

State Estimation provides an estimated value of measurands for all correctly telemetered/non-telemetered/incorrect data and hence acts as a cross-check reference helping in Bad Data detection.

Output of the State Estimator provides Voltage Magnitude and Angle at each bus and hence gives a base-case for all the Network Applications and some of the generation applications to carry out various studies in order to help grid operator in real-time operation.

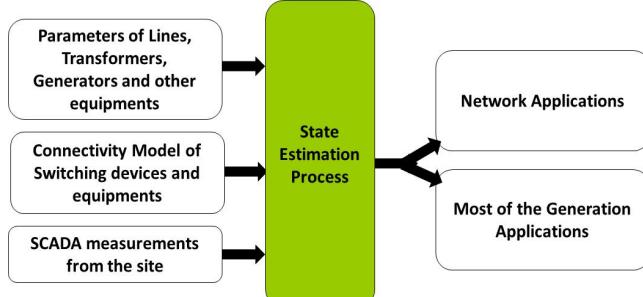
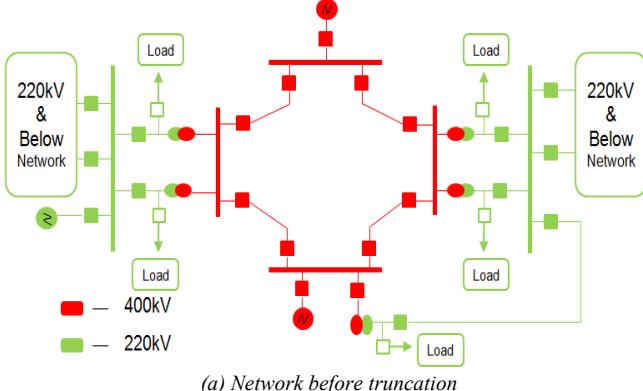


Fig.3: Base case generation from State Estimation process

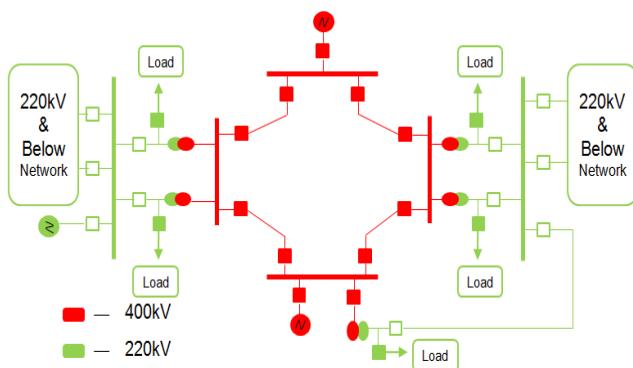
III. Corrections Done to Improve State Estimator Solution

1. Network Truncation

The Network Model at NLDC is vast consisting of more than 1800 sub-stations. Updating and maintaining (or tuning) such a large network model for State Estimation is very difficult. In order to focus on the main network and considering only on the major portion (say 400kV level and above) Network Truncation is done.



(a) Network before truncation



(b) Network after truncation

Fig.4: Truncation of network at 400kV and above voltage level at NLDC

While carrying out network truncation; the external model is ignored and a Load/Injection is modeled at the point of truncation with the real-time MW and MVAR data of the mapped to it.

Facility to study 400 kv network of NLDC					
NR	NER	ER	SR	VR	EX
ALL OPEN Open all switching devices and disable statical retrieval from scada	ALL OPEN				
ALL FREE Open all switching devices and enable statical retrieval from scada	ALL FREE				
REDUCE OPEN Open all switching devices not at 400 kv and connect pseudo loads at LV side of all 400kV ICTs	REDUCE OPEN				
REDUCE FREE Open all switching devices not at 400 kv statical retrieval from scada and disconnects pseudo loads	REDUCE FREE				
Steps for Truncation: <ul style="list-style-type: none"> Click on "REDUCE OPEN" opens all switching devices NOT at above 400KV level and connects modeled loads at LV side of all 400kV ICTs Click on "REDUCE FREE" connects the different regional networks through all defined regional links. 	I CONNECT I CONNECT	NE CONNECT DIS-CONNECT	ER CONNECT DIS-CONNECT	SR CONNECT DIS-CONNECT	ER CONNECT DIS-CONNECT
CONNECT ALL DIS-CONNECT ALL CONNECT 220 KV Connect selected 220 kv substations. File : rnetv\connect_220kv_L1\listbd.in memlist\memlist2	CONNECT ALL DIS-CONNECT ALL				
	CONNECT 220 KV				

Fig.5: Display at NLDC to facilitate truncation of network at 400kV and above level

2. Network Parameters

State Estimation requires correct model parameters of the network. Incorrect parameters of various power system equipments impact the State Estimator output.

