

FINAL

FIVE-YEAR REVIEW REPORT Five-Year Review of Interim Remedial Action at Former Area P Lagoons Louisiana Army Ammunition Plant Shreveport, Louisiana

Prepared for:

U.S. ARMY ENVIRONMENTAL CENTER ABERDEEN PROVING GROUND, MARYLAND 21010

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SCIENCE APPLICATIONS INTERNATIONAL CORPORATION 1710 Goodridge Drive McLean, Virginia 22101 FIVE-YEAR REVIEW REPORT FIVE-YEAR REVIEW OF INTERIM REMEDIAL ACTION AT FORMER AREA P LAGOONS LOUISIANA ARMY AMMUNITION PLANT, SHREVEPORT, LOUISIANA

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LIST OF ACRONYMS AND ABBREVIATIONS

AMCCOM	U. S. Army Armament, Munitions, and Chemical Command
ASTM	American Society for Testing and Materials
BDL	Below Detection Limit
BLS	Below Land Surface
CCV	Continuing Calibration Verification
CERCLA	Comprehensive Environmental Response, Compensation, and Liability Act
cfs	Cubic Feet per Second
coc	Contaminant of Concern
CRL	Certified Reporting Limit
DCL	DataChem Laboratories
1,3- DNB	1,3- Dinitrobenzene
2,4- DNT	2,4,- Dinitrotoluene
2,6- DNT	2,6- Dinitrotoluene
DO	Dissolved Oxygen
DQO	Data Quality Objective
EPA	U. S. Environmental Protection Agency
ESA	Endangered Species Act
ETA	Engineering Technologies and Associates, Inc.
FFA	Federal Facilities Agreement
ft/day	Feet per Day
ft/year	Feet per Year
GOCO	Government-Owned, Contractor-Operated
gpd/ft	Gallons per Day per Foot
HAL	Health Advisory Level
HEAST	Health Effects Assessment Summary Table

- HMX Cyclotetramethylenetetranitramine
- ICV Initial Calibration Verification
- IMP Generally Improving
- IRA Interim Remedial Action

LIST OF ACRONYMS AND ABBREVIATIONS (continued)

- IRP Installation Restoration Program
- IRDMIS Installation Restoration Data Management Information System
- KOC Soil Sorption Constant
- KOW Log Water Partition Coefficient
- LAAP Louisiana Army Ammunition Plant
- LAP Load-Assemble-Pack
- LCS Laboratory Control Sample
- LDEQ Louisiana Department of Environmental Quality
- LSU Louisiana State University
- MCL Maximum Contaminant Level
- MCLG Maximum Contaminant Level Goal
- MS/MSD Matrix Spike/Matrix Spike Duplicate
- MSL Mean Sea Level
- NB Nitrobenzene
- NGVD National Geodetic Vertical Datum
- NPL National Priorities List
- OSWER Office of Solid Waste and Emergency Response
- PARCC Precision, Accuracy, Representativeness, Comparability, and Completeness
- ppm Parts per Million
- PRI Potomac Research Institute
- QA Quality Assurance
- QA/QC Quality Assurance/Quality Control
- QAPP Quality Assurance Project Plan
- QC Quality Control
- RDX Hexahydro-1,3,5-trinitro-1,3,5-triazine

RfD Reference Dose

SAIC Science Applications International Corporation

- SDWA Safe Drinking Water Act
- SOP Standard Operating Procedure

LIST OF ACRONYMS AND ABBREVIATIONS (continued)

- SOW Statement of Work
- STA Stabilized Condition
- TETRYL N-methyl-N,2,4,6-tetranitroaniline
- 1,3,5-TNB 1,3,5-Trinitrobenzene
- TNT Trinitrotoluene
- 2,4,6-TNT 2,4,6-Trinitrotoluene
- USAGE U.S. Army Corps of Engineers
- USAEC U.S. Army Environmental Center
- USATHAMA U.S. Army Toxic and Hazardous Materials Agency
- USFWS U.S. Fish and Wildlife Service

EXECUTIVE SUMMARY

Science Applications International Corporation (SAIC), under-contract to the U. S. Army Environmental Center (USAEC), has completed a Five-Year Review to assess the effectiveness of the interim remedial action at the Former Area P Lagoons site at the Louisiana Army Ammunition Plant (LAAP). This review is conducted in accordance with the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA) of 1980 and U.S. Environmental Protection Agency (EPA) guidance (EPA 1991, USATHAMA 1992).

LAAP is a government-owned, contractor-operated (GOCO) facility and is under contractual agreement with Thiokol Corporation to manufacture metal shell parts and load-assemble-pack (LAP) ammunition items. The facility is located approximately 22 miles east of Shreveport, Louisiana, and covers 14,974 acres.

The scope of this Five-Year Review consisted of preparing project work plans, conducting field investigation activities, evaluating sampling data, and preparing a Five-Year Review Report. The final project work plans were submitted to USAEC and appropriate regulatory agencies on February 18, 1994. The field program was conducted from February 21 through March 8, 1994. Specific subtasks of the field program included inspecting the cap and fence surrounding Area P, surveying the surface elevation of the cap, and determining shallow groundwater quality at Area P by sampling 13 wells located on and adjacent to Area P.

The objectives of the Five-Year Review of the Interim Remedial Action at Former Area P Lagoons are to:

- Determine if the clay cap of the Former Area P Lagoons has been effective in preventing surface erosion of incinerated soil
- Determine if the clay cap has been effective in minimizing infiltration of rainwater through residual explosive-contaminated soil existing below the depth of the incinerated soil
- Determine the integrity of the clay cap and the fence surrounding Area P.

SUMMARY OF CAP AND FENCE INSPECTION

SAIC conducted a cap and fence inspection on February 21 and 22, 1994. The cap inspection identified bare spots greater than 1 foot in area. This study recommended that these bare spots be seeded and mulched to prevent erosion. A low-lying area near the southwestern boundary of Area P also was identified. Water tends to pond in this area after periods of heavy precipitation. The fence inspection identified one area on the northeast boundary that was damaged by a fallen pine tree. The fence has since been repaired by LAAP personnel.

SUMMARY OF TOPOGRAPHIC SURVEY OF AREA P CAP

The Area P cap was topographically surveyed by Fanner, Downs, and Associates between March 3 and 9, 1994. The survey was conducted to determine if any subsidence has occurred at Area P by comparing the 1994 and 1990 surface elevations. The 1994 topographic survey indicates that no subsidence has occurred since the cap was installed in 1990.

SUMMARY OF GROUNDWATER SAMPLING RESULTS

Twelve of the proposed 13 wells were sampled during the Five-Year Review of Area P. Due to bent well casings, well G0010 was substituted with well G0014, and well G0011 could not be sampled. The samples were analyzed for explosives only, since they have been identified as contaminants of concern (COCs) for Area P.

Nine wells screened in the Upper Terrace aquifer were sampled during the Five-Year Review of Area P Lagoons. Concentrations of hexahydro-1, 3,5-trinitro-1, 3,5-triazine (RDX), 1,3,5-trinitrobenzene (1,3,5-TNB), 1,3-dinitrobenzene (1,3-DNB), 2,4,6-trinitrotoluene (2,4,6-TNT), and nitrobenzene (NB) were above the drinking water health advisory levels (HALs). Concentrations of 2,4-dinitrotoluene (2,4-DNT), 2,6- dinitrotoluene (2,6-DNT), cyclotetramethylenetetranitramine (HMX), and N-memyl-N,2,4,6-tetranitroaniline (TETRYL) were below the HALs. The maximum concentration for explosives was detected in well G0104 located southwest of Area P. The 1994 concentration, indicating that the groundwater quality at Area P has improved since the remedial measure was completed.

SAIC sampled three wells screened in the Lower Terrace aquifer during the Five-Year Review field investigation activities. The COCs detected in the Lower Terrace aquifer at Area P were the same as those found in the Upper Terrace aquifer. As in the Upper Terrace aquifer, the concentrations of RDX, 1,3,5-TNB, 1,3-DNB, 2,4,6-TNT, and NB were above the HALs. Generally, the concentration of the COCs in the Lower Terrace aquifer was less than the concentration detected in the Upper Terrace aquifer. The concentration in the Lower Terrace aquifer was higher than the 1990 concentration for wells G0105 and G0106 located southwest of Area P. This may be a result of downward migration of the COCs from the Upper Terrace aquifer.

Three ponded areas were identified during the Five-Year Review of Area P. Water tends to pond in these areas after periods of heavy precipitation. A ponded area was identified on the Area P cap near wells G0068, G0109, and G0110. This area, which is along the drainage pathway from the Area P cap, should be filled with soil and graded to blend smoothly with the surrounding area. The area should be seeded and mulched to prevent erosion. The ponding of the water observed in the southwest comer of the Area P cap after periods of heavy precipitation is a result of the surface drainage pattern from the cap. The ponded area south of well G0012 is outside the cap area. No maintenance is recommended for these two areas.

SUMMARY OF GROUNDWATER ANALYSIS

A statistical regression analysis approach was used to identify the groundwater trends at Area P. Groundwater sampling data were evaluated from 1980 through 1994. Quadratic and linear analyses were conducted for 108 sampling data sets (12 wells x 9 COCs). Trend categories were assigned to each of the data sets based on improving, deteriorating, and stable groundwater quality of COCs. Data sets with no specific trend also were identified. Based on the trend categories, trend indices were determined by well for each COC, and Area P overall. The overall trend indices for both the Upper and Lower Terrace aquifers were positive, indicating that the groundwater quality at Area P is generally improving.

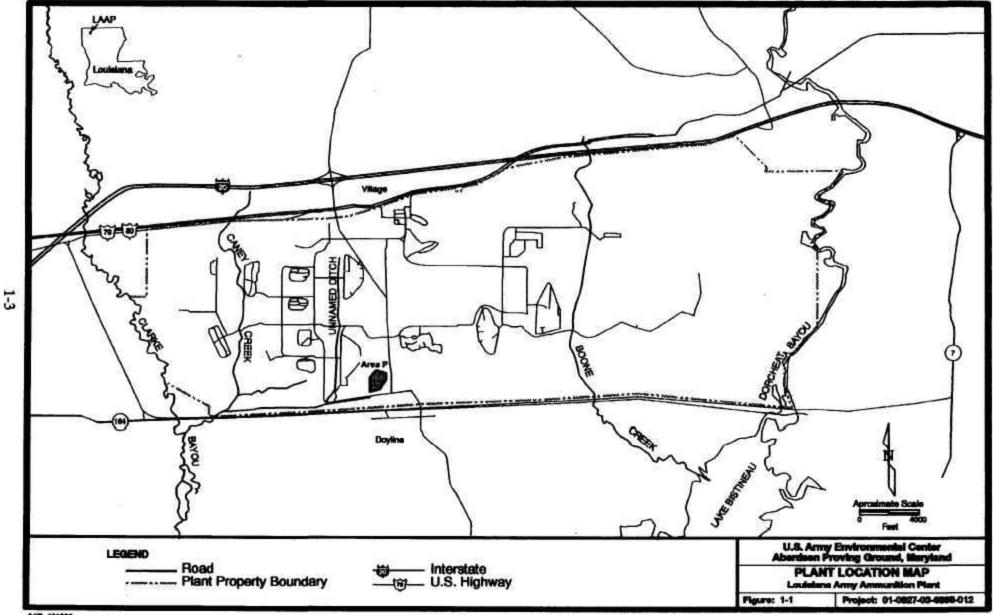
1. INTRODUCTION

Science Applications International Corporation (SAIC) prepared this Five-Year Review Report of Former Area P Lagoons to satisfy the requirements of Task Order No. 0010 (LAW EUN A009) of the U. S. Army Environmental Center (USAEC) Contract No. DAAA15-91-D-0017. Task Order 0010 requires SAIC to perform a Five-Year Review of the interim remedial action effectiveness at Former Area P Lagoons at Louisiana Army Ammunition Plant (LAAP), a U. S. Army Armament, Munitions, and Chemical Command (AMCCOM) installation, in accordance with the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA) of 1980 and U.S. Environmental Protection Agency (EPA) guidance (EPA 1991, USATHAMA 1992).

1.1 REGULATORY INITIATIVES

According to CERCLA, a review of the remedy effectiveness at Area P must be conducted every 5 years unless future risk assessments indicate that health risks at the site are acceptable for unrestricted use. Section 121c of CERCLA requires that, for "a remedial action that results in any hazardous substances, pollutants, or contaminants remaining at the site,"the U.S. Army "shall review such remedial action no less often than every five years after the initiation of such remedial action to ensure that human health and the environment are being protected by the remedial action being implemented." The EPA Office of Solid Waste and Emergency Response (OSWER) Directive 9320.2-03B, states "... EPA will ensure that five-year reviews are conducted for all remedial actions which result in hazardous substances, pollutants, or contaminants remaining at the site above levels that allow for unlimited use and unrestricted exposure" (EPA 1989).

The Five-Year Review of interim remedial actions completed at the Former Area P Lagoons in 1990 is being conducted at LAAP in accordance with CERCLA under the Federal Facilities Agreement (FFA) signed by EPA Region VI, the Louisiana Department of Environmental Quality (LDEQ), and the U.S. Army on February 10, 1989.



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1.2 OBJECTIVES OF FIVE-YEAR REVIEW

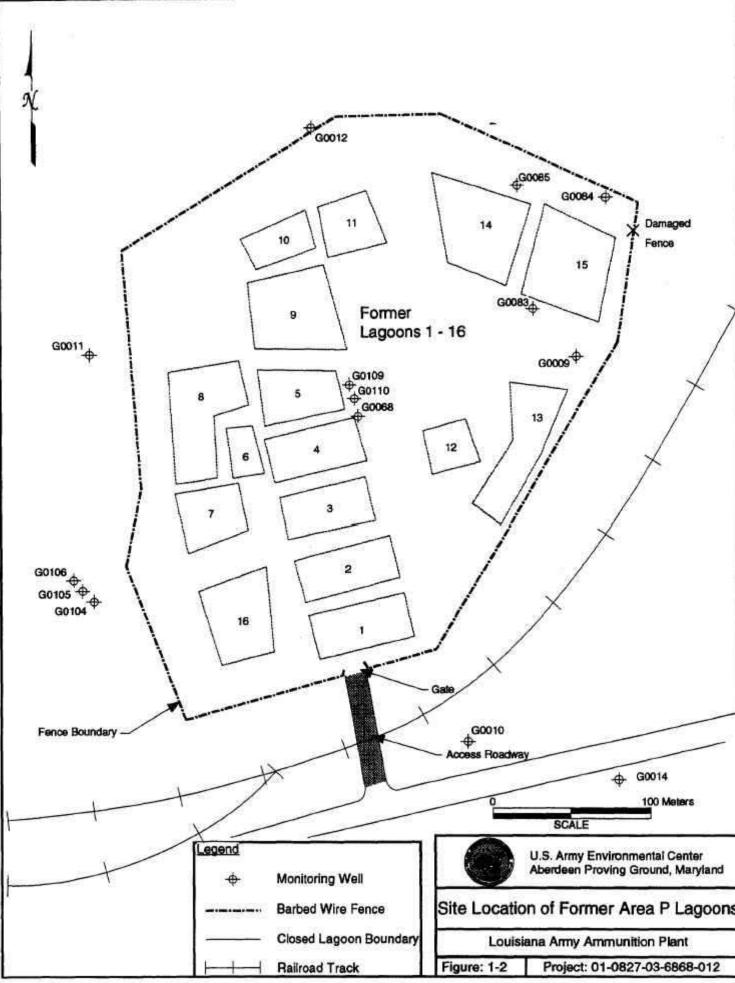
The primary objectives of this Five-Year Review of Area P, as outlined in the statement of work (SOW) and Maintenance Plan for LAAP (USATHAMA 1992), was to inspect the current site conditions, determine the effectiveness of the interim remedial measure (cap), and identify any additional actions that should be taken in accordance with CERCLA. To accomplish these objectives, data were collected during the following inspection, survey, and monitoring activities:

- Cap inspection
- Fence inspection
- Groundwater sampling and analysis
- Topographic survey of Area P cap.

The field investigation activities were conducted between February 21 and March 4, 1994. The objective of the cap inspection was to determine the stability of the cap; hence, its capability to be effective. The objective of the fence inspection was to determine if access to Area P is being controlled. The groundwater sampling was conducted to evaluate the groundwater quality in the shallow aquifer. The sample results were compared with the historical data to determine variations in explosive compound concentrations. The objective of the topographic survey was to determine if any subsidence of the cap had occurred since its installation in 1990.

1.3 SITE DESCRIPTION

LAAP is a government- owned, contractor-operated (GOCO) facility located approximately 22 miles east of Shreveport, Louisiana, and is under contractual agreement with Thiokol Corporation to manufacture metal shell parts and load-assemble-pack (LAP) ammunition items. The facility is bound to the north by Interstate 20 and U.S. Highway 80, to the south by State Route 164, to the east by Dorcheat Bayou, and to the west by Clarke Bayou. A map of the general vicinity is provided in Figure 1-1. Two streams, Boone Creek and Caney Creek, flow north to south across the site. LAAP lies within both the Bossier and Webster Parishes and consists of 14,974 acres of land, of which 74 acres are administrative and residential, 2,970



acres are devoted to production lines and mission support facilities, and 11,930 acres are woodlands. The area surrounding LAAP is used primarily for agriculture, with some residential and commercial development. The closest community to LAAP is the village of Doyline, which is adjacent to the southern boundary. The area topography is relatively level to moderately rolling, with elevations ranging from 170 to 225 feet above mean sea level (MSL). All surface drainage from LAAP is discharged into Lake Bistineau, located approximately 2 miles south of the installation.

1.4 SITE HISTORY

The primary mission of LAAP is to load, assemble, and pack ammunition items; manufacture ammunition metal parts; and provide associated support functions for ammunition production. Eight ammunition lines and one ammonium nitrate graining plant were constructed by the Silas Mason Company between July 1941 and May 1942. Production ceased in August 1945 at the conclusion of World War IL The plant was placed on standby status in September 1945, and in November 1945, the Federal Government relieved Silas Mason Company of responsibilities for plant operations (USATHAMA 1992).

Remington Rand, Inc., under contractual agreement with the Federal Government, reactivated the plant in February 1951 and maintained operations during the Korean Conflict. Ammunition production was suspended and the facility was again placed on standby status in October 1957.

In September 1962, the Federal Government again reactivated the facility and contracted Sperry Rand Corporation to operate the munitions production in support of the Vietnam Conflict. Thiokol Corporation took over the facility operations in 1974 when Sperry Rand Corporation relinquished the contract.

Area P consisted of 16 unlined lagoons of approximately 25 acres in area and is located in the south-central part of the installation, as shown in Figure 1-2. The Area P Lagoons were in active use between 1940 and 1981. During this time, untreated explosives-laden wastewater from industrial operations within LAAP was collected in concrete sumps at each of various industrial areas and hauled by tanker trucks to Area P. The wastewater is now listed as hazardous waste according to 40 CFR 261.32, Waste from Specific Source, and classified "K047-Pink/Red Water from Trinitrotoluene (TNT) Operations."

LAAP was placed on the National Priorities List (NPL) in March 1989 due to contamination caused by past disposal of explosives-laden wastewater into unlined surface impoundments. Numerous investigations have been conducted for the Area P Lagoons to determine the nature and extent of soil and groundwater contamination. An interim remedial action was initiated in 1988 because the explosives- contaminated wastewater at Area P was found to be contributing to groundwater contamination. The source of the contamination was remediated by draining and treating wastewater in the lagoons, excavating the soil from the lagoons and adjacent areas, and treating the soil in an incinerator to destroy the explosives. The lagoons were excavated until a total field-determined explosives concentration of less than 100 parts per million (ppm) was reached. The incineration of 101,929 tons of soil and the treatment of 53,604,490 gallons of wastewater and rainwater collected within the 16 former pink-water lagoons was completed in 1990. The area was backfilled with the incinerated soil, capped, and vegetated.

The lagoons were covered with a minimum 2-foot thick compacted cap ofuncontaminated clay soil from Area P and a nearby borrow pit on LAAP. The remediation of the site increased the elevation of the lagoon area above the surrounding topography to promote surface drainage. Drainage was to the west and south, matching the prevailing drainage in that area. After periods of heavy precipitation, most of the runoff from Area P cap drains to the Unnamed Ditch located south of Area P. This ditch runs west along the plant boundary to Caney Creek before leaving the plant.

The clay cap covers not only the lagoons, but all of the original Area P. It is compacted to at least 90 percent of the standard proctor density for the material used. The cap is covered with 4 inches of topsoil and has a slope of at least 1 percent over the lagoons. The cap is vegetated and fenced with posted signs.

1.5 REPORT ORGANIZATION

The remainder of this Five-Year Review Report contains the following sections:

- Section 2, Study Area Characterization, presents an overview of the environmental setting at Area P of LAAP.
- Section 3, Five-Year Review Results and Significance of Findings, presents field sampling data evaluation, cap and fence inspection findings, evaluation of the topographic survey of the Area P cap, and groundwater trend analysis.
- Section 4, Conclusions and Recommendations, presents the findings of the Five-Year Review and presents recommendations for corrective measures and future Five-Year Reviews of Area P.

2. STUDY AREA CHARACTERIZATION

2.1 INTRODUCTION

This section presents the regional physical setting of the Louisiana Army Ammunition Plant (LAAP). A brief summary of the geographic setting, hydrology, geology, hydrogeology, ecology, and demographics of the LAAP area is included.

2.2 GEOGRAPHIC SETTING

Northwest Louisiana lies within the East Texas Timber Belt subdivision of the West Gulf Coastal Plain physiographic province. LAAP is located in an area with three major landform types, including uplands in the west, slightly rolling low land in the east, and the ancient Red River floodplain underlying the central portion of the installation. The elevation is approximately 130 feet above mean sea level (MSL) at Dorcheat Bayou to the east, and approximately 180 feet above MSL at the Clarke Bayou to the west. The maximum elevation at LAAP is approximately 225 feet above MSL. The topography is primarily the result of erosion caused by surface drainage to the tributaries of the Red River and has generated a relatively level to moderately rolling topography.

2.3 HYDROLOGY

2.3.1 Climate

The climate of northwest Louisiana has been characterized as continental, with cool winters and hot summers. The mean winter temperature is 45°F, and the average monthly minimum temperature is 35°F. January is the coldest month, with temperatures approximately 40°F. The mean summer temperature is 81°F, while the average monthly maximum temperature during the summer is 92°F. July is the hottest month, with temperatures averaging 83F. The relative humidity is 60 percent for 75 percent of the year and less than 40 percent for only 7 percent of the year.

The town of Minden lies approximately 2 miles northeast of the LAAP boundary and has an average annual rainfall of 53 inches per year. Monthly rainfall averages 5 inches during winter and spring, and 3 inches during summer and autumn. The wettest months are October and November, while the least amount of rain generally falls during August and September. During the winter, 98.6 percent of the precipitation is rain. An average of only 2 inches of snow falls each winter.

During the summer, the prevailing southerly winds provide a moist, warm, tropical climate; however, erratic pressure distributions occasionally generate westerly winds and hot, dry weather. These same prevailing patterns alternately generate moist tropical air and dry, cold air during the winter. As a result, temperature changes can be extreme. Figure 2-1 provides a "wind rose" showing wind directions and velocities for the LAAP area.

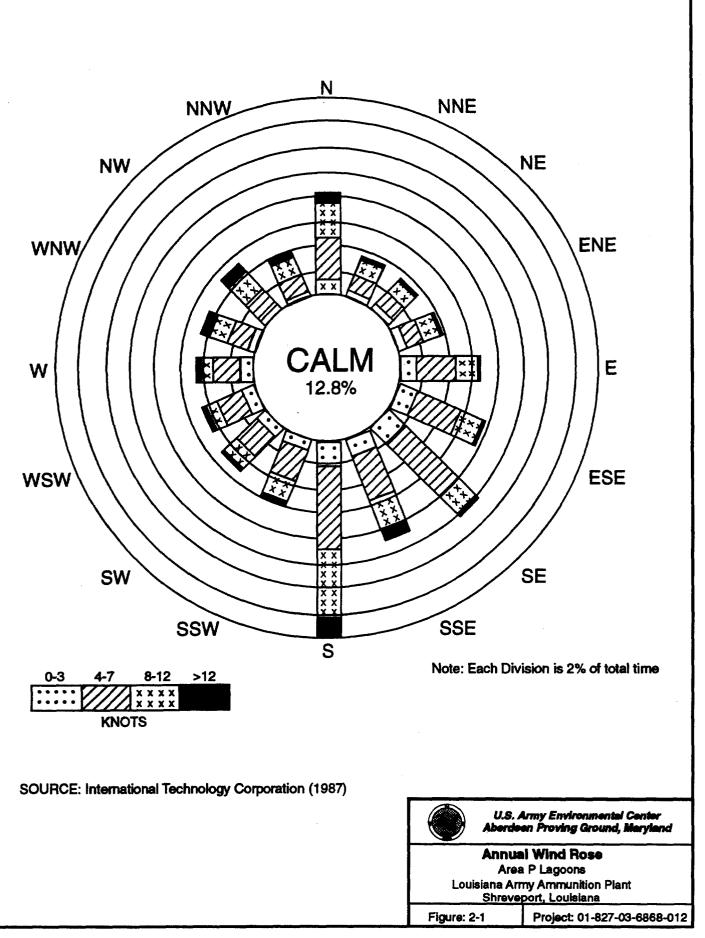
2.3.2 Surface Water Hydrology

Surface drainage for the installation (Figure 1-1) flows into Lake

Bistineau (located 2 miles south of the plant) by way of Clarke Bayou, Caney Creek, Boone Creek, an unnamed drainage ditch, and Dorcheat Bayou. These main drainages are generally intermittent, slow-moving (less than 1 cubic foot per second [cfs]), shallow streams (less than 6 feet deep). Characteristically, surface water drainages at LAAP have minimal flow, turbid water, and eroded banks. The bottom substrate is generally composed of silty clay with an abundance of decaying plant material. Water quality measurements are variable, and most locations have relatively low levels of dissolved oxygen (DO) (ESE 1992). All of these waterways, with the exception of the unnamed drainage ditch, originate north of the facility.

The Clarke Bayou flows to the southward along the western edge of the installation, establishing the western boundary. Clarke Bayou and one of its tributaries, Caney Creek, are the primary drainage pathways for the western quarter of LAAP, which includes Area P. Caney Creek, located 1 to 2 miles east of Clarke Bayou, flows due south across the installation, as shown in Figure 1-1 (ESE 1992).

Surface drainage for the majority of the eastern to central portion of the installation is controlled by Boone Creek and its tributaries, which are located on the eastern third of the property. The unnamed, manmade drainage ditch within LAAP lies 6.4 miles west of Boone



Creek. The ditch originates just north of Area C and flows in a southerly direction toward the plant boundary. The ditch then turns to the west and continues to its junction with Caney Creek.

2.4 GEOLOGY 2.4.1 Regional Geology

The geologic units underlying LAAP consist of unconsolidated sediments ranging in age from Eocene to Pleistocene. The major strata are the Pleistocene terrace deposits (alluvium), and the Tertiary Claiborne Group Formations (Sparta Sand, Cane River, and Carrizo Sand), and the Tertiary Wilcox Group. Table 2-1 summarizes the major stratigraphic units in northeast Louisiana.

The Pleistocene terrace deposits cover the entire surface of LAAP. This uppermost geologic strata is an alluvium consisting of interlayered, discontinuous sand seams, silt, and clay. These sediments represent floodplain and fluvial deposits of the ancestral Red River and have been classified into four separate terraces. LAAP is positioned on the Montgomery terrace, the second youngest terrace in this classification. The thickness of the Pleistocene section at LAAP ranges from 30 to 150 feet and rests unconformably on top of the Claiborne Group. Formations at the installation had been eroded before or during deposition of the terrace strata, resulting in a structural unconformity. At LAAP, the Claiborne Group consists of the Sparta Sand, Cane River, and Carrizo Sand formations.

The Eocene Sparta Sand, a member of the Claiborne Group, lies unconformably below the Pleistocene terrace deposits. The formation consists of nonmarine massive sand, silty sand, and silty shale, with occasional lignite and lignitic shale (Payne 1968). Recent researchers (ETA 1991) have reported regional dips of approximately two degrees (170 feet/mile) to the northeast for the Sparta Sand and the subsequent underlying units.

The basal sand and gravel of the Pleistocene terraces and those of the Sparta Sand physically appear to be similar. However, the Sparta Sand probably does not exist at Area P. The current theory regarding me Sparta Sand was presented by Engineering Technology and Associates, Inc. (ETA) in 1991. As per ETA's report, " Sparta Sand is not present at Area P

System	Stra	tigraphic Unit	Description and typical thickness	Hydrologic unit -												
Quaternary		race deposits lifferentiated)	Sand, gravel, and some clay. Limited to western part of study area. Thickness probably about 50 ft.	Terrace aquifer												
			Cook Mountain Formation	Clay, partly sandy; glau- conitic. Thickness about 100 to 200 ft.	Confining bed											
	Group	Şparta Sand	Interbedded clay and fine to medium sand; lignitic. Thickness about 400 to 700 ft. Unit is 20 to 100 percent sand.	Sparta aquif e r												
Tertiary	Claiborne (Clatborne Group	Claiborne G	Claiborne G	Claiborne (Claiborne (Claiborne (Claiborne (Claiborne (Claiborne (Claiborne (Claiborne (Claiborne	Cane River Formation	Clay; glauconitic, lignitic. Thickness about 100 to 300 ft.	Confining bed
			Carrizo Sand	Fine to coarse sand; discontinuous. Thickness to 150 ft.	Wilson Coming and for											
	Wilcox Group	Undifferentiated	Interbedded clay, sand, silt; lignitic. Thickness about 390 to 850 ft. Unit is 20 to 30 percent sand.	Wilcox-Carrizo aquifer												
	Midway Group	Undifferentiated	Dense clay. Thickness about 600 ft.	Confining bed												

Table 2-1. Generalized Geologic Column, Northeast Louisiana

Source: USACE, 1984

•

because the Cane River Formation has been truncated from its usual thickness of 200 feet down to 80 feet. This erosional truncation could not occur without also truncating the Sparta Sand above." For purposes of hydrogeologic characterization, a precise stratigraphic identification of the formations is not necessary, since the hydrogeologic characteristics of the lower Pleistocene are similar to the Sparta. Therefore, in the hydrogeologic discussion contained in this report, the two units have been combined into one aquifer, the Lower Terrace/Sparta Sand aquifer.

The Eocene Cane River Formation lies directly below the Sparta Sand and follows the same northeasterly dip as the overlying unit. The Cane River Formation consists primarily of marine clay with abundant foraminifera, but also contains some silt and shale, often gray-green in color (Martin et al. 1954). Regionally, the thickness of the Cane River Formation varies from 100 to 300 feet.

The Eocene Carrizo Sand, the oldest member of the Claibome Group, underlies the Cane River Formation and consists of fine-to coarse-grained sand deposited on the eroded surface of the underlying Wilcox Formation. Because of nondeposition or erosion, the Carrizo Sand is a discontinuous unit. Payne (1975) reports the Carrizo to be absent over most of LAAP. Where it does exist, the Carrizo is composed primarily of well-sorted sand deposited as fill.

The Wilcox Group sediments consist mainly of nonmarine, white to gray, thin bedded micaceous sand and sandy shale. Regionally, the sequence varies in thickness from 350 to 1,000 feet; however, maximum thickness at LAAP is approximately 550 feet.

2.4.2 Geology of Area P

The geologic units underlying Area P consist of unconsolidated Pleistocene- aged upper terrace deposits, Lower Terrace/Sparta Sand, the Cane River Formation, and the Wilcox Formation. Although the geology at Area P is highly variable in the Pleistocene terrace deposits, some general trends have been identified. The alluvium in the immediate vicinity of the former lagoons is predominantly sand and silty sand with lesser quantities of interbedded silt and clay. Similar conditions apparently exist to the east and north of the lagoons. South of the lagoons, the alluvium is extremely variable and ranges from predominantly clay to predominantly sand. At Area P, these deposits extend from the surface to a depth of approximately 40 to 50 feet below land surface (BLS).

Several previous reports describe the Sparta Sand at Area P; however, ETA's 1991 report *Groundwater Model for Selected Sites at the Louisiana Army Ammunition Plant*, indicates that the Sparta Sand does not exist at Area P due to an erosional truncation of the formation. For purposes of this report, the exact lithologic identification is not necessary. The sands of the basal Pleistocene (Sparta) range in thickness from 8 to 30 feet. The upper part of the sand is generally a fine quartz sand; however, the unit generally becomes coarser with depth and grades into medium- to coarse-grained sand.

The Cane River Formation lies below the sand of the basal Pleistocene.

The unit consists of bluish- green to dark gray, finely laminated, interbedded clay, silt, and sand. The Wilcox Formation is projected to be 175 feet BLS at Area P. It consists mainly of nonmarine, white to gray, thin bedded micaceous sand and sandy shale.

2.5 HYDROGEOLOGY

The hydrologic units underlying Area P and the characteristics of each of the geologic units are discussed below.

2.5.2 Upper Terrace Aquifer

The shallow aquifer underlying LAAP consists of Pleistocene terrace deposits that form the entire surface of LAAP. Groundwater in the Upper Terrace aquifer generally exists under water-table (unconfined) conditions at depths typically 25 feet BLS. The direction of groundwater flow in the Upper Terrace aquifer is controlled primarily by topography and the surface water system. Although terrace aquifer production wells are not located at LAAP, the aquifer supports production wells off me installation. Domestic wells using the terrace aquifer have been completed in the surrounding towns of Haughton, Princeton, Dixie Inn, Minden, Sibley, and Doyline.

Groundwater quality simulations conducted at Area P by ETA in 1991 show contaminant migration in the Upper Terrace aquifer generally travels downward with a small amount of horizontal spreading (ETA 1991). Water level measurements collected during the Five- Year Review in the Upper Terrace aquifer indicate that the regional groundwater flow is toward the southwest (Figure 2- 2).

2.5.2 Lower Terrace/Sparta Sand Aquifer

Directly beneath the Upper Terrace aquifer is the Lower Terrace/Sparta Sand aquifer, an important aquifer in the north- central portion of the state and the principal source of drinking water for the town of Minden, located 2 miles northeast of LAAP. However, the Lower Terrace/Sparta Sand thins rapidly from Minden westward into LAAP. At Area P, the Lower Terrace/Sparta Sand does not exist (ETA 1991).

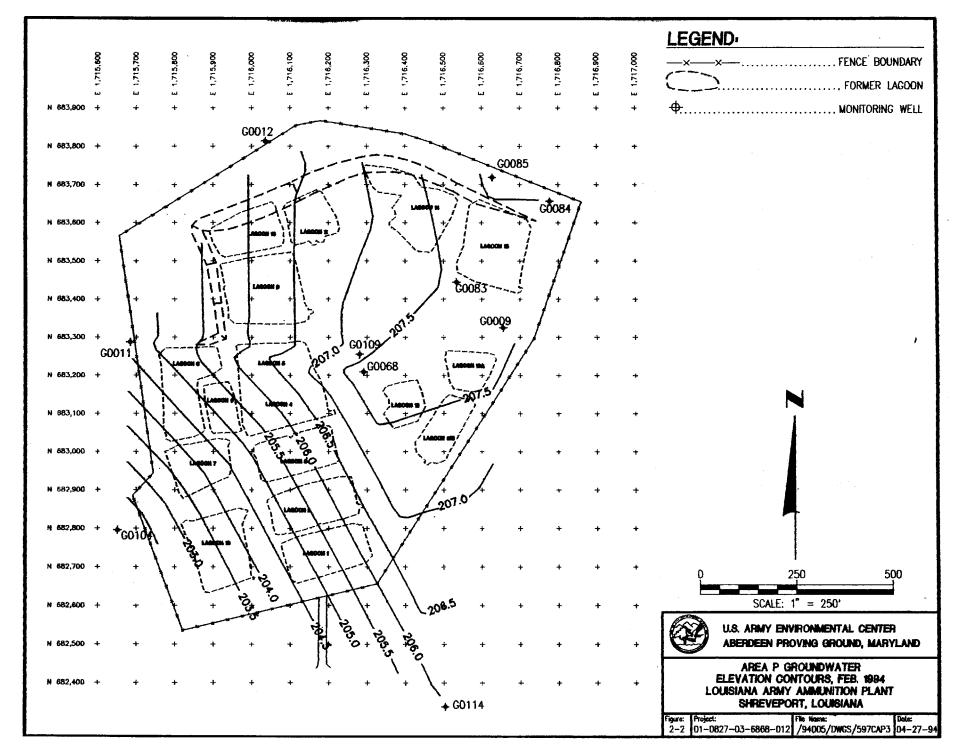
Where the Lower Terrace/Sparta Sand aquifer exists on the LAAP facility, a hydraulic communication exists between mis aquifer and the overlying Terrace deposits, resulting in unconfined conditions. The groundwater flow in this shallow aquifer also is dominated by the surface topography and surface water system and groundwater flow direction is generally toward the streams that bisect LAAP.

2.5.3 Wilcox Group/Carrizo Sand Aquifer

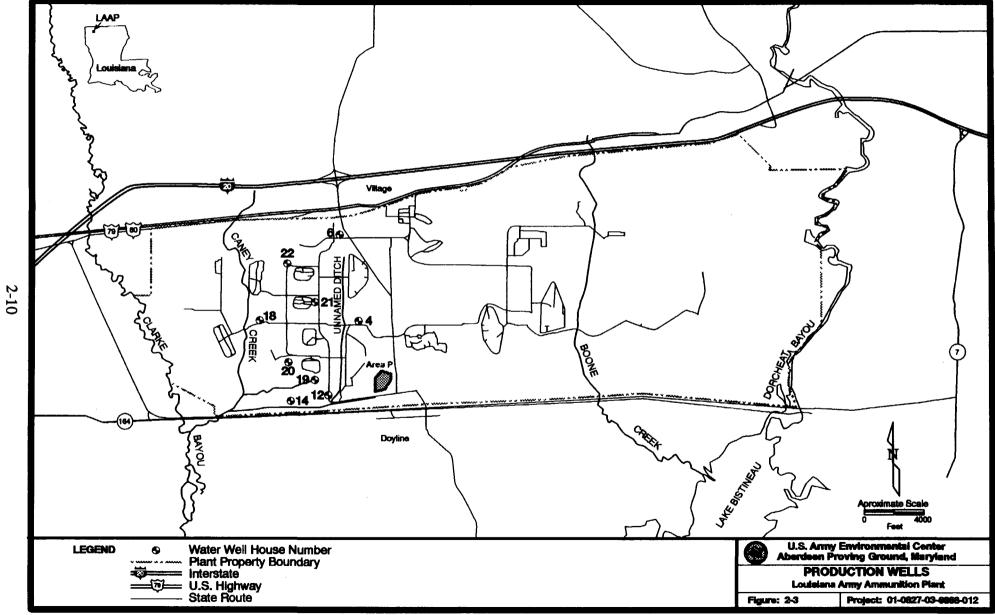
The Wilcox Group/Carrizo Sand aquifer is the principal aquifer supplying groundwater to LAAP. The average depth of the formation ranges from 100 feet BLS in the southwestern portion of the installation to 500 feet BLS in the

northeastern portion. A groundwater gradient of 50 feet per mile toward the northeast exists in the Wilcox/Carrizo aquifer, and aquifer pumping test data show that the sand has an average transmissivity of 5,000 gpd/ft and a storage coefficient of 0.0002 (ESE 1992). LAAP had previously derived all of its water for plant operation from wells screened in sand layers of the Wilcox aquifer. Locations of all previously used water wells on the plant in the Wilcox formation are shown in Figure 2-3.

The Cane River formation, a stratum of low permeability, overlies the Wilcox aquifer and acts as a confining layer. Because of the confining Cane River formation and the dip of the



2-9



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Wilcox strata, the hydrostatic head of the Wilcox aquifer rises above the contact between the Cane River Formation and the Wilcox Group. The Wilcox sand is recharged by precipitation that falls upon the Wilcox outcrop areas, and from overlying Quaternary strata where hydrostatic pressure in the Wilcox is less than the overlying material. Perennial streams that cross both the areas and the Quaternary deposits also help recharge the aquifer.

2.6 DEMOGRAPHICS

The area surrounding LAAP is primarily rural, with several small towns located in the near vicinity. The cities of Shreveport (population 198,525) and Bossier City (population 52,721) are approximately 20 miles west of LAAP. The town of Minden (population 15,489) is 2 miles northeast of the installation. The village of Doyline (population 896) is south and adjacent to the facility.

3. FIVE-YEAR REVIEW RESULTS AND SIGNIFICANCE OF FINDINGS

This section presents the results of the field investigation activities conducted during the Five-Year Review of Area P. These activities were conducted from February 21 through March 8, 1994. The field investigation techniques, methods, and procedures used during the Five-Year Review are presented in the Field Sampling Design Plan (SAIC 1994).

3.1 CAP AND FENCE INSPECTION

In 1990, after the incineration and backfilling of the contaminated soils at the Area P lagoons, the original Area P, including the lagoons, were covered with a minimum of 2 feet of compacted clay and 4 inches of topsoil. The cap was vegetated and fenced with posted signs. The cap was installed to minimize rainwater infiltration through soils laden with residual explosives contamination. The fence is maintained to prevent unauthorized access. The fence and cap will be maintained indefinitely.

3.2.1 Objectives

As a part of interim remedial action, guidelines and procedures for inspection and maintenance of the integrity of the cap and fence were established (USATHAMA 1992). These guidelines and procedures were used to conduct the cap and fence inspection. The guidelines for cap inspection included identifying the following:

- Bare soil spots larger than 1 square foot in area
- Eroded areas deeper than 4 inches
- Ponded areas larger than approximately 20 feet in diameter and deeper than 6 inches
- Any nongrasses that are found growing on the cap
- Any subsided areas

• Surface cracks.

The guidelines for fence inspection included identifying loose or broken wire strands and disturbed or missing fence post and signs.

3.1.2 Significance of Findings

A cap and fence inspection was conducted on February 21 and 22, 1994. The cap inspection identified bare spots greater than 1 square foot in area on the cap (Figure 3-1). A low-lying area near the southwest boundary of Area P and near monitoring wells G0068, G0109, and G0110 also was identified. Water tends to pond in these areas after periods of heavy precipitation (Figure 3-1). The ponding of water in the southwest corner of the Area P cap after periods of heavy precipitation is a result of the surface drainage pattern from the cap. The ponded area south of well G0012 is outside the cap area. The fence inspection identified one area on the northeast boundary damaged by a fallen pine tree. The fence damage was a result of an ice storm that hit the Shreveport area on February 17, 1994. The fence has since been repaired by Louisiana Army Ammunition Plant (LAAP) personnel.

3.2 TOPOGRAPHIC SURVEY OF AREA P CAP

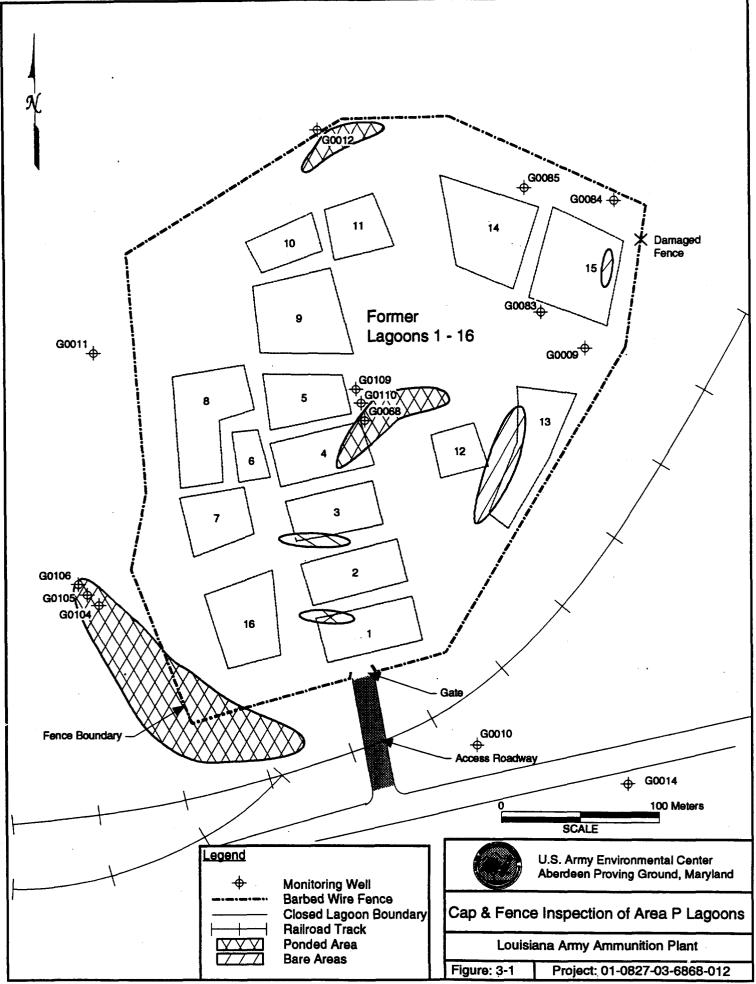
As a part of the Five-Year Review, a topographic survey of the surface elevations of the Area P cap was conducted. The survey was conducted from March 3 through 9, 1994, by Fanner, Downs and Associates of Natchitoches, Louisiana. All survey elevations were tied to the National Geodetic Vertical Datum (NGVD) elevation and the previous local grid system used at Area P in 1990. Elevations were determined along the same 100-foot grid that was constructed during the 1990 survey.

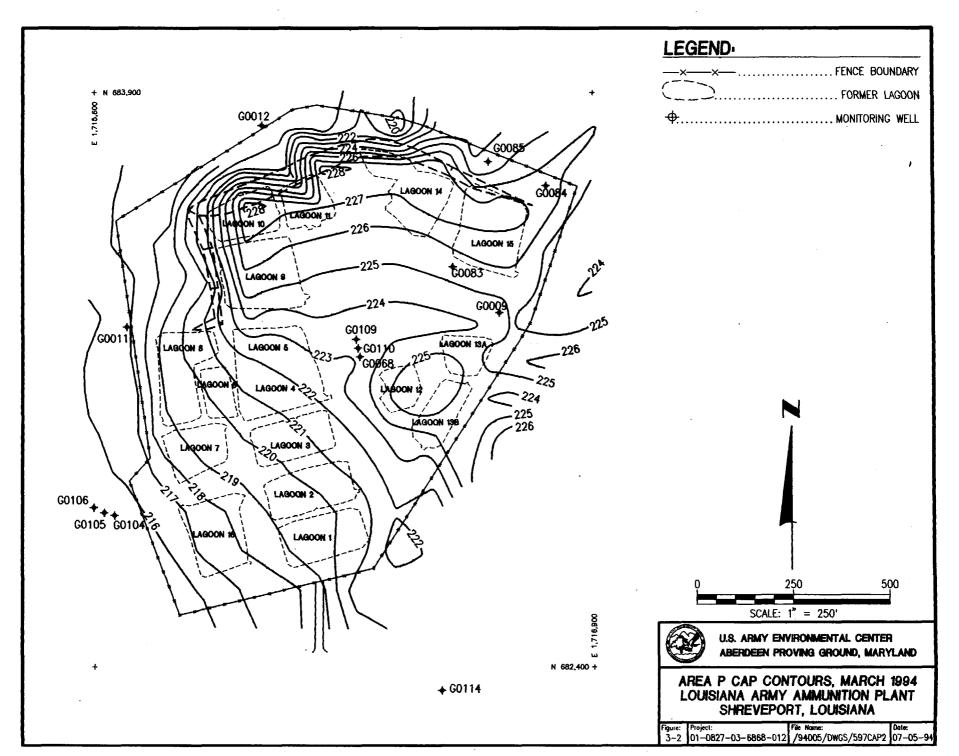
3.2.1 Objective

The objective of the topographic survey of the Area P cap was to determine if cap subsidence has occurred by comparing the survey results from the Five-Year Review to the 1990 survey (USATHAMA 1992). The impermeable cap, installed as a part of the 1990 remedial action, requires the elevation of Area P to be above the surrounding area to promote drainage. Drainage in 1990 was to the west and south, matching prevailing drainage in that area.

3.2.2 Significance of Findings

The topographic survey of the Area P cap indicated that no major subsidence has occurred since the cap was installed in 1990 (Figure 3-2). The 1990 and the 1994 survey maps





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are included in the pocket at the end of this report. The drainage from the cap is to the west and south. The survey was conducted along a 100-foot grid. Therefore, any subsidence between the grid points may not be shown on the topographic map. The area north of the cap and inside the Area P perimeter fence has a natural gradient. The 1990 topographic survey drawing does not show complete contours along the "grading limits" near the northern boundary of the cap (elevation 221 to 226 feet above MSL).

3.3 GROUNDWATER SAMPLING RESULTS

This section summarizes the results of the 1994 groundwater sampling conducted at Area P. A groundwater contamination trend analysis is presented in Section 3.4. The groundwater samples were analyzed for explosives only. The raw data used to compile the sampling result analysis in this section are contained within the Installation Restoration Data Management Information System (IRDMIS) and are summarized in Appendix A. These data have been reorganized and presented in this section to facilitate reporting. Groundwater Sampling Forms, Chain-of-Custody Forms, Water Level Measurement data sheets, and Well Construction Logs are provided in Appendix B.

The descriptions presented below represent the assessment of the detected concentrations of the contaminants of concern (COCs) that were determined by the 1992 Risk Assessment (ESE 1992). The COCs for groundwater at Area P, which includes both the Upper and Lower Terrace aquifers, are as follows:

- Hexahydro-1, 3,5-trinitro-1, 3,5-triazine(RDX)
- Cyclotetramethylenetetranitramine (HMX)
- 2,4,6-Trinitrotoluene (2,4,6-TNT)
- 1,3-Dinitrobenzene (1,3-DNB)
- 2,4-Dinitrotoluene (2,4-DNT)
- 2,6-Dinitrotoluene (2,6-DNT)
- 1,3,5-Trinitrobenzene (1,3,5-TNB)
- Nitrobenzene (NB)
- N-methyl- N, 2,4,6-tetranitroaniline (TETRYL).

The chemical and physical properties of the COCs, including water solubility, log water partition coefficient (Kow). sou sorption constant (Koc), vapor pressure, and Henry's law constant, are provided in Table 3-1. These properties affect the potential contaminant migration.

Maximum contaminant levels (MCLs) and maximum contaminant level goals (MCLGs) promulgated under the Safe Drinking Water Act (SDWA) do not exist for these COCs. Therefore, the COC concentrations were compared to the drinking water health advisory levels (HALs) presented in Table 3-2. These levels have been derived using the reference dose (RfD) values for noncarcinogenic nitrocompounds.

3.3.1 Objectives

In order to obtain a comprehensive data base for historical and future groundwater contamination comparison, 12 monitoring wells located on and adjacent to Area P were sampled and analyzed for explosive compounds Figure 3-3). Due to bent well casings, well G0010 was substituted with well G0014, and well G0011 could not be sampled. Table 3-3 summarizes well construction data for the wells investigated during the Five-Year Review, including well depth and organization that constructed the wells. The shallow wells (20 to 36 feet deep) are screened in the Upper Terrace aquifer and used to monitor the top of the water table aquifer. The deeper wells are screened in the unconfirmed aquifer of the Lower Terrace/Sparta Sand and used to monitor the bottom of the water table aquifer.

The groundwater sampling results from the Five-Year Review of Area P are presented in Table 3-4. The 1990 sampling results obtained immediately after the Area P cap was installed are presented in Table 3-5. The Five-Year Review sampling data have been compared to the 1990 data in Sections 3.3.2 and 3.3.3 to evaluate the impact of the cap on shallow groundwater quality since the installation of the cap. Section 3.4 compares the groundwater monitoring data collected during the 1994 sampling effort with the historical data and discusses the trend in the groundwater quality. The historical sampling results are provided in Appendix C.

Contaminant of Concern	Molecular Weight (g/mole)	Water Solubility (mg/L)	Log K _{ow}	K _∞ (mL/g)	Vapor Pressure (mm Hg)	Henry's Law Constant (atm•m ³ /mole)
1,3-Dinitrobenzene	168	530	1.49	36	1.3E-04	8.0E-07
2,4-Dinitrotoluene	182	280	1.98	250	2.2E-04	1.9E-07
2,6-Dinitrotoluene	182	210	1.89	78	5.7E-04	4.9E-07
нмх	296	5	0.12	3.5	3.3E-14	2.6E-15
Nitrobenzene	123	1,900	1.85	3.6	1.5E-01	1.3E-05
RDX	222	60	0.85	100	4.0E-09	2.0E-11
Tetryl	287	80	1.65	49	5.7E-09	2.7E-11
1,3,5-Trinitrobenzene	213	380	1.18	20	3.0E-06	2.2E-09
2,4,6-Trinitrotoluene	227	150	2.00	520	5.5E-06	1.1E-08

Table 3-1. Physical and Chemical Properties of the Contaminants of Concern at Area P Louisiana Army Ammunition Plant

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Note: $atm \cdot m^3/mole = atmosphere \cdot cubic meters per mole$

g/mole = grams per mole

 K_{ow} = octanol: water partition coefficient

 K_{∞} = soil sorption constant per unit weight organic carbon

mg/L = milligrams per liter

mL/g = milliliters per gram

mm Hg = millimeters of mercury

HMX = cyclotetramethylenetetranitramine

Morrison and Boyd 1983

RDX = cyclotrimethylenetrinitramine/cyclonite

Tetryl = nitramine/N-methyl-N,2,4,6-tetranitroaniline.

Sources:

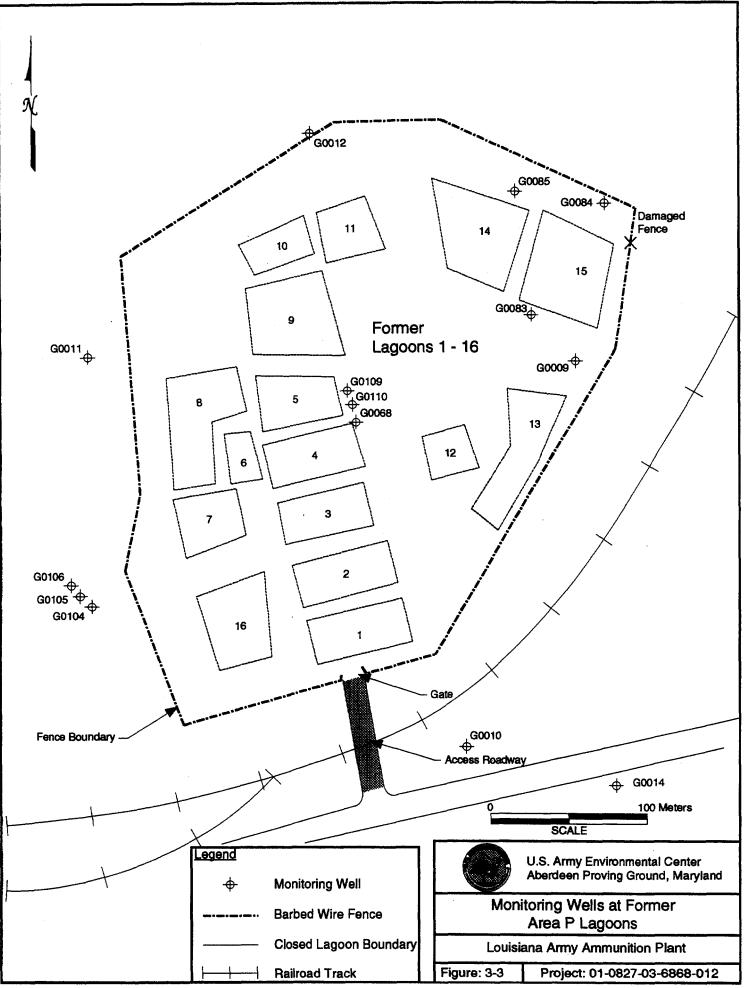
ESE 1992

Perry's Chemical Engineering Handbook 1984

Analyte	Oral RfD ®	HALs (µg/L)
RDX	3x10^-3	
		2.0
НМХ	5x10^-2	400.0
1,3,5-TNB	5x10^-5	3.5
2 , 4-DNT	2x10^-3	1,000.0
1,3-DNB	1x10^-4	1.0
2,6-DNT	1x10^-3(b)	1,000.0
2,4,6-TNT	5x10^4	2.0
Tetryl	1x10^-2(b)	430.0
NB	5x10^-4	
		3.5

Table 3-2. Health Advisory Levels for Groundwater at Area P Lagoons, LAAP

- (a) RfD obtained from IRDMIS, April 1994.
- (b) Oral RfD obtained from Health Effects Assessment Summary Tables (HEAST) March 1993.



Year Installed	Well No.	Total Depth (feet)	Aquifer Screened	Organization Conducting Investigation
1979	G0009	25.00	Upper Terrace	USAEHA
1979	G0012	27.52	Upper Terrace	USAEHA
1981	G0068	34.24	Upper Terrace	USATHAMA (EEI)
1982	G0083	32.47	Upper Terrace	USATHAMA (EEI)
1982	G0084	35.65	Upper Terrace	USATHAMA (EEI)
1982	G0085	35.32	Upper Terrace	USATHAMA (EEI)
1986	G0014	29.87	Upper Terrace	USATHAMA (ESE)
1986	G0104	35.62	Upper Terrace	USATHAMA (ESE)
1986	G0105	56.10	Sparta Sand	USATHAMA (ESE)
1986*	G0106	64.20	Sparta Sand	USATHAMA (ESE)
1986	G0109	27.15	Upper Terrace	USATHAMA (ESE)
1986	G0110	86.10	Sparta Sand	USATHAMA (ESE)

Table 3-3. Area P Monitoring Well Data

*Pump lost within well and currently remains in the well.

			· · · · ·		Upper T	errace Aquif	er Wells		••••••••••••••••••••••••••••••••••••••		Lower T	errace Aquif	er Wells
Parameter	HAL	GO009	GO012	GO014	GO068	GO083	GO084	G0085	GO104	GO109	GO105	G0106	GO110
		1994	1994	1994	1994	1994	1994	1994	1994	1994	1994	1994	1994
Units: ug/L													
RDX	2	430	3100 LT*	14.4	2500	1200	120	3800	8400	3100	330	4100	2800
нмх	400	26	110	2.92	350 LT	99	14	310 LT	370 LT	300	360	53 LT	130
2,4,6 TNT	2	28,3	8700	0.426 LT	8600	3100	250	4200	11000	8600	16.5	8800	570
1,3 DNB	1	0.458 LT	35	0.458 LT	82	5.6	0.46 LT	32	580	8.2	320	330	24
2,4 DNT	1000	37	120	0.397 LT	350	95	12	79	570	330	54	640	120
2,6 DNT	1000	0.6 LT	32.3 LT	0.6 LT	60 LT	12 LT	12 LT	59 LT	60 LT	60 LT	60 LT	60 LT	60 LT
1,3,5 TNB	3.5	59	950	0.429 LT	490	800	920	3800	6300	95	3900	970	460
NB	3.5	0.682 LT	12.3 L.T*	0.682 LT	68 L.T*	14 LT*	0.682 LT	67 L.T*	68 L.T*	6.8 LT*	68 L.T*	68 LT*	6.8LT*
TETRYL	430	0.631 LT	6.3 LT	0.631 LT	31	95	5.66	310	130	39.9	3.71	63 LT	0.63 LT

.

Table 3-4. Groundwater Sampling Data for Area P - 1994 Louisiana Army Ammunition Plant

Shaded area represents concentration above HAL HAL: Health Advisory Level

LT: Less than

*: Concentration reported as "LT" due to interference during sample analysis.

		Upper Terrace Aquifer Wells											
Parameter	HAL	AL GO009 GO012		0012	GOO	14	GOO	68	GO083 GO08			084	
		1990	1994	1990	1994	1990	1994	1990	1994	1990	1994	1990	1994
Units: ug/L													
RDX	2	568.2	430	2700	3100 LT*	33.8	14.4	6500	2500	2900	1200	290	120
нмх	400	48.3	26	82 LT	110	6.95	2.92	700	350 LT	350	99	11.8	14
2,4,6 TNT	2	55,6	28.3	760	3700	0.588 LT	0.426 LT	5100	3600	5300	3100	560	250
1,3 DNB	1	0.7	0.458 LT	42	35	0.519 LT	0.458 LT	60	82	0.519 LT	5.6	0.519 LT	0.46 LT
2,4 DNT	1000	2.4	37	40.2	120	0.612 LT	0.397 LT	100	350	29	95	3.06	12
2,6 DNT	1000	1.15 LT	0.6 LT	11.4	32.3 LT	1.15 LT	0.6 LT	58 LT	60 LT	58 LT	12 LT	58 LT	12 LT
1,3,5 TNB	3.5	31.1	29	67	950	0.626 LT	0.429 LT	310	490	730	800	550	320
NB	3.5	1.07 LT	0.682 LT	1.07 LT	12.3 LT*	1.07	0.682 LT	320	68 LT*	1.07 LT	14 LT*	1.07	0.682 L1
TETRYL	430	1.5	0.631 LT	0.556 LT	6.3 LT	0.556 LT	0.631 LT	28 LT	31	28 LT	95	28 LT	5.66

Table 3–5. Groundwater Sampling Data for Area P: 1990–1994 Louisiana Army Ammunition Plant

Shaded area represents concentration above HAL

HAL: Health Advisory Level

LT: Less than

*: Concentration reported as "LT" due to interference during sample analysis.

			Uppe	er Terrace	Aquifer V	Vells			Lowe	er Terrace	Aquifer V	Vells	
Parameter	HAL	G00	085	GO	104	GO	109	GO	105	G0	106	GO	110
		1990	1994	1990	1994	1990	1994	1990	1994	1990	1994	1990	1994
Units: ug/L													
RDX	2	7600	3800	1900	8400	4200	3100	1300	330	2500	4100	3200	2800
нмх	400	1000	310 LT	910	370 LT	750	300	210	360	82 LT	53 LT	139.5	130
2,4,6 TNT	2	16000	4200	15000	11000	1800	3600	94	16.5	1300	8800	760	570
1,3 DNB	1	120	32	660	580	23	8.2	90	320	240	330	26 LT	24
2,4 DNT	1000	130	79	720	570	36.3	330	33	54	200	640	84	120
2,6 DNT	1000	58 LT	59 LT	58 LT	60 LT	58 LT	60 LT	6.32	60 LT	29.1	60 LT	58 LT	60 LT
1,3,5 TNB	3.5	7300	3800	6700	6300	28	95	1200	3900	370	970	420	460
NB	3.5	1.07 LT	67 LT*	4000	68 LT*	1.07 LT	6.8 LT*	600	68 LT*	1.07	68 LT*	1.07 LT	6.8 LT*
TETRYL	430	28 LT	310	28 LT	130	28 LT	39.9	0.556 LT	3.71	0.556 LT	63 LT	28 LT	0.63 LT
Shaded area	a repre	sents con	centration	n above H	AL			L	<u> </u>	1	L	1	<u> </u>

Table 3-5.Groundwater Sampling Data for Area P: 1990-1994Louisiana Army Ammunition Plant (Cont.)

Shaded area represents concentration above HAL

HAL: Health Advisory Level

LT: Less than

*: Concentration reported as "LT" due to interference during sample analysis.

3.3.2 Upper Terrace Aquifer - Groundwater Sampling Results

Nine monitoring wells, screened in the Upper Terrace aquifer and located on and adjacent to Area P, were sampled by Science Applications International Corporation (SAIC) in 1994. These wells were installed between 1979 and 1986 (see Table 3-3). All nine COCs were detected in the Upper Terrace aquifer at Area P. The following sections discuss the analytical data for each COC detected in 1994 and compare this data to the concentrations detected in 1990. The 1994 nitrocompounds distribution in the Upper Terrace aquifer is shown in Figure 3-4.

