



Tennessee Valley Authority, 1101 Market Street, Chattanooga, Tennessee 37402

CNL-14-077

June 13, 2014

10 CFR 50.4

ATTN: Document Control Desk
U.S. Nuclear Regulatory Commission
Washington, D.C. 20555-0001

Watts Bar Nuclear Plant, Unit 2
Construction Permit No. CPPR-92
NRC Docket No. 50-391

Watts Bar Nuclear Plant, Unit 1
Facility Operating License No. NPF-90
NRC Docket No. 50-390

Subject: Responses to Degraded Voltage Issue Requests for Additional Information

- References:
1. Letter from TVA to NRC, "Watts Bar Nuclear Plant (WBN) Unit 2 - Safety Evaluation Report Supplement 22 (SSER22) - Response to NRC Required Action Item, dated August 12, 2011 [ML11229A020]
 2. Letter from TVA to NRC, "Watts Bar Nuclear Plant, Unit 2 - NUREG-0847 Supplemental Safety Evaluation Report (SSER) Related to the Operation of Watts Bar Nuclear Plant, Unit 2, Appendix HH Open Item 30 - Power System Degraded Voltage," dated June 7, 2012 [ML12160A350]
 3. NRC Regulatory Issue Summary (RIS) 2011-12, Revision 1, "Adequacy of station Electrical Distribution System Voltages," dated December 29, 2011 [ML113050583]
 4. NRC Electronic Mail (email) from Siva Lingam to Gordon Arent, on Watts Bar 2 - Open Phase and Open Item 30 RAIs, dated February 27, 2014
 5. NRC Public Meeting Announcement with Tennessee Valley Authority (TVA) regarding Safety Evaluation Report electrical open items related to Watts Bar Nuclear Plant, Unit 2, April 24, 2014 [ML14100A313]
 6. Letter from NRC to TVA, "Watts Bar Nuclear Plant - NRC Integrated Inspection Report 05000390/2010005," dated January 28, 2011 [ML110280456]

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By letter dated August 12, 2011 (Reference 1), Tennessee Valley Authority (TVA) provided a response to NUREG-0847, Supplement 22, "Safety Evaluation Report Related to the Operation of Watts Bar Nuclear Plant, Unit 2," Appendix HH, Open Item 30.

By letter dated June 7, 2012 (Reference 2), TVA submitted updated information related to the offsite and onsite power system degraded voltage studies for safety-related electrical equipment. This submittal included excerpts from STUDY-EEB-WBN-12-001, "Sensitivity Study of Degraded Voltage Relay (DVR) Protection During Motor Starting," Revision 1. The information provided in Reference 2 demonstrated the impact of using a methodology meeting the intent of the guidance provided in Nuclear Regulatory Commission (NRC) Regulatory Issue Summary (RIS) 2011-12, "Adequacy of station Electrical Distribution System Voltages," Revision 1 (Reference 3).

On February 27, 2014, TVA received additional requests for information related to open phase and NUREG-0847, Open Item 30 (Reference 4), including questions associated with Watts Bar Nuclear Plant (WBN), Unit 2 Final Safety Analysis Report (FSAR) Section 8.3. The responses to these requests for additional information (RAIs) are included in this transmittal as Enclosure 1.

On April 24, 2014, the NRC conducted a public meeting with members of TVA (Reference 5). The purpose of the meeting was to discuss the status of electrical open items resulting from the NRC review of the FSAR for WBN Unit 2.

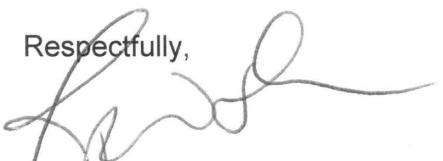
TVA addressed a non-cited violation (NCV) identified in Reference 6 by performing a motor starting analysis in the calculation of record at the DVR dropout analytical limit as opposed to the DVR reset. The analysis is provided in Appendix H of Enclosure 2.

Enclosure 1 to this letter also provides the TVA response to the information requested at the April 24, 2014 public meeting, including responses to the RAIs received in Reference 4. Enclosure 2 provides a copy of the Sensitivity Study of Degraded Voltage Relay (DVR) Protection During Motor Starting, Revision 2, performed by TVA to address the additional concerns with the DVR protection scheme at WBN.

Please address any questions regarding this submittal to Gordon Arent at (423) 365-2004.

I declare under penalty of perjury that the foregoing is true and correct. Executed on the 13th day of June 2014.

Respectfully,



J. W. Shea
Vice President, Nuclear Licensing

Enclosures
cc: See Page 2

ENCLOSURE 1

**TENNESSEE VALLEY AUTHORITY
RESPONSE TO REQUEST FOR ADDITIONAL INFORMATION FOR FSAR SECTION 8.3
ELECTRICAL OPEN ITEMS (TAC NO. ME2731)**

1.0 DESCRIPTION

This enclosure provides information related to degraded voltage protection at Watts Bar Nuclear Plant (WBN). The enclosure provides an overview of the licensing correspondence regarding degraded voltage as it applies to WBN Unit 2 licensing, findings, and remedial actions taken as a result of Nuclear Regulatory Commission (NRC) inspections of degraded voltage relays (DVRs).

2.0 BACKGROUND

TVA has performed calculations to evaluate and document the adequacy of the WBN auxiliary power system for two unit operation. Calculation WBN-EEB-EDQ000-999-2007-0002, "AC Auxiliary Power System Analysis," (Reference 1) verifies that adequate voltage is available for starting safety-related motors (individually) under degraded voltage conditions. Calculation WBN-EEB-MS-TI06-0029, "Degraded Voltage Analysis," (Reference 2) demonstrates that the WBN auxiliary power system complies with NRC Branch Technical Position PSB-1, establishes the basis for the degraded and loss of voltage relay setpoints and their associated time delays, ensures that the voltage level is adequate to allow required safety-related electrical equipment and devices to successfully complete their safety function, and ensures that the duration of the degraded voltage at a given voltage level does not result in thermal degradation or damage of the equipment. TVA Calculation EDQ00299920080003, "Class 1E MCC Control Circuit Voltage Analysis and Transformer Sizing," (Reference 3) and Calculation WBNEEBMSTI020020, "120V AC Class 1E Distribution Panel and Transformer Sizing and Voltage Drop Calculation," (Reference 4) evaluate the control circuits of the Class 1E loads to determine if the circuits will operate adequately, as intended under worst-case voltage drop conditions. In addition, TVA has performed STUDY-EEB-WBN-12-001, "Degraded Voltage Relay (DVR) Protection During Motor Starting," (Reference 5) to evaluate whether the existing DVR setpoint provides the minimum required voltages at the terminals of the Class 1E loads during motor starting (automatic start during a design basis event or individually) while still connected to the preferred offsite power source. A copy of STUDY-EEB-WBN-12-001, Revision 2 is provided in Enclosure 2.

In 2010, two independent but related events resulted in DVR settings at WBN requiring additional evaluation. First, NRC inspections (References 6 and 7) conducted at WBN identified conditions where the DVR setpoint value in the calculation of record was non-conservative with respect to the voltage specified in Technical Specifications (TS). Secondly, TVA submitted WBN Unit 2 Final Safety Analysis Report (FSAR) amendments addressing Section 8, "Electric Power."

On January 28, 2011, TVA received a non-cited violation (NCV) of low safety significance regarding the failure to use the DVR setpoint values specified in TS and configured in the 6.9 kV bus based on the electrical design calculation (Reference 6). The NRC concluded that the availability, reliability and operability of the 6.9 kV safety buses was impacted due to a non-conservative degraded voltage input being used in the safety related motor start and running calculations.

On January 31, 2011, the NRC issued NUREG-0847, Supplement 22, "Safety Evaluation Report, Related to the Operation of Watts Bar Nuclear Plant, Unit 2," Supplement 22, Appendix HH. Appendix HH contained Open Item 30, stating:

TVA should confirm that all safety-related equipment (in addition to the Class 1E motors) will have adequate starting and running voltage at the most limiting safety-related components (such as motor-operated valves (MOVs), contactors, solenoid valves or relays) at the DVR setpoint dropout setting. TVA should also confirm that (1) the motor starting transient studies are based on the dropout voltage value of DVR and time delay, (2) the steady-state voltage drop studies are carried out by maximizing running loads on the Class 1E distribution system (bounding combination of safety systems loads), with the voltage at 6.9 kV Class 1E buses (monitored by the DVRs) at or just above the DVR dropout setting, and (3) the DVR settings do not credit any equipment operation (such as LTC transformers) upstream of the 6.9-kV Class 1E buses. TVA should also confirm that the final technical specifications (TSs) are properly derived from these analytical values for the degraded voltage settings.

By letter dated August 12, 2011 (Reference 8), TVA provided a response to NUREG-0847, Supplement 22, Appendix HH, Open Item 30. In the enclosure to the letter, and in response to Open Item 30, TVA informed the NRC that it had performed a motor-starting transient study assuming the 6.9 kV Shutdown Boards were maintained at the DVR dropout setting and applied the worst-case accident block-start loading (bounding combination of safety system loads). Additionally, the response indicated that the analysis did not credit any non-Class 1E equipment upstream of the 6.9 kV Class 1E buses (such as automatic load tap changers (LTCs) or administratively controlled grid capacity). TVA confirmed that the Class 1E motors required to start and mitigate an accident would have adequate voltage.

On June 7, 2012, TVA submitted updated information related to the offsite and onsite power system degraded voltage studies for safety-related electrical equipment (Reference 9). In Reference 9, TVA submitted excerpts from the Reference 5 sensitivity study of motor starting relative to the existing DVR setpoint. The purpose of the study was to address issues concerning DVR protection at WBN as documented in 1) NRC NCV 05000390/2010005-003, "Failure to use Worst Case 6900 VAC Bus Voltage in design calculations," 2) NUREG-0847, Supplement 22, "Safety Evaluation Report Related to the Operation of Watts Bar Nuclear Plant, Unit 2," Appendix HH, Open Item 30, and 3) recent regulatory developments in the industry with respect to DVR protection and analysis including RIS 2011-12. The study was performed for both WBN Unit 1 and Unit 2.

Subsequently, on February 27, 2014, TVA received a request for additional information (RAI) via NRC Electronic Mail (Reference 10) related to certain aspects of the degraded voltage methodology used at WBN. Responses to these RAIs are provided in Section 3.0 of this enclosure.

On April 24, 2014, the NRC staff conducted a public meeting with members of TVA (Reference 11). The purpose of the meeting was to discuss the status of electrical open items resulting from the NRC review of the FSAR for WBN Unit 2 including the previous correspondence and the February 27, 2014 RAIs. The meeting allowed TVA to present the history of the regulatory guidance/industry events/actions implemented at WBN with regards to degraded voltage, highlights of the analysis performed by TVA on loss of voltage (LOV) and DVR settings, aspects of the TVA conformance with

Branch Technical Position PSB-1, and highlights of the TVA response to SSER Open Item 30.

3.0 RESPONSES TO REQUESTS FOR ADDITIONAL INFORMATION

By email dated February 27, 2014, the NRC forwarded a request for additional information. The NRC stated questions and TVA's responses are presented below.

NRC Request for Additional Information

The staff of the Electrical Engineering Branch (EEEB) of the Division of Engineering has previously requested information on open items associated with NUREG-0847, "Supplemental Safety Evaluation Report (SSER) Related to the Operation of Watts Bar Nuclear Plant, Unit 2." In order to complete the review and close these items, the staff requests additional information from the licensee, as described below:

BACKGROUND

In letter dated June 7, 2012, the Tennessee Valley Authority (TVA) provided a response to Open Item 30 (power system degraded voltage) with respect to SSER, Appendix HH.

The response states that the methodology used in the study was developed to meet the intent of Regulatory Issue Summary (RIS) 2011-12, "Adequacy of Station Electrical Distribution System Voltages".

The RIS states, "The licensee's voltage calculations should provide the basis for proper operation of the plant safety-related electrical distribution system, *when supplied from the offsite circuit(s) (from the transmission network)*. (*emphasis added*) These calculations should demonstrate that the voltage requirements (both starting and running voltages) of all plant safety-related systems and components are satisfied based on operation of the transmission system (including the bounding transmission system single contingency in terms of voltage drop) and the plant onsite electric power system during all operating configurations of transmission network and plant systems."

The TVA response states that to perform the analysis, the 6.9 kV shutdown boards were disconnected from all offsite power source(s) and a dedicated fixed voltage source was added to each 6.9 kV shutdown board (6.9 kV shutdown board was used as a swing bus). The source voltage was set to the degraded voltage relay (DVR) analytical dropout limit of 6555 V.

RAI QUESTION 1

Based on the above statements:

- a) Please explain how disconnecting the shutdown boards from offsite power source(s) meets the intent of guidance provided in the RIS section cited above.
- b) Please explain how the voltage drop through station services transformers (CSST A, B, C and D) is accounted for during block starting or sequential starting of emergency loads in the analyses provided.

- c) If the shutdown bus is considered a ‘dedicated fixed voltage source’ or a swing bus, then please confirm that the calculation process assumes the swing bus to be an infinite source of real and reactive power. If not, provide basis for the assumption used.
- d) From bus voltage perspective, discuss how this simulation depicts the dynamic response capabilities of the shutdown boards compared to the real and reactive power demand of motor starts postulated during accident conditions with offsite source(s) supplying power through CSST A, B, C and D including all worst-case operating and loading configurations.

TVA Response

During discussions between the NRC and TVA at the April 24, 2014 public meeting, the NRC accepted the study case information presented by TVA and clarified that a response to Question 1 was no longer required. Enclosure 2, Appendix H includes the study cases presented and discussed during the April 24, 2014 public meeting.

RAI QUESTION 2

The analyses states that for contactors, relays and solenoid valves, adequacy of pickup voltage was performed as part of the Control Circuit Voltage Drop (CCVD) analysis. This analysis was performed considering a steady state minimum voltage of 432V at the motor control center (MCC) bus. Please confirm that 432V is the minimum voltage required for operability of all equipment (minimum voltage required at component terminal) with nominal operating voltage of 480V and lower (230/120V) voltage systems supplied from the 480V system.

TVA Response

432 V at the 480V AC Shutdown Boards and MCCs, ensures that the safety-related equipment connected to the Class 1E system is capable of performing their intended function. TVA’s analysis of this is contained in Calculations EDQ00299920080003, “Class 1E MCC Control Circuit Voltage Analysis and Transformer Sizing,” (Reference 3) and WBNEEBMSTI020020, “120V AC Class 1E Distribution Panel and Transformer Sizing and Voltage Drop Calculation,” (Reference 4).

RAI QUESTION 3

The analyses states that the MCC transient bus voltage under degraded voltage conditions (at DVR dropout voltage of 6555V) drops below 432V due to starting of large motors on the 480V switchgear and recovers to a value of >432V within 4 seconds. Please confirm that the duration and magnitude of voltage drop and recovery during block starting of all safety related loads and sequenced start of loads remains within the acceptable range without actuating any protective devices (accident analyses perspective) if the 6.9kV busses remain connected to the 161kV offsite power source through the CSSTs.

TVA Response

The magnitude and duration of the < 4 second dip below 432V is acceptable for all equipment as discussed in TVA Calculation WBN-EEB-EDQ000-999-2007-0002, “AC Auxiliary Power

Systems Analysis," and does not actuate any protective device, as discussed in TVA Calculation WBN-EEB-MS-TI06-0029, "Degraded Voltage Analysis."

RAI QUESTION 4

Calculation Number WBN-EEB-EDQ000-999-2007-0002 1 submitted in response to preliminary request for additional information regarding Unit 2 licensing process states the following:

"One 161 kV transmission line and CSSTs A and D, or the other transmission line and CSSTs B and C, shall be capable of starting and running all required safety-related loads and powering all running BOP loads for a design basis accident in one unit and orderly shutdown of the other unit. The analysis for the Class 1 E power system shall evaluate all equipment that is started by a safety injection signal (SIS) as starting at the same time unless the load's control circuitry has sequential time delay, and that all continuous loads that could be operating as required by the process, whether safety-related or not, are running. The analyses in this calculation evaluate the starting of the equipment required to mitigate an accident in accordance with the above requirements for one Unit and simultaneous orderly shutdown of the other unit. The worst case bases for this evaluation is assuming a 161 kV grid pre-event voltage of 164kV and a subsequent 161 kV grid drop of 9kV at event initiation resulting in a post event 161kV grid voltage of 153kV. The analyses shows that all equipment required to start to mitigate an accident receive adequate starting voltage within the time period (5 seconds) of Reference 2.16 for the cases when both CSST C and D are available and also when only one CSST (either C or D) is available."

Enclosure 1 attached to TVA letter dated July 31, 2010, provided similar information (reference pages E1-63 and 64) regarding the capability of the electrical power system described in FSAR Section 8.1. Please clarify that the impact of the voltage drop in the 161kV system coupled with the voltage drop in CSSTs during block loading of accident loads is accounted for in the degraded voltage relay setpoint calculation performed in accordance with the recommendations of RIS 2011-12.

TVA Response

During discussions between the NRC and TVA at the April 24, 2014 public meeting, the NRC accepted the study case information presented by TVA and clarified that a response to Question 4 was no longer required. Enclosure 2, Appendix H includes the study cases presented and discussed during the April 24, 2014 public meeting.

RAI QUESTION 5

- 1) In response to NRC letter dated December 20, 2013, for resolving open phase condition (OPC) design vulnerability within electric system at Watts Bar 2, TVA stated that:

Vulnerability studies of the OPC faults have been completed for WBN and additional operator meetings are being scheduled to communicate the results. For the analyzed configurations, the vulnerability studies showed existing protection automatically actuates and provides protection to the Class-1E system for grounded open phase

conditions. Vulnerability to an ungrounded open phase condition has been identified for some analyzed configurations.

The TVA nuclear fleet has endorsed the generic schedule provided in the Industry OPC Initiative.

To resolve the OPC design vulnerability at Watts Bar 2, staff requests that TVA provide design features and analyses information in the Final Safety Analysis Report to automatically detect and alarm in the main control room for OPC with and without a high impedance ground condition including two open phase condition on the high voltage side of a transformer connecting a credited GDC-17 offsite power circuit to the transmission system. For OPC, automatic detection and actuation circuits will transfer loads required to mitigate postulated accidents to an alternate power source and ensure that safety functions are preserved, as required by the current licensing bases. The OPC should be sensitive enough to identify an open phase condition under all operating electrical system configurations and loading conditions for which they are required to be operable and should minimize misoperation, maloperation, and spurious actuation. In addition, the staff requests TVA to address the limiting conditions of operation and surveillance requirements that must be added to the plant Technical Specifications to meet the provisions of 10CFR50.36 (c) (2) and c(3).

The above information is required from TVA for staff to reach the necessary safety conclusion that the electrical power system for Watts Bar Unit 2 design meets the 10 CFR Part 50, Appendix A, GDC 17, 10 CFR 50.55a(h)(2), and 10 CFR 50.36 requirements with respect to addressing electric power system design vulnerability due to OPC which could affect the safety functions of both onsite and offsite power systems.

TVA Response

As requested by the NRC staff during discussions with TVA on June 4, 2014, the response to Question 5 is being provided in a separate transmittal.

4.0 Non-cited Violation (NCV) 05000390/2010005-003

On January 28, 2011, TVA received a NCV of low safety significance (green) regarding the failure to use the DVR setpoint values specified in TS and configured in the 6.9 kV bus based on the electrical design calculation (Reference 6). The NRC concluded that the availability, reliability and operability of the 6.9 kV safety buses was impacted due to a non-conservative degraded voltage input being used in the safety related motor start and running calculations.

TVA STUDY-EEB-WBN-12-001, "Sensitivity Study of Degraded Voltage Relay (DVR) Protection During Motor Starting," (Reference 5) evaluates whether the DVR setpoint provides the minimum required voltages at the terminals of the Class 1E loads during motor starting (automatic start during a design basis event or individually) while still connected to the preferred offsite power source. The study concludes that adequate starting voltage is available to each Class 1E load when the 6.9 kV Shutdown Boards are at the DVR dropout setpoint for the following cases: 1) during a design basis event (all Class 1E loads that are automatically actuated for a safety injection (SI) signal), and 2) when individually starting a motor (all Class 1E loads, even if not SI actuated). Therefore, the existing DVR setpoints are adequate.

A copy of the study is provided in Enclosure 2 to address issues concerning DVR protection at WBN as documented in NRC NCV 05000390/2010005-003.

References

1. TVA Calculation WBN-EEB-EDQ000-999-2007-0002, AC Auxiliary Power Systems Analysis, Revision 38, May 28, 2014
2. TVA Calculation WBN-EEB-MS-TI06-0029, Degraded Voltage Analysis, Revision 36, March 13, 2014
3. TVA Calculation EDQ00299920080003, "Class 1E MCC Control Circuit Voltage Analysis and Transformer Sizing," Revision 10, dated February 1, 2014
4. TVA Calculation WBNEEBMSTI020020, "120V AC Class 1E Distribution Panel and Transformer Sizing and Voltage Drop Calculation," Revision 15, dated August 3, 2011
5. TVA STUDY-EEB-WBN-12-001, Degraded Voltage Relay (DVR) Protection During Motor Starting, Revision 001
6. Letter from NRC to TVA, "Watts Bar Nuclear Plant - NRC Integrated Inspection Report 05000390/2010005," dated January 28, 2011
7. Letter from NRC to TVA, "Watts Bar Nuclear Plant - NRC Component Design Bases Inspection - Inspection Report 05000390/2010006," dated June 11, 2010 [ML101620543]
8. Letter from TVA to NRC, "Watts Bar Nuclear Plant (WBN) Unit 2 - Safety Evaluation Report Supplement 22 (SSER22) - Response to NRC Required Action Item," dated August 12, 2011 [ML11229A020]
9. Letter from TVA to NRC, "Watts Bar Nuclear Plant, Unit 2 - NUREG-0847 Supplemental Safety Evaluation Report (SSER) Related to the Operation of Watts Bar Nuclear Plant, Unit 2, Appendix HH Open Item 30 - Power System Degraded Voltage," dated June 7, 2012 [ML12160A350]
10. NRC Electronic Mail (email) from Siva Lingam to Gordon Arent, on Watts Bar 2 - Open Phase and Open Item 30 RAIs, dated February 27, 2014
11. Summary of April 24, 2014 Meeting with Tennessee Valley Authority Regarding Watts Bar Nuclear Plant, Unit 2, Open Item for Licensing, May 29, 2014 [ML14118A201]

ENCLOSURE 2

**STUDY-EEB-WBN-12-001,
DEGRADED VOTAGE RECOVERY ANALYSIS for DBE,
Revision 2**

NPG CALCULATION COVERSHEET / CTS UPDATE

Page 1

<u>REV 0 EDMS/RIMS NO.</u> T93120417020	<u>CTS TYPE:</u> Calculation	<u>EDMS TYPE:</u> CALCULATIONS (NUCLEAR)	<u>EDMS ACCESSION NO (N/A for REV. 0)</u>		
<u>Calc Title:</u> Sensitivity Study of Degraded Voltage Relay (DVR) Protection During Motor Starting					
<u>ORG</u> CALC ID	<u>PLANT</u> NUC	<u>BRANCH</u> WBN	<u>NUMBER</u> STUDY-EEB-WBN-12-001	<u>CUR REV</u> 001	<u>NEW REV</u> 002
<u>CTS UPDATE ONLY</u> <input type="checkbox"/> (Verifier and Approval Signatures Not Required)			<u>NO CTS CHANGES</u> <input checked="" type="checkbox"/> (For calc revision, CTS has been reviewed and no CTS changes required)		
<u>UNIT</u> (check one) 0 <input checked="" type="checkbox"/> , 1 <input type="checkbox"/> , 2 <input type="checkbox"/> , 3 <input type="checkbox"/>	<u>SYSTEMS</u> N/A		<u>UNIDS</u> N/A		
<u>DCN, EDC, N/A</u> See Revision Log	<u>APPLICABLE DESIGN DOCUMENT(S)</u> See References				<u>CLASSIFICATION</u> FO
<u>QUALITY RELATED?</u> Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	<u>SAFETY RELATED?</u> (If yes, QR = yes) Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	<u>UNVERIFIED ASSUMPTION</u> Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	<u>SPECIAL REQUIREMENTS AND/OR LIMITING CONDITIONS?</u> Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	<u>DESIGN OUTPUT ATTACHMENT?</u> Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	<u>SARTS and/or ISFSI SAR/CoC AFFECTED</u> Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>
<u>CALCULATION NUMBER REQUESTOR</u> Name: Anil Bangalore PHONE: 423 365 1610		<u>PREPARING DISCIPLINE</u> EEB	<u>VERIFICATION METHOD</u> DESIGN REVIEW	<u>NEW METHOD OF ANALYSIS</u> <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	
<u>PREPARER</u> (PRINT NAME AND SIGN) Daljeet Bhatia <i>Daljeet Bhatia</i>		<u>DATE</u> 5/29/14	<u>CHECKER</u> (PRINT NAME AND SIGN) Vinu Patel <i>Vinu Patel</i>		<u>DATE</u> 5/29/14
<u>VERIFIER</u> (PRINT NAME AND SIGN) N/A <i>ACB</i> <i>5/30/14</i>		<u>DATE</u>	<u>APPROVAL</u> (PRINT NAME AND SIGN) Ronald E Cox <i>Ronald E. Cox</i>		<u>DATE</u> 6/3/14
<u>STATEMENT OF PROBLEM/ABSTRACT</u> <i>Statement of problem</i> Issues were raised by the NRC concerning degraded voltage relay (DVR) protection which can be summarized as the need to determine if the DVR setpoint provides the minimum required voltages at the terminals of the Class 1E loads during motor starting (automatic starting during a DBE or individually) while still connected to the preferred offsite power source.					
<u>Abstract</u> This study is being performed as a sensitivity study to see the impact to the DVR setpoint and/or plant response if the current methodology is changed and determine if adequate starting voltage is available to each Class 1E load when the 6.9kV Shutdown Boards are at the DVR dropout setpoint (analytical limit) for the following cases:					
<ul style="list-style-type: none"> • During a design basis event (DBE): all Class 1E loads that are automatically actuated for a safety injection signal (SI-Phase A or SI-Phase B). • When individually starting a motor (single motor start): all Class 1E loads, even if not SI-actuated. 					
This study will also show that for a degraded voltage condition, overcurrent protective devices associated with Class 1E loads will not trip during SI-actuated motor starting and subsequent start on the emergency diesel generator. This analysis is performed for both Unit 1 and Unit 2.					
The study has a Compact Disk (CD) that contains Appendices C, D, E, F and G (ETAP output reports).					
<u>MICROFICHE/EFICHE</u> Yes <input type="checkbox"/> No <input checked="" type="checkbox"/> <u>FICHE NUMBER(S)</u>					

NPG CALCULATION COVERSHEET / CTS UPDATE

Page 1A

BOSS-REFERENCES (A-add, D-delete)

CTS ONLY UPDATES:

Following are required only when making keyword/cross reference CTS updates and page 1 of form NEDP-2-1 is not included:

PREPARER (PRINT NAME AND SIGN)	DATE	CHECKER (PRINT NAME AND SIGN)	DATE
PREPARER PHONE NO.	EDMS ACCESSION NO.		

NPG CALCULATION RECORD OF REVISION	
CALCULATION IDENTIFIER	STUDY-EEB-WBN-12-001
Title	Sensitivity Study of Degraded Voltage Relay (DVR) Protection During Motor Starting
Revision No.	DESCRIPTION OF REVISION
000	<p>Initial issue. This sensitivity study also completes one of the corrective actions (298321-005) in PER 298321.</p> <p>Total number of pages: 127 This calculation also contains a CD which stores the ETAP output files and is stored in the calculation library for reference.</p> <p>Special Requirements/Limiting Conditions: None Successor Calculations: None</p>
001	<p>Revised to incorporate comments from Licensing, revised section 7 to add analysis for Control Circuit Voltage Drop and added Introduction to Appendix A.</p> <p>Pages added: 13, Appendix A (page i, ii) Pages revised & replaced: 1, 2, 3, 5 thru 9, 11, Att. 4 (pages 10, 11), Att. 5 (pages 7, 8) Pages deleted: None</p> <p>Total number of pages: 130</p> <p>This study was prepared in accordance with procedure requirements, utilizing standard calculation format and forms. This study is a one-time sensitivity study to determine the impact, if any, to the plant if a new degraded voltage methodology is implemented.</p> <p>Special Requirements/Limiting Conditions: None Successor Calculations: None</p>

NPG CALCULATION RECORD OF REVISION	
CALCULATION IDENTIFIER	STUDY-EEB-WBN-12-001
Title	Sensitivity Study of Degraded Voltage Relay (DVR) Protection During Motor Starting
Revision No.	DESCRIPTION OF REVISION
002	<p>This revision involves the following:</p> <ul style="list-style-type: none"> • Rerun Dynamic and Static Motor Starting analysis with the revised database incorporating all modifications performed to support U2 completion and ongoing modifications to the operating Unit 1. • Perform additional degraded voltage analysis utilizing the offsite power as a swing source. This additional analysis is being performed in Appendix H.. <p>Pages added: 2A, 4A, App. H (5 pages), Att. 5 (pages 8A, 8B, 8C, 8D)</p> <p>Pages revised & replaced: 1, 1A, 3, 5, 6, 10, 13, App. A (pages 1 - 25), App. B (page 1), Att. 4 (pages 10, 11), Att. 5 (pages 7, 8)</p> <p>Pages deleted: Appendix A (pages 26-27)</p> <p>This calculation contains a CD which stores the revised ETAP Reports for Appendices C, D, E, F and G.</p> <p>Total number of pages for Calculation: $130 + 11 - 2 = 139$</p> <p>This study was prepared in accordance with procedure requirements, utilizing standard calculation format and forms. This study determines the impact, if any, to the plant if a new degraded voltage methodology is implemented.</p> <p>Special Requirements/Limiting Conditions: None Successor Calculations: None</p>

NPG CALCULATION TABLE OF CONTENTS

Calculation Identifier: STUDY-EEB-WBN-12-001	Revision: 002
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Document Identifier	323702, 323703
Document Type	FILE
Initiated Date	20140523
Key Items	ELECTRICAL CALCULATION
Equipment Name	ETAP
Reference	STUDY-EEB-WBN-12-001 R2
Description	Input Files for WBN CALC 12-001 R2
Added By User	dsbhatia
Property	BSL
Data Added	05/23/2014
Document Category	FILEKEEPER
Organization	NUCLEAR
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Resp Org	WBNP

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WBNDATA.OTI	05/19/2014 @ 1:42 PM	05/22/2014 @ 1:42 PM
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1.0 Purpose

The purpose of this study is to address the issues concerning degraded voltage relay (DVR) protection at WBN as documented in:

1. WBN NCV 05000390/2010005-003 "Failure to Use Worst Case 6900 VAC Bus Voltage in Design Calculations"
2. Watts Bar (WBN) Unit 2 NUREG-0847, Supplement 22, RAI Item 30
3. Recent regulatory developments in the industry with respect to DVR protection and analysis including NRC Regulatory Issue Summary (RIS) 2011-12, "Adequacy of Station Electrical Distribution System Voltages"
4. Additional NRC comments received in public meeting

These issues can be summarized as the need to determine if the DVR setpoint provides the minimum required voltages at the terminals of the Class 1E loads during motor starting (automatic starting during a design basis event or individually) while still connected to the preferred offsite power source.

Currently, the DVR analytical limit is determined by the Degraded Voltage Analysis calculation (Ref. 2.1), using methodology consistent with industry standard IEEE Std. 741-1997 and station licensing basis. The DVR setpoint methodology has not previously considered motor starting voltage as a basis of the relay setpoint. This study is being performed as a sensitivity study to see the impact to the setpoint and/or plant response if the current methodology is changed.

1.1 Scope

This study determines if adequate starting voltage is available to each Class 1E load when the 6.9kV Shutdown Boards are at the DVR dropout setpoint (analytical limit) for the following cases:

- During a design basis event (DBE): all Class 1E loads that are automatically actuated for a safety injection signal (SI-Phase A or SI-Phase B).
- When individually starting a motor (single motor start): all Class 1E loads, even if not SI-actuated.

This study will also show that for a degraded voltage condition¹, overcurrent protective devices associated with Class 1E loads will not trip during SI-actuated motor starting and subsequent start on the emergency diesel generator.

This analysis is performed for both Unit 1 and Unit 2.

2.0 References

- 2.1 Calculation WBNNEBMSTI060029, Revision 33 "Degraded Voltage Analysis"
- 2.2 Calculation EDQ00099920070002, R37, "AC Auxiliary Power System Analysis (dual unit operation)"
- 2.3 Calculation WBNNEBEDQ1999010001, R75, "AC Auxiliary Power System Analysis"
- 2.4 NRC Regulatory Issue Summary (RIS) 2011-12, Revision 1, "Adequacy of Station Electrical Distribution System Voltages"
- 2.5 Watts Bar (WBN) Unit 1 NCV 05000390/2010005-03, "Failure to Use Worst Case 6900 VAC Bus Voltage in Design Calculations"
- 2.6 Watts Bar (WBN) Unit 2 NUREG-0847, Supplement 22, "Safety Evaluation Report Related to the operation of Watts Bar Nuclear Plant, Unit 2", RAI Item 30
- 2.7 Calculation WBNNEBMSTI060010, R76, "Auxiliary Power System Analysis on 1E Buses" (Historical Reference)

¹ A degraded voltage condition is when the 6.9kV Shutdown Board voltage drops below the DVR setpoint, but not below the loss of voltage (LOV) setpoint, and does not recover.

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- 2.8 Calculation WBPE2119202001, R8, "6.9kV Shutdown Logic Boards Undervoltage Relays Requirements/Demonstrated Accuracy Calculation"
- 2.9 Limitorque Maintenance Update 92-2 (RIMS L33930113 803) - Extract from Design Guide DG-E2.4.6
- 2.10 TVA General Engineering Specification DS-E9.4.1, R1, Selection and Specifications of Motors
- 2.11 NEMA MG-1-1998, Motors and Generators
- 2.12 PER 298321
- 2.13 Calculation EDX-000-999-2004-0002, R3, TSS Grid Voltage Study of WBN's Offsite Power System

3.0 Bases/Assumptions

- 3.1 The DVR dropout analytical limit (6555V) as determined in the Degraded Voltage Analysis calculation (Ref. 2.1) will be used to determine the available starting voltage.
- 3.2 The ETAP model used to perform offsite power analysis for dual unit operation (Ref. 2.2) is used to perform the motor starting analysis.
- 3.3 All process controlled loads (random loads) are conservatively considered to start at zero seconds in a DBE.
- 3.4 The Phase A Start Sequence evaluates a Safety Injection Initiation without receipt of a Phase B Containment Isolation (High Containment Pressure). The Phase B Start Sequence evaluates a Safety Injection Initiation with receipt of a Phase B Containment Isolation.

The short term steady state loading at the 480V level is higher during a Phase A start sequence than during a Phase B and results in a lower voltage at the 480V busses. However, piping breaks associated with a Phase A Start Sequence are small and will result in ECCS equipment being removed from service within a short period after the event (less than an hour). This will result in a much lower overall long term loading for a Phase A event when compared to a Phase B.

This study uses short term Phase A loading for the single motor start analysis since it is the most conservative loading. If, however the starting voltage (480V) is not acceptable using the Phase A loading, then Phase B loading is used provided:

- The load is only required for a Phase B event, or
- The load is required to be manually started at a time that is at least 2 hours after the initiation of a Phase A event.

This assumption is conservative since the long term 480V loading for a Phase B event is higher than for a Phase A event.

- 3.5 The 89-10 MOVs for WBN utilize motor actuators which have 'hammer-blow' feature, which allows the motor to start turning prior to engaging the mechanical load of the operator (i.e. start unloaded). The actual motor current draw is typically 50% of the full locked-rotor current (Ref. 2.9). Initially all MOVs are evaluated using full locked-rotor current but if the available voltage does not meet the required voltage criteria, the available voltage is re-calculated taking credit for the 'hammer-blow' feature. These MOVs are identified in Appendix A.

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4.0 Methodology/Approach

The methodology used in this study was developed to meet the intent of Regulatory Issue Summary (RIS) 2011-12, "Adequacy of Station Electrical Distribution System Voltages". The RIS states the protective function of the DVR setpoint is to ensure adequate starting voltage to all Class 1E equipment for all operating and accident conditions. Additionally, the RIS states that the DVR setpoint must be based on the starting voltage requirement at the terminal of the most limiting component and must account for the effect of all components which could affect voltage, this includes offsite power circuits, the plant distribution system, as well as all Class 1E and non-Class 1E loads.

However, the RIS does not prescribe the specific methodology to be used for the motor starting analysis, and there is no industry consensus on how to best address DVR protection for motor starting scenarios.² In actuality, the ability to start motors cannot be determined by monitoring voltage alone. The ability to start motors can only be determined by power system capacity, which is the ability to maintain voltage while providing the required starting current. Therefore, the very premise of using a voltage relay to protect motor starting ability requires an assumption of the power source capacity, which seems to violate the stated purpose of the DVR protective function.

An analytical approach is used in this study to determine the acceptability of the voltage during any Class 1E motor starting scenario that bounds any value of upstream capacity. This approach is based on the fact that for any Class 1E motor starting event (single motor or group of motors), the voltage at the DVR monitored bus can only respond in one of three ways:

1. The voltage decreases to the DVR setpoint, or above (i.e. DVR does not actuate)
2. The voltage decreases below the DVR setpoint and does not recover (i.e. DVR actuates and transfers loads to the DGs after the specified time)
3. The voltage decreases below the DVR setpoint and does recover (i.e. DVR actuates but does not initiate transfer since voltage remains above the LOV setpoint and recovers above the DVR reset value prior to timeout)

Analyses are performed for each of these situations as follows:

1. A starting voltage analysis is performed using a technique known as the "independent source" method. The voltage at the DVR monitored bus (i.e. 6.9kV Shutdown Board) is set at the DVR setpoint (dropout analytical limit) using an independent fixed voltage source. Since the initial DVR bus voltage prior to the event can be ignored, this simple technique produces correct voltages for downstream loads immediately after the initiation of the event. The analysis is performed for DBE motor starting (SI-actuated loads) as well as individual motor starts.
2. A protective device analysis is performed using a technique known as the "start-start" method. Since this is truly a degraded voltage situation, there is no need for a starting voltage analysis. However, an analysis should be performed to demonstrate that the Class 1E loads will be successfully transferred to the DG and started prior to their protective devices tripping. This "start-start" analysis was previously performed in the Degraded Voltage Analysis calculation (reference 2.1) and the results are reprinted in this study.
3. For DBE motor starting events, a bounding analysis is performed to demonstrate that any possible voltage transient caused by DBE motor starting, including drop to the LOV setpoint, will also result in successful recovery above DVR reset within 5 seconds (without crediting automatic load tap changers). For individual motor starting events, this situation is bounded by the starting voltage analysis from item 1 since the analysis at DVR dropout is more conservative than analysis at the DVR reset value.

These analyses bound any possible voltage outcome at the DVR monitored bus when starting any Class 1E motor required for any scenario.

² IEEE Power & Energy Society, Nuclear Power Engineering Committee (NPEC), Working Group 4.7 (Protection of Class 1E Power Systems and Equipment) meeting minutes of January 24, 2012, San Antonio, TX.

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5.0 Design Input Data

- 5.1 For individual minimum motor starting voltage requirements, see Appendix A.
- 5.2 The degraded voltage relay setpoints are as follows (Ref. 2.1, 2.8 & Att. 2 of this study):

	<u>Dropout (V)</u>	<u>Reset (V)</u>
Nominal Setpoint	6600	6642
Allowable Value	6570	6672
Analytical Limit	6555	N/A
Operational Limit	N/A	6681

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6.0 Computations and Analysis

The motor starting analysis is performed using ETAP V7.0.0N and the existing ETAP model used to perform offsite power system analysis for two unit operation (Ref. 2.2).

6.1 Starting Voltage Analysis

The 6.9kV shutdown boards were disconnected from all offsite power source(s) and a dedicated fixed voltage source was added to each 6.9kV shutdown board. The source voltage was set to the DVR dropout setting of 6555V (Section 5.2).

Using the load configuration in the existing Unit 1& 2 ETAP model, the following analyses were performed:

- Dynamic Motor Starting – Safety Injection Signal Phase A (SIA)
- Dynamic Motor Starting – Safety Injection Signal Phase B (SIB)
- Static Motor Starting (starting individual motor): This analysis is performed with SIA since this provides the worst case voltages on the 480V system. For this analysis, motor starting study case is generated to individually start each Class 1E motor. Resolutions to loads requiring additional review are annotated in Appendix A. If the starting voltage using Phase A is not acceptable, analysis is performed using Phase B loading

DBE Motor Starting:

Each study case is run for a total simulation time of 15 seconds. Since it is considered that by this time all motors have been accelerated and the APS system has come to a steady state condition. ETAP reports provide terminal voltage and current for every motor which starts at 0+ second up to 15 seconds in steps of 0.1 second.

The output reports are saved as U1 sdbds at DVDO-Complete (Study Case U1-DV-SIBms, Config. DV-LOCA-U1), U2 sdbds at DVDO-Complete (Study Case U2SIB-DV(N), Config. DV-LOCA-U2) and U12 sdbds at DVDO-Complete (Study Case U1/2SIA, Config. Deg Volt SU) in folder J:\wbn\ETAP Reports - Dynamic Motor Analysis.

Single Motor Starting:

Each study case is run using 'Study Case ID U1/2SIA and Config. Deg Volt SU'.

The output reports, in pdf format, are saved in folders J:\wbn\ETAP Reports - Shutdown Boards 1A and 1B and J:\wbn\ETAP Reports Shutdown Boards 2A and 2B\New Reports. Due to the large number of output reports, the output report names are not listed.

These analyses did not credit any non-Class 1E equipment upstream of the 6.9-kV Class 1E buses (such as LTC transformers or administratively controlled grid capacity). The available starting voltage for each motor is then documented and compared to the required starting voltage.

6.2 Protective Device Analysis (Start-Start scenario):

The scenario evaluated for the short time delay is an SI concurrent with the degraded voltage condition such that a block start attempt is made. A determination is made of the time permitted to allow voltage to return above the degraded voltage relay setpoint reset limit under block start transient conditions and still assure a subsequent start on the diesel if the voltage fails to recover, thus, making this a start-start evaluation. To evaluate the effect of the starting currents during the start-start scenario, the effect on overcurrent protective devices are considered. The board voltages at the onset of the event are, considered normal (i.e. no preheat). The degraded voltage condition presumes that the voltage does not recover but remains below the degraded voltage relay setpoint subjecting the SI initiated motors to starting currents for the time delay selected and then sequence onto the emergency diesel generators. The design calculated worst-case transient voltage dip during the accident loading sequence is used. This is conservative, because a lower voltage would produce less starting current for the motors.

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The above evaluation is performed for the safety related loads required for Units 1 and 2 which would be actuated for an SI as follows:

- Motor loads fed from 6.9kV and 480V Switchgear & MCCs, MOVs & Static loads fed from the MCCs are evaluated to determine the effect of the start-start heating of the overcurrent protective devices (breakers/TOLs), such that starting on the diesel without tripping can be assured.
- Protective devices are also evaluated for the 6.6kV and 460V safety-related motors that operate during non-accident conditions. The evaluation considers that the safety bus voltage is equivalent to operation at the lower boundary of the degraded voltage relay dropout. The protective devices are evaluated to ensure that operation of the safety-related loads can be sustained indefinitely at this voltage without protective device trip.
- SI actuated medium voltage (6.6kV) motor loads are evaluated to ensure that their thermal damage limits are not exceeded during the start-start event.
- 120VAC control power transformer (CPT) fuse time characteristics are evaluated to determine if the fuse could blow when carrying rated inrush current of the starter and any other normally energized devices for the safety analysis time of 11.5 seconds (upper boundary of the degraded voltage relay time delay, Attachment 2) or 12 seconds in the start-start scenario.
- MCC 120VAC distribution panel fuse time characteristics are evaluated to determine if the fuses melt during the start attempts. It is considered that circuit components required to pick-up during starting will be at inrush conditions.

6.3 Voltage Recovery Analysis:

See Appendix B for voltage recovery analysis for DBE for detailed purpose, approach, bases and assumptions and computations.

In addition, Appendix H demonstrates the adequacy of the DVR protection scheme if the voltage source is placed at the switchyard bus and the grid voltage and capacity is set

1. Such that the DVR monitored bus voltage is at the DVR dropout analytical limit prior to DBE initiation
2. To support successful voltage recovery following DBE motor starting

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7.0 Summary of Results

7.1 Starting Voltage Analysis

See Appendix A for summary of the results. Based on a review of the results, all safety related loads have adequate starting voltage during DVR conditions and the existing setpoints for the degraded voltage relay are considered acceptable.

Note: ERCW Screen Wash Pumps are not assured to have adequate voltage as analyzed. However per N3-67-4002 this load is not required to be manually placed into service until 12 hours into a design basis event. This provides sufficient time to take corrective actions such as correcting the grid condition, adjusting the tap changers on the CSSTs or transferring the shutdown board(s) to the diesel generators.

Control Circuit Voltage Drop (CCVD) Analysis

With respect to the contactors, relays and solenoid valves, adequacy of pickup voltage for these control components (contactors, solenoid valves, relays) were performed as part of the Control Circuit Voltage Drop (CCVD) analysis. This analysis was performed considering a steady state minimum voltage of 432V at the MCC bus. All the components were determined to have adequate pickup voltage upon implementation of the issued design changes as identified in the CCVD calculation prior to Unit 2 fuel load.

The MCC transient bus voltage under degraded voltage conditions (at DVR dropout voltage of 6555V) drops below 432V due to starting of large motors on the 480V switchgear. This voltage, however, recovers to a value of >432V within 4 seconds. Since the startup of the safety related equipment may not have adequate starting voltage due to transient voltage conditions, Westinghouse evaluated the impact of additional 5 second delay for the startup of the safety injection pumps and feedwater isolation valves with offsite power available, and concluded the following: "This safety evaluation concludes that an additional five second delay for the startup of the safety injection pumps and an additional five second delay in the closure of the feedwater isolation valve does not impact the conclusions of the safety analysis that form the Watts Bar licensing basis (SECL-92-029; RIIMS No. T33930330990)".

Based on the above, the analysis performed to verify adequacy of available voltage for the contactors, solenoid valves, relays is considered to be adequate and, therefore, no further analysis under the transient voltage conditions has been performed.

7.2 Protective Device Analysis

Motors Actuated by SI Signal:

As discussed in Attachment 7, there is no adverse effect of the start-start heating on the overcurrent devices on the safety related motors which would be actuated by safety injection signal and powered from safety related 6.9kV and 480V switchgears and 480V MCCs while operating at the lower boundary of the degraded voltage relay setting (6555V).

Non-Accident Safety Related Motors:

Based on the analysis, operation of safety-related loads with the 6.9kV Shutdown Board voltage operating at the lower boundary of the degraded voltage relay 6555V, will not cause tripping of protective devices. Static loads (constant impedance) are not considered, since operation at lower voltage results in less current. Therefore, operation at the lower boundary of the degraded voltage relay dropout setting would not trip the motors.

TOL Evaluation:

The generic evaluation of TOL's, in Attachment 7, showed that only motors having locked rotor current in excess of 850% are required to be evaluated further. A review of the WBN ETAP database, showed that four motors have a locked rotor current greater than 850% and start for an accident. An evaluation of those four loads shows that their TOL's are set at 115%. Therefore they would not be an issue, because it would increase their tolerance for tripping by an additional 15%.

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Fuse Evaluation for MCCs 120VAC CPT Circuits and 120VAC Distribution Panel Loads:

Based on the evaluation in Attachment 7, fuses for all the 120V AC CPT Circuits and 120V AC Distribution Panel Loads are considered acceptable, the fuses will carry inrush current and will not blow or melt for at least 12 seconds during a start-start scenario.

The upper boundary limit for the time delay is 11.5 seconds, which is the maximum total time allowed for loss of voltage detection and emergency diesel generator start in the WBN safety analysis as documented in the FSAR. Based on the evaluation performed in Attachment 7, it has been determined that protective devices will not trip prior to 12 seconds for start-start operation of motors at a degraded voltage at which time period disconnection from offsite power and reconnection to the emergency diesel generators occurs.