2.1 Correction in Line Parameters

Incorrect line parameters cause change in impedance of paths, hence different flows (MW and MVAR) than actual, and change in the estimated angles at the station buses. Many cases of incorrect parameters were observed and rectified. An example is shown in **Fig.6**.

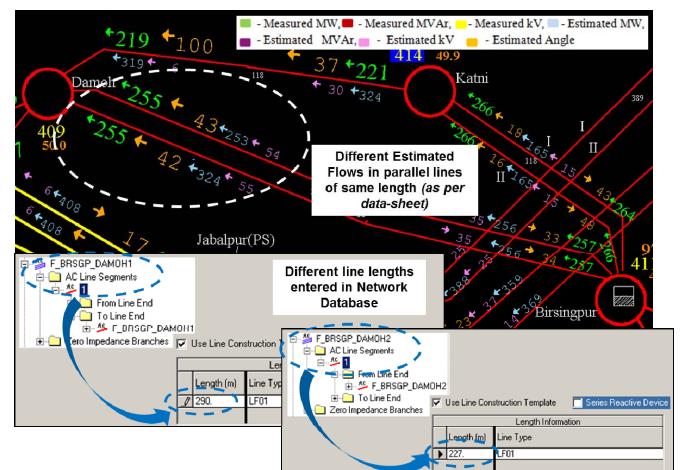


Fig.6: Impact of different line length on SE output

2.2 Correction in ICT Parameters

In transformers the tap changer types and winding parameters were corrected at many places in database. ICT parameters include Series Resistance, Series Reactance, Tap Changer details (number of taps and step size), Nominal voltage of HV and LV side, placement of Tap changer (HV or LV side), etc.

For number of ICTs in database, it was found that the Step size was incorrect (in magnitude or sign) and also Tap changer was placed at both HV and LV side, which is not as per the field equipment. Generally, Tap changer is put on HV side of transformer. Further, Resistance and Reactance were also corrected for many ICTs as per its MVA ratings and design.

It was found that in some stations all the ICTs are not of the same MVA rating and hence possess different impedance

and different MW flow. In all such cases the parameters of ICTs were changed accordingly.

2.3 Correction in Generating Unit Parameters

In the Network database, the Generating Units need to be properly defined with number of parameters such as Maximum/Minimum MW capacity, Maximum/Minimum MVAR capacity, MVA rating, etc. The generating unit parameters were taken from the Annual Compendium Booklet of POSOCO and updated in database.

All these parameters impact the State Estimator Output considerably. An example is shown in *Fig.7*.

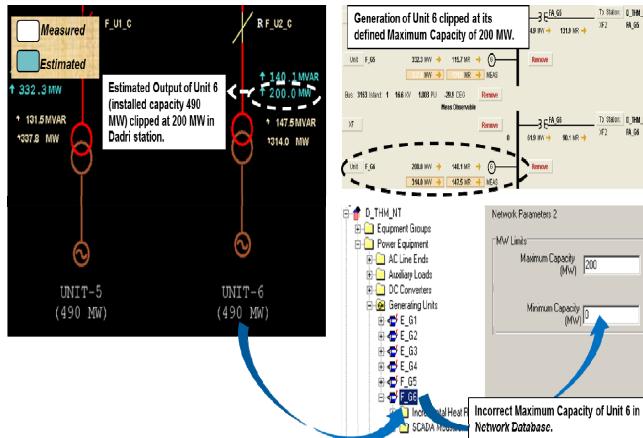


Fig.7: Impact of incorrect Maximum/Minimum MW limits on SE output

3. Incorrect Mapping of switching devices between NLDC and RLDCs

In order to exchange data between two systems with different naming convention in ICCP, it is required that ICCP mapping shall be done at either of the ends. In case of incorrect ICCP mapping the topology of the system as changed on the site is not exactly replicated at NLDC. An example is shown in *Fig.8*.