3.3.2.1 RDX

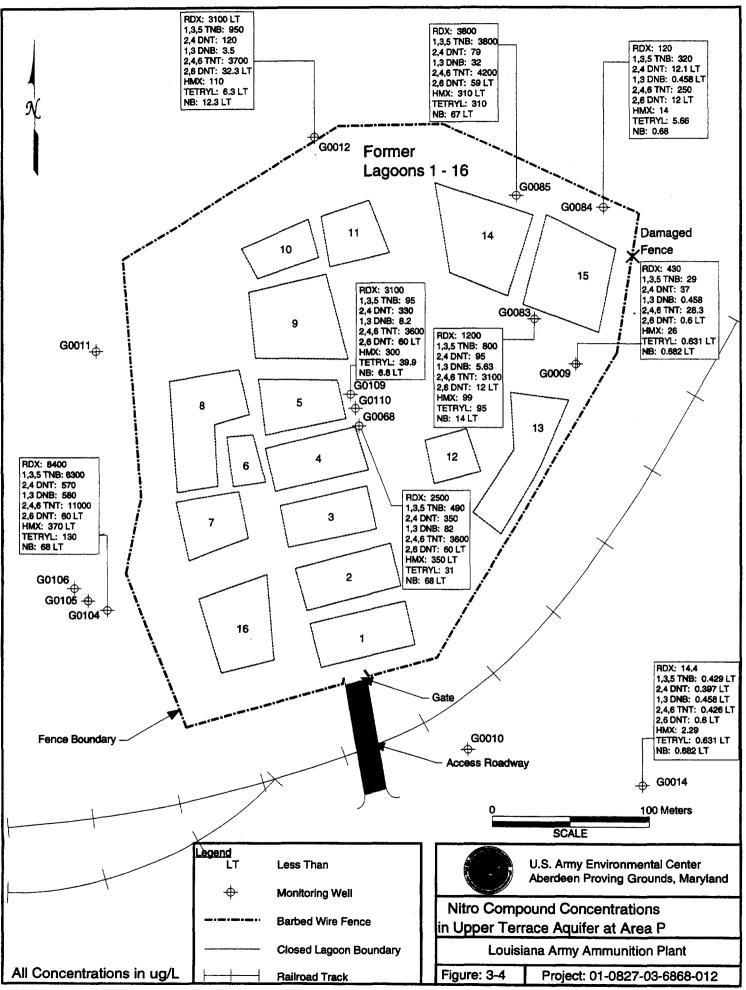
Analytical results of RDX in the Upper Terrace aquifer ranged from a minimum of 14.4 μ g/L in well G0014 to 8,400 μ g/L in well G0104 (see Table 3-4). The 1994 concentrations detected in all wells exceeded the HAL of 2.0 μ g/L.

In 1990, levels of RDX in the Upper Terrace aquifer ranged from 33.8 μ g/L in well G0014 to 7,600 μ g/L in well G0085 (see Table 3-5). All wells sampled exceeded the HAL of 2.0 μ g/L.

Higher levels of RDX were detected in samples collected from wells G0068, G0085, and G0109, located inside Area P, and wells G0012 and G0104, located west of Area P (see Figure 3-4). These wells are located in the general direction of groundwater flow in this area (see Figure 2-2). A similar trend was observed during the 1990 sampling event (ESE 1992). With the exception of well G0104 located west of Area P, the 1994 concentrations are lower than the 1990 concentrations. The historical data indicate that the maximum concentration of RDX was detected in well G0012 (43,200 μ g/L) during the March 1985 sampling event.

3.3.2.2 HMX

Analytical results of HMX ranged from below detection limit (BDL) to 370 μ g/L (see Table 3-4). The highest concentration of HMX was detected in well G0104 located west of Area P (see Figure 3-4). No samples collected during the 1994 sampling event exceeded the HAL of 400 μ g/L.



In 1990, levels of HMX ranged from BDL to 1,000 μ g/L (see Table 3-5). Wells G0068, G0085, G0104, and G0109 exceeded the HALs in 1990. The 1994 concentrations are lower than the 1990 concentrations. The maximum concentration of HMX was detected in well G0012 (8,850 μ g/L) in March 1983. In 1994, well G0012 had an HMX concentration of 110 μ g/L.

3.3.2.3 2,4,6-TNT

In 1994, the concentration of 2,4,6-TNT ranged from BDL to 11,000 μ g/L in well G0104 (see Table 3-4). All wells located in Area P and wells G0012 and G0104 located adjacent to Area P had concentrations exceeding the HAL of 2.0 μ g/L. Wells G0012 and G0109 had higher concentrations in 1994 than in 1990.

In 1990, eight wells had concentrations above the HAL of 2.0 μ g/L. The concentration levels ranged from 55.6 μ g/L in well G0009 to 16,000.0 μ g/L in well G0085. 2,4,6-TNT was detected in well G0104 at a concentration of 15,000 μ g/L (see Table 3- 5). In February 1988, well G0104 had 2,4,6-TNT concentrations of 25,000 μ g/L.

3.3.2.4 1,3-DNB

Analytical results of 1,3-DNB ranged from BDL to 580 μ g/L in well G0104. Wells G0009, G0012, G0068, G0083, G0085, G0104, and G0109 had concentrations above the HAL of 1.0 μ g/L (see Table 3- 4). The distribution of 1,3-DNB concentration is shown in Figure 3-4. Wells G0068 and G0083 had higher concentrations in 1994 than in 1990.

In 1990, the maximum concentration detected was 660 $\mu g/L$ in well G0104. Wells G0012, G0068, G0085, G0104, and G0109 had concentrations above the HAL of 1.0 $\mu g/L$ (see Table 3-5).

3.3.2.5 2,4-DNT

In 1994, the highest concentration of 2,4-DNT was found in well G0104 (570 μ g/L). This concentration is below the HAL of 1,000 μ g/L. In 1994, samples collected from wells G0068 (350 μ g/L) and G0109 (330 μ g/L), located inside Area P, and well G0104 (570 μ g/L), located west of Area P, had relatively higher levels of 2,4-DNT (see Figure 3- 4). In 1990, the concentration ranged from 2.4 μ g/L in well G0109 to 720.0 μ g/L in well G0104 (see Table 3-5). In February 1988, well G0104 had a 2,4-DNT concentration of 770 μ g/L. Historical data indicate that concentrations of 2,4-DNT has been below the HAL of 1,000 μ g/L.

3.3.2.6 2,6-DNT

All sample results for 2,6-DNT in 1994 were below the instrument detection limit and the HAL of 1,000 μ g/L (see Table 3-4). In 1990, none of the sampled wells exceeded the HAL (Table 3-5). The maximum concentration of 2,4-DNT was detected in well G0012 (400 μ g/L) during the March 1983 sampling event. This level is below the HAL of 1,000 μ g/L.

3.3.2.7 1,3,5-TNB

Analytical results of 1,3,5-TNB ranged from BDL to 6,300 μ g/L. All wells in Area P and wells G0104 and G0012 located adjacent to Area P had concentrations exceeding the HAL of 3.5 μ g/L (see Table 3-4). The maximum concentration was detected in well G0104 located west of Area P. Well G0085 located near the northern boundary of Area P had a concentration of 3,800 μ g/L.

In 1990, the maximum concentration was detected in well G0085 (7,300 μ g/L). Well G0104 had a concentration of 6,700 μ g/L. All wells in Area P and wells G0104 and G0012 located adjacent to Area P had concentrations exceeding the HALs (see Table 3-5). The maximum concentration of 1,3,5-TNB was detected in July 1986 in well G0104 (7,700 μ g/L).

3.3.2.8 NB

In 1994, sample results of NB for wells G0009, G0104, and G0084 had concentrations below the instrument detection limit and the HAL of 3.5 μ g/L. Results of NB for wells G0012 (12.3 μ g/L), G0068 (68 μ g/L), G0083 (14 μ g/L), G0085 (67 μ g/L), G0104 (68 μ g/L), and G0109 (6.8 μ g/L) were affected by interferences during analysis. Therefore, the concentrations have been reported as "less than (LT)." Sample results from wells G0068 and G0104 were rejected due to low recoveries.

In 1990, wells G0068 (320 $\mu g/L)$ and G0104 (4,000 $\mu g/L)$ had concentrations above the HALs. These concentrations are significantly higher than the 1994 concentration of NB (see Table 3-4).

3.3.2.9 TETRYL

In 1994, the TETRYL concentration ranged from BDL to 310 μ g/L in well G0085 (see Table 3-4). These concentrations were below the HAL of 430 μ g/L. The distribution of TETRYL concentration is presented in Figure 3-4.

During the 1990 sampling event, only well G0009 had a detectable concentration of TETRYL (1.5 μ g/L) (see Table 3-5). The maximum concentration of TETRYL was detected in well G0012 (1,500 μ g/L) during the August 1983 sampling event.

3.3.3 Lower Terrace/Sparta Sand Aquifer - Groundwater Sampling Results

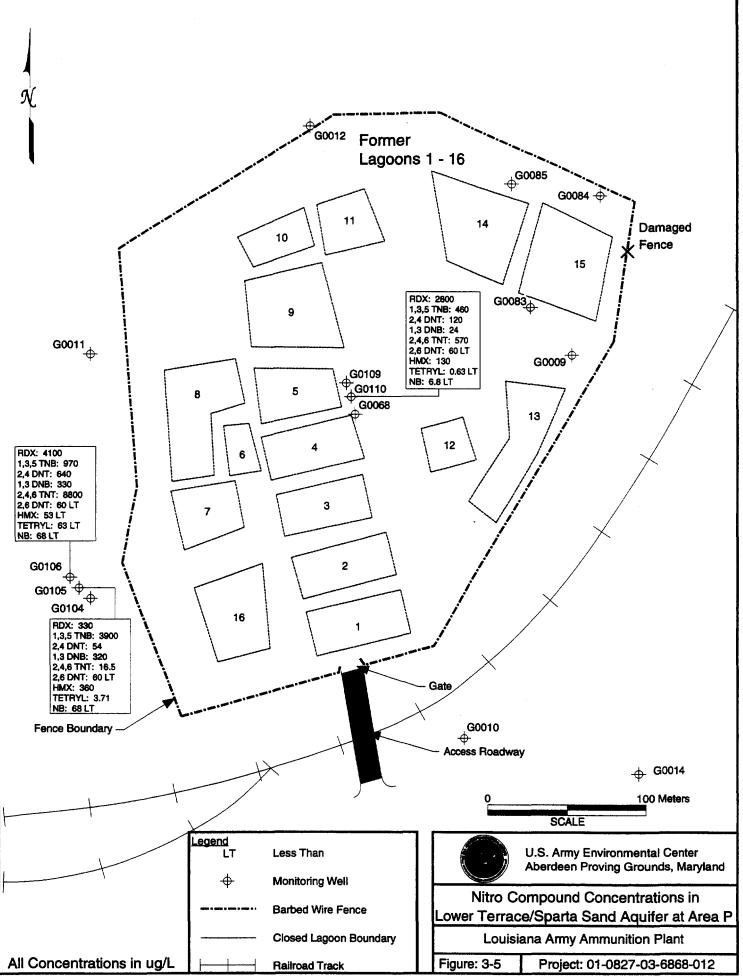
Three monitoring wells, G0105, G0106, and G0110, screened in the Lower Terrace/Sparta Sand aquifer, were sampled in 1994 (see Figure 3-3). These wells were installed in 1986, and therefore, have limited historical sampling data. The COCs detected in the Lower Terrace at Area P are the same as those found in the Upper Terrace aquifer. The following section describes the concentration range of each COC detected in 1994 and compares the concentrations to the 1990 concentrations detected in wells G0105, G0106, and G0110. The COC distribution is shown in Figure 3-5.

3.3.3.1 RDX

Analytical results of RDX in the Lower Terrace aquifer ranged from 330 μ g/L in well G0105 to 4,100 μ g/L in well G0106 (see Table 3-4). All wells sampled had RDX concentrations exceeding the HAL of 2.0 μ g/L. The distribution

of RDX is shown in Figure 3-5.

In 1990, the levels of RDX in the Lower Terrace aquifer ranged from 1,300 μ g/L in well G0105 to 3,200 μ g/L in well G0110 (see Table 3-5). The 1994 concentration of RDX for well G0106 was higher than the 1990 concentration. This well is located west of Area P.



3.3.3.2 HMX

Analytical results of HMX ranged from BDL to 360 μ g/L in well G0105 (see Table 3-4). In 1990, the maximum concentration of HMX was detected in well G0110 (139.5 μ g/L) (see Table 3-5). No samples collected during the 1990 and 1994 sampling events exceeded the HAL of 400 μ g/L.

3.3.3.3 2,4,6-TNT

In 1994, wells G0105 (17 $\mu g/L)$, G0106 (8,800 $\mu g/L)$, and G0110 (570 $\mu g/L)$ had 2,4,6-TNT concentrations above the HAL of 2.0 $\mu g/L.$

In 1990, all three wells had concentrations exceeding the HAL of 2.0 μ g/L. The concentration levels ranged from 94 μ g/L in well G0105 to 1,300 μ g/L in well G0106 (see Table 3-6). Well G0110 located on Area P had 2,4,6-TNT concentrations of 760 μ g/L. The 1994 concentration of 2,4,6-TNT was generally higher than the 1990 concentration. The 1994 concentration of 2,4,6-TNT was generally higher than the 1990 concentration.

3.3.3.4 1,3-DNB

Analytical results of 1,3-DNB ranged from 24 μ g/L in well G0110 to 330 μ g/L in well G0104. All three wells sampled in 1994 had concentrations exceeding the HAL of 1.0 μ g/L (see Table 3-4). In 1990, the concentrations ranged from less than 26 μ g/L in well G0110 to 240 μ g/L in well G0104 (see Table 3-5). The 1994 concentration of 1,3-DNB was generally higher than the 1990 concentration.

3.3.3.5 2,4-DNT

In 1994, no wells sampled in the Lower Terrace/Sparta Sand aquifer exceeded the HAL of 1,000 $\mu g/L$ (see Table 3-4). The maximum concentration was detected in well G0106 (640 $\mu g/L)$.

Well No.	No. of Sampling Events	No. of COCs with Four or More Data Points							
Upper Terrace Aquifer									
G0009	17	8							
G0012	18	9							
G0014	16	9							
G0068	6	9							
G0083	2	0							
G0084	2	0							
G0085	2	0							
G0104	4	9							
G0109	4	9							
Lower Terrace/Sparta Sand Aq	uifer								
G0105	3	0							
G0106	2	0							
G0110	4	7							

Table 3-6. Groundwater Data Available for Trend Analysis

Note: Number of data sets with four or more data points: 60.

In 1990, the concentration level ranged from 33 μ g/L in well G0105 to 200 g/L in well G0106. The 1994 concentration of 2,4-DNT in the Lower Terrace aquifer was generally higher than the 1990 concentration.

3.3.3.6 2,6-DNT

All sample results for 2,6-DNT were below the instrument detection limit and the HAL of 1,000 μ g/L (see Table 3-4). In 1990, none of the wells sampled exceeded the 2,6-DNT HALs.

3.3.3.7 1,3,5-TNB

Concentrations of 1,3,5-TNB ranged from 460 μ g/L in well G0110 to 3,900 μ g/L in well G0105 (see Table 3- 4). These levels exceeded the HAL of 3.5 μ g/L. In 1990, wells G0105, G0106, and G0110 had concentrations exceeding the HALs. The 1994 concentrations of 1,3,5-TNB in the Lower Terrace aquifer are higher than the 1990 concentrations.

3.3.3.8 NB

In 1994, the results for weUs G0105 (68 g/L), G0106 (68 μ g/L), and G0110 (6.8 μ g/L) were affected by interferences during analysis. Therefore, the concentrations have been reported as "less than LT." Sample results from well G0106 was rejected due to low recoveries.

3.3.3.9 TETRYL

In 1994, TETRYL concentrations ranged from BDL to 3.7 μ g/L in well G0105. These concentrations are below the HAL of 430 μ g/L. During the 1990 sampling event, concentrations of TETRYL were below the instrument detection limit and the HAL (see Table 3-5).

3.3.4 Summary of Groundwater Sampling Results

Nine wells screened in the Upper Terrace aquifer had concentrations of RDX, 1,3,5-TNB, 1,3-DNB, 2,4,6-TNT, and NB above the HALs. Concentrations of 2,4-DNT, 2,6-DNT, and HMX were below the respective HALs. The maximum concentration of explosives was detected in well G0104 located southwest of Area P. Historical data indicate that the maximum COC concentrations were detected in well G0104. These concentrations were detected prior to implementation of the interim remedial action. The 1994 concentration of explosives in the Upper Terrace aquifer was lower than the 1990 concentration, indicating that the groundwater quality at Area P had unproved since the remedial measure was completed.

Three wells screened in the Lower Terrace aquifer were sampled during the 1994 field investigation activities. As in the Upper Terrace aquifer, concentrations of RDX, 1,3,5-TNB, 1,3-DNB, 2,4,6-TNT, and NB were above the HALs. Generally, the concentrations of the COCs in the Lower Terrace aquifer were less than the concentrations detected in the Upper Terrace aquifer. However, the 1994 concentrations in the Lower Terrace aquifer were higher than the 1990 concentrations for wells G0105 and G0106 located southwest of Area P. This increase in concentration can be attributed to the downward movement of contamination from the Upper Terrace aquifer. Groundwater quality simulation conducted at Area P by ETA in 1991 showed similar migration patterns.

3.4 TREND ANALYSIS IN GROUNDWATER MONITORING DATA AT AREA P

This section compares the groundwater monitoring data collected during the 1994 sampling effort with the historical data and discusses the trends in the groundwater quality. Statistical regression analysis was used to characterize temporal trends of COC concentrations measured in groundwater samples collected at Area P.

3.4.1 Objectives

The objectives for conducting the trend analysis in the groundwater monitoring data at Area P include:

• Conducting a review of the historical data and data collected during the Five-Year Review field investigation effort in order to identify the trends of groundwater quality at Area P

• Evaluating the effectiveness of the interim remedial action (IRA) on the groundwater quality.

3.4.2 Background

Groundwater data were reviewed for 12 monitoring wells located on and adjacent to Area P. Nine of these wells are screened in the Upper Terrace aquifer and the other three are screened in the Lower Terrace/Sparta Sand aquifer.

Upper Terrace Aquifer

- G0009 G0084
- G0012 G0085
- G0014 G0104
- G0068 G0109
- G0083

Lower Terrace/Sparta Sand Aquifer

- G0105
- G0106
- G0110

The nine COCs identified for groundwater at Area P are listed below:

- RDX
- HMX
- 1,3-DNB
- 2,4-DNT
- 2,6-DNT
- 1,3,5-TNB
- 2,4,6-TNT
- TETRYL
- NB.

Groundwater sampling data for Area P are available from January 1980 through March 1994. Groundwater monitoring data for each well are presented in Appendix C (Tables C-1 through C-12). Table 3-6 summarizes data available for groundwater trend analysis. For this study, a data set is composed of a COC and a monitoring well, and the sampling event represents the data points for this data set. Therefore, corresponding to the data set for 2,4-DNT in well G0009, the February 1994 and the July 1986 concentrations are two data points. For each well, the number of COCs with more than four data points also are presented. To provide an accurate representation of the trend, a minimum of four data points were selected to be considered a "valid data set." Two data points can yield a perfect linear fit (a straight line joining the two points), while three points can provide a perfect quadratic fit (a curve passing through the three points).

3.4.3 Approach

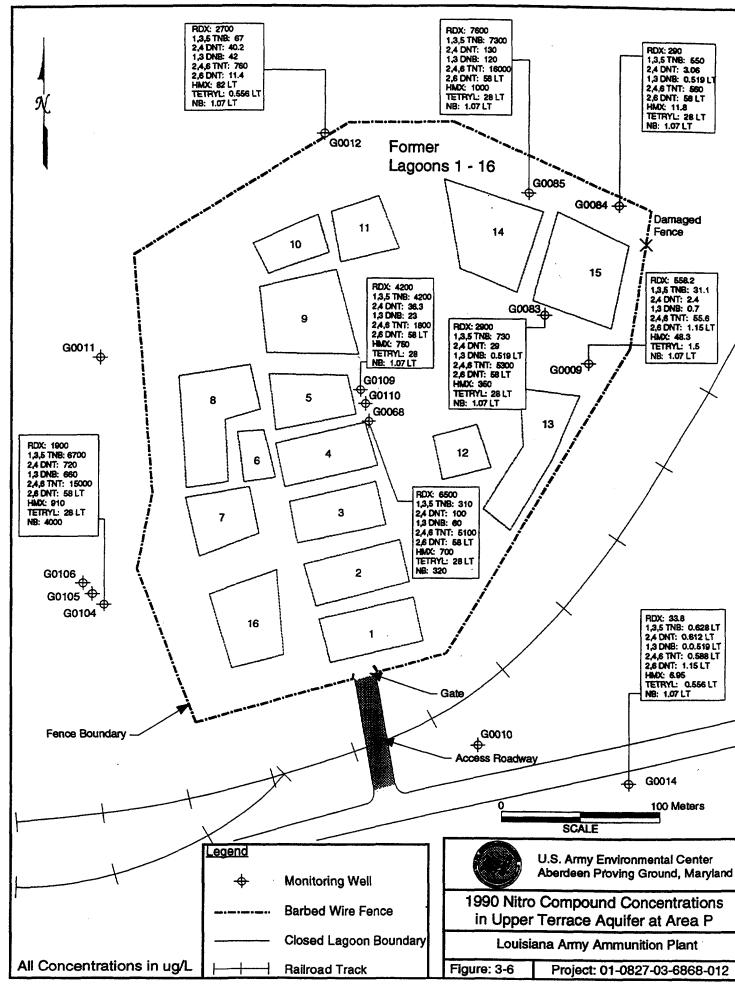
Statistical regression methods previously used at other sites to evaluate groundwater trends were used in this study (Lachance and Stoline 1993; Stoline, Passero, and Barcelona 1993). The primary objective of this regression analysis is to identify the trend in groundwater quality using the sampling data available from 1980 through 1994.

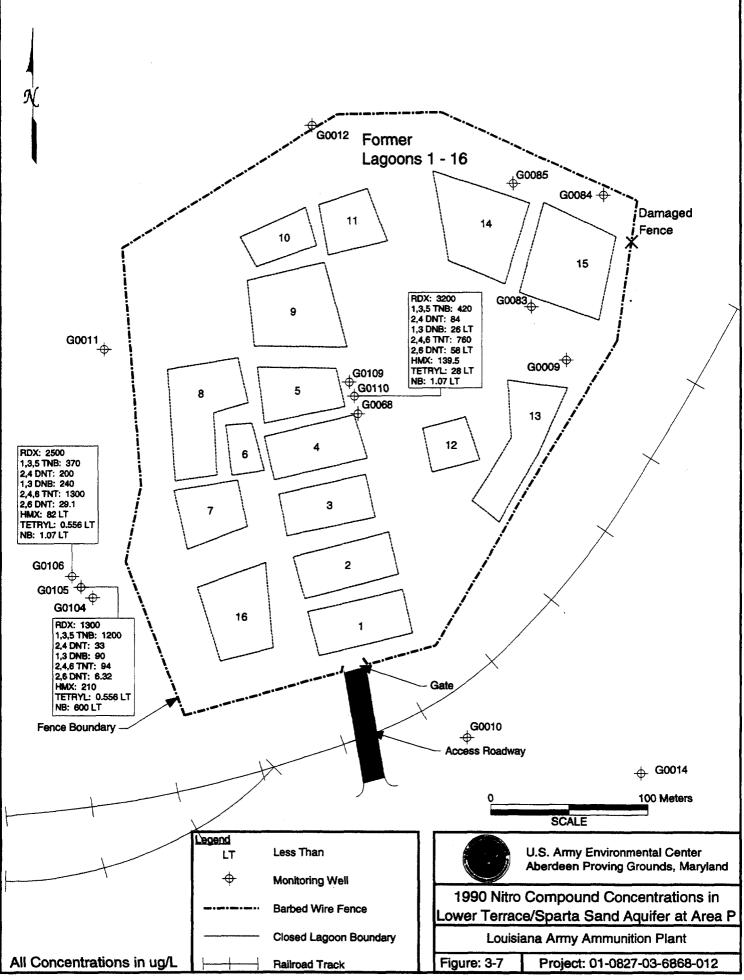
Two methods were used in evaluating well sampling data to identify the trends in groundwater quality. Bar charts were used to illustrate the available groundwater sampling data. These charts were used for the subjective assignment of trend categories and comparison with regression analysis. The subjective assignment was based on a visual interpretation of the groundwater data. A regression analysis was conducted on the available data to determine the trend in groundwater quality and the effectiveness of the IRA. The results from these approaches are presented in more detail in the following sections.

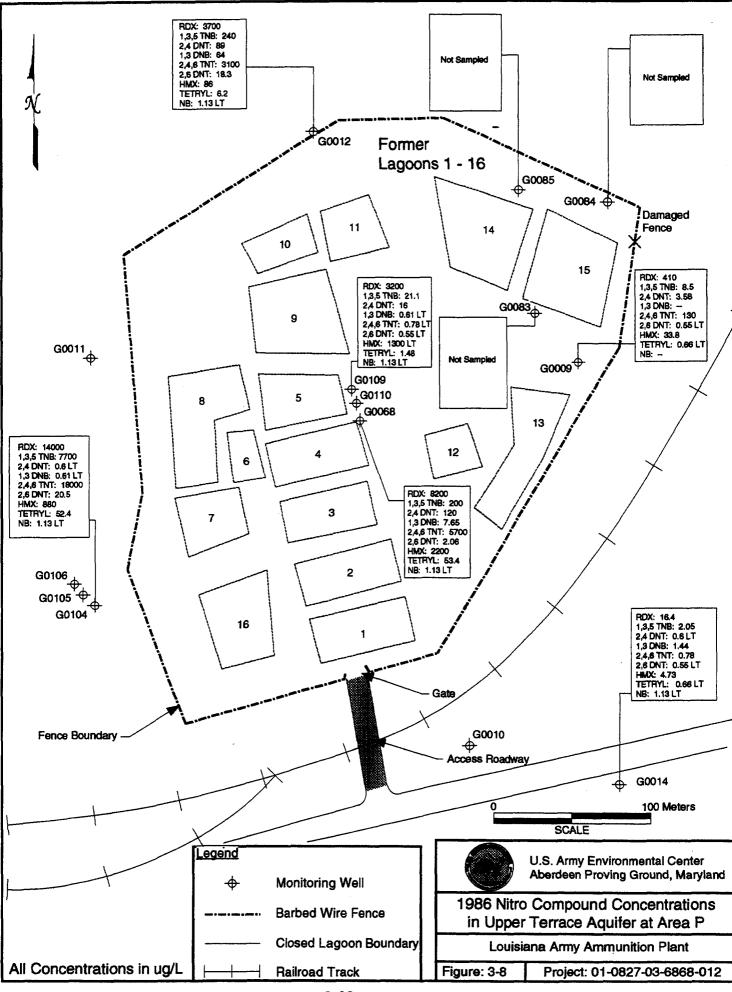
3.4.3.1 Bar Charts

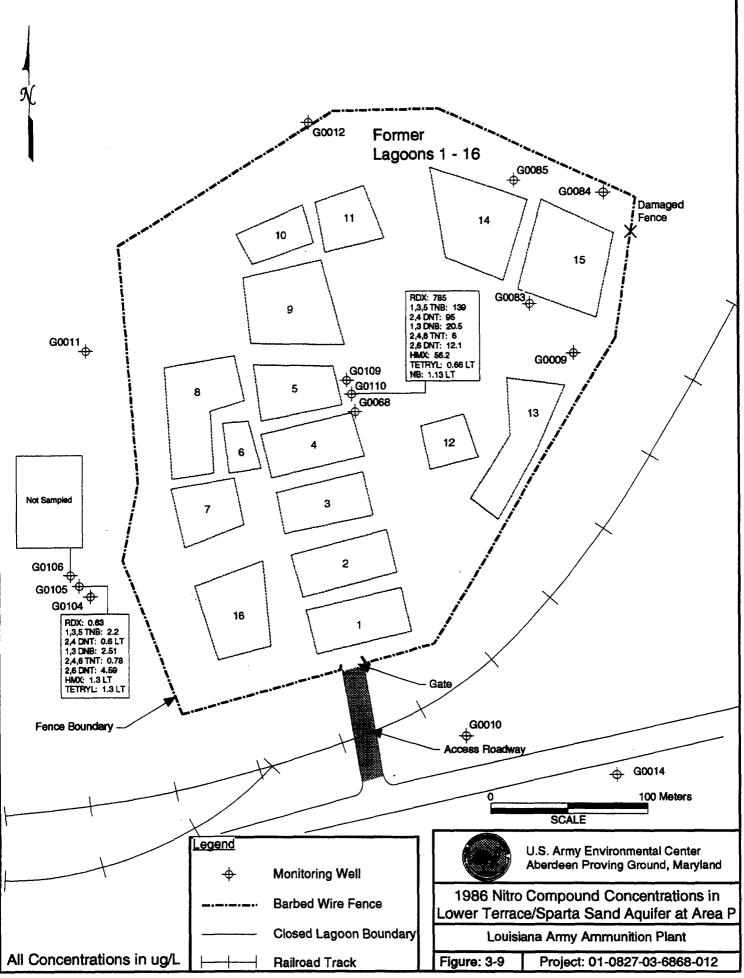
Bar charts showing the concentration of COCs for each sampling event are presented for each well in Appendix C (Figures C-1 through C-18). These charts show the variation in concentrations of COCs over time at a particular well. Contaminants that were detected at concentrations below the HALs were not included in these bar charts.

Figure 3-6 shows the contaminant concentrations at the site in the Upper Terrace aquifer from the 1990 sampling event. The data for the Lower Terrace/Sparta Sand aquifer for this sampling event are shown in Figure 3-7. The contaminant concentrations for the 1986 sampling event are depicted in Figures 3-8 and 3-9 for the Upper Terrace and Lower Terrace/Sparta Sand aquifers, respectively. The data for the most recent sampling activity in 1994 are included in Section 3.3. These figures, along with the bar charts, were used for subjective assignment of trend categories.









3.4.3.2 Regression Analysis

A description of the regression analysis software used to identify the trend of groundwater quality is included in this section. The trends were identified on the basis of the curves generated by the regression software.

Regression Analysis Software - Groundwater monitoring results were plotted as a function of time using the Microsoft ® Excel- Version 5.0. The plots are included in Appendix D. Each plot contains the following information:

- A line connecting the data points
- A line showing the regression fit with the linear equation (y = a+ bt)
- A curve showing the regression fit with the quadratic equation (y =a + bt + ct2)

where: a, b, and c = constants t = time y = concentration.

Groundwater Quality Trend Categories— There are a total of 108 data sets (12 wells by 9 COCs), 60 of which are valid data sets (i.e., number of data sets with 4 or more data points). One of the eight trend categories identified in Table 3-7 was assigned to each of these data sets. The rules used for assigning trend categories are shown in Table 3-8 and are discussed below:

Four observations were chosen as the minimum number of data points needed in order to attempt fitting the regression models. Therefore, if m (number of observations) is less than four, the model Z was selected.
If at least four data points are available (m S 4), but all concentrations are below the detection limits, the model ND was selected.

Table 3-7	. Groundwater	Quality	Trend	Categories
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Model Code	Trend Category	Regression Trend Model	Model
Z	Less than 4 data points	No model	none
ND	Nondetect or zero	No model	none
NM	No model fits data	No model	none
С	Constant	у = с	constant
ID	Increasing then decreasing	y = a + bt + ct2, c<0	quadratic
DI	Decreasing then increasing	y = a + bt + ct2, c>0	quadratic
I	Increasing	y = a + bt, b>0	linear -
D	Decreasing	y = a + bt, b<0	linear

Table 3-8. Trend Model Selection Rules

Rule	Selection of Trend Category
Rule l	If $m < 3$ or $m = 3$, the model Z is selected.
Rule 2	If m > 3 and no data point is a detectable value, the model ND is selected.
Rule 3	If m > 3 and at least one data point is a detectable value, the quadratic fit is attempted. If a maximum exists, ID is selected. If a minimum exists for the quadratic fit, DI is selected. If no point of inflection (maximum or minimum vertex) exists for the curve within the sampling period (1980 through 1994), a linear fit is selected.

Rule 4	If the linear fit has a positive slope, I is selected; for a negative slope, D is selected. For slope 0, C is selected.
Rule 5	If neither the quadratic nor linear regression models fit the data, NM is selected. The NM code was selected during subjective analysis only.

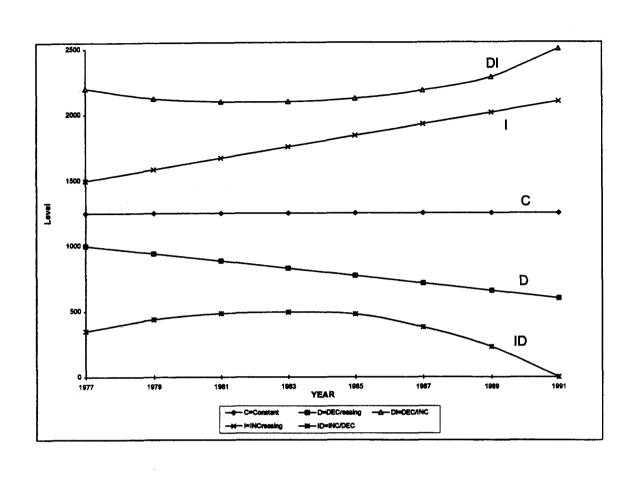
- When four data points are available and at least one of these points is a detectable value, the regression analysis software was first used to fit a quadratic curve. The non-detectable values were assigned a value of one-half the detection limit for that particular compound. The model code DI (decreasing then increasing) or ID (increasing then decreasing) was assigned to this quadratic curve if a minimum or a maximum value (i.e., a vertex) was observed within the sampling interval (1980 through 1994).
- If the quadratic curve had no point of inflection (maximum or minimum vertex) within the sampling interval evaluated, a linear fit was selected for the data set and a model code D, I, or C was assigned depending on the slope of the straight line.
- If no model could fit the data, the NM code was chosen to indicate that none of the trend models adequately characterize the data. The NM code was used during subjective analysis only.

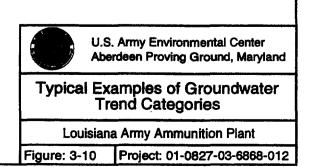
Figure 3-10 shows typical examples of the quadratic and linear regression curves.

Groundwater Quality Trend Conditions- Four groundwater quality trend conditions were defined using the trend categories listed in Table 3-7. Those COCs, which either showed a decrease in the concentration level throughout all of the sampling events (D) or an initial increase, followed by a decrease in the concentration level during the latter sampling events (ID), are considered indicative of generally improving (IMP) groundwater quality. Contaminants showing a persistent increase in concentration during all sampling events (I), or those that showed an initial decrease in concentration followed by an increase in concentration during the latter sampling events (DI), are indicative of generally deteriorating (DET) groundwater quality. Similarly, the stabilized condition (STA) included the constant concentration (C) category. The NM, ND, and Z categories were grouped as unidentified (UNI). Table 3-9 shows the trend categories comprising each trend condition.

Table 3-9.	Groundwater	Quality	Trend	Conditions
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Trend Condition	Trend Categories	Definition			
IMP	D, ID	Improvement			
DET	I, DI	Deterioration			
STA	C	Stabilization			
UNI	NM, ND, Z	Unidentified			





Groundwater Trend Index- For each well, a trend index (TI) was assigned and defined as:

TI = NIMP + NSTA - NDET where:

NIMP, NSTA and NDET are numbers of trends classified as IMP, STA, and DET, respectively, for a given well. The STA trend was considered a positive TI because it indicated no deterioration in the groundwater quality. The UNI trends are not used in determining the TI. Clearly, a well with a larger TI value shows more evidence of improving groundwater quality than one with a smaller TI value. TI values were calculated for each individual well (based on the trends for the 9 COCs) and for each COC (based on the trends for the 12 wells). Calculations for the TIs are included in Appendix E. Table 3-10 shows the trend categories assigned to each of the 108 data sets. The sum of the individual TIs for all the wells in each aquifer yielded the overall trend index (OTI) for that aquifer. The TI for each well and the OTI values for the two aquifers are included in the table. In addition, the TI values for each well and the OTI also were determined for those data sets that had all concentration levels above the HALs. It is expected that these TI values (without HALs) will exclude any uncertainties in the trend analysis associated with the low concentration values (below HALs).

Effectiveness Assessment of the Area P Cap- In the evaluation of trend categories (ID, DI, I, D, and C), the trend category ID can be particularly useful in the assessment for the potential positive impact of the IRA upon groundwater quality trends. An ID trend shows evidence of recent improvement after an initial period of deterioration. The dates of maximum concentration were estimated from the plots (see Appendix D) and are included in Table 3-11. A comparison of the capping date with the estimated date of maximum contamination was used to support conclusions regarding the cap effectiveness.

The DI trend categories also were evaluated during the assessment of cap effectiveness to identify any negative impact of the IRA on the groundwater quality. The dates of the minimum vertex for the DI trends were compared to the period of remedial activity.

Subjective Determination of Trends- Using bar charts generated for the available data (concentration versus time), the trend fits were subjectively determined by qualitative evaluation of sampling data. The subjective approach was conducted to verify the objective findings made

Aquifer	Upper Terrace Aquifer							Lower Terrace/Sparta Sand Aquifer				
Contaminant/Well	009	012*	014*	068	083	084	085	104*	109	105*	106*	110
DNB	z	D	ID	DI	Z	z	Z	ID	ID	Z	Z	Z
2,4-DNT	DI	I	ID	DI	Z	z	Z	ID	DI	Z	Z	ID
2,6-DNT	ID	ID	ND	DI	Z	z	z	I	ND	Z	Z	Z
НМХ	D	D	D	D	Z	z	Z	ID	ID	Z	Z	D
Nitrobenzene	ND	ND	ND	ID	Z	·Z	Z	ND	ND	Z	Z	Z
RDX	D	ID	ID	D	Z	z	Z	ID	ID	Z	Z	ID
Tetryl	ID	ID	ND	NM	Z	z	Z	DI	I	Z	Z	Z
1,3,5-TNB	DI	DI	ID	I	Z	Z	z	DI	I	Z	z	I
2,4,6-TNT	D	ID	ID	ID	Z	z	Ż	ID	I	Z	Z	ID
TI without HALs ALL DATA	+1/3 +3/7	+4/8 +4/8	+3/3 +6/6	0/6 +0/8	0/0 0/0	0/0 0/0	0/0 0/0	+2/7 +2/9	0/4 -1/7	0/0 0/0	0/0 0/0	+2/4 +3/5

Table 3-10. Computer-determined Trends in Groundwater Quality

Overall TI for Upper Terrace Aquifer without HALs + 10/30 All data + 14/44 Overall TI for Lower Terrace without HALs +2/4 All data +3/5

Note: Shaded areas indicate concentration levels for the contaminant in that monitoring well were below the HALs established for that contaminant at LAAP. Asterisk () denotes wells located outside the capped area. TI is presented for all data, and for data excluding the data sets with concentrations below HALs (without HALs).

,

Well No.	Contaminant	Estimated Maximum Concentration Date
		concentration bate
G0009	2,6-DNT	March 1982
	Tetryl	January 1982
G0012*	2,6-DNT	January 1982
GOOTZ"	RDX	July 1987
	Tetryl	January 1983
	TNT	August 1987
	1111	August 1907
G0014*	DNB	April 1984
	2,4-DNT	December 1981
	RDX	March 1987
	TNB	November 1984 September
	TNT	1984
G0068	Nitrobenzene TNT	January 1990
00000	NICIODENZENE INI	July 1989
		5 diy 1969
G0083	None	None
G0084	None	None
G0085	None	None
G0104*	DNB	January 1993
	2,4-DNT	March 1991
	HMX	December 1988 August
	RDX	1989
	TNT	March 1988
G0109	DNB	January 1991
	HMX	August 1989
	RDX	January 1990
G0105*	None	None
G0106*	None	None
G0110	2,4-DNT	April 1988
-	HMX	September 1991
	RDX	June 1991
	TNT	May 1990

Table 3-11. Estimated Dates of Maximum Concentration for ID Trends

Note: *denote monitoring wells located outside the Area P cap.

by the computer based on the regression analysis. The subjective trends are included in Appendix E. These subjective findings were compared to the computer- determined trend types in Table 3-12. The computer-determined trends are those that were based on the regression analysis. The diagonal values indicate agreement of the subjective trends with the computer determined trends. For example, out of a total of seven computer-determined I trends, one was subjectively assigned NM, one was assigned C, and the remaining five were assigned I. Therefore, five subjective-determined trends were in agreement with the seven computer determined I trends.

Table 3-12. Subjective Versus Computer-determined Trend Types

Computer-determined Trend Type		Suk			-deteri Type	mined	Total (Computer- determined Trends)
	UNI	С	I	D	ID	DI	
UNI	55	0	0	0	0	0	55
С	0	0	0	0	0	0	0
I	1	1	5	0	0	0	7
D	1	0	0	3	1	0	5
ID	2	0	0	0	25	0	27
DI	1	0	1	0	4	8	14
Total (Subjective Trends)	60	1	6	3	30	8	108
	Diag	onal	. Tot	al:	96/10	8	

Note: The UNI trend type includes Z, ND, and NM trend categories.

3.4.4 Discussion of Findings from Groundwater Trend Analysis

Groundwater sampling data collected over a period of 14 years (1980 through 1994) were evaluated for 12 monitoring wells and 9 COCs. Nine monitoring wells are screened in the Upper Terrace aquifer and the other three are screened in the Lower Terrace/Sparta Sand aquifer. At least four data points would be required to provide a more accurate representation of the data using the computer regression analysis for each data set for identifying the groundwater quality trends. Two data points can yield a perfect linear fit, whereas three points can provide a perfect quadratic fit; therefore, a minimum of four data points were selected for computer regression analysis. Out of the possible 108 data sets (12 wells x 9 contaminants), 60 sets have 4 or more data points and were used for trend analysis; 48 data sets had less than 4 data points. The following sections describe the findings from the trend analysis. Supporting data are included in Appendix E.

The 48 data sets that had less than 4 data points were assigned category Z. Out of the remaining 60 data sets, no contaminants were positively detected in 7 data sets. These seven data sets were, therefore, assigned ND. Groundwater quality trend categories were assigned to each of the 53 remaining valid data sets (46 for the Upper Terrace aquifer and 7 for the Lower Terrace/Sparta Sand aquifer) on the basis of the regression curves generated by the software.

Upper Terrace Aquifer- The quadratic fit was selected if there was a point of inflection (maximum or minimum value) for the curve within the sampling interval (1980 through 1994), and accordingly, a DI or ID category was assigned. Out of the 46 valid data sets for the Upper Terrace aquifer, 23 were ID and 13 were DI. No point of inflection was observed in 10 data sets; therefore, a linear model was selected. Using the linear model, four data sets were categorized as D, while six were found to be I.

The OTI for the wells sampled is +8 out of 46, which indicates that the groundwater quality condition in the Upper Terrace aquifer at Area P is generally improving. A positive TI was calculated for three wells (G0012, G0014, and G0104). Wells G0009 (TI = - 1), G0068 (TI = - 1), and G0109 (TI = - 1) had negative TI values. G0109 and G0068 are located in the center of Area P inside the cap, adjacent to each other. G0009 is located close to these wells within the cap.

Among the COCs, RDX and TNT showed the greatest improving trend with an ID or D category for five of the six wells (with four or more sampling events). The contaminants 2,6-DNT, TETRYL, and 1,3,5-TNB showed an overall deteriorating trend (negative TI values) with increasing concentration levels. The contaminants 2,6-DNT and 1,3,5-TNB are possible degradation products of several other COCs.

In order to eliminate the uncertainty in the groundwater quality trends at lower concentrations, the 15 data sets comprising contaminant concentrations below the HALs were eliminated from the 46 valid data sets. No significant change was found in the conclusions from this trend analysis after removing the 15 data sets with concentrations below the HALs. The overall TI for Area P was + 9 for the 31 data sets. G0009, G0068, and G0109 exhibited TI values of -1/3, 0/6, and 0/4, indicating that the conditions at these wells are either stable or deteriorating. Among the contaminants, 1,3,5-TNB showed deteriorating trends (increasing concentration levels). Similarly, there was no change in the improving trend in the case of RDX orTNT.

Lower Terrace/Sparta Sand Aquifer- Voces wells, G0105, G0106, and G0110, sampled during the Area P Five-Year Review, are screened in the Lower Terrace/Sparta Sand aquifer. Wells G0105 and G0106 had less than four data points, and therefore, were categorized as Z. The overall trend in this aquifer based on well G0110 was found to be improving (TI = + 3). The contaminants 1,3,5-TNB and 2,6-DNT had a deteriorating trend (DI or I). As observed in the case of the Upper Terrace aquifer, excluding the two data sets that had concentrations below the HALs did not affect the overall improving trend at the site. **Effectiveness of the Area P Cap**- The data. sets that exhibited ID trends based on the regression fits were used to assess the effectiveness of the cap. Twenty-seven data sets had ID trends; 23 of these data sets were in the Upper Terrace aquifer, while 4 were in the Lower Terrace/Sparta Sand aquifer (see Table 3-11). The date of the maximum concentration (maximum vertex) was estimated from the data plots for these data sets (Appendix D).

An evaluation of the dates of maximum concentration indicated two distinct periods of maximum concentration in the Upper Terrace aquifer, and one period for the Lower Terrace/Sparta Sand aquifer. For the Upper Terrace aquifer, 7 (of 23) maximum values were observed between 1982 and 1984. Use of the lagoons for disposal ceased in 1980; it is possible that concentration levels started decreasing after a reasonable lag time (2 to 4 years) after the inactivity. The other period when the maximum values occurred was between 1987 and 1991 (14 of 23 points). Excavation of contaminated soil took place from November 1988 through August 1990. The Area P lagoons were capped in August 1990. After a reasonable lag time (0 to 3 years), the decrease in concentration levels after 1987 through 1991 could be attributed to the remediation activities.

For the Lower Terrace aquifer, the maximum values (four of four) were observed between 1988 and 1991, indicating that a downward trend in the concentration levels began during that time period. This downward trend in concentration levels also may be caused by the remediation activities at Area P assuming there was a time lag after the activity.

The DI trend categories were evaluated to identify any negative impact from the cap on the groundwater quality. The dates of the minimum vertex for DI trend categories are provided in Appendix E. Ten of the 14 lowest values were present between 1987 through 1991, which corresponds to the time of remediation activity and capping at Area P. However, no conclusion can be drawn from this observation because of the following uncertainties:

- Six data sets were subjectively assigned ID, I, and NM categories.
- Four data sets are for 1,3,5-TNB and TETRYL. The contaminant 1,3,5-TNB is a possible breakdown product, and therefore, had higher concentration levels after activities at the lagoons had ceased.
- Six data sets had concentration levels below the HALs.

On the basis of the above evaluation of the ID maximum values and the DI minimum values, results indicate that the cap and the remediation activity have resulted in an improvement of the groundwater quality at LAAP. However, due to the anomalies in computer regression and presence of breakdown products, some contaminants showed an increase in concentration levels during that period.

Precipitation data were evaluated for the period 1980 through 1994 to determine if there was any correlation between the precipitation and the groundwater concentration levels. A comparison of these data is presented in Appendix E. There was no specific correlation between the precipitation data and the nitro compounds concentration in the groundwater.

Comparison of the Computer-determined Trends with Subjective

Trends—During the trend analysis, 108 data sets were assigned groundwater categories based on specific rules applied to computer-generated regression curves. A comparison of these trends with the subjective trends indicated that 96 data sets (89 percent) had similar trends. However, excluding the 55 data sets (which were either Z or ND), 41 data sets out of the remaining 53 (77 percent) had matching trends.

The highest discrepancy between the subjective and the computer determinations was in the DI trend category. Four of the 13 computer determined DI were subjectively assigned ID because of increase in concentration levels in the early sampling events. One computer-determined DI was subjectively assigned an I because the concentration levels were higher than the previous rounds. Due to the fluctuating trend, one computer-determined DI was assigned an NM (no model) during the subjective analysis.

The subjective trends in groundwater quality are provided in Appendix E. The TI values based on the subjective trends were higher than the TI values based on the computer- determined trends for the Upper Terrace Aquifer. All wells had a positive TI except GO 109. The OTI for the Upper Terrace Aquifer was +18/46 (compared to the computer-generated OTI of +8/46). For the Lower Terrace Aquifer, the TI was lower for the subjective analysis because one computer- determined D trend was assigned a NM because of the fluctuations in concentration levels.

3.4.5 Conclusions

The conclusions drawn from the statistical groundwater trend analysis are summarized below.

Upper Terrace Aquifer

- The trend index of the wells sampled was +8, indicating the groundwater quality at Area P is improving. Of the 46 valid data sets, 23 were ID, 4 were D, 6 were I, and 13 were DI.
- RDX and TNT showed the best improving trend, whereas 2,6-DNT, TETRYL, and 1,3,5-TNB overall had a deteriorating trend.
- Excluding data sets with concentration below the HALs did not affect the overall improving trend at Area P.

Lower Terrace/Sparta Sand Aquifer

- Data sets from only one well (G0110) were available for trend analysis.
- The trend index of the wells sampled was +3, indicating that groundwater quality is improving.
- All contaminants had an improving trend except 1,3,5-TNB and 2,6-DNT.

• Excluding data sets with concentration below the HALs did not affect the overall trend conditions.

Assessment of Effectiveness of Cap

- Two distinct maximum periods of groundwater contamination were observed in the Upper Terrace aquifer. Seven (of 23) maximum values were observed between 1982 and 1984. The other period was between 1987 and 1991 (14 of 23 points). Remediadon activities (1988 through 1990), followed by capping of the site in 1990, may possibly account for the decreasing concentration levels after that time period.
- In the Lower Terrace/Sparta Sand aquifer, 4 (of 4) maximum values were observed between 1988 and 1991. Decrease in concentration after 1991 can be attributed to the remediation activities that were conducted from November 1988 through August 1990.
- No conclusion can be drawn from the evaluation of the minimum values for the DI curves because of several uncertainties.

3.5 QUALITY ASSURANCE/QUALITY CONTROL PROGRAM

A comprehensive quality assurance/ quality control (QA/QC) program was followed during the Five-Year Review of Interim Remedial Action conducted for the LAAP former Area P Lagoons to ensure that the analytical results and the decisions based on these results are representative of the environmental conditions at the site. The objectives of the Five-Year Review of the Area P Lagoons was to evaluate the effectiveness of the interim remedial measure. The following documents were utilized during evaluation of the QC data: the U.S. Army Toxic and Hazardous Material Agency (USATHAMA) Quality Assurance Program, PAM 11-41 (January 1990) for groundwater samples; QC requirements described in guidelines and specifications described in the Quality Assurance Project Plans (QAPPs) submitted as part of the project work plans prepared by SAIC, the Installation Restoration Data Management Information System (ERDMIS), Volume II Data Dictionary, Potomac Research Institute (PRI) (1994.1), and Laboratory Data Validation Functional Guidelines for Evaluating Organics Analysis (1988). The numbers of groundwater samples collected in addition to the numbers of field QC samples collected and selected laboratory QC (i.e., matrix spikes and matrix spike duplicates [MS/MSD]) samples analyzed, are summarized in Appendix F. The data review and validation worksheets are referenced within the subsection describing the applicable analysis. The QC checks and results are summarized below.

3.5.1 Data Quality Objectives

DQOs are quantitative and qualitative indicators of data quality. They are established based on the purpose of the project and the intended use of the data, human-based risk assessment requirements, and remedial design requirements. EPA has established the following primary analytical DQOs for environmental studies: precision, accuracy, representativeness, comparability, and completeness (PARCC).

3.5.1.1 Precision

Precision is defined as the reproducibility or degree of agreement among replicate measurements of the same quantity. Specifically, it is a quantitative measure of the variability of a group of measurements compared to their average value. The closer the numerical values of the measurements are to each other, the more precise the measurement is. Precision was expressed as the percentage of the difference between results of replicate samples for a given compound or element. Relative percent difference (RPD) was calculated using the equation given in Appendix F.

Precision was evaluated based on the analysis of three different types of QC samples: the U.S. Army Environmental Center (USAEC) Class 1 laboratory QC duplicate sample spike recoveries (laboratory control sample [LCS]), MS/MSD samples, and replicate field sample analyses. USAEC Class 1 laboratory QC duplicate sample spike recoveries are required as part of the USAEC analytical program for all methods and provide ongoing information on the performance of each lot for each analytical method in a standard matrix. For each analytical lot, the results of these sample spike recoveries were compiled on single-day and three-day control charts (i.e., X-bar and range) and submitted to the USAEC Chemistry Branch for approval. Upon final approval by the USAEC Chemistry Branch, the data within each lot was revised at Phase 3 in IRDMIS.

Same single-day (high spike concentration) control charts were outside QC criteria for: RDX, 1,3,5-TNB, 2,4,6-TNT, 2,4-dinitrotoluene (2,4-DNT), and NB for lots AIUD and AIWV; and RDX, 1,3,5-TNB, NB, and 2,4,6-TNT for lot AIYH and AJDT. Out-of-control situations in these lots are expected to have a negligible impact on data quality, and are discussed in Appendix F, Section F.

One sample per 20 collected samples was randomly selected to be spiked as an MS/MSD sample. MS/MSD analyses aided in detecting any systematic problems in the analysis and also helped determine how well the target analytes could be recovered from environmental matrices, identifying a matrix effect. Three aliquots were collected for the sample designated to be analyzed for MS/MSD. MS/MSD samples were prepared by routinely analyzing the first aliquot for the parameters of interest, while the remaining two aliquots were spiked with known quantities of the parameters of interest before analysis. The RPD between the two spike results (MS/MSD) was not calculated because background concentration was greater than the spike level.

Sample collection reproducibility and media variability were measured by the analysis of field replicates. Field replicates were collected using the same techniques as those used to collect the environmental samples. One sample in 10 was collected for each similar matrix. Sample collection reproducibility and media variability were evaluated based on the RPD values between the two replicate samples. The RPD between field replicates indicates that environmental conditions at the site are spatially and temporally variable. The data should be utilized with this consideration. No sample was qualified based on the results of these replicate samples since EPA has no guidelines for this QC parameter. However, the amount of heterogeneity of the matrices is shown by the number of times the replicate samples collected and calculated exceeded the selected control limits, based on EPA acceptance criteria. Immediately after purging, all groundwater samples were collected from existing monitoring wells at LAAP using Teflon ® bailers. The samples were shipped to DataChem Laboratories (DCL) for explosives-related compounds analysis. Field replicate RPD values were calculated only for compounds detected in concentrations greater than the certified reporting limits (CRLs) in both replicate pair samples. The explosive water field replicates did not exceed the control limit of 30 percent for RPD acceptance criteria. In general, the RPD between field replicates was low. Based on these RPD results and the acceptable laboratory QC results, the sample collection DQO for reproducibility is considered to have been met. A comprehensive discussion of all replicate sample results is presented in Appendix F, Section F. 2.3.

The overall goal for analytical precision was greater than 95 percent of all data generated by field or laboratory methods within the contract-required or method-recommended (as defined by the appropriate USAEC method or SAIC standard operating procedure [SOP] control limits.

3.5.1.2 Accuracy

Accuracy, or the bias in a measurement system, is a measure of the closeness of a reported concentration to the true value. The closer the numerical value of the measurement approaches the true value or actual concentration, the more accurate the measurement is. Analytical accuracy is expressed as the percent recovery of a compound or element that has been added to the environmental sample at a known concentration before analysis. The percent recovery values were calculated using the equation given in Appendix F.

Analytical accuracy was determined through the use of Class 1 USAEC laboratory QC sample spike recoveries for explosives. The accuracy of the analysis and the matrix effect of the water samples upon the analytical methodology was determined through the use of MS/MSD analyses conducted on the environmental samples as described for precision determinations. The percent recoveries of the target compounds were calculated and used as an indication of the accuracy of the analyses performed.

One field sample was randomly selected to be spiked as an MS/MSD sample. The information gathered was not used to assess the effect of matrix on sample recovery. Recoveries were not calculated because background concentration was greater than the spiking level. The laboratory accuracy for this project was qualitatively assessed by evaluating the following laboratory QC information: method blank, initial calibration verification (ICV), continuing calibration verification (CCV), and USAEC Class 1 laboratory QC sample spike results calculated from all analyses conducted on environmental samples. Each type of spiked sample provided different information on the accuracy of the measurement system.

USAEC QC samples were used as the primary control of accuracy in the laboratory system. The contract laboratory plotted the mean percent recovery and range of percent recovery on control charts prepared for each control compound. The laboratory utilized the percent recovery of each compound in spiked QC samples, the average percent recovery, and the difference between the percent recovery of two high spiked samples in a continuous assessment of method accuracy. Thirty-two percent recovery values (of 135 values) were out-of control. The flag code (i.e., "7") was applied to three RDX and five 2,4,6-TNT concentrations to indicate that the QC samples' low spike recovery was outside of QC criteria. The flag code (i.e., "L") was applied to six NB concentrations to indicate that NB data were rejected due to low recovery for the low spike. Despite these values, no systematic laboratory error was detected, and the results are considered to have little impact on the overall environmental data quality.

In addition, an analysis accuracy was calculated for method UW25 based on found versus recovered compounds. Analysis accuracies are reported with each applicable lot of data to USAEC. Concentrations reported in IRDMIS reflect the accuracy of the analytical method.

The general objective for analytical accuracy was to meet 100 percent of the calibration, internal standard, and surrogate recovery criteria, as defined by the USAEC procedure. The general objective for sample accuracy was that greater than 95 percent of the USAEC QC samples and MS/MSD analyses be within the USAEC required control limits or that matrix interferences could be demonstrated through MS/MSD results. Sampling accuracy was maximized by the adherence to the strict quality assurance (QA) program presented in the Five-Year Review of the Area P Lagoons Quality Assurance Project Plan (QAPP). All field procedures used during the investigation were documented as SOPs. Equipment rinsate blanks were prepared to assess any cross- contamination mat may have occurred.

All supporting explosives QC information (i.e, method blanks, ICVs, and CCVs) was qualitatively evaluated with respect to the analytical accuracy DQO. The method blank results for groundwater were generally below the CRLs with one exception. Lot AIWV had a method blank with the concentration of 1,3,5-TNB above the CRL. As a result, 1,3,5-TNB concentrations in three field samples was flagged (i. e., "B") to indicate that this explosives related compound was found in the associated method blank. Percent recovery results from the ICVs and CCVs were within the limits specified in DCL performance-demonstrated method UW25. The overall laboratory accuracy is acceptable, and as such, the analytical DQO for accuracy was met.

Sampling accuracy was maximized by the adherence to the strict quality assurance (QA) program presented in the Five-Year Review of the Area P Lagoons QAPP. All procedures (i.e., groundwater sample collection, equipment decontamination, and health monitoring equipment calibration and operation) used were documented as standard operating procedures (SOPs). Equipment rinsate blanks were prepared to ensure that all samples represent the particular site from which they were collected, assess any cross-contamination that may have occurred, and flag the associated analytical data accordingly.

The flag code (i.e., "G") was applied to the 1,3,5-TNB and RDX in SAIC01 Site ID G0009, SAIC04 Site ID G0083; SAIC02 and SAIC03 Site ID G0084 to indicate that these compounds were detected in the associated equipment rinsate blank.

Based on an evaluation of the explosives- related compounds detected in the equipment rinsate blanks, the overall field accuracy is acceptable. As a result, the field DQO for accuracy is considered to have been met. A comprehensive discussion of the field QC results is presented in Appendix F, Section F. 2.

3.5.1.3 Representativeness

Representativeness was defined as the degree to which the data accurately and precisely represent a characteristic of a population, parameter variations at a sampling location, a process condition, or an environmental condition. Sample representativeness was ensured by collecting sufficient samples of a population medium, properly distributed with respect to location and time. Representativeness was assessed by reviewing sample collection methods, equipment, and sample containers, in addition to evaluating the RPD values from the field replicate samples and the concentrations of explosivesrelated compounds detected in the equipment rinsate blanks and method blanks. The reproducibility of a representative set of samples reflects the degree of heterogeneity of the sampled medium, as well as the effectiveness of the sample collection techniques.

Based on the evaluation of the factors described above and summarized in Appendix F, Section F. 3, the samples collected are considered to be representative of the environmental conditions at LAAP.

3.5.1.4 Comparability

Comparability is a qualitative parameter expressing the confidence with which one data set can be compared to another, and is limited to the other PARCC parameters, because only when precision and accuracy are known can one data set be compared to another. The characteristic of comparability reflects the consistency of sample collection and handling procedures, analytical techniques, and expression of results in units consistent with other organizations reporting similar data. To optimize comparability, only the specific methods and protocols that were specified in the Five-Year Review of the Area P Lagoons QAPP, as required by the USATHAMA Quality Assurance Program, PAM 11-41 (January 1990), were used to collect and analyze samples. By using consistent sampling and analysis procedures, all data sets were comparable within the sites at LAAP and between sites at the installation to ensure that decisions and priorities were based on a consistent data base. No changes to planned procedures were implemented that would affect data comparability. Comparability also was ensured by the analysis of USAEC reference materials, establishing that the analytical procedures used were generating valid data.

All groundwater samples collected for explosives analyses were analyzed using DCL performance-demonstrated method UW25. Based on the precision and accuracy assessment presented above, the data collected are considered to be comparable with the data collected during previous investigations.

3.5.1.5 Completeness

Completeness was defined as the percentage of valid data obtained from a measurement system. For data to be considered valid, they must have met all acceptance criteria, including accuracy and precision, as well as any other criteria specified by the analytical methods used. Project completeness was calculated using the equation given in Appendix F.

For analytical data to be considered usable, each data point must be

satisfactorily validated. The completeness objective established for this project was 90 percent. Based on the evaluation of the field and laboratory QC results presented in Appendix F, Sections F.2 and F.3, 96.7 percent of the sample data collected for explosives analyses during the Five-Year Review of the Area P Lagoons were used as the basis for all recommendations presented in this report. All explosives analyses for groundwater and field QC samples were performed within the holding times.

Completeness of the data also was evaluated by comparing work plan sampling requirements to the completed chain- of-custody forms to establish that all samples required by the work plan were in fact collected. Upon completion of this process, analytical result in the IRDMIS data base and laboratory data packages were compared to those required by the chainofcustody to establish that the results for all samples taken were in the data base.

3.5.2 Field Infernal Quality Control Checks

Collection and analysis of source water samples, equipment rinsate blanks, and field replicates are provided as QC checks on the integrity of sample collection and handling and equipment decontamination procedures.

The following summarizes the field QC samples that were collected during the Five-Year Review at LAAP:

- Duplicate water samples were collected on October 12 and 13,1993 from Well No. 6 (source water) on Post and the reagent-grade water used as the final rinse in the decontamination procedures and submitted to DataChem Laboratories (DCL) for analysis using DCL performance-demonstrated method UW25 for explosives. These samples were analyzed on October 22 and November 10, 1993. No explosive compounds were detected in the samples.
- One equipment rinsate blank was collected each day groundwater samples were collected by pouring USAEC-approved source or distilled water into, through, and/or over a clean piece of sampling equipment (e.g., bailers), and then dispensing the water into prepared sample bottles. These blanks were analyzed for explosive- related compounds by DCL performance-demonstrated method UW25.
- One field replicate was collected for every 10 groundwater samples collected. Two field replicates were collected during this field investigation. Field replicates were collected at the same time and in the same manner as the other samples. Field replicates are a separate sample, obtained from the same monitoring point. Results of the field replicate analyses are used to assess the precision of the field sampling techniques, not that of the analytical techniques.

Section 4.3 and Appendix F discuss the field QC sample analyses and their impact on the data quality.

3.5.3 Laboratory Quality Control Checks

In accordance with the USATHAMA Quality Assurance Program, PAM 11-41 (January 1990), laboratory QC samples were analyzed with each lot of environmental samples. These QC samples monitor the performance of the analytical method by which a particular lot is being analyzed. The results (recoveries) of these QC samples are plotted on single-day and three-point moving average control charts. Control charts are used to monitor the variations in the precision and accuracy of routine analysis and detect trends in these variations. In addition to USAEC laboratory QC spike samples, MS/MSD samples were collected and analyzed to monitor analytical accuracy and precision.

3.5.3.1 Matrix Spike/Matrix Spike Duplicates

MS/MSDs were collected and analyzed to evaluate the accuracy and precision of the analysis and matrix effect of the sample on the analytical methodology. A pair of MS/MSD samples was analyzed for every 20 samples of similar matrix received at the laboratory. Samples identified as field QC samples (i.e., equipment rinsates and field replicates) were not used for MS/MSD analysis. Control limits of 75 to 125 percent were used for evaluating « MS/MSD recoveries.

3.5.3.2 USAEC Class 1 Method - UW25

Groundwater and field QC samples were analyzed for explosives using DataChem Laboratories (DCL) performance-demonstrated method UW25. The following types of USAEC QC samples were included with each analytical lot:

- At least one standard matrix method blank.
- Three standard matrix spike QC samples—One spike at approximately 2 times and 2 spikes at 10 times the certified reporting limit (CRL). The standard matrix spike QC samples contained all control analytes, as specified in the DCL performance demonstrated method UW25.

USAEC procedures require the use of control charts to monitor performance, accuracy, and precision during an analysis. For each lot, data from the spike QC sample at 2 times the CRL was plotted on the three-point x-bar and range control charts, while the data from the 2 spiked QC samples at 10 times the CRL were plotted on the single day x-bar and range control charts.

As analytical lots are analyzed, the data from the spiked QC samples within a lot are evaluated against the control chart limits to determine if that lot of samples is "in control." Each individual data point was tested as an outlier using Dixon's test at the 98 percent confidence level. Data points that fall outside of these control limits required immediate investigation, explanation, and/or corrective action. All QC data and control charts must be evaluated daily to ensure that an analytical method remains in control. Failure to do so may result in samples being reanalyzed and/ or data being discarded.

3.5.3.3 Control Chart Review

Analysis of the QC results may result in the laboratory or SAIC applying a flagging code to a particular analyte(s) for all samples associated with that analytical lot. These flagging codes are assigned to indicate other-than-usual analytical conditions or results (e.g., high spike not within the control limits, result is unconfirmed). Upon receipt of the laboratory QA report and associated control charts, the USAEC Chemistry Branch reviews all QC data and determines whether or not the lots are in control, if the data are usable without qualifiers, or if the data are usable with a data qualifier applied.

