyst, and temperature fluctuations. Due to the coexistence of PdO or Pd states in the palladium catalyst and the strong interdependence of catalytic activity and hysteresis on the support materials, palladium catalysts exhibit normal hysteresis during CO oxidation due to the decomposition and reformation of PdO.

In our previous work, we have reported the synthesis and the catalytic activity of the Pd/SiO_2 catalyst. In continuation of this work, we provide detailed information on the influence of pretreatment conditions on the catalyst microstructure and dispersion of Pd, thermal stability, and catalyst performance. The mesoporous Pd/SiO_2 aerogel catalyst with well-dispersed Pd nanoparticles was evaluated for CO oxidation under ignition/extinction conditions, wherein the possibility of using the hysteresis effect to attain high conversions at lower reaction temperatures were explored. The Pd/SiO_2 catalyst is a CO oxidation catalyst with high catalytic activity at a temperature range of (150 to 250 °C). It has excellent thermal stability, which could stabilize the active phase for CO oxidation by

increasing the metal-support interaction and dispersion of Pd species. This study reports the experimental data on the catalytic activity, hysteresis, and thermal stability during the CO oxidation over the Pd/SiO_2 catalyst, which is found to be intensely dependent on the preparation, pretreatment conditions, and external parameters. The preparation and treatment conditions' effect under dynamic reaction conditions provide a correlation between the catalyst structure and activity, as well as the role of thermal effects on the observed hysteresis behavior.

2. Results and Discussion

2.1. Catalytic Activity and Hysteresis Behavior of Pd/SiO₂ Catalysts

2.1.1. CO Conversion Efficiency and Light-Off Testing

Catalytic CO oxidation was performed under constant gas composition where the concentration of CO is 3.5%, with a surplus of oxygen (20% concentration) balanced in helium to allow for the complete CO conversion. The result was obtained under controlled heating (heating rate is 10 °C/min), and subsequent normal cooling conditions (ignition/extinction) as a function of the reaction (catalyst) temperature and not the feed gas inlet temperature, as reported by other researchers in this field [17]. In this context, we defined the ignition or light-off temperature (T_{ig}) as the temperature at which the CO conversion efficiency reaches 3% during heating and extinction or light-out temperature (T_{ext}) as the temperature at which the CO conversion efficiency reaches 3% during heating and extinction or light-out temperature (T_{ext}) as the temperature at which the CO conversion efficiency is 50% during ignition and extinction.

Figure 1a presents the conversion efficiency and catalyst temperature during the catalytic CO conversion test as a function of time, while Figure 1b shows the conversion efficiency as a function of the catalyst temperature for two consecutive light-off cycles. The figures show clearly the exothermic evolution as a function of time and the hysteresis effect for oxidation reaction. During heating (ignition), three active conversion zones can be distinguished in which the reaction takes place at varying catalyst temperatures. In Zone I, when the catalyst temperature is below 214 °C, the reaction rate is slow, leading to low CO conversion as it is kinetically controlled. In Zone II, intermediate conversion zone when the temperature is above 214 °C, the reaction rate is slightly higher, leading to better CO conversions as it is controlled by internal diffusion and mass transfer limitations in the SiO₂ porous support [18]. In Zone III, the full conversion zone when the temperature increased to above 276 °C, at which the CO conversion efficiency reaches 50%, the reaction rate is high and controlled by external (gas phase) diffusion without any mass transfer limitations.



Figure 1. (a) Reaction temperature and carbon monoxide (CO) conversion efficiency during typical light-off testing in a synthetic gas reactor as a function of time, (b) CO conversion efficiency, and hysteresis effect as a function of the reaction (catalyst) temperature.

On the other hand, during cooling (extinction), the reaction kinetics and diffusion of gas molecules play a role due to temperature differences between the high exothermic reaction heat generated at the catalyst surface and the reduced gas temperature at the reactor inlet, when the reactor is below the ignition temperature (below 214 °C). This leads to kinetic bi-stability, where the surface nanoparticles alternate between active (PdO) and in-active (Pd) states [19]. The self-sustained oscillations and hysteresis appear during cooling of the catalyst under the flow of the reaction gas mixture. The cycling experiments for the first and second light-off were performed, where the first ignition was obtained at 88.6 °C. These results confirm that the hysteresis effect could help attain and maintain high CO conversions while oscillating between higher and lower temperatures. Upon heating/cooling, a significant hysteresis was observed at 121–296 °C. This effect can help in reducing the temperature for the second light-off for CO conversions over a Pd/SiO₂ catalyst by lowering the temperature along the extinction leg to a point below the ignition temperature as a result of the convective heat transfer associated with the temperature of the incoming gas, the CO oxidation reaction exotherm, and conduction of heat along the catalyst. Table 1 summarizes and compares the catalytic ignition and extinction profile and hysteresis width of the Pd/SiO₂ aerogel catalyst during the first light-off (fresh catalyst) and the second light-off (heat-treated catalyst in the CO/O_2 mixture) cycles. The second light-off demonstrated higher activity compared to the first light-off cycle, as shown in Figure 1b. The temperature of the second light-off and hysteresis width were shifted to lower values compared to the first light-off cycle. Reportedly, Pd⁰ metal particles are preferably formed under a reducing CO atmosphere, whereas, under oxidizing O₂ atmosphere, Pd^{2+} or PdO particles should be formed [20]. The heating in the CO/O₂ mixture caused the CO conversion ignition temperature (T_{ig}) of Pd/SiO₂ to decrease from 214 to 195 °C, and the full CO conversion was achieved at (T_{100}) of 272 °C rather than 296 °C, while the hysteresis width decreased from 121 to 108 °C. The results might be attributed to the removal of moisture and hydrocarbons from the surface of the catalyst, increasing the metal-support interaction, as observed in XPS and XRD [2], the formation of palladium silicide, reduction of metal hydroxide, and oxidation of metallic Pd lead to improving the active site for the CO oxidation reaction.

Table 1. Comparison between the catalytic ignition and extinction profile, and hysteresis width of Pd/SiO₂ aerogel catalysts of the first and the second light-off (ignition) cycles.

Light-Off Cycle	T_{ig} (°C)	<i>T</i> ₅₀ (°C)	T_{100} (°C)	T_{ex} (°C)	Hysteresis Width (°C)
First light-off	214	276	296	138	121
Second light-off	195	247	272	123	108

Where T_{ig} is the ignition temperature at 3% conversion in °C, T_{50} is the temperature at 50% conversion in °C, T_{100} is the temperature at 100% conversion in °C, T_{ex} is the extinction temperature at 3% conversion in °C, and hysteresis width is at 50% conversion in °C.

Furthermore, the removal of silanol groups increases the metal dispersion and the catalytic activity of the Pd/SiO_2 catalyst [21]. Note that the conversion curve remained the same even after four cycles. The effect of heating rate on the catalytic activity, hysteresis, and ignition/extinction profile of the Pd/SiO_2 aerogel catalyst will be reported in a future manuscript.

To further investigate the catalytic activity and hysteresis behavior of the catalyst during the first and second light-off (or before and after catalytic conversion experiments), changes in the catalyst's porosity, surface area, Pd particle size, the oxidation state of Pd, crystallography, and pore size were investigated before and after the CO oxidation reaction.

The porosity of the catalyst assumes a role in the catalytic activity and the hysteresis activity during the CO oxidation reaction. The N2 adsorption-desorption characteristics of fresh (as prepared) Pd/SiO₂ aerogel isotherms and pore size distribution before the CO oxidation reaction was performed. The isotherms of the fresh sample with the N₂ uptake consistent with type IV (according to the IUPAC classification), and a narrow H₂ type hysteresis loop at $p/p_0 > 0.75$ are shown in Figure S1, suggesting mesoporous and microporous characteristics due to capillary condensation in silica [22]. The increment of adsorption at $p/p_0 = 1.0$ was caused by larger mesopores, typical in mesoporous materials [23]. This wider hysteresis loop is known to occur when the distributions of the pore radius are wide [24]. The effect of heat treatment in the CO/O_2 atmosphere (after the first light-off) on the morphologies, surface area, and pore volume distributions were investigated to clarify the higher catalytic activity in the second light-off observed for CO oxidation on the Pd/SiO₂ catalyst. The structural properties of both samples were shown in Table 2 and illustrated in Figure S1. The fresh Pd/SiO₂ aerogel catalyst shows continuous pore volume distribution with diameters between 2 and 80 nm. However, N2 adsorption-desorption characteristics of the Pd/SiO₂ aerogel pore size distribution after CO oxidation (after the first light-off) show a pore volume with continuous distribution of pore diameters (between 2 and 60 nm). The higher temperature during the CO oxidation does not affect the integrity of the catalyst. However, the quantity of large mesopores and macropores is eliminated due to the collapse following the heat treatment, leading to a higher ratio of micropores and small mesopores, as reported by Gage et al. [25]. BET results show that the average pore diameter of the Pd/SiO₂ aerogel slightly reduced to 15.6 nm and the pore volume slightly increased to $0.06 \text{ cm}^3/\text{g}$, although the surface area reduced to ~940.9 m²/g. The decrease in the surface area could be attributed to the sintering of the large excess palladium particles outside the pores as found in electron microscopy, which will be discussed later.

Table 2. Structural properties of fresh Pd/SiO₂ aerogel catalysts and after the first light-off.

Catalyst Pd/SiO ₂	BET Surface Area (gm ⁻¹)	Pore Diameter ^a (nm)	Pore Volume ^a (cm ³ g ⁻¹)
Fresh	1113.65	15.7	0.05
After the first light-off	940.86	15.6	0.06

^a Calculated by the Barrett, Joyner, and Halenda (BJH) method from the desorption isotherm.

To study the effect of the particles size of the catalyst on the catalytic activity and hysteresis width during the CO oxidation reaction, the TEM of the catalyst before (fresh) (Figure 2a) and after CO oxidation (first light-off) (Figure 2b) was performed. The presence of a large number of smaller Pd particles (2–5 nm) in the framework (marked by yellow arrows) located inside the mesoporous framework of SiO₂ aerogels homogeneously dispersed within the SiO₂ network and a few large surface particles (20–40 nm) (marked by magenta arrows). This unique texture is believed to occur due in the samples prepared by the sol-gel synthesis resulting in a better catalytic activity and effectively hindering the sintering of Pd particles [26]. The average size estimated from over 200 particles shows a mean size of the Pd particles in as-synthesized particles as 6.1 nm. Figure 2d,e shows the TEM micrographs of typical samples after CO oxidation. The mean size of Pd particles following the completion of the reaction was found to grow to ~7.8 nm due to the sintering, as also observed from the X-ray diffraction (XRD) analysis, and reported in a previous work [2].



Figure 2. TEM micrographs and the corresponding estimated particle size distribution of Pd/SiO₂ aerogel catalysts (**a–c**) before, and (**d–f**) after the catalytic CO oxidation.

The XPS spectrum of the core level Pd 3d peaks were obtained from the samples at different points and verified by the NIST Standard XPS Database for PdOx/Pd and Pd/SiO_x. The deconvolution of the spectrum of Pd 3d shows two spin-orbital states, $3d_{5/2}$ and $3d_{3/2}$ [2]. The Pd 3d and O 1s XPS peaks located in the near-surface region of freshly prepared Pd/SiO₂ samples, at 250 °C (full CO conversion), and after catalytic CO oxidation were investigated to understand the chemical environment, palladium oxidation state, and active species before and after the CO oxidation reaction. The Pd 3d showed peaks for Pd $3d_{5/2}$ and Pd $3d_{3/2}$ and fitted with the mixed Pd(0) and PdO combined spectrum. Table 3 summarizes the binding energies (BEs) of palladium Pd $3d_{5/2}$, Pd 3d_{3/2}, and the binding energy (BE) of the corresponding O 1s peak [27]. The O 1s peak was fitted with three components due to the overlap of O 1s and Pd 3P3/2 peaks following Zemlyanove et al. [28]. Figure 3 shows Pd 3d and O 1s spectra of the reduced Pd/SiO₂ catalysts along with the deconvoluted peaks. Figure 3a shows Pd 3d spectra for the fresh (or as prepared) catalyst with two peaks at binding energies (BE) at 334.06 and 339.3 eV assigned to the metallic palladium Pd(0) and two peaks observed at 335.8 and 341 eV assigned to Pd²⁺ or PdO, respectively. This clearly indicates that most of Pd exists in the form of Pd metal with only a small fraction in the Pd²⁺ form. Upon increasing

the temperature to 250 °C (Figure 3b), the obtained spectrum of the sample shows that the low energy doublet of $3d_{5/2}$ is shifted to 335.1 eV which could be assigned to the photoemission of electrons from Pd²⁺ and the high energy doublet is shifted to 336.1 eV due to the oxidation of smaller Pd particles (2–3 nm) or Pd²⁺ cations within the catalyst structure [29]. The increase in BE of Pd 3d for the catalyst annealed at 250 °C affirms the increase in formation of PdO, indicating that the surface of Pd is highly oxidized. After the CO oxidation reaction (Figure 3c,f) the deconvolution of the Pd 3d peaks show Pd(0) and Pd²⁺ (PdO) peaks with higher concentration of PdO compared to freshly prepared samples.

Table 3. List of the binding energies of palladium species (Pd and PdO) and the binding energy of the corresponding O 1s peak located in the near-surface region of Pd/SiO₂ catalysts.

Catalyst		Binding Energy, eV	
Catalyst	Pd 3d _{5/2}	Pd 3d _{3/2}	O 1s
Fresh	334.1	339.3	531.5
At 250 °C	335.13	340.23	531.6
After CO oxidation	334.8	339.9	531.8



Figure 3. High-resolution XPS spectra of Pd 3d of (**a**) fresh Pd/SiO₂ catalysts, (**b**) Pd/SiO₂ catalysts annealed at 250 °C (full CO conversion), and (**c**) Pd/SiO₂ catalysts after the heating/cooling cycle in the CO/O₂ reaction mixture, and the deconvolution of O 1s XPS spectrum: (**d**) Before CO oxidation, (**e**) at 250 °C, and (**f**) after CO oxidation.

To analyze the change in the concentration of Pd^{2+} before and after CO oxidation, we compared the areas under the Pd $3d_{5/2}$ of Pd(0):Pd²⁺ peaks before CO oxidation (Figure 3a) to the ratio of areas of the peaks after CO oxidation (Figure 3c). The ratio of areas under the peaks of Pd(0):Pd²⁺ were 1.8:1 before and 1:1.6 after CO oxidation, respectively, indicating that the PdO concentration increases after CO oxidation, suggesting a lowering of the activation energy and confirming that the active phase for CO oxidation is PdO [29]. The increase in surface oxygen concentration (Pd-O) after the reaction (Figure 3f) could aid the activation of the C-O bond in the CO molecule for other oxidation reactions as reported elsewhere [23]. This increase is also accompanied by a reduction of oxygen concentration (O-Pd-O), which suggests that Pd interacts with the SiO₂ support [30,31]. Oxygen in SiO₂ loses electrons resulting in a shift and bending of the Fermi level. O₂ initially diffuses to the metallic Pd surface, where it is adsorbed to form an active adsorption state. Following this, the oxygen atoms interact with the Pd atoms on the surface to form PdO. Results obtained from the XPS analysis show that the active sites and the state of Pd can provide valuable information on the metal-support interaction in the Pd/SiO₂ catalyst through monitoring of the electronic modifications of the Pd surface before and after the CO oxidation. This observation is consistent with the XRD [2] and TEM results. The XPS of the freshly prepared Pd/SiO₂ aerogel catalyst confirms that the Pd nanoparticles are attached to the support material through oxygen atoms of either the free silanol or siloxane groups present on the silica-network as oxygen is highly electronegative and can draw more electrons from Pd nanoparticles, resulting in higher BE for the Pd atoms in the Pd/SiO₂ catalyst.

2.1.2. Effect of Annealing Atmosphere on Catalytic Efficiency and Hysteresis of $\rm Pd/SiO_2$ Aerogel Catalyst

The oxidation state of Pd alone cannot explain the change of the catalytic activity and hysteresis behavior before and after the heat treatment. To examine the thermal stability and catalytic performance of the catalyst aiming at optimizing the best condition for Pd active sites, we conducted several experiments to support our results. It has been reported that the catalyst support modification can contribute to the activity and hysteresis behavior of the catalyst due to its binding to the catalyst metal. This metal-support interaction modifies both the electronic and geometric properties of the catalyst support, which influences the activity of the catalytic sites on the metal surface and enhances active sites [23]. Reportedly, the hysteresis effect depended on the pretreatment of catalysts and was attributed to the changes in the catalyst structure for CO oxidation on partially oxidized Pd nanoparticles, where hysteresis effects were found to depend on the pretreatment of catalyst samples [32]. Pretreatment conditions of the catalyst influence the catalytic activity, and metal-support interaction motivated by the oxidation state of metal and the nature of the reactions. The effect of the catalyst pretreatment on the hysteresis behavior was reported and attributed to the changes in the catalyst structure [17]. Therefore, the pretreatment atmosphere is an essential factor that influences the final state of the catalyst and metalsupport interaction. Oxidizing or reducing the atmosphere can yield oxide active or metallic phases depending on the temperature of the treatment.

The effect of the pretreatment atmosphere on catalytic activities, hysteresis, and ignition/extinction curves of Pd/SiO₂ aerogel catalyst was studied, and the results are summarized in Table 4 and Figure 4. The catalytic ignition/extinction curves and hysteresis of Pd/SiO₂ aerogel catalyst freshly prepared and annealed in different atmospheres have been plotted. It is clear that under ignition, the catalytic activities of annealed samples are higher, and the ignition temperatures are shifted to lower temperatures, which are attributed to the efficient removal of adsorbents from the surface, improving the exposure of active sites to fresh adsorbates possibly led by the decomposition of the metal complex to metal or metal oxide. However, the best activity and highest increase in the hysteresis width was observed for the sample treated in air. The results can be explained based on the gas composition of the annealing atmosphere, the reactant gas mixture, and the nature of gas used in the annealing atmosphere (reducing or oxidizing). Although, He and N_2 are inert gasses and do not affect the oxidation state of the freshly prepared Pd/SiO₂ aerogel catalyst, the thermal treatment at high temperature can affect the physio-chemical properties of the catalyst. The Pd/SiO₂-air aerogel sample showed the best catalytic activity compared to the untreated Pd/SiO2 and Pd/SiO2-N2 aerogel samples, a plausible reason being that during the reaction, some of the metallic Pd nanoparticles converts to PdO as observed in XPS results, and the interfaces between Pd and PdO act as active catalytic sites. During extinction, the sample treated in N_2 gas shows an extinction temperature of 123 °C and hysteresis width of 104 °C, while the Pd/SiO₂-air aerogel sample, on the other hand, has an extinction temperature of 79 °C and a wider hysteresis width of 138 °C. This may arise from the formation of PdO in the Pd/SiO₂-air aerogel sample in the whole bulk of the catalyst during heating in the presence of excess O_2 through surface oxidation of metallic Pd preceded by diffusion of oxygen atoms from the bulk of the catalyst [33]. During extinction, the surface PdO is reduced directly to metallic Pd. The appearance of the

hysteresis loop can be associated with the slow transition from an oxygen-enriched surface and surface palladium oxide formation, present during extinction, to a CO-covered surface including Pd reduction, resulting in reversible formation of surface Pd oxide. Since Pd in the Pd/SiO₂-air aerogel sample was oxidized entirely, the reduction of Pd oxide will take a longer time than in the Pd/SiO₂ aerogel treated in N₂ samples, resulting in the broadening of the hysteresis curve [34].

Table 4. Catalytic ignition and extinction profile of Pd/SiO_2 aerogel catalysts annealed in different atmospheres.

Gas	T_{ig} (°C)	<i>T</i> ₅₀ (°C)	<i>T</i> ₁₀₀ (°C)	T_{ex} (°C)	Hysteresis Width (°C)
Untreated	214	276	296	138	121
Air	212	223	225	79	138
N ₂	212	248	287	123	104



Figure 4. Comparison between the catalytic activity curves of Pd/SiO₂ aerogel catalysts annealed in different atmospheres during ignition and extinction.

To investigate the thermal stability of Pd/SiO₂ aerogel catalyst and the surface oxidation and reduction of Pd/SiO₂, TGA was performed up to 600 °C at a heating rate of 10 °C/min in air and N₂ atmospheres, while the DSC of Pd/SiO₂ aerogel was carried out under heating (red) and cooling (black) at a heating rate of 10 °C/min in air and N₂ atmospheres up to 300 °C, which corresponds to the temperature where full CO conversion is reached. TG-DSC spectra are shown in Figure 5. During heating, TGA and DSC studies for samples treated in an air environment showed two exothermic peaks and one endothermic peak, as shown in Figure 5a,c. The spectra indicate clearly that the catalyst is thermally stable up to 600 °C. A weight loss of ~3 wt% occurs when the samples are heated from 50 to 100 °C due to the loss of physically adsorbed water and ethanol from the porous catalyst.



Figure 5. (**a**,**c**) Thermal gravimetric analysis-differential scanning calorimetry (TGA-DSC) of Pd/SiO₂ aerogel catalysts heated in the air atmosphere, (**b**,**d**) TGA-DSC of Pd/SiO₂ aerogel catalysts heated in the N₂ atmosphere.

These results are consistent with the DSC results, which show an endothermic peak in the region from room temperature up to 125 °C. Furthermore, an exothermic peak accompanied by an endothermic peak between 215 and 243 °C can be attributed to the surface oxidation of palladium accompanied with the reduction of silica surface, indicative of the formation of the interface between the palladium and silica support [35]. During the cooling ramp, as shown in Figure 5c, two exothermic peaks at 315 and 225 °C accompanied with an endothermic peak in between, could be attributed to the reduction of the small domain PdO to Pd⁰ on the surface of PdO, leading to polycrystalline particles that easily re-oxidize upon cooling due to the lack of Pd nucleation sites on the surface of the metal particles. Moreover, this could be associated with the combustion of unreacted organics such as Si–CH₃ groups from the synthesis process. This behavior was observed previously by Datye et al. on the surface of Pd/Al_2O_3 when the catalysts were heated in air [36] and Colussi et al. at higher temperature on Pd/Al₂O₃ and Pd/CeO₂/Al₂O₃, where they reported re-dispersion of Pd on the surface of oxide and transformation between Pd and PdO [37]. The temperature of this transformation was reported to strongly depend on the characteristics of the oxide support [38]. The results agree with the XPS analysis and catalytic tests of Pd/SiO₂ treated in air under heating/cooling cycles. However, TGA and DSC studies for samples treated in a nitrogen environment showed only well-resolved steps, Figure 5b,d. The major weight loss (about 5 wt%) was observed between 50 and 125 °C as evident in the DSC, as the broad endothermic peak in the curve in Figure 5d is attributed to the loss of water from the porous catalyst [39]. After 125 °C, the weight loss until 600 °C is attributed to the condensation of silanol groups from the surface of pristine silica aerogel, which was experimentally found to occur between 150 and 500 °C, as reported by Mueller et al. [40]. No peaks were observed during the cooling cycle which suggest that most of Pd in the sample is in the metallic state.

It is well known that the support nature and composition of SiO_2 and pretreatment conditions (oxidation or reduction treatments) have a direct impact on the metal-support interaction and ratio of oxidized and reduced forms of the supported palladium metal. To investigate the thermal effect on the catalytic activities, hysteresis behavior, and surface oxidation and reduction of Pd/SiO_2 heated in air and N_2 atmospheres, we preformed FTIR spectroscopy of Pd/SiO₂ aerogel catalyst annealed in different atmospheres (N₂ and air) and compared it to the untreated catalysts. Figure S2 compares FTIR spectra of freshly prepared Pd/SiO₂ aerogel catalysts and after the heat treatment at 450 °C in air and nitrogen atmospheres. Room-temperature FTIR spectra of Pd/SiO₂ samples measured in spectral range (400–4000 cm⁻¹) were recorded and compared to the untreated samples to determine the changes after annealing in N₂ and air atmospheres. The FTIR spectra of both samples revealed several sharp, well-defined absorption bands within the measured spectral range. The spectra show bands centered at 567, 794.5, and 1049.1 cm⁻¹ with a shoulder peak at 1162.9 cm⁻¹ corresponding to stretching vibrations of siloxane groups (Si-O-Si bonds), respectively [41], while the peak centered at 954.5 cm⁻¹ corresponds to the stretching vibration of silanol groups (Si-OH) in the silica lattice suggesting the presence of a considerable amount of silanol groups on the silica surface or pores in all the samples. A small peak observed at 2987.2 cm^{-1} is assigned to the vibrations of the stretching vibration of -CH₃ and -CH₂ groups indicating the presence of a small amount of Si-OC₂H₅ groups, which can be attributed to an incomplete condensation during gelation [42]. The low-intensity peak at 3367.1 cm^{-1} is assigned to -OH stretching vibrations [43].

The FTIR spectra of the Pd/SiO₂ sample treated in air show that all peaks are shifted to a higher wavenumber compared to the untreated sample indicating the interaction between Pd and SiO₂, which can affect the formation of the Si-O-Si network as observed in Cu/SiO_2 [44] leading to a stronger metal-support interaction. The intensity of the peak at 958.45 cm⁻¹ is considerably lower, while that at 794.5 cm⁻¹ increases indicating the formation of new Si-O-Si bonds via the reduction of Si-OH bonds as a result of the condensation reaction between Si–O and the Pd metal. This reaction could shrink the SiO₂ network, which might be responsible for decreasing the pore volume and, consequently, surface area, as observed in N_2 adsorption-desorption results suggesting that the SiO₂ framework is formed by the Si-O-Si bonds [19]. Furthermore, the intensity of the peak at 3367.1 cm^{-1} , which is assigned to -OH stretching vibrations decreases, suggesting removal of the adsorbed OH or water. However, the FTIR spectra of Pd/SiO₂ sample treated in a nitrogen atmosphere showed similar spectra of the untreated sample (no shift is observed) except for reducing the intensity of the peak at 1162.9 cm⁻¹, which indicates the reduction of the Si-O-Si bond. The results suggest that the heat treatment in N₂ environment did not affect the interaction between Pd and the SiO₂ network.

2.1.3. Effect of Annealing Temperature on Catalytic Efficiency and Hysteresis of $\rm Pd/SiO_2$ Aerogel Catalyst

A further impact of annealing temperature on the catalytic activity, hysteresis, and ignition/extinction of Pd/SiO₂ treated in the air aerogel catalyst was studied by annealing some samples at 450 and 750 °C in air as summarized in Table 5 and shown in Figure 6. During the ignition cycle, the air-annealed catalysts demonstrated higher activity compared to the freshly prepared catalysts mainly due to the removal of moisture and hydrocarbons from the surface of the catalyst and the reduction of metal oxide to metallic Pd and improving the active site for the CO oxidation reaction. The catalyst treated at 450 °C in air shows better activity than fresh catalysts due to the removal of silanol groups, which increases the metal dispersion and the catalytic activity of Pd/SiO₂ catalyst [21]. The results indicate that the heat treatment in air does not probably affect the Pd clusters or particles as they are pinned to the silica surface, and the diffusion of ions is difficult, preventing sintering. The Pd clusters showed resistance to sintering upon calcination to 550 °C in air, which was attributed to the confinement of Pd clusters within mesopores [45].

Annealing Temperature	T_{ig} (°C)	<i>T</i> ₅₀ (°C)	<i>T</i> ₁₀₀ (°C)	T_{ex} (°C)	Hysteresis Width (°C)
Untreated	214	276	296	138	121
450 °C Air	212	223	225	79	138
750 °C Air	214	251	259	157	70

Table 5. Catalytic ignition and extinction profile of Pd/SiO_2 aerogel catalysts annealed in air for 1 h at different temperatures.



Figure 6. Comparison between the catalytic activity curves of Pd/SiO₂ aerogel catalysts annealed for 1 h in air at different temperatures during ignition and extinction cycles.

The Pd/SiO₂-air aerogel catalyst initially contained a considerable amount of metal oxide; heating in air will ensure that the sample is fully oxidized at 450 °C. In studies on the catalytic activities conducted in the CO/O₂ mixture, PdO will undergo a reduction to Pd, which in-effect would prevent any Pd particle growth (due to sintering) up to 700 °C, except for outermost particles (outside the pores). Upon annealing at 750 °C, all PdO will be reduced to metallic Pd and this will lead to the growth and sintering of metallic Pd particles which would lower catalytic activity [46]. The presence of fully oxidized Pd particles and well-defined active sites in the samples annealed at 450 °C in air ensures higher activity and lower extinction temperature. The as-prepared samples contain a considerable amount of metallic Pd, and most of the active sites are blocked, making it less active even during extinction. For samples annealed at 750 °C, the growth and sintering of the Pd particles lead to a lower activity resulting in narrower hysteresis width and lower ignition temperature compared to the sample treated at 450 °C.

Based on the experimental results, the origin of the high thermal stability and catalytic performance of Pd/SiO_2 aerogel catalysts were attributed to their mesoporous structures as confirmed by the N_2 adsorption-desorption isotherm, XPS, FTIR, and TEM. The results also confirmed that the catalyst structure could protect the Pd nanoparticles from sintering during the thermal treatment and catalytic CO oxidation reaction. The thermal stability of the Pd/SiO₂ catalyst highly depends on the oxidative/reductive nature of the gas environment. Under the CO oxidation reaction in the oxygen atmosphere, a small amount of Pd is converted to PdO. However, under air atmosphere, the porous structure of the silica is still stable, and the formation of small Pd particles inside the SiO₂ pores and on the surface increases as temperature increases.

Moreover, the absence of reducing gases in air leads to the oxidation of Pd particles, which directly impacts thermal stability and catalyst performance. The same behavior

was observed under air and H₂ environment [47]. The FTIR results confirmed that the interaction of Pd sites with -OH on the SiO₂ stabilizes the catalyst surface resulting in excellent thermal stability. Consequently, the Pd/SiO₂ catalysts showed a much more stable CO oxidation performance after annealing in air. These results agree well with recent studies, suggesting that the thermal treatment by annealing and catalytic CO oxidation at high temperatures (below 500) enhances the stability of Pd/SiO₂ catalyst under catalytic CO oxidation reactions due to its structure stability [48].

To understand the effect of annealing temperature on the catalytic activities, hysteresis behavior, and surface oxidation and reduction of Pd/SiO₂ catalyst heated in air atmosphere at different temperatures. We performed FTIR spectroscopy of Pd/SiO₂ aerogel catalyst annealed at 450 and 750 °C in air atmospheres than the untreated catalyst. Figure S3 shows FTIR spectra of the freshly prepared Pd/SiO₂ aerogel catalyst and after the heat treatment at 450 and 750 $^{\circ}$ C in air, respectively. The infrared absorption is similar to the discussion mentioned above in Figure S2 with bands centered at 567, 794.5, and 1049.1 cm⁻¹ with a shoulder at 1162.9 cm⁻¹ corresponding to stretching vibrations of siloxane groups (Si–O–Si bonds), respectively. A peak centered at 954.5 cm^{-1} corresponds to the stretching vibration of silanol groups (Si-OH) in the silica lattice which suggest the presence of a considerable amount of silanol groups on the silica surface or the pores in all samples. Small peaks observed at 2987.2 and 3367.1 cm⁻¹ are assigned to the stretching vibration of -CH₃ and -CH₂ to -OH stretching vibrations or water, as reported earlier. As the annealing temperature increases, the peak at 958.45 cm⁻¹ slowly disappears, the intensity of the peak at 2987.2 cm⁻¹ decreases, while that of the peak at 794.5 cm⁻¹ increases. This suggests the formation of additional Si-O-Si bonds by the condensation reaction. The peaks at 1710 and 3367.1 cm⁻¹ that belong to vibrations of water molecules decrease with the increasing annealing temperature due to the removal of water from the SiO₂ network structure [23]. The results suggest that heating to 750 °C could lead to the formation of additional Si–O–Si bonds, which strengthens the SiO₂ network structure [19]. The presence of 958.45 cm⁻¹, which corresponds to the stretching vibration of silanol groups (Si-OH) in the sample heated at 450 °C, enhanced the Pd-silica interaction, facilitating the dispersion of Pd particles.

2.2. Hysteresis Behavior during (Ignition/Extinction) Cycles

The reaction mechanism of CO oxidation during ignition/extinction cycles was reported by many researchers. CO is strongly adsorbed onto Pd, inhibiting the formation of active oxygen needed for low-temperature CO oxidation. Hence, low-temperature CO oxidation over Pd catalysts proceeds via Langmuir–Hinshelwood. Such adsorption has been shown to occur during CO oxidation on Pd metal catalysts under low O_2 pressure, wherein CO and O_2 gas are adsorbed on free adsorption sites on the Pd metal surface, followed by the interaction of the adsorbed CO and O, respectively, on the Pd active sites, resulting in the palladium oxide (PdO) surface. However, the reduction of PdO proceeds via the Mars-van Krevelen mechanism, where CO is adsorbed on the PdO surface [49].

The TEM results of large surface particles in the Pd/SiO₂ catalyst suggest that the as prepared catalyst contains Pd particles and a small amount of PdO particles on the surface, as shown in Figure 7a, while at 250 °C, the surface is almost fully covered with oxide as shown in Figure 7b, suggesting the formation of surface and bulk oxides. The TEM image of the particles after the heating/cooling cycle (Figure 7c) shows that part of the Pd (0) surface is restored, and the PdO surface is destroyed with a small island of 2D PdO observed. Similar observations in the literature suggested the oxidation of Pd and the formation of surface oxide during heating [12]. At higher temperatures, wherein the formation of 3D PdO is preferential on the catalyst surface while during cooling conditions, the 3D PdO is reduced to the Pd surface. The TEM results agree well with the XPS peak fitting, which show a shift of Pd $3d_{5/2}$ peak towards higher BE (Figure 3b) with respect to the metal peak (Figure 3a) due to the interaction with atomic oxygen to form PdO during the CO oxidation reaction. However, during cooling to room temperature (after heating/cooling

cycle) and as a result of the reaction medium (Figure 3c), PdO particles are reduced, leading to a decrease in the oxide intensity. In this region, the metallic palladium Pd(0) and the PdO particles co-exist, which serve as intermediates causing the self-sustained oscillation and hysteresis. A similar behavior was reported for Pd/Al_2O_3 systems [12].



Figure 7. TEM of (a) the fresh Pd/SiO₂ catalysts, (b) Pd/SiO₂ catalysts annealed at 250 °C in air, and (c) after heating/cooling cycle in the CO/O₂ reaction mixture.

In our study, XPS and TEM results suggest that the oxidation state, morphology of the Pd/SiO_2 catalyst, and the large palladium surface particles, changed before, during, and after the CO oxidation reaction. The presence of surface and subsurface Pd (0) and PdO with 2D morphologies, and the interplay between the two phases (reversed oxidation of Pd (0) and reduction or decomposition of PdO) causes the oscillatory behavior and hysteresis during the CO oxidation reaction, which aid the catalytic activity by lowering the activation energy after the first light-off.

3. Experimental Methodology

3.1. Catalyst Synthesis

The catalysts were prepared using the sol-gel method and dried under conditions with supercritical ethanol at 260 °C. This synthesis method described in a previous study [26] ensured the synthesis of well-dispersed Pd nanoparticles on a silica support. The silica gel was impregnated with metal ions before the drying step to replace the pores previously filled with the solvents used in the synthesis, which leads to hierarchical porosity. The advantage of this synthesis method is the possibility of producing highly dispersed and stable Pd catalysts with controlled structures and catalytic performances. The resulting Pd/SiO₂ catalyst is composed of accessible palladium particles located inside the pores or within the network silica particles, which result in sinter-proof Pd particles. The active catalytic sites are easily accessed by the reactants by diffusing through micropores and mesopores with no mass transfer limitations [23].

In a typical synthesis with tetraethyl orthosilicate (TEOS, Sigma-Aldrich, St. Louis, MO, USA, 98%) and ethanol, the resultant solution is aged overnight in a sealed container to obtain a gel [18]. The wet-gel obtained is then transferred to a solution of palladium precursor (PdCl₂, Sigma-Aldrich, St. Louis, MO, USA) in ethanol. The silica aerogels are dipped in the solutions of Pd ions in ethanol to ensure the exchange of ethanol in the gel with the Pd ions in the solution, followed by the ethanol supercritical drying at

260 °C. Dried Pd supported silica aerogels were annealed at a heating rate of 10 °C under atmospheric pressure (1 atm) in two different ambient conditions: Air (Pd/SiO₂–air), nitrogen (Pd/SiO₂–N₂), each at a 100 mL/min flow rate. All catalytic experiments and characterization were carried out using powdered aerogels.

3.2. Catalysts Characterization

The Pd/SiO₂ aerogel catalysts were characterized by X-ray photoelectron spectroscopy (XPS; Omicron Nanotechnology, Germany) with a monochromatic Al K_{α} radiation (energy = 1486.6 eV) working at 15 kV, which was used to study the surface states of the catalyst. The obtained XPS spectra were calibrated with respect to the C 1s feature at 285 eV [49]. The catalyst's surface area and pore sizes were determined using a Rise 1010 surface area and porosity analyzer (Jinan Rise Science and Technology Co., Ltd., Jinan, China). The Brunauer–Emmett–Teller (BET) and Langmuir models based specific surface area were calculated from the nitrogen adsorption-desorption isotherms recorded at 77 K at the relative pressure range of $P/P_0 = 0.05-0.2$. Pore size distributions were calculated using the desorption branches of the isotherms using the Barrett-Joyner-Halenda (BJH) model [50]. Transmission electron microscopy (TEM) measurements were carried out using a (JEM2100F field emission transmission electron microscope (TEM)) operating at a voltage of 200 kV (JEOL Ltd., Tokyo, Japan). Fourier transform infrared (FTIR) spectroscopy was performed using the FTIR650 spectrometer equipped with a LA-025-1100 universal ATR unit (Labfreez Instruments (Hunan) Co., Ltd., Changsha, China). Thermogravimetric analysis (TGA) and differential scanning calorimetry (DSC) were performed using the TG 2100D (Analytical Technologies Limited, Shanghai, China) analyzer at a ramp rate of 10 °C/min to reach (from 23 to 800 °C) in air (flow rate of 100 cc/min).

3.3. Catalyst Activity Testing

Catalytic activities of the synthesized samples were carried out in a custom-built fixed-bed continuous flow reactor placed inside a programmable tube furnace coupled to an infrared gas analyzer (ACS-CO2 infrared analyzer) [2]. Twenty milligrams of powdered metal loaded aerogel catalyst was placed in the middle of a quartz tube and sandwiched between two pieces of glass wool to form a cylindrical pellet. The catalyst temperature was recorded using an Omega K-type thermocouple inserted in the middle of the sample. The reactant gas mixture containing 3.5 wt% CO and 20 wt% O₂ in helium was flown through the reactor at 100 mL/min (calculated weight hourly space velocity (WHSV) was approximately 300,000 mL $g^{-1}h^{-1}$. CO conversion was assessed by measuring CO₂ in the outflow with an IR analyzer, and the catalytic activity was expressed by the CO conversion in the effluent gas. The temperature and the concentration data were collected using a National Instruments multifunction USB-6008 and NI-DAQmx (National Instruments, Roscoe, IL, USA) data acquisition system and recorded using a custom-built LabVIEW data acquisition software. The gas flow rate was controlled by a set of digital mass flow controllers. The flow rate of the mixture was maintained at 100 mL/min, while the catalyst was heated to different temperatures (25-600 °C). All the experiments were performed at an atmospheric pressure (1 atm) with a heating rate of 10 $^{\circ}$ C/min (ignition or activation) until the CO conversion reaches a full conversion (100%), then the furnace was switched off, and the sample was left to cool naturally until the CO conversion became zero (0%) (extinction or relaxation). Catalyst conditioning was achieved by calcination of the catalyst at 450 °C in air atmosphere for 1 h. For the other experiments, the calcination temperature was changed to 750 °C in air or N₂ for 1 h. The process is capable of removing moisture and improving the active sites. The ignition/light-off and extinction/light-out temperatures denoted the temperatures where the CO conversion reaches 3% during ignition and extinction curves. The CO conversion of the catalyst was measured as a function of the catalyst temperature and calculated using the following relation:

$$\text{CO conversion} (\%) = \frac{[\text{CO}]_{\text{in}} \text{vol.}\% - [\text{CO}]_{\text{out}} \text{vol.}\%}{[\text{CO}]_{\text{in}} \text{vol.}\%} \times 100$$
(1)
where $[CO]_{in}$ is the CO concentration in the reaction gas mixture and $[CO]_{out}$ is the concentration in the product gas mixture.

4. Conclusions

In this work, the low temperature CO oxidation and hysteresis behavior as a function of the catalyst temperature under optimum reaction conditions was investigated over a range of pretreatment mixture/conditions and temperatures that directly affect the nature of the active site. Carefully designed control experiments provide strong evidence that the pretreatment temperature and medium, nature of the support (porosity, thermal conductivity), the stability of the active site, and their formation were crucial factors in enhancing the catalytic performance. The best low-temperature CO oxidation performance was achieved by pretreating the catalyst in an air atmosphere at 450 $^{\circ}$ C. Recent studies suggest that the catalyst activation and the CO conversion hysteresis is attributed to local heating and heat dissipation by the support, respectively. However, the results presented here suggest that pretreatment conditions in N2 or air, and the pretreatment temperature have a direct impact on the catalyst activation and hysteresis behavior, in addition to the structural and chemical effect of the catalyst. The active site formation is influenced by the presence of oxidative or reductive pretreatment gas, and the surface morphological and chemical changes of the Pd during the reaction due to CO and O_2 adsorption to achieve the lower activation energy. Therefore, the hysteresis arises from the stabilization of these active sites by forming different oxidation states of Pd during the ignition and alteration of PdO to Pd during the extinction. These results were realized by the XPS, which suggest partial oxidation of Pd and the formation of different surface oxides reaching full oxidation at 250 °C. These results were confirmed by TEM, which show the formation and reduction of PdO during heating/cooling cycles. The TGA and DSC results confirm the surface oxidation and reduction behavior of Pd/SiO_2 in air for both the ignition and extinction cycles. Furthermore, the catalyst structure including the particle size distribution, the porosity of the sample, and thermal stability contribute to the catalytic activity and hysteresis phenomenon. This study confirms that the structure-activity relationship is very crucial for the design of a highly active and thermally stable catalyst for CO oxidation as a model reaction, which could aid the design of next-generation catalysts for CO oxidation.

Supplementary Materials: The following are available online at https://www.mdpi.com/2073-4 344/11/1/131/s1. Figure S1: Langmuir isotherms of N2 adsorption and desorption (a) and pore diameter distribution (b) of fresh Pd/SiO₂ aerogel catalysts before and after the catalytic CO oxidation (first light-off); Figure S2: Comparison between FTIR spectra of fresh Pd/SiO₂ aerogel catalysts and after the heat treatment at 450 °C in the air and nitrogen atmosphere; Figure S3: Comparison between FTIR spectra of fresh Pd/SiO₂ aerogel catalysts and after the heat treatment at 450 °C in air.

Author Contributions: R.M.A.S. synthesized materials, performed experiments and characterization, analyzed data, wrote and edited the entire paper; J.D. supervised the work and the quality of the manuscript; K.M.S. participated in characterization and data analysis; M.T.Z.M. and M.A.G. performed and analyzed XPS data. The authors worked together to prepare this manuscript. All authors have read and agreed to the published version of the manuscript.

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Article Biojet Fuel Production from Waste of Palm Oil Mill Effluent through Enzymatic Hydrolysis and Decarboxylation

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Abstract: Palm oil mill effluent (POME), wastewater discharged from the palm oil refinery industry, is classified as an environmental pollutant. In this work, a heterogeneous catalytic process for biojet fuel or green kerosene production was investigated. The enzymatic hydrolysis of POME was firstly performed in order to obtain hydrolysed POME (HPOME) rich in free fatty acid (FFA) content. The variations of the water content (30 to 50), temperature (30 to 60 °C) and agitation speed (150 to 250 rpm) were evaluated. The optimal condition for the POME hydrolysis reaction was obtained at a 50% v/v water content, 40 °C and 200 rpm. The highest FFA yield (Y_{FA}) of 90% was obtained. Subsequently, FFA in HPOME was converted into hydrocarbon fuels via a hydrocracking reaction catalysed by Pd/Al₂O₃ at 400 °C, 10 bars H₂ for 1 h under a high pressure autoclave reactor (HPAR). The refined-biofuel yield (94%) and the biojet selectivity (57.44%) were achieved. In this study, we are the first group to successfully demonstrate the POME waste valorisation towards renewable biojet fuel production based on biochemical and thermochemical routes. The process can be applied for the sustainable management of POME waste. It promises to be a high value-added product parallel to the alleviation of wastewater environmental issues.

Keywords: palm oil mill effluent; enzymatic hydrolysis; decarboxylation; green gasoline; green kerosene and green diesel

1. Introduction

Biojet fuel, classified as green kerosene derived from biomass, is generally blended with petroleum-based kerosene. The range of the jet fuel carbon number is strictly controlled to be between 8 and 16 in order to obtain desirable fuel properties and meet the strict standard specifications of the American Society for Testing and Materials (ASTM) D1655. Since the primary function of biojet fuel is to power an aircraft, the energy content and combustion quality are significant key factors. Other important properties are stability, lubricity, fluidity, volatility, noncorrosivity and cleanliness [1]. Typically, there are four routes to produce green kerosene from bio-feedstocks: (i) Hydro-processing of fatty acids and natural triglycerides; (ii) Hydrothermal liquefaction of algal biomass and pyrolysis of lignocellulosic materials; (iii) Gas-to-jet fuel platform: the gasification reaction of biomass in order to obtain syngas, which is subsequently converted into hydrocarbon fuel via the Fischer–Tropsch reaction; and (iv) Alcohol-to-jet platform: bio-based alcohols are sequentially dehydrated, oligomerized and hydrogenated in order to generate biojet fuel. Currently, only the hydroprocessing of oil/fat is selected for renewable jet fuel production at the industrial scale [2]. The key factors to decide on suitable raw materials for this



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Copyright: © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). process are availability, potential yield and especially the price. It is quite cheap, classified as waste, and it also plays an important role in the total production cost. Thus, palm oil can be considered as feedstock for bio-aviation fuel production because it is the least expensive vegetable oil [3]. However, the major challenge of first-generation feedstock is food competition.

In palm oil milling plants, large quantities of palm oil mill effluent (POME) are produced during the milling process. According to its high pH values, biochemical oxygen demand (BOD) and chemical oxygen demand (COD), it was classified as an industrial waste. It was discharged as wastewater containing high BOD (>25,000 mg·L⁻¹), which accounted for 100 times more pollution than municipal wastes [4,5]. Nowadays, the biological process named anaerobic digestion is the most common method for POME treatment when creating value-added products, including fertilizer and biogas. In addition, applications of biogas capture and membrane separation were reported in an integrated reactor for the production of biogas from POME, leading to a higher energy yield and lower greenhouse gas (GHG) emissions [6,7].

Considering new applications of POME, the production of hydrocarbon fuel from waste triglyceride is an interesting possible route for delivering clean fuel and as a response to environmental issues. The use of free fatty acid (FFA) as a feedstock for biojet fuel production has been reported as a cost-effective process due to a low hydrogen pressure, mild cracking reaction, short retention time and high yield, as compared to oil/fats [8–12]. In addition, the noble metals palladium (Pd) and platinum (Pt) were also proven to be high potential catalysts in decarboxylation reactions. They showed a high catalytic efficiency for biofuel production from triglycerides (TG) and free fatty acids (FFA) due to their high hydrogenation ability [13–15]. Accordingly, consecutive processes for hydrocarbon fuel have been developed, and triglycerides were hydrolysed to FFA under a high pressure and temperature, followed by the decarboxylation of FFA [16,17].

In this study, a new strategy to decrease an environmental pollutant of POME was presented. A combination of biochemical and thermochemical processes was firstly applied to generate renewable biojet fuel from POME. The enzymatic hydrolysis of POME was carried out in order to obtain FFA. After that, it was converted to hydrocarbon fuels via a hydrocracking reaction under mild conditions.