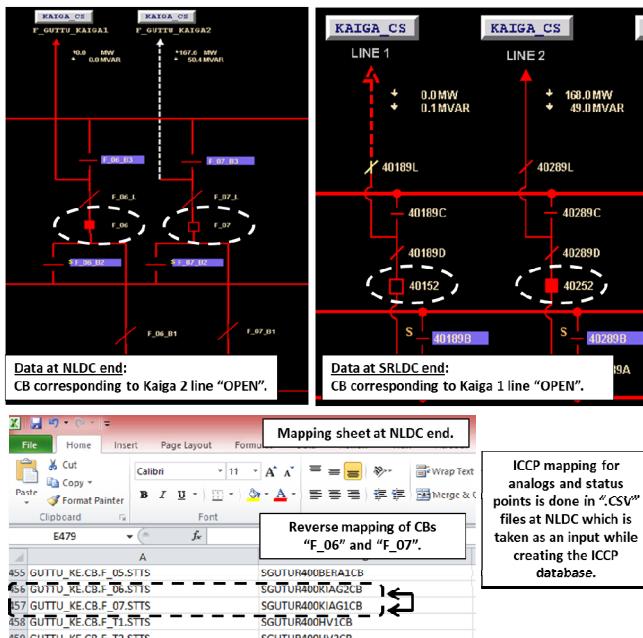


Fig.8: Incorrect mapping of switching device at NLDC

4. Topology Correction

The first step executed by almost all the State Estimator applications worldwide is Topology Processing. Topology Processor extracts the line-energised network out of the total

network based on position of switching devices (i.e. Circuit Breakers and Isolators). If the output of topology processor deviates from the actual scenario at the site (due to incorrect/unavailable status) then output of SE application would also not of much use and many-a-times would not give a converged solution.

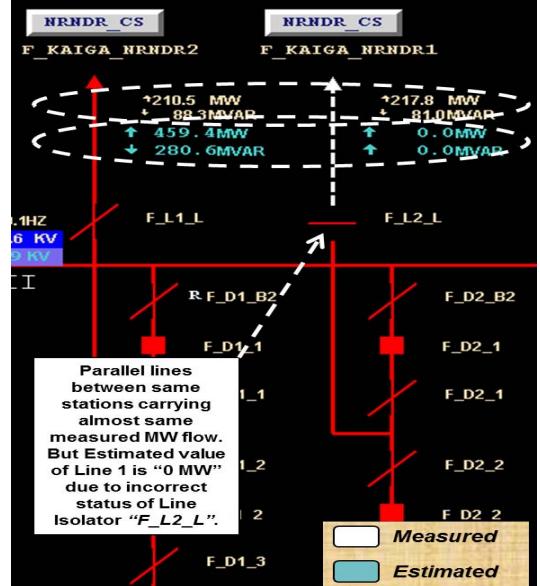


Fig.9: Impact of incorrect topology on SE output

First step taken towards Topology Correction is “Auto Replacement” of CB/Isolator positions to “CLOSED” using a script provided by vendor. Under this approach all switching devices which have “Suspect”, “Between” or “Garbage” status are replaced as “CLOSED” in Network data (real-time SCADA displays remain unaffected).