4. CONCLUSIONS AND RECOMMENDATIONS

This section summarizes the principal findings of the Five-Year Review conducted at Area P. Recommendations for corrective actions and future Five-Year Reviews also are discussed.

4.1 EFFECTIVENESS OF INTERIM REMEDIAL ACTION

The groundwater sampling data for the Upper Terrace and Lower Terrace/Sparta Sand aquifers indicate that the concentrations of hexahydro-1, 3,5-trinitro-1, 3,5-triazine (RDX), 1,3,5-trinitrobenzene (1,3,5-TNB), 1,3-dinitrobenzene (1,3-DNB), 2,4,6-trinitrotoluene (2,4,6-TNT), and nitrobenzene (NB) are above the drinking water health advisory levels (HALs). However, these concentrations are lower than the 1990 concentrations, indicating that the groundwater quality at Area P has generally improved since the interim remedial measure was completed. This conclusion was supported by the statistical analysis conducted to evaluate trends in groundwater quality at Area P. Explosive concentrations were generally higher west of Area P for both the Upper Terrace and the Lower Terrace/Sparta Sand aquifers. Similar trends were observed when evaluating the 1990 groundwater sampling data.

The topographic survey of the cap indicates that no major subsidence has occurred at Area P. The surface drainage from the Area P cap is to the west and south, matching prevailing drainage in that area.

4.2 ACTIONS TAKEN OR PROPOSED ON THE BASIS OF THE FIVE-YEAR REVIEW

Damage to a portion of the fence by a fallen pine tree was identified during the Five-Year Review. The fence has since been repaired by Louisiana Army Ammunition Plant (LAAP) personnel. The cap inspection also identified sections of bare ground that were greater than 1 foot in area. It has been recommended that these areas be seeded and mulched to prevent erosion. According to the Maintenance Plan, such seeded areas should be checked monthly to ensure an erosion resistant grass cover has been established before returning to the quarterly inspection schedule.

Three ponded areas were identified during the Five-Year Review of Area P. Water tends to pond in these areas after periods of heavy precipitation. A ponded area was identified on the Area P cap near wells G0068, G0109, and G0110. This area, which is along the drainage pathway from the Area P cap, should be filled with soil and graded to blend smoothly with the surrounding area. The area should be seeded and mulched to prevent erosion. The ponding of the water observed in the southwest comer of the Area P cap after periods of heavy precipitation is a result of the surface drainage pattern from the cap. The ponded area south of well G0012 is outside the cap area. No maintenance is recommended for these two areas.

Wells G0010 and G0011, located south and west of Area P, respectively, and screened in the Upper Terrace aquifer, have a bent well casing. These wells cannot be sampled, and therefore, should be abandoned. Well G0011 installed in 1979 is one of the few wells at Area P that has good historical sample data. No well in the immediate vicinity can be used as a replacement for well G0011. Sample data from the new replacement well, if installed, can be used with the historical data from well G0011 to evaluate the groundwater contamination levels west of Area P. Therefore, it is recommended that a new well be installed to replace well G0011. Well G0014 can be substituted for well G0010 for the future Five-Year Review at Area P. Some of the wells at Area P were installed between 1979 and 1982. The integrity of these wells should be checked to evaluate their potential impact on sampling data.

4.3 SCOPE AND NATURE OF FUTURE REVIEWS

The present scope of field investigation activities should be continued during the next Five-Year Review of Area P scheduled for February 1999. In addition, the effectiveness of the cap should be measured using standard field techniques for measurement of infiltration rate (e.g., use of Double-Ring Infiltrometer, American Society for Testing and Materials [ASTM] Method D 5093- 90). This test method is particularly useful for measuring liquid flow through soil moisture barriers, such as compacted clay cap.

This method produces a direct measurement of infiltration rate, not hydraulic conductivity. Although the units of infiltration rate and hydraulic conductivity are similar, there is a distinct difference between these two quantities. They cannot be directly related unless the hydraulic boundary conditions, such as hydraulic gradient and the extent of lateral flow of water, are known or can be reliably estimated.

The infiltration rate of water through soil is measured using a double-ring infiltrometer. The infiltrometer consists of an open outer and a sealed inner ring. The rings are embedded and sealed on the cap. Both rings are filled with water such that the inner ring is submerged. The rate of flow is measured by connecting a flexible bag filled with a known weight of water to a port on the inner ring. As water infiltrates into the ground from the inner ring, an equal amount of water flows into the inner ring from the flexible bag. After a known interval of time, the flexible bag is removed and weighed. The weight loss, converted to a volume, is equal to the amount of water that has infiltrated into the ground. An infiltration rate is then determined from this volume of water, the area of the inner ring, and the interval of time. This process is repeated and a plot of infiltration rate versus time is constructed (ASTM 1994).

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APPENDIX A IRDMB DATA

Data Summary Table: Groundwater - Area P Lagoons, Groundwater and Associated Replicate Sample Results, Louisiana Army Ammunition Plant

Site ID Field Sample Number Site Type Collection Date Depth (ft) Associated Field QC Sample - Site ID Associated Field QC Sample - Field S							G0009 SAICRB02 RNSW 2/25/94 0 N/A N/A		S	G0012 SAIC01 WELL 2/24/94 19.76 G0012 AICRB01		S/	G0012 AICRB01 RNSW 2/24/94 0 N/A N/A		S	G0014 SAICO1 WELL 2/24/94 14.86 G0012 AICRB01	
Explosives (UW25) Laboratory ID Number Parameter	Units	CRL		UB01176 FC	DQ		UB01175 FC	DQ		UB01144 FC	DQ		UB01143 FC			UB01145 FC	DQ
1,3,5-Trinitrobenzene 1,3-Dinitrobenzene	µg/L	0.21 0.458	LT	29 UGB 0.458	1	LT	0.42 CB 0.458	1		950 C 35 C		LT LT	0.21		LT	0.429 K 0.458	
2,4,6-Trinitrotoluene	µg/L µg/L	0.438	51	28.3 C7	JN	LT	0.426 7	JN		3700 C		LT	0.436		LT	0.438	
2,4-Dinitrotoluene	µg/L	0.397		37 UQ	Ν	LT	0.397	N		120 C		LT	0.397		LT	0.397	
2,6-Dinitrotoluene Cyclotetramethylenetetranitramine	µg/L	0.6 0.533	LT	0.6 26 C			0.6 0.533		LT	32.3 K 110 C		LT LT	0.6 0.533		LT	0.6 2.92 C	
Nitrobenzene	μg/L μα/L	0.682	LT	0.682		LI	2.66 U		LT	12.3 K		LT	0.535 1.84 K		LT	2.92 C 0.682	
Hexahydro-1,3,5-trinitro-1,3,5-triazine		0.416		430 CG			0.746 U		LŤ	3100 K7	J	LT	0.416 K7	J		14.4 C7	J
N-methyl-N,2,4,6,-tetranitroanalline	µg/L	0.631	LT	0.631		LT	0.631		LT	6.3 JI		LT	0.631		LT	0.631	

Data Summary Table: Groundwater - Area P Lagoons, Groundwater and Associated Replicate Sample Results, Louisiana Army Ammunition Plant (Continued)

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Site ID	G0068	G0083	G0084	G0084	G0085
Field Sample Number	SAIC01	SAIC04	SAIC02	SAIC03	SAIC01
Site Type	WELL	WELL	WELL	WELL	WELL
Collection Date	3/1/94	2/25/94	2/25/94	2/25/94	3/3/94
Depth (ft)	16	19.8	21.6	21.6	20
Associated Field QC Sample - Site ID	GO-146	G0009	G0009	G0009	GO-150
Associated Field QC Sample - Field Sample No.	SAICRB04	SAICRB02	SAICRB02	SAICRB02	SAICRB06

Explosives (UW25)

Laboratory ID Number				UB01226		U	B01179			UB01177			JB01178		UB01270	
Parameter	Units	CRL		FC	DQ		FC	DQ	-	FC	DQ		FC DQ		FC	DQ
1,3,5-Trinitrobenzene	hð\r	0.21		490 C			800 UGB	1		320 UGB	1		310 DUG 1		3800 C	
1,3-Dinitrobenzene	µg/L	0.458		82 C			5.63 C		LT	0.458		LT	0.458 D		32 C	
2,4,6-Trinitrotoluene	µg/L	0.426		3600 C	J		3100 C7	JN		250 C7	JN		240 DC7 JN		4200 C	
2,4-Dinitrotoluene	µg/L	0.397		350 UQ	j		95 UQ	N		12.1 UQ	N		11.2 DUQ N		79 C	J
2,6-Dinitrotoluene	µg/L	0.6	LT	60 JI		LT	12		LT	0.6		LT	12 D	LT	59 K	
Cyclotetramethylenetetranitramine	µg/L	0.533	LT	350 K			99 C			13.3 U			14 DUQ	LT	310 K	
Nitrobenzene	µg/L	0.682	LT	68 LJI	J	LT	14 JI		LT	0.682		LT	0,682 D	LT	67 K	
Hexahydro-1,3,5-trinitro-1,3,5-triazine		0.416		2500 C			1200 CG			110 CG			120 DCG		3800 C	
N-methyl-N,2,4,6,-tetranitroanailine	µg/L	0.631		31 U			95 U			5.66 U			5.03 DU		310 C	

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Data Summary Table: Groundwater - Area P Lagoons, Groundwater and Associated Replicate Sample Results, Louisiana Army Ammunition Plant (Continued)

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Site ID Field Sample Number Site Type Collection Date Depth (ft) Associated Field QC Sample - Site II Associated Field QC Sample - Field 5		No.		G0104 SAIC01 WELL 3/2/94 18 GO-145 SAICRB05			G0104 SAIC01 WELL 3/2/94 18 GO-145 SAICRB05			G0105 SAIC01 WELL 2/28/94 25 G0110 SAICRB03		SA	G0106 SAIC01 WELL 3/1/94 57 GO-146 AICRB04		S	G0109 SAIC01 WELL 2/28/94 23 G0110 AICRB03	
Explosives (UW25) Laboratory ID Number Parameter	Units	CRL		UB01242 FC	DQ		UB01243 FC		<u></u>	UB01192 FC	DQ	ι	JB01225 FC	DQ		UB01193 FC	DQ
1,3,5-Trinitrobenzene 1,3-Dinitrobenzene 2,4,6-Trinitrotoluene 2,4-Dinitrotoluene 2,6-Dinitrotoluene Cyclotetramethylenetetranitramine Nitrobenzene Hexahydro-1,3,5-trinitro-1,3,5-triazine N-methyl-N,2,4,6,-tetranitroanailine	μg/L μg/L μg/L μg/L μg/L μg/L	0.21 0.458 0.426 0.397 0.6 0.533	LT LT LT	6000 C 560 C 11000 C 550 C 60 JI 370 K 68 LJI 7100 C 120 C	ـــــــــــــــــــــــــــــــــــــ	LT LT LT	6300 DC 580 DC 11000 DC 570 DC 60 DJI 310 DK 68 DLJI 8400 DC 130 DC	J J	LT LT	3900 C 320 UQ 16.5 C 54 C 60 JI 360 C 68 JI 330 C 3.71 U		LT LT LT LT	970 C 330 C 8800 C 640 C 60 JI 53 JI 68 LJI 4100 C 63 JI	ـــــــــــــــــــــــــــــــــــــ	LT LT	95 C 8.21 UQ 3600 C 330 C 60 JI 300 C 6.8 JI 3100 C 39.9 U	

Data Summary Table: Groundwater - Area P Lagoons, Groundwater and Associated Replicate Sample Results, Louisiana Army Ammunition Plant (Continued)

Site ID	G0110	G0110	GO-145	GO-146	GO-150
Field Sample Number	SAIC01	SAICRB03	SAICRB05	SAICRB04	SAICRB06
Site Type	WELL	RNSW	RNSW	RNSW	RNSW
Collection Date	2/28/94	2/28/94	3/2/94	3/1/94	3/3/94
Depth (ft)	32	0	0	0	0
Associated Field QC Sample - Site ID	G0110	N/A	N/A	N/A	N/A
Associated Field QC Sample - Field Sample No.	SAICRB03	N/A	N/A	N/A	N/A

Explosives (UW25)

Laboratory ID Number			U	B01191			UB01190			JB01240			UB01223		1	JB01267	
Parameter	Units	CRL		FC	DQ		FC	DQ		FC	DQ		FC	DQ		FC	DQ
1,3,5-Trinitrobenzene	µg/L	0.21		460 C		LT	0.21										
1,3-Dinitrobenzene	µg/L	0.458		24 UQ		LT	0.458										
2,4,6-Trinitrotoluene	µg/L	0.426		570 C		LT	0.426		LT	0.426	J	LT	0,426	J	LT	0.426	
2,4-Dinitrotoluene	µg/L	0.397		120 C		LT	0.397		LT	0.397	J	LT	0.397	J	LT	0.397	J
2,6-Dinitrotojuene	µg/L	0.6	LT	60 JI		LT	0.6										
Cyclotetramethylenetetranitramine	µg/L	0.533		130 C		LT	0.533		LT	0.533			5.03 C		LT	0.533	
Nitrobenzene	µg/L	0.682	LT	6.8 JI			2.95 UQ		LT	0.682 L	ال	LT	0.682 L	J	LT	0.682	
Hexahydro-1,3,5-trinitro-1,3,5-triazine		0.416		2800 C		LT	0.416										
N-methyl-N,2,4,6,-tetranitroanailine	µg/L	0.631	LT	0.631		LT	0.631		LT	0.631		LT	0.631		LŤ	0.631	

N/A - Not applicable

ID - Identification

QC - Quality Control

CRL - Certified reporting limit

LT - Less than

FC - Flagging codes:

B - Analyte found in the method blank or QC blank as well as the sample

C - Analysis confirmed

D - Duplicate analysis

G - Analyte found in rinse blank as well as field sample.

1 - Interferences in sample caused the quantitation and /or identification to be suspect

J - Value is estimated

K - Reported results affected by interferences or high background

L - Out of control, data rejected due to low recoveries.

Q - Sample Interference obscured peak of interest

U - Analysis is unconfirmed

7 - Low spike recovery is not within control limits

DQ - Data qualifiers:

I - The low-spike recovery is high.

J - The low-spike recovery is low.

N - The high-spike recovery is low.

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Final Documentation Appendix Report Installation :Louisiana AAP, LA (LO) File Type: CGW Sampling Date Range: 01-SEP-93 27-JUN-94

TAPH #6 SAICO1 0.0 12-0CT-93 US UAX3229 UM25/W 06-20-2 2.6-0Thirditume 1.1 6.1 1.6 ULL 10-96-77 Trinitrolume LT .625 ULL .1 .6 ULL ULL ULL ULL ULL .1 .6 ULL ULL .1 .625 ULL .1 .626 ULL .1 .620 ULL .1 .620 ULL .1 .620 .1 .1 .620 .1 .1 .1 .1 .1 .1 .1 .1 .1	Site Type	Site ID	Field Sample No.	Depth	Sample Date	Lab	Lab Anly. No.	Meth/ Matrix	CAS No.	Analyte Description	Meas. Bool.	. Conc.	Unit Meas.	Flag Codes	Data Quals
MELL 20009 SAICO1 18.2 25-FEB-94 UB UB01176 UM2574				0.0		UB	UA03229	UW25/W	06-20-2	2.6-Dinitrotoluene					
Vell 21-82-4 10% / Cyclonite / Hordhydro-13,5- it it 446 Uii it 10% / Cyclonite / Hordhydro-13,5- it 1 .416 Uii it 11 .5 11 .416 Uii it 11 .5 11 .416 Uii SAIC02 0.0 12-001-93 Uii UA03228 UV25/N 0-010 - mirbane 1 .531 Uii 99-35-4 11,35-111011006/marene / Essence of mirbane LT .683 Uii 0 99-35-4 11,35-111011006/marene / Essence filterono iii 11 .66 Uii 0 99-35-4 11,35-111011006/marene / Essence filterono iii 11 .66 Uii 0 21-82-4 10 0-02-2 .2,4-50111000100e / alpha- 11 .66 Uii 0 21-82-4 10 0-02-2 .2,4-50111000100e / alpha- 11 .63 Uii 0 21-82-4 10 0-02-2 .2,4-50111000100e / alpha- 11 .63 U										2,4,6-Trinitrotoluene / alpha-		.426			
VELL 60009 SAICO1 18.2 25-FEB-94 UB UB01176 UV25/V 13.5-Trinitrobenzene LT .631 UGL VELL 60009 SAICO1 18.2 25-FEB-94 UB UB01176 UV25/V 13.5-Trinitrobenzene LT .631 UGL VELL 60009 SAICO1 18.2 25-FEB-94 UB UB01176 UV25/V 16.6-7 .											LT		UGL		
VELL GOOD SAICO2 0.0 12-0CT-93 UB UA03228 UU25/W Good										trinitro-1.3.5-triazine *			UGL		
SAIC02 0.0 12-0CT-93 UB UA03228 UW25/H 06-95-3 Microbenzene / Essence of mirbane / LT .682 UGL 99-35-4 1,3,5-Trinitrobuzene LT .21 UGL H 99-35-4 1,3,5-Trinitrobuzene LT .21 UGL H 10-5 06-20-7 2,4,6-Trinitrobuzene LT .458 UGL D 11-1 .426 UGL D									79-45-8	Tetryl / N-Methyl-N,2,4,6-	LT		UGL		
SAICO2 0.0 12-0CT-93 UB UA0322B UW25/W 06-20-2 2,6-Dinitrotoburge LT .45B UGL D 99-35-4 1,3-5Trinitroberzene LT .45B UGL D 99-35-4 1,3-5Trinitroberzene LT .45B UGL D 99-35-4 1,3-5Trinitrobluene LT .426 UGL D 18-96-7 2,4,6-Trinitrotoluene LT .426 UGL D 21-14-2 2,4-Dinitrotoluene LT .426 UGL D 21-14-2 2,4-Dinitrotoluene LT .416 UGL D 21-14-2 2,4-Dinitrotoluene LT .4651 UGL D 79-45-8 Tetryl / M-Kethyl-H,2,4,6- LT .416 UGL D 90-35-4 1.0 of mirbane LT .651 UGL D 90-35-4 1.0 of mirbane LT .651 UGL D WELL 60009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,6-Dinitrotoluene <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>LT</td><td></td><td></td><td></td><td></td></td<>											LT				
SAIC02 0.0 12-0CT-93 UB UA03228 UW25/W 06-20-2 2.4-0-initrotoluene LT .626 UGL D 18-90-7 2.4-0-initrotoluene LT .626 UGL D 21-14-2 2.4-0-initrotoluene LT .626 UGL D 21-14-2 2.4-0-initrotoluene LT .397 UGL D 21-14-2 2.4-0-initrotoluene LT .397 UGL D 21-14-2 2.4-0-initrotoluene LT .631 UGL D 40 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>Oil of mirbane</td><td></td><td></td><td></td><td></td><td></td></t<>										Oil of mirbane					
SAICO2 0.0 12-OCT-93 UB UA03228 UW25/W 06-20-2 2.6-01111rotoluene LT .426 UGL D 18-96-7 Z4,6-5711nitrotoluene LT .426 UGL D 21-14-2 Z,4-0111rotoluene LT .426 UGL D 21-14-2 Z,4-0111rotoluene LT .466 UGL D 79-45-8 Terryl / N=Methyl-N, Z,4,6-7 LT .631 UGL D 79-45-8 Terryl / N=Methyl-N, Z,4,6-7 LT .631 UGL D 91-41-0 Cycloterterantframet/signeterterantframine LT .533 UGL D 92-55-0 1,3-51rinitrobenzene LT .682 UGL D 99-55-0 1,3-51rinitrobenzene LT .682 UGL D WELL 60009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,6-51rinitrobenzene LT .682 UGL D WELL 60009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W														H	I
WELL 60009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 24,6-Trinitrobluene LT .426 UGL D WELL 60009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,4,6-Trinitrobluene LT .426 UGL D WELL 60009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,4,6-Trinitrobarzene / Escence of mirbane / LT .631 UGL D 0610 mirinitrobarzene / Escence of mirbane LT .458 UGL D 99-35-4 13.5-Trinitrobarzene / Escence of mirbane LT .458 UGL D 99-35-4 13.5-Trinitrobarzene LT .458 UGL D 99-35-4 13.5-Trinitrobarzene LT .458 UGL D 18-96-7 2,4,6-Trinitrobarzene LT .458 UGL D 18-96-7 2,4,6-Trinitrobarzene / Escence of mirbane LT .631 UGL C 19-14-0 Cyclottramethylenetetranitramine / * .77 UGL															
WELL 60012 SAICO1 18.2 25-FEB-94 UB UB01176 UW25/V 06-20-2 2,6-Dinitrotoluene LT .533 UGL D WELL 60012 SAICO1 18.2 25-FEB-94 UB UB01176 UW25/V 06-20-2 2,6-Dinitrotoluene LT .631 UGL D 0012 SAICO1 18.2 25-FEB-94 UB UB01176 UW25/V 06-20-2 2,6-Dinitrotoluene LT .632 UGL D 0010 of mirbane LT .632 UGL D			SA1CO2	0.0	12-0CT-93	UB	UA03228	UW25/W				.6			
VELL 80009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,6-Dinitrotoluene LT .631 UGL D WELL 80009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,6-Dinitrotoluene LT .631 UGL D Vell 60012 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,6-Dinitrotoluene LT .631 UGL D Vell 60009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,6-Dinitrotoluene LT .640 UGL D Vell 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,6-Dinitrotoluene LT .631 UGL D Vell 18.96-7 2,4-0-11itrotoluene 37 UGL D C7 18-96-7 2,4-0-11itrotoluene 37 UGL C C C C 19-65 Nitrobenzene 15-5-triaizine* - . C C										Trinitrotoluene				-	
WELL G0009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,4-0-11itroblance IT .631 UGL D WELL G0009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,4-0-11itroblance IT .631 UGL D WELL G0009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,4-0-11itroblance IT .458 UGL D WELL G0009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,4-0-11itroblance IT .458 UGL D WELL G0009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,4-0-11itroblance IT .458 UGL D 18-96-7 2,4-0-11itroblance JS-triain* 37 UGL UGL C 21-14-2 2,4-0-11itroblance JS-triain* 37 UGL C C 97-35-3 Vitrobenzene JS-triain* 1 .682 UGL C <td></td> <td>-</td> <td></td>														-	
WELL 00009 SAICO1 18.2 25-FEB-94 UB UB01176 UW25/W 0 99-35-4 (7, 5)-Trinitrobenzene LT .632 UGL D WELL 00009 SAICO1 18.2 25-FEB-94 UB UB01176 UW25/W 0 99-35-4 (7, 5)-Trinitrobenzene LT .642 UGL D WELL 00009 SAICO1 18.2 25-FEB-94 UB UB01176 UW25/W 0 6-20-2 2,6-Dinitroboluene LT .640 UGL D WELL 00009 SAICO1 18.2 25-FEB-94 UB UB01176 UW25/W 0 6-20-2 2,6-Dinitrobluene LT .630 UGL D 18-96-7 2,4,6-Trinitrobluene 37 UGL UGL C Trinitrobluene 37 UGL UGL C 21-14-2 2,4-FEB-94 UB UB01144 UW25/W 1,3,5-Trinitrobenzene LT .631 UGL C 90-35-4 1,3,5-Trinitrobenzene Essence of m										trinitro-1,3,5-triazine *			UGL	D	
P 98-95-3 Nitrobenzene / Essence of mirbane / LT .682 UGL D Oil of mirbane 99-35-4 1,3,5-Trinitrobenzene LT .21 UGL DH WELL G0009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/M 06-22 2,6-Dinitrobenzene LT .458 UGL D WELL G0009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/M 06-22 2,6-Dinitrobluene LT .458 UGL D WELL G0009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/M 06-22 2,6-Dinitrobluene LT .458 UGL D 18-96-7 2,4,6-Trinitrotoluene LT .430 UGL C7 18-96-7 2,4-0 initrotoluene 37 UGL UQ 21-14-2 2,4-0 initrotoluene 37 UGL C 21-14-2 2,4-0 initrotoluene LT .631 UGL C 99-35-4 1,3,5-Trinitrobenzene / Essence of mirbane / LT .682 UGL C 99-35-4 1										tetranitroaniline / Nitramine / *			UGL	D	
WELL 60009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/M 062-2 2,6-Dinitrobenzene LT .21 UGL DH WELL 60009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/M 062-2 2,6-Dinitrobenzene LT .458 UGL D WELL 60009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/M 062-2 2,6-Dinitroblene LT .458 UGL D WELL 60009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/M 062-2 2,6-Dinitroblene LT .458 UGL D 18-96-7 2,4,6-Trinitrotoluene 17.5-triazine * 										Cyclotetramethylenetetranitramine		.533			
WELL 00009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 (06-20-2) 2,6-Dinitrotoluene 2,6-Dinitrotoluene / alpha- Trinitrotoluene LT .458 UGL D WELL 00009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,6-Dinitrotoluene / alpha- Trinitrotoluene .6 UGL C7 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,6-Dinitrotoluene / alpha- Trinitrotoluene .37 UGL UQ 21-14-2 2,4-Dinitrotoluene .37 UGL C 21-82-4 RDX / Cyclonit / Hexahydro-1,3,5- .430 UGL C 21-82-4 RDX / Cyclonit / Hexahydro-1,3,5- .430 UGL C 79-45-8 Tetryl / N-Methyl-N,2,4,6- LT .631 UGL C 91-41-0 Cyclotetramethylenetetranitramine / * .6622 UGL C 98-95-3 Nitrobenzene / Essence of mirbane / LT .682 UGL UGL 60012 SAIC01 19.8 24-FEB-94 UB UB01144 UW25/W 06-20-2		Ą								Nitrobenzene / Essence of mirbane /			UGL	-	
WELL 60009 SAIC01 18.2 25-FEB-94 UB UB01176 UW25/W 06-20-2 2,6-Dinitrotoluene LT .6 UGL 18-96-7 2,4,6-Trinitrotoluene/alpha- Trinitrotoluene 28.3 UGL C7 21-14-2 2,4-0initrotoluene 37 UGL UQ 21-82-4 RDX / Cyclonite / Hexahydro-1,3,5- 430 UGL C 79-45-8 Tetryl / N-Methyl-N,2,4,6- LT .631 UGL C 91-41-0 Cyclotetramethylenetetranitramine 26 UGL C 98-95-3 Nitrobenzene / Essence of mirbane / LT .682 UGL 0012 SAIC01 19.8 24-FEB-94 UB UB01144 UW25/W 06-20-2 2,6-Dinitrotoluene LT .458 UGL 60012 SAIC01 19.8 24-FEB-94 UB UB01144 UW25/W 06-20-2 2,6-Dinitrotoluene LT .32.3 UGL K 18-96-7 2,4,6-Trinitrotoluene LT .458 UGL C C 18-96-7 2,4,6-Trinitrotoluene LT .32.3		ίn.												DH	I
18-96-7 2,4,6-Trinitrotoluene 28.3 UGL C7 Trinitrotoluene 37 UGL UQ 21-14-2 2,4-Dinitrotoluene 37 UGL C 21-82-4 RDX / Cyclonite / Hexahydro-1,3,5- 430 UGL C rinitro-1,3,5-triazine * 79-45-8 Tetryl / N-Methyl-N,2,4,6- LT .631 UGL C 18-96-7 Cyclotetramethylenetetranitramine / * 91-41-0 Cyclotetramethylenetetranitramine 26 UGL C 98-95-3 Nitrobenzene / Essence of mirbane / LT .682 UGL 011 of mirbane 60012 SAIC01 19.8 24-FEB-94 UB UB01144 UW25/W 06-20-2 2,6-Dinitrotoluene LT .458 UGL G0012 SAIC01 19.8 24-FEB-94 UB UB01144 UW25/W 06-20-2 2,6-Dinitrotoluene LT 18-96-7<												.458		D	
G0012 SAICO1 19.8 24-FEB-94 UB UB UB01144 UW25/W 06-20-2 2,6-Dinitrotoluene 12,3-triazine * 13,5-triazine * 14,3,5-triazine * 14,3,5-triazine * 14,3,5-triazine * 14,3,5-triazine * 14,3,5-triazine * 14,1-0	WELL	60009	SAIC01	18.2	25-FEB-94	UB	UB01176	UW25/W			LT				
21-82-4 RDX / Cyclonite / Hexahydro-1,3,5- 430 UGL C trinitro-1,3,5-triazine * 79-45-8 Tetryl / N-Methyl-N,2,4,6- LT .631 UGL 79-45-8 Tetryl / N-Methyl-N,2,4,6- LT .631 UGL C 1000000000000000000000000000000000000										Trinitrotoluene			UGL	C7	JN
trinitro-1,3,5-triazine *79-45-8Tetryl / N-Methyl-N,2,4,6-LT.631UGLtetranitroaniline / Nitramine / *91-41-0Cyclotetramethylenetetranitramine26UGL98-95-3Nitrobenzene / Essence of mirbane / LT.682UGL0il of mirbane99-35-41,3,5-Trinitrobenzene29UGL99-65-01,3-DinitrobenzeneLT.458UGL99-65-01,3-DinitrobenzeneLT.458UGL18-96-72,4,6-TrinitrotolueneAT3700UGL21-14-22,4-Dinitrotoluene120UGLC														UQ	N
tetranitroaniline / Nitramine / * 91-41-0 Cyclotetramethylenetetranitramine 26 UGL C 98-95-3 Nitrobenzene / Essence of mirbane / LT .682 UGL 0il of mirbane 99-35-4 1,3,5-Trinitrobenzene 29 UGL U 99-65-0 1,3-Dinitrobenzene LT .458 UGL 99-65-0 1,3-Dinitrobenzene LT .458 UGL 18-96-7 2,4,6-Trinitrotoluene / alpha										trinitro-1,3,5-triazine *			•	C	
98-95-3 Nitrobenzene / Essence of mirbane / LT .682 UGL Oil of mirbane 99-35-4 1,3,5-Trinitrobenzene 29 UGL U 99-65-0 1,3-Dinitrobenzene LT .458 UGL G0012 SAIC01 19.8 24-FEB-94 UB UB01144 UW25/W 06-20-2 2,6-Dinitrotoluene LT 32.3 UGL K 18-96-7 2,4,6-Trinitrotoluene / alpha- 3700 UGL C Trinitrotoluene 21-14-2 2,4-Dinitrotoluene 120 UGL C										tetranitroaniline / Nitramine / *	LT				
Oil of mirbane Oil of mirbane 99-35-4 1,3,5-Trinitrobenzene 29 UGL U 99-35-4 1,3,5-Trinitrobenzene LT .458 UGL 90012 SAIC01 19.8 24-FEB-94 UB UB01144 UW25/W 06-20-2 2,6-Dinitrotoluene LT 32.3 UGL K 18-96-7 2,4,6-Trinitrotoluene / alpha- 3700 UGL C Trinitrotoluene 21-14-2 2,4-Dinitrotoluene 120 UGL C														C	
99-65-0 1,3-Dinitrobenzene LT .458 UGL GOO12 SAICO1 19.8 24-FEB-94 UB UBO1144 UW25/W 06-20-2 2,6-Dinitrotoluene LT 32.3 UGL K 18-96-7 2,4,6-Trinitrotoluene / alpha- 3700 UGL C Trinitrotoluene 120 UGL C 21-14-2 2,4-Dinitrotoluene 120 UGL C											LT				
G0012 SAICO1 19.8 24-FEB-94 UB UB01144 UW25/W 06-20-2 2,6-Dinitrotoluene LT 32.3 UGL K 18-96-7 2,4,6-Trinitrotoluene / alpha- 3700 UGL C Trinitrotoluene 21-14-2 2,4-Dinitrotoluene 120 UGL C														U	I
18-96-7 2,4,6-Trinitrotoluene / alpha- 3700 UGL C Trinitrotoluene 21-14-2 2,4-Dinitrotoluene 120 UGL C									99-65-0						
18-96-7 2,4,6-Trinitrotoluene / alpha- 3700 UGL C Trinitrotoluene 21-14-2 2,4-Dinitrotoluene 120 UGL C		G0012	SAIC01	19.8	24-FEB-94	UB	UB01144	UW25/W	06-20-2	2,6-Dinitrotoluene	LT		UGL	K	
21-14-2 2,4-Dinitrotoluene 120 UGL C										2,4,6-Trinitrotoluene / alpha-			UGL		
												120	UGL	С	

* - Analyte Description has been truncated. See Data Dictionary

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Final Documentation Appendix Report Installation :Louisiana AAP, LA (LO) File Type: CGW Sampling Date Range: 01-SEP-93 27-JUN-9

27-JUN-94

Site Type	Site ID	Field Sample No.	Depth	Sample Date	Lab	Lab Anly. No.	Meth/ Matrix	CAS No.	Analyte Description	Meas. Bool.	Conc.	Unit Meas.	Flag Codes	Data Quals
WELL	G0012	SAIC01	19.8	24-FEB-94	UB	UB01144	UW25/W	21-82-4	RDX / Cyclonite / Hexahydro-1,3,5- trinitro-1,3,5-triazine *	LT	3100	UGL	K7	L
								79-45-8	Tetryl / N-Methyl-N,2,4,6- tetranitroaniline / Nitramine / *	LT	6.3	UGL	JI	
								91-41-0	Cyclotetramethylenetetranitramine		110	UGL	C	
								98-95-3	Nitrobenzene / Essence of mirbane / Oil of mirbane	LT	12.3	UGL	ĸ	
								99-35-4	1,3,5-Trinítrobenzene		950	UGL	С	
								99-65-0	1.3-Dinitrobenzene		35	UGL	С	
	G0014	SAIC01	14.9	24-FEB-94	UB	UB01145	UW25/W	06-20-2	2.6-Dinitrotoluene	LT	.6	UGL	-	
					•••		0	18-96-7	2,4,6-Trinitrotoluene / alpha-	LŤ	.426	UGL		
								21-14-2	Trinitrotoluene 2.4-Dinitrotoluene	LT	.397	UGL		
								21-82-4		L)			C7	
									RDX / Cyclonite / Hexahydro-1,3,5- trinitro-1,3,5-triazine *		14.4	UGL	U7	J
								79-45-8	Tetryl / N-Methyl-N,2,4,6- tetranitroaniline / Nitramine / *	LT	.631	UGL		
								91-41-0	Cyclotetramethylenetetranitramine		2.92	UGL	С	
								98-95-3	Nitrobenzene / Essence of mirbane / Oil of mirbane	LT	.682	UGL		
								99-35-4	1,3,5-Trinitrobenzene	LT	.429	UGL	К	
								99-65-0	1.3-Dinitrobenzene	īτ	.458	UGL		
	G0068	SAIC01	16-0	01-MAR-94	UB	UB01226	UW25/W	06-20-2	2.6-Dinitrotoluene	ΐτ	60	UGL] IL	
A-6	20000	ONTOOT	1010		00	0001220	UNES/ W	18-96-7	2,4,6-Trinitrotoluene / alpha- Trinitrotoluene		3600	UGL	C	J
•••								21-14-2	2,4-Dinitrotoluene		350	UGL	UQ	J
								21-82-4	RDX / Cyclonite / Hexahydro-1,3,5-		2500	UGL	C	J
								79-45-8	trinitro-1,3,5-triazine * Tetryl / N-Methyl-N,2,4,6-		31	UGL	ບ	
								91-41-0	tetranitroaniline / Nitramine / *		750	1101	v	
									Cyclotetramethylenetetranitramine	LT	350	UGL	K 7ji	
								98-95-3	Nitrobenzene / Essence of mirbane / Oil of mirbane	LT	68	UGL		J
								99-35-4	1,3,5-Trinitrobenzene		490	UGL	C	
								99-65- 0	1,3-Dinitrobenzene		82	UGL	C	
	G00 83	SAICO4	19.8	25-FEB-94	UB	UB01179	UW25/W	06-20-2	2,6-Dinitrotoluene	LT	12	UGL		
								18-96-7	2,4,6-Trinitrotoluene / alpha- Trinitrotoluene		3100	UGL	C7	JN
								21-14-2	2,4-Dinitrotoluene		95	UGL	UQ	N
								21-82-4	RDX / Cyclonite / Hexahydro-1,3,5~ trinitro-1,3,5-triazine *		1200	UGL	C	
								79-45-8	Tetryl / N-Methyl-N,2,4,6- tetranitroaniline / Nitramine / *		95	UGL	U	
								91-41-0	Cyclotetramethylenetetranitramine		99	UGL	С	
								71 TI V					v	

* - Analyte Description has been truncated. See Data Dictionary

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Final Documentation Appendix Report Installation :Louisiana AAP, LA (LO) File Type: CGW Sampling Date Range: 01-SEP-93 27-JUN-9 27-JUN-94

Site Type	Site ID	Field Sample No.	Depth	Sample Date	Lab	Lab Anly. No.		CAS No.	Analyte Description	Meas. Bool.	Conc.	Unit Meas.	Flag Codes	0ata Auals
WELL	G0083	SAIC04	19.8	25-FEB-94	UB	UB01179	UW25/W	98-95-3	Nitrobenzene / Essence of mirbane /	LT	14	UGL	JI	** = = =
								99-35-4	Oil of mirbane 1,3,5-Trinitrobenzene		800	1101		•
•								99-65-0	1,3-Dinitrobenzene		5.63	UGL UGL	U C	I
	60084	SAIC02	21.6	25-FEB-94	UB	UB01177	UW25/W	06-20-2	2,6-Dinitrotoluene	LT			6	
	60004	SAILOZ	21.0	23"FED-74	υp	OBUITT	UW237W	18-96-7		LI	.6 250	UGL	07	
									2,4,6-Trinitrotoluene / alpha- Trinitrotoluene			UGL	C7	JN
								21-14-2	2,4-Dinitrotoluene		12.1	UGL	UQ	N
								21-82-4	RDX / Cyclonite / Hexahydro-1,3,5- trinitro-1,3,5-triazine *		110	UGL	C	
								79-45-8	Tetryl / N-Methyl-N,2,4,6-		5.66	UGL	U	
									tetranitroaniline / Nitramine / *					
								91-41-0	Cyclotetramethylenetetranitramine		13.3	UGL	U	
								98-95-3	Nitrobenzene / Essence of mirbane / Oil of mirbane	LT	.682	UGL		
								99-35-4	1,3,5-Trinitrobenzene		320	UGL	U	I
								99-65-0	1.3-Dinitrobenzene	LT	.458	UGL	-	-
		SAIC03	21.6	25-FEB-94	UB	UB01178	UW25/W	06-20-2	2,6-Dinitrotoluene	LT	12	UGL	D	
								18-96-7	2,4,6-Trinitrotoluene / alpha-		240	UGL	DC7	JN
									Trinitrotoluene					
								21-14-2	2,4-Dinitrotoluene		11.2	UGL	DUQ	N
~								21-82-4	RDX / Cyclonite / Hexahydro-1,3,5- trinitro-1,3,5-triazine *		120	UGL	DC	
A-7								79-45-8	Tetryl / N-Methyl-N,2,4,6- tetranitroaniline / Nitramine / *		5.03	UGL	DU	
								91-41-0	Cyclotetramethylenetetranitramine		14	UGL	DUQ	
								98-95-3	Nitrobenzene / Essence of mirbane /	LT	.682	UGL	D	
									Oil of mirbane		1002		5	
								99-35-4	1,3,5-Trinitrobenzene		310	UGL	DU	1
								99-65-0	1,3-Dinitrobenzene	LT	.458	UGL	D	
	G0085	SAIC01	20.0	03-MAR-94	ŰВ	UB01270	UW25/W	06-20-2	2,6-Dinitrotoluene	LT	59	UGL	ĸ	
	40005	0/1001	2010	Var Pirtu 74	00	0001210		18-96-7	2,4,6-Trinitrotoluene / alpha-	L 1	4200	UGL	ĉ	
								10-30-1	Trinitrotoluene		4200	Out	6	
								21-14-2	2,4-Dinitrotoluene		79	UGL	C	J
								21-82-4	RDX / Cyclonite / Hexahydro-1,3,5-		3800	UGL	č	ŭ
									trinitro-1,3,5-triazine *		2000		Ū	
								79-45-8	Tetryl / N-Methyl-N,2,4,6-		310	UGL	C	
									tetranitroaniline / Nitramine / *				-	
								91-41-0	Cyclotetramethylenetetranitramine	LT	310	UGL	ĸ	
								98-95-3	Nitrobenzene / Essence of mirbane / Oil of mirbane	ĹŤ	67	UGL	ĸ	
								99-35-4	1,3,5-Trinitrobenzene		3800	UGL	C	
								99-65-0	1,3-Dinitrobenzene		32	UGL	č	
	G0104	SAIC01	18.0	02-MAR-94	UB	UB01242	UW25/W	06-20-2	2,6-Dinitrotoluene	LT	52 60	UGL	JI	
	WY 104	SALCOL	10.0	V6"FIAR"74	UD	0001242	UWCJ/W	00-20-2	2,0°0 mil trototaene	L1	00	UGL	91	

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Final Documentation Appendix Report Installation :Louisiana AAP, LA (LO) File Type: CGW Sampling Date Range: 01-SEP-93 27-JUN-S

27-JUN-94

Site Type	Site ID	Field Sample No.	Depth	Sample Date	Lab	Lab Anly. No.	Meth/ Matrix	CAS No.	Analyte Description	Meas. Bool.	Conc.	Unit Meas.	Flag Codes	Data Quals
WELL	G0104	SAIC01	18.0	02-MAR-94	UB	UB01242	UW25/W	18-96-7	2,4,6-Trinitrotoluene / alpha- Trinitrotoluene		11000	UGL	C	J
								21-14-2	2,4-Dinitrotoluene		550	UGL	С	J
								21-82-4	RDX / Cyclonite / Hexahydro-1,3,5- trinitro-1,3,5-triazine *		7100	UGL	č	•
				•				79-45-8	Tetryl / N-Methyl-N,2,4,6- tetranitroaniline / Nitramine / *		120	UGL	C	
								91-41-0	Cyclotetramethylenetetranitramine	LT	370	UGL	κ	
								98-95-3	Nitrobenzene / Essence of mirbane / Oil of mirbane	LT	68	UGL	7J I	L
								99-35-4	1,3,5-Trinitrobenzene		6000	UGL	C	
								99-65-0	1,3-Dinitrobenzene		560	UGL	C	
						UB01243	UW25/W	06-20-2	2,6-Dinitrotoluene	LT	60	UGL	DJI	
								18-96-7	2,4,6-Trinitrotoluene / alpha- Trinitrotoluene		11000	UGL	DC	J
								21-14-2	2,4-Dinitrotoluene		570	UGL	DC	J
								21-82-4	RDX / Cyclonite / Hexahydro-1,3,5- trinitro-1,3,5-triazine *		8400	UGL	DC	
								79-45-8	Tetryl / N-Methyl-N,2,4,6- tetranitroaniline / Nitramine / *		130	UGL	DC	
								91-41-0	Cyclotetramethylenetetranitramine	LT	310	UGL	DK	
A-8								98-95-3	Nitrobenzene / Essence of mirbane / Oil of mirbane	LT	68	UGL	D7J1	J
								99-35-4	1,3,5-Trinitrobenzene		6300	UGL	DC	
								99-65-0	1,3-Dinitrobenzene		580	UGL	ĐC	
	G0105	SAIC01	25.0	28-FEB-94	UB	UB01192	UW25/W	06-20-2	2,6-Dinitrotoluene	LT	60	UGL	JI	
					•		·	18-96-7	2,4,6-Trinitrotoluene / alpha- Trinitrotoluene		16.5	UGL	C	
								21-14-2	2,4-Dinitrotoluene		54	UGL	C	
								21-82-4	RDX / Cyclonite / Hexahydro-1,3,5- trinitro-1,3,5-triazine *		330	UGL	C	
								79-45-8	Tetryl / N-Methyl-N,2,4,6- tetranitroaniline / Nitramine / *		3.71	UGL	U	
								91-41-0	Cyclotetramethylenetetranitramine		360	UGL	C	
								98-95-3	Nitrobenzene / Essence of mirbane / Oil of mirbane	LT	68	UGL	11	
								99-35-4	1,3,5-Trinitrobenzene		3900	UGL	С	
								99-65-0	1,3-Dinitrobenzene		320	UGL	ŬQ	
	G0106	SAIC01	57.0	01-MAR-94	UB	UB01225	UW25/W	06-20-2	2,6-Dinitrotoluene	LT	60	UGL	JI	
								18-96-7	2,4,6-Trinitrotoluene / alpha- Trinitrotoluene		8800	UGL	Ċ	J
								21-14-2	2,4-Dinitrotoluene		640	UGL	С	J
								21-82-4	RDX / Cyclonite / Hexahydro-1,3,5- trinitro-1,3,5-triazine *		4100	UGL	č	-

* - Analyte Description has been truncated. See Data Dictionary

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Final Documentation Appendix Report Installation :Louisiana AAP, LA (LO) File Type: CGW Sampling Date Range: 01-SEP-93 27-JUN-9 27-JUN-94

Site Type	Site ID	Field Sample No.	Depth	Sample Date	Lab	Lab Anly. No.	Meth/ Matrix	CAS No.	Analyte Description	Meas. Bool.	Conc.	Unit Meas.	Flag Codes	pata Quals
WELL	G0106	SAIC01	57.0		UB	UB01225	UW25/W	79-45-8	Tetryl / N-Methyl-N,2,4,6- tetranitroaniline / Nitramine / *	LT	63	UGL	JI	/
								91-41-0	Cyclotetramethylenetetranitramine	LT	53	UGL	JI	
								98-95-3	Nitrobenzene / Essence of mirbane / Oil of mirbane	LT	68	UGL	7J1	Ŀ
								99-35-4	1,3,5-Trinitrobenzene		970	UGL	C	
								99-65-0	1,3-Dinitrobenzene		330	UGL	C	
	G0109	SAIC01	23.0	28-FEB-94	UB	UB01193	UW25/W	06-20-2	2,6-Dinitrotoluene	LT	60	UGL	JI	
								18-96-7	2,4,6-Trinitrotoluene / alpha- Trinitrotoluene		3600	UGL.	C	
								21-14-2	2,4-Dinitrotoluene		330	UGL	C	
								21-82-4	RDX / Cyclonite / Hexahydro-1,3,5- trinitro-1,3,5-triazine *		3100	UGL	C	
								79-45-8	Tetryl / N-Methyl-N,2,4,6- tetranitroaniline / Nitramine / *		39.9	UGL	U	
								91-41-0	Cyclotetramethylenetetranitramine		300	UGL	C	
								98-95-3	Nitrobenzene / Essence of mirbane / Oil of mirbane	LT	6.8	UGL	JI	
								99-35-4	1,3,5-Trinitrobenzene		95	UGL	С	
								99-65-0	1,3-Dinitrobenzene		8.21	UGL	UQ	
	G0110	SAIC01	32.0	28-FEB-94	UB	UB01191	UW25/W	06-20-2	2,6-Dinitrotoluene	LT	60	UGL	JI	
A-9								18-96-7	2,4,6-Trinitrotoluene / alpha- Trinitrotoluene		570	UGL	C	
ف								21-14-2	2,4-Dinitrotoluene		120	UGL	C	
								21-82-4	RDX / Cyclonite / Hexahydro-1,3,5- trinitro-1,3,5-triazine *		2800	UGL	C	
								79-45-8	Tetryl / N-Methyl-N,2,4,6- tetranitroaniline / Nitramine / *	LT	.631	UGL		
								91-41-0	Cyclotetramethylenetetranitramine		130	UGL	C	
								98-95-3	Nitrobenzene / Essence of mirbane /	LT	6.8	UGL	JI	
									Oil of mirbane				~.	
								99-35-4	1,3,5-Trinitrobenzene		460	UGL	C	
								99-65-0	1,3-Dinitrobenzene		24	UGL	ŭq	

** End of Report - 211 Records Found **

. * - Analyte Description has been truncated. See Data Dictionary

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Chemical Quality Control Report

Installation: Louisiana AAP, LA

Analysis Date Range: 01-SEP-93 to 27-JUN-94

Non-Detected Compounds are included

Lab Lot	Field Sample #	Analyte	QC Type	Spike	Media Type	Туре	SiteID	Meth/ Matrix	Analysis Date	Bool	Measurement Value	Unit	Flag Codes	Data Quals	Prog
UB AFGX		135TNB 135TNB 135TNB 135TNB 135TNB 130NB 130NB 130NB 130NB 246TNT 246TNT 246TNT 246TNT 246TNT 240NT 240NT 240NT 260NT 260NT 260NT 260NT 260NT 260NT 260NT 260NT 260NT 260NT 27	M S S S M S S S M S S S M S S S M S S S M S S S M S S S M S S S M S S S M S S S M S S S M S S S M S S S M S S S	.000 .400 16.000 16.000 .000 .000 .000 .000 .00				UW25/W UW25/W	22-0CT-93 22-0CT-93	LT LT LT LT LT LT LT LT LT LT LT LT LT	$\begin{array}{c} .27\\ .713\\ 12.4\\ 12.8\\ .458\\ .458\\ .458\\ .458\\ .458\\ .426\\ .565\\ 26\\ 25.2\\ .397\\ .59\\ 11.3\\ 12\\ .6\\ .6\\ .6\\ .6\\ .533\\ .$	UGL	HHHH		LIT LIT LIT LIT LIT LIT LIT LIT LIT LIT
UB AFIO	SAICO1 SAICO1 SAICO1 SAICO1 SAICO1 SAICO1 SAICO1 SAICO1 SAICO2 SAICO2 SAICO2	TETRYL 135TNB 13DNB 246TNT 24DNT 26DNT HMX NB RDX TETRYL 135TNB 13DNB 246TNT	S RRRRR RRRRRRRRRRRRRRRRRRRRRRR	.000 .000 .000 .000 .000 .000 .000 .00	CGW CGW CGW CGW CGW CGW CGW CGW	RNSW RNSW RNSW RNSW RNSW RNSW RNSW RNSW	#6 #6 #6 #6 #6 #6 #6 #6 #6 #6	UW25/W UW25/W UW25/W UW25/W UW25/W UW25/W UW25/W UW25/W UW25/W UW25/W UW25/W UW25/W	22-0CT-93 10-NOV-93 10-NOV-93 10-NOV-93 10-NOV-93 10-NOV-93 10-NOV-93 10-NOV-93 10-NOV-93 10-NOV-93 10-NOV-93 10-NOV-93 10-NOV-93	LT LT LT LT LT LT LT LT LT LT LT LT LT	.631 .631 .458 .426 .397 .6 .533 .682 .416 .631 .21 .458 .426		D D D		LIT Mon Mon Mon Mon Mon Mon Mon Mon Mon Mon

Chemical Quality Control Report

Installation: Louisiana AAP, LA

Analysis Date Range: 01-SEP-93 to 27-JUN-94

Non-Detected Compounds are included

Lab Lot	Field Sample #	Analyte	Туре	Spike	Media Type	Туре	Site _	10	Meth/ Matrix	Analysis Date	Bool M	leasurement Value	Unit	Flag Codes	Data Quals	Prog
UB AFIO	SAIC02	24DNT	R	.000	CGW	RNSW	#6		UW25/W	10-NOV-93	LT	.397		D		MON
	SAIC02	26DNT	R	.000	CGW	RNSW	#6		UW25/W	10-NOV-93	LT	.6		D		MON
	SAICO2 SAICO2	HMX	R R	.000 .000	CGW CGW	RNSW			UW25/W	10-NOV-93 10-NOV-93	LT LT	.533 .682		D D		MON
	SAICO2	NB RDX	R	.000	CGW	RNSW RNSW	#0 #6		UW25/W UW25/W	10-NOV-93	LT	.416		D		mon Mon
	SAICO2	TETRYL	R	.000	CGW	RNSW	#6		UW25/W	10-NOV-93	ĨŤ	.631		D		MON
		135TNB	M	.000	CQC				UW25/W	10-NOV-93	LT	.21	UGL	-		LIT
		135TNB	S	.400	CQC				UW25/W	10-NOV-93		.398	UGL			LIT
		135TNB	S	16.000	CQC				UW25/W	10-NOV-93		16	UGL			LIT
		135TNB	S	16.000	CQC				UW25/W	10-NOV-93		16.5	UGL			LIT
		13DNB	M	.000	CQC				UW25/W	10-NOV-93	LT	-458	UGL			LIT
		13DNB 13DNB	S S	.000	CQC CQC				UW25/W UW25/W	10-NOV-93 10-NOV-93	LT LT	.458 .458	UGL UGL			LIT LIT
		13DNB	S	.000	CQC				UW25/W	10-NOV-93	LT	.458	UGL			LIT
		246TNT	Ň	.000	CQC				UW25/W	10-NOV-93	īτ	.426	UGL			LIT
		246TNT 246TNT	S	.800	CQC				UW25/W	10-NOV-93		.581	UGL			LIT
		246TNT	S	32.000	CQC				UW25/W	10-NOV-93		33.6	UGL			LIT
		246TNT	S	32.000	CQC				UW25/W	10-NOV-93		32.9	UGL			LIT
~		24DNT	M	.000	CQC				UW25/W		LT	.397	UGL			LIT
1		24DNT	S	.800	CQC				UW25/W	10-NOV-93		.588	UGL			LIT
A-11		24DNT 24DNT	S S	16.000 16.000	CQC CQC				UW25/W UW25/W	10-NOV-93 10-NOV-93		14.5 14.2	UGL UGL			LIT LIT
		26DNT	M	.000	CQC				UW25/W	10-NOV-93	LT	.6	UGL			LIT
		26DNT	S	.000	CQC				UW25/W	10-NOV-93	LT	.6	UGL			LIT
		26DNT	S	.000	CQC				UW25/W	10-NOV-93	LT	.6 .6	UGL			LIT
		26DNT	S	.000	CQC				UW25/W	10-NOV-93	LT	.6	UGL			LIT
		HMX	M	.000	COC				UW25/W	10-NOV-93	LT	.533	UGL			LIT
		HMX	S	.000	CQC				UW25/W	10-NOV-93	LT	.533	UGL			LIT
		HMX HMX	S	.000	CQC CQC				UW25/W UW25/W	10-NOV-93 10-NOV-93	LT	.533	UGL			LIT
		NB	S M	.000 .000	CQC				UW25/W	10-NOV-93	LT LT	.533 .682	UGL UGL			LIT LIT
		NB	S	1.400	CQC				UW25/W	10-NOV-93	L 1	1.08	UGL			LIT
		NB	s	32.000	CQC				UW25/W	10-NOV-93		28.6	UGL			LIT
		NB	S	32.000	CQC				UW25/W	10-NOV-93		27.3	UGL			LIT
		RDX	М	.000	CQC				UW25/W	10-NOV-93	LT	.416	UGL			LIT
		RDX	S	.800	CQC				UW25/W	10-NOV-93		.704	UGL			LIT
		RDX	S	32.000	CQC				UW25/W	10-NOV-93		33.7	UGL			LIT
		RDX	S	32.000	CQC				UW25/W	10-NOV-93	1 7	32.5	UGL			LIT
		TETRYL Tetryl	M S	.000 .000	090 090				UW25/W UW25/W	10-NOV-93 10-NOV-93	LT LT	.631 .631	UGL UGL			LIT LIT
		TETRYL	S	.000	CQC				UW25/W	10-NOV-93	LT	.631	UGL			LIT
		TETRYL	S	.000					UW25/W		LT	.631	UGL			LIT
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Chemical Quality Control Report

Installation: Louisiana AAP, LA

Analysis Date Range: 01-SEP-93 to 27-JUN-94

Non-Detected Compounds are included

Lab	Lot	Field Sample #	Analyte	Type	QCSpike	Media Type		Site _	ID	Meth/ Matrix	Analysis Date	Bool	Measurement Value	Unit	Flag Codes	Data Quals	Prog
			•		•												
UB	AIUD	SAICRB01	135TNB	R	.000	CGW	RNSW	G0012		UW25/W	02-MAR-94	LT	.21	UGL			MON
	-	SAICRB01	13DNB	R	.000	CGW	RNSW	G0012		UW25/W	02-MAR-94	LT	.458	UGL			MON
		SAICRB01	246TNT	R	.000	CGW	RNSW	G0012		UW25/W	02-MAR-94	LT	.426	UGL			MON
		SAICRB01	24DNT	R	.000	CGW	RNSW	G0012		UW25/W	02-MAR-94	LT	.397	UGL			MON
		SAICRB01	26DNT	R	.000	CGW	RNSW	G0012		UW25/W	02-MAR-94	LT	.6	UGL			MON
		SAICR801	HMX	R	.000	CGW	RNSW	G0012		UW25/W	02-MAR-94	ŁT	.533	UGL			MON
		SAICRB01	NB	R	.000	CGW	RNSW	G0012		UW25/W	02-MAR-94	LT	1.84	UGL	K		MON
		SAICRB01	RDX	R	.000	CGW	RNSW	G0012		UW25/W	02-MAR-94	LT	.416	UGL	7	3	MON
		SAICRB01	TETRYL	R	.000	CGW	RNSW	G0012		UW25/W	02-MAR-94	LT	.631	UGL			MON
			135TNB	M	.000	CQC				UW25/W		LT	.21	UGL			LIT
			135TNB	S	.400	CQC				UW25/W	02-MAR-94		.439	UGL			LIT
			135TNB	S	16.000	CQC				UW25/W	02-MAR-94		14.5	UGL			LIT
			135TNB 13DNB	S	16.000 .000	292 292				UW25/W	02-MAR-94		13.9 .458	UGL UGL			LIT
			13DNB	M	.000	CQC				UW25/W UW25/W	02-MAR-94 02-MAR-94	LT	.458	UGL			LIT
			13DNB	S S	.000	CQC				UW25/W	02-MAR-94	LT	.458	UGL			LIT LIT
			13DNB	S	.000	CQC				UW25/W	02-MAR-94	LT	.458	UGL			LIT
	$\mathbf{\Sigma}$		246TNT	M	.000	CQC				UW25/W	02-MAR-94		.426	UGL			LIT
	T		246TNT	S	.800	CQC				UW25/W	02-MAR-94	FG (.585	UGL			LIT
	A-12		246TNT	š	32.000	CQC				UW25/W	02-MAR-94		27.9	UGL			LIT
	• •		246TNT	s	32.000	CQC				UW25/W	02-MAR-94		26.5	UGL			LIT
			24DNT	M	.000	CQC				UW25/W	02-MAR-94	LT	.397	UGL			LĨŤ
			24DNT	S	.800	CQC				UW25/W	02-MAR-94		.625	UGL			LIT
			24DNT	S	16,000	CQC				UW25/W	02-MAR-94		13.8	UGL			LIT
			24DNT	S	16.000	CQC				UW25/W	02-MAR-94		12.6	UGL			LIT
			26DNT	М	.000	CQC				UW25/W	02-MAR-94	LT	.6	UGL			LIT
			26DNT	S	.000	CQC				UW25/W	02-MAR-94	LT	.6	UGL			LIT
			26DNT	S	.000	CQC				UW25/W	02-MAR-94	LT	.6	UGL			LIT
			26DNT	S	.000	CQC				UW25/W	02-MAR-94	LT	.6	UGL			LIT
			HMX	M	.000	CQC				UW25/W	02-MAR-94	LT	.533	UGL			LIT
			HMX	S	.000	CQC				UW25/W	02-MAR-94	LT	.533	UGL			LIT
			HMX	S	.000	CQC				UW25/W	02-MAR-94	LT	.533	UGL			LIT
			HMX	S	.000	CQC				UW25/W	02-MAR-94	LT	.533	UGL			LIT
			NB	м	.000	CQC				UW25/W	02-MAR-94	LT	.682	UGL			LIT
			NB	S	1.400	CQC				UW25/W	02-MAR-94		1.12	UGL			LIT
			NB	S	32.000	CQC				UW25/W	02-MAR-94		27.3	UGL			LIT

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Installation: Louisiana AAP, LA

Analysis Date Range: 01-SEP-93 to 27-JUN-94

Non-Detected Compounds are included

Lab Lot	Field Sample #	Analyte	Туре	Spike	Media Type	Туре	SiteID	Meth/ Matrix	Analysis Date	Bool	Measurement Value	Unit	Flag Codes	Data Quals	Prog
UB AIUD		NB RDX RDX RDX RDX TETRYL TETRYL TETRYL TETRYL	9 E 9 9 9 E 9 9 9	32.000 .000 32.000 32.000 .000 .000 .000	202 202 202 202 202			UW25/W UW25/W UW25/W UW25/W UW25/W UW25/W UW25/W UW25/W UW25/W	02-MAR-94 02-MAR-94 02-MAR-94 02-MAR-94 02-MAR-94 02-MAR-94 02-MAR-94 02-MAR-94 02-MAR-94	LT LT LT	25.2 .416 .573 31.3 .631 .631 .631 .631	UGL UGL UGL UGL UGL UGL UGL	7 7	ե Ե Ե	LIT LIT LIT LIT LIT LIT LIT LIT
ub aiwa A-13	SAICRB03 SAICRB03 SAICRB03 SAICRB03 SAICRB03 SAICRB03 SAICRB03 SAICRB03 SAICRB03	135TNB 130NB 246TNT 240NT 240NT 240NT 240NT 240NT 25TNB 135TNB 135TNB 135TNB 135TNB 135TNB 135TNB 135NB 135NB 130NB 246TNT 246TNT 246TNT 246TNT 246TNT 240NT	RRRRRRRK%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%	$\begin{array}{c} .000\\$		RNSW RNSW RNSW RNSSW RNSSW RNSSW RNSSW RNSSW RNSSW	G0110 G0110 G0110 G0110 G0110 G0110 G0110 G0110	UW25/W UW25/W	29-MAR-94 29-MAR-94		.21 .458 .426 .397 .6 .533 2.95 .416 .631 .21 .497 15.5 15.3 .458 .458 .458 .458 .458 .458 .458 .458	UGL UGL UGL UGL UGL UGL UGL UGL UGL UGL	UQ		MON MON MON MON MON MON MON MON MON LIT LIT LIT LIT LIT LIT LIT LIT LIT LIT

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Chemical Quality Control Report

Installation: Louisiana AAP, LA

Analysis Date Range: 01-SEP-93 to 27-JUN-94

Non-Detected Compounds are included

Lab	Lot	Field Sample #	Analyte	Type Q(Spike	Media Type	Туре	SiteID	Meth/ Matrix	Analysis Date	Bool	Measurement Value	Unit	Flag Codes	Data Quals	Prog
UB	AIWA		RDX RDX TETRYL TETRYL TETRYL TETRYL	S S M S S S	32.000 32.000 .000 .000 .000	CQC CQC CQC			UW25/W UW25/W UW25/W UW25/W UW25/W UW25/W	29-MAR-94 29-MAR-94 29-MAR-94 29-MAR-94 29-MAR-94 29-MAR-94	LT LT	33.5 32.9 .631 .631 .631 .631 .631	UGL UGL UGL UGL UGL UGL		·	LIT LIT LIT LIT LIT LIT
UB	AIWV A-14	SAIC05 SAIC05 SAIC05 SAIC05 SAIC05 SAIC05 SAIC05 SAIC05 SAIC06 SAIC05 SAIC06 SAIC06 SAIC06 SAIC06 SAIC06 SAIC06 SAIC06 SAIC06 SAIC06 SAIC06 SAIC06 SAIC06 SAIC06 SAIC05 SAIC05 SAIC05 SAIC05 SAIC05 SAIC05 SAIC05 SAIC05 SAIC05 SAIC05 SAIC05 SAIC05 SAIC05 SAIC06 SAICR02	135TNB 13DNB 246TNT 24DNT 26DNT HMX NB RDX TETRYL 135TNB 13DNB 246TNT 24DNT 26DNT HMX NB RDX TETRYL 135TNB 13DNB 13DNB 135TNB 135TNB 135TNB 135TNB 135TNB 135TNB 135TNB 135TNB 135TNB 135TNB 135TNB 135TNB 135TNB 135TNB 135TNB 135TNB	N N N N N N N N N N N N N N N N N N N	16.000 .000 32.000 32.000 32.000 32.000 16.000 .000 32.000 16.000 .000 .000 .000 .000 .000 .00	CGW CGW CGW CGW CGW CGW CGW CGW CGW CGW	WEELLLLLLLLLLLLLWWWWWWWWWWWWWWWWWWWWWW	60083 60089 60009 60009 60009 60009 60009 60009 60009 60009 60009 60009 60009	UW25/W UW25/W	16-MAR-94 16-MAR-94		830 4.73 3200 140 12 150 24.2 1900 88 780 5.09 3000 130 12 130 25 1600 88 .42 .458 .426 .397 .6 .533 2.66 .746 .631 .304 .578 16.7 15.5 .458 .458 .458 .458	UGL UGL UGL UGL UGL UGL UGL UGL UGL UGL	JI D D D D D D D D C 7		MON MON MON MON MON MON MON MON MON MON
			246TNT 246TNT 246TNT 246TNT 24DNT 24DNT 24DNT	M S S S M S S	.000 .800 32.000 32.000 .000 .800 16.000	CQC CQC CQC CQC			UW25/W UW25/W UW25/W UW25/W UW25/W UW25/W	16-MAR-94 16-MAR-94 16-MAR-94 16-MAR-94 16-MAR-94 16-MAR-94		.426 .46 24.3 25.3 .397 .49 11.4	UGL UGL UGL UGL UGL UGL	7 7	JN JN JN N N N	LIT LIT LIT LIT LIT LIT LIT