7.3 Voltage Recovery Analysis

The voltage recovery analysis shows that in all cases the voltage on the 6.9kV shutdown boards 1A, 1B, 2A and 2B recovers above the DVR reset value (operational limit of 6681V) within 4 seconds.

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8.0 Conclusions

- 8.1 This study determines that adequate starting voltage is available to each Class 1E load when the 6.9kV Shutdown Boards are at the DVR dropout setpoint (analytical limit) for the following cases:
 - During a design basis event (DBE): all Class 1E loads that are automatically actuated for a safety injection signal (SI-Phase A or SI-Phase B).
 - When individually starting a motor (single motor start): all Class 1E loads, even if not SI-actuated.
- 8.2 This study shows that for a degraded voltage condition, overcurrent protective devices associated with Class 1E loads will not trip during SI-actuated motor starting and subsequent start on the emergency diesel generator.
- 8.3 The bounding voltage recovery analysis in Appendix B demonstrates that any possible voltage transient caused by DBE motor starting, including drop to the LOV setpoint, will also result in successful recovery above DVR reset within 4 seconds.
- 8.4 The outcome of the analysis in Appendix H demonstrates the adequacy of the DVR protection scheme.

Therefore, using motor starting voltage as a basis for the relay setpoint shows no impact to the DVR setpoint and/or the plant response.

Appendix A

Introduction

This appendix is a summary tabulation of the results for the various motor starting scenarios described in Section 6.0. The analyses in Appendix A were developed using the methodology and applicable inputs from References 2.2, and 2.3. Voltage values were obtained from the applicable ETAP files and output reports in this study. The key information and results are determined as follows:

A. Minimum Motor Starting Voltage

Minimum motor starting voltages are based on Attachments 1, 3 and 6 of this study. The minimum motor starting voltages used are:

6600 Volt Motors - 5280 Volts (80%)***

460 Volt Motors - 391 Volts (85%)**

460 Volt Air Compressors - 368 Volts (80%)**

89-10 MOVs - Valve thrust and torque design margin calculations/evaluations based on motor terminal voltage as documented in Attachments 4 and 5 of this study.

Non 89-10 MOVs - 368 Volts (80%)**

** Percentages are based on 460 Volt rated motor voltage. For motors rated other than 480V, the same percentages are applicable. The minimum starting voltage may be different from the above voltage if it is based on manufacturer's data or test report as documented in Attachments 3 and 6 of this study.

*** 80% for all motors except for the ERCW Pump motor which requires 90% and the Auxiliary Feedwater Pump motor which requires 85%

B. Motor Starting Evaluation Results

Individual motor starting evaluation results are tabulated for all class 1E safety-related motors and motor operated valves. As summarized in Section 6.1 of this study the following steps were performed:

1. Motor terminal voltage with Phase A loading is compared against the minimum motor starting requirements above. If acceptable voltage is obtained, no further action is required.
2. Motor terminal voltage with Phase B loading is compared against the minimum motor starting requirements above. If acceptable voltage is obtained, no further action is required.
3. Single motor start terminal voltage with Phase A loading or with Phase B loading provided the Phase B criteria in section 3.4 of this study applies is compared against the minimum motor starting requirements above. If acceptable voltage is obtained, no further action is required.

4. Individual circuit operating evaluations are performed based on when the motor is in service such as the ERCW Screen Wash Pump.
5. For 89-10 MOVs, See Section C below.

C. 89-10 Motor Operated Valve Evaluation Results

For Unit 1 and Unit 2 89-10 MOVs that did not meet the required valve motor starting voltage criteria, as a first step the calculated starting voltages for these MOVs were provided to Mechanical discipline (valve group) to evaluate if the revised voltages were acceptable. Based on the new thrust and torque calculations and calculated new design margins by mechanical valve group, the new available starting voltage for some MOVs was determined to be acceptable. However, some of the MOVs still did not meet either the required voltage or the minimum design margin criteria. Available voltage for these MOVs were re-evaluated further using the hammer-blow (HB) feature (see Section 3.5) which resulted in improved starting voltage available at the motor terminals. The available voltage with HB feature was again evaluated by the mechanical valve group and determined to be acceptable.

Appendix A

1A Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
		SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%)	
ETAP Bus ID/ Compt No	Load Description	6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV/460V Base	Reference
6.9KV Shutdown Board 1A-A								
12-10 AFW	Aux Feedwater PMP 1A-A 1-MTR-3-118-A (600 HP)	99.09	Starts	99.09	Starts	99.07	85	Att. 3
12-13 CSP	CNTMT SPRAY PMP 1A-A 1-MTR-72-27-A (700 HP)	N/A	Not Running	98.80	Starts	98.79	80	Att. 3
12-14 RHR	RHR PUMP 1A-A 1-MTR-74-10-A (400 HP)	98.97	Starts	98.97	Starts	98.97	80	Att. 3
12-15 SI	SAFETY INJ PMP 1A-A 1-MTR-63-10-A (400 HP)	98.94	Starts	98.94	Starts	98.94	80	Att. 3
12-18 CCP	CNTFGL CHRG PMP 1A-A 1-MTR-62-108-A (600 HP)	98.87	Starts	98.87	Starts	98.87	80	Att. 3
12-8 ERCW	ERCW PMP A-A 0-MTR-67-28-A (800 HP)	N/A	Starts (A-A or B-A start, but not both, other is not running)	N/A	Starts (A-A or B-A start, but not both, other is not running)	96.46	90	Att. 3
12-9 ERCW	ERCW PMP B-A 0-MTR-67-32-A (800 HP)	93.26	Starts (A-A or B-A start, but not both, other is not running)	93.26	Starts (A-A or B-A start, but not both, other is not running)	93.12	90	Same as ERCW Pmp A-A (Att. 3)
480V Shutdown Board 1A1-A								
125-3B	Comp Cooling Sys Pump 1A-A 1-MTR-70-46-A (350hp)	83.52 (8s)	Starts	84.13 (8s)	Starts	83.56	70	Att. 3
126-10C	Containment Air Rtn Fan 1A-A 1-MTR-30-38-A (100hp)	N/A	Not Running Starts @ 9 Min	N/A	Not Running Starts @ 9 Min	80.97 (SIB)	80	Att. 6
126-7C	Reac Lwr Compt Clr Fan 1A-A 1-MTR-30-74-A (60hp)	N/A	Running	N/A	Trips	81.73	80	Att. 3
126-9C	Elec Bd Rm AHU A-A 0-MTR-31-30B-A (50hp)	N/A	Running	N/A	Running	83.82	80	Att. 6
126-7A	Spent Fuel Pit Pump C-S 0-MTR-78-35-S (100hp)	N/A	Running	N/A	Running	80.77	80	Att. 6
480V Shutdown Board 1A2-A								
127-2C	Control Rm A/C A-A Compressor 0-MTR-31-80-2/A (250hp)	N/A	Running	N/A	Running	90.08	80	Att. 1
127-3B	Comp Cooling Sys Pump C-S 0-MTR-70-51-S (350hp)	81.61 (8s)	Starts	82.07 (8s)	Starts	80.61	70	Att. 3
128-7D	Reac Lwr Compt Clr Fan 1C-A 1-MTR-30-77-A (60hp)	N/A	Running	N/A	Trips	81.25	80	Att. 3
128-9D	480V SD Bd Rtn AHU A-A 0-MTR-31-45-A (75hp)	N/A	Running	N/A	Running	87.36	85	Att. 1
480V C&A Vent Board 1A1-A								
203-12B	Cont Bldg Emerg Press Fan A-A 0-MTR-31-6-A (1hp)	85.89	Starts	87.23	Starts	87.60	85	Att. 1
203-13D	ERCW Scrn Wash Pump 1A-A 1-MTR-67-431-A (40hp)	N/A	N/A	N/A	N/A	73.63	75	Att. 3 See Sec. 7.1 for Justification

Appendix A

1A Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No		SI Phase A DBE Actuation	Terminal Voltage (%)	SI Phase B DBE Actuation	Terminal Voltage (%)	Individual Motor Start	Minimum Required Voltage	
		6.6kV / 460V Base		6.6kV / 460V Base		Terminal Voltage (%)	Terminal Voltage V(%)	
		SI Phase A	SI Phase B	SI Phase B	6.6kV / 460V Base	Base	Bases for Minimum Required Voltage	
203-2A	Cont Bldg Emerg Air CU Fan A-A 0-MTR-31-8-A (10hp)	86.39	Starts	87.73	Starts	89.23	85	Att. 1
203-3C	Cntrmt Spray Pump 1A-A Clr Fan 1-MTR-30-177-A (7.5hp)	N/A	Running	81.87	Starts	83.18	80	Att. 3
203-4D	Emerg Gas Trtmt Sys Fan A-A 0-MTR-65-23-A (20hp)	87.24	Starts	88.59	Starts	90.95	75	Att. 3
203-6B	ERCW Str 1A-A 1-MTR-67-9-A (3hp)	N/A	Running	N/A	Running	76.43	75	Att. 3
203-10A	Cntfg Chrg Pmp 1A-A Rm Clr Fan, 1-MTR-30-183-A, (5 HP)	84.47	Starts	85.79	Starts	86.76	80	Att. 3
203-10B	PEN RM EL 713 CLR FAN 1A-A, 1-MTR-30-196-A, (3HP)	86.68	Starts	88.03	Starts	90.30	80	Att. 3
203-10C	Pipe Chase Clr Fan 1A-A, 1-MTR-30-201-A, (3 HP)	85.43	Starts	86.76	Starts	88.55	80	Att. 3
203-11A	480V Bd RM 1B PR SUP FAN 1B1-A 1-MTR-31-478-A, (3HP)	N/A	N/A	N/A	N/A	92.18	85	Att. 1
203-11C	480V Bd Rm 1A A/C Ahu 1A-A 1-MTR-31-461-A (15 HP)	N/A	N/A	N/A	N/A	90.06	85	Att. 1
203-11D	Cont Rm Ahu A-A 0-MTR-31-12-A (60 HP)	N/A	N/A	N/A	N/A	88.19	85	Att. 1
203-12A	125V Vtl Bat Rm II ExhFan 1B1-A 1-MTR-31-285-A (0.33 HP)	N/A	N/A	N/A	N/A	91.18	85	Att. 1
203-12C	480V Bd Rm 1A A/C Cond 1A-A 1-MTR-31-290-A, (15 HP)	N/A	N/A	N/A	N/A	90.76	85	Att. 1
203-12F1	Cntrmt Purge Air Radn Exh Mon 1-RE-90-130-A, (0.75 HP)	N/A	N/A	N/A	N/A	92.73	85	Att. 1
203-2C	PEN RM EL 692 CLR FAN 1A-A 1-MTR-30-186-A, (3HP)	86.13	Starts	87.47	Starts	90.42	80	Att. 3
203-4A	Btry Rm El 692 Exh Fan A-A 0-MTR-31-28-A (1.5HP)	N/A	N/A	N/A	N/A	88.45	85	Att. 1
203-4B	5TH VITL BATT.RM.EX. FAN 1B1-A 0-MTR-31-493B-A (0.25 HP)	N/A	N/A	N/A	N/A	94.40	85	Att. 1
203-5A	SFP Pmp A-A&TB Bst Prm SpClrFan 0-MTR-30-192-A (7.5HP)	86.00	Starts	87.34	Starts	89.67	80	Att. 3
203-5E	CCS & AFW PMPS SP CLR FAN A-A 1-MTR-30-190-A (20HP)	87.31	Starts	88.66	Starts	90.70	80	Att. 3
203-6A	Shutdown Bd Rm I Press Fan A-A 0-MTR-31-64-A (3HP)	N/A	N/A	N/A	N/A	92.71	85	Att. 1
203-6C	Traveling Scrn 1A-A 1-MTR-67-434-A (5HP)	N/A	N/A	N/A	N/A	80.36	80	Att. 3
203-6F1	Cntrmt Bldg Lvr Compt Air Mon 1-RE-90-106-A (3HP)	N/A	N/A	N/A	N/A	92.68	85	Att. 1
203-7B	125V Vtl Bat Rm I ExhFan 1A1-A 1-MTR-31-287-A (0.33HP)	N/A	N/A	N/A	N/A	91.40	85	Att. 1
203-8A	Safety Inj Pmp 1A-A Rm Clr Fan 1-MTR-30-180-A (5HP)	83.34	Starts	84.63	Starts	85.19	80	Att. 3
203-8B	Pen Rm El 737 Clr Fan 1A-A 1-MTR-30-194-A (3HP)	88.04	Starts	89.41	Starts	92.28	80	Att. 3
203-8C	480V Xfrm Rm 1A Exh Fan 1A2-A 1-MTR-30-244G-A (3HP)	N/A	N/A	N/A	N/A	89.57	80	Att. 3

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1A Boards

EVALUATION OF CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No		SI Phase A DBE Actuation	Terminal Voltage (%)	SI Phase B DBE Actuation	Terminal Voltage (%)	Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		6.6kV / 460V Base		6.6kV / 460V Base		Terminal Voltage (%)	Terminal Voltage V(%)	
		SI Phase A	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base	6.6kV / 460V Base	6.6kV / 460V Base	Reference
203-8D	480V Xfmr Rm 1A Exh Fan 1A3-A 1-MTR-30-244H-A (3HP)	N/A	N/A	N/A	N/A	91.34	80	Att. 3
203-8F1	CONT RM A/C A-A CONTROL/O.PMP 0-MTR-31-80/3-A (3.11 HP)	N/A	N/A	N/A	N/A	92.86	85	Att. 1
203-9A	RHR Pmp 1A-A Rm Clr Fan 1-MTR-30-175-A (5HP)	82.51	Starts	83.79	Starts	84.25	80	Att. 3
203-9B	Cont Rm A/C Circ Pmp A-A 0-MTR-31-80/1-A (15HP)	N/A	N/A	N/A	N/A	89.07	85	Att. 1
203-9C	480V Bd Rm 1A Pr Sup Fan 1A1-A 1-MTR-31-462-A (3HP)	N/A	N/A	N/A	N/A	92.92	85	Att. 1
203-9D	480V Xfmr Rm 1A Exh Fan 1A1-A 1-MTR-30-244F-A (3HP)	N/A	N/A	N/A	N/A	89.49	80	Att. 3
203-9F1	Cont Rm Intake Mon 0-RE-90-205-A (0.75HP)	N/A	N/A	N/A	N/A	93.17	85	Att. 1
203-4E	ERCW Str 1A-A Backwash Vlv 1-FCV-67-9A-A (0.33HP)	N/A	N/A	N/A	N/A	82.02	80	Att. 1
203-6E	ERCW Str 1A-A Flush Vlv 1-FCV-67-9B-A (0.33HP)	N/A	N/A	N/A	N/A	82.70	80	Att. 1
203-7D	RHR PMP 1A-A INLET FCV 1-FCV-74-3-A (5.2HP)	N/A	N/A	N/A	N/A	91.31	Pass	Att. 4 / Acceptable Margin
203-7E	RWST TO SPRAY HDR 1A FCV 1-FCV-72-22-A (3.2HP)	N/A	N/A	N/A	N/A	86.27	Pass	Att. 4 / Acceptable Margin
480V C&A Vent Board 1A2-A								
None								
480V Diesel Aux Board 1A1-A								
217-2B	DG 1A-A Rm Exh Fan 1-A 1-MTR-30-447-A (15hp)	91.83	Starts	92.48	Starts	92.64	85	Att. 1
217-3D	DG 1A-A Day Tk FO XFR PMP 1 1-MTR-18-55/1-A (1hp)	91.77	Random	92.43	Random	94.74	85	Att. 1
217-4B	DG 1A-A AUX LUBEOL CIRC PMP A 1-MTR-82-AOPA1A (0.75hp)	92.10	Random	92.75	Random	94.57	85	Att. 1
217-4D	Dg Rm 1A-A Pnl Vent Fan 1-MTR-30-491-A (15HP)	N/A	N/A	N/A	N/A	92.14	85	Att. 1
217-4E	Dg 1A-A 480V Elec Bd Rm Ex Fan 1-MTR-30-459-A (2HP)	91.95	N/A	92.60	N/A	94.29	85	Att. 1
217-3A	EM DG HX 1A1 & 1A2 SPLV VLV 1-FCV-67-66-A (0.13HP)	82.50	N/A	83.08	N/A	85.85	Pass	Att. 5
217-6A	DG 1A-A Muffler Rm Exh Fan 1-MTR-30-463 (0.5hp)	91.88	Starts	92.54	Running	95.01	85	Att. 1
480V Diesel Aux Board 1A2-A								
218-2B	DG 1A-A Rm Exh Fan 2-A 1-MTR-30-451-A (15hp)	92.40	Starts	92.86	Running/ Starts	92.94	85	Att. 1
218-3D	DG 1A-A DAY TNK FO XFR PMP 2 1-MTR-18-54/1-A (1hp)	91.63	Random	92.08	Random	93.94	85	Att. 1
218-2A	DG 1A-A AUX LUBEOL CIRC PMP B 1-MTR-82-AOPB1A (0.75HP)	N/A	N/A	N/A	N/A	93.76	85	Att. 1
218-2D	Dg 1A-A Lube Oil Crc Pmp 2 1-MTR-82-A2-A (1HP)	N/A	N/A	N/A	N/A	93.46	85	Att. 1
218-5F1	Dg Bldg Co2 Refrigeration Unit 0-PKG-39-37 (2HP)	N/A	N/A	N/A	N/A	94.53	85	Att. 1

1A Boards

EVALUATION OF CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)							
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage							
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts							
ETAP Bus ID/ Compt No		SI Phase A DBE Actuation	Terminal Voltage (%)	SI Phase B DBE Actuation	Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage (%)	Terminal Voltage V(%)	
		6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	Reference
480V RMOV Board 1A1-A							
235-5C	Lower CNTMT 1B CLRS ISLN VLv 1-FCV-67-97-A (0.13hp)	N/A	Not Running	81.71	Starts	85.11	Pass
235-7A	Seal Flow Ret Isln Vlv 1-FCV-62-63-A (1.9hp)	78.93	Closes on Ph A (Starts)	80.15	Closes on Ph B (Starts)	83.38	Pass
235-7B	CHARGING FLOW ISLN VLV 1-FCV-62-90-A (1.9hp)	85.86	Closes on SI (Starts)	87.20	Closes on SI (Starts)	90.69	Pass
235-8B	Vol Cont Tank Outlet Isln Vlv 1-LCV-62-132-A (1.9hp)	80.54	Closes on SI (Starts)	81.79	Closes on SI (Starts)	85.08	Pass
235-9A	RWST To Charging Pmp Vlv Cont 1-LCV-62-135-A (1.9hp)	83.79	Opens on SI (Starts)	85.09	Opens on SI (Starts)	88.51	Pass
235-9D	RCP Oil Lir Cntrml Iso Vlv 1-FCV-70-100 (0.13hp)	N/A	Not Running	81.60	Closes (Starts)	84.97	Pass
235-11A	SIS Pmp Inlet to CVCS Chrg Pmp 1-FCV-63-7 (1.9hp)	N/A	Not Running	N/A	Not Running	88.21*	Pass
235-11D	SIS Boron Inj Tank Shutoff Vlv 1-FCV-63-26 (1.9hp)	86.95	Opens on SI (Starts)	88.30	Opens on SI (Starts)	91.83	Pass
235-12B	Cntrmt Sump To RHR Pmp A-A 1-FCV-63-72-A (13hp)	N/A	Operate about 20 minutes after SI	N/A	Operate about 20 minutes after SI	86.95	Pass
235-13E	Cntrmt Spray Hdr 1A Isln Vlv 1-FCV-72-39-A (3.2hp)	N/A	Not Running	89.45 (5s)	Opens on Ph B (Starts)	91.80*	Pass
235-14D	RHR Pmp 1A-A Min Flow Vlv 1-FCV-74-12-A (0.13hp)	80.60	Random	81.86	Random	85.24	Pass
235-15D	LWR CNTMT 1D CLRS ISLN VLV 1-FCV-67-89-A (0.13hp)	N/A	Not Running	81.83	Closes (Starts)	85.21	Pass
235-17B	Cntrmt Standpipe Isln Vlv 1-FCV-26-240-A (0.67hp)	82.41	Close (Start)	83.69	Close (Start)	87.08	Pass
235-18E	RCP Spray Isln Vlv 1-FCV-26-243-A (0.67hp)	83.68	Close (Start)	84.98	Close (Start)	88.42	Pass
235-2E1	RWST To RHR Pmp Flow Cont Vlv 1-FCV-63-1-A (5.2HP)	N/A	N/A	N/A	N/A	92.09*	Pass
235-5B	RHR Sys Isln Vlv 1-FCV-74-1-A (2.6HP)	N/A	N/A	N/A	N/A	90.74*	Pass
235-6D	RCS Press Relief FCV 1-FCV-68-333-A (1.9HP)	N/A	N/A	N/A	N/A	89.2*	Pass
235-10B	SIS Pmp Recirc To RWST 1-FCV-63-3-A (0.7HP)	N/A	N/A	N/A	N/A	90.70*	Pass

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Appendix A
1A Boards

EVALUATION OF CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No		SI Phase A DBE Actuation Terminal Voltage (%)	SI Phase B DBE Actuation Terminal Voltage (%)	Individual Motor Start Terminal Voltage (%)	Minimum Required Voltage Terminal Voltage V(%)	Bases for Minimum Required Voltage	Base	Reference
235-10F	Cont Spray Pmp 1A-A Recirc FCV 1-FCV-72-34-A (0.13HP)	N/A	N/A	N/A	89.39*	Pass		Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
235-11B	RHR Hx A To CVCS Chrgr Pmp 1-FCV-63-8-A (1.9HP)	N/A	N/A	N/A	87.56	Pass		Att. 4 / Acceptable Margin
235-12A	SIS Pmp 1A-A Inlet Vlv 1-FCV-63-47-A (1.9HP)	N/A	N/A	N/A	88.18*	Pass		Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
235-12D	SIS To RCS Loops 2&3 FCV 1-FCV-63-93-A (1.6 HP)	N/A	N/A	N/A	90.73	Pass		Att. 4 / Acceptable Margin
235-12E	SIS Pmp 1A-A Outlet FCV 1-FCV-63-152-A (1.9HP)	N/A	N/A	N/A	88.48*	Pass		Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
235-13A	SIS Pmp Out RCS Lp 1&3 Hot Leg 1-FCV-63-156-A (1.9HP)	N/A	N/A	N/A	89.28*	Pass		Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
235-13B	Cntrmt Sump To Spray Hdr 1A FCV 1-FCV-72-44-A (3.2HP)	N/A	N/A	N/A	90.33*	Pass		Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
235-14A	RHR Spray Hdr 1A Isn Vlv 1-FCV-72-40-A (1.9HP)	N/A	N/A	N/A	87.74	Pass		Att. 4 / Acceptable Margin
235-14E	RHR Hx 1A Bypass Vlv 1-FCV-74-33-A (2HP)	N/A	N/A	N/A	85.35	Pass		Att. 4 / Acceptable Margin
235-4E	AFW Pmp A-A Lube Oil Pmp A-A 1-MTR-3-118D-A (0.25HP)	N/A	Manual	N/A	89.80	85		Att. 1
480V RMOV Board 1A2-A								
236-17E	480V Bd Rm 1A A/C Compressor 1A-1 1-MTR-31-465-A (50hp)	N/A	Running	N/A	91.94	85		Att. 1
236-2A	ERCW Hdr A Isn Vlv 1-FCV-3-116 (0.25hp)	N/A	Random	N/A	84.14	Pass		Att. 4
236-3A	ERCW Hdr A Isn Vlv 1-FCV-3-136 (0.33hp)	N/A	Random	N/A	84.72	Pass		Att. 4
236-3D	St Gen No 1 FW Isn Vlv 1-FCV-3-33-A (39.4hp)	81.97	Use 89-10 starts	82.77	Use 89-10 starts	82.79	Pass	Att. 4
236-4D	St Gen No 3 FW Isn Vlv 1-FCV-3-87 (39.4hp)	79.85	Use 89-10 starts	80.63	Use 89-10 starts	80.80	Pass	Att. 4
236-7D	Lwr Cntrmt Clr 1A Disch Iso Vlv 1-FCV-67-87-A (0.13hp)	N/A	Not Running	84.74	Closes (Starts)	86.85	Pass	Att. 4
236-7F	Upr Cntrmt Vt Clr 1A Sup Iso Vlv 1-FCV-67-130-A (0.13hp)	N/A	Not Running	82.36	Closes (Starts)	84.42	Pass	Att. 1
236-8B	Lwr Cntrmt 1A Clr Sply Isn Vlv 1-FCV-67-107-A (0.33hp)	N/A	Not Running	85.38	Closes (Starts)	87.49	Pass	Att. 4

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Appendix A

1A Boards

EVALUATION OF CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)							
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage							
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts							
ETAP Bus ID/ Compt No		SI Phase A DBE Actuation	SI Phase B DBE Actuation	Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage	Reference
		Terminal Voltage (%)					
		6.6kV / 460V Base	6.6kV / 460V Base				
236-8D	Lwr Cntrmt 1C Clr Disch Iso Vlv 1-FCV-67-95-A (0.13hp)	N/A	Not Running	84.49	Closes (Starts)	86.59	Pass
236-8F	Upr Cntrm Vt Clr 1C Sup Iso Vlv 1-FCV-67-133-A (0.13hp)	N/A	Not Running	81.29	Closes (Starts)	83.32	Pass
236-9A	Lwr Cntrmt 1C Clr Sply Isln Vlv 1-FCV-67-99-A (0.33hp)	N/A	Not Running	85.07	Closes (Starts)	87.17	Pass
236-9B	Lwr CNTMT 1B CLR DISCH ISO VLV 1-FCV-67-104-A (0.33hp)	N/A	Not Running	85.41	Closes (Starts)	87.53	Pass
236-9D	Up Cntrmt VT Clr 1A Disc Iso Vlv 1-FCV-67-295 (0.13hp)	N/A	Not Running	79.88	Closes (Starts)	81.87	Pass
236-9F	Upr Cntrm Vt Clr 1B Sup Iso Vlv 1-FCV-67-139-A (0.13hp)	N/A	Not Running	81.29	Closes (Starts)	83.32	Pass
236-10A	Lwr Cntrmt 1D Clr Disch Iso Vlv 1-FCV-67-112-A (0.33hp)	N/A	Not Running	85.46	Closes (Starts)	87.58	Pass
236-10D	UP CNTM VT CLR 1C DISH ISO VLV 1-FCV-67-296-A (0.13hp)	N/A	Not Running	81.33	Closes (Starts)	83.36	Pass
236-10F	UP CNTM VT CLR 1D DISH ISO VLV 1-FCV-67-142-A (0.13hp)	N/A	Not Running	82.36	Closes (Starts)	84.42	Pass
236-11D	RCP Thrm Barr Rtn Cntrmt Iso Vlv 1-FCV-70-90-A (0.7hp)	N/A	Not Running	86.05	Closes (Starts)	88.16	Pass
236-11E	RCP Thrm Barr Cntrmt Isln Vlv 1-FCV-70-133-A (0.13hp)	N/A	Not Running	83.85	Closes (Starts)	85.94	Pass
236-12D	RCP Oil Clr Rtn Cntrmt Isln Vlv 1-FCV-70-92-A (0.13hp)	N/A	Not Running	85.13	Closes (Starts)	87.25	Pass
236-16D	Excs Ldtn Hx Cont Init Iso Vlv 1-FCV-70-143-A (0.33hp)	83.86	Closes on Phase A	84.68	Closes on Phase A	86.78	Pass
236-2B	ERCW Hdr A Isln Vlv 1-FCV-3-116B-A (0.25HP)	N/A	N/A	N/A	N/A	84.13	Pass
236-2D	AFWP Turb Stm Sup Fm Stm Gen 1 1-FCV-1-15-A (1HP)	N/A	N/A	N/A	N/A	92.47*	Pass
236-2E	St Flow To AFWP Turb Isln Vlv 1-FCV-1-17-A (1HP)	N/A	N/A	N/A	N/A	89.46	Pass
236-3B	ERCW Hdr A Isln Vlv 1-FCV-3-136B-A (0.33HP)	N/A	N/A	N/A	N/A	84.72	Pass
236-5A	Sample Hx Isln Vlv 1-FCV-70-215-A (0.13HP)	N/A	N/A	N/A	N/A	86.73	Pass
236-5E	Cntrmt Spray Hx 1A Sup Cont Vlv 1-FCV-67-125-A (0.33HP)	N/A	N/A	N/A	N/A	92.51*	Pass
236-5F	Cntrmt Spray Hx 1A Disch Vlv 1-FCV-67-126-A (0.33HP)	N/A	N/A	N/A	N/A	92.19*	Pass

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Appendix A

1A Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No		SI Phase A DBE Actuation Terminal Voltage (%)	SI Phase B DBE Actuation Terminal Voltage (%)	Individual Motor Start Terminal Voltage (%)	Minimum Required Voltage Terminal Voltage V(%)	6.6kV/460V Base	Bases for Minimum Required Voltage	Reference
236-6A	AFWP Turb St Sply Frm St gen 4 1-FCV-1-16-A (1HP)	N/A	N/A	N/A	N/A	92.52*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
236-6D	RHR Sys Isln Bypass Vlv 1-FCV-74-8-A (1.6HP)	N/A	N/A	N/A	N/A	90.99*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
236-11A	Cmpnt Clg Hx A Disch Cont Vlv 1-FCV-67-146-A (0.3HP)	N/A	N/A	N/A	N/A	88.07	Pass	Att. 4 / Acceptable Margin
236-12B	SS&Con AirCpsr Sup Hdr A Iso V 0-FCV-67-205-A (0.33HP)	N/A	N/A	N/A	N/A	87.86	Pass	Att. 4 / Acceptable Margin
236-15A	CCS HX A ERCW BYPASS FCV 1-FCV-67-143-A (0.13HP)	N/A	N/A	N/A	N/A	84.62	Pass	Att.4
236-16E	RHR Hx A-A Outlet Vlv 1-FCV-70-156-A (0.33HP)	N/A	N/A	N/A	N/A	88.86	Pass	Att. 4 / Acceptable Margin
236-17A	Sample Hx Hdr Outlet Vlv 1-FCV-70-183-A (0.13HP)	N/A	N/A	N/A	N/A	86.09	Pass	Att. 4
236-17B	SFPCS Hx Sply Hdr Isln Vlv 0-FCV-70-197-A (0.3HP)	N/A	N/A	N/A	N/A	89.74	Pass	Att. 4 / Acceptable Margin
480V Reac Vent Board 1A-A								
None								

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Appendix A

1B Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)							
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage							
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts							
ETAP Bus ID/ Compt No	Load Description	6.6kV / 460V Base	SI Phase A DBE Actuation	SI Phase B DBE Actuation	Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
			Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%)	
6.9kV Shutdown Board 1B-B							
13-10 AFW	Aux Feedwater PMP 1B-B 1-MTR-3-128-B (600 HP)	99.01	Starts	99.01	Starts	98.98	85
13-13 CSP	CNTWMT SPRAY PMP 1B-B 1-MTR-72-10-B (700 HP)	N/A	Not Running	98.70	Start	98.69	80
13-14 RHR	RHR PUMP 1B-B 1-MTR-74-20-B (400 HP)	99.12	Starts	99.12	Starts	99.12	80
13-15 SI	SAFETY INJ PMP 1B-B 1-MTR-63-15-B (400 HP)	98.85	Starts	98.85	Starts	98.84	80
13-18 CCP	CNTFGL CHRG PMP 1B-B 1-MTR-62-104-B (600 HP)	98.78	Starts	98.78	Starts	98.78	80
13-8 ERCW	ERCW PMP F-B 0-MTR-67-51-B (800 HP)	N/A	Starts (F-B or E-B start, but not both, other is not running)	N/A	Starts (F-B or E-B start, but not both, other is not running)	96.20	90
13-9 ERCW	ERCW PMP E-B 0-MTR-67-47-B (800 HP)	95.10	Starts (E-B or F-B start, but not both, other is not running)	95.10	Starts (E-B or F-B start, but not both, other is not running)	95.01	90
480V Shutdown Board 1B1-B							
129-3C	Comp Cooling Sys Pump 1B-B 1-MTR-70-38-B (350hp)	80.89 (8s)	Starts	81.53 (8s)	Starts	80.63	70
130-7A	Elec Bd Rm AHU C-B 0-MTR-31-31-B (50hp)	N/A	Running	N/A	Running	90.28	80
130-7D	Reac Lwr Compt Clr Fan 1B-B 1-MTR-30-75-B (60hp)	N/A	Running	N/A	Trips	82.24	80
480V Shutdown Board 1B2-B							
131-2B	Control Rm A/C B-B Compressor 0-MTR-31-96-2-B (250hp)	N/A	Running	N/A	Running	83.25	80
131-3C	SHDN BD RM CHLR PKG B-B Compressor 0-MTR-31-49-2-B (240hp)	N/A	Running	N/A	Running	87.92	85
132-7D	Reac Lwr Compt Clr Fan 1D-B 1-MTR-30-78-B (60hp)	N/A	Running	N/A	Trips	82.33	80
132-9A	Spent Fuel Pit Pmp B-B 0-MTR-78-9-B (100hp)	N/A	Running	N/A	Running	83.47	80
132-9C	Cntrmt Air Rtn Fan 1B-B 1-MTR-30-39-B (100hp)	N/A	Not Running Starts @ 9 Min)	N/A	Not Running Starts @ 9 Min)	80.27 (SIB)	80
132-9D	480V SD Bd Rm AHU C-B 0-MTR-31-55-B (75hp)	N/A	Running	N/A	Running	86.74	85
480V C&A Vent Board 1B1-B							
205-11A	Cont Bldg Emerg Press Fan B-B, 0-MTR-31-5-B (1hp)	89.06	Starts	90.34	Starts	91.38	85
205-13D	ERCW Scrn Wash Pump 1B-B 1-MTR-67-440-B (40hp)	N/A	N/A	N/A	N/A	73.47 (SIB)	75

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Appendix A
1B Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	6.6kV / 460V Base	SI Phase A DBE Actuation	SI Phase B DBE Actuation	Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage	
			Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%)		
205-2A	Cont Bldg Em Air Clnup Fan B-B 0-MTR-31-7-B (10hp)	87.77	Starts	89.03	Starts	89.81	85	Att. 1
205-3C	Critmt Spray Pump 1B-B Rm Clr Fan 1-MTR-30-178-B (7.5hp)	N/A	Random	87.96	Starts	89.52	80	Att. 3
205-4D	Emerg Gas Trtmnt Sys Fan B-B 0-MTR-65-42-B (20hp)	86.53	Starts	87.78	Starts	88.81	80	Att. 3
205-6B	ERCW Str 1B-B 1-MTR-67-10-B (3hp)	N/A	Running	N/A	Running	76.88	75	Att. 3
205-7E	RWST to Spray Hdr 1A Vlv 1-FCV-72-22 (3.2hp)	N/A	Stopped (No auto Start)	N/A	Stopped (No auto Start)	88.14 (SIB)	Pass	Att. 4 / Acceptable Margin
205-4E	ERCW Str 1B-B Backwash Vlv 1-FCV-67-10A-B (0.33HP)	N/A	N/A	N/A	N/A	82.31	80	Att. 1
205-6E	ERCW Str 1B-B Flush Vlv 1-FCV-67-10B-B (0.33HP)	N/A	N/A	N/A	N/A	82.32	80	Att. 1
205-7D	RHR PMP 1B-B INLET FCV 1-FCV-74-21-B (5.2HP)	N/A	N/A	N/A	N/A	91.09	Pass	Att. 4 / Acceptable Margin
205-2C	Pen Rm El 713 Clr Fan 1B-B 1-MTR-30-197-B (3HP)	87.64	Starts	88.90	Starts	90.90	80	Att. 3
205-3A	Shdn Bd Rm Clr CW Cir Pmp B-B 0-MTR-31-49-1-B (25HP)	N/A	N/A	N/A	N/A	90.61	85	Att. 1
205-3B	Pipe Chase Clr Fan 1B-B 1-MTR-30-202-B (3HP)	86.47	Starts	87.72	Starts	89.20	80	Att. 3
205-3F1	Cntmt Bldg Upper Compt Air Mon 1-RE-90-112-B (3HP)	N/A	N/A	N/A	N/A	89.78	85	Att. 1
205-4A	Battery Rm El 692 Exh Fan B-B 0-MTR-31-29-B (1.5HP)	N/A	N/A	N/A	N/A	87.82	85	Att. 1
205-4F1	CNTMT PURGE AIR EXH MON 1-RE-90-131-B (0.75HP)	N/A	N/A	N/A	N/A	92.86	85	Att. 1
205-5A	SFP PmpB-B&TB Bst Pmp SpClrFan 0-MTR-30-193-B (7.5HP)	86.27	Starts	87.51	Starts	88.78	80	Att. 3
205-5E	CCS & AFW Pumps Sp Clr Fan B-B 1-MTR-30-191-B (20HP)	86.59	Starts	87.83	Starts	88.44	80	Att. 3
205-6A	SHUTDOWN BD RM A PRESS FAN C-B 0-MTR-31-67-B (3HP)	N/A	N/A	N/A	N/A	91.61	85	Att. 1
205-6C	Traveling Scrn 1B-B 1-MTR-67-445-B (5HP)	N/A	N/A	N/A	N/A	80.61 (SIB)	80	Att.3
205-7B	125V Vtl Bat Rm I Ex Fan 1A2-B 1-MTR-31-288-B (0.33HP)	N/A	N/A	N/A	N/A	91.17	85	Att. 1
205-7C	High Press Fir Pmp Str B-B 0-MTR-26-14-B (0.75HP)	N/A	N/A	N/A	N/A	86.83	85	Att. 1
205-8A	Safety Inj Pmp 1B-B Rm Clr Fan 1-MTR-30-179-B (5HP)	N/A	N/A	N/A	N/A	86.06	80	Att.3
205-8B	Pen Rm El 692 Clr Fan 1B-B 1-MTR-30-187-B (3HP)	N/A	N/A	N/A	N/A	89.52	80	Att.3
205-8C	Shtdn Xfrm Rm 1B Exh Fan 1B2-B 1-MTR-30-248F-B (3HP)	N/A	N/A	N/A	N/A	89.94	80	Att.3
205-8D	Shtdn Xfrm Rm 1B Exh Fan 1B3- 1-MTR-30-248G-B (3HP)	N/A	N/A	N/A	N/A	89.89	80	Att.3

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Appendix A

1B Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)							
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage							
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts							
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation	SI Phase B DBE Actuation	Individual Motor Start	Minimum Required Voltage	6.6kV / 460V Base	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage (%)		
205-8E	Cont Rm A/C Cir Pmp B-B 0-MTR-31-96/1-B (15HP)	N/A	N/A	N/A	85.40	85	Att. 1
205-8F1	CONT RM A/C B-B CONTROL/O.PMP 0-MTR-31-96/3-B (3HP)	N/A	N/A	N/A	91.69	85	Att. 1
205-9A	RHR Pmp 1B-Rm Clr Fan 1-MTR-30-176-B (5HP)	83.13	Starts	84.33	Starts	83.45	80
205-9B	5th Vlt Batt Rrn Exh Fan 1B2-B 0-MTR-31-496B-B (0.25HP)	N/A	N/A	N/A	N/A	93.69	85
205-9C	480V Bd Rm 1A Pr Sup Fan 1A2-B 1-MTR-31-463-B (3HP)	N/A	N/A	N/A	N/A	92.36	85
205-9D	Shtdn Xfrm Rm 1B Exh Fan 1B1-B 1-MTR-30-248E-B (3HP)	N/A	N/A	N/A	N/A	87.59	80
205-9E	Pen Rm El 737 Clr Fan 1B-B 1-MTR-30-195-B (3HP)	87.45	Starts	88.71	Starts	89.63	80
205-10A	Cntfg Chrg Pmp 1B-B Rm Clr Fan 1-MTR-30-182-B (5HP)	84.65	Starts	85.87	Starts	85.42	80
205-10B	480V Bd Rm 1B Pr Sup Fan 1B2-B 1-MTR-31-477-B (3HP)	N/A	N/A	N/A	N/A	92.22	85
205-10C	125V VTL BAT RM II EXFAN 1B2-B 1-MTR-31-286-B (0.33HP)	N/A	N/A	N/A	N/A	91.01	85
205-10F1	Cont Rm Intake Mon 0-RE-90-206-B (0.75HP)	N/A	N/A	N/A	N/A	89.58	85
205-11B	480V Bd Rm 1B A/C Ahu 1B-B 1-MTR-31-475-B (20HP)	N/A	N/A	N/A	N/A	89.39	85
205-11C	480V Bd Rm 1B A/C Cond 1B-B 1-MTR-31-289-B (20HP)	N/A	N/A	N/A	N/A	91.40	85
205-11D	Cont Rm Ahu B-B 0-MTR-31-11-B (60HP)	N/A	N/A	N/A	N/A	87.63	85
480V C&A Vent Board 1B2-B							
None							
480V Diesel Aux Board 1B1-B							
219-2B	DG 1B-B RM EXH FAN 1-B 1-MTR-30-449-B (15hp)	90.80	Starts	91.41	Start	91.42	85
219-3D	DG 1B-B DAY TNK FO XFR PMP 1 1-MTR-18-55/2-B (1hp)	90.85	Random	91.46	Random	93.65	85
219-4B	Dg 1B-B Aux LubeOil Circ Pmp A 1-MTR-82-AOPA2B (0.75hp)	91.49	Starts	92.11	Starts	93.89	85
219-6A	DG 1B-B Muffler Rm Exh Fan 1-MTR-30-465 (0.5hp)	91.27	Starts	91.88	Starts	94.31	85
219-2D	Dg 1B-B Lube Oil Circ Pmp 1 1-MTR-82-B1-B (1HP)	N/A	N/A	N/A	N/A	93.79	85
219-4E	DG 1B-B 480V ELEC BD RM EX FAN 1-MTR-30-461-B (2HP)	N/A	N/A	N/A	N/A	93.52	85
480V Diesel Aux Board 1B2-B							
220-2B	DG 1B-B Rm Exh Fan 2-B 1-MTR-30-453-B (15hp)	91.32	Starts	91.79	Starts	92.60	85
220-3D	DG 1B-B DAY TNK FO XFR PMP 2 1-MTR-18-54/2-B (1HP)	91.14	Starts	91.60	Starts	94.85	85
220-2A	Dg 1B-B Aux LubeOil Circ Pmp B 1-MTR-82-AOPB2B (0.75HP)	N/A	N/A	N/A	N/A	94.33	85

Appendix A

1B Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No		Load Description	6.6kV / 460V Base	SI Phase A DBE Actuation	SI Phase B DBE Actuation	Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
				Terminal Voltage (%)	Terminal Voltage (%)	Terminal Voltage (%)	Terminal Voltage V(%)	
220-2D	Dg 1B-B Lube Oil Circ Pmp 2 1-MTR-82-B2-B (1HP)	N/A	N/A	N/A	N/A	94.71	85	Att. 1
480V RMOV Board 1B1-B								
237-3F2	SIS ACCUM TANK FLOW ISOL VLV 1-FCV-63-98-B (6.6hp)	91.28	Opens on SI (Starts)	92.56	Opens on SI (Starts)	94.86	Pass	Att. 1
237-6D	Seal Flow Ret Isln Vlv 1-FCV-62-61-B (1.9hp)	81.68	Closes on Ph A (Starts)	82.82	Closes on Ph B (Starts)	85.18	Pass	Att. 4
237-7A	CHRG FLOW ISLN VLV 1-FCV-62-91-B (1.9hp)	86.42	Closes on SI (Starts)	87.63	Closes on SI (Starts)	90.11	Pass	Att. 4
237-8A	Vol Cont Tank Outlet Isln Vlv 1-LCV-62-133-B (1.9hp)	81.82	Closes on SI (Starts)	82.97	Closes on SI (Starts)	85.33	Pass	Att. 4
237-8B	RWST To Charging Pmp Vlv Cont 1-LCV-62-136-B (1.9hp)	79.51	Opens on SI (Starts)	80.63	Opens on SI (Starts)	82.92	Pass	Att. 4
237-10A	SIS 1A-A DSH TO RWST SHTFF VLV 1-FCV-63-4-B (0.7hp)	N/A	Not Running or Starting	N/A	Not Running or Starting	84.83	Pass	Att. 4/ Acceptable Margin
237-10B	RWST To SIS Pump Flow Cont Vlv 1-FCV-63-5-B (1.9hp)	N/A	Not Running or Starting	N/A	Not Running or Starting	88.02*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
237-11A	SIS PMP INLT TO CVCS CHRG PMP 1-FCV-63-6-B (1.9hp)	N/A	Not Running or Starting	N/A	Not Running or Starting	88.21*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
237-11E	SIS Boron Inj Tank Shutoff Vlv 1-FCV-63-25-B (1.9hp)	82.98	Opens on SI (Starts)	84.14	Opens on SI (Starts)	86.53	Pass	Att. 4
237-12B	SIS Pmp 1B-B Inlet Vlv 1-FCV-63-48-B (1.9hp)	N/A	Not Running or Starting	N/A	Not Running or Starting	90.23*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
237-12D	CNTMT SUMP TO RHR PMP B-B 1-FCV-63-73-B (13hp)	N/A	Opens at approx. 20 min	N/A	Opens at approx. 20 min	88.20	Pass	Att. 4/ Acceptable Margin
237-14A	Cntrmt Spray Hdr 1B Isln Vlv 1-FCV-72-2-B (3.2hp)	N/A	Closed, Not Running	92.98* (5s)	Opens, Starting.	92.86*	Pass	Att. 4 (5 sec after SI) - Time Delay added per DCN 52834
237-15B	RHR Pmp 1B-B Min Flow Vlv 1-FCV-74-24-B (0.13hp)	79.61	Opens, Starting.	80.73	Opens, Starting.	83.12	Pass	Att. 4
237-17D	AFW Pmp B-B Lube Oil Pmp B-B 1-MTR-3-128D-B (0.25HP)	N/A	N/A	N/A	N/A	89.64	85	Att. 1
237-5E	RCS Press Relief Flow Cont Vlv 1-FCV-68-332-B (1.9HP)	N/A	N/A	N/A	N/A	88.06*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
237-9B	RHR To RCS H.L. 1&3 Flow Iso V 1-FCV-63-172-B (2.6HP)	N/A	N/A	N/A	N/A	86.20	Pass	Att. 4 / Acceptable Margin

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Appendix A

1B Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)							
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage							
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts							
ETAP Bus ID/ Compt No	Load Description	6.6kV / 460V Base	SI Phase A DBE Actuation	SI Phase B DBE Actuation	Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
			Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage (%)	Terminal Voltage V(%)
237-9F	Cont Spray Pmp 1B-B Recirc FCV 1-FCV-72-13-B (0.13HP)	N/A	N/A	N/A	N/A	90.08*	Pass
237-11B	RHR Hx B To SIS Pmp 1-FCV-63-11-B (2HP)	N/A	N/A	N/A	N/A	85.98	Pass
237-12E	SIS To RCS Loops 1&4 FCV 1-FCV-63-94-B (1.6HP)	N/A	N/A	N/A	N/A	90.80	Pass
237-13A	SIS Pmp 1B-B Outlet FCV 1-FCV-63-153-B (1.9HP)	N/A	N/A	N/A	N/A	88.75*	Pass
237-13B	SIS PMP OUT RCS LP 2&4 H. LEG 1-FCV-63-157-B (1.9HP)	N/A	N/A	N/A	N/A	91.36*	Pass
237-13D	SIS 1B-B Dsh To RWST Shftf Vlv 1-FCV-63-175-B (0.7HP)	N/A	N/A	N/A	N/A	84.86	Pass
237-14D	RHR Spray Hdr 1B Isln Vlv 1-FCV-72-41-B (1.9HP)	N/A	N/A	N/A	N/A	85.82	Pass
237-14E	Cntmt Sump To Spray Hdr 1B FCV 1-FCV-72-45-B (3.2HP)	N/A	N/A	N/A	N/A	89.68*	Pass
237-15D	RHR Hx 1B Bypass Vlv 1-FCV-74-35-B (1.9HP)	N/A	N/A	N/A	N/A	83.17	Pass
480V RMOV Board 1B2-B							
238-2A	ERCW Hdr B Isln Vlv 1-FCV-3-126A-B (0.25hp)	N/A	Random	N/A	Random	83.60	Pass
238-3A	ERCW Hdr B Isln Vlv 1-FCV-3-179A-B (0.33hp)	N/A	Random	N/A	Random	83.71	Pass
238-3D	ST GEN NO 2 FW ISLN VLV 1-FCV-3-47-B (39.4hp)	80.64	Starts	81.41	Starts	82.74	Pass
238-4D	St Gen No 4 FW Isln Vlv 1-FCV-3-100-B (39.4hp)	80.64	Use 89-10 start	81.41	Use 89-10 start	82.74	Pass
238-5C	LWR CNTMT 1A CLRS ISLN VLV 1-FCV-67-113-B (0.13hp)	N/A	Not Running	82.01	Closes (Starts)	85.62	Pass
238-6D	RCP Thrm Bar Rtn Cntmt Iso Vlv 1-FCV-70-87-B (0.7hp)	N/A	Not Running	84.16	Closes (Starts)	87.83	Pass
238-6E	RCP THRM BAR CNTMT ISO VLV 1-FCV-70-134-B (0.13hp)	N/A	Not Running	82.33	Closes (Starts)	85.96	Pass
238-7D	Lwr Cntmt 1B Clr Dish Iso Vlv 1-FCV-67-103-B (0.13hp)	N/A	Not Running	82.80	Closes (Starts)	86.22	Pass
238-7F	Up Cntm Vt Clr 1A Dish Iso Vlv 1-FCV-67-131-B (0.13hp)	N/A	Not Running	80.64	Closes (Starts)	83.98	Pass
238-8D	Lwr Cntmt 1D Clr Dish Iso Vlv 1-FCV-67-111-B (0.13hp)	N/A	Not Running	83.11	Closes (Starts)	86.55	Pass

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Appendix A

1B Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)							
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage							
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts							
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation	SI Phase B DBE Actuation	Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage	
		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage (%)		
6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base		
238-8F	Up Cntrn Vt Clr 1C Dish Iso Vlv 1-FCV-67-134-B (0.13hp)	N/A	Not Running	80.60	Closes (Starts)	83.93	Pass
238-9A	Lwr Cntrmt 1A Clr Dish Iso Vlv 1-FCV-67-88-B (0.33hp)	N/A	Not Running	83.71	Closes (Starts)	87.16	Pass
238-9B	Lwr Cntrmt 1C Clr Dish Iso Vlv 1-FCV-67-96-B (0.33hp)	N/A	Not Running	83.83	Closes (Starts)	87.28	Pass
238-9D	Up Cntrn Vt Clr 1B Dish Iso Vlv 1-FCV-67-297-B (0.13hp)	N/A	Not Running	81.49	Closes (Starts)	84.87	Pass
238-9F	Up Cntrn Vt Clr 1B Sup Iso Vlv 1-FCV-67-138-B (0.13hp)	N/A	Not Running	80.55	Closes (Starts)	83.88	Pass
238-10A	Lwr Cntrmt 1B Clr Sply Isln Vlv 1-FCV-67-91-B (0.33hp)	N/A	Not Running	83.74	Closes (Starts)	87.21	Pass
238-10B	Lwr Cntrmt 1D Clr Sply Isln Vlv 1-FCV-67-83-B (0.33hp)	N/A	Not Running	84.33	Closes (Starts)	87.82	Pass
238-10D	UP CNTM VT CLR 1D DIS ISO VLV 1-FCV-67-298-B (0.13hp)	N/A	Not Running	80.13	Closes (Starts)	83.46	Pass
238-10F	Up Cntrn Vt Clr 1D Sup Iso Vlv 1-FCV-67-141-B (0.13hp)	N/A	Not Running	80.92	Closes (Starts)	84.29	Pass
238-11D	LWR CNTMT 1C CLRS ISLN VLV 1-FCV-67-105-B (0.13hp)	N/A	Not Running	81.77	Closes (Starts)	85.16	Pass
238-13D	RCP Oil Clr Rtn Cntrnt Isln Vlv 1-FCV-70-89-B (0.13hp)	N/A	Not Running	83.44	Closes (Starts)	86.91	Pass
238-13F	RCP Oil Clr Hdr Cntrmt Isln Vlv 1-FCV-70-140-B (0.33hp)	N/A	Not Running	83.64	Closes (Starts)	87.10	Pass
238-18D	480V Bd Rm 1B A/C Cprsr 1B-B 1-MTR-31-447-B (75HP)	N/A	N/A	N/A	89.30	85	Att. 1
238-2B	ERCW Hdr B Isln Vlv 1-FCV-3-126B-B (0.25HP)	N/A	N/A	N/A	83.62	Pass	Att. 4
238-2E	St Flow To AFWP Turb Isln Vlv 1-FCV-1-18-B (1HP)	N/A	N/A	N/A	92.50*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
238-3B	ERCW Hdr B Isln Vlv 1-FCV-3-179B-B (0.33HP)	N/A	N/A	N/A	83.72	Pass	
238-5E	Cntrmt Spray Hx 1B Sup Cont Vlv 1-FCV-67-123-B (0.33HP)	N/A	N/A	N/A	92.08*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
238-5F	Cntrmt Spray Hx 1B Disch Vlv 1-FCV-67-124-B (0.33HP)	N/A	N/A	N/A	91.73*	Pass	
238-11B	STA S & C AC SUP HDR B ISO VLV 0-FCV-67-208-B (0.33HP)	N/A	N/A	N/A	91.28*	Pass	Att. 4
238-17D	CCS HX B ERCW BYPASS FCV 0-FCV-67-144-B (0.13HP)	N/A	N/A	N/A	84.33	Pass	Att. 4 / Acceptable Margin
480V Reac Vent Board 1B-B							
None							

Appendix A

1B Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)							
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage							
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts							
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation	SI Phase B DBE Actuation	Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage	
		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage (%)		
6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base	6.6kV / 460V Base	Reference

* This MOV terminal voltage is calculated taking credit for the hammer blow feature.