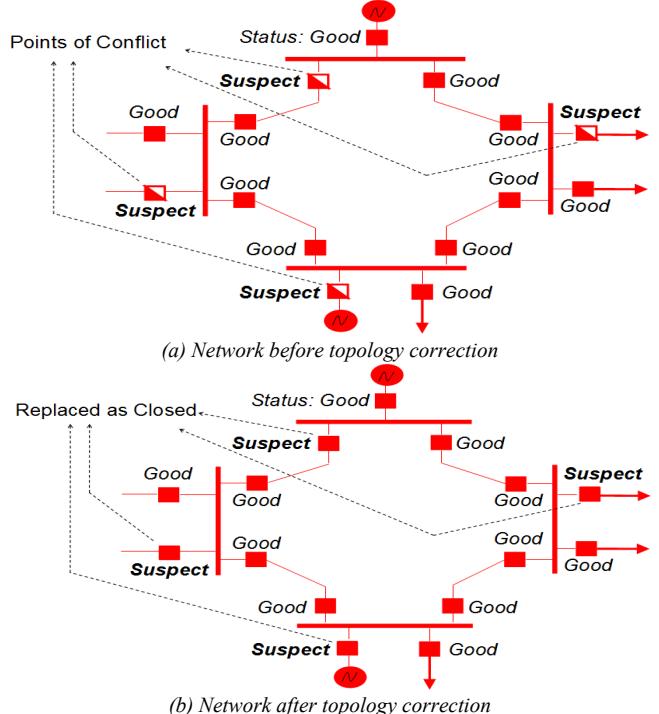


Fig.10: Topology Correction approach

Switching devices with “Suspect” quality status leads to point of conflict as it is not possible to make out whether the associated line is charged or under outage/tripping.

Status of switching devices with “Suspect” quality can be replaced as *CLOSED* for State Estimator application.

Another approach is to keep the last good value. Different vendors may have different approaches to handle this. Whatever approach is chosen one has to look at such device status & validate them and get the telemetry issue fixed. **Fig.11** further elaborates this approach of correcting the status information.

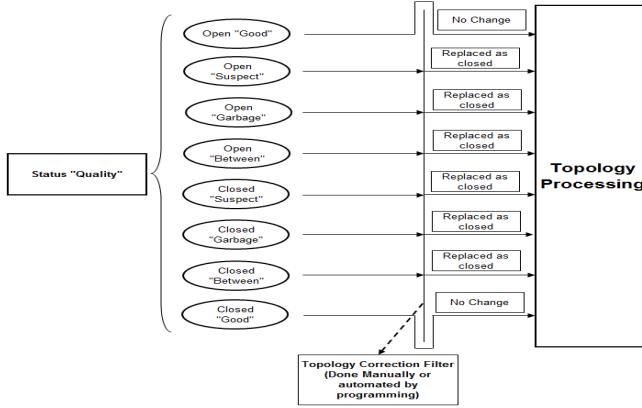


Fig.11: Topology correction

The status of switching devices with “Good” Quality remains unchanged.

5. Topology Estimation

Topology estimation checks could be performed on network to find ambiguity with respect to the line flows and status of the corresponding switching devices. Coherency warnings generated could be used to tune the network. The threshold for analog data for generating Coherency Warning is kept as 50 MW.

The drawback of topology estimation checks in NLDC system is that it does not consider the entire connectivity of the equipment to the bus. It only checks the coherency with the switching device (say Line Isolator) directly connected with the equipment.

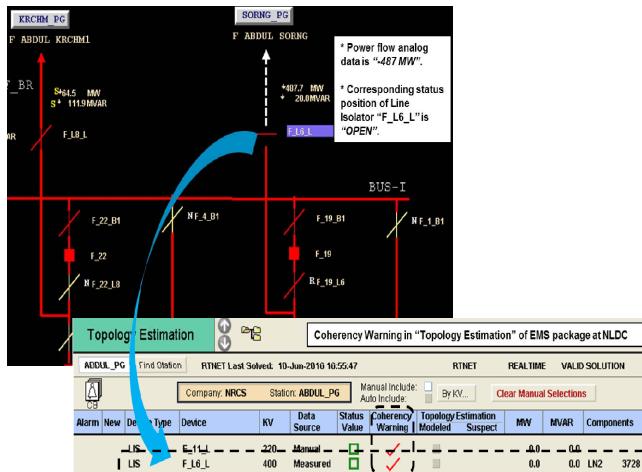


Fig.12: Topology Estimation with coherency warnings at NLDC

6. Status of Series Compensation

Indian Power System has more than 40 nos. of series compensation (FSCs and TCSCs) and the status of its bypass CB/Isolator is of utmost importance in depicting whether the Series Compensation device is in service or not. It was found that at many stations either the status of bypass CB/Isolator was incorrect or “suspect” leading to incorrect State Estimation at that point.