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Chemical Quality Control Report

Installation: Louisiana AAP, LA

Analysis Date Range: 01-SEP-93 to 27-JUN-94

Non-Detected Compounds are included

Lab Lot	Field Sample # /	Analyte	Туре	Spike	Media Type	Type	SiteID	Meth/ Matrix	Analysis Date	Bool	Measurement Value	Unit	Flag Codes	Data Quals	Prog
ub aiwv A-15		24DNT 26DNT 26DNT 26DNT 26DNT 26DNT HMX HMX HMX HMX HMX HMX HMX NB NB NB NB NB NB NB NB RDX RDX RDX RDX RDX TETRYL TETRYL TETRYL	S M S S S M S S S M S S S M S S S M S S S M S S S M S S S M S S S M S S S M S S S M S S S M S S S S	16.000 .000 .000 .000 .000 .000 .000 .00	CQC CQC CQC CQC CQC CQC CQC CQC CQC CQC			UW25/W UW25/W	16-MAR-94 16-MAR-94 16-MAR-94 16-MAR-94 16-MAR-94 16-MAR-94 16-MAR-94 16-MAR-94 16-MAR-94 16-MAR-94	LT LT LT LT LT LT LT LT LT	11 .6 .6 .533 .533 .533 .533 .533 .682 1.04 24.1 24.8 .416 .762 30 29.7 .631 .631 .631	UGL UGL UGL UGL UGL UGL UGL UGL UGL UGL		N	LIT LIT LIT LIT LIT LIT LIT LIT LIT LIT
UB AIYH	SAICO1 SAICO1 SAICO1 SAICO1 SAICO1 SAICO1 SAICO1 SAICRB04 SAICRB04 SAICRB04 SAICRB04 SAICRB04 SAICRB04 SAICRB04 SAICRB04 SAICRB04 SAICRB04 SAICRB04	135TNB 246TNT 240NT 240NT 240NT 240NT HMX RDX TETRYL 260NT 135TNB 1246TNT 240NT 240NT 135TNB 130NB 135TNB 135TNB 135TNB 135TNB 130NB 130NB 130NB 130NB 130NB	R R R R R R R R R R R R R R R R M S S S M S S S M	.000 .000 .000 .000 .000 .000 .000 .00	CGW CGW CGW CGW CGW CGW CQC CQC CQC CQC CQC CQC	RNSW RNSW RNSW RNSW RNSW RNSW RNSW RNSW	GO- 145 GO- 145 GO- 145 GO- 145 GO- 145 GO- 145 GO- 145 GO- 145 GO- 145 GO- 146 GO- 146 GO- 146 GO- 146 GO- 146 GO- 146 GO- 146 GO- 146 GO- 146	UW25/W UW25/W	30-MAR-94 30-MAR-94 30-MAR-94 30-MAR-94 30-MAR-94 30-MAR-94 29-MAR-94 29-MAR-94 29-MAR-94 29-MAR-94 29-MAR-94 29-MAR-94 29-MAR-94 29-MAR-94 29-MAR-94 29-MAR-94 29-MAR-94 29-MAR-94 29-MAR-94 29-MAR-94	LT LT LT LT LT LT	.21 .458 .426 .397 .6 .533 .682 .416 .631 .21 .458 .426 .397 .6 5.03 .682 .416 .631 .21 .371 16.5 14 .458 .458 .458 .458 .458 .458 .458	UGL UGL UGL UGL UGL UGL	7 C 7	1 1 1 1	MON MON MON MON MON MON MON MON MON MON

Chemical Quality Control Report

Installation: Louisiana AAP, LA

Analysis Date Range: 01-SEP-93 to 27-JUN-94

Non-Detected Compounds are included

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Leh	Lot	Field Sample #	Analyte	Туре	QCSpike	Media Type	Type S	Site	Meth/ Matrix	Analysis Date	Bool	Measurement Value	Unit	Flag Codes	Data Quals	Prog
		Sample #	•		-		iype	10			5001			COUES		
UB	AIYH		246TNT	S	.800	CQC			UW25/W	29-MAR-94		.481	UGL		J	LIT
			246TNT 246TNT	S S	32.000 32.000	CQC CQC			UW25/W UW25/W	29-MAR-94 29-MAR-94		27.2 26.3	UGL UGL		4	LIT
			2401N1 24DNT	5	.000	CQC			UW25/W	29-MAR-94	LT	.397	UGL		0	LIT LIT
			24DNT	S	.800	CQC			UW25/W	29-MAR-94	61	.447	UGL		.1	LIT
			24DNT	5	16.000	CQC			UW25/W	29-MAR-94		12.5	UGL		.) .)	LIT
			24DNT	Š	16.000	CQC			UW25/W	29-MAR-94		13.3	UGL		1	LIT
			26DNT	M	.000	CQC			UW25/W	29-MAR-94	LT	.6	UGL		•	LIT
			26DNT	S	.000	CQC			UW25/W	29-MAR-94	ĹΤ	.6	UGL			LIT
			26DNT	S	.000	CQC			UW25/W	29-MAR-94	LT	.6	UGL			LIT
			26DNT	S	.000	CQC			UW25/W	29-MAR-94	LT	.6	UGL			LIT
			HMX	M	.000	CQC			UW25/W	29-MAR-94	LT	.533	UGL			LIT
			HMX	S	.000	CQC			UW25/W	29-MAR-94	LT	.533	UGL			LIT
			HMX	S	.000	CQC			UW25/W	29-MAR-94	LT	.533	UGL			LIT
			HMX	S	.000	CQC			UW25/W	29-MAR-94	LT	.533	UGL	-		LIT
			NB	M	.000	CQC			UW25/W	29-MAR-94	LT	.682	UGL	7	J	LIT
			NB	S	1.400	CQC			UW25/W	29-MAR-94		.716	UGL	7	J.	LIT
			NB	S	32.000 32.000	CQC			UW25/W	29-MAR-94		23.1	UGL	7	1	LIT
	•		NB	S	52.000	202			UW25/W	29-MAR-94		26.1	UGL	7	J	LIT
	A-16		RDX	m O	.000	CQC			UW25/W	29-MAR-94	LT	.416	UGL			LIT
	÷		RDX RDX	5	.800 32.000	CQC CQC			UW25/W UW25/W	29-MAR-94 29-MAR-94		.727 33.7	UGL UGL			LIT
	σ		RDX	S	32.000	CQC			UW25/W	29-MAR-94		29.8	UGL			LIT LIT
			TETRYL	M	.000	CQC			UW25/W	29-MAR-94	LT	.631	UGL			LIT
			TETRYL	ri S	.000	CQC			UW25/W	29-MAR-94	LT	.631	UGL			LIT
			TETRYL	s	.000	CQC			UW25/W	29-MAR-94	LT	.631	UGL			LIT
			TETRYL	s	.000	CQC			UW25/W	29-MAR-94	LT	.631	UGL		•	LIT
UB	AJDT	SAICRB06	135TNB	R	.000	CGW	RNSW	GO-150	UW25/W	08-APR-94	LT	.21	UGL			MON
		SAICRB06	13DNB	R	.000	CGW	RNSW	GO-150	UW25/W	08-APR-94	ĒŤ	.458	UGL			MON
		SAICRB06	246TNT	R	.000	CGW	RNSW	GO-150	UW25/W	08-APR-94	Ĩ.T	.426	UGL			MON
		SAICRB06	24DNT	R	.000	CGW	RNSW	GO-150	UW25/W	08-APR-94	ΪŤ	.397	UGL		J	MON
		SAICRB06	26DNT	R	.000	CGW	RNSW	GO-150	UW25/W	08-APR-94	ĹΤ	.6	UGL		-	MON
		SAICRB06	HMX	R	.000	CGW	RNSW	GO-150	UW25/W	08-APR-94	LT	.533	UGL			MON
		SAICRB06	NB	R	.000	CGW	RNSW	GO-150	UW25/W	08-APR-94	LT	.682	UGL			MON

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Installation: Louisiana AAP, LA

Analysis Date Range: 01-SEP-93 to 27-JUN-94

Non-Detected Compounds are included

Field Lab Lot Sample # Analy	e Type Spike	Media Site Type Type ID	Meth/ Analysis Matrix Date	Measurement Bool Value U	Flag Data Jnit Codes Quais Prog
Lab Lot Sample # Analy UB AJDT SAICRBO6 SAICRBO6 SAICRBO6 TETRYI 135TNK	e Type Spike R .000 R .000 M .000 S .400 S 16.000 S 16.000 S 16.000 S .000 S 16.000 S .000 S .000 S .000 S .000 S .000 S .000 S .000 S .000 S .800 S .32.000 S .000 S 16.000 S .000 S 16.000 S .000 S .000 S .2000 M .000 S .2000 S .32.000 .000 S .	Type Type ID CGW RNSW GO-150 CGC RNSW GO-150 CAC CAC CAC CAC <td< td=""><td>Matrix Date UW25/W 08-APR-94 <t< td=""><td>Bool Value U LT .416 U LT .631 U LT .21 U .359 U 15.5 14.9 U 14.9 LT .458 U .27.8 U 28.9 U .27.8 U .431 U .13.1 U .13.1 U LT .66 U U LT .66 U U LT .533 U U <!--</td--><td>Init Codes Quais Prog JGL MON JGL MON JGL LIT JGL J JGL LIT JGL LIT </td></td></t<></td></td<>	Matrix Date UW25/W 08-APR-94 UW25/W 08-APR-94 <t< td=""><td>Bool Value U LT .416 U LT .631 U LT .21 U .359 U 15.5 14.9 U 14.9 LT .458 U .27.8 U 28.9 U .27.8 U .431 U .13.1 U .13.1 U LT .66 U U LT .66 U U LT .533 U U <!--</td--><td>Init Codes Quais Prog JGL MON JGL MON JGL LIT JGL J JGL LIT JGL LIT </td></td></t<>	Bool Value U LT .416 U LT .631 U LT .21 U .359 U 15.5 14.9 U 14.9 LT .458 U .27.8 U 28.9 U .27.8 U .431 U .13.1 U .13.1 U LT .66 U U LT .66 U U LT .533 U U </td <td>Init Codes Quais Prog JGL MON JGL MON JGL LIT JGL J JGL LIT JGL LIT </td>	Init Codes Quais Prog JGL MON JGL MON JGL LIT JGL J JGL LIT JGL LIT
TETRY	s .000		UW25/W 08-APR-94 UW25/W 08-APR-94	LT .631 U	JGL LIT JGL LIT

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** End of Report - 9647 Records Found **

APPENDIX B WELL DEVELOPMENT AND SAMPLING FORMS

WELL DEVELOPMENT FORMS



Well Development Form (Field Sheet)
Project Name and Number: LAAP FIVE - YEAR REVIEW
Well Number and Location: AREA P, GOOD9
Development Crew: J. Patel, C. Fontung J. Pullom Driller (if applicable):A
Water Levels/Time: Initial: 18.42 Broc Pumping: Final: 18.19 Broc
Total Well Depth: Initial: NA Final: 22.8 Broc
Date and Time: Begin: 2/24/94 1610 Completed: 2/25/94 1140
Development: Method(s): <u>2" SUBMERSIBLE REPLACED BY BAILING</u>
DUE TO LARGE % OF SUSPENDED SOLDS
Total Quantity of Water Removed: 39 gals

			Field Measurements					
Date/Time and Pump Setting	Discharge Rate* and Measurement Method	● <i>F</i> Temp (2€)	Specific Conductivity (umhos/cm)	pH (Standard Units)	Turbidity	Remarks (Including Sand Production)		
2/24/94		હવં	0.10× 10	(q.Z	V. TURBID	LARGE % OF FAVES		
2/25/94	BAILING	69	G-1/X10	6.2	TURBID	,		
1[[0	BAILING	້ ຮ ບ	0./0x/0	5.7.	PARTON			
1230		. 69°F	0.18 x 10	4.43	PARTLY TURBID	% of Frates Greatly Reduce		
	·							
LA26E 4	MOUNT OF P	RTICULAT	ES int H	20 0874	WED FR	om well,		
LARGE A	TO USE THE HOUNT BE H ALLONS FRI	20 REMO	SIBLE A. VED. BAIO	HP TO ; ER USI	20126E WE	REMOVE		
	nute or bailer capacity		1	L		<u> </u>		



Well Development Form

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(Field Sheet)

Project Name and Number: LAAP FIVE - YEAR REVIEW
Vell Number and Location: 60012, SALCOL
Development Crew: C. FontanA Driller (if applicable):
Vater Levels/Time: Initial: 17.12 Broc. Pumping: Final:
Total Well Depth: Initial: <u>25.0 800</u> Final:
Date and Time: Begin: 2/23/94 1640 Completed: 2/24/94 1255
Development: Method(s): WELL BAILED, INITIAL PUMPING NOT ABLE
TO CLEAR SEDIMENT THROUGH RUMP.
Total Quantity of Water Removed: <u>SO GALLOUS REMOVED W</u> gals

BAILER

Date/Time	Discharge Rate*		Field Mea	Remarks			
and Pump Setting	and Measurement Method	Temp (Ser	Specific Conductivity (umhos/cm)	pH (Standard Units)	Turbidity	(Including Sand Production)	
z/23/94 1640	BALLING	70°F	0,31210	6.9	mu00 y	CHIZIS TO BA	10
1710	BAILING	68°F	0.25×10	6.6	CLO UDY	LARGE AMART	0
1740	BAILIND	64 F	0.2 ×10	6.5	cronzy		
1800	BAILING	62°F	0.11X10	6.2	P. CLOUDY		
2/24/24	BAILINEG	62°F	0,11,20	6.2	P. CLOUS	9	
1050	BALIND	62°F	6. jox 10	6.35	P. CLOUDY		
1130	BAILING	63°F	0.11×10	6.30	P. CLOUDY		
1210	BAILING	4°20	0.12410	6-14-	CLEAR	HZOH45 CLEARED UP - STILL SMAL % SUSPENDED SOUDS	

*gallons per minute or bailer capacity



mployee-Owned Company				·····				
	W	ell Dev (F	elopn ield She	•	orm			
Project Name and I	Number:	AAP	FIVE	484	R RET	VREW		
Well Number and L	ocation:	60014	-					
Development Crew								
Water Levels/Time:							: NR	
Total Well Depth:	Initial:		Fin	al:				
Date and Time:	Begin: <u>}</u>	23/94 0	590Z Com	pleted: <u>z</u>	/24/24	1- 19	230	
Development:	Method(s): _	PUMA	46 W	TH 2	" SUR	46751	BLE	
	PUMP,	,						
	Total Quanti	ty of Water R	emoved:				24	gals

د مهدمذه

		Field Measurements					
Date/Time and Pump Setting	Discharge Rate* and Measurement Method	Temp (°C)	Specific Conductivity (umhos/cm)	pH (Standard Units)	Turbidity	Remarks (Including Sand Production)	
2/23/94 0985	~Zgul/min	56°C	0.62%	5.90	U. TURBA		
0928	, Lį	61,2°C	0,382	06.48	17		
0948	(1	59.0	0.37×10	6.50	PARTE T	URBAD	
1420	(1	57.1	0.37410	6.45	4	4	
2/24/14	17	49.0	1.14×10	6.44	εį.	11	
0920 18 10 1410	// []	50.0 50.0	1.13×10 1.12×10		u Party	(1 TURBID	
	DWATEIZ NO					HOWEVER	
PARAM	ETERS ST.	4312120	D AND	FIVE.	TIMES	WELL	
VOLUM	E CRITERIA	4 WAS	MET. G	IELL R	ECHARE	S Scow,	
SAMPLO	E WILL BE	FILTER	222 20,	21416 E	YPLOSIU	ES ANALYS	
*gallons per min	nute or bailer capacity						

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(Field Sheet)
Project Name and Number: LAAP FIVE-YEAR REVIEW
Well Number and Location: <u>AREA</u> P. WELL 60068
Development Crew: W. STONER, C. FONRANA Driller (if applicable): 4/4
Water Levels/Time: Initial: 19-2 Broc 0932 Pumping: Final: Final: Final:
Total Well Depth: Initial: 36.02 BtoC Final:
Date and Time: Begin: <u>z/28/94 0932</u> Completed: <u>3/1/94 1645</u>
Development: Method(s): <u>BAILER USED TO PURGE WELL</u>

<u>~70</u> gais

٦

Total Quantity of Water Removed:

Date/Time and Pump Setting			Field Measurements					
	and Pump	Discharge Rate* and Measurement Method	°F Temp_(°C)	Specific Conductivity (umhos/cm)	pH (Standard Units)	Turbidity	Remarks (Including Sand Production)	
1/28/94 12.44		45	3.7 × 10	7.8	V. TUEBID			
5/1/94		62.4	362.410	7-66	CLOUDY			
1650 1320		62.0	3.6x10	7.61	P. CLOUDY			
1645		61.0	3.62×10	7, 8	CLEAR			

*gallons per minute or bailer capacity



nployee-Owned Company
Well Development Form (Field Sheet)
Project Name and Number: LAAP FIVE YEAR REVIEW
Well Number and Location: AREA P, WELL 60083
Development Crew: C. Font TANA, J. PENDLETON Driller (if applicable): N/A
Water Levels/Time: Initial: <u>19.76 втос</u> Pumping: Final: <u>JR</u>
Total Well Depth: Initial:Final:
Date and Time: Begin: <u>//32_ z/z4/94_</u> Completed:
Development: Method(s): <u>2" SUBMERSIBLE PUMP (REDIFLO Z)</u>

_ gals

Total Quantity of Water Removed: 55

1				Field Mea	surements		
Date/Time and Pump Setting	Mea	arge Rate* and surement lethod	°∕≓ Temp (₽С)	Specific Conductivity (umhos/cm)	pH (Standard Units)	Turbidity	Remarks (Including Sand Production)
134			43°	015×10	7.55	CLEAR	
1156			63.5	0.12×10	6.55	V. CLEAR	
0530			64.8	0.11 × 10	5.43	CLEAIZ	PH METERZ
1545			62.4-	0.11×10	NR	CLEAIZ	NOT OPERATIAN
1620			62.0	0.11 × 10	4.4	P. CLOUDY	
2/25/94 0832			55.4	0,18×10	5.4	P. CLOUDY	
0830			53.7	0.15×10	4,93	CLEAR	
0940			0.23	0.10×10	NR	CLEAIZ	
1340			\$5.2	0.10 ×10	5.36	CLEAR	
1343			52'	0,10×10	5,32	CLEAR	
WELL 60	E80	PUMPED	Dey Six	TIMES O	NETS COU		THE DAVE
HZO CI	EAZ	DURING	PURGINE	•			TWO DAYS,
				L	<u> </u>	L	L

*gallons per minute or bailer capacity



Employee-Owned Co	ompany	when the second s			·····		
	W		elopme		n		
		(Fie	eld Sheet)			
Project Name	e and Number:	AAP FIN	JE -YEAR	REVIEW	١		
Well Number	and Location:	trea P	6008	34			
Development	Crew: J. PEVOLE	TON, C. FON	TANA Drille	er (if applicabl	e): <u>~/4</u>	.21.6	
Water Levels	/Time: Initial:	19.75	Pumpi	ng:		inal: <u>N; 21.6</u>	Broc
Total Well De	epth: Initial:	35.62	Final:				
Date and Tim	,	y				<u> </u>	
Development	t: Method(s): _	2" SUBME	TZSIBLE	Pump (1	PEDIFLO	2)	
	<u></u>			<u> </u>	······		
	Total Quantit	y of Water Re	emoved:	~35		gals	
[]		r					
Date/Time	Discharge Rate*		Field Mea	surements	r	Remarks	
and Pump Setting	and Measurement Method	°F Temp (°C)	Specific Conductivity (umhos/cm)	pH (Standard Units)	Turbidity	(Including Sand Production)	
2/24/74		62,5	9,4×10		{	RECHARGE V, SLOW	
		52.8	1.0 × 100	5.74	CLEAR	Dentrate	

and Pump Setting	and Measurement Method	Temp (°C)	Specific Conductivity (umhos/cm)	pH (Standard Units)	Turbidity	(Including Sand Production)
2/24/14 1722 2/25/94 0850 0856		62,5 52,8 52.4	9,4×10 1.0 ×100 1.0×100	5.7	VI CLEAR CLEAR CLEAR CLEAR	RECHARGE V. SLOW RECHARGE V. SLOW
1300		52.0	1.0 ¥100			SLOW
TO PURE	SE OF WEL $SE CALCULAT S% RULE(W)TE SAMPLE 7$	ED TOT	AL, ST NY RECH	IMES TI IZGE 85	FF WELL	- VOLUME,

*gallons per minute or bailer capacity



nployee-Owned Company
Well Development Form
(Field Sheet)
Project Name and Number: <u>LAAP FIVE YEAR REVIEW</u>
Well Number and Location: <u>AREA P, 60085</u>
Development Crew: Wayne Stoner, Clinis Fortune Driller (if applicable): NA
Water Levels/Time: Initial: 18.38 370 Pumping: Final: 20 Broc.
Total Well Depth: Initial: <u>35.23 'втос</u> Final:
Date and Time: Begin: 3/2/94 1730 Completed: 3/3/94 0931
Development: Method(s): 2" SUBMERSIBLE GRUNDFOS RUMP (REDIFLO 2)

Total Quantity of Water Removed: ______ Aj>prox, 53 gals

. · ·

Date/Time and Pump Setting						
	Discharge Rate* and Measurement Method	Temp (°C)	Specific Conductivity (umhos/cm)	pH (Standard Units)	Turbidity	Remarks (Including Sand Production)
3/2/94	~ Zgal (min ~ Zgal (nin	62.7°F 57.2	7,70×10	NIZ	Р. тоевод 1, 11	
/3/94 0823	~ 1 gcl./min (BUCKET/WATCH)	12.9	4.53×10	NR	P. TURBID	
0825	-1gel/min	14.7	12.55×10	NR	P. TURBID	
	~ . 8 5 1/ min	16.1	12.87×10	NIZ	CLEAR	
0845		15.9	11.95 x 10	NIZ	CLEAR	
0905	~ · 8 sul/min	18.7	12.27×10	NR	CLEAR	
0925		20.3	12.45×10	NR	CLEAR	



Employee-Owned Company
Well Development Form (Field Sheet)
Project Name and Number:
Well Number and Location: AREA P, WELL 60 104
Development Crew: J. PENDLEYON, W. STONETZ Driller (if applicable): N/A
Water Levels/Time: Initial: 14.47 BTOC Pumping: Final: 18 BTOC
Total Well Depth: Initial: 35.47 Final:
Date and Time: Begin: $3/2/94$ 0905 Completed: $3/2/94$ R30 Development: Method(s): $2^{\prime\prime}$ SUBMERSIBLE PUMP (REDIFLO 2)
Development: Method(s): 2" SUBMERSIBLE PUMP (REDIFLO 2)

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Total Quantity of Water Removed: ______ gais

Date/Time and Pump Setting	Discharge Rate* and Measurement Method	Temp (°C)	Specific Conductivity (umhos/cm)	pH (Standard Units)	Turbidity	Remarks (Including Sand Production)
Setting 3/2/94 0965 1210 1220 1225 1227	~ Zgelfard ~ Zgelfard ~ Zgelfunn ~ Zgelfunn	62.3 60.5 62.1 62.7 62.3	(umhos/cm) 4.32 ×100 4.32 ×100 4.32 ×100 4.31 ×100 4.25 ×100		P. CLOUDY CLEAR CLEAR II CLEAR	·
L	l]	<u> </u>		

*gallons per minute or bailer capacity

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mployee-Owned Company
Well Development Form
(Field Sheet) _
Project Name and Number: <u>LAAP FIVE - YEAR REVIEW</u>
Well Number and Location: AREA P, WELL GOIOS
Development Crew: <u>J. PENDLETON C. Formula</u> Driller (if applicable): <u>NA</u>
Water Levels/Time: Initial: 17.16 BTOC 1620 Pumping: Final: HE 25 Broc
Total Well Depth: Initial: 56,20 Final:
Date and Time: Begin: 2/28/94 1640 Completed: 2/28/94 1735
Development: Method(s): <u>z"SUBMERSIBLE PUMP (REDIFLO Z)</u>

Total Quantity of Water Removed:

<u>160</u> gals

Discharge Rate* and Measurement Method	Temp (£G)	Specific Conductivity (umhos/cm)	pH (Standard Units)	Turbidity	Remarks (Including Sand Production)
DOMP OPERATIONS	76.0	4-16×100	6-8	CLEAR	GEEENISH-TELL
	7.57	4.96×100	පිරි-ఎ	CLEAR	
	64.6	4.35 ×100	6.89	CLEAIZ	
	65.D	4.19 x 100	6.94	CLEAR	
				•	
,					
-	Measurement Method	and Measurement Method PomP oreparento AT - Zas bachun 72.7 64.6	Discharge Rate* and Measurement MethodTemp (LG)*Specific Conductivity (umhos/cm)PomP oPEPArrado AT* ~ ZaS bachuan 76.0 4.16×100 AT* ~ ZaS bachuan 72.7 4.96×100 64.4 4.35×100	$\begin{array}{c c} and \\ Measurement \\ Method \end{array} \qquad Temp (LG)^{*} \begin{array}{c} Specific \\ Conductivity \\ (umhos/cm) \end{array} \qquad \begin{array}{c} pH \\ (Standard \\ Units) \end{array} \\ \hline \\ pomp operation \\ AT - Z_nS \ bit fum \\ \hline \\ 7L_nO \\ 4.16 \times 100 \\ \hline \\ 4.96 \times 100 \\ \hline \\ 6.88 \\ \hline \\ 64.4 \end{array} \\ \begin{array}{c} c \\ 4.35 \times 100 \\ \hline \\ 6.89 \\ \hline \\ \end{array} \\ \end{array}$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $

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(Field Sheet)
oject Name and Number: LAAP FIVE - YEAR REVIEW
ell Number and Location: <u>AREA P</u> , WELL GO 100
evelopment Crew: C. Formana, J. PENDLETON Driller (if applicable): NA
ater Levels/Time: Initial: 16.49 Broc 1630 Pumping: Final: ~57 Broc
tal Well Depth: Initial: <u>64.44</u> Final:
ate and Time: Begin: 2/28/94 1715 Completed: 3/1/94 1715 1630
evelopment: Method(s): <u>2"SUBMERSIBLE RUMP (REDIFLO Z)</u>

Total Quantity of Water Removed:

95 gals

Date/Time and Pump Setting						
	Discharge Rate* and Measurement Method	Temp (°C)	Specific Conductivity (umhos/cm)	pH (Standard Units)	Turbidity	Remarks (Including Sand Production)
2/28/94 1721	AJUNT OPERATING AT ~ 1.5 GAL/MIN	64.9	3.21 X1000	NR.	CLEATZ	GREENISH/SELLA
1746		56.4				
5/1/94_						
0905	1.5 GAL from	54.2	4.5× 100	9.07	CLEAR	
0925	1.56Aclum	62.5	7.35×100	NOT FUNICITION	L CLEAR	GREENISH YELL
1620	1.0 Green	42.4	7.44100	ų	ઘ	TINT TO HEC
1630	1.0 6AL mm	62.0	7.6 4100	Ľ١	ι	` L
Five h	ELL VOLUMES	were n	OT RELO	NERED	Row 4	ELL
wer	WAS RECOVERI	16 -10 SC	owly to	OBTAIN	S TH	ES
	VOLUME OF					
	WELL.					
			1			

*gallons per minute or bailer capacity



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ployee-Owned Company
Well Development Form
(Field Sheet)
roject Name and Number: <u>LAAP FIVE - YEAR REVIEW</u>
Vell Number and Location: AREA P, WELL 60109
Development Crew: W. STONER, C. FOUTHUA Driller (if applicable): N/A
Vater Levels/Time: Initial: 19.1 BTOC 0854 Pumping: Final: Final:
otal Well Depth: Initial: Final:
Date and Time: Begin: 2/25/94 1400 Completed: 2/28/94 1320
Development: Method(s): 2" SUBMERSIBLE PUMP (REDIFLO Z)
Total Quantity of Water Removed: gals

Date/Time and Pump Setting						
	Discharge Rate* and Measurement Method	Temp (°C)	Specific Conductivity (umhos/cm)	pH (Standard Units)	Turbidity	Remarks (Including Sand Production)
2/25/14 2/28/44 0854 1248 1320		52 67 67.8 68.0	0.10×10 0.10×10 0.10×10 0.10×10	4.1 6.09 6.08	P. TURBID II II P. TURBID CLEAIZ	>



mpioyee-Owned Company
Well Development Form
(Field Sheet)
(FIEIG SI IEEI)
_
Project Name and Number: LAAP FIVE - YEAR REVIEW
Well Number and Location: AREA P, WELL 60110
Development Crown T Dr. 10 1 The All C T de LA Driller (if appliable); 1/4
Development Crew: J. PENDLETON, C. FOUTANA Driller (if applicable): N/4
Water Levels/Time: Initial: <u>25.83</u> Pumping: Final: <u>32 Broc</u>
Total Well Depth: Initial: <u>86.09 Broc</u> Final:
· · · · · · · · · · · · · · · · · · ·
Date and Time: Begin: 2/28/94 0927 Completed: 2/28/94 1232
Development: Method(s): 2" SUBMERSIBLE PUMP SET AT ~45 BTOC

gals

155

Total Quantity of Water Removed:

-

Date/Time and Pump Setting						
	Discharge Rate* and Measurement Method	Temp (°C)	Specific Conductivity (umhos/cm)	pH (Standard Units)	Turbidity	Remarks (Including Sand Production)
2/28/94-0927	~ ZGAL/MIN	54.4	04110	6.55	P. CLOUDY	
1020	~36gi/min	71°F	0.1 ×10	6.50	n 6	
110		68	0,1×10	6,48	1 1	
1232		ω7.φ	0.1 X10	6.47	CLEATZ	
DEEP	WELL IN LO ER READWG	WER 7	ERRACE	SPARTA	SAND	AQUIFER
DEEP	WELL IN LO	WER 7	ERRACE	STAILTA	5441)	4-QUIFER
PARAMET	ER READING	p consis	TENT	72492006	FOUT-F	URGM16
		<u>l</u>	1	L	<u> </u>	<u> </u>

*gallons per minute or bailer capacity

SAMPLING FORM



Employee-Owned Company
Sampling Form
(Field Sheet)
Project Name and Number: LAAP FIVE - YEAR REVIEW
Sampling Crew: CHEIS FONTANA, JOHN PENDLETON
Sampling Point Number: 60009
Sampling Location: MONITOR WELL 60009
Sample Type: S GW SW Soil SED Other:
Date and Time Sample Collected: 2/25/94 12:17
Weather Conditions: CLEAR & SUNNY, STRONG WIND ~ 10-15 mph FROM NORTH
Purging Information (if applicable):
Method: SUBMERSIBLE AND BAILING (LARGE % OF FINES IN 420)
Quantity of Water Purged: 39 GALLANS
Disposition of Purge Water: H20 UERY TURBID AT BELIANIALS OF THE
PURGING PROCESS THEN BECAME ALMOST CLEAR
Date and Time of Purging: Start: $\frac{2}{24/94}$ 1610 End: $\frac{2}{25/94}$ 1140
Comments: H2O STILL PATETLY CLOUDY AT THE GUD OF PURGIAG
Groundwater:
Date and Time Collected: 2/25/94 1217
Sampling Depth: 18' 10 Borrow
Water Level: ~ 18' 870C
Sampling Method/Equipment: <u>Borrow</u> FILLING TEFLON BAILER Field Measurements: pHO10400 Temp: 68° Cond: 0.10×10 Alkalinity:
Date and Time Filtered (if applicable):
Comments: 420 STILL W: 40 OF FILIES SUSPENDED
IN SOLN. ZINSATE BLANK TAKEN OF THIS WELL
Surface Water:
Date and Time Collected:
Collection Method:
Date and Time Filtered (if applicable): Cond: Turbidity:
Comments:
\
Soils/Sediment Sampling:
Date and Time Collected:
Sampling Depth:
Comments:

a. -



Sampling Form (Field Sheet)
Project Name and Number: LAAP FIVE - YEAR REVIEW
Sampling Crew: CHELS FOUTHUR, JOHN PENDLETON
Sampling Point Number: 60012, 5A1C01
Sampling Location: MONITOR WELL GOOIZ
Sample Type: 🛛 GW 🗌 SW 🗌 Soil 🗌 SED 🗍 Other
Date and Time Sample Collected: FEB. 24, 1994 1255
Weather Conditions: SUMY & CLEAR, TEMP. HIGH 40'S, CALM
Purging Information (if applicable):
Method: BAILING WITH BOTTOM FILLING BAILER
Quantity of Water Purged: <u>APPEOX</u> , 50 GALLONS Disposition of Purge Water: <u>PARTLY TURBID, SMALL PERCENT 6F</u>
RED CLAY SUSPENDED IN SOLUTION.
Date and Time of Purging: Start: <u>Z/23/94</u> 1650 End: <u>Z/24/94</u> 1245 Comments: <u>BAILING USED INITIALLY TO REMOVE SUSPENDED AND</u>
SETTLED CLAY PARTICLES #30 BECOMES CLEAR WITH REMOVALI
Groundwater: Date and Time Collected: <u>FEB. 24, 1994</u> 1255 Sampling Depth: <u>Zo' TO BOTTOM 1</u> Water Level: <u>19.76' BTOL</u> Sampling Method/Equipment: <u>DISPOSABLE BAILER</u>
Field Measurements: pH <u>6.14</u> Temp: <u>62</u> Cond: <u>1.2.×</u> Alkalinity: Date and Time Filtered (if applicable): <u>NA</u> Comments: <u>Restance BLACK FACEN AT THIS SEC</u>
PRIOR_ TO SAMPLING
Surface Water:
Date and Time Collected:
Collection Method: Date and Time Filtered (if applicable)
Field Measurements: pH Temp: Cond: Turbidity:
Comments:
Soils/Sediment Sampling:
Date and Time Collected:
Sampling Depth:Sampling Method:
Comments:

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White: File Pink: Field Manager Yellow: Supervisory Geologist Goldenrod: Field Book



Sampling Form (Field Sheet)
Project Name and Number: LAAP FIVE YEAR REVIEW
Sampling Crew: CHIZIS FONTANA, JOHN PENDLETON
Sampling Point Number: 60014, 541C01
Sampling Location: MONITOR WELL 60014
Sample Type: 🛛 GW 🗌 SW 🗌 Soil 🗌 SED 🗍 Other
Date and Time Sample Collected: FEB. 24, 1994
Weather Conditions: <u>SUNNY & CLEAR, TEMP.</u> IN HIGH SOS
Purging Information (if applicable): Method: 2" SUBMERSIBLE Pump
Disposition of Purge Water: <u>PARTLY TURBID</u> WITH LARGE PERCENT 6F SUSPENDED SOLIDS
Date and Time of Purging: Start: 2/24/94 0920 End: 2/24/94 1430 Comments: WELL IS VERY SLOW RECHARGER, UNABLE TO RECOVER 5 TIMES THE WELL VOLUME.
Groundwater:
Date and Time Collected: FEB. 24, 1994 Sampling Depth: APPESC. 15 TO BOTTOM Water Level: 14.86 ' BTOC Sampling Method/Equipment: DISPOSABLE BAILER Field Measurements: pH 6.45 Temp: SO Cond: III Alkalinity: Image: So Comments: Image: So Samplicable): Image: So
Surface Water:
Date and Time Collected:
Date and Time Filtered (if applicable) Field Measurements: pH Temp: Cond: Turbidity: Comments:
Soils/Sediment Sampling:
Date and Time Collected:
Sampling Depth: Sampling Method:
Comments:

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	Sampling Form
	(Field Sheet)
Project Name and Number: LAA	P FIVE - YEAR REVIEW
	4, J. PENDLETON
	······································
	<u>8</u>
Sampling Location: Mod 170R C	well 60068
	W Soil SED Other:
Date and Time Sample Collected:	3/1/94 1648
Weather Conditions: RANNING	WITH TEMPERATURE IN LOW SOS, WIND
	Suph From North
Purging Information (if applicable):	
Quantity of Water Purged:	USED to PURGE WELL
	INITIALY VERY TURBID HOWEVER
Hzo DID CLEA	HR UP DURING PURGING PROCESS
	ent: 2/28/94 0932 End: 3/1/94 1645
Comments:	
Water Level: ~16 B Sampling Method/Equipment: Field Measurements: pH_7.	BOTTOM FILLING TEFLON BAILER. B Temp: <u>GI°F</u> Cond: 3.LZX 10 Alkalinity: <u>NIZ</u> icable): <u>N/A</u>
Surface Water.	
Collection Method:	
Date and Time Filtered (if appli	
	Temp: Cond: Turbidity:
Comments:	
	No contraction of the second s
Soils/Sediment Sampling:	~~
Date and Time Collected:	
Compline Death.	
Sampling Depth:	
Sampling Method:	
Sampling Method:	() () ()

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Sampling Form (Field Sheet)
Project Name and Number: <u>LAAP FIVE YEAR REVIEW</u> Sampling Crew: <u>Chr.s FoutAwA</u> , John PENDLETON
Sampling Point Number: 600 83, SAICOL
Sampling Location:
Sample Type: X GW SW Soil SED Other
Weather Conditions: <u>CLEAR & SUNINY</u> , LIGHT WIND
Purging Information (if applicable):
Method: <u>2"</u> SUBMERSIBLE PUMP Quantity of Water Purged: <u>Approx. SS GALLOUS PURGED</u> Disposition of Purge Water: <u>PARTLY TURBID</u> , <u>SmAUL PERCENT OF PED (LAY SUPERDED</u> <u>IN SOLUTION</u> . INTIAL PUMP HAD CLEAR WATER Date and Time of Purging: Start: <u>2-24.94</u> <u>11'132</u> End: <u>2-25-94</u> 13'SO Comments: <u>WELL HAD A SLOW RECLARGE TIME</u>
Groundwater: Date and Time Collected: $\frac{2}{2} - \frac{24}{2} - 94 = \frac{2}{2} - $
Sampling Depth: 19.8 TO BOTTOM OF WELL Water Level: 19.76 BTOL Sampling Method/Equipment: $2''$ SubmEqs, SLE PLMP Field Measurements: pH 5.36 Temp: $55.4'$ Cond: $01400m/06$ Alkalinity: NR Date and Time Filtered (if applicable): N(A Comments: MS/MSD TAKEN FROM THIS WELL ON $2/25/24$, 6
LITERS OF SAMPLE (TOTAL) TALEN FROM WELL
Date and Time Collected: Collection Method: Date and Time Filtered (if applicable) Field Measurements: pH Temp: Cond: Turbidity: Comments:
Soils/Sediment Sampling:
Date and Time Collected:

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	• •
	(Field Sheet)
Project N	ame and Number: LAAP FIDE YEAR REVIEW
	Crew: OHN PENDLETON, CLP.S FONTANA
	Point Number: <u>60084</u> , SAICOL
Sampling	Location: MONITOR NELL GOOBY
Sample T	ype: 🗗 GW 🔲 SW 🔲 Soil- 🗌 SED 🔲 Other
•	Time Sample Collected: 2-25-94 13:10
	Conditions: <u>CLEAR & SUNNY</u> , STRUNG WIND 10-15 MPh FRM N
Weather	Conditions: <u>CLEAR & SUNNY</u> , STRUNG WIND TO IS MITH FRAM N
Puraina	Information (if applicable):
• •	sthod: 2" SUBMERSIBLE RUMP
Ou	antity of Water Purged: ~35 GALLONS RECOVERED FROM WELL
Dis	sposition of Purge Water: WATER IS CLEAR
Da	te and Time of Purging: Start: <u>2-24-94</u> 17:20 End: <u>2125/94</u> 0657 Imments: WELL IS A VELAY SLOW RECLARGER
0	
Da Sa Wa	te and Time Collected: $2 - 25 - 94$ 13'10 mpling Depth: $\frac{21.6}{19.75}$ BTOC
Sa Wa Sa Fie Da Co Surface Da Co Da Fie	te and Time Collected: <u>2-25-94</u> 13'10 mpling Depth: <u>21.6</u> TO BOTTOM OF WELL ater Level: <u>19.75</u> BTOL mpling Method/Equipment: <u>Bottom FLUING TEFLON BALLER</u> He Measurements: pH <u>5.74</u> Temp: <u>5.28</u> Cond: <u>0.10/10/04</u> S Alkalinity: <u>N/IC</u> te and Time Filtered (if applicable): <u>N/A</u> mments: <u>DOPULATE SAMPLE TAKEN AT THIS</u> WELL, <u>4 LITER</u> (TOTAL) OF SAMPLE COLLECTED FROM WELL. Water: te and Time Collected: illection Method: te and Time Filtered (if applicable) te mp: Cond: Temp: Cond: Turbidity:
Da Sa Via Sa Fie Da Co Surface Da Co Da Fie	te and Time Collected: $2 \cdot 25 \cdot 94'$ 13'10 mpling Depth: $\frac{21.6}{19.75}$ To Barrow OF WELL ater Level: 19.75 BTOL mpling Method/Equipment: Barrow FILLING TEFLON BALLER hd Measurements: pH $51.74'$ Temp: 528 Cond: 0.10×10^{-10} Alkalinity: N/IC te and Time Filtered (if applicable): N/A mmments: DOPLICATE SAMPLE TAKEN AT THIS WELL, 4 LITER (TOTAL) OF SAMPLE COLLECTED FROM WELL. Water: te and Time Collected: blection Method: te and Time Filtered (if applicable)
Da Sa Via Sa Fie Da Co Surface Da Co Da Fie	te and Time Collected: <u>2-25-94</u> 13'10 mpling Depth: <u>21.6</u> TO BOTTOM OF WELL ater Level: <u>19.75</u> BTOL mpling Method/Equipment: <u>Bottom FLUING TEFLON BALLER</u> He Measurements: pH <u>5.74</u> Temp: <u>5.28</u> Cond: <u>0.10/10/04</u> S Alkalinity: <u>N/IC</u> te and Time Filtered (if applicable): <u>N/A</u> mments: <u>DOPULATE SAMPLE TAKEN AT THIS</u> WELL, <u>4 LITER</u> (TOTAL) OF SAMPLE COLLECTED FROM WELL. Water: te and Time Collected: illection Method: te and Time Filtered (if applicable) te mp: Cond: Temp: Cond: Turbidity:
Da Sa Wa Sa Fie Da Co Da Co Da Fie Co	te and Time Collected: <u>2-25-94</u> 13'10 mpling Depth: <u>21.6</u> TO BOTTOM OF WELL ater Level: <u>19.75</u> BTOL mpling Method/Equipment: <u>Bottom FLUING TEFLON BALLER</u> He Measurements: pH <u>5.74</u> Temp: <u>5.28</u> Cond: <u>0.10/10/04</u> S Alkalinity: <u>N/IC</u> te and Time Filtered (if applicable): <u>N/A</u> mments: <u>DOPULATE SAMPLE TAKEN AT THIS</u> WELL, <u>4 LITER</u> (TOTAL) OF SAMPLE COLLECTED FROM WELL. Water: te and Time Collected: illection Method: te and Time Filtered (if applicable) te mp: Cond: Temp: Cond: Turbidity:
Da Sa Wa Sa Fie Da Co Da Co Da Fie Co Soils/Se Da	te and Time Collected: <u>2-25-94</u> 13:10 mpling Depth: <u>21.6</u> TO BETTEM OF WELL mpling Method/Equipment: <u>BETTEM OF WELL</u> Measurements: pH <u>5:74</u> Temp: <u>5:28</u> Cond: <u>0.10/10 und/5</u> Alkalinity: <u>N/12</u> te and Time Filtered (if applicable): <u>N/A</u> mments: <u>DSPLICATE SAMPLE TAKEN AT THIS WELL</u> , <u>4 LITER</u> (TOTAL) OF SAMPLE COLLECTED FROM WELL. Water: te and Time Filtered (if applicable) te and Time Collected: <u>1000000000000000000000000000000000000</u>
Da Sa Wa Sa Fie Da Co Da Goils/Sea Da Soils/Sea Da Sa	te and Time Collected: <u>2-25-94</u> 13:10 mpling Depth: <u>21.6</u> TO BETTEM OF WELL ater Level: <u>19.75</u> BTOL mpling Method/Equipment: <u>Berrow</u> Fillindo <u>TEFLON</u> <u>BALLER</u> ed Measurements: pH <u>5:74</u> Temp: <u>5:28</u> Cond: <u>0.107.00</u> 445 Alkalinity: <u>N/12</u> te and Time Filtered (if applicable): <u>N/A</u> mments: <u>DSPLICATE SAMPLE TAKEN AT THIS</u> <u>WELL</u> , <u>4 LITER</u> (TOTAL) OF <u>SAMPLE</u> COLLECTED FROM <u>WELL</u> . Water: te and Time Filtered (if applicable) te and Time Filtered (if applicable) He d Measurements: pH <u>Temp</u> : <u>Cond</u> : <u>Turbidity</u> : <u>mments</u> diment Sampling: te and Time Collected: <u>Mathematication</u>
Da Sa Wa Sa Fie Da Co Da Co Da Fie Co Da Soils/Seu Da Sa Sa	te and Time Collected: 2-25-94 13'10 mpling Depth: <u>21.6</u> TO Barrow of Well ater Level: <u>19.75</u> BTOL mpling Method/Equipment: Borrow Filled of TEFLON BALLER Measurements: pH <u>51.74</u> Temp: <u>5.28</u> Cond: <u>0.1010000000</u> Alkalinity: <u>N/IZ</u> te and Time Filtered (if applicable): <u>N/A</u> mments: <u>DOPLICATE SAMPLE TAKEN AT THIS WELL</u> , <u>4 LITER</u> (TOTAL) OF SAMPLE COLLECTED FROM WELL. Water: te and Time Collected: <u>Network</u> Measurements: pH <u>Temp:</u> Cond: <u>Turbidity:</u> mments: <u>Difference</u> diment Sampling: te and Time Collected: <u>Measurements:</u> <u>Difference</u> mpling Depth: <u>mments</u> mpling Method: <u>Samples</u> <u>Collected</u> : <u>Samples</u> <u>Cond</u> <u>Cond</u> <u>Cond</u> <u>Measurements</u> <u>Cond</u> <u>Measurements</u> <u>Cond</u> <u>C</u>
Da Sa Wa Sa Fie Da Co Da Co Da Fie Co Da Soils/Seu Da Sa Sa	te and Time Collected: <u>2-25-94</u> 13:10 mpling Depth: <u>21.6</u> TO BETTEM OF WELL ater Level: <u>19.75</u> BTOL mpling Method/Equipment: <u>Berrow</u> Fillindo <u>TEFLON</u> <u>BALLER</u> ed Measurements: pH <u>5:74</u> Temp: <u>5:28</u> Cond: <u>0.107.00</u> 445 Alkalinity: <u>N/12</u> te and Time Filtered (if applicable): <u>N/A</u> mments: <u>DSPLICATE SAMPLE TAKEN AT THIS</u> <u>WELL</u> , <u>4 LITER</u> (TOTAL) OF <u>SAMPLE</u> COLLECTED FROM <u>WELL</u> . Water: te and Time Filtered (if applicable) te and Time Filtered (if applicable) He d Measurements: pH <u>Temp</u> : <u>Cond</u> : <u>Turbidity</u> : <u>mments</u> diment Sampling: te and Time Collected: <u>Mathematication</u>

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Sampling Form		
(Field Sheet)		
oject Name and Number: <u>LAAP FIVE - YEAR REVIEW</u>	-	
ampling Crew: <u>C. Forthand</u> , W. Stower, John F	_	
ampling Point Number: 60085		
ampling Location: MONITOR WELL 60085		
	r:	
ate and Time Sample Collected: $3/3/94$ 0955	·	
the and time sample conected. 373717038		
eather Conditions: SUNNY WITH TEMPERATURE IN h	HGH BOS, CAUM	
urging Information (if applicable):		
Method: 2" SUBMERSIBLE DUMP (REDIFLO 2))	
Quantity of Water Purged: <u>53</u> GALLO45		
Disposition of Purge Water: H2 O CLEMIZ		
Date and Time of Purging: Start: $3/2/94$ 1730 End: $3/2$	3/94 0931	
Comments:	•	
	·····	
roundwater:		
Date and Time Collected: 3/3/94 0955		
Date and Time Collected: 3/3/94 0955 Sampling Depth: 20 +0 Borrow OF WELL		
Date and Time Collected: $3/3/94$ 0955 Sampling Depth: 20' +0 Bottom OF WELL Water Level: $-19'$ BTOC	······································	
Date and Time Collected: 3/3/94 0955 Sampling Depth: 20 70 Borrow OF WELL Water Level: ~ 19 BTOC Sampling Method/Equipment: Borrow Filler TEFLON BA	HLER	
Date and Time Collected: 3/3/94 0955 Sampling Depth: 20' to Bottom OF WELL Water Level: <u>~ 19' BTOC</u> Sampling Method/Equipment: Bottom Filler/6 TEFLON BA Field Measurements: pH_NR_ Temp: 67° F Cond: 10.07×10 A		
Date and Time Collected: $3/3/94$ 0955 Sampling Depth: 20' +0 Bottom OF WELL Water Level: $-19'$ BTOC Sampling Method/Equipment: Bottom Filler/6 TEFLOW BA Field Measurements: pH_NR_ Temp: $67^{\circ}F$ Cond: 10.07×10 A Date and Time Filtered (if applicable): $N/4$		
Date and Time Collected: 3/3/94 0955 Sampling Depth: 20' to Bottom OF WELL Water Level: ~ 19' BTOC Sampling Method/Equipment: Bottom Filler/6 TEFLON BA Field Measurements: pH_NR_ Temp: 67° F Cond: 10.07×10 A		
Date and Time Collected: $3/3/94$ 0955 Sampling Depth: 20 +0 Bottom OF WELL Water Level: $-19'$ BTOC Sampling Method/Equipment: Bottom Filler/6 TEFLOW BA Field Measurements: pH_NR_ Temp: 67° F Cond: 10.07×10 A Date and Time Filtered (if applicable): $N/4$		
Date and Time Collected: $3/3/94$ 0955 Sampling Depth: 20' +0 Bottom OF WELL Water Level: $-19' BTOC$ Sampling Method/Equipment: Bottom Filler/6 TEFLOW BA Field Measurements: pH_NR_ Temp: 67° F Cond: 10.07×10 A Date and Time Filtered (if applicable): $N/4$		
Date and Time Collected: $3/3/94$ 0955 Sampling Depth: <u>20' +0</u> <u>Bottom</u> <u>off</u> <u>Wett</u> Water Level: <u>~19' Btoc</u> Sampling Method/Equipment: <u>Bottom</u> <u>Filler/Br</u> Sampling Method/Equipment: <u>Bottom</u> <u>Filler/Br</u> Sampling Method/Equipment: <u>Bottom</u> <u>Filler/Br</u> Date and Time Filtered (if applicable): <u>N/A</u> Comments: <u>Sampling Condection</u>	HLER Ikalinity: <u>NR</u>	
Date and Time Collected: <u>3/3/94</u> 0955 Sampling Depth: <u>20' +0</u> <u>Bettom</u> <u>of</u> <u>Wetto</u> Water Level: <u>~19' Broc</u> Sampling Method/Equipment: <u>Betrom</u> <u>Fillen/6</u> <u>Teflon/ Ba</u> Field Measurements: pH_ <u>NR</u> Temp: <u>67° F</u> Cond: <u>10.07×10</u> <u>A</u> Date and Time Filtered (if applicable): <u>W</u> [<u>A</u> Comments: <u>Date and Time Collected</u> : <u></u>	HLER Ikalinity: <u>NR</u>	
Date and Time Collected: <u>3/3/94</u> 0955 Sampling Depth: <u>20' +0</u> <u>Bettom</u> <u>off</u> <u>Wetto</u> Water Level: <u>~19' BTOC</u> Sampling Method/Equipment: <u>Bettom</u> <u>Fillen/6</u> <u>TEFLON/ BA</u> Field Measurements: pH_ <u>NR</u> Temp: <u>67° F</u> Cond: <u>10.07×10</u> <u>A</u> Date and Time Filtered (if applicable): <u>W</u> [<u>A</u> Comments: <u>Date and Time Collected</u> : <u>Collection Method</u>	ucez Ikalinity: <u>NR</u>	
Date and Time Collected: <u>3/3/94</u> 0955 Sampling Depth: <u>20' +0</u> <u>Botrom</u> <u>of</u> <u>Wett</u> Water Level: <u>~ 19' Broc</u> Sampling Method/Equipment: <u>Botrom</u> <u>Fitur/6 Tertor/ Br</u> Field Measurements: pH_ <u>17</u> Temp: <u>67° F</u> Cond: <u>10.07×10</u> <u>P</u> Date and Time Filtered (if applicable): <u>W1/4</u> Comments: Date and Time Collected: Collection Methods: Date and Time Filtered (if applicable):	Ikalinity: <u>NR</u>	
Date and Time Collected: 3/3/94 0955 Sampling Depth: 20' +0 Botrow of Wett Water Level:	Ikalinity: <u>NR</u>	
Date and Time Collected: <u>3/3/94</u> 0955 Sampling Depth: <u>20' to Bottom of Wett</u> Water Level: <u>~ 19' Btoc</u> Sampling Method/Equipment: <u>Bottom Fitual6 Tertod Ba</u> Field Measurements: pH <u>~ 17</u> Temp: <u>67° F</u> Cond: <u>10.07×10</u> A Date and Time Filtered (if applicable): <u>w/A</u> Comments: Date and Time Collected: Collection Methods: Date and Time Filtered (if applicable):	Ikalinity: <u>NR</u>	
Date and Time Collected: 3/3/94 0955 Sampling Depth: 20' to Botrow of Wett Water Level: ~ 19' BTOC Sampling Method/Equipment: Botrow Fitue/6 Terlow BA Field Measurements: pH	ucer Ikalinity: <u>NR</u>	
Date and Time Collected: 3/3/94 0955 Sampling Depth: 20 to Bettrom 0F Wett Water Level: ~ 19' BTOC Sampling Method/Equipment: Bettrom Filler Bettrom Fettod Battrom Sampling Method/Equipment: Bettrom Filler Cond: 10.07×10 / Sampling Method/Equipments: pH AIR Temp: Cond: 10.07×10 / Date and Time Filtered (if applicable):	ucer Ikalinity: <u>NR</u>	
Date and Time Collected: 3/3/94 0955 Sampling Depth: 20 70 Bettom 0F Wett Water Level: ~ 19' BTOC Sampling Method/Equipment: Bettom Fillen/6 TEFLON/ Battom Sampling Method/Equipment: Bettom Fillen/6 TEFLON/ Battom Batom<	ucer Ikalinity: <u>NR</u>	
Date and Time Collected: 3/3/94 0955 Sampling Depth: 20 70 Botrom 0F Wetcl Water Level: ~ 19' Broc Sampling Method/Equipment: Botrom Field Measurements: ph Sampling Method/Equipment: Botrom Field Measurements: ph Date and Time Filtered (if applicable): M/4 Cond: 10,07×10 µ Date and Time Filtered (if applicable): M/4 Comments: 10,07×10 µ Date and Time Filtered (if applicable): M/4 Comments: 10,07×10 µ Date and Time Filtered (if applicable): Source Water: Source Water: 10,07×10 µ Date and Time Filtered (if applicable): Source Water: Source Water: Source Water: Date and Time Filtered (if applicable): Temp: Cond: Cond: Source Water: Date and Time Filtered (if applicable): Temp: Cond: Source Water: Source Water: Date and Time Filtered (if applicable): Temp: Cond: Source Water: Source Water: Date and Time Collected:	ucer Ikalinity: <u>NR</u>	
Date and Time Collected: 3/3/94 0955 Sampling Depth: 20' +0 30 + 70 + 0 Water Level: ~ 19' & B + 0 C Sampling Method/Equipment: Be + 70 + 0 Sampling Method/Equipment: Picura/6 + 72 + 0 Date and Time Filtered (if applicable): M/4 Comments:	ucer Ikalinity: <u>NR</u>	
Date and Time Collected: 3/3/94 0955 Sampling Depth: 20 70 Bottom 0F Weill Water Level: ~ 19 Bto C Sampling Method/Equipment: Battom Filled Veille Battom Filled Veille Battom Battom Battom Filled Veille Battom Filled Veille Battom Battom	ucer Ikalinity: <u>NR</u>	
Date and Time Collected: 3/3/94 0955 Sampling Depth: 20' +0 30 + 70 + 0 Water Level: ~ 19' & B + 0 C Sampling Method/Equipment: Be + 70 + 0 Sampling Method/Equipment: Picura/6 + 72 + 0 Date and Time Filtered (if applicable): M/4 Comments:	ucer Ikalinity: <u>NR</u>	
Date and Time Collected: 3/3/94 0955 Sampling Depth: 20' +0 B077044 0F Water Level: 19' 870C Sampling Method/Equipment: Bo77044 Filled TEFLON/ BA Field Measurements: pH_NR Temp: G7°F Cond: 10.07×10 A Date and Time Filtered (if applicable): N/A M/A Comments:	ucer Ikalinity: <u>NR</u>	

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	Sampling Form
	(Field Sheet)
ject Name and Number:	AP FINE- YEAR IZEVIEW
anling Crew T. P. dist	in C. Fontena, W. Stoucr
npling Point Number: <u>60</u>	
	21NG WELL 60104
· · · ·	SW Soil SED Other:
e and Time Sample Collected: _	3/2/94 12:40
	IT W. TEMPERATURE IN MID. 405, WIND
Fean N	orth up to ~15mph.
ging Information (if applicable)	
Method: 2" SUBMER	SIBLE GRUNDEDS PUMP (REDIFLO Z)
Quantity of Water Purged:	~100 GALLONS
Disposition of Purge Water:_	CLEAR W, GREENSH YELLOW COLOR
Data and Time of Durning	Start: 3/2/94 0905 End: 3/2/94 1230
Comments (J=1)	REED QUICKLY & RECHARGE WAS PROGABLY
BEST OF AREA	•
Date and Time Collected: Sampling Depth:18 Water Level:76	BTOL TO BOTTOM BTOL
	t Borrow FILLING TEFLON BAILER
Field Measurements: pH	Temp: <u>62.3</u> Cond: <u>4.257/00</u> Alkalinity:
Date and Time Filtered (if ap	
	ABSERVED TO HAVE A GREEKISH YELLOW
COLOIZ.	
· · · · ·	
rface Water:	
Date and Time Collected:	
Date and Time Filtered (if ap	plicable):
Field Measurements: pH	
Comments:	
<u></u>	
the Cardina and Compting	
ils/Sediment Sampling: Date and Time Collected	
Sampling Depth:	
ils/Sediment Sampling: Date and Time Collected: Sampling Depth: Sampling Method:	NA.
Comments:	



(Field Sheet)
Project Name and Number: LARP FIVE YEAR REVIEW
Sampling Crew: WAYNE STONER, JOHN PENDELTON, CLRIS FONTANA
Sampling Point Number: 60105, 5AICO(
Sampling Location: MONITORING WELL GO105
Sample Type: 🕅 GW 🗌 SW 🗌 Soil 🗌 SED 🔤 Other
Date and Time Sample Collected: 2-28-94 17:55
Weather Conditions: SUMLY ACLEAR
Purging Information (if applicable):
Method: 21 Submersible Rump
Quantity of Water Purged:
Disposition of Purge Water:YEllow: SL CLEAR FLuiD
Date and Time of Purging: Start: 2-28-94 16:40 End: 2-28-94 17:
Comments:
Date and Time Collected: 2-28-94 17:55 Sampling Depth: 25 FT TO BOTTOM OF WELL Water Level: 17.16 BTOC Sampling Method/Equipment: 01 306 ME2SIGE PLMP Field Measurements: pH 11.73? Temp: 564 Cond: 11 × 10 Alkalinity:
Date and Time Filtered (if applicable): N/A
Comments:
Surface Water:
Date and Time Collected:
Collection Method:
Date and Time Filtered (if applicable)
Field Measurements: pH Temp: Cond: Turbidity: _
Comments:
Soils/Sediment Sampling:
Date and Time Collected:
Sampling Depth:
Sampling Method:
Comments:

White: File Pink: Field Manager Yellow: Supervisory Geologist Goldenrod: Field Book



Sampling Form
(Field Sheet)
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Project Name and Number: LAAP FIVE-YEAR REVIEW
Sampling Crew: CHRIS FONTANA, JOHN PENDLETON
Sampling Point Number: 60106, SALCOL
Sampling Location: MONITORING WELL GOIDO
Sample Type: X GW Soil Soil SED Other:
Date and Time Sample Collected: $3/1/94$ 16:35
Weather Conditions: RANING WITH TEMPERATURES 14 LOW SO'S
WIND ~ 5 mply from Nextet
Purging Information (if applicable):
Method: 2" SUBMERSIBLE PUMP (GRUNDEDS REDIFICO 2)
Quantity of Water Purged: ~ 95 GALLONS
Disposition of Purge Water: CLEAR with GREE/ISH YELLOW TINT
Date and Time of Purging: Start: 2/28/94 1715 End: 3/1/94 1715 (630
Comments: WELL PURGED DASILY, RECHARGED OWNER, GREEVISH
YELLOW LOLDR OBSERVED DURING PURGING.
Groundwater:
Date and Time Collected: 3/1/94 16:35
Sampling Depth: ~57'BTOC
Water Level: <u>~56 BTOL</u> Sampling Method/Equipment: <u>Borrow</u> FULING TEELOW <u>BALLER</u>
Field Measurements: pH_NRTemp: _ <u>62 °F</u> Cond: <u>7.6xco</u> Alkalinity:
Date and Time Filtered (if applicable): <u>NA</u>
Comments: GREENISH YELLOW TINT OBSERVED THROUGHOUT PURGMUG
ACTUITY
Surface Water:
Date and Time Collected:
Date and Time Filtered (if applicable):Cond:Turbidity:
Comments:
Soils/Sediment Sampling: Date and Time Collected:
Soils/Sediment Sampling: Date and Time Collected:
Sampling Method:
Comments:

Science Applications International Corporation 1710 Goodridge Drive, McLean, Virginia 22102 White: File Pink: Field Manager Yellow: Supervisory Geologist Goldenrod: Field Book •

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Sampling Form
(Field Sheet)
Project Name and Number: <u>LAAP FIVE YEAR REVIEW</u>
Sampling Crew:WAYNE STONER, JOHN PENDELTON, CHRIS FOUTANA
Sampling Point Number: <u>66109</u> , SAIL of
Sampling Location: 56 MULLITORING WELL 60109
Sample Type: B GW - D SW D Soil D SED D Other
Date and Time Sample Collected: 2-28-94 1410
Weather Conditions: <u>CLEAR + Sunity</u>
Purging Information (if applicable):
Method: 2 <u>SubmERSIDLE</u>
Quantity of Water Purged:42 GAUses
Disposition of Purge Water:
Date and Time of Purging: Start: <u> </u>
Comments: <u>Slow RECLARGED WELL</u>
Groundwater:
Date and Time Collected: 2-28-94 14,10
Sampling Depth: 33 FEET
Water Level: <u>24.27 FEET</u> Sampling Method/Equipment: ∂^{II} Submers, WE PumP
Sampling Method/Equipment: <u>3¹¹ Submers, WE PumP</u> Field Measurements: pH <u>6.00</u> Temp: <u>60</u> Cond: <u>0.10116</u> Alkalinity: <u>N IC</u>
Date and Time Filtered (if applicable): N/A
Comments:
Surface Water:
Date and Time Collected:
Collection Method:
Date and Time Filtered (if applicable) Field Measurements: pH Temp: Cond: Turbidity: Comments:
Comments:
T/
Soils/Sediment Sampling:
Date and Time Collected:
Sampling Depth:
Sampling Method:
Comments:

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White: File Pink: Field Manager Yellow: Supervisory Geologist Goldenrod: Field Book



Sampling Form	
(Field Sheet)	
Project Name and Number: <u>LAAP FIVE YEAR REVIEW</u>	
Sampling Crew: WAYNE STONER, JOHN PENDELTON, CHENS FONTANA	<u> </u>
Sampling Point Number: <u>Gollo, SAICOL</u>	
Sampling Location: Mourtoe, AG AVELL 60/10	
Sample Type: 🖾 GW 🛛 – 🗔 SW – 🗔 Soil 🛛 SED – 🗔 Other	
Date and Time Sample Collected: 2-28-99 19:25	
Weather Conditions: CLEAR + SUNNY	•
Purging Information (if applicable):	
Method: <u>2" SUBMERSIBLE PUMP</u>	
Quantity of Water Purged: 155 GALLINS	· · · · · · · · · · · · · · · · · · ·
Disposition of Purge Water: PAPTY TURBID TO CLEAR	
Date and Time of Purging: Start: <u>2-28-94</u> , 0927 End: <u>2-28-9</u> Comments: <u>WATER RECOVERED</u> COULLY FROM WELL, RE	<u>4 1234-</u> GHARGE
VERY GOOD.	0447080
Groundwater:	
Date and Time Collected:	
Sampling Depth: 32 FT. TO Borrow OF WELL	
Water Level: 32.85 BTOC	
Sampling Method/Equipment:	
	alinity: <u>N.R</u>
Date and Time Filtered (if applicable):	PRINT
TO SAMPLE COLLECTION	
Surface Water:	
Date and Time Collected:	
Collection Method:	
Date and Time Filtered (if applicable)	r + 44.
	bidity:
Comments:	
Soils/Sediment Sampling:	
Date and Time Collected:	
Sampling Depth:	
Sampling Method:	<u> </u>
Comments:	

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White: File Pink: Field Manager Yellow: Supervisory Geologist Goldenrod: Field Book

DRILLING LOGS

DRILLING LOG

	ÓJECT Cation	Monitoring Well Installa tion DATE <u>30 Sep :79</u> LAAP DRILLERS <u>Smithson</u>				
DR		G <u>Smal</u> D	<u>1 Trailer Mounted</u> rill Rig	- BORE HOLE BH 9		
Ē	DEPTH	SAMPLE TYPE BLOWS PER 6 IN	DESCRIPTION		REMARKS	
			Yellow-Red Clay-Silt		WT=15.5' - 2 Oct TD=22 ft	
	5		Gray Sandy Silt and Re (Marbled appearance)	d Clay	-	,
	 		Red Clay, Moist		•	
	10		•			
			-			•
	15		Red-Orange Silty Sand			•

HSE-ES Form 78, 1 Jun 80

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Replaces USAEHA Form 95, 12 Aug 74, which will be used.