2. Results and Discussion

2.1. Influence of Temperature on Hydrolysis Reaction

The results showed that the hydrolysis degrees of POME increased considerably from 30 °C to 40 °C and presented a downward trend when the reaction temperature was higher than 40 °C (see Figure 1A). This can be explained by the fact that the viscosity of the substrate can be reduced by a higher temperature, resulting in a high catalytic rate of lipase. As a result, a higher FFA yield was observed in the mixture reaction. However, an excessively high temperature caused the enzyme structure to be denatured and to eventually deactivate. Thus, by increasing the reaction temperature to more than 40 °C, the hydrolysis degree of the three raw materials decreased slightly, as shown in Figure 1. Meanwhile, the highest hydrolysis degree of POME (89.51 \pm 0.04%) was obtained at 40 °C. Therefore, the reaction temperature of 40 °C was selected to investigate the effect of the water content on the hydrolysis reaction in the following experiment. Furthermore, the results obtained were in agreement with the previous work [18], which reported an enzymatic POME hydrolysis. They found that the maximum hydrolytic rate of lipase was achieved at 40 °C.

2.2. Influence of Water Content on Hydrolysis Reaction

The results illustrated that the hydrolysis degree of POME kept continually rising as the water content increased from 30 to 50% v/v (see Figure 1B). This can be explained by the fact that the enzymatic hydrolysis reaction is a reversible reaction. It is controlled by the amount of water in the mixture solution. Normally, excess water affects the hydrol-

ysis reaction in a positive way; however, a high water content (60% v/v) resulted in the hydrolysis degree decreasing dramatically [19]. When the water in the mixture solution was 50% v/v, the maximum FFA yield of 89.48 \pm 0.05% was obtained. Therefore, the water content was fixed at 50% v/v for the following experiments. The results obtained were in agreement with the previous work [20], which reported that as the molar ratio of oil to water increased from 1:1 to 1:4, the fatty acid yield also increased continuously. However, the fatty acid yield decreased as the ratio of oil to water increased up to 1:5.

2.3. Influence of Agitation Rate on Hydrolysis Reaction

The results observed showed that the agitation rate affected the hydrolysis reaction in a positive way, as it was clearly seen that the hydrolysis degree of POME significantly increased between the agitation rates of 100 rpm and 200 rpm (see Figure 1C). This might due to a higher agitation rate creating more oil-water interface, where the catalysis of the hydrolysis reaction via lipase occurred; this led to a high FFA yield. However, increasing the agitation rate up to 250 rpm caused a lower hydrolysis degree of POME. The agitation can reduce the droplet size and increase the interface area between oil and water, leading to a higher activity of lipase. However, the enzyme activity can be gradually decreased under a high agitation rate due to the shear stress [21]. The highest FFA yield (90 \pm 0.04%) was observed under an agitation rate of 200 rpm. Therefore, this rate was chosen as the optimal rate for the enzymatic hydrolysis of POME.



(A)

Figure 1. Cont.



Figure 1. Enzymatic hydrolysis of POME, (**A**) the effect of the temperature, (**B**) the effect of the water content, and (**C**) the effect of the agitation rate (standard deviation (SD) ≤ 0.05).

2.4. Fatty Acid Composition of Hydolysed Palm Oil Mill Effluent (HPOME)

In Table 1, the major fatty acid compositions of HPOME were palmitic acid (50%), oleic acid (34%), steric acid (13%) and others. An equal proportion between saturated fatty acids, palmitic acid (C16:0) and stearic acid (C18:0), and unsaturated fatty acid of oleic acid (C18:1) was also found.

Fatty Acid	Formula	Molecular Weight	Structure	% wt.
Capric acid	C10H20O2	172.26	C10:0	0.07 ± 0.06
Lauric acid	$C_{12}H_{24}O_2$	200.32	C12:0	0.09 ± 0.03
Myristic acid	$C_{14}H_{28}O_2$	228.37	C14:0	1.78 ± 0.06
Palmitic acid	C ₁₆ H ₃₂ O ₂	256.42	C16:0	50.03 ± 0.04
Stearic acid	C ₁₈ H ₃₆ O ₂	284.48	C18:0	13.04 ± 0.03
Oleic acid	$C_{18}H_{34}O_2$	282.47	C18:1	34.02 ± 0.05

Table 1. Fatty acid composition of hydrolysed palm oil mill effluent (HPOME).

2.5. Production of Hydrocarbon Fuels via Hydrocracking Reaction

Following the hydrocracking reaction of fatty acid in HPOME, a crude bio-fuel yield of 96 \pm 0.04% was obtained. Based on the volume fraction, crude biofuel could be classified into three kinds: green kerosene (54 \pm 0.03%), green diesel (30 \pm 0.04%) and green gasoline (10 \pm 0.04%), respectively. In addition, their selectivity was also reached at 57.44 \pm 0.06%, 31.91 \pm 0.03% and 10.64 \pm 0.05%, as illustrated in Figure 2.





2.6. Characterisation of Refined Biofuels

The characteristic of refined biofuels in terms of the carbon number was analysed by Gas chromatography- Mass spectroscopy (GC–MS). According to the result in Figure 3, the carbon atom distribution of refined biofuels was mainly in the ranges of kerosene (C9–C15) and diesel (C15–C18). This was due to three major fatty acid compositions of HPOME: palmitic acid (C16:0), stearic acid (C18:0) and oleic acid (C18:1). One carbon atom of the carboxyl group (–COOH) was eliminated during decarboxylation [22]. It should be noted that the refined biofuels were produced and measured in triplicate for reproducibility.



Figure 3. Carbon distribution of refined biofuel obtained from the hydrocracking reaction of HPOME (SD less than 1.00).

2.7. Comparative Green Kerosene Yields Obtained from Hydrocracking Reaction of Different Waste Oils

Based on the results in Table 2, enzymatic hydrolysis coupled with the hydrocracking reaction of POME could serve the highest green kerosene yield when compared to the single hydrocracking reaction of other waste oils. The production of green kerosene from waste cooking oil [23] was operated at the lowest temperature (380 °C), and a high green kerosene yield of 40.50% was also observed. However, this took a longer reaction time than in other works. The results clearly indicated that HPOME could be efficiently transformed into hydrocarbon fuel by using only a 1% catalyst loading, low H₂ pressure (10 bar), moderate temperature (400 °C) and short reaction time (1 h). This was due to the decarboxylation of fatty acids having a higher efficiency than triglycerides [17]. Therefore, the heterogeneous catalytic process could be considered as a high potential process for renewable jet fuel production in the future.

Feedstocks	Catalysts	Operating Conditions	Green Kerosene Yield (%)	References
HPOME	0.3% Pd/Al ₂ O ₃	1% catalyst loading, 10 bar $\rm H_2,$ $400~^\circ C$ and 1 h	54.00	This work
Waste cooking oil	10% Ni/Meso-Y	5% catalyst loading, 30 bar H ₂ , 380 °C and 8 h	40.50	[23]
Waste lubricant oil	5% Fe/Al ₂ O ₃	4% catalyst loading, 6.8 bar $\rm H_2,$ $450~^{\circ}C$ and 1.25 h	24.16	[24]
Waste lubricant oil	0.5% Fe/SiO ₂ -Al ₂ O ₃	4% catalyst loading, 6.8 bar $\rm H_2,$ $430~^\circ C$ and 1 h	11.41	[24]

Table 2. Comparative green kerosene production from waste oils through the hydrocracking reaction in batch mode.

3. Materials and Methods

3.1. Materials

Samples of low-cost raw material of palm oil mill effluent (POME) were collected from the waste water lagoon of E-san palm oil industry, Sakonakhorn, Thailand. A chemical catalyst, Pd/Al₂O₃, was purchased from Sigma (Missouri, MO, USA). An immobilised lipase of *Rhizopus oryzae* on sodium alginate (SAL beads) was prepared by a simple entrapment technique in a CaCl₂ solution. First, sodium alginate (2 g) was added into 100 mL of phosphate buffer (pH 7.0) solution. Then, it was heated at 40 °C until a homogeneous solution was obtained. After that, it was cooled down to room temperature. Subsequently, lipase (2 g) was mixed with alginate solution (100 mL). The mixture solution was dropped into 0.1 M CaCl₂ by a sterile syringe and stored at 4 °C for 12 h to form an alginate bead (Diameter size of 3 mm.). Finally, the immobilised bead was washed three times with distilled water and was kept in distilled water at 4 °C before being used as a biocatalyst in the hydrolysis reaction. The hydrolytic activity of the SAL beads was 360 U/mg. This was determined by the spectrophotometric method using p-nitrophenyl laurate (p-NPL) as the substrate [25].

3.2. Pretreatment of POME via Enzymatic Hydrolysis

The contaminants contained in POME, such as trunks barks and leaves, were separated by gravity method using a separating funnel [20]. Consequently, SAL beads (2 g), POME (100 mL) and distilled water (50% v/v) were loaded into a 250-mL Erlenmeyer flask. The hydrolysis reaction was conducted in an incubator shaker at 40 °C, 200 rpm for 4 h. The samples were further analysed to determine the FFA content, as described by a previous study [26]. The fatty acid yield (Y_{FA}) was calculated as shown in Equation (1). The fatty profile of hydrolysed POME (HPOME) was analysed by gas chromatography-spectrometry (GC-MS) following the standard method EN 1403. The HPOME sample (50 mg) and a 0.5 M methanolic sodium hydroxide solution (5 mL) were added into a reflux flask connected to the condenser. The reaction mixture in the reflux flask was heated to 140–160 $^{\circ}$ C for 5 min for a saponification reaction. Subsequently, a boron trifluoride-methanol solution (5 mL) was added and heated to 140–160 $^{\circ}$ C for 5 min for a methylation reaction. The mixture solution was cooled down to room temperature, followed by adding hexane (5 mL) and saturated sodium chloride solution (10 mL) in order to obtain fatty acid methyl ester (FAME). The bi-layer of the mixture reaction was observed. The FAME in the hexanic phase (upper layer) was dried by adding anhydrous sodium sulfate (1 g) and was filtrated through Whatman paper No. 1. Last, the samples were dissolved in heptane and filtrated through a microfilter (0.45 µm) before being injected into GC-MS equipped with a FID detector in order to identify the fatty acid composition, as described in previous studies [27]. The operating condition for the fatty acids' profile analysis was explained by Muanruksa et al. [28]. First, a 250-mg sample was filled into a 10-mL vial, followed by the addition of 5 mL of internal standard (methyl haptadecanoate solution, 10 mg/mL). Subsequently, the sample was analysed by gas chromatography-mass spectroscopy (GC-MS) (GC-2010, Shimadzu, Tokyo Japan) equipped with a 30-m long and 0.25-mm diameter

capillary column lined with a 0.25-µm(Rtx-5 ms, Rextex). Samples were injected in a split/column flow ratio of 24:1. Helium was used as the carrier gas at a flow rate of 1 mL/min. The injection temperature was 250 °C, and the column oven's temperature was 250 °C (programmed to start at 120 °C, held at this temperature for 5 min and heated at a rate of 3 °C/min to 250 °C).

$$YFA(\%) = \frac{FA2 - FA1}{FA2} \times 100\%$$
(1)

when FA1 is the FFA content of the oil sample before the hydrolysis reaction, and FA2 is the FFA content of the oil sample after the hydrolysis reaction.

3.3. Decarboxylation of Fatty Acid in HPOME

The hydrocarbon fuel production from hydrolysed POME (HPOME) was carried out in a high pressure batch reactor (HPAR) (See Figure 4). Raw materials of HPOME (100 mL) and Pd/Al₂O₃ (1 g) were loaded in a chamber of the reactor. Then, hydrogen was flushed three times to remove the oxygen in the reaction. Subsequently, it was fed to the reactor until a hydrogen pressure of 10 bars was reached at the initial stage, and the reaction temperature was set at 400 °C and kept constant for 1 h. Finally, the crude biofuel was refined by using a fractional distillation technique (ASTM D86).



Figure 4. Schematic diagram of high pressure autoclave reactor (HPAR).

3.4. Fractional Distillation

A commercially manual distillation apparatus (Koehler model K45200, New York, NY, USA) was used to conduct fractional distillation in this research work. The apparatus components met the standard of the ASTM D86 specifications, including a 125-mL sidearm

distillation flask (borosilicate glass), a 100-mL graduated cylinder with 1.0-mL graduation intervals and a mercury thermometer. The graduate cylinder was centered under the condenser tube exit to allow condensate drops to fall to the bottom of the cylinder. The HPOME (100 mL) was taken to be used as a liquid sample in the fractional distillation at 1 atm. The refined-biofuel products could be classified into three types based on their boiling points, including gasoline (50–150 °C), kerosene (150–280 °C) and diesel (280–360 °C), respectively. The percentages of crude-biofuel yield, refined-biofuel yield, green diesel selectivity, green kerosene selectivity and green gasoline selectivity were determined as described in Equations (2)–(6).

The liquid products were analysed by gas chromatography–mass spectroscopy (GC–MS) using a flame ionization detector (GC-FID-QP2010 Shimadzu, Tokyo, Japan) equipped with HT5 capillary columns (length of 15 m, diameter of 0.25 mm, film of 0.1 μ m), as described by a previous study [29]. The liquid samples (40 mg) were diluted via 4 mL hexane (high performance liquid chromatography (HPLC) grade). Then, 0.5 μ L of diluted sample was injected into the column. Helium was used as the carrier gas, and the flow rate was set at 1.5 mL/min. The oven temperature was first operated at 50 °C, held for 1 min, and then increased to 220 °C at the rate of 9 °C/min, followed by an increase of 20 °C/min to 350 °C, before being increased to 380 °C at the rate of 10 °C/min and held for 5 min. The n-alkanes and n-alkenes (C8–C20) were used as the chemical standard for the calibration curves to identify the composition of the liquid product. The internal standard was 1-bromohexane [27].

$$% Crude - biofuel yield = \frac{Total liquid product (mL)}{HPOME (mL)} \times 100\%$$
(2)

$$\% Refined - biofuel yield = \frac{Total \ distilled \ biofuels \ (mL)}{Crude \ biofuel \ (mL)} \times 100\%$$
(3)

$$\% Green \ diesel \ selectivity = \frac{Distilled \ green \ diesel \ (mL)}{Total \ refined - biofuel \ (mL)} \times 100\%$$
(4)

% Green kerosene selectivity =
$$\frac{Distilled green kerosene (mL)}{Total refined - biofuel (mL)} \times 100\%$$
 (5)

$$%Green gasoline selectivity = \frac{Distilled green gasoline (mL)}{Total refined - biofuel (mL)} \times 100\%$$
(6)

4. Conclusions

A combination of biochemical and thermochemical processes for the production of renewable biojet fuel from POME has successfully been performed in this study. The process provided a high efficiency in terms of a high green kerosene yield and a high selectivity of green kerosene. Additionally, the hydrocracking reaction could be carried out entirely using a low amount of catalyst, low H_2 pressure, moderate temperature and short reaction time. It was apparently indicated that the pretreatment of POME via the hydrolysis reaction was catalysed by immobilised lipase, resulting in positive effects on the hydrocracking reaction. Therefore, the POME showed a high potential use as a second-generation feedstock for producing biojet fuel. The heterogeneous catalytic process can be classified as a possible pathway for figuring out environmental issues related to POME, as well as for the development of a sustainable renewable energy production.

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Abstract: Photocatalytic and antibacterial activity of nanoparticles are strongly governed by their morphology. By varying the type of solvent used, one can obtain different shapes of ZnO nanoparticles and tune the amount of reactive oxygen species (ROS) and metal ion (Zn^{2+}) generation, which in turn dictates their activity. ZnO nanostructures were fabricated via facile wet chemical method by varying the type of solvents. Solar light assisted photocatalytic degradation of caffeine and antibacterial activity against *E. coli* were examined in presence ZnO nanostructures. In addition to an elaborate nanoparticle characterization, adsorption and kinetic experiments were performed to determine the ability of nanostructures to degrade caffeine. Zone of inhibition, time kill assay and electron microscopy imaging were carried out to assess the antibacterial activity. Experimental findings indicate that ZnO nanospheres generated maximum ROS and Zn²⁺ ions followed by ZnO nanopetals and ZnO nanorods. As a result, ZnO nanospheres exhibited highest degradation of caffeine as well as killing of *E. coli*. While ROS is mainly responsible for the photocatalytic activity of nanostructures, their antibacterial activity is mostly due to the combination of ROS, metal ion, physical attrition and cell internalization.

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Copyright: © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). Keywords: zinc oxide; nanosphere; nanorod; nanopetal; photocatalytic; antibacterial; caffeine; reactive oxygen species (ROS); degradation; pathogen

1. Introduction

Caffeine is one of the most abundant xenobiotics that causes water pollution due to its high daily consumption across the globe [1]. Apart from food industry, caffeine is also extensively used in the pharmaceutical industry [2,3]. Another pollutant found in wastewater effluents that causes serious health concerns are pathogenic microorganisms. *Escherichia coli* (*E. coli*) is a common pathogen found in aquatic environment and is known to cause several enteric diseases even at low concentrations [4]. Hence, it is imperative to treat these detrimental effluents before they can be discharged to water bodies. The conventional techniques employed by researchers for wastewater treatment are easy to handle and in most cases reusable [5]. However, most of the processes such as activated sludge-based technique, ion-exchange and coagulation have low treatment efficiencies and they are not cost effective in the long run. Even the advanced techniques such as membrane filtration faces a serious drawback of fouling that increases energy consumption and lowers the separation efficiency. To overcome these obstacles, nanotechnology offers a versatile and promising solution for the degradation of organic matter and elimination of microbes from wastewater in a cost-effective way.

A variety of nanomaterials have been investigated as photocatalysts for treating emerging contaminants from wastewater [6,7]. ZnO was selected for this study because of its low cost, simple synthesis technique and it can safely be used as antibacterial agent in food products [8–11]. It has been reported that ZnO nanoparticles can degrade a variety of contaminants and are effective against a wide range of bacteria but ZnO morphology

largely governs its photocatalytic and antibacterial properties [12–16]. A comparison of how different shape of ZnO nanoparticles affect its photocatalytic and antibacterial activity (against *E. coli*) is shown in Table 1. Despite the fact that morphology governs the photocatalytic activity of ZnO, there has been limited research to study the shape dependent photocatalytic and antibacterial activity of nanomaterials. A fundamental understanding of difference in activities arising from different nanoparticle morphologies and their mechanism of action is still unknown. Moreover, most of the previous studies have utilized UV irradiated nanoparticles for the photocatalytic degradation of caffeine [17–19].

	Particle Size (nm)	Model Pollutant	Photocatalytic Activity (% Degradation)	Maximum %Reduction in E. coli Growth	Ref
	9.6-25.5	Methylene blue (MB)	82.1% at 180 min UV exposure	69.2% at 100 μg/mL	[20]
ZnO sphere	133.7–260.2	MB	18% and 29% after 1 h UV exposure (1 g/L)	30 and 35% after 1 h exposure (1 g/L) $$	[21]
*	53.99	MB	95.45% after 180 min	Not reported	[22]
	4.35	4-nitrophenol	78% in 100 min	85% in 5 h at 100 µg/mL	[13]
	65.00	Acid Orange 74	80% after 80 min	99.93% at 20 min at 20 ppm NP	[23]
	214 22 1 172 22	MP	06 E2 after 180 min	Not non out of	[22]
7nO metale	214.36 × 176.22	IVID	90.52 after 180 min	00.07% often 20 min at 20 mm NID	[22]
ZnO petais	45.0	Acid Orange 74	90% after 80 min	99.97% after 20 min at 20 ppm INP	[23]
	$(1.41-1.8) \times (0.33-0.4)$	methylene blue and Congo red	81% for CR and 67% for MB after 80 min	90% for 150 mg/mL after 6 h	[24]
	155.0	MB	87.12 after 180 min	Not reported	[22]
ZnO rod	20.0	Orange II	100% after 150 minsolar irradiation with 1 mg/mL	100% in >3 h (1 mg/mL)	[25]
	76.0	Acid Orange 74	70% after 80 min	99.8% after 20 min t 20 ppm NP	[23]

Table 1. Comparison of photocatalytic and antibacterial activity of different shapes of ZnO nanoparticles

This study aims at determining the photocatalytic dependence of different nanostructures using solar light which is relatively inexpensive compared to the UV light. There are studies that individually report different nanostructures for their photocatalytic and antibacterial activity, but to the best of our knowledge, this is the first report to study the comparative solvent induced morphology-dependent photocatalytic and antibacterial mechanism of action of ZnO nanostructures. The goals of this study are: (i) To investigate the adsorption of caffeine on different morphology of nanoparticles (in dark) (ii) To evaluate the effect of initial caffeine concentration, amount of nanostructures and solar light intensity on the rate of caffeine degradation and estimate their kinetic rate constants, and (iii) study the antibacterial activity of ZnO nanostructures on *E. coli*.

2. Results and Discussion

2.1. Nanoparticle Characterization

2.1.1. Electron Microscopy

From the SEM images (Figure 1a–c), ZnO appears as well-defined nanospheres, nanorods and nanopetals under the influence of different solvents. PEG400 gives rise to spherical morphology; for water, we obtain petals attached to each other and for toluene, we obtain nanorod like structure. The morphological parameters are presented in Table 2. From the TEM images (Figure 1d–f), it can be seen that nanospherical ZnO are the smallest of all structures with an average diameter of 10.18 nm. Nanorods exhibited a mean width of 157 nm and a length of 1.43 μ m while nanopetals have an average thickness of 31.85 nm. The EDX analysis of nanoparticles is shown in the Supplementary Information (Table S1). It can be seen that the elemental composition does not change significantly with the change in ZnO morphology.



Figure 1. SEM (**a**–**c**) and TEM (**d**–**f**) images of ZnO nanomaterials synthesized in different solvents (**a**,**d**) PEG400 (**b**,**e**) water (**c**,**f**) toluene. (**g**) XRD spectra of different ZnO shapes (**h**) XRD spectra in the 2 θ range 30–40° showing the crystal growth direction.

Sample	Average Particle Diameter (nm) (TEM)	BET Specific Surface Area (m ² /g)	Total Pore Volume (cc/g)	Average Pore Diameter (nm)	Point of Zero Charge
ZnO sphere	10.18	92.22	0.15	6.64	4.90
ZnO petal	31.85 (petal thickness)	12.02	0.03	10.70	6.00
ZnO rod	157.00 (diameter)	6.60	0.017	10.26	6.80

Table 2. Characterization of ZnO nanostructures.

2.1.2. BET

The BET parameters for different morphologies of ZnO nanoparticles is given in Table 2. According to these results, the synthesized nanostructures have a mesoporous nature [26]. ZnO sphere had the largest specific surface area, highest pore volume and lowest average pore diameter. ZnO petals and rods has different specific surface areas and total pore volume but the average pore diameters were similar. These parameters are used to determine the effectiveness of nanoparticles.

2.1.3. X-ray Diffraction (XRD)

Figure 1g,h shows the XRD spectra of ZnO nanoparticles prepared in different solvents. The peaks at 31.85°, 34.52°, 36.23°, 47.50°, 56.50°, 62.9°, 66.29°, 67.92° and 68.82° indicate wurtzite hexagonal ZnO structure (JCPDS 89-1397). The preferred growth direction for ZnO were (101) for spheres and petals and (002) for ZnO rods. It can be seen that the (101) peak for ZnO nanorods is shifted towards lower diffraction angle. This may be attributed to the change in growth direction from (101) to (002) thereby reducing the strain along (101) direction.

2.1.4. Zeta Potential and Zn²⁺ Generation

The point of zero charge is indicative of the net charge of particles in the solution. A plot of zeta potential for different morphologies of ZnO is presented in Figure 2a. It was observed that the point of zero charge (pH_{ZC}) varied for different nanostructures. The pH_{ZC} for ZnO spheres was ~4.9 (4.86) while it shifted to 6.0 for petals and 6.8 for rods. The lower pH_{ZC} for spheres indicate better stability of spheres compared to other nanostructures at neutral pH. The lower pH_{ZC} of ZnO spheres is due to the presence of PEG molecules on ZnO nanoparticles. It has been shown in literature that the presence of differences in surface energy arising from the shape controlling process. Different surface energy of nanoparticle shapes leads to dissimilar adsorption of protons and hydroxyl ions on nanoparticles [28].



Figure 2. Cont.



Figure 2. (a) Zeta potential and (b) Zn^{2+} release curves of ZnO nanostructures synthesized using different solvents. Degradation kinetics of (c) NBT and (d) TA in presence of ZnO nanostructures for the quantification of superoxide ($\bullet O_2^-$) and hydroxyl radicals ($\bullet OH$), respectively.

The Zn^{2+} release profile is presented in Figure 2b. The ion release rates followed an order ZnO spheres > ZnO petals > ZnO rods.

2.1.5. Generation of Hydroxyl (OH•) and Superoxide Radicals ($\bullet O_2^-$)

The formation of superoxide radicals by ZnO nanostructures was analysed by nitroblue tetrazolium (NBT) assay and the plots are shown in Figure 2c. The reduction in absorbance of NBT with time was recorded and correlated with the concentration using standard calibaration curve. The extent of degradation can be directly correlated to the extent of ROS generatio which follows a similar trend like metal ion release: ZnO spheres > ZnO petals> ZnO rods.

Terephthalic acid degradation is a commonly used technique for the detection of hydroxyl radicals [29,30]. Terephthalic acid does not show any fluorescence peak but the product of terephthalic acid and hydroxyl radicals (2-hydroxyterephthalic acid) shows a characteristic fluorescent peak at 425 nm. The degradation rate of terephthalic acid by hydroxyl radicals is plotted in Figure 2d. It can be noted that the rate of generation of OH• is maximum in the first 40 min after which it slows down and stops. The fluorescence spectra of terephthalic acid in absence and presence of nanoparticles after 40 min is presented in the Supplementary Information (Figure S1). The intensity of fluorescent peak is indicative of the amount of OH• generated by the nanostructures and thus it is evident that ZnO sphere produces maximum number of OH• followed by ZnO petals and ZnO rods. This is similar to the trend showed by $\bullet O_2^{-}$.

2.2. Mechanism of Morphology Change with the Choice of Solvent

The main factors that lead to change in nanoparticle morphology are: seeding and growth direction, hydrolysis and solvent templating [31–33]. Spherical nanoparticles were formed in case of PEG because glycol chains surround Zn^{2+} ions and inhibit particle agglomeration. Moreover, PEG consists of two polar hydroxyl groups that bind to (002) plane (*c* direction) and promote growth along the (101) plane thus leading to spherical morphology [31]. On the contrary when water is used as a solvent, the rate of hydrolysis increases and the amount of ([Zn(OH)₄]²⁻) seeds increases. To reduce the overall surface energy of the system, petal like morphology is formed that attach to each other in a "template-like" fashion so that the system moves towards a more energetically favored low energy state [31]. Rod like ZnO nanostructures are formed when the crystals selectively grow along normal of the (002) plane is ineffective which directs the formation of ZnO along the perpendicular (002) plane giving rise to nanorods [31].

2.3. Caffeine Degradation2.3.1. Adsorption Study

A calibration curve for caffeine has been shown in the Supplementary Information (Figure S2). Figure 3 shows that the equilibrium adsorption capacity (q_e) increased with the increase in initial concentration of caffeine. At high caffeine concentrations, the adsorption sites get saturated and q_e either remains constant or decreases due to desorption. The increase in adsorption with the increase in caffeine concentration can be attributed to the high concertation gradient which promoted the mass transfer of aqueous caffeine towards solid ZnO nanostructures. We also studied the time dependence of adsorption process and found that the adsorption of caffeine on ZnO nanostructures was a two-stage process and it reached equilibrium in almost 45 min (unaffected by the concentrations of ZnO and caffeine and type of nanoparticles). The first 20 min witnessed a rapid adsorption followed by a slower phase of 25 min of gradual uptake. A large number of unoccupied adsorption sites on ZnO nanostructures promoted an initial rapid adsorption and the rate slowed down when most of these sites were occupied.





Langmuir and Freundlich isotherms (Equations (2) and (3)) were used to fit the adsorption data and the plots are shown in Figure 3. The equilibrium adsorption capacity of ZnO nanostructures was calculated at different initial concentration of caffeine and the

isotherm parameters are presented in Table 3. The coefficient of regression (\mathbb{R}^2) and chisquare values (χ^2) were also tabulated for the assessment of goodness-of-fit for these models. We note that although both these models describe the experimental data well, yet Langmuir model provides a better fit since the correlation coefficient (\mathbb{R}^2) values for Langmuir adsorption isotherm is higher than that for Freundlich isotherm. Langmuir isotherm is based on the assumption that the molecules to be adsorbed form a monolayer on the adsorbent surface and there is ideally no chemical reaction involved between the two (physisorption). In this study, the experimentally determined adsorption capacity is similar to the theoretical one, thus supporting the Langmuir isotherm.

Comm10	I	Langmuir Model				Freundlich Model		
Sample	q _m (mg/g)	b (L/mg)	R ²	x ²	1/n	$K_{f} (mg^{1-1/n} (L)^{1/n}(g)^{-1})$	R ²	x ²
ZnO-sphere	12.57	0.06	0.89	0.61	0.45	1.74	0.80	0.85
ZnO-petal	5.28	0.14	0.78	0.14	0.28	1.64	0.77	0.14
ZnO-rod	6.04	0.09	0.78	0.26	0.36	1.26	0.64	0.44

Table 3. Isotherm parameters for Langmuir and Freundlich adsorption models.

Freundlich isotherm is based on the assumption that there are chemical interactions involved between the molecules to be adsorbed and a heterogeneous adsorbing surface (chemisorption) leading to the formation of a multiple layers of adsorbing molecule. In our case, Freundlich isotherm fits the data as well, suggesting that caffeine molecules occupy heterogeneous adsorption sites on ZnO nanostructure surfaces and chemical interaction between caffeine molecules and ZnO may also contribute to the adsorption process. From Table 3, it can be seen that the values for b in Langmuir isotherm fall in between 0 and 1 which implies that the adsorption of caffeine on ZnO nanostructures is favorable [32]. Similarly, the parameter 1/n < 1 in Freundlich isotherm also implies a favorable adsorption.

It was found that the maximum adsorption capacity (Q_m) for ZnO spheres (12.57 mg/g) was double compared to ZnO rods and petals. This difference in maximum adsorption capacities can be attributed to the different shapes, sizes and porosity of ZnO nanostructures.

2.3.2. Photocatalytic Experiments

We first tried to rule out the effect of photolysis from photocatalysis and for this purpose, we studied the degradation of caffeine in presence of 250 mW/m^2 visible light and absence of nanoparticles. The results shown in Supplementary Information (Figure S3) indicate that caffeine is only slightly affected by photolysis and thus we can exclude the effect of photolysis and perform photocatalytic study to describe the degradation. Next, we estimated the effect of different initial caffeine concentrations, ZnO concentration and morphologies and visible light intensities on the photocatalytic degradation of caffeine.

Nanoparticle Dosage

The effect of nanoparticle dosage on caffeine degradation was analyzed to find the lowest dosage at which the interaction of nanoparticles with caffeine can be maximized. We tested the degradation of caffeine at four different concentrations of ZnO (0.5, 1.0, 1.5 and 2.0 g/L) and it was seen that caffeine degraded faster when nanoparticle concentration was increased from 0.5 to 1.0 g/L for all morphologies of nanoparticles but it decreased at higher concentrations. This phenomenon can be explained by the tendency of nanoparticles to agglomerate at higher concentrations leading to a decrease in overall available surface area and an increase in diffusion time. Hence a nanoparticle dosage of 1.0 g/L was chosen for all subsequent experiments.

Initial Concentration of Caffeine and Nanoparticle Morphology

After the adsorption equilibrium was reached, we subjected the samples to 250 mW/cm^2 of simulated solar light and 1.0 g/L nanoparticle dosage for the photocatalytic experi-

ments. The photocatalytic data was fitted to pseudo-first order and pseudo-second order kinetic model (Equations (4) and (5)) as shown in Figure 4 and the value of rate constants were calculated from the above-mentioned equations using non-linear regression (Levenberg–Marquardt algorithm, 10^{-5} tolerance). From the R² values (shown in Table 4), it can be concluded that the experimental data can be suitably represented by both the kinetic models with high correlation coefficients. The rate constants for ZnO sphere falls with the rise in amount of caffeine. ZnO spheres exhibited the highest value of degradation rate constant at the lowest caffeine concertation of 10 ppm (k₁-1.323 min⁻¹, k₂-1.74 g/mg min). This is about 1.1 times (k₁ and k₂) higher than that achieved by petals whereas 1.6-(k₁) and 2.2-(k₂) times higher than the degradation achieved by ZnO rods. At highest concentration, ZnO spheres are 1.4-(first order) and 2.8-fold (second order) higher than ZnO petals whereas 2.6-(first order) and 2.5-fold (second order) higher compared to ZnO rods. Thus, the differences in the rate of caffeine degradation is more pronounced at higher concentrations irrespective of the morphology.

Table 4. Kinetic rate parameters for caffeine degradation by ZnO nanostructures (Experimental conditions: $[ZnO] = 1.0 \text{ g L}^{-1}$, light intensity = 250 mW/cm²).

Sample	Parameter	Caffeine Concentration (ppm)					Light Intensity (mW/cm ²)		
Sampre		10	20	30	40	50	50	150	250
	$0.1 \text{ k}_1 * (\min^{-1})$	1.32	1.33	0.69	0.48	0.43	0.21	0.23	0.48
7nO sphere	R ²	0.97	0.97	0.96	0.96	0.98	0.97	0.99	0.99
ZhO sphere	0.01 k ₂ * (g/mg min)	1.74	0.97	0.26	0.16	0.10	0.07	0.06	0.09
	R ²	0.94	0.99	0.99	0.98	0.99	0.97	0.99	0.99
7.0	$0.1 \text{ k}_1 \text{ (min}^{-1})$	1.24	0.61	0.59	0.24	0.32	0.11	0.26	0.43
	R ²	0.99	0.95	0.96	0.98	0.97	0.99	0.95	0.97
ZhO petai	0.01 k ₂ (g/mg min)	1.65	0.34	0.22	0.05	0.07	0.03	0.05	0.07
	R ²	0.98	0.97	0.99	0.99	0.98	0.99	0.97	0.99
	$0.1 \ k_1 \ (min^{-1})$	0.81	0.35	0.15	0.12	0.16	0.10	0.03	0.12
ZnO rod	R ²	0.96	0.98	0.98	0.98	0.99	0.96	0.99	0.99
	0.01 k ₂ (g/mg min)	0.77	0.15	0.03	0.02	0.04	0.02	0.01	0.02
		0.96	0.99	0.98	0.99	0.99	0.96	0.99	0.99

* k1 is pseudo-first order rate constant, and k2 is pseudo-second order rate constant.

In terms of percentage degradation, it can be seen that ZnO spheres could degrade 72.5% of 30 ppm caffeine in 30 min and complete degradation was achieved in 120 min while the degradation rates for ZnO petals was 69% in 30 min and complete degradation in 135 min and rods was only 37% after 30 min and complete degradation in and complete degradation in 180 min. The corresponding degradation rates for different morphologies of ZnO can be listed as follows: ZnO spheres > ZnO petals > ZnO rods. Based on these findings, it could be perceived that the enhanced generation of ROS (Figure 2) in case of ZnO spheres might contribute to the increased photocatalytic activity.



Figure 4. Kinetic model for the adsorption of caffeine on ZnO nanostructures at (a-c) various caffeine concentrations and (d-f) different light intensity. (—) and (- -) represent pseudo-first-order and pseudo-second-order model, respectively.

Light Intensity

The degradation constant for caffeine increased with the increase in light intensity as a result of ROS generation and subsequent oxidation of caffeine (Figure 4d–f). The rate constants ae presented in Table 4 and it was evident that a light intensity of 250 mW/cm² resulted in the highest rate of degradation.

When the solar light is incident on these nanostructures, photons are adsorbed on the surface of nanostructures causing electron-hole pair to form. These pairs reach the surface of nanostructures, the electrons (in conduction band) are scavenged by the O_2 molecules present in the medium leading to the generation of ROS ($\bullet O_2^-$) and the holes remain in the valance band. The holes also contribute to the generation of other ROS species (such as $\bullet OH$) by reacting with water molecules. These radicals react with the caffeine molecules, subsequently degrading it into harmless products such as CO_2 and H_2O .

2.4. Antibacterial Activity

2.4.1. Minimum Inhibitory Concentration (MIC)

The minimum inhibitory concentration (MIC) of nanostructures for *E. coli* is listed in Table 5. MIC values for different nanostructures (for both *S.aureus* and *E. coli*) under consideration is as follows: ZnO sphere < ZnO rod < ZnO petal. Maximum value of MIC among all the nanostructures (90 μ g/mL) was chosen for all subsequent experiments.

Sample	MIC Value (µg/mL)	Reference
	60	[33,34]
ZnO-sphere	78	[14]
_	65	This study
	25	[34,35]
ZnO-petals	5	[35,36]
-	72	This study
	2	[36,37]
ZnO-rods	512	[37,38]
	90	This study

Table 5. MIC values for different morphologies of ZnO against E. coli.

2.4.2. Zone of Inhibition (Disc Diffusion Assay)

The antibacterial property of ZnO nanostructures was assessed against *E. coli* by standard disc diffusion assay. The diameter of zone of inhibitions obtained after overnight incubation with nanostructures (different concentrations) was measured and shown in Figure 5a,b. Among the different shapes of ZnO, ZnO spheres showed the best activity whereas ZnO petals and rods produced almost similar zone of inhibitions.

2.4.3. Cell Viability Assay (CFU/mL)

To quantitatively assess the interaction of nanostructures with bacteria, the antibacterial tests were carried out in by suspending nanostructures (90 μ g/mL) in liquid media contaning bacteria under constant shaking in dark at 37 °C. The number of viable bacteria were noted by counting the number of colonies (CFU/mL) and shown in Figure 5c. It was found that ZnO sphere and petals reduced the growth of bacteria to nearly 2.0 log CFU and 2.8 log CFU within 12 h, respectively. However, ZnO rods showed a much lower antibacterial activity of 5.0 log CFU reduction after 12 h treatment time. Thus among the different shapes of ZnO, ZnO spheres showed the highest reduction in cell viability followed by ZnO petals and ZnO rods.



Figure 5. (**a**,**b**) Zone of inhibition (cm) formed in disc diffusion assay against *E. coli* for different concentration of nanostructures (20, 60, 100, 150 μ g/mL) (**c**) Cell viability assay, and (**d**) Protein leakage analysis for *E. coli* treated with different morphologies of ZnO nanostructures.

2.4.4. Protein Leakage Analysis

In order to further confirm the rupture of membrane and leakage of cellular contents, the concentration of protein leaked out of the cell was monitored with time. Higher protein leakage is associated with a greated degree of membrane disruption. Leakage of proteins was detected in the medium containing nanostructure-exposed cells whereas almost negligible protein leakage was observed for untreated *E. coli* (Figure 5d). Maximum protein leakage was observed after 3 h for ZnO spheres and petals (32.59 and 22.41 μ g/mL, respectively) and 2 h for rods (21.08 μ g/mL). The permeability of cell membranes increase after proteins are leaked out in the soution which leads to oxidative stress in the cells [39].

2.4.5. Imaging

The FESEM images and EDS spectra of control and nanoparticle treated *E. coli* are shown in Figure 6a,c,e,g,i–k. Before the antibacterial treatment, *E. coli* had a well-defined rod shape and an integrated cell wall structure. On exposure to nanostructures, the original shape of bacteria was damaged with holes and ruptured cell membrane and the nanostructures were seen to be in close proximity with the cells. Drainage of cell contents from *E. coli* was also evident. *E. coli* following nanoparticle exposure revealed the presence of ZnO



petals near the cells (Figure 6g). EDS spectra of bacteria-nanoparticle system indicates ZnO peaks which indicates ZnO around the damaged bacteria specimen.

Figure 6. Scanning electron microscope images (**a**,**c**,**e**,**g**), Transmission electron microscope images (**b**,**d**,**f**,**h**) and EDS spectra for (**i**–**k**) for (**a**,**b**) Control (**c**,**d**,**i**) *E. coli* treated with ZnO sphere (**e**,**f**,**j**) *E. coli* treated with ZnO petals (**g**,**h**,**k**) *E. coli* treated with ZnO rod.

To further visualize the direct interaction between nanostructures and bacteria, TEM imaging experiments were performed. ZnO spheres penetrated the cell walls and internalize the cells leading to cell death (Figure 6e). ZnO petals did not internalize the cells (Figure 6f) and the antibacterial activity can be attributed to physical attrition. No internalization was seen in case of ZnO rods as well (Figure 6h), which implies that the sharp edges of ZnO rods pierced the cells and physical attrition led to the cell damage. Apart from physical attrition and cell internalization, ROS generation and Zn²⁺ toxicity are also responsible for the antibacterial activity of nanostructures. All the structures were found to adhere to the bacteria cell walls but except for ZnO spheres, no internalization was observed for other particles. Thus, cell wall damage and cytoplasm leakage for rods and petals was caused by other mechanisms such as physical attrition, ROS generation and cation release. The small size of ZnO spheres enable them to penetrate the bacterial cell resulting in cell death. The ROS and cations react with the intracellular contents of the bacteria and inactivate the cell. Studies have shown that ROS released from bigger nanostructures interacts with the cell membrane of these bacteria and oxidize the phospholipid contents of the membrane [13,40]. However, for smaller structures, the internalized contents are more damaged compared to the cell membrane. Thus, the rigidity of cell membrane, generation of holes and pits on the surface and leakage of internal contents

are mostly determined by the morphology of nanostructures. Another theory that may find its applicability in this case is the abrasiveness of different nanostructures. ZnO rods have rough edges and sharp ends that causes mechanical damage to the membranes (physical attrition and piercing action) creating holes and pits causing localized leakage of cell contents.

All the antibacterial experiments with ZnO nanostructures were conducted in dark, suggesting that the cell membrane distortion by physical interaction with nanostructures and reaction of cell contents with cations might be a bigger contributor to cell damage compared to ROS [41,42].

Being a chemical process, there is no directly visible effect of nanoparticle shape on caffeine degradation and it is mostly governed by the ROS and Zn^{2+} released by nanostructures. On the contrary, shape of nanoparticles were visually evident to play a major role in *E. coli* disinfection since physical interaction of nanoparticles with bacteria is one of the ways that lead to cell death. For example, nanoparticles with sharp edges have a different mechanism of killing bacteria as compared to smooth surfaces. However, in addition to shape, we cannot also rule out the role of surface area in the photocatalytic and antibacterial activity of ZnO nanoparticles. For example, nanoparticles with larger surface area (ZnO sphere) were found to generate more ROS and Zn^{2+} as compared to the ones with lower surface area (ZnO petals and rods), thus affecting caffeine degradation in different ways. Additionally, smaller nanoparticles could internalize the bacterial cell and distort the cellular contents as compared to larger nanostructures that were limited to outer cell wall damage. Thus, the effect of surface area must also be considered in addition to shape to gain a clear understanding of the photocatalytic and antibacterial activity of these nanostructures.

3. Experimental Details

3.1. Materials

All the materials used in this work were of analytical grade and used without further purification. Zinc nitrate hexahydrate [99%] was purchased from JT Baker Chemicals, Phillipsburg, NJ, USA and sodium hydroxide [NaOH] was obtained from Caledon Laboratories Ltd., Georgetown, ON, Canada. Caffeine and polyethylene glycol (Kollisolv PEG E 400) were procured from Sigma Aldrich, Oakville, ON, Canada. Pure agar and Luria Bertani (LB) media were provided by HI MEDIA Laboratories, Bengaluru, Karnataka, India. Bacteria *Escherichia coli* (NCIM 2137) was purchased from NCIM, NCL Pune, Pune, Maharashtra, India.

3.2. Method

3.2.1. Synthesis of Nanoparticles

Different morphologies of ZnO nanoparticles were obtained by the hydrolysis reaction of zinc nitrate hexahydrate $Zn(NO_3)_2$ ·6H₂O in different solvents. The details of the synthesis procedure can be found elsewhere [14]. Briefly, 0.1 M Zn(NO₃)₂·6H₂O in 100 mL solvent (either PEG400 or water or toluene) was kept under magnetic stirring followed by the addition of 2 M NaOH. After 45 min, the nanoparticles were collected by ultracentrifugation, washing, overnight drying for 12 h and calcining at 300 °C.

3.2.2. Characterization of Nanomaterials

The synthesized nanoparticles were characterized using scanning electron microscope (SEM, Hitachi, Tokyo, Japan) for surface morphology. Nanoparticles were coated with platinum before imaging to avoid the charge accumulation near the surface of the particles. The shape and size of the nanomaterials were assessed using a JEOL High-Resolution Transmission Electron Microscope (HRTEM, Tokyo, Japan). BET analysis was performed for the estimation of porosity and specific surface area of nanomaterials using a Quantachrome ASiQwin-Automated Gas Sorption Data Acquisition and Reduction instrument (outgassing time: 1.5 h, temperature: 270 °C, Boynton Beach, FL, USA) with nitrogen as the

adsorption gas. The phase composition of the samples was determined using a Panalytical High Resolution XRD-I, PW 3040/60 (Chennai, Tamil Nadu, India). The 2-theta angle was from 30° to 80° using a CuK α radiation ($\lambda = 1.5418$ Å). Zeta potential of particles was measured by Zetasizer Nano-ZS-90 (Malvern Instruments, Malvern, UK) with the scattering angle in the range of 90° to 25°. Nanoparticles (10 μ g/mL) were ultrasonically dispersed in distilled water and measured under automatic mode. Dissolution of metal ions in water was studied for all the nanoparticles at a concentration of 90µg/mL. Aliquots from the supernatant of the suspension were collected and nanoparticles were separated by centrifugation. The supernatant was analyzed by PinAAcle 900 H atomic absorption spectrometer (AAS), Waltham, MA, USA. The standard deviation of triplicate measurements has been reported for all the experiments. The superoxide radicals $(\bullet O_2^{-})$ from ZnO nanoparticles were measured using nitroblue tetrazolium (NBT) assay [14]. One mM NBT was added to 100 mL of methanol (4%) and nanoparticles (90 μ g/mL) under magnetic stirring, regular samples were withdrawn and UV-vis spectra was recorded from 200-400 nm. The hydroxyl radicals (OH•) were estimated by measuring the reaction product of terephthalic acid in solution. Briefly, a solution of 0.5 mM of terephthalic acid was prepared in NaOH and ZnO nanoparticles (90 μ g/mL) were ultrasonically dispersed in the solution. Samples were withdrawn, centrifuged and the excitation fluorescence spectra was taken at 315 nm using.

3.2.3. Photocatalytic Degradation of Caffeine Adsorption Study

The adsorption of caffeine on different morphology of ZnO nanoparticles was studied using UV–vis spectrophotometer (UV-3600, Shimadzu Scientific Instruments, Columbia, MD, USA) and the spectra were recorded in a range of 250–350 nm. Batch adsorption experiments were conducted with 1 g/L of ZnO nanoparticles with different caffeine concentrations (~10, 20, 30, 40, 50 ppm) under shaking in dark at 150 rpm for 2 h. The adsorption studies were performed to determine the time required to reach equilibrium and to calculate the adsorption coefficients. The equilibrium adsorption capacity of caffeine on nanoparticles (q_e , mg/g) was calculated by Equation (1):

$$q_e = (C_0 - C_e) \times \frac{V}{W} \tag{1}$$

where C_0 and C_e are the initial and equilibrium concentrations of caffeine (ppm), respectively, *V* is the volume of caffeine solution (L) and *W* is the weight of nanoparticles used (g).

Adsorption isotherms are fundamental for describing the adsorption capability of adsorbents. The equilibrium adsorption isotherms were developed by plotting the equilibrium concentration of caffeine and its corresponding uptake. The Langmuir isotherm is based on the assumption of monolayer adsorption of adsorbate on the adsorbent surface, and is given by the following expression:

$$q_e = \frac{bq_m C_e}{1 + bC_e} \tag{2}$$

where, C_e (mg/L) and q_e (mg/g) represent the concentration and amount of adsorbed material, respectively and q_m (mg/g) and b (L/mg) are the maximum adsorption capacity and Langmuir constant, respectively. The Freundlich isotherm is valid for adsorption on a heterogeneous surface and is given by

$$q_e = K_F(C_e)^{\frac{1}{n}} \tag{3}$$

where, K_F (mg/g) and *n* are capacity and adsorption favorability, respectively.