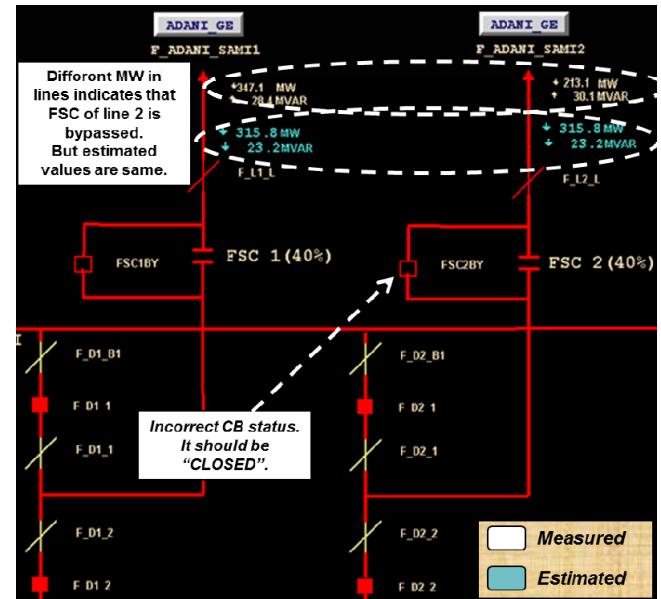


Fig.13: Incorrect status of bypass switching device of Series compensation

7. Modeling of Loads and Injections to cater HVDC connections

The HVDC lines are generally modeled as Truncated Loads/Injections with the real-time power flow data on the converter transformers mapped onto it. The AC filter banks are modeled as a set of Capacitors connected directly to the bus in order to provide the required MVARS. One of the examples of +/- 500kV Mundra-Mahendragarh HVDC Bipole is shown in **Fig.14**.

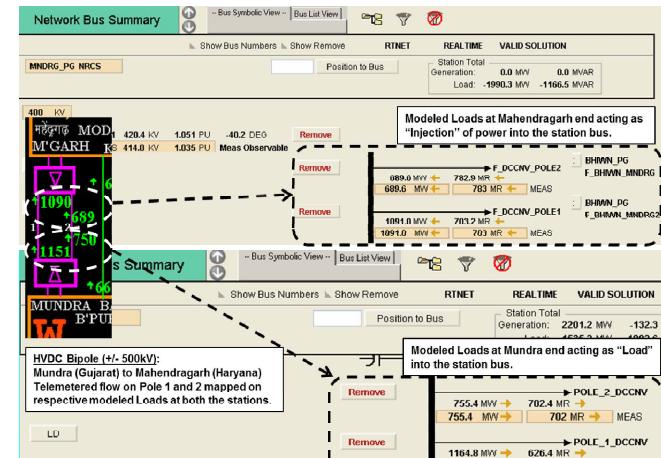


Fig.14: Modeling of Loads to cater HVDC flows in the network

8. Reverse Flow on parallel ICTs

In a number of stations it was observed that the MW,MVAR flow on parallel ICTs was opposite to each other. In some stations it was also found that the flow on ICTs was from LV to HV side without any source of generation at the Low Voltage side.

While truncation of network the secondary of some ICTs at 400/(less than 400kV) level the modeled loads at the point of truncation are mapped with either its primary or secondary value (as available). In case both side measurements are available, then either of it can be mapped to the modeled load. If the sign of value at Primary or Secondary gets reversed then it may cause the modeled load to act as Injection of power into the bus. An example is shown in **Fig.15** and **Fig.16**.

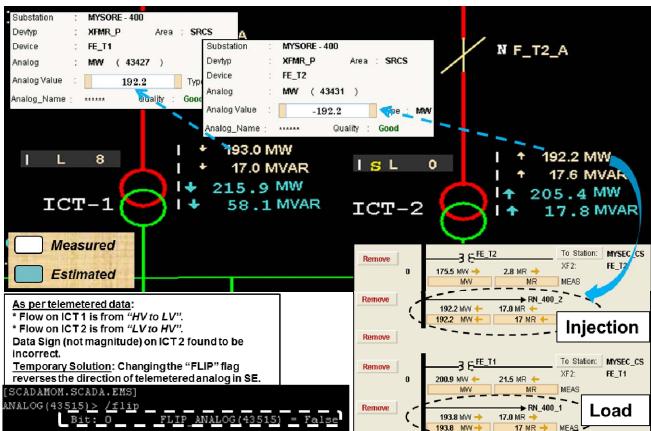


Fig.15: Impact of Reverse flow in parallel ICT on SE at NLDC in case of truncation at that point