Appendix A

2A Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit) Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
		SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
ETAP Bus ID/ Compt No	Load Description	6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base	Reference
6.9KV Shutdown Board 2A-A								
14-10 AFW	AUX FEEDWTR PMP 2A-A 2-MTR-3-118-A (600hp)	98.98	Starts	98.98	Starts	98.94	85	Att. 3
14-13 CSP	CNTMT SPRAY PMP 2A-A 2-MTR-72-27-A (700hp)	N/A	Not Running	N/A	Starts	98.60	80	Based on Unit 1 motor data (Att. 3)
14-14 RHR	RHR PMP 2A-A 2-MTR-74-10-A (400hp)	99.08	Starts	99.08	Starts	99.08	80	Based on Unit 1 motor data (Att. 3)
14-15 SI	SAFETY INJ PMP 2A-A 2-MTR-63-10-A (400hp)	98.83	Starts	98.83	Starts	98.83	80	Based on Unit 1 motor data (Att. 3)
14-18 CCP	CNTFGL CHRG PMP 2A-A 2-MTR-62-108-A (600hp)	98.98	Starts	98.98	Starts	98.97	80	Att. 3
14-8 ERCW	ERCW PMP D-A 0-MTR-67-40-A (800hp)	N/A	Starts (D-A or C-A start, but not both, other is not running)	N/A	Starts (D-A or C-A start, but not both, other is not running)	96.59	90	Att. 3
14-9 ERCW	ERCW PMP C-A 0-MTR-67-36-A (800hp)	96.67	Starts (D-A or C-A start, but not both, other is not running)	96.67	Starts (D-A or C-A start, but not both, other is not running)	96.61	90	Same as ERCW Pmp D-A (Att. 3)
480V Shutdown Board 2A1-A								
133-3B	Cmpnt Clg Sys Pmp 2A-A 2-MTR-70-59-A (350hp)	81.38 (8s)	Starts	81.78 (8s)	Starts	81.26	70	Att. 3
134-10C	Cntrmt Air Rtn Fan 2A-A 2-MTR-30-38-A (100hp)	N/A	Not Running Starts @ 9 Min	N/A	Not Running Starts @ 9 Min	82.41 (SIB)	80	Att. 6
134-7C	Reac Lwr Compt Clr Fan 2A-A 2-MTR-30-74-A (60hp)	N/A	Running	N/A	Trips	83.31	80	Based on Unit 1 motor data (Att. 3)
134-9C	Elec Bd Rm AHU B-A 0-MTR-31-30D-A (50hp)	N/A	Running	N/A	Running	83.48	80	Att. 6
480V Shutdown Board 2A2-A								
135-2C	Elec Bd Rm A/C A-A Cprsr 0-MTR-31-128/2-A (250hp)	N/A	Running	N/A	Running	86.06	85	Att. 1
135-3C	SHDN BD RM CHLR PKG A-A CPRSR 0-MTR-31-36/2-A (240hp)	N/A	Running	N/A	Running	91.51	85	Att. 1
136-7D	REAC LWR COMPT CLR FAN 2C-A 2-MTR-30-77-A (60hp)	N/A	Running	N/A	Trips	81.11	80	Based on Unit 1 motor data (Att. 3)
136-8D	480V SHUTDOWN BD RM AHU B-A 0-MTR-31-44-A (75hp)	N/A	Running	N/A	Running	86.84	85	Att. 1
136-9D	Spent Fuel Plt Pmp A-A 0-MTR-78-12-A (100hp)	N/A	Running	N/A	Running	82.29	80	Att. 6
480V Reactor Vent Board 2A-A								
None								
480V C&A Vent Board 2A1-A								
207-10A	Cntfg Chrg Pmp 2A-A Rm Clr Fan 2-MTR-30-183-A (5HP)	83.44	Starts on SI	84.19	Starts on SI	86.10	80	Based on Unit 1 motor data (Att. 3)

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Appendix A

2A Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation	SI Phase B DBE Actuation	Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage	Reference	R2
		Terminal Voltage (%)			Terminal Voltage (%)			
		6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base	
207-10B	Pen Rm El 713 Clr Fan 2A-A 2-MTR-30-196-A (3HP)	87.11	Starts on SI	87.89	Starts on SI	90.89	80	Based on Unit 1 motor data (Att. 3)
207-10C	Pipe Chase Clr Fan 2A-A 2-MTR-30-201-A (3HP)	84.55	Starts on SI	85.31	Starts on SI	86.93	80	Based on Unit 1 motor data (Att. 3)
207-10D	ABGTS HUM HTR A-A 0-HTR-30-147-A (50.008kW)	N/A	Starts on ABI (from SI)	N/A	Starts on ABI (from SI)	N/A	Static Load	N/A
207-11A	480V Bd Rm 2B Pr Sup Fan 2B1-A 2-MTR-31-478-A (3HP)	N/A	Running	N/A	Running	92.41	85	Att. 1
207-11C	480V Bd Rm 2A A/C Ahu 2A-A 2-MTR-31-461-A (10HP)	N/A	Running	N/A	Running	88.57	85	Att. 1
207-12A	125V Vital Bat Rm Iff Ex Fan 2B1-A 2-MTR-31-285-A (0.33HP)	N/A	Running	N/A	Running	91.84	85	Att. 1
207-12C	480V Bd Rm 2A A/C Cond 2A-A 2-MTR-31-290-A (15HP)	N/A	Running	N/A	Running	91.02	85	Att. 1
207-12F1	Cntmt Purge Air Radn Exh Mon 2-RE-90-130-A (0.75HP)	N/A	Running	N/A	Running	93.49	85	Att. 1
207-13D	ERCW SCREEN WASH PUMP 2A-A 2-MTR-67-437-A (40HP)	N/A	Running	N/A	Running	76.53	75	Att. 3 Also See Sec. 7.1
207-2A	AUX CONTROL AIR COMPRESSOR A-A 0-MTR-32-60-A (20hp)	N/A	Not Running	N/A	Not Running	84.61	80	Att. 1
207-2C	Pen Rm El 692 Clr Fan 2A-A 2-MTR-30-186-A (3HP)	84.16	Starts on SI	84.92	Starts on SI	86.97	80	Based on Unit 1 motor data (Att. 3)
207-3A	Shdn Bd Rm Chfr CW Cir Pmp A-A 0-MTR-31-36/1-A (25HP)	N/A	Running	N/A	Running	86.75	85	Att. 1
207-3C	Cntr Spray Pmp 2A-A Rm Clr Fan 2-MTR-30-177-A (7.5HP)	N/A	Running	84.21	Starts on Phase B	87.19	80	Based on Unit 1 motor data (Att. 3)
207-3D	AUX BLDG Gas Trtmt Sys Fan A-A 2-MTR-30-146-A (50hp)	83.76	Starts On ABI (from SI)	84.51	Starts On ABI	89.53	80	Att. 3
207-4A	EG Trtmt Sys A-A Rm Clr Fan 2-MTR-30-200-A (3HP)	86.11	Starts on ABI (from SI)	86.89	Starts on ABI (from SI)	91.20	80	Att. 3
207-4E	ERCW Str 2A-A Backwash Vlv 2-FCV-67-9A-A (0.33HP)	N/A	N/A	N/A	N/A	83.90	80	Att. 1
207-5E	AFW & BA XFR SPACE CLR FAN A-A 2-MTR-30-184-A (15HP)	87.08	Starts on ABI (from SI)	87.87	Starts on ABI (from SI)	90.96	80	Based on Unit 1 motor data (Att. 3)
207-6B	ERCW Str 2A-A 2-MTR-67-9-A (3HP)	N/A	Running	N/A	Running	82.53	75	Att. 3
207-6C	Traveling Scrn 2A-A 2-MTR-67-439-A (3HP)	N/A	N/A	N/A	N/A	81.49	80	Att. 3
207-7B	125V VIT BAT RM IV EXFAN 2A1-A 2-MTR-31-287-A (0.33HP)	N/A	Running	N/A	Running	92.12	85	Att. 1
207-7A	Safety Inj Pmp 2A-A Rm Clr Fan 2-MTR-30-180-A (5HP)	84.46 (2s)	Starts on Pump Start	80.70	Starts on Pump Start	81.70	80	Based on Unit 1 motor data (Att. 3)
207-7B	Pen Rm El 737 Clr Fan 2A-A 2-MTR-30-194-A (3HP)	87.66	Starts on ABI (from SI)	88.45	Starts on ABI (from SI)	92.45	80	Att. 3
207-7C	480V Xfrm Rm 2A Exh Fan 2A2-A 2-MTR-30-250F-A (3HP)	N/A	Running	N/A	Running	91.94	80	Att. 3
207-7D	480V Xfrm Rm 2A Exh Fan 2A3-A 2-MTR-30-250G-A (3HP)	N/A	Running	N/A	Running	91.94	80	Att. 3
207-8F1	EL BD RM A/C A-A CONTROL/D.PMP 0-MTR-31-128/3-A (3.11HP)	N/A	Running	N/A	Running	91.13	85	Att. 1

Appendix A

2A Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No		Load Description	6.6kV / 460V Base	SI Phase A DBE Actuation	SI Phase B DBE Actuation	Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
				Terminal Voltage (%)	Terminal Voltage (%)	Terminal Voltage (%)	Terminal Voltage V(%)	
207-9A	RHR Pmp 2A-A Rm Clr Fan 2-MTR-30-175-A (1.5HP)		84.23 (2s)	Starts on SI	80.47	Starts on SI	81.35	80
207-9B	C.BIDG Ele BdRm AC Cir Pmp A-A 0-MTR-31-128/1-A (20HP)		N/A	Running	N/A	Running	88.10	85
207-9C	480V Bd Rm 2A Pr Sup Fan 2A1-A 2-MTR-31-462-A (3HP)		N/A	Running	N/A	Running	92.31	85
207-9D	480V Xfrm Rm 2A Exh Fan 2A1-A 2-MTR-30-250E-A (3HP)		N/A	Running	N/A	Running	91.49	85
207-9F1	Cont Rm Intake Mon 0-RE-90-125-A (0.75HP)		N/A	Running	N/A	Running	93.16	85
207-7E	RWST To Spray Hdr 2A FCV 2-FCV-72-22-A (3.2HP)		N/A	N/A	N/A	N/A	86.30	Pass
480V C&A Vent Board 2A2-A								
None								
480V Diesel Aux Board 2A1-A								
221-2B	DG 2A-A RM EXH FAN 1-A 2-MTR-30-448-A (15hp)		92.28	Starts	92.66	Starts	93.44	85
221-2D	DG 2A-A Lube Oil Circ Pmp 1 2-MTR-82-A1-A (1hp)		N/A	Running	N/A	Running	94.72	85
221-3A	EM DG ENG HX 2A1 & 2A2 SUP VLV 2-FCV-67-66-A (0.13hp)		82.55	Starts	82.90	Starts	85.97	Pass
221-3D	DG 2A-A DAY TNK FO XFR PMP 1 2-MTR-18-55/3-A (1hp)		91.55	Random	91.94	Random	94.78	85
221-4B	DG 2A-A Aux LubeOil Circ Pmp A 2-MTR-82-AOPA1A (0.75hp)		N/A	Running	N/A	Running	94.97	85
221-6A	DG 2A-A Muffler Rm Exh Fan 2-MTR-30-464 (0.5hp)		91.99	Starts on Diesel Start from SI	92.37	Starts on Diesel Start from SI	94.90	85
221-4D	DG Rm 2A-A Pnl Vent Fan 2-MTR-30-492-A (15HP)		N/A	N/A	N/A	N/A	92.29	85
221-4E	2A-A 480V ELEC BD RM EX FAN 2-MTR-30-460-A (2HP)		N/A	N/A	N/A	N/A	95.16	85
480V Diesel Aux Board 2A2-A								
222-2A	DG 2A-A Aux LubeOil Circ Pmp B 2-MTR-82-AOPB1A (0.75hp)		N/A	Running	N/A	Running	94.93	85
222-2B	DG 2A-A RM EXH FAN 2-A 2-MTR-30-452-A (15hp)		92.59	Starts	92.85	Starts	93.29	85
222-2D	DG 2A-A Lube Oil Circ Pmp 2 2-MTR-82-A2-A (1hp)		N/A	Running	N/A	Running	94.98	85
222-3D	DG 2A-A DAY TNK FO XFR PMP 2 2-MTR-18-54/3-A (1hp)		92.18	Random	92.44	Random	94.94	85
480V RMOV Board 2A1-A								
239-10F	Cntrmt Spray Pmp 2A-A Recirc FCV 2-FCV-72-34-A (0.13hp)		N/A	Not Running	N/A	Closes 10s after Phase B	89.37	Pass
239-11D	SIS Boron Inj Tank Shutoff Vlv 2-FCV-63-26-A (1.9hp)		86.11	Opens on SI (Starts)	86.83	Opens on SI (Starts)	92.06	Pass
239-12B	Cntrmt Sump To RHR Pmp A-A 2-FCV-63-72-A (1.3hp)		N/A	Operate about 20 minutes after SI	N/A	Operate about 20 minutes after SI	91.21	Pass
								Att. 5 / Acceptable Margin

Appendix A

2A Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No		Load Description	6.6kV / 460V Base	SI Phase A DBE Actuation	SI Phase B DBE Actuation	Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
				Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage (%)	
239-13E	Cntrnt Spray Hdr 2A Isln Vlv 2-FCV-72-39-A (3.2hp)		N/A	Not Running	83.13	Opens on Ph B (Starts)	87.97	Pass
239-14D	RHR Pmp 2A-A Min Flow Vlv 2-FCV-74-12-A (0.13hp)		83.91	Random	84.61	Random	89.71	Pass
239-15D	LWR CNTMT 2A CLRS SUP ISLN VLV 2-FCV-67-89-A (0.33hp)		N/A	Not Running	87.91	Closes (Starts)	93.22	Pass
239-17B	Cntrnt Standpipe Isln Vlv 2-FCV-26-240-A (0.67hp)		82.10	Close (Starts)	82.78	Close (Starts)	87.74	Pass
239-18E	RCP Spray Isln Vlv 2-FCV-26-243-A (0.67hp)		81.17	Close (Starts)	81.85	Close (Starts)	86.47	Pass
239-7A	Seal Flow Ret Isln Vlv 2-FCV-62-63-A (1.9hp)		77.85	Closes on Ph A (Starts)	78.50	Closes on Ph A (Starts)	83.16	Pass
239-7B	CHRG FLOW ISLN VLV 2-FCV-62-90-A (1.9hp)		85.16	Closes on SI	85.86	Closes on SI	90.94	Pass
239-8B	Vol Cont Tank Outlet Isln Vlv 2-LCV-62-132-A (1.9hp)		80.78	Closes on SI	81.45	Closes on SI	86.28	Pass
239-5C	LWR CNTMT 2C CLRS SUP ISLN VLV 2-FCV-67-97-A (0.33hp)		N/A	Not Running	87.71	Closes (Starts)	93.00	Pass
239-9A	RWST TO CHARGING PMPS CONT 2-LCV-62-135-A (1.9hp)		84.82	Opens on SI (Starts)	85.52	Opens on SI (Starts)	90.58	Pass
239-9D	2-FCV-70-100A (0.33hp)		N/A	Not Running	87.19	Closes on Phase B	92.46	Pass
239-10B	SIS PMPS RECIRC TO RWST 2-FCV-63-3-A (0.7HP)		N/A	N/A	N/A	N/A	89.43	Pass
239-2B	Boric Acid Transfer Pmp 2A-A 2-MTR-62-230-A (15HP)		N/A	N/A	N/A	N/A	92.42	85
239-11A	SIS Pmp Inlet To CVCS Chrg Pmp 2-FCV-63-7-A (1.9HP)		N/A	N/A	N/A	N/A	81.98	Pass
239-14E	RHR Hx 2A Bypass Vlv 2-FCV-74-33-A (1.9HP)		N/A	N/A	N/A	N/A	84.67	Pass
239-2C	THERM BAR SYS BSTIR PMP 2A-A 2-MTR-70-131-A (10HP)		N/A	N/A	N/A	N/A	86.94	85
239-11B	RHR Hx A To CVCS Chgr Pmp 2-FCV-63-8-A (1.9HP)		N/A	N/A	N/A	N/A	89.05	Pass
239-2E1	RWST To RHR Pmp Flow Cont Vlv 2-FCV-63-1-A (5.2HP)		N/A	N/A	N/A	N/A	91.80	Pass
239-3E	Cntrgl Chrg Pmp 2A-A AOP 2-MTR-62-AOP-A (2HP)		N/A	N/A	N/A	N/A	86.44	85
239-12A	SIS Pmp 2A-A Inlet Vlv 2-FCV-63-47-A (1.9HP)		N/A	N/A	N/A	N/A	79.72	Pass
239-4E	APW Pmp A-A Lube Oil Pmp A-A 2-MTR-3-118D-A (0.25HP)		N/A	N/A	N/A	N/A	88.24	85
239-12D	SIS To RCS Loops 2&3 FCV 2-FCV-63-93-A (1.6HP)		N/A	N/A	N/A	N/A	93.00	Pass
239-12E	SIS Pmp 2A-A Outlet FCV 2-FCV-63-152-A (1.9HP)		N/A	N/A	N/A	N/A	85.61	Pass
239-13A	SIS Pmp Out RCS Lp 1&3 Hot Leg 2-FCV-63-156-A (1.9HP)		N/A	N/A	N/A	N/A	85.58	Pass

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Appendix A
2A Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit) Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%)	
ETAP Bus ID/ Compt No	Load Description	6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base	Reference
239-6D	RCS Press Relief FCV 2-FCV-68-333-A (1.9HP)	N/A	N/A	N/A	N/A	86.46	Pass	Att. 5 / Acceptable Margin
239-13B	Cntrmt Sump To Spray Hdr 2A FCV 2-FCV-72-44-A (3.2HP)	N/A	N/A	N/A	N/A	80.63	Pass	Att. 5 / Acceptable Margin
239-14A	RHR Spray Hdr 2A Isln Vlv 2-FCV-72-40-A (1.9HP)	N/A	N/A	N/A	N/A	88.31	Pass	Att. 5 / Acceptable Margin
480V RMOV Board 2A2-A								
240-10A	Lwr Cntrm 2D Clr Dish Iso Vlv 2-FCV-67-112-A (0.33hp)	N/A	Not Running	89.57	Closes (Starts)	92.14	Pass	Att. 5
240-10D	Up Cntrm Vt Clr 2C Dish Iso Vlv 2-FCV-67-296-A (0.13hp)	N/A	Not Running	88.24	Closes (Starts)	90.77	Pass	Att. 5
240-10F	Up Cntrm Vt Clr 2D Dish Iso Vlv 2-FCV-67-142-A (0.13hp)	N/A	Not Running	89.61	Closes (Starts)	92.18	Pass	Att. 5
240-11D	RCP Thrm Barr Rtn Cntrm Iso Vlv 2-FCV-70-90-A (0.7hp)	N/A	Not Running	87.25	Closes (Starts)	89.73	Pass	Att. 5
240-11E	RCP Thrm Barr Cntrm Isln Vlv 2-FCV-70-133-A (0.13hp)	N/A	Not Running	87.62	Closes (Starts)	90.14	Pass	Att. 5
240-12D	RCP Oil Clr Rtn Cntrm Isln Vlv 2-FCV-70-92-A (0.13hp)	N/A	Not Running	88.59	Closes (Starts)	91.77	Pass	Att. 5
240-16D	Excs Ldtd Hx Cont Init Iso Vlv 2-FCV-70-143-A (0.33hp)	88.49	Closes on Phase A	88.93	Closes on Phase A	91.48	Pass	Att. 5
240-3D	St Gen No 1 FW Isln Vlv 2-FCV-3-33-A (39.4hp)	85.33	Use 89-10 start	85.75	Use 89-10 start	86.38	Pass	Att. 5
240-4D	St Gen No 3 FW Isln Vlv 2-FCV-3-87-A (39.4hp)	87.00	Use 89-10 start	87.43	Use 89-10 start	88.05	Pass	Att. 5
240-7D	Lwr Cntrm 2A Clr Dish Iso Vlv 2-FCV-67-87-A (0.13hp)	N/A	Not Running	89.73	Closes (Starts)	92.31	Pass	Att. 5
240-7F	Up Cntrm Vt Clr 2A Sup Iso Vlv 2-FCV-67-130-A (0.13hp)	N/A	Not Running	89.63	Closes (Starts)	92.20	Pass	Att. 5
240-8B	Lwr Cntrmt 2A Clr Sply Isln Vlv 2-FCV-67-107-A (0.33hp)	N/A	Not Running	89.57	Closes (Starts)	92.14	Pass	Att. 5
240-8D	Lwr Cntr 2C Clr Dish Iso Vlv 2-FCV-67-95-A (0.13hp)	N/A	Not Running	89.45	Closes (Starts)	92.02	Pass	Att. 5
240-8F	Up Cntrm Vt Clr 2C Sup Iso Vlv 2-FCV-67-133-A (0.13hp)	N/A	Not Running	89.59	Closes (Starts)	92.16	Pass	Att. 5
240-9A	Lwr Cntrmt 2C Clr Sply Isln Vlv 2-FCV-67-99-A (0.33hp)	N/A	Not Running	89.40	Closes (Starts)	91.97	Pass	Att. 5
240-9B	Lwr Cntr 2B Clr Dish Iso Vlv 2-FCV-67-104-A (0.33hp)	N/A	Not Running	89.40	Closes (Starts)	91.97	Pass	Att. 5
240-9D	Up Cntrm Vt Clr 2A Dish Iso Vlv 2-FCV-67-295-A (0.13hp)	N/A	Not Running	88.06	Closes (Starts)	90.59	Pass	Att. 5
240-9F	Up Cntrm Vt Clr 2B Dish Iso Vlv 2-FCV-67-139-A (0.13hp)	N/A	Not Running	89.61	Closes (Starts)	92.18	Pass	Att. 5
240-11A	Cmpnt Clg Hx A Disch Cont Vlv 2-FCV-67-146-A (0.3HP)	N/A	N/A	N/A	N/A	89.64	Pass	Att. 5 / Acceptable Margin
240-15A	CCS HX B ERcw BYPASS FCV 2-FCV-67-143-A (0.13HP)	N/A	N/A	N/A	N/A	92.44	Pass	Att. 5 / Acceptable Margin
240-16E	RHR Hx A-A Outlet Vlv 2-FCV-70-156-A (0.33HP)	N/A	N/A	N/A	N/A	89.63	Pass	Att. 5 / Acceptable Margin

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Appendix A

2A Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit) Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
		SI Phase A DBE Actuation	SI Phase B DBE Actuation	Individual Motor Start	Minimum Required Voltage		Bases for Minimum Required Voltage	
					Terminal Voltage (%)	Terminal Voltage (%)		
ETAP Bus ID/ Compt No	Load Description	6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V	Base
240-17A	Sample Hx Hdr Outlet Vlv 2-FCV-70-183-A (0.13HP)	N/A	N/A	N/A	N/A	90.15	Pass	Att. 5 / Acceptable Margin
240-17E	480V BD RM 2A A/C CPRSR 2A-A 2-MTR-31-465-A (50HP)	N/A	N/A	N/A	N/A	91.53	85	Att. 1
240-2A	ERCW Hdr A Isln Vlv 2-FCV-3-116A-A (0.25HP)	N/A	N/A	N/A	N/A	91.06	Pass	Att. 5 / Acceptable Margin
240-2B	ERCW Hdr A Isln Vlv 2-FCV-3-116B-A (0.25HP)	N/A	N/A	N/A	N/A	90.94	Pass	Att. 5 / Acceptable Margin
240-2D	AFWP Turb Stm Sup Fm Stm Gen 1 2-FCV-1-15-A (1HP)	N/A	N/A	N/A	N/A	91.38	Pass	Att. 5 / Acceptable Margin
240-3A	ERCW Hdr A Isln Vlv 2-FCV-3-136A-A (0.33HP)	N/A	N/A	N/A	N/A	90.06	Pass	Att. 5 / Acceptable Margin
240-3B	ERCW Hdr A Isln Vlv 2-FCV-3-136B-A (0.33HP)	N/A	N/A	N/A	N/A	90.07	Pass	Att. 5 / Acceptable Margin
240-5A	Sample Hx Isln Vlv 2-FCV-70-215-A (0.13HP)	N/A	N/A	N/A	N/A	90.31	Pass	Att. 5 / Acceptable Margin
240-5E	Cntrmt Spray Hx 2A Sup Cont Vlv 2-FCV-67-125-A (0.33HP)	N/A	N/A	N/A	N/A	91.49	Pass	Att. 5 / Acceptable Margin
240-5F	Cntrmt Spray Hx 2A Disch Vlv 2-FCV-67-126-A (0.33HP)	N/A	N/A	N/A	N/A	91.49	Pass	Att. 5 / Acceptable Margin
240-6A	AFWP Turb Stm Sup Fm Stm Gen 4 2-FCV-1-16-A (1HP)	N/A	N/A	N/A	N/A	91.37	Pass	Att. 5 / Acceptable Margin

* This MOV terminal voltage is calculated taking credit for the hammer blow feature.

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Appendix A

2B Boards

EVALUATION OF CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit) Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts							
		SI Phase A DBE Actuation	SI Phase B DBE Actuation	Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage	
		Terminal Voltage (%)		Terminal Voltage (%)			
ETAP Bus ID/ Compt No	Load Description	6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base
6.9kV Shutdown Board 2B-B							
15-10 AFW	Aux Feedwater PMP 2B-B 2-MTR-3-128-B (600 HP)	99.11	Starts	99.11	Starts	99.09	85
15-13 CSP	CNT/MT SPRAY PMP 2B-B 2-MTR-72-10-B (700 HP)	N/A	Not Running	98.93	Starts	98.93	80
15-14 RHR	RHR PUMP 2B-B 2-MTR-74-20-B (400 HP)	99.03	Starts	99.03	Starts	99.03	80
15-15 SI	SAFETY INJ PMP 2B-B 2-MTR-63-15-B (400 HP)	99.05	Starts	99.05	Starts	99.05	80
15-18 CCP	CNT/FL CHRG PMP 2B-B 2-MTR-62-104-B (600 HP)	99.00	Starts	99.00	Starts	98.99	80
15-8 ERCW	ERCW PMP H-B 0-MTR-67-59-B (800 HP)	N/A	Starts (H-B or G-B start, but not both, other is not running)	N/A	Starts (H-B or G-B start, but not both, other is not running)	96.05	90
15-9 ERCW	ERCW PMP G-B 0-MTR-67-55-B (800 HP)	96.72	Starts (H-B or G-B start, but not both, other is not running)	96.72	Starts (H-B or G-B start, but not both, other is not running)	6.66	90
480V Shutdown Board 2B1-B							
137-3C	Cmplt Clg Sys Pmp 2B-B 2-MTR-70-33-B (350 hp)	81.40 (8s)	Starts	81.79 (8s)	Starts	81.19	70
138-7A	Elec Bd Rm AHU D-B 0-MTR-31-31D-B (50 hp)	N/A	Running	N/A	Running	85.53	80
138-7B	Spent Fuel Pit Pmp C-S ALT FDR 0-MTR-78-35-S (100 hp)	N/A	Running	N/A	Running	85.82	80
138-7D	Reac Lwr Compt Clr Fan 2B-B 2-MTR-30-75-B (60 hp)	N/A	Running	N/A	Trips	83.93	80
480V Shutdown Board 2B2-A							
139-2B	Elect Bd rm A/C B-B Cprsr 0-MTR-31-129/2-B (250 hp)	N/A	Running	N/A	Running	86.53	85
139-2D	Cmplt Clg Sys Pmp C-S 0-MTR-70-51-S (350 hp)	N/A	Running	N/A	Running	69.99 (SIB)	70
140-7D	Reac Lwr Compt Clr Fan 2D-B 2-MTR-30-78-B (60 hp)	N/A	Running	N/A	Trips	86.42	80
140-9C	Cnmt Air Rtn Fan 2B-B 2-MTR-30-39-B (100 hp)	N/A	Not Running Starts @ 9 Min	N/A	Not Running Starts @ 9 Min	84.87	80
140-9D	480V Shutdown Bd Rm AHU D-B 0-MTR-31-61-B (75 hp)	N/A	Running	N/A	Running	88.06	85
480V CA Vent Board 2B1-B							
209-2A	Aux Cont Air Cprsr B-B 0-MTR-32-86-B (20 hp)	N/A	Not Running	N/A	Not Running	84.56	80
209-2C	Pen Rm El713 Clr Fan 2B-B 2-MTR-30-197-B (3 hp)	87.20	Starts on ABI	88.00	Starts on ABI	91.06	80
209-3B	Pipe Chase Clr Fan 2B-B 2-MTR-30-202-B (3 hp)	87.25	Starts on ABI	88.06	Starts on ABI	91.11	80
209-3C	Cntrm Spray Pmp 2B-B Rm Clr Fan 2-MTR-30-178-B (7.5 hp)	83.48	Random	84.25	Starts on Pump Start	86.17	80

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Appendix A

2B Boards

EVALUATION OF CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit) Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts							
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%)
ETAP Bus ID/ Compt No	Load Description	6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V
209-3D	Aux Bldg Gas Trtmt Sys Fan B-B 2-MTR-30-157-B (50 hp)	82.90	Starts on ABI	83.66	Starts on ABI	88.68	80
209-4A	BATTERY RIM EL 692 EXH FAN C-B 0-MTR-31-27-B (2 hp)	N/A	Running	N/A	Running	89.95	85
209-5E	AFWP&BA XFR PMP SP CLR FAN B-B 2-MTR-30-185-B (15 hp)	87.24	Starts on ABI	88.05	Starts on ABI	88.81	80
209-6B	ERCW Str 2B-B 2-MTR-67-10-B (3 hp)	N/A	Running	N/A	Running	77.30	75
209-6C	Traveling Scrn 2B-B 2-MTR-67-10-B (5 hp)	N/A	Running	N/A	Running	81.68	80
209-7B	125V Vit Bat Rm IV ExFan 2A2-B 2-MTR-31-288-B (0.33 hp)	N/A	Running	N/A	Running	92.11	85
209-7D	RHR Pmp 2B-B Inlet FCV 2-FCV-74-21-B (5.2 hp)	N/A	Not Running	N/A	Not Running	93.70	Pass
209-8A	Safety Inj Pmp 2B-B Rm Clr Fan 2-MTR-30-179-B (5 hp)	84.79	Starts on Pump Start	85.58	Starts on Pump Start	87.41	80
209-8B	Pen Rm El 692 Clr Fan 2B-B 2-MTR-30-187-B (3 hp)	86.61	Starts on ABI	87.41	Starts on ABI	89.49	80
209-8C	Shtdn Xfrm Rm 2B Exh Fan 2B2-B 2-MTR-30-246G-B (3 hp)	N/A	Running	N/A	Running	91.83	80
209-8D	Shtdn Xfrm Rm 2B Exh Fan 2B3-B 2-MTR-30-246H-B (3 hp)	N/A	Running	N/A	Running	92.14	80
209-8E	C.Bldg Ele BdRm AC Clr Pmp B-B 0-MTR-31-129/1-B (20 hp)	N/A	Running	N/A	Running	88.44	85
209-8F1	EL BD RM A/C B-B CONTROL/O.PMP 0-MTR-31-129/3-B (3 hp)	N/A	Running	N/A	Running	92.33	85
209-9A	RHR Pmp 2B-B Rm Clr Fan 2-MTR-30-176-B (5 hp)	81.19	Starts on Pump Start	81.94	Starts on Pump Start	82.53	80
209-9C	480V Bd Rm 2A Pr Sup Fan 2A2-B 2-MTR-31-463-B (3 hp)	N/A	Running	N/A	Running	92.84	85
209-9D	Shtdn Xfrm Rm 2B Exh Fan 2B1-B 2-MTR-30-246F-B (3 hp)	N/A	Running	N/A	Running	92.45	80
209-9E	Pen Rm El 737 Clr Fan 2B-B 2-MTR-30-195-B (3 hp)	87.63	Starts on ABI	88.43	Starts on ABI	91.70	80
209-10A	Cnfg Chrg Pmp 2B-B Rm Clr Fan 2-MTR-30-182-B (5 hp)	86.12	Starts on Pump Start	86.91	Starts on Pump Start	89.04	80
209-10B	480V Bd Rm 2B Pr Sup Fan 2B2-B 2-MTR-31-477-B (3 hp)	N/A	Running	N/A	Running	93.15	85
209-10C	125V Vit BatRm III ExFan 2B2-B 2-MTR-31-286-B (0.33 hp)	N/A	Running	N/A	Running	91.90	85
209-10F1	Cont Rm Intake Mon O-RE-90-126-B (0.75 hp)	N/A	Running	N/A	Running	93.11	85
209-11B	480V Bd Rm 2B A/C cond 2B-B 2-MTR-31-475-B (20 hp)	N/A	Running	N/A	Running	90.81	85
209-11C	480V Bd Rm 2B A/C Ahu 2B-B 2-MTR-31-289-B (20 hp)	N/A	Running	N/A	Running	90.23	85
209-12B	EG Trtmt Sys B-B Rm Clr Fan 2-MTR-30-207-B (3 hp)	87.39	Starts on ABI	88.20	Starts on ABI	91.70	80
209-13D	ERCW Scrn Wash Pmp 2B-B 2-MTR-67-447-B (40 hp)	N/A	N/A	N/A	N/A	74.69	75
209-7E	RWST To Spray Hdr 2B FCV 2-FCV-72-21-B (3.3 hp)	N/A	Not Running	N/A	Not Running	87.70	Pass
209-6E	ERCW Str 2B-B Flush Vlv 2-FCV-67-10B-B (0.33HP)	N/A	N/A	N/A	N/A	83.36	80
209-4E	ERCW Str 2B-B Backwash Vlv 2-FCV-67-10A-B (0.33HP)	N/A	N/A	N/A	N/A	83.62	80

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Appendix A

2B Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit) Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
		SI Phase A	SI Phase B			Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		DBE Actuation	DBE Actuation			Terminal Voltage (%)	Terminal Voltage (%)	
ETAP Bus ID/ Compt No	Load Description	6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base	Reference
480V CA Vent Board 2B2-B								
None								
480V Diesel Aux Board 2B1-B								
223-2B	DG 2B-B RM EXH FAN 1B 2-MTR-30-450-B (15 hp)	92.48	Starts	92.88	Start	94.64	85	Att. 3
223-2D	DG 2B-B Lube Oil Circ Pmp 1 2-MTR-82-81-B (1 hp)	N/A	Running	N/A	Running	95.14	85	Att. 1
223-3A	EM DG ENG SUP VLV FROM HDR 1B 2-FCV-67-67-B (0.13hp)	82.55	Open on Diesel Start	82.90	Open on Diesel Start	86.33	Pass	Att. 5
223-3D	DG 2B-B DAY TNK FO XFR PMP 1 2-MTR-18-55/4-B (1 hp)	92.31	Random	92.71	Random	95.03	85	Att. 1
223-4D	DG Rm 2B-B Pnl Vent Fan 2-MTR-30-494-B (15 hp)	N/A	Running	N/A	Running	92.52	85	Att. 3
223-4E	DG 2B-B 480V Elec Bd Rm Ex Fan 2-MTR-30-462-B (2 hp)	N/A	Running	N/A	Running	94.63	85	Att. 1
223-6A	Dg 2B-B Muffler Rm Exh Fan 2-MTR-30-466 (0.5HP)	92.72	Starts	93.11	Starts	95.56	85	Att. 3
480V Diesel Aux Board 2B2-B								
224-2A	DG 2B-B Aux LubeOil Circ Pmp B 2-MTR-82-ACPB2B (0.75 hp)	N/A	Running	N/A	Running	94.71	85	Att. 1
224-2B	DG 2B-B RM EXH FAN 2-B 2-MTR-30-454-B (15 hp)	92.76	Starts	92.99	Starts	93.13	85	Att. 3
224-2D	DG 2B-B Lube Oil circ Pmp 2 2-MTR-82-82-B (1 hp)	N/A	Running	N/A	Running	94.83	85	Att. 1
224-3D	DG 2B-B DAY TNK FO XFR PMP 2 2-MTR-18-54/4-B (1 hp)	92.53	Random	92.76	Random	94.80	85	Att. 1
480V RMOV Board 2B1-B								
241-17D	AFW Pmp B-B Lube Oil Pmp B-B 2-MTR-3-128D-B (0.25 hp)	N/A	Running	N/A	Running	88.48	85	Att. 1
241-3F2	SIS Accum Tank Flow Isol Vlv 2-FCV-63-98-B (19.5 hp)	N/A	Not Running	N/A	Not Running	86.66	Pass	Att. 5 / Acceptable Margin
241-5A	HPFP Sys Low Level Intake Vlv 0-FCV-26-8-B (0.13 hp)	N/A	Not Running	N/A	Not Running	80.91	80	Att. 1
241-5E	RCS Press Relief FCV 2-FCV-68-332-B (2 hp)	N/A	Not Running	N/A	Not Running	84.25	Pass	Att. 5 / Acceptable Margin
241-6D	Seal Flow Ret Isln Vlv 2-FCV-62-61-B (1.9 hp)	82.53	Closes on Ph A (Starts)	83.24	Not Running	87.63	Pass	Att. 5 / Acceptable Margin
241-7A	CHRG FLOW ISLN VLV 2-FCV-62-91-B (1.9 hp)	86.71	Closes on SI	87.45	Closes on SI	92.06	Pass	Att. 5 / Acceptable Margin
241-8A	Vol Cont Tank Outlet Isln Vlv 2-LCV-62-133-B (1.9 hp)	81.30	Closes on SI	82.00	Closes on SI	86.25	Pass	Att. 5 / Acceptable Margin
241-8B	RWST TO CHRG PMP VALVE CONT 2-LCV-62-136-B (1.9 hp)	80.20	Opens on SI	80.89	Opens on SI	85.08	Pass	Att. 5 / Acceptable Margin
241-9B	RHR To RCS H.L. 1&3 Flow Iso V 2-FCV-63-172-B (2.6 hp)	N/A	Not Running	N/A	Not Running	80.97	Pass	Att. 5 / Acceptable Margin
241-9F	Cntrm spray Pmp 2B-B Recirc FCV 2-FCV-72-13-B (0.1 hp)	N/A	Not Running	N/A	Starts 10s after Phase B	89.77	Pass	Att. 5
241-10A	SIS 2B-B Dsh To RWST Shftf Vlv 2-FCV-63-4-B (0.66 hp)	N/A	Not Running	N/A	Not Running	89.02	Pass	Att. 5 / Acceptable Margin
241-10B	RWST To SIS Pump FCV 2-FCV-63-5-B (2 hp)	N/A	Not Running	N/A	Not Running	83.31	Pass	Att. 5 / Acceptable Margin
241-11A	SIS Pmp Inlet To CVCS Chrg Pmp 2-FCV-63-6-B (2 hp)	N/A	Not Running	N/A	Not Running	81.72	Pass	Att. 5 / Acceptable Margin

Appendix A

2B Boards

EVALUATION OF CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit) Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage (%)	
241-11B	RHR Hx B to SIS Pmp 2-FCV-63-11-B (2 hp)	N/A	Not Running	N/A	Not Running	87.60	Pass	Att. 5 / Acceptable Margin
241-11E	SIS Baror Inj Tank Shutoff Vlv 2-FCV-63-25-B (1.9 hp)	86.65	Closes on SI	87.40	Closes on SI	91.98	Pass	Att. 5 / Acceptable Margin
241-12B	SIS Pmp 2B-B Inlet Vlv 2-FCV-63-48-B (2 hp)	N/A	Not Running	N/A	Not Running	84.14	Pass	Att. 5 / Acceptable Margin
241-12D	Cntrmt Sump To RHR Pmp B-B 2-FCV-63-73-B (13.2 hp)	N/A	Open at 20 Min after SI	N/A	Open at 20 Min after SI	91.40	Pass	Att. 5 / Acceptable Margin
241-12E	SIS To RCS Loops 1 & 4 FCV 2-FCV-63-94-B (1.6 hp)	N/A	Not Running	N/A	Not Running	92.80	Pass	Att. 5 / Acceptable Margin
241-13A	SIS Pmp 2B-B Outlet FCV 2-FCV-63-153-B (2 hp)	N/A	Not Running	N/A	Not Running	85.71	Pass	Att. 5 / Acceptable Margin
241-13B	SIS pmp Out RCS Lp 2&4 Hot Leg 2-FCV-63-157-B (2 hp)	N/A	Not Running	N/A	Not Running	88.35	Pass	Att. 5 / Acceptable Margin
241-13D	SIS 2B-B Dsh to RWST Shtrff Vlv 2-FCV-63-175-B (0.66 hp)	N/A	Not Running	N/A	Not Running	89.50	Pass	Att. 5 / Acceptable Margin
241-14A	Cntrmt Spray Hdr 2B Isln Vlv 2-FCV-72-2-B (3.2 hp)	N/A	Not Running	85.96	Open on Phase B	90.37	Pass	Att. 5 / Acceptable Margin
241-14D	RHR SPRAY HDR 2B ISOL VLV 2-FCV-72-41-B (2 hp)	N/A	Not Running	N/A	Not Running	88.15	Pass	Att. 5 / Acceptable Margin
241-14E	Cntrmt Sump To Spray Hdr 2B FCV 2-FCV-72-45-B (3.3 hp)	N/A	Not Running	N/A	Not Running	82.22	Pass	Att. 5 / Acceptable Margin
241-15B	RHR Pmp 2B-B Min Flow Vlv 2-FCV-74-24-B (0.1 hp)	85.18	Start on RHR pump start on SI	85.91	Start on RHR pump start on SI	90.53	Pass	Att. 5 / Acceptable Margin
241-15D	RHR Hx 2B Bypass Vlv 2-FCV-74-35-B (2 hp)	N/A	Not Running	N/A	Not Running	79.68	Pass	Att. 5 / Acceptable Margin
480V RMOV Board 2B2-B								
242-18D	480V Bd Rm 2B A/C Cprsr 2B-B 2-MTR-31-447-B (75 hp)	N/A	Running	N/A	Running	90.83	85	Att. 1
242-2A	ERCW Hdr B Isln Vlv 2-FCV-3-126A-B (0.67 hp)	N/A	Not Running	N/A	Not Running	89.82	Pass	Att. 5 / Acceptable Margin
242-2B	ERCW Hdr B Isln Vlv 2-FCV-3-126B-B (0.67 hp)	N/A	Not Running	N/A	Not Running	89.81	Pass	Att. 5 / Acceptable Margin
242-2E	St Flow To AFWP Turb Isln Vlv 2-FCV-1-18-B (1 hp)	N/A	Running	N/A	Running	91.06	Pass	Att. 5 / Acceptable Margin
242-3A	ERCW Hdr B Isln Vlv 2-FCV-3-179A-B (0.33 hp)	N/A	Random	N/A	Random	90.39	Pass	Att. 5 / Acceptable Margin
242-3B	ERCW Hdr B Isln Vlv 2-FCV-3-179B-B (0.33 hp)	N/A	Random	N/A	Random	90.20	Pass	Att. 5 / Acceptable Margin
242-3D	St Gen No 2 FW Isln Vlv 2-FCV-3-47-B (39.4 hp)	85.16	Use 89-10 start	85.41	Use 89-10 start	87.81	Pass	Att. 5
242-4D	St Gen No 4 FW Isln Vlv 2-FCV-3-100-B (39.4 hp)	86.16	Use 89-10 start	86.41	Use 89-10 start	88.83	Pass	Att. 5
242-5C	LWR CNTMT 2A CLRS SUP ISLN VLV 2-FCV-67-113B (0.3 hp)	N/A	Not Running	88.43	Closes (Starts)	91.99	Pass	Att. 5
242-5E	Cntrmt Spray Hx 2B Sup Cont Vlv 2-FCV-67-123-B (0.33 hp)	N/A	Not Running	N/A	Not Running	91.41	Pass	Att. 5 / Acceptable Margin
242-5F	Cntrmt Spray Hx 2B Sup Disch Vlv 2-FCV-67-124-B (0.33 hp)	N/A	Not Running	N/A	Not Running	91.00	Pass	Att. 5 / Acceptable Margin
242-6D	RCP Thrm Barr Rtn Cntrm Iso Vlv 2-FCV-70-87-B (0.7 hp)	N/A	Not Running	87.62	Closes (Starts)	91.14	Pass	Att. 5

Appendix A
2B Boards

EVALUATION OF CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit) Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A		SI Phase B		Individual Motor Start Terminal Voltage (%)	Minimum Required Voltage Terminal Voltage V(%)	Bases for Minimum Required Voltage
		DBE Actuation	Terminal Voltage (%)	DBE Actuation	Terminal Voltage (%)			
242-6E	RCP Thrm Barr Cntmt Isln Vlv 2-FCV-70-134-B (0.1 hp)	N/A	Not Running	87.60	Closes (Starts)	91.14	Pass	Att. 5
242-7D	Lwr Cntmt 2B Clr Dish Isln Vlv 2-FCV-67-103-B (0.1 hp)	N/A	Not Running	87.51	Closes (Starts)	91.04	Pass	Att. 5
242-7F	Up Cntm Vt Clr 2A Dish Iso Vlv 2-FCV-67-131-B (0.1 hp)	N/A	Not Running	87.18	Closes (Starts)	90.69	Pass	Att. 5
242-8D	Lwr Cntmt 2D Clr Dish Iso Vlv 2-FCV-67-111-B (0.1 hp)	N/A	Not Running	87.93	Closes (Starts)	91.48	Pass	Att. 5
242-8F	Up Cntm Vt Clr 2C dish Iso Vlv 2-FCV-67-134-B (0.1 hp)	N/A	Not Running	87.18	Closes (Starts)	85.63	Pass	Att. 5
242-9A	Lwr Cntm 2A Clr Dish Iso Vlv 2-FCV-67-88-B (0.3 hp)	N/A	Not Running	86.92	Closes (Starts)	90.43	Pass	Att. 5
242-9B	Lwr Cntm 2C Clr Dish Iso Vlv 2-FCV-67-96-B (0.3 hp)	N/A	Not Running	87.02	Closes (Starts)	90.53	Pass	Att. 5
242-9D	Up Cntm Vt Clr 2B Dish Iso Vlv 2-FCV-67-297-B (0.1 hp)	N/A	Not Running	86.19	Closes (Starts)	89.66	Pass	Att. 5
242-9F	Up Cntm Vt Clr 2B Sup Isln Vlv 2-FCV-67-138-B (0.1 hp)	N/A	Not Running	87.18	Closes (Starts)	90.69	Pass	Att. 5
242-10A	Lwr Cntmt 2B Clr Sply Isln Vlv 2-FCV-67-91-B (0.3 hp)	N/A	Not Running	86.93	Closes (Starts)	90.43	Pass	Att. 5
242-10B	Lwr Cntmt 2D Clr Sply Isln Vlv 2-FCV-67-83-B (0.3 hp)	N/A	Not Running	87.23	Closes (Starts)	90.75	Pass	Att. 5
242-10D	Up Cntm Vt Clr 2D Dish Iso Vlv 2-FCV-67-298-B (0.1 hp)	N/A	Not Running	86.87	Closes (Starts)	90.37	Pass	Att. 5
242-10F	Up Cntm Vt Clr 2D Sup Isln Vlv 2-FCV-67-141-B (0.1 hp)	N/A	Not Running	87.18	Closes (Starts)	90.69	Pass	Att. 5
242-11B	LWR CNTMT 2B CLRS SUP ISLN VLV 2-FCV-67-105-B (0.3 hp)	N/A	Not Running	88.09	Closes (Starts)	91.65	Pass	Att. 5
242-12B	CCS Hx C Disch Vlv To Hdr B 0-FCV-67-152-B (0.7 hp)	N/A	Running	N/A	Running	89.74	Pass	Att. 4
242-13D	RCP OIL CLR RTN CNTMT ISLN VLV 2-FCV-70-89-B (0.3 hp)	N/A	Not Running	88.11	Closes (Starts)	91.67	Pass	Att. 5
242-13F	RCP Oil Clr Hdr Cntmt Isln Vlv 2-FCV-70-140-B (0.3 hp)	N/A	Not Running	86.94	Closes (Starts)	90.45	Pass	Att. 5
242-17A	SPPCS Hx Sply Hdr Isln Vlv 0-FCV-70-194-B (0.33 hp)	N/A	Not Running	N/A	Not Running	92.18*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
242-15E	RHR Hx B-B Outlet Vlv 2-FCV-70-155-B (0.33 hp)	N/A	Not Running	N/A	Not Running	91.47	Pass	Att 5
480V Reactor Vent Board 2B-B								
None								

* This MOV terminal voltage is calculated taking credit for the hammer blow feature.