Kinetic Study

In a typical kinetic study, the important variables that affect the photocatalytic process are photocatalyst concentration, initial concentration of pollutant and light intensity. Batch experiments were conducted using nanoparticle/caffeine suspension of required concentration at neutral pH. The solution was kept under shaking at 150 rpm and the samples were analyzed in UV–vis spectrophotometer at regular intervals. The aliquots were filtered through a 0.45 μ m filter prior to the absorbance measurements. A solar simulator (SS1 KW, ScienceTech, London, ON, Canada) equipped with a 1000 W Xe arc lamp and an Air-Mass (AM) 1.5 G filter was used to irradiate the sample with visible light.

The optimum amount of ZnO nanoparticles required for caffeine degradation was determined first. For this, four different concentrations of nanoparticles (0.5, 1, 1.5, 2 g/L). To investigate the effect of light intensity on caffeine degradation four different light intensities (50, 150 and 250 mW/cm²) were used at optimum dosage of nanoparticles (1 g/L) and 30 ppm caffeine concentration. The initial concentration of caffeine (10, 20, 30, 40, 50 ppm) was subsequently varied at 250 mW/cm² light intensity (which provides highest degradation). All the experiments were carried out under constant magnetic stirring at room temperature. From the adsorption studies, it was seen that the adsorption equilibrium was reached after 1.5 h and accordingly, the photocatalytic experiments were carried out after 1.5 h of dark reaction.

The kinetics of caffeine adsorption by nanoparticles was investigated using a pseudofirst-order and pseudo-second-order kinetics, given by the following equations:

$$q_t = q_e(1 - \exp(k_1 t)) \tag{4}$$

$$q_t = \frac{k_2 q_e^2 t}{1 + k_2 q_e t}$$
(5)

where, q_t and q_c are the adsorption capacities of nanoparticles (mg/g) at time *t* and equilibrium respectively and k_1 (min⁻¹) and k_2 (g/mg min) are the pseudo-first-order and pseudo-second order rate constants, respectively.

3.2.4. Bacterial Toxicity Assessment

E. coli was incubated overnight in Luria Bertani (LB) broth at 37 $^{\circ}$ C under constant shaking (120 rpm). The CFU/mL of bacteria was adjusted to 10⁸ for all the experiments unless otherwise stated.

Minimum Inhibitory Concentration (MIC)

The MIC value is the minimum concentration of nanomaterials that prevents any visible development of pathogen colonies. To obtain the MIC values, overnight grown cultures of *E. coli* and nanostructures (10–150 μ g/mL) were mixed and incubated for 24 h. The optical density (OD) was recorded at 590 nm and the MIC value was reported as the one that inhibited the growth of 99% bacteria. The MIC value obtained from experiments (90 μ g/mL) will be used for all subsequent experiments unless otherwise stated.

Zone of Inhibition

For the disc diffusion assay, different concentrations of nanoparticles (25, 50, 75, 100 and 150 μ g/mL) were ultrasonically coated on paper discs (8 mm). Ten μ L bacteria (10⁸ CFU/mL) was spread on solidified agar plates and the paper disk was positioned above the bacteria coated agar and kept at 37 °C for 12 h. The zone diameter (mm) after incubation was measured and a mean value of triplicate experiments was noted.

Cell Viability Assay (CFU/mL)

Change in bacterial CFU with time in absence and presence of nanoparticles provides an estimate of the antibacterial strength of nanoparticles. Bacteria was incubated at 37 $^{\circ}$ C with nanoparticles and the CFU was recorded at intermediate times for a duration of 12 h. The CFU value obtained from the average of three experiments falling within 95% confidence interval were recorded.

Protein Leakage Analysis (Bradford Assay)

The protein released by nanoparticle treated deformed cells was quantified by Bradford assay [43]. Briefly, cells were washed and re-dispersed in PBS along with nanoparticles and incubated under shaking at 120 rpm and 30 °C. Aliquots of sample (1 mL) were withdrawn every hour, centrifuged and a solution of 200 μ L supernatant and 800 μ L Bradford's reagent was prepared and incubated in dark for 10 min. The absorbance of the samples was measured at 595 nm with the help of a spectrophotometer.

Imaging of Bacteria-Nanoparticle Interaction

Damage to the bacteria cell morphology before and after exposure to nanoparticles was observed in SEM. Samples were platinum coated prior to the SEM analysis. Bacteria treated with nanoparticles for 10 h were dropped on a coverslip, kept in 2.5% glutaraldehyde solution for 12 h at 4 °C and then dehydrated using ethanol. And the samples were vacuum dried prior to imaging. For the TEM imaging, a drop of untreated and treated bacteria was dropped on a carbon coated copper grid, dried and imaged.

4. Conclusions

Morphology-controlled ZnO were successfully synthesized by wet chemical process. The nature of solvent used for synthesis had a significant impact on the size and direction of crystal growth. Electron microscopy images showed that sphere, petal and rod-like ZnO were formed in PEG400, water and toluene, respectively. These nanostructures were studied for caffeine degradation and *E. coli* disinfection. The ROS and Zn^{2+} ions generated by these nanostructures were mainly responsible for the nanoparticle activity. The ROS consisted of O_2^- and OH• while H₂O₂ was found to be insufficient to show any photocatalytic or antibacterial activity. These nanostructures were very effective for the degradation of caffeine using solar light which has a relatively low operating cost compared to UV photocatalytic processes. The nanostructures were also effective in killing 99% of bacteria at low concentrations. However, some questions still remain unanswered and further studies are needed to determine the intermediate products of caffeine degradation by different nanostructures. Future studies should also focus on how photocatalytic and antibacterial activity are affected by other parameters such as water chemistry, pH, temperature, etc. and the toxicity of different nanostructures in environment.

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Article



N-Donor Ligand Supported "ReO₂⁺": A Pre-Catalyst for the Deoxydehydration of Diols and Polyols

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Abstract: A selected number of tetradentate N₂Py₂ ligand-supported ReO₂⁺ complexes and a monodentate pyridine-supported ReO₂⁺ complex have been investigated as catalysts for the deoxydehydration (DODH) of diols and polyols. In situ ¹H NMR experiments showed that these N-donor ligand-supported ReO₂⁺ complexes are only the pre-catalyst of the DODH reaction. Treatment of (N₂Py₂) ReO₂⁺ with an excess amount of water generates an active species for DODH catalysis; use of the Re-product of this reaction shows a much shorter induction period compared to the pristine complex. No ligand is coordinated to the "water-treated" complex indicating that the real catalyst is formed after ligand dissociation. IR analysis suggested this catalyst to be a rhenium-oxide/hydroxide oligomer. The monodentate pyridine ligand is much easier to dissociate from the metal center than a tetradentate N₂Py₂ ligand, which makes the Py₄ReO₂⁺-initiated DODH reaction more efficient. For the Py₄ReO₂⁺-initiated DODH of diols and biomass-based polyols, both PPh₃ and 3-pentanol could be used as a reductant. Excellent olefin yields are achieved.

Keywords: deoxydehydration reactions; rhenium-based pre-catalyst; biomass conversion

1. Introduction

Cellulosic biomass is currently being considered as a potential renewable feedstock for the chemical industry [1]. Unlike petroleum-based resources, the typical platform molecules that can be obtained after depolymerization of cellulosic biomass are overfunctionalized with oxygen-based functional groups. Accordingly, one of the challenges of using cellulosic biomass for chemical production is its defunctionalization to building blocks of lower oxygen content. Several pathways, for example, dehydration [2], deoxygenation [3,4], and deoxydehydration [5,6] have been reported for this purpose during the past two decades. Among these, deoxydehydration (DODH) reactions are known as an efficient way to remove vicinal hydroxyl groups to form the corresponding olefins. Metal complexes, such as vanadium complexes [7–10], molybdenum complexes [11–18], and rhenium complexes [5,19] have been reported to be able to catalyze the DODH of diols and polyols. In terms of activity and selectivity, rhenium complexes have shown unique properties amongst these complexes. Trioxo-rhenium complexes are known as catalysts for DODH reactions since the first Cp^{*}ReO₃-catalyzed DODH reaction was described by Cook and Andrews [20]. Later on, new catalysts based on Cp-ligands were reported by Klein Gebbink et al. [21,22]. Next to the development of new Re-based DODH catalysts, investigations in this field have also focused on the mechanism by which the rhenium catalysts operate in DODH reactions [23]. It is generally agreed that the catalytic cycle of these high-valent rhenium catalysts consists of three steps: a. reduction of the Re(VII) trioxo complex to a Re(V) dioxo species, b. condensation of the diol substrate to form a Re-diolate intermediate, and c. olefin extrusion from the reduced diolate intermediate to form the organic reaction product and regenerate the Re(VII)

trioxo complex (Scheme 1). The reduction step can proceed either before or after the condensation step, and the order of these steps is highly dependent on the combination of metal, reductant, and substrate. From these mechanistic considerations it becomes clear that only two oxo ligands are involved in actual bond making and breaking in the catalytic cycle, and that one oxo ligand (shown in red in Scheme 1) can in principle be considered as a spectator ligand. The question thus arises whether or not Re(V) dioxo complexes are also capable of catalyzing DODH reactions of diols and polyols.



Scheme 1. Proposed catalytic cycle of the trioxo-rhenium catalyzed deoxydehydration (DODH) of diols.

Using a Re(V) dioxo complex as the catalyst, catalysis could proceed through a Re(V) \leftrightarrow Re(III) cycle instead of a Re(VII) \leftrightarrow Re(V) one. In 2013, a Re(V) \leftrightarrow Re(III) catalytic cycle was proposed by Abu-Omar et al. for a DODH reaction catalyzed by methyltrioxorhenium (MTO) using a secondary alcohol as reductant (Scheme 2) [24]. In this mechanism, MTO is reduced to methyldioxorhenium (MDO) via reduction by the secondary alcohol or via oxidative cleavage of an aromatic diolate ligand of a Re(VII)-diolate formed through condensation of the diol with MTO. MDO then condenses with a next diol to form a Re(V)-diolate intermediate, which would be further reduced by a secondary alcohol to form a Re(III)-diolate species, followed by olefin extrusion to regenerate MDO. In this reaction sequence, the Re(V) dioxo species MDO is considered as the true catalyst of the DODH reaction.



Scheme 2. Proposed mechanism of methyltrioxorhenium (MTO)-catalyzed DODH via a $Re(V) \leftrightarrow Re(III)$ cycle. [24].

Besides the mechanistic proposal by Abu-Omar, Nicholas et al. have investigated *trans*-[(Py)₄ReO₂]⁺ dioxo-rhenium complexes, i.e., *trans*-[(Py₄)ReO₂]PF₆ and *trans*-[(Py₄)ReO₂]Cl, as a catalyst for the deoxydehydration of 1,2-decanediol using zinc as reductant [25]. Even though this reaction starts from a Re(V) dioxo species, a Re(V) \leftrightarrow Re(VII) catalytic cycle was proposed. In a reaction of 1,2-decanediol (1.6 equiv.) and *trans*-[(Py₄)ReO₂]Cl (1.0 equiv.), 98% of 1-decene (with respect to Re) formed and no oxidation products of the diol (aldehydes, ketones) were detected. This result indicated that the starting Re(V) complex is not reduced by the diol, i.e., a Re(V) \leftrightarrow Re(VII) redox change is involved in the reaction and a [(Py)_nRe(VII)O₃]⁺ intermediate is generated during the reaction (Scheme 3). In other words, catalytic cycles involving either a Re(V) \leftrightarrow Re(VII) or a Re(V) \leftrightarrow Re(VII) interconversion have been proposed for DODH catalysis starting from a Re(V) dioxo species.



Scheme 3. Stochiometric reaction of 1,2-decanediol and trans-[(Py₄)ReO₂]Cl [25].

Recently, a series of *cis*-dioxo-rhenium(V/VI) complexes containing tetradentate N₂Py₂ ligands were reported by Che and coworkers [26]. The authors showed, amongst other, that the [(BPMCN)ReO₂]²⁺ ion (BPMCN = N^1 , N^2 -dimethyl- N^1 , N^2 -bis(pyridin-2-ylmethyl)cyclohexane-1,2-diamine), which was prepared by constant potential oxidation of [(BPMCN)ReO₂]⁺, is able to oxidize hydrocarbons with weak C–H bonds (75.5–76.3 kcal mol⁻¹) via hydrogen atom abstraction. In view of the discussion above, Re(V) dioxo complexes like the ones reported by Che could be interesting catalyst candidates for deoxydehydration reactions. Accordingly, we set out to synthesize *cis*-dioxo-rhenium(V) complexes supported by tetradentate N₂Py₂ ligands and to investigate these as catalysts for the DODH of vicinal diols.

2. Results and Discussion

2.1. Synthesis of Rhenium Complexes

For our initial study, *cis*-[(*S*,*S*-BPBP)ReO₂]PF₆ (1) (*S*,*S*-BPBP = (2*S*,2'*S*)-1,1'-bis(pyridin-2-ylmethyl)-2,2'-bipyrrolidine), *cis*-[(BPMEN)ReO₂]PF₆ (2) (BPMEN = N^1 , N^2 -dimethyl- N^1 , N^2 -bis(pyridin-2-ylmethyl)ethane-1,2-diamine), and *cis*-[(B^{mdm}PMEN)ReO₂]PF₆ (3) (B^{mdm}PMEN = N^1 , N^2 -bis((4-methoxy-3,*S*-dimethylpyridin-2-yl)methyl)- N^1 , N^2 -dimethyl ethane-1,2-diamine) (Scheme 4) were synthesized according to the protocol developed by Che et al. for the synthesis of 1 [25]. To this end, reaction of IReO₂(PPh₃)₂ with the corresponding N₂Py₂ ligand in dichloromethane afforded crude *cis*-[(N₂Py₂)ReO₂], which was then reacted with NH₄PF₆ to afford 2 and 3 in 40% and 31% yields, respectively. The structures of 2 and 3 were established by X-ray crystal structure determination (Figure 1). Diffraction-quality crystals of 2 were obtained by vapor diffusion of diethyl ether into a methanol solution of the complex.



cis-[(S,S-BPBP)ReO₂]PF₆ (1) *cis*-[(BPMEN)ReO₂]PF₆ (2) *cis*-[(B^{mdm}PMEN)ReO₂]PF₆ (3)

Scheme 4. Dioxo-rhenium complexes 1, 2, and 3.



Figure 1. Molecular structures of (**a**). *cis*-[(BPMEN)ReO₂]⁺ (**2**) and (**b**). *cis*-[($B^{mdm}PMEN$)ReO₂]⁺ (**3**) in the crystal, drawn at the 50% probability level. Hydrogen atoms and the PF₆ counterions are omitted for clarity. For compound **3**, the corrystallized methanol solvent molecule is omitted as well.

These two new *cis*-dioxo-rhenium(V) complexes adopt a pseudo-octahedral geometry with a *cis*- α configuration of the ligand, similar to the geometry of **1**. Also the bond distances and angles are very similar to that of *cis*-[(*S*,*S*-BPBP)ReO₂]⁺ reported by Che [26]. Selected bond distances and angles are given in Table 1. For all of these three structures, the N(pyridine)–Re distances are shorter than the N(amine)–Re distances and the planes of the pyridine rings are tilted under a small angle with respect to the N(pyridine)–Re bonds (Table 2). Complexes **1**, **2**, and **3** are chiral at the amine nitrogens. Complexes **1** and **2** are enantiopure in the crystal, while complex **3** is racemic in the crystal. The tetradentate N₂Py₂ ligands of these complexes are well-known ligands for non-heme iron and manganese oxidation catalysts. Interestingly, for both N₂Py₂ supported high-valent rhenium complexes and N₂Py₂ supported low-valent iron/manganese complexes, the same pseudo-octahedral geometry is observed. Further characterization of complexes **2** and **3** included ¹H NMR, ¹³C NMR, ESI-MS, and elemental analysis (see Supplementary Material).

	1	2	3
Re-O1	1.765(4)	1.750(3)	1.745(3)
Re-O2	1.749(4)	1.747(4)	1.749(3)
Re-N1	2.122(5)	2.126(4)	2.122(4)
Re-N4	2.132(5)	2.124(4)	2.116(4)
Re-N2	2.258(5)	2.286(4)	2.266(4)
Re-N3	2.252(4)	2.284(4)	2.279(4)
O1-Re-O2	122.5(2)	123.1(2)	122.60(16)
N1-Re-N4	176.3(2)	174.53(16)	174.85(13)
N2-Re-N3	75.47(19)	75.89(15)	76.69(13)

Table 1. Selected bond distances (Å) and angles (°) of *cis*-dioxo-rhenium complexes, *cis*-[(S,S-BPBP)ReO₂]PF₆ (1) [27], *cis*-[(BPMEN)ReO₂]PF₆ (2), and *cis*-[(BP^{mdm}MEN)ReO₂]PF₆ (3).

Table 2. Angle between pyridine ring and N-Re bond [°].

	1	2	3
N1-Re	2.0(3)	6.8(2)	2.67(19)
N4-Re	1.8(3)	6.7(2)	0.93(18)

2.2. Initial Catalytic Activity Investigation of Complexes 1–3

Next, we investigated the use of **1**, **2**, and **3** as catalysts in the DODH of vicinal diols by using 1,2-octanediol as a benchmark substrate and triphenylphosphine (PPh₃) as reductant. Only trace amounts of 1-octene formed when the reaction was performed at 135 °C using 2 mol% **1** as catalyst and 1.1 equiv. of PPh₃ as reductant. The reaction temperature was then gradually increased from 135 °C to 180 °C. The yield of 1-octene jumped from 11% to quantitative when the temperature was increased from 165 °C to 180 °C (Table 3, entries 1–4). Similarly, when **2** was used as catalyst, an elevated reaction temperature was increased from 150 °C to 180 °C to 180 °C (Table 3, entries 1–4). Similarly, when **2** was used as catalyst, an elevated reaction temperature was increased from 150 °C to 180 °C (Table 3, entries 5, 6). For all three complexes, full conversion and quantitative 1-octene yield were achieved when the reaction was performed at 180 °C for 15 h under N₂ (Table 3, entries 4, 5, and 7).

Entry	Catalyst	Time	Temperature	Yield [b]	Conversion
1	1	15 h	135 °C	2%	2%
2	1	15 h	150 °C	6%	7%
3	1	15 h	165 °C	11%	12%
4	1	15 h	180 °C	>99%	>99%
5	2	15 h	150 °C	16%	16%
6	2	15 h	180 °C	>99%	>99%
7	3	15 h	180 °C	>99%	>99%
8	1	3 h	180 °C	27%	27%
9	2	3 h	180 °C	34%	34%
10	3	3 h	180 °C	41%	41%
11	IReO ₂ (PPh ₃) ₂	3 h	180 °C	14%	16%
12	trans-[(Py4)ReO2]PF6	3 h	180 °C	>99%	>99%
13 [c]	1	7 h	180 °C	75%	75%
14 [c]	2	7 h	180 °C	90%	90%
15 [c]	3	7 h	180 °C	84%	84%

Table 3. Deoxydehydration of 1,2-octanediol catalyzed by dioxo-rhenium complexes. [a].

[a] Reaction conditions: 1,2-octanediol (0.5 mmol), PPh₃ (0.55 mmol, 1.1 equiv.), catalyst (0.01 mmol, 2 mol%), PhCl (5 mL), N₂. [b] 1-Octene yield was determined by ¹H NMR using mesitylene (0.5 mmol) as an internal standard. [c] For the initial 3 h, the reaction was performed under N₂; for the next 4 h, the reaction was performed under air.

In order to compare the reactivity of 1, 2, and 3, a shorter reaction time was chosen. After 3 h of reaction at $180 \degree$ C, significantly lower olefin yields (27–41%) were found than for a reaction time of 15 h
at this reaction temperature, albeit at 100% 1-octene selectivity. These findings show that the nature of N_2Py_2 ligand has an effect on the proficiency of the dioxo-rhenium complexes in catalysis and that these complexes do not show any isomerization of the olefin product under the current conditions. Remarkably, in DODH reactions catalyzed by Cp-based trioxo-rhenium complexes, olefin isomers are formed when the reactions are performed at higher temperatures (180 °C) [27].

The precursor of these dioxo complexes, i.e., iododioxobis(triphenylphosphine)rhenium (IReO₂(PPh₃)₂), was also investigated for its DODH activity and gave a 1-octene yield of only 14% with 2% of octene isomers being formed. $trans-[(Py_4)ReO_2]PF_6$ was also tested for this DODH reaction, aiming at providing information on the effect of the configuration of the oxo ligands (cis or trans) on catalysis. Surprisingly, this complex showed the best activity among all dioxo-rhenium complexes tested in our study (Table 3, compare entries 8-11). After the reaction mixture was heated at 180 °C for 3 h, a full substrate conversion and quantitative 1-octene product yield was achieved with trans-[(Py_4)ReO₂]PF₆ (entry 11), while the reactions using the three N₂Py₂-ligated *cis*-dioxo-rhenium complexes reached much lower conversions (entries 8-10). As mentioned in the introduction section, Nicholas et al. have carried out a stochiometric reaction between 1,2-decanediol (1.6 equiv.) and trans-[(Py4)ReO2]Cl (1.0 equiv.) to form 1.0 equiv. of 1-decene and no diol oxidation products. From this observation, they concluded that the starting Re(V) complex is converted to a $[(Py)_n Re(VII)O_3]^+$ species, which would also involve pyridine ligand(s) dissociation, and that DODH catalysis using this Re(V) dioxo complex would proceed through a $Re(V) \leftrightarrow Re(VII)$ cycle [25]. On the basis of these considerations, we assume that $[(N_2Py_2)ReO_2]^+$ -catalyzed DODH reactions can also proceed through a Re(V)↔Re(VII) cycle. In this case though, the formal oxidation to a Re(VII)-trioxo species (resulting from a single DODH reaction) would be more difficult compared to trans-[(Py₄)ReO₂]PF₆, since the tetradentate N₂Py₂ ligand is more strongly coordinated to the Re center than the monodentate pyridine donors in trans-[(Py₄)ReO₂]PF₆. This could then explain why trans-[(Py₄)ReO₂]PF₆ has a higher catalytic activity compared to complexes 1-3.

As a last aspect of these initial studies, we investigated the sensitivity of DODH catalysis by complexes 1–3. Accordingly, the reaction mixtures of entries 7–9 were then heated for another 4 h under air in the closed reaction vessel. Interestingly, the presence of O_2 does not seem to hamper the reactivity and might even slightly promote the reactions (Table 3, entries 13–15).

2.3. Initial Mechanistic Studies

After the initial study of the catalytic DODH activity of complexes 1–3, the time-course profiles of the DODH of 1,2-octanediol by these N₂Py₂-ligated dioxo-rhenium complexes were investigated. In situ ¹H NMR experiments were carried out using 1,2-octanediol (0.05 mmol), PPh₃ (0.055 mmol, 1.1 equiv.), Re-catalyst (0.005 mmol, 10 mol%), and mesitylene (0.05 mmol, 1.0 equiv., internal standard) in toluene-D₈ (0.5 mL) at 180 °C under an inert N₂ atmosphere.

Except *cis*-[(BPMEN)ReO₂]PF₆ (**2**), *cis*-[(BP^{mdm}MEN)ReO₂]PF₆ (**3**), and *trans*-[(Py₄)ReO₂]PF₆, the dioxo-rhenium complex *cis*-[(BPMEN)ReO₂]BPh₄ (**6**) was also included in these studies in order to investigate a possible effect of the counter anion on catalyst activity. For complexes **2**, **3**, and **6**, an induction period was observed. For the reaction catalyzed by **2**, a typical sigmoidal trend for 1-octene formation was found. No 1-octene formation was observed during the initial 5 min., followed by a gradual increase in 1-octene formation until 120 min. After this induction period, formation of 1-octene proceeded at a much higher rate, with the highest yield (86%) reached after 300 min (Scheme 5a). Modification of the N₂Py₂ ligand framework lead to changes in this reaction profile. When *cis*-[(BP^{mdm}MEN)ReO₂]PF₆ (**3**) was used as catalyst, the sigmoidal reaction curve showed a much shorter induction period. In this case the highest product yield (90%) was reached after 210 min (Scheme 5b). Furthermore, changing the counter anion also resulted in a different reaction profile, i.e., the induction period was significantly shorter for the BPh₄⁻ salt **6** than for PF₆⁻ salt **2** (Scheme 5a,c). However, the three complexes **2**, **3**, and **6** give a very similar final 1-octene yield and reached this yield within approximately the same time.





Scheme 5. Time-course profiles of the formation of 1-octene in Re-catalyzed DODH of 1,2-octanediol with PPh₃ as reductant using different Re-catalysts: (a) *cis*-[(BPMEN)ReO₂]PF₆ (2); (b) *cis*-[(BPMEM)ReO₂]PF₆ (3); (c) *cis*-[(BPMEN)ReO₂]BPh₄ (6), (d) *trans*-[(Py₄)ReO₂]PF₆ (4); (e) pyridinium perrhenate. *Reaction conditions*: 1,2-octanediol (0.05 mmol), PPh₃ (0.055 mmol, 1.1 equiv.), Re-catalyst (0.005 mmol, 10 mol%), mesitylene (0.05 mmol, 1.0 equiv., internal standard), toluene-D₈ (0.5 mL), 180 °C, N₂.

In the reaction profile for the DODH reaction catalyzed by *trans*- $[(Py_4)ReO_2]PF_6$ no induction period was observed and 24% of 1-octene had formed after 5 min, while full conversion was achieved after 15 min. The reaction rate in this case was much higher than that for the other three complexes. In all of these four reactions, no formation of olefin products resulting from 1-octene isomerization was observed.

After the investigation of the time-course profiles of these "ReO₂"-catalyzed deoxydehydrations, the reaction mixtures were analyzed by means of ESI-MS measurements. For the DODH reaction of 1,2-octanediol catalyzed by **1**, both protonated ligand (ES+ m/z 323.2225; calc. 323.2230) and ReO₄⁻ (ES- m/z 250.8320; calc. 250.9360) signals were detected by ESI-MS measurements on the crude reaction mixture after the reaction (Figure 2). The signal for the protonated ligand signal was also detected when subjecting pristine complex **1** to ESI-MS analysis, in addition to the signal of the

[(*S*,*S*-BPBP)ReO₂] cation (*m*/z 541.1534; calcd. 541.1608). The signal for the intact [(*S*,*S*-BPBP)ReO₂] cation was, however not observed in the analysis of the crude DODH reaction mixture. The absence of **1**, as well as the appearance of protonated ligand and ReO₄⁻, indicates that the starting dioxo-rhenium complex decomposes under the conditions of the DODH reaction and that perrhenate is formed during the reaction. In case of the DODH of 1,2-octanediol catalyzed by **1**, besides the signal for the protonated ligand, signals at *m*/z 480.2455, 576.2290, 669.2780, 857.2693, were detected in positive ion mode. While the signals at *m*/z 480.2455, 576.2290, 857.2693 did not match the isotope distribution of either mono- or multi-rhenium species, the signal at *m*/z 669.2780 can be assigned to the [(*S*,*S*-BPBP)ReO(1,2-octanediolate)]⁺ ion (calcd. 669.2809), which represents the product formed upon the condensation of [(*S*,*S*-BPBP)ReO₂]⁺ and 1,2-octanediol. This diolate could either form 1-octene by olefin extrusion and generate [(*S*,*S*-BPBP)ReO₃]⁺, or be reduced by PPh₃ to form [(*S*,*S*-BPBP)Re(1,2-octanediolate)]⁺, followed by olefin extrusion to regenerate [(*S*,*S*-BPBP)ReO₂]⁺. In the former case, a 20e⁻ species [(*S*,*S*-BPBP)ReO₃]⁺ would be formed, which could set the stage for N₂Py₂ ligand dissociation and formal decomposition of the starting dioxo-complex.

These combined MS and reaction profile observations indicate that complexes 2, 3, and 6 act as pre-catalysts in DODH reactions. Our initial assumption was that the N₂Py₂-supported complexes show slower kinetics due the more difficult formation of a putative Re(VII) trioxo species as a result of stronger ligand chelation (*vide supra*). The MS data now show the presence of protonated ligand and the perthenate anion ReO₄⁻ in the crude DODH reaction mixtures of these complexes, suggesting that full ligand dissociation and rhenium oxidation may take place as part of precatalyst activation.

Based on these observations, we decided to investigate the DODH activity of the pyridinium perrhenate salt [PyH][ReO₄]. Pyridinium perrhenate was earlier reported as catalyst for the DODH of diols by Love and coworkers [28]. In their work, aromatic vicinal diols were converted to the corresponding olefins with moderate to excellent yields (22% to quantitative) at a relatively low temperature (90 °C) in chloroform using 5 mol% lutidinium perrhenate as catalyst and 1.09 equiv. PPh₃ as reductant. For aliphatic vicinal diol substrates, a higher reaction temperature of 140 °C was needed for the DODH reaction to proceed, and only moderate olefin yields (21–51%) were obtained after 16 h. When carrying out the DODH reaction of 1,2-octanediol with [PyH][ReO₄] as catalyst under our reaction conditions, we found quantitative 1-octene formation within approx. 20 min without the formation of octane isomers. The time-course profile of this reaction showed a very short induction period and indicated that the reaction rate was not as high as for *trans*-[(Py₄)ReO₂]PF₆ (Scheme 5d,e). This comparison between time-course profiles seems to suggest that perrhenate is the active species that is formed when *trans*-[(Py₄)ReO₂]PF₆ is used in DODH catalysis. On the other hand, the difference in reaction rates does not rule out the possible involvement of yet another active species.



Figure 2. ESI-MS analysis: (a) MS ES+ trace of the crude reaction mixture of the DODH reaction of 1,2-octanediol by **1**; (b) MS ES- trace of the crude reaction mixture of the DODH reaction of 1,2-octanediol by **1**; (c) MS ES+ trace of **1**.

2.4. Investigation of the Active Species

In order to further probe the nature of the active species in DODH reactions catalyzed by dioxo-rhenium complexes, we decided to explore the DODH reaction of erythritol using these complexes. Erythritol is an interesting substrate in DODH chemistry, since it can lead to the formation of 1,3-butadiene as the reaction product starting from a bio-based source. In addition, this tetraol substrate can engage in a number of side-reactions, including dehydrative cyclisation and internal deoxydehydration, and its product distribution profile has been used to investigate the involvement of different active species during DODH catalysis. For the Cp^{*}ReO₃-catalyzed DODH of erythritol using PPh₃ as reductant and PhCl as solvent, instead of 2,5-dihydrofuran, *cis*-2-butene-1,4-diol and 3-butene-1,2-diol were detected as byproduct. Also, for the Cp^{ttt}ReO₃-catalyzed DODH of erythritol using PPh₃ as reductant and PhCl as solvent, both *cis*-2-butene-1,4-diol and *trans*-2-butene-1,4-diol were detected as byproduct.

2,5-dihydrofuran is highly dependent on the solvent and reductant; when 3-octanol was used as solvent and reductant, 2,5-dihydrofuran was the only byproduct detected with either Cp^{ttt}ReO₃, Cp^{tt}ReO₃, or MTO as catalyst. [21,22,30]

cis-[(BPMEN)ReO₂]PF₆ (**2**), *trans*-[(Py₄)ReO₂]PF₆ (**4**), and pyridinium perrhenate were then tested for the DODH of erythritol using PPh₃ as reductant and PhCl as solvent. The reactions were performed at 180 °C for 1.5 h under N₂. The total yield of 1,3-butadiene plus 2,5-dihydrofuran was 57%, 80%, and 83%, respectively. In addition, different product distributions were observed; the ratio of 1,3-butadiene and 2,5-dihydrofuran products was 5.3:1, 9.0:1, and 15.6:1, respectively (Scheme 6). Upon prolonging the reaction from 1.5 h to 3 h, the total yield of 1,3-butadiene plus 2,5-dihydrofuran increased to 68% and 84% for **2** and *trans*-[(Py₄)ReO₂]PF₆, while a lower 72% was observed for the perrhenate catalyzed reaction. The latter decrease could be the result of secondary reactions of the rather reactive butadiene and 2,5-dihydrofuran products slightly changed to 5.2:1, 9.5:1, and 11:1 for the prolonged reactions.



Scheme 6. DODH of erythritol using cis-[(BPMEN)ReO₂]PF₆ (2), trans-[(Py₄)ReO₂]PF₆ (4), and pyridinium perrhenate as catalyst.

Overall, the product distribution was quite consistent for these three catalysts. The differences observed in product formation and distribution in these experiments do not provide solid proof that perhenate is the (only) active species in "ReO₂" catalyzed DODH reactions. In addition, the absence of *cis*-2-butene-1,4-diol, *trans*-2-butene-1,4-diol, and 3-butene-1,2-diol byproducts indicated that these three reactions do not proceed through the same active species and/or do not form the same Re-based side products as Cp^{*}ReO₃ and Cp^{ttt}ReO₃ in the PPh₃/PhCl system. On the other hand, as mentioned above, in all cases of using a secondary alcohol as both solvent and reductant, 2,5-dihydrofuran was the only detected byproduct, just like for our experiments using the PPh₃/PhCl conditions; indicating that for the dioxo-rhenium and perrhenate systems the same or similar active species could actually be involved as for the Re-trioxo systems.

Since neither the time-course profile nor the product distribution studies could provide full evidence that perrhenate is the active species in dioxo-rhenium-catalyzed DODH reaction, we have sought for other means of probing the nature of the active species in these reactions. On basis of the time-course profile the DODH reaction catalyzed by **2** (Scheme 5a), the activation/formation of the active species could proceed in a two-step manner. After a small amount of olefin product had formed, a second phase in product formation was observed before the rate of product formation really took on. Accordingly, we considered the possibility that the active species might be generated through the

involvement of the initial rhenium complexes and one of the products formed in the DODH reaction, i.e., next to olefin also water and triphenylphosphine oxide (OPPh₃).

We first turned our attention to the possible role of water on the speciation of rhenium in the DODH reactions. It is known that in the present of water methyltrioxorhenium (MTO) will form a gold-colored rhenium oligomer $\{H_{0.5}[(CH_3)_{0.92}ReO_3]\}$ in high yield (ca. 70%) at 70 °C, in addition to the formation of O_2 , HReO₄, and methane (ca. 30% in total) [31,32]. Thus, we were curious about the species formed from the dioxo-rhenium complexes and water. Accordingly, cis-[(BPMEN)ReO₂]BPh₄ (6) was heated in CD₃CN at 180 °C for 2 h in the presence of 50 equiv. of water. ¹H NMR analysis of the reaction after this period did not indicate the presence of non-coordinated BPMEN ligand. Next, this "water-treated" complex, i.e., the resulting reaction mixture, was used as catalyst in the DODH of 1,2-octanediol under our standard reaction conditions. In this case, 86% of 1-octene formed after 2 h at 180 °C and again without the formation of olefin isomers. The time-course profile of this reaction shows that only 3% of 1-octene had formed after 10 min, but that the overall induction period was significantly shorter than using pristine cis-[(BPMEN)ReO₂]BPh₄ as catalyst (Figure 3). After the induction period, the two reaction profiles are rather similar, which indicates that the same active species might be involved and the formation of this species might involve a reaction with water at high temperature. Comparing the time-course profile of DODH reactions using complex 6 and "water-treated" 6 as catalyst, the latter one is much faster. In both cases though, no olefin isomers were formed during the reaction and the final yield of 1-octene was the same (95%).



Figure 3. Time-course profile of the DODH reaction of 1,2-octanediol using *cis*-[(BPMEN)ReO₂]BPh₄ and "water-treated" *cis*-[(BPMEN)ReO₂]BPh₄ as catalyst. Reaction conditions: 1,2-octanediol (0.05 mmol), PPh₃ (0.055 mmol, 1.1 equiv.), Re-catalyst (0.005 mmol, 10 mol%), mesitylene (0.05 mmol, 1.0 equiv., internal standard), toluene-D₈ (0.5 mL), 180 °C, N₂.

Next, we compared the IR spectra of **6** before and after treatment with water to that of pyridinium perrhenate (Figure 4). The IR spectrum of pristine *cis*-[(BPMEN)ReO₂]BPh₄ shows a sharp and intense signal at 813 cm⁻¹ assigned to Re = O stretching, while the IR of pyridinium perrhenate shows relatively broad and intense signals at 863, 741, and 672 cm⁻¹ assigned to Re = O stretching of the perrhenate anion. In the IR spectrum of "water-treated" *cis*-[(BPMEN)ReO₂]BPh₄ the most intense signal in the 500–1000 cm⁻¹ range was found at 907 cm⁻¹, which again was assigned to Re = O stretching, albeit at significantly higher wave numbers compared to pristine **6**. Two less intense bands were also observed in this range, at 761 and 706 cm⁻¹. Comparing these three spectra, it is obvious that no *cis*-[(BPMEN)ReO₂]BPh₄ is left after water treatment. The similarities in the 500–1000 cm⁻¹ range for pyridinium perrhenate and "water-treated" *cis*-[(BPMEN)ReO₂]BPh₄ suggest that ReO₄⁻ is formed

upon water treatment of **6**. In the range of 1000–2000 cm⁻¹, very different signals were observed, likely due to the presence of different organic ligands.



Figure 4. IR spectra of *cis*-[(BPMEN)ReO₂]BPh₄, pyridinium perrhenate, and "water-treated" *cis*-[(BPMEN)ReO₂]BPh₄.

Recently, Marrone and d'Alessandro et al. have reported a study on the active species in rhenium-catalyzed DODH reactions using secondary alcohols as reductant [33]. An induction period was observed for the DODH of glycerol using methyltrioxorhenium (MTO), trioxo-rhenium (ReO₃), rhenium pentachloride (ReCl₅), hepta-oxo-dirhenium (Re₂O₇), rhenium triiodide (ReI₃), and IReO₂(PPh₃)₂ as catalyst and 2,4-dimethyl-3-pentanol (DMP) as reductant. After removal of the volatile reaction products and the DMP reductant, the residues of these reactions were used as the catalyst in subsequent DODH experiments and no induction periods were observed. IR spectra of these active residues were collected and compared. A few intense and broad signals were detected in the 1800–3750 cm⁻¹ range, and these signals could be assigned to C-H and O-H stretching vibrations. In our IR spectra of "water-treated" cis-[(BPMEN)ReO₂]BPh₄, these kind of intense and broad signals $(3346, 3053, 2852 \text{ cm}^{-1})$ were also observed in this range. In the range of $1000-1750 \text{ cm}^{-1}$, multiple intense signals were detected by Marrone and d'Alessandro while in our case, much less intense signals were observed. Since this range is where C–O stretching and C–C–H, C–O–H bending vibrations are located, these differences indicate that related species may have formed but these are not identical. In both studies, the most intense signals appeared in the 600-1000 cm⁻¹ range. In the study of Marrone and d'Alessandro, the most intense signal appears at 920 cm⁻¹ for the Re = O stretching vibration in all cases studied, independent from the rhenium sources. In our case this vibration is found at 907 cm⁻¹. A less intense band around 700 cm⁻¹ was also observed in all cases by Marrone and d'Alessandro, and assigned to either the out-of-plane bending of O-H bonds or the stretching of the Re–O–Re oxo-bridges. Overall, rather similar spectra were obtained in these two studies. By further investigating the MTO-catalyzed DODH of glycerol, Marrone and d'Alessandro proposed a Re(VII) alkoxide oligomer as the actual active species could form alongside methane from the reaction of MTO and the secondary alcohol reductant. A very important observation from their study is the formation of a catalytically active black solid in all cases. In our present study though, we did not observe the formation of black precipitates.

As described in Marrone and d'Alessandro's work, an active DODH species is formed from the reaction of the Re source and a secondary alcohol. Although in our system, we do not use a secondary alcohol reductant, an active species seems to form from a reaction with water, and obviously a vicinal diol is present as the substrate. A possibility would be that in our case a rhenium-oxide/hydroxide

oligomer is formed instead of a Re(VII) alkoxide oligomer as proposed by Marrone and d'Alessandro. The differences seen in the 1000–1750 cm⁻¹ range in IR analysis would support this assumption. As mentioned before, IR analysis of the { $H_{0.5}[(CH_3)_{0.92}ReO_3]$ } oligomer, the reaction product of MTO and water, shows signals at 912 (vs), 881 (sh), 851 (sh), and 758 cm⁻¹ (m). [32] These signals could be assigned to Re = O stretching vibrations. Although not identical, we observed quite similar IR vibrations in the 600–1000 cm⁻¹ region (Table 4). For the { $H_{0.5}[(CH_3)_{0.92}ReO_3]$ } oligomer, a methyl group is bound to the rhenium center, although not in a 1:1 ratio. In our case, no coordinated ligand was observed after the water treatment at 180 °C. This comparison lends further credit to the proposed formation of a rhenium-oxide/hydroxide oligomer as the active species in DODH catalysis.

"Water-Treated" cis-[(BPMEN)ReO ₂]BPh ₄	$\{H_{0.5}[(CH_3)_{0.92}ReO_3]\}$	Re(VII) Alkoxide Oligomer
907 (vs)	912 (vs)	920 (vs)
	881 (sh)	
	851 (sh)	
761 (m)	758 (m)	
706 (w)		around 700 (m)

Table 4. Comparison of IR signals in $600-1000 \text{ cm}^{-1}$ region of "water-treated" *cis*-[(BPMEN)ReO₂]BPh₄, {H_{0.5}[(CH₃)_{0.92}ReO₃]} [32], and the Re(VII) alkoxide oligomer [33].

2.5. Substrate Scope

Previously, trans-[(Py4)ReO2]PF6 (10 mol%) was used by Nicholas et al. as catalyst in the DODH of 1,2-decanediol using Zn as reductant and benzene as solvent to give 67% of 1-decene with full-substrate conversion at 150 °C in 24 h. In our system, 1,2-octanediol was quantitively converted to 1-octene at 180 °C in 3 h using only 2 mol% of trans-[(Py4)ReO2]PF6. Remarkably, upon increase of the catalyst loading under our conditions to 10 mol%, the reaction was done in 15 min at 180 °C. For the Cp-based trioxorhenium-catalyzed DODH systems, much longer reaction times are needed to realize the full conversion of 1,2-octanediol. As mentioned before, no isomers were observed under our reaction conditions, while small amount of isomers were observed under the same conditions for Cp-based trioxorhenium catalysts [27]. Furthermore, for the deoxydehydration of erythritol (vide supra), trans-[(Py₄)ReO₂]PF₆ was quite a competitive catalyst (Scheme 6). This initial catalytic capacity test of trans-[(Py4)ReO₂]PF₆ encouraged us to apply this precatalyst to other substrates (Table 5). When the aromatic vicinal diol 1-phenylethane-1,2-diol was used as substrate, a quantitative styrene yield was obtained (Table 5, entry 1). For the DODH of 1,4-anhydroerythritol, 97% of 2,5-dihydrofuran was formed (Table 5, entry 2); this 2,5-dihydrofuran yield is competitive to the one obtained from the MTO/3-pentanol system, which provides 95% of 2,5-dihydrofuran [30]. Glycerol, a biomass-derived triol, was also investigated in our reaction system and gave a quantitative amount of allyl alcohol (entry 3). Although quantitative allyl alcohol formation is also obtained by the Cp^{tt}ReO₃/3-octanol system [23], the air-stable property of trans- $[(Py_4)ReO_2]PF_6$ makes this catalyst system more attractive. trans-[(Py₄)ReO₂]PF₆ also catalyzes the DODH of biomass-derived L-(+)-tartaric acid and mucic acid. When using L-(+)-tartaric acid as substrate, there was no product detected using PPh3 as reductant and PhCl as solvent. This is most likely due to the poor substrate solubility in PhCl. Using 3-pentanol as both solvent and reductant gave 84% of the corresponding olefins as a mixture of fumaric acid and fumarate esters. Along a similar vein, a total yield of muconic acid and muconates of 65% was obtained using mucic acid as substrate (Table 5, entry 5). In the case of Cp^{tt}ReO₃-catalyzed DODH of mucic acid, a slightly higher product yield of 71% was found, albeit at 5 mol% catalyst loading. Overall, *trans*-[(Py₄)ReO₂]PF₆ is a good pre-catalyst for the DODH of diols and biomass-derived polyols.



Table 5. trans-[(Py₄)ReO₂]PF₆ catalyzed deoxydehydration [a].

[a] Olefin yield was determined by 1H NMR using mesitylene (1.0 equiv., 0.5 mmol) as an internal standard.

3. Materials and Methods

All chemicals including solvents were degassed by either freeze-pump-thaw cycles or degasification under vacuum. Triphenylphosphine was crystallized from ethanol and dried under vacuum. Iododioxobis(triphenylphosphine)rhenium (IReO₂(PPh₃)₂) was purchased from Sigma-Aldrich and used without further purification. *cis*-[(*S*,*S*-BPBP)ReO₂]PF₆ [26], BPMEN [34], BP^{mdm}MEN [34], and *trans*-[(Py₄)ReO₂]PF₆ [25] were prepared according to known literature procedures. Unless otherwise stated, all other commercial chemicals were used without further purification. NMR spectra were recorded on a Varian VNMRS400 (400 MHz) instrument at 298 K. ESI-MS spectra were recorded using a Waters LCT Premier XE instrument. IR spectra were recorded with a Perkin–Elmer Spectrum One FTIR spectrometer. All olefinic products are known compounds and were calibrated against mesitylene for quantification.

4. Conclusions

Two new tetradentate N-donor ligand-supported ReO₂⁺ complexes, *cis*-[(BPMEN)ReO₂]PF₆ (2) and cis-[(B^{mdm}PMEN)ReO₂]PF₆ (3), were synthesized and fully characterized in this chapter. These complexes, along with the complex cis-[(S,S-BPBP)ReO₂]PF₆ (1) earlier reported by Che, were found to be active in DODH reactions of diols, suggesting that Re(V) dioxo complexes are able to be involved in DODH catalysis. However, an induction period was observed for the DODH reaction of 1,2-octanediol using these N₂Py₂ supported dioxo-rhenium complexes. Under the same reaction conditions, no induction period was observed for trans-[(Py4)ReO2]PF6 and a much shorter induction period was observed for pyridinium perrhenate. ESI-MS analysis of the reaction mixtures of DODH reactions catalyzed by *cis*-[(BPMEN)ReO₂]PF₆ showed the formation of protonated ligand and the ReO₄⁻ anion during catalysis. These combined observations suggested that the Re(V) dioxo complexes might act as precatalysts in DODH catalysis. Treatment of cis-[(BPMEN)ReO2]BPh4 with an excess amount of water generated a species that is also active in DODH catalysis and that displayed a much shorter induction period than the pristine complex. A similar reaction rate and final 1-octene yield indicated that pristine and "water-treated" cis-[(BPMEN)ReO₂]BPh₄ generate the same active DODH species. By comparing the IR spectra of various complexes before and after catalysis and a number of Re-compounds from the literature, we believe that ligand dissociation takes place after the first DODH reaction in which a Re-trioxo species is formed, to subsequently form a rhenium-oxide/hydroxide oligomer that is capable of catalytic turn-over. The remarkably high catalytic activity of trans-[(Py4)ReO2]PF6 can be

explained by the more facile dissociation of pyridine from the Re center compared to the tetradentate N_2Py_2 ligands.

Last but not the least, several vicinal diols and biomass-derived polyols were applied to the simple *trans*-[(Py_4)ReO_2]PF_6 catalyst in combination either PPh₃ or 3-pentanol as reductant. Excellent to quantitative olefin yields were obtained for vicinal diol substrates. In the case of bio-based polyols, good olefin yield was obtained when 3-pentanol was used as solvent and reductant.

Supplementary Materials: The following are available online at http://www.mdpi.com/2073-4344/10/7/754/s1, the synthesis and characterization of *cis*-[(BPMEN)ReO₂]PF₆ (**2**), *cis*-[($B^{mdm}PMEN$)ReO₂]PF₆ (**3**), and *cis*-[(BPMEN)ReO₂]BPh₄ (**6**); the general procedure of catalysis and the ¹H NMR data for olefin products.