It can be resolved temporarily (until data sign is corrected from site) by changing the “FLIP” flag associated with the Analog as “TRUE”. By doing this the incorrect value (in sign) will be reversed before getting transferred to SE application.

As per the sign convention of ICT related data in Load Despatch Centres, different philosophy for measuring transformer data is followed in different Regions. In Northern Region, when, power flows from HV side to LV side analog measurement is taken as Positive whether it is measured on HV side or LV side. Whereas, in other regions the flow directions are positive when the power flows from bus into the transformer. Hence the association of “FLIP” flag with modelled loads shall be as per **Table 1**.

Analog Data (HV side is referred as Primary)	Power flow from HV to LV	Power flow from LV to HV	FLIP Flag Status:		Flip Flag Status:	
			When Primary measurement mapped to load	NRLDC	When Secondary measurement mapped to load	NRLDC
Trf. Pri. MW/ MVAR	Positive	Negative	FALSE	FALSE	--	--
Trf. Sec. MW/ MVAR	Negative	Positive	--	--	FALSE	TRUE

Table 1: Association of “FLIP” flag at NLDC with measurements on ICTs mapped on loads at points of truncation

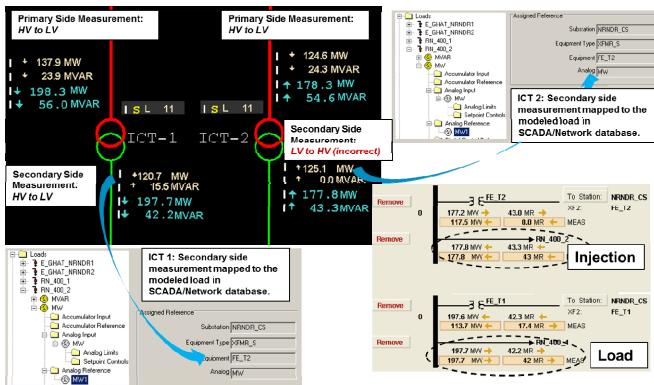


Fig.16: Impact of measurement mapping at modeled loads from Primary and Secondary end (including case of sign reversal)

9. Inserting calculated values on non-measured loads

Some of the State Estimation Algorithms do not try to change the MW and MVAR corresponding to loads. It either uses the real-time data-telemetry assigned to it or a Pseudo measurement taken from Load Scheduling (or any other source). If a Pseudo measurement is used then it has a high uncertainty level. In order to improve the State Estimator

solution the value of Load can be calculated online and inserted into the measurement of truncated loads. The most common way to calculate the Loads is by Bus Summation and equating the same to Zero.

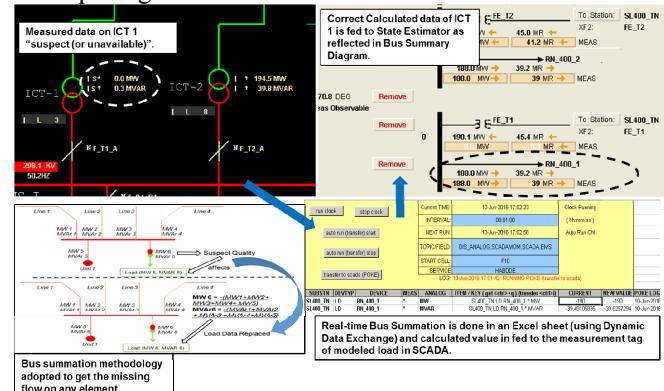


Fig.17: Inserting calculated values on non-measured loads

10. Modeling of Equivalent Generator in special cases

In many cases it was observed that the status of switching devices associated with Units was “suspect” leading to problem in topology Estimation whether to include the unit in SE process or not. In order to cater it, an equivalent generator was modeled and the sum of individual units was mapped to it. The equivalent generator always remains in-service and generates as per the “sum of all individual units”. An example is shown in **Fig.18**.