R2

Voltage Recovery Analysis for DBE

Purpose

The purpose of the attachment is to demonstrate that any possible voltage transient caused by motor starting during a DBE (SI with Phase A or Phase B isolation), including drop to the LOV setpoint, will also result in successful recovery above DVR reset within 5 seconds.

Approach

This transient voltage dip and recovery analysis is similar to that analyzed by the offsite power analysis (reference 2.2) which shows that the voltage recovers above the DVR reset within 5 seconds. However, the offsite power analysis credits the use of automatic load tap changers (LTC) for voltage recovery and also assumes minimum operable grid capacity. The offsite power analysis accounts for minimum operable grid capacity by using an extremely conservative technique of forcing the switchyard voltage to the minimum allowable post-event voltage. This technique ignores the voltage recovery that would occur once the larger motors accelerate.

In this analysis, the offsite power source has been modeled using a classical Thevenin equivalent impedance technique (fixed voltage source behind impedance). The impedance chosen is equivalent to that grid capacity that would result in the voltage at the 6.9kV Shutdown Boards dropping all the way to the loss of voltage (LOV) relay setpoint during initial DBE motor starting (block-start of ECCS loads).

Bases/Assumptions

- The offsite power LTCs (CSST C & D) are not allowed to correct the voltage during the motor starting event. However, they are allowed to adjust the voltage prior to the event. This is conservative because it will result in the worst-case voltage transient with no voltage recovery from the LTCs.
- The auxiliary power system is assumed to be in normal alignment prior to the event (Unit Boards and RCP Boards on USSTs, Common Boards on CSSTs A/B, Shutdown Boards on CSSTs C/D). This is conservative, because it puts the least amount of load on the offsite power source prior to the event and thereby results in a "stiffer" offsite power source impedance (i.e. less recovery). In addition, aligning the Shutdown Boards to CSSTs A/B would result in even greater recovery due to the Unit Board load shed feature.
- The 161kV Switchyard voltage is assumed to be at the minimum operable voltage prior to the event. This is conservative, because it will also result in a "stiffer" offsite power source impedance (i.e. less recovery).

Computations

Using the existing ETAP model used to perform offsite power analysis for two unit operation (Ref. 2.2), a dynamic motor starting analysis was performed for both SI-Phase A and SI-Phase B events on each unit. Using a trial and error technique, the switchyard source capacity (MVA_{sc}) was adjusted until the applicable 6.9kV Shutdown Board voltages just equaled the LOV setpoint (80% nominal) at $t=0+$ in the event being studied.

Each dynamic motor starting study case (SIA and SIB) was run for at least 5 seconds. The associated ETAP reports provide the voltage during the event in 0.1 second intervals for each 6.9kV Shutdown Board.

Results

A plot of the worst-case voltage recovery is shown for both U1 SIB and U2 SIB. The results show that in all cases the 6.9kV Shutdown Board voltage recovers above the DVR reset value (operational limit of 6681V) within 4 seconds.

Conclusions

This bounding analysis demonstrates that any possible voltage transient caused by DBE motor starting, including drop to the LOV setpoint, will also result in successful recovery above DVR reset within 5 seconds.

Project: Watts Bar Nuclear Plant
Location: //chachaapp5/etaps/wbnp/
Contract:
Engineer:

ETAP
7.0.0N
Study Case: U1 SIB-U2

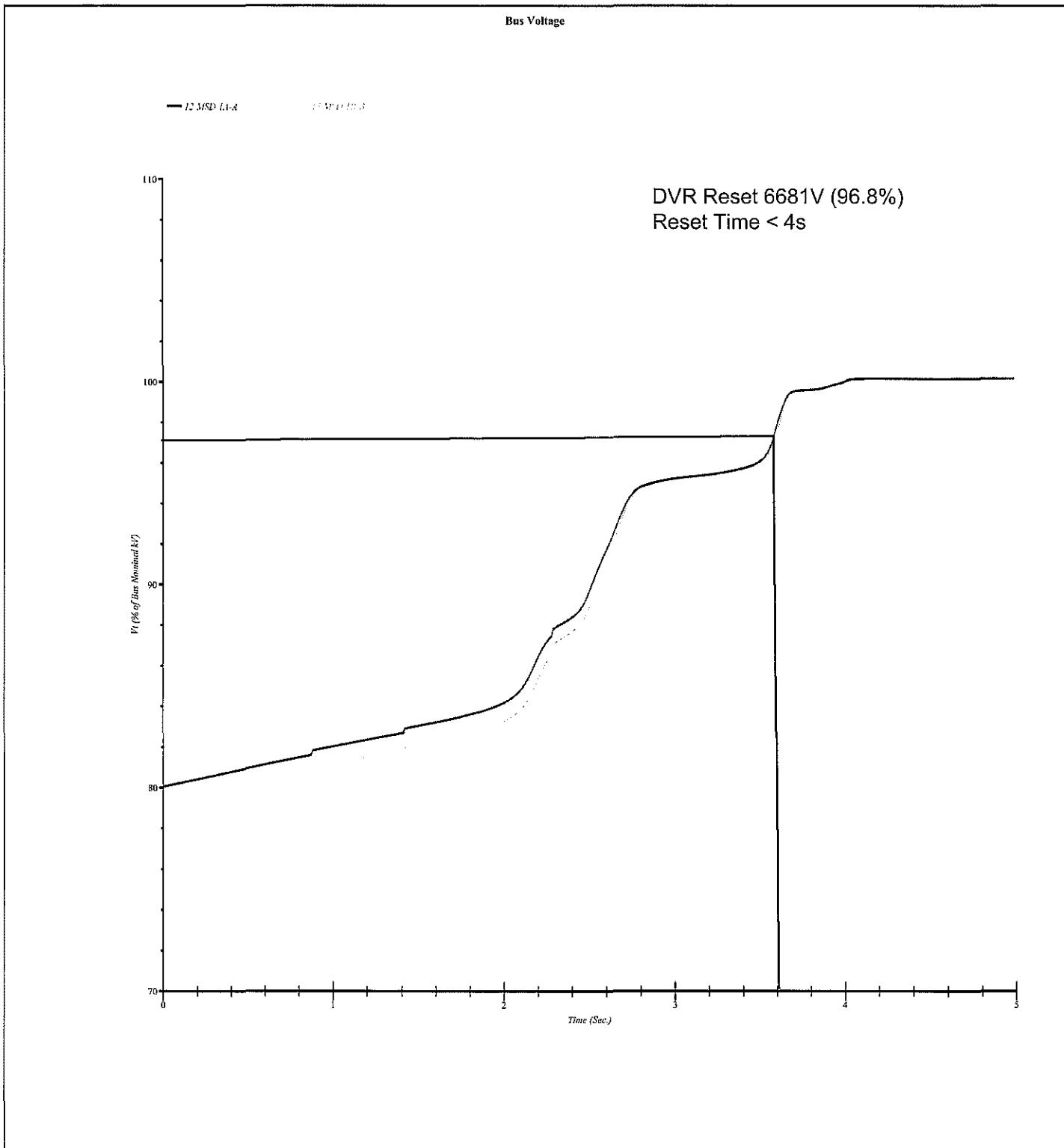
Date: 03-21-2012
SN: 90TVA12DC2
Revision: Unit 1&2
Config.: N 4 CSST-U2

WBN-EEB-MS-TI06-0029

Unit 1 SI Phase B. Plant in normal alignment (4CSSTs) at lowest operable grid (161kV). No LTC during the event.

Project File: J:\wbnp\R0 EDQ00099920120004 (DVR Analysis)\DVR Analysis WBN\ DVR LOV Recovery Analysis\WBNDATA
Output Report: U1SIB-152MVA

MOTOR STARTING ANALYSIS



Project: Watts Bar Nuclear Plant
Location: //chachaapp5/etaps/wbnp/
Contract:
Engineer:

ETAP
7.0.0N
Study Case: U1/2 SIA

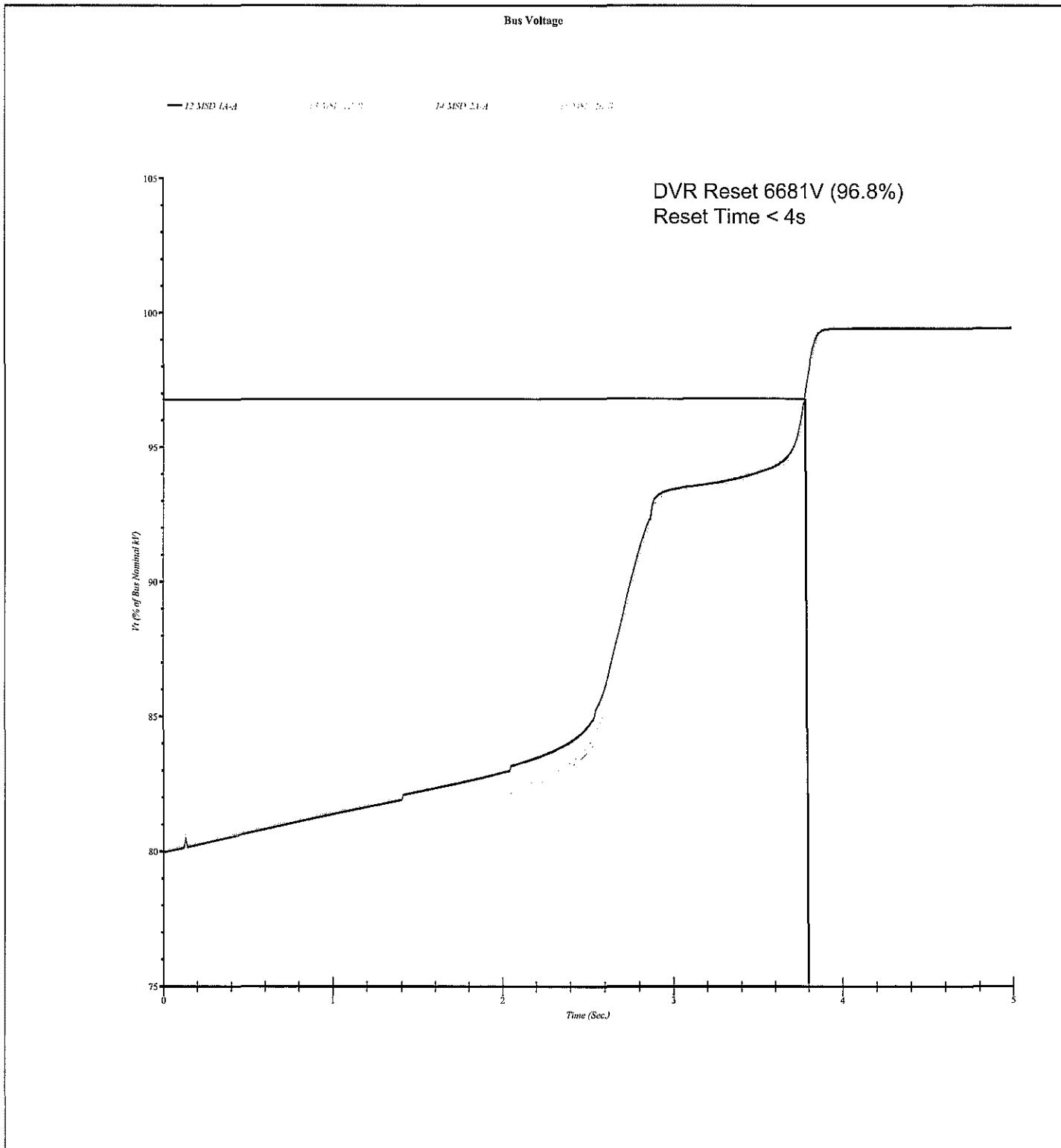
Date: 03-21-2012
SN: 90TVA12DC2
Revision: Unit 1&2
Config.: N 4 CSST-U2

WBN-EEB-MS-TI06-0029

Unit 1/2 SI Phase A. Plant in normal alignment (4CSSTs) at lowest operable grid (161kV). No LTC during the event.

Project File: J:\wbnp\R0 EDQ00099920120004 (DVR Analysis)\DVR Analysis WBN\ DVR LOV Recovery Analysis\WBNDATA
Output Report: U12-SIA

MOTOR STARTING ANALYSIS



Project: Watts Bar Nuclear Plant
Location: //chacbaapp5/etaps/wbnp/
Contract:
Engineer:

ETAP
7.0.0N
Study Case: U2 SIB-U2

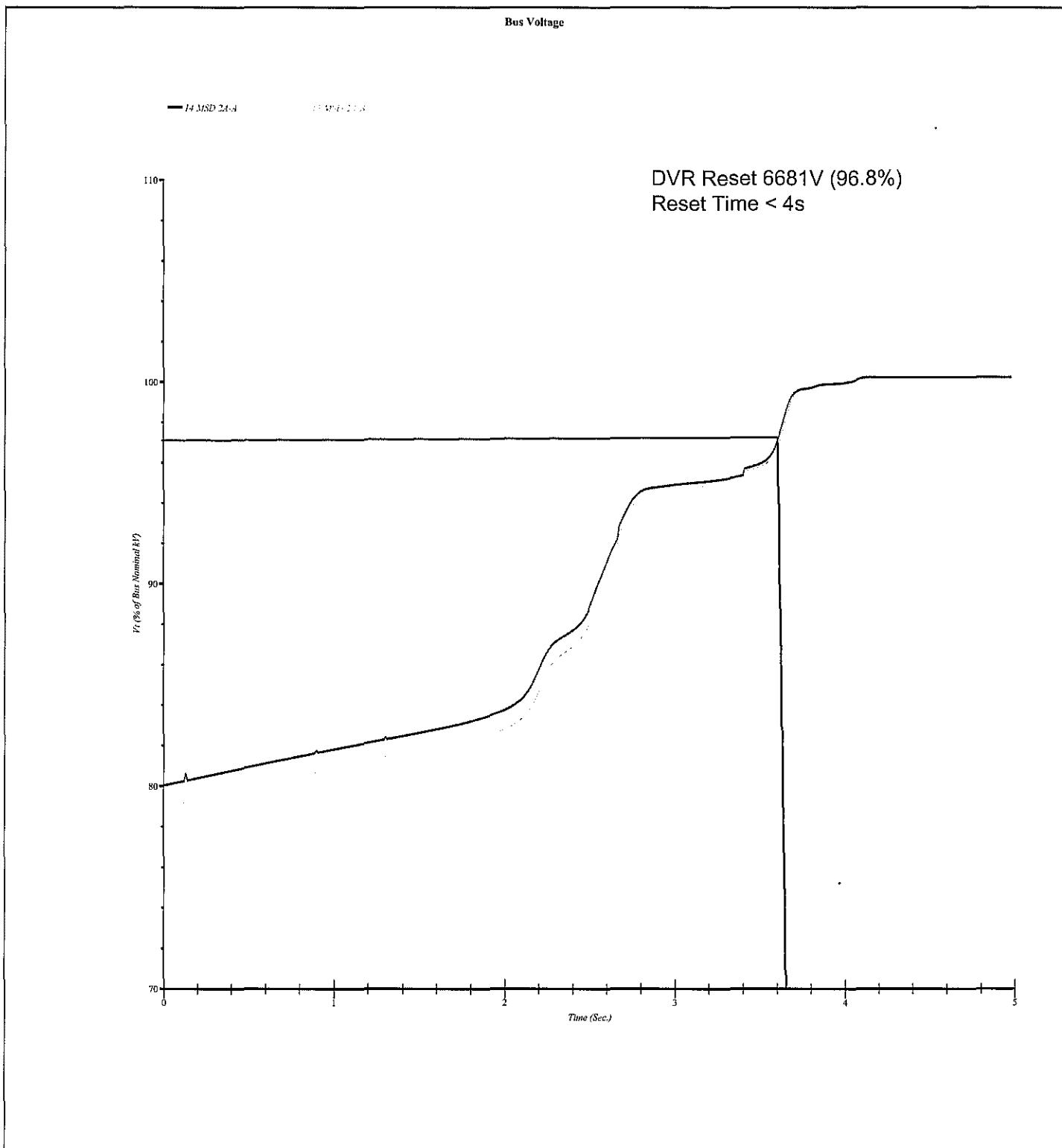
Date: 03-21-2012
SN: 90TVA12DC2
Revision: Unit 1&2
Config.: N 4 CSST-U2

WBN-EEB-MS-TI06-0029

Unit 2 SI Phase B. Plant in normal alignment (4CSSTs) at lowest operable grid (161kV). No LTC during the event.

Project File: J:\wbnp\R0 EDQ00099920120004 (DVR Analysis)\DVR Analysis WBN\ DVR LOV Recovery Analysis\WBNDATA
Output Report: U2SIB-152MVA

MOTOR STARTING ANALYSIS



Degraded Voltage Recovery Analysis for DBE

Purpose

The purpose of this appendix is to address NRC comments concerning the adequacy of the analytical methodology for the motor starting cases previously analyzed in this study to support DBE. The nature of the comments concerned the initial voltage used in the analysis at the DVR monitored bus and fell into two general areas:

1. Demonstrate the adequacy of the DVR protection scheme if the voltage source is placed at the switchyard bus and the grid voltage is set such that the DVR monitored bus voltage is at the DVR dropout analytical limit prior to the DBE initiation.
2. Demonstrate the adequacy of the DVR protection scheme if the voltage source is placed at the switchyard bus and both grid voltage and capacity are adjusted to any value that will support successful voltage recovery following DBE motor starting (i.e. Class 1E loads remain on offsite power).

Approach

This appendix follows a similar analytical technique as described in Appendix B. Additional study cases were set up to address the NRC comments as follows:

Study Case 1: The grid is set to strongest capacity (maximum short-circuit strength) and grid voltage is lowered until the DVR monitored bus voltage reaches the DVR analytical limit prior to DBE initiation. The outcome of this evaluation should demonstrate that the Class 1E bus voltage will not be able to successfully recover (i.e. reset the DVR) following the DBE initiation.

Study Case 2: Grid voltage and capacity are adjusted until the lowest possible initial voltage is found (at the DVR monitored bus) that allows successful recovery following DBE motor starting (i.e. the resulting voltage dip recovers from the Loss of Voltage relay (LOV) and also resets the DVR in a bounding fashion). The outcome of this evaluation should demonstrate that any combination of initial grid voltage and capacity that results in successful recovery of the Class 1E bus voltage does so because of the proper acceleration of the accident initiated motors on the 6.9kV 1E buses.

Analysis is performed for each study case using normal offsite power alignment via CSSTs C & D as well as alignment via CSSTs A & B (Shutdown Boards aligned to Start Buses via Unit Boards).

Bases/Assumptions

All the bases and assumptions listed in Appendix B of this study are applicable to this appendix. (Ref. Attachment 2 for relay setpoints)

Computations

The existing ETAP model from offsite power analysis for two unit operation (Ref. 2.2) was used to perform dynamic motor starting analyses similar to Appendix B. The analysis was performed considering a DBE for Unit 1 (SI with Phase B isolation). Detailed evaluation was performed for 6.9kV Shutdown Board 1A-A only (aligned to CSSTs A, B, C, or D) as the results are considered to be representative of the other Shutdown Boards for the purposes of these analyses.

Study Case 1:

- 1) The utility source model was placed on the 161kV switchyard bus.
- 2) The applicable CSST automatic load tap changers (LTC) were placed in manual (i.e. not working).

- 3) Using normal plant operation loading, the source voltage was lowered until the voltage at the DVR monitored bus (6.9kV Shutdown Board) was exactly at 6555V (DVR dropout analytical limit).
- 4) The source capacity was set to the maximum short-circuit strength (Ref PSO Study), which allows the greatest ability of the grid to recover the Class 1E bus voltage above the DVR reset value following DBE motor starting.

Study Case 2:

- 1) The utility source model was placed on the 161kV switchyard bus.
- 2) The applicable CSST automatic load tap changers (LTC) were placed in manual (i.e. not working).
- 3) Normal plant operation loading was used prior to the DBE initiation.
- 4) The source voltage and capacity were adjusted as required to achieve all of the following criteria:
 - a) voltage at the 6.9kV Shutdown Board is not lower than 6555V (DVR dropout analytical limit) prior to DBE initiation.
 - b) if the voltage dip produced by DBE initiation (at the 6.9kV Shutdown Board) drops below the LOV relay setpoint, it also recovers above the setpoint within the relay timeout (nominal settings used for convenience)
 - c) the voltage at the 6.9kV Shutdown Board recovers to (exactly) the DVR reset point following the initial "block start" transient (nominal setting used for convenience).

Each dynamic motor starting study case was run for 5 seconds. The associated ETAP results provide the voltage profile in percent in 0.01 second intervals at the 6.9kV Shutdown Board. These values were plotted to evaluate the results. The existing offsite power analysis voltage profile for the same DBE (minimum grid capability) were also added on the same plots for general comparison (see Figures 1 and 2 of this appendix).

The following study cases have been run:

<u>Study Case</u>	<u>ETAP Configuration</u>	<u>ETAP MS Case</u>	<u>ETAP Report Name</u>
1	NCSSTABD-U2	U1SIB-U2	DVR DO AB
1	N4 CSST-U2	U1SIB-U2	DVR DO CD
2	NCSSTABD-U2	U1SIB-U2	WC Grid AB
2	N4 CSST-U2	U1SIB-U2	WC Grid CD

Results

Based on the study cases the results are summarized below:

Study Case 1 -

Voltage at the DVR monitored bus is at DVR dropout with a strong grid capacity. The evaluation shows (Ref. Figure 1) without the load tap changer, the DVR will not reset and Class 1E buses will disconnect from offsite power and transfer to the DGs as designed. Transfer to DG is acceptable because previous protective device analysis shows the successful transfer to the onsite power supply with all required Class 1E loads achieving adequate voltage for starting and running within required time limits.

Study Case 2 -

Voltage at the DVR monitored bus is at the lowest possible initial voltage that allows successful recovery. This case, while not representative of any actual postulated grid, results in the worst conceivable grid that allows Class 1E buses to remain on offsite power. The evaluation shows (Ref Figure 2) the DVR recovery time is not significantly different than that shown for offsite power analysis (minimum qualified grid). This case demonstrates that any conceivable voltage transient caused by motor starting, even at the threshold of LOV timeout and DVR timeout, will result in recovery of voltage (DVR reset or above) within 4 seconds.

Conclusions

The outcomes of these additional requested analysis demonstrate the adequacy of the DVR protection scheme based on:

- 1) If the LOV relay times out
 - a. Class 1E buses disconnect from offsite power and transfer to the DGs
 - b. Based on previous analysis, Class 1E components have adequate voltage for starting and running within analyzed time limits
- 2) If the LOV relay does not time out, then either:
 - a. The DVR times out
 - i. Class 1E buses disconnect from off site power and transfer to the DGs
 - ii. Based on previous analyses, Class 1E components have adequate voltage for starting and running within analyzed time limits
 - OR
 - b. The DVR does not time out
 - i. Class 1E buses remain connected to off site power
 - ii. Based on previous analyses, Class 1E components have adequate voltage for starting and running within analyzed time limits

DVR at Dropout Prior to LOCA, Shdn Bd 1A-A, U1 SIB

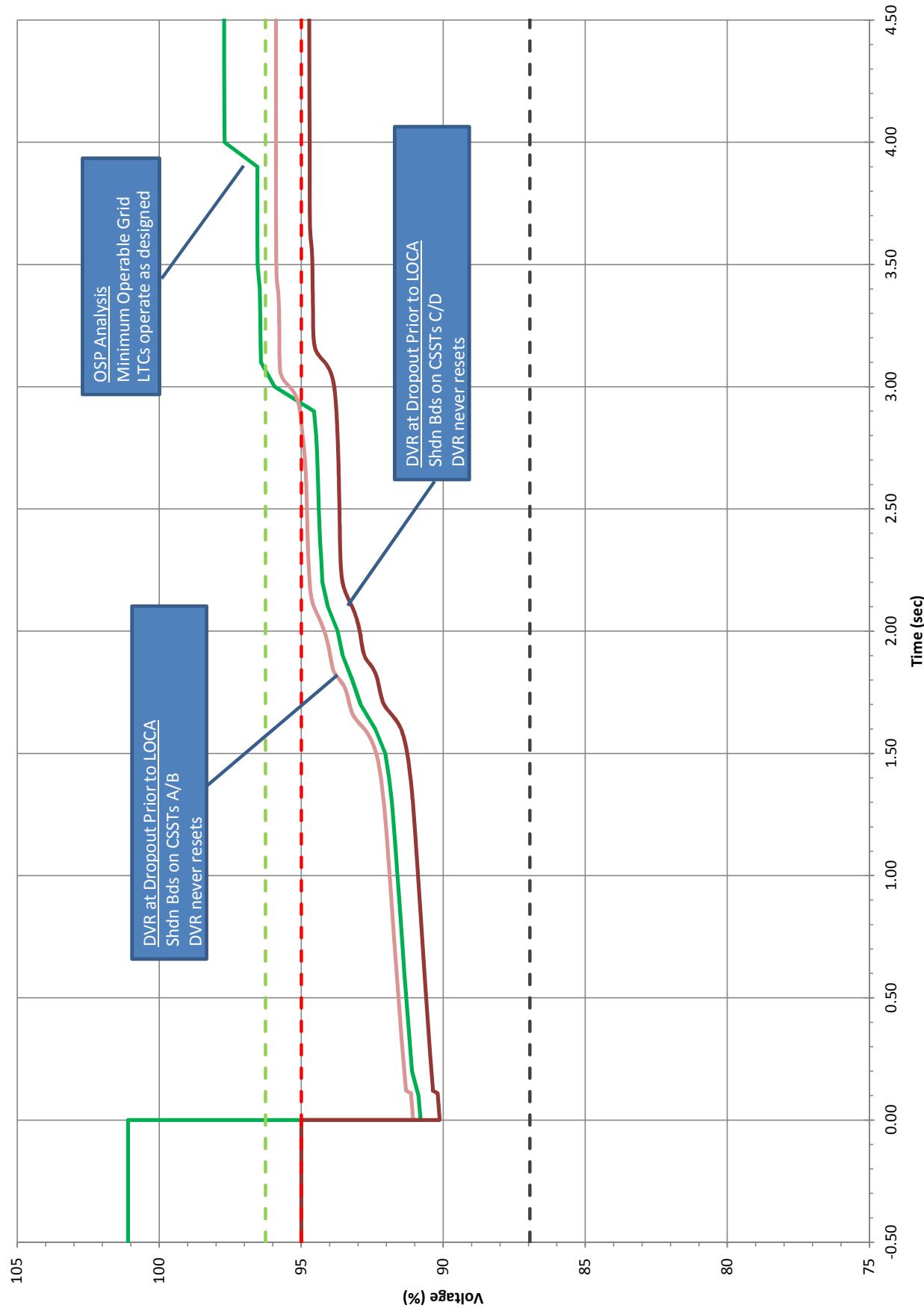


FIGURE 1
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Worst-Case Grid that Recovers, Shdn Bd 1A-A, U1 SIB

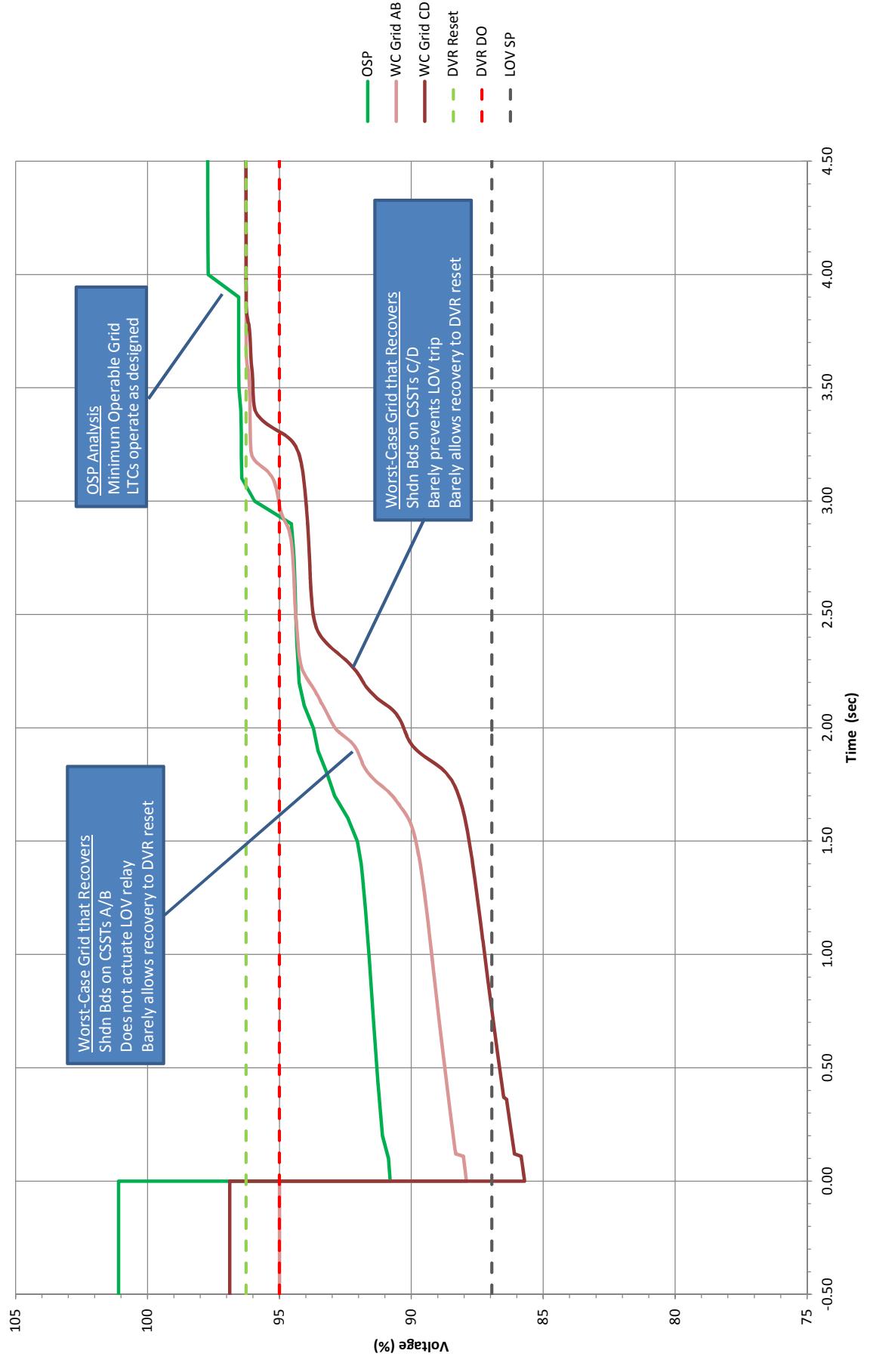


FIGURE 2
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CALCULATION SHEET

CALC NUMBER: WBN-EEB-EDQ000-999-2007-0002

REV. NO 20

SHEET NO. 11

3.0 DESIGN INPUT DATA & REQUIREMENTS

The evaluation documented in this calculation was previously performed and documented in the following calculations:

WBN EEB-MS-TI05-0001, Auxiliary Power System Database (TELAS)
WBN EEB-MS-TI06-0002, Auxiliary Power System Analysis (ELMS-NON1E),
WBN EEB-MS-TI06-0010, Auxiliary Power System Analysis on 1E Buses (ELMS-1E).

The design input data identified in these calculations are still valid and will not be repeated here. Only new and significant design input data will be identified here.

3.1 "WBN ETAP CONVERSION, Phase 1 - database Conversion", RIMS B43 990303 001

3.2 Not used

3.3 Acceptable Voltage Ranges

3.3.1 Steady State Board Voltages

6.9kV Switchgear 480V Switchgear/MCCs

Max:	7260V (2)	508V (2)
Min:	6681V (1)	440V (2)

- (1) This is the reset operational limit for the degraded voltage relay (Sec. 3.12).
(2) Per Table 1 of ANSI C84.1 (Ref. 2.23), Utilization Voltage Range B.

3.3.2 Minimum Operating Voltages

Running Motors

6.6kV** 460V*

Max:	7260V	506V
Min:	5940V	414V

480V Static Loads

Max: 528V
Min: 432V (this voltage is conservative compared to the Range B utilization voltage of 424V in Ref. 2.23)

* NEMA MG1 Section 12.45 requires that motors shall operate with variation in voltage up to plus or minus 10% of rated voltage (Reference 2.24).

** Ref. 2.23, Utilization Voltage Range B.

3.3.3 Minimum Motor Starting Voltages

<u>6.6kV Motors</u>	<u>460V Motors</u>	<u>460V Air Comp</u>	<u>89-10 MOVs</u>	<u>Non 89-10 MOVs</u>
5280 (80%)***	391V (85%)**	368V (80%)**	Att. 11.5	368V (80%)**

** Percentages are based on 460V rated motor voltage. For motors rated other than 460V the same percentages are applicable. The minimum starting voltage for these motors may be different from the above voltage if it is based on manufacturer's data or test reports per Att. 11.4.

*** 80% for all motors except the for ERCW Pump motor which requires 90% and Aux Feedwater Pump motor which requires 85%. See Attachment 11.4 for motor starting voltage.

The minimum motor voltages for LV motors are based on the following:

Class 1E motors up to 30HP, NEMA Type B, provide 150 percent starting torque at full voltage which corresponds to close to 100 percent torque at 80 percent voltage (Ref. 2.24). For loads, such as fans, as the speed increases, so does the torque requirement. Other loads such as positive-displacement compressors start unloaded and do not require a

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Figure 8.3

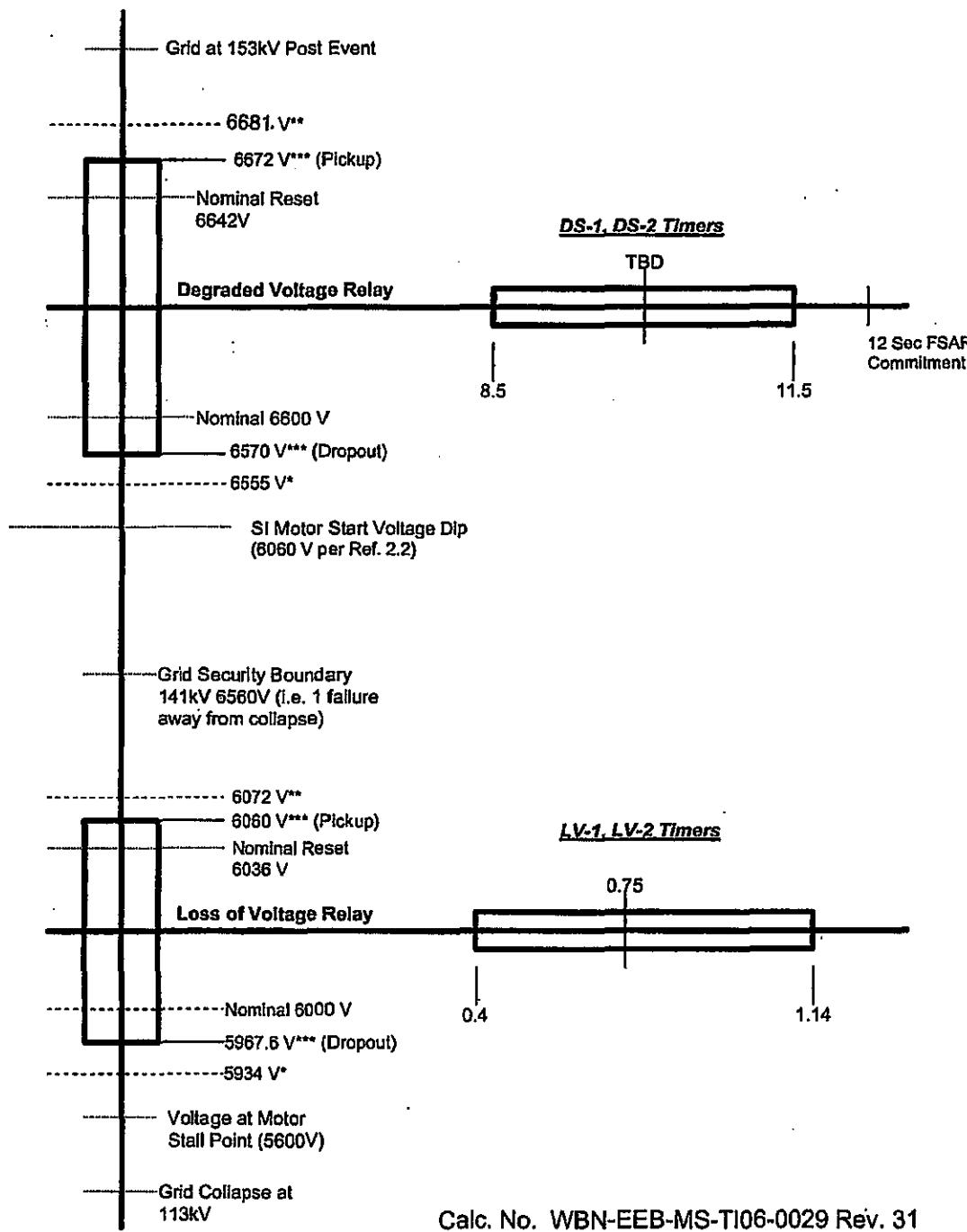


Figure 8.3 - Degraded Voltage and Loss-of-Voltage Relay Setpoint

* Analytical Limit (Ref. 2.20)

** Operational Limit (Ref. 2.20)

*** Allowable Value (Excludes PT accuracy - Ref. 2.16)

This page replaced by R20

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Attachment 3
Required Motor Starting Voltage
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Attachment 10.5

Block Motor Start Data

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ATTACHMENT 10.5 - BLOCK MOTOR START DATA