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Article Catalytic Cracking of Heavy Crude Oil over Iron-Based Catalyst Obtained from Galvanic Industry Wastes

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Abstract: Sewage sludge from the galvanic industry represents a problem to the environment, due to its high metal content that makes it a hazardous waste and must be treated or disposed of properly. This study aimed to evaluate the sludge from three galvanic industries and determine its possible use as catalysts for the synthesis of materials. Catalyst was obtained from a thermal process based on dried between 100–120 °C and calcination of sludges between 400 to 700 °C. The physical–chemical properties of the catalyst were analyzed by several techniques as physisorption of N₂ and chemisorption of CO of the material. Catalytic activity was analyzed by thermogravimetric analysis of a thermo-catalytic decomposition of crude oil. The best conditions for catalyst synthesis were calcination between 400 and 500 °C, the temperature of reduction between 750 and 850 °C for 15 min. The catalytic material had mainly Fe as active phase and the specific surface between 17.68–96.15 m²·g⁻¹, the catalysts promote around 6% more weight-loss of crude oil in the thermal decomposition compared with assays without the catalyst. The results show that the residual sludge of galvanic industries after thermal treatment can be used as catalytic materials due to the easiness of synthesis procedures required, the low E-factor obtained and the recycling of industrial waste promoted.

Keywords: sludge; catalytic material; galvanic industry; waste valorization

1. Introduction

The generation of waste worldwide for 2016 was estimated at 2.01 billion tons, while the world generation is expected to reach 3.30 billion $t \cdot day^{-1}$ by 2100 [1]. The global trend shows that industrial waste generation is almost 18 times higher than municipal waste. Industrial waste increases significantly as income level increases [1]. Among these is the waste from the galvanic industry, which produces on average in the United States about 150,000 $t \cdot year^{-1}$ [2], similar values are reported by the European Union [3]. Sludge represents approximately 25 m³ for every million tons of textile wastewater and two-thirds of these sludges have physicochemical properties that can be modified [4,5].

The recovery of galvanic baths is beneficial in the mechanical industry to avoid corrosion problems in materials [6]. Nevertheless, it generates hazardous industrial waste as the residual sludge of the process baths, mainly from rinsing in the stages of stripping and degrease [7].

Since galvanic sludge wastes are hazardous due to their chemical composition, they need final treatment or disposal in a safe landfill. Worldwide the implemented skills are mainly: disposal in

soils, thermal treatments as pyrolysis/incineration [8–11], encapsulation [12], as a component of other solid materials [3,7,13–15]. Similarly, some techniques as inertization of heavy metals present in this type of sludge have been studied [2]. However, these treatments represent additional costs for galvanic companies.

The sludge of the galvanic industry has been mainly treated by thermochemical processes such as pyrolysis and incineration. The byproducts of this process have been used as adsorbents [5,16]. Due to the diverse metallic content of this residual industrial sludge, there is the possibility of recovering these residues for the synthesis of catalysts [15,17–20]. Sludge obtained from waste from textile industries, aluminum, galvanic and tannery can be converted on a catalyst for the oxidation of the propane, getting conversions of more than 95% [21,22].

Catalysts prepared from the sludge of the process of ferrite were tried for CO conversion, the results indicate that the Cu-ferrite catalyst can convert CO to CO₂ at an inlet CO concentration of 4000 ppm and a space velocity of 6000 h⁻¹ were held at 140 °C [23]. The selective catalytic NO reduction was studied using metal catalyst doped with carbon from the residual sludge of ferrite, at 300 °C conversion >99.7% of NO was reported [24]. The sludge waste from wastewater treatment in the textile industries has metals like Fe and Cr were used as catalytic materials during their reducing phase for the decomposition of hydrocarbons [25]. Fe–char catalyst from tank cleaning oily sludge for the catalytic cracking of oily sludge at 800 °C, the oil conversion efficiency reached is around 95.8% [26]. Carbon–silica derived from SiC–Si sludge has been proven as support for Fe catalysts; better results are shown when Fe was loaded by chemical vapor infiltration than incipient wetness impregnation [27]. Metallic iron from the dyeing sludge ash was probed as a catalyst for biomass gasification. It showed similar behavior that of the commercially available iron–chrome-based catalyst for the same equivalent total amount of Fe₂O₃ [28].

This work has aimed to evaluate residual sludge from the galvanic industry as catalysts for which this work raises the synthesis of catalytic materials applied in the reactions of cracking of heavy crude oil.

2. Results and Discussion

2.1. Sludge and Catalyst Characterization

The thermal treatment (calcination) provided the catalytic characteristics at the residual sludge as the drying of the internal water, volatile substances. The metallic content in the sludge was oxidized in this process. Elemental analysis was done to evaluate the organic material eliminated by calcination.

The results of the elemental analysis and physical properties of the dried sludges and catalytic material obtained are shown in Table 1. With a prior drying process can be observed that the optimal drying temperature is 120 °C for L1 and L2 and 100 °C for L3, the differences in the drying temperature can be due at the presence of different compounds and additives on the sludges [29–31].

There was observed that thermal treatment promotes changes in the physical-chemical composition of raw sludge. A higher quantity of sulfur was detected on C3, probably due to the use of sulfuric acid and other sulfur compounds in the galvanic process, with the increase of temperature, these compounds could be converted in oxides [32]. On the C1 and C2 catalyst, the sulfur content was constant. From L2 and its derived catalytic material C2, the content of carbon is higher than the others. It could be due to carbonates and surfactants used on the stripping process [33]. Carbon and sulfur values are low compared with the reported by other authors in this type of sludge, finding carbon content between 25% to 40% and for sulfur between 4% and 22% [5,13,16].

Table 1 shows the effects of calcination temperature on the reduction of surface area and pore volume of catalytic materials. The decrease of surface area can be associated with the collapse of the pore structure [21,34]. The catalyst with the highest surface area was C1. For calcination temperature of 400 °C, the three catalysts showed more upper surface area than the other temperatures, but the high organic content can decrease the catalytic activity. Due to the low surface area, the samples calcined

at 700 °C have not been used on the catalytic activity test because the physisorption capability can be disfavored.

Sample	Τ, °C	% N	% C	% H	% S	Surface Area, $m^2 \cdot g^{-1}$	Pore Volume, cm ³ ·g ⁻¹	E-Factor
L1	120	0.10	2.36	2.05	0.94	nm	nm	nm
	400	0.02	0.65	0.35	0.39	96.15	0.12	
C1	500	0.05	0.44	0.19	0.38	71.37	0.10	0.1
	700	0.03	0.16	0.08	0.35	14.98	0.02	
L2	120	0.15	6.48	0.52	0.20	nm	nm	nm
	400	0.02	5.48	0.18	0.22	73.46	0.10	
C2	500	0.03	5.48	0.14	0.23	63.36	0.09	0.1
	700	0.01	4.77	0.08	0.20	27.56	0.03	
L3	100	1.11	5.86	1.35	2.94	nm	nm	nm
	400	0.04	1.74	0.08	3.71	29.72	0.03	
C3	500	0.03	0.40	0.08	4.23	17.68	0.02	0.3
	700	0.02	0.20	0.06	4.42	4.53	0.01	

Table 1. Elemental analysis and physical properties of dried residual sludges (L1–L3) and catalytic material synthesized (C1–C3).

nm: not measured.

To determinate the sustainability of this process, the Environmental Factor (E) was calculated [35–37]. E-factor correlates the actual amount of waste produced in the process with the desired product (E = mass of waste/mass of product). In this case, the desired product was the catalyst. The ideal E-factor is zero. The values E-factor are in Table 1; there were between 0.1 and 0.3. This process is sustainable because it can valorize industrial waste minimizing the waste produced in the process [35]. The galvanic companies gave the information that raw sludges had metallic content based on iron and zinc. The MSDS and technical data sheets of the streams on the galvanic processes verified it.

Figure 1 shows the FTIR analysis that allows the identification of functional groups for both sludge and catalytic materials. On L1 and C1 OH groups were observed, probably due to Zn(OH) (1407, 1478 and 1630 cm⁻¹) and other bands in 448 cm⁻¹ (Fe₂O₃) and 584 cm⁻¹ (Fe₃O₄) [38]. For L2 and C2 were identified bands on 2864 and 875 cm⁻¹ correlated with FeOO bond, on 464 cm⁻¹ for Fe₂O₃ and 799 cm⁻¹ for FeO. The presence of ZnO (606, 712 and 571 cm⁻¹) and C3 can be associated with FeSO₄ [40]. In the sludges, it was observed other peaks at 2923 and 3373 cm⁻¹, related to OH bonds due to the presence of the Fe–Zn hydroxyl groups on the surface [41], these bonds decrease its intensity while the calcination temperature increases.



Figure 1. Fourier transform infrared spectroscopy (FTIR) spectra of galvanic sludge and catalytic material.

2.2. Catalyst Reducibility Analysis

The reducibility capability of the synthesized catalysts was studied using the reduction at program temperature (TPR) with hydrogen as a reduction agent, H₂–TPR profiles are shown in Figure 2. C1 and C2 catalysts show three regions for reduction: the first region around 300–550 °C, the second and the prominent area around 550–800 °C, while the third region located between 800–900 °C. In the case of C3 shows only one prominent peak at 650 °C.



Figure 2. Temperature-programmed reduction (TPR) profile for C1, C2 and C3 calcined at 500 °C.

Similar behavior has been shown for other Fe based catalysts, for Fe/Al₂O₃ catalyst. Other authors have shown the same three areas that were evidenced in this work. The first one between 250–460 °C that can be described as a transformation towards Fe₂O₃, a second region that is between 480–800 °C that the authors associate with Fe₃O₄ formation. Moreover, the last area that is between 830–950 °C, which is related to the Fe formation [42,43].

Likewise, in this work, the second region again is dominant, but concluded that the area could be ascribable at Fe or Zn sulfides. The first region only is present when the Fe sulfides are doped with Zn and the third region increases at the same time, more content of zinc was loaded. Concerning catalyst C3, a particular behavior was found, since the presence of Zn significantly displaced the temperature towards a higher temperature for C1 and C2, this behavior is similar to other studies [44]. Therefore, the reduction peak of ZnO to a metallic state is around 700 °C, but interactions with sulfur compounds can change the reduction temperature at about 650 °C [45]. With this analysis is inferred that the C1–C2 mainly had iron phases while C3 has Fe–Zn.

Figure 3 shows a study of the time influence on the reducibility of the catalyst. The catalysts were analyzed at three different times, 15, 30 and 45 min. The reduction was made at 750 °C for C1, at 850 °C for C2 and 800 °C for C3 to compare the reducibility at different temperatures. In this test, the same behavior of the previous analysis is evidenced, in which the three catalysts present the same peaks (Figure 2). On the three catalysts was observed the complete reducibility. These results are important to be able to extrapolate at some point, the process at an industrial scale.



Figure 3. TPR profiles for C1, C2 and C3 at different reduction times on stream.

2.3. Metallic and Textural Properties of the Catalytic Material

The calcined catalyst and the raw sludge were not analyzed through X-ray diffraction (XRD). A similar metallic composition was found in the TPR analysis and while for catalysis application, the synthesized material was reduced. In the case of the reduced catalyst, an XRD analysis was performed. Peak identification was completed with the platform AtomWork: Inorganic Materials Database from NIMS Materials Database (National Institute for Materials Science, Tsukuba, Ibaraki, Japan) [46].

XRD patterns are shown in Figure 4, C1 and C2 had similar patterns, but in the C3, more quantity of peaks had appeared. In the three catalysts were observed mainly peaks corresponding to iron structures and other structures as Zn were defined by FTIR [47–53].

Sulfide structures as FeS ($2\theta = 26.8, 28.5, 32.85^{\circ}$) were identified in three catalysts, but in C3, ZnS ($2\theta = 30.5^{\circ}$) were identified too. This compound agreed with the sulfur content quantified in the elemental analysis; for this reason, the peaks in C3 were better defined.

ZnO structures were present in all the catalysts ($2\theta = 31.7, 34.28^{\circ}$), but C3 had more presence of this structure peaks than the other catalysts ($2\theta = 47.49, 56.52, 62.8, 67.9$ and 72.7°), ZnO₂ ($2\theta = 41.23^{\circ}$) on C2 and C3, but ZnO peak ($2\theta = 36.23^{\circ}$) were seen only in C3. The principal presence in the Zn structures in C3 could be associated with the TPR analysis, in which a single main peak was evident, due to the presence of these structures. In the case of the other two catalysts, the behavior was different because it presented three reduction regions.

Different iron structures were identified in the three catalysts analyzed. Fe₃O₄ ($2\theta = 35.5^{\circ}$) were found in C1, Fe₂O₃ ($2\theta = 39.67^{\circ}$) were identified in C2 and FeO ($2\theta = 50.50, 51.5^{\circ}$), while for C3 the three iron compounds Fe₃O₄ ($2\theta = 35.5^{\circ}$), Fe₂O₃ ($2\theta = 39.67^{\circ}$) and FeO ($2\theta = 50.50, 51.5^{\circ}$) were evidenced. The main peak of FeO ($2\theta = 44.6, 65.1^{\circ}$) was prominent in C1 and C2, while in the case of C3 was decomposed in two lower peaks. Of the three catalysts, C2 had a lower intensity compared to the other two catalysts.



Figure 4. XRD patterns of reduced catalysts C1, C2 and C3.

Scanning electron microscopy-energy dispersive spectrometry (SEM-EDS) confirmed the presence of these metallic phases on the catalytic material. On the surface of C1 were quantified 41.65% Fe and 16.91% Zn, C2 has 19.56% Fe and 7.33% Zn, while C3 has 7.22% Fe and 33.26% Zn. The results were concordant with XRD element identification. The surface morphology of the catalysts by SEM microscopy is shown in Figure 5.



(a)

(b)



(c)

Figure 5. SEM images of C1 (a), C2 (b) and C3 (c) calcined at 550 °C (view at 500×).

No homogeneous particles can be observed in C1–C2, while for C3, it can see some regularity size. Similarly, no crystal-defined structures of catalytic material were found in any of the catalysts evaluated. It may be due to the low homogeneity of the raw sludge. Likewise, differences in morphology between C1 and C3 can be seen, which may be related to the differences in the evaluated surface areas, 96.15 and 17.68 m²·g⁻¹, respectively (Table 1). To obtain irregular particles with good crystallinity is needed high reaction temperature of 1050 °C [54], but this temperature can cause sinterization for catalyst purposes.

2.4. Catalytic Evaluation of the Synthesized Materials

The chemisorption capacity of the catalytic material was analyzed with CO pulses (Figure 6). This information is important to identify catalytic applications correlated at the CO conversion. For catalysts C1 and C2, it was observed that both could adsorb CO. It is evident that in both the saturation of the surface is in the third pulse, around 10 min. In addition, the adsorption rate is similar for C1 and C2. Therefore, these could be used in CO reactions.



Figure 6. Thermal conductivity detector (TCD) response to CO pulse chemisorption by C1, C2 and C3. C1 and C2 saturation reached after 2 peaks (10 min), C3 saturation reached after 1 peak (3 min).

A different behavior was found for C3. The first time it was not possible to detect any signal. The CO flux was increased, observing a rapid saturation on the second peak around 3 min, a shorter time than in the other two catalysts. This behavior could be attributed to the Zn content compared to the other two that the main compound is iron. In addition, another factor is its low specific surface.

Therefore, this catalyst, C3, does not have characteristics to be used as a catalyst in CO processes.

The catalytic activity of the synthesized materials was analyzed in a reaction to the thermal decomposition of heavy crude oil. The reaction was carried out by thermogravimetric analysis (TGA) in an N_2 atmosphere. This technique has been used previously to characterize the heavy crude oils [55–57].

The loss of mass is considered as indicative of catalytic decomposition, where higher mass-loss on crude oil was regarded as better catalytic activity. These assays were compared with reactions without catalyst and a reaction performed with a commercial catalyst (FCC type, 265 m²·g⁻¹) at the

same space–time (0.15 g catalyst g^{-1} crude oil). The results are in Table 2; all the catalysts promote the weight-loss while the temperature increases as expected.

Temperature of Reaction, °C	Sample	Weight Loss, %	Kinetic Expression	R ²	Rate of Mass Loss (avg.), mg∙min ⁻¹
400	Crude oil without catalyst	54.30	$\tfrac{dm}{dt} = 0.0015 \ m_A^{0.5}$	0.90	0.57
	Crude oil + C1	59.28	$\frac{dm}{dt} = 0.0017 \ m_A^{0.5}$	0.92	0.61
	Crude oil + commercial cat.	56.00	$\frac{dm}{dt} = 0.0020 \; m_A^{0.5}$	0.95	0.65
450 -	Crude oil without catalyst	73.20	$\frac{dm}{dt} = 0.0016 \; m_{\rm A}^{0.5}$	0.91	0.64
	Crude oil + C2	84.50	$\tfrac{dm}{dt} = 0.0018 \; m_A^{0.5}$	0.90	0.71
	Crude oil + C3	82.10	$\tfrac{dm}{dt} = 0.0019 \; m_{\rm A}^{0.5}$	0.92	0.69
	Crude oil + commercial cat.	77.95	$\tfrac{dm}{dt} = 0.0019 \; m_A^{0.5}$	0.94	0.81

Table 2. Effect of the catalyst on the weight loss of crude oil on the thermal decomposition reaction.

dm, differential mass; dt, differential time; mA, mass at time (t), mg.

The three catalysts promote around 5% more mass-loss than the experiment without catalyst and some higher mass-loss compared with a commercial catalyst (C2–C3). For C2 and C3, the mass-loss was enhanced at temperatures higher than 400 °C. The catalytic effect was analyzed by mass-loss data, and it was used to define a kinetic model. The kinetic analysis was done applying the integral method of linearization of kinetic expression 2 m^{0.5} vs. time. The kinetic order of 0.5 provided the best fit with the experimental data according to the determination coefficient (\mathbb{R}^2).

The average rate of mass loss was calculated for the reactions. The experimental data were replaced in the kinetic expression for each time. The numerical value at $\left(\frac{dm}{dt}\right)$ was obtained for the extension of reaction.

Kinetic expressions showed that the rate of thermal decomposition promoted by catalytic material derived from sludge had similar values than the commercial catalyst, and an evident higher rate than the test without a catalyst, mainly in C2 and C3 to the reaction at 450 °C. For a technical limitation due to the highly exothermic reaction presented by crude oil itself, it was not able to perform thermal decomposition experiments above 450 °C.

These results permit concluded that the catalyst can be used in cracking applications to replace commercial catalysts.

3. Materials and Methods

The samples of sludges were taken from three galvanic companies with similar technologies located in Quito, Ecuador (Table 3). For company 1 the sludge was named L1; for company 2, L2 and company 3, L3. The catalytic materials derived from the sludges were identified as C1, C2 and C3.

Company	Sludge	Catalytic Material
Company 1	L1	C1
Company 2	L2	C2
Company 3	L3	C3

Table 3. Nomenclature used for the different sludges evaluated.

All the analyses of characterization were performed in triplicate to guarantee the best possible results.

3.1. Catalytic Preparation

The residual sludges were dried as is described on ASTM-D2216 in a drying oven (Nabertherm-TR60, Bahnhofstr, Lilienthal, Germany) for 4 h. The dried sludges were sieved between 150–180 μ m with a Tyler's-sieve series.

The residual sludges were calcined between 400–700 $^{\circ}$ C for 4 h in a muffle furnace (Thermo Scientific- Thermolyne, Waltham, MA, USA). This process was done to remove the organic residues and to oxidize the metallic phase on the sludges. After the thermal process, the residual sludges were considered as catalytic material.

The sludges and the catalytic material were analyzed by elemental analysis based on the ASTM-D5373 to identify the organic material in an elemental analyzer (Elementar-Vario Macro Cube, Langenselbold, Germany). Around 10 mg of the sample was exposed to oxidative decomposition at 1150 °C and subsequent reduction at 850 °C, to quantify carbon, hydrogen, nitrogen and sulfur (CHNS) composition. Before the experiment, the samples were prepared by digestion microwave system (Milestone-ETHOS UP, Sorisole, BG, Italy).

Fourier-transformed infrared spectroscopy (FTIR) (PerkinElmer-Spectrum Two spectrometer, Waltham, MA, USA) was used to identify the bonds related to organic and inorganic compounds on the sludges. The dried samples were pulverized in an agate mortar and then mixed with KBr (PerkinElmer, Waltham, MA, USA), in a weight ratio 1:100. Later, a pellet was formed in a press and then read on FTIR.

3.2. Catalyst Characterization

The surface area and pore volume of the catalytic material were determined by N_2 adsorption–desorption in a surface area analyzer (Horiba-SA 9600, minami-ku, Kyoto, Japan). The equipment uses the flowing gas method to acquire gas adsorption and desorption curves, and the surface area was by the single-point BET method. A sample of 0.15 g was loaded in a *U*-tube and degasified for 2 h at 300 °C to clean the surface. Later, the N_2 adsorption–desorption was done using liquid N_2 (Enox S.A, Quito, Pichincha, Ecuador).

Temperature-programmed reduction (TPR) was done to study the reducibility of the catalysts in an automated chemisorption analyzer (Micromeritics-AutoChem II, 2920, Norcross, GA, USA). The catalyst samples (200 mg) were reduced at the heating rate of 10 °C·min⁻¹ up 1000 °C under a flow (50 mL·min⁻¹) of 10% H₂/Ar (99.999%, INDURA, Quito, Pichincha, Ecuador). The consumption of hydrogen was monitored with a thermal conductivity detector (TCD). Experiments were performed at 15, 30 and 45 min to define the effect to the time on the total reduction.

X-ray diffraction was done (Malvern Panalytical-Empyrean, Malvern Worcestershire, UK) with CuK α radiation source and Scanning electron microscopy SEM/EDS in a (TESCAN-MIRA3 FEG SEM, Brno, Kohoutovice, Czech Republic) were used to study the metallic content on the reduced catalyst. These assays were done in an external laboratory CENCINAT ESPE Laboratory (Sangolquí, Pichincha, Ecuador).

3.3. Catalytic Material Evaluation

The CO chemisorption was studied with CO pulses technique (Micromeritics-AutoChem II, 2920, Norcross, GA, USA). Before the experiments, the catalysts were reduced, as described previously. Chemisorption experiments were done with 200 mg of the samples at 50 °C [58] exposed at the catalyst at 10% CO/He (99,999%, INDURA, Quito, Pichincha, Ecuador). The total adsorption amount of CO was detected by TCD. The gas uptake was measured from a sequence of small pulses until saturation was obtained.

The catalytic activity of the synthesized materials was evaluated with a thermal decomposition reaction with a crude oil sample (18.9 °API, PETROECUADOR, Esmeraldas, Esmeraldas, Ecuador). A thermogravimetric analysis in a thermo-balance (Mettler Toledo-TGA1 SF/1100, Columbus, OH, USA),

was realized in a reaction atmosphere of N₂ (30 mL·min⁻¹, 99,999%, INDURA, Quito, Pichincha, Ecuador) to determine the loss of mass promoted for the catalytic activity. In this assay, a space–time of 0.15 g catalyst g⁻¹ crude oil was used. The studies were performed at 400 °C for C1 and 450 °C for C2–C3 with a rate of heating to 10 °C·min⁻¹. The reaction had 1 h to time on stream and the mass loss was recorded every 35 s.

Before the study, the catalytic material was reduced in a 10% H2/Ar. Assays without catalyst and FCC commercial catalyst (GRACE-ResidCrackeR, Columbia, MD, USA) were done to compare the catalytic effect on the crude oil. The reaction rate of thermo-catalytic decomposition was determined through the integral method of data analysis considering the loss of mass vs. time of reaction.

4. Conclusions

Due to the metal content—mainly iron in their composition—sludge from wastewater treatment from galvanic industries can be used as catalytic material in the thermal decomposition of hydrocarbons—after a thermal treatment.

The best catalytic activity was evidenced at the sludges calcinated at 400 °C for C1 and 500 °C for C2–C3. The catalysts had specific surface areas of 96.15, 63.36 and 17.68 $m^2 \cdot g^{-1}$, respectively. For the reduction of the catalyst, the best condition of time was 15 min and 750, 850 and 800 °C for C1, C2 and C3, respectively. The prepared catalyst evidenced at CO chemisorption capacity, those with the best performance were catalysts C1 and C2.

The catalytic material enhanced the rate of reaction on the thermal decomposition of crude oil promotes more weight-loss in a thermo-gravimetric analysis compared to the reactions without the catalyst.

The synthesis presented here is a good and sustainable alternative to commercial (heavy oil cracking) catalysts due to the easiness of synthesis procedures required, the low E-factor obtained and the recycling of industrial waste promoted.

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Article A Highly Efficient Monolayer Pt Nanoparticle Catalyst Prepared on a Glass Fiber Surface

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Abstract: Over the past few years, various nanoparticle-supported precious metal-based catalysts have been investigated to reduce the emission of harmful substances from automobiles. Generally, precious metal nanoparticle-based exhaust gas catalysts are prepared using the impregnation method. However, these catalysts suffer from the low catalytic activity of the precious metal nanoparticles involved. Therefore, in this study, we developed a novel method for preparing highly efficient glass fiber-supported Pt nanoparticle catalysts. We uniformly deposited a single layer of platinum particles on the support surface using a chemically adsorbed monomolecular film. The octane combustion performance of the resulting catalyst was compared with that of a commercial catalyst. The precious metal loading ratio of the proposed catalyst was approximately seven times that of the commercial catalyst. Approximately one-twelfth of the mass of the proposed catalyst exhibited a performance comparable to that of the commercial catalyst. Thus, the synthesis method used herein can be used to reduce the weight, size, and manufacturing cost of exhaust gas purification devices used in cars.

Keywords: nanoparticle; exhaust gas catalyst; precious metal; chemically adsorbed monomolecular film

1. Introduction

Carbon monoxide, hydrocarbons, nitrogen oxides (NO_x), and particulate matter such as soot are harmful air pollutants emitted from automobiles. Vehicle emission regulations are becoming increasingly stringent. To reduce the emission of harmful pollutants from automobiles and meet the demand for energy conservation, researchers have attempted to improve the performance of precious metal catalysts used in automobile exhaust gas purification devices and fuel cells. Conventionally, these catalysts are supported on a porous oxide such as silicon dioxide (silica: SiO₂) or aluminum oxide (alumina: Al_2O_3) or a substrate with a large specific surface area such as activated carbon. Supported precious metal nanoparticle catalysts based on metals such as Pt, Rh, and Pd have been widely investigated [1–4]. Such precious metal nanoparticle-based catalysts are typically prepared using the impregnation method [5]. However, the precious metal nanoparticles in the catalysts prepared using this method aggregate at high temperatures, and hence show poor dispersion. Moreover, it is difficult to control the nanoparticle diameter using this method. This results in a significant reduction in the effective surface area and catalytic activity of the nanoparticles. Moreover, precious metals (particularly Pt group metals) are highly expensive, and hence should ideally be used in limited quantities. Motivated by these challenges, herein, we developed a novel method for preparing highly efficient glass fiber-supported Pt nanoparticle catalysts. We deposited Pt nanoparticles uniformly on a chemically

adsorbed monomolecular film formed on the surface of a glass fiber support. The nanoparticles were densely packed in a single layer to avoid wastage. The monomolecular film could be removed by heat treatment. The objective of this study was to develop a highly efficient Pt catalyst with a large effective surface area that could maintain high stability and catalytic activity even under high temperature environments such as engine exhaust devices.

2. Results and Discussion

2.1. Observation of Pt Catalyst

Figure 1 shows the field emission scanning electron microscopy (FE-SEM) images of the Pt catalyst surface. Table 1 lists the precious metal loading rates (precious metal particle weight/catalyst weight \times 100) of the Pt catalyst prepared herein and the commercial catalyst.





Figure 1. FE-SEM images of the Pt catalyst on the glass fiber substrate: (a) before curing, (b) after curing, and (c) on the glass fiber substrate without the 3-mercaptopropyltrimethoxysilane (MPTS) monolayer after the Pt nanoparticle treatment.

Table 1. Precious metal loading rates (precious metal particle weight/catalyst weight \times 100) of the catalysts.

-	Catalyst Weight (g)	Precious Metal Particle Weight (g)	Loading Rate (wt%)
Pt catalyst	0.047	0.0060	12.7
Commercial catalyst sample	0.9722	0.0165	1.7

Figure 1a,b reveal that Pt nanoparticles (on the scale of 10 nm) were dispersed on a single layer on the surface of the glass fiber substrate. Moreover, the Pt particles exhibited minimal aggregation because of sintering at 350 °C (Figure 1b). However, the Pt particles could not be grafted when the 3-mercaptopropyltrimethoxysilane (MPTS) monolayer was formed (Figure 1c). This suggests that using a chemically adsorbed monolayer with a terminal thiol (-SH) is an effective route for forming a single layer of Pt particles with a large specific surface area. As can be observed from Table 1, the loading ratio of the Pt catalyst prepared in this study was approximately seven times larger than that of the commercially available catalyst.

2.2. Thermal Characterization during Catalyst Preparation

Figure 2 shows the thermogravimetry–differential scanning calorimetry (TG–DSC) results of the Pt catalyst. The catalyst showed weight loss as the temperature approached 200 °C. Hence, a DSC peak was observed. This peak can be attributed to the volatilization of MPTS, whose boiling point is approximately 215 °C. The results show that the weight of the MPTS lost by volatilization decreased and that the chemisorbed monomolecular film was sufficiently removed by heating the catalyst at 350 °C.



Figure 2. Thermogravimetry-differential scanning calorimetry (TG-DSC) curves of the Pt catalyst.

2.3. Effective Surface Area of the Catalyst

Figure 3 shows the X-ray diffraction (XRD) results of the Pt catalyst before and after the heat treatment. The catalyst showed a Pt peak at 2θ = approximately 40°. After heat treatment, the intensity of this peak increased, whereas the full width at half maximum decreased. This suggests that the particles aggregated, and the particle diameter increased after the heat treatment. This also suggests that the specific surface area of the particles decreased after the heat treatment. However, as the peak obtained after the heat treatment was not extremely sharp, it can be stated that the specific surface area required for the catalytic reaction was sufficient.

It was assumed that the particles shown in Figure 1 a were approximately 5 nm in diameter. In addition, the surface area and volume per particle were approximately 3.14×10^{-16} m² and 5.24×10^{-19} cm³, respectively. Since the density of platinum was 21.45 g/cm³, the weight and number of units per particle were 1.12×10^{-17} g and 8.90×10^{16} , respectively. Moreover, the BET surface area was approximately 27.96 m²/g. In contrast, Figure 3 shows that the BET surface area decreased to approximately 14.02 m²/g because the half width before and after heating had nearly doubled in size. Furthermore, as described above, since the catalytic effect was considered to be saturated at 300 °C or higher, it was found that a sufficient catalytic effect was exhibited by the BET surface area of

the platinum particles after the heat treatment. In the referenced literature, the average particle size of platinum was 62 nm. The BET surface area calculated from this was approximately 4.37 mm²/g. From this, it is considered that the platinum catalyst developed in this study has a large BET surface area and exhibits high performance [6].



Figure 3. XRD patterns of the Pt catalyst before and after the heat treatment.

2.4. Catalyst Performance Evaluation

Figures 4 and 5 show the amount of water generated and the octane combustion rates of the catalysts as a function of temperature, respectively. In the absence of a catalyst, the amount of water produced by the combustion of octane remained nearly constant at temperatures up to 300 °C. However, the amount of water generated increased substantially with an increase in temperature to 400 °C. This can be attributed to octane self-burning. Volatile organic compounds (VOCs) typically burn completely to form water and carbon dioxide with an increase in temperature from approximately 750 to 850 °C (direct combustion method) [7]. Thus, at 400 °C, octane acted as a VOC and underwent combustion even in the absence of the catalyst, thus producing a large amount of water. At 200 °C, the amount of water produced in the presence of the catalysts (both the Pt and commercial catalyst) was higher than that produced in the absence of the catalysts. Furthermore, at temperatures \geq 300 °C, the catalysts showed no significant change in the amount of water produced. This indicates that the performance of the catalysts could be evaluated at temperatures ≥ 200 °C. However, the performance of the catalysts saturated at temperatures higher than 300 °C. These results indicate that the performance of the Pt catalysts prepared in this study was comparable to that of the commercial catalyst. As can be observed from Table 2, the Pt catalyst showed a higher octane combustion rate per gram of the catalyst and precious metal particles than the commercial catalyst.

Table 2. Precious metal nanoparticle utilization efficiency of the catalysts.

Heating Temperature	Combustion Rate of Octane per g of Catalyst (%)		Octane Combustion Rate per g of Precious Metal Particles (%)	
-	Commercial Catalyst Pt Catalyst		Commercial Catalyst	Pt Catalyst
50	2.2	56.2	97.8	466.3
100	5.1	49.9	232.4	414.2
200	18.3	195.3	825.5	1620.3
300	40.9	460.7	1848.5	3822.5
400	43.5	536.4	1964.7	4450.6



Figure 4. Amount of water produced by the combustion of octane as a function of the catalyst temperature.



Figure 5. Combustion rate of octane for the catalysts as a function of the catalyst temperature.

At temperatures of 200 °C or higher, the Pt catalyst showed an octane combustion rate that was approximately 12 times higher per gram than that of the commercial catalyst. On the contrary, the octane combustion rate per gram of the precious metal particles of the Pt catalyst was approximately two times higher than that of the commercial catalyst. Pt and Pd show the same catalytic performance for the combustion of hydrocarbons [8]. However, the performance of 1/12th of the mass of the Pt catalyst prepared in this study was comparable to that of the commercial catalyst prepared using the conventional method. This indicates that the precious metal utilization efficiency of the Pt catalyst was higher than that of the commercial catalyst. These results suggest that the Pt catalyst developed in this study was approximately two times more efficient than the commercially available catalyst. Therefore,

the synthesis method used in this study can be applied to prepare catalysts for exhaust gas purification devices used in cars to reduce their weight, size, and cost. However, further investigation is required to evaluate the efficiency of this method in the presence of coke.

3. Materials and Methods

3.1. Preparation of Platinum Catalyst

The glass fiber substrate (manufactured by Masuda Rika Kogyo Co., Ltd.) (Osaka, Japan) was heated at 350 °C for 1 h using an electric furnace to remove organic matter from its surface. After the heat treatment, the glass fiber was ultrasonically cleaned with ethanol for 5 min. After drying, the material was further irradiated under air atmosphere for 10 min using an excimer light irradiation device (Ushio Inc., UER20-172B) (Tokyo, Japan), and the surface was further oxidized with generated ozone to achieve hydrophilization. After the irradiation, the glass fiber was immersed at room temperature for 2 h in a chemical adsorption solution prepared under the conditions listed in Table 3 [9].

Table 3. Conditions for preparing the adsorption solution.

-	Chemicals	Concentration	Amount
Solvent	Aqua solvent G-21 (Aqua Chemical Co., Ltd., Chuo-ku, Japan)	Undiluted	50 mL
Adsorbent	3-mercaptopropyltrimethoxysilane (MPTS) (dehydrated chloroform dilution)	0.1 M	76.5 μL
Catalyst	Tetra chlorosilane (TCS) (dehydrated chloroform dilution)	0.01 M	2.5 mL

MPTS (Shin-Etsu Chemical Co., Ltd.) (Tokyo, Japan) was used as the chemical adsorbent in this study (Figure 6). After immersion in the chemical adsorption solution, the glass fiber was removed and subjected to ultrasonic washing with ethanol for 5 min to deposit a monomolecular film on its surface. The glass fiber with the monomolecular film was then placed in a sample case and left under air atmosphere for at least 24 h. Finally, the glass fiber was washed with chloroform, acetone, and ethanol, and then dried.



Figure 6. Chemical structure of MPTS.

Figure 7 shows the Fourier-transform infrared-reflection absorption spectroscopy (FTIR-RAS) (Massachusetts, USA) profile of the glass substrate with the MPTS film. The absorption peaks corresponding to the carbon chains of MPTS confirm the chemical adsorption of MPTS onto the glass substrate [10]. In order to graft the substrate with Pt particles, it was immersed for 4 h in a dispersion of Pt nanoparticles (manufactured by Shikoku Keisoku Co.; size distribution of the particles is shown in Figure 8) (Kagawa, Japan) (adsorption solvent = ethylene glycol) prepared to a particle concentration of 2.5 wt% [11].



Figure 7. Fourier-transform infrared-reflection absorption spectroscopy (FTIR-RAS) profile of the MPTS monolayer adsorbed on the glass plate.



Figure 8. Particle-size distribution of the Pt nanoparticles.

Immersion was achieved by ultrasonically stirring the Pt nanoparticle dispersion using an ultrasonic homogenizer. Then, ultrasonic cleaning was carried out using ethanol to prepare the glass fibers and to graft Pt nanoparticles onto them. Thereafter, the monomolecular film was decomposed and Pt was cured by heating the resulting assembly at 350 °C, using an electric furnace (Tokyo, Japan) under air atmosphere for 30 min. Finally, the catalyst with Pt nanoparticles deposited on the surface of glass fibers was obtained. The schematic of the platinum catalyst preparation process is shown in Figure 9.

The surface morphology of the Pt catalyst was observed before and after the heat treatment by carrying out FE-SEM measurements (Tokyo, Japan) to confirm the grafting of Pt particles. For comparison, the FE-SEM analysis of the glass fibers without the MPTS film was also carried out. In order to measure the weight of the Pt nanoparticles grafted onto the glass fiber surface, the catalyst was added to a hydrofluoric acid aqueous solution (which was handled with the utmost care) [12]. The glass fibers dissolved into this solution and the Pt nanoparticles could be recovered by filtering. The recovered Pt nanoparticles were weighed, and the loading ratio was calculated by measuring the mass of the remaining Pt particles.



Figure 9. Schematic of the Pt catalyst preparation process.

3.2. Catalyst Performance Evaluation

In order to compare the catalyst loading ratio, a commercially available catalyst (Suzuki Corporation, Exhaust Manifold: Precious metal component: Pd) (Nagano, Japan) was dissolved in hydrofluoric acid, concentrated nitric acid, and an aqueous hydrogen peroxide solution. This metal catalyst was then filtered and weighed to calculate its metal loading ratio. Then, tubing was piped so that the gas flowed from the air inlet to the flask, catalyst section, trap pipe, and draft, as shown in Figure 10. In the catalyst section, the Pt catalyst with a measured mass was packed in a U-shaped pipe, which was placed in a mantle heater. The temperature of the mantle heater was controlled using a voltage regulator and thermostat. Furthermore, octane (C8H18) (Osaka, Japan) was introduced into the flask beforehand, molecular sieves were placed in the trap tube and weighed, and dry air (humidity approximately 0.2%) was injected at a flow rate of 0.8 L/min for 90 min from the air inlet. After 90 min, the flow of dry air was interrupted, and the mass of the trap tube containing the octane-containing flask and the molecular sieve weight were measured using an electronic balance. These tests were carried out at 50, 100, 200, 300, and 400 °C. The same experiments were carried out for the commercially available catalyst, the Pd catalyst from Suzuki. Furthermore, the TG-DSC curve of the Pt catalyst was obtained before carrying out the heat treatment to determine the difference between the weight of the catalyst in the presence and absence of the chemically adsorbed monomolecular film. The XRD measurements (Kyoto, Japan) of the catalyst were conducted before and after the heat treatment to confirm the change in the state of Pt.



Figure 10. Schematic of the device used for evaluating the catalyst performance.

4. Conclusions

Herein, we proposed a novel method for developing highly efficient Pt catalysts using a reactive chemically adsorbed monomolecular film, Pt nanoparticle dispersion, and glass fiber substrate. The Pt catalyst investigated in this study was prepared by depositing a reactive chemically adsorbed monomolecular film with a thiol group at the molecular terminal on the surface of a hydrophilized glass fiber. The monomolecular film enabled the uniform and dense grafting of Pt nanoparticles on the surface of the glass fiber as a single layer. In addition, the Pt loading ratio of the catalyst was approximately 12.7 wt%. This indicates that the chemically adsorbed monomolecular film on the Pt catalyst could support more platinum than the commercially available catalyst. The catalytic performances of the Pt and commercially available catalysts were evaluated on the basis of their octane combustion rates. Both the catalysts exhibited catalytic performance at temperatures \geq 200 °C. At 300 °C, the octane combustion rates of the catalysts were 80% or more. Moreover, at 50–400 °C, the octane combustion rates of both the catalysts were approximately the same. Hence, no difference was observed in the catalytic performance of the catalysts. Furthermore, Pt catalysts have been found to exhibit catalytic performance comparable to that of Pd catalysts under lean conditions [6]. In addition, Pt is cheaper than Pd [13]. In this study, we successfully prepared a highly efficient Pt catalyst with superior catalytic performance and lower Pt loading than the commercially available catalyst. The catalyst prepared in this study is a potential candidate for application in car exhaust purification devices as it can reduce the weight, size, and cost of these devices. However, in this study, we evaluated the catalyst performance only on the basis of octane combustion. Hence, further evaluation under a gas atmosphere is also necessary.

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Article Kinetic and Mechanistic Study of Rhodamine B Degradation by H₂O₂ and Cu/Al₂O₃/g-C₃N₄ Composite

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Abstract: The classic Fenton reaction, which is driven by iron species, has been widely explored for pollutant degradation, but is strictly limited to acidic conditions. In this work, a copper-based Fenton-like catalyst Cu/Al₂O₃/g-C₃N₄ was proposed that achieves high degradation efficiencies for Rhodamine B (Rh B) in a wide range of pH 4.9–11.0. The Cu/Al₂O₃ composite was first prepared via a hydrothermal method followed by a calcination process. The obtained Cu/Al₂O₃ composite was subsequently stabilized on graphitic carbon nitride $(g-C_3N_4)$ by the formation of C–O–Cu bonds. The obtained composites were characterized through FT-IR, XRD, TEM, XPS, and N₂ adsorption/desorption isotherms, and the immobilized Cu⁺ was proven to be active sites. The effects of Cu content, $g-C_3N_4$ content, H_2O_2 concentration, and pH on Rh B degradation were systematically investigated. The effect of the catalyst dose was confirmed with a specific reaction rate constant of $(5.9 \pm 0.07) \times 10^{-9} \text{ m} \cdot \text{s}^{-1}$ and the activation energy was calculated to be 71.0 kJ/mol. In 100 min 96.4% of Rh B (initial concentration 20 mg/L, unadjusted pH (4.9)) was removed in the presence of 1 g/L of catalyst and 10 mM of H₂O₂ at 25 °C, with an observed reaction rate constant of $6.47 \times 10^{-4} \text{ s}^{-1}$. High degradation rates are achieved at neutral and alkaline conditions and a low copper leaching (0.55 mg/L) was observed even after four reaction cycles. Hydroxyl radical (HO·) was identified as the reactive oxygen species by using isopropanol as a radical scavenger and by ESR analysis. HPLC-MS revealed that the degradation of Rh B on Cu/Al₂O₃/CN composite involves N-de-ethylation, hydroxylation, de-carboxylation, chromophore cleavage, ring opening, and the mineralization process. Based on the results above, a tentative mechanism for the catalytic performance of the $Cu/Al_2O_3/g-C_3N_4$ composite was proposed. In summary, the characteristics of high degradation rate constants, low ion leaching, and the excellent applicability in neutral and alkaline conditions prove the Cu/Al₂O₃/g-C₃N₄ composite to be a superior Fenton-like catalyst compared to many conventional ones.

Keywords: Cu/Al₂O₃/g-C₃N₄; Fenton-like; H₂O₂; hydroxyl radical; Rhodamine B

1. Introduction

With the rapid development of industry, persistent organic pollutants in water have attracted widespread attention due to their persistence, bioaccumulation, and high toxicity [1,2]. So far, advanced oxidation processes (AOPs) have been found to be one of the most promising methods to treat persistent organic pollutants in water [3–7]. Due to the in-situ formed highly reactive and non-selective hydroxyl radicals (HO·) during the process, AOPs are capable of mineralizing almost all organic compounds to CO_2 , H_2O , and small organic compounds [8–11].
As a typical AOP, Fenton reaction is efficient for HO· production, but still faces some limitations, such as the strict acidic pH range (pH < 4) [12,13], formation of iron sludge [14,15], and high cost for catalyst recycling [16,17]. A number of non-ferrous metals, such as copper [18], manganese [19], and titanium [20], have been developed as alternatives. In particular, Cu⁺ reacts with H₂O₂ in a similar manner to Fe²⁺, but with a much higher reaction rate constant (as shown in Equations (1) and (2)). In contrast to Fe³⁺ that forms the insoluble [Fe(H₂O)₆]³⁺ complex at pH > 5, Cu²⁺ forms the aquo complex [Cu(H₂O)₆]²⁺ that predominates at neutral conditions, making Cu⁺ own a wider pH range for application [21]. Additionally, it is known that Cu²⁺ could form certain complexes with organic degradation intermediates, which could react with H₂O₂ to generate more HO· [22].

$$Fe^{2+} + H_2O_2 \rightarrow Fe^{3+} + HO + OH^-$$
 (k = 63 - 76 M⁻¹·s⁻¹) (1)

$$Cu^{+} + H_2O_2 \rightarrow Cu^{2+} + HO + OH^{-}$$
 (k = 1.0 × 10⁴ M⁻¹·s⁻¹) (2)

However, Cu^+ ions are prone to disproportionation in acidic aqueous solution and can be easily oxidized by dissolved O₂, thereby limiting the application in the aqueous environment [23]. One common strategy for the preparation of copper-based catalysts is the immobilization of copper species on support materials, for example, the immobilization of Cu^+/Cu^{2+} , copper oxide, or the copper-organic complex [24] on various matrixes like metal oxides [25–27], molecular sieve [28,29], and graphitic carbon nitride (g-C₃N₄) [30,31].

With a suitable band gap (2.7 eV) and high response to visible light, g-C₃N₄ has been intensively explored as a photocatalyst for energy and environmental applications [3,32–34]. Apart from this, g-C₃N₄ could also be applied as a Fenton-like catalyst in the absence of light irradiation through the combination with other materials [35,36]. g-C₃N₄ has a 2D planar structure in which tri-s-triazine units are connected by tertiary amines. Typical π -conjugated graphitic planes are formed via the sp² hybridization of carbon and nitrogen atoms [37], which brings a large specific surface area, thus providing more reaction sites for heterogeneous reaction. Besides, g-C₃N₄ shows strong affinity for H₂O₂ and could easily adsorb them to the surface, thereby providing larger chances for their contact with other catalytic materials loaded on g-C₃N₄ [34]. Additionally, numerous external groups (–NH₂, –NH, –N, and –OH) on the surface may serve as strong Lewis base sites for nanoparticle deposition or metal inclusion [38]. The incorporation of metallic elements into the g-C₃N₄ matrix could induce the production of delocalized electrons, which promotes the catalytic reactions [36,39]. As a typical example, Xu et al. constructed the Cu-Al₂O₃-g-C₃N₄ system, in which a small amount of g-C₃N₄ was used to coordinate with Cu ions to induce the formation of an electron-rich Cu centre and decrease the electron density of the π -electron conjugated system through cation- π interactions [40].

Inspired by the above-mentioned research, a similar but distinguishing efficient Cu/Al₂O₃/g-C₃N₄ composite was proposed in this work, with which H₂O₂ activating was promoted in a different approach. Copper species were bonded to the Al₂O₃ framework to act as the catalytic component and g-C₃N₄ was used in large amounts to act as support for the Cu/Al₂O₃ composite. The decomposition of H₂O₂ was promoted by the strong adsorption of H₂O₂ on the g-C₃N₄ matrix. The obtained composites were characterized through Fourier transform infrared (FT-IR) spectroscopy, X-ray diffraction (XRD), transmission electron microscopy (TEM), X-ray photoelectron spectroscopy (XPS), and N₂ adsorption/desorption isotherms. The optimal synthetic parameters and experimental conditions, including the Cu content, g-C₃N₄ content, H₂O₂ concentration, and pH value were determined. Besides, the effect of the catalyst dose and temperature were confirmed by calculating specific reaction rate constant and activation energy, and the durability and low leaching were evaluated in recycling experiments and electron spin resonance (ESR) analysis, while the degradation products of Rh B were identified by high performance liquid chromatography-mass spectrometry (HPLC-MS)

analysis. Based on the results, the catalytic mechanism of Rh B degradation on $Cu/Al_2O_3/g-C_3N_4$ composite was proposed.