B-25

DRILLING LOG

2

PROJECT	Monitoring Well Installation	DATE	30 Sept 79
LOCATION	LAAP	DRILLERS	<u>Smithson</u>

DRILL RIG Small Trailer Mounted Drill Rig

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BORE HOLE

BH Q

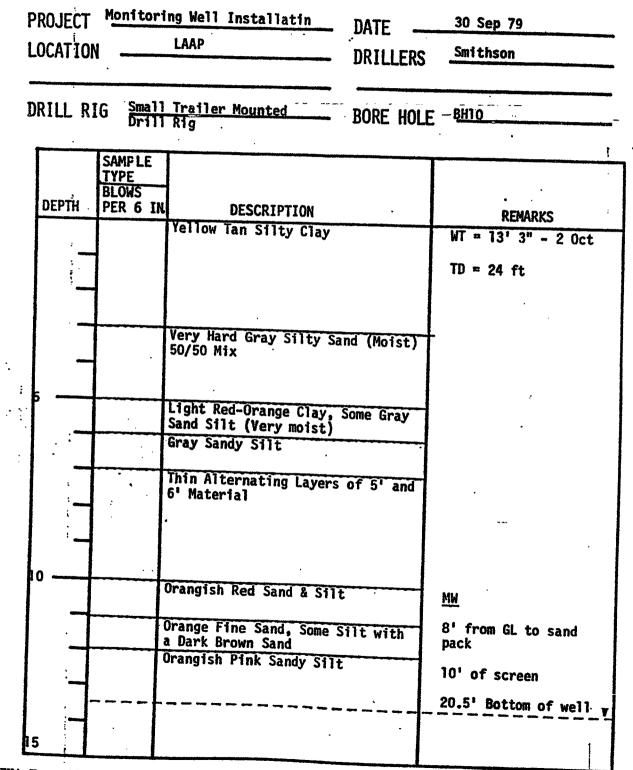
;

	SAMP LE TYPE		
DEPTH	BLOWS PER 6 IN	DESCRIPTION	REMARKS
15			
, 			
20		· .	<u>MW</u> 9' from GL to sand pack
			10' of screen 21.5' Bottom of well
			Total Depth 22 ft
* 		•	•
			1
	1	•	

HSHB-ES Form 78, 1 Jun 80 Replaces USAEHA Form 95, 12 Aug 74, which will be used.

B-26

DRILLING LOG



USAEHA Form 95, 12 Aug 74

B-27

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DRILLING LOG

PROJECT	Monitoring Well Installation	– DATE –––	30 Sep 79	
LOCATION	LAAP	- DRILLERS	Smithson	
DRILL RI	G Small Trailer Mounted	- BORE HOLE-		