MOTOR NO.	BOARD NAME	COPP	MOTOR NAME	HP	FLI	LPA	LRPF	MOTOR Z#	MOTOR R#	MOTOR J#	CABLE NO.	CABLE SIZE	CABLE LENGTH	CABLE R	CABLE JI	TOL NO.	TOL R	TOTAL R	TOTAL JK	MIN VOLT SEC	ACCEL (X)	START TIME	VOLTAGE	REV
* 2	6.9KV SHDTN BD 1A-A	13	CNTMT SPRAY PMP 1A-A	700.00	52.58	294.0	0.33	12.9609	4.2771	12.2349	1PP625A	3-IC #2/0	630	0.1085	0.0780			0.0684	0.0491	80	3.30	5308.1		
* 3	6.9KV SHDTN BD 1A-A	14	RHR PMP 1A-A	400.00	30.00	187.5	0.33	20.3227	6.6252	19.2125	1PP575A	3-IC #2/0	663	0.1085	0.0780			0.0719	0.0517	80	3.60	5298.8		
* 4	6.9KV SHDTN BD 1A-A	15	SAFETY INJ PMP 1A-A	400.00	31.00	219.0	0.30	17.3996	5.2199	16.5982	1PP600A	3-IC #2/0	518	0.1085	0.0780			0.0671	0.0482	80	4.00	5300.1		
* 5	6.9KV SHDTN BD 1A-A	8	ERCW PMP A-B	800.00	63.00	344.0	0.19	11.0771	2.1046	10.8753	1PP675A	3-IC #2/0	3338	0.1085	0.0780			0.3622	0.2604	80	3.60	5116.2		
* 6	6.9KV SHDTN BD 1A-A	10	AUX FEEDWTR PMP 1A-A	500.00	49.50	300.0	0.20	12.7017	2.5463	12.4451	1PP650A	3-IC #2/0	339	0.1085	0.0780			0.0358	0.0257	85	6.60	5624.3		
* 7	6.9KV SHDTN BD 1A-A	18	CNTFGL CHRG PMP 1A-A	500.00	45.00	289.7	0.33	14.1287	4.9450	13.2351	1PP550A	3-IC #2/0	531	0.1085	0.0780			0.0576	0.0414	80	4.55	5302.1		
* 8	6.9KV SHDTN BD 1B-B	14	RHR PMP 1B-B	400.00	30.00	187.5	0.33	20.3227	6.6252	19.2125	1PP587B	3-IC #2/0	376	0.1085	0.0780			0.0408	0.0293	80	3.60	5290.7		
* 9	6.9KV SHDTN BD 1B-B	15	SAFETY INJ PMP 1B-B	400.00	31.00	219.0	0.30	17.3996	5.2199	16.5982	1PP612B	3-IC #2/0	780	0.1085	0.0780			0.0845	0.0608	80	4.00	5305.4		
* 10	6.9KV SHDTN BD 1B-B	18	CNTFGL CHRG PMP 1B-B	600.00	45.00	269.7	0.35	14.1287	4.9450	13.2351	1PP552B	3-IC #2/0	598	0.1085	0.0780			0.0757	0.0544	80	4.65	5309.0		
* 11	6.9KV SHDTN BD 1B-B	8	ERCW PMP F-B	800.00	63.00	344.0	0.19	11.0771	2.1046	10.8753	1PP700B	3-IC #2/0	3639	0.1085	0.0780			0.3948	0.2838	80	3.60	6132.3		
* 12	6.9KV SHDTN BD 1B-B	10	AUX FEEDWTR PMP 1B-B	500.00	49.50	300.0	0.20	12.7017	2.5463	12.4451	1PP652B	3-IC #2/0	446	0.1085	0.0780			0.0484	0.0348	85	6.60	5629.4		
* 13	6.9KV SHDTN BD 1B-B	8	CNTMT SPRAY PMP 1B-B	700.00	52.58	294.0	0.33	12.9609	4.2771	12.2349	1PP637B	3-IC #2/0	756	0.1085	0.0780			0.0820	0.0590	80	3.30	5313.8		
* 14	480V RI MOV BD 1A1-A	3200	3B CPMNT CLS SVS PMP 1A-A	350.00	389.00	2084.0	0.30	0.1274	0.0392	0.1216	1PL4725A	3-IC #500	675	0.0314	0.0540			0.0106	0.0182	70	3.10	374.1		
44	480V RI MOV BD 1A1-A	18E	RCP SPRAY ISLN VLV	0.67	2.10	10.5	0.60	25.2934	15.1761	20.2348	1V9165A	1-3C #12	486	2.1500	0.0765	T21	1.0700	2.1149	0.0372	85		411.9		
45	480V RX MOV BD 1A1-A	3E	CNTFGL CHRG PMP 1A-A ADP	2.00	3.10	22.6	0.62	11.7670	7.2955	9.2324	1PL6145A	1-3C #12	600	2.1500	0.0765	T31	0.1410	1.4910	0.0459	85		423.2		
49	480V RX MOV BD 1A1-A	BB	VOL CONT TANK OUTLET ISLN VLV	1.90	3.50	26.0	0.60	10.2147	6.1288	8.1717	1V2750A	1-3C #12	500	2.1500	0.0765	T29	0.2370	1.3120	0.0383	85		424.1		
* 51	480V RX MOV BD 1A1-A	7B	CHARGING FLOW ISLN VLV	1.90	3.50	26.0	0.60	10.2147	6.1288	8.1717	1V2247A	1-3C #12	684	2.1500	0.0765	T29	0.2370	1.7676	0.0523	80		409.3		
52	480V RX MOV BD 1A1-A	7A	SEAL FLOW RET ISQL VLV	1.90	3.50	26.0	0.60	10.2147	6.1288	8.1717	1V2800A	1-3C #12	616	2.1500	0.0765	T29	0.2370	1.5614	0.0471	80		405.5		
53	480V RX MOV BD 1A1-A	9A	RSTW TO CHARGING PMP VLV CONT	1.90	3.50	26.0	0.60	10.2147	6.1288	8.1717	1V2070A	1-3C #12	434	2.1500	0.0765	T29	0.2370	1.1701	0.0332	80		395.6		
57	480V RX MOV BD 1A1-A	11D	STS BORON INJ TANK SHUTOFF VLV	1.90	3.50	26.0	0.60	10.2147	6.1288	8.1717	1V2680A	1-3C #12	528	2.1500	0.0765	T29	0.2370	1.3722	0.0404	80		400.7		
64	480V RX MOV BD 1A1-A	11E	SIS BIT INLET SHUTOFF VLV	1.90	3.50	26.0	0.60	10.2147	6.1288	8.1717	1V2655A	1-3C #10	532	1.3500	0.0765	T29	0.2370	0.9552	0.0375	85		415.1		
75	480V RX MOV BD 1A1-A	17C	ANHNULOS STANDPIPE ISQL VLV	0.67	2.10	10.5	0.60	25.2934	15.1761	20.2348	1V9360A	1-3C #12	532	2.1500	0.0765	T21	1.0700	2.2138	0.0407	85		412.9		
* 78	480V RX MOV BD 1A1-A	13E	CNTMT SPRAY HDR 1A ISLN VLV	3.20	5.20	35.0	0.60	7.3773	4.4264	5.9018	1V2820A	1-3C #10	352	1.3500	0.0705	T32	0.1000	0.5752	0.0248	80		395.8		
81	480V RX MOV BD 1A1-A	14D	RHR PMP 1A-A MIX FLOW VLV	0.13	0.45	2.6	0.60	102.1466	61.2880	81.7173	1V1935A	1-3C #12	670	2.1500	0.0765	T9	11.7200	13.1605	0.0513	80		398.4		
* 85	480V RX MOV BD 1A1-A	17B	CNTMT STANDPIPE ISLN VLV	0.67	2.10	10.5	0.60	25.2934	15.1761	20.2348	1V9147A	1-3C #12	696	2.1500	0.0765	T21	1.0700	2.5664	0.0532	85		416.6		
* 89	480V DSL AUX BD 1A1A	5A	DG 1A-A AIR CPSRS 2	5.00	7.10	44.5	0.62	5.9681	3.7002	4.6826	1PL2195	1-3C #12	100	2.1500	0.0765	T39	0.6288	0.2438	0.0677	85		401.5		
* 91	480V DSL AUX BD 1A1A	3A	EM DX 1A1 & 1A2 SPLV VLV	0.13	0.39	2.6	0.60	102.1466	61.2880	81.7173	1PL2145A	1-3C #12	155	2.1500	0.0765	T8	13.9500	14.2832	0.0119	85		426.1		
* 93	480V DSL AUX BD 1A1A	6A	DG 1A-A MUFFLER RM EXH FAN	1.50	2.65	20.0	0.62	13.2791	8.2330	10.4188	1PL2235	1-3C #12	62	2.1500	0.0765	T28	0.2950	0.4283	0.0047	85		399.6		
95	480V DSL AUX BD 1A1A	2B	DG 1A-A RM EXH FAN 1-A	15.00	19.50	118.4	0.49	2.2427	1.0289	1.9550	1PL2620A	1-3C #8	105	0.8490	0.0705	T49	0.0057	0.0949	0.0074	85		400.5		
* 101	480V DSL AUX BD 1A1A	4D	DR RM 1A-PNL VENT FAN	15.00	20.00	118.4	0.49	2.2427	1.0289	1.9550	1PL3444A	1-3C #8	130	0.8490	0.0705	T48	0.0083	0.1186	0.0892	85		402.9		
* 104	480V CEA VT BD 1A1-A	10C	Pipe Chase CLR FAN 1A-A	3.00	4.00	25.2	0.66	10.3599	6.9979	7.8003	1PL3071A	1-3C #10	600	1.3500	0.0705	T32	0.1000	0.9100	0.0423	80		390.9		
105	480V CEA VT BD 1A1-A	9A	RHR PMP 1A-R CLR FAN	5.00	6.10	45.0	0.62	5.9018	3.6591	4.6306	1PL3031A	1-3C #10	624	1.3500	0.0705	T37	0.0430	0.8854	0.0440	80		406.5		
* 106	480V CEA VT BD 1A1-A	3C	CNTMT SPRAY PMP 1A-R CLR FAN	7.50	9.00	62.0	0.57	4.2836	2.4416	3.5196	1PL3051A	1-3C #10	630	1.3500	0.0705	T40	0.0229	0.8734	0.0444	80		418.2		
* 107	480V CEA VT BD 1A1-A	8A	SAFETY INJ PMP 1A-R CLR FAN	5.00	6.10	45.0	0.62	5.9018	3.6591	4.6306	1PL2981A	1-3C #10	632	1.3500	0.0705	T37	0.0430	0.8962	0.0446	80		407.0		
108	480V CEA VT BD 1A1-A	10A	CNTFGL CHRG PMP 1A-R CLR FAN	5.00	6.10	45.0	0.62	5.9018	3.6591	4.6306	1PL3001A	1-3C #10	447	1.3500	0.0705	T37	0.0430	0.6465	0.0315	80		395.7		
109	480V CEA VT BD 1A1-A	5A	SFP PMP A-1A70 BST PN SPCLRFAN	7.50	9.00	62.0	0.57	4.2636	2.4416	3.5196	1PL3151A	1-3C #10	240	1.3500	0.0705	T40	0.0229	0.3469	0.0169	80		386.9		
* 110	480V CEA VT BD 1A1-A	5E	CDS & AFM PNPS SP CLR FAN A-A	20.00	24.00	139.3	0.38	1.8984	0.7138	1.7591	1PL3191A	1-3C #8	400	0.8490	0.0705	T50	0.0036	0.3432	0.0282	80		402.5		
111	480V CEA VT BD 1A1-A	6B	PEM RM EL 737 CLR FAN 1A-A	3.00	4.00	25.3	0.65	10.4973	6.8127	7.9852	1PL3091A	1-3C #10	172	1.3500	0.0705	T32	0.1000	0.3322	0.0121	80		386.9		
112	480V CEA VT BD 1A1-A	2C	PEM RM EL 692 CLR FAN 1A-A	3.00	4.00	25.0	0.62	10.6232	6.5854	8.3350	1PL3131A	1-3C #10	486	1.3500	0.0705	T32	0.1000	0.7561	0.0343	80		385.7		
113	480V CEA VT BD 1A1-A	10B	PEM RM EL 713 CLR FAN 1A-A	3.00	4.00	26.0	0.62	10.2147	6.3331	8.0144	1PL3111A	1-3C #10	396	1.3500	0.0705	T32	0.1000	0.5346	0.0279	80		383.4		
* 117	480V CEA VT BD 1A1-A	2A	CONT BLDG EMERG AIR CU FAN A-A	10.00	12.20	110.0	0.53	2.4144	1.2795	2.0474	1PL3301A	1-3C #8	240	0.8490	0.0705	T43	0.0139	0.2176	0.0169	85		412.0		
* 118	480V CEA VT BD 1A1-A	12B	CONT BLDG EMERG PRESS FAN A-A	1.00	1.70	15.0	0.62	17.7054	10.9774	13.8917	1PL3787A	1-3C #12	682	2.1500	0.0765	T25	0.4950	1.9613	0.0322	85		420.1		
119	480V CEA VT BD 1A1-A	4D	EMERG GAS TRITIUM SYS A-A	20.00	25.00	132.0	0.46	2.0120	0.9255	1.7855	1PL3520A	1-3C #8	356	0.8490	0.0705	T50	0.0036	0.3168	0.0253	75		375.7		
208	480V RI MOV BD 1A2-A	3D	ST GEN NO.1 FW ISQL VLV	39.40	48.10	494.0	0.45	0.5376	0.2419	0.4801	1V2980A	3-IC #300	850	0.0500	0.0585	T53	0.0023	0.0448	0.0497	70		360.8		
			ST GEN NO.1 FW ISQL VLV BRAKE	0.30	2.6																			

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ATTACHMENT 10.5 - BLOCK MOTORE START DATA

MOTOR NO.	BOARD NAME	COP	MOTOR NAME	HP	FL1	LRA	LPFF	MOTOR Z#	MOTOR R#	MOTOR j#	CABLE NO.	CABLE SIZE	CABLE LENGTH	R	TOL	TOL	TOTAL R	TOTAL j#	TOTAL SEC	VOLTAGE	ACCEL REV
																			(X)	(X)	
221	480V RI MDV BD 1A2-A	7D	LWR CNTMT CLR 1A DISCH ISO VLV	0.13	0.60	3.5	0.60	75.8803	45.5282	60.7043	1V2261A	1-3C #12	375	2.1500	0.0765	T12	7.5300	8.3363	0.0287	85	418.6
222	480V RI MDV BD 1A2-A	7F	UPR CHTM VT CLR 1A SUP ISO VLV	0.13	0.45	3.2	0.60	84.3115	50.5869	67.4492	1V2262A	1-3C #12	35	2.1500	0.0765			0.0753	0.0027		
223	480V RI MDV BD 1A2-A	BF	UPR CHTM VT CLR IC SUP ISO VLV	0.13	0.45	3.2	0.60	84.3115	50.5869	67.4492	1V3035A	1-3C #12	250	2.1500	0.0765	T9	11.7200	12.2575	0.0191	85	427.6
224	480V RI MDV BD 1A2-A	BB	LWR CHTMT 1A CLR SPLY ISOL VLV	0.33	0.95	5.7	0.60	46.5932	27.9559	37.2745	1V1990A	1-3C #12	441	2.1500	0.0765	T15	3.7900	4.7382	0.0337	85	416.3
225	480V RI MDV BD 1A2-A	9A	LWR CHTMT IC CLR SPLY ISOL VLV	0.33	0.95	5.7	0.60	46.5932	27.9559	37.2745	1V2020A	1-3C #12	535	2.1500	0.0765	T15	3.7900	4.9403	0.0409	85	417.5
226	480V RI MDV BD 1A2-A	10D	UP CHTM VT CLR IC DISCH ISO VLV	0.13	0.45	3.1	0.60	84.3000	50.7480	67.6640	1V3036A	1-3C #12	472	2.1500	0.0765	T9	11.7200	12.7348	0.0361	85	430.5
229	480V RI MDV BD 1A2-A	9F	UP CHTM VT CLR 1B DISCH ISO VLV	0.13	0.45	3.2	0.60	84.3115	50.5869	67.4492	1V3050A	1-3C #12	200	2.1500	0.0765			0.4300	0.0153		
230	480V RI MDV BD 1A2-A	9B	LWR CHTMT 1B CLR DISCH ISO VLV	0.33	0.95	5.7	0.60	46.5932	27.9559	37.2745	1V2030A	1-3C #12	510	2.1500	0.0765	T15	3.7900	4.8865	0.0390	85	417.1
231	480V RI MDV BD 1A2-A	8D	LWR CHTMT IC CLR DISCH ISO VLV	0.13	0.60	3.5	0.60	75.8803	45.5282	60.7043	1V3210A	1-3C #12	494	2.1500	0.0765	T12	7.5300	8.5921	0.0378	85	419.5
233	480V RI MDV BD 1A2-A	10F	UP CHTM VT CLR 1D DISCH ISO VLV	0.13	0.45	3.2	0.60	84.3115	50.5869	67.4492	1V2070A	1-3C #12	250	2.1500	0.0765	T9	11.7200	12.2575	0.0191	85	427.6
234	480V RI MDV BD 1A2-A	10A	LWR CHTMT ID CLR DISCH ISO VLV	0.33	0.95	5.7	0.60	46.5932	27.9559	37.2745	1V2090A	1-3C #12	416	2.1500	0.0765	T15	3.7900	4.6844	0.0318	85	416.0
*237	480V RI MDV BD 1A2-A	11D	RCP THRM BARR RTN CHTM ISO VLV	0.70	2.30	12.0	0.60	22.1318	13.2791	17.7054	1V2650A	1-3C #12	650	2.1500	0.0765	T24	0.6320	2.0295	0.0497	85	414.2
*238	480V RI MDV BD 1A2-A	11E	RCP THRM BARR CHTMT ISOL VLV	0.13	0.45	2.6	0.60	102.1466	61.2880	81.7173	1V2650A	1-3C #12	650	2.1500	0.0765	T9	11.7200	13.1175	0.0497	85	423.2
241	480V RI MDV BD 1A2-A	12D	RCP OIL CLR RTN CHTMT ISLN VLV	0.13	0.60	3.2	0.60	84.3115	50.5869	67.4492	1V2867A	1-3C #12	625	2.1500	0.0765	T12	7.5300	8.8738	0.0478	85	417.2
242	480V RI MDV BD 1A2-A	12F	RCP OIL CLR HTR CHTMT ISLN VLV	0.33	0.95	5.7	0.60	46.5932	27.9559	37.2745	1V2878A	1-3C #12	650	2.1500	0.0765	T14	4.7200	6.1175	0.0497	85	424.1
*251	480V RI MDV BD 1A2-A	16D	EXCS LTBR HI CONT IRLT ISO VLV	0.33	0.95	5.7	0.60	46.5932	27.9559	37.2745	1V2292A	1-3C #12	650	2.1500	0.0765	T15	3.7900	5.1875	0.0497	85	418.9
255	480V RI MDV BD 1A2-A	13E	ANNULUS SPR ISLN VLV	1.00	2.10	5.0	0.60	53.1162	31.8697	42.4930	1V9157A	1-3C #12	600	2.1500	0.0765	T19	1.5600	2.9560	0.0459	85	404.7
*287	480V DSL AUX BD 1A2A	5A	DG 1A-A AIR CPRSR I	5.00	7.10	44.5	0.62	5.9695	3.7011	4.6836	PL2200	1-3C #12	74	2.1500	0.0765	T39	0.0288	0.1879	0.0057	85	399.0
*289	480V DSL AUX BD 1A2A	2B	DG 1A-A RN EXH FAR 2-A	15.00	19.50	118.4	0.49	2.2430	1.0991	1.9551	PL2629A	1-3C #8	65	0.8490	0.0705	T49	0.0057	0.0518	0.8047	85	397.1
*301	480V SDSD 1B1-B	3200	3C CMPT CLS 5YS PNP 1B-B	350.00	355.00	2094.0	0.30	0.1274	0.0382	6.1216	PL14743B	3-1C #300	575	0.0500	0.0585		0.0144	0.9168		85	374.1
*327	480V RI MDV BD 1B1-B	4D	CNTFGL CHRG PNP 1B-B AOP	2.00	3.10	22.6	0.62	11.7670	7.2955	9.2324	PL6152B	1-3C #12	648	2.1500	0.0765	T31	0.1410	1.5342	0.0496	85	425.7
328	480V RI MDV BD 1B1-B	8A	VOL CDTN TANK OUTLET ISLN VLV	1.90	3.50	26.0	0.60	10.2147	6.1288	8.1717	1V2770B	1-3C #12	485	2.1500	0.0765	T29	0.2370	1.2798	0.0371	85	423.3
330	480V RI MDV BD 1B1-B	7A	CHRG FLOW ISLN VLV	1.90	3.50	26.0	0.60	10.2147	6.1288	8.1717	1V2255B	1-3C #12	670	2.1500	0.0765	T29	0.2370	1.6775	0.0513	85	408.5
333	480V RI MDV BD 1B1-B	6D	SEAL FLOW RET ISLN VLV	1.90	3.50	26.0	0.60	10.2147	6.1288	8.1717	1V2808B	1-3C #12	282	2.1500	0.0765	T29	0.2370	0.8433	0.0216	85	398.8
334	480V RI MDV BD 1B1-B	6B	RST TO CHARGING PNP VLV CONT	1.90	3.50	26.0	0.60	10.2147	6.1288	8.1717	1V2100B	1-3C #12	612	2.1500	0.0765		0.4508	0.0111		85	
*336	480V RI MDV BD 1B1-B	17B	ANNULUS STANDPIPE ISLN VLV	0.67	2.10	5.0	0.60	53.1162	31.8697	42.4930	1V9155B	1-3C #12	850	2.1500	0.0765	T19	1.5600	3.4875	0.0650	85	407.3
*340	480V RI MDV BD 1B1-B	11E	SIS BURON TNJ TANK SHUTOFF VLV	1.90	3.50	26.0	0.60	10.2147	6.1288	8.1717	1V2687B	1-3C #10	642	1.3500	0.0705	T29	0.2370	1.1037	0.0453	85	419.0
*350	480V RI MDV BD 1B1-B	14A	CNTAT SPRAY HTR 1B ISLN VLV	3.20	5.20	35.0	0.60	7.3773	4.4254	5.9018	1V8208B	1-3C #10	430	1.3500	0.0705	T32	0.1000	0.6005	0.0303	85	390.5
*364	480V RI MDV BD 1B1-B	15B	RHR PNP 1B-B MIN FLOW VLV	0.13	0.45	3.2	0.60	84.3115	50.5869	67.4492	1V9158A	1-3C #12	825	2.1500	0.0765	T19	11.7200	13.4559	0.0632	85	406.3
*369	480V DSL AUX BD 1B1B	5A	DG 1B-B AIR CPRSR 2	5.00	7.10	44.5	0.62	5.9681	3.7002	4.6826	PL2215	1-3C #12	120	2.1500	0.0765	T39	0.0288	0.2658	0.0092	85	403.4
*371	480V DSL AUX BD 1B1B	3A	EM DG ENG HI SUP VLV FM HTR 1B	0.13	0.39	2.6	0.60	102.1466	61.2880	81.7173	PL2157B	1-3C #12	158	2.1500	0.0765	T8	13.9500	14.2897	0.0121	85	426.1
*373	480V DSL AUX BD 1B1B	6A	DG 1B-B MUFFLER RN EXH FAN	1.50	2.65	20.0	0.62	13.2791	8.2330	10.4181	PL2249	1-3C #12	65	2.1500	0.0765	T28	0.2950	0.4347	0.0050	85	399.2
376	480V DSL AUX BD 1B1B	2B	DG 1B-B RN EXH FAN 1-B	15.00	19.50	118.4	0.49	2.2431	1.0991	1.9553	PL2656B	1-3C #8	132	0.8490	0.0705	T49	0.0057	0.1178	0.0093	85	402.8
*381	480V DSL AUX BD 1B1B	4B	DG RN 1B-B PNL VENT FAN	15.00	20.00	118.4	0.49	2.2431	1.0991	1.9553	PL3452B	1-3C #8	150	0.8490	0.0705	T49	0.0057	0.1178	0.0093	85	404.7
*383	480V CEA VT BD 1B1-B	3B	PIPE CHASE CLR FAN 1B-B	3.00	4.00	25.2	0.66	10.5389	6.9979	7.8803	PL3081B	1-3C #10	392	1.3500	0.0705	T32	0.1000	0.8992	0.0417	85	390.6
*384	480V CEA VT BD 1B1-B	9A	RHR PNP 1B-B RN CLR FAN	5.00	6.10	45.0	0.62	5.9018	3.6591	4.6306	PL3041B	1-3C #10	756	1.3500	0.0705	T37	0.0430	1.0535	0.0533	85	414.7
*385	480V CEA VT BD 1B1-B	3C	CNTAT SPRAY PNP 1B-B RN CLR FAN	7.50	9.00	62.0	0.57	4.2836	2.4416	3.5196	PL3061B	1-3C #10	594	1.3500	0.0705	T40	0.0229	0.6248	0.0419	85	415.2
386	480V CEA VT BD 1B1-B	5A	SFP PMFB-BLTB BST PNP SPCLRFAN	7.50	9.00	62.0	0.57	4.2836	2.4416	3.5196	PL3161B	1-3C #10	520	1.3500	0.0705	T40	0.0229	0.7245	0.0367	85	409.1
387	480V CEA VT BD 1B1-B	5E	CCS & FW FURPS SP CLR FAN B-B	20.00	24.50	139.9	0.38	1.8384	0.7138	1.7591	PL3201B	1-3C #8	370	0.8490	0.0705	T50	0.0036	0.3177	0.0261	85	404.7
388	480V CEA VT BD 1B1-B	8A	SAFETY INJ PNP 1B-B RN CLR FAN	5.00	6.10	50.1	0.62	5.2958	3.2840	4.1559	PL2991B	1-3C #10	756	1.3500	0.0705	T37	0.0430	1.0636	0.0533	85	420.4
389	480V CEA VT BD 1B1-B	10A	CNTF GL CHRG PNP 1B-B RN CLR FAN	5.00	6.10	45.0	0.62	5.9018	3.6591	4.6306	PL3011B	1-3C #10	596	1.3500	0.0705	T37	0.0430	0.8476	0.0420	85	404.8
390	480V CEA VT BD 1B1-B	8B	PEN RM EL E92 CLR FAN 1B-B	3.00	4.00	25.0	0.62	10.6232	6.5864	8.3356	PL3141B	1-3C #10	540	1.3500	0.0705	T32	0.1000	0.8256	0.0381	85	402.4
391	480V CEA VT BD 1B1-B	2C	PEN RM EL 713 CLR FAN 1B-B	3.00	4.00	26.0	0.62	10.2147	6.3321	8.0144	PL3121B	1-3C #10	404	1.3500	0.0705	T32	0.1000	0.6454	0.0285	85	383.5
392	480V CEA VT BD 1B1-B	9E	PEN RM EL 737 CLR FAN 1B-B	3.00	4.00	25.3	0.65	10.4973	5.8127	7.9862	PL3101B	1-3C #10	410	1.3500	0.0705	T32	0.1000	0.6525	0.0289	85	384.0
*397	480V CEA VT BD 1B1-B	11A	COHT BLDG EMERS PRESS FAN B-B	1.00	1.70	15.0	0.62	17.7054	10.9774	12.8917	PL3795B	1-3C #12	150	2.1500	0.0765	T25	0.4950	0.8175	0.0115	85	402.6

WBN-EEB-MS-TI06-0010 R0
ATTACHMENT 10.5 - BLOCK MOTOR START DATA

MOTOR NO.	BOARD NAME	COMP	MOTOR NAME	HP	FLI	LRA	LRPF	MOTOR Zn	MOTOR Ra	MOTOR Jx	CABLE NO.	CABLE SIZE	CABLE LENGTH	CABLE R	CABLE Jx	CABLE TOL NO.	TOL R	TOL Jx	MIN ACCEL			
																			VOLT SEC	REQ		
#398	480V CLA VT BD 181-B	2A	CONT BLDG EM AIR CLRUP FAN B-B	16.00	12.20	110.0	0.53	2.4144	1.2796	2.0474	1PL3308B	1-3C #8	210	0.8490	0.0705	T43	0.0139	0.1922	0.0148	85	410.3	
#399	480V CLA VT BD 181-B	4D	EMERG GAS TRINT SYS FAN B-B	20.00	25.00	132.0	0.46	2.0120	0.9255	1.7865	JPL3530B	1-3C #8	550	0.8490	0.0705	T50	0.0036	0.4790	0.0395	75	9.70	
498	480V RI MOV BD 182-B	3D	ST GEN HD 2 FW ISLN VLV	39.40	48.10	494.0	0.45	0.6792	0.3057	0.5066	IV3000B	3-1C #300	850	0.0500	0.0585	T53	0.0023	0.0873	0.0497	70	362.7	
			ST GEN HD 2 FW ISLN VLV BRAKE			0.30	2.6	1.00	176.9231	176.9231	0.0000	IV3000B	3-1C #4	824	0.3363	0.0630		0.4393	0.9935	0.1038	80	370.1
#500	480V RI MOV BD 182-B	4D	ST GEN HD 4 FW ISLN VLV	39.40	48.10	494.0	0.45	0.6792	0.3057	0.5066	IV3010B	3-1C #300	850	0.0500	0.0585	T53	0.0023	0.0873	0.0497	70	362.7	
			ST GEN HD 4 FW ISLN VLV BRAKE			0.30	2.6	1.00	176.9231	176.9231	0.0000	IV3010B	3-1C #4	724	0.3363	0.0630		0.4393	0.9263	0.0912	80	369.9
505	480V RI MOV BD 182-B	6D	RCP THRM BAR RTN CHTMT ISO VLV	0.70	2.30	12.0	0.60	22.1318	13.2791	17.7054	IV2640B	1-3C #12	618	2.1500	0.0765	T24	0.6320	1.9607	0.0473	85	415.9	
506	480V RX MOV BD 182-B	6E	RCP THRM BAR CHTMT ISO VLV	0.13	0.45	2.6	0.60	102.1465	61.2880	81.7173	IV2670B	1-3C #12	522	2.1500	0.0765	T9	11.7200	12.8423	0.0399	85	422.4	
507	480V RX MOV BD 182-B	9D	UP CHTM VT CLR 1B DISH ISO VLV	0.13	0.45	2.6	0.60	102.1465	61.2880	81.7173	IV3106B	1-3C #12	463	2.1500	0.0765	T9	11.7200	12.7155	0.0354	85	424.6	
#510	480V RI MOV BD 182-B	7D	LWR CHTMT 1B CLR DISH ISO VLV	0.13	0.60	3.5	0.60	75.8803	45.5282	60.7043	IV2275B	1-3C #12	649	2.1500	0.0765	T12	7.5300	8.9254	0.0495	85	420.7	
											IV2276B	1-3C #12	40	2.1500	0.0765			0.0860	0.0931			
S11	480V RX MOV BD 182-B	9F	UP CHTM VT CLR 1B SUP ISO VLV	0.13	0.45	3.1	0.60	84.5800	50.7480	67.6560	IV3051B	1-3C #12	545	2.1500	0.0765	T9	11.7200	12.8918	0.0417	85	429.6	
S12	480V RX MOV BD 182-B	10F	UP CHTM VT CLR 1D SUP ISO VLV	0.13	0.45	3.2	0.60	84.3115	50.5859	67.4492	IV3056B	1-3C #12	304	2.1500	0.0765	T9	11.7200	12.3736	0.0233	85	428.0	
S13	480V RI MOV BD 182-B	10A	LWR CHTMT 1B CLR SPLY ISLN VLV	0.33	0.95	5.7	0.60	46.5932	27.9559	37.2745	IV2050B	1-3C #12	513	2.1500	0.0765	T15	3.7900	4.8593	0.0392	85	417.2	
S14	480V RI MOV BD 182-B	10B	LWR CHTMT 1D CLR SPLY ISLN VLV	0.33	0.95	5.7	0.60	46.5932	27.9559	37.2745	IV2050B	1-3C #12	337	2.1500	0.0765	T15	3.7900	4.5146	0.0258	85	415.0	
S15	480V RI MOV BD 182-B	10D	UP CHTM VT CLR 1D DIS ISO VLV	0.13	0.45	3.14	0.60	84.5800	50.7480	67.6560	IV3120B	1-3C #12	253	2.1500	0.0765	T9	11.7200	12.2683	0.0195	85	429.9	
S18	480V RX MOV BD 182-B	7F	UP CHTM VT CIR 1A DISH ISO VLV	0.13	0.45	3.2	0.60	84.3115	50.5869	67.4492	IV3028B	1-3C #12	340	2.1500	0.0765		0.7310	0.0260				
S19	480V RX MOV BD 182-B	9A	LWR CHTMT 1A CIR DISH ISO VLV	0.33	0.95	5.7	0.60	46.5932	27.9559	37.2745	IV2010B	1-3C #12	472	2.1500	0.0765	T9	11.7200	12.7348	0.0361	85	429.2	
S20	480V RI MOV BD 182-B	BD	LWR CHTMT 1D CIR DISH ISO VLV	0.13	0.60	3.5	0.60	75.8803	45.5282	60.7043	IV2283B	1-3C #12	463	2.1500	0.0765	T12	7.5300	8.5255	0.0354	85	419.5	
S22	480V RX MOV BD 182-B	BF	UP CHTM VT CIR 1C DISH ISO VLV	0.13	0.45	3.2	0.60	84.3115	50.5869	67.4492	IV3043B	1-3C #12	495	2.1500	0.0765	T9	11.7200	12.7843	0.0379	85	429.3	
S23	480V RX MOV BD 182-B	9B	LWR CHTMT 1C CIR DISH ISO VLV	0.33	0.95	5.7	0.60	46.5932	27.9559	37.2745	IV2040B	1-3C #12	488	2.1500	0.0765	T15	3.7900	4.8392	0.0373	85	416.9	
S29	480V RI MOV BD 182-B	12F	ARHULUS SPR FSLN VLV	0.57	2.10	5.0	0.60	53.1162	31.8697	42.4930	IV3170B	1-3C #12	720	2.1500	0.0765	T15	1.6500	3.2688	0.0551	85	405.9	
S34	480V RX MOV BD 182-B	13F	RCP DIL CLR HOR CHTMT ISLN VLV	0.33	0.95	5.7	0.60	46.5932	27.9559	37.2745	IV2888B	1-3C #12	546	2.1500	0.0765	T15	3.7900	4.9639	0.0418	85	417.6	
S40	480V RX MOV BD 182-B	13D	RCP DIL CLR RTN CHTMT ISLN VLV	0.13	0.60	3.5	0.60	75.8803	45.5282	60.7043	IV2854B	1-3C #12	265	2.1500	0.0765	T12	7.5300	8.0998	0.0203	85	418.2	
#570	480V DSL AUX BD 182B	5A	DG 1B-B A1R CPRSR 1	5.00	7.10	44.5	0.62	5.9681	3.7002	4.6826	PL2220	1-3C #12	100	2.1500	0.0765	T39	0.0288	0.2438	0.0077	85	401.5	
#572	480V DSL AUX BD 182B	2B	DG 1B-B RM EXH FAN 2-B	15.00	19.50	118.4	0.49	2.2427	1.0991	1.9353	PL2665B	1-3C #8	110	0.8490	0.0705	T49	0.0057	0.0951	0.0079	85	401.0	
#585	6.9KV SHDN BD 2A-A	1B	CNTFL CRG PMP 2A-A	600.00	45.00	269.7	0.35	14.1237	4.9450	13.2351	2PP550A	3-1C #2/0	673	0.1085	0.0780			0.0730	0.0525	80	4.65 5308.0	
587	6.9KV SHDN BD 2A-A	B	ERCH PMP D-A	800.00	63.00	344.0	0.19	11.0771	2.1046	10.8753	2PP567A	3-1C #2/0	3186	0.1085	0.0780			0.3457	0.2485	80	3.60 5429.4	
588	6.9KV SHDN BD 2A-A	10	AUX FEEDWTR PMP 2A-A	600.00	49.50	300.0	0.20	12.7017	2.5403	12.4451	2PP575A	3-1C #2/0	470	0.1085	0.0780			0.0510	0.0367	85	6.60 5630.4	
596	6.9KV SHDN BD 2B-B	B	ERCH PMP H-B	800.00	63.00	344.0	0.19	11.0771	2.1046	10.8753	2PP712B	3-1C #2/0	3822	0.1085	0.0780			0.4147	0.2981	90	3.60 6142.1	
#597	6.9KV SHDN BD 2B-B	10	AUX FEEDWTR PMP 2B-B	600.00	49.50	300.0	0.20	12.7017	2.5403	12.4451	2PP567B	3-1C #2/0	300	0.1085	0.0780			0.0326	0.0234	85	6.60 5623.0	
#650	480V DSL AUX BD 2A1A	5A	DG 2A-A AIR CPRSR 2	5.00	7.10	44.5	0.62	5.9681	3.7002	4.6826	PL2205	1-3C #12	100	2.1500	0.0765	T39	0.0268	0.2438	0.0077	85	401.5	
#662	480V DSL AUX BD 2A1A	3A	EM DS EXH HR 2A1 & 2A2 SUP VLV	0.13	0.39	2.6	0.60	102.1465	61.2880	81.7173	PL2160A	1-3C #12	160	2.1500	0.0765	T8	13.9500	14.2940	0.0122	85	426.1	
#664	480V DSL AUX BD 2A1A	6A	DG 2A-A RHF NFFL EXH FAN	1.50	2.65	20.0	0.62	13.2791	8.2330	10.4188	PL2242	1-3C #12	52	2.1500	0.0765	T28	0.2950	0.4068	0.0040	85	398.5	
667	480V DSL AUX BD 2A1A	2B	DS 2A-A RM EXH FAN 1-A	15.00	19.50	118.4	0.49	2.2427	1.0989	1.9350	2PL2638A	1-3C #8	70	0.8490	0.0705	T49	0.0057	0.0652	0.0049	85	397.4	
#672	480V DSL AUX BD 2A1A	4D	DG RM 2A-A PNL VENT FAN	15.00	20.00	118.4	0.49	2.2427	1.0989	1.9350	PL2449A	1-3C #8	130	0.8490	0.0705	T48	0.0083	0.1185	0.0092	85	402.9	
674	480V CLA VT BD 2A1-A	10C	PIPE CHASE CLR FAN 2A-A	3.00	4.30	25.2	0.66	10.5393	6.9979	7.8803	2PL3071A	1-3C #10	700	1.3500	0.0705	T32	0.1000	1.0450	0.0494	85	419.0	
#679	480V CLA VT BD 2A1-A	5E	ATW SRA ITR SPACE CLR FAN A-A	15.00	20.20	105.2	0.49	2.5236	1.2368	2.1999	2PL3151A	1-3C #8	210	0.8490	0.0705	T48	0.0083	0.1866	0.0148	85	407.9	
680	480V CLA VT BD 2A1-A	8B	PEF RR EL 737 CLR FAN 2A-A	3.00	4.00	25.5	0.65	10.4027	6.8658	7.8152	2PL3091A	1-3C #10	262	1.3500	0.0705	T32	0.1000	0.4537	0.0185	80	2.40 379.3	
#681	480V CLA VT BD 2A1-A	2C	PEF RM EL 892 CLR FAN 2A-A	3.00	4.30	26.7	0.62	9.9506	6.1694	7.0072	2PL3131A	1-3C #10	776	1.3500	0.0705	T48	0.1000	1.4745	0.0547	85	422.0	
682	480V CLA VT BD 2A1-A	10B	PEF RM EL 713 CLR FAN 2A-A	2.00	4.00	26.7	0.62	9.9506	6.1694	7.8072	2PL3111A	1-3C #10	250	1.3500	0.0705	T32	0.1000	0.5725	0.0247	85	406.1	
683	480V CLA VT BD 2A1-A	4A	EG TRINT SYS A-A RM CLR FAN	3.00	4.10	27.0	0.53	9.8263	5.2133	8.3412	2PL3774A	1-3C #10	500	1.3500	0.0705	T32	0.1000	0.7750	0.0233	80	1.05 385.2	
#690	480V CLA VT BD 2A1-A	3B	ATW BLDG GAS TRINT SYS FAN A-A	50.00	62.00	304.0	0.37	0.8736	0.3232	0.8116	2PL3748A	1-3C #12	550	0.2134	0.0615	T35	0.0012	0.1186	0.0338	75	9.10 376.7	
#693	480V DSL AUX BD 2A2A	5A	DG 2A-A AIR CPRSR 1	5.00	7.25	46.0	0.62	5.7735	3.5795	4.5299	PL2210	1-3C #10	82	2.1500	0.0765	T38	0.0348	0.2111	0.0063	85	400.3	
#845	480V DSL AUX BD 2A2A	28	DG 2A-A RM EXH FAN 2-A	15.00	19.50	118.4	0.49	2.2427	1.0983	1.9550	PL2647											

17-Sep-92

WBN-EEB-MS-TI06-0010 R0
 ATTACHMENT 10.5 - BLOCK MOTOR START DATA

MOTOR No.	BOARD NAME	COMP	MOTOR NAME	HP	FLI	LRA	LRPF	MOTOR Zs	MOTOR Rm	MOTOR Jm	CABLE NO.	CABLE SIZE	CABLE LENGTH	CABLE R	TOL NO.	TOL R	MIN ACCEL				
																	TOTAL R	TOTAL JX	START TIME VOLT SEC (z)	VOLTAGE REQ	
#301	480V SDBD 2B1-B	3200	3C CNPNT CL6 5YS PMP 2B-B	350.00	399.00	2084.0	0.30	0.1274	0.0382	0.1216	2PL4742B	3-IC #500	675	0.0314	0.0540		0.0106	0.0182	70	3.10	374.1
											2PL4742B	3-IC #500	675	0.0314	0.0540						
#914	480V DSL AUX BD	2B1B	5A DG 2B-B AIR CPRSR 2	5.00	7.10	44.5	0.52	5.9681	3.7002	4.6826	PL2225	1-3C #12	122	2.1500	0.0765	T39	0.0288	0.2911	0.0093	85	403.6
#915	480V DSL AUX BD	2B1B	3A EN DG EN6 SUP VLV FROM HDR 1B	0.13	0.39	2.6	0.52	102.1466	53.3309	80.1444	PL2180B	1-3C #12	162	2.1500	0.0765	TB	13.3500	14.2903	0.0124	85	427.1
#918	480V DSL AUX BD	2B1B	6A DG 2B-B MUFFLER RM EXH FAN	1.50	2.65	28.0	0.52	13.2791	8.2330	10.4188	PL2255	1-3C #12	80	2.1500	0.0765	T29	0.2370	0.4090	0.0061	85	398.7
#921	480V DSL AUX BD	2B1B	2B DG 2B-B RM EXH FAN FAN 1B	15.00	19.50	118.4	0.49	2.2427	1.0989	1.9550	PL2674B	1-3C #8	120	0.8490	0.0705	T49	0.0057	0.1076	0.0083	85	401.8
#927	480V DSL AUX BD	2B1B	4D DG RM 2B-B PNL VENT FAN	15.00	20.00	118.4	0.49	2.2427	1.0989	1.9550	PL3456B	1-3C #8	150	0.8490	0.0705	T48	0.0083	0.1357	0.0106	85	404.7
92B	480V CEA VT BD	2B1-B	3B PIPE CHASE CLR FAN 2B-B	3.00	4.00	25.2	0.56	10.5389	5.9979	7.8803	2PL3081B	1-3C #10	460	1.3500	0.0705	T32	0.1000	0.7210	0.0324	85	410.1
#931	480V CEA VT BD	2B1-B	5E AFMPUBA XFP PMP SP CLR FAN B-B	15.00	19.00	133.5	0.49	1.9897	9.9749	1.7344	2PL3161B	1-3C #8	250	0.8490	0.0705	T49	0.0057	0.2180	0.0175	85	416.5
#934	480V CEA VT BD	2B1-B	8B PEN RM EL 692 CLR FAN 2B-B	3.00	4.30	26.7	0.52	9.9506	6.1694	7.8072	2PL3141B	1-3C #10	458	1.3500	0.0705	T32	0.1000	0.7183	0.0323	85	410.1
#935	480V CEA VT BD	2B1-B	2C PEN RM EL 713 CLR FAN 2B-B	3.00	4.30	26.7	0.52	9.9506	6.1694	7.8072	2PL3121B	1-3C #10	305	1.3500	0.0705	T32	0.1000	0.5131	0.0216	85	404.5
#936	480V CEA VT BD	2B1-B	9E PEN RM EL 737 CLR FAN 2B-B	3.00	4.00	24.6	0.56	10.7960	7.1261	8.1012	2PL3101B	1-3C #10	340	1.3500	0.0705	T32	0.1000	0.5590	0.0240	80	381.5
942	480V CEA VT BD	2B1-B	12B EG TRMT SYS B-B RM CLR FAN	3.00	4.10	27.0	0.53	9.8363	5.2133	8.3412	2PL3201B	1-3C #10	367	1.3500	0.0705	T32	0.1000	0.5955	0.0259	80	381.1
#943	480V CEA VT BD	2B1-B	3D AUX BLDG GAS TRMT SYS FAN B-B	50.00	62.00	304.0	0.37	0.8735	0.3232	0.8115	2PL3768B	1-3C #2	350	0.2134	0.0615	T55	0.0012	0.0759	0.0215	75	9.10
#1057	480V RX MOV BD	2B2-B	12B CCS H/C DISCH VLV TO HDR B	0.57	1.90	7.6	0.50	35.1298	21.0779	28.1038	292791B	1-3C #12	342	2.1500	0.0765	T24	0.6320	1.3673	0.0262	85	400.5
#1102	480V DSL AUX BD	2B2B	5A DG 2B-B AIR CPRSP 1	5.00	7.25	44.5	0.52	5.9681	3.7002	4.6826	PL2230	1-3C #12	115	2.1500	0.0765	T39	0.0289	0.2750	0.0088	85	402.9
#1104	480V DSL AUX BD	2B2B	2B DG 2B-B RM EX FAN 2-B	15.00	19.50	118.4	0.49	2.2427	1.0989	1.9550	PL2683B	1-3C #9	114	0.8490	0.0705	T49	0.0057	0.1025	0.0080	85	401.3
#1119	480V RX MOV BD	1B2-B	SC RCP OIL CLR SUP CNTMT ISOL VLV	0.13	0.60	3.5	0.60	75.8803	45.5282	60.7043	1V800B	1-3C #10	408	1.3500	0.0705	T11	9.2500	9.8953	0.0337	85	423.7 IR4
											1V801B	1-3C #10	70	1.3500	0.0765						426.0 IR4
											1V817A	1-3C #12	175	2.1500	0.0765						294.9 IR4

AcP 9-21-92
 294.9 IR4

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ATTACHMENT 11.4.