2. Results and Discussion

2.1. Structural Characterization of Composites

 Cu_{12}/Al_2O_3 and $Cu_{12}/Al_2O_3/CN_{1.3}$ (the naming rules of catalysts are indicated in experimental section) were selected as the typical Cu/Al_2O_3 and $Cu/Al_2O_3/CN$ composite to compare their structures with Al_2O_3 and CN. The FT-IR spectra of Al_2O_3 , Cu/Al_2O_3 , CN, and $Cu/Al_2O_3/CN$ samples were recorded to distinguish the functional groups. As shown in Figure 1, the two peaks at 1513 cm⁻¹ and 1636 cm⁻¹ in the FT-IR spectra of Al_2O_3 and Cu/Al_2O_3 are attributed to the C=C vibrations and C=O vibrations, which are derived from glucose added in the preparation process [40]. As observed for CN, the sharp peak at 810 cm⁻¹ is ascribed to the breathing mode of tri-s-triazine units, and the peaks in the region of 1200-1600 cm⁻¹ are assigned to the stretching vibration of the CN heterocycle [31]. In addition, the peak at 3173 cm⁻¹ corresponds to the N–H stretching vibration [36]. All these characteristic peaks could be observed in the $Cu/Al_2O_3/CN$ composite, indicating that the chemical structure of CN was not affected by the introduction of Cu/Al_2O_3 .



Figure 1. FT-IR spectra of Al₂O₃, Cu/Al₂O₃, CN, and Cu/Al₂O₃/CN samples.

The X-ray diffraction patterns of Al_2O_3 , Cu/Al_2O_3 , CN, and $Cu/Al_2O_3/CN$ samples were investigated to determine the crystalline structures, as presented in Figure 2. It is clearly observed that the major crystalline structure of Al_2O_3 is the γ -alumina phase (JCPDS No. 10-0425) [41]. In comparison with pure Al_2O_3 , new peaks are founded at 35.2°, 38.5°, 48.8°, 53.4°, 58.2°, 66.2°, and 68.1° in the XRD pattern of Cu/Al_2O_3 , which represent the (002), (111), (20-2), (020), (202), (31-1), and (220) planes of the copper oxide phase (JCPDS No. 48-1548), respectively [40]. The peak at 61.5° is referred to the diffraction of the (220) plane of cuprous oxide phase (JCPDS No. 65-3288) [42]. These results imply that the copper species were successfully bonded to the Al_2O_3 framework. From the pattern of CN, two main diffraction peaks could be found at 13.0° and 26.9°, which correspond to the interlayer stacking (100) plane of tri-s-triazine units and the (002) plane arising from the interlayer stacking of aromatic systems (JCPDS No. 87-1526) [43]. All the diffraction peaks of Cu/Al_2O_3 and CN could be found in the pattern of Cu/Al_2O_3/CN composite, indicating the successful synthesis of the Cu/Al_2O_3/CN composite.

The microstructures of Al₂O₃, Cu/Al₂O₃, CN, and Cu/Al₂O₃/CN samples were analyzed by TEM. The results are shown in Figure 3. As can be seen in Figure 3A,B, the lattice spacing was confirmed to be 0.29 nm, which corresponds to the (220) lattice planes of γ -alumina [44], and was consistent with the results obtained by XRD. In Figure 3C, it can be seen that the copper bonded alumina framework was rod like. The lattice spacing in Figure 3D was confirmed to be 0.24 nm, which corresponds to the (111) lattice planes of copper oxide confirmed by XRD [45]. In Figure 3E, it is clear that CN shows

a two-dimensional structure with a wide pore size distribution [35]. According to Figure 3F, it can be observed that the rod like Cu/Al_2O_3 was embedded in the CN matrix, indicating the successful combination of Cu/Al_2O_3 and CN.



Figure 2. XRD patterns of the synthesized samples (a) Cu/Al₂O₃/CN, (b) Cu/Al₂O₃, (c) CN, and (d) Al₂O₃.



Figure 3. TEM images of (A,B) Al₂O₃, (C,D) Cu/Al₂O₃, (E) CN, and (F) Cu/Al₂O₃/CN.

The XPS spectra of the $Cu/Al_2O_3/CN$ composite before and after the reaction were obtained to investigate its surface chemical states and elemental composition. The results are shown in Figure 4

and Table 1. The peaks of the C 1s spectrum at 281.5 eV and 284.6 eV were assigned to C–H and C–C, respectively. Notably, the peak at 285.1 eV was attributed to C–O–H or C–O–metal, which could confirm that Cu/Al₂O₃ was stabilized on the CN matrix by the C–O–Cu bonds [36,40]. For N 1s, the peaks at 395.1 eV, 395.7 eV, and 397.1 eV were ascribed to triazine rings C-N-C, tertiary nitrogen $N-(C)_3$, and sp²-type C=N bond, indicating that the structure of CN was not changed [36]. The XPS spectrum of Cu 2p in Figure 4C displayed three main peaks at 932.0 eV, 934.0 eV, and 941.5 eV, which correspond to Cu^+ , Cu^{2+} , and satellite peaks of copper species, respectively [40,41]. As the binding energy of Cu^+ and Cu^0 are very close, it is difficult to distinguish between Cu^+ and Cu^0 by the XPS feature of Cu $2p_{3/2}$. The Cu LMM peak is normally applied to distinguish between the Cu⁰ and Cu⁺ according to previous studies [46,47]. However, due to the relatively low copper content in the sample, the presence of Cu⁺ cannot be judged by the Cu LMM peak. The results of the XRD patterns could be used instead to confirm the presence of Cu⁺. Two peaks of the Al 2p spectrum were observed at 74.1 eV and 75.0 eV in Figure 4D, which were attributed to Al-O-Al and Al-O-Cu, indicating that copper species were bonded to Al₂O₃ framework [46]. The Cu 2p XPS spectrum of the used Cu/Al₂O₃/CN composite is shown in Figure 4E. The peaks at 931.7 eV, 933.6 eV, and 941.5 eV still represent Cu⁺, Cu²⁺, and satellite peaks of copper species, respectively. The Cu⁺ to Cu²⁺ ratio on the Cu/Al₂O₃/CN composite was 2.34 before reaction and decreased to 1.42 after reaction, indicating that copper species were the active sites and the conversion of Cu^+ to Cu^{2+} was involved in the reaction [48].



Figure 4. (A) C 1s, (B) N 1s, (C) Cu 2p, and (D) Al 2p XPS spectra of Cu/Al₂O₃/CN composite before reaction, and (E) Cu 2p spectrum of the Cu/Al₂O₃/CN composite after reaction.

	BE/eV	Chemical Bonds		BE/eV	Chemical Bonds
C 1s	281.5	C-H	N 1s	395.1	C-N-C
	284.6	C-C		395.7	N-(C)3
	285.1	C-O		397.1	C=N
Cu 2p	932.0/931.7	Cu ⁺	Al 2p	74.1	Al-O-Al
	934.0/933.6	Cu ²⁺	*	75.0	Al-O-Cu

Table 1. XPS results of the Cu/Al₂O₃/CN composite.

BE denotes the binding energy.

The N₂ adsorption/desorption isotherm and the pore size distribution of the Al₂O₃, Cu/Al₂O₃, CN, and Cu/Al₂O₃/CN samples are shown in Figure 5. The specific surface area of Al₂O₃ reaches 133.1 \pm 0.5 m²/g with a pore width of 6.7 nm, and the introduction of copper species leads to a decline to 119.5 \pm 1.0 m²/g and 5.3 nm, respectively. All the CN containing samples show typical IV isotherms with the H3 hysteresis loop, indicating the existence of a typical mesoporous structure with slit-like pores in CN [22]. Additionally, when Cu/Al₂O₃ was stabilized on the CN matrix, the specific surface area increased from 72.2 \pm 0.9 m²/g for CN to 146.6 \pm 1.0 m²/g for Cu/Al₂O₃/CN, which is more beneficial for the adsorption of organic pollutants and H₂O₂ on the catalyst surface and proves that the fabrication of the Cu/Al₂O₃/CN composite is not merely a physical mixing process. In summary, a higher specific surface area and smaller pore width are achieved in the Cu/Al₂O₃/CN composite.



Figure 5. N₂ adsorption/desorption isotherm and the pore size distribution (insert) of the Al₂O₃, Cu/Al₂O₃, CN, and Cu/Al₂O₃/CN.

2.2. Catalytic Performance of Composites

The effect of Cu content, CN content, H_2O_2 concentration, and pH value were investigated to obtain the optimal synthetic parameters and reaction conditions. Besides, the effect of the catalyst dose and temperature was confirmed by calculating the specific reaction rate constant and activation energy (E_a). The durability and ion leaching of the composite were evaluated by the recycling experiments. In addition, the reactive species generated were identified by ESR analysis and radical scavenging experiments, and then the catalytic mechanism of Rh B on Cu/Al₂O₃/CN composite was proposed by confirming intermediates using HPLC-MS.

2.2.1. Effect of Cu Content

In order to obtain the optimal Cu content for catalyst fabrication, a series of Cu_x/Al_2O_3 composites (x = 0, 4, 7, 9, 12, and 15 wt %) were prepared to compare their catalytic performances on the removal of Rh B in the presence of H_2O_2 . As shown in Figure 6, in the absence of copper decoration, Al_2O_3 exhibited negligible catalytic capacity for Rh B degradation, with 3.0% Rh B removed in 100 min. The degradation was enhanced by copper doping and the rate progressively increased from x = 0 to

x = 12, after which the degradation rate started to decrease. During the synthesis process of Cu/Al₂O₃ composite, copper species were bonded to the Al₂O₃ framework. However, there is an upper limit (x = 12) for the amount of copper species that could enter the Al₂O₃ framework, so part of the copper species would be present as the extra framework if excess copper was introduced [47]. The extra framework copper species may impede the contact between H₂O₂ and framework copper species, thereby limiting the decomposition of H₂O₂ [22,41]. Therefore, the optimal Cu content was confirmed to be x = 12 and Cu₁₂/Al₂O₃ was selected as optimal components for further studies.



Figure 6. [Rh B]/[Rh B]₀ as a function of time in the presence of 1 g/L Cu_x/Al_2O_3 composite (x = 0, 4, 7, 9, 12, and 15 wt %). Reaction conditions: [Rh B]₀ = 20 mg/L, [H₂O₂]₀ = 10 mM, V = 100 mL, T = 25 °C, pH 4.9 (unadjusted).

2.2.2. Effect of CN Content

A fixed amount (0.1 g) of the Cu_{12}/Al_2O_3 composite was loaded on different amounts of CN to determine the optimal CN content. The degradation of Rh B in the presence of $Cu_{12}/Al_2O_3/CN_v$ (y = 0, 0.7, 1.3, 2.0, and 2.7 wt %) is presented in Figure 7. As shown, the Cu₁₂/Al₂O₃ composite shows acceptable catalytic property for Rh B degradation, removing 34.6% Rh B in 100 min. Additionally, it is apparent that the introduction of CN leads to a corresponding enhancement of the degradation rate. With CN incorporated, part of Al₂O₃/Cu_{0.9} was stabilized on CN sheets by the formation of C–O–Cu bonds. Aqueous H_2O_2 are easily bonded to the surface of CN [34], providing larger chances for its contact with immobilized Cu⁺, which brought a significant improvement in catalytic property. Consequently, the degradation ratio within 100 min increased from 34.6% to 96.4% in the CN range of y = 0 to y = 1.3. However, excess CN incorporation from y = 1.3 to y = 2.7 did not further improve the degradation ratio. In the presence of adequate CN (y = 1.3), Cu₁₂/Al₂O₃ is fully loaded on the CN interlayers, resulting in the largest degradation ratio exhibited in Figure 7. When the amount of CN was largely in excess to Cu_{12}/Al_2O_3 , the mass ratio of Cu_{12}/Al_2O_3 in $Cu/Al_2O_3/CN$ decreased accordingly, thereby limiting the further improvement of catalytic property. Therefore, the optimal CN content was confirmed as y = 1.3 and $Cu_{12}/Al_2O_3/CN_{1.3}$ was selected as the typical composite for further studies. The Cu/Al₂O₃/CN composite in the following text refers to the Cu₁₂/Al₂O₃/CN_{1,3} composite unless addition descriptions were used.



Figure 7. [Rh B]/[Rh B]₀ as a function of time in the presence of 1 g/L Cu₁₂/Al₂O₃/CN_y composite (y = 0, 0.7, 1.3, 2.0, and 2.7 wt %). Reaction conditions: [Rh B]₀ = 20 mg/L, $[H_2O_2]_0$ = 10 mM, V = 100 mL, T = 25 °C, pH 4.9 (unadjusted).

2.2.3. Synergistic Effect

To verify the synergistic effect of Cu_{12}/Al_2O_3 and CN on the degradation of Rh B, four samples were prepared and their catalytic properties were compared in the same condition. The results are presented in Figure 8. It can be seen that both Cu_{12}/Al_2O_3 and CN show a weak catalytic property. Notably, CN exhibited a fine adsorption capacity for Rh B, which is attributed to its large specific surface area and multiple groups on the surface. By physically mixing Cu_{12}/Al_2O_3 and CN, the adsorption capacity for Rh B decreased but a higher degradation rate was observed. This may be attributed to the fact that immobilized copper species form an adsorption competition with Rh B on CN sheets, leading to a portion of adsorptive sites occupied by immobilized copper, which lowers the adsorption of Rh B but accelerates its degradation. In the $Cu/Al_2O_3/CN$ composite, much stronger bonds were formed between Cu and C–O–H as C–O–Cu, leading to a much lower adsorption capacity and a synergistically enhanced degradation property for Rh B.



Figure 8. [Rh B]/[Rh B]₀ as a function of time in the presence of 1 g/L different samples. Reaction conditions: [Rh B]₀ = 20 mg/L, $[H_2O_2]_0 = 10$ mM, V = 100 mL, T = 25 °C, pH 4.9 (unadjusted).

2.2.4. Effect of pH

The homogeneous Fenton reaction is strictly limited to acidic conditions (pH < 4), which limits its application in neutral and alkaline conditions [4,12]. Therefore, the effect of pH is an important criterion for the evaluation of catalytic performance of catalysts, especially the ones that involve potential dissolved metal ion species. To evaluate the practical applicability of the Cu/Al₂O₃/CN

composite in various pH conditions, a series of experiments were carried out ranging from pH 3.0 to pH 11.0. The initial pH value of 20 mg/L Rh B is 4.9, so this value (unadjusted pH) was used as a replacement of pH 5.0. The Rh B solutions were adjusted to predetermined pH values with the addition of 1 M HCl or NaOH. In all the experiments, the initial pH values underwent a slight increase with the extent of 1.0 ± 0.3 units, which could be attributed to the formation of OH⁻ in the H₂O₂ decomposition process. The degradation of Rh B is shown in Figure 9. It is evident that rapid degradations of Rh B were achieved at pH values higher than pKa of Rh B (3.7), and a lower pH value of 3.0 led to a remarkable repression. This is mainly attributed to the different existence forms of Rh B at different pH conditions. At pH values higher than 3.7, the carboxyl group of cationic RhB⁺ is deprotonated and the dye is transformed into zwitterionic RhB[±] with a higher hydrophilic character that is prone to reacting with HO radical [49]. Additionally, the scavenging effect of HO radical by H⁺ becomes stronger at low pH values [50,51], and H_2O_2 would become more stable under strong acid conditions to form oxonium $[H_3O_2]^+$, which inhibits its reaction with active species to generate HO radical in the presence of a large amount of H⁺ [48]. According to the Eh-pH diagram of Cu-H₂O [52,53], CuO and Cu₂O remain stable under alkaline conditions, which is beneficial for the catalytic degradation of Rh B. Despite the fact that more O_2 .⁻ radicals are produced in alkaline conditions that consumes HO· radical and H₂O₂, the degradation rates did not decline in higher pH conditions and even remarkably increased at pH 11.0, which may be attributed to the change of hydrophobic property of the dye and its interaction with negatively charged catalyst surface in strong alkaline conditions [49]. In summary, a remarkable degradation rate could be achieved in neutral and alkaline conditions, which is superior to classic Fenton reaction. Since there is no drastic difference in the removal of Rh B in the range of pH 4.9-9.0, Rh B solution with the unadjusted pH value of 4.9 was used for subsequent experiments.



Figure 9. [Rh B]/[Rh B]₀ as a function of time with the different pH conditions in the presence of 1 g/L of the Cu/Al₂O₃/CN composite. Reaction conditions: [Rh B]₀ = 20 mg/L, $[H_2O_2]_0 = 10$ mM, V = 100 mL, T = 25 °C.

2.2.5. Effect of H₂O₂ Concentration

Since H_2O_2 is the main source of HO_1 in the Fenton-like reaction, the effect of H_2O_2 on the degradation of Rh B in the presence of Cu/Al₂O₃/CN composite was investigated. As calculated by Equation (3), the stoichiometric amount of H_2O_2 to achieve total mineralization of 20 mg/L Rh B was calculated to be 3.0 mM, and the effect of H_2O_2 concentration was investigated in the range of 1–10 mM.

$$C_{28}H_{31}CIN_2O_3 + 73H_2O_2 \rightarrow 28CO_2 + 87H_2O + HCl + 2HNO_3$$
 (3)

The evolution of H_2O_2 with an initial concentration of 10 mM was taken as an example for kinetics analysis, the result of which is presented in Figure S1A. The residual concentration of H_2O_2 evolves linearly with reaction time, demonstrating the zero-order reaction kinetics during the reaction, which is attributed to the fact that H_2O_2 was present in large excess compared to Rh B. Only 11.9% of H_2O_2 was consumed in this experiment, which is far less significant than the Rh B decline that reached up to 96.4%. Therefore, more emphasis was stressed on the evolution of Rh B in this work. The normalized concentration of Rh B ([Rh B]/[Rh B]₀) and its logarithm are plotted as a function of the reaction time in Figure S1B,C for kinetic analysis. The plot of ln([Rh B]/[Rh B]_0) versus reaction time was linearly fitted with an R^2 of 0.9913, which demonstrated that the Rh B decline followed a pseudo first-order kinetics, as confirmed by some photocatalytic and Fenton-like systems [48,54]. The negative slope of the fitted curve represents the observed reaction rate constant k_{abs} , which was 5.14×10^{-4} s⁻¹ for this experiment. The decline of Rh B with different initial H₂O₂ concentrations was recorded in Figure 10 together with the corresponding reaction rate constants. As expected, the degradation rate increased with increasing H₂O₂ concentration. The initial H₂O₂ concentration of 10 mM led to an efficient degradation with a rate constant of $5.14 \times 10^{-4} \text{ s}^{-1}$, which is a satisfactory value for subsequent activity evaluations. Certainly, larger reaction rates could be achieved with higher H₂O₂ concentrations, but considering the fact that H_2O_2 also acts as an HO scavenger (as shown in Equation (4)) that lowers the efficiency of using H_2O_2 , exorbitant concentrations were not used [4]. The emphasis is not to seek for an 'optimal' H₂O₂ concentration, so [H₂O₂]₀ was fixed at 10 mM for other experiments in this work.

$$H_2O_2 + HO \rightarrow HO_2 + H_2O \tag{4}$$



Figure 10. [Rh B]/[Rh B]₀ as a function of time and the corresponding reaction rate constants (insert) with different H_2O_2 concentrations in the presence of 1 g/L of the Cu/Al₂O₃/CN composite at room temperature. Reaction conditions: [Rh B]₀ = 20 mg/L, V = 100 mL, pH 4.9 (unadjusted).

2.2.6. The Effect of the Catalyst Dose

The value of k_{obs} describes the rate that a reaction happens, and this value is dependent on the dose of the catalyst, which means a larger amount of the catalyst leads to a larger reaction rate constant. In this work, different amounts of catalyst (0.4–1.0 g/L) were used to catalyze Rh B degradation to check the effect of the catalyst dose on the reaction rate. Considering the facts that surface reaction dominates in heterogeneous systems and surface area plays a significant role, it would be unfair to use mass concentration for intersystem comparisons, which does not give consideration to the particle size and shape. Thus, in this work, the catalyst dose is represented by surface area concentration (SA/V), which is the product of mass concentration (g/L) and specific surface area (m²/g) and has a unit of m⁻¹. The concept of surface area concentration was first proposed by Matheson and Tratnyek as a general independent variable to correlate with the contaminants removal rate constants, as it incorporates most of the effects of grain size and shape [55], and now it is widely used in many heterogeneous systems

for kinetic study [35,56–59]. One example for the unit conversion is exhibited in Equation (5), with a mass concentration of 1 g/L and the specific surface area of 146.6 m^2/g for the Cu/Al₂O₃/CN composite.

$$\frac{SA}{V} = 1 g/L \times 146.6 m^2/g = 146.6 m^2/L = 146.6 m^2/(10^{-3} m^3) = 1.466 \times 10^5 m^2/m^3 = 1.466 \times 10^5 m^{-1} (5)$$

Figure 11A depicts $\ln([Rh B]/[Rh B]_0)$ as a function of time with different surface area concentrations (SA/V) of catalyst at 25 °C. All the $\ln([Rh B]/[Rh B]_0)$ plots were linearly fitted with reaction time, reconfirming the pseudo first-order kinetics in all cases. The key parameters of the fitted curves are listed in Table 2, and k_{obs} is plotted as a function of SA/V in Figure 11B. As shown, a linear fitted curve was achieved ($R^2 = 0.9948$), demonstrating that k_{obs} was linearly related to SA/V within certain limits, which is in accordance with previous reports [35,60,61]. The slope of this fitted line represents the specific reaction rate constant k_{SA} , which is the normalization of k_{obs} to SA/V (i.e., $k_{SA} = k_{obs}$ normalized to SA/V) [62]. The units for k_{obs} and SA/V are s⁻¹ and m⁻¹, respectively, so the unit for k_{SA} should be m·s⁻¹. The specific reaction rate constant k_{SA} could be regarded as a general descriptor of reactivity of heterogeneous catalysts [55,62], and is calculated to be (5.9 ± 0.07) × 10⁻⁹ m·s⁻¹ in this work. Judging from the k_{obs} data obtained in this work, much more rapid degradation of Rh B is achieved in the presence of the proposed catalyst compared with many other conventional ones like CuO nanowires, CuO nanoparticles, CuO nanoflowers, and commercial CuO [63,64].



Figure 11. (A) $\ln([Rh B]/[Rh B]_0)$ as a function of reaction time with different surface area concentrations (5.86–14.66 × 10⁴ m⁻¹). Reaction conditions: [Rh B]_0 = 20 mg/L, [H₂O₂]_0 = 10 mM, V = 100 mL, T = 25 °C, pH 4.9 (unadjusted). (B) k_{obs} as a function of SA/V. The k_{obs} values were obtained from Figure 11A.

Table 2. The key parameters of the fitted curves in Figure 11A.

Catalyst Dose (g/L)	SA/V (10 ⁵ m ⁻¹)	V k_{obs} Standard Deviation n^{-1}) (10^{-4} s^{-1}) (10^{-5} s^{-1})		R ² (%)
0.4	0.586	1.33	0.317	99.72
0.6	0.879	2.73	0.592	99.73
0.8	1.172	4.63	0.859	99.83
0.9	1.319	5.44	0.409	99.98
1.0	1.466	6.47	1.042	99.87

2.2.7. Activation Energy

Generally, the activation energy (E_a) of the reaction could be calculated by the Arrhenius equation: $k_{obs} = k_1 \cdot e^{-E_a/RT}$, which can be integrated as

$$ln(k_{obs}) = \frac{-E_a}{RT} + ln(k_1) \tag{6}$$

where E_a , R, and T represent the activation energy for the reaction, the gas constant, and the absolute temperature, respectively [35]. To estimate the activation energy of the reaction, a series of experiments were conducted at different temperatures from 20 to 40 °C. The ln([Rh B]/[Rh B]_0) was plotted as a function of time in Figure 12A to obtain k_{obs} at different temperatures. The key parameters of the fitted curves were listed in Table 3, and ln(k_{obs}) was plotted as a function of 1/T (K⁻¹) in Figure 12B to obtain E_a .



Figure 12. (**A**) $\ln([Rh B]/[Rh B]_0)$ as a function of reaction time at different temperatures (20–40 °C) in the presence of 1 g/L of the Cu/Al₂O₃/CN composite. Reaction conditions: [Rh B]₀ = 20 mg/L, $[H_2O_2]_0 = 10$ mM, V = 100 mL, pH 4.9 (unadjusted). (**B**) $\ln(k_{obs})$ as a function of 1/T. The k_{obs} values are obtained from Figure 12A.

Temperature (°C)	k_{obs} (10 ⁻³ s ⁻¹)	Standard Deviation (10^{-5} s^{-1})	R ² (%)
20	0.358	0.689	99.70
25	0.647	1.042	99.87
30	1.07	2.184	99.71
35	1.57	2.081	99.91
40	2.34	8.081	99.53

Table 3. The key parameters of the fitted curves in Figure 12A.

As can be seen from Figure 12A, with the increase of temperature, the degradation rate of Rh B increased significantly. In addition, all the ln([Rh B]/[Rh B]_0) plots were linearly fitted with reaction time, reconfirming the pseudo first-order kinetics at different temperatures. The ln(k_{obs}) is linearly fitted with 1/T with an R² of 0.9926 as shown in Figure 12B. According to the Arrhenius equation, the slope of this fitting curve equals to $-E_a/R$, and the activation energy E_a was calculated to be 71.0 kJ/mol. This value was lower than a series of other similar reactions, such as the degradation of Congo red by Fenton reagent (85.9 kJ/mol), the degradation of phenol by diamond supported gold nanoparticles (90.0 kJ/mol), and the iron oxide coating Fenton-like catalyst (96.9 kJ/mol) [65–67].

2.2.8. Recycling Experiments

In order to evaluate the stability of the Cu/Al₂O₃/CN composite, recycling experiments were performed. After each cycle, the suspension was filtered, washed, and dried to obtain the remaining composite. The recovered composite was subsequently subjected to a second cycle under the same reaction conditions. The leaching of copper species was measured at the end of each reaction cycle. The results are presented in Figure 13 and Table 4. Despite that the reaction rate constant decreased to some extent, efficient removal of Rh B was still achieved with a degradation ratio of 89.7% in 50 min after four cycles with a k_{obs} value of $0.77 \times 10^{-3} \text{ s}^{-1}$, indicating that the catalytic property of the composite was efficient and long-lasting. The slight decline in catalytic performance may be attributed

to the loss of Cu species in catalyst. The leaching of copper species increased from 0.16 mg/L in the first cycle to 0.55 mg/L in the fourth cycle, which shows an increasing trend. This could be regarded as a shortcoming of the proposed catalyst, and it also provides a direction for further improvement. It is remarkable that, despite the fact that copper leaching increases with cycle numbers, only 0.55 mg/L copper species were released to the solution even after four reaction cycles, i.e., copper leaching was remained at a very low level, which is far below the European standard of effluent (2 mg/L) [48].



Figure 13. Recycling performance of the Cu/Al₂O₃/CN composite for Rh B degradation in the presence of 1 g/L of the Cu/Al₂O₃/CN composite. Reaction conditions: [Rh B]₀ = 10 mg/L, [H₂O₂]₀ = 10 mM, V = 100 mL, 25 °C, pH 4.9 (unadjusted).

Recycling Cycles	1st	2nd	3rd	4th
Removal ratio	96.8%	95.5%	91.8%	89.7%
$k_{obs} (10^{-3} \text{ s}^{-1})$	1.37	1.12	0.83	0.77
Cu leaching (mg/L)	0.16	0.37	0.43	0.55

Table 4. *k*_{obs} and Cu leaching in the recycling experiments.

In some systems the dissolved metal species could form certain complexes that are able to catalyze the decomposition of H_2O_2 , thereby persistently generating HO· [36,68]. To determine the effect of dissolved copper species on Rh B degradation, the suspension containing Cu/Al₂O₃/CN composite was filtered at 40 min to remove catalyst particles, and the residual Rh B in the filtrate was monitored over time. As shown in Figure S2, negligible Rh B degradation was observed in the filtrate, indicating that the dissolved copper species had little effect on Rh B degradation, so only surface reaction dominates in the system containing the Cu/Al₂O₃/CN composite. With a tiny loss of copper species, the Cu/Al₂O₃/CN composite remains highly reactive and could efficiently catalyze the degradation of Rh B. The main features of the proposed Cu/Al₂O₃/CN composite and some other copper-based Fenton-like catalysts on Rh B degradation are listed in Table S1 [27,40,48,63,64,69–73]. The superiority of the Cu/Al₂O₃/CN composite in this work is supported by its high degradation rate constant, low copper leaching, and excellent applicability in neutral and alkaline conditions.

2.3. Catalytic Mechanism

In order to ascertain the Rh B degradation mechanism by the Cu/Al₂O₃/CN composite, both the reactive species and degradation products were identified in the Rh B degradation process. The reactive species were identified by a radical scavenger and ESR analysis, and HPLC-MS analysis was used to separate the degradation products and to identify each component. A tentative mechanism was proposed based on the abovementioned results.

2.3.1. Scavenging Experiments

Isopropanol (IPA) was employed as the HO· scavenger due to its rapid reaction rate with HO· $(1.9 \times 10^{-9} \text{ M}^{-1} \cdot \text{s}^{-1})$ [38]. As shown in Figure 14A, by increasing the IPA concentration from 10 to 100 mM, the scavenging effect became more significant, which indicates that HO· radical is the primary oxidation species in the catalytic reaction. This conclusion is also supported by the ESR experiment in which different radicals were trapped by DMPO to form different adducts that have different spectra [74,75]. As shown in Figure 14B, no ESR signal was observed in the absence of H₂O₂. With the addition of H₂O₂, a four-line ESR signal was observed with the relative intensity of 1:2:2:1, which is the characteristic spectrum of the DMPO-HO· adduct. This result reconfirmed the existence of HO· as main reactive species. Additionally, the characteristic spectrum of DMPO-O₂·⁻ with a relative intensity of 1:1:1:1 was also observed in Figure 14C. O₂·⁻ may arise from the reaction between HO· and H₂O₂ as shown in Equation (4). Notably, the intensity of the DMPO-HO· signal reached maximum at 10 min, while the intensity of DMPO-O₂·⁻ signal continuously increased over time, which supports that the observed O₂·⁻ radicals were generated from HO· radicals.



Figure 14. (**A**) [Rh B]/[Rh B]₀ as a function of time in the presence of different concentrations of IPA and N₂ bubbling. ESR spectra of (**B**) DMPO-HO· adducts in aqueous solution and (**C**) DMPO-O₂·⁻ adducts in methanol solution recorded with the Cu/Al₂O₃/CN composite.

Moreover, the effect of dissolved oxygen on Rh B degradation was checked by N₂ bubbling. The Rh B solution was purged by N₂ for 30 min before the reaction to dissipate dissolved oxygen. As shown in Figure 14A, the presence and absence of dissolved oxygen exerted no significant influences on Rh B degradation, indicating that oxygen was not the source of HO·, and the HO· radicals mainly arose from H₂O₂. In summary, HO· was identified as the major reactive species generated in the reaction, and the O₂·⁻ was generated via the reaction of HO· and H₂O₂.

2.3.2. HPLC-MS Analysis

Since HO· was confirmed as the main contributing reactive species, the $Cu/Al_2O_3/CN$ system exhibited a universal degradation peroperty for other organic pollutants as expected. As shown in Figure S3, the degradation ratios of methyl orange (MO), Rh B, and methylene blue (MB) in 100 min were 55.3%, 96.4%, and 93.1%, respectively. Particularly, the degradation products of Rh B were identified by HPLC-MS analysis.

The HPLC chromatograms of samples extracted at different reaction times were recorded in Figure S4. The two main peaks at 14.7 and 16.9 min corresponded to N-de-ethylated intermediate and Rh B, respectively, which were confirmed by MS identification [76]. It is clear that the peak of Rh B decreased with time, which was accompanied with the formation and subsequent elimination of other peaks. This implies that some transformation products were formed in the degradation process, and these produced compounds were further degraded into smaller products.

Based on the results above and previous reports [76–79], the possible degradation pathways of Rh B are proposed in Figure 15, which could be mainly summarized as N-de-ethylation, chromophore cleavage, ring opening and mineralization process. The MS spectra of each product were shown in Figure S5. A compound with a m/z value of 443 was identified to be Rh B, and the intermediates with m/z values of 415 and 387 were identified as N, N-diethyl-N'-ethyl rhodamine (DER), and N, N-diethyl rhodamine (DR), respectively. The intermediates with the m/z value of 387 could also be N-ethyl-N'-ethyl rhodamine (EER), which is the isomer of DR and has an ethyl on each side. These intermediates prove that in the first stage Rh B was degraded through a stepwise N-de-ethylation pathway, which finally forms an intermediate with an m/z value of 318 [79]. At the same time, the de-carboxylation process occurs and forms the product with a m/z value of 274 [80], and the central carbon of Rh B was also attacked by HO· radicals to form the hydroxylated product (m/z = 459) via the additive reaction [78]. There were two unidentified peaks with m/z values of 453 and 475, which could be regarded as the $[M + H]^+$ and $[M + Na]^+$ adducts of an unknown intermediate. To the best of our knowledge, no such pseudomolecule ion with m/z = 453 was previously reported in Rh B degradation, and we deemed that this compound might not exert a significant influence on the whole degradation pathway. Thus, it is marked unidentified in the present work. In the next stage, non-selective HOdirectly attacks the center carbon of these N-de-ethylated intermediates, leading to the cleavage of the conjugated xanthene structure [81]. The intermediates with m/z values of 340, 245, 230, and 223 were identified from this process [82–85]. After the chromophore cleavage process, the ring opening process occurs and forms smaller molecules. The ring opening products such as tricarballylic acid, 7-oxooctanoic acid, and propionic acid with m/z values of 177, 158, and 74 were identified [81]. In the final stage, these small molecules were possibly mineralized to CO₂, H₂O, NO₃⁻, NH₄⁺, etc.

Based on the results and analysis above, a tentative mechanism for the catalytic performance of the Cu/Al₂O₃/CN composite was proposed. Copper species were bonded to the Al₂O₃ framework, which facilitates the conversion of H₂O₂ to HO· by Fenton-like reaction and broadens the pH range for application. CN provides a large surface area and multiple functional groups to load Cu/Al₂O₃ composite by the formation of C–O–Cu bonds. In the presence of the Cu/Al₂O₃/CN composite, aqueous H₂O₂ could be easily adsorbed to the surface of CN, increasing its chance to contact with immobilized copper species to generate HO·. The catalytic process is surface predominant and the tiny leaching of copper species leads to an efficient and long-lasting catalytic property. O₂.⁻ is generated via the reaction of HO· and H₂O₂, and the highly reactive HO· attacks Rh B molecules, leading to the degradation of Rh B into smaller molecules.



Figure 15. Illustration of the proposed Rh B degradation pathways.

3. Experimental

3.1. Materials

The chemicals used in the present work included aluminum nitrate nonahydrate (Al(NO₃)₃·9H₂O, CAS[7784-27-2], 99%), copper(II) nitrate trihydrate (Cu(NO₃)₃·3H₂O, CAS[10031-43-3], 99%), D(+)– glucose monohydrate (C₆H₁₂O₆·H₂O, CAS[14431-43-7], 99%), urea (CH₄N₂O, CAS[57-13-6], 99%), Rhodamine B (Rh B, C₂₈H₃₁ClN₂O₃, CAS[81-88-9], 99.7%), methylene blue trihydrate (MB, C₁₆H₁₆ClN₃S·3H₂O, CAS[7720-79-3], 82%), methyl orange (MO, C₁₄H₁₄N₃NaO₃S, CAS[547-58-0], 98.5%), hydrogen peroxide (H₂O₂, CAS[7722-84-1], 30 wt %), potassium iodide (KI, CAS[7681-11-0], 99%), acetic acid (C₂H₄O₂, CAS[64-19-7], 99.5%), sodium acetate anhydrous (CH₃COONa, CAS[127-09-3], 99%), isopropanol (IPA, C₃H₈O, CAS[67-63-0], 99.7%) (Sinopharm, Beijing, China), and ammonium molybdate (di) ((NH₄)₂Mo₂O₇, CAS[27546-07-2], Mo 56.5%, Macklin, Shanghai, China). All chemicals were used without further purification. All the solutions were prepared in deionized water.

3.2. Preparation of Composites

3.2.1. Preparation of Cu/Al₂O₃

Cu/Al₂O₃ composite was prepared via a hydrothermal method followed by a calcination process [40]. Typically, 7.5 g of Al(NO₃)₃·9H₂O, 5.0 g of C₆H₁₂O₆, 0.9 g of Cu(NO₃)₂·3H₂O, and 60 mL of ultrapure water were added to a 100 mL breaker, and stirred at 25 °C for 1 h. The solution was transferred into a 100 mL Teflon-lined autoclave, then heated to 180 °C and kept for 20 h in an oven. After suction filtering, and water washing to neutral, the obtained product was added to an alumina crucible with a cover and then heated to 550 °C with a ramping rate of 5 °C/min in a muffle furnace and hold at 550 °C for 4 h. After naturally cooling down to room temperature, the product Cu/Al₂O₃ was obtained, and labeled as Cu₁₂/Al₂O₃, where 12 represents the initial mass ratio of Cu(NO₃)₂·3H₂O to Al(NO₃)₃·9H₂O in percentage. Following the same procedure, a series of Cu_x/Al₂O₃ composites (x = 4, 7, 9, 12, and 15 wt %) were prepared in order to obtain the optimal Cu content.

3.2.2. Preparation of g-C₃N₄

Pure g-C₃N₄ was prepared following the thermal polymerization process reported in a previous study [35]. Typically, 50 g of urea was added to an alumina crucible with a cover and then heated to 550 °C with a ramping rate of 5 °C/min in a muffle furnace and hold at 550 °C for 3 h. After naturally cooling down to room temperature, the product g-C₃N₄ was obtained, and labeled as CN.

3.2.3. Preparation of Cu/Al₂O₃/CN

The Cu/Al₂O₃/CN composite was prepared using the samples obtained in Sections 3.2.1 and 3.2.2. Typically, 0.1 g of the Cu₁₂/Al₂O₃ composite and 0.1 g of CN were immersed in 100 mL ultrapure water. The suspension was dispersed by ultrasound for 30 min. After drying at 80 °C and grinding to powder, the product Cu/Al₂O₃/CN composite was obtained, and labeled as Cu₁₂/Al₂O₃/CN_{1.3}, where 1.3 represents the initial mass ratio of CN to Al(NO₃)₃·9H₂O in percentage. Additionally, a series of Cu₁₂/Al₂O₃/CN_y composites (y = 0.7, 1.3, 2.0, and 2.7 wt %) were prepared by the same synthetic process to obtain the optimal CN content.

3.3. Characterization of Prepared Composites

The Fourier transform infrared (FT-IR) spectra of prepared samples were recorded by a Nicolet iS5 (Thermo Fisher Scientific, Waltham, MA., USA) FT-IR spectrometer with KBr pellets to confirm the functional groups of materials.

X-ray diffraction (XRD) patterns were recorded with D8 advance (Bruker, Karlsruhe, Germany) diffractometer using Bragg–Brentano geometry over the 2 θ range of 10–70° with a Cu K α irradiation (λ = 1.54 Å) to obtain the crystal structure of materials.

The morphology of the synthesized samples was visualized by a JET-2100F (JEOL, Akishima, Japan) transmission electron microscope (TEM).

X-ray photoelectron spectroscopy (XPS) data was recorded at 100 W power with a 20 eV pass energy on an ESCALAB 250Xi instrument (Thermo Fisher Scientific, Waltham, MA., USA).

The Brunauer–Emmett–Teller (B.E.T) method via isothermal adsorption and desorption of high purity nitrogen using a TriStar II 3020 (Micromeritics, Norcross, GA., USA) instrument was used to determine the specific surface area of synthesized samples.

The degradation intermediates were identified by a high performance liquid chromatography-mass spectrometry (HPLC-MS, thermo TSQ Quantum Ultra, Waltham, MA., USA). The samples were chromatographically separated by a 2.1 mm × 150 mm XB C18 column with a particle size of 3 μ m (Welch, Shanghai, China) with acetonitrile/0.1% formic acid (8:92, *v*/*v*) as the mobile phase The flow rate was 0.3 mL/min and the injection volume was 20 μ L. The eluent was detected by a diode array detector at the wavelength of 555 nm. The total ion current was recorded by quadrupole in a positive mode with electrospray ionization as ion source.

The concentration of the dissolved copper species was measured by a Prodigy 7 (Teledyne Leeman Labs, Hudson, NH., USA) inductively coupled plasma-optical emission spectrometer (ICP-OES).

The electron spin resonance (ESR) signals of radicals spin-trapped by 5,5-dimethyl-pyrroline-N-oxide (DMPO) were detected by a Bruker/A300 spectrometer (Bruker, Karlsruhe, Germany) with or without the addition of H_2O_2 in different air saturated methanol/aqueous dispersions.

The concentration of H_2O_2 and Rh B was measured by the UV-5500PC UV-visible spectrophotometer (METASH, Shanghai, China) and V-5600 spectrophotometer (METASH, Shanghai, China). The samples were weighted using a ME204E microbalance (Mettler Toledo, Shanghai, China). The pH of the solution was measured by Starter 2100 pH meter (Ohaus, Shanghai, China) with an accuracy of \pm 0.01 pH units.

3.4. Catalytic Experiments

Rh B was selected to evaluate the catalytic performance of the synthesized samples. All experiments were performed in dark conditions. Typically, 0.1 g of sample was placed into 100 mL of 20 mg/L Rh B solution, and then the suspension was stirred continuously for 1 h prior to the addition of H_2O_2 , in order to achieve Rh B adsorption/desorption equilibrium. Afterwards, predetermined amount of H_2O_2 was added in the suspension under constant stirring to trigger the reaction. At given time intervals, 4 mL samples were collected with a syringe and filtered using a Millipore filter (220 nm, Tianjin, China). The concentrations of Rh B and H_2O_2 in the filtrate were measured and plotted as a function of time.

The concentrations of Rh B and H_2O_2 in solutions were measured using a UV-visible spectrophotometer due to its convenience and easy operation. The produced intermediates may interfere the measurements, but the experimental error in the determination of Rh B and H_2O_2 concentration was less than 2%, which is acceptable for subsequent discussions. Generally, the absorbance of Rh B was measured at 555 nm in which Rh B had the maximum absorption. The concentration of H_2O_2 was determined by the Ghormley triiodide method reported in previous work [68]. The I⁻ could be oxidized by H_2O_2 to form I_3^- in the presence of catalyst (NH₄)₂Mo₂O₇ (ADM). The I_3^- has the maximum absorption peak at the wavelength of 350 nm, thus the standard curve of the absorbance of I_3^- as a function of H_2O_2 concentration can be obtained.

Radical scavenger experiments were carried out to investigate the reactive oxygen species in the system. The scavenger IPA was added into the suspension after the adsorption/desorption equilibrium prior to the addition of H_2O_2 . Additionally, Rh B solution was purged with N_2 prior to the addition of composite to exclude O_2 .

4. Conclusions

An efficient Fenton-like Cu/Al₂O₃/CN composite was proposed in this work. The characterizations show that Cu species were immobilized on the Al₂O₃ framework in the form of Cu²⁺ and Cu⁺, and the introduction of CN increases its specific surface area and adsorption capacity for Rh B. The Cu/Al₂O₃/CN composite showed an excellent catalytic performance in a wide range of pH (4.9–11.0). The specific reaction rate constant of Rh B degradation was calculated as $(5.9 \pm 0.07) \times 10^{-9} \text{ m} \text{ s}^{-1}$, and the activation energy was calculated to be 71.0 kJ/mol. The recycling experiment demonstrated its durability for Rh B removal and proved that the degradation reaction was surface doninated, with a negligible leaching of copper species in solution. HO· and O₂·⁻ were both major reactive oxygen species generated in the reaction, and HO· was mainly responsible for Rh B degradation, which involves N-de-ethylation, hydroxylation, de-carboxylation, chromophore cleavage, ring opening, and the mineralization process. This work shows that Cu/Al₂O₃/CN composite is a promising Fenton-like catalyst with high activity and stability for the treatment of water pollution.

Supplementary Materials: The following are available online at http://www.mdpi.com/2073-4344/10/3/317/s1, Figure S1: (A) [H₂O₂], (B) [Rh B]/[Rh B]₀, and (C) ln ([Rh B]/ [Rh B]₀) as a function of time in the presence of 1 g/L of the Cu/Al₂O₃/CN composite at room temperature. Reaction conditions: [Rh B]₀ = 20 mg/L, [H₂O₂]₀ = 10 mM, V = 100 mL, pH 4.9 (unadjusted); Figure S2: [Rh B]/[Rh B]₀ as a function of time in nonfiltered Cu/Al₂O₃/CN suspension and filtrates obtained at selected time intervals. Reaction conditions: [catalyst] = 1 g/L, [Rh B]₀ = 20 mg/L, [H₂O₂]₀ = 10 mM, V = 100 mL, 25 °C, pH 4.9 (unadjusted); Figure S3: C/C₀ as a function of time with different organic pollutants in the presence of 1 g/L of the Cu/Al₂O₃/CN composite. Reaction conditions: [dye] = 20 mg/L, [H₂O₂]₀ = 10 mM, V = 100 mL, 25 °C, pH 4.9 (unadjusted); Figure S4: HPLC chromatograms of samples extracted at different reaction times. Reaction conditions: [catalyst] = 1 g/L, [dye] = 20 mg/L, [H₂O₂]₀ = 10 mM, V = 100 mL, 25 °C, pH 4.9 (unadjusted); Figure S4: HPLC chromatograms of samples extracted at different reaction times. Reaction conditions: [catalyst] = 1 g/L, [dye] = 20 mg/L, [H₂O₂]₀ = 10 mM, V = 100 mL, 25 °C, pH 4.9 (unadjusted); Figure S4: HPLC chromatograms of samples extracted at different reaction times. Reaction conditions: [catalyst] = 1 g/L, [dye] = 20 mg/L, [H₂O₂]₀ = 10 mM, V = 100 mL, 25 °C, pH 4.9 (unadjusted); Figure S4: HPLC chromatograms of samples extracted at 60 min in Rh B degradation.; Table S1: Comparison of the catalytic activities of the Cu/Al₂O₃/CN composite with other copper-based Fenton-like catalysts.

Author Contributions: M.Y. conceived the experiments; C.Z. and Z.L. designed and performed the experiments; L.F. and Y.G. analyzed the data; Y.F. contributed analysis tools; C.Z., Z.L. and M.Y. wrote the paper. All authors have read and agreed to the published version of the manuscript.

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Article Effect of Zirconia on Hydrothermally Synthesized Co₃O₄/TiO₂ Catalyst for NO_x Reduction from Engine Emissions

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Abstract: Effect of zirconia on the 6 wt.% Co_3O_4/TiO_2 catalyst for NO_x reduction is investigated in this paper. Co_3O_4/TiO_2 catalyst was prepared by using hydrothermal method and then was promoted with zirconia by impregnation to get 8% wt. ZrO_2 - Co_3O_4/TiO_2 catalyst. Catalysts were characterized by using XRD, SEM, and TGA. Catalysts real time activity was tested by coating them on stainless steel wire meshes, containing them in a mild steel shell and mounting them at the exhaust tailpipe of a 72 cm³ motorcycle engine. Zirconia promoted catalyst showed higher conversion efficiency of NO_X than the simple Co_3O_4/TiO_2 catalyst due to small crystalline size, fouling inhibition and thermal stability.