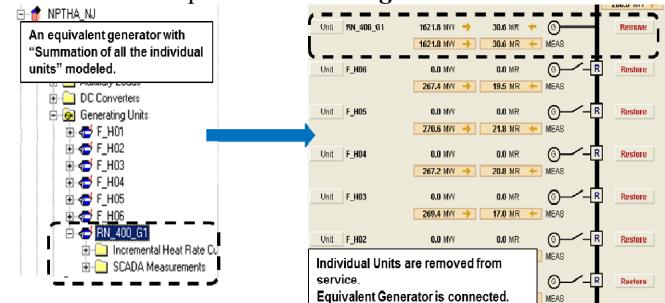


Fig.18: Modeling of equivalent generator

11. Tap Position of Transformers

At many sub-stations the Tap position of the ICTs is not available with “good” quality. As the OLTC of transformers is not frequently changed, it is manually replaced by Conforming its position from the field level. An example is given in **Fig.19**.

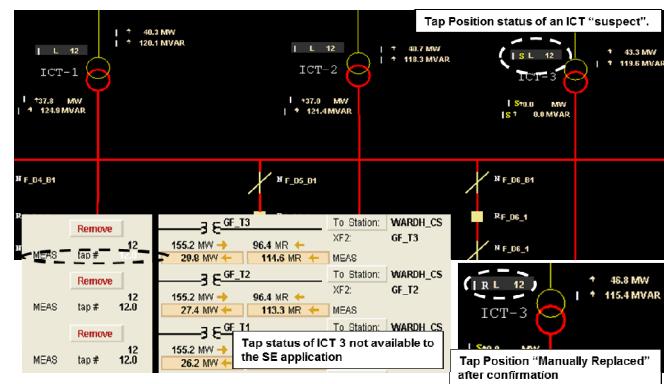


Fig.19: Unavailability of OLTC of ICTs

12. Re-initialising the parameters of State Estimation

The state estimation application has various parameters which need to be initiated after certain conditions are met every time it runs. In a large power system network, it is

many-a-times required to re-set it after certain defined number of run-times.

13. Threshold of Solution cost and other parameters

Many a times it is observed that the voltage and angle convergence is achieved while referring the analysis report, but the Solution is declared as Invalid. Generally, it is due to high cost of the solution exceeding the threshold limit as defined for it. Either the threshold limit of Solution Cost is increased temporarily or further tuning is done to handle such problems.

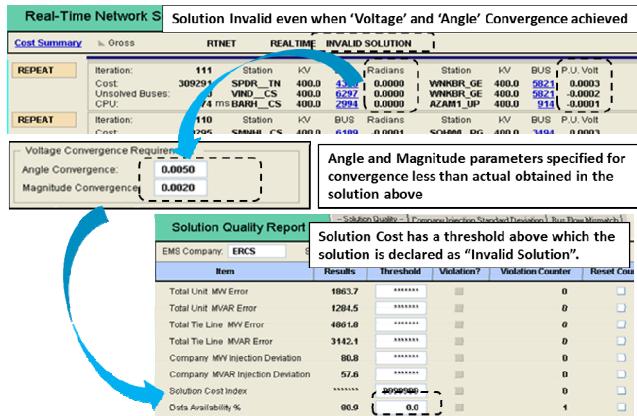


Fig.20: Threshold of Solution Cost in SE Application at NLDC

14. Unexpected connectivity changes at the site level

Due to various construction related problems (like Right of Way i.e. RoW, Contractual issues, material management issues, labour issues, modification in transmission planning, etc.) the line and bay connectivity changes either temporarily or permanently. It is many-a-times not known to the operator and when informed requires corresponding modeling change in SCADA and Network database.

It is also observed that many lines are modelled in database but do not get commissioned on site due to delay in construction. Such lines are set to “manually remove” from Network Database.