	SAMP LE Type		
DEPTH	BLOWS PER 6 IN	DESCRIPTION	REMARKS
			•
		· · · ·	ł
20			
		•	
-	·	Red Clay, Dense	- <u>-</u>
-			Total Depth 24 ft
25			
			```
-			
:			

USAEHA Form 95, 12 Aug 74

B-28

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#### DRILLING LOG

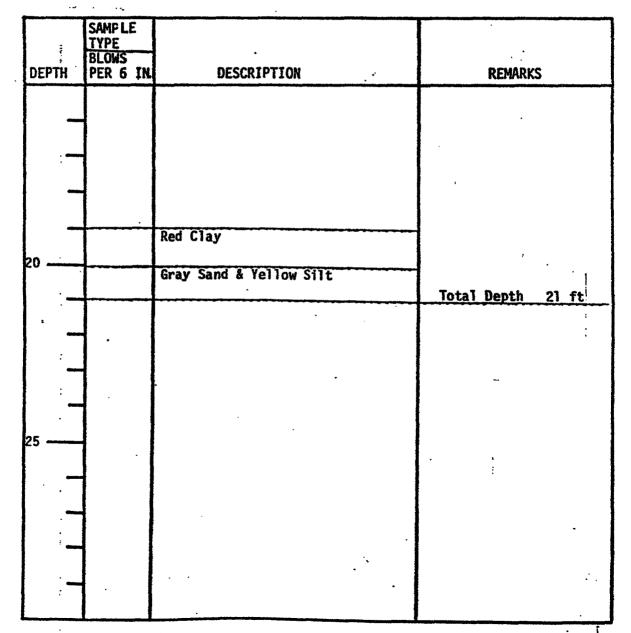
PROJECT Mor	itoring Well Install LAAP	lation DATE DRILLERS	1 Oct 79 Smithson
DRILL RIG	Small Trailer Mounte Drill Rig	edBORE HOLI	EBHII
TYP	WS 6 IN DESCRI		REMARKS
	Grass, Tan Sil	lt, Moist	WT = 14 ft TD = 21 ft
	Tan Silty Clay	y (Perched Water)	
	Very Fine Gra	y Sand & Silt	
		·	
			<u>HW</u> 5' from GL to sand pack 10' of screen
			20' Bottom of well

USAEHA Form 95, 12 Aug 74

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#### DRILLING LOG

PROJECT	Monitoring Well Installation	DATE	1 Oct 79
LOCATION	LAAP	DRILLERS	Smithson
DRIĪL RĪČ	Small Trailer Mounted	BORE HOLE	BH11



USAEHA Form 95, 12 Aug 74

B-30

#### DRILLING LOG

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	ROJECT DCATION	LAAD	ng Well Installation	DATE	1 Oct 79 Smithson
D	RILL RI	G <u>Small</u> Drill	Trailer Mounted Rig	BORE HOLE	<u>BH12</u>
	; DEPTH	SAMPLE TYPE BLOWS PER 6 IN	DESCRIPTION	Hada Lawy	REMARKS WT = 16' 6" - 2 Oct
			Red Clay, Part of Man	Made Levy	TD = 26 ft
	-				
	5		Dark Gray Silty Sand	· .	
	_		Tan Very Fine Sand &	5112	
	-				·
	10				MW 9.5' from GL to sand pack
	· · ·		Gray Silty Sand, Very	Dense	10' of screen 25' Bottom of well
	15		Gray Fine Sand, Littl Moist	e Fines	¢

USAEHA Form 95, 12 Aug 74

B-31

### DRILLING LOG

PROJECT Monitoring Well Installation OCATION LAAP			DATE Drillers	1 Oct 79 Smithson	
RILL RI	G Small	Trailer Mounted	BORE HOLE	<u>BH12</u>	
DEPTH	SAMPLE TYPE BLOWS PER 6 IN	DESCRIPTION	• .	REMARKS	
-	· · · · · · · · · · · · · · · · · · ·			<u>WT_16'_6"_ v</u>	
				· ·	
20	·	lan Medium Sand, Very	wet		
			-		
-	: •	Gray Silty Sand, Like	at 12'		
25				Total Depth 26'	

USAEHA Form 95, 12 Aug 74

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B-32

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# DRILLING LOG

	1.8.8.0	g Well Installation	DATE DRILLERS	30 Sep 79 Smithson	
DRILL RIG Small Trailer Mounted		Trailer Mounted	BORE HOLE	BH13	
DEPTH	SAMPLE TYPE BLOWS PER 6 IN	DESCRIPTION		REMARKS	
		Top Soil, Red Clay with Organics Tan Silty Clay		WT = 2' 6" - 2 Oct TD = 21 ft WT 2' 6" $-$	
5		Very Wet			
		White Sand Silt & Red ( (Marble cake appearance)	Clay e)		
				<u>MW</u> 2' to sand 10' of screen 20.5' Bottom of well	
-			. `		

USAEHA Form 95, 12 Aug 74

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## DRILLING LOG

PROJECT Location		g Well Installation	•	<u>30 Sep 79</u> Smithson
DRILL RI	G Small Drill	Trailer Mounted Rig	- BORE HOLE	BH13
DEPTH	SAMPLE TYPE BLOWS PER 6 IN	DESCRIPTION		REMARKS
		• • • •		
			-	
20		Hard Dense Red Clay		
	· · · ·			Total Depth 21'
				:
25				-
			` -	

USAEHA Form 95, 12 Aug 74

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### DRILLING LOG

PROJECT Location		g Well Installation	DATE DRILLERS	29 Sep 79 Smithson
DRILL RI	G Small Drill	Trailer Mounted Rig	BORE HOLE	B <u>H14</u>
; DEPTH	SAMPLE TYPE BLOWS PER 6 IN	DESCRIPTION		REMARKS
		Top Soil, Silty Loam Yellowish Silty Clay		WT = 14' - 9 Oct TD = 30 ft
		Light Red Clay		
5				
		Gray Fine Sandy Silt, Red Silty Clay (Marble appearance)	Yellow cake	
10		Bright Light Red Clay		<u>MW</u> 14' from GL to sand pack
		Light Pink Silty Fine	Sand	10' of screen 30' Bottom of well
T5 -	•••••	Very Moist		<u>WT 14'</u>

USAEHA Form 95, 12 Aug 74

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### DRILLING LOG

ROJECT OCATION	LAAP	•	DATE DRILLERS	Smithson
RILL RI	G <u>Small Tr</u> Drill Ri	ailer Mounted	BORE HOLE	BH14
DEPTH	SAMPLE TYPE BLOWS PER 6 IN	DESCRIPTION		REMARKS
·				
-				
-	D	ense Red Clay	· · · · · ·	
20				
		•		
_	:			
25				
-				
-				
				· ].
30				Total Depth 30"

### DRILLING LOG

	ROJECT	1 840	ng Well Installation	DAIE	9 Sep 79 Smithson
L	OCATION	97 9 97 97		DRILLERS	
D	RILL RI	G Small Drill	Trailer Mounted Rig	BORE HOLE	BH15
	DEPTH	SAMPLE TYPE BLOWS PER 6 IN	DESCRIPTION		REMARKS
	VEPIN	PER O IN	Top Soil, Sandy Silt	· · · · · · · · · · · · · · · · · · ·	WT = 15.5' - 1  Oct
	-		Reddish-Light-Brown-S	ilty Slay	TD - 22.5 ft
	-		Yellowish-Orange Clay Fine Sand	Silt, Some	. <b>t</b>
	5				• .
			Light Orangish-Red Si	Ity Clay	
	10	} !			MW
		]	·		1' to sand
					10' of screen
					22.5 Botton of well
				• .	
ļ	15			I	

USAEHA Form 95, 12 Aug 74

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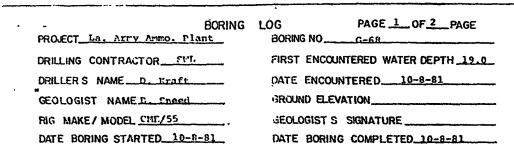
### DRILLING LOG

PROJECT LOCATION	Monitoring Well Installation		29 Sep 79 Smithson
DRILL RI	G - <u>Small Trailer Mounted</u> Drill Rig	BORE HOLE	<u>BH15</u>

	SAMPLE TYPE BLOWS		. [ . :
DEPTH	PER 6 IN	DESCRIPTION	REMARKS
			WT 15.5' V
-			
		Pinkish Fine Sand, Some Silts & Clays	
	1		
<b>.</b>	]		
[ -			,
20	1	<i></i>	
:			Very hard drilling at 21'
-	-		Total Durith Ad Fl
			Total Depth 22.5'
-			
· -	÷		
			:
25			
		-	
	]		
-	4		
			· •
-	1		
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USAEHA Form 95, 12 Aug 74

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ELEV	DEPTH	EGEND	CLASSIFATION OF MATERIALS	% CORE RECOV ERY	SAMPLE	REMARKS	]
	111	GM	Reddish tan silty sandy clayey gravel with prganics. Topsoil f	12/ 12	51	Sample taken from Auger.	
	10111111111111111111111111111111111111	er	prganics. Topsoil f Sharp Strong brown with red sandy clay, jointed, stiff. 5 2.5 yr - /6 2.5 yr - 4/8 Woist with no free water. Fluvial. No apparent bedding Led clayey silt firm slightly moist. No free water. No apparent bedding, 2.5 yr - 4/8 Fluvial clays - 25t	t 13/ 1;	4 5.5 5.5 9 8 83 10,5	Depths - Drilled - ft. Sample - in. Recovery - in./in. Sampler - S.S Split Spoon S.T Shelby Tube S.C. All samples in plastic bags except as noted. Fole drilled with E.S.A.	
	15_			18/ 1	14. 8 54 15.9	Could not obtain sample with S.S. from 19-20.5 Sample taken from Auger.	

PROJECT ___

ş

BORING.

BORING	LOG PAGE _2_OF _2_PAGE BORING NOG~68
DRILLING CONTRACTOR_SPT.	FIRST ENCOUNTERED WATER DEPTH 19.0
DRILLER S NAME D. Kraft	DATE ENCOUNTERED 10-8-81
GEOLOGIST NAME R. Sneed	GROUND ELEVATION
RIG MAKE / MODEL CMI:/55	EOLOGIST S SIGNATURE
DATE BORING STARTED 10-8-81	DATE BORING COMPLETED 10-8-81

:

	£LÉV	DEPTH	LEGENC	CLASSIFATION OF MATERIALS	% CORE RECOV ERY	BOX OR SAMPLE NO	REMARKS	
2 · 2 ·		25		Ned plastic clay stiff to very stiff 2.5 yr - 4/6 Fluvial No bedding apparent.	16/ 18 18/ 18/	24 56 25.		
		35 -		Red clayey silt firm with free water. 2.5 yr 4/8 No bedding apparent. Fluvial Clays - 25 6/10 T.D. 35.5		_34 58 35.3	 5-5-	

PROJECT

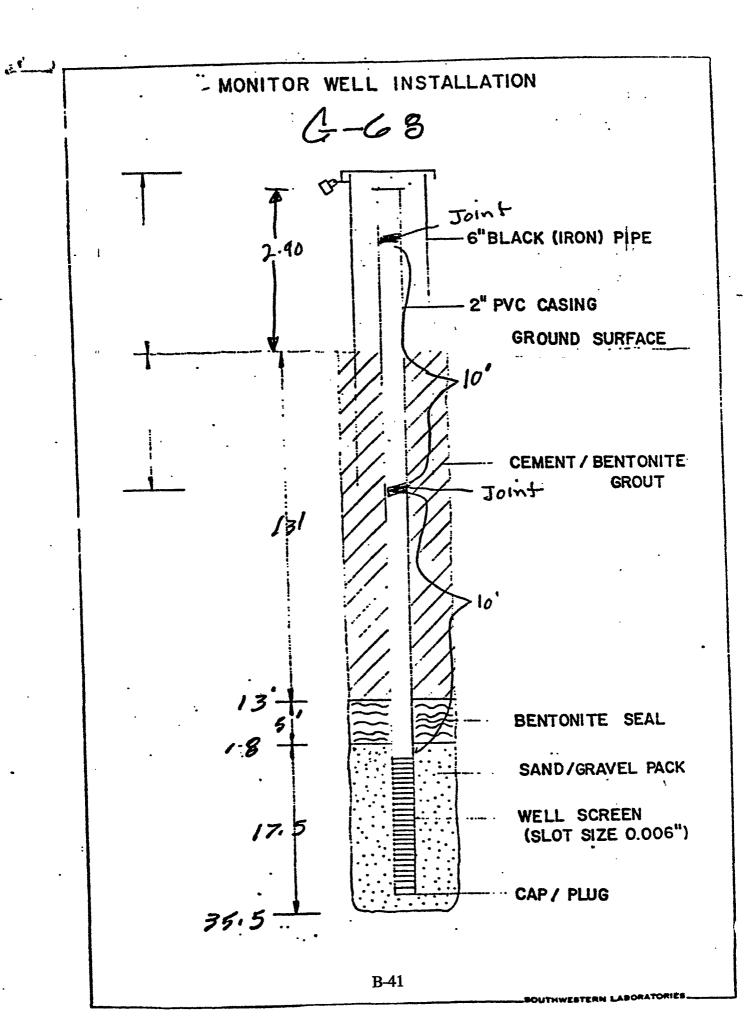
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1.71

.

BORING

B-40



MONITOR WELL REPORT

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PROJECT LAAP, Pink Water L	agoon .	Page
LOCATIONShreveport, LA		Well NoG-83
Date Completed <u>9-29-82</u> Origina	i Depth <u>29.0 ft</u>	Aquifer
Inspected By D. Primeaux		
Checked By		Depth Interval
	Elevation of top of surface corriser pipe.	asing / N/A
Ground	Height of top of surface casing pipe above ground surface.	/riser 3.5 ft
Elevation	Depth of surface seal below g	around
Elevation	surface	<u> </u>
0. 	Type of surface seal: <u>Sac-cr</u>	
0. 0.	I.D. of surface casing.	<u>6 inch</u>
	Type of surface casing: Ste	e1
		د 
	Depth of surface casing below	ground <u>1.5 ft</u>
	I. D. of riser pipe.	<u>3.0 inch</u>
	Type of riser pipe: Sched 4	10_PVC
e c c	Diameter of borehole	6 inch
	Depth of borehole	29.0
Water	Type of backfill: Cement Ben	atonite Grout
and the second sec	Elev./depth top of seal. Type of seal: <u>Bentonite</u>	•
δ , l	Elev./depth bottom of seal.	17.3
bł	Type of sand pack. No. 375	
	Depth of top of sand pack.	
Stratigraphy	Elev./depth top of screened sec	tion. $19.0$
	Type of screened section: Sch Discribe openings 10 slot	manufactured
Generalized	I.D. of screened section.	
	Elev./depth_bottom_of_screened	section 29.0 ft
e l	Length of blank section.	0.0 ft
Barrad	Elev. / depth bottom of plugged section.	blank 29.0 ft
	Elev./depth bottom of sand co	
	Type of backfill below observa	
	Elev / depth of hole.	29.0 ft
	B-42	, بېلىكى يېرىكى يېرىكى بېرىكى يېرىكى يېرى تې تې تې تې تې تې تېرىكى يېرىكى يېر

## MONITOR WELL REPORT

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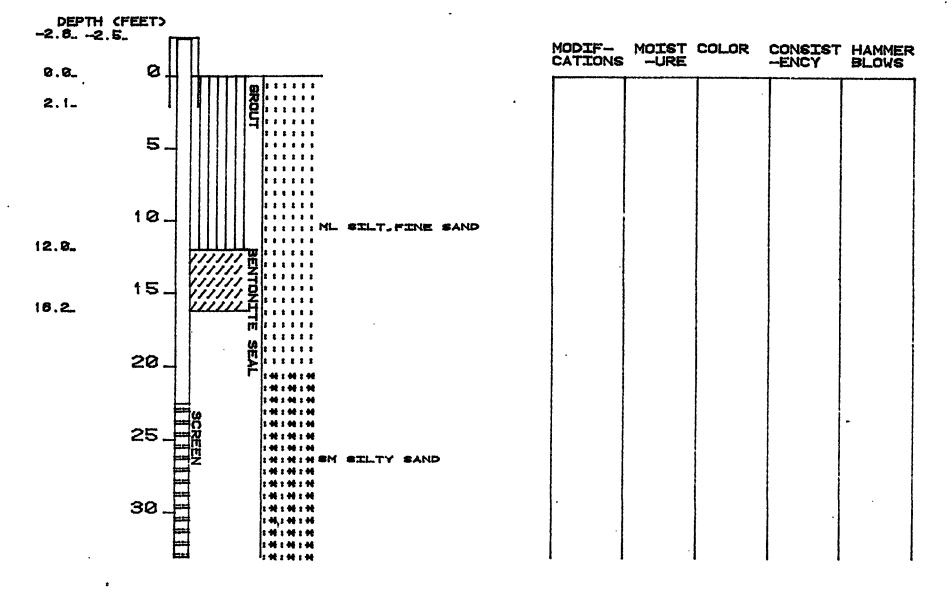
PROJECT L	AAP, Pink Water T	agoon	Page of
i i	Shreveport, La		Well NoG-34
			Aquifer
i i i i i i i i i i i i i i i i i i i		Date <u>9-28-82</u>	Aquiter
	-	1	·····
Checked By		Date I	Depth Intervol
Generalized Stratigraphy and Water Level		Elevation of top of surface casing, pipe above ground surface. Depth of surface seal below gr surface Type of surface seal: <u>Sac-cr</u> L.D. of surface casing. <u>Stee</u> Depth of surface casing: <u>Stee</u> Depth of surface casing below L.D. of riser pipe. Type of riser pipe. Type of riser pipe: <u>Sched 4</u> Diameter of borehole Depth of borehole Type of backfill: <u>Cement Be</u> Elev./depth top of seal. Type of seal: <u>Bentonite Pi</u> Elev./depth bottom of seal. Type of sand pack. <u>No. 375</u> Depth of top of sand pack. Elev./depth top of screened section: <u>Schee</u> Discribe openings <u>6 slot m</u> <u>Screen</u> L.D. of screened section. Elev./depth bottom of sand cal type of blank section. Elev./depth of hole. B-43	$\frac{N/A}{riser}$ $\frac{3.2 \text{ ft}}{1.8 \text{ ft}}$ $\frac{6 \text{ inch}}{3.0 \text{ inch}}$ $\frac{6 \text{ inch}}{32.5}$ $\frac{6 \text{ inch}}{32.5}$ $\frac{6 \text{ inch}}{32.5}$ $\frac{6 \text{ inch}}{32.5}$ $\frac{18.5}{291!\text{ lets}}$ $\frac{18.5}{19.5}$ $\frac{21.5 \text{ ft}}{22.5}$ $\frac{3.0 \text{ inch}}{21.5 \text{ ft}}$

# MONITOR WELL REPORT

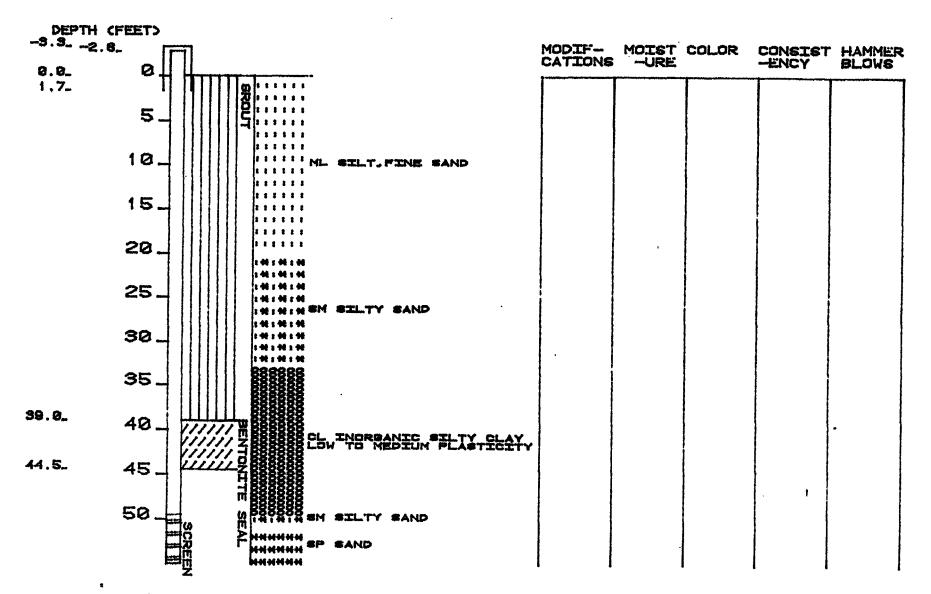
•

F	PROJECT	AAP Pink	. Wat	er Lac	1 <u>00n</u> P	Page	of <u>3</u>
T i	OCATION	hreveport	<u>, LA</u>		v	Nell No	G-85
	Date Completed_	<u>9/28/32</u>	_=	_ Origina		Aquifer	
,	nspected By	D. Prim	eaux	-	Date <u>9/28/82</u>	•	
1		:				epth Interval	
=					<u>_</u>		
Ē	Ground Elevation	1121 10 00 00 00 00 00 00 00 00 00 00 00 00		10000000000000000000000000000000000000	Elevation of top of surface casin riser pipe. Height of top of surface casing/r pipe above ground surface. Depth of surface seal below grou surface Type of surface seal: <u>Sac-crete</u> L.D. of surface casing. Type of surface casing: <u>Steel</u> Depth of surface casing below grou L.D. of riser pipe. Type of riser pipe: <u>Sched 40 PV</u>	riser	<u>N/A</u> 2.8 ft 2.2 ft <u>6 inch</u> <u>2.2 ft</u> <u>3 inch</u> <u>5 inch</u>
- 1	- 1			<b> </b>	Diameter of borehole Depth of borehole		32.5 ft
					Type of backfill: Cement Benton	nite	
		-			Elev./depth top of seal. Type of seal: <u>Bentonite Pi Pel</u>		<u>18.0</u> 19.0
	2				Elev./depth bottom of seal.	 h a	
			E	<b>†</b>	Type of sand pack. <u>No. 375 San</u> Depth of top of sand pack.	<u></u>	21.0 ft
					Elev./depth top of screened section Type of screened section: <u>Sched</u>	n. 49 PVC	22.5 ft
					Discribe openings 10 Slot manu: Screen	factured	-
	Ceneralize a		日		I.D. of screened section.	·	<u>3 inch</u>
				۰. ۹	Elev./depth bottom of screened se	ection	32.5 ft
				┫	Length of blank section.		<u>0.0 ft</u>
			e	<b>ĭ</b> ∣ <b>∙−−−</b>	Elev./depth bottom of plugged blo section.	onk	<u>32 ft</u>
-	-		¦   ◀	ļ	Elev./depth bottom of sand colum	nn. '	N/A
			•	· <u></u> <u> </u>	Type of backfill below observation pipe. <u>N/A</u>	n	
		_	L	<b>-</b>	Elev./depth of hole.		<u>32.5 ft</u>

B-44

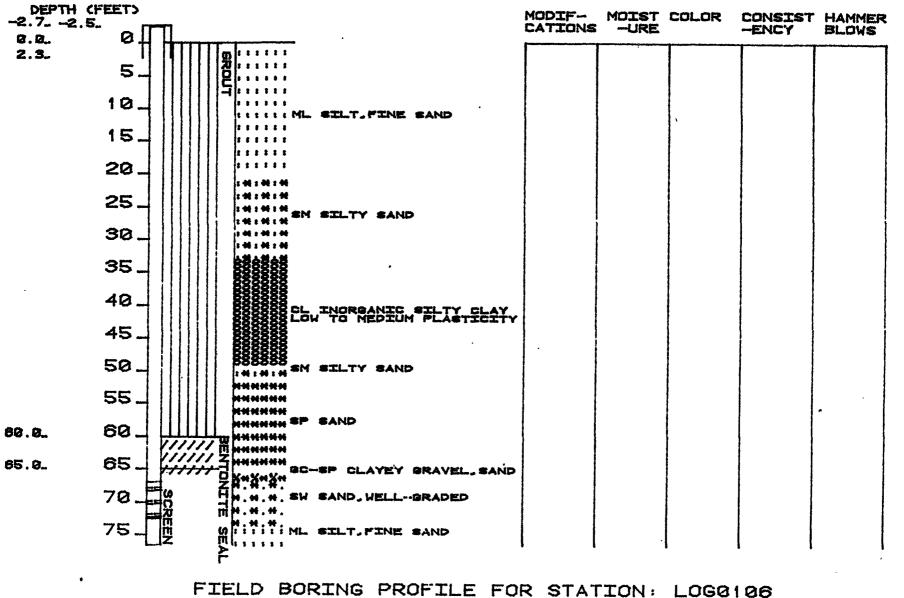


FIELD BORING PROFILE FOR STATION: LOG0104 DATE COMPLETED: 4/29/86 WELL DIAMETER: 4" DRILLING METHOD: ROTARY DEVELOPEMENT:



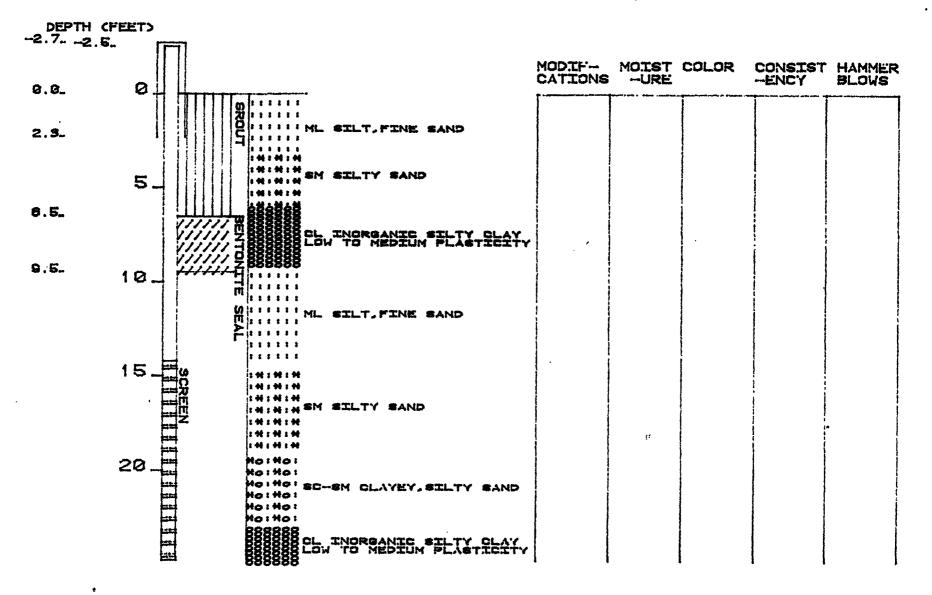
FIELD BORING PROFILE FOR STATION: LOG0105 DATE COMPLETED: 4/28/86 WELL DIAMETER: 4" DRILLING METHOD: ROTARY DEVELOPEMENT:

B-46

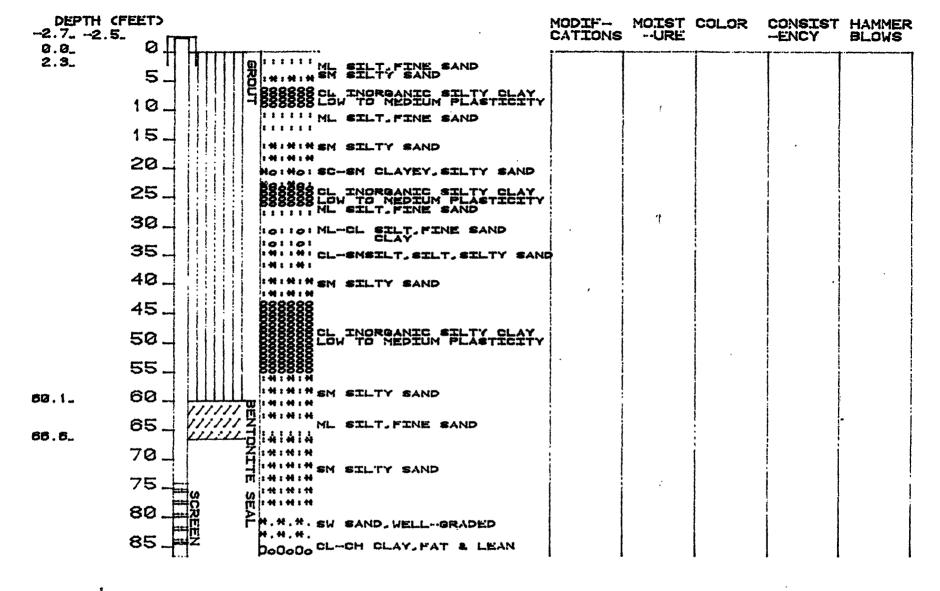


DATE COMPLETED: 4/26/86 WELL DIAMETER: 4" DRILLING METHOD : ROTARY **DEVELOPEMENT:** 

B-47



FIELD BORING PROFILE FOR STATION: LOGO 09 DATE COMPLETED: 4/18/86 WELL DIAMETER: 4" DRILLING METHOD: ROTARY DEVELOPEMENT:



FIELD BORING PROFILE FOR STATION: LOGO110

DATE COMPLETED: 4/15/86 WELL DIAMETER: 4" DRILLING METHOD: ROTARY DEVELOPEMENT:

B-49

## CHAIN-OF-CUSTODY FORMS

Ξ.			Science Applica	ntions			C	h <b>al</b>	n, oi	f Cu	ustc	ody	' Re	CO	rd						Shipment No.
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Nan	me / 2	10 60	002.000	Dr. L	et les	y Var													Ē	0. 0	Address 460 6 2 57 LEDTZ
Add	aress	(70)3	3) <u>556-</u>	7038	3	02011													•	F	SALT (ALL CONS. ONAME
	ject Manag		Parte	¥			10													ç	land recorder
	ject Name		AAD				N													002	Phone (001) 266-7700
1	)/P.O. No																			A	Contact Name
	mpler (Signa	anre)	5/4	(Pri	nted Name	2. Ileton	13			1									į	- NE	OBSERVATIONS, COMMENTS,
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White: Laboratory Pink: Project Manager Yellow: Project QAO Goldenrod: Field Project Manager

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White: Laboratory Pink: Project Manager Yellow: Project QAO Goldenrod: Field Project Manager



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Page 1 of 1

COC No.: **L002** Date: 2/25/94 ۳

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Job/P.O. No.	01-0827-0	3-6868-008						Ξ														ΪŤ	Fax (801)-268-9992
Sampler (Sig	nature)		(	Printed Nar	ne)	2		Exp-WA (1)(A)														Î	Contact Kevin Griffith
	/h.	÷	1	ANAND.	m /	422		dx						- 1								N E R	OBSERVATIONS, COMMENTS
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	G0084	SAIC01	WELL	21.6	2/25/94	13:10	WA	2														2	
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Signature				Signature																			Field: 5 °C
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			a second	<u> </u>								Shade	d areas	to be	comp	leted b	oy lab			•			1710 Goodridge Drive, McLean, VA 22102
Company			L	Company								L											(703) 827-4856
Science Applicati	ions Internati	onal Corporatio	n				White: L	aborat	ory		Pink:	Project	Manag	aer.		Yellow	w: Proi	iect Q/	10		Golder	nrod: F	Field Project Manager

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SALE.											Bee			age		of	1	с 			<b>L003</b> 2/28/94
Name <u>Science Applications Interna</u> Address <u>1710 Goodridge Dr., McLe</u> Phone Number <u>(703)-749-8903</u> Project Manager <u>Janardan Patel</u> Project Name <u>Louisiana Army Amm</u> Job/P.O. No. <u>01-0827-03-6868-000</u> Sampler (Signature)	ean, VA 221	02 <u>t</u> Printed Nan	D.f	्रेवाद		Exp-WA (1)(A)								ameter	5				TEMP. WD	NO OF CONTALZERS	Laboratory Name DATACHEM LABORATORIES Address <u>960 West LeVoy Drive</u> Salt Lake City, Utah <u>84123-2547</u> Phone ( <u>801)-266-7700</u> Fax ( <u>801)-268-9992</u> Contact <u>Kevin Griffith</u> OBSERVATIONS, COMMENTS
Leboratory No. Site ID Field Sample # G0110 SAICRB-03	Site Type WELL	Depth O	Date 2/28/94	Time 13:37	Matrix WA	2						-	-+								SPECIAL INSTRUCTIONS
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G0105 SAIC01	WELL	25	2/28/94	17:55	WA	2			†			+	$\neg$							2	
G0109 SAIC01	WELL	23	2/28/94	14:10	WA	2						1								2	
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Printed Name	Time	Printed Name					Time			nstructi Shaded (		o be c	compi	eted b	y isb				ι		SAIC Location Washington, D.C. 1710 Goodridge Drive, McLean, VA 22102
Company Science Applications International Corpora	<u> </u>	Company			White: L				Pink: Pi						w: Proj						(703) 827-4856 Field Project Manager

Science Applications International Corporation

Goldenrod: Field Project Manager



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Page	1	of 1	

COC No.: **L004** Date: 3/1/94

**Requested Parameters** Name Science Applications International Corporation Laboratory Name DATACHEM N O. Address 1710 Goodridge Dr., McLean, VA 22102 LABORATORIES PF Phone Number (703)-749-8903 Address 960 West LeVoy Drive Project Manager Janardan Patel Salt Lake City, Utah 84123-2547 CONT Project Name Louisiana Army Ammunition Plant Phone (801)-266-7700 Exp-WA (1)(A) Job/P.O. No. 01-0827-03-6868-008 Fax (801)-268-9992 Sampler (Signature) A-ZHRS (Printed Name) **Contact Kevin Griffith** TEMP. Rud John  $\mathcal{O}$ **OBSERVATIONS, COMMENTS** -Field Sample # Site Type Date Time Matrix SPECIAL INSTRUCTIONS aboratory No. Site ID Depth GO-146 SAICRB-004 RSNW 0 3/1/94 14:10 WA 2 2 QC Test Code = R WELL 22 3/1/94 14:46 WA 2 2 GO-146 SAIC01 2 G0106 SAIC01 WELL 57 3/1/94 16:35 WA 2 G0068 SAIC01 WELL 16 3/1/94 16:48 WA 2 2 CB-08 3/1/94 WA 1 1 ÷... Received by Date **Total Number of Containers:** 9 Relinguished by Date Shipment Method: Federal Express Airbill No.: 4214010570 Notes: 1 Signature 1. UW25, UW27 Custody Seal 1 No.: L004A 14 ı İr Custody Seal 2 No.: L004B Field COC No.s: Findlicton Time Time NA Printed Name Printed Name 930 A. Cool 4º NA 4 : NA NA Company Company NA Relinguished by Date Received by Date NA Temperature Blank Signature Signature Field: 3 °C Lab: Time Time Printed Name Printed Name SAIC Location Washington, D.C. instructions: Shaded areas to be completed by lab 1710 Goodridge Drive, McLean, VA 22102 Company Company (703) 827-4856

Science Applications International Corporation

White: Laboratory

Pink: Project Manager

Yellow: Project QAQ

Goldenrod: Field Project Manager

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													Pa	age	1	of	1		D	ate:	3/2/94
Name <u>Science Applications Internation</u> Address <u>1710 Goodridge Dr., McLear</u> Phone Number ( <u>703)-749-8903</u> Project Manager <u>Janardan Patel</u> Project Name <u>Louisiana Army Ammur</u> Job/P.O. No. <u>01-0827-03-6868-008</u> Sampler (Signature)	n, VA_221	02	1e) D. P.	d let	Matrix	Exp-WA (1)(A)	TEMP				Re	<u>gueste</u>	d Para	ameter	5	-		1		20 OF CO2F	Laboratory Name DATACHEM LABORATORIES Address <u>960 West LeVoy Drive</u> Salt Lake City, Utah <u>84123-2547</u> Phone ( <u>801)-266-7700</u> Fax ( <u>801)-268-9992</u> Contact <u>Kevin Griffith</u> OBSERVATIONS, COMMENTS SPECIAL INSTRUCTIONS
GO-145 SAIC01	RSNW	0	3/2/94	12:15	WA	2														2	QC Test Code = R
GO-145 SAIC01	WELL	20	3/2/94	12:25	WA	2		ļ										ľ		2	
G0104 SAIC01	WELL	18	3/2/94	12:40	WA	2							_							2	
G0104 SAIC01	WELL	18	3/2/94	12:40	WA	2															Flagging Code ⇔D
CB-09		 0	3/2/94		WA		1								-			<u> </u>		1	
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Relinquished by	Date	Received by	/				Date	•		1											NA
Signature	Time	Signature																			Temperature Blank Field: 5 °C Lab;
Printed Name	Time	Printed Name					Time	<b>,</b>		Instruc Shade		to be	compl	leted b	ay lab				7 1		SAIC Location Washington, D.C. 1710 Goodridge Drive, McLean, VA 22102
Company Science Applications International Corporation	n	Company			White: I	shore			Diak:	Project	Maga			Veller	Ora	lect Q/			Coldo	nrod. I	(703) 827-4856 Field Project Manager

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COC No.: **L006** Page 1 of 1 Date: 3/3/94

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7/	GO-150	SAICRB-006	RSNW	0	3/3/94	15:05	WA	2						$\Box$					$\Box$		$\Box$	2	QC Test Code = R
7	GO-150	SAIC01	WELL	14	3/3/94	15:15	WA	2											$\Box$			2	
	GO-151	SAIC01	WELL	15	3/3/94	16:30	WA	2							$\Box$				$\Box$		$\Box$	2	
	G0085	SAIC01	WELL	20	3/3/94	9:55	WA	2							$\Box$	$\Box'$			$\Box$			2	
	ð.	CB-10			3/3/94	<u> </u>	WA		1						$\Box'$							1	
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Signature			Date	Signature					Value									•					Temperature Blank Field: 4 °C
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Printed Name			Time	Printed Name					Time	•	S	Instruc Shade		s to be	i comp	pleted	by lab					4.	SAIC Location Washington, D.C. 1710 Goodridge Drive, McLean, VA 22102 (703) 827-4856
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Science Applications International Corporation

White: Laboratory

Pink: Project Manager

Yellow: Project QAO

Goldenrod: Field Project Manager

# APPENDIX C GROUNDWATER CONCENTRATION DATA TABLES AND BAR CHARTS

### APPENDIX C GROUNDWATER CONCENTRATION DATA TABLES AND BAR CHARTS

This appendix contains groundwater concentration data tables for the sampling events from January 1980 through March 1994. Data are presented for the following nine contaminants of concern (COCs):

- RDX
- HMX
- 2,4,6- trinitrotoluene (2,4,6-TNT)
- 1,3-dinitrobenzene (1,3-DNB)
- 2,4-dinitrotoluene (2,4-DNT)
- 2,6-dinitrotoluene (2,6-DNT)
- 1,3,5-trinitrobenzene (1,3,5-TNB)
- nitrobenzene (NB), and
- Tetryl.

The health advisory level (HAL) for each of these COCs is included in these tables. The concentration levels below the instrument detection limits (IDLs) are shaded in the tables.

Bar charts are provided for those COCs that exceed the HALs. For the sake of clarity, each bar chart was limited to around 35 data points (number of sampling events times number of COCs). For example, G0009 has 17 sampling events; therefore, only two COCs were presented on one bar chart. Also, COCs with similar concentration ranges were grouped together and presented on the same bar chart for better definition of concentration levels. Some of the COCs had data for selected sampling events; these COCs were presented together also. A sampling event was not included m the bar charts if no contaminants were detected during that event.

Analyte	Health Advisory Level	GO009 (Jan 1980)	GO009 (Dec 1981)	GO009 (July 1982)	GO009 (Aug 1982)	GO009 (Dec 1982)	GO009 (Feb 1983)	GO009 (June 1983)	GO009 (Aug 1983)	GO009 (Dec 1983)	GO009 (Mar. 1984)	GO009 (June 1984)	GO009 (Aug. 1984)	GO009 (Dec 1984)	GO009 (Mar. 1985)	GO009 (July 1986)	GO009 (Oct 1990)	GO009 (Feb 1994)
RDX	2	1580	1720		3540	4900 240	1660	908 100	800 100	380 100	730 300	670 100		440 100	2560		558.2	430
HMX 1,3,5 TNB	400 3.5		90.6	168 												8.5	48.3 31.1	26 29
2,4 DNT 1,3 DNB	1000	9	6.32	50	47	100	100	100	100	100	10	6	8	7	6	3.58	2.4 0.7	37
2,6 DNT 2,4,6 TNT	1000	3 200	1.6 273	50 690	8 870	100 410	100 200	100 290	100 260	100 195	100 220	1 200	1 302	220	192	0.55 130	1,15 55.6	0.46 0.6 28
TETRYL	430		22.8 2.1				an siñă						a 10			0.66	1.5	0.63
NB	3.5		9.595 A <b>.92</b> 0															

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Note: Shaded areas represent instrument detection limit (LT)

#### TABLE C-2 Groundwater Sampling Data for Area P, LAAP Concentration in Upper Terrace Aquifer Units: ug/L

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Analyte	Health Advisory Level	GO→012 (Jan 1980)	GO-012 (Dec 1981)	GO-012 (July 1982)	GO-012 (Aug 1982)	GO-012 (Dec 1982)	GO012 (Mar. 1983)	GO-012 (May 1983)	GO-012 (Aug 1983)	GO-012 (Dec 1983)	GO012 (Mar 1984)	GO-012 (June 1984)	GO-012 (Aug 1984)	GO-012 (Dec 1984)	GO012 (Mar 1985)	GO012 (July 1986)	GO-012 (Oct 1990)	GO-012 (Feb 1994)
RDX	2	10500	4500 52	5650	3670	2500	1960	7600	5500	100	14500	7740	5200	13600	43200	3700	2700	3100
нмх	400			153	110	100	8850				220	280	250	523	680	86	82	110
1,3,5 TNB	3.5		146 109													240	67	950
2,4 DNT	1000	183	105 102.73		84	100	100	100	130	100	76	210	137	349	337	89	40.2	120
1,3 DNB	1		135 65 10													64	42	35
2,6 DNT	1000	48	43.2 10	50	120	100	400	100	200	183	271	62	32	32	44	18.3	11.4	32.3
2,4,6 TNT	2	4460	2436.97 92	2540	1430	850	10700	2230	2600		6220	6230	2630	10600	12700	3100	760	3700
TETRYL	430	15	. 6.6	160	100	100		100	1500	001:00	SSE 50	10	10		⁻ 38	6.2	0,556	
NB	3.5		<u></u>	*** ***												1,13		

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Note: Shaded areas represent instrument detection limit (LT)

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#### TABLE C-3 Groundwater Sampling Data for Area P, LAAP Concentration in Upper Terrace Aquifer Units: ug/L

Analyte	Health Advisory Level	GO014 (Jan 1980)	GO014 (Dec 1981)	GO014 (June 1982)	GO014 (Aug 1982)	GO014 (Dec 1982)	GO014 (Mar 1983)	GO014 (June 1983)	GO014 (Aug 1983)	GO014 (Feb 1984)	GO014 (May 1984)	GO014 (Sep 1984)	GO014 (Nov 1984)	GO014 (Mar 1985)	GO014 (July 1986)	GO014 (Oct 1990)	GO014 (Feb 1994)
RDX	2	50	53.4	100	100	100	110	877	1500	57	300	170	150	1300	16.4	33.8	14.4
нмх	400					100	S S 8100	665		100	100	203	>> <b>100</b>	100	• 4.73	6.95	2.92
1,3,5 TNB	3.5		2.5												2.05	0.626	0,429
2,4 DNT	1000	900 - S <b>t</b>			t	100	100	100	aa 😳 100	3	10		2029) <b>(</b>	(gra <b>1990)</b>	0.6	0.612	0.397
1,3 DNB	1														1.44	0.519	0.458
2,6 DNT	· 1000	1997 (M <b>R</b> )				100	100	SSEC 100	100		in sea an	asu ni <b>su</b>		827-3 <b>.</b> ¥	0.55	1.15	0,6
2,4,6 TNT	2	<u> Angel</u>	2.5	n feilige	2	100	<u> 100 % % % % % % % % % % % % % % % % % %</u>		34 100	3	10	2010 M	20	14	0.78	0.588	0,426
TETRYL	430		6			100	2001/200	100	100			11 - H ( <b>10</b> -			0.66	0.556	0.631
NB	3.5		21												<u> </u>	1.07	0.682

Note: Shaded area represent instrument detection limit (LT).

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#### 07-Jul-94

TABLE C-4 Groundwater Sampling Data for Area P, LAAP Concentration in Upper Terrace Aquifer Units; ug/L

07-Jul-94

Analyte	Health Advisory Level	G0068 (Novl9 1981)	G0068 (Novl6 1981)	G0068 (July 1986)	G0068 (Feb 1988)	G0068 (Oct1990)	G0068 (Feb 1994)
RDX	2	17800	50	8200	9800	6500	2500
НМХ	400			2200	1200	700	350
1,3,5 TNB	3.5	70.4 4		200	110	310	490
2,4 DNT	1000	55 61		4.81	120	100	350
1,3 DNB	1	41 62.7		7.65	71	60	82
2,6 DNT	1000	28 23.3		2.06	5.5	58	60
2,4,6 TNT	2	260 3610		5700	7400	5100	3600
TETRYL	430	15		53.4	6.6	28	31
NB	3.5	2.1		1.13		320	68

Note: Shaded areas represent instrument detection limit (LT).

TABLE C-5 Groundwater Sampling Data for Area P, LAAP Concentration in Upper Terrace Aquifer Units: ug/L

### 07-Jul-94

Analyte	Health Advisory Level	G0083 (Oct 1990)	G0083 (Feb 1994)
RDX	2	2900	1200
нмх	400	350	99
1,3,5 TNB	3.5	730	800
2,4 DNT	1000	29	95
1,3 DNB	1	0.519	5.6
2,6 DNT	1000	58	12
2,4,6 TNT	2	5300	3100
TETRYL	430	28	95
NB	3.5	1.07	14

Note: Shaded areas represent instrument detection limit ( LT).

TABLE C-6 Groundwater Sampling Data for Area P, LAAP Concentration in Upper Terrace Aquifer Units: ug/L

### 23-Jun-94

Analyte	Health Advisory Level	G0084 (Oct 1990)	G0084 (Feb 1994)
RDX	2	290	120
НМХ	400	11.8	14
1,3,5 TNB	3.5	550	320
2,4 DNT	1000	3.06	12
1,3 DNB	1	0.519	0.46
2,6 DNT	1000	58	12
2,4,6 TNT	2	560	250
TETRYL	430	28	5.7
NB	3.5	1.07	0.68

Note: Shaded areas represent instrument detection limit.

TABLE C-7 Groundwater Sampling Data for Area P, LAAP Concentration in Upper Terrace Aquifer Units: ug/L

### 23-Jun-94

Analyte	Health Advisory Level	G0085 (Oct 1990)	G0085 (Feb 1994)
RDX	2	7600	3800
HMX	400	1000	310
1,3,5 TNB	3.5	7300	3800
2,4 DNT	1000	130	79
1,3 DNB	1	120	32
2,6 DNT	1000	58	59
2,4,6 TNT	2	16000	4200
TETRYL	430	28	310
NB	3.5	1.07	67

Note: Shaded areas represent instrument detection limit (LT).

TABLE C-8 Groundwater Sampling Data for Area P, LAAP Concentration in Upper Terrace Aquifer Units: ug/L

07-Jul-94

Analyte	Health Advisory Level	G0104 (July 1986)	G0104 (Feb 1988)	G0104 (Oct 1990)	G0104 (Feb 1994)
RDX	2	14000	27000	19000 12000	8400
НМХ	400	880	1100	910 750	370
1,3,5 TNB	3.5	7700	4800	6700 6100	6300
2,4 DNT	1000	0.6	770	720 660	570
1,3 DNB	1	0.61	7.8	660 660	580
2,6 DNT	1000	20.5	55	58 58	60
2,4,6 TNT	2	18000	25000	15000 15000	11000
TETRYL	430	52.4	66	28 28	130
NB	3.5	1.13	11.3	4000 3800	68

Note: Shaded areas represent instrument detection limit (LT).

TABLE C-9 Groundwater Sampling Data for Area P, LAAP Concentration in Lower Terrace/Sparta Sand Aquifer Units: ug/L

23-Jun-9	94
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Analyte	Health Advisory Level	G0105 (July 1986)	G0105 (Jan 1988)	G0105 (Sep 1990)	G0105 (Feb 1994)
RDX	2	0.63	18.4	1300	330
HMX	400	1.3	2.89	210	360
1,3,5 TNB	3.5	2.2	0.56	1200	3900
2,4DNT	1000	0.6	0.6	33	54
1,3 DNB	1	2.51	0.61	90	320
2,6DNT	1000	4.59	2.5	6.32	60
2,4,6 TNT	2	0.78	0.78	94	17
NB	3.5	1.13	1.13	600	68
TETRYL	430	0.66	0.66	0.556	3.7

Note: Shaded areas represent instrument detection limit.

TABLE C-10 Groundwater Sampling Data for Area P, LAAP Concentration in Lower Terrace/Sparta Sand Aquifer Units: ug/L

07-Jul-94

Analyte	Health Advisory Level	G0106 (Oct 1990)	G0106 (Feb 1994)
RDX	2	2500	4100
HMX	400	82	53
1,3,5 TNB	3.5	370	970
2,4DNT	1000	200	640
1,3 DNB	1	240	330
2,6 DNT	1000	29.1	60
2,4,6 TNT	2	1300	8800
TETRYL	430	0.556	63
NB	3.5	1.07	68

TABLE C-11 Groundwater Sampling Data for Area P, LAAP Concentration in Upper Terrace Aquifer Units: ug/L

23-Jun-94

Analyte	Health Advisory Level	G0109 (July 1986)	G0109 (Jan. 1988)	G0109 (Oct 1990)	G0109 (Feb 1994)
RDX	2	3200	5600	4200	3100
HMX	400	1300	120	750	300
1,3,5 TNB	3.5	21.1	28	73	95
2,4 DNT	1000	16	19	36.3	330
1,3DNB	1	0.61	2.05	23	8.2
2,6DNT	1000	0.55	5.5	58	60
2,4,6 TNT	2	0.78	2900	1800	3600
TETRYL	430	1.48	6.6	28	40
NB	3.5	1.13	1.13	1.07	6.8

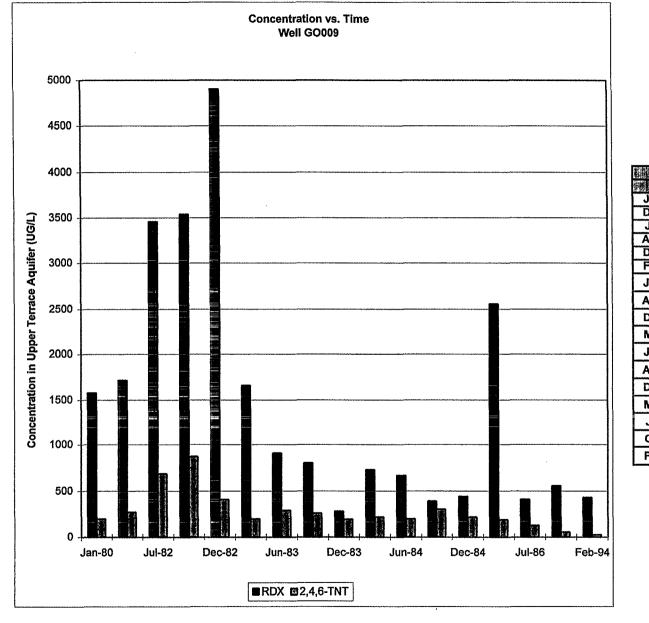
Note: Shaded areas represent instrument detection limit.

TABLE C-12 Groun	dwater	Sampling Data for Area P, LAAP
Concentration in	Lower	Terrace/Sparta Sand Aquifer
Units: ug/L		

### 08-Jul-94

Analyte	Health Advisory Level	G0110 (July 1986)	G0110 (Jan 1988)	G0110 (Oct 1990)	G0110 (Feb 1994)
RDX	2	785	3110	3200	2800
HMX	400	56.2	111	139.5	130
1,3,5 TNB	3.5	139	103	420	460
2,4 DNT	1000	95	226	84	120
1,3DNB	1	20.5	49	26	24
2,6DNT	1000	12.1	8.3	58	60
2,4,6 TNT	2	6	2060	760	570
TETRYL	430			28	0.63
NB	3.5			1.07	6.8

Note: Shaded areas represent instrument detection limit (LT)



<b>1.11.13,封</b> 律	<b>READ</b> X	121430-TNL
<b>HAUN</b>		12211
Jan-80	1580	200
Dec-81	1720	273
Jul-82	3460	690
Aug-82	3540	870
Dec-82	4900	410
Feb-83	1660	200
Jun-83	908	290
Aug-83	800	260
Dec-83	280	195
Mar-84	730	220
Jun-84	670	200
Aug-84	390	302
Dec-84	440	220
Mar-85	2560	192
Jul-86	410	130
Oct-90	558.2	55.6
Feb-94	430	28

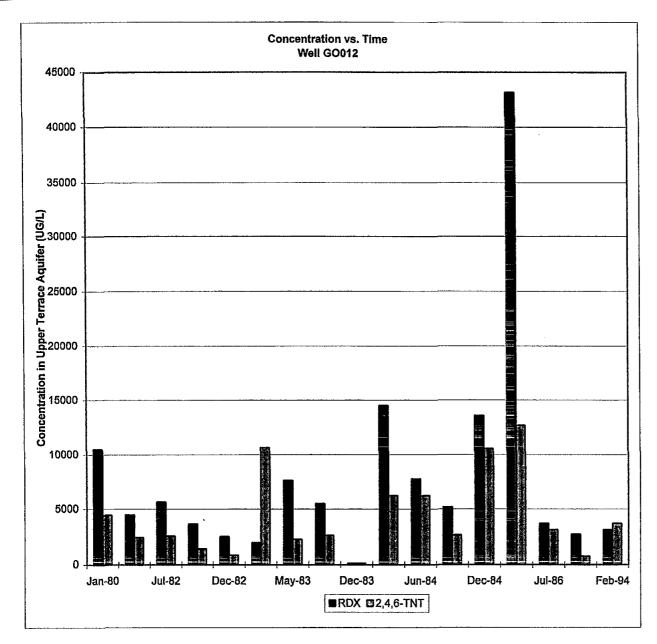
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U.S. Army Environmental Center Aberdeen Proving Ground, Maryland

Concentration vs. Time Well GO009 Louisiana Army Ammunition Plant Figure: C-1 Project: 01-0827-03-6868-012

C-13



		11:020 Mill		
Jan-80	10500	4460		
Dec-81	4500	2436.97		
Jul-82	5650	2540		
Aug-82	3670	1430		
Dec-82	2500	850		
Маг-83	1960	10700		
May-83	7600	2230		
Aug-83	5500	2600		
Dec-83	100	100		
Mar-84	14500	6220		
Jun-84	7740	6230		
Aug-84	5200	2630		
Dec-84	13600	10600		
Mar-85	43200	12700		
Jul-86	3700	3100		
Oct-90	2700	760		
Feb-94	3100	3700		

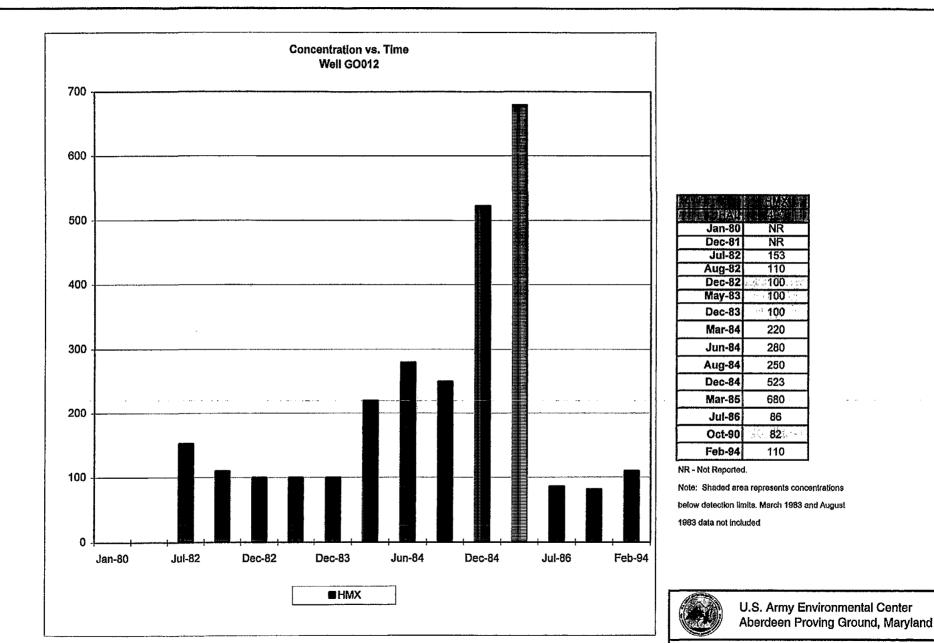
Note: Shaded area represents concentrations

below detection limits.



U.S. Army Environmental Center Aberdeen Proving Ground, Maryland

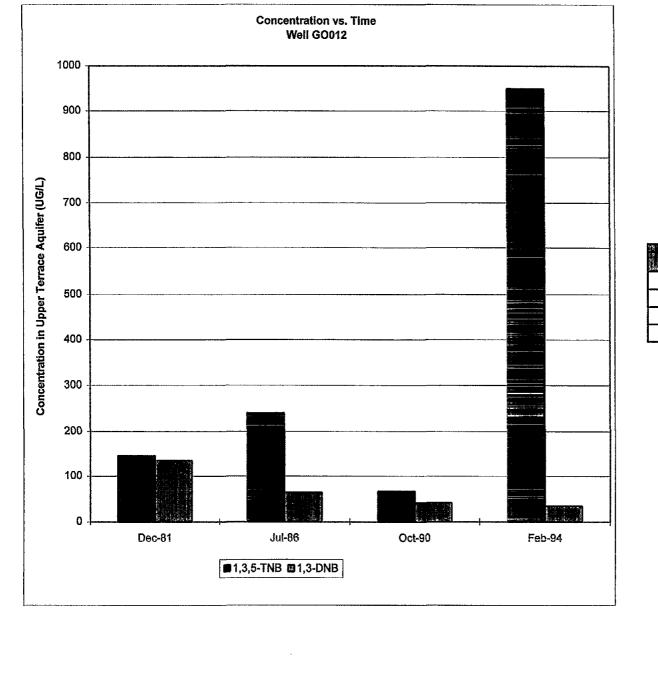
Concentration vs. Time Well GO012		
Louisiar	a Army Ammunition Plant	
Figure: C-3 Project: 01-0827-03-6868-012		



Concentration vs. Time Well GQ105

Louisiana Army Ammunition Plant

C-16



HAL		BERRY STREET
Dec-81	146	135
Jul-86	240	64
Oct-90	67	42
Feb-94	950	35



U.S. Army Environmental Center Aberdeen Proving Ground, Maryland

Concentration vs. Time Well GO012 Louisiana Army Ammunition Plant Figure: C-5 Project: 01-0827-03-6868-012

**Concentration vs. Time** Well GO012 45000 40000 35000 Concentration in Upper Terrace Aquifer (UG/L) 30000 25000 20000 15000 10000 5000

May-83

Dec-82

Dec-83

RDX 2,4,6-TNT

Jun-84

Dec-84

Jul-86

Feb-94

Jan-80	50	NR
Dec-81	53.4	NR
Jun-82	<u>-</u> 100	NR
Aug-82	100	NR
Dec-82	100	100
Mar-83	110	100
Jun-83	877	665
Aug-83	1500	100 😒
Feb-84	57	100
May-84	300	100
Sep-84	170	203
Nov-84	150	100
Mar-85	1300	100
Jul-86	16.4	4.73
Oct-90	33.8	6.95
Feb-94	14.4	2.92

below detection limits

NR: Not Reported



U.S. Army Environmental Center Aberdeen Proving Ground, Maryland

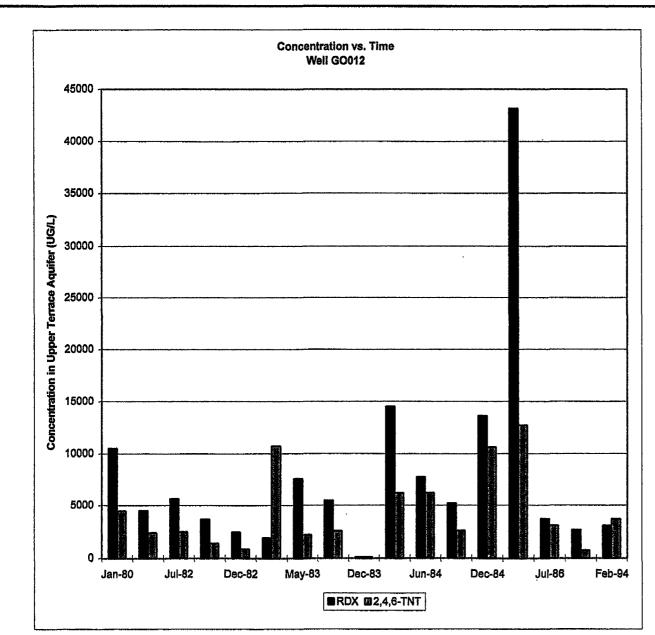
Concentration vs. Time Well GO012

Louisiana Army Ammunition Plant

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Jan-80

Jui-82



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		C CLE
<b>CONTRACTOR</b>	lahalah Sarah Sarah	
Jan-80	50	NR
Dec-81	53.4	NR
Jun-82	≥100<	NR
Aug-82	100	NR
Dec-82	100,000	100*
Mar-83	110	100
Jun-83	877	665
Aug-83	1500	5°+0100.5
Feb-84	57	233 <b>100</b> - Juni
May-84	300	100
Sep-84	170	203
Nov-84	150	100 8.3
Mar-85	1300	4 ¹⁴ 100
Jul-86	16.4	4.73
Oct-90	33.8	6.95
Feb-94	14.4	2.92

Note: Shaded area represents concentrations

below detection limits.

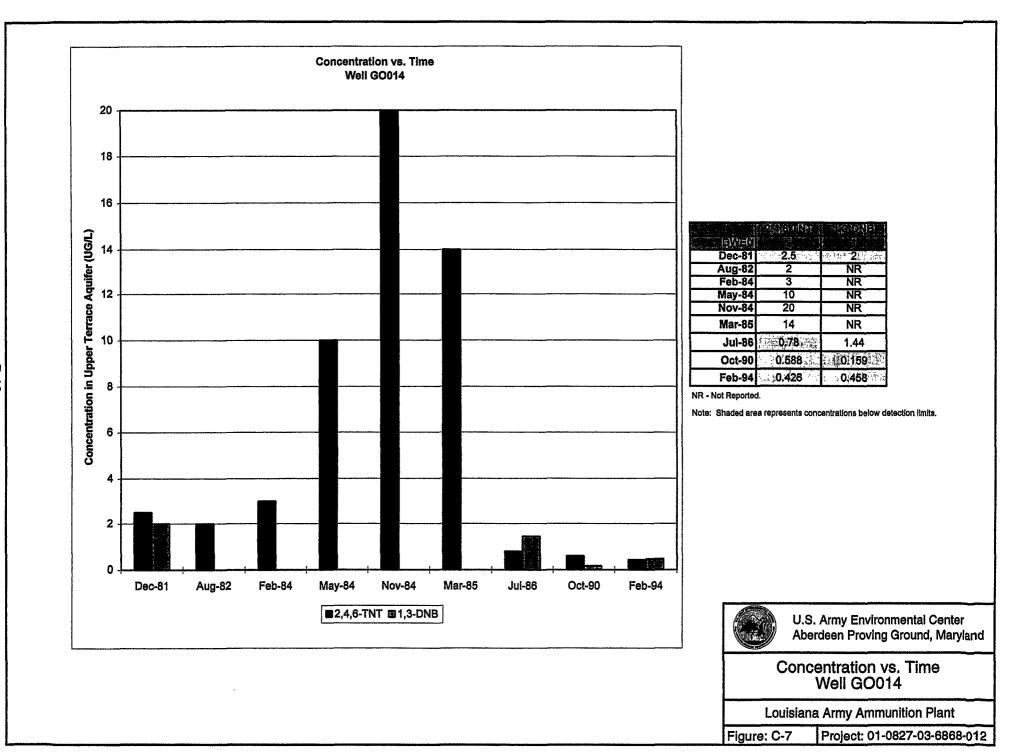
NR: Not Reported



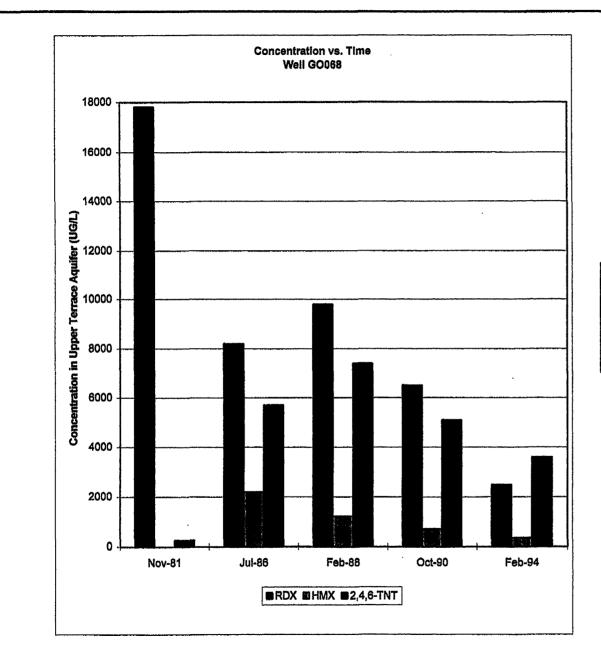
U.S. Army Environmental Center Aberdeen Proving Ground, Maryland

Concentration vs. Time Well GO012

Louisiana Army Ammunition Plant



C-19



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	and the second		Contraction of the second
Nov-81	17800	NR	260
Jui-86	8200	2200	5700
Feb-88	9800	1200	7400
Oct-90	6500	700	5100
Feb-94	2500	350	3600

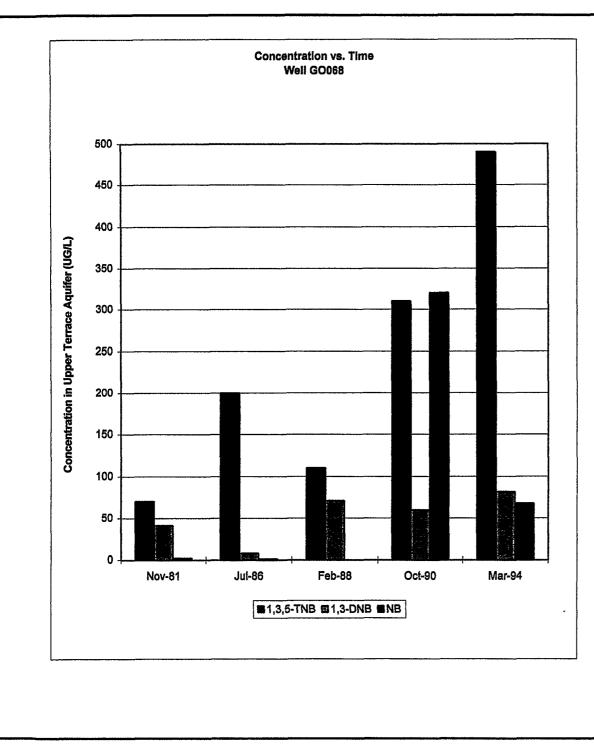




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Concentration vs. Time Well GO068

Louisiana Army Ammunition Plant



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Nov-81	70.4	41	2.1
Jul-86	200	7.65	1.13
Feb-88	110	71	NR
Oct-90	310	60	320
Mar-94	490	82	68

NA - Not Available.

NR - Not Reported

Note: Shaded area represents concentrations below detection limits.



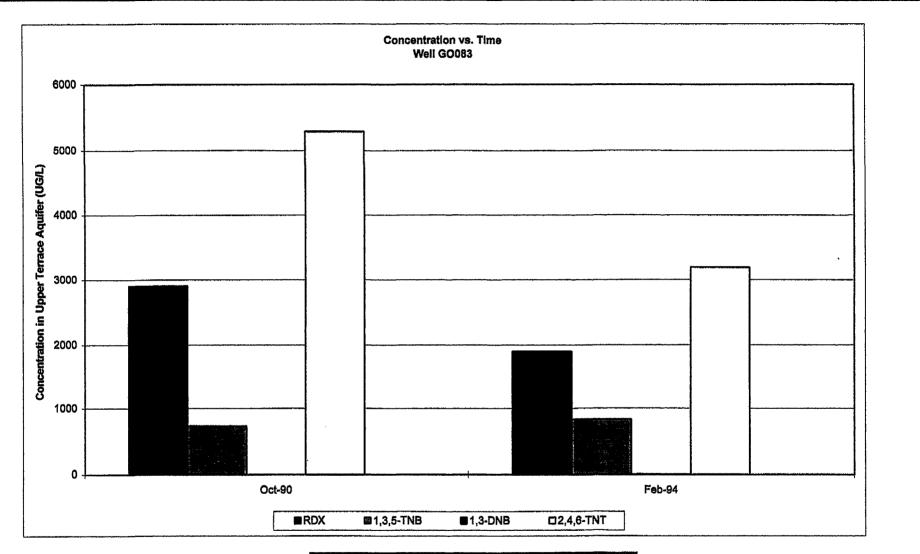
U.S. Army Environmental Center Aberdeen Proving Ground, Maryland

Concentration vs. Time Well GO068

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Louisiana Army Ammunition Plant

Figure: C-9 Project: 01-0827-03-6868-012

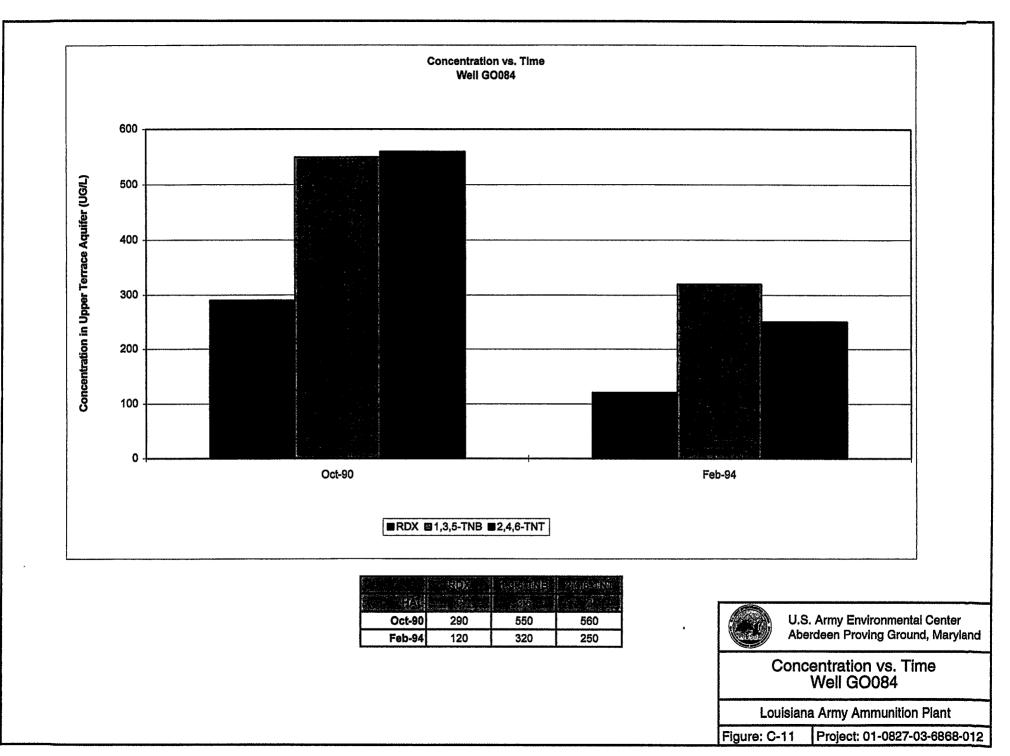


Feb-94	1900	830	5.6	3200
Oct-90	2900	730	0,519	5300
	The second s			
		1:18:26:21	() ( ( <b>)</b> ( ) ( )	

U.S. Army Environmental Center Aberdeen Proving Ground, Maryland

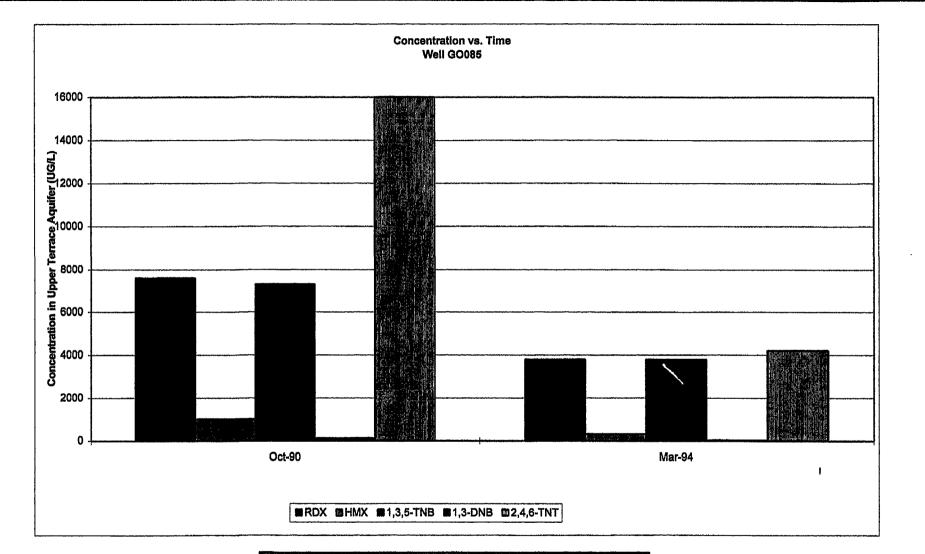
Concentration vs. Time Well GO083

Louisiana Army Ammunition Plant



C-23

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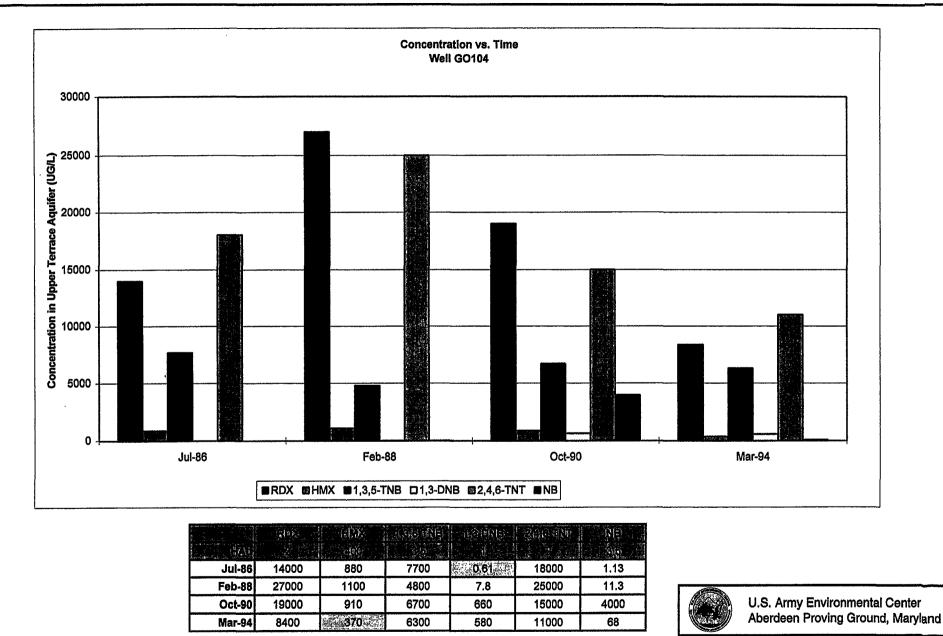
				Sec. States	
Oct-90	7600	1000	7300	120	16000
Mar-94	3800	310	3800	32	4200



U.S. Army Environmental Center Aberdeen Proving Ground, Maryland

Concentration vs. Time Well GO085

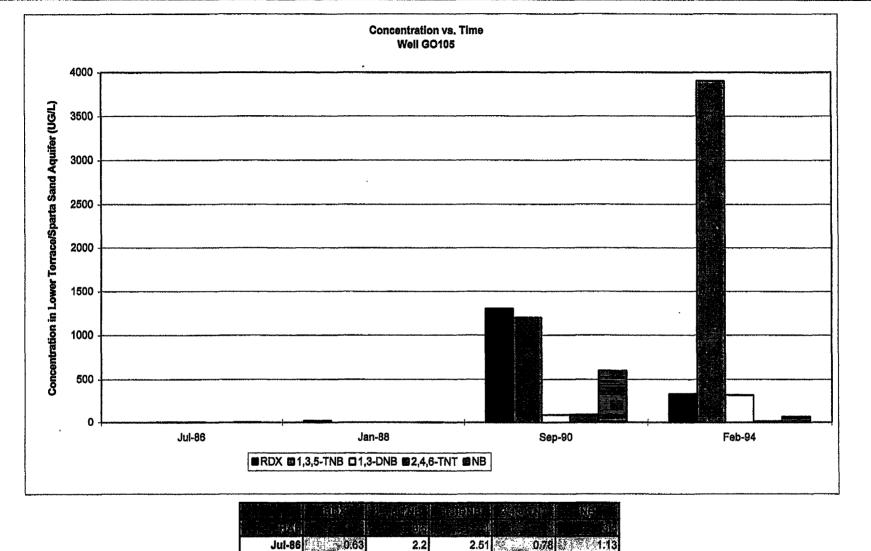
Louisiana Army Ammunition Plant



Concentration vs. Time Well GO104

Louisiana Army Ammunition Plant

Figure: C-13 Project: 01-0827-03-6868-012



Jan-88	18.4		0.61	0.78	1.18
Sep-90	1300	1200	90	94	600
Feb-94	330	3900	320	17	£72 x 2 68



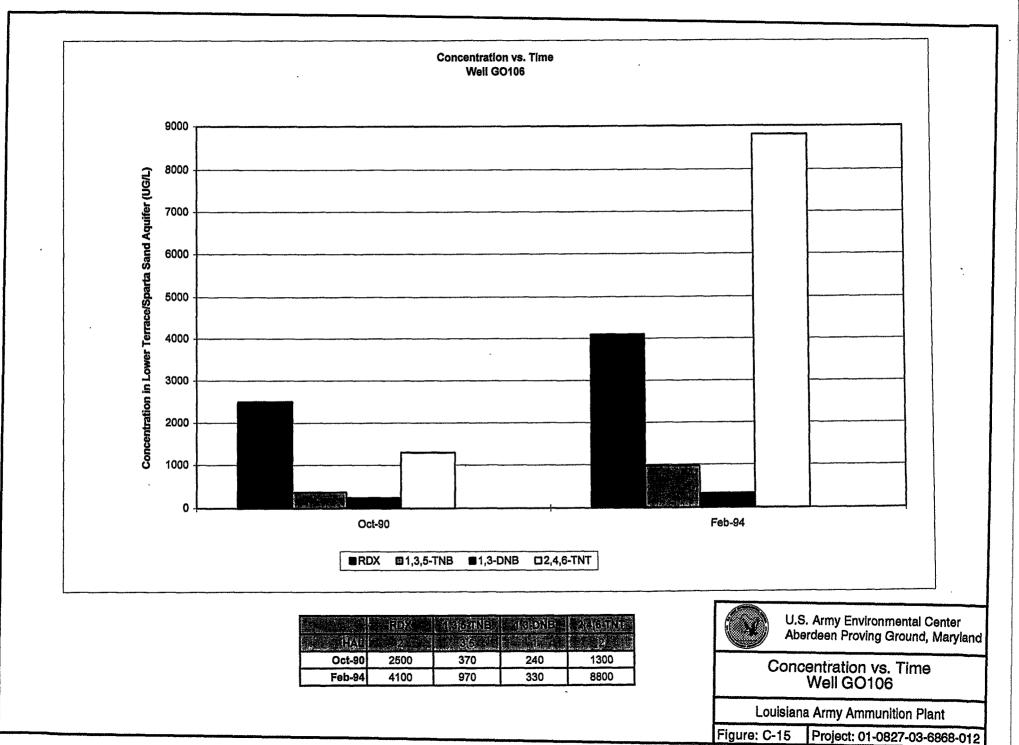
U.S. Army Environmental Center Aberdeen Proving Ground, Maryland

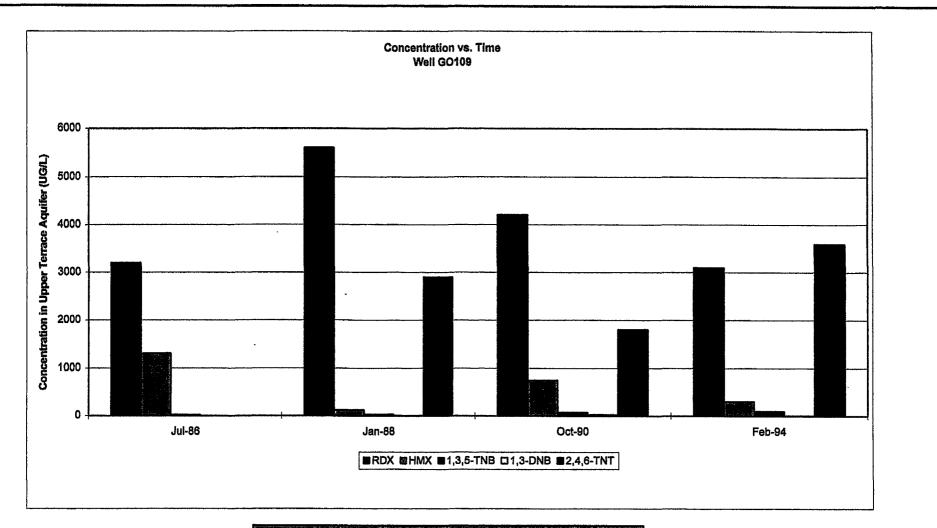
Concentration vs. Time Well GO105

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Louisiana Army Ammunition Plant

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	1.00		1.015 PNF-1	1.5 993	ASSO TON
	ana shake shi sa l				
Jul-86	3200	1300	21.1	0.61	0.78
Jan-88	5600	120	28	2.05	2900
Oct-90	4200	750	73	23	1800
Feb-94	3100	300	95	8.2	3600

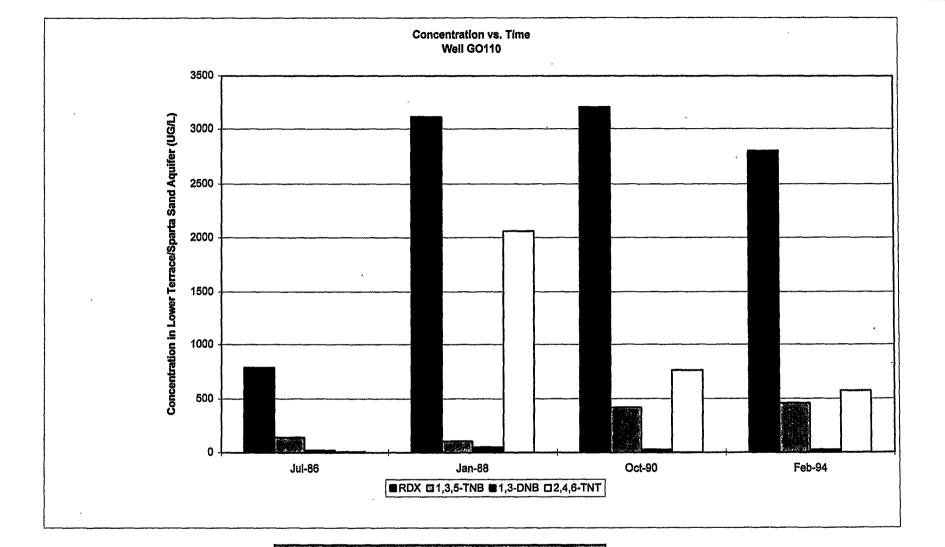
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U.S. Army Environmental Center Aberdeen Proving Ground, Maryland

Concentration vs. Time Well GO109

Louisiana Army Ammunition Plant

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Jul-86	785	139	20.5	6
Jan-88	3110	103	49	2060
Oct-90	3200	420	26.	760
Feb-94	2800	460	24	570

U.S. Army Environmental Center Aberdeen Proving Ground, Maryland		
Concentration vs. Time Well GO110		
Louisiana Army Ammunition Plant		
 Figure: C-17 Project: 01-0827-03-6868-		

C-29

APPENDIX D GROUNDWATER CONCENTRATION REGRESSION ANALYSIS PLOTS

#### APPENDIX D

#### GROUNDWATER CONCENTRATION REGRESSION ANALYSIS PLOTS

This appendix contains the groundwater concentration regression analysis plots. These plots present the variation of concentration with time. The plots are presented for each of the 53 data sets (well and COC), which were "valid data sets", with four or more data points (concentration levels) and at least one data point above the instrument detection limit.

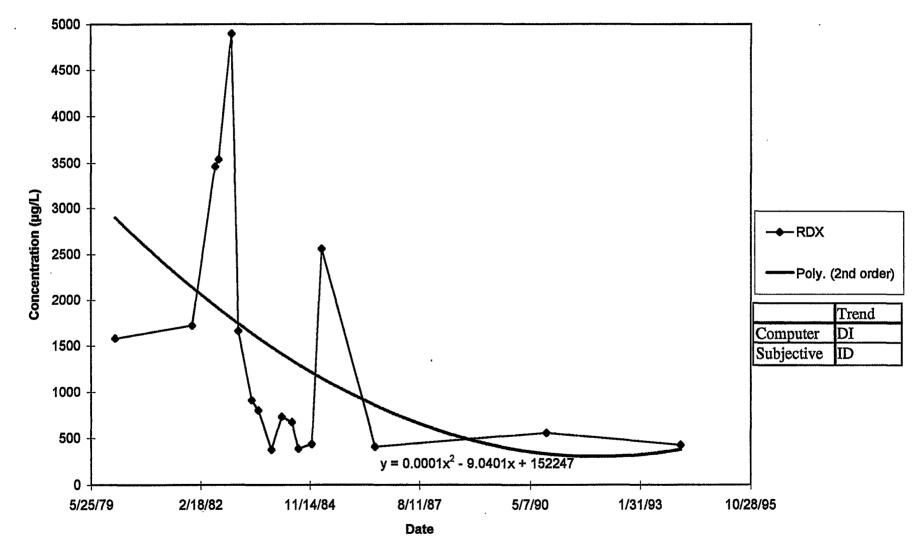
Data are presented for the following nine contaminants of concern (COCs):

- RDX
- HMX
- 2,4,6-trinitrotoluene (2,4,6-TNT)
- 1,3-dinitrobenzene (1,3-DNB)
- 2,4-dinitrotoluene (2,4-DNT)
- 2,6-dinitrotoluene (2,6-DNT)
- 1,3,5-trinitrobenzene (1,3,5-TNB)
- nitrobenzene (NB), and Tetryl.

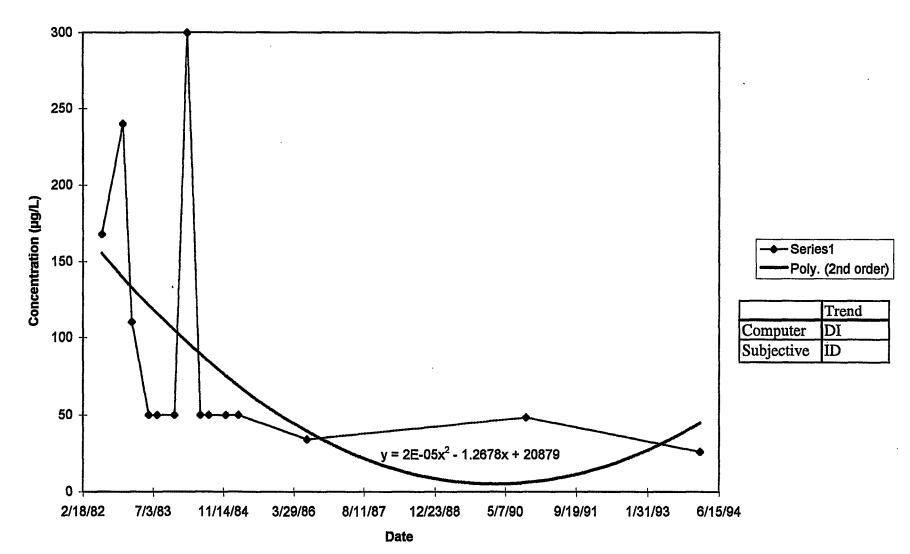
For each plot, a line joining each of me data points (Series 1), and the computerdetermined regression curve which best fits the data (Series 1 linear or 2nd order quadratic) is shown. Both the computer- determined and subjective trends (D, ID, I, DI, or C) selected for that data set are provided. The no model (NM) was selected for the subjective determination only. An equation for each of me regression curves is provided also.

Statistical Trend Analysis: RDX - Well G0009

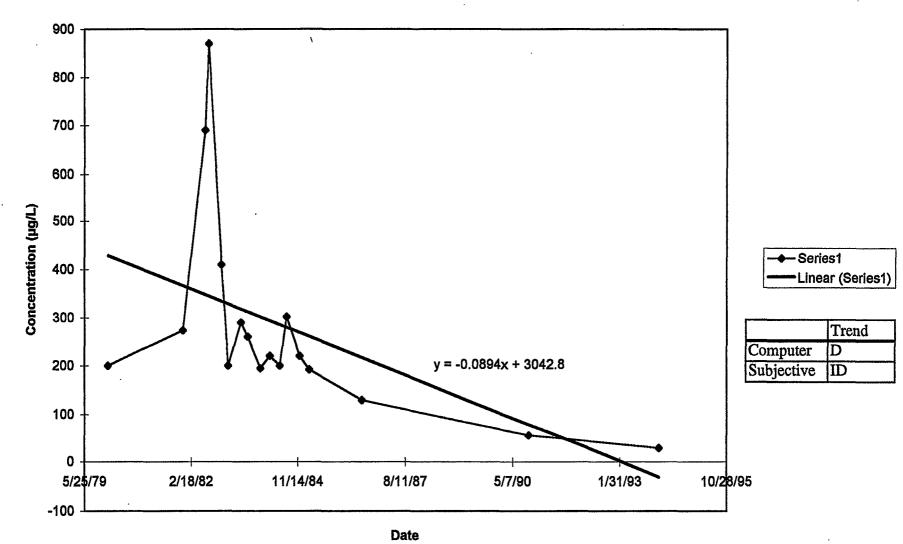
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Statistical Trend Analysis: HMX - Well G0009

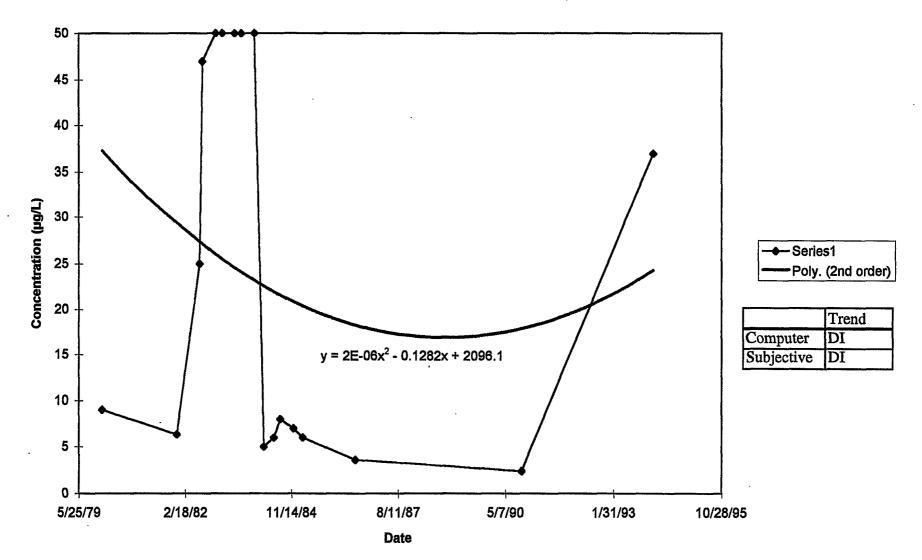


## Statistical Trend Analysis: 2,4,6-TNT - Well G0009



Statistical Trend Analysis: 2,4-DNT - Well G0009

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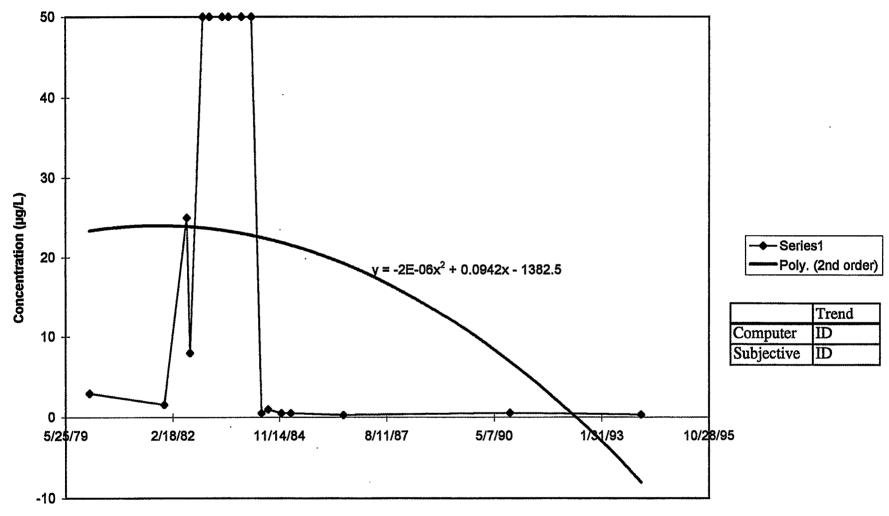


D4

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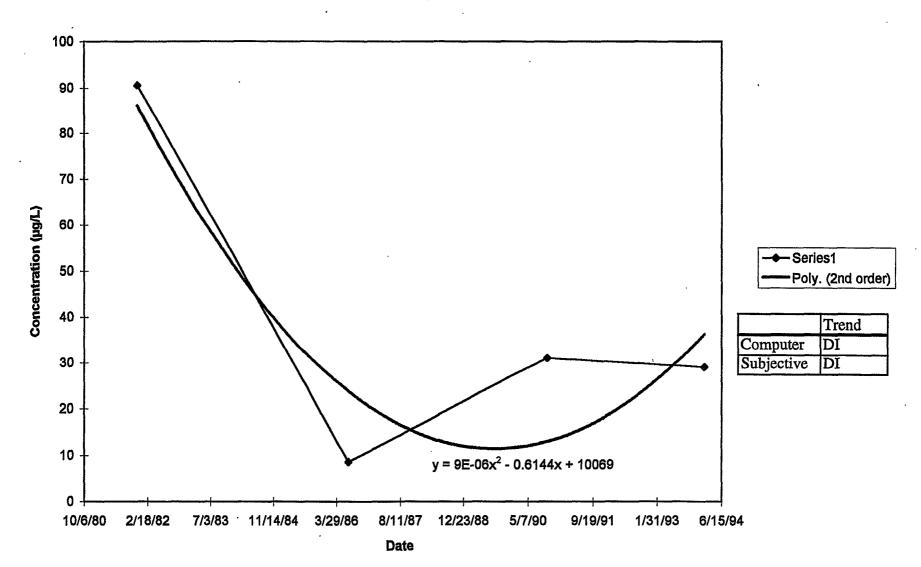
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Statistical Trend Analysis: 2,6-DNT - Well G0009



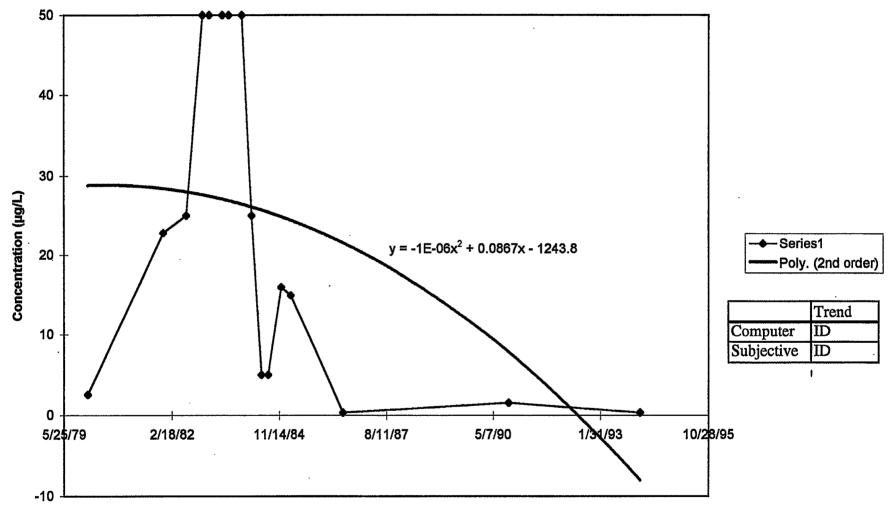
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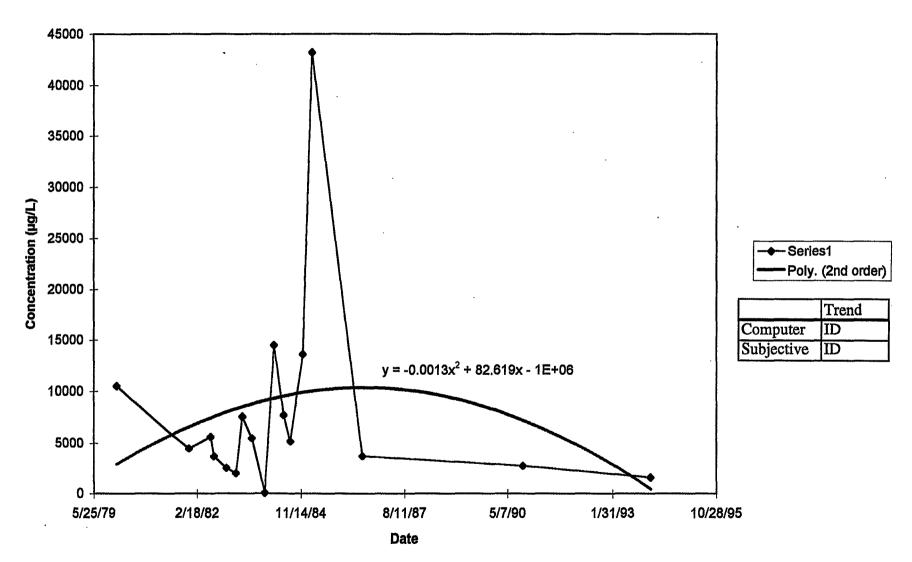


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Statistical Trend Analysis: Tetryl - Well G0009

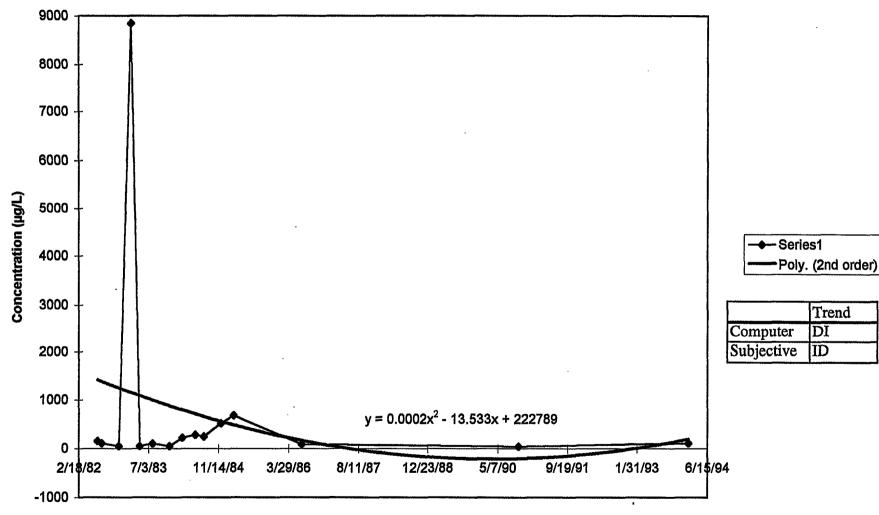


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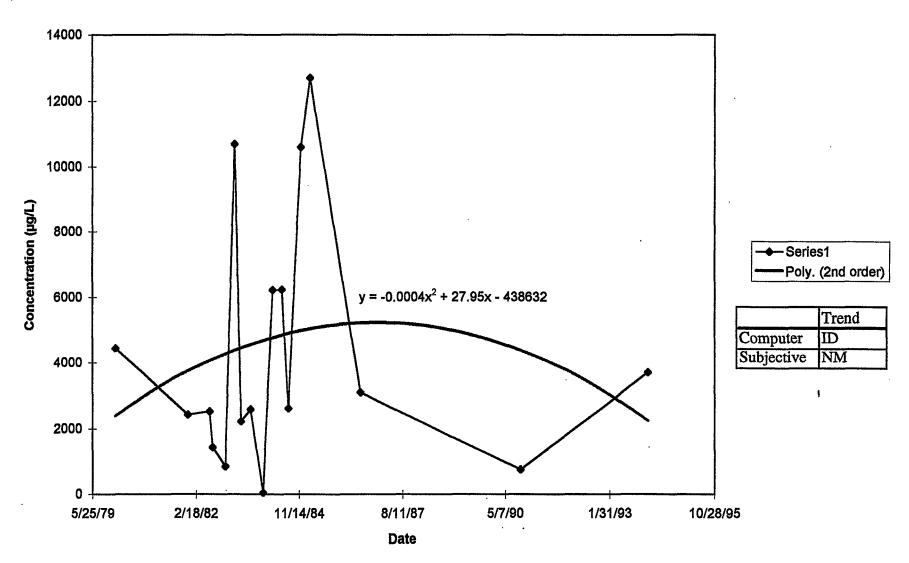
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Statistical Trend Analysis: HMX - Well G0012

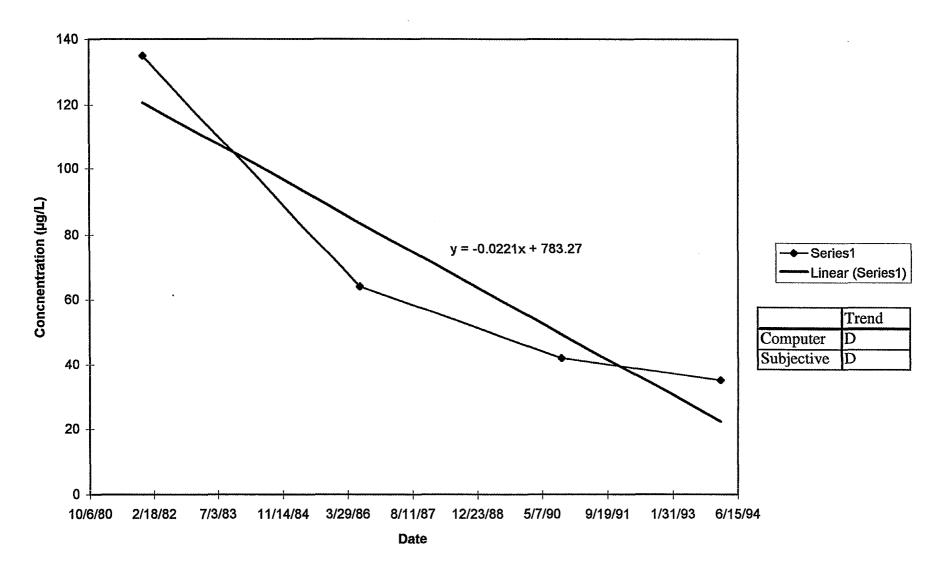


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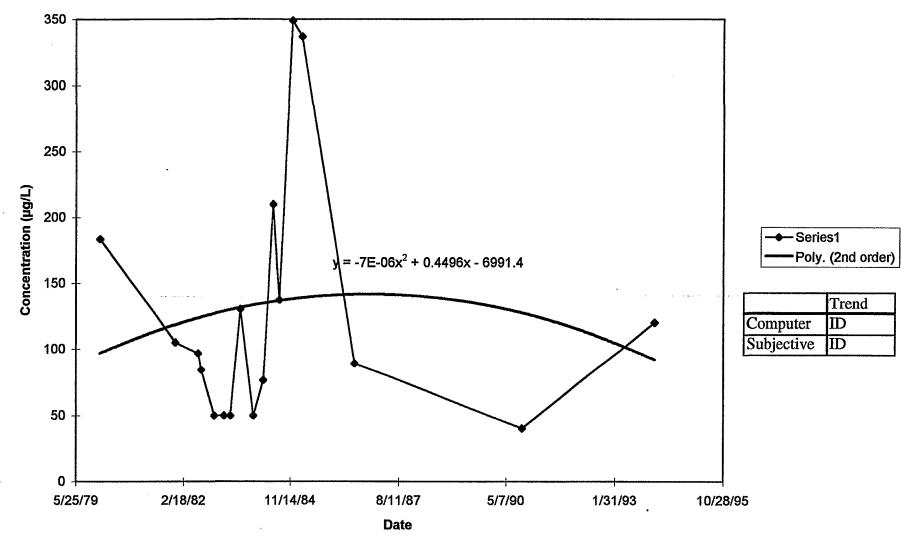
Statistical Trend Analysis: 2,4,6-TNT - Well G0012



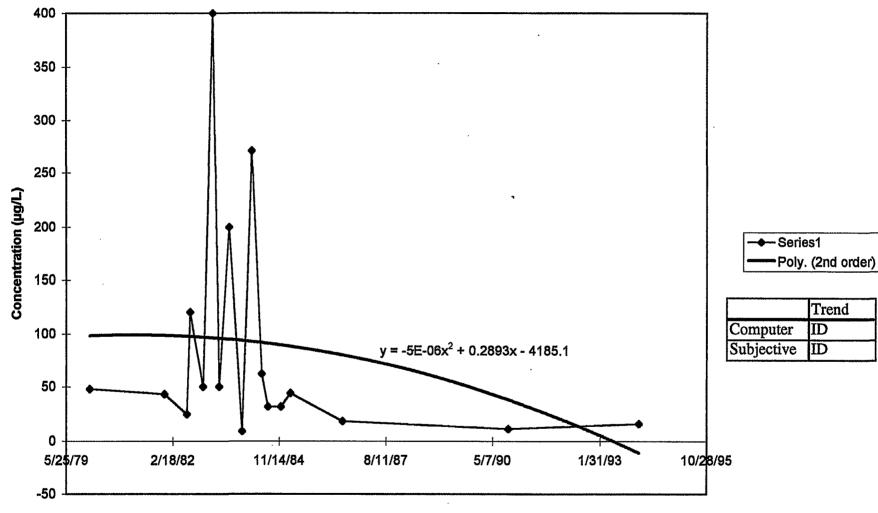
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Statistical Trend Analysis: 2,4-DNT - Well G0012

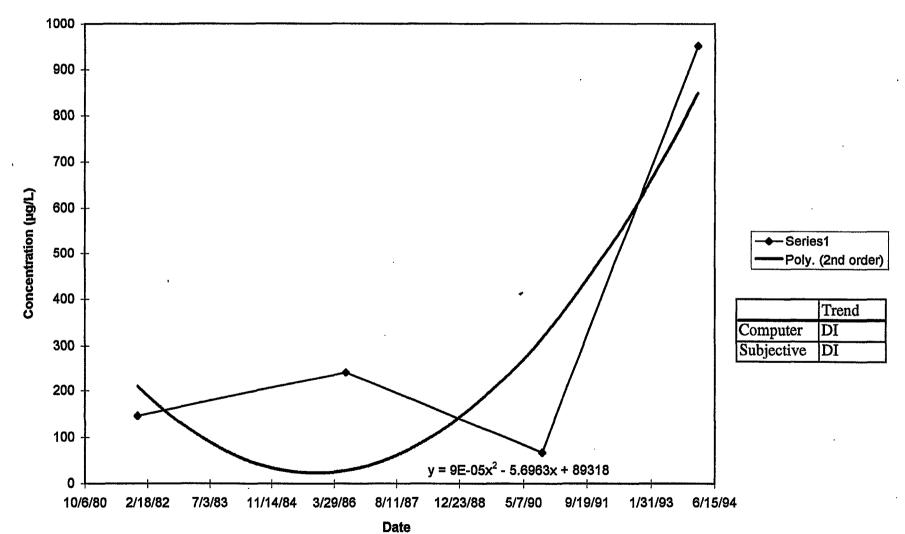


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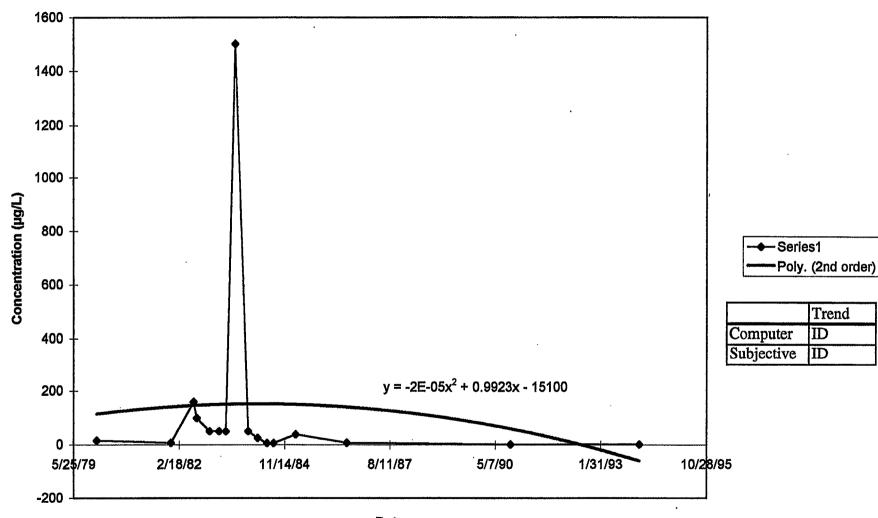


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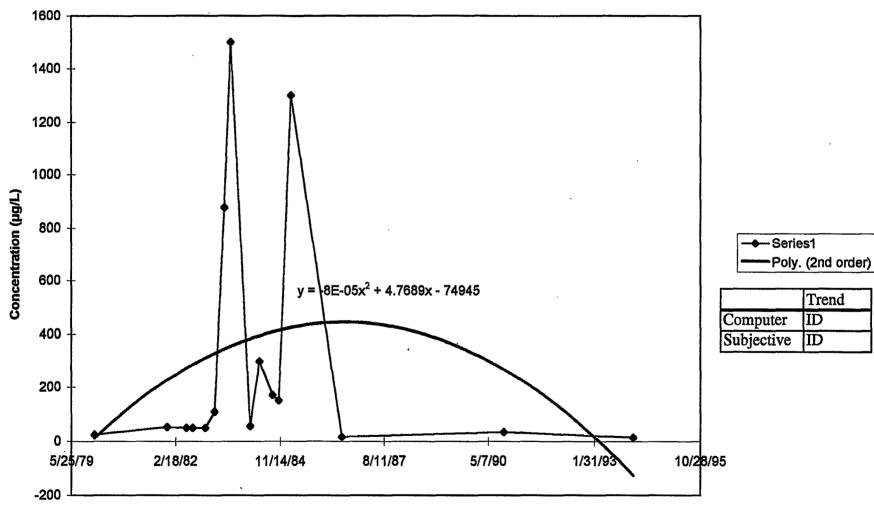
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### Statistical Trend Analysis: Tetryl - Well G0012

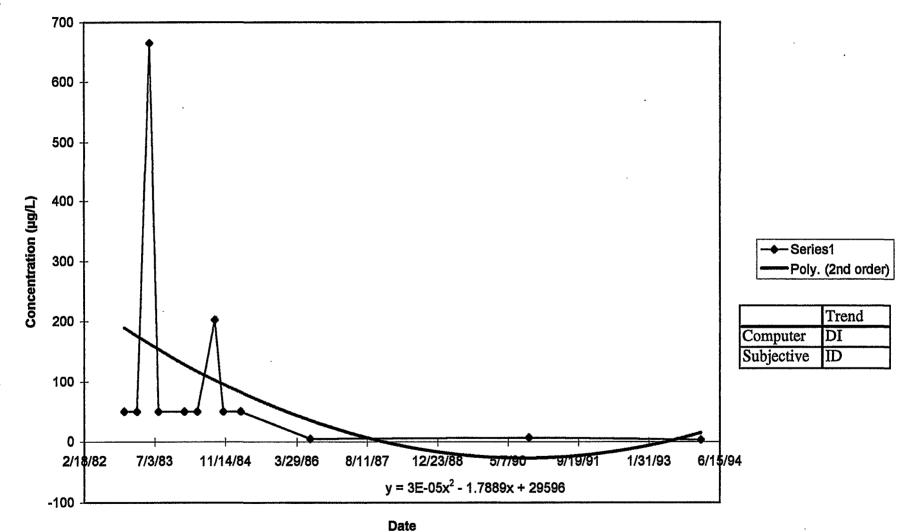


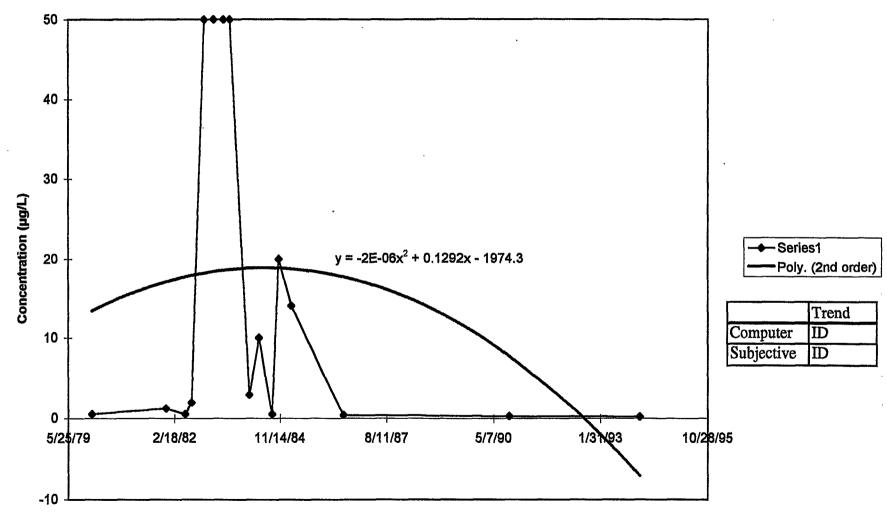
Statistical Trend Analysis: RDX - G0014



Date

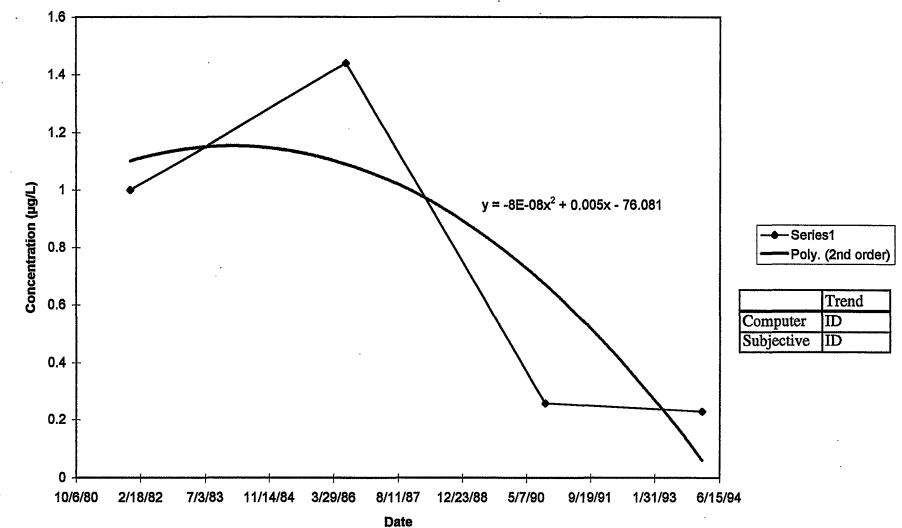
Statistical Trend Analysis: HMX - Well G0014



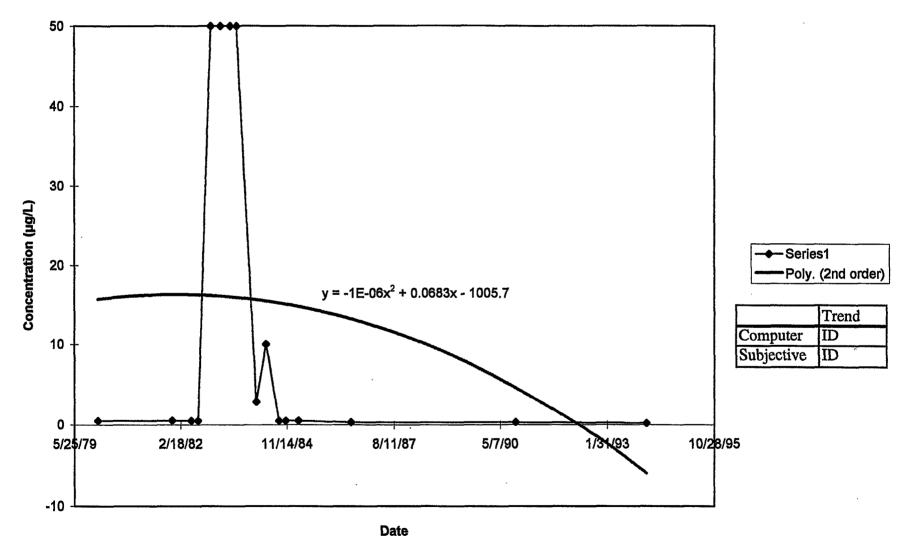


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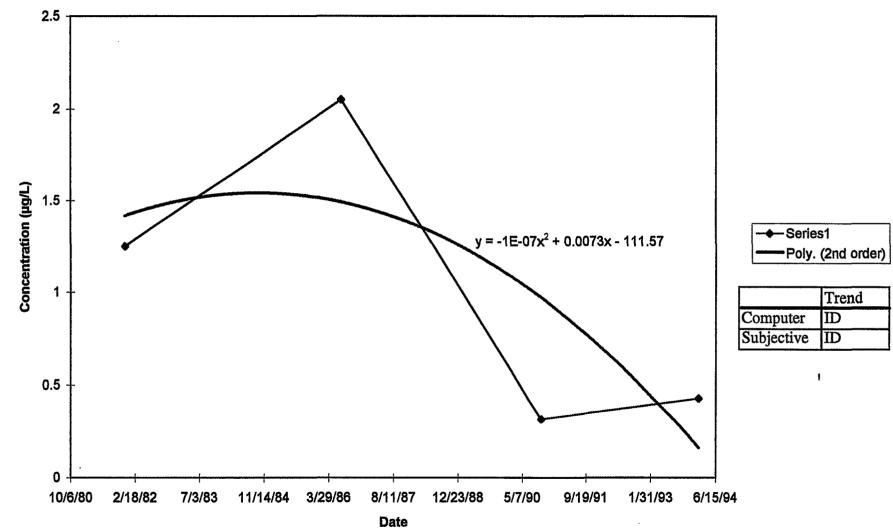
#### Statistical Trend Analysis: 1,3-DNB - Well G0014



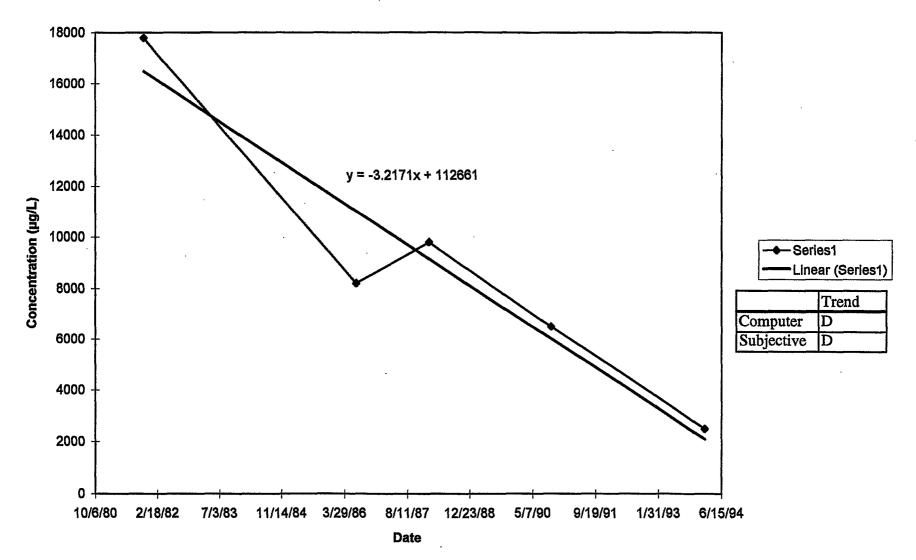
Statistical Trend Analysis: 2,4-DNT - Well G0014





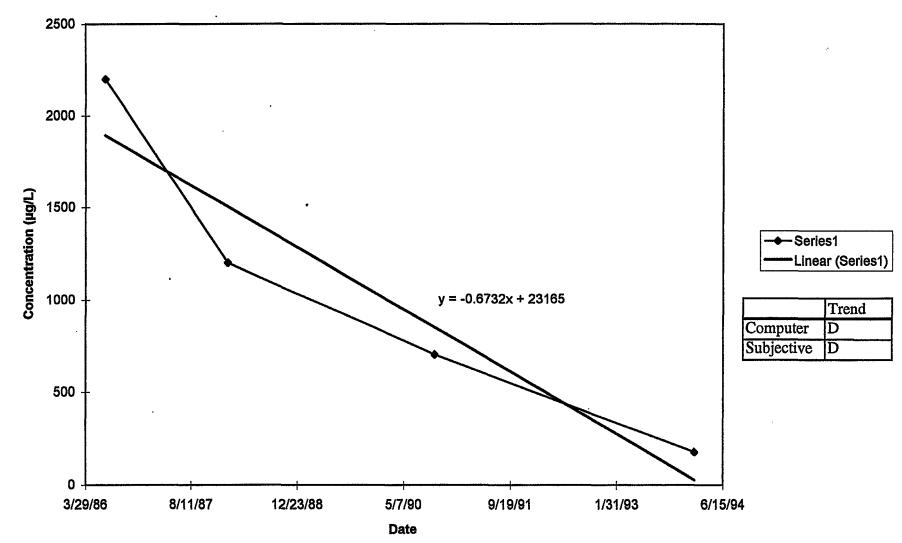


Statistical Trend Analysis: RDX - G0068

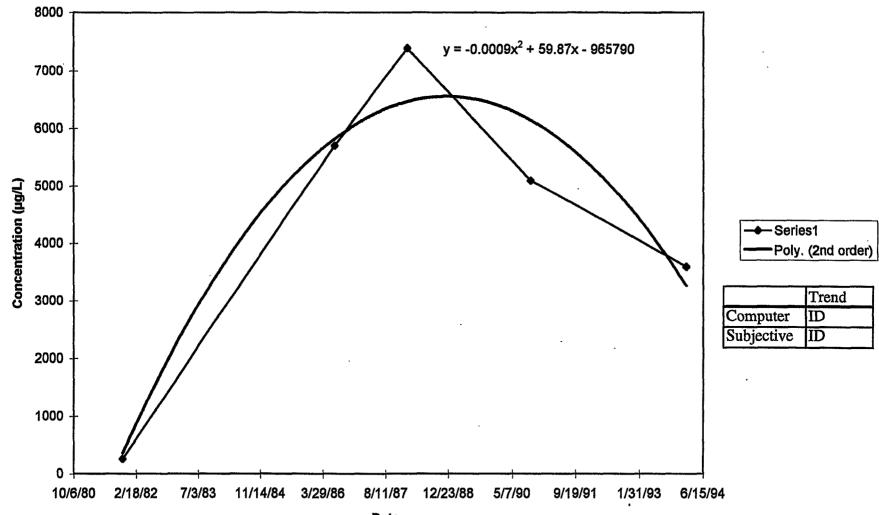


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Statistical Trend Analysis: HMX - Well G0068

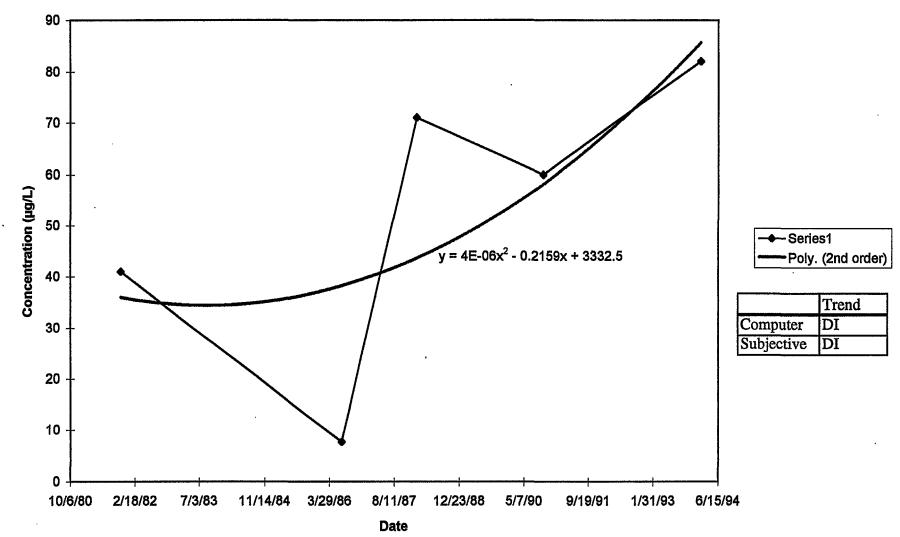


Statistical Trend Analysis: 2,4,6-TNT - Well G0068

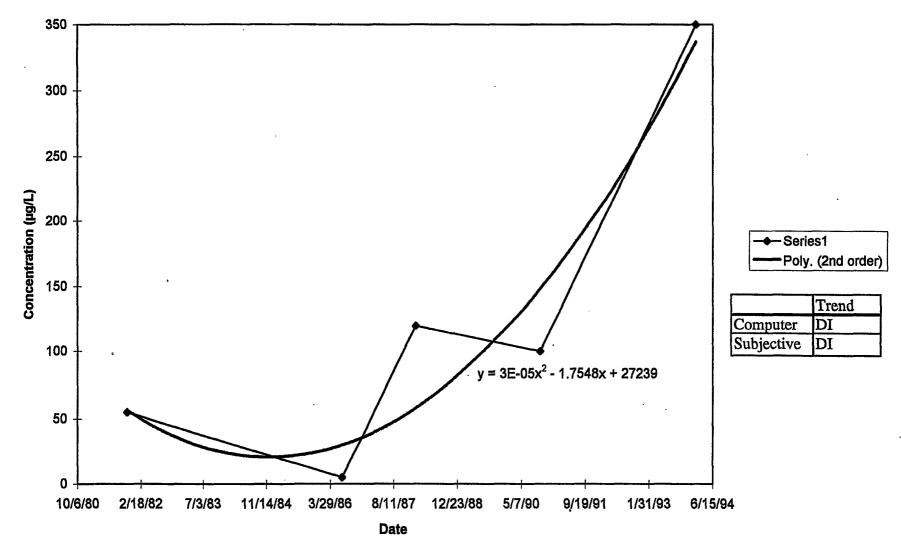


Date

Statistical Trend Analysis: 1,3-DNB - Well G0068

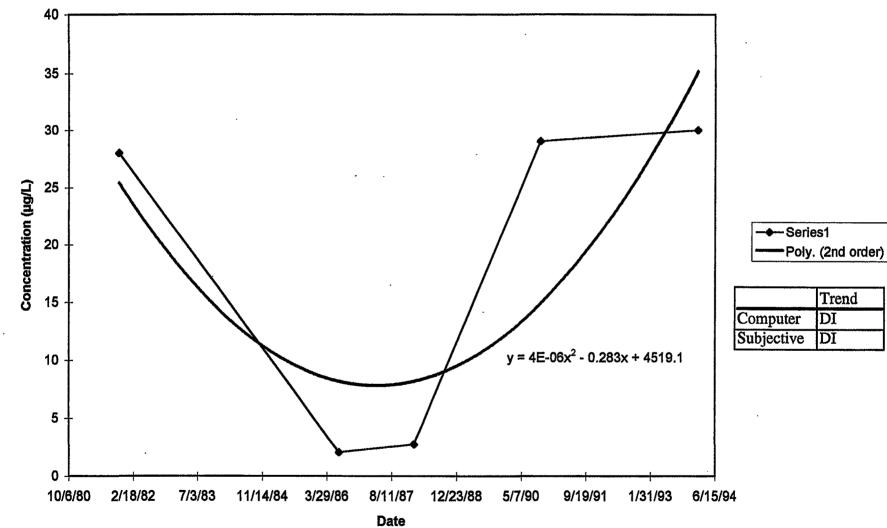


Statistical Trend Analysis: 2,4-DNT - Well G0068

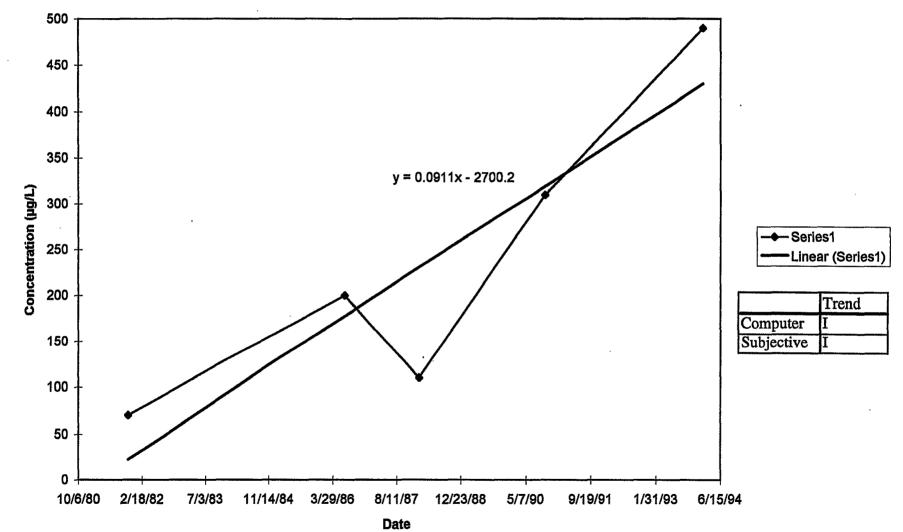


Statistical Trend Analysis: 2,6-DNT - Well G0068

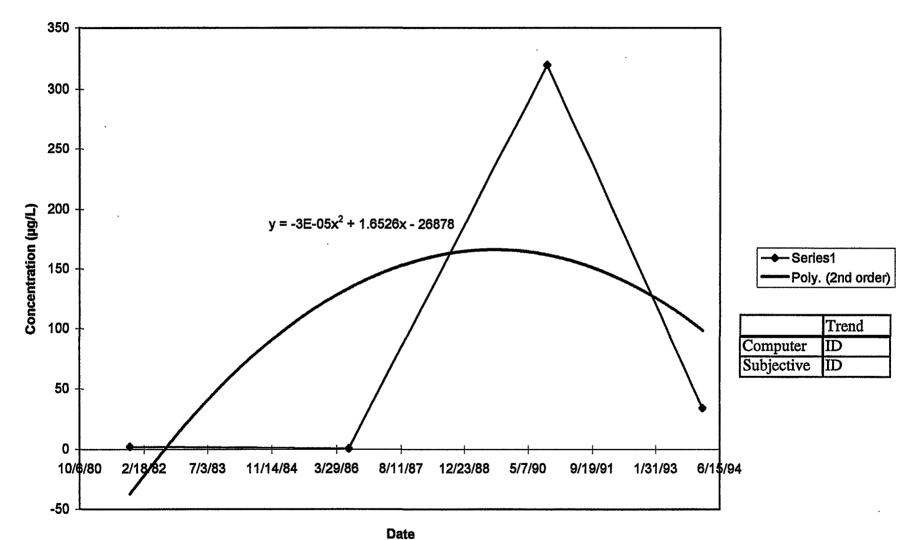
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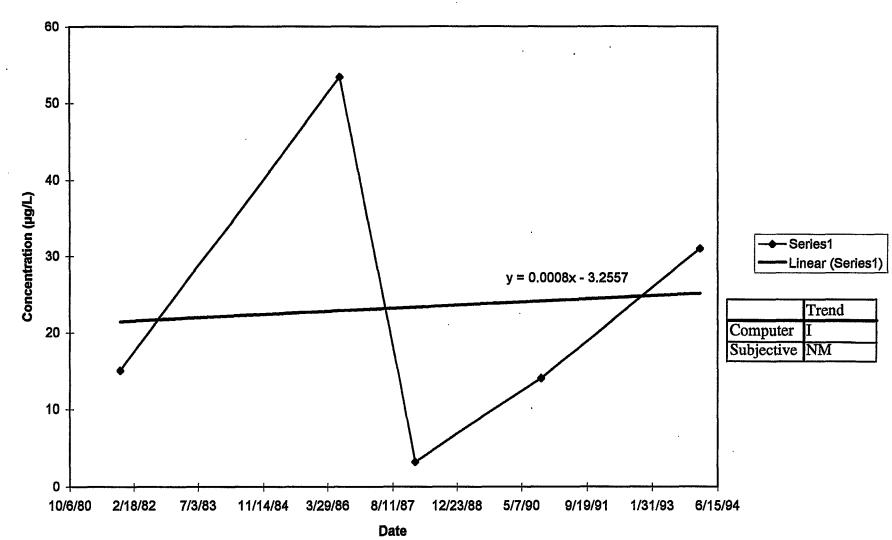
Statistical Trend Analysis: 1,3,5-TNB - Well G0068



Statistical Trend Analysis: NB - Well G0068

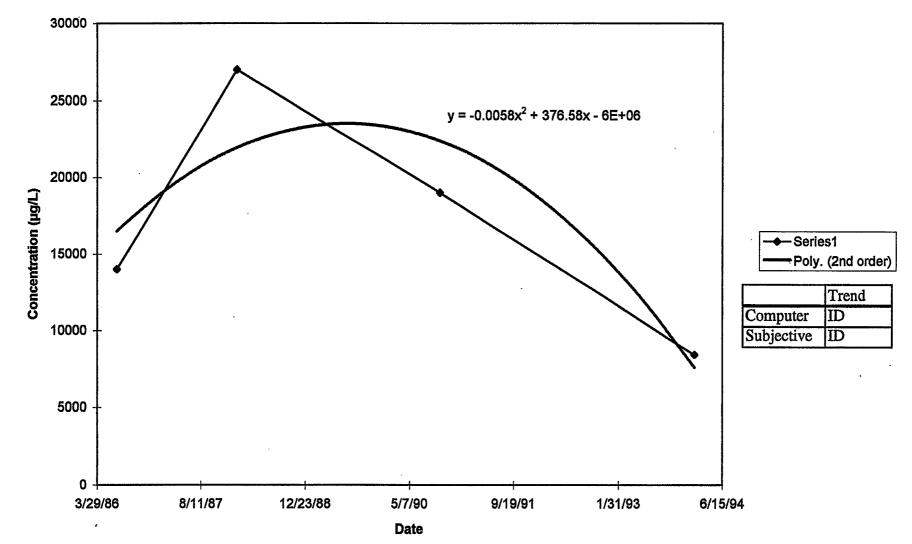


Statistical Trend Analysis: Tetryl - Well G0068

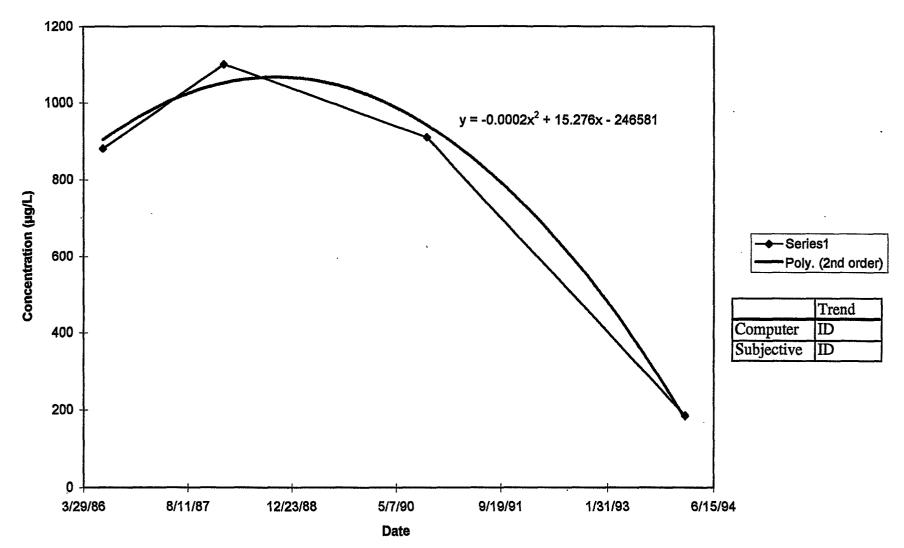


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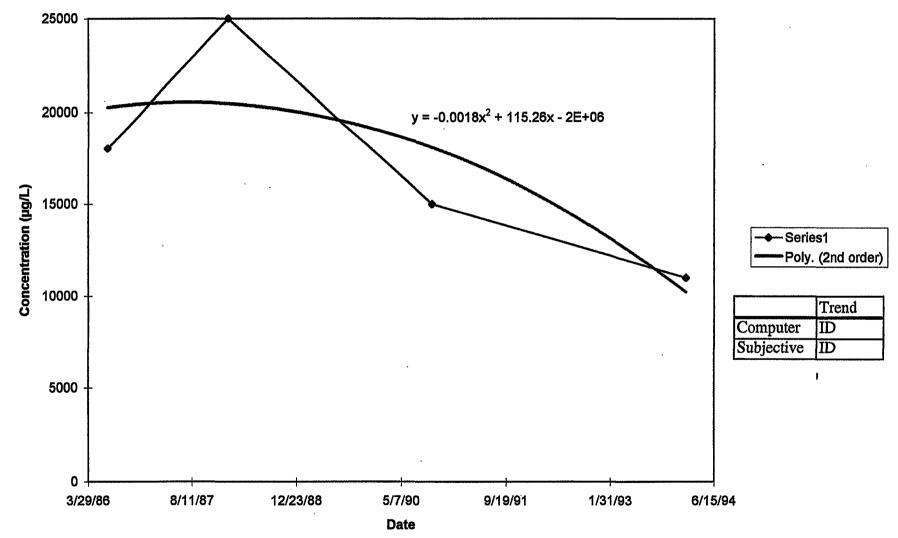
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Statistical Trend Analysis: HMX - Well G0104

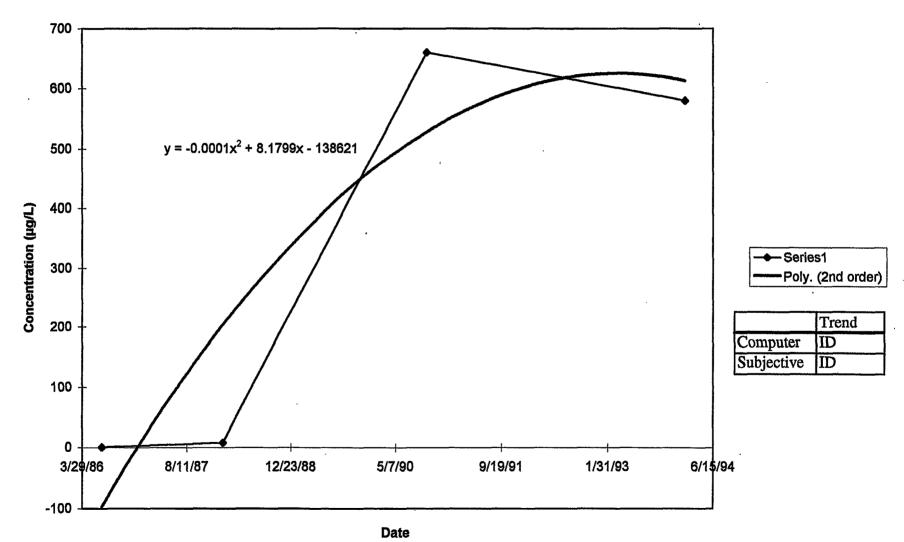


Statistical Trend Analysis: 2,4,6-TNT - Well G0104

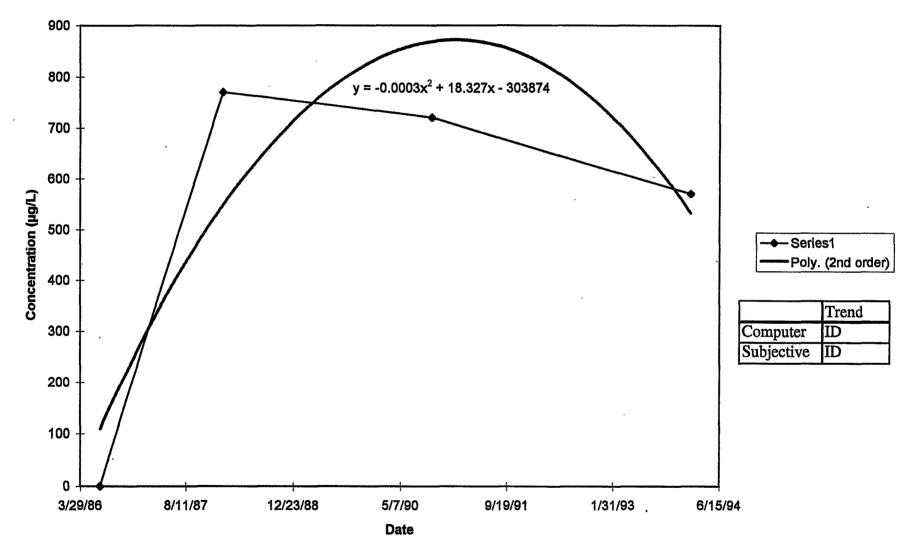


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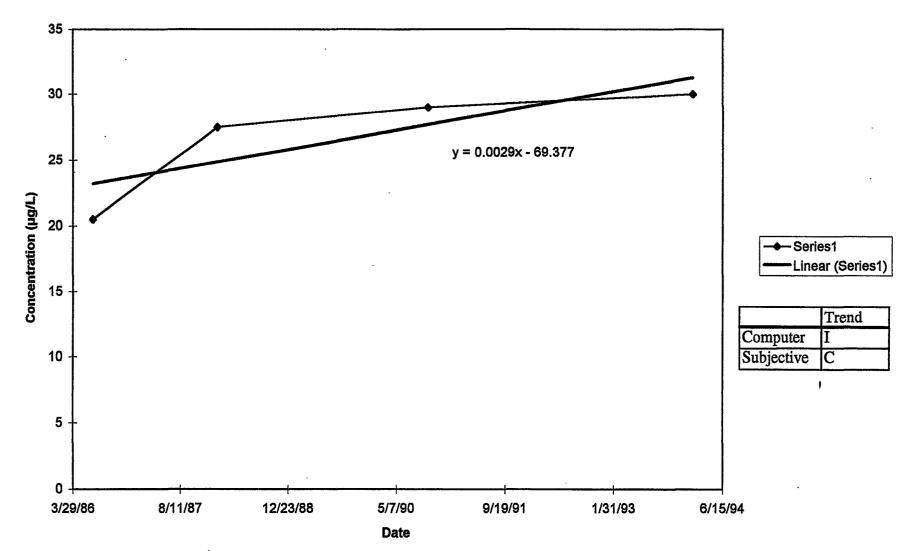
Statistical Trend Analysis: 1,3-DNB - Well G0104



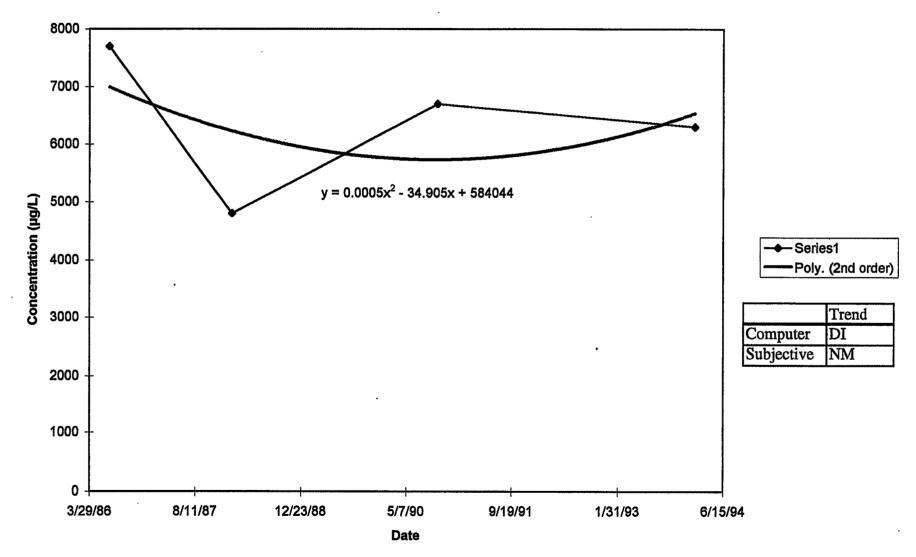
Statistical Trend Analysis: 2,4-DNT - Well G0104



Statistical Trend Analysis: 2,6-DNT - Well G0104

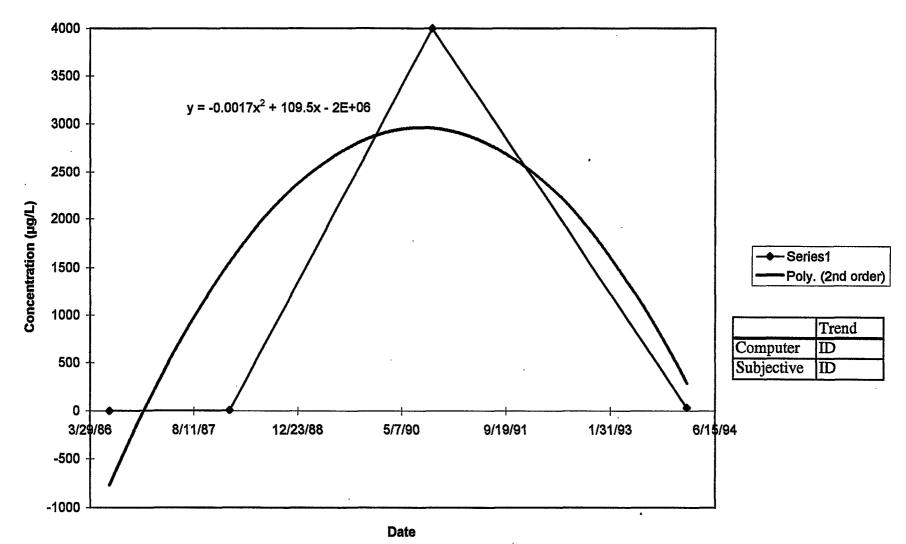


Statistical Trend Analysis: 1,3,5-TNB - Well G0104

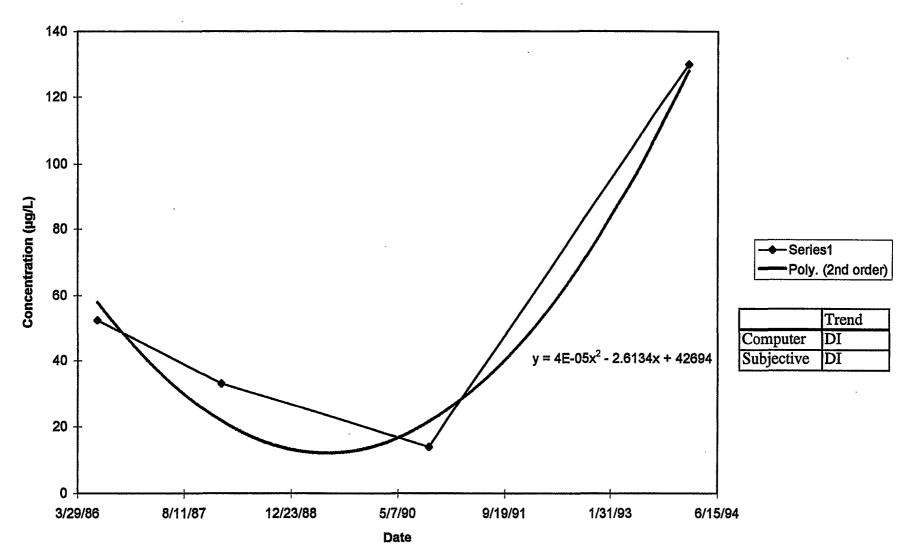


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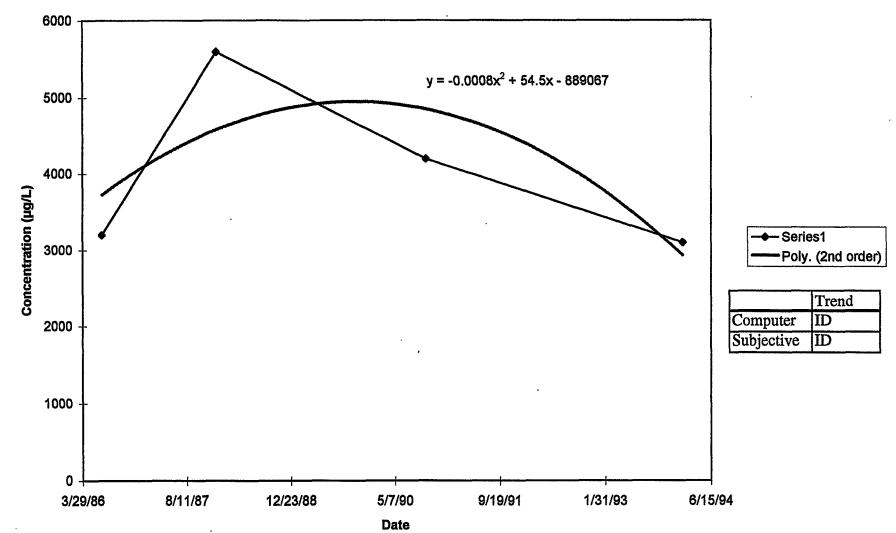