Keywords: Co₃O₄/TiO₂ catalyst; ZrO₂-Co₃O₄/TiO₂ catalyst; NO_X reduction; CO and HC oxidation

1. Introduction

Pollutant gas emission from automotive vehicles is one of the biggest contributors to air pollution in most cities of the world [1–4]. Annually, 4.2 million people die due to the ambient air pollution throughout the world [5,6]. Since the introduction of the clean air act in 1970, a number of efforts have been made to reduce the engine exhaust pollution. Engine exhaust emissions contain three major pollutants—carbon monoxide (CO), nitrogen oxides (NOx), and hydrocarbons (HCs)—which need to be tackled [7]. Different methods, such as thermal reactors, diesel particulate filters (DPFs), selective catalytic reduction SCR, changes in engine design, oxygenated fuels, and catalytic converters had been adopted to truncate this concern to the minimum level [4,8]. Gasoline blended with 3% oxygen by weight reduces 30% of CO emissions but NO_X concentration increases which can swell ozone problems [9]. Conventionally catalytic converters employ Pt, Pd, and Rh as catalysts with innovations, such as the introduction of CeO_2 or CeO_2 -ZrO₂ composite for managing the time lag from switching between lean to rich condition or vice versa [10]. These metals are emitted out due to high temperatures, mechanical friction, stresses, and chemical reactions to the roadside soils which cause disruption in plant growth [11]. Due to high solubility of PGEs with various compounds, the presence of these metals in the environment can cause many health threats, such as nausea, tumors, sensitization, pregnancy loss and other human health issues [12,13]. Moreover, due to thermal aging, Rh₂O₃ reacts with Al₂O₃ to form an inactive compound, Pt sintering occurs at 700 °C and at high temperature of 900 °C sintering of γ -AL₂O₃ occurs and it transforms to α -AL₂O₃ which has less surface area [14]. These metals are rarest of the elements present on the earth ranging from 5 to 15 ppm in ores mines and from 0.022 ppb for Ir to 0.52 ppb for Pd [15,16]. The automotive industry consumed 37% of platinum, 72% of palladium and 79% of rhodium in 2013 [15]. Due to the scarcity of these

metals, increasing prices and health hazards, it is a requirement to find a replacement which is less rare, less expensive, and competitively active. Over time, many pure metals and metal oxides were tested as alternatives to these PGEs for redox reactions in catalytic converters i.e., Au, Ni, Cu, MnO₂, CoO, Co_3O_4 and CuO [15,17–19]. Co_3O_4 over different supports was investigated as a catalyst for oxidation of CO and HC in exhaust emission control system and demonstrated low temperature activity [20,21]. Wang et al. [22] experimented by preparing a cobalt oxide catalyst with three different supports, such as TiO₂, Al₂O₃ and SiO₂ by using the incipient wetness impregnation method. He expressed that the type of cobalt oxide and type of support used had a great effect on the activity and the surface area. He concluded that CoO_x/TiO₂ showed very significant results towards CO conversion. Hu et al. [23] performed the oxidation of CO on cobalt oxides nanobelts and nanocubes. He revealed that the shape Co_3O_4 had a great effect on the catalytic activity towards CO as nanobelts depicted more conversion efficiency than nanocubes. Jia et al. [24] prepared Co_3O_4 -SiO₂ nanocomposite as catalyst with high surface area for oxidation of CO. He observed that the catalyst showed activity at a very low temperature of even -76 °C. He concluded that there was some adsorption of water molecules on the exterior of catalyst which caused abnormal behavior in the activity of catalyst. Xie et al. [25] reported that Co₃O₄ showed high activity for carbon monoxide conversion surprisingly at temperature of -77 °C and remained stable under the moist conditions. He observed that under the stoichiometric conditions, conversion efficiency of Co₃O₄ catalyst was 96% at temperature of 200 °C but the conversion efficiency decreased at temperature of 150 °C to 40% due the presence of moisture content.

On the other hand, due to high thermal stability, high surface area, and highly resistant towards poisoning TiO_2 was widely used for catalyst support as an alternate to alumina [26,27]. Titanium dioxide exists in three crystalline phas.

es that are anatase, brookite, and rutile however anatase and rutile play a role in applications of titanium dioxide. Anatase is less dense and less stable than rutile at ambient temperature and pressure conditions [28]. Zhu et al. [29] studied the effect of TiO₂ structure on catalytic properties of copper oxide supported by anatase or rutile for NO reduction by CO reaction. He concluded that copper oxide supported by rutile TiO₂ was more active than supported by anatase TiO₂. Presently, commercially available three way catalysis systems have ceria or ceria-zirconia along with alumina and precious metal to increase the conversion efficiency. The incorporation of ceria-zirconia mixture into automotive catalysts was to enhance the oxygen storage capacity (OSC) for the redox reactions by releasing/storing oxygen depending upon A/F ratio and other factors [30]. Extensive studies were carried on ceria, zirconia, and a mixture of both as OSC is very important for the increment of CO oxidation as well as the reduction of NOx at the same time. Transition metal oxides showed a great potential to have oxygen vacancies on the surface like TiO_2 , ZrO_2 and V_2O_5 [31]. Yu et al. [32] studied the adsorption and oxidation of CO by O₂ at the surface of rutile TiO₂. Li et al. [33] calculated the oxygen vacancies on anatase and rutile TiO₂ and concluded that both phases have oxygen vacancies but in case of rutile more stable oxygen vacancy was found on the surface rather on subsurface. In the case of zirconia, oxygen vacancies are produced by doping but undoped zirconia also contains bulk concentration of oxygen vacancies [34,35]. In this work, we are going to present the effect of zirconia on hydrothermally produced Co₃O₄/TiO₂ catalyst for petrol engine emissions control system with Co_3O_4 being our oxidation catalyst and TiO_2 as reduction catalyst. Zirconia was impregnated on a catalyst and a new 8% wt. ZrO₂-Co₃O₄/TiO₂ was prepared. Both catalysts were coated on round wire meshes then placed in a mild steel clam shell and mounted on the exhaust of a motorcycle. The zirconia promoted catalyst showed more qualities of reductive catalyst as less NO_x were seen after the reaction inside the catalytic converter.

2. Results and Discussions

2.1. X-ray Diffraction (XRD)

All phases of the prepared catalyst were identified by using JCPDS powder diffraction file. In XRD analysis of Co_3O_4/TiO_2 , the phase of titania identified was rutile and no peaks of other phases of titania were noticed. XRD pattern of Co_3O_4/TiO_2 catalyst is shown in Figure 1a. TiO₂ showed peaks at 2 theta values of 27.45°, 36.06°, 41.22°, 44.04°, 54.31°, 56.6°, 62.7°, 64.03°, 69.008° and 69.78°. Diffraction peaks of rutile titania are in complete match with JCPDS card no. 21-1276. Crystallite size of titania nanoparticles was calculated by Sherrer equation which was 65 nm on average. TiO₂ exhibited tetragonal crystal structure with the cell parameters as a = 4.593 Å, b = 4.593 Å and c = 2.959 Å. In XRD analysis of the catalyst the cubic crystal structure of cobalt oxide Co_3O_4 was identified with the cell parameters a = 8.084 Å, b = 8.084 Å and c = 8.084 Å. The pattern in Figure 1a shows strong peaks at the 2 theta values of 19° , 31.2° , 36.84° , 44.85° , 55.6° and 65.2° for Co_3O_4 matching with JCPDS card no. 42-1467. Crystallite size of cobalt oxide was determined by using Sherrer equation which came out to be 26 nm. No other peaks of Co(OH)₂ or any impurity were observed. XRD pattern of 8 wt.% ZrO₂-Co₃O₄/TiO₂ is shown in Figure 1b. Co₃O₄, TiO₂ and ZrO₂ were detected successfully. Peaks of monoclinic crystal structure of zirconia (ZrO₂) were observed at 24.04°, 24.44°, 28.17°, 31.46°, 34.15°, 34.38°, 49.26° and 50.55°. Crystallite size of zirconia was calculated as 32 nm on average. In 8 wt% ZrO₂-Co₃O₄/TiO₂ crystallite size of TiO₂ and Co₃O₄ calculated by Sherrer equation decreased to 58 nm and 22 nm respectively as compared to Co₃O₄/TiO₂.



Figure 1. XRD patterns of catalysts (a) Co₃O₄/TiO₂ (b) 8% wt. ZrO₂-Co₃O₄/TiO₂.

2.2. Scanning Electron Microscopy (SEM)

SEM images of the samples are shown in Figure 2 with different scaling. It was observed that the particles of titania and both catalysts were spherical in shape and size, were in range of 50–170 nm. SEM images of titania nanoparticles and both catalysts are shown in Figure 2a–c. It was observed size and the shape of the particles were uniform without many variations. Titania nanoparticles image show that boundaries of particles are clear and well defined but after loading of Co_3O_4 clear structure starts diminishing. After addition of zirconia that smooth and well defined structure lessens very much. SEM images of a coated wire pieces before and after testing are shown in Figure 2d–g. Slight removal of the coated material was observed after testing and also there was some agglomeration of coated material after testing. This ascertains that coating technique needs to be upgraded. EDS (Energy-dispersive X-ray spectroscopy) patterns are shown in Figure 3. It was noticed in EDS analysis that there was no deposition of emission particles on coated wires with the catalysts after repetitive testing at varying conditions.



Figure 2. SEM images of (a) TiO_2 nanoparticles (b) Co_3O_4/TiO_2 (c) 8 wt.% ZrO_2 - Co_3O_4/TiO_2 (d) Bef test 8 wt.% ZrO_2 - Co_3O_4/TiO_2 coated wire (e) Aft test 8 wt.%. ZrO_2 - Co_3O_4/TiO_2 coated wire (f) Bef test 8 wt.% ZrO_2 - Co_3O_4/TiO_2 coated wire (g) Aft test 8 wt.% ZrO_2 - Co_3O_4/TiO_2 .



Figure 3. EDS patterns of (a) Uncoated wire (b) Co_3O_4/TiO_2 coated wire before test (c) 8 wt.% ZrO_2 - Co_3O_4/TiO_2 coated wire before test (d) Co_3O_4/TiO_2 coated wire after test (e) 8 wt.% ZrO_2 - Co_3O_4/TiO_2 coated wire after test.

2.3. Thermogravimetric Analysis (TGA)

Cyclic heating and cooling technique was carried out to find out the oxygen storage capacity (δ) of both catalysts as shown in Figure 4a,b. During real driving conditions when vehicle is accelerated, AFR fluctuates due to which NO_X emissions are increased. CeO₂ was used in conventional three way catalysts to overcome this fluctuating AFR issue as it has the ability to store/release oxygen during varying conditions. Zirconia with different mole fractions was added to give thermal stability and decrease sintering of CeO₂ [36]. In our case, we added 8 wt.% ZrO₂ in Co₃O₄/TiO₂ catalyst and investigated its effects on thermal stability and oxygen storage capacity of the catalyst. For this purpose, catalysts powders were put in the furnace of a TG analyzer turn by turn. Powders were heated from room temperature to 800 °C in the presence of air stream to provide atmospheric conditions with flow rate of 10 mL/min. Weight loss in the first heating cycle was calculated as 6.84% for Co₃O₄/TiO₂ catalyst and 7.22% for 8 wt.% ZrO₂-Co₃O₄/TiO₂ which corresponds to both loss of water and also oxygen molecules [37,38]. From 28 °C to 105 °C zirconia promoted catalyst lost 2.21% of weight while other catalyst experienced 0.51% of weight loss which indicates loss of moisture. After that, zirconia

promoted catalyst exhibited more stability and lost 5.03% weight compared to 6.67% of simple catalyst. Then, they were cooled to 169 °C in the presence of an air stream with same flow during which zirconia promoted catalyst gathered 1.87% and simple catalyst gathered 3.37% of weight which corresponds to oxygen gaining of both catalysts [36]. The OSC value (δ) of zirconia promoted catalyst was calculated to be 1.4 µmol/g and for simple catalyst it was 1.6 µmol/g which are quite significant values as per literature [39]. The zirconia promoted catalyst displayed less oxygen storage capacity which is due to crystal structural defects; the introduction of Zr into a Co framework on a corresponding level would compensate the volume increase related to Co^{2+} reduction. This would decrease the influence of valence change; shorten the Co-O bond length in the ZrO₂-Co₃O₄/TiO₂ as a result it detains some of oxygen sites on cobalt oxide and titania [40]. There was 3.54% weight loss observed for simple catalyst in second heating cycle while zirconia promoted catalyst lost 2.2% weight as shown in Figure 4a,b which corresponds to the oxygen releasing capacity of the catalysts in atmospheric conditions. Results of TGA show that with addition of zirconia, which is highly stable molecule, catalyst gained thermal stability but oxygen gaining and releasing ability decreased which also affected the catalytic activity that is discussed in later part of the paper. A decrease in crystalline size was observed by addition of ZrO₂ on Co₃O₄/TiO₂, which may attribute to increase in thermal stability of ZrO₂-Co₃O₄/TiO₂. Hofmann et al. [31] studied oxygen vacancies on rutile TiO_2 (both active catalyst and support) and reported that it has significant ability to store and release oxygen. After addition of the zirconia in Co_3O_4/TiO_2 catalyst, it captures some of oxygen vacant sites of titania which results in a lower OSC value.



Figure 4. Plots for measurements of oxygen storage capacity (OSC) of (a) Co_3O_4/TiO_2 and (b) 8 wt.% ZrO_2 - Co_3O_4/TiO_2 .

2.4. Brunauer-Emmett-Teller (BET)

The surface area and pore volume for the Co_3O_4/TiO_2 catalyst were found to be 24.3 m²/g and 0.14 cm³/g, respectively, while the zirconia promoted catalyst surface area and pore volume were found to be 13.09 m²/g and 0.071 cm³/g, respectively. Reason behind decrement in surface area of zirconia promoted catalyst is that ZrO_2 which has higher density (5.68 gcm⁻³) than titania, exhibits low surface area which is because of defects in crystal structural. This would decrease the influence of valence change; shorten the Co-O bond length in the ZrO_2 -Co₃O₄/TiO₂, as a result it detains some of oxygen sites on cobalt oxide and titania may results in low surface area and low pore volume [41,42]. The N₂ adsoption-desorption isotherm of both catalysts is shown in Figure 5a,b.



 $Figure 5. \ Nitrogen adsorption-desorption is otherm of (a) Co_3O_4/TiO_2 \ catalyst (b) \\ 8 \ wt. \% \ ZrO_2-Co_3O_4/TiO_2 \ catalyst.$

2.5. Catalytic Activity

RPMs of the engine shaft increased manually from 1500 to 6000 at intervals of 1500. Temperature of the exhaust gases also increased giving values 121 °C, 257 °C, 284 °C, and 391 °C with respect to RPMs of 1500, 3000, 4500, and 6000. In the case of NO_X the maximum conversion efficiency was noticed at 6000 RPMs as shown in Figure 6 which was 71.4% for simple catalyst but zirconia promoted catalyst showed higher efficiency of 75% for NO_X reduction shown in Figure 7. The highest efficiency of zirconia promoted catalyst is due to absence of moisture content at high temperature, the poisoning of catalyst was diminished when temperature reach above 300 °C thus it provides more sites for reaction. Furthermore, NO_X amount in the gas stream was maximum in its range. While lambda value at this point was 1.323 which showed that the air to fuel ratio (AFR) inside the combustion chamber of motorcycle engine was 19.5:1 and the air fuel mixture was lean. Shah et al. [40] coated wire meshes with zirconia and reported that it reduced HCs in exhaust stream by 35%. In the case of CO, maximum conversion efficiency was noticed at 1500 RPMs which was 78.15% for simple catalyst shown in Figure 8 and slightly higher 78.65% for zirconia promoted catalyst as shown in Figure 9. CO oxidation is strongly dependent on morphology of catalysts and oxidation state of transition metals in catalyst. The oxidation state of Co in the prepared Co₃O₄/TiO₂ and ZrO₂-Co₃O₄/TiO₂ was expected to be +2 in both cases with tetrahedral and octahedral geometries respectively. Despite similar Co coordination environments, the catalytic activity and selectivity was considerably improved by the Zr modification of the Co_3O_4/TiO_2 . This was endorsed to the change in oxygen donor ability and Co–O bond strength of the ≡TiO–Zr–O sites of Co–Zr/TiO₂ compared with the ≡TiO– ligands in Co/TiO₂. The tuning of the support TiO₂ oxygen donation ability by use of an anchoring site (e.g., \equiv TiO-Zr-O⁻) can be used to alter both rate and selectivity of conversion efficiency i.e., (NO_x, CO, HC). Possibly Co^{2+} active sites prefer to associate with $\equiv TiO - Zr - O^{-}$ sites as compare to $\equiv TiO - [42,43]$ as shown in below Figure 10. Furthermore, zirconia promoted catalyst efficiency is attributed by the presence of zirconia that effect on redox properties through dispersion of active phases which oxidize CO more efficiently. Moreover, at this point CO amount in exhaust gas was maximum in its range which decreases drastically with temperature increment from 1500 to 6000 RPMs. The inlet lambda value was noticed to be same 1.323 thus the AFR value of 19.5:1. Higher AFR indicating that air fuel mixture is lean thus oxidation reactions are more favorable. The outlet lambda value after the catalyst was recorded as 6.02 which mean that catalyst is working properly.







Figure 7. Conversion of NO_{χ} with 8 wt.% ZrO₂-Co₃O₄/TiO₂.



Figure 8. Conversion of CO with Co_3O_4/TiO_2 .



Figure 9. Conversion of CO with 8 wt.% ZrO₂-Co₃O₄/TiO₂.



Figure 10. Graphical diagram of 8 wt.% ZrO₂-Co₃O₄/TiO₂ and Co₃O₄/TiO₂.

Furthermore, the type of basic sites together with whole basicity and whole acidity of the ZrO_2 -based catalysts also effect the HC, CO, and NO_x conversion on active sites. The Lewis basic sites of ZrO_2 consist of coordinately unsaturated O^{-2} species and the Lewis acidic sites is Zr^{4+} species [42–46]. Overall reactions on the surface of catalysts were given below in Figure 11:



Figure 11. Conversions of NO_x, CO, HC to N₂, CO₂, and H₂O on 8 wt.% ZrO_2 -Co₃O₄/TiO₂.

Amin et al. [39] developed a copper-based catalytic converter and reported that it converted HCs by 33% and CO by 66% at full load. Patel et al. [47] made a copper-based catalytic converter and reported conversion efficiencies as 50–62% for CO, 20–27% for NO_X and 35–40% HCs. Makwana et al. fabricated a catalytic converter by coating nickel on steel wire meshes and reported efficiencies as 40% and 35% for HCs, and CO, respectively. Hydrocarbons conversion efficiency was noticed as

82.5% for simple catalyst at 1500 RPMs as shown in Figure 12 but in case of promoted catalyst HC conversion decreased and gave highest value of 81% shown in Figure 13. The decrease in efficiency is due to presence of moisture content that absorb very easily on the Lewis acid site of the catalyst at a lower temperature i.e., 121 °C, As a result it lowers the vacancies of oxygen for oxidation on zirconia promoted Co_3O_4 . Furthermore, the zirconia promoted catalyst displayed less oxygen storage capacity which is due to zirconia captures some of oxygen sites on cobalt oxide and titania. Enhanced catalytic performance of ZrO₂ promoted catalyst may be attributed to small crystalline size (calculated by the sSherrer equation). As crystalline small decrease, the no of catalytic active sites increases accordingly. Therefore, it leads to the better conversion efficiency of the reactants towards product formation. Also due to increase in thermal stability of ZrO₂ promoted catalyst at higher temperatures, catalyst becomes more resistance towards sintering process which could lead to better catalytic performance. ZrO₂ is also reported to prevent deactivation of catalyst in catalytic converters, which is caused by fouling process due to incomplete combustion of fuel. The catalytic activity results are summarized in Tables 1–3.

Table 1. Real time conversion results of NO_X with both catalysts.

RPM	NO_{χ} (ppm) for Co_3O_4/TiO_2		-	NO_X (ppm) for 8 wt.% ZrO_2 - Co_3O_4 /Ti O_2		-
-	Before	After	Efficiency (%)	Before	After	Efficiency (%)
1500	42	16	61.9	49	22	55.1
3000	70	24	65.7	54	18	66.6
4500	87	27	69.8	65	19	70.7
6000	131	38	71	132	33	75

CO (% vol.) for 8 wt.% **RPM** CO (% vol.) for Co₃O₄/TiO₂ ZrO2- Co3O4/TiO2 -Before After Efficiency (%) Before After Efficiency (%) 4.99 3.42 0.73 1500 1.09 78.1 78.6 4.24 73.3 2.82 0.72 74.8 3000 1.13 4500 1.55 0.53 65.8 2.47 0.79 68 6000 1.51 0.63 58.2 1.2 0.49 59.1

Table 2. Real time conversion results of CO with both catalysts.

Table 3. Real time conversion results of HCs with both catalysts.

RPM	HCs (ppm) for Co ₃ O ₄ /TiO ₂		-	HCs (ppm) for Co ₃ O ₄	-	
-	Before	After	Efficiency (%)	Before	After	Efficiency (%)
1500	414	72	82.6	418	78	81.3
3000	198	45	77.2	237	56	76.3
4500	124	38	69.3	128	42	67.1
6000	39	15	61.5	40	14	65

With increasing RPMs, the temperature also increased and the ppm value of hydrocarbons production inside combustion chamber decreased. Thus, confirming that amount of CO, NOx and HCs producing inside combustion chamber heavily depends on the temperature inside combustion chamber.

After addition of zirconia in catalyst, there was a negative effect on oxidation reactions as it suppressed the oxidation reaction of HCs. HC conversion efficiency was less in ZrO_2 promoted catalyst compared to the other one. This is because zirconia captures some of the active sites of Co_3O_4 which is our oxidation catalyst. Moreover, mostly transition metals oxides have the tendency to work as reduction catalysts [48]. TiO₂ was used as our reduction catalyst for NO_X, so addition of ZrO_2 itself

being a metal oxide which develops the reduction property at higher energies, contributed towards NOx reduction. It should be noted that about (50%–80%) of HCs are emitted during the cold start period which is about 200 s from the starting of an engine [49].



Figure 12. HC Conversions with Co₃O₄/TiO₂.



Figure 13. HC conversions with 8 wt.% ZrO_2 - Co_3O_4 /Ti O_2 .

Therefore, a good catalytic converter should convert maximum unburnt hydrocarbons during this span of time, maintained its high metal dispersion and high catalytic activity. In our case, both the catalysts showed maximum conversion efficiency for HCs in the beginning at the lowest RPMs. Uncoated wires mesh showed zero conversion of gases.

3. Experimental Section

3.1. Catalyst Preparation

For synthesis of TiO₂ nanoparticles, 60 g of titania powder (BDH) was added 400 mL of distilled water. The mixture was stirred for 24 h at 800 rpm and then it was allowed to settle down for 12 h. Then settled material was dried in oven for 12 h at 100 °C. The dried material was continuously crushed by using a pestle and mortar and then it was allowed to calcine at 500 °C for 6 h in a furnace. Co_3O_4/TiO_2 Catalyst was prepared by using hydrothermal synthesis method. For that purpose, 2.75 g of cobalt nitrate hexahydrate $Co(NO_3)_2.6H_2O$ (Panreac, Barcelona, Spain) was added to 30 mL of distilled water while stirring at room temperature to give 6 wt.% loading of Co_3O_4 over TiO_2 support. A mixture of potassium hydroxide KOH and water was added dropwise as precipitating agent for the formation of $Co(OH)_2$. The color of the mixture changed from pink to purple after addition of KOH. The pH value

of the solution was continuously monitored while adding KOH so that it should reach 8. Because as per literature [36] pH value from 8–9 gives a uniform size of Co_3O_4 while increasing pH to 11 or 12 give an irregular shape. Moreover, the condensation of $Co(OH)_2$ occurs at higher pH value due to which there are substantial chances of agglomeration of nanoparticles. After that, a 30% mass fraction of H_2O_2 (DAEJUNG, Busan, South Korea) was added dropwise in the solution as oxidant to convert $Co(OH)_2$ into spinel Co_3O_4 [36]. Color of the mixture started turning into brown from purple after addition of hydrogen peroxide. 4 g of titania nanoparticles were stirred in 40mL of water for one hour and then poured into a stainless steel autoclave along with the suspension already prepared. The autoclave was sealed and was put in a furnace at 180 °C for 10 h. Distilled water and ethanol were respectively used to wash the obtained material from autoclave and then it was dried in an oven at 100 °C for 8 h. 8% wt. zirconia (UNI-CHEM, Belgrade, Serbia) which is 0.15 g for 1 g of Co_3O_4/TiO_2 catalyst so that it completely soaked the powder. Then it was kept in oven at 100 °C for 5 h and calcined at 400 °C for 6 h to have 8% wt. ZrO₂- Co_3O_4/TiO_2 .

3.2. Characterization

Powder X-ray diffraction (XRD) patterns were recorded by using Bruker D8 (Karlsruhe, Germany) Advance using Cu-k α radiation operating at 40 kV and 30 mA with 0.02° step size. Samples were scanned ranging the 2 θ values from 10° to 70°. Tescan Vega3 scanning electron microscope (Brno, Czech Republic) was used to analyze the morphology of prepared catalysts and coated wires operating at 20 kV. Schimadzu DTG-60H (Kyoto, Japan) with an alumina pan was used to analyze the thermal stability and the oxygen storage capacity (OSC) of the zirconia promoted catalyst with temperature ranging from 28 °C to 800 °C with heating and cooling rate of 10 °C/min. Brunauer–Emmett–Teller (BET) surface areas of both catalysts were studied using N₂ adsorption and desorption isotherms with the help of Quantachrome, NOVA 2200e at –195.8 °C. Samples were degassed in vacuum at 300 °C for 3 h.

3.3. Fabrication and Testing of Catalytic Converter

3.3.1. Preparation of Wire Meshes

A SS-304 wire mesh sheet of 4 × 4 feet size was cut into 48 circular pieces of 6 cm diameter each as shown in Figure 14 by using a manual table cutter. Before coating the catalyst on the wire meshes, they were pretreated with 10% HCL. For this purpose wire meshes were kept dipping in 10% HCL for half an hour. After that distilled water was used to wash them and kept in an oven for drying for an hour at 100 °C. In this way, impurities were removed from the stainless steel structure. Cell density of wire meshes was 64 cells per square inch.



Figure 14. Wire mesh piece.

3.3.2. Catalyst Slurry

Catalyst slurry was prepared for coating it onto the wire mesh substrate. For this purpose, 3 g sodium metabisulfite (BDH) and 270 g of sodium silicate solution (Sigma-Aldrich, St. Louis, MI, USA) were added together for each catalyst separately while stirring shown in Figure 15. 30 g of each catalyst was added to this mixture and stirred for 12 h then it was coated on wire meshes.



Figure 15. Catalyst slurry preparation.

3.3.3. Catalyst Coating

30 g of each catalyst was deposited on the pretreated wire meshes by using the dip coating method. After immersing, a blower was used to remove the extra material from the wires of structure. This immersion and blowing was repeated three times to achieve uniformity. The coated wire meshes were calcined in a furnace for 5 h at 400 $^{\circ}$ C to remove the impurities and then cooled at the room temperature.

3.3.4. Wire Meshes Arrangement

24 circular wire meshes (for each catalyst) after being coated were arranged on a threaded bar with 4 mm diameter with 1mm thick washers between them to keep them away from intermingling. Both sides of the bar were closed by using hexagonal nut. These catalysts coated wire mesh structures were respectively placed in mild steel clam shell as shown in Figure 16 for activity testing with an inner diameter of 6.2 cm and sealed with Teflon lining to prevent any leakage of gases.



Figure 16. Coated wire meshes arrangement

3.4. Activity Test

The fabricated catalytic converters were mounted at the exhaust pipe of a 70 cc petrol engine as shown in Figure 17 with 72 cm³ displacement, 47 mm bore, and 41.4 mm stroke length was used. Test readings were taken by using Crypton's gas analyzer (Birmingham, UK) for CO and HC conversions
but for NO_x readings E instruments' E4500-2 was used. Catalytic activity readings were taken at 1500, 3000, 4500, and 6000 revolutions per minute which were manually set. Engine shaft angular speed was measured by a DT-2234B photo type digital tachometer.



Figure 17. Catalytic converter mounted on engine exhaust for testing

4. Conclusions

Two alternative catalysts, Co_3O_4/TiO_2 and 8% wt. $ZrO_2 - Co_3O_4/TiO_2$ along with a wire mesh-based substrate, were successfully developed and found very active for CO, HC, and NO_X conversions. Zirconia promoted catalyst showed more promising towards NO_X conversion. The cobalt supported by the titania Co_3O_4/TiO_2 catalyst shows a performance towards conversion of carbon monoxide, nitrogen oxides and unburnt hydrocarbons to a value of 78.1%, 61.9%, and 82.6% efficiency at 1500 RPM. Whereas, the conversion efficiency of zirconia promoted $ZrO_2 - Co_3O_4/TiO_2$ catalyst is 81.3%, 78.6%, and 55.1% towards HCs, CO, and NOx respectively at 1500 RPM value. Due to small crystalline size, thermal stability, and fouling inhibition, the ZrO_2 promoted Co_3O_4/TiO_2 catalyst showed better conversion efficiency towards CO and NOx. The slightly lower efficiency of zirconia promoted catalyst towards HCs is due to the non-availability of the vacancies of oxygen for oxidation on Co_3O_4 . Both the catalysts showed selectivity towards CO, NO_X and HC and have comparable performance with respect to be the activity of a conventional catalyst.

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Article Heterogeneous Nanomagnetic Catalyst from Cupriferous Mineral Processing Gangue for the Production of Biodiesel

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Abstract: The commercialisation of biodiesel as an alternative energy source is challenged by high production costs. The cost of feedstock, catalyst and separation of the dissolved catalyst (homogeneous catalyst) from the product are the major contributors to the total manufacturing cost of biodiesel. This study investigated the potential of a heterogeneous catalyst produced from mineral processing waste for biodiesel production. Tailings from the concentration of cupriferous minerals served as the starting material for synthesis of the catalyst. The nanomagnetic catalysts were prepared using co-precipitation (CMCO) and sol-gel (CMSG) methods, combined with zero-valent iron nanoparticles (ZVINPs) to form a hydride catalyst (CMSG/ZVINPs). Catalyst properties were assessed using SEM, TEM, BET and EDX. The catalyst activity was enhanced by a large number of basic sites that were afforded by the presence of calcite and magnesite. Good surface areas and particle sizes of 58.9 m^2/g and 15.4 nm, and 52.6 m^2/g and 16.9 nm were observed for the catalysts that were prepared using the CMSG and CMCO methods, respectively. 173 emu/g mass magnetisation was obtained for CMSG/ZVINPs, which was sufficient for the catalyst to be regenerated and reused for biodiesel production by exploiting the magnetic properties. The maximum yield obtained with this catalyst was 88% and an average of 27% decrease in biodiesel yield was observed after four reaction cycles. The physicochemical properties of the biodiesel produced complied with the ASTM standard specification. The results showed that mineral processing tailings are a viable starting material for catalyst preparation in biodiesel production.

Keywords: biodiesel; heterogeneous nano-magnetic catalyst; edible oil wastewater sludge

1. Introduction

The main purpose of ore beneficiation in the mineral processing industries is to increase the metal content. Pyrometallurgy or hydrometallurgy processes are employed depending on their nature (sulfide, oxides, or mixed), or on the initial metal purity in the ore [1]. Hydrometallurgy is the most suitable process for low-grade ores [2]. The essential concentration operation after the ore has been reduced into an appropriate size, for valuable mineral liberation from the unwanted material (gangue), is froth flotation. This involves the chemical separation of gangue from the mineral (fraction containing the valuable metal of interest) [1,2]. Gangue can be acidic (mainly containing silica and quartz), as in the case of sulfide ores or alkaline (mainly dolomite and calcite), as found in oxide and mixed ores [2]. Dolomite is mainly comprised of calcium and magnesium, and it is the dominant material in the tailings effluent from froth flotation process [2,3].

Catalysts that are used for biodiesel production are classified vis-à-vis their mode of action and reaction phases, into homogeneous, heterogeneous, and enzymatic catalysts [4]. The selection of a

catalyst for any process depends on a number of parameters, including, cost, availability, activity, selectivity, and stability [5,6]. Homogeneous-catalysed transesterification, which is the conventional method that is used to produce biodiesel from vegetable oils, utilises potassium hydroxide (KOH) or sodium hydroxide (NaOH) as homogenous base catalysts to produce high yields of biodiesel under moderate conditions. This approach is impaired by soap formation in the presence of water, especially when low-cost feedstocks are utilised. This results in separation difficulties during biodiesel purification [4,7]. Magnesium oxide (MgO) and calcium oxide (CaO) have been shown to have high catalytic activities, good robustness, and favourable resistance to acid [8]. It is envisaged that the use of heterogeneous magnetic catalysts produced from MgO and CaO for biodiesel production will enable more efficient mass transfer than conventional heterogeneous catalysts due to the high surface area and ferromagnetic properties of the nanoparticles. This might reduce catalyst loading and improve the biodiesel yield, ultimately reducing biodiesel production costs [9]. Amani et al. [8] identified MgO as a promising heterogeneous catalyst for the transesterification of soybean and vegetable oils into biodiesel, with a maximum biodiesel yield of 79% with 10 wt.% catalyst loading. It has been shown that these oxides do not require magnetic cations to become ferromagnetic, and a novel type of magnetism, which is tentatively called interface magnetism, has been recognised. Under certain conditions, magnetism arises in the absence of transition metal elements, and this phenomenon confers potential ferromagnetic properties to MgO and CaO [8,10].

The use of nanomagnetic catalysts is a promising alternative in the transesterification process, because the magnetic separation generally avoids the loss of catalyst and increases its reusability in comparison to filtration or centrifugation separation [11,12]. Nanomagnetic catalysts have been widely applied in the fields of photocatalysis [13], biocatalysis [14], and phase-transfer catalysis [15], in addition to a large specific surface area and high catalytic activity. Ying and Chen [16] stabilised the cells of lipase-producing *Bacillus subtilis* on the net of a hydrophobic carrier with Fe₃O₄ magnetic particles. for the transesterification of waste cooking oils with methanol, while Xie and Ma [17] immobilised lipase on Fe₃O₄ nanoparticles for biodiesel production. In these instances, the magnetic particles did not possess catalytic properties; they merely acted as immobilisation matrices for enhancing catalyst recovery. Ali et al. [18] synthesised a nanocatalyst of CaO supported by Fe₃O₄ magnetic particles using the chemical precipitation method. A maximum biodiesel yield of 69.7% was obtained under optimum conditions (65 °C, 300 min., 20 methanol/oil molar ratio, and 10 wt.% of CaO/Fe₃O₄ catalyst loading) using palm seed oil as feedstock.

The synthesis of oxide nanoparticles can be grouped into two main streams, based on the liquid-solid and gas-solid nature of the transformations [7]. Liquid-solid transformations are the most broadly used methods. Catalyst preparation aims at ensuring suitable activity, selectivity, and stability. These are related to the physical and chemical properties of the starting material, as well as the parameters that are inherent in the preparation method [19]. In this study, the CMSG and CMCO methods were investigated for the catalyst synthesis from mineral processing wastes, due to their low-cost when compared to other techniques.

The co-precipitation method (CMCO): Co-precipitation involves dissolving a salt precursor (mainly chloride or nitrate) in water or other solvents to precipitate the oxo-hydroxide [O(OH)] with the help of a base. The control of size and chemical homogeneity in the case of mixed metal oxides are difficult to achieve. This may be overcome by the use of surfactants and high-gravity reactive precipitation methods [8,20].

The sol-gel method (CMSG): The method prepares metal oxides via hydrolysis of precursors, usually alkoxides in alcohol solution, resulting in the corresponding [O(OH)] group. The condensation of molecules by dehydration leads to the formation of a network of the metal hydroxide. Hydroxyl-species undergo polymerisation by condensation and form a dense porous gel. Appropriate drying and calcination lead to ultrafine porous oxides [7,15]. Irrespective of the preparation method that was used to obtain ultrafine nano-oxides, crystallisation does not follow a traditional nucleation

and growth mechanism [21]. The crystallisation mechanisms may be a function of the chemical nature of the oxide and the process temperature [22].

In the conventional biodiesel production process, oil is derived from oilseed crops, which is associated with the food versus fuel dilemma [23,24]. In this study, the oil and alcohol that were employed for the transesterification reaction for biodiesel production were extracted from edible oil wastewater sludge. The heterogeneous nanomagnetic catalyst, which was used in mediating the reaction, was prepared from waste without magnetite support, in the presence of ZVINPs to enhance the catalyst mass transfer abilities during this process [23].

2. Results and Discussion

2.1. Gangue Characterisation

EDX analysis was conducted to assess the elemental composition and purity of the gangue material and the prepared catalysts. The results that were obtained from the EDX analysis of the gangue material showed predominance of magnesium (4 *cps/ev*) and calcium (4.2 *cps/ev*) (Figure 1). The predominance of magnesium or other related transitional metals in heterogeneous catalysts has been widely shown to have a positive impact on their mass transfer capabilities in the transesterification process, subsequently enhancing the biodiesel production at lower reaction rates [22].



Figure 1. EDX results of the raw material (gangue) used to prepare the catalyst.

On the Linus Pauling scale, magnesium and calcium are characterised by electronegativity values of 1.32 and 1, respectively [25,26]. This is an important factor that can enable the catalyst to exhibit higher basicity and improved catalytic activity for better biodiesel yield during the transesterification reaction. The peak maxima were obtained at 1.3 and 3.6 keV for magnesium and calcium, respectively (Figure 1).

2.2. Brunauer-Emmett-Teller (BET) Surface Area Analysis and Barrett-Joyner-Halenda (BJH) Pore Size and Volume Analysis

The surface area of the catalysts was determined using BET analyses, while the pore size and specific pore volume were determined using the adsorption and desorption techniques (BJH analyses). Results showed that an increase in nitric acid concentration increased the surface area of all catalysts (Table 1).

Sample	Surface Area (m ² /g)	Average Pore Size (Å)	References
CMCO ₂ *	52.6 ± 0.37	135.6 ± 0.13	This study
CMSG ₃ *	58.7 ± 0.55	169.3 ± 0.21	This study
CMSG ₃ /ZVINPs ₂ *	53.5 ± 1.52	148.5 ± 0.09	This study
CaO/Fe ₃ O ₄	59.1	8.5	[26]
KF/Ca-Mg-Al	109.4	27	[14]
hydrotalcite	100.4	3.7	[14]

Table 1. Comparison of surface areas and pore sizes of the prepared catalysts with previous studies.

* Only the best results are represented in this table. Results are expressed as averages \pm standard deviation (n = 3); With CMCO = Catalyst prepared using the co-precipitation method, CMSG = Catalyst prepared using the sol-gel method, ZVINPs = Zerovalent iron nanoparticles.

The results also indicated (Table 2) that CMSG₃ had the highest surface area of 58.7 m²/g. The adsorption average pore width (4 V/A by BET) was 169.3 Å for CMCO₂ with a BJH adsorption average pore width (4 V/A) of 146.7 Å and a BJH desorption average pore width (4 V/A) of 148.5 Å, compared to 155.1 Å for CMSG₃ with BJH Adsorption average pore width (4V/A) of 135.6 Å and BJH desorption average pore width (4 V/A) of 153.9 Å.

Table 2. Mass magnetisation of catalysts prepared.

Catalysts	Average Mass Magnetisation (emu/g)
CMCO1	153 ± 0.71
CMCO ₂	168 ± 1.45
CMCO ₃	159 ± 0.97
CMSG ₁	76 ± 1.94
CMSG ₂	91 ± 1.06
CMSG ₃	84 ± 0.56
CMSG ₃ /ZVINPs ₁	134 ± 2.52
CMSG ₃ /ZVINPs ₂	173 ± 0.36
CMSG ₃ /ZVINPs ₃	162 ± 1.27

The effect of synthesis methods on the surface area of CMCOs and CMSGs was significant, with CMSG₃ maintaining a higher surface area when compared to the CMCO₂ sample. Cross-sectional area measurements showed that all of the tested samples were mesoporous. The results that were obtained in the current study agree with previous reports. Report by Xie and Fan [27] investigated the production of biodiesel using tetra alkyl ammonium hydroxides that were immobilised on mesoporous silica as a solid catalyst. Using the co-precipitation method, the catalyst samples prepared were characterised by maximum surface area of 61 m²/g. Similarly, Rashtizadeh et al. [28] and Teo et al. [29] achieved a surface area of 59 m²/g when nanocomposite and mesoporous materials containing calcium oxide were prepared.

2.3. Microscopic Observations

SEM micrographs at 20 nm scale (Figure 2A–F) show the three-dimensional (3-D) morphology of the CMCO and CMSG catalysts, while Figure 3A–F are TEM micrographs of the same catalysts at 200 nm scale and 5.00 KX magnification. The catalysts prepared using the sol-gel method had a more elongated shape and uniform distribution, while those that were prepared using the co-precipitation method exhibited strong agglomeration and a higher degree of variation in size. For the CMSG catalysts, the micrographs were homogeneous microstructures (Figure 3). This can be attributed to the fact that, in the sol-gel process, the open structure of the gelatinous state formed allows for free crystal agglomeration, resulting in a more spherical and uniform structure [25]. Taufiq-Yap and Lee reported similar observations [20]. They showed that sol-gel catalysts were characterised by better homogeneity and phase purity with sintering at low temperatures (≤ 200 °C), as opposed to the co-precipitated catalyst often described as lower phase purity catalysts [25].



Figure 2. SEM results of the prepared catalyst (A: $CMCO_1/B$: $CMCO_2/C$: $CMCO_3/D$: $CMSG_1/E$: $CMSG_2/F$: $CMSG_3$) [EHT = 5.00 keV, WD = 4.7 mm, Mag = 5.00 K X, 20 nm scale].



Figure 3. TEM results of the prepared catalyst (A: $CMCO_1/B$: $CMCO_2/C$: $CMCO_3/D$: $CMSG_1/E$: $CMSG_2/F$: $CMSG_3$) [EHT = 5.00 keV, WD = 4.7 mm, Mag = 5.00 K X, 200 nm and 1 μ m scale].

Large pores separated the CaO and MgO aggregates in the CMCOs samples (Figure 3). An approximate quantification of CMSG₃ samples indicated that the size of aggregates, as well as the width of pores between those aggregates, were in the range of 16 to 17 nm in comparison to 15 to 17 nm for the CMSG samples. For the catalysts that were prepared by the sol-gel technique (Figure 3F), there was a clear indication of localisation of metal nanoparticles in very small pores of the support structure. Farooq et al. [9] and Rahstizadeh et al. [28] reported a similar observation. Additionally, there was a uniform material contrast, justifying the clear visibility of calcium and iron as compared to magnesium based on a single peak that was represented in the spectrum (Figure 3).

The pH was increased from $CMCO_1$ to $CMCO_3$ by decreasing the HNO_3 concentration from 1.5 M to 0.5 M. Alhassan et al. [30] suggested that pH decreases before reaction completion might adversely affect the precipitation stage of the metal oxide catalyst, so the pH was carefully monitored. The pH adjustment was carried out in an attempt to enhance co-precipitation, which is favoured in

a more alkaline environment. The optimum concentration was 1M HNO₃ for the CMCO₂ catalyst. It was unclear why the microscopic characteristics and surface area of CMCO₃ were inferior to those of CMCO₂. The increase in ethylene glycol concentration positively contributed to the good quality of the gel that was obtained using the CMSG method (Figure 3F). This agrees with the reports by Zebarjad et al. [31]. In their study, high purity MgO sol-gel particles were synthesised with sizes that ranged from 30 nm to several µm. The optimal CMSG catalyst exhibited more desirable structural properties than its CMCO counterpart, being more agglomerated and interconnected (Figure 3D–F).

2.4. Magnetic Susceptibility and Mass Magnetisation Calculations

In order to quantify the sample's magnetic strength, the magnetic susceptibility of each catalyst sample was converted into mass magnetisation using Gouw's principle [8,10] (Table 2). The CMCO sample exhibited higher magnetic than the CMSG catalyst. This might be attributed to (i) the presence of iron originating from the magnetite in the sample and/or (ii) the size of the catalysts, which were smaller than the super paramagnetic critical size of 27 nm, as described by Zebarjad et al. [31]. There was no major hysteresis in the magnetisation for either sample, which suggests that the particles were paramagnetic.

The CMSG samples were coupled to ZVINPs to boost the saturation magnetisation of the CMSG catalyst while conserving the optimum surface area for mass transfer. Maximum and minimum mass magnetisations were obtained for $CMSG_3/ZVINPs_2$ (173 emu/g) and $CMSG_3$ (84 emu/g), respectively, indicating that the magnetic separation and regeneration of $CMSG_3/ZVINPs_2$ would be most favourable.

In this study, paramagnetism was confirmed by demonstrating that the catalyst particles in a bottle were attracted to a neodymium magnet outside the bottle. Paramagnetism (i.e., responsiveness to an applied magnetic field without permanent magnetisation) was an essential property, because it allowed for the CMSG₃/ZVINPs₂ to be separated from the mixture of biodiesel and glycerol under an external magnetic field, which was coupled with electrostatic separation to improve the sedimentation of glycerol.

2.5. Evaluation of Catalytic Performance

Biodiesel obtained from the transesterification process mediated by the CMSG₃/ZVINPs₂ catalyst was analysed to assess its quality. As previously described [23], the biodiesel was complied with selected standard specifications (Table 3).

Properties	Unit	Measurement Standards	Commercial Diesel (50ppm Sulphur)	Biodiesel [23]
Viscosity at 40 °C	m²/s	ASTM D445	$3.0*10^{-6}\pm0.87$	$3.7 * 10^{-6} \pm 0.71$
Density at 15 °C	kg/m ³	ASTM D941	830.0 ± 0.78	832.62 ± 0.69
HHV	MJ/kg	ASTM D2015	48.12 ± 1.59	45.75 ± 1.21
Flash point	°C	ASTM D93	50.4 ± 0.73	61.3 ± 0.64

Table 3. Comparison of the synthesised biodiesel (obtained using $CMSG_3/ZVINPs_2$) quality and the commercial diesel [23].

Results are expressed as averages \pm standard deviation (n = 2).

Selected catalysts were used to produce biodiesel, and regenerated over four reaction cycles (Figure 4A–D). All of the catalysts were able to mediate biodiesel production (83–88%) up until the fourth reaction cycle. In the case of the catalysts that were not coupled with ZVINPs, the biodiesel yield that was obtained using CMCO₂ (Figure 4A) decreased from a maximum of 88% biodiesel yield to a minimum of 64%. In contrast, CMSG₃ exhibited the worst performance (Figure 4B), losing 39% of its activity after four transesterification cycles. This indicated that the co-precipitation method yielded a more robust catalyst than the sol-gel method in this instance. The hydride catalysts (CMSG/ZVINPs) showed an enhancement in performance (Figure 4C,D) over the CMSG catalyst. This was attributed to

the enhanced mass magnetisation (Table 2) that was conferred by the ZVINPs. Factors, such as loss of catalyst during the separation [32], catalyst surface saturation [11,19], and catalyst leaching, are likely to have contributed to the reduction in the biodiesel yield [9] when using the regenerated catalysts.



Figure 4. (A) Recycled $CMCO_2$; (B) $CMSG_3$; (C) $CMSG_3$ /ZVINPs₂; and, (D) $CMSG_3$ /ZVINPs₃. Effect on the biodiesel yield (Error bars represent the standard deviation from the mean (n = 3)).

Vishal et al. [33] investigated the use of *n*-hexane to improve the catalytic activity of the catalyst that was used to convert jatropha oil into biodiesel. A reduction in biodiesel yield from 98 to 89% after

five reaction cycles was attributed to the loss of catalyst material during the separation process and the oversaturation of the catalyst's pores. Devarapaga et al. [34] described a decrease in biodiesel yield during three reaction cycles when using a novel β -tricalcium phosphate catalyst; the authors attributed the loss in performance to a high FFA concentration in the feedstock that neutralised the functional basic sites of the catalyst. In this instance, the catalyst efficiency was affected by the ability of that particular catalyst to influence the reaction rate, the biodiesel yield through the transesterification process, as well as the extent to which the catalyst could be regenerated while conserving its catalytic activity for biodiesel production. While the sol-gel method was easier to perform and less time consuming, and it resulted in a catalyst with good specific surface areas, the biodiesel yield was negatively affected. This could be due to the lower stability of CMSGs during the reaction. The catalyst sample could have disaggregated when stirring was applied into the vessel [34].

3. Materials and Methods

3.1. Materials

Sodium hydroxide pellets (98%), anhydrous hexane (95%), sodium chloride (anhydrous \geq 99%), anhydrous ethylene glycol (C₂H₆O₂) (99%), ferric sulphate, sodium borohydride, and nitric acid (70%) used in this study were obtained from Sigma Aldrich (Sigma-Aldrich, St Louis, MO, USA), distilled water. Gangue material was obtained from a mineral processing plant in the Rustenburg region (South Africa) from cupriferous minerals that were generated from the concentration (floatation process) of sulfide ores.