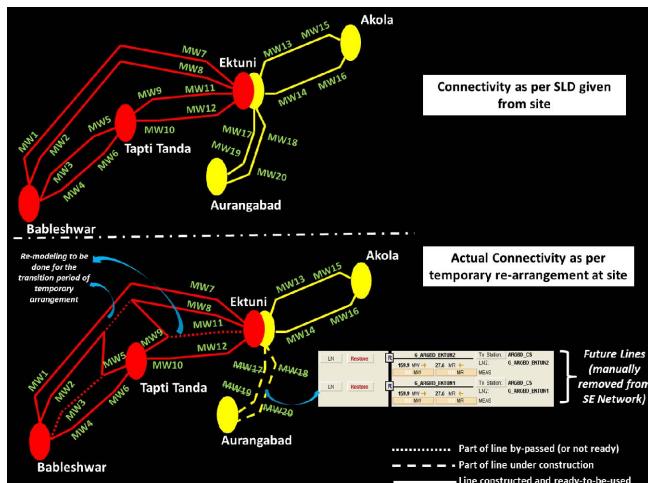


Fig.21: Re-arrangement of connectivity at the site level

An example of temporary re-arrangement is shown in Fig.21. It was observed that certain sections of few 400kV lines were not complete and hence re-arrangement as shown in Fig.21 above was done on temporary basis to facilitate early use of assets by the utilities. To compensate it, re-modelling of lines was done in database at NLDC. Moreover, two circuits of 765kV level were not

commissioned in time. So these circuits were set to “manually removed” from Network.

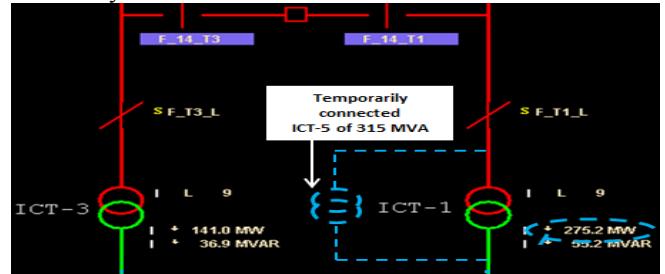


Fig.22: Parallel connection of ICT in same bay

In a special case at Mandaula substation as shown in Fig.22 it was found that the spare 400/220kV ICT was connected in parallel with ICT-1 in the same bay in order to meet the high load in Delhi during Commonwealth Games 2010 and High Summer Peak Load in 2015. In all such cases the parameters of ICTs must be put accordingly.

IV. Solution Quality of SE

After continuous correction of database parameters, connectivity model, topology errors and rectifying the bad-data by getting it corrected from the field, the cost of SE solution decreased significantly.

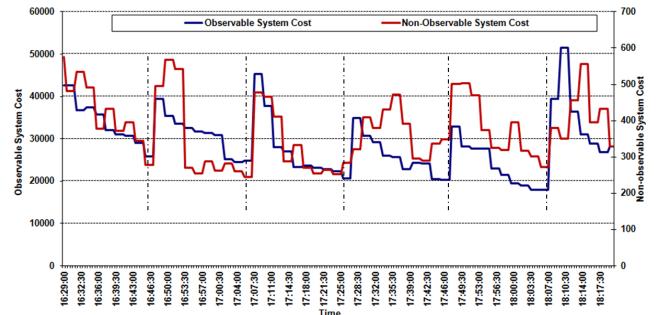


Fig.23: Reduction in SE Solution cost

V. Conclusion

Bad data and Incorrect Network Model Database severely affects the output of State Estimator and it needs to be corrected and maintained with utmost importance. As Topology formation is an initial and critical part of SE application but due to various reasons its telemetry is not correctly available from site. Efforts shall be made by the State and Central Utilities to provide the correct status of the switching devices by rectifying the related issues at site. Topology Estimation shall provide feature of auto-detecting the incorrect status of switching device on the basis of comparing the status with corresponding device MW flow and simultaneously correcting it. After all the efforts in tuning SE, it was found that Cost of State Estimator Solution decreased and a better converged solution was obtained from State Estimator Application at NLDC.

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REFERENCES

- [1] Power generation, operation and control, Allen J. Wood and Bruce F. Wollenberg, Second edition, 1996.
- [2] Power System State estimation – Theory and Implementation, Ali Abur and Antonio Gomez Exposito, 2004 edition.