Statistical Trend Analysis: NB - Well G0104



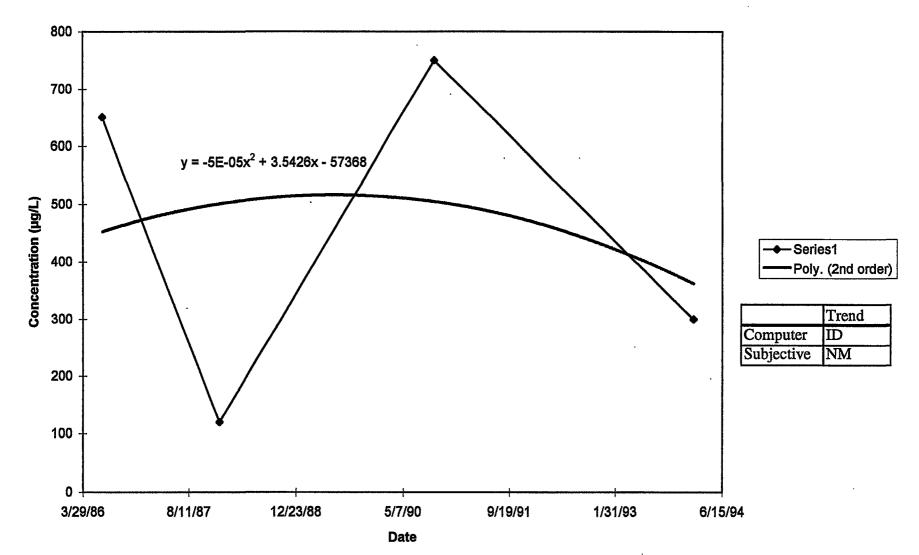
Statistical Trend Analysis: Tetryl - Well G0104



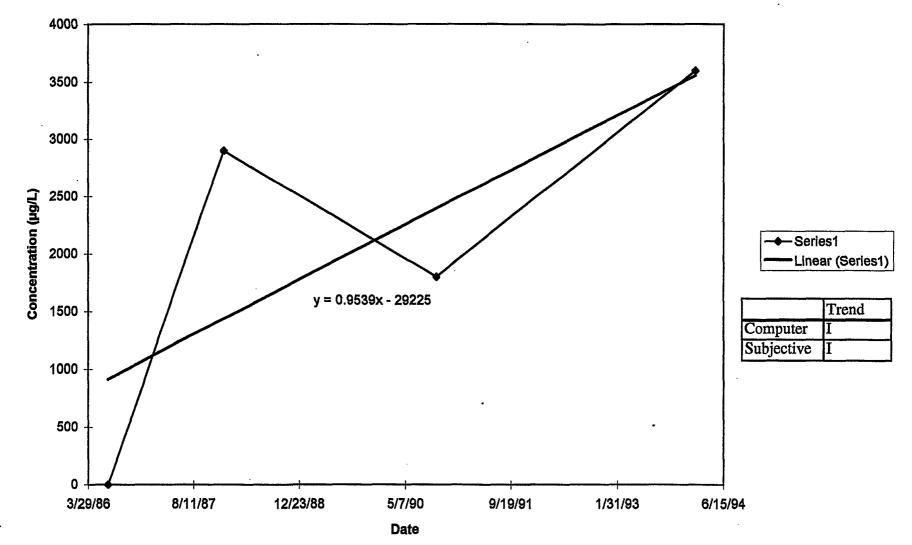
Statistical Trend Analysis: RDX - Well G0109



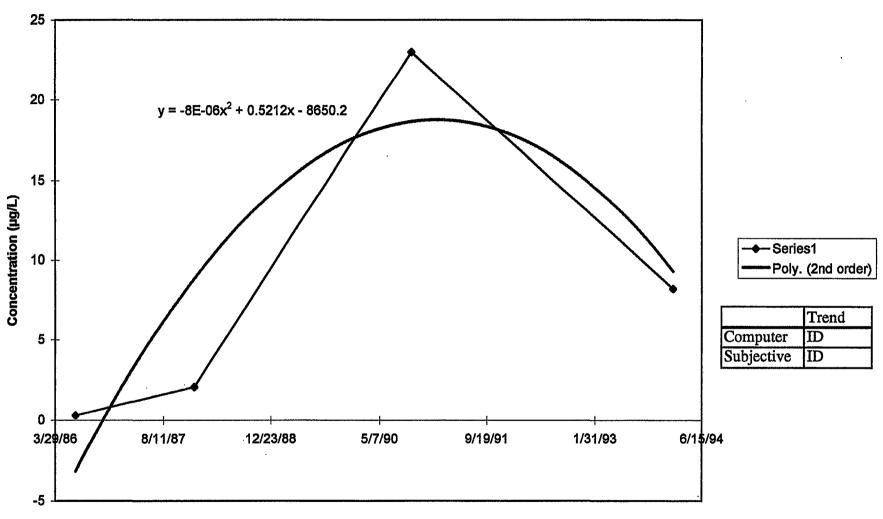
Statistical Trend Analysis: HMX - Well G0109



Statistical Trend Analysis: 2,4,6-TNT - Well G0109

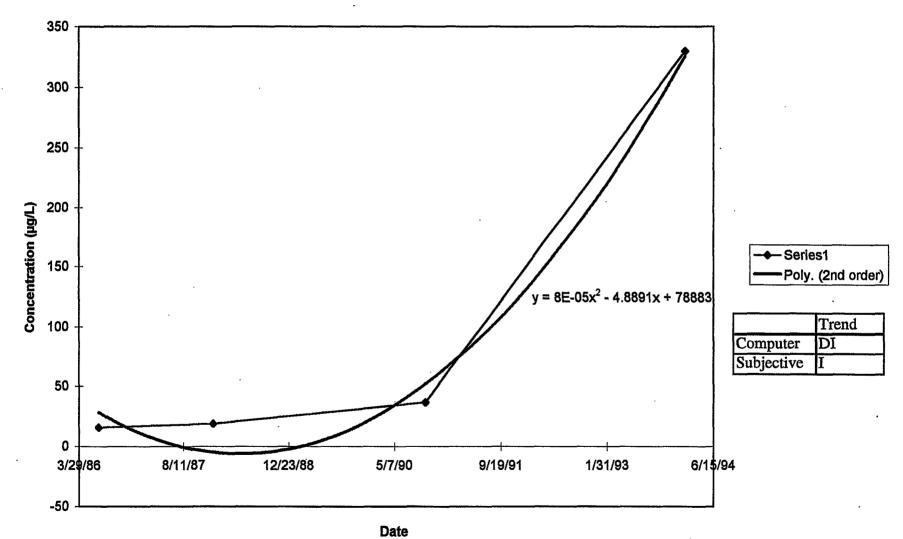


# Statistical Trend Analysis: 1,3-DNB - Well G0109

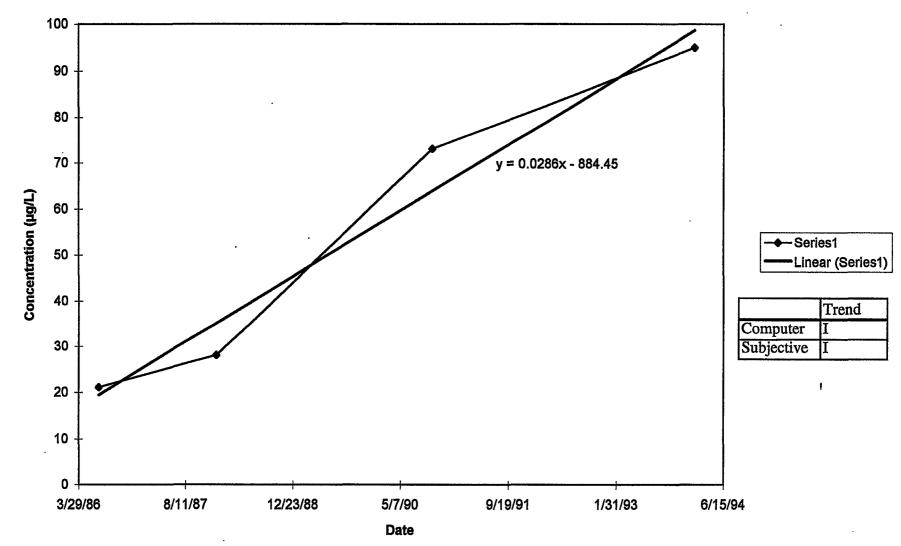


Date

Statistical Trend Analysis: 2,4-DNT - Well G0109

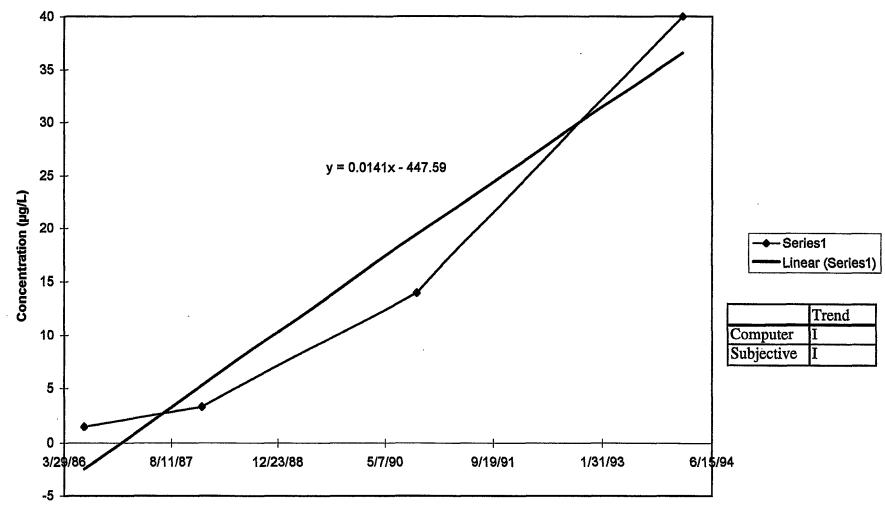


Statistical Trend Analysis: 1,3,5-TNB - Well G0109



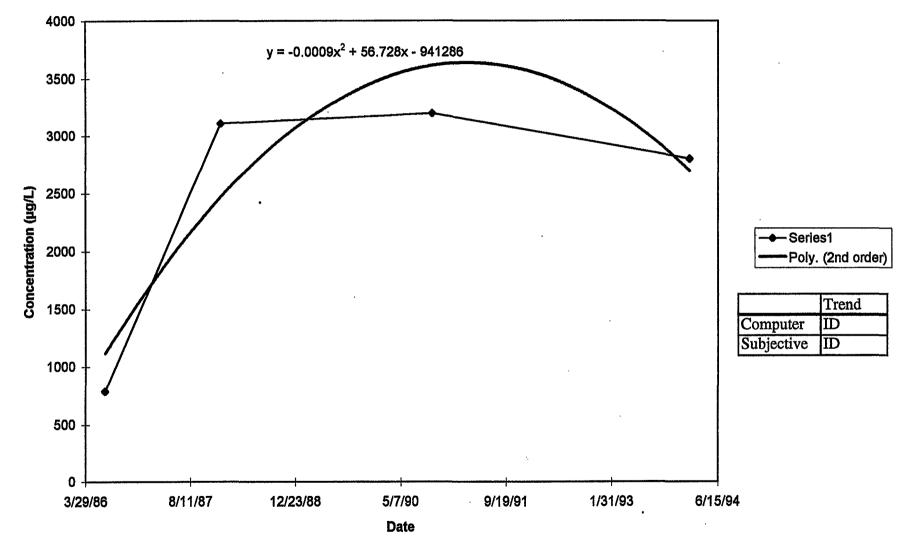
Statistical Trend Analysis: Tetryl - Well G0109

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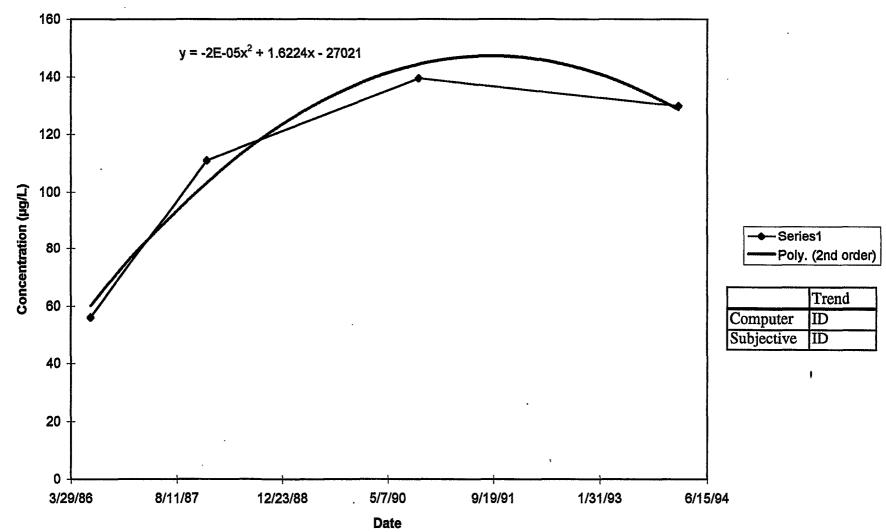


Date

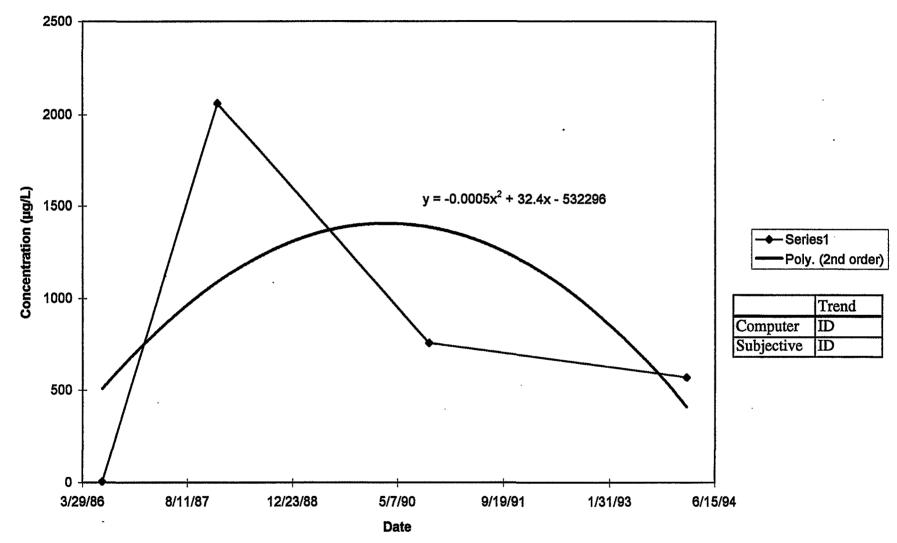
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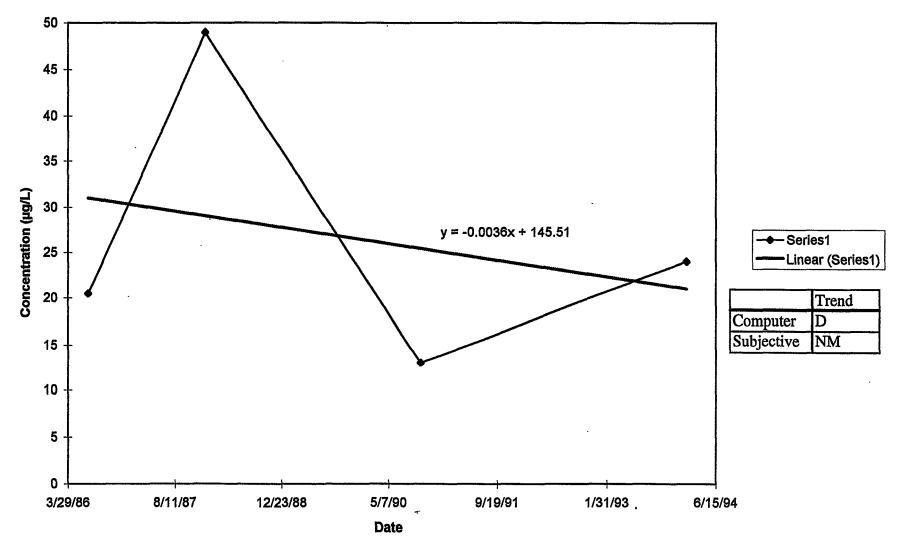


Statistical Trend Analysis: HMX - Well G0110

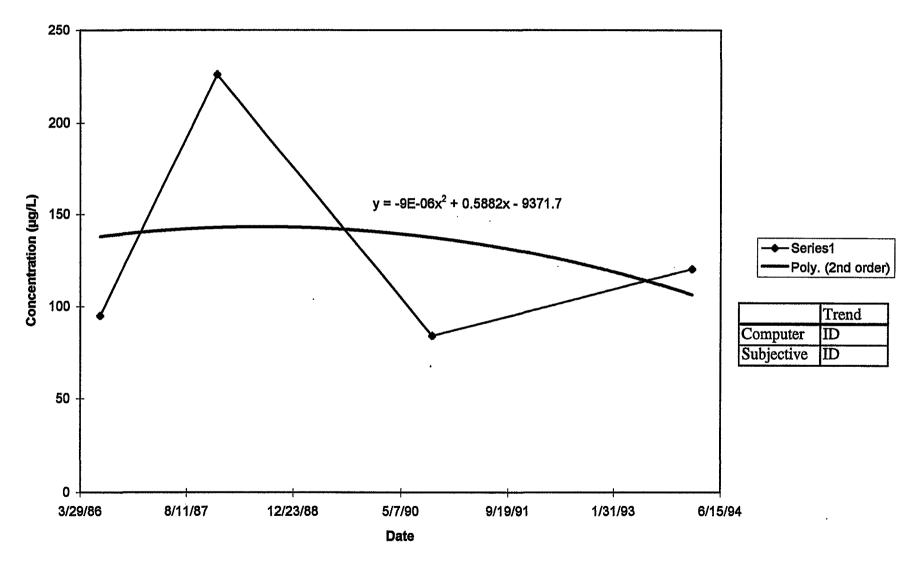


Statistical Trend Analysis: 2,4,6-TNT - Well G0110

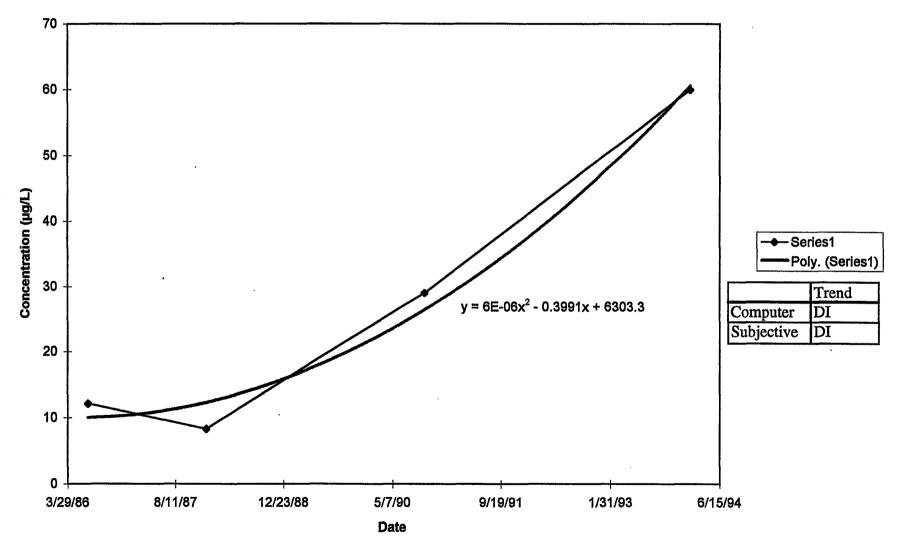




Statistical Trend Analysis: 2,4-DNT - Well G0110



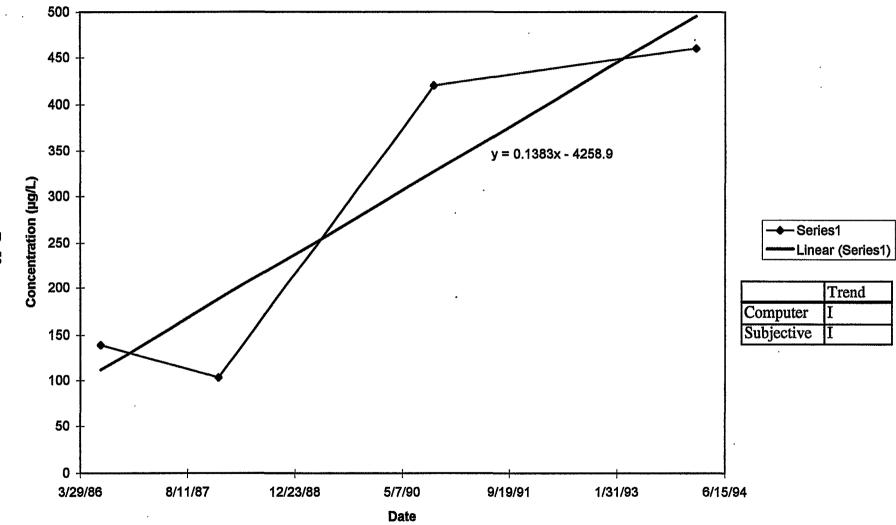
Statistical Trend Analysis: 2,6-DNT - Well G0110



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Statistical Trend Analysis: 1,3,5-TNB - Well G0110

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APPENDIX E TREND ANALYSIS SUPPORTING DATA

#### APPENDIX E TREND ANALYSIS SUPPORTING DATA

This appendix contains supporting data for the trend index (TI) values presented in the report and other related tables. The following tables are provided in this appendix:

Table E-1. Trend Index Calculations by Well

Table E-2. Trend Index Calculations by Well (within cap)

Table E-3. Trend Index Calculations by Well (outside cap)

Table E-4. Trend Index Calculations by Contaminants

Table E-5. Subjective Trends in Groundwater Quality

Table E-6. Estimated Dates of Minimum Concentrations in DI Trends

#### TABLE E-1. TREND INDEX CALCULATIONS BY WELL FIVE YEAR REVIEW REPORT LOUISIANA ARMY AMMUNITION PLANT

Well No.	NIM	Ρ	NS	ΤΑ	NC	)ET		NI		ISTA-NDET	VALID DA	TA SETS
	w/o HAL	All	w/o HAL	All	w/o HAL	All	w/o HAL	All	w/o HAL	All	w/o HAL	All
Upper Terrace	9											
GO-009	1	3	0	0	2	4	2	2	-1	1	3	
GO-012*	6	6	0	0	2	2	1	1	4	4	8	
GO-014*	3	5	0	0	0	1	3	3	3	4	3	
GO-068	3	4	0	0	3	5	0	0	0	-1	6	
GO-083								9		0		
GO-084								9		0		
GO-085								9		Ó		
GO-104*	5	6	0	0	2	3	0	0	3	3	7	
GO-109	2	3	0	0	2	4	2	2	0	1	4	
TOTAL	20	27	0	0	11	19	8	35	9	8	31	
Lower Terrace	e/Sparta Sand	•										
GO-105*								9		0		
GO-106*	{							9		0		
GO-110	4	5	0	0	1	2	2	2	3	3	5	
TOTAL	4	5	0	0	1	2	2	20	3	3	5	

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NOTE: Asterisk (*) denotes wells located outside the cap. HAL - Drinking Water Health Advisory Level

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### TABLE E-2. TREND INDEX CALCULATIONS BY WELL (WITHIN CAP)FIVE YEAR REVIEW REPORT LOUISIANA ARMY AMMUNITION PLANT

Well No.	NIM	1P	NS [.]	ΓA I	ND	ET	U	NI	TI=NIMP+N	ISTA-NDET		
	w/o HAL	All	w/o HAL	All	w/o HAL	All	w/o HAL	All	w/o HAL	All	w/o HAL	All
Upper Terrace	Э										· · · · · · · · · · · · · · · · · · ·	
GO-009	1	3	0	0	2	4	2	2	-1	. –1	3	
GO-068	3	4	0	0	3	5	0	0	0	-1	6	
GO-083						——		9		0		
GO-084								9		0		
GO-085								9		0		
GO-109	2	3	0	0	2	4	2	2	0	<u>`                                    </u>	4	
TOTAL	6	10	0	0	7	13	4	31	-1	-3	13	
Lower Terrace	e/Sparta Sand	Ł										
GO-110	4	5	0	0	. 1	2	2	2	. 3	3	5	
		5	0	0		2	2	2	3	3	5	

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# TABLE E-3. TREND INDEX CALCULATIONS BY WELL (OUTSIDE CAP)FIVE YEAR REVIEW REPORTLOUISIANA ARMY AMMUNITION PLANT

Well No.	NIM	IP	NS	TA	ND		UN	1	TI=NIMP+N	ISTA-NDET		
[	w/o HAL	All	w/o HAL	All	w/o HAL	All	w/o HAL	All	w/o HAL	All	w/o HAL	All
<b>Upper Terrace</b>												
GO-012	6	6	0	0	2	2	1	1	4	4	8	8
GO-014	3	5	0	0	0	1	3	3	3	4	3	6
GO-104	5	6	0	0	2	3	0	0	3	3	7	9
TOTAL	14	17	0	0	4	6	4	4	10	11	18	23
Lower Terrace	/Sparta Sanc	i										
GO-105			——					9		0		0
GO-106								9		0		0
ΤΟΤΑL	0	0	0	0	0	0	0	18	0	0	0	0

Note: HAL – Drinking Water Health Advisory Level

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# TABLE E-4. TREND INDEX CALCULATIONS BY CONTAMINANTSFIVE YEAR REVIEW REPORTLOUISIANA ARMY AMMUNITION PLANT

Well No.	NIM	<b>&gt;</b>	NST	A	ND	ÊT	U	NI	TI=NIMP+N	STA-NDET	ET VALID DATA SETS	
	w/o HAL	All	w/o HAL	All	w/o HAL	All	w/o HAL	All	w/o HAL	All	w/o HAL	All
DNB	4	5	0	0	1	1	6	6	3	4	5	. 6
2,4-DNT	3	4	0	0	1	3	5	5	2	1	4	7
2,6-DNT	1	2	0	0	0	3	7	7	1	-1	1	5
HMX	1	4	0	0	1	3	5	5	0	1	2	7
NB	1	2	0	0	0	0	10	10	1	2	1	2
RDX	6	6	0	0	1	1	5	5	5	5	7	7
TETRYL	1	2	0	0	1	3	7	7	0	-1	2	5
TNB	1	1	0	0	6	6	5	5	-5	-5	7	7
TNT	6	6	0	0	1	1	5	5	5	5	7	7
TOTAL	24	32	0	0	12	21	55	55	12	11	36	53

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Note: HAL - Drinking Water Health Advisory Level

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#### 07-Jul-94

Aquifer				Uppe	r Terrace A	Aquifer			-	Lower Terrace/Sparta Sand Aquifer			
Contaminant/Well	009	012*	014*	068	083	084	085	104*	109	105*	106*	110	
1,3-DNB	Z	D	ID	DI	Z	Z	Z	ID	ID	Z	Z	NM	
2,4-DNT	Dl	ID	ID	DI	Z	Z	Z	ID	I	Z	Z	ID	
2,6-DNT	ID	ID	ND	DI	Z	Z	Z	C	ND	Z	Z	DI	
НМХ	D	D	D	D	Z	Z	Z	ID	NM	Z	z	ID	
Nitrobenzene	ND	ND	ND	ID	Z	Z	Z	ID	ND	Z	Z	Z	
RDX	ID	ID	ID	D	Z	Z	Z	ID	ID	Z	Z	ID	
Tetryl	ID	ID	ND	NM	Z	z	Z	DI	I	Z	Z	Z	
1,3,5-TNB	DI	DI	ID	I	Z	z	Z	NM	I	Z	Z	Ι	
2,4,6-TNT	D	NM	ID	ID	Z	Z	Z	ID	I	Z	Z	ID	
Trend Index (TI) W/O HAL ALL DATA	+1/3 +3/7	+5/8 +5/8	+3/3 +6/6	0/6 0/9	0/0 0/0	0/0 0/0	0/0 0/0	+4/7 +6/9	0/4 -2/7	0/0 0/0	0/0 0/0	+2/5 +2/7	

#### Table E-5. Subjective Trends in Groundwater Quality

OTI for Upper Terrace Aquifer w/o HAL +13/30

All data

+18/46

OTI for Lower Terrace w/o HAL +2/5 All data +2/7

#### Table E-5. Subjective trends in groundwater quality (continued)

Note: Shaded areas indicate concentration levels for the contaminant in that monitoring well were below the Health Advisory Level established for that contaminant at LAAP. Trends in bold indicate discrepancy with the computer- determined trend. An asterisk 0 denotes wells located outside the capped area. Trend index (TI) is presented for all data, and for data excluding the data sets with concentrations below HALs (w/o HAL).

OTI - Overall Trend Index HAL - Health Advisory Level

Trend Index, TI = NIMP + NSTA - NDET

where,

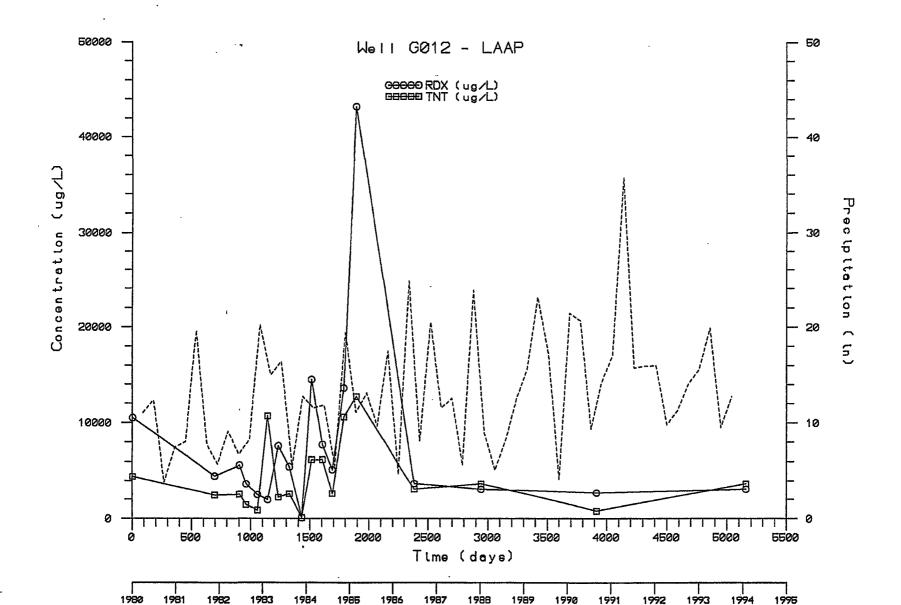
NIMP is number of improving conditions (ID and D) NSTA is number of static conditions (C) NDET is number of deteriorating conditions (DI and I).

Well No.	Contaminant	Estimated Minimum Concentration Date
G0009	RDX HMX 2,4-DNT 1,3,5-TNB	April 1991 <b>May 1990 July 1989</b> August 1989
G0012*	HMX 1,3,5-TNB	August 1989 November 1985
G0014*	НМХ	December 1999
G0068	DNB 2,4-DNT 2,6-DNT	August 1983 November 1984 <i>April 1987</i>
G0083	None	None
G0084	None	None
G0085	None	None
G0104*	Tetryl 1,3,5-TNB	June 1989 October 1990
G0109	2,4-DNT	May 1988
G0105*	None	None
G0106*	None	None
G0110	2,6-DNT	April 1986

Table E-6. Estimated dates of minimum concentration with DI trends

Notes: (*) denote monitoring wells located outside the Area P cap.

Italicized minima are for the contaminant levels below the Health Advisory Levels (HALs)



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APPENDIX F DATA QUALITY ASSESSMENT

#### APPENDIX F. DATA QUALITY ASSESSMENT

#### F.1 INTRODUCTION

A comprehensive quality assurance/quality control (QA/QC) program was followed during the Five-Year Review of Interim Remedial Action conducted at the Louisiana Army Ammunition Plant (LAAP) Former Area P Lagoons, located in Shreveport, Louisiana, to ensure that the analytical results and the decisions based on these results are representative of the environmental conditions at the site. The objectives of the Five-Year Review of the Area P Lagoons was to evaluate the effectiveness of the interim remedial measures. The following documents were used during evaluation of the quality control (QC) data: the U. S. Army Toxic and Hazardous Material Agency (USATHAMA) Quality Assurance Program, PAM 11-41 (January 1990) for groundwater samples; QC requirements detailed in guidelines and specifications described in the Quality Assurance Project Plans (QAPPs) submitted as part of the project work plans prepared by Science Applications International Corporation (SAIC); the Installation Restoration Data Management Information System (IBDMIS), Volume II Data Dictionary, Potomac Research Institute (PRI) (1994); and the U.S. Environmental Protection Agency's (EPA's) Laboratory Data Validation Functional Guidelines for Evaluating Organics Analysis (1988). The numbers of groundwater samples collected, in addition to the numbers of field QC samples collected and selected laboratory QC (i.e., matrix spikes and matrix spike duplicates) samples analyzed, are presented in Table F-1. The data review and validation worksheets are referenced within the subsection describing the applicable analysis. The QC checks and results are summarized below.

#### F.1.1 Data Quality Objectives

A comparison of the analytical results to the project data quality objectives (DQOs) as defined in the QAPP formed the basis for evaluating the quality of the analytical data. As described in the QAPP, analytical data must be of a known and acceptable quality in order to be used to evaluate site contamination at LAAP. DQOs are set to define and establish the criteria against which the fitness of the data will be judged. DQOs are quantitative and qualitative indicators of data quality. The DQO process is designed to ensure that the type,

# Table F-1. Analytical Methods and Total Number of Groundwater Samples Collected Louisiana Army Ammunition Plant

	ANALYTICAL	DETECTION					TOTAL
	METHOD	T TA /TT	WATER	REPLICATES	EQUIPMENT	MS/MSD	NUMBER
PARAMETER	METHOD	LIMIT	SAMPLES		BLANKS		OF ANALYSES
EXPLOSIVES							
1,3,5 - Trinitrobenzene	UW25	(a)	12	2	6	1/1	22
1,3 - Dinitrobenzene	UW25	(a)	12	2	6	1/1	22
2,4,6 - Trinitrotoluene	UW25	(a)	12	2	6	1/1	22
2,4 - Dinitrotoluene	UW25	(a)	12	2	6	1/1	22
2,6 - Dinitrotoluene	UW25	(a)	12	2	6	1/1	22
Cyclotetramethylenetetranitramine	UW25	(a)	12	2	6	1/1	22
Nitrobenzene	UW25	(a)	12	2	6	1/1	22
Hexahydro-1,3,5-trinitro-1,3,5-triazine	UW25	(a)	12	2	6	1/1	22
N-methyl-N,2,4,6-tetranitroanailine	UW25	(a)	12	2	6	1/1	22

(a) - Detection limits are matrix and sample specific. All certified reporting limits are listed on the comprehensive tables located in Section 3.

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quantity, and quality of environmental data used in decision making are appropriate for the intended application. Determination of data quality is based on evaluation of the precision, accuracy, representativeness, comparability, and completeness (PARCC) characteristics of the data.

#### F.1.1.1 Precision

Precision is defined as the reproducibility, or degree of agreement, among replicate measurements of me same quantity. Specifically, it is a quantitative measure of the variability of a group of measurements compared to their average value. The overall precision of measurement data is a mixture of sampling and analytical factors. Precision is stated in terms of standard deviation, coefficient of variation, range, and relative range. The closer the numerical values of the measurements are to each other, the more precise the measurement is. Analytical precision can be measured through the analysis of U.S. Army Environmental Center (USAEC) Class 1 laboratory QC duplicate sample spike recoveries, and sampling precision and spatial variability of contamination can be assessed through the analysis of field replicates. Precision was expressed as the percentage of the difference between results of duplicate samples for a given compound or element. Relative percent difference (RPD) was calculated using the following equation:

where:

V1 = Concentration of the compound or element in the sample V2 = Concentration of the compound or element in the duplicate/ replicate.

Precision was evaluated based on the analysis of three different types of QC samples: USAEC Class 1 laboratory QC duplicate sample spike recoveries (LCS), matrix spike and matrix spike duplicate (MS/MSD) samples, and replicate field sample analyses. The first type of QC sample, USAEC Class 1 laboratory QC duplicate sample spike recoveries, is required as part of the USAEC analytical program for all methods and provides ongoing information on the performance of each lot for each analytical method in a standard matrix. For each analytical lot, the results of these sample spike recoveries were compiled on single-day and three-day control charts (i.e., X-bar and range) and submitted to the USAEC Chemistry Branch for approval. Upon final approval by the USAEC Chemistry Branch, the data within each lot will be revised at phase 3 in the Installation Restoration Data Management Information System (IRDMIS).

Same single-day (high spike concentration) control charts were outside QC criteria for: hexahydro-l, 3,5-trinitro-l, 3,5-triazine (RDX), 1,3,5-trinitrobenzene (135TNB), 2,4,6- trinitrotoluene ( 246TNT), 2,4dinitrotoluene (24DNT), and nitrobenzene (NB) for lots AIUD and AIWV; and RDX, 135TNB, NB, and 246TNT for lots AIYH and AJDT. Out-of-control situations in these lots are expected to have a negligible impact on data quality, and are discussed in Section F.3.1 of this appendix.

One sample per 20 samples collected was randomly selected to be spiked

as an MS/MSD sample. MS/MSD analyses help to detect any systematic problems in the analysis and also help determine how well the target analytes can be recovered from environmental matrices, identifying a matrix effect. Three aliquots were collected for the sample designated to be analyzed for MS/MSD. MS/MSD samples were prepared by routinely analyzing the first aliquot for the parameters of interest, while the remaining two aliquots were spiked with known quantities of the parameters of interest before analysis. The relative percent difference (RPD) between the two spike results (MS/MSD) was not calculated because background concentration was greater than the spike level.

Replicate field samples are the third type of QC sample. Sample collection reproducibility and media variability were measured by the analysis of field replicates. Field replicates were collected using the same techniques as those used to collect the environmental samples. One sample in 10 for each similar matrices was collected. Sample collection reproducibility and media variability were evaluated based on the RPD values between the two replicate samples. The RPD between field replicates indicates that environmental conditions at the site are spatially and temporally variable. The data should be utilized with this consideration. No sample was qualified based on the results of these replicate samples, since EPA has no guidelines for this QC parameter. However, the amount of heterogeneity of the matrices is shown by the number of times the replicate samples collected and calculated exceeded the selected control limits, based on EPA acceptance criteria.

Immediately after purging, groundwater samples were collected from existing monitoring wells at LAAP using Teflon ® bailers. The samples were shipped to DataChem Laboratories (DCL) for explosives-related compounds analysis. Field replicate RPD values were calculated only for compounds detected in concentrations greater than the certified reporting limits (CRLs) in both replicate pair samples. The explosive water field replicate did not exceed the control limit of 30 percent for RPD acceptance criteria. In general, the RPD between field replicates was low. Based on these RPD results and the acceptable laboratory QC results, the sample collection DQO for reproducibility is considered to have been met. A comprehensive discussion of all replicate sample results is presented in Section F. 2.3.

#### F.1.1.2 Accuracy

Accuracy, or the bias in a measurement system, is a measure of the closeness of a reported concentration to the true value. The closer the numerical value of the measurement approaches the true value, or actual concentration, the more accurate the measurement is. Analytical accuracy is expressed as the percent recovery of a compound or element that has been added to the environmental sample at a known concentration before analysis. The percent recovery values were calculated using the following equation:

- where: Sa = Concentration of the compound or element added to the sample. Ss = Total compound or element concentration detected in the spiked sample
  - So = Concentration of the compound or element detected in the unspiked sample

One field sample was randomly selected to be analyzed as an MS/MSD sample. The information gathered was not used to assess the effect of matrix on sample recovery. Recoveries were not calculated because background concentration was greater than the spiking level. The laboratory accuracy for this project was qualitatively assessed by evaluating the following laboratory QC information: method blank, initial calibration verification (ICV), continuing calibration verification (CCV), and USAEC Class 1 laboratory QC sample spike results calculated from all analyses conducted on environmental samples. Each type of spiked sample provided different information on the accuracy of the measurement system.

USAEC QC samples were used as the primary control of accuracy in the laboratory system. The laboratory plotted me mean percent recovery and range of percent recovery on control charts prepared for each control compound. The laboratory utilized the percent recovery of each compound in spiked QC samples, the average percent recovery, and the difference between the percent recovery of two high spiked samples in a continuous assessment of method accuracy. Thirty-two percent recovery values (of 135 values) were out-of-control. The flag code (i.e., "7") was applied to three RDX and five 246TNT concentrations to indicate that the QC samples' low spike recovery was outside of QC criteria. The flag code (i.e., "L") was applied to six NB concentrations to indicate that NB data were rejected due to low recovery for the low spike. Despite these values, no systematic laboratory error was detected, and the results are considered to have little impact on the overall environmental data quality.

In addition, an analysis accuracy was calculated for method UW25 based on found versus recovered compounds. Analysis accuracies are reported with each applicable lot of data to USAEC. Concentrations reported in IRDMIS reflect the accuracy of the analytical method.

All supporting explosives QC information (i.e, method blanks, ICVs, and CCVs) was qualitatively evaluated with respect to the analytical accuracy DQO. The method blank results for groundwater were generally below the CRLs with one exception. Lot AIWV had a method blank with the concentration of 135TNB above the CRL. As a result, 135TNB concentrations in three field samples was flagged (i.e., "B") to indicate that this explosives-related compound was found in the associated method blank. Percent recovery results from the ICVs and CCVs were within the limits specified in DCL performance demonstrated method UW25. The overall laboratory accuracy is acceptable, and as such, the analytical DQO for accuracy was met.

Sampling accuracy was maximized by the adherence to the strict quality assurance (QA) program presented in the Five-Year Review of the Area P Lagoons QAPP. All procedures (i.e., groundwater sample collection, equipment decontamination, and health monitoring equipment calibration and operation) used were documented as standard operating procedures (SOPs). Monitoring of field activities that affected accuracy was performed by assessing the results of the equipment rinsate analyses. Equipment rinsate blanks were prepared to ensure that all samples represent the particular site from which they were collected, assess any cross-contamination mat may have occurred, and flag the associated analytical data accordingly.

The flag code (i.e., "G") was applied to me 135TNB and RDX in SAICO1

Site ID G0009, SAIC04 Site ID G0083, and SAIC02 and SAIC03 Site ID G0084 to indicate that these compounds were detected in the associated equipment rinsate blank.

Based on an evaluation of the explosives- related compounds detected in the equipment rinsate blanks, the overall field accuracy is acceptable. As a result, the field DQO for accuracy is considered to have been met. A comprehensive discussion of me field QC results is presented in Section F. 2.

#### F.1.1.3 Representativeness

Representativeness was defined as the degree to which the data accurately and precisely represent a characteristic of a population, parameter variations at a sampling location, a process condition, or an environmental condition. Sample representativeness was ensured by collecting sufficient samples of a population medium, properly distributed with respect to location and time. Representativeness was assess by reviewing sample collection methods, equipment, and sample containers, in addition to evaluating the RPD values from the field replicate samples and the concentrations of explosivesrelated compounds detected in the equipment rinsate blanks and method blanks. The reproducibility of a representative set of samples reflects the degree of heterogeneity of the sampled medium, as well as the effectiveness of the sample collection techniques.

Based on the evaluation of the factors described above and summarized in Section F. 3, the samples collected are considered to be representative of the environmental conditions at LAAP.

#### F.1.1.4 Comparability

Comparability is a qualitative parameter expressing the confidence with which one data set can be compared to another and is limited to the other PARCC parameters, because only when precision and accuracy are known can one data set be compared to another. The characteristic of comparability reflects the consistency of sample collection and handling procedures, analytical techniques, and expression of results in units consistent with other organizations reporting similar data. To optimize comparability, only the specific methods and protocols mat were specified in the Five-Year Review of the Area P Lagoons QAPP, as required by the USATHAMA Quality Assurance Program, PAM 11-41 (January 1990), were used to collect and analyze samples. By using consistent sampling and analysis procedures, all data sets were comparable within the sites at LAAP and between sites at the installation to ensure that decisions and priorities were based on a consistent data base. No changes to planned procedures were implemented that would affect data comparability. Comparability also was ensured by the analysis of USAEC reference materials, establishing that the analytical procedures used were generating valid data.

All groundwater samples collected for explosives analyses were analyzed using DCL performance demonstrated method UW25. Based on the precision and accuracy assessment presented above, the data collected are considered to be comparable with me data collected during previous investigations.

#### F.1.1.5 Completeness

Completeness was defined as the percentage of valid data obtained from the sampling and analysis process. For data to be considered valid, they must have met all acceptance criteria, including accuracy and precision, as well as any other criteria specified by the analytical methods used.

Project completeness was calculated using the following equation:

where:

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DPv = Valid data points
DPp = Planned data points.
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For analytical data to be usable, each data point must be satisfactorily validated. The completeness objectives established for this project were 90 percent. Based on the evaluation of the field and laboratory QC results presented in Sections F.2 and F.3, 96.7 percent of the sample data collected for explosives analyses were used as the basis for all recommendations presented in this report. All explosives analyses for the groundwater and field QC samples were performed within the holding times.

Completeness of the data also was evaluated by comparing work plan sampling requirements to the completed chain-of-custody forms to establish that all samples required by the work plan were in fact collected. Upon completion of this process, analytical results in the IRDMIS data base and laboratory data packages were compared to those required by the chainof-custody to establish that the results for all samples taken were indeed in the data base.

#### F.2 FIELD QUALITY CONTROL ASSESSMENT

Six equipment rinsate blanks, two source water samples, and two field replicates were collected and analyzed for explosives-related compounds using the same laboratory techniques as those used for the environmental samples. The analytical results obtained from the field QC samples are used to assess the efficiency and effectiveness of the sample collection, handling, and equipment decontamination procedures used in the field. Table F- 2 contains a crossreference of environmental samples to the associated equipment rinsate blank samples.

#### F.2.1 Duplicate Source Water Samples and Equipment Rinsate Blanks

Duplicate source water samples and equipment rinsate blanks were collected to assess the impact of decontamination procedures on analytical results.

Duplicate source water results provided information on the water used to decontaminate the sample collection devices. The source water samples were found to be free -of any explosives-related compounds. Thus, any compound detected in the equipment rinsates would be due to decontamination procedures and not from the water used to perform the decontamination. Table F-3a summarizes the concentrations of the explosives-related compounds in the duplicate water source water sample.

Equipment rinsate blanks provided a measure of the cumulative contamination derived from the field sampling equipment, sample transit, storage, and analysis. Equipment rinsate blanks were prepared for manual and small automated sampling equipment used to collect environmental samples. One equipment rinsate blank was collected daily by pouring analyte free water through a recently decontaminated sample collection device into a prepared sample container appropriate for the required analysis. Equipment rinsate blanks were shipped to the laboratory to be analyzed using the methods required for the environmental samples collected on the same day. Table F-3b summarizes the concentrations of me compounds detected in the equipment rinsate blanks collected during the Five-Year Review of the Area P Lagoons.

Explosives Analysis—Duplicate source water samples (i.e., SAICO1 and SAICO2), used to determine that the water used for equipment decontamination was free of explosives, were collected on October 12, 1993. Duplicate source water samples were analyzed for explosives related compounds. These analyses were performed before the field work began and the results were submitted to the USAEC Chemistry Branch for approval. No explosives- related compounds were detected.

				Associated	Requested Analysis
Site ID	Field Sample	Lab Sample	Collection	Equipment	
	Number	Number	Date	Rinsate	Explosives
G0012	SAIC01	<b>UB01144</b>	2/24/94	G0012	х
G0014	SAIC01	UB01145	2/24/94	G0012	X
G0009	SAIC01	UB01176	2/25/94	G0009	x
G0083	SAIC01	UB01179	2/25/94	G0009	х
G0083	SAIC02	UB01179M	2/25/94	G0009	Х
G0083	SAIC03	UB01179M	2/25/94	G0009	х
G0084	SAIC01	UB01177	2/25/94	G0009	х
G0084	SAIC02	<b>UB01178</b>	2/25/94	G0009	Х
G0105	SAIC01	UB01192	2/28/94	G0110	Х
G0109	SAIC01	UB01193	2/28/94	G0110	х
G0110	SAIC01	<b>UB01191</b>	2/28/94	G0110	х
G0106	SAIC01	UB01225	3/1/94	GO-146	х
G0068	SAIC01	UB01226	3/1/94	GO-146	Х
G0104	SAIC01	UB01242	3/2/94	GO-145	х
G0104	SAIC02	UB01243	3/2/94	GO-145	х
G0085	SAIC01	<b>UB01270</b>	3/3/94	GO-150	x

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 Table F - 2. Equipment Rinsate Cross Reference - Groundwater - Area P Lagoons,

 Louisiana Army Ammunition Plant

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#### Table F-3a. Data Summary Table: Groundwater - Area P Lagoons, Source Water Results, Louisiana Army Ammunition Plant

Site ID	#6	#6	#6	#6	······
Field Sample Number	SAIC01	SAIC01	SAIC02	SAIC02	
Site Type	RNSW	TAPW	RNSW	TAPW	
Collection Date	10/13/94	10/12/94	10/13/94	10/12/94	
Depth (ft)	0	0	0	0	
Associated Field QC Sample - Site iD	N/A	N/A	N/A	N/A	
Associated Field QC Sample - Field Sample No.	N/A	N/A	N/A	N/A	

#### Explosives (UW25)

Laboratory ID Number				UA03234		Ų	JA03229			UA03235			JA03228	
Parameter	Units	CRL		FC	DQ									
1,3,5-Trinitrobenzene	µg/L	0.21	LT	0.21		LT	0.21 H		LT	0.21 D		LT	0.21 DH	
1,3-Dinitrobenzene	µg/L	0.458	LT	0.458	1	LT	0.458		LT	0.458 D		LT	0,458 D	
2,4,6-Trinitrotoluene	µg/L	0.426	LT	0.426		LT	0.426		LT	0.426 D		LT	0.426 D	
2,4-Dinitrotoluene	µg/L	0.397	LT	0.397		LT	0.397		LT	0.397 D		LT	0.397 D	
2,6-Dinitrotoluene	µg/L	0.6	LT	0.6		LT	0.6		LT	0.6 D		LT	0.6 D	
Cyclotetramethylenetetranitramine		0.533	LT	0.533		LT	0.533		LT	0.533 D		LT	0.533 D	
Nitrobenzene	µg/L	0.682	LT	0.682	1	LT	0.682		LT	0.682 D		LT	0.682 D	
lexahydro-1,3,5-trinitro-1,3,5-triazine	µg/L	0.416	LT	0.416		LT	0.416		LT	0.416 D		LT	0.416 D	
N-methyl-N,2,4,6,-tetranitroanailine	µg/L	0.631	ĹΪ	0.631		LŤ	0,631		LT	0.631 D		LT	0.631 D	

N/A - Not applicable ID - Identification

QC - Quality Control CRL - Certified reporting limit

LT - Less than

FC - Flagging Codes: D - Duplicate analysis

H - Out of control but data accepted due to high recoveries

DQ - Data Qualifiers:

I - The low-spike recovery is high.

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## Table F-3b. Data Summary Table: Groundwater - Area P Lagoons, Quality Control, Equipment Rinsates,Louisiana Army Ammunition Plant

Site ID				G0009			G0012			G0110		GO-145			GO-146		
Field Sample Number			S	AICRB02		S	AICRB01		S	AICRB03	S	AICRB05		S	AICRB04		
Site Type				RNSW			RNSW			RNSW		RNSW 3/2/94			RNSW		
Collection Date			2/25/94			2/25/94 2/24/94			2/24/94 . 2/28/94					3/1/94			
Depth (ft)		0			0 N/A				0		0		0				
Associated Field QC Sample - Site ID					N/A				N/A			N/A			N/A		
Associated Field QC Sample - Field Sa	ample N	io.		N/A			N/A		N/A			N/A			N/A		
Explosives (UW25)			_														
aboratory ID Number	( Inlin	001		UB01175	2		UB01143	50		UB01190		UB01240	50		UB01223		
aboratory ID Number Parameter	Units			FC	DQ		FC	DQ		FC DQ	·····	FC	DQ		FC	DQ	
aboratory ID Number Parameter I,3,5-Trinitrobenzene	µg/L	0.21		FC 0.42 CB	DQ	LT	FC 0.21	DQ	LT	FC DQ 0.21	LT	FC 0.21	DQ	LT	FC	DQ	
aboratory ID Number Parameter ,3,5-Trinitrobenzene ,3-Dinitrobenzene	μg/L μg/L	0.21 0.458	LT	FC 0.42 CB 0.458	1	LT LT	0.21 0.458	DQ	LT LT	FC DQ 0.21 0.458	LT LT	FC 0.21 0.458	DQ J	LT LT	0.21 0.458	DQ	
aboratory ID Number arameter ,3,5-Trinitrobenzene ,3-Dinitrobenzene ,4,6-Trinitrotoluene	μg/L μg/L μg/L	0.21 0.458 0.426	LT LT	FC 0.42 CB 0.458 0.426 7	DQ I JN N	LT LT LT	FC 0.21 0.458 0.426	DQ	LT LT LT	FC DQ 0.21 0.458 0.426	LT	FC 0.21 0.458 0.426	DQ J	LT LT LT	FC 0.21 0.458 0.426	DQ J	
aboratory ID Number arameter ,3,5-Trinitrobenzene ,3-Dinitrobenzene ,4,6-Trinitrotoluene ,4-Dinitrotoluene	μg/L μg/L μg/L	0.21 0.458	LT	FC 0.42 CB 0.458	1	LT LT	0.21 0.458	DQ	LT LT	FC DQ 0.21 0.458	LT LT LT	FC 0.21 0.458	DQ J J	LT LT	0.21 0.458	DQ J J	
aboratory ID Number arameter ,3,5-Trinitrobenzene ,4,6-Trinitrotoluene ,4-Dinitrotoluene ,6-Dinitrotoluene	μg/L μg/L μg/L μg/L μg/L	0.21 0.458 0.426 0.397	LT LT LT	FC 0.42 CB 0.458 0.426 7 0.397	1	LT LT LT LT	FC 0.21 0.458 0.426 0.397	DQ	LT LT LT LT	FC DQ 0.21 0.458 0.426 0.397	LT LT LT	0.21 0.458 0.426 0.397	DQ J J	LT LT LT LT	FC 0.21 0.458 0.426 0.397	J J	
aboratory ID Number Parameter ,3,6-Trinitrobenzene ,4,6-Trinitrotoluene ,4-Dinitrotoluene ,6-Dinitrotoluene Syclotetramethylenetetranitramine	μg/L μg/L μg/L	0.21 0.458 0.426 0.397 0.6	LT LT LT LT	FC 0.42 CB 0.458 0.426 7 0.397 0.6	1	LT LT LT LT LT	FC 0.21 0.458 0.426 0.397 0.6	DQ	LT LT LT LT LT	FC DQ 0.21 0.458 0.426 0.397 0.6	LT LT LT LT LT	FC 0.21 0.458 0.426 0.397 0.6	DQ J J	LT LT LT LT	FC 0.21 0.458 0.426 0.397 0.6	DQ J J	
aboratory ID Number Parameter 1,3,5-Trinitrobenzene 2,4,6-Trinitrotoluene 2,4-Dinitrotoluene 2,6-Dinitrotoluene	μg/L μg/L μg/L μg/L μg/L	0.21 0.458 0.426 0.397 0.6 0.533	LT LT LT LT	FC 0.42 CB 0.458 0.426 7 0.397 0.6 0.533	1	LT LT LT LT LT	FC 0.21 0.458 0.426 0.397 0.6 0.533	<u>DQ</u>	LT LT LT LT LT	FC DQ 0.21 0.458 0.426 0.397 0.6 0.533	LT LT LT LT LT LT	FC 0.21 0.458 0.426 0.397 0.6 0.533	L L	LT LT LT LT LT LT	FC 0.21 0.458 0.426 0.397 0.6 5.03 C	Dd 1 1	

### Table F-3b. Data Summary Table: Groundwater - Area P Lagoons, Quality Control, Equipment Rinsates, Louisiana Army Ammunition Plant (Continued)

Site ID	GO-150	
Field Sample Number	SAICRB06	
Site Type	RNSW	
Collection Date	3/3/94	
Depth (ft)	0	
Associated Field QC Sample - Site ID	N/A	
Associated Field QC Sample - Field Sample No.	N/A	

#### Explosives (UW25)

PULLED ALLEN						
Laboratory ID Number				UB01267		
Parameter	Units	CRL		F	C DQ	
1,3,5-Trinitrobenzene	µg/L	0.21	LT	0.21		
1,3-Dinitrobenzene	µg/L	0.458	LT	0.458		•
2,4,6-Trinitrotoluene	µg/L	0.426	LT	0.426		
2,4-Dinitrotoluene	µg/L	0.397	LT	0.397	J	
2,6-Dinitrotoluene	µg/L	0.6	LT	0.6		
Cyclotetramethylenetetranitramine	µg/L	0.533	LT	0.533		
Nitrobenzene	µg/L	0.682	LT	0.682		
Hexahydro-1,3,5-trinitro-1,3,5-triazine	µg/L	0.416	LT	0.416		
N-methyl-N,2,4,6,-tetranitroanailine	µg/L	0.631	LT	0.631		

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- N/A Not applicable
- ID Identification
- QC Quality Control
- CRL Certified reporting limit
- LT Less than
- FC Flagging Codes:
  - B Analyte was found in the method blank or QC blank as well as the sample.
  - C Analysis confirmed
  - K Reported results affected by interferences or high background
  - L Out of control, data rejected due to low recoveries.
  - Q Sample interference obscured peak of interest
  - U Analysis is unconfirmed
  - 7 Low spike recovery is not within control limits
- DQ Data Qualifiers:
  - I The low-spike recovery is high.
  - J The low-spike recovery is low.
  - N The high-spike recovery is low.

Six equipment blanks (i.e., SAICRB01, SAICRB02, SAICRB03, SAICRB04, SAICRB05, and SAICRB06) were collected and analyzed by DCL for explosivesrelated compounds using DCL performance demonstrated method UW25. 135TNT, NB, and RDX were detected in SAICRB02 at concentrations of 0.42 µg/L, 2.7 µg/L, and 0.75 µg/L, respectively. 135TNT and RDX concentrations detected in field sample SAIC01 Site ID G0009, SAIC04 and SAIC05 Site ID G0083, SAIC02 and SAIC03 Site ID G0084, and NB concentrations detected in SAIC05 and SAIC06 Site ID G0083 were flagged (i.e., "G") to indicate that the compound concentration was found in the associated equipment rinsate blank.

Nitrobenzene was detected in SAICRB03 (2.9  $\mu$ g/L) and hexahydro-1,3,5-trinitro-1,3,5-triazine (HMX) in SAICRB04 (5  $\mu$ g/L); however, since these compounds were not detected in the associated environmental samples, no flag codes were applied.

#### F.2.3 Field Replicates

One replicate environmental sample was collected for every 10 environmental samples, as required by the project-specific QAPP and me USATHAMA Quality Assurance Program, PAM 11-41 (January 1990). The RPD value of each detected compound was reviewed to assess the sample collection reproducibility and matrix variability. A total of 16 groundwater and 2 replicate samples were collected. One field replicate groundwater sample was collected after each 10 environmental samples, as indicated on the chain-of-custody forms.

As required by the Five-Year Review of the Area P Lagoons QAPP, the first bailer volume was used to fill the sample bottles. The next bailer volume was used to fill the replicate sample bottles. No specific control limits for field replicates were established in part because the natural heterogeneity of the environmental media proved to have a much greater influence than that imparted by field activities.

Replicate results were evaluated using 30 RPD EPA acceptance criteria for water samples. Table F-4 summarizes the concentrations of the explosives-related compounds detected in the groundwater replicate pairs.

#### Table F-4. Data Summary Table: Groundwater - Area P Lagoons, Results of Replicated Groundwater Sampling Analysis, Louisiana Army Ammunition Plant

Site ID	G0084	G0084	G0104	G0104	
Field Sample Number	SAIC02	SAIC03	SAIC01	SAIC01	
Site Type	WELL	WELL	WELL	WELL	
Collection Date	2/25/94	2/25/94	3/2/94	3/2/94	
Depth (ft)	21.6	21.6	· 18	18	
Associated Field QC Sample - Site ID	G0009	* G0009	GO-145	GO-145	
Associated Field QC Sample - Field Sample No.	SAICRB02	SAICRB02	SAICRB05	SAICRB05	

#### Explosives (UW25)

ENDIOSIACS INLINO	_														and the second
Laboratory ID Number				UB01177			UB01178		L L	B01242		้ เ	JB01243		
Parameter	Units	CRL		FC	DQ		FC	DQ		FC	DQ		FC	DQ	
1,3,5-Trinitrobenzene	µg/L	0.21		320 UGB	Т		310 DUG	Т		6000 C			6300 DC		
1,3-Dinitrobenzene	µg/L	0.458	LT	0.458		LT	0.458 D			560 C			580 DC		
2,4,6-Trinitrotoluene		0.426		250 C7	JN		240 DC7	JN		11000 C	J		11000 DC	J	
2,4-Dinitrotoluene	µg/L	0.397		12.1 UQ	Ν		11.2 DUQ	N		550 C	J		570 DC	J	
2,6-Dinitrotoluene	µg/L	0,6	LT	0.6		LT	12 D		LT	60 JI		LT	60 DJI		
Cyclotetramethylenetetranitramine	µg/L	0.533		13.3 U			14 DUQ		LT	370 K		LT	310 DK		
Nitrobenzene		0.682	LT	0.682		LT	0.682 D		LT	68 LJI	J	LT	68 DLJ	J	
Hexahydro-1,3,5-trinitro-1,3,5-triazine	ug/L	0.416		110 CG			120 DCG			7100 C			8400 DC		
N-methyl-N,2,4,6,-tetranitroanalline	µg/L	0.631		5.66 U			5.03 DU			120 C			130 DC		

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N/A - Not applicable

- ID Identification
- QC Quality Control
- CRL Certified reporting limit
- LT Less than
- FC Flagging codes:
  - B Analyte found in the method blank or QC blank as well as the sample.
  - C Analysis confirmed

  - G Analytes to chamber of the second   - J Value is estimated
  - K Reported results affected by Interferences or high background
  - L Out of control, data rejected due to low recoveries.
  - Q Sample interference obscured peak of interest
  - U Analysis is unconfirmed
  - 7 Low spike recovery is not within control limits
- DQ Data Qualifiers;
  - I The low-spike recovery is high.
  - J The low-spike recovery is low.
  - N The high-spike recovery is low,

**Explosives Analysis**—Sixteen groundwater samples were collected and analyzed for explosives-related compounds using DCL performance demonstrated method UW25. Two groundwater samples (i.e., SAICO1 site ID G0083 and SAICO1 site ID G0104) were collected in duplicate. RPD values were not calculated for compounds less than the CRL in both the sample and replicate sample. The explosives field replicate RPDs did not exceed the control limit of 30 percent.

#### F.3 LABORATORY QUALITY CONTROL ASSESSMENT

All groundwater samples and equipment rinsate blanks collected were analyzed using the DCL performance demonstrated method, from the following reference:

• The Determination of Explosives in Water by High Performance Liquid Chromatography, Method Number: UW25.

Data verification and validation of the resulting analytical data packages ensured that me DCL produced an acceptable quality level for results. All data were flagged using the guidelines and specifications described in the following documents:

- User's Guide, The Installation Restoration Data Management Information System (IRDMIS), Volume II Data Dictionary, Potomac Research Institute (PRI), 1994.
- Laboratory Data Validation Functional Guidelines For Evaluating Organics Analyses, EPA Contract Laboratory Program, February 1988
- U.S. Army Toxic and Hazardous Materials Agency (USATHAMA) Quality Assurance Program, PAM 11-41. (January 1990).

If necessary, flagging codes are assigned to data points by the laboratory and SAIC. Each data point was assessed to determine whether the value was considered usable (i.e., no qualifier), usable but flagged (i.e., "G," "U," and "Q"), or not usable (i.e., "L"). All flag codes used were applied to all data (i.e., detected and less than the CRL values), as necessary, on the IRDMIS data presentation tables in Appendix A, and to the appropriate detected values summarized in the data tables presented in Section F.3.1. All flag codes are defined at the bottom of each table presenting analytical data.