Calc. STUDY-EEB-WBN-12-001

Attachment 3

Required Motor Starting Voltage

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ATTACHMENT 11.4.
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Required Motor Starting Voltage
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Attachment 10.6

480V Switchgear and Motor Control Center Motor Starting Voltages

ENG_TITLE	BOARD	COMP_NO	EQUIP_ID_NO	LOAD_SF	FLI	LVA	LPF	Z _m	Re	J _m	CABLE	CABLE	CABLE	MOTOR	MIN	ACCEL	REV					
											NO.	SIZE	LEN	R _c	J _{dc}	START	START	TIME	VOLT	VOLT	SEC	(#)
LVSG VOLTAGE =416.4V UNLESS NOTED OTHERWISE																						
Aux Bldg Gen Sply Fan 1A	480V SHDN BD 1A1-A	2C	1-MTR-30-103	100.0	1.15	120.0	622	0.31	0.42658	0.13236	0.40594	IPL5140	4/0	105	0.00723	0.00646	437.8					
COMPONENT COOL SYS PUMP 1A-A	480V SHDN BD 1A1-A	3B	1-MTR-70-46-A	350.0	1.15	389.0	2084	0.30	0.12744	0.09323	0.12157	IPL4725A	500MCH	509	0.00799	0.01374	397.9	70s	3.1	PARALLEL	COND	
CRDM Clr Fan 1A-A Mtr 1	480V SHDN BD 1A1-A	3B	1-MTR-30-83/1-A	75.0	1.15	97.0	413	0.33	0.64305	0.21221	0.66703	IPL4800A	1/0	460	0.06219	0.02760	408.1			AMP	FAIL	
Rear Lnr Compt Clr Fan 1A-A	480V SHDN BD 1A1-A	7C	1-MTR-30-74-A	50.0	1.00	73.8	583	0.29	0.45554	0.13302	0.43569	IPL4750A	#2	650	0.13871	0.03998	368.0	80s	12.0	ECH	11001480	DCH F-11816-A
	480V SHDN BD 1A1-A	7C										IPL4751A	#2	30	0.00540	0.00185						DCH F-11816-B
CRDM Clr Fan 1A-A Mtr 2	480V SHDN BD 1A1-A	7D	1-MTR-30-83/2-A	75.0	1.15	97.0	413	0.33	0.64305	0.21221	0.66703	IPL4816A	1/0	477	0.06449	0.02862	407.0			AMP	FAIL	
Elec Bd Rx AHU A-A	480V SHDN BD 1A1-A	9C	0-MTR-31-308-A	50.0	1.15	58.5	395	0.37	0.67236	0.24877	0.62464	IPL4500A	4/0	500	0.03445	0.03075	420.4					
Cont Air Rtu Fan 1A-A	480V SHDN BD 1A1-A	9C	1-MTR-30-38-A	100.0	1.00	115.0	849	-0.31	0.39562	0.09474	0.29856	IPL4875A	4/0	490	0.03376	0.03014	386.5			AMP	FAIL	
CONT RM A/C A-A CPRS	480V SHDN BD 1A2-A	2C	0-MTR-31-80/2-A	250.0	1.15	275.0	1825	0.24	0.14552	0.03493	0.14127	IPL4522A	4/0	141	0.00436	0.00434	430.4			PARALLEL	COND	
COMPONENT COOL SYS PUMP C-5	480V SHDN BD 1A2-A	3B	0-MTR-70-51-S	350.0	1.15	389.0	2084	0.30	0.12744	0.03823	0.12157	IPL4730A	300MCH	575	0.01438	0.01682	384.3	70s	3.1	PARALLEL	COND	
	480V SHDN BD 1A2-A	3B										IPL4734A	300MCH						300 MCH IMPEDANCE			
	480V SHDN BD 1A2-A	3B										IPL4735S	500MCH						USED FOR ENTIRE			
	480V SHDN BD 1A2-A	3B										IPL4736S	500MCH						LENGTH			
AUX CONT & SERV AIR CPRS A	480V SHDN BD 1A2-A	3D	0-MTR-32-25	125.0	1.15	162.0	770	0.28	0.34491	0.09657	0.33111	IPL5033A	4/0	517	0.03562	0.03180	398.6	80s				
Station Fire Pmp 1A-A	480V SHDN BD 1A2-A	40	1-MTR-28-1-A	200.0	1.00	230.0	1179	0.27	0.22515	0.06079	0.21678	IPL5003A	500MCH	3220	0.05055	0.06964	316.3	58s		PARALLEL	COND	LVSG VOLT=454.4
Spent Fuel Pit Pmp C-5 (SPARE)	480V SHDN BD 1A2-A	40	0-MTR-78-35-S	100.0	1.15	115.0	647	0.42	0.41067	0.17246	0.37269	IPL4504A	4/0	539	0.03714	0.03315	396.6			AMP	FAIL	
CRD Mech Clr Fan 1C-A Mtr 1	480V SHDN BD 1A2-A	7A	1-MTR-30-68/I-A	75.0	1.15	97.0	413	0.33	0.64305	0.21221	0.66703	IPL4820A	1/0	543	0.07341	0.03258	403.9			AMP	FAIL	
CRD Mech Clr Fan 1C-A Mtr 2	480V SHDN BD 1A2-A	7A	1-MTR-30-77-A	60.0	1.00	73.8	583	0.29	0.45554	0.13302	0.43569	IPL4775A	#2	660	0.10864	0.04059	388.0	80s	12.0	ECH	11001480	DCH F-11816-A
CRD Mech Clr Fan 1C-A Mtr 2	480V SHDN BD 1A2-A	7A	1-MTR-30-88/2-A	75.0	1.15	97.0	416	0.33	0.53888	0.21093	0.60309	IPL4834A	1/0	530	0.07166	0.03180	404.4			AMP	FAIL	
	480V SHDN BD 1A2-A	7A										IPL4837A	1/0	53	0.01257	0.00558						
480V Shutdown Bd Rx AHU A-A	480V SHDN BD 1A2-A	9D	0-MTR-31-45-A	75.0	1.15	92.0	592	0.33	0.44854	0.14802	0.42341	IPL5104A	#2	130	0.02774	0.00800	429.8					
Aux Bldg Gen Sply Fan 1B	480V SHDN BD 1B1-B	2B	1-MTR-30-102	100.0	1.15	120.0	624	0.31	0.42561	0.13194	0.40464	IPL5160	4/0	122	0.00841	0.00750	436.4					
COMPONENT COOL SYS PUMP 1B-B	480V SHDN BD 1B1-B	3C	1-MTR-70-58-B	350.0	1.15	389.0	2084	0.30	0.12744	0.03823	0.12157	IPL4742B	300MCH	575	0.01438	0.01682	384.3	70s	3.1	PARALLEL	COND	
RECIPROCATING CHARGING PUMP	480V SHDN BD 1B1-B	3B	1-MTR-62-101	200.0	1.15	221.0	1579	0.25	0.16820	0.04205	0.16285	IPL5025A	400MCH	391	0.00747	0.01056	416.3					
AUX CONT & SERV AIR CPRS B	480V SHDN BD 1B1-B	3D	0-MTR-32-26	125.0	1.15	162.0	770	0.28	0.34491	0.09657	0.33111	IPL5089	4/0	795	0.05478	0.04889	376.4	80s				
Elec Bd Rx AHU C-B	480V SHDN BD 1B1-B	7A	0-MTR-31-31B-B	50.0	1.15	62.5	360	0.30	0.73773	0.22756	0.68537	IPL4456B	#2	650	0.13871	0.03998	394.9			AMP	FAIL	
CRD Mech Clr Fan 1B-B Mtr 1	480V SHDN BD 1B1-B	7C	1-MTR-30-92/1-B	75.0	1.15	97.0	413	0.33	0.64305	0.21221	0.66703	IPL4839B	1/0	588	0.07950	0.03526	400.4			AMP	FAIL	
Rear Lnr Compt Clr Fan 1B-B	480V SHDN BD 1B1-B	7C	1-MTR-30-75-B	60.0	1.00	73.8	583	0.29	0.45554	0.13302	0.43569	IPL4764B	#2	650	0.13871	0.03998	368.0	80s	12.0	ECH	11001480	DCH F-11819-A
	480V SHDN BD 1B1-B	7D										IPL4765B	#2	30	0.00640	0.00185						DCH F-11819-B
CRD Mech Clr Fan 1B-B Mtr 2	480V SHDN BD 1B1-B	100	1-MTR-30-92/2-B	75.0	1.15	97.0	413	0.33	0.64305	0.21221	0.66703	IPL4853B	1/0	578	0.07815	0.03468	401.0			AMP	FAIL	
CONT RM A/C B-B CPRS	480V SHDN BD 1B2-B	2B	0-MTR-31-96/2-B	250.0	1.15	275.0	1825	0.24	0.14552	0.03493	0.14127	IPL4429B	400MCH	600	0.01146	0.01620	392.0			PARALLEL	COND	DCH F-11885-A
	480V SHDN BD 1B2-B	2B										IPL4430B	400MCH	600								
	480V SHDN BD 1B2-B	2B											4/0	20	0.00138	0.00123						
480V Shdn Bd Rx Chiller B-B	480V SHDN BD 1B2-B	3C	0-MTR-31-49/2-B	240.0		247.0	1209	0.24	0.21957	0.05272	0.21325	IPL5266B	300MCH	282	0.01410	0.01650	409.8					
Station Fire Pmp 1B-B	480V SHDN BD 1B2-B	40	1-MTR-25-4-B	200.0	1.00	230.0	1179	0.27	0.22515	0.06079	0.21678	IPL5017B	500MCH	3333	0.05233	0.08999	312.9	58s		PARALLEL	COND	LVSG VOLT=454.4
	480V SHDN BD 1B2-B	40										IPL5018B	500MCH	3333								

REV

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ATTACHMENT 10.6 - LOW VOLTAGE SWITCHGEAR MOTOR STARTING VOLTAGES

THIS SHEET ADDED BY REV 4

ENG_TITLE	BOARD	COMP	EQUIPID_NO	LOAD	SF	FLI	URR	URP	Zn	Rn	Jn	CABLE NO.	CABLE SIZE	CABLE LENGTH	Re	dc	MOTOR MIN VOLT	ACCEL TIME	REMARKS
																	VOLT SEC	(%) (\$\$)	
LVSG VOLTAGE =446.4V UNLESS NOTED OTHERWISE																			
Aux Bldg Gen Exhaust Fan 1B	480V SHDN BD 1E2-B	7A	1-MTR-30-162	125.0	1.00	147.0	854	0.29	0.31098	0.09019	0.29762	1PL5170	4/0	320	0.02205	0.01968	412.5		
CRD Mech Clr Fan 10-B Mtr 1	480V SHDN BD 1E2-B	7B	1-MTR-30-80/1-B	75.0	1.15	97.0	413	0.33	0.64305	0.21221	0.60703	1PL48559	1/0	437	0.05908	0.02622	409.4	AMP FAIL	
Reac Lur Compt Clr Fan 10-B	480V SHDN BD 1E2-B	7D	1-MTR-30-78-B	60.0	1.00	73.8	583	0.29	0.45554	0.13302	0.43569	1PL47898	1/0	113	0.01528	0.00678			
Coolnt Air Rtn Fan 1B-B	480V SHDN BD 1E2-B	9C	1-MTR-30-39-B	100.0	1.00	115.0	829	0.31	0.32025	0.09943	0.30495	1PL48858	4/0	640	0.13658	0.03936	368.0 80%	12.0 ECH 11001480	
	480V SHDN BD 1E2-B	9C										1PL47908	4/2	40	0.00854	0.00246		DCN F-12119-A	
	480V SHDN BD 1E2-B	9C										1PL48868	250MCM	120	0.00714	0.00684		DCN F-12119-A	
Spent Fuel Pit Pmp B-B	480V SHDN BD 1E2-B	9A	0-MTR-78-9-B	100.0	1.15	115.0	647	0.42	0.41067	0.17248	0.37269	1PL48958	400MCM	2/0	10	0.00109	0.00060		F-12813-A
	480V SHDN BD 1E2-B	9C										1PL48958	582	65	0.02223	0.03143	403.7	F-12813-A	
480V Shutdown Bd Rm AHU C-B	480V SHDN BD 1E2-B	90	0-MTR-31-55-B	75.0	1.15	92.0	592	0.33	0.44662	0.14904	0.42349	1PL55208	4/0	240	0.01554	0.01476	421.7		
	480V SHDN BD 1E2-B	90										1PL55208	4/2	50	0.01067	0.00938			
CRD Mech Clr Fan 10-B Mtr 2	480V SHDN BD 1E2-B	10C	1-MTR-30-80/2-B	75.0	1.15	97.0	413	0.33	0.64305	0.21221	0.60703	1PL48738	1/0	418	0.05651	0.02508	410.6	AMP FAIL	
	480V SHDN BD 1E2-B	10C										1PL48748	1/0	113	0.01528	0.00678			
Aux Bldg Gen Sply Fan 2A	480V SHDN BD 2AI-A	2C	2-MTR-30-104	100.0	1.15	120.0	630	0.31	0.42156	0.13068	0.40079	2PL5140	4/0	64	0.00579	0.00517	439.4		
COMPONENT COOL SYS PUMP 2A-A	480V SHDN BD 2AI-A	3B	2-MTR-70-59-A	350.0	1.15	389.0	2084	0.30	0.12744	0.03823	0.12157	2PL4725A	500MCM	675	0.01060	0.01823	384.2 70%	3.1 PARALLEL COND	
	480V SHDN BD 2AI-A	3B										2PL4725A	500MCM	675					
CRD Mech Clr Fan 2A-A Mtr 1	480V SHDN BD 2AI-A	7C	2-MTR-30-83/1-A	75.0		97.0													
Reac Lur Compt Clr Fan 2A-A	480V SHDN BD 2AI-A	7C	2-MTR-30-74-A	40.0		47.0													
CRD Mech Clr Fan 2A-A Mtr 2	480V SHDN BD 2AI-A	7D	2-MTR-30-83/2-A	75.0		97.0													
Elec Bd Rm AHU B-A	480V SHDN BD 2AI-A	9C	0-MTR-31-300-A	50.0	1.15	55.5	395	0.37	0.57236	0.24877	0.52454	2PL4500A	4/2	620	0.13231	0.03813	392.6	AMP FAIL	
Coolnt Air Rtn Fan 2H-A	480V SHDN BD 2AI-A	10C	2-MTR-30-38-A	100.0		115.0													
Elec Bd Rm A/C A-A Cprsr	480V SHDN BD 2AI-A	2C	3MTR-31-128/2-A	250.0	1.15	275.0	1825	0.24	0.14552	0.03493	0.14127	2PL4520A	4/0	350	0.01206	0.01076	408.2	PARALLEL COND	
	480V SHDN BD 2AI-A	2C										2PL4522A	4/0	350					
480V Shdn Bd Rm Chlr A-A	480V SHDN BD 2AI-A	3C	0-MTR-31-36/2-A	240.0		247.0	1209	0.24	0.21967	0.05272	0.21325	2PL5120A	300MCM	192	0.00960	0.01123	420.9	AMP FAIL	
Aux Bldg Gen Exhaust Fan 2A	480V SHDN BD 2AI-A	7B	2-MTR-30-274	125.0	1.00	147.0	865	0.29	0.30658	0.08894	0.29350	2PL5150	4/0	359	0.02542	0.02269	407.2		
Fuel Handling Exhaust Fan A	480V SHDN BD 2AI-A	7C	0-MTR-30-138	100.0	1.15	120.0	624	0.31	0.42561	0.13154	0.40464	2PL5111	4/0	229	0.01578	0.01408	427.9		
480V SHUTDOWN BD RM AHU B-A	480V SHDN BD 2AI-A	60	0-MTR-31-44-A	75.0	1.15	92.0	592	0.33	0.44862	0.14804	0.42349	2PL5180A	4/2	306	0.04530	0.01882	407.8	AMP FAIL	
Station Fire Pmp 2A-A	480V SHDN BD 2AI-A	4D	2-MTR-25-9-A	200.0	1.00	230.0	1179	0.27	0.22515	0.06079	0.21578	2PL5003A	500MCM	2902	0.04399	0.07565	329.3 68%	PARALLEL COND	
	480V SHDN BD 2AI-A	4D										2PL5004A	500MCM	2902					
Spent Fuel Pit Pmp A-A	480V SHDN BD 2AI-A	90	0-MTR-78-12-A	100.0		113.8	647	0.42	0.41067	0.17248	0.37269	2PL48954	4/0	743	0.05119	0.04569	386.4	AMP FAIL	
CRD Mech Clr Fan 2C-A Mtr 2	480V SHDN BD 2AI-A	94	2-MTR-30-88/2-A	75.0		97.0													
REAC LUR COMPT CLR FAN 2C-A	480V SHDN BD 2AI-A	7D	2-MTR-30-77-A	40.0		54.0													
CRD MECH CLR FAN C-A MTR 1	480V SHDN BD 2AI-A	74	2-MTR-30-88/1-A	75.0		97.0													
Aux Bldg Gen Sply Fan 2B	480V SHDN BD 2B1-B	2B	2-MTR-30-105	100.0	1.15	120.0	626	0.31	0.42425	0.13152	0.40335	2PL5160	4/0	76	0.00524	0.00467	440.1		
COMPONENT COOL SYS PUMP 2B-B	480V SHDN BD 2B1-B	3C	2-MTR-70-33-B	350.0	1.15	389.0	2084	0.30	0.12744	0.03823	0.12157	2PL4742B	500MCM	675	0.01060	0.01823	384.2 70%	3.1 PARALLEL COND	
	480V SHDN BD 2B1-B	3C										2PL4742B	500MCM	675					
Elec Bd Rm AHU D-B	480V SHDN BD 2B1-B	7A	0-MTR-31-31D-B	50.0	1.15	62.5	360	0.37	0.73773	0.27296	0.68537	2PL4460B	4/2	538	0.11461	0.03309	403.4		
Reciprocating Charging Pmp	480V SHDN BD 2B1-B	3B	2-MTR-62-101	200.0		221.0													
Spent Fuel Pit Pmp C-S ALT FDR	480V SHDN BD 2B1-B	7B	0-MTR-78-35-S	100.0	1.15	115.0	647	0.42	0.41067	0.17248	0.37269	2PL4540B	1/0	268	0.03623	0.01606	410.3	AMP FAIL	
	480V SHDN BD 2B1-B	7B										2PL4541B	1/0	47	0.00535	0.00282		AMP FAIL	
Reac Lur Compt Clr Fan 2B-B	480V SHDN BD 2B1-B	7D	2-MTR-30-75-B	40.0		54.0													
CRD MECH CLR FAN 2B-B MTR 2	480V SHDN BD 2B1-B	100	2-MTR-30-92/2	75.0		97.0													
CRD Mech Clr Fan 2B-B Mtr 1	480V SHDN BD 2B1-B	7C	2-MTR-30-92/1-B	75.0		97.0													
Elec Bd Rm A/C B-B Cprsr	480V SHDN BD 2B2-B	2B	0-MTR-31-129/2-B	250.0	1.15	275.0	1825	0.24	0.14552	0.03493	0.14127	2PL4440B	4/0	315	0.01085	0.00959	411.8	PARALLEL COND	
	480V SHDN BD 2B2-B	2B										2PL4443B	4/0	315					
COMPONENT COOL SYS PUMP C-S	480V SHDN BD 2B2-B	2D	0-MTR-70-51-S	350.0	1.15	389.0	2084	0.30	0.12744	0.03823	0.12157	2PL4733B	500MCM	1500	0.02355	0.04160	328.0 70%	3.1 PARALLEL COND	
	480V SHDN BD 2B2-B	2D										2PL4734B	500MCM	1500					
	480V SHDN BD 2B2-B	2D										2PL4735B	500MCM						
	480V SHDN BD 2B2-B	2D										2PL4736B	500MCM						

REF. TITLE	BOARD NO.	CIRP	ENDUT. NO	UND. S	ELI	1IN	LEFF	IN	IN	DC	CABLE	CABLE	MOTOR KIN.	ACEL. REVESSES	REV.
											NO.	SIZE	LEN	DC	
LUG VOLTAGE 446.4V UNLESS NOTED OTHERWISE															
Air Bldg Gen Exhaust Fan 2B	480V SHIN BD 222-1	7A	2-MTR-31-20	125.0	1.00	147.0	850	0.29	0.21245	0.09561	0.23992	29.5170	470	444	0.0359
Fuel Pumpline Exhaust Fan B	480V SHIN BD 222-3	7C	0-MTR-31-39	105.0	1.15	120.0	624	0.31	0.12158	0.13194	0.44444	29.5100	470	248	0.0359
480V Shutdown Bd & PDU D-3	480V SHIN BD 222-B	7D	0-MTR-31-61-B	75.0	1.15	92.0	592	0.33	0.44862	0.14894	0.43349	29.5208	470	170	0.0171
Station Fire Pmp 25-B	480V SHIN BD 222-8	4D	2-MTR-31-18	200.0	1.00	230.0	1179	0.27	0.25115	0.08779	0.21578	29.5078	500	32	0.0167
														0.0038	
														32.4	322.4
														0.00070	
														0.04573	
														0.00070	
														29.5018	500
														29.5018	

THIS SHEET ADDED BY REV 4

FIG. 1-4 IN GCP/BS 32 10-31-92
CROTON 5 10-31-92

APPENDIX 10.5 - 404 SWITCHGEAR AND MOTOR CONTROL CENTER LOGIC SHARING TOPICS

[REDACTED] \$ MILLION MOTOR STARTING VOLTAGE = 151 OF 180V. EXCEPT FOTEC. CANE LENGTH 5000 IS DESIGN LENGTH PLUS 500 FT. 5% MINIMUM CABLE LENGTH

Report #5- GCP/JS Date 10-31-92
Received 10-31-92

10-10-10-10-10-10-10 INSTRUMENT 10-5 - 400 SERVICED AND 400 CONTROL CENTER MOTOR STARTING VEHICLES

5 HUNTER MOTOR STARTING VOLTAGE = 115 OR 460V, EXCITING RATIO .65 ACCELERATION TIME IS AT 10% STARTING VOLTAGE, SIXTY FORTY. 1 CABLE LENGTH OVER 15 FEET, LIGHT PLATE 100 FEET.

30-054-17

Prepared By G.C.P / RS Date 10-31-92

Checked By _____ Date 12-1-18

ATTACHMENT 10.1 - 48V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES
(TABLE 12 - UNIT 1 MCC MOTOR STARTING VOLTAGES FROM HBN-BEN-XS-T105-0002 R02)

EAC_TITLE	NODE_NO	BOARD	COMPT_EQUIPID_NO	LOAD	FLY	LRA	LRPP	In	Ns	JIN	OVAL_SIZE	Rho	CABLE	CIRCL	Re	jle	IND-BLOCK		MOTOR	MOTOR	TIME	REMARKS					
																	SIZE	No.	SIZE	LEN	Re	jle	START	SPARK	SPARK	SEC	
SHUTDOWN BD IN & PRESS FAN C-B	205	CIA_VENT	BD_181-8	8A	0-XTR-31-51-1	3.00	4.50	20.0	0.62	3.4150	5.4807	7.4120	734	0.07100	IPL36118	J12	110	0.3401	0.8122	427.7							
KRCW STRLIVER 1B-3	205	CIA_VENT	BD_181-8	8E	1-XTR-67-108-B	3.00	4.00	30.1	0.62	3.4292	5.4741	6.3274	736	0.05500	IPL39203	J14	2100	0.7062	0.1323	350.7	750						
Traveling Scra 1B-3	205	CIA_VENT	BD_181-8	8C	1-XTR-67-445-B	5.00	6.00	41.1	0.62	6.4618	3.9541	5.1104	738	0.09183	IPL39493	J12	2100	0.4181	0.3292	360.8	808						
TRCH Str 1B-1 Flush Fly	205	CIA_VENT	BD_181-8	8Z	1-YCY-67-108-B	0.33	0.75	5.75	0.60	45.1680	27.5214	36.1351	713	4.72080	IPL39388	J18	3425	2.9018	0.2415	395.8							
5th Vel Batt In Jack Fan 1A2-B	205	CIA_VENT	BD_181-8	7A	0-XTR-31-456A-B	1.50	2.50	14.5	0.62	18.3159	11.3353	11.1707	728	0.23500	IPL61502	J12	237	0.3895	0.4181	427.8							
125V Vel Batt In 1 Ex Fan 1A2-B	205	CIA_VENT	BD_181-8	7B	1-YTR-31-288-B	8.33	0.80	5.2	0.62	51.8135	31.6554	40.0732	717	2.20508	IPL36558	J12	274	0.5388	0.0218	425.1							
High Press Pipe Ins Ste A-B	205	CIA_VENT	BD_181-8	7C	0-XTR-26-14-B	0.75	2.05	8.5	0.62	31.3926	19.4634	21.6307	726	0.42100	IPL33182	J10	1246	1.5622	0.0078	431.9							
KRR Fap 1B-8 Infat FCR	205	CIA_VENT	BD_181-8	7D	1-FCV-75-21-B	5.20	10.60	60.0	0.10	4.6251	2.8553	3.5011	749	0.02283	IPL30008	J12	1170	0.2453	0.0220	417.2							
RESE To Spray Bdr 1A FCY	205	CIA_VENT	BD_181-8	7D	1-YCY-75-21-B	3.20	5.20	16.0	0.10	1.3713	4.4264	5.9018	732	0.18600	IPL18508	J18	615	0.5731	0.0475	411.8							
Safety Ins Fap 1B-8 In Clr Fan	205	CIA_VENT	BD_181-8	7E	1-XTR-30-175-B	5.00	8.10	50.1	0.62	5.2318	1.2810	4.1553	737	0.04300	IPL23918	J10	754	1.0708	0.9533	385.1	318.1	801	2.1				
Pen In El 452 Clr Fan 1B-8	205	CIA_VENT	BD_181-8	7F	1-XTR-30-187-B	3.00	4.00	25.0	0.62	10.6222	5.5964	4.3358	732	0.18600	IPL33118	J10	570	0.7250	0.0381	413.9	410.3	801	2.4				
Sktda Xinc In 1B End Fan 1A2-B	205	CIA_VENT	BD_181-8	7G	1-XTR-30-240-B	3.00	4.10	27.4	0.62	9.6327	6.4651	7.2390	731	0.07180	IPL28738	J12	232	0.5818	0.0208	419.9							
Sktda Xinc In 1B End Fan 1B1-B	205	CIA_VENT	BD_181-8	7H	1-XTR-30-240C-B	3.00	4.10	27.4	0.62	9.6327	6.4651	7.2390	731	0.07100	IPL24628	J12	276	0.5938	0.0211	419.7							
Cost In A/C Clr Fap 8-B	205	CIA_VENT	BD_181-8	7I	0-XTR-31-315-E/1-B	15.00	20.00	111.4	0.49	2.2431	1.0931	1.3551	749	0.00572	IPL34338	J18	337	0.2882	0.0239	388.3							
Cost In A/C Sys Oil Fap	205	CIA_VENT	BD_181-8	7J	0-XTR-31-315-E/1-C	3.00	4.10	32.6	0.62	8.2398	5.1455	6.5117	747	0.18600	IPL33383	J18	374	0.3173	0.0264	428.6							
KRR Fap 1B-8 In Clr Fan	205	CIA_VENT	BD_181-8	7K	1-XTR-30-175-B	3.00	6.10	45.0	0.62	5.3018	3.8591	4.6306	737	0.04180	IPL30418	J10	756	1.0705	0.9533	310.0	341.3	801	2.1				
5th Vill Batt In End Fan 1A2-B	205	CIA_VENT	BD_181-8	7N	0-XTR-31-456B-A	1.50	2.50	14.5	0.62	18.3159	11.3353	11.1707	728	0.23500	IPL61452	J12	237	0.5016	0.0181	427.8							
450V Bd In 1A Pe Sys Fan 1A2-B	205	CIA_VENT	BD_181-8	7C	1-XTR-31-456-B	3.00	4.60	28.0	0.62	5.4807	5.8807	7.1120	738	0.07180	IPL38878	J10	150	0.2025	0.0166	431.8							
Sktda Xinc In 1B End Fan 1A2-B	205	CIA_VENT	BD_181-8	7P	1-XTR-30-240-B	3.00	4.40	27.4	0.62	9.6327	6.4651	7.2390	731	0.07100	IPL28708	J12	418	-0.5417	0.0335	409.4							
Pen In El 737 Clr Fan 1B-8	205	CIA_VENT	BD_181-8	7E	1-XTR-30-195-B	3.00	4.00	25.3	0.65	10.6313	6.8227	7.5952	732	0.18600	IPL31011	J10	410	0.5535	0.0209	421.7	411.9	801	2.4				
Catty Chrg Fap 1B-8 In Clr Fan	205	CIA_VENT	BD_181-8	7L	1-XTR-30-182-B	5.00	6.10	45.0	0.62	5.3018	3.6591	4.6306	737	0.04180	IPL32118	J10	356	0.2466	0.0128	308.8	332.7	801	2.1				
125V Bd In 10 Pe Sys Fan 1A2-B	205	CIA_VENT	BD_181-8	7O	1-XTR-31-417-B	1.00	4.50	22.0	0.62	8.4550	5.8207	7.1120	738	0.07180	IPL34958	J10	150	0.2132	0.0181	431.5							
125V VEL BET AN II EXPAIR 1A2-B	205	CIA_VENT	BD_181-8	7Q	1-XTR-31-456B-A	1.50	2.50	14.5	0.62	18.3159	11.3353	11.1707	728	0.23500	IPL61452	J12	237	0.5016	0.0181	427.8							
Coat Ins Intake Man	205	CIA_VENT	BD_181-8	1021	4-XTR-30-246-B	1.00	1.00	5.5	0.65	49.1817	31.9641	37.3748	712	2.05000	IPL37378	J12	768	0.5678	0.0201	425.2							
Coat Ehd Energy Press Fan 1-B	205	CIA_VENT	BD_181-8	1021	1-XTR-31-456-B	1.00	1.70	15.0	0.62	17.7054	10.3974	11.1117	725	0.43500	IPL37352	J12	150	0.3225	0.0183	427.3	419.5						
450V Bd In 1A 1/C Cond 1B-8	205	CIA_VENT	BD_181-8	1021	1-XTR-31-456-B	20.00	25.80	132.0	0.62	1.4703	0.8603	1.4601	751	0.08318	IPL46748	J18	210	0.2782	0.0149	417.1							
450V Bd In 1B 1/C Cond 1B-8	205	CIA_VENT	BD_181-8	1021	1-XTR-32-243-B	20.00	25.00	112.0	0.65	1.4703	0.8603	1.4601	751	0.08318	IPL46938	J18	164	0.1392	0.0118	422.1							
Coat In A/C 8-B	205	CIA_VENT	BD_181-8	1103	0-XTR-31-11-B	50.00	72.00	113.0	0.50	0.6431	0.3215	0.3556	750	0.00124	IPL24048	J12	234	0.8216	0.0002	425.2							
Catty Chrg Fap In Clr Fan	205	CIA_VENT	BD_181-8	1221	1-XTR-30-182-B	3.00	4.30	26.7	0.62	3.9663	6.1671	7.4043	733	0.08000	IPL30211	J10	400	0.5300	0.0202	421.3							
Catty Chrg Press Fan 1-B	205	CIA_VENT	BD_181-8	1221	0-XTR-31-2-B	2.00	3.65	27.0	0.62	3.9363	6.0985	7.2176	731	0.04160	IPL32492	J8	174	0.1177	0.0123	431.6							
GASEOUS/EPL RASH NDS	205	CIA_VENT	BD_181-8	1221	0-PBL-50-1337	5.00	7.18	44.5																			
Cond Tac Fap Air End Box	205	CIA_VENT	BD_181-8	1271	1-XTR-31-99-B	1.40	1.80	5.4	0.15	49.1812	31.9642	37.3748	712	1.21200	IPL37398	J10	924	1.2124	0.0651	432.4							
Aux Chrg Fap 1B	205	CIA_VENT	BD_181-8	1321	1-XTR-32-4-B	1.00	1.80	12.5	0.62	21.1558	13.1413	15.1301	725	0.43500	IPL29348	J12	256	0.5710	0.0103	426.1							
Aux Chrg Dair Fap	205	CIA_VENT	BD_181-8	1321	0-XTR-32-4-B	1.00	1.80	11.1	0.62	21.5614	14.5975	11.4730	725	0.43500	IPL16165	J12	356	0.7356	0.0272	425.2							
Calmt Angelus Tac Fan 1B	205	CIA_VENT	BD_181-8	1321	1-XTR-65-74	5.00	8.10	50.1	0.62	5.2988	3.2840	4.1559	731	0.03483	IPL36160	J12	702	1.4813	0.0588	356.4					FAILED		

(UNIMCWD) \$ MINIMUM MOTOR STARTING VOLTAGE = 55% OF 160V, EXCEPT NOTED. \$5 ACCELERATION TIME IS AT 10% STARTING VOLTAGE, EXCEPT NOTED. * CABLE LENGTH USED IS DESIGN LENGTH PLUS 100 FEET. ** MAXIMUM CABLE LENGTH 2100 FEET.

Calc. STUDY-EEB-WBN-12-001
Attachment 3
Required Motor Starting Voltage
Page 12 of 26

WBN-EEB-ED-Q000-999-2007-0002, R0

ATTACHMENT 11.4,
Page 12 of 26

Required
Page 12 of

Required Motor Starting Voltage

30-Oct-92

Prepared By G.C.P./R.S. Date 10-31-92

Checked By Pat 10-31-92

WBN-EEB-MS-T106-D010 TO ATTACHMENT 10.6 - 480V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING TOLERANCES
(TABLE 62 - UNIT 1 MCC MOTOR STARTING TOLERANCES FROM WBN-EEB-MS-T106-0002 R10)

ENG. NAME	NODE_ID	BOARD	COMPY_EQUIPNO TO	LOAD	PLI	IRL	LPPF	In	In	jms	OVER SIZE	REL	CABLE NO.	CABLE SIZE LENGTH	Re	jke	IRD	BLOCK	MIC	ACCEL	TIME REMARKS	REV	
																	START	START	SEC	VOLT	VOLT	VOLT	
FRCK SCREEN WASH PUMP 1B-B	205	CER VENT BD	181-8	13D 1-MTR-67-440-A	40.00	19.20	230.0	0.38	0.5151	4.3480	0.8471	T54	0.0202	IPL3905B	2-1/8	2108	0.1120	0.0630	348.6	751			
	205	CER VENT BD	181-8	13D														74/8	1386	0.0955	0.0852		
Shd 1d In Chlr Pkg 1-B O. Pmp	205	CER VENT BD	181-8	13F2 0-MTR-31-(9/3-B	2.00	1.18	12.5	0.62	21.2485	13.1728	16.6700			IPL3763	1/8	370	0.4959	0.0261	433.2		4.75hp		
Toilet And Locker In Kbh Fan	204	CER VENT BD	182-B	28	0-MTR-31-41A	0.33	1.00	10.0	0.62	26.5581	16.4660	20.8375	T18	1.07500	IPL3654	1/2	210	0.14515	0.0161	418.3			
Supply In Hood Kbh Fan 1B	204	CER VENT BD	182-B	33	1-MTR-30-284	1.06	1.70	15.0	0.62	17.7054	10.3774	13.8317	T24	0.63280	IPL3626	1/2	540	1.1510	0.0413	412.2			
Supply In Hood Kbh Fan 1C	204	CER VENT BD	182-B	3C	1-MTR-30-46	1.00	1.70	15.0	0.62	17.7054	10.3774	13.8317	T24	0.63200	IPL3631	1/2	540	1.1610	0.0413	412.2			
South Main St Vlt Step Kbh Fan	204	CER VENT BD	182-B	48	1-MTR-30-302	3.00	4.60	32.0	0.52	8.2394	5.1456	6.5117	T33	0.48008	IPL3433	1/2	568	1.2212	0.0435	397.2			
South Main St Vlt Kbh Fan	201	CER VENT BD	182-B	63	1-MTR-30-25	3.00	4.60	32.0	0.62	8.2394	5.1456	6.5117	T33	0.01080	IPL2913	1/2	568	1.2112	0.0435	397.2			
Coat Rod Or Eptt In A/C IB	204	CER VENT BD	182-B	91	3-MTR-30-CRS	47.50	78.40	378.5	0.40	0.7017	0.2807	0.6431			IPL3671	2/6	501	0.0544	0.0301	410.6			
Dg 1A-1 Dryer Hood Exh Fan	217	DSL AUX BD	1A1-A	2A	1-MTR-30-455-A	0.33	1.00	10.0	0.52	26.5581	16.4660	20.8375	T19	1.66080	PL2580A	1/2	85	0.1828	0.0965	421.2			
DG 1A-1 RM EXH FAN 1-A	217	DSL AUX BD	1A1-A	2B	1-MTR-30-447-A	15.00	19.50	118.4	0.49	2.2431	1.0391	1.9553	T49	0.00572	PL2620A	1/2	105	0.0891	0.0074	429.6	422.8		
Dg 1A-1 Lube Oil Circ Pmp 1	217	DSL AUX BD	1A1-A	2B	1-MTR-32-31-A	1.00	1.95	8.3	0.62	32.1917	13.3598	25.2576	T26	0.42180	PL2735A	1/2	92	0.1578	0.0078	434.7			
Ex Hx Xy 1A1 & 1A2 SPAL VLV	217	DSL AUX BD	1A1-A	3A	1-PCT-67-55-A	0.13	0.35	2.60	0.60	102.1466	61.2880	81.7173	T8	13.95000	PL2146A	1/2	155	0.3333	0.0119	403.0	396.4	881	
Dg 1A-1 Day Trk Po Iffr Pmp 1-A	217	DSL AUX BD	1A1-A	3B	1-MTR-18-55-A	1.00	1.85	13.3	0.62	23.5444	14.5375	18.4730	T26	0.42180	PL2714A	1/2	96	0.2864	0.0077	432.7			
DG 1A-1 2XU LUMEOIL CIRC PMP A	217	DSL AUX BD	1A1-A	4B	1-MTR-92-100A-A	0.75	1.27	11.5	0.75	23.0404	17.3205	15.2753	T13	0.00000	PL3326A	1/2	60	0.1290	0.0045	428.9		0-05146-A	
Dg 1A-1 Pm1 Vent Fan	217	DSL AUX BD	1A1-A	4B	1-MTR-30-491-A	15.00	20.00	118.4	0.49	2.2431	1.0391	1.9553	T48	0.00825	PL3444A	1/8	130	0.1104	0.0092	427.0	419.2		
Dg 1A-1 480V Elec Bd Exh Fan	217	DSL AUX BD	1A1-A	4C	1-MTR-30-459-A	2.00	2.70	22.6	0.62	11.7514	7.2855	9.2202	T29	0.23700	PL2520A	1/0	95	0.1203	0.0067	431.4			
Dg 1A-1 Air Cprse 1	217	DSL AUX BD	1A1-A	5A	1-MTR-32-181	5.00	7.10	44.5	0.62	5.9695	3.7011	4.5836	T39	0.02578	PL2195	1/2	108	0.2158	0.0077	428.5	428.7		
Dg 1A-1 Muffler In Kbh Fan	217	DSL AUX BD	1A1-A	6A	1-MTR-30-463	1.50	2.65	20.6	0.62	13.2791	8.2330	16.4188	T28	0.29300	PL2235	1/2	62	0.1333	0.0097	431.1	423.3		
DG 1A-1 RM EXH DILIGEN CIRC PMP A	218	DSL AUX BD	1A2-A	2A	1-MTR-82-100B-A	0.75	1.27	11.5	0.75	23.0348	17.3205	15.2753	T23	0.00800	PL3321A	1/2	174	0.3784	0.0135	423.4		0-05146-A	
DG 1A-1 RM EXH FAN 2-A	218	DSL AUX BD	1A2-A	2B	1-MTR-30-451-A	15.00	19.50	118.4	0.49	2.2431	1.0391	1.9553	T49	0.00572	PL2629A	1/2	66	0.0569	0.0047	433.3	425.4		
Dg 1A-1 Lube Oil Circ Pmp 2	218	DSL AUX BD	1A2-A	2B	1-MTR-82-42-A	1.00	1.70	15.0	0.62	17.7054	10.3774	13.8317	T24	0.63200	PL2736A	1/2	170	0.3635	0.0130	424.5			
Ex Hx EK 1A1 & 1A2 SUP VLV	218	DSL AUX BD	1A2-A	3A	1-PCT-67-51-A	0.13	0.35	2.60	0.60	102.1466	61.2880	81.7173	T8	13.95000	PL2140A	1/2	110	0.2365	0.0084	404.0			
Dg 1A-1 Day Trk Po Iffr Pmp 2-A	218	DSL AUX BD	1A2-A	3B	1-MTR-11-54-A	1.00	1.85	11.3	0.62	23.5444	14.5375	18.4730	T26	0.42180	PL2782A	1/2	172	0.3698	0.0132	430.7			
DG 1A-1 AIR CRSE 1	218	DSL AUX BD	1A2-A	5A	1-MTR-82-182	5.00	7.16	44.5	0.62	5.9695	3.7011	4.5836	T39	0.01078	PL2108	1/2	74	0.1591	0.0057	431.1	(23.3)		
Dg 1A-1 Air Cprse 2	218	DSL AUX BD	1A2-A	5B	9-PKG-35-37	2.00	3.10	25.0	0.62	10.6232	6.5864	8.3350			PL2765	1/0	158	0.1025	0.0106	434.5			
Lube Oil & Co2 Stor In Exh Fan	218	DSL AUX BD	1A2-A	6A	1-MTR-30-470	0.75	1.40	12.5	0.62	21.2465	13.1728	16.5700	T22	0.05900	PL2527	1/2	140	0.3018	0.0107	424.7			
Dg 1A-1 Battery Hood Exh Fan	219	DSL AUX BD	1B1-B	2A	1-MTR-30-457-A	0.33	1.00	10.0	0.52	26.5581	16.4660	20.8375	T18	1.67500	PL2590B	1/2	166	0.2159	0.0077	430.7			
DG 1A-1 RM EXH FAN 1-B	219	DSL AUX BD	1B1-B	2B	1-MTR-30-449-B	15.00	19.50	118.4	0.49	2.2431	1.0391	1.9553	T49	0.00572	PL2635B	1/2	132	0.1121	0.0093	422.1	419.3		
Dg 1A-1 Lube Oil Circ Pmp 1	219	DSL AUX BD	1B1-B	2B	1-MTR-82-41-B	1.00	2.05	11.3	0.62	23.5144	14.5973	18.4730	T26	0.42180	PL2740B	1/2	152	0.3268	0.0116	431.2			
Ex DG EXH RM SUP VLV IN HDE 1B	219	DSL AUX BD	1B1-B	3A	1-PCT-67-47-B	0.13	0.39	2.60	0.60	102.1466	61.2880	81.7173	T8	13.95000	PL2147B	1/2	158	0.3397	0.0121	403.7	396.4	404	
Dg 1A-1 Day Trk Po Iffr Pmp 1-B	219	DSL AUX BD	1B1-B	3B	1-MTR-32-181-B	1.00	1.85	11.3	0.62	23.5444	14.5973	18.4730	T26	0.42180	PL2735B	1/2	168	0.3512	0.0129	430.8			
Dg 1A-1 Air LubOil Circ Pmp A	219	DSL AUX BD	1B1-B	4B	1-MTR-82-100A-B	0.75	1.27	11.5	0.75	23.0348	17.3205	15.2753	T23	0.00800	PL3322B	1/2	60	0.1290	0.0046	426.9		0-05146-A	
Dg 1A-1 Pm1 Vent Fan	219	DSL AUX BD	1B1-B	4B	1-MTR-30-453-B	15.00	20.00	118.4	0.49	2.2431	1.0391	1.9553	T48	0.00825	PL3152B	1/8	150	0.3274	0.0106	425.1	417.4		
DC 1A-1 480V SLCG BD RM EX FAN	219	DSL AUX BD	1B1-B	4C	1-MTR-30-461-B	2.40	2.75	22.6	0.62	11.7514	7.2855	9.2202	T29	0.23700	PL2530B	1/0	38	0.1323	0.0063	431.3			
Dg 1A-1 Air Cprse 2	219	DSL AUX BD	1B1-B	5A	1-MTR-82-211	3.00	7.10	48.5	0.62	5.9691	3.7002	4.5836	T39	0.02878	PL2215	1/2	126	0.2518	0.0092	426.5	418.7		

{ULMCCWD} \$ MINIMUM MOTOR STARTING VOLTAGE = 85% OF 460V, EXCEPT NOTED. \$ ACCELERATION TIME IS AT 80% STARTING VOLTAGE, EXCEPT NOTED. * CABLE LENGTH USED IS BUSBAR LENGTH PLUS 100 FEET. ** MAXIMUM CABLE LENGTH (1200 FEET

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30-Oct-01

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Prepared By GCP/RS Date 10-31-97
Checked By GCP/RS Date 10-31-97

WBN-EEB-MS-1000-0001 Rev 06
(TABLE 12 - UNIT 1 AC MOTOR STARTING VOLTAGES FROM FPN-EEB-MS-1000-0002 (11))

FIG. NAME	TYPE	NAME	COMPT	EQUIP/ITEM	LOAD	P1	T1	L1	R1	S1	SW1	CABLE	IC	IEC	TOP BLOCK MIN ACCEL	TOP BLOCK MAX TIME REMAIN	STAY STAY STAY SEC	VOLT VOLT VOLT	(40) (132) (5) (35)
By 10-5 Muffler Pa 210 Pab	210	BSL ACT AD 101-3	1A	1-MTR-30-415	1.50	2.15	20.0	0.62	13.2791	6.2330	10.4103	721	0.23500	FL2243	112	55	0.1394	0.0050	431.0 423.2
By 10-5 LubOil Circ Pab 8	220	BSL ACT AD 101-4	2A	1-MTR-42-1012-1	0.75	1.27	11.5	0.75	23.8146	17.3705	15.2153	923	0.20600	FL3233	112	116	0.3184	0.0135	423.4
By 10-5 Lub Oil Fan 2-4	220	BSL ACT AD 101-4	2B	1-MTR-30-1013-1	15.00	11.50	118.4	0.49	7.2431	1.9791	1.9553	749	0.60317	FL26653	112	116	0.4834	0.0071	429.1 421.3
By 10-5 Lub Oil Circ Pab 1	220	BSL ACT AD 101-4	2D	1-MTR-42-1012-1	1.00	2.05	11.3	0.62	33.3444	14.5915	10.4139	526	0.12100	FL2241B	112	116	0.3193	0.0142	430.3
Zener Diode Spec Vbf 21	220	BSL ACT AD 101-4	2E	1-MTR-42-1015-8	0.13	0.38	7.60	0.59	10.1446	61.7210	61.7213	98	13.56000	FL2313B	112	130	0.2795	0.0191	443.9
By 10-5 Lub Oil Fan Pab 2-4	220	BSL ACT AD 101-4	3A	1-MTR-30-1013-8	1.00	1.15	51.3	0.42	23.8146	14.5915	10.4139	526	0.12100	FL2241B	112	116	0.3140	0.0121	431.4
By 10-5 Air Cpt Pa 210 Pab 1	220	BSL ACT AD 101-4	3A	1-MTR-30-210	5.60	7.10	44.5	0.52	5.4661	3.3092	4.6925	824.5	0.02170	PC2250	112	130	0.2150	0.0017	424.5 420.7
D.C. IN EER VBF 2	225	BSL ACT AD 101-5	4B	0-MTR-30-117-5	15.00	11.40	105.2	0.48	2.5256	1.2316	2.1994	C7216	0.00570	PA2176S	112	116	0.00314	0.00710	430.3
D.C. IN EER VBF 1	225	BSL ACT AD 101-5	4B	0-MTR-30-314-5	15.00	14.30	105.2	0.48	2.5256	1.2316	2.1994	C7216	0.00570	PA2176S	112	116	0.00314	0.00710	430.3
ASPH AND AD IN EER VBF	225	BSL ACT AD 101-5	CA	0-MTR-30-311-5	1.50	1.35	13.4	0.62	15.8197	12.3341	15.3615	C7216	0.42000	PA2176S	110	119	0.1520	0.00815	431.1
6.4KV HS. IN	225	BSL ACT AD 101-5	CE	0-MTR-30-310-5	10.00	12.04	78.3	0.53	5.3460	1.7440	2.4834	CL	0.10160	FL43555	112	116	0.3449	0.0071	431.4
REACT TO BSL GEN 0C-5 EER VBF	225	BSL ACT AD 101-5	DE	1-MTR-42-1013-5	0.13	0.15	3.26	0.50	41.4666	43.8366	33.1323	CP5410B	0.76060	PE2301S	112	140	0.3018	0.0197	405.0
REACT TO BSL GEN 0C-5 EER VBF	225	BSL ACT AD 101-5	DE	1-MTR-42-1017-5	0.13	0.15	3.76	0.40	41.4666	43.8366	33.1323	CP5410B	0.76060	PE2301S	112	120	0.2715	0.0199	405.0
DC AIR COMP 1	225	BSL ACT AD 101-5	DE	1-MTR-42-1017-5	0.13	0.15	3.76	0.40	41.4666	43.8366	33.1323	CP5410B	0.76060	PE2301S	112	120	0.2715	0.0199	405.0
DC AIR COMP 2	225	BSL ACT AD 101-5	DE	0-MTR-30-1018-5	1.00	1.00	10.8	0.62	26.4701	16.4168	20.7952	C7216	0.12800	FL2324S	112	116	0.1631	0.0158	433.3
D.C. DAY TANK POF TRANS PMP 1	225	BSL ACT AD 101-5	DE	0-MTR-30-1018-5	1.00	2.40	10.0	0.52	26.4701	16.4168	20.7952	C7216	0.12800	FL2324S	112	206	0.4380	0.0153	431.3
D.C. DAY TANK POF TRANS PMP 2	225	BSL ACT AD 101-5	DE	0-MTR-30-1018-5	1.00	2.40	10.0	0.52	26.4701	16.4168	20.7952	C7216	0.12800	FL2324S	112	206	0.4380	0.0153	431.3
BSL GEN EIG A Lube Oil PMP 1	225	BSL ACT AD 101-5	EA	0-MTR-42-1013-5	2.00	3.50	22.6	0.42	11.7477	7.7455	5.2324	C7113	0.03100	FL2317S	112	150	0.3235	0.0115	430.0
BSL GEN EIG B Lube Oil PMP 2	225	BSL ACT AD 101-5	EA	0-MTR-42-1013-5	2.00	3.50	22.6	0.42	11.7477	7.7455	5.2324	C7113	0.03100	FL2317S	112	150	0.3235	0.0115	430.0
FUEL OIL TRANSFER HS EER VBF	225	BSL ACT AD 101-5	CA	0-MTR-30-323-1	6.50	1.00	10.0	0.42	26.5511	16.4600	20.4915	C7113	0.17000	FL2316S	112	150	0.3235	0.0115	416.7
EG ELEC PUMP 712125-1 PMP	225	BSL ACT AD 101-5	DE	0-MTR-30-310-1	20.00	11.00	100.3	0.51	2.6486	1.1036	2.2558	C7113	0.01660	FL2315S	112	232	0.1970	0.0166	419.6
DE AIR COMP 1	225	BSL ACT AD 101-5	DE	0-MTR-42-310-1	5.00	7.10	44.5	0.42	5.1655	3.1021	6.1655	C7113	0.16335	FL2315S	112	116	0.2135	0.0053	423.4
DE AIR COMP 2	225	BSL ACT AD 101-5	DE	0-MTR-42-310-1	5.00	7.10	44.5	0.42	5.1655	3.1021	6.1655	C7113	0.16335	FL2315S	112	120	0.2536	0.0052	426.4
BSG KDFP4F AND EER PMP	225	BSL ACT AD 101-5	EA	0-MTR-30-323-1	1.50	1.95	12.5	0.62	21.2463	13.1720	16.4200	C7113	0.12000	FL2315S	112	155	0.1141	0.0042	422.4
Boric Acid Transfer Pmp 1A-4	225	BSL ACT AD 101-5	EA	1-MTR-57-110-1	1.50	1.00	105.2	0.49	2.5234	1.3165	2.1395	C7113	0.01397	FL216101A	112	134	0.3585	0.01056	402.3
Boric Acid Transfer Pmp 1A-1	225	BSL ACT AD 101-5	EA	1-MTR-57-110-1	1.50	1.00	105.2	0.49	2.5234	1.3165	2.1395	C7113	0.01397	FL216101A	112	134	0.3085	0.01056	403.4
TRIM VALVE 555 BSR PMP 1A-4	225	BSL ACT AD 101-5	EA	1-MTR-57-110-1	18.00	14.00	20.0	0.53	3.7832	2.0451	3.2042	C7113	0.31214	FL2161204	112	136	0.3631	0.0302	411.2
THE MIX TO COMP 1A	225	BSL ACT AD 101-5	EA	1-MTR-57-110-1	2.00	3.10	22.6	0.62	11.7476	7.7455	5.2324	C7113	0.14760	FL2161450	112	600	1.2406	0.0459	406.5
CHARGE CHARG EP 1A-1 PMP	225	BSL ACT AD 101-5	EA	1-MTR-57-110-1	2.00	3.10	22.6	0.62	11.7476	7.7455	5.2324	C7113	0.14760	FL2161450	112	600	1.2406	0.0459	406.5
FOR EER TO COMP 100	225	BSL ACT AD 101-5	EA	1-MTR-57-110-1	8.13	8.50	1.58	0.60	75.0103	45.5712	50.7043	C7113	0.25000	FL2161204	112	433	0.6116	0.0119	405.9 398.5
1st Crnt 15 CIR SUP VBF [1]	225	BSL ACT AD 101-5	EA	1-MTR-57-110-1	8.13	8.50	1.58	0.60	75.0103	45.5712	50.7043	C7113	0.25000	FL2161204	110	60	0.6116	0.0142	405.9 398.5
HPP 75 A 100 KWT TO 1000	225	BSL ACT AD 101-5	EA	0-1CF-14-5-4	6.13	9.75	5.7	0.60	46.5932	27.3553	31.2745	C7113	0.7105	FL2161204	112	1045	2.12468	0.0799	385.2

1000V 1.5 MINIMUM MOTOR STARTING VOLTAGE = 10% OF 400V. EXCEPT FOR 10. 5% ACCELERATION TIME IS AT 10% STARTING VOLTAGE, EXCEPT NOTED. 1. CABLE LENGTH USED IS DESIGN LENGTH 100' FEET. 2. MAXIMUM CABLE LENGTH <100' FEET.