3.2. Catalyst Preparation

The gangue sample that originated from cupriferous mineral processing was obtained from the outlet of bulk oil flotation cells and these samples were characterised by EDX to identify the phases and unit cell dimensions in the samples. This was then subjected to the different catalyst synthesis methods, as described in Sections 3.2.1–3.2.3.

3.2.1. Sol-gel Method

The catalyst was prepared following the method described by Chen et al. [25] with the following modifications: 10 g of gangue was dissolved in warm (60 °C) 1 mol/L nitric acid (HNO₃) into a 500 cm³ beaker. The slurry was placed into an evaporative basin until crystals were formed. Nine g of the crystals were dissolved in 100 mL of distilled water, added to 15 mL of $C_2H_6O_2$ to obtain catalyst CMSG₁, to 20 mL of $C_2H_6O_2$ to obtain catalyst CMSG₂, and to 25 mL of $C_2H_6O_2$ to synthesise catalyst CMSG₃. The mixing time for all the catalysts was kept constant at 2 h. During mixing, drops of 2 M NaOH was added until a clear white gel was obtained. The gel was then kept static for 2 h for the reaction to complete, and then washed with distilled water. After filtration using Whatman's filter paper PTFE (pore size $0.5 \,\mu$ m), the washed, pH-adjusted gel (pH = 10) was dried by heating at 80 °C for 2 h and then placed in a desiccator for 1 h. The dry gel was milled to form a white powder, which was decarbonised by gradually heating to 800 °C in an oven.

3.2.2. Co-precipitation Method

Three CMCO catalysts were prepared using the co-precipitation method that was adapted from Lu et al. [35] based on different hematite-double nitrate of calcium and magnesium ratios $[(Fe_3O_4)/(Ca,Mg)(NO_3)_2]$ samples were accordingly labelled as CMCO₁ (1:2); CMCO₂ (1:3); and, CMCO₃ (1:4). The Fe₃O₄ value was varied to investigate the enhancement of the magnetic susceptibility of the catalyst for separation purposes

3.2.3. Catalyst Mixed with Zero-Valent Iron Nanoparticles (ZVINPs)

ZVINPs were prepared according to the stoichiometry shown in Equation (1) using the sulphate method [27]; 0.5 M sodium borohydride was added to an equal volume of 0.28 M ferrous sulphate at 0.15 L/min.

$$2Fe^{2+}_{(aq)} + BH_4^{-}_{(aq)} + 3H_2O_{(l)} \rightarrow 2Fe_{(s)} + H_2BO_3^{-}_{(aq)} + 4H^+_{(aq)} + 2H_2_{(g)}$$
(1)

The CMSG₃ catalyst was then mixed with ZVINPs to form a hybrid catalyst. Three catalysts were obtained depending on the mixing ratio: $CMSG_3/ZVINPs_1$ (2:1), $CMSG_3/ZVINPs_2$ (3:1), and $CMSG_3/ZVINPs_3$ (4:1). CMSG catalysts were amalgamated with ZVINPs to improve their magnetic susceptibility for separation purposes. In theory, magnetic separation can reduce the production costs by eliminating the need for more expensive separation methods, such as centrifugation. CMCO catalysts were not amalgamated with ZVINPs, because the co-precipitation method was significantly longer.

3.3. Biodiesel Production and Separation

Biodiesel was produced through a transesterification reaction using oil extracted from edible oil wastewater sludge and bioethanol (originating from the edible oil wastewater sludge residues after oil extraction). The process was separately mediated using different catalysts (CMCO₂, CMSG₃, CMSG₃/ZVINPs₂, and CMSG₃/ZVINPs₃), as previously described [23,24]. The triglycerides extracted from waste that was mainly contained monounsaturated fats. The catalysts were CaO and MgO-based. The use of these two compounds are known to result in higher biodiesel yield, at faster reaction rates, lower temperatures, and low catalyst loading [8,21,23,24]. The transesterification process was carried out in a 500 mL flask using a 1:6 oil/ethanol molar ratio and catalyst dosages were selected at 3, 5, and 8 wt.%. The temperature was set at 75 °C for 2 h. All of the runs were performed in triplicate. After the reaction was completed, the collected catalyst was washed with ethanol and then dried at 80 °C for 2 h before being used.

The electrostatic method was used to separate the biodiesel from the glycerol using LG electronics Neon transformer (Seoul, South Korea). The transformer electrodes were immersed in a flask containing 1 L biodiesel/glycerol mixture. The transformer was then set at 8 kV and adjusted for 25 mA. This separation process was completed after 20 min. This technique was adapted from Mayvan et al. [36].

The yield of biodiesel obtained was calculated using Equations (2) and (3) relating the weight of oil in the raw material and the weight of biodiesel obtained after glycerol separation. These findings were compared with the values that were obtained using a GC-FID 6980A that was manufactured by Agilent (Santa Clara, CA, USA). The column used was a HP88 (60 m \times 150 µm, 0.250 µm) manufactured by Agilent Technologies (Santa Clara, CA, USA).

$$Yield (\%) = \frac{Weight Biodiesel}{Weight Oil} \times 100$$
(2)

$$Conversion (\%) = \frac{Weight_{Glycerol} - Weight_{Biodiesel}}{Weight_{Biodiesel}} \times 100$$
(3)

3.4. Recovery of Catalyst from Biodiesel

A magnetic field that was provided by a lightweight (75 g) neodymium magnet assembly with a 2 cm air gap and magnetic field of approximately 0.22 T (Tesla) was used to recover the catalyst. This magnet assembly was immersed into the flasks containing 500 mL biodiesel at ambient temperature for 10 min, while stirring at 50 rpm. The collected catalyst was then washed with ethanol and then dried in an oven at 80 °C for 2 h [23,24].

3.5. Catalyst Characterisation and Performance

The morphology and particle sizes of the raw materials, as well as the catalysts, were assessed by EDX (STADI P, STOE model, Darmstadt, Germany). An Auriga (Carl Zeiss model, Jena, Germany). High-resolution scanning electron microscope (HRSEM) was used with a resolution of 1.5 nm to provide details from a focused electron beam across the surface of the sample. These images were magnified using an Auriga TF 20 high-resolution transmission electron microscope (Carl Zeiss model, Jena, Germany) with a resolution of 0.25 nm for 45 min. to 2 h for sample mapping and imaging. Furthermore, an Aztec series (Hitachi High-Technologies, Tokyo, Japan) TM 4000 energy dispersive X-ray analyser with a 30 mm² detector) was employed to provide the elemental identification and quantitative composition of the prepared catalyst. Catalyst surface areas were studied using a VF-Sorb 2400CE BET (Brunauer-Emmett-Teller) surface area analyser (Beijing, China). The magnetic susceptibilities of the catalysts were calculated based on Gouw's principle [32]. These results were confirmed by the PS PRO Gauss meter (Corby, United Kingdom). The performance of these catalysts was evaluated based on their abilities to improve the yield of biodiesel that is produced from edible oil wastewater sludge at different catalyst dosages (3, 5, and 8 wt.%) and ethanol-oil ratios (3:1, 6:1, and 9:1), respectively. The particle surface area was confirmed using BET analysis.

4. Conclusions

The catalysts that were obtained from cupriferous mineral processing wastes were successfully prepared and characterised using TEM, SEM, EDX, and BET. The mass magnetisation analysis showed that the nanocatalyst samples were magnetic. The quality of the CMSG catalysts was not affected by the increase in ethylene glycol concentrations. Further, as for the catalysts that were prepared using the co-precipitation method CMCO, the magnetite ratio chosen in this study did not considerably increase their respective mass magnetisation. The reusability of the catalyst preparation over four cycles of transesterification reaction has the potential to reduce the cost of biodiesel production. The maintenance of 50–72% catalytic activities, as demonstrated by the biodiesel yields, after four cycles suggest that the catalysts can be used for more cycles. Properties of the biodiesel that were produced from the edible oil wastewater sludge using these catalysts were within the biodiesel standard specifications.

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Low-Temperature Selective Catalytic Reduction of NO with NH₃ over Natural Iron Ore Catalyst

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Abstract: The selective catalytic reduction of NO with NH₃ at low temperatures has been investigated with natural iron ore catalysts. Four iron ore raw materials from different locations were taken and processed to be used as catalysts. The methods of X-ray diffraction (XRD), X-ray fluorescence (XRF), Brunauer-Emmett-Teller (BET), X-ray photoelectron spectroscopy (XPS), hydrogen temperature-programmed reduction (H₂-TPR), ammonia temperature-programmed desorption (NH₃-TPD), scanning electron microscopy (SEM) and Fourier-transform infrared spectroscopy (FTIR) were used to characterize the materials. The results showed that the sample A (comprised mainly of α -Fe₂O₃ and γ -Fe₂O₃), calcined at 250 °C, achieved excellent selective catalytic reduction (SCR) activity (above 80% at 170–350 °C) and N₂ selectivity (above 90% up to 250 °C) at low temperatures. Suitable calcination temperature, large surface area, high concentration of surface-adsorbed oxygen, good reducibility, lots of acid sites and adsorption of the reactants were responsible for the excellent SCR performance of the iron ore. However, the addition of H₂O and SO₂ in the feed gas showed some adverse effects on the SCR reaction in the presence of SO₂, which could cause pore plugging and result in the suppression of the catalytic activity.

Keywords: natural iron ore; NO; low-temperature; selective catalytic reduction

1. Introduction

Current global major environmental problems, such as smog, rain, fine particle pollution, and ozone depletion are credited to nitrogen oxides (NO_x, x = 1, 2) [1]. Around the world, NO_x legislation has become more and more stringent due to the increased awareness in society about protecting the environment [2]. Therefore, in the modern era, a lot of focus is given to the removal of NO_x by the researchers. To meet these stringent regulations of NO_x with ammonia (NH₃) has become the most effective and extensively used NO_x reduction technology [3]. Vanadium-based catalysts (V₂O₅/TiO₂ or V₂O₅-WO₃/TiO₂) are the most common industrial catalysts for SCR of NO_x with NH₃, for which the most efficient reaction temperature range is 300~400 °C [4]. Since the operating temperature range is high, that is why the catalyst must be placed upstream of the desulfurizing section and the particulate removal device, to avoid reheating the flue gas; but it can cause deactivation due to the high concentration of sulfur dioxide and dust [5]. Other issues include high activity for the oxidation of SO₂ to SO₃ [6], the formation of N₂O at high temperatures [7] and the toxicity of vanadium to the environment [8]. That is why recently, environmental catalysis has put great efforts into the development of V-free NH₃-SCR catalysts.

Some other transition metal oxide-based catalysts (Cr, Mn, Fe, Ni, Zr, Co, Cu, La, etc.) have shown good NH₃-SCR performance [9]. For example, Ma et al. prepared TiO₂-supported iron

oxide catalysts. It was found that $Fe_2(SO_4)_3/TiO_2$ catalysts have shown excellent NO_x conversions in the NH₃-SCR reaction at low temperatures [10]. Chen et al. synthesized a series of Fe–Mn oxide-based catalysts by three different synthesis methods: the citric acid method, the coprecipitation method and the solid reaction method [11]. The results exhibited that the catalytic activity of the catalyst prepared by the citric acid method ($Fe_{(0.4)}$ -MnO_x(CA-500)) was higher (around 98.8% NO_x conversion at 120 °C) than other catalysts. Sankar et al. applied two preparation techniques (impregnation and deposition–precipitation) to synthesize the Mn–Fe/TiO₂ catalysts, and concluded that the deposition–precipitation technique-based catalyst (25 wt % Mn_{0.75}Fe_{0.25}Ti) showed superior catalytic activity (97% at 200 °C) [12]. Likewise, Wu et al. prepared a FeMnTiO_x-mixed oxide catalyst by cetyltrimethylammonium bromide (CTAB)-assisted coprecipitation method [13,14]. It was found that the NO_x conversion was around 80~100% at 100~350 °C. Zhang et al. prepared catalysts by loading Mn–FeO_x and MnO₂–Fe₂O₃–CeO₂–Ce₂O₃ onto carbon nanotubes (CNTs) support, respectively [15,16]. The NO_x conversion at low temperatures, yet there exist some difficulties in their sophisticated preparation methods, as well as the fact that the preparation cost of these catalysts is very high.

For many centuries, the oxides of iron have been serving humankind. The first use of yellow and red ochres was in prehistoric paintings in the caves. After that, the role of iron oxides in our lives has seen an unbelievable expansion. Their primary applications include the steel industry (as a precursor of iron and steel), the ecosphere (their activity as absorbents), and chemical reactions (their ability to catalyze various chemical reactions). Around 80% of the world's iron ore production consists of sedimentary iron ore, and the significant proportion of these sedimentary iron ore deposits in the world is made up of iron oxides [17].

Previously, the NO conversion of manganese ore has been investigated in some studies. Park et al. used natural manganese ore for NO reduction and studied its catalytic activity [18]. Similarly, Zhu et al. also studied the performance of natural manganese ore catalysts and showed that the NH₃-SCR activity of the manganese-based catalyst reached 80% at 120 °C [19]. Gui et al. studied the performance of iron and iron ore particles as catalysts in a magnetically fluidized bed [20]. The results showed that the catalytic activity of the iron ore was not affected much by the magnetic field. However, some of these studies were unable to clarify why the temperature of NO conversion was reduced by those catalysts.

Inspired by the idea of finding a catalyst with low preparation cost, high NO conversion and nominal environmental pollution, natural iron ore as a De–NO_x catalyst is investigated in this study. The methods of XRD, XRF, BET, XPS, H₂-TPR, NH₃-TPD, SEM and FT-IR were used to characterize the materials. The results showed that the sample A which calcined at 250 °C achieved excellent SCR activity (above 80% at 170–350 °C) and N₂ selectivity (above 90% up to 250 °C) at low temperatures. Suitable calcination temperature, large surface area, high concentration of surface-adsorbed oxygen, good reducibility, lots of acid sites and adsorption of the reactants, were responsible for the excellent SCR performance of the iron ore. However, the addition of H₂O and SO₂ in the feed gas showed some adverse effects on the SCR activity. The FT-IR analysis indicated the formation of sulfate salts on the surface of the catalyst during the SCR reaction in the presence of SO₂, which could cause pore plugging and result in a reduction of the catalytic activity.

2. Results and Discussion

2.1. NH₃-SCR Activity and Selectivity

For different samples calcined at 250 °C, the low-temperature SCR removal activity, and N₂ selectivity at different reaction temperatures, are shown in Figure 1A and Table 1, respectively. It can be seen that sample A exhibited the best activity and selectivity among other samples in a wide temperature range with NO conversion above 90% from 200–290 °C and the N₂ selectivity above 90% up to 250 °C.

It can be concluded that the catalytic activity and selectivity of all the samples were different from each other, which could result from the difference in their material structure, surface properties and composition of the iron ore. The catalytic activity and selectivity of the catalysts at low temperatures followed the particular sequence: Sample D < Sample B < Sample C < Sample A. In addition, it can be seen that the NO conversion of sample A is higher than the Mn–Ce– γ –Al₂O₃ catalyst [21] within 150–300 °C, even though the gas hourly space velocity (GHSV) of our experiments is higher than that of the literature.



Figure 1. (**A**) NO conversion of different iron ore samples calcined at 250 °C and the Mn–Ce– γ –Al₂O₃ catalyst reported in literature [21]; (**B**) Influence of calcination temperature on the NO conversion of sample A. Our reaction conditions: 500 ppm NO, 500 ppm NH₃, 3 vol % O₂, N₂ balance, the flow rate of 145 mL·min⁻¹, and gas hourly space velocity (GHSV) = 20,000 h⁻¹. Reaction conditions of literature [21]: 700 ppm NO, 700 ppm NH₃, 3 vol % O₂, N₂ as balance, and GHSV = 10,000 h⁻¹.

Samples	50 °C	150 °C	250 °C	350 °C
Sample A	96.66%	95.43%	91.98%	85.45%
Sample B	96.66%	94.50%	83.45%	70.35%
Sample C	96.66%	94.52%	86.35%	80.84%
Sample D	96.66%	94.13%	78.78%	59.47%

Table 1. N₂ selectivity of the calcined samples (at 250 °C) at different reaction temperatures.

Calcination of a catalyst can help to obtain a large specific surface area and better dispersion of the active ingredients of the catalyst [2]. To find out the suitable calcination temperature for iron ore catalysts, sample A was thermally treated to different temperatures ($250 \,^{\circ}$ C, $350 \,^{\circ}$ C, $450 \,^{\circ}$ C) and the NO conversions are shown in Figure 1B. The results showed that the NO conversions of the thermally-treated samples were better than the sample without thermal treatment. For example, at 200 $\,^{\circ}$ C reaction temperature, the NO conversion of sample A that calcined at 250 $\,^{\circ}$ C was 91%, whereas the catalytic activity of sample A without calcination was just 64%. Additionally, the sample A calcined at 250 $\,^{\circ}$ C and 450 $\,^{\circ}$ C, respectively, indicating the possible severe morphology changes in the iron ore sample after high calcination temperatures of 350 and 450 $\,^{\circ}$ C (as shown in SEM results). Higher calcination temperatures cause a decrease of the surface area and the mobility of lattice oxygen, which may be the reason for the lower catalytic activity of these samples [19,21].

2.2. NO, and NH₃ Oxidation Activity

It was reported that with the increase in the NO₂/NO molar ratio in the feeding gas fast SCR reaction: NO + NO₂ + $2NH_3 \rightarrow 2N_2 + 3H_2O$ could be promoted, which can significantly boost the

low-temperature SCR activity of the catalyst [16,22]. That is why separate NO oxidation activities of the different samples were tested and the results are demonstrated in Figure 2A.

It can be seen that with the rise in temperature the NO oxidation activities increased, first up to the 300 °C reaction temperature, and then decreased. Some evident differences could be seen between the NO oxidation activity and SCR activity of the samples which could be ascribed to the role of NH₃ during SCR reaction; in a real SCR reaction, the presence of NH₃ would increase the NO to NO₂ conversion as compared to the pure NO oxidation. NO conversion to NO₂ was proven to be a slow step for an SCR reaction, and the NO₂ generated was rapidly consumed in the existence of ammonia [22]. Sample A comprising the larger weight fraction of γ -Fe₂O₃ exhibited the highest NO conversion to NO₂ as well as the NH₃–SCR activity. Figure 2B shows that the NH₃ oxidation increased with the rise in temperature. This increase in the NH₃ oxidation at high temperatures is considered as a side reaction which aids in the formation of NO in the NH₃–SCR system and also causes the deactivation of the catalysts at high temperatures [13].



Figure 2. (A) NO oxidation activity; (B) NH₃ oxidation activity. Reaction conditions: 500 ppm NO or 500 ppm NH₃, 3 vol % O_2 , N_2 balance, flow rate of 145 mL·min⁻¹, and GHSV = 20,000 h⁻¹.

2.3. Characterization

XRD patterns of the different iron ore samples without calcination are shown in Figure 3. It can be seen that the samples consist of three minerals of iron: γ -Fe₂O₃ (maghemite, JCPDS 00-39-1346), α -Fe₂O₃ (hematite, JCPDS 01-089-8104) and α -Fe₀OH (goethite, JCPDS 00-017-0536).

The diffraction spectra of sample A indicated that three main phases of ferric oxide (α -Fe₂O₃, α -FeOOH and γ -Fe₂O₃,) were present in it, and through quantitative analysis by the Rietveld method it was found that the ratio of these three phases in sample A was 59.4:11.5:29.1, respectively. Similarly, in sample C the ratio was 67.7:24.1:8.2, respectively. Diffraction spectra of sample B showed that α -Fe₂O₃ and α -FeOOH were the two phases present in the sample and existed in 27.4:72.6, respectively. Whereas, in sample D the ratio was 7.7:92.3, respectively.

The XRD spectra in Figure 3 depicts that the sample A comprised mainly of α -Fe₂O₃ and γ -Fe₂O₃ and the weight fraction of γ -Fe₂O₃ was found highest among other samples. With a change in the temperature range, the catalytic influence of these two components varies. The optimum temperature of the NO conversion of γ -Fe₂O₃ is relatively low as compared to α -Fe₂O₃ [23]. It is known that the lattice of γ -Fe₂O₃ has point defects created by its cation vacancies [24]. These point lattice defects could be useful in providing more active sites for the catalytic reaction to take place, as well as contribute to the surface electron transfer in the SCR reaction. So the existence of γ -Fe₂O₃ could be crucial for the low-temperature SCR activity of the iron ore.

Partly magnified XRD spectra of the 'not calcined' as well as 'calcined' sample A at different temperatures is shown in Figure 4. Sample A without calcination exhibited sharp crystalline peaks of

 α -Fe₂O₃ and γ -Fe₂O₃, indicating good crystallinity (Figure 4A). After calcining the sample to 250 °C, both phases of the Fe₂O₃ were still intact, but the intensities of the peaks were much lower, indicating a poor crystallinity (amorphous structure formation verified by SEM) which was beneficial for obtaining high SCR activity at low temperatures. However, with a further rise in calcination temperature above 250 °C, the γ -Fe₂O₃ phase (peak at 63.99°) in the sample has been converted into the α -Fe₂O₃ phase (peak at 64.17°). Cao et al. also concluded that after increasing the calcination temperature above 250 °C, the γ -Fe₂O₃ particles started to engulf their surrounding crystals and the different sizes of the α -Fe₂O₃ particles formed [25], which resulted in the decrease of surface area. According to the Scherrer formula (Equation (5)), the half-width of the diffraction peak and the crystallite size of the material are inversely proportional to each other. So, the average crystallite sizes of the sample that was calcined at 350 °C and 450 °C, respectively are larger than the sample calcined at 250 °C, which could be related to the sintering (frittage) phenomenon at higher temperatures and the formation of α -Fe₂O₃. That is why the samples calcined at a higher calcination temperature (350 °C, 450 °C) exhibited lower catalytic activity and selectivity than the sample calcined at 250 °C (Figure 1, Table 1).



Figure 3. XRD spectra of different iron ore samples.



Figure 4. Partly magnified XRD spectra of sample A: (**A**) transformation of γ -Fe₂O₃ to α -Fe₂O₃ above 250 °C; (**B**) formation of Al_{0.94}Fe_{1.06}O₃ in the calcined samples.

In addition, it can be seen in Figure 4A (not calcined sample), apart from α -Fe₂O₃ peaks, two small peaks appear at 36.8° and 40.25° which correspond to the O₇P₂Si crystals phase (JCPDS 00-022-1274), and one peak at 42.46° represents the presence of SiO₂ (JCPDS 00-046-1045). In calcined samples, the

peaks of O₇P₂Si are not present. However, the peaks of Al_{0.94}Fe_{1.06}O₃ (JCPDS 00-011-0562) at 28.36°, and SiO₂ at 26.7° are detected (Figure 4B). These results exhibited that the O₇P₂Si was decomposed to SiO₂, and after calcination Al_{0.94}Fe_{1.06}O₃ was formed. This formation of Al_{0.94}Fe_{1.06}O₃ may have aided in a better NO reduction of sample A.

The elemental compositions of the iron ore samples show that Fe, O, Al and Si are the major elements present in these samples (Table 2). Natural iron ore was composed mainly of ferric oxide (XRD). Ferric oxide, particularly maghemite (γ -Fe₂O₃) particles, exhibited good SCR activity at low temperatures [26], and the interactions of some major elements like Al and Si with ferric oxide could be beneficial for the low-temperature SCR activity [27–29]. XRD results indicated the formation of Al_{0.94}Fe_{1.06}O₃ and SiO₂ (from the decomposition of O₇P₂Si) after calcining the catalyst, which may have assisted in a better NO reduction of sample A.

Elements	Sample A (%)	Sample B (%)	Sample C (%)	Sample D (%)
Fe	60.961	68.099	67.853	64.32
О	31.564	26.630	25.801	28.95
Al	1.706	2.043	2.243	2.13
Si	3.386	1.080	1.881	2.95
Р	0.029	0.066	0.082	0.087

Table 2. Iron ore samples with their major elements and their mass percentages.

BET surface areas and average crystallite size of the catalysts are shown in Tables 3 and 4. It can be seen from Table 3 that BET surface areas of the calcined samples are much higher than the non-calcined sample, and a decline in the surface area of sample A was observed with a rise in calcination temperature (350 °C and 450 °C). In addition, it can be seen from Table 3 that the surface area of the catalysts and the average crystallite size are inversely proportional to each other. Table 4 is comprised of BET surface areas and the average crystallite size of the different samples of the iron ore calcined at 250 °C. Sample A exhibited the highest surface area among other samples. Larger surface area can help to provide more active sites on the surface of the catalyst by which flue gas adsorption could be promoted. That is why the catalytic activity and selectivity of the sample A calcined at 250 °C was the best among other samples (Figure 1, Table 1).

Calcination Temperature (°C)	BET Surface Area (m ² ·g ⁻¹)	Average Crystallite Size (nm)
Not calcined	21.63	43.24
250	42.52	19.62
350	36.76	33.98
450	28.14	38.24

Table 3. Sample A BET surface area at different calcination temperatures.

Table 4. Four ore samples and their BET surface area (calcined at 250 °C).

Samples	BET Surface Area (m ² ·g ⁻¹)	Average Crystallite Size (nm)
Sample A	42.52	19.63
Sample B	26.81	39.64
Sample C	38.87	29.74
Sample D	22.84	42.04

XPS analysis was performed to identify the oxidation state of the surface elements of the iron ore samples. For samples A and D, the binding energy values (in eV) and valence state ratios of O are shown in Table 5. The XPS spectrum of the samples in the Fe2p and O1s regions are shown in Figure 5.

Figure 5A shows the Fe2p spectra of the samples A and D. For sample A, the characteristic peaks of Fe $2p_{3/2}$, Fe $2p_{3/2}$ satellite, Fe $2p_{1/2}$ and Fe $2p_{1/2}$ satellite were located at 710.8, 718.7, 724.7 and 732.5

eV, respectively [30]. Whereas for sample D, the characteristics peaks have shown a little higher BE values (Fe 2p_{3/2} (710.9), Fe 2p_{3/2} satellite (718.9), Fe2p_{1/2} (724.8) and Fe 2p_{1/2} satellite (732.9) (in eV)). The Fe2p_{3/2} envelopes of both the samples showed multiple splitting spectra and are in good agreement with the Gupta and Sen (GS) multiples [30]. The fitted 2p_{3/2} envelopes in the samples correspond well to the presence of iron oxide in the Fe^{3+} state [31]. The result is in good agreement with the XRD data (Figures 3 and 4). The XPS spectrum of the Samples A and D in the O1s region is shown in Figure 5B. After deconvolution of the peaks, the O1s spectra peaks of both of the samples can be separated into three peaks. According to the literature [32], the peak at the lower BE around 529.9 eV corresponds to the lattice oxygen (denoted as $O\beta$); the second one at a bit higher BE value around 531.4 eV corresponds to the surface adsorbed oxygen (denoted as $O\alpha$); the third peak around 532.6 corresponds to the peak originates from chemisorbed water (indicated as $O\gamma$). It is reported that surface chemisorbed oxygen $(O\alpha)$ is highly active in the oxidation reaction because of its higher mobility than the lattice oxygen $(O\beta)$ [33], and the high SCR activity could be correlated with the high relative concentration ratio of $O\alpha/O\alpha + O\beta + O\gamma$ on the surface of the catalyst. As shown in Table 5, the concentration ratio of $O\alpha/(O\alpha + O\beta + O\gamma)$ of sample A was 44%; whereas, the concentration ratio of sample D was 39%. Therefore, the higher NO conversion of sample A could be due to higher values of surface chemisorbed oxygen ($O\alpha$).



Figure 5. XPS spectrum of (A) Fe2p; (B) O1s of sample A and sample D, calcined at 250 °C.

Samples	Οβ		Οα		Ογ		$= AO_{\alpha}/A(O\alpha + O\beta + O\gamma) (\%)$
1	BE (eV)	Area	BE (eV)	Area	BE (eV)	Area	
Sample A	529.9	7841	531.4	10784	532.6	5483.9	44
Sample D	529.8	7016	531.4	6117	532.6	2469.5	39

Table 5. Comparison of samples A and D: binding energies and valance state ratio of O.

To examine the redox properties of samples A and D, temperature-programmed reduction (H₂-TPR) experiments were conducted. Generally, the hydrogen consumption peaks located at 250–500 °C are attributed to surface lattice oxygen, and peaks at 500–700 °C are attributed to bulk lattice oxygen [34]. Figure 6A shows the H₂-TPR profiles of samples A and D. It can be seen that two well-separated reduction peaks were present in the H₂-TPR profiles of the catalysts. Surface lattice oxygen was credited with the first stage of the reduction process from hematite to magnetite (α -Fe₂O₃ \rightarrow Fe₃O₄) in the low-temperature peak, and the bulk lattice oxygen was responsible for the reduction of magnetite to metallic iron (Fe₃O₄ \rightarrow Fe) in the high-temperature peak. In point of fact, with a sample heating rate of 5.5 °C per minute and higher, two heavily overlapped peaks could be observed in the high-temperature region (as shown in Figure 6A). That is why the reduction of magnetite was believed to happen in a two-step magnetite reduction sequence, i.e., 2Fe₃O₄ \rightarrow 6FeO \rightarrow 6Fe [35]. Sample D was

characterized by four different reduction peaks at 297 °C, 368 °C, 528 °C and 638 °C, corresponding to the reduction of Fe_2O_3 to Fe_3O_4 (297 °C, 368 °C), Fe_3O_4 to FeO (528 °C), and FeO to Fe (638 °C) [36,37]. However, the results exhibited that the corresponding temperatures to the reduction peaks have shifted to lower values for the sample A, which indicated higher mobility of the oxygen species in the sample A. Since the reducibility can be indicated by the reduction peak temperature, the lower reduction peak temperature indicated the stronger reducibility. Therefore, the catalytic activity of sample A was better than that of sample D.

One of the main processes of the NH₃–SCR reaction is the adsorption and activation of ammonia on the acid sites that are present on a catalyst's surface. To examine this, NH₃–TPD experiments were conducted. It can be seen from Figure 6B that the samples have three NH₃ desorption peaks from 50~500 °C. For sample A, two desorption peaks can be observed at 135 °C and 192 °C, which can be attributed to NH⁴⁺ bound to weak Brønsted acid sites [38]. Whereas, the third peak is centered at 267 °C (strong peak), respectively. The peak above 200 °C can be ascribed to NH⁴⁺ bound to strong Brønsted acid sites, and the coordinated NH₃ bound to Lewis acid sites [39,40]. So NH₃–TPD results showed the presence of both Lewis and weak Brønsted acid sites in the catalysts for ammonia adsorption. It is interesting to note that the peak area of Lewis acid sites and weak Brønsted acid sites are obviously larger than those of sample D. The peak area implies the amount of ammonia adsorption in the sample [19], and this indicated that sample D has less number of acid sites than the sample A. Therefore, the catalytic activity and selectivity of the sample A was higher than the sample D.



Figure 6. (A) H₂-TPR profiles; (B) NH₃-TPD profiles of samples A and D, calcined at 250 °C.

A scanning electron microscope was used to observe the influence of calcination on the micromorphology of the iron ore sample A (Figure 7). It can be seen from Figure 7A,B that calcination of the sample at 250 °C resulted in the formation of an amorphous structure of the iron ore, which is also shown by the XRD results (Figure 4A). An amorphous structure usually has a higher surface area than a crystallized structure [21].

Therefore, the BET surface area of the sample A calcined at 250 °C is much higher than that of the non-calcined sample (Table 3). However, with a rise in calcination temperature the aggregated particles appeared due to the sintering phenomenon which becomes a worse further increase in calcination temperature (Figure 7C,D). This sintering phenomenon caused a decrease in the surface area (Table 3) and consequently the number of active sites for the SCR reaction. So, the calcination temperature of 250 °C was found suitable for the iron ore sample to achieve optimum NH₃–SCR performance at low temperatures.



Figure 7. SEM images of sample A: (A) Not Calcined; calcined at (B) 250 °C; (C) 350 °C; and (D) 450 °C.

2.4. Influence of H₂O and SO₂ on SCR Activity

The influence of SO₂ and H₂O on the SCR activity was investigated at 200 °C (Figure 8). To test SO₂ tolerance, 150 ppm SO₂ was added to the simulated flue gas after 50 min of stable reaction. It can be seen that the NO conversion showed a negligible decrease and the NO conversion still remained above 85% after 100 min. However, the NO conversion decreased from 85% to 65% in 200 min, and after that, the NO conversion became almost stable. When the SO₂ feed was stopped after 400 min, the NO conversion was restored to some extent. Compared with the previous reports [41,42], our experiments exhibited that the iron ore sample had better tolerance to SO₂ at 200 °C in one hour of added SO₂. However, after this time, substantial deactivation occurred due to the formation of sulfates on the surface of the catalyst, which resulted in a sharp decrease in NO conversion. The coexistence of H₂O and SO₂ led to more catalyst deactivation to the addition of a single gas (SO₂), because H₂O can compete with the gaseous NH₃ for the active sites [43]. When 5 vol % H₂O and 150 ppm SO₂ were added to the simulated flue gas after 50 min of stable reaction, the synergy effects of the H₂O and SO₂ could be seen on the NO conversion of the iron ore catalyst.

To authenticate the formation of ammonium sulfates the FT-IR analysis of the fresh and the deactivated sample was carried out, and the results are shown in Figure 9. By comparison, some new bands at 1117, 1400 and 3250 cm⁻¹ were found in the spectra of the sample poisoned by the SO₂ gas. The new bands at 1117 and 1400 cm⁻¹ are credited to the adsorption peak of SO₄²⁻ [44,45], whereas, the band at 3250 cm⁻¹ is ascribed to the corresponding N–H stretching vibration of NH⁴⁺ ions [42]. These results showed that sulfate salts such as (NH₄)₂SO₄ and NH₄HSO₄ were formed during the SCR reaction on the iron ore sample, which could cause pore plugging and result in a reduction of the catalytic activity.



Figure 8. Influence of H₂O and SO₂ on SCR activity at 200 °C. Reaction conditions: 500 ppm NO, 500 ppm NH₃, 3 vol % O₂, 150 ppm SO₂, 5 vol % H₂O (when used), flow rate of 145 mL·min⁻¹, N₂ balance, and GHSV = 20,000 h⁻¹.



Figure 9. FT-IR spectra of fresh sample and the sample after SO₂ poisoning.

3. Materials and Methods

3.1. Materials and Reagents

In this study, four iron ore raw materials from different locations were taken and processed to be used as catalysts. Among them, two were mined in Australia and the other two in Brazil. To prepare the catalysts, the raw materials were processed as follows: At first, the iron ore raw materials were dried at 105 °C for 4 h, and then ZM-200 Ultra Centrifugal Mill (Retsch, Germany) was used to ground the ore to make 100-mesh powder. Then, these ground samples were again dried at 105 °C for 5 h. Finally, these ground samples were calcined at 250 °C, 350 °C and 450 °C, respectively, for 6 h to obtain the catalysts.

3.2. Experimental Setup and Governing Equations

The experimental setup consisted of a simulated flue gas system, an electrically heated test rig, a fixed-bed quartz reactor and a flue gas analyzer system. The reactor was made of quartz glass (6 mm i.d \times 500 mm length). A K-type thermocouple of 2 mm diameter with an accuracy of 2.5 °C was inserted into the reactor to obtain the data of the flue gas temperature from the reactor inlet and outlet. The catalyst powder (500 mg) was loaded inside the reactor and was heated to the desired temperature by an electrically heated test rig. The reaction gas consisted of 500 ppm NO, 500 ppm NH₃, 3 vol % O_2 , 150 ppm SO₂ (when used), 5 vol % H_2O (when used), with balance N_2 at a total flow rate of 145 mL·min⁻¹ and gas hourly space velocity (GHSV) of 20,000 h⁻¹. Water vapors were generated by passing N2 through a heated gas-wash bottle containing deionized water. Mass flow controllers (MFCs) (CS200A, CS200D, Sevenstar, Beijing, China) were used to control the flow of simulated flue gas. A flue gas analyzer (Testo 350, Lenzkirch, Germany) was used to constantly monitor the concentrations of NO, NO₂, O₂ and SO₂. To test N₂ selectivity, the outlet gas compositions were detected by GC-14C with Porapak Q column (Shimadzu, Kyoto, Japan) and FT-IR spectrometer (Vertex70v, Billerica, USA) with a scanning range of 4000–400 cm⁻¹, 0.15 cm⁻¹ resolution and an average of 32 scans for each spectrum. By using the concentration of gases at steady state, the NO conversion and N₂ selectivity were calculated according to the following equations:

NO conversion (%) =
$$\frac{[\text{NO}]_{in} - [\text{NO}]_{out}}{[\text{NO}]_{in}} \times 100\%$$
(1)

$$N_{2} \text{ selectivity } (\%) = \frac{[NO]_{in} + [NH_{3}]_{in} - [NO]_{out} - [NH_{3}]_{out} - 2[N_{2}O]_{out}}{[NO]_{in} + [NH_{3}]_{in} - [NO]_{out} - [NH_{3}]_{out}} \times 100\%$$
(2)

where [NO]_{*in*} represents the NO concentration at the inlet of the reactor (ppm), and [NO]_{*out*} represents the NO concentration at the outlet of the reactor (ppm).

Both NO and NH₃ oxidation tests were conducted in the same reactor with a 500 mg sample. For NO oxidation, the feed gas consisted of 500 ppm NO, 3 vol % O₂, and balance N₂. For NH₃ oxidation, the feed gas consisted of 500 ppm NH₃, 3 vol % O₂, and balance N₂. The total flow rate was 145 mL·min⁻¹. The NO to NO₂ conversion percentage was calculated using the following equation:

NO to NO₂ conversion (%) =
$$\frac{[NO_2]_{out}}{[NO]_{in}} \times 100\%$$
 (3)

The NH₃ conversion percentage was calculated using the following equation:

NH₃ conversion (%) =
$$\frac{[NH_3]_{in} - [NH_3]_{out}}{[NH_3]_{in}} \times 100\%$$
 (4)

where $[NH_3]_{in}$ and $[NH_3]_{out}$ were the concentration of NH_3 in the inlet and outlet flue gases, respectively (ppm).

The Scherrer formula is shown as follows.

$$D = 0.94 \times \lambda / (\beta \times Cos\theta) \tag{5}$$

where *D* represents the average diameter of crystallite, λ denotes the wavelength of the incident X-ray, β is the half-width of the diffraction peak, and θ is the diffraction angle.

3.3. Characterization Used

X-ray powder diffraction (XRD) measurements were carried out to determine the crystalline structures of the catalysts with CuK α radiation on a D8 Advance X-ray diffractometer (Bruker, Billerica,

USA). The scan rate of diffraction pattern was 1° min⁻¹, with a resolution of 0.02° and the diffraction pattern was taken in a 2θ range of 10~90°.

An XRF-1800 sequential X-ray fluorescence spectrometer (Shimadzu, Japan) was used to carry the elemental analysis of the ore samples.

An Autosorb-IQ3 (Quantachrome; Anton Paar, Austria) analyzer was used to determine the Brunauer-Emmett-Teller (BET) surface properties of the catalysts. To examine the surface characteristics of the catalysts, the samples were undergone by N_2 adsorption at 77 K, and after that, the samples were degassed under vacuum for 12 h at 180 °C.

X-ray photoelectron spectroscopy (XPS) analysis was performed on an AXIS Ultra DLD (Shimadzu Kratos, Kyoto, Japan) X-ray photoelectron spectrometer with a spherical mirror and concentric hemispherical detector operating at constant pass energy (PE = 46.95 eV). All binding energies (BE) were referenced to the C1s line at 284.6 eV.

A Scanning electron microscope (SEM) S-3400 (Hitachi, Tokyo, Japan) was used to study the micromorphologies of the catalysts.

An AutoChem II 2920 (Micrometrics, Norcross, USA) instrument was used to conduct temperature-programmed reduction (H₂-TPR) experiments. Each catalyst (100 mg) was placed in a quartz U-tube reactor to conduct the experiment. The samples were pretreated in He at 100 °C for 1 h before reduction and then cooled to a temperature of 50 °C. Then the samples were heated from 50~700 °C with a heating rate of $5.5 \,^{\circ}\text{C}\cdot\text{min}^{-1}$ and were simultaneously introduced to a mixture of gases (90% Ar and 10% H₂) with a flow rate of 0.03 L·min⁻¹. A thermal conductivity detector (TCD) was used to determine the content of H₂ in the effluent gas.

An AutoChem II 2920 (Micrometrics, USA) instrument was used to conduct temperature-programmed desorption (NH₃–TPD) experiments. Each catalyst (100 mg) was placed in a quartz U-tube reactor to conduct the experiment. The samples were pretreated at 100 °C in He gas atmosphere with a flow rate of 0.03 L·min⁻¹ for 2 h. After that, the samples were cooled to a temperature of 50 °C, and at this temperature, the samples were fed with a mixture of gases (10% NH₃ and 90% He) until saturation. Then, He gas was used for cleaning the samples. After this, the samples were heated to 550 °C with a heating rate of 10 °C·min⁻¹.

A Fourier transform infrared spectrometer Nicolet 6700 (Thermo Fisher, Waltham, USA) with spectral range 4000–400 cm⁻¹ was used to identify the sulfur-based species present on the surface of the deactivated catalyst.

4. Conclusions

In this work, iron ore raw materials from different locations were taken and processed to be used as catalysts for the NH₃–SCR of NO at low temperatures. The existence of the γ -Fe₂O₃ (maghemite) phase along with a suitable calcination temperature was found crucial for the NH₃–SCR performance of the iron ore at low temperatures. It was found that sample A (composed mainly of α -Fe₂O₃ and γ -Fe₂O₃) calcined at 250 °C exhibited poor crystallinity, large surface area, high concentration of surface-adsorbed oxygen, good reducibility, lots of acid sites, as well as adsorption of the reactants, which brought about excellent SCR activity (above 80% at 170–350 °C) and N₂ selectivity (above 90% up to 250 °C) at low temperatures. However, the addition of H₂O and SO₂ in the feed gas showed some adverse effects on the SCR activity.

FT-IR analysis confirmed the presence of sulfate salts $((NH_4)_2SO_4 \text{ and } NH_4HSO_4)$ during the SCR reaction in the presence of SO₂, which could cause pore plugging and result in the suppression of the catalytic activity.

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Fe Speciation in Iron Modified Natural Zeolites as Sustainable Environmental Catalysts

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Abstract: Natural purified mordenite from Palmarito de Cauto (ZP) deposit, Cuba, was subjected to a hydrothermal ion exchange process in acid medium with Fe^{2+} or Fe^{3+} salts ($Fe^{2+}ZP$ and $Fe^{3+}ZP$). The set of samples was characterized regarding their textural properties, morphology, and crystallinity, and tested in the NO reduction with CO/C₃H₆. Infrared spectroscopy coupled with NO as a probe molecule was used to give a qualitative description of the Fe species' nature and distribution. The exchange process caused an increase in the iron loading of the samples and a redistribution, resulting in more dispersed Fe^{2+} and Fe^{3+} species. When contacted with the NO probe, $Fe^{2+}ZP$ showed the highest intensity of nitrosyl bands, assigned to NO adducts on isolated/highly dispersed Fe^{2+}/Fe^{3+} extra-framework sites and Fe_xO_y clusters. This sample is also characterized by the highest NO sorption capacity and activity in NO reduction. $Fe^{3+}ZP$ showed a higher intensity of nitrosonium (NO⁺) species, without a correlation to NO storage and conversion, pointing to the reactivity of small Fe_xO_y aggregates in providing oxygen atoms for the NO to NO⁺ reaction. The same sites are proposed to be responsible for the higher production of CO₂ observed on this sample, and thus to be detrimental to the activity in NO SCR.

Keywords: natural zeolite; mordenite; Iron exchange; FTIR-NO; HRTEM; NO reduction

1. Introduction

Transition metal ion-exchanged zeolites are being considered for practical applications in diesel and stationary combustion sources' emission control due to good stability at high temperatures and other qualities. Among other metals, iron has shown interesting catalytic properties and it is particularly attractive due to its low cost and non-toxic nature [1]. The activity of Fe-zeolites in the selective catalytic reduction (SCR) of NO_x has been studied in two main processes, i.e., with ammonia (NH₃-SCR) [2–8] and hydrocarbons (HC-SCR) as reducing agents. In the latter case, a variety of compounds, such as C_3H_6 [9], iso and n- C_8H_{18} [10], C_3H_8 [11], iso- C_4H_{10} [12], and C_2H_5OH [13], have been evaluated. Even though NH₃-SCR is recognized among the most efficient deNO_x processes, HC-SRC has the main advantage of using a gas mixture very similar to that found in exhausts [14,15], avoiding the use and related safety/environmental concerns of NH₃ sources. Natural zeolites, such as mordenite, have also drawn attention as sustainable materials due to their ion exchange properties, thermal stability, availability, and low price. Therefore, efficient and low-cost catalysts could be developed from natural mordenite modified with transition metal ions, such as iron.

Several types of iron species, such as isolated or binuclear ions, and iron oxide clusters stabilized in zeolite pores, have been proposed as active sites in NO_x and N_2O decomposition processes. Rutkowska et al. proposed that monomeric Fe^{3+} cations and small Fe_xO_y oligomers in Fe-beta zeolites are more active than larger iron oxide aggregates in the catalytic decomposition and reduction of N₂O [16]. Kim et al. pointed to the activity of small Fe²⁺-enriched iron oxide clusters in zeolite pores, maximized by reduction with hydrogen, in the same reaction [17]. Similar oligonuclear $Fe_x O_y$ clusters, coupled to isolated Fe^{3+} ions, were reported to be active in Fe-containing AlPO-5, where N₂O SCR was carried out with CH₄ in the presence of water vapor and oxygen [18]. The authors also pointed out that larger Fe₂O₃ particles are able to activate both SCR and methane combustion only at temperatures higher than 500 °C. Fe-exchanged MOR, FER, BETA, and ZSM-5 prepared with iron (III) acetylacetonate precursor were shown to present a mixture of Fe³⁺ and Fe²⁺, with catalytic activity in the NO reduction with C_3H_6 dependent on the Fe²⁺/Fe³⁺ ratio, especially at low temperatures [19]. Fe/MOR showed the highest NO_x adsorption capacity and catalytic activity in the 200 to 400 °C temperature range. These few (not exhaustive) examples give a taste about the complexity of iron species that can be formed within zeolite pores. Zeolite's inner (and external) surface is indeed intrinsically rich in sites (negatively charged framework oxygen atoms, defective silanols, and silanol nests) able to stabilize Fe sites with a variety of coordination, nucleation, and oxidation states, strongly affecting their catalytic activity and selectivity [20].

Our team has earlier reported the characterization of a purified natural mordenite from Palmarito de Cauto deposit (Cuba), ion-exchanged by hydrothermal treatments with Fe^{2+} and Fe^{3+} salts. The three samples (parent ZP, Fe^{2+} ZP, and Fe^{3+} ZP, see the experimental section for details) were characterized by diffuse reflectance UV-Vis and Mössbauer spectroscopies [21]. These techniques showed the presence of a large variety of iron species already in the not-exchanged parent material: Highly dispersed Fe ions in extra framework positions, octahedral Fe ions in oligomeric clusters of the Fe_xO_y type inside the channels, and larger iron oxide/hydroxide clusters and Fe_2O_3 particles located on the external surface of the zeolite crystals. After the hydrothermal exchange, the presence of Fe^{2+} and Fe^{3+} in the $Fe^{2+}ZP$ and $Fe^{3+}ZP$ samples, respectively, was confirmed by Mössbauer and UV-Vis. Moreover, iron oxide agglomerates are favored in $Fe^{3+}ZP$, and dispersed cationic species in $Fe^{2+}ZP$. Together with a plethora of oxy-hydroxides clusters/aggregates, Fe^{2+} were proposed to be present in extra-framework positions as a charge compensating cations. The formation of Brønsted sites, likely formed by insertion of Fe^{3+} ions in framework positions during hydrothermal treatment, was moreover assessed by infrared spectroscopy in $Fe^{3+}ZP$.