#### F.3.1 Explosives Compound Analysis (DCL Performance Demonstrated Method UW25)

Fourteen groundwater samples and 6 equipment blanks were collected and analyzed by DCL for explosives using DCL performance demonstrated method UW25. Data quality was evaluated using the guidelines and control limits specified for holding times, initial and continuing calibration verification, method blank and USAEC QC spike samples, and MS/MSD results. The explosives data review and validation worksheets are presented in Tables F-5a and F-5b.

Holding Times—Holding times were defined as the maximum amount of time allowed to elapse between the date and time of sample collection and the date and time the sample was extracted. Holding times were further defined as the maximum amount of time allowed to elapse between the date and time of extraction and sample analysis. DCL was required to meet holding times of 7 days for samples collected for explosives analysis. All analyses were required within 40 days after extraction.

Analysis of samples that have exceeded the method-recommended holding times may result in the following: 1)concentrations of compounds that would have been detected ordinarily are undetected due to chemical transformation, compound volatilization, or biodegradation; 2)reported concentrations lower than those originally present, due to the factors previously stated; 3)or reported concentrations greater than those originally present in the sample due to external contamination of water samples. Based on an evaluation of all field samples and equipment rinsate blanks analyzed for explosives-related compounds using DCL method UW25, all holding time criteria were met.

Initial Calibration Results—The sensitivity limit of the detectors and the linear range of the analytical systems for each compound were established by injecting a calibration standard. Calibration of the high-performance liquid chromatography (HPLC) used to analyze the samples collected during the Five-Year Review of the Area P Lagoons was established and validated by injecting a blank and eight standards into the liquid chromatograph system. Calibration standards were analyzed and linear calibration curves were generated from the data. Before analysis, the operating parameters were adjusted to optimize instrument response. Retention

Site ID	Field Sample Number	Site Type	Laboratory Sample Name	Sampling Date	Extraction Date	Analysis Date	Initial Calibration (ICV) and Daily Calibration (CCV)	Method Blank Results	
Lot AIUD									
G0012	SAICRB01	RNSW	UB01143	2/24/94	2/28/94	3/3/94	All ICV and CCV percent recoveries	No compounds detected at	
G0012	SAIC01	Well	UB01144	2/24/94	2/28/94	3/3/94	within control limits (75-125)	concentration greater than the CRL	
G0014	SAIC01	Well	UB01145	2/24/94	2/28/94	3/3/94			
Lot AIWV									
G0009	SAICRB02	RNSW	UB01175	2/25/94	3/02/94	3/22/94	All ICV and CCV percent recoveries within control limits (75-125)	Compounds detected at concentration greater than the CRL	
G0009	SAIC01	Well	UB01176	2/25/94	3/02/94	3/22/94		*135TNB=0.304 µg/L	
G0084	SAIC01	Well	UB01177	2/25/94	3/02/94	3/22/94			
G0084	SAIC01	Well	UB01178	2/25/94	3/02/94	3/22/94			
G0083	SAIC01	Well	UB01179	2/25/94	3/02/94	3/22/94			
G0083	SAIC01MS	Well	UB01179M	2/25/94	3/02/94	3/22/94			
G0083	SAIC01MSD	Well	UB01179M	2/25/94	3/02/94	3/22/94		1	
Lot AIYH									
GO-146	SAICRB04	RNSW	UB01223	3/01/94	3/03/94	3/29/94	All ICV and CCV percent recoveries	No compounds detected at	
G0106	SAIC01	Well	UB01225	3/01/94	3/03/94	3/29/94	within control limits (75-125)	concentration greater than the CRL	
G0068	SAIC01	Well	UB01226	3/01/94	3/03/94	3/29/94			

## Table F-5a: Explosive Analysis, Louisiana Army Ammunition Plant, Five-Year Review of Area P Lagoons Data Review and Validation

	Laboratory			Matrix Spike	Duplicate Spiked			
Site ID	Field Sample	Site Type	Sample	Low (2xCRL)	High (10xCRL)	QC Results (10xCRL)	Matrix Spike	Matrix Spike
Lot AIUD	Number		Name	(ZXCRL)		(IVXCRL)	Results	Duplicate Results
G0012	SAICRB01	RNSW	UB01143	All recoveries met QC criteria, except: RDX=71.6%	All recoveries met QC criteria, except: RDX=947%;	All recoveries met QC criteria, except: RDX=97.8%;	No MS analyzed for lot AIUD.	No MSD analyzed for lot AIUD.
G0012	SAIC01	Well	UB01144		135TNB=86.9%; NB=78.8%; 246TNT=82.8%.	135TNB=90.6%; NB=85.3%; 246TNT=87.2%.		
G0014	SAIC01	Well	UB01145					
Lot AIWV								-
G0009	SAICRB02	RNSW	UB01175	All recoveries met QC criteria, except: 135TNB=145%	All recoveries met QC criteria, except: RDX=92.8%;	All recoveries met QC criteria, except: RDX=93.8%;	No percent recoveries were calculated due to	No RPD values were calculated due to
G0009	SAIC01	Well	UB01176	246TNT=57.5%.	135TNB=104%; NB=75.3%; 246TNT=75.9%; 24DNT=71.3%.	NB=77.5%; 246TNT=79.1%	background concentration greater than the spike level.	background concentration greater than the spike level.
G0084	SAIC01	Well	UB01177		2401111-73.370, 242111-71.370.	2412141-00.070.	greater man me spike level.	greater than the spike level.
G0084	SAIC01	Well	UB01178					
G0083	SAIC01	Well	UB01179					
G0083	SAIC01MS	Well	UB01179M					
G0083	SAIC01MSD	Well	UB01179M					
Lot AIYH								
GO-146	SAICRB04	RNSW	UB01223	All recoveries met QC	All recoveries met QC	All recoveries met QC	No MS analyzed	No MSD analyzed
G0106	SAIC01	Well	UB01225	criteria, except: NB=51.1% 246TNT=60.1%;	criteria.	criteria, except: RDX=105%; 135TNB=103%; NB=72.2%;	for lot AIYH	for lot AIYH
G0068	SAIC01	Well	UB01226	24DNT=55.9%.		246TNT=85%.		

### Table F-5a. Explosive Analysis, Louisiana Army Ammunition Plant, Five-Year Review of Area P Lagoons Data Review and Validation (Continued)

Site ID	Field Sample Number	Site Type	Laboratory Sample Name	Equipment Blank Results	Flagged Results
Lot AIUD					
G0012	SAICRB01	RNSW	UB01143	No compounds detected	NB LT 1.840K /RDX LT 0.416K7 µg/L
G0012	SAIC01	Well	UB01144	at concentration greater the CRL in SAICRB01	135TNB=950C/13DNB=35C/246TNT=3700C/24DNT=120C/26DNT LT 32.3K/HMX=110C/ NB LT 12.3K/RDX LT 3100K7/TERYL LT 6.3JI ug/L
G0014	SAIC01	Well	UB01145		135TNB LT 0.429K/ HMX=2.92C/RDX=14.4C7 µg/L
Lot AIWV					
G0009	SAICRB02	RNSW	UB01175	Compounds detected	135TNB=0.42CB/246TNT LT 0.43 "7"/NB=2.7U/RDX=0.75U µg/L
G0009	SAIC01	Well	UB01176	at concentration greater	135TNB=29UGB/246TNT=28C7/24DNT=37UQ/HMX=26C/RDX=430C µg/L
G0084	SAIC01	Well	UB01177	the CRL in SAICRB02	135TNB=320UGB/246TNT=250C7/24DNT=112UQ/HMX=13U/RDX=110CG/TERYL=5.7U µg/
. G0084	SAIC01	Well	UB01178	*135TNB=0.42/ NB=2.7/RDX=0.75 μg/L	135TNB=310DUGB/13DNB LT 0.46D/246TNT=240DC7/24DNT=11DUQ/26DNT LT 12D/ HMX=14DUQ/NB LT 068D/RDX=120DUQ/TERYL=5DU µg/L
G0083	SAIC01	Well	UB01179		135TNB=800UGB/13DNB =5.6C/246TNT=3100C7/24DNT=95UQ/HMX=99C/NB LT 14JI/ /RDX=1200CG/TERYL=95U µg/L
G0083	SAIC01MS	Well	UB01179M		135TNT=830GB/246TNT=3200 "7"/26DNB LT 12JI/NB=24G/RDX=1900G µg/L
G0083	SAIC01MSD	Well	UB01179M		135TNB=780DGB/13DNB=5.1D/246TNT=3000D7/24DNT=130D/26DNT LT 12DJI/HMX=130D NB=25DG/RDX=1600DG/TERYL=88D µg/L
Lot AIYH					
GO-146	SAICRB04	RNSW	UB01223	Compound detected at concentration greater	HMX=5C/NB LT 0.68L µg/L.
G0106	SAIC01	Well	UB01225	the CRL in SAICRB04 *HMX=5 μg/L	135TNB=970C/13DNB=330C/246TNT=8800C/24DNT=640C/26DNT LT 60JI/HMX LT 53JI/ /NB LT 68JL/RDX 4100C/TERYL LT 63JI µg/L
G0068	SAIC01	Well	UB01226		135TNB=490C/13DNB=82C/246TNT=3600C/24DNT=350UQ/26DNT LT 60JI/HMX LT 350K/ NB LT 68JL/RDX=2500C/TERYL=31U µg/L

 Table F-5a. Explosive Analysis, Louisiana Army Ammunition Plant, Five Year Review of Area P Lagoons

 Data Review and Validation (Continued)

LT =Less than (Boolean)

Flag Codes:

B=Analyte found in the method blank as well as the sample

C=Analysis was confirmed

D=Duplicate analysis.

G=Analyte found in rinse blank as well as field sample

K=Reported results are affeted by interferences or high background

I=Interferences in the sample make quantitation and /or indentification to be suspect

J=Value is estimated

L=Out of control, data rejected due to low recoveries.

Q=Sample interference obscured peak of interest

U=Analysis was unconfirmed

7=Low spike recovery is not within control limits.

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Site ID	Field Sample Number	Site Type	Laboratory Sample Name	Sampling Date	Extraction Date	Analysis Date	Initial Calibration (ICV) and Daily Calibration (CCV)	Blank Results QC Sample	
Lot AIYH									
GO-145	SAICRB05	RNSW	UB01240	3/02/94	3/03/94	3/29/94	All ICV and CCV percent recoveries	No compounds detected at	
G0104	SAIC01	Well	UB01242	3/02/94	3/03/94	3/29/94	within control limits (75-125)	concentration greater than the CRL	
G0104	SAIC01	Well	UB01243	3/02/94	3/03/94	3/29/94			
Lot AIWA									
G0110	SAICRB03	RNSW	UB01190	2/28/94	3/01/94	3/29/94	All ICV and CCV percent recoveries	No compounds detected at	
G0110	SAIC01	Well	UB01191	2/28/94	3/01/94	3/29/94	within control limits (75-125)	concentration greater than the CRL	
G0105	SAIC01	Well	UB01192	2/28/94	3/01/94	3/29/94			
G0109	SAIC01	Well	UB01193	2/28/94	3/01/94	3/29/94			
Lot AJDT									
GO-150	SAICRB06	RNSW	UB01267	3/03/94	3/10/94	4/08/94	All ICV and CCV percent recoveries within control limits (75-125)	No compounds detected at   concentration greater than the CRL	
G0085	SAIC01	Well	UB01270	3/03/94	3/10/94	4/08/94		Concentration greater than the CKL	

### Table F-5b. Explosive Analysis, Louisiana Army Ammunition Plant, Five Year Review of Area P LagoonsData Review and Validation

			Laboratory	QC Sample	e Matrix Spike	Duplicate Spiked			
Site ID	Field Sample Number	Site Type	Sample Name	Low High (2xCRL) (10xCRL)		QC Results (10xCRL)	Matrix Spike Results	Matrix Spike Duplicate Results	
Lot AIYH									
GO-145	SAICRB05	RNSW	UB01240	All recoveries met QC criteria, except: NB=51.1%	All recoveries met QC criteria, except: RDX=93.1%;	All recoveries met QC criteria, except: RDX=105%;	No MS analyzed for lot AIYH.	No MS/MSD analyzed for lot AIYH.	
G0104	SAIC01	Well	UB01242	246TNT=60.1%.	135TNB=87.5%; NB=81.6%; 246TNT=82.2%.	135TNB=103%; NB=72.2%; 246TNT=85%.			
G0104	SAIC01	Well	UB01243						
Lot AIWA									
G0110	SAICRB03	RNSW	UB01190	All recoveries met QC criteria, except: NB=51.1%	All recoveries met QC criteria, except: RDX=93.1%;	All recoveries met QC criteria, except: RDX=105%;	No MS analyzed for lot AIYH.	No MS/MSD analyzed for lot AIWA.	
G0110	SAIC01	Well	UB01191	246TNT=60.1%	135TNB=87.5%; NB=81.6%; 246TNT=82.2%.	135TNB=103%; NB=72.2%; 246TNT=85%.			
G0105	SAIC01	Well	UB01192						
G0109	SAIC01	Well	UB01193						
Lot AJDT									
GO-150	SAICRB06	RNSW	UB01267	All recoveries met QC criteria, except: NB=71.2%	All recoveries met QC criteria, except: RDX=90.6%;	All recoveries met QC criteria, except:246TNT=90.3%	, .	No MS/MSD analyzed for lot AJDT.	
G0085	SAIC01	Well	UB01270	246TNT=61.1%.	135TNB=93.1%; NB=85.6%; 246TNT=86.9%.	onop.2701111-70.376			

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### Table F-5b. Explosive Analysis, Louisiana Army Ammunition Plant, Five Year Review of Area P LagoonsData Review and Validation (Continued)

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Site ID	Field Sample Number	Site Type	Laboratory Sample Name	Equipment Blank Results	Flagged Results
Lot AIYH					
GO-145 G0104 G0104	SAICRB05 SAIC01 SAIC01	RNSW Well Well	UB01240 UB01242 UB01243	No compounds detected at concentration greater the CRL in SAICRB05	NB LT 0.68L µg/L 135TNB=6000C/13DNB=560C/246TNT=1100C/24DNT=550C/ 26DNT LT 60JI/HMX LT 370K/NB LT 68JIL/RDX=7100C/TERYL=120C µg/L 135TNB=6300DC/13DNB=580DC/246TNT=1100DC/24DNT=570DC/ 26DNT LT 60DJI/HMX LT 310DK/NB LT 68DJIL/RDX=8400DC/TERYL=130DCµg/L
Lot AIWA					
G0110	SAICRB03	RNSW	UB01190	Compound detected at concentration greater	NB≂29UQ μg/L
G0110	SAIC01	Well	UB01191	the CRL in SAICRB03 *NB=2.9 µg/L	135TNB=460C/13DNB=24UQ/246TNT=570C/24DNT=120C/ 26DNT LT 60JI/HMX=130C/NB LT 6.8JI/RDX=2800C µg/L
G0105	SAIC01	Well	UB01192		135TNB=3900C/13DNB=320UQ/246TNT=17C/24DNT=54C/ 26DNT LT 60JI/HMX=360C/NB LT 6.8JI/RDX=330C/TERYL=3.7U µg/L
G0109	SAIC01	Well	UB01193		135TNB=95C/13DNB=8.2UQ/246TNT=3600C/24DNT=330C/ 26DNT LT 60JI/HMX=300C/NB LT 6.8JI/RDX=3100C/TERYL=40U µg/L
Lot AJDT					
GO-150	SAICRB06	RNSW	UB01267	No compound detected at concentration greater	None Applied
G0085	SAIC01	Well	UB01270	the CRL in SAICRB06.	135TNB=1.52C/246TNT=2.93C/RDX=5.04C/TERYL=1.12C µg/L

#### Table F-5b. Explosive Analysis, Louisiana Army Ammunition Plant, Five Year Review of Area P Lagoons Data Review and Validation (Continued)

LT =Less than (Boolean)

Flag Codes:

B=Analyte found in the method blank as well as the sample

C=Analysis was confirmed

D=Duplicate analysis.

G=Analyte found in rinse blank as well as field sample

K=Reported results are affeted by interferences or high background I=Interferences in the sample make quantitation and /or indentification to be suspect

J=Value is estimated

L=Out of control, data rejected due to low recoveries.

Q=Sample interference obscured peak of interest

U=Analysis was unconfirmed

7=Low spike recovery is not within control limits.

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APPENDIX G ASTM METHOD D5093-90

#### Standard Test Method for Field Measurement of Infiltration Rate Using a Double-Ring Infiltrometer with a Sealed-Inner Ring¹

This standard is issued under the fixed designation D 5093; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (e) indicates an editorial change since the last revision or reapproval.

#### 1. Scope

1.1 This test method describes a procedure for measuring the infiltration rate of water through in-place soils using a double-ring infiltrometer with a sealed inner ring.

1.2 This test method is useful for soils with infiltration rates in the range of  $1 \times 10^{-7}$  m/s to  $1 \times 10^{-10}$  m/s. When infiltration rates  $\ge 1 \times 10^{-7}$  m/s are to be measured Test Method D 3385 shall be used.

1.3 This test method provides a direct measurement of infiltration rate, not hydraulic conductivity. Although the units of infiltration rate and hydraulic conductivity are similar, there is a distinct difference between these two quantities. They cannot be directly related unless the hydraulic boundary conditions, such as hydraulic gradient and the extent of lateral flow of water are known or can be reliably estimated.

1.4 This test method can be used for natural soil deposits, recompacted soil layers, and amended soils such as soil bentonite and soil lime mixtures.

1.5 The values stated in SI, units are to be regarded as standard. The values in parentheses are for information only.

1.6 This standard does not purport to address the safety problems associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

#### 2. Referenced Documents

2.1 ASTM Standards:

- D653 Terminology Relating to Soil, Rock, and Contained Fluids²
- D 3385 Test Method for Infiltration Rate of Soils in Field Using Double Ring Infiltrometers²

#### 3. Terminology

3.1 Definitions:

3.1.1 *infiltration*—downward entry of liquid into a porous body.

3.1.2 infiltration rate, I—quantity of liquid entering a porous material  $(m^3)$  per unit area  $(m^2)$  per unit time (s), expressed in units of m/s.

3.1.3 infiltrometer---a device used to pond liquid on a porous body and to allow for the measurement of the rate at

which liquid enters the porous body.

3.1.4 For definitions of other terms used in this test method, see Terminology D 653.

#### 4. Summary of Test Method

4.1 The infiltration rate of water through soil is measured using a double-ring infiltrometer with a sealed or covered inner ring (Fig. 1). The infiltrometer consists of an open outer and a sealed inner ring. The rings are embedded and sealed in trenches excavated in the soil. Both rings are filled with water such that the inner ring is submerged.

4.2 The rate of flow is measured by connecting a flexible bag filled with a known weight of water to a port on the inner ring. As water infiltrates into the ground from the inner ring, an equal amount of water flows into the inner ring from the flexible bag. After a known interval of time, the flexible bag is removed and weighed. The weight loss, converted to a volume, is equal to the amount of water that has infiltrated into the ground. An infiltration rate is then determined from this volume of water, the area of the inner ring, and the interval of time. This process is repeated and a plot of infiltration rate versus time is constructed. The test is continued until the infiltration rate becomes steady or until it becomes equal to or less than a specified value.

#### 5. Significance and Use

5.1 This test method provides a means to measure low infiltration rates associated with fine-grained, clayey soils, and are in the range of  $1 \times 10^{-7}$  m/s to  $1 \times 10^{-9}$  m/s.

5.2 This test method is particularly useful for measuring liquid flow through soil moisture barriers such as compacted clay liner or covers used at waste disposal facilities, for canal and reservoir liners, for seepage blankets, and for amended soil liners such as those used for retention ponds or storage tanks.

5.3 The purpose of the sealed inner ring is to: (1) provide

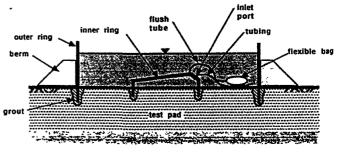


FIG. 1 Schematic Of A Double-Ring Infiltrometer With A Sealed Inner Ring

¹ This test method is under the jurisdiction of ASTM Committee D-18 on Soil and Rock and is the direct responsibility of Subcommittee D18.04 on Hydrologic Properties of Soil and Rocks.

Current edition approved June 29, 1990. Published August 1990.

² Annual Book of ASTM Standards, Vol 04.08.

a means to measure the actual amount of flow rather than a drop in water elevation which is the flow measurement procedure used in Test Method D 3385 and (2) to eliminate evaporation losses.

5.4 The purpose of the outer ring is to promote onedimensional, vertical flow beneath the inner ring. The use of large diameter rings and large depths of embedments helps to ensure that flow is essentially one-dimensional.

5.5 This test method provides a means to measure infiltration rate over a relatively large area of soil. Tests on large volumes of soil can be more representative than tests on small volumes of soil.

5.6 The data obtained from this test method are most useful when the soil layer being tested has a uniform distribution of pore space, and when the density and degree of saturation and the hydraulic conductivity of the material underlying the soil layer are known.

5.7 Changes in water temperature can introduce significant error in the volume change measurements. Temperature changes will cause water to flow in or out of the inner ring due to expansion or contraction of the inner ring and the water contained within the inner ring.

5.8 The problem of temperature changes can be minimized by insulating the rings, by allowing enough flow to occur so that the amount of flow resulting from a temperature change is not significant compared to that due to infiltration, or by connecting and disconnecting the bag from the inner ring when the water in the inner ring is at the same temperature.

5.9 If the soil being tested will later be subjected to increased overburden stress, then the infiltration rate can be expected to decrease as the overburden stress increases. Laboratory hydraulic conductivity tests are recommended for studies of the influence of level of stress on the hydraulic properties of the soil.

#### 6. Apparatus

6.1 Infiltrometer Rings—The rings shall be constructed of a stiff, corrosion-resistant material such as metal, plastic, or fiberglass. The shape of the rings can be circular or square. However, square rings are recommended because it is easier to excavate straight trenches in the soil. The rings can be of any size provided: (1) the minimum width or diameter of the inner ring is 610 mm (24 in.); and (2) a minimum distance of 610 mm is maintained between the inner and outer ring. The following is a description of a set of rings that can be constructed from commonly available materials, incorporates the requirements described above, and has worked well in the field.

6.1.1 Outer Ring—A square ring (Fig. 2) comprised of four sheets of aluminum approximately 3.6 m by 910 mm by 2 mm (12 ft by 36 in. by 0.080 in.) The top edge of the aluminum sheet is bent 90° in order to provide rigidity: A hole is provided in the center of the top edge. One edge of each sheet is bent 90°. Holes are drilled along each side edge so that the sheets can be bolted at the corners. A flat rubber gasket provides a seal at each corner. A wire cable approximately 15 m long with a clamp may be needed to tie the top edges together.

6.1.2 Inner Ring—A square ring (Fig. 3), 1.52 m (5 ft) on a side, made of fiberglass provided with two ports. The top is

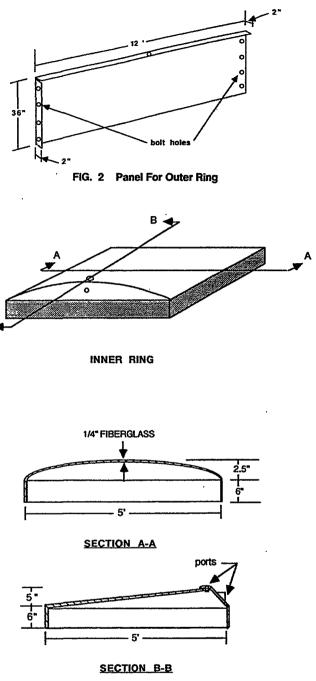


FIG. 3 Inner Ring

shaped in such a way as to vent air from the ring as it is filled. A port is provided at the highest point so that any air that accumulates in the ring during the test can be flushed out. One port must be located at the top of the ring. The other port must be located beneath the top port. A 150 mm (6 in.) skirt, that is embedded into the soil, is provided along the edge of the ring. Barbed fittings that accept flexible tubing are attached to the ports. Handles are provided at each corner of the inner ring.

6.2 *Flexible Bag*—Two clear flexible bags with a capacity of 1000 to 3000 mL. Intravenous bags available from medical supply stores work well. A means for attaching a

shut-off valve to the bag shall be provided. The shut-off valve shall be provided with a barbed fitting that will connect to the inlet tube on the inner ring.

6.3 *Tubing*—Clear, flexible tubing approximately 4.5 m (15 ft) long with a minimum ID of 6 mm (1/4 in.)

6.4 Scissors or Knife.

6.5 Excavation Tools.

6.5.1 *Mason's Hammer*—Hammer with a blade approximately 120 mm long and 40 mm wide.

6.5.2 Trenching Machine—Capable of excavating a trench with a maximum width of 150 mm (6 in.) and a depth of 460 mm (18 in.)

6.5.3 *Chain Saw*—(Optional—see Note 1) Equipped with a carbide-tipped chain and bar.

6.5.4 Hand Shovel, garden type.

6.6 Levels—A surveyor's level and rod and a carpenter's level.

6.7 Buckets—Five buckets with a capacity of approximately 20 L (5 gal.)

6.8 *Blocks*—Cinder blocks to serve as a platform for the flexible bag.

6.9 Cover—An opaque cover to place on top of the outer ring. The cover can be a tarp or plywood supported by wooden beams.

6.10 Grout—A bentonite grout for filling the trenches and sealing the rings in place.

6.11 *Mixing Equipment*—A large (four bag) grout mixer for mixing the bentonite grout.

6.12 Trowel.

6.13 Thermometer—Readable to  $0.5^{\circ}$ C with a range of 0 to 50°C.

6.14 Scale-Capacity of 4000 g and an accuracy of 1 g.

6.15 Watch—Readable to 1 s.

6.16 *Water Supply*—Preferably water of the same quality as that involved in the problem being examined. Approximately 5600 L (1400 gal) are needed for this test.

6.17 Splash Guard—Plywood, rubber sheet, or burlap 600 by 600 mm (2 by 2 ft).

#### 7. Test Site

7.1 The test requires an area of approximately 7.3 by 7.3 m (24 by 24 ft).

7.2 The slope to the test area should be no greater than approximately 3 %.

7.3 The test may be set up in a pit if infiltration rates are desired at depth rather than at the surface.

7.4 The test area shall be covered with a sheet of plastic to keep the surface from drying.

7.5 Representative samples of the soil to be tested shall be taken before and after the test to determine its moisture content, density, and specific gravity. The thickness of the layer being tested shall be determined as well as the approximate hydraulic conductivity of the layer beneath it.

#### 8. Procedure

8.1 Assembly of Outer Ring—Wipe off gaskets and side edges of the outer ring. Align gasket between the edges and bolt edges together.

8.2 Excavation of Trenches:

8.2.1 Place both rings on the area to be tested. Center the inner ring within the outer ring. Make sure that the outer

ring is square by using the tape measure to check that the length of the diagonals are equal.

8.2.2 If plastic is covering the test area, cut out thin strips along the edge of each ring so that the trenches can be excavated. Leave as much of the plastic on as possible in order to keep the soil from drying.

8.2.3 Use the bottom edge of each ring to scribe a line on the ground to use as a guide for excavating the trenches.

8.2.4 Note the orientation of the rings and set them aside.

8.2.5 Use the surveyor's level and check the ground elevation where the corners of each ring will be. Note the high spots and excavate deeper in these areas so that the rings will be level.

8.2.6 Use the trenching machine and excavate a trench for the outer ring. The trench should be about 146 mm (18 in.) deep. Excavate deeper at high spots.

8.2.7 Use a small hand shovel to remove any loose material in the trenches.

8.2.8 Place the outer ring in the trench and use the carpenter's level to check that the top of the ring is reasonably level ( $\pm 30$  mm). Also check that the outer ring is square. Remove the ring and excavate any areas keeping the ring from being level and square.

8.2.9 Set the outer ring aside and cover the trenches to prevent the soil from drying.

8.2.10 Use the mason's hammer and excavate a trench 50 by 110 mm (2 by 4.5 in.) for the inner ring. Excavate deeper in high spots so that the inner ring will sit level in the trench. Excavate the trench carefully so that the surrounding soil is disturbed as little as possible. When using the mason's hammer, it is best to start by digging down several inches in one spot and then advancing the trench forward by chopping down on the soil. Do not pry the soil up as this tends to lift up large wedges of soil, opens cracks, and causes the trench to be oversized.

8.2.11 Place the inner ring in the trench to check the fit. Excavate any areas where the ring does not fit. Use a surveyor's level to check the elevation of the corners of the ring. The inner ring needs to be level or slightly tilted so that the back end is slightly lower than the front end.

8.2.12 Set the ring aside and cover the trenches.

NOTE 1—A chain saw that is equipped with a carbide-tipped chain and a bar may be used to excavate the trenches. Use of a chain saw will not only reduce the time needed to excavate the trench but will also greatly decrease the amount of grout needed to fill the trenches. If a chain saw is used, the trenches need only be 25 mm (1 in.) wide. A chain saw will not work well in some soils. A trial trench should be made to determine if it will work.

#### 8.3 Installation of Rings:

8.3.1 Use the grout mixer to prepare enough grout to fill the trenches. The hydraulic conductivity of the grout should be less than approximately  $1 \times 10^{-8}$  m/s.

8.3.2 Fill the trenches to within 2.5 mm (1 in.) of the top of the trench. Rod or tamp the grout to remove any entrapped air.

8.3.3 Lift the inner ring and center it over the inner ring trench. Lower it into the trench and slowly push it down. Keep the ring level as it is pushed into place.

8.3.4 Use a surveyor's level to check that the ring is level. 8.3.5 Use a trowel to press the grout against the outside

wall of the ring in order to ensure a good seal.

8.3.6 Cover the grout with plastic to prevent desiccation.

8.3.7 Lift the outer ring and center it over the outer ring trench.

8.3.8 Keep the ring level and push it into place.

8.3.9 Use the carpenter's level to make sure that the ring is level.

8.3.10 Use a trowel to push the grout against both the inside and the outside of the ring to ensure a good seal.

8.3.11 Cover the grout with plastic to prevent desiccation.

8.3.12 Place several cinder blocks between the inner and outer rings in the vicinity of the ports on the inner ring. These blocks will be used as a platform to stand on when connecting the fittings to the inner ring and also to support the flexible bags. The blocks should be no higher than 100 mm (4 in.)

8.3.13 Pile soil along the outside of the outer ring to a height of at least 30 cm (12 in.) This soil places an overburden pressure on the grout that will prevent it from being pushed out of the trench when the rings are filled with water.

**8.4** *Filling the Rings:* 

8.4.1 Fill two buckets with water and place one on each back corner of the inner ring. The buckets are placed on the inner ring to counteract the uplift force that acts on the ring as it is being filled. Make sure that the buckets are placed on the edge of the ring, not in the center as this may overstress the ring and cause it to crack. Do not to spill any water around the inner ring as this will make it difficult to check for leaks in the seal.

8.4.2 Place an empty bucket upside down on the ground near the top port on the inner ring. Place a second bucket on the first bucket. Fill the second bucket with water. Cut a length of the flexible tubing long enough to reach from the top bucket to the top port on the inner ring. Siphon the water from the bucket to the inner ring. Allow the siphoning to continue until the depth of the water in the inner ring is approximately 25 mm (1 in.). Avoid spilling any water around the inner ring during this filling process as this will make it difficult to check for leaks. Any other suitable method for adding the required volume of water to the inner ring may also be used.

8.4.3 Let the water stand in the inner ring for at least 30 min. Check for leaks in the inner ring seal and repair any that are found.

8.4.4 Start filling the outer ring slowly so as not to scour the soil and muddy the water. Direct the water so that it hits a splashboard first. Fill the outer ring until the water level is approximately 100 mm (4 in.) above the top of the inner ring. While the rings are being filled, use a board or shovel handle to gently tap the inner ring to dislodge air bubbles that are trapped inside. Continue tapping on the inner ring until bubbles cease to emerge from the top port.

8.4.6 Remove the buckets from the top of the inner ring.

8.5 Installation of Fittings and Tubing:

8.5.1 Wrap the threads of the two barbed fittings with TFE-fluorocarbon tape.

8.5.2 Saturate the fittings and connect them to the inner ring. Screw one of the barbed fittings into the top port and the other barbed fitting into one of the lower ports. Use caution when screwing the fittings into the ports as the threads in fiberglass inner rings can be easily damaged. 8.5.3 Cut two lengths of the clear flexible tubing, one 900-mm (3-ft) piece and one 1800-mm (6-ft) piece.

8.5.4 Saturate the tubing by placing it under water. Be sure to remove all air bubbles.

8.5.5 Connect one end of the 1.8-m (6-ft) piece to the fitting in the top port and seal the other end with a plug fitting. Do not let air into the tube during this process. This tube is the flush tube.

8.5.6 Connect the end of the 900-mm (3-ft) piece to the barbed fitting in the lower port. Prop the open end of this tube on the cinder block platform. Water is being drawn into this tube so be sure not to allow the open end of the tube to float to the surface and draw in air or sink to the bottom and draw in mud. This tube is the inlet tube.

8.6 Covering the Rings:

8.6.1 Cover the rings with either a tarp or plywood. The purpose of the cover is to minimize evaporation, minimize temperature changes, and inhibit the growth of algae.

8.6.2 Provide a means in the cover that makes it convenient to access the front of the inner ring to connect and disconnect the measurement bag.

8.7 Maintaining the Water Level:

8.7.1 Place a mark indicating the water elevation on the inside wall of the outer ring near the cinder blocks.

8.7.2 Observe the water level within the outer ring during the test and refill the ring to this mark before the water level drops more than 25 mm (1 in.) below the mark. Record the date, time, and the amount of water added.

8.8 Purging the Inner Ring—During the test, air may accumulate beneath the inner ring. This air may introduce error in flow measurements and consequently should be purged on a regular basis as follows.

8.8.1 Disconnect bag, if one is present, from end of inlet tube.

8.8.2 Lift the plugged end of the flush tube out of outer ring and below the water level in the outer ring so that water can be siphoned out of inner ring.

8.8.3 Remove plug from end of flush tube. Water and air if present will start to flow out of inner ring. If air completely fills the tube, the syphon will be lost. If this happens, saturate the tube and restart the siphon.

8.8.4 Allow water to flow from end of tube until air ceases to emerge from inner ring. Replace plug in end of flush tube and place tube back into outer ring. Note the approximate volume of purged air. Volume can be determined by multiplying the flow area of the flush tube by the height of the air bubbles which flow out of the tube.

8.8.5 Wait at least 30 min before taking any flow measurements.

8.8.6 Purge the inner ring on a weekly basis until no significant amount of air is found.

8.9 Measurements:

8.9.1 Attach the shut-off valve to the flexible bag and fill the bag with water. Remove all air bubbles from the bag. Use water that has been degassed or allow the bag to sit overnight so that the water can degas. If left to sit overnight, remove any air bubbles. Do not overfill the bag so that the water inside is under pressure.

8.9.2 Dry the outside of the bag and record its weight to the nearest gram.

8.9.3 With the shut-off valve closed, attach the bag to the

open end of the inlet tube connected to the inner ring. Be sure not to trap any air bubbles in the inlet tubing or in the valve when attaching the bag. Lay the bag down on the cinder block platform.

8.9.4 Record the time, date, temperature of the water in the outer ring, and the depth of the water in the outer ring, and then carefully open the shut-off valve on the bag. Check that the inlet tube is not pinched and that the bag is arranged in such a manner that water can flow freely from it into the inner ring.

8.9.5 Sometime before the bag empties, close the shut-off valve, disconnect the bag from the inlet tube, and record the date, time, temperature of the water in the outer ring and the depth of the water in the outer ring. Be sure to prop the open end of the inlet hose as pointed out in 8.5.6. Do not leave the bag on long enough to empty as this will create a suction in the inner ring and cause leaks in the grout seal.

8.9.8 Dry the bag and record the weight of it to the nearest gram.

8.9.9 Refill the bag and repeat 8.9.2 through 8.9.8 until the infiltration rate (see Section 9) becomes steady or drops below a predetermined value.

NOTE 2—The reading times are governed primarily by the length of time the bag can remain connected to the inner ring without emptying. This length of time can only be determined through experience. Initially, flow rates will be high and the bag may need to be disconnected after several hours. As the test progresses, the flow rate will slow and the length of time it takes the bag to empty may increase to several days or weeks.

A second important factor that governs when readings should be made is the temperature of the water. In order to minimize the effects of temperature changes on the measured flow rate, the bag should be disconnected from the inner ring when the water is at the same temperature (within  $\pm 2^{\circ}$ C) as when the bag was connected. More consistent readings are usually obtained if readings are made between 7 am and 9 am.

NOTE 3—It is not necessary to have the bag connected to the inner ring continuously. Flow only needs to be measured over timed intervals so that a plot of infiltration rate versus time can be constructed. The infiltration rate is not influenced by whether or not the bag is connected to the inlet tube. If the flow rate is high, it is more convenient to connect the bag to the inner ring for several hours a day and leave the inlet tube open in the outer ring for the remainder of the time.

NOTE 4—When connecting or disconnecting the bag from the inner ring, do not raise the bag above the level of the water in the outer ring with the shut-off valve open. This would cause an uplift force to act on the inner ring and could cause it to rise out of the trench.

8.10 Ending Test:

8.10.1 Remove the fittings and tubing from the inner ring.

8.10.2 Drain water from rings.

8.10.3 Excavate the grout from around the rings and pull the rings out of the ground.

8.10.4 Excavate a narrow trench in the area encompassed by the inner ring and take moisture content samples every 25 mm (1 in.) to a depth of 150 mm (6 in.) below the observed wetting front. An alternative to this is to push a thin-walled sampling tube into the soil, extrude the soil, and slice it every 25 mm (1 in.) for moisture content samples.

#### 9. Calculation

9.1 Calculate the infiltration rate for each timed interval as follows:

$$I(\mathrm{m/s}) = \frac{Q}{tA} \times 10^{-6}$$

where:

Q = volume of flow, mL,

 $= W_1 - W_2$ 

 $W_1$  = initial weight of bag, g,

 $W_2 = \text{final weight of bag, g,}$ 

 $t = \text{time of flow, s} = t_2 - t_1,$  $t_1 = \text{time shut-off valve on bag was opened,}$ 

 $t_1$  = time shut-off valve on bag was opened,  $t_2$  = time shut-off valve was closed, and

 $t_2$  = time shut-off valve was closed, and A = area of inner ring, m².

9.2 Calculate the amount of flow which resulted from any temperature fluctuations for each timed interval (see Note 5). If the flow due to temperature fluctuations is greater than 20 % of the total flow measured, then correct the flow used to calculate the infiltration rate by this amount.

Note 5—Expansion and contraction of the inner ring due to temperature changes will cause water to flow into or out of the measurement bag. The inner ring should be calibrated to determine if the flow resulting from temperature change is significant compared to flow due to infiltration. Calibration can be performed by sealing the inner ring to the bottom of a small plastic pool. Fill the pool and ring with water and allow the temperature to reach equilibrium. Connect a measurement bag to the inner ring and add ice to the pool water to lower the temperature several degrees. Allow the temperature to reach equilibrium and remove the bag. Determine the weight loss/gain and convert it to a volume of water. Divide this volume of water by the change in temperature to obtain a calibration factor for temperature changes.

9.3 Note the volume of air expelled from the weekly purging of the inner ring. Compare this volume of air with the volume of infiltration that occurred during the time the air collected in the inner ring. If this volume is significant, (that is, 20 % of that used to determine infiltration in 9.1,) then adjust the infiltration rates in 9.1 to account for it.

#### 10. Report

10.1 Report the following information:

10.1.1 A data sheet such as the one shown in Fig. 4,

10.1.2 A semi-log plot of infiltration versus time such as that shown in Fig. 5,

10.2 Additional optional information that can be presented in the report includes the following,

10.2.1 Thickness of layer tested,

10.2.2 A description of material beneath the layer tested,

10.2.3 Total and dry density of the layer tested,

10.2.4 Initial moisture content of the layer tested,

10.2.5 Initial degree of saturation,

10.2.6 Moisture contents of samples taken after termination of test,

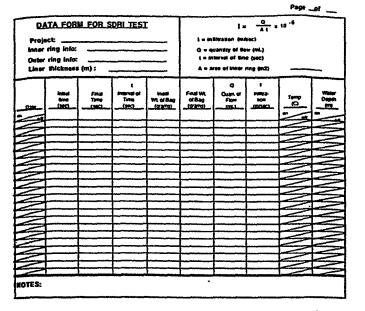
10.2.7 Estimate of the depth to the saturation front.

#### 11. Precision and Bias

11.1 Precision—Due to the nature of the soil or rock materials tested by this test method, it is either not feasible or too costly at this time to produce multiple specimens which have uniform physical properties. Any variation observed in the data is just as likely to be due to specimen variation as to operator or laboratory testing variation. Subcommittee (IIII) D 5093

(CM/SEC)

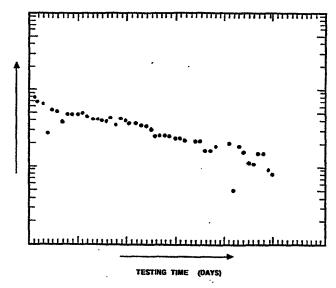
INFILTRATION RATE



#### FIG. 4 Data Sheet For Infiltration Test Using A Double-Ring Infiltrometer With A Sealed Inner Ring

D18.04 welcomes proposals that would allow for development of a valid precision statement.

11.2 Bias-There is no accepted reference value for this





test method, therefore, bias cannot be determined.

#### 12. Keywords

12.1 double ring infiltration; in-place infiltration; soil moisture infiltrometer

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