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(Added by Rev 5)

Revista

Prepared by G.S.C.P. File # 11-1-92
Entered by G.S.C.P. Date 11/1/02

10-11-12-13-14-15-16-17-18-19-20-21-22-23-24-25-26-27-28-29-30-31-32-33-34-35-36-37-38-39-40-41-42-43-44-45-46-47-48-49-50-51-52 - QM1 MOTOR SWING POSITION PUMP 10-11-12-13-14-15-16-17-18-19-20-21-22-23-24-25-26-27-28-29-30-31-32-33-34-35-36-37-38-39-40-41-42-43-44-45-46-47-48-49-50-51-52 - QM2 MOTOR CONTROL CENTER MOTOR SWING POSITION PUMP 10-11-12-13-14-15-16-17-18-19-20-21-22-23-24-25-26-27-28-29-30-31-32-33-34-35-36-37-38-39-40-41-42-43-44-45-46-47-48-49-50-51-52

10-001-02

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05-Nov-93

SI-EER-MS-T106-0010 EG ATTACHMENT 10.6 - 480V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES
TABLE L2 - UNIT 1 MCC MOTOR STARTING VOLTAGES FROM WBN-EER-MS-T106-0002 Rev 1

AC_TITLE	NODE_NO	BOARD	COMPT 10	EQUIPID_NO	LOAD	PLI	LEA	LPPF	IC	IE	JXL	OVOL	REL	CABLE SIZE	CABLE NO.	CABLE SIZE LENGTH	RC	JIC	IND	BLOCK	MIN	ACCEL	REV		
																			START	START	START	SEC			
																			VOlt	VOLT	VOLT	(sec)	(440) (432) (5) (66)		
score last fm Circ Fan 1A	235	RMOV BD 1A1-A	150																						
score last fm Circ Fan 1A	235	RMOV BD 1A1-A	16A 1-MTR-31-265	3.00	4.30	26.7	0.62	9.9469	6.1671	7.8043	T33	8.88000	1PL6300	#10	456	0.61556	0.0321	420.7							
score last fm Circ Fan 1A	235	RMOV BD 1A1-A	16B 1-MTR-77-129	1.50	2.40	16.9	0.62	15.670	9.7259	12.3021	T27	8.36200	1PL6268	#10	435	0.54773	0.0307	423.0							
score last fm Circ Fan 1A	235	RMOV BD 1A1-A	16D 0-PCV-26-141-A	0.26	0.55	5.7	0.60	46.5932	27.9559	37.2745	T12	7.53000	1V19801	#12	1816	2.1444	0.0777	382.2							
score last fm Circ Fan 1A	235	RMOV BD 1A1-A	16D																						
score last fm Circ Fan 1A	235	RMOV BD 1A1-A	16Z 0-PCV-26-7-A	0.26	0.55	5.7	0.60	46.5932	27.9559	37.2745	T12	7.53000	1V1987A	#12	1030	2.2145	0.0788	382.0							
score last fm Circ Fan 1A	235	RMOV BD 1A1-A	16E																						
score last fm Circ Fan 1A	235	RMOV BD 1A1-A	16Z 1-MTR-31-303/2	3.00	4.60	32.0	0.62	8.2994	5.1456	6.5117		1PL6289	#10	636	0.8505	0.0444	411.0								
score last fm Circ Fan 1A	235	RMOV BD 1A1-A	176 1-PCV-26-249-A	0.67	2.10	10.5	0.60	25.2934	15.1761	20.2348	T21	8.07000	1V19147A	#12	456	1.4954	0.0532	412.9 405.4							
score last fm Circ Fan 1A	235	RMOV BD 1A1-A	176 1-PCV-26-242-A	0.67	2.10	10.5	0.60	25.2934	15.1761	20.2348	T21	8.07000	1V19369A	#12	532	1.1436	0.0407	416.6 409.1							
score last fm Circ Fan 1A	235	RMOV BD 1A1-A	177																						
efueling Wtr Pfrcs Pmp A-A	235	RMOV BD 1A1-A	18A 0-MTR-78-19-A	26.00	26.00	145.0	0.46	1.6326	0.8425	1.6263	T51	8.00318	1PL6385A	#2	818	0.1746	0.8503	409.4							
efueling Wtr Pfrcs Pmp A-A	235	RMOV BD 1A1-A	18C 1-MTR-31-303/1	3.00	4.20	30.1	0.62	6.6292	5.4741	6.9274	T33	8.08000	1PL6281	#12	584	1.2556	0.0447	398.8							
efueling Wtr Pfrcs Pmp A-A	235	RMOV BD 1A1-A	18D 0-MTR-61-226	1.00	2.05	12.5	0.62	21.1787	15.1308	16.5152	T26	6.42100	1PL6265	#12	500	1.0750	0.0383	420.4							
efueling Wtr Pfrcs Pmp A-A	235	RMOV BD 1A1-A	18E 1-PCV-26-243-A	0.67	2.10	10.5	0.60	25.1934	15.1761	20.2348	T21	8.07000	1V19165A	#12	486	1.0445	0.0372	417.7 418.1							
EFGR Edr 1 Isln Vlv	236	RMOV BD 1A2-A	2A 1-PCV-3-116A-A	0.25	0.55	4.3	0.60	61.7631	37.0578	49.4104	T11	9.25000	1V19530A	#12	312	0.6657	0.0243	394.4							
EFGR Edr 1 Isln Vlv	236	RMOV BD 1A2-A	2B 1-PCV-3-116A-A	0.25	0.55	4.3	0.60	61.7631	37.0578	49.4104	T11	9.25000	1V1950A	#12	320	0.6800	0.0245	395.4							
EFPR Turb Stm Sop Fm Stm Gen 1	236	RMOV BD 1A2-A	2B 1-PCV-1-15-A	1.00	2.80	17.8	0.60	14.2923	8.9522	11.9362	T24	8.63200	1V1830A	#16	1206	1.6206	0.0365	399.5							
EFGR Turb Stm Sop Fm Stm Gen 1	236	RMOV BD 1A2-A	2B 1-PCV-1-17-A	1.00	2.80	17.8	0.60	14.2923	8.9522	11.9362	T24	8.63200	1V1620A	#16	1206	1.6206	0.0365	399.5							
EFGR Edr 1 Isln Vlv	236	RMOV BD 1A2-A	3A 1-PCV-3-136A-A	0.33	0.75	5.7	0.60	46.5932	27.9559	37.2745	T13	6.15000	1V19950A	#12	436	0.9374	0.0334	400.5							
EFGR Edr 1 Isln Vlv	236	RMOV BD 1A2-A	3B 1-PCV-3-136A-A	0.33	0.75	5.7	0.60	46.5932	27.9559	37.2745	T13	6.15000	1V1950A	#12	436	0.9374	0.0334	400.5							
EI Gen No 1 PW Isln Vlv	236	RMOV BD 1A2-A	3D 1-PCV-3-33-A	39.48	48.10	494.0	0.45	0.5376	0.2419	6.4801	T53	8.00226	1V2980A	#6	800	0.0406	0.0468	390.5 383.4	70%						
EI Gen No 1 PW Isln Vlv	236	RMOV BD 1A2-A	4A 1-PCV-3-191	1.60	4.00	25.0	0.60	10.4232	6.3735	8.4986	T26	9.15506	1V13566	#12	372	0.6586	0.0245	415.2							
EI Gen No 1 PW Isln Vlv	236	RMOV BD 1A2-A	4B 1-PCV-3-192	1.60	4.00	25.0	0.60	10.4232	6.3739	8.4986	T26	9.15500	1V1323C	#12	750	1.6125	0.0374	392.5							
EI Gen No 3 PW Isln Vlv	236	RMOV BD 1A2-A	4D 1-PCV-3-87-A	39.40	48.10	494.0	0.45	0.5376	0.2415	6.4801	T53	8.00226	1V2990A	#6	800	0.0406	0.0468	390.5 383.4	70%						
Sample Hx Isln Vlv	236	RMOV BD 1A2-A	52 1-PCV-70-215-A	0.13	0.80	1.15	0.60	64.3115	50.5169	47.4492	T11	9.25000	1V2566A	#12	550	1.1825	0.0421	407.7							
Sply Edr 1A To Hdr 25 Isln Vlv	236	RMOV BD 1A2-A	56 1-PCV-67-147-A	0.70	2.30	12.00	0.60	22.1313	15.2791	17.7054	T26	6.42100	1V2430A	#12	334	0.5051	0.0373	426.3							
Hydrogen Det Sys	236	RMOV BD 1A2-A	5D1 1-H2XN-43-206	4.16	5.22																				
Detnt Spray Hx 1A Sop Coat Vlv	236	RMOV BD 1A2-A	5E 1-PCV-67-125-A	0.33	0.55	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	1V220GA	#12	304	0.6556	0.0233	419.5							
Detnt Spray Hx 1A Sop Coat Vlv	236	RMOV BD 1A2-A	5F 1-PCV-67-126-A	0.33	0.55	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	1V220BA	#12	472	1.0146	0.0361	419.5							
EFPR Turb St Sply Frz St gen 4	236	RMOV BD 1A2-A	6A 1-PCV-1-16-A	1.00	2.80	17.8	0.60	14.9203	8.9522	11.9362	T24	8.63200	1V1820A	#16	1208	1.6208	0.0345	399.5							
EHS Sys Isln Bypass Vlv	236	RMOV BD 1A2-A	6D 1-PCV-74-8-A	1.60	4.00	25.0	0.60	10.5232	6.3739	8.4986	T31	0.14100	1V2140A	#12	341	0.8152	0.0291	409.7							
EHS Sys Isln Bypass Vlv	236	RMOV BD 1A2-A	6D																						
EHCR Edr 1A Isln Vlv before Str	236	RMOV BD 1A2-A	75 1-PCV-67-22-A	0.33	0.55	5.70	0.60	46.5932	27.9559	37.2745	T17	2.20500	1V2338A	#5	2100	1.7025	0.1481	404.2							

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ATTACHMENT 11.4,

Attachment 3

Required Motor Starting Voltage

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THIS SHEET ADDED BY REV_6

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ATTACHMENT 11.4,
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ग्रन्थालय असाम सरकारी कैलेज ग्रन्थालय
ग्रन्थालय असाम सरकारी कैलेज ग्रन्थालय

• 1/2 HORSEPOWER, 115 VOLTS, 60 CYCLES, 1725 RPM, 1.15 AMPERES, 1.15 INCHES OF WATER HEAD, 1.15 INCHES OF VACUUM, 1.15 HORSES POWER.

SH-EEE-MS-T106-0010 Rev ATTACHMENT 10.6 - 480V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES
TABLE D2 - LIST 1 MCC MOTOR STARTING VOLTAGES FROM WBN-EEE-MS-T106-0002 (118)

LG_TITLE	NODE_NG	BOARD	COMP	EQUIPID_NO	LOAD	PLI	LRB	LRPP	Rt	Rn	JIC	OVDL	RtoI	CABLE	Rc	JIC	1NE	BLOCK	MIS	ACCEL	REMARKS	REV		
																	SIZE	SIZE	LENG	NO.	START	START	TIME	
																	VOLT	VOLT	VOLT	VOLT	SEC			
																	(440)	(432)	(\$)	(\$)	(\$)			
IS Aeron Isol Tank Shutoff Vlv	237	RMOV BD 181-E	11E	1-PCV-63-25-B	1.96	3.56	26.0	0.60	10.2147	6.1286	8.1717	T29	0.23700	IV26878	110	642	0.8667	0.0453	410.6	403.1				
IS Arm Isol Throlt Shutoff Vlv	237	RMOV BD 181-E	12A	1-PCV-63-40-B	1.96	3.56	26.0	0.60	10.2147	6.1286	8.1717	T29	0.23700	IV27038	110	746	1.0071	0.0526	404.1					
IS Pmp 18-E Inlet Vlv	237	RMOV BD 181-E	12B	1-PCV-63-46-B	1.96	3.56	26.0	0.60	10.2147	6.1286	8.1717	T29	0.23700	IV2350E	110	1200	1.0182	0.0846	402.7					
atmt Sump To RHE Pmp E-E	237	RMOV BD 181-E	12D	1-PCV-53-73-E	13.00	18.40	131.0	0.50	1.5395	0.9693	1.6708	T46	0.01080	IV3140B	110	36	0.0405	0.0021	415.1					
																110	1170	0.1582	0.0702					
IS To RCS Loops 144 PCV	237	RMOV BD 181-E	12E	1-PCV-63-94-B	1.66	4.00	25.0	0.60	10.6232	6.3735	8.4986	T30	0.17908	IV2380E	110	744	0.3971	0.0513	424.2					
IS Pmp 18-B Ductlet PCV	237	RMOV BD 181-E	13A	1-PCV-63-153-B	1.96	3.56	26.0	0.60	10.2147	6.1286	8.1717	T29	0.23700	IV2368E	110	664	1.4275	0.0508	396.7					
IS Pmp OUT RCS LP 244 E, LEG	237	RMOV BD 181-E	13B	1-PCV-63-157-B	1.96	3.56	26.0	0.60	10.2147	6.1286	8.1717	T29	0.23700	IV2392E	110	551	0.7433	0.0386	413.8					
IS 18-E Duct To RHE Shutoff Vlv	237	RMOV BD 181-E	13D	1-PCV-63-175-B	0.79	2.56	16.0	0.60	16.5988	0.9593	15.2791	T24	0.63780	IV2302B	110	764	1.6426	0.0384	403.5					
atmt Spray Hdr 16 Isol Vlv	237	RMOV BD 181-E	14A	1-PCV-72-72-E	3.26	5.20	36.0	0.56	7.3773	4.4264	5.9018	T32	0.10000	IV2630E	110	430	0.5805	0.0303	414.4	407.2	80%			
Spray Hdr 16 Isol Vlv	237	RMOV BD 181-E	14B	1-PCV-72-41-E	1.96	3.56	26.0	0.60	10.2147	6.1286	8.1717	T29	0.23700	IV2752B	110	732	0.9882	0.0516	407.4					
atmt Sump To Spray Hdr 18 PCV	237	RMOV BD 181-E	14C	1-PCV-72-45-E	3.26	5.20	36.0	0.60	7.3773	4.4264	5.9018	T31	0.10000	IV1800E	110	675	0.9351	0.0478	402.6					
IS Pmp 18-B Min Flow Vlv	237	RMOV BD 181-E	15B	1-PCV-74-24-B	0.12	0.45	3.2	0.56	84.3115	50.5865	67.4492	T9	11.72000	IV1915E	110	821	1.7759	0.0632	398.5	391.3	80%			
IS Rx 18 Bypass Vlv	237	RMOV BD 181-E	15D	1-PCV-74-35-B	1.96	3.56	26.0	0.60	10.2147	6.1286	8.1717	T29	0.23700	IV2612B	110	654	1.4061	0.0500	397.3					
Score Inst Rx Circ Fan 1h	237	RMOV BD 181-E	16A	1-MTR-31-266	3.00	4.30	25.7	0.62	9.9469	6.1671	7.8043	T33	0.08000	IPL64310	110	430	0.3805	0.0303	421.1					
DCM TO COMP 7D	237	RMOV BD 181-E	16P2																					
annulus Standpipe Isol Vlv	237	RMOV BD 181-E	17B	1-PCV-26-241-S	0.67	2.10	5.0	0.60	53.1162	31.2867	42.4930	T35	1.66800	IV9155E	110	650	1.8275	0.0630	421.4	414.7				
IS Pmp 2-B Lube Oil Pump E-E	237	RMOV BD 181-E	17D	1-MTR-3-126B-E	0.25	0.56	3.5	0.62	75.0003	47.0454	53.5736	T33	6.15000	IPL6330E	110	500	1.0750	0.0383	414.3					
Score Inst Rx Ch Wtr Cprst 1E	237	RMOV BD 181-E	17P2	1-MER-31-324/2	5.06	4.80	95.6	0.62	2.7956	1.7333	2.1354		IPL64291	110	430	0.5805	0.0303	382.3						
Refueling Wtr Pfrz Pmp E-E	237	RMOV BD 181-E	18A	0-MTR-78-10-E	20.06	26.00	145.0	0.16	1.8316	6.6425	1.5263	T51	0.00316	IPL6430E	110	876	0.1874	0.0504	407.3					
Score Inst Rx Circ Pump 1E	237	RMOV BD 181-E	18C	1-MTR-31-324/1	3.06	4.20	30.1	0.62	8.6292	5.4741	6.9274	T33	0.05000	IPL6285	110	724	1.1244	0.0581	403.3					
DCM Bldg 8 Isol Vlv	237	RMOV BD 181-E	18D	0-MTR-41-2	1.06	2.20	12.5	0.62	21.1958	11.1113	16.6301	T26	0.42100	IPL6275	110	344	1.1695	0.0416	413.2					
DCM Bldg 8 Shflst Vlv	237	RMOV BD 181-E	18E	0-PCV-26-142-E	0.26	0.55	5.7	0.16	46.5932	27.9559	37.2745	T12	7.53000	IV995E	110	1282	2.7563	0.0991	375.2	404				
DCM Bldg 8 Shflst Vlv	237	RMOV BD 181-E	18F																					
DCM Bldg 8 Isol Vlv	238	RMOV BD 182-E	2A	1-PCV-3-1261-E	0.25	0.55	4.3	0.66	61.7631	37.0578	49.4104	T11	9.25000	IV2940E	110	472	1.0148	0.0361	397.1					
DCM Bldg 8 Isol Vlv	238	RMOV BD 182-E	2B	1-PCV-3-1262-E	0.25	0.55	4.3	0.66	61.7631	37.0578	49.4104	T11	9.25000	IV2950E	110	476	1.0016	0.0356	397.1					
Flow To AFMP Turb Isol Vlv	238	RMOV BD 182-E	2E	1-PCV-3-18-E	1.06	2.80	17.5	0.60	14.9203	8.9522	11.9362	T24	6.43200	IV2630E	110	5208	1.6200	0.0846	399.5					
DCM Bldg 8 Isol Vlv	238	RMOV BD 182-E	3A	1-PCV-3-179B-E	0.33	0.75	5.7	0.60	46.5932	27.9559	37.2745	T13	6.15000	IV2800E	110	558	1.1397	0.0427	399.1					
DCM Bldg 8 Isol Vlv	238	RMOV BD 182-E	3B	1-PCV-3-179B-E	0.33	0.75	5.7	0.60	46.5932	27.9559	37.2745	T13	6.15000	IV2130E	110	556	1.1954	0.0425	399.1					
GEN NO 2 FW ISLN VLV	238	RMOV BD 182-E	3B	1-PCV-3-47-E	33.46	48.10	494.0	0.45	0.5376	0.2419	0.4801	T51	0.00226	IV3000E	110	800	0.0408	0.0468	398.5	383.4	70%			
																110	20	0.0027	0.0012					
Dop 3 Deaeration Line Vlv	238	RMOV BD 182-E	4A	1-PCV-3-193	1.50	4.00	25.0	0.60	10.6232	6.3735	8.4966	T26	0.29500	IV3250	110	800	1.7200	0.0612	390.0					
Dop 4 Deaeration Line Vlv	238	RMOV BD 182-E	4E	1-PCV-3-194	1.60	4.00	25.0	0.60	10.6232	6.3739	8.4966	T26	0.29500	IV3270	110	656	1.3935	0.0497	397.1					
Geo No 4 FW Isol Vlv	238	RMOV BD 182-E	4D	1-PCV-3-194-E	33.46	48.10	494.0	0.45	0.5376	0.2419	0.4801	T51	0.00226	IV3010E	110	800	0.0408	0.0468	398.5	383.4	70%			
																110	20	0.0027	0.0012					

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ATTACHMENT 114,

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THIS SHEET ADDED BY REV 6

UNCORRECTED! 5 MINIMUM MOTOR STARTING VOLTAGE = 85% OF 480V, EXCEPT NOTED. 50 ACCELERATION TIME IS AT 80% STARTING VOLTAGE, EXCEPT NOTED. * CABLE LENGTH USED IS DESIGN LENGTH PLUS 100 FEET. ** MAXIMUM CABLE LENGTH <1200 FEET

30-Oct-72

5
Prepared By GCP/RS Date 10-31-72
Checked By *[Signature]* Date 10-31-72

WBN-EEB-MS-T106-0010 R0 ATTACHMENT 10.6 - 480V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES
(TABLE E2 - UNIT 1 MCC MOTOR STARTING VOLTAGES FROM WBN-EEB-MS-T106-0002 R18)

ENG_TITLE	NODE_NO	BOARD	COMPT_EQUPED_NO NO	LOAD	PLI	LDA	LRFF	Tn	Fn	jic	OWD SIZE	Rel	CABLE NO.	CABLE SIZE LENGTH	Re	jic	IND	BLOCK	MIN	ACCL	REMARKS	REV
																	MOTOR	MOTOR	MOTOR	TIME		
																	START	START	START	SRC		
																	VOLT	VOLT	VOLT	VOLT	(440) (432) { } (65)	
HPPF Com Hdr To Id PCV	238 RMOT BD 182-B	51	1-PCV-26-17-B	0.33	0.75	5.7	0.60	46.5932	27.9559	37.2745	T14	4.72000	IV33301	\$10	1234	1.6659	0.0870	393.7		101		
	238 RMOT BD 182-B	58														\$10	2100	1.7429	0.1482			
CNFE Building Return Valve	238 RMOT BD 182-B	58	1-PCV-70-206-B	0.13	0.45	2.60	0.60	102.1466	61.2810	81.7173	T9	11.72000	IV40293	\$12	638	1.5007	0.0534	466.3				
Lwr Cnmt 1A Cir SUP Vlv (1K)	238 RMOT BD 182-B	50	1-PCV-53-113-B	0.13	0.60	3.50	0.60	75.8803	45.5282	60.7043	T11	3.25000	IV38003	\$10	404	0.5508	0.0288	406.1	396.6	X-11413-A		
	238 RMOT BD 182-B	5C														\$10	70	0.9445	0.0049			X-11413-A
Cnmt Spray 1A 1A Sup Cont Vlv	238 RMOT BD 182-B	52	1-PCV-67-123-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T15	2.95000	IV21603	\$12	412	0.8152	0.0315	418.3				
Cnmt Spray 1A 1A Disch Vlv	238 RMOT BD 182-B	5P	1-PCV-47-124-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	IV21703	\$12	600	1.2500	0.0359	415.9				
KCP TURR BAR RTR CNFE ISO VLV	238 RMOT BD 182-B	5D	1-PCV-70-87-B	0.20	2.30	12.00	0.60	22.1318	13.2791	17.7054	T24	0.63205	IV26101	\$12	618	1.3287	0.0473	415.2	408.6			
KCP TURR BAR CNFE ISO VLV	238 RMOT BD 182-B	5E	1-PCV-30-134-B	0.13	0.45	2.60	0.60	102.1466	61.2810	81.7173	T9	11.72000	IV26102	\$12	572	1.1223	0.0399	487.3	399.8			
Lwr Cnmt 1A Cir Disk Isol Vlv	238 RMOT BD 182-B	7D	1-PCV-67-103-B	0.13	0.60	3.50	0.60	75.8803	45.5282	60.7043	T12	7.53000	IV22758	\$12	549	1.3954	0.0496	403.9	401.5			
Up Cnmt Vt Clr 1A Disk Isol Vlv	238 RMOT BD 182-B	77	1-PCV-67-131-B	0.13	0.45	3.15	0.60	44.3115	50.5869	67.4492	T9	11.72000	IV38248	\$12	472	1.0148	0.0361	400.9	393.6			
KCCH Idc 1A Iso Vlv before Str	238 RMOT BD 182-B	8A	1-PCV-67-24-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	IV26498	\$12	2100	1.7429	0.1481	397.6		101		
	238 RMOT BD 182-B	8E														\$12	1247	2.4812	0.0351			
A. Ridg KMC Sep Hdr 1A Iso Vlv	238 RMOT BD 182-B	48	1-PCV-67-82-B	0.67	1.90	7.56	0.60	35.1298	31.0773	28.1038	T24	0.63200	IV26608	\$12	630	1.3545	0.0482	424.7				
Lwr Cnmt 1A Cir Disk Isol Vlv	238 RMOT BD 182-B	4D	1-PCV-67-111-B	0.13	0.60	3.50	0.60	75.8803	45.5282	60.7043	T12	7.53000	IV22838	\$12	463	0.9955	0.0354	410.1	402.7			
Up Cnmt Vt Clr 1C Disk Isol Vlv	238 RMOT BD 182-B	4F	1-PCV-67-134-B	0.13	0.45	3.15	0.60	44.3115	50.5869	67.4492	T9	11.72000	IV38438	\$12	495	1.0683	0.0379	400.7	393.4			
Lwr Cnmt 1A Cir Disk Isol Vlv	238 RMOT BD 182-B	51	1-PCV-67-85-B	0.13	0.95	5.70	0.60	46.5932	27.9559	37.2745	T15	3.79000	IV26108	\$12	525	1.3288	0.0402	412.2	404.7			
Lwr Cnmt 1C-Cir Disk Isol Vlv	238 RMOT BD 182-B	5B	1-PCV-67-96-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T15	3.79000	IV26408	\$12	418	1.0492	0.0373	412.7	405.2			
Up Cnmt Vt Clr 1B Disk Isol Vlv	238 RMOT BD 182-B	5D	1-PCV-67-297-B	0.13	0.45	2.60	0.60	102.1466	61.2810	81.7173	T9	11.72000	IV31048	\$12	463	0.9955	0.0351	405.1	400.1			
	238 RMOT BD 182-B	5E														\$12	410	0.9456	0.0337			
Up Cnmt Vt Clr 1B Sep Isol Vlv	238 RMOT BD 182-B	57	1-PCV-67-113-B	0.13	0.45	3.14	0.60	44.3115	50.5869	67.4492	T9	11.72000	IV36518	\$12	545	1.1718	0.0413	400.5	393.2			
Lwr Cnmt 1B Cir Sply Isol Vlv	238 RMOT BD 182-B	10A	1-PCV-67-91-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T15	3.19800	IV26508	\$12	513	1.1058	0.0392	412.4	404.9	X-11413-A		
Lwr Cnmt 1B Cir Sply Isol Vlv	238 RMOT BD 182-B	10B	1-PCV-67-93-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T15	3.19800	IV26508	\$12	337	0.7246	0.0258	414.6	407.0	X-11413-A		
UP CNFM Vt Clr 1B DIS ISO VLV	238 RMOT BD 182-B	10D	1-PCV-67-298-B	0.13	0.45	3.14	0.60	44.3115	50.5869	67.4492	T9	11.72000	IV31208	\$12	255	0.5483	0.0195	405.2	392.9			
	238 RMOT BD 182-B	10E														\$12	340	0.7310	0.0260			
Up Cnmt Vt Clr 1D Sep Isol Vlv	238 RMOT BD 182-B	10F	1-PCV-67-141-B	0.13	0.45	3.15	0.60	44.3115	50.5869	67.4492	T9	11.72000	IV36698	\$12	304	0.6516	0.0233	402.0	394.7			
A. Ridg AirCir Sep Hdr 1A Iso V	238 RMOT BD 182-B	11A	1-PCV-67-124-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	4.72000	IV24168	\$12	373	0.8620	0.0285	409.0				
SFA S & C AC SUP HDR 1B ISO VLV	238 RMOT BD 182-B	11B	1-PCV-57-208-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T15	3.75000	IV24488	\$12	458	0.5947	0.0350	403.1				
Lwr Cnmt 1C Cir SUP VLV (1K)	238 RMOT BD 182-B	11B	1-PCV-67-105-B	0.13	0.60	3.50	0.60	75.8803	45.5282	60.7043	T11	9.25000	IV30838	\$10	512	0.8262	0.0431	405.1	397.7	X-11413-A		
	238 RMOT BD 182-B	11D														\$10	65	0.5078	0.0046			X-11413-A
Hydrogen Det Sys	238 RMOT BD 182-B	11P1	1-X2AN-43-210	4.16	5.22																	
ID Hdr & Disch Vlv To Clg Ter	238 RMOT BD 182-B	12A	0-PCV-67-362	1.00	2.00	15.00	0.60	16.5918	9.9593	13.2751	T29	0.23700	IV3230	\$12	1554	3.3411	0.1189	383.5		101		
ERCH To Capnt Clg Hr A	238 RMOT BD 182-B	12B	1-PCV-67-478-B	0.38	2.38	12.00	0.60	22.1318	13.2791	17.7054	T16	0.42100	IV33568	\$12	500	1.0150	0.0383	421.7				
FOR ERCH To Comp Ds	238 RMOT BD 182-B	12B	1-PCV-70-87-B	0.10	2.30	12.00	0.60	22.1318	13.2791	17.7054	T24	0.43200	IV26108	\$12	518	1.1137	0.0336	415.2				
	238 RMOT BD 182-B	12B														\$12	160	0.2150	0.0077			
AMMULUS SPK ISLN VLV	238 RMOT BD 182-B	12F	1-PCV-26-244-B	0.17	2.10	5.00	0.60	53.1162	31.8697	42.4330	T19	1.66000	IV31701	\$12	720	1.3480	0.0551	423.8				
CCS Hr A & C Inlet Isln Vlv	238 RMOT BD 182-B	13B	1-PCV-78-13-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	IV25018	\$12	416	0.8944	0.0318	418.2				

{DINCCDV} 5 MINIMUM MOTOR STARTING VOLTAGE = 85% OF 460V, EXCEPT NOTED. 55 ACCELERATION TIME IS AT 80% STARTING VOLTAGE, EXCEPT NOTED. * CABLE LENGTH USED IS DESIGN LENGTH PLUS 100 FEET. ** MAXIMUM CABLE LENGTH <1200 FEET

11

*These 1/8's
are my runs*

30-Oct-12

Revision

WBN-EEB-ED-Q000-999-2007-0002, R0
 TABLE U2 - UNIT 1 MCC MOTOR STARTING TORQUES FROM WBN-EEB-MS-1005-0001 [14]

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ATTACHMENT 11.4,
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Calc. STUDY-EEB-WBN-12-001
 Attachment 3
 Required Motor Starting Voltage
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PAGE 186A
 (Added by Rev 5)

INC_ID	INC_TYPE	INC_ID	BOARD	CONF_EQUIP_ID	CONF	REV	TRA	LETF	TR	TR	OND	PLT	CABIN	CABIN	PC	PC	BLK	MIN	ACCEL	REMARKS
10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	(440) (432) (5) (5)
ACP Oil Ctr Mtn Catlet 1slb Plr	234 R007 RD 1M2-A	130 1-ICF-74-35-5	0.13	0.46	3.50	0.40	75.4003	45.5202	60.3643	712	7.510600	1729548			112	265	0.5938	0.0293	411.4 (01.9	
ACP Oil Ctr Mtn Catlet 1slb Plr	234 R007 RD 1M2-A	130 1-ICF-74-10-2	0.33	0.95	5.10	0.50	46.5337	23.4559	31.2745	715	3.79060	1729488			112	180	0.2150	0.0077		
CCS M C Outlet Plr	234 R007 RD 2M7-S	131 0-ICF-74-10-2	0.33	0.95	5.10	0.60	46.5332	23.3558	31.2745	715	2.45900	1729522			112	346	1.2139	0.0119	412.0 (01.5	
MTR M 8 Bar Inlet Plr	234 R007 RD 1M2-A	130 1-ICF-74-35-4	0.33	0.95	5.10	0.60	46.5332	23.3559	31.2745	715	2.45900	1729548			112	354	0.7113	0.0271	413.3	
CCS Mtn 3 To C-S Outl 1slb Plr	234 R007 RD 1M2-A	130 1-ICF-74-25-5	0.37	0.95	5.10	0.60	46.5331	23.3558	31.2745	715	2.45900	1729548			112	462	0.9133	0.0353	417.5	
CCS Plts 1A-4 To 1A-4 Isla Plr	234 R007 RD 1M2-A	130 1-ICF-74-35-4	0.37	1.50	7.50	0.60	46.5331	23.3558	31.2745	715	2.45900	1729548			112	570	1.2155	0.0106	415.7	
31R Fr 1 Mtn Hdr 1slb Plr	234 R007 RD 1M2-A	130 1-ICF-74-35-5	0.33	0.95	5.10	0.60	46.5332	23.3559	31.2745	715	2.45900	1729548			112	576	0.7139	0.0291	415.4	
CCS Fr A F C Outlet 1slb Plr	234 R007 RD 1M2-A	130 1-ICF-74-35-4	0.33	0.95	5.10	0.60	46.5332	23.3559	31.2745	715	2.45900	1729548			112	346	1.2139	0.0295	415.4	
CCSP Mtn 1B To C-S Inl 1slb Plr	234 R007 RD 1M2-A	130 1-ICF-74-65-8	0.67	1.90	16.00	0.50	16.5494	9.9351	13.2211	724	0.43200	1729446			112	513	1.2112	0.0435	410.2	
Fr A 8 Bar Outlet Plr	234 R007 RD 1M2-A	130 1-ICF-74-152-8	0.33	0.95	5.10	0.60	46.5332	23.3559	31.2745	715	2.45900	1729548			112	512	1.2109	0.0392	413.0	
CCSP Mtn 1B To C-S Inl 1slb Plr	234 R007 RD 1M2-A	130 1-ICF-74-25-5	0.67	1.90	7.50	0.60	35.1295	21.0711	26.1089	724	0.43200	1729548			112	504	1.0133	0.0396	416.8	
TOP BAR TO COMP 02	234 R007 RD 1M2-A	130 1-ICF-74-134-5	0.13	0.45	7.50	0.60	46.1027	14.1665	21.2810	81.7173	15	1.72600	1729708			112	521	1.2123	0.0351	407.3
CCS Fr C Light Plr	234 R007 RD 1M2-A	130 1-ICF-74-22-3	0.33	0.95	5.10	0.60	46.5332	23.3559	31.2745	715	2.45900	1729548			112	502	1.0793	0.0384	417.1	
CCSP Mtn 1B To C-S Outl 1slb Plr	234 R007 RD 1M2-A	130 1-ICF-74-27-5	0.33	0.95	5.10	0.60	46.5332	23.3559	31.2745	715	2.45900	1729548			112	502	1.0793	0.0384	417.1	
CCS Fr C Slstv AVASS Comp 1slb Plr	234 R007 RD 1M2-A	130 1-ICF-87-1A4-1	0.13	0.45	1.15	0.50	46.3115	20.5854	67.6162	73	11.32000	1729728			112	431	0.5813	0.0261	402.1	
407 Fr 1A In A/C Cplcr 10-8	234 R007 RD 1M2-A	130 1-ICF-87-1A4-1	75.00	51.50	512.5	0.13	6.4895	0.1516	0.4621	1729548				112	197	0.0713	0.0013	403.2		
Cabat Pl 1 Ept Dr Comp Plr 1A	234 R007 RD 1M2-A	130 1-ICF-87-1D5A	3.00	4.60	31.3	0.42	7.8143	4.8572	6.1460	735	0.01600	1729553			112	472	0.6372	0.0333	399.5	
Incuse Fluz Bet Dr Unit 10	235 R007 RD 1D1-A	130 1-ICF-87-1D10	3.42	7.25	32.0	0.62	1.2394	3.1155	6.5127	1729554				112	210	0.5115	0.1051	409.3		
Incuse Fluz Bet Dr Unit 12	235 R007 RD 1D1-A	130 1-ICF-87-1D12	3.42	7.25	32.0	0.62	1.2394	3.1155	6.5117	1729554				110	431	0.6651	0.0348	405.1		
Incuse Fluz Bet Dr Unit 17	235 R007 RD 1D1-A	130 1-ICF-87-1D17	3.42	7.25	32.0	0.62	1.2394	3.1155	6.5117	1729554				110	270	0.3445	0.0130	405.1		
Ice Cond Fr Ctg Plr	235 R007 RD 1D1-A	3E													110	431	0.6655	0.0348	405.1	
Spreading Fr 5pl Yzn	235 R007 RD 1D1-A	130 1-ICF-87-1D1-51	22.75	27.00	222.5	0.43	1.1816	0.5133	1.0176	751	0.08318	1729554			112	371	0.3150	0.0242	340.1	
Spreading Fr 5pl Yzn	235 R007 RD 1D1-A	130 1-ICF-87-1D1-46	0.35	1.00	0.50	0.52	26.5591	16.4466	20.0135	910	1.41500	1729548			112	410	1.4670	0.0520	406.0	
Basic Gas Oper Big A	235 R007 RD 1D1-A	130 1-ICF-87-1D1-46	3.00	6.00	32.0	0.62	1.2394	3.1155	6.5117	734	1.41500	1729548			112	750	1.4125	0.0574	395.4	
Basic Gas Oper Big A	235 R007 RD 1D1-A	130 1-ICF-87-1D1-46	25.00	30.00	151.4	0.43	1.3154	2.5715	1.2147	735	0.40226	1729548			115	426	0.2242	0.0290	393.6	
Reac Cool Plt 1 Gfl Lift Plr	235 R007 RD 1D1-A	130 1-ICF-87-1D1-46	10.00	13.00	81.0	0.53	3.2738	1.7370	1.7370	745	0.01238	1729548			110	519	0.6485	0.0310	340.6	
Reac Cool Plt 2 Gfl Lift Plr	235 R007 RD 1D1-A	130 1-ICF-87-1D1-46	10.00	13.00	81.0	0.53	1.2739	1.7370	1.7370	745	0.01238	1729548			110	75	1.0103	0.0323	409.3	
Reac Cool Plt 3 Gfl Lift Plr	235 R007 RD 1D1-A	130 1-ICF-87-1D1-46	10.00	13.00	81.0	0.53	1.2739	1.7370	1.7370	745	0.01238	1729548			110	655	0.6274	0.0324	385.3	
Reac Paper Comp Ctr 7m 1A	235 R007 RD 1D1-A	130 1-ICF-87-1D1-45	5.00	9.10	34.5	0.62	1.2336	4.1665	5.2153	746	0.01238	1729548			110	495	0.6500	0.0312	374.5	
Reac Upper Comp Ctr Plr 1C	235 R007 RD 1D1-A	90	5.40	9.10	34.5	0.62	6.3136	4.1665	5.2153	746	0.01238	1729548			112	459	0.3875	0.0314		
Computer Room Inv No. 1	235 R007 RD 1D1-A	100	100	100	100	100	100	100	100	100	100	100	100	100	110	460	0.5210	0.0314	393.3	
Reac Coal Dr 1C Plr 1A	235 R007 RD 1D1-A	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	0.3140	0.0312	409.3
																			110 465 0.4778 0.0328 377.3	

WBN-EEB-ED-Q000-999-2007-0002, R0
 TABLE U2 - UNIT 1 MCC MOTOR STARTING TORQUES FROM WBN-EEB-MS-1005-0001 [14]
 TABLE U2 - UNIT 1 MCC MOTOR STARTING VOLTAGE IS 400V, EXCEPT UNIT 100 WHICH IS 460V.
 ACCELERATION TIME IS AT 0% STARTING VOLTAGE, EXCEPT FOR 100 WHICH IS 100%.
 MAXIMUM CABLE LENGTH 100 FEET.

30-Oct-11

Prepared By: G.C.P. / RS Date 10-31-2011
 Checked By: *[Signature]* / *[Signature]*

WBN-EEB-ED-Q000-999-2007-0002, R0
 TABLE 12 - UNIT 1 MCC MOTOR STARTING VOLTAGES FROM 901-740-055-1010-0002 (111)

MCC_VIN#	UNIT_ID	BOARD	CORECT_VOLTAGE_10	L1A	L1B	L1C	L2A	L2B	L2C	CH1	CH2	CH3	CH4	CH5	CH6	CH7	CH8	CH9	CH10	CH11	CH12	CH13	CH14	CH15	CH16	CH17	CH18	CH19	CH20	CH21	CH22	CH23	CH24	CH25	CH26	CH27	CH28	CH29	CH30	CH31	CH32	CH33	CH34	CH35	CH36	CH37	CH38	CH39	CH40	CH41	CH42	CH43	CH44	CH45	CH46	CH47	CH48	CH49	CH50	CH51	CH52	CH53	CH54	CH55	CH56	CH57	CH58	CH59	CH60	CH61	CH62	CH63	CH64	CH65	CH66	CH67	CH68	CH69	CH70	CH71	CH72	CH73	CH74	CH75	CH76	CH77	CH78	CH79	CH80	CH81	CH82	CH83	CH84	CH85	CH86	CH87	CH88	CH89	CH90	CH91	CH92	CH93	CH94	CH95	CH96	CH97	CH98	CH99	CH100	CH101	CH102	CH103	CH104	CH105	CH106	CH107	CH108	CH109	CH110	CH111	CH112	CH113	CH114	CH115	CH116	CH117	CH118	CH119	CH120	CH121	CH122	CH123	CH124	CH125	CH126	CH127	CH128	CH129	CH130	CH131	CH132	CH133	CH134	CH135	CH136	CH137	CH138	CH139	CH140	CH141	CH142	CH143	CH144	CH145	CH146	CH147	CH148	CH149	CH150	CH151	CH152	CH153	CH154	CH155	CH156	CH157	CH158	CH159	CH160	CH161	CH162	CH163	CH164	CH165	CH166	CH167	CH168	CH169	CH170	CH171	CH172	CH173	CH174	CH175	CH176	CH177	CH178	CH179	CH180	CH181	CH182	CH183	CH184	CH185	CH186	CH187	CH188	CH189	CH190	CH191	CH192	CH193	CH194	CH195	CH196	CH197	CH198	CH199	CH200	CH201	CH202	CH203	CH204	CH205	CH206	CH207	CH208	CH209	CH210	CH211	CH212	CH213	CH214	CH215	CH216	CH217	CH218	CH219	CH220	CH221	CH222	CH223</
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MSH-FEB-16-TI06-0010 R10 ATTACHMENT 1D.6 - 480V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES
(TABLE 13 - UNIT 2 MCC MOTOR STARTING VOLTAGES FROM MSH-FEB-16-TI06-0012 R18)

ENG_TITLE	NODE_NO	BOARD	COMPT NO	EQUIP_ID_NO	LOAD	FLI	LRA	LPF	Zn	Rn	Jn	QMD	Rtol	CABLE NO.	CABLE SIZE	LEN	Rc	Jc	IDC	BLOCK	MIN	ACCEL	REMARKS	REV
																		START	START	START	SEC			
																	VOLT	VOLT	VOLT	VOLT				
AUX CONTROL AIR COMPRESSOR A-A	207	CIA VENT BD	2A1-A	2A 0-MTR-32-60-A	20.00	26.00	157.89	0.46	1.6821	0.7737	1.4935	T51	0.00318	2PL3785A	12	1275	0.2721	0.0784	391.6	(440)	(415)	(+)	(\\$)	
Shdn Bd Ra Chlr Clr Pnp A-A	207	CIA VENT BD	2A1-A	3A 0-MTR-31-36/1-A	25.00	31.00	197.4	0.43	1.3454	0.5785	1.2147	T53	0.00226	2PL4020A	18	364	0.3090	0.0257	387.8					
Aux Bldg Gas Inrtal Sys Fan A-A	207	CIA VENT BD	2A1-A	3D 2-MTR-30-146-A	50.00	62.00	304.0	0.37	0.8736	0.3232	0.8116	T56	0.00124	2PL3746A	12	550	0.1174	0.0338	401.0	380.1	80%	7.4	AMP FAIL	
EG Trtnt Sys A-A Ra Clr Fan	207	CIA VENT BD	2A1-A	4A 2-MTR-30-200-A	50.00	4.10	27.0	0.53	9.8363	5.2133	8.3412	T32	0.10000	2PL3774A	110	530	0.6750	0.0353	420.3	396.4	80%	1.05		
ERCV Str 2A-A Backash Vlv	207	CIA VENT BD	2A1-A	4E 2-FCV-67-94-A	0.33	0.75	5.79	0.60	45.8689	27.5214	36.6951	T14	4.72000	2PL4040A	18	2798	2.3755	0.1973	399.9					
AFM & BA XFR SPACE CLR FAN A-A	207	CIA VENT BD	2A1-A	5E 2-MTR-30-184-A	15.00	20.20	105.2	0.49	2.5236	1.2366	2.1999	T8A	0.00625	2PL3151A	18	210	0.1783	0.0148	421.8	397.8				
Shutdown Bd Ra B Press Fan B-A	207	CIA VENT BD	2A1-A	6A 0-MTR-31-62-A	3.00	4.60	28.0	0.62	9.4850	5.8807	7.4420	T33	0.08000	2PL3601A	12	175	0.3763	0.0134	426.5					
ERCV STRAINER 2A-A	207	CIA VENT BD	2A1-A	6B 2-MTR-67-94-A	3.00	6.00	30.1	0.62	8.8292	5.4741	6.9274	T36	0.05500	2PL3913A	18	2106	0.7062	0.1323	380.7		75%			
207 CIA VENT BD 2A1-A 6B	207	CIA VENT BD	2A1-A	6C 2-MTR-67-439-A	5.00	6.80	41.1	0.61	6.4618	3.9546	5.1104	T38	0.03483	2PL3880A	12	2100	0.4481	0.1292	373.6		80%			
Traveling Scrn 2A-A	207	CIA VENT BD	2A1-A	6C													10	764	1.0014	0.0539				
ERCV Str 2A-A Flush Vlv	207	CIA VENT BD	2A1-A	6E 2-FCV-67-98-A	0.33	0.75	5.79	0.60	45.8689	27.5214	36.6951	T14	4.72000	2PL3808A	18	2790	2.3667	0.1967	399.0					
125V VIT BAT RM IV EXFAN 2A1-A	207	CIA VENT BD	2A1-A	78 2-MTR-31-287-A	0.33	0.80	5.2	0.62	51.0733	31.6654	40.0722	T17	2.20500	2PL3550A	12	318	0.6837	0.0243	421.6		P-04468-A			
Pen El El 737 Clr Fans 2A-A	207	CIA VENT BD	2A1-A	88 2-MTR-30-194-A	3.00	4.00	25.5	0.66	10.4027	6.8616	7.8088	T32	0.10000	2PL3091A	18	262	0.3537	0.0185	426.9	402.7	80%	2.4		
480V Xfar Ra 2A Exh Fan 2A2-A	207	CIA VENT BD	2A1-A	8C 2-MTR-30-250F-A	3.00	4.40	27.4	0.67	9.6927	6.4457	7.2390	T34	0.07100	2PL2854A	12	200	0.4300	0.0153	424.6		H-13273-A			
480V Xfar Ra 2A Exh Fan 2A3-A	207	CIA VENT BD	2A1-A	8D 2-MTR-30-250G-A	3.00	4.40	27.4	0.67	9.6927	6.4457	7.2390	T34	0.07100	2PL2854A	12	200	0.4300	0.0153	424.6		H-13273-A			
Elect Bd Ra A/C Sys Oil Pnp	207	CIA VENT BD	2A1-A	8F1 0-MTR-31-128/5-A	3.11	3.90	31.0	0.62	8.5471	5.3116	6.7218			2PL3252A	18	650	0.5519	0.0458	421.0					
C.Bldg Ele B/Ra AC Cir Pnp A-A	207	CIA VENT BD	2A1-A	98 0-MTR-31-128/1-A	20.00	25.00	157.9	0.46	1.6820	0.7737	1.4934	T51	0.00318	2PL4000A	12	596	0.1272	0.0367	410.6		H-09701-A			
207 CIA VENT BD 2A1-A 98	207	CIA VENT BD	2A1-A	9C 2-MTR-31-462-A	3.00	4.60	28.0	0.62	9.4850	5.8807	7.4420	T34	0.07100	2PL3470A	18	274	0.3699	0.0193	426.8		F-12766-A			
480V Bd Ra 2A Pr Sop Fan 2A1-A	207	CIA VENT BD	2A1-A	9D 2-MTR-30-250E-A	3.00	4.40	27.4	0.67	9.6927	6.4457	7.2390	T34	0.07100	2PL2846A	12	226	0.4859	0.0173	422.9		H-13273-A			
Cont Rm Intake Non	207	CIA VENT BD	2A1-A	9F1 0-RE-90-125-A	1.40	1.80	5.4	0.65	49.1817	31.9681	37.3748			2PL3181A	18	518	0.6993	0.0265	435.7					
480V Bd Ra 2B Pr Sop Fan 2B1-A	207	CIA VENT BD	2A1-A	11A 2-MTR-31-476-A	3.00	4.60	28.0	0.62	9.4850	5.8807	7.4420	T34	0.07100	2PL3480A	18	250	0.3375	0.0176	427.7					
480V Bd Ra 2A A/C Adu 2A-B	207	CIA VENT BD	2A1-A	11C 2-MTR-31-451-A	10.00	12.00	78.9	0.53	3.3660	1.7840	2.8544	T44	0.01214	2PL4050A	18	500	0.6750	0.0353	389.5		AMP FAIL			
125V Vtbdaln III Ex Fan 2B1-A	207	CIA VENT BD	2A1-A	12A 2-MTR-31-285-A	0.33	0.80	5.2	0.62	51.0733	31.6654	40.0722	T17	2.20500	2PL3570A	12	322	0.6193	0.0246	424.5		P-04468-A			
480V Bd Ra 2A A/C Cond 2A-H	207	CIA VENT BD	2A1-A	12C 2-MTR-31-290-A	15.00	21.00	111.0	0.49	2.3926	1.1274	2.0657	T49	0.00572	2PL4080A	18	236	0.2428	0.0202	414.4		AMP FAIL			
ERCV SCREEN WASH PUMP 2A-A	207	CIA VENT BD	2A1-A	130 2-MTR-67-137-A	40.00	49.00	290.0	0.38	0.9158	0.3486	0.8471	T54	0.00202	2PL3600A	2-10	2100	0.1420	0.0430	366.1					
207 CIA VENT BD 2A1-A 130	207	CIA VENT BD	2A1-A	13F1 0-MTR-31-35/3-A	2.00	4.17	12.5	0.62	21.2465	13.1720	16.6700			2PL3770A	18	758	0.0522	0.0466						
Shdn Bd Ra Chlr Pkg A-A Oil Pnp	207	CIA VENT BD	2A1-A	13F1 0-MTR-31-35/3-A	2.00	4.17	12.5	0.62	21.2465	13.1720	16.6700			2PL3770A	18	450	0.5075	0.0317	431.7		.75ip			
Supply Rm Hood Exh Fan 2A	208	CIA VENT BD	2A2-A	4A 2-MTR-30-67	1.50	2.65	20.0	0.62	13.2791	8.2330	10.4188	T29	0.23700	2PL3621	12	650	1.3975	0.0497	406.1					
AUX CONT AIR CRPSR B-B	209	CIA VENT BD	2B1-B	2A 0-MTR-32-95-B	20.00	27.00	157.89	0.46	1.6821	0.7737	1.4935	T51	0.00318	2PL3798B	18/L0	1750	0.2366	0.1050	391.0					
PEN RM EL 713 CLR FAN 2B-B	209	CIA VENT BD	2B1-B	2C 2-MTR-30-197-B	3.00	4.30	26.70	0.62	9.9469	6.1671	7.8043	T34	0.07100	2PL3212B	18/L0	436	0.5886	0.0307	421.2	397.2	F-14692-A *			
Aux Bldg Gas Inrtal Sys Fan B-B	209	CIA VENT BD	2B1-B	30 2-MTR-30-157-B	50.00	62.00	304.0	0.37	0.8736	0.3232	0.8116	T54	0.00124	2PL3768B	18/L2	350	0.0747	0.0215	416.1	392.4				
BATTERY RM EL 692 EXH FAN C-B	209	CIA VENT BD	2B1-B	4A 0-MTR-31-27-B	2.00	2.70	22.0	0.60	12.0219	7.2431	9.6575	T29	0.23700	2PL2898B	18/L2	398	0.8557	0.0304	415.6					
ERCV Str 2B-B Backash Vlv	209	CIA VENT BD	2B1-B	4C 2-FCV-67-104-B	0.33	0.75	5.79	0.60	45.8689	27.5214	36.6951	T14	4.72000	2PL3998B	18/L2	3184	2.7032	0.2245	396.9					
ERCV STRAINER	209	CIA VENT BD	2B1-B	4E 2-FCV-67-108-B	3.00	6.00	30.1	0.62	8.8292	5.4741	6.9274	T36	0.05500	2PL3920B	18/L2	2100	0.7062	0.1323	357.0		75%			
209 CIA VENT BD 2B1-B 4E 2-FCV-67-108-B	209	CIA VENT BD	2B1-B	4F 2-MTR-67-108-B	3.00	6.00	30.1	0.62	8.8292	5.4741	6.9274	T36	0.05500	2PL3920B	18/L0	1450	1.3575	0.1022						
Traveling Scrn 2B-B	209	CIA VENT BD	2B1-B	4G 2-MTR-67-451-B	5.00	6.80	41.1	0.61	6.4618	3.9546	5.1104	T38	0.03483	2PL3940B	18/L2	2100	0.4481	0.1292	377.5		80%			
ERCV Str 2B-B Flush Vlv	209	CIA VENT BD	2B1-B	4H 2-FCV-67-108-B	0.33	0.75	5.70	0.60	46.5932	27.5559	37.2745	T14	4.72000	2PL3988B	18/L2	3256	2.7643	0.2225	397.2		F-10614-A			
209 CIA VENT BD 2B1-B 4H 2-FCV-67-108-B	209	CIA VENT BD	2B1-B	4I 2-FCV-67-108-B	0.33	0.75	5.70	0.60	46.5932	27.5559	37.2745	T14	4.72000	2PL3988B	18/L2	10	0.0215	0.0008			F-10614-A			
125V Vlt Bat Ra IV ExFan 2A2-B	209	CIA VENT BD	2B1-B	78 2-MTR-31-288-B	0.33	0.80	5.2	0.62	51.0733	31.6654	40.0722	T17	2.20500	2PL3558B	18/L2	280	0.6020	0.0214	425.0		P-04468-A			
Shdn Xfar Ra 2B Exh Fan 2B2-B	209	CIA VENT BD	2B1-B	8C 2-MTR-30-246-B	3.00	4.40	27.4	0.67	9.6927	6.4457	7.2390	T34	0.07100	2PL2878B	18/L2	200	0.4300	0.0153	424.6					
Shdn Xfar Ra 2B Exh Fan 2B3-B	209	CIA VENT BD	2B1-B	8D 2-MTR-30-246-B	3.00	4.40	27.4	0.67	9.6927	6.4457	7.2390	T34	0.07100	2PL2882B	18/L2	178	0.3827	0.0136	426.1					
C.Bldg Ele B/Ra AC Cir Pnp B-B	209	CIA VENT BD	2B1-B	8E 0-MTR-31-129/1-B	20.00	25.00	157.9	0.46	1.6820	0.7737	1.4934	T51	0.00318	2PL3900B	18/L2	546	0.1165	0.0336	412.5		H-09700-A			
209 CIA VENT BD 2B1-B 8E	209	CIA VENT BD	2B1-B	8F												18	50	0.0425	0.0035			F-12463-A		

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ATTACHMENT 11.4.