The use of natural zeolites as catalyst has an intrinsic limitation related to phase purity, which cannot be controlled as carefully as for synthetic ones [22–25]. This also implies that the interpretation of the results can be very complex. On the other hand, these are relatively low-cost catalyst materials and importantly, no templates need to be used for their preparation, thus lowering the environmental impact of the process. With this respect, we here report about a detailed physico-chemical characterization of the set of samples ZP, Fe²⁺ZP, and Fe³⁺ZP, trying to correlate the nature and distribution of present Fe species to the NO storage and conversion in the CO/C₃H₆ SCR of NO, which is used as a test reaction.

2. Results

2.1. Elemental Analysis

The iron content of the starting material ZP, and its exchanged forms $Fe^{2+}ZP$ and $Fe^{3+}ZP$, are 1.55%, 3.06%, and 2.68%, respectively. As discussed with more detail in our earlier paper [21], iron is already present in the natural zeolite sample. However, after the hydrothermal exchange treatments,

the amount of iron increases, as a result of ion exchange of Fe^{2+} and Fe^{3+} with cations present in the natural mordenite, mainly Ca^{2+} and Na^+ .

2.2. Catalytic Activity in HC-SCR

The catalytic activity of the set of samples in the NO reduction with CO/C_3H_6 in the presence of oxygen was measured as a function of temperature, as summarized in Figures 1 and 2. Figure 1 shows the change in the amount of NO and CO₂ in the gas output, monitored from 25 up to 500 °C. Figure 2 reports the NO conversion, which is negligible below 170 °C for all samples. Before carrying out the catalytic test, a steady state concentration of the gas in the flow was reached, around 700 ppm for NO at the reactor outlet. Once this condition was reached, the increase of temperature caused the desorption of the NO absorbed on the catalyst's surface. This can be seen in Figure 1a as a positive peak between RT and 200 to 250 °C. In this interval, no NO conversion is thus observed in Figure 2. Above this temperature, the negative peaks in Figure 1a correspond to NO conversion, as described below. It is well known that adsorption is the primary step in a catalytic reaction. Accordingly, studies reported on the catalytic test with Fe-MOR [19] and Cu-MFI [26] showed that these catalysts both have great capacities for NO adsorption and high catalytic activity for the selective reduction of NO. In agreement with these reports, the amount of NO absorbed/desorbed during the first step of NO interaction (from RT to 200 °C, Figure 1a) is related to the adsorption capacity of the materials. Thus, $Fe^{2+}ZP$ shows a higher NO adsorption capacity with respect to $Fe^{3+}ZP$ and, even more, with the ZP sample (full, dashed and dotted lines, respectively).

Coming to the different catalytic performances of the samples, ZP shows the lowest activity, with a low conversion (8%) starting from 170 °C, as shown in Figure 2. On the contrary, the highest activity is observed for Fe²⁺ZP sample (34%), followed by Fe³⁺ZP (19%), indicating the importance of the ion exchange hydrothermal process in order to increase the population of active sites. The conversion of Fe²⁺ZP is comparable to literature data obtained in similar conditions [19]. Moreover, Fe²⁺ZP shows a reaction onset below 190 °C while Fe³⁺ZP only starts to be significantly active in NO reduction at around 240 °C.



Figure 1. Behavior of the catalytic desorption–reduction of NO with CO/C_3H_6 and O_2 (**a**) and corresponding CO_2 formation (**b**) over the parent zeolite (ZP) and exchanged samples as function of temperature.



Figure 2. Dependence of NO conversion (%) with CO/C_3H_6 on the parent zeolite (ZP) and the exchanged samples as function of reaction temperature.

The formation of CO₂ during NO reduction with CO/C₃H₆ was also followed, and is presented in Figure 1b. The highest CO₂ production is observed on sample Fe³⁺ZP, while Fe²⁺ZP and ZP have similar CO₂ productivity. This trend is not correlated to the zeolite's activity in NO reduction, and can be explained by a direct oxidation of CO and C₃H₆ by O₂. This suggests that sample Fe³⁺ZP, only mildly active in NO reduction, is instead a good oxidation catalyst. This reactivity could be related to the presence of small Fe_xO_y aggregates, providing oxygen atoms and reversible electron transfer involving Fe³⁺/Fe²⁺ ions. The formation of these species after Fe³⁺ insertion in parent ZP was observed by UV-Vis spectroscopy in our previous report [21]. Thus, CO and/or C₃H₆ oxidation may be one of the reasons for the lower activity in NO reduction of Fe³⁺ZP with respect to Fe²⁺ZP.

Although the NO conversion levels achieved by using natural zeolite-based catalysts (included those studied in this work) are not elevated, the related studies provide important knowledge on the iron speciation in the samples and on their reactivity, as discussed in the following where a detailed physico-chemical characterization of the materials is reported.

2.3. XRD Analysis

The XRD patterns of the samples are shown in Figure 3. In parent ZP, the diffraction peaks of the mordenite structure are present, as can be seen in the figure where they are indexed to the (hkl) corresponding crystallographic planes. The diffraction pattern also shows peak related to impurity phases (quartz and clinoptinolite), as labeled in Figure 3. A small change in the intensity of the peaks is observed on $Fe^{2+}ZP$ and $Fe^{3+}ZP$, as is often observed after ion exchange as a consequence of changes in the location and concentration of extra-framework cations in the zeolite channels [27,28]. This suggests that the crystalline structure of mordenite was not altered by the treatment with acid solutions, and that the zeolite is stable under applied conditions.

Besides the changes in intensity mentioned above, a small negative shift (about 0.14 degrees in average) with respect to parent ZP is observed for the position of most of the peaks of sample $Fe^{3+}ZP$, which is instead negligible for $Fe^{2+}ZP$ (Table 1). This corresponds to an increase of the distances between crystallographic planes, and can be associated to an expansion of the zeolite matrix due to the incorporation of iron into the mordenite framework [29,30]. Indeed, this observation is in very good agreement with infrared evidences obtained for the formation of Brønsted Fe(OH)Si sites after hydrothermal treatment with Fe^{3+} [21].



Figure 3. XRD patterns of the samples, with hkl labels of the mordenite structure. Q: quartz, C: clinoptilolite.

Table 1. Peaks position analysis of sample ZP and its exchange form, with the measured negative shift in brackets.

Plane	Peak Position (Shift)				
	ZP	Fe ²⁺ ZP	Fe ³⁺ ZP		
111	13.57	13.55 (0.02)	13.44 (0.11)		
310	15.41	15.40 (0.01)	15.27 (0.13)		
330	19.77	19.74 (0.03)	19.59 (0.15)		
202	25.76	25.76	25.63 (0.13)		
402	31.06	31.04 (0.02)	30.89 (0.15)		

2.4. Textural Properties

The textural properties of the three samples, determined by low-temperature nitrogen sorption measurements, are summarized in Table 2. A small increase in the specific surface area is observed passing from parent ZP to its exchanged forms. This trend can be related to the used exchange process, likely removing impurities or extra-phases (e.g., amorphous volcanic glass) from the zeolite particles' external surface. Moreover, the small increase in total surface area is accompanied by a mild decrease in the micropores' surface area and volume (see last columns of Table 2), in agreement with the formation of low solubility iron oxy-hydroxides phases inside the mordenite channels, as testified by our previous work [21]. This could be explained by a reaction of exchanged iron cations with atmospheric oxygen and OH- groups retained (adsorbed or occluded) in the zeolite pores, which are liberated during the ion exchange. Numerous studies are available in the literature on the occurrence of these processes, mainly during ion exchange [31–35]. Also, Fe³⁺ hydrolysis is expected to occur to a greater extent than that of Fe²⁺ [36,37]. However, we acknowledge that the observed changes are very small, being very
close to the experimental error of 5%, so that formation of occluded particles should be limited to a restricted amount of small clusters/aggregates, in agreement with the absence of extra peaks in the XRD patterns of exchanged samples. No evidence for the formation of mesoporosity (often observed after acid treatment of zeolites) was observed, in agreement with the high stability of mordenite in these conditions.

Sample	SSA _{BET} (m ² /g)	SSA_{Lang} (m ² /g)	SSA _{ext} (m ² /g)	V _{mic} (cm ³ /g)	A_{mic} (m ² /g)
ZP	244	312	3	0.109	241
Fe ²⁺ ZP	259	331	26	0.105	233
Fe ³⁺ ZP	256	328	26	0.104	230

Table 2. Textural properties of the studied samples.

 SSA_{BET} = Specific surface area calculated using the standard Brunauer–Emmet–Teller (BET) method. SSA_{Lang} = Specific surface area, calculated from Langmuir method. SSA_{ext} = External surface area, calculated using the t-plot method. V_{mic} = Micropore volume, calculated using the t-plot method. A_{mic} = Micropore surface area, calculated using the t-plot method.

2.5. HRTEM Analysis

High-resolution TEM was used to investigate the effect of hydrothermal ion exchange on the morphology of the parent natural purified mordenite ZP. Measurements were carried out at 100 kV in order to avoid beam-induced damaging of the zeolite particles [38]. Figure 4 shows the TEM images of ZP sample, which is composed of particles of irregular shape, with sizes in the range of 200 to 400 nm, formed by the agglomeration of smaller particles. The left-hand panel of Figure 4 shows a magnification, allowing us to appreciate the crystalline nature of the zeolite. The measured lattice distance is 0.38 nm, in agreement with the (241) plane of mordenite [39].



Figure 4. HRTEM images of ZP, with magnification of a particle border allowing appreciation of the mordenite lattice planes.

Representative TEM images of $Fe^{2+}ZP$ and $Fe^{3+}ZP$ samples are shown in Figures 5 and 6, respectively. In both cases, the morphology of the main particles is similar to that of ZP sample, with relatively large agglomerates of regular crystalline particles. Smaller particles (1 to 5 nm) can be appreciated in the figure magnifications, which could be related to the clinoptilolite extra phase on the basis of the measured crystallographic fringes.



Figure 5. HRTEM images of Fe²⁺ZP sample. Arrows in the bottom part of left-hand panel indicate the presence of small particles of extra phases. Some of these can be also seen in the right-hand magnification, where particles' size and crystalline fringes' distances were measured.



Figure 6. HRTEM images of $Fe^{3+}ZP$ sample. The left-hand panel reports magnifications of the central image, showing the presence of nanometric-sized particles, likely related to the clinoptilolite extra phase.

EDS microanalysis carried out at different magnifications indicates a large heterogeneity in the iron distribution in all samples. Moreover, this analysis (spectra not reported) shows a difference in the cation exchange capability: While ZP and Fe³⁺ZP samples show the presence of Mg, Na, K, Ca, and Fe, the Fe²⁺ZP sample only presents Ca and Fe, in agreement with previous reports [21].

2.6. NO Adsorption Studies Followed by FTIR

The adsorption of NO or NO₂ on acid- and metal-exchanged zeolites followed by infrared spectroscopy is a well-known method for the characterization of exposed ions, through the formation of adsorbed complexes with characteristic vibrational fingerprints. Moreover, indirect indications about the Brønsted or metal ions' reactivity can be inferred by observing the formation of adsorbed NO/NO₂ reaction products, such as nitrosonium ions NO⁺, nitrates NO₃⁻, nitrites NO₂⁻, and/or water [40–44].

NO adsorption experiments were carried out at room temperature (RT) on ZP, Fe²⁺ZP, and Fe³⁺ZP, after oxidation and reduction treatments. Modifications in the spectra upon dosing NO were observed in the OH stretching (ν OH, from 3800 to 3000 cm⁻¹), in the nitrosonium and nitrosyl (from 2300 to 1700 cm⁻¹), and in the water bending δ (H₂O) and nitrate (from 1750 to 1300 cm⁻¹) regions. Spectra discussion will be mainly focused on the nitrosonium/nitrosyl region, showing the most intense and informative bands.

2.6.1. ZP Sample

The results obtained on the oxidized and reduced ZP sample are shown in Figure 7A and B, respectively. On oxidized ZP, three groups of bands are present: One centered at 2265 cm⁻¹, a second between 2200 and 1920 cm⁻¹, and a third one between 1920 and 1700 cm⁻¹. Some of these are also present in the reduced sample (bottom), though with lower intensity. The first group is formed by an intense band at 2265 cm⁻¹, with shoulders at 2282 and 2251 cm⁻¹, which can be assigned as N₂O formed upon reaction with NO on different Fe^{x+} (x = 2, 3) surface sites on small iron oxide particles [43,45–47].



Figure 7. Infrared spectra in the nitrosonium/ nytrosyl region of NO adsorbed at RT on oxidized (A) and reduced (B) ZP sample, oxidized (C) and reduced (D) $Fe^{2+}ZP$ sample, and oxidized (E) and reduced (F) $Fe^{3+}ZP$ sample. Equilibrium $P_{NO} = 0.4$ mBar (a) and subsequent stepwise evacuation up to dynamic vacuum (e).

Coming to the second group of bands, it is composed of a broad absorption, with a maximum at 2139 cm⁻¹ and a shoulder at 2070 cm⁻¹, with a very broad band centered at 1975 cm⁻¹, which are not present on the reduced sample. Similar bands have been assigned by different authors to NO⁺ [48–50], formed by the reaction of NO with adsorbed oxygen atoms, and with the formation of NO₂, which then reacts with protons to give NO⁺ and water [51]. Similarly, Rivallan et al. proposed that NO₂ is transformed into physisorbed HNO₃, which mediates the formation of NO⁺ ions that exchange zeolite protons [44]. This interpretation is in agreement with the absence of these bands in the reduced sample (B). On the whole, these spectra indicate the activity of oxidized ZP sample in oxidizing NO, thanks to the presence of oxygen atoms, which are likely adsorbed on the surface of small iron oxides.

Finally, the third group of bands in the 1950 to 1700 cm^{-1} region is readily assigned to nitrosylic adducts on Fe²⁺/Fe³⁺ extra-framework sites [44–46]. These bands are very weak on both oxidized and reduced ZP samples and will be described in more detail in the following. Since they are typical of highly dispersed extra-framework iron sites, their low intensity indicates that most iron in this sample is present as large iron oxide particles.

2.6.2. Fe²⁺ZP and Fe³⁺ZP Samples

The infrared spectra measured upon NO adsorption on $Fe^{2+}ZP$ and $Fe^{3+}ZP$ are reported in Figure 7 (C,D and E,F, respectively). In both samples, the set of bands assigned to N₂O adsorbed on Fe^{x+} (x = 2, 3) sites is weaker with respect to that observed on the oxidized ZP sample, in agreement with their assignment to surface sites present on small iron oxide clusters. As for the bands assigned to NO⁺ ions, they have different position and intensity depending on the sample and activation treatment (oxidized or reduced, C,E or D,F, respectively). In detail, the oxidized $Fe^{2+}ZP$ sample shows a main component centered at 2141 cm⁻¹ (shoulder at 2065 cm⁻¹), which is similar to that observed on ZP). As observed on the ZP sample, this band almost disappears after the reduction treatment. On the contrary, a very intense band is observed on oxidized $Fe^{3+}ZP$ at 2155 cm⁻¹, which decreases but still shows considerable intensity after reduction (spectra E and F). This suggests that the reactivity of NO with adsorbed oxygen strongly depends on the nature of the inserted iron species. Namely, this reaction takes place mostly in $Fe^{3+}ZP$, while oxidized ZP and $Fe^{2+}ZP$ have a similar lower activity. The different positions of the NO⁺ band suggest different local environments, which could be due to vicinal iron and Brønsted sites. This is in agreement with our previous results, showing the presence of Fe(OH)Si Brønsted sites in $Fe^{3+}ZP$ [21].

Coming to the nitrosyl region, the oxidized $Fe^{2+}ZP$ sample shows a relatively intense peak at 1878 cm⁻¹, with shoulders at 1902 cm⁻¹ and 1817 cm⁻¹ and a very weak band at 1755 cm⁻¹ (curves C). A much higher intensity is observed after reduction (curves D). A similar trend with a lower intensity is observed on sample $Fe^{3+}ZP$ (curves E). Bands in this spectral region have often been observed on synthetic Fe-zeolites, and are mainly ascribed to highly dispersed Fe^{2+} and Fe^{3+} sites [19,44,45,52,53].

3. Discussion

Several types of iron active sites, such as isolated iron cations, binuclear oxygen-bridged Fe species, iron oxide clusters, hydrocyanic acid, isocyanate species, etc., have been reported for the selective catalytic reduction of NO_x [23,54–56], but their precise assignment remains a controversial issue. We consider that such iron active species are heavily dependent on the applied method to incorporate iron, the used iron source, and the homogeneity of the resulting sample. In this report, the most active sample is the Fe²⁺ZP sample, which also shows the highest dispersity of inserted Fe ions, as probed by NO (intensity of the nitrosyl bands in the 1950 to 1700 cm⁻¹).

The mechanism and the nature of intermediate species in producing N_2 in the selective catalytic reduction of NO_x is also a topic of controversy. Some intermediate species, such as NO_2 , nitrosyl, nitro, nitrate, NO-NO triplet species, and dissociatively chemisorbed NO, have been proposed. Several studies have outlined that NO_2 in particular plays an important role in the reduction of NO_x to N_2 . It has been reported that NO is oxidized to NO_2 with oxygen and then the resulting NO_2 reacts with

hydrocarbons to form an active intermediate [53,57–59]. In our case, NO adsorption shows nitrosyl complexes as primary compounds formed in the most active $Fe^{2+}ZP$, NO⁺ in $Fe^{3+}ZP$, and N₂O in the least active ZP. We can thus tentatively draw a correlation between the abundance of dispersed sites able to add NO as ligand(s) without its disproportionation at RT (bands in the 1950–1700 cm⁻¹ region), and the catalytic activity in NO conversion. On the contrary, neither NO⁺ nor N₂O formation at RT can be directly related to the samples' catalytic activity. In both cases, these features can be associated with the presence of agglomerated particles, in line with early studies by UV-Vis diffuse reflectance and Mössbauer spectroscopies [21].

On the other hand, it is observed that the maximum reduction of NO on Fe²⁺ZP takes place at 410 °C. After this temperature, NO reduction starts to decrease. According to [53], such a decrement can be associated to a shift in the NO adsorption equilibrium (adsorption is usually an exothermic process) and to the properties of iron species active in NO reduction at higher temperatures.

Finally, the reported results also allow for some semi-quantitative considerations about the extinction coefficients of the bands related to different adsorbed species formed upon NO adsorption. As mentioned above, the sample with higher activity ($Fe^{2+}ZP$) is not only characterized by the highest nitrosyl band intensity, but also the highest NO sorption capacity. This should be, at first approximation, related to the overall integrated area of the adsorbed specie. However, by comparing the infrared results of Figure 7, the highest integrated area among the three samples is observed in $Fe^{3+}ZP$, particularly in the nitrosonium region. Since this does not correspond in a higher NO sorption capacity, we can conclude that NO⁺ species are characterized by a higher extinction coefficient with respect to nitrosyl bands.

4. Materials and Methods

A purified zeolite material was obtained from the zeolitic rock of Palmarito de Cauto deposit, via magnetic and gravimetric purifications [60]. This zeolite is a mixture of ~70% of mordenite with other phases (clinoptilolite-heulandite, montmorillonite, quartz, feldspar, and iron oxides). The chemical composition of the sample in oxide form, with the balance as water, is 61.93% SiO₂; 13.42% Al₂O₃; 4.95% CaO; 2.53% Fe₂O₃; 1.14% MgO; 1.52% K₂O; 2.33% Na₂O; and 1.22% FeO. This purified zeolite is referred to as the natural mordenite (ZP).

In order to obtain natural mordenite forms modified with iron, ZP samples with a particle size class of +38–74 μ m, were exchanged at pH = 2 with FeSO₄ and Fe(NO₃)₃ 0.05 N solutions. The exchanges were carried out with a solid/liquid ratio of 1 g/20 mL at 80 °C while stirring for 24 h and replacing exchange solutions after 12 h. The resulting samples were washed (firstly with acidified distilled water and then with distilled water) until nitrate and sulfate anions were totally removed and pH was neutral. They were then oven dried at 100 °C and stored in a desiccator. The ZP forms modified with Fe²⁺ and Fe³⁺ were designated as Fe²⁺ZP and Fe³⁺ZP, respectively.

Elemental analysis of the samples was obtained by flame photometry (Na and K) and atomic emission spectrometry with inductively coupled plasma (Si, Al, Fe, Ca, and Mg) using a Corning 400 photometer and an EPECTROFLAME Modula F spectrometer, respectively. To this aim, the samples were firstly dissolved using a mixture of fluoridric and perchloric acids. Powder X-ray diffraction (XRD) patterns of ZP, Fe²⁺ZP, and Fe³⁺ZP samples were measured with a D8 Advance Bruker X-ray diffractometer (Bruker AXS GmbH, Berlin, Germany) with Cu-K α monochromatic radiation (1.5406 Å) with 40 kV and a current of 20 mA. The XRD patterns were registered in the 2 θ range from 10 to 80° at room temperature (RT). N₂ gas adsorption/desorption isotherms were measured by means of a Micromeritics TriStar II device (Norcross, GA, USA) at liquid nitrogen temperature (–196 °C, LNT). Before the sorption measurements, the samples were pretreated in vacuum for 8 h at 350 °C. High resolution transition electron microscope (HRTEM) images of the samples were registered with a JEOL 3010-UHR microscope (Tokyo, Japan) with an acceleration potential of 100 kV, by dispersing the powdered samples on a copper grid covered with a lacey carbon film. Infrared spectra were recorded on a BRUKER FTIR-66 spectrometer with a resolution of 2 cm⁻¹, using an MCT detector. Measurements were carried out using a home-made cell, allowing in situ thermal treatment, gas dosage, and measurement at RT. Thin self-supporting pellets for transmission measurements (around 10 mg/cm²) were prepared with a hydraulic press. Oxidation treatments were carried out by dosing 60 Torr of O₂ at 550 °C for 1 h after a heating ramp in vacuum. Similarly, reduction activation was carried out at 400 °C for 1 h with 60 Torr of H₂. In both cases, the samples were evacuated before cooling down to RT. NO, carefully distilled, was dosed on the samples at RT after measuring the zeolite-activated reference spectra. Spectra were measured following a stepwise NO pressure (P_{NO}) reduction.

Catalytic activity tests of the samples in the selective catalytic reduction of NO with CO/C₃H₆ were done in a quartz flow reactor, using 100 mg of catalysts, within a 25 to 500 °C temperature interval with a ramp rate of 5 °C/min. The NO (0.09%), C₃H₆ (0.22%), O₂ (0.46%), and CO (1.179%) reaction mixture was prepared by mixing individual flows with mass-flow controllers. A total flow of 55 mL/min was obtained using N₂ as a diluent. Effluent gases were analyzed with a CAI ZRE gas analyzer. Before the catalytic test, the samples were pretreated in oxygen flow (0.5% in N₂) up to 350 °C with ramp rate of 5 °C/min. The temperature was then decreased to 25 °C and the flow was switched to the reaction mixture.

5. Conclusions

Iron-mordenite forms (Fe²⁺ZP and Fe³⁺ZP) were obtained from natural purified mordenite from Palmarito de Cauto (ZP) deposit, Cuba, by hydrothermal ion-exchange processes in acid medium with Fe²⁺ and Fe³⁺ cations. Only small variations were observed in the samples' crystallinity and textural properties after ion exchange, the latter ascribed to the dissolution in the acidic environment of large iron oxide particles from the zeolite external surface with parallel formation of small Fe_xO_y clusters within the zeolite pores. In Fe³⁺ZP, a shift in the diffraction peaks' angular position was observed, which corresponds to an increment in the inter-planar distance and expansion of the zeolite matrix due to the incorporation of Fe³⁺ into the mordenite framework.

The activity in HC-SCR (used as a reaction test) was found to be dependent upon the ion exchange process, with $Fe^{2+}ZP$ showing the highest catalytic activity, followed by $Fe^{3+}ZP$ and ZP samples. The same order $Fe^{2+}ZP >> Fe^{3+}ZP >> ZP$ was also observed in the NO sorption capacity of the samples at low temperatures (<170–200 °C).

In agreement with these results, FTIR-NO studies showed a higher intensity of the nitrosyl bands formed upon NO adsorption on the Fe²⁺ZP sample. These bands (present on both oxidized and reduced samples) are related to isolated/highly dispersed Fe^{2+}/Fe^{3+} ions in extra-framework positions, which are more abundant in Fe²⁺ZP and are responsible for the high sorption capacity (and likely activity) of this sample. On the contrary, the intensity of nitrosonium ions NO⁺, formed upon reaction of NO with oxygen and likely protons, and more abundant on Fe³⁺ZP sample, could not be related to neither NO sorption capacity or activity.

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Article

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Oxidative Degradation of Trichloroethylene over Fe₂O₃-Doped Mayenite: Chlorine Poisoning Mitigation and Improved Catalytic Performance

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Abstract: Mayenite was recently successfully employed as an active catalyst for trichloroethylene (TCE) oxidation. It was effective in promoting the conversion of TCE in less harmful products (CO₂ and HCl) with high activity and selectivity. However, there is a potential limitation to the use of mayenite in the industrial degradation of chlorinated compounds—its limited operating lifespan owing to chlorine poisoning of the catalyst. To overcome this problem, in this work, mayenite-based catalysts loaded with iron (Fe/mayenite) were prepared and tested for TCE oxidation in a gaseous phase. The catalysts were characterized using different physico-chemical techniques, including XRD, ICP, N₂-sorption (BET), H₂-TPR analysis, SEM-EDX, XPS FESEM-EDS, and Raman. Fe/mayenite was found to be more active and stable than the pure material for TCE oxidation, maintaining the same selectivity. This result was interpreted as the synergistic effect of the metal and the oxo-anionic species present in the mayenite framework, thus promoting TCE oxidation, while avoiding catalyst deactivation.

Keywords: trichloroethylene; mayenite; catalytic oxidation; iron; chlorine poisoning

1. Introduction

Trichloroethylene (TCE) is a chlorinated volatile organic solvent belonging to the class of dense non aqueous phase liquids (DNAPL) pollutants [1–3]. Several strategies have been considered for TCE remediation, including the use of CaO [4], bioremediation [5,6] and adsorption processes with activated charcoal or zeolites [7,8]. In addition, as TCE is highly volatile, it can be easily stripped from the remediation media (water, surfactant solutions, removed soils, etc.) with air flux and directed to further treatments in gas phase [9,10]. In this respect, catalytic heterogeneous oxidation is becoming a popular alternative to thermal incineration for treating exhausted gases rich in TCE, as catalysts lower operative temperatures and improve selectivity of the reaction towards less harmful products, with high benefits in terms of energy consumption and environmental impact.

Several heterogeneous catalysts have been developed and tested for gaseous TCE oxidation. Catalytic systems based on noble metals, particularly Pt and Pd, have been extensively employed, showing good results in terms of activity and selectivity, as reported by Gonzalez-Velasco and co-workers in a recently published review [11]. Less-expensive catalysts, based on metallic oxides, have

also been prepared as uniform catalyst or supported on high surface materials (e.g., γ -Al₂O₃) [12,13]. Blanch-Raga et al. reported the oxidation of TCE over different mixed oxides derived from hydrotalcites [14], with the Co(Fe/Al) catalyst being the most active ($T_{50\%} = 280$ °C and $T_{90\%} = 340$ °C at Gas Hourly Space Velocity, GHSV = $15,000 \text{ h}^{-1}$ and [TCE] = 1000 ppm) due to its acidic and oxidative properties. Zeolites also represent an important type of active catalysts for the oxidation of TCE and many papers have reported on the synergic effect of acidic sites in zeolites [15] with metal catalysts in order to improve the performance of the whole catalytic system. Romero-Saez et al. [16], studied the performance of iron-doped ZSM-5 zeolite for TCE oxidation, finding that a ZSM-5 containing 2 wt% of Fe quantitatively oxidizes 1000 ppm of TCE at 500 °C and GHSV = $13,500 \text{ h}^{-1}$. This paper shows that the formation of active iron (III) species, as Fe₂O₃ nanoparticles, was most likely responsible for the enhanced catalytic performance of the zeolite. Nevertheless the catalyst suffers some deactivation after 16 h of reaction due to the formation of FeCl₃ [16]. Recently, Palomares et al. reported a remarkably high selectivity towards CO₂ during TCE oxidation with Cu and Co-doped beta zeolites. The best results ($T_{50\%}$ = 310 °C and $T_{90\%}$ = 360 °C at GHSV = 15,000 h⁻¹ and [TCE] = 1000 ppm) were obtained by using Cu-doped zeolite, which combined the acid sites of the zeolite with the redox properties of the copper ions [17]. Notwithstanding, zeolites-based catalysts suffer some drawbacks, which include coke formation, deactivation, and formation of chlorinated by-products [14].

In previous works, we reported about the oxidation of TCE by using the mesoporous calcium aluminate mayenite ($Ca_{12}Al_{14}O_{33}$) as a catalyst [18–22]; mayenite had a good overall performance, showing high activity and selectivity towards nontoxic compounds, and fair thermal stability and recyclability. As a main drawback, the material shows a certain tendency towards chlorine poisoning, leading to slow deactivation of the catalyst. Mayenite has a zeolite-type structure with interconnected cages and a positive electric charge per unit cell that is balanced by O^{2–} ions (free oxygen ions) [23]. The free oxygen ions can be substituted by other species (Cl⁻, H⁻, NH₂⁻, etc.) [24,25] and can migrate from the bulk to the surface at temperatures higher than 400 °C [26], thus conferring to the mayenite oxidative properties exploited for many applications [27–29]; for instance, as Ni support for the catalytic reforming of tar [30–32].

With the aim of further improving mayenite activity for TCE oxidation and mitigating deactivation of the material, in this work, we use a mayenite containing iron that is employed for the catalytic oxidation of TCE. The performance of the system has been evaluated by means of the light-off curve and the structural properties of the material have been characterized, before and after the reaction, by means of different physico-chemical techniques, including XRD, ICP analysis, N₂-sorption (BET), H₂-TPR analysis, SEM-EDX, FESEM-EDS, XPS, and Raman spectroscopy. We have prepared catalysts with different iron content and compared the activity and stability of this material with those of pure mayenite.

2. Results and Discussion

Figure 1 shows the XRD patterns of mayenite and Fe/Mayenite loaded with 2% of Fe₂O₃ (1.5% Fe/mayenite has an identical spectrum). The mayenite XRD pattern presented typical peaks of mayenite around $2\theta = 18.1^{\circ}$, 30° , 33.4° , 36.7° , 41.2° , 46.7° , 55.2° and 57.4° . Ca₃Al₂O₆ (\bullet) and CaAl₂O₄ (Δ) were also found as impurities formed during the mayenite preparation processes [33].



Figure 1. XRD patterns of mayenite (black) and 2.0% Fe/mayenite (blue).

The Fe/mayenite catalyst clearly maintains the crystalline structure of mayenite. Furthermore, no peaks associated with iron oxides were observed in the Fe/mayenite samples; this is due to the low metal loading in the mayenite and their good dispersion on the mayenite support [34].

Table 1 shows the metal loading and specific surface area of the catalysts. The BET surface area of mayenite was 11.7 m²/g, in line with data reported for this type of material [27]. The Fe/mayenite samples had BET surface area values similar to that of mayenite, showing that the incorporation of iron does not modify its textural properties. ICP analysis confirmed that the iron content was close to the nominal value.

Catalyst	Fe Content (wt.%)	BET Surface Area (m ² /g)	
Mayenite	-	11.7	
1.5% Fe/mayenite	1.72	11.5	
2.0% Fe/mayenite	2.30	11.2	

Table 1. Iron content and BET surface area of the catalysts.

Fe/mayenite is a porous material (view SI, Figure S1), characterized by large pores with dimensions of μ m (macropores) and nm (mesopores) composed of calcium, aluminium, oxygen, and iron with an approximate content of 34%, 40%, 26%, and 2 wt.%, respectively. The structure and composition of the synthetized materials were also characterised by FESEM-EDS analysis, which yielded similar results, but allowed a detailed distribution of the atomic content. Figure 2 shows the results obtained, observing the most abundant elements in mayenite, i.e., aluminium, calcium, and oxygen. Iron atoms appear in low quantity and with a homogenous distribution in the mayenite, demonstrating good iron dispersion on the mayenite support. Moreover, the FESEM images of Fe/mayenite and pure mayenite (not shown) showed no significant differences in terms of morphology, maintaining the typical morphology of mayenite in both cases.



Figure 2. (a) FESEM micrograph (magnification of \times 5500) of Fe/mayenite; atomic mapping of Fe/mayenite: (b) Al (purple); (c) O (green); (d) Ca (blue); (e) Fe (red).

TPR study of the catalysts is reported in Figure 3. All samples have similar hydrogen consumption, but present different TPR profiles. As can be seen, two peaks are observed for mayenite: the first one is a smaller band that appears around 550 °C, while the second is more intense and has the maximum at 620 °C. The first corresponds to the dissociative adsorption of H₂ in a heterolitic fashion [35] and the second to the reaction of these species with extra framework O_x^- and O_2^{2-} anions [36]. Iron-containing mayenites show a different profile with a unique band centred at 550 °C for the sample with 1.5% Fe or at 530 °C for the sample containing 2% Fe. These bands are assigned to the reduction of extra framework O_x^- and $O_2^{2^-}$ anions that in these catalysts are coincident with the band assigned to the dissociative adsorption of H₂ with consequential water formation, as previously reported for iron oxide-based catalysts [37]. Also, a small shoulder at 400–450 °C can be observed in the sample with higher iron content. This shoulder is assigned to the reduction of Fe³⁺ to Fe²⁺, as reported by Romero-Saez et al. for Fe/zeolite samples [16]. Quantification of the hydrogen consumption shows similar results for the different samples, as the main species reduced in all the catalysts are the anionic oxygens present in the mayenite. The low iron content of the Fe/mayenite and the only partial reaction of the Fe³⁺ species results in a negligible consumption of hydrogen compared to that necessary for the oxygen species reduction. The results also show that there is a relationship between the content of iron and the shift towards lower temperatures of the extra framework O_x^- and O_2^{2-} reduction peak. This indicates that there is an interaction between iron species and anionic oxygen, which improves the redox properties of the catalysts containing iron.



Figure 3. H₂-TPR profiles of mayenite (black), 1.5% Fe/mayenite (red), and 2.0% Fe/mayenite (blue).

The synthetized catalysts have been evaluated for oxidation of trichloroethylene by monitoring the conversion percentage calculated by means of Equation (1) as a function of the temperature (light-off curve). As shown in Figure 4, 2.0% Fe/mayenite has the best conversion rate among the different catalysts tested.



Figure 4. TCE conversion in wet conditions for mayenite (black), 1.5% (red), and 2.0% (blue) Fe/mayenite.

Blank experiments performed without a catalyst showed no significant TCE conversion below 550 °C. T_{50} and T_{90} (temperature at which 50% and 90% of the TCE was depleted, respectively) were found significantly lower for Fe/mayenite, with respect to pure mayenite (Table 2). In particular,

pure mayenite, used as a reference, showed $T_{50} = 410$ °C and $T_{90} = 550$ °C; 2.0% Fe/mayenite has a $T_{50} = 300$ °C and $T_{90} = 460$ °C and for 1.5% Fe/mayenite T_{50} was found slightly higher (375 °C), whilst T_{90} was the same as 2.0% iron-loaded mayenite. Conversion rates at 365 °C were also calculated according to Equation (2) for the three catalysts and reported in Table 2. Preliminary experiments revealed that an iron loading higher than ~2% in the mayenite did not significantly improve the conversion performance.

Catalyst	T ₅₀ (°C)	T ₉₀ (°C)	Conversion Rate (mol g ⁻¹ s ⁻¹)
Mayenite	410	550	5.58×10^{-6}
1.5% Fe/mayenite	375	460	7.14×10^{-6}
2.0% Fe/mayenite	300	460	1.05×10^{-5}

Table 2. Catalysts activity in terms of T₅₀ and T₉₀ and conversion rate at 365 °C.

The results show an increased catalytic activity of mayenite in the presence of iron. This can be explained by the synergistic effect of dispersed iron with the ionic oxygen species (O^{2^-} and $O_2^{2^-}$) present in the mayenite framework. In fact, iron species have a twofold role: *i*) they are active oxidants [11,16] and, *ii*) they make easier the interaction of the atmospheric O_2 to form O^{2^-} and $O_2^{2^-}$, responsible for the TCE oxidation [26]. Both roles result in improved redox and catalytic properties for Fe/mayenite, when compared with pure mayenite, as the TPR and catalytic results have shown.

The results of selectivity tests showed that, for all the catalysts, CO_2 and CO were the main oxidation reaction products (CO/CO_2 ratio was 50:50 for all the investigated temperatures and catalysts), while only HCl was detected as a chlorinated product.

2% Fe/mayenite stability was evaluated for several hours (12 h) at stationary conditions (T = 460 °C, 1700 ppm TCE, GHSV = 6000 h⁻¹, 0.8 g of catalyst). As highlighted in Figure 5, the presence of iron on the mayenite surface drastically improved the stability of the material. Indeed, after 2 h of reaction, pure mayenite showed a significant loss in activity, whilst 2.0% Fe/mayenite retained catalytic activity. Only a partial deactivation of the 2% Fe/mayenite catalyst was observed after 12 h of reaction, decreasing the conversion from 95% to 80%.



Figure 5. Comparison of catalyst stability (T = 460 °C, 1700 ppm TCE, GHSV = 6000 h^{-1} , 0.8 g of catalyst).

These results are interesting because stability of the catalyst is essential for possible commercial use of the material. As reported in previous works, the deactivation mechanism of mayenite catalyst is related with the displacement of active oxygen species by chloride ions [19,20,24,25]. In particular, the formation of HCl during the reaction caused a partial irreversible substitution of the anionic oxygen species $(O_x^{x^-})$ by chloride ions forming chloromayenite [19,22], with consequent deactivation of the catalyst. It is observed that the presence of iron in mayenite modifies this mechanism, probably because the Fe species catalyze the interaction of the atmospheric O_2 to form O^{2-} and O_2^{2-} , making reversible the substitution of chloride ions by oxygen and avoiding or diminishing the formation of chloromayenite. In order to understand the role of iron in improving the stability of the material, XRD, SEM-EDX, FESEM-mapping, XPS, and Raman analyses of fresh and used catalysts were performed. XRD patterns and SEM images did not show important differences before and after the reaction, indicating a high structural stability of the material both in the absence and in the presence of iron (see Supplementary Materials for details, Figures S2 and S3a). Nevertheless, the EDX spectrum (Figure S3b) of the 2% Fe/mayenite sample after the stability test shows the presence of chloride. This is clearly observed in Figure 6 with the atomic mapping of Fe/mayenite after reaction. Comparing these images with those of the catalyst before reaction (Figure 2), it is observed that after the 12 h reaction, mayenite has the same morphology and distribution as Ca, Al, O and Fe atoms, revealing high stability of Fe/mayenite. It is observed that iron atoms do not agglomerate after reaction, indicating high stability of the metal supported on the mayenite. The main difference with the material before reaction is the presence of Cl atoms (orange points). The Cl mapping shows that this element has the same distribution as Ca atoms, suggesting that Cl is mainly interacting with Ca, because the basic properties of this element favour interaction with an acidic molecule as HCl. Different distribution of Cl and Fe atoms suggests that $FeCl_3$ was not formed, as it occurs in zeolites [16], indicating a high stability of the Fe species not poisoned by the chloride present on the catalyst surface.



Figure 6. (a) FESEM micrograph (magnification of \times 5500) of post-reaction Fe/mayenite; atomic mapping of post-reaction Fe/mayenite: (b) Al (purple); (c) O (green); (d) Ca (blue); (e) Fe (red); (f) Cl (orange).

The full XPS spectra of the mayenite containing iron before and after reaction are shown in Fig S4, where a peak at 200 eV is observed in the sample after reaction corresponding to the binding energy of Cl (2p) with two contributions at 200 and 189.7 eV, characteristic of Cl $(2p_{3/2})$ and Cl $(2p_{1/2}$ for ionic chlorine (Cl⁻) [38]. The presence of this peak in the sample after reaction coincides with a decrease in the relative intensity of the O peak at 530.9 eV due to the oxygen surface species consumption during the reaction. On the other hand, Figure 7 shows a complex multiplet-split Fe 2p XPS spectra.

At least two contributions are observed: the first one is centred at 709.5 eV and the second, which is more intense, is centred at 711.8 eV. These peaks have been assigned to Fe^{2+} ($2p_{3/2}$) and Fe^{3+} ($2p_{3/2}$), respectively, indicating the formation of Fe_2O_3 , probably together with Fe_3O_4 [38,39]. After reaction, an increase in the band centred at 711.8 eV, together with a small shift to the highest eV, is observed; it could be related with the disappearance of the Fe^{2+} contribution in the Fe_3O_4 phase or the formation of $FeCl_3$ [39]. These results reveal that after 12 h of reaction, part of the HCl formed in the reaction interacts with the mayenite and some chloride species are formed on the catalyst surface. Nevertheless, these species are not irreversibly adsorbed on the ionic vacancies (as in the case with pure mayenite [19,22]) and oxidant centres (anionic oxygen) are present after reaction. This is due to a synergic action of the iron present in the mayenite surface, which catalyses $O_x^{x^-}$ regeneration with the gas-phase oxygen present in the reaction media.



Figure 7. XPS spectra for the Fe (2p) of the Fe/mayenite (2% Fe) before and after reaction.

To understand this process better, Raman spectroscopy studies were conducted; the results are given in Figure 8. It is shown that in Fe/mayenite, the signal for oxygen O_2^- at 1075 cm⁻¹ is preserved after the catalytic test. Similar results were obtained in the XPS analysis of the samples after reaction (see Supplementary Materials). This does not occur with pure mayenite [19,22], demonstrating that the redox properties of iron catalyze the regeneration of anionic oxygen by the O_2 present in the gas feed and avoid the irreversible chlorine poisoning of mayenite.



Figure 8. Raman spectra of Fe/mayenite (2.0%), fresh (top) and after reaction (bottom).

These results clearly show that the presence of well-dispersed iron on the mayenite surface improves the redox properties of the mayenite together with its stability, due to the ability of iron to catalyse the regeneration of the anionic oxygen responsible for TCE oxidation.

3. Materials and Methods

3.1. Materials

Trichloroethylene, calcium hydroxide, aluminium hydroxide, iron (III) acetylacetonate (Fe(acac)₃), toluene, and nitric acid were purchased from Sigma Aldrich and used without further purification.

3.2. Catalyst Preparation and Characterization

Details on the experimental methods are reported in the Supplementary Materials; here, we briefly sketch the basic procedures employed in this work. Mayenite was prepared by following the ceramic method described by Li et al. [40], starting with a mixture of calcium and aluminium hydroxide. Successively, mayenite was loaded with two different amounts of iron (1.5 and 2.0%) by using a solution of Fe(acac)₃ [41].

Diffraction patterns were recorded on a Bruker D8 Advance automatic diffractometer, operating with nickel-filtered $CuK\alpha$ radiation.

The iron content of Fe/mayenite catalyst was determined by ICP-OES analysis using a Perkin Elmer Optima 7000 DV after digestion of the sample in HNO₃. Three replicates for each sample were made.

The BET surface areas were determined with an 11-point BET analysis, after a degassing procedure in vacuum at 200 $^{\circ}$ C, by using a Nova Quantachrome 4200e instrument.

Temperature programmed reduction (TPR) of samples (10–20 mg) was measured with a TPD-TPR Autochem 2910 analyzer in the range of 25–800 °C.

The morphological and elemental analysis of the catalysts was performed by a scanning electron microscope (SEM, Tescan Vega LMU) equipped with a X-Ray energy dispersive microanalysis of

elements (EDX, Bruker Quantax 800). Additionally, Fe/mayenite was characterized by field emission scanning electronic microscope (FESEM, ZEISS ULTRA 55).

X-ray photoelectron spectroscopy (XPS) was performed by using a SPECS spectrometer equipped with a Phoibos 150MCD-9 multichannel analyser. CasaXPS software was used for spectra treatment.

Raman spectra were recorded at RT with a 514 nm laser excitation on a Renishaw Raman Spectrometer (in via) equipped with a CCD detector. The laser power on the sample was 25 mW and a total of 20 acquisitions were taken for each spectra.

3.3. Experimental Setup and Catalytic Reactions

The experiments were performed in a stainless-steel fixed bed reactor, with the catalysts (0.8 g) placed between two quartz fiberglass stoppers. The cylindrical reactor (150 mm × 18 mm i.d., 22 mm o.d.) was placed in a furnace and the temperature was controlled via a K-thermocouple located inside the reactor.

Catalytic oxidations were monitored in the temperature range of 150–550 °C and the catalysts were kept at an operative temperature in air for 30 min before flow of TCE. The inlet gas was prepared by flowing a stream of air through pure TCE at room temperature; the final gas composition was [TCE] = 1700 ppm in wet air (RH = 60%). The Gas Hourly Space Velocity (GHSV) was set to 6000 h⁻¹ by flowing the inlet gas at 110 mL/min. The residence time, based on the packing volume of the catalyst, was 0.87 s. Blank experiments were performed in the same conditions to evaluate the thermal oxidation.

3.4. Analytical Methods

Post-reaction gases were collected in a Tedlar sampling bag (SKC Inc., Eighty Four, PA, USA) for further analyses. To evaluate the conversion yield, the organic species were determined by means of GC-MS (Agilent 7890A) equipped with a DB 17-MS column (30 m × 0.25 mm, 0.25 µm). [CO] and [CO₂] were measured with an NDIRS on line system (Q-Track Plus IAQ Monitor, TSI), placed at the reactor outlet [23]. [Cl₂] and [HCI] were determined by tritation and ion chromatographic (IC) analyses of two aqueous solutions obtained by bubbling the reactor effluent gases into two water solutions (6 × 10^{-2} M solution of KI and 0.1 M of H₂SO₄ for Cl₂ and 2.6/0.76 mM solution of NaHCO₃/Na₂CO₃ for Cl⁻). The production of Cl₂ was also assessed by SIM mode GC-MS analysis, using the same operative conditions described for the organic compounds [42]. The reproducibility of the results was checked by triplicate analyses (error < 5%). More details about products characterization are reported in our previous work [19].

The conversion yield was calculated as the ratio between the reacted TCE over the total TCE introduced into the reactor (1):

TCE conversion [%] =
$$\frac{m_{\text{TCE}}^i - m_{\text{TCE}}^o}{m_{\text{TCE}}^i} \times 100$$
 (1)

where m_{TCE}^i are the moles of TCE introduced into the reactor and m_{TCE}^o are the number of moles measured in the outlet gases; the reaction rate was calculated in terms of converted mass of TCE with respect to the catalyst mass and the residence time of the gas in the reactor (2):

conversion rate
$$\left[\frac{mol}{g \times s}\right] = \frac{\text{moles of converted TCE}}{\text{catalyst mass } \times \text{ residence time}}$$
 (2)

4. Conclusions

Iron-doped mayenite catalysts were prepared with different metal loading, obtaining active and selective catalysts able to quantitatively oxidize TCE in the gas phase. All the synthesized catalysts showed good performances for TCE oxidation, totally converted in CO₂, CO, and HCl. Mayenite loaded with 2% iron was found to be the best catalyst in terms of T_{50} (300 °C). This result was correlated with

an optimum combination of the oxidative properties of the mayenite active support with the redox properties of iron, as TPR, XPS, and Raman results have shown.

2.0% Fe/mayenite showed good stability in terms of TCE conversion, respect to pure mayenite. The results only show some deactivation after 12 h of reaction, with a small decrease in the TCE conversion from 95% to 80%. In contrast, pure mayenite had significant deactivation (TCE conversion decrease from 80% to 40%) after 4 h of reaction. The atomic mapping of the samples shows that iron is well dispersed on the mayenite surface, minimizing catalyst deactivation and improving mayenite oxidant activity.

In conclusion, Fe/mayenite was found to be a promising catalyst due to several advantages such as: (i) total conversion of TCE in less-harmful products (CO₂, CO and HCl), (ii) absence of noble and heavy metals, thus reducing costs and the environmental impact, (iii) low cost of catalyst precursors and low deactivation.

Supplementary Materials: The following are available online at http://www.mdpi.com/2073-4344/9/9/747/s1, Figure S1 SEM and EDX analyses of 2.0% Fe/mayenite; Figure S2 XRD patterns of 2.0% Fe/mayenite; Figure S3 SEM and EDX spectrum of 2% Fe/mayenite after reaction; Figure S4 XPS survey spectra of the 2.0% Fe/mayenite.

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