Required Motor Starting Voltage

Attachment 3

10-Sep-97

WBN-EEB-MS-TI05-0010 R10 ATTACHMENT 10.6 - 480V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES
(TABLE L3 - UNIT 2 MCC MOTOR STARTING VOLTAGES FROM WBN-EEB-MS-TI05-0002 R18)

ENG_TITLE	NODE_NO	BOARD	COMP_EQUIP_ID	LOAD	PLI	LRA	LREF	Zn	Ra	DXn	GND	RDI	CABLE	CABLE	RC	JCT	IND_BLOCK	MIN_ACCEL	REV
																	START_VOLT	START_VOLT	
																	(440)	(415)	
																	(\\$)	(\\$)	
Elec Bd Ra A/C Sys Oil Pmp	209	CIA VENT BD	281-B	8F1 OHTR-31-129/3-B	3.00	3.90	31.0	0.62	8.5671	5.3116	5.7218		ZPL383X	#8	448	0.3804	0.0316	426.8	
480V Bd Ra 2A Pr Sup Fan 2A-B	209	CIA VENT BD	281-B	9C 2-MTR-31-463-B	3.00	4.50	20.0	0.62	9.4850	5.8887	7.4420 T34	0.07100	ZPL384X	#10	280	0.2700	0.0141	429.8	
Shdza Xfar Ra 2B Exh Fan 2B1-B	209	CIA VENT BD	281-B	90 2-MTR-30-245-B	3.00	4.40	27.4	0.67	9.5927	6.4457	7.2390 T34	0.07100	ZPL2870X	#12	150	0.3225	0.0115	427.9	80%
Pen Re El 737 Clr Fan 2B-B	209	CIA VENT BD	281-B	9E 2-MTR-30-195-B	3.00	4.00	24.6	0.66	10.3048	7.1311	8.1172 T32	0.10000	ZPL3010X	#10	340	0.4590	0.0240	424.5	400.4 80%
480V Bd Ra 2B Pr Sup Fan 2B2-B	209	CIA VENT BD	281-B	10B 2-MTR-31-477-B	3.00	4.50	20.0	0.62	9.4850	5.8897	7.4420 T34	0.07100	ZPL3495X	#10	156	0.2105	0.0110	431.6	
125V Vit Balta III ExFan 2B2-B	209	CIA VENT BD	281-B	10C 2-MTR-31-284-B	0.33	0.80	5.2	0.62	51.0733	31.6554	40.0722 T12	2.20500	ZPL3575X	#12	266	0.5719	0.0203	425.2	
Cont Ra Intake Nva	209	CIA VENT BD	281-B	10F1 0-RE-90-126-B	1.40	1.80	5.4	0.65	49.1817	31.9681	37.3748		ZPL3815X	#10	482	0.6507	0.0340	436.0	
480V Bd Ra 2B A/C Abv 2B-B	209	CIA VENT BD	281-B	11B 2-MTR-31-475-B	20.00	25.00	142.0	0.46	1.8703	0.8603	1.6607 T51	0.00318	ZPL4070X	#8	280	0.2377	0.0197	409.6	
480V Bd Ra 2B A/C Cond 2B-B	209	CIA VENT BD	281-B	11C 2-MTR-31-289-B	20.00	25.00	142.0	0.46	1.8703	0.8603	1.6607 T51	0.00318	ZPL4098X	#8	266	0.2258	0.0188	411.1	
EG Trtnt Sys B-B Plr Clr Fan	209	CIA VENT BD	281-B	12B 2-MTR-30-207-B	3.00	4.10	27.0	0.53	9.8368	5.2133	8.3412 T32	0.10000	ZPL3201X	#10	367	0.4955	0.0259	424.9	400.8 80%
EROW Scrn Wash Pmp 2B-B	209	CIA VENT BD	281-B	130 2-MTR-67-447-B	40.00	49.00	290.0	0.38	0.9158	0.3480	0.8471 T54	0.00202	ZPL3959X	2-1/0	2100	0.1420	0.0530	358.1	75%
	209	CIA VENT BD	281-B	130 2-MTR-67-447-B										#4/0	1032	0.0714	0.0538		
Dg 2-A Sttry Hood Exh Fan	221	DSL AUX BD	281-A	2A 2-MTR-30-456-A	0.33	2.20	9.3	0.62	28.5495	17.7627	22.4785 T28	0.29500	ZPL2585X	#12	100	0.2150	0.0077	435.1	
Dg 2-A-R EXH FAN 1-A	221	DSL AUX BD	281-A	2B 2-MTR-30-449-A	15.00	19.50	118.4	0.49	2.2431	1.0991	1.9553 T49	0.00572	ZPL2638X	#8	70	0.0594	0.0049	432.9	405.3
Dg 2-A-Lube Oil Circ Pmp 1	221	DSL AUX BD	281-A	2D 2-MTR-82-401-A	1.00	1.70	15.0	0.62	17.7054	10.9774	12.8917 T24	0.63200	ZPL2270X	#12	170	0.3655	0.0120	424.5	
EM Dg ENG RX 2A1 & 2A2 SUP VLV	221	DSL AUX BD	281-A	3A 2-FEV-67-66-A	0.13	0.39	2.60	0.60	102.1466	61.2880	81.7173 T8	13.95000	ZPL2160X	#12	160	0.3440	0.0122	403.7	380.8
Dg 2-A Day Tnk Fo Xfr Pmp 1-A	221	DSL AUX BD	281-A	3D 2-MTR-18-55-A	1.00	1.85	11.3	0.62	23.5444	14.5975	18.4730 T26	0.42100	ZPL2720X	#12	160	0.3440	0.0122	431.0	
Dg 2-A Aux LubeOil Circ Pmp A	221	DSL AUX BD	281-A	4B 2-MTR-82-A0P8-A	0.75	1.27	11.5	0.62	23.0940	17.3205	15.2753 T23	0.08000	ZPL3424X	#8	60	0.1290	0.0046	426.9	
Dg Ra 2A-P Plr Vent Fan	221	DSL AUX BD	281-A	4D 2-MTR-30-492-A	15.00	20.00	118.4	0.49	2.2431	1.0991	1.9553 T49	0.00825	ZPL3424X	#8	130	0.1104	0.0092	427.0	402.7
2A 480V ELEC BD Ra EX FAN	221	DSL AUX BD	281-A	4E 2-MTR-30-450-A	2.00	2.70	22.6	0.62	11.7722	7.2988	9.2365 T29	0.23700	ZPL2525X	#10	90	0.1215	0.0063	431.6	
Dg 2A-A Air Cprsr 2	221	DSL AUX BD	281-A	5A 2-MTR-82-241-A	5.00	7.10	44.5	0.62	5.9695	3.7011	4.6836 T39	0.02878	ZPL2205X	#12	100	0.2150	0.0077	428.5	404.2
Dg 2A-A Muffler Ra Exh Fan	221	DSL AUX BD	281-A	6A 2-MTR-30-464-A	1.50	2.65	20.0	0.62	13.2791	8.2330	10.4188 T28	0.29500	ZPL2242X	#12	52	0.1118	0.0040	431.6	407.1
Dg 2-A Aux LubeOil Circ Pmp B	222	DSL AUX BD	282-A	2A 2-MTR-82-A0P8-A	0.75	1.27	11.5	0.75	23.0940	17.3205	15.2753 T23	0.08000	ZPL3252X	#12	176	0.3784	0.0135	423.4	
Dg 2A-R EXH FAN 2-A	222	DSL AUX BD	282-A	2B 2-MTR-30-452-A	15.00	19.50	118.4	0.49	2.2431	1.0991	1.9553 T49	0.00572	ZPL2647X	#8	100	0.0849	0.0071	430.1	405.6
Dg 2A-Lube Oil Circ Pmp 2	222	DSL AUX BD	282-A	2D 2-MTR-82-A2-A	1.00	2.05	12.5	0.62	21.1956	13.1413	16.6301 T26	0.42100	ZPL2278X	#12	180	0.3670	0.0138	429.4	
EM Dg ENG RX 2A1 & 2A2 SUP VLV	222	DSL AUX BD	282-A	3A 2-FEV-67-68-A	0.13	0.39	2.60	0.60	102.1466	61.2880	81.7173 T8	13.95000	ZPL2153X	#12	100	0.2150	0.0077	404.1	381.1
Dg 2A-Day Tnk Fo Xfr Pmp 2-A	222	DSL AUX BD	282-A	3D 2-MTR-18-54-A	1.00	1.85	11.3	0.62	23.5444	14.5975	18.4730 T26	0.42100	ZPL2722X	#12	180	0.3670	0.0138	430.5	
Dg 2A-Air Cprsr 1	222	DSL AUX BD	282-A	5A 2-MTR-82-240-A	5.00	7.25	46.0	0.62	5.7735	3.5795	4.5299 T38	0.03483	ZPL2210X	#12	82	0.1763	0.0063	429.7	405.3
Dg 2-B Sttry Hood Exh Fan	223	DSL AUX BD	281-B	2A 2-MTR-30-458-B	0.33	1.00	10.0	0.62	26.5581	16.4660	20.8975 T18	1.87500	ZPL2598X	#12	200	0.4300	0.0153	416.5	
Dg 2-B-R EXH FAN 1-B	223	DSL AUX BD	281-B	2B 2-MTR-30-450-B	15.00	19.50	118.4	0.49	2.2431	1.0991	1.9553 T49	0.00572	ZPL2647X	#8	120	0.1019	0.0065	428.2	403.9
Dg 2-B-Lube Oil Circ Pmp 1	223	DSL AUX BD	281-B	2D 2-MTR-82-81-B	1.00	1.95	7.9	0.62	33.6605	20.8695	26.4101 T26	0.42100	ZPL2742X	#12	160	0.3440	0.0122	433.7	
EM Dg ENG RX 2B1 & 2B2 SUP VLV	223	DSL AUX BD	281-B	3A 2-FEV-67-68-B	0.13	0.39	2.60	0.60	102.1466	61.2880	81.7173 T8	13.95000	ZPL2180X	#12	162	0.3483	0.0124	403.7	380.8
Dg 2-B Day Tnk Fo Xfr Pmp 1-B	223	DSL AUX BD	281-B	3D 2-MTR-18-55-B	1.00	1.85	11.3	0.62	23.5444	14.5975	18.4730 T26	0.42100	ZPL2730X	#12	174	0.3741	0.0133	430.6	
Dg 2-B-Aux LubeOil Circ Pmp A	223	DSL AUX BD	281-B	4B 2-MTR-82-A0P8-B	0.75	1.27	11.5	0.75	23.0940	17.3205	15.2753 T23	0.08000	ZPL3258X	#12	60	0.1290	0.0046	426.9	
Dg Ra 2B-P Plr Vent Fan	223	DSL AUX BD	281-B	4D 2-MTR-30-494-B	15.00	20.00	118.4	0.49	2.2431	1.0991	1.9553 T49	0.00825	ZPL3458X	#8	150	0.1274	0.0105	425.1	401.0
Dg 2B-B 480V Elec Bd Ra Ex FAN	223	DSL AUX BD	281-B	4E 2-MTR-30-452-B	2.00	2.70	22.6	0.62	11.7722	7.2988	9.2365 T29	0.23700	ZPL2538X	#10	150	0.2025	0.0105	429.6	
Dg 2B-B Air Cprsr 2	223	DSL AUX BD	281-B	5A 2-MTR-82-271-A	5.00	7.10	44.5	0.62	5.9681	3.7002	4.6826 T39	0.02878	ZPL2222X	#12	122	0.2623	0.0053	426.3	402.1
Dg 2B-B Muffler Ra Exh Fan	223	DSL AUX BD	281-B	6A 2-MTR-30-466-A	1.50	2.65	20.0	0.62	13.2791	8.2330	10.4188 T29	0.23700	ZPL2255X	#12	80	0.1720	0.0061	431.5	407.0
Dg 2B-B Aux LubeOil Circ Pmp B	224	DSL AUX BD	282-B	2A 2-MTR-82-A0P8-B	0.75	1.27	11.5	0.75	23.0940	17.3205	15.2753 T23	0.08000	ZPL3278X	#12	176	0.3784	0.0135	423.4	
Dg 2B-B-R EXH FAN 2-B	224	DSL AUX BD	282-B	2B 2-MTR-30-454-B	15.00	19.50	118.4	0.49	2.2431	1.0991	1.9553 T49	0.00572	ZPL2658X	#8	114	0.0968	0.0080	428.8	404.4
Dg 2B-B-Lube Oil Circ Pmp 2	224	DSL AUX BD	282-B	2D 2-MTR-82-82-B	1.00	2.05	11.3	0.62	23.5444	14.5975	18.4730 T26	0.42100	ZPL2743X	#12	180	0.3870	0.0138	430.5	
EM Dg ENG RX 2B1 & 2B2 SUP VLV	224	DSL AUX BD	282-B	3A 2-FEV-67-65-B	0.13	0.39	2.60	0.60	102.1466	61.2880	81.7173 T8	13.95000	ZPL2187X	#12	126	0.2709	0.0076	403.9	
Dg 2B-B Day Tnk Fo Xfr Pmp 2-B	224	DSL AUX BD	282-B	3D 2-MTR-18-54-B	1.00	1.85	11.3	0.62	23.5444	14.5975	18.4730 T26	0.42100	ZPL2732X	#12	180	0.3870	0.0138	430.5	
Dg Bldg Fuel Oil Xfr Pmp	224	DSL AUX BD	282-B	4B 2-MTR-18-58-B	7.50	11.00	63.5	0.57	4.1624	2.3840	3.4364 T42	0.01503	ZPL2450X	#10	100	0.1350	0.0071	430.4	
Dg 2B-B Air Cprsr 1	224	DSL AUX BD	282-B	5A 2-MTR-82-270	5.00	7.25	44.5	0.62	5.9681	3.7002	4.6826 T39	0.02878	ZPL2230X	#12	115	0.2473	0.0088	427.0	402.7

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ATTACHMENT 3

ATTACHMENT 10.6 - 48KV SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES
 TABLE L3 - UNIT 2 MCC MOTOR STARTING VOLTAGES FROM EBB-EEB-MS-T006-0002.R0

ENG_TITLE	NODE_ID	BOARD	COPyID_NP	L090	FL1	LEA	LEFF	Ta	Ra	Jc	QD	Rsd	CABLE	REV
Boric Acid Transfer Pnp 2kV-A	239	RMV ED 241-A	28	2+T07-62-230-A	15.00	18.00	105.2	0.49	2.5245	1.2370	2.2097	148	0.0825 251.616A	\$6
Boric Acid Transfer Pnp 2kV-A	239	RMV ED 241-A	28	2+T07-62-230-A	7.50	13.00	105.2	0.49	2.5245	1.2370	2.2097	143	0.0139 251.616A	\$8
Vol Cont Tstt Isln Vlv	239	RMV ED 241-A	88	2+T07-62-32-E	1.90	3.50	26.0	0.50	10.2447	6.1238	8.1717	179	0.2370 252.60A	\$8
Catal. Sprdg Isln Vlv	239	RMV ED 241-A	173	2+T07-26-24-A	0.67	2.80	16.0	0.50	16.5986	9.9593	13.2791	174	0.6320 251.67A	\$12
Annulus Standp Isln Vlv	239	RMV ED 241-A	173	2+T07-26-24-A	0.67	2.80	16.0	0.50	16.5986	9.9593	13.2791	174	0.6320 252.60A	\$12
HPC Spray Isln Vlv	239	RMV ED 241-A	186	2+T07-26-24-A	0.67	2.80	16.0	0.50	16.5986	9.9593	13.2791	174	0.6320 251.65A	\$12
Catal. Spray Isln Sup Elec Vlv	240	RMV ED 242-A	EE	2+T07-67-125-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	117	2.52500 252.60A	\$12
ERCP Hst 24 Iso Vlv Before Str	240	RMV ED 242-A	78	2+T07-67-22-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	117	2.52500 252.60A	\$18
240 RMV ED 242-A	78		2+T07-67-22-A	0.67	1.90	7.56	0.50	35.1298	21.0779	26.1038	124	0.5200 251.60A	\$12	
A/Bldg AirCir Svc Hst 24 Iso V	240	RMV ED 242-A	98	2+T07-67-125-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	114	4.7200 252.60A	\$12
Cent Ctg Isln Disch Cont Vlv	240	RMV ED 242-A	114	2+T07-67-165-A	0.67	1.90	7.56	0.50	35.1298	21.0779	26.1038	124	0.6320 252.60A	\$12
CNE BLSK SUPPLY VALVE	240	RMV ED 242-A	11F	6+T07-26-208-A	0.13	0.45	2.60	0.50	102.1166	51.2660	81.1717	179	11.72000 240.20A	\$12
HPC Hst Clr Rn Crft Isln Vlv	240	RMV ED 242-A	120	2+T07-70-22-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	115	3.75000 252.67A	\$12
SPL Rfr 26 To HR 18 ISLN VLV	240	RMV ED 242-A	134	2+T07-70-23-A	0.67	1.90	12.00	0.50	22.1318	13.2791	17.781	124	0.6320 251.60A	\$12
To HR A DTS 4V To CLS TIR	240	RMV ED 242-A	138	6+T07-67-360	1.00	2.80	16.00	0.50	15.5986	9.9593	13.2791	179	0.23700 252.60A	\$12
BR & Gas Strip Evap Plg Fcv	240	RMV ED 242-F	130	2+T07-70-165-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	115	3.75000 251.64A	\$12
Annulus Spst Isln Vlv	240	RMV ED 242-A	135	2+T07-26-24-A	0.67	2.80	16.0	0.50	16.5986	9.9593	13.2791	174	0.6320 251.61A	\$12
BHR Hst A/Ht Inlet Vlv	240	RMV ED 242-A	140	2+T07-70-24-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
Kiss Eptl Hst Inlet Vlv	240	RMV ED 242-A	148	2+T07-67-4-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
CES IR B & C OUTLET ISLN VLV	240	RMV ED 242-A	140	2+T07-70-15-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
CES IR B & C OUTLET ISLN VLV	240	RMV ED 242-A	14E	2+T07-70-195-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
CES IR B & C OUTLET ISLN VLV	240	RMV ED 242-A	15A	2+T07-47-143-A	0.13	0.45	3.15	0.50	84.3115	50.5869	67.4492	179	11.72000 240.04A	\$10
CES IR B & C OUTLET ISLN VLV	240	RMV ED 242-A	15B	2+T07-70-18-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
CDS IR B & C OUTLET ISLN VLV	240	RMV ED 242-A	15D	2+T07-70-16-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
DPS Sys Low Level Intake Vlv	240	RMV ED 242-A	16E	2+T07-70-156-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
BHR Hst A/A Outlet Vlv	240	RMV ED 242-A	17E	2+T07-31-465-A	50.00	57.00	350.8	0.37	0.751	0.2801	0.7033		241.9255A	\$12
Boric Acid Transfer Pnp 2kV-B	241	RMV ED 241-B	25	2+T07-62-22-A	7.50	13.00	105.2	0.45	2.5245	1.2370	2.2097	143	0.0139 251.616A	\$10
Boric Acid Transfer Pnp 2kV-B	241	RMV ED 241-B	28	2+T07-62-22-A	15.00	18.00	105.2	0.45	2.5245	1.2370	2.2097	148	0.0825 251.616A	\$12
CNE BLSK SUPPLY VALVE	241	RMV ED 241-B	3E	2+T07-70-207-A	0.13	0.45	2.60	0.50	102.1166	51.2660	81.3173	179	11.72000 240.04A	\$12
HPP Sys Low Level Intake Vlv	241	RMV ED 241-B	59	6+T07-26-68-A	0.13	0.45	3.15	0.50	84.3115	50.5869	67.4492	179	11.72000 240.04A	\$12
Vol Cont Tstt Isln Vlv	241	RMV ED 241-B	6A	2+T07-70-18-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
Annulus Standp Isln Vlv	241	RMV ED 241-B	173	2+T07-26-24-A	0.67	2.80	16.0	0.50	16.5986	9.9593	13.2791	174	0.6320 251.67A	\$12
ERCP Hst 24 Iso Vlv Before Str	241	RMV ED 241-B	177	2+T07-31-347-Z	3.00	4.50	32.0							
Boric Acid Transfer Pnp 2kV-B	242	RMV ED 242-B	5A	6+T07-26-15	0.07	0.50	2.6	0.50	102.1166	61.2880	81.3173	179	11.72000 240.04A	\$12
HPP Cm Hst Fcv	242	RMV ED 242-B	59	6+T07-26-16	0.07	0.50	2.6	0.50	102.1166	61.2880	81.3173	179	11.72000 240.04A	\$12
Catal. Sprdg Isln Vlv	242	RMV ED 242-B	5E	2+T07-67-125-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
Catal. Sprdg Isln Disch Vlv	242	RMV ED 242-B	5F	2+T07-67-248-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
ERCP Hst 24 Iso Vlv	242	RMV ED 242-B	59	6+T07-26-24-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	117	2.52500 252.60A	\$12
Annulus Standp Isln Vlv	242	RMV ED 242-B	6A	2+T07-26-247-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	117	2.52500 251.65A	\$12
ERCP Hst 24 Iso Vlv Before Str	242	RMV ED 242-B	65	6+T07-26-22-A	0.67	1.90	7.56	0.50	35.1298	21.0779	26.1038	124	0.5200 251.60A	\$12
A/Bldg AirCir Svc Hst 24 Iso V	242	RMV ED 242-B	78	2+T07-67-22-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	114	4.7200 252.60A	\$12
Cent Ctg Isln Disch Cont Vlv	242	RMV ED 242-B	114	2+T07-67-165-A	0.67	1.90	7.56	0.50	35.1298	21.0779	26.1038	124	0.6320 252.60A	\$12
CNE BLSK SUPPLY VALVE	242	RMV ED 242-B	11F	6+T07-26-208-A	0.13	0.45	2.60	0.50	102.1166	51.2660	81.3173	179	11.72000 240.04A	\$12
HPP Cm Hst Fcv	242	RMV ED 242-B	120	2+T07-70-22-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	115	3.75000 252.67A	\$12
Catal. Sprdg Isln Vlv	242	RMV ED 242-B	124	2+T07-67-360	1.00	2.80	16.00	0.50	16.5986	9.9593	13.2791	174	0.6320 251.65A	\$12
ERCP Hst 24 Iso Vlv	242	RMV ED 242-B	125	6+T07-26-68-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
Vol Cont Tstt Isln Vlv	242	RMV ED 242-B	128	2+T07-70-18-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
Annulus Standp Isln Vlv	242	RMV ED 242-B	131	2+T07-70-16-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
ERCP Hst 24 Iso Vlv	242	RMV ED 242-B	132	6+T07-70-156-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
HPP Cm Hst Fcv	242	RMV ED 242-B	137	2+T07-31-465-A	50.00	57.00	350.8	0.37	0.751	0.2801	0.7033		241.9255A	\$12
Boric Acid Transfer Pnp 2kV-B	243	RMV ED 241-B	25	2+T07-62-22-A	7.50	13.00	105.2	0.45	2.5245	1.2370	2.2097	143	0.0139 251.616A	\$10
Boric Acid Transfer Pnp 2kV-B	243	RMV ED 241-B	28	2+T07-62-22-A	15.00	18.00	105.2	0.45	2.5245	1.2370	2.2097	148	0.0825 251.616A	\$12
CNE BLSK SUPPLY VALVE	243	RMV ED 241-B	3E	2+T07-70-207-A	0.13	0.45	2.60	0.50	102.1166	51.2660	81.3173	179	11.72000 240.04A	\$12
HPP Sys Low Level Intake Vlv	243	RMV ED 241-B	59	6+T07-26-68-A	0.13	0.45	3.15	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
Vol Cont Tstt Isln Vlv	243	RMV ED 241-B	6A	2+T07-70-18-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
Annulus Standp Isln Vlv	243	RMV ED 241-B	173	2+T07-26-24-A	0.67	2.80	16.0	0.50	16.5986	9.9593	13.2791	174	0.6320 251.67A	\$12
ERCP Hst 24 Iso Vlv	243	RMV ED 241-B	177	2+T07-31-347-Z	3.00	4.50	32.0							
HPP Cm Hst Fcv	243	RMV ED 241-B	59	6+T07-26-15	0.07	0.50	2.6	0.50	102.1166	61.2880	81.3173	179	11.72000 240.04A	\$12
Catal. Sprdg Isln Vlv	243	RMV ED 241-B	5F	2+T07-67-125-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
ERCP Hst 24 Iso Vlv	243	RMV ED 241-B	59	6+T07-26-165-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
HPP Cm Hst Fcv	243	RMV ED 241-B	65	6+T07-26-16	0.07	0.50	2.6	0.50	102.1166	61.2880	81.3173	179	11.72000 240.04A	\$12
Catal. Sprdg Isln Vlv	243	RMV ED 241-B	6F	2+T07-67-125-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	116	3.75000 252.60A	\$12
ERCP Hst 24 Iso Vlv	243	RMV ED 241-B	69	6+T07-26-24-A	0.33	0.95	5.70	0.50	46.5932	21.9359	31.2745	117	2.52500 252.60A	\$12
Boric Acid Transfer Pnp 2kV-B	244	RMV ED 242-B	25	2+T07-62-22-A	1.90	3.50	26.0	0.50</td						

WBN-EEB-HS-TI06-0010 RIG ATTACHMENT 10.6 - 480V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES
(TABLE L3 - UNIT 2 NCC MOTOR STARTING VOLTAGES FROM WBN-EEB-HS-TI06-0002 R18)

ENG_TITLE	NODE_ND	BOARD	COMP_EQUIP_ID_NO	LOAD	FLI	LRA	LRPF	Z _m	R _m	J _m	GND	REAL	CABLE	AC	DC	IND_BLOCK	MIN	ACCEL	REV	
																START	START	START	SEC	
																VOLT	VOLT	VOLT	(440) (415) (*) (st)	
CES Hx C Disch Vlv To Htr B	242 RM0V BD 282-B		12B 0-FCV-67-152-B	0.67	1.90	7.56	0.60	33.1298	21.0779	28.1038	T24	0.63200	2PL291B	#12	342	0.7353	0.0262	429.5	405.1	VALVE
Analogus Spr Isln Vlv	242 RM0V BD 282-B		12F 2-FCV-26-244-B	0.67	2.80	16.0	0.60	16.5988	9.3933	13.2791	T24	0.63200	2PL270B	#14	700	2.3891	0.0578	392.4		
Solv Htr 28 To Rdg TA Isln Vlv	242 RM0V BD 282-B		13A 2-FCV-67-147-B	0.70	2.30	12.00	0.60	22.1318	13.2791	17.7054	T26	0.42100	2PL242B	#12	494	1.0621	0.0378	421.3		
CES Hx B & C Inlet Isln Vlv	242 RM0V BD 282-B		13B 2-FCV-70-14-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	2PL250B	#12	572	1.2298	0.0438	416.3		
R/R Hx B Htr Inlet Vlv	242 RM0V BD 282-B		14B 2-FCV-70-3-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	2PL248B	#12	386	0.8299	0.0295	416.3		
CSP 2AA22BB To C-S Outl Iso V	242 RM0V BD 282-B		14D 2-FCV-70-28-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	2PL253B	#12	566	1.2169	0.0433	416.4		
CES Pmps 2A-A To 2B-B Isln Vlv	242 RM0V BD 282-B		14E 2-FCV-70-39-B	0.67	1.90	7.56	0.60	35.1298	21.0779	28.1038	T24	0.63200	2PL220B	#12	566	1.2169	0.0433	425.8	TELAS R11	
R/R Hx B Rdg Htr Isln Vlv	242 RM0V BD 282-B		15A 2-FCV-70-75-B	0.33	0.75	5.70	0.60	46.5932	27.9559	37.2745	T14	4.72000	2PL170B	#12	704	1.5136	0.0539	405.0		
CES Hx B & C Outlet Isln Vlv	242 RM0V BD 282-B		15B 2-FCV-70-196-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	2PL248B	#12	366	0.7869	0.0289	418.8		
CSP 2AA22BB To C-S Inlt Iso V	242 RM0V BD 282-B		15D 2-FCV-70-78-B	0.67	1.90	7.56	0.60	35.1298	21.0779	28.1038	T24	0.63200	2PL254B	#12	570	1.2255	0.0436	425.7	TELAS R11	
R/R Hx B-B Outlet Vlv	242 RM0V BD 282-B		15E 2-FCV-70-153-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	2PL255B	#12	470	1.0105	0.0360	417.5		
CSP 2AA22BB Ta-C-S Inlt Iso V	242 RM0V BD 282-B		16A 2-FCV-70-76-B	0.67	1.90	7.56	0.60	35.1298	21.0779	28.1038	T24	0.63200	2PL250B	#12	560	1.2040	0.0428	425.9	TELAS R11	
SPCS Hx Soly Htr Isln Vlv	242 RM0V BD 282-B		17A 0-FCV-70-194-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	2PL251B	#12	416	0.9944	0.0318	418.2		
CSP 2AA22BB To C-S Outl Iso V	242 RM0V BD 282-B		17B 2-FCV-70-29-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	2PL253B	#12	556	1.1954	0.0423	416.5		
480V BD Ra 28 A/C Cprst 28-B	242 RM0V BD 282-B		180 2-MTR-31-447-B	75.00	90.00	526.2	0.33	0.5047	0.1665	0.4764		2PL360B	#12	170	0.0363	0.0105	421.0		AMP FAIL	
Waste Gas Cprst Pkg B	245 RX VENT BD 2A-A		60 0-MTR-77-105	25.00	30.00	197.4	0.43	1.3454	0.5785	1.2147	T53	0.00226	2PL546B	#16	640	0.3416	0.0442	379.3		FAILED NDR-IE
Cont Bay Sump Pkg 1	246 RX VENT BD 2B-B		651 2-MTR-40-2	5.00	7.25	46.0	0.62	5.7735	3.5796	4.5299		2PL695	#10	976	1.3176	0.0688	378.1		FAILED NDR-IE	
COMPUTER ROOM AHU NO. 2	246 RX VENT BD 2B-B		118 0-MTR-31-498	7.50	9.60	60.0	0.57	4.4264	2.5230	3.6369	T41	0.01808	2PL390B	#16	1180	0.5299	0.0814	398.5		

FAILED NDR-IE
FAILED NDR-IE

WBN-EEB-ED-Q000-999-2007-0002, R0

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Calc. STUDY EEB-WBN-12-001
Attachment 3
Required Motor Starting Voltage
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THIS SHEET ADDED BY REV. 4

Calculation No.:
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ATTACHMENT 11.9 Required Voltage 89-10 MOV's - Unit 1 Page 1 of 9
JOG Review Plan

Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

VALVEID	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
0-FCV-067-0144	B	SS SS	O to C C to O	C = 388.3 O = 388.3	Steady State Voltage
0-FCV-067-0152	B	0 SS	C to O O to C	O = 395.1 C = 414	Need Best avail Voltage at t=0 sec from SI
0-FCV-067-0205	A	SS SS	O to C C to O	C = 429.9 O = 429.9	Steady State Voltage
0-FCV-067-0208	B	SS SS	O to C C to O	C = 428.9 O = 428.9	Steady State Voltage
0-FCV-070-0194	B	SS SS	O to C C to O	C = 440.9 O = 440.9	Steady State Voltage
0-FCV-070-0197	A	SS SS	O to C C to O	C = 439.1 O = 439.1	Steady State Voltage
1-FCV-001-0015	A	SS SS	O to C C to O	C = 414 O = 414	Steady State Voltage
1-FCV-001-0016	A	SS SS	O to C C to O	C = 414 O = 414	Steady State Voltage
1-FCV-001-0017	A	SS SS	O to C C to O	C = 408.1 O = 408.1	Steady State Voltage
1-FCV-001-0018	B	SS SS	O to C C to O	C = 413.3 O = 413.3	Steady State Voltage
1-FCV-001-0051	S	0 SS	C to O O to C	O = 90.49 C = 90.49	125 V DC Motor, Need Best Avail Voltage at T=0 sec from SI
1-FCV-003-0033	A	0 4 SS	O to C O to C C to O	C = 322 C = 389.5 O = 414	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=4 sec forward from SI (normally open MOV). Need SS voltage for non-safety related opening stroke.
Motor Brake (1-FCV-003-0033)	A	0	energize	368	Needs 80% of 460 voltage @ T=0
1-FCV-003-0047	B	0 4 SS	O to C O to C C to O	C = 322 C = 381.5 O = 414	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=4 sec forward from SI (normally open MOV). Need SS voltage for non-safety related opening stroke.
Motor Brake (1-FCV-003-0047)	B	0	energize	368	Needs 80% of 460 voltage @ T=0

Calculation No.:
WBNEEBEDQ1999010001

ATTACHMENT 11.9 Required Voltage 89-10 MOV's - Unit 1 Page 2 of 9
JOG Review Plan
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Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

VALVEID	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
1-FCV-003-0087	A	0 4 SS	O to C O to C C to O	C = 322 C = 377.0 O = 403.0	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=4 sec forward from SI (normally open MOV). Need SS voltage for non-safety related opening stroke.
Motor Brake (1-FCV-003-0087)	A	0	energize	368	Needs 80% of 460 voltage @ T=0
1-FCV-003-0100	B	0 4 SS	O to C O to C C to O	C = 322 C = 381.5 O = 414	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=4 sec forward from SI (normally open MOV). Need SS voltage for non-safety related opening stroke.
Motor Brake (1-FCV-003-0100)	B	0	energize	368	Needs 80% of 460 voltage @ T=0
1-FCV-003-0116A	A	SS SS	C to O O to C	O = 383.6 C = 383.6	Steady State Voltage
1-FCV-003-0116B	A	SS SS	C to O O to C	O = 383.6 C = 383.6	Steady State Voltage
1-FCV-003-0126A	B	SS SS	C to O O to C	O = 381.9 C = 381.9	Steady State Voltage
1-FCV-003-0126B	B	SS SS	C to O O to C	O = 382 C = 382	Steady State Voltage
1-FCV-003-0136A	A	SS SS	C to O O to C	O = 386.3 C = 386.3	Steady State Voltage
1-FCV-003-0136B	A	SS SS	C to O O to C	O = 386.3 C = 386.3	Steady State Voltage
1-FCV-003-0179A	B	SS SS	C to O O to C	O = 384.5 C = 384.5	Steady State Voltage
1-FCV-003-0179B	B	SS SS	C to O O to C	O = 384.5 C = 384.5	Steady State Voltage
1-FCV-026-0240	A	0 5 SS	O to C O to C C to O	C = 322 C = 403.5 O = 427.2	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-026-0243	A	0 5 SS	O to C O to C C to O	C = 322 C = 409.7 O = 422.4	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-062-0061	B	0 5 SS	O to C O to C C to O	C = 322 C = 386.6 O = 393.7	Need 70% Voltage at t=0 sec Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).

Calculation No.:
WBNEEBEDQ1999010001

ATTACHMENT 11.9**JOG Review Plan****Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs**

VALVED	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
1-FCV-062-0063	A	0 5 SS	O to C O to C C to O	C = 322 C = 381.1 O = 409.2	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-062-0090	A	0 5 SS	O to C O to C C to O	C = 322 C = 414 O = 414	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-062-0091	B	0 5 SS	O to C O to C C to O	C = 322 C = 414 O = 414	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-062-0138	B	SS SS	C to O O to C	O = 407.5 C = 407.5	Steady State Voltage
1-FCV-063-0001	A	SS SS	O to C C to O	C = 413.5 O = 413.5	Steady State Voltage
1-FCV-063-0003	A	SS SS	O to C C to O	C = 400.5 O = 400.5	Steady State Voltage
1-FCV-063-0004	B	SS SS	O to C C to O	C = 390 O = 390	Steady State Voltage
1-FCV-063-0005	B	SS SS	O to C C to O	C = 399.5 O = 399.5	Steady State Voltage
1-FCV-063-0006	B	SS SS	C to O O to C	O = 401.1 C = 401.1	Steady State Voltage
1-FCV-063-0007	A	SS SS	C to O O to C	O = 403.5 C = 403.5	Steady State Voltage
1-FCV-063-0008	A	SS SS	C to O O to C	O = 429.8 C = 429.8	Steady State Voltage
1-FCV-063-0011	B	SS SS	C to O O to C	O = 415.7 C = 415.7	Steady State Voltage
1-FCV-063-0022	B	SS SS	O to C C to O	C = 401.4 O = 401.4	Steady State Voltage
1-FCV-063-0025	B	0 SS	C to O O to C	O = 361.8 C = 414	Need Best avail Voltage at t=0 sec from SI for opening stroke, need steady state for closing stroke.

Calculation No.:
WBNEEBEDQ1999010001

ATTACHMENT 11.9 Required Voltage 89-10 MOV's - Unit 1 Page 4 of 9
JOG Review Plan

Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

VALVEID	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
1-FCV-063-0026	A	0 SS	C to O O to C	O = 343.4 C = 414	Temporary minimum requirement in support of DCN 52837 Stage 2. Need Best avail Voltage at t=0 sec from SI for opening stroke, need steady state for closing stroke.
		0 SS	C to O O to C	O = 370 C = 414	Long term minimum requirement in support of DCN 52837 Stage 3. Need Best avail Voltage at t=0 sec from SI for opening stroke, need steady state for closing stroke.
1-FCV-063-0047	A	SS SS	O to C C to O	C = 403 O = 403	Steady State Voltage
1-FCV-063-0048	B	SS SS	O to C C to O	C = 418.8 O = 418.8	Steady State Voltage
1-FCV-063-0072	A	SS SS	C to O O to C	O = 404.3 C = 404.3	Steady State Voltage
1-FCV-063-0073	B	SS SS	C to O O to C	O = 408.7 C = 408.7	Steady State Voltage
1-FCV-063-0093	A	SS SS	C to O O to C	O = 419.6 C = 419.6	Steady State Voltage
1-FCV-063-0094	B	SS SS	C to O O to C	O = 418.2 C = 418.2	Steady State Voltage
1-FCV-063-0152	A	SS SS	O to C C to O	C = 405.8 C = 405.8	Steady State Voltage
1-FCV-063-0153	B	SS SS	O to C C to O	C = 405.8 O = 405.8	Steady State Voltage
1-FCV-063-0156	A	SS SS	C to O O to C	O = 412.7 C = 412.7	Steady State Voltage
1-FCV-063-0157	B	SS SS	C to O O to C	O = 414 C = 414	Steady State Voltage
1-FCV-063-0172	B	SS SS	C to O O to C	O = 396.7 C = 396.7	Steady State Voltage
1-FCV-063-0175	B	SS SS	O to C C to O	C = 390.7 O = 390.7	Steady State Voltage
1-FCV-067-0083	B	0 5 SS	O to C O to C C to O	C = 322 C = 395.1 O = 404.3	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).

Calculation No.:
WBNEEBEDQ1999010001

ATTACHMENT 11.9 Required Voltage 89-10 MOV's - Unit 1 Page 5 of 9
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Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

VALVEID	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
1-FCV-067-0087	A	0 5 SS	O to C O to C C to O	C = 322 C = 392.4 O = 399.6	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0088	B	0 5 SS	O to C O to C C to O	C = 322 C = 392.2 O = 401.3	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0089	A	0 5 SS	O to C O to C C to O	C = 322 C = 386.7 O = 393.6	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0091	B	0 5 SS	O to C O to C C to O	C = 322 C = 392.4 O = 401.5	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0095	A	0 5 SS	O to C O to C C to O	C = 322 C = 391.6 O = 398.5	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0096	B	0 5 SS	O to C O to C C to O	C = 322 C = 392.8 O = 401.9	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0097	A	0 5 SS	O to C O to C C to O	C = 322 C = 385.9 O = 393	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0099	A	0 5 SS	O to C O to C C to O	C = 322 C = 393.9 O = 401.2	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0103	B	0 5 SS	O to C O to C C to O	C = 322 C = 388 O = 397	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0104	A	0 5 SS	O to C O to C C to O	C = 322 C = 394.3 O = 401.6	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0105	B	0 5 SS	O to C O to C C to O	C = 322 C = 383.1 O = 392	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0107	A	0 5 SS	O to C O to C C to O	C = 322 C = 395.3 O = 402.7	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).

Calculation No.:
WBNEEBEDQ1999010001

ATTACHMENT 11.9 Required Voltage 89-10 MOV's - Unit 1 Page 6 of 9
JOG Review Plan

Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

VALVEID	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
1-FCV-067-0111	B	0 5 SS	O to C O to C C to O	C = 322 C = 389.4 O = 398.5	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0112	A	0 5 SS	O to C O to C C to O	C = 322 C = 395.7 O = 403.1	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0113	B	0 5 SS	O to C O to C C to O	C = 322 C = 384.3 O = 393.2	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0123	B	SS SS	C to O O to C	O = 436.3 C = 436.3	Steady State Voltage
1-FCV-067-0124	B	SS SS	C to O O to C	O = 433.0 C = 433.0	Steady State Voltage
1-FCV-067-0125	A	SS SS	C to O O to C	O = 438.2 C = 438.2	Steady State Voltage
1-FCV-067-0126	A	SS SS	C to O O to C	O = 435.3 C = 435.3	Steady State Voltage
1-FCV-067-0143	A	SS SS	C to O O to C	O = 388.4 C = 388.4	Steady State Voltage
1-FCV-067-0146	A	SS SS	C to O O to C	O = 431 C = 431	Steady State Voltage
1-FCV-068-0332	B	SS SS	C to O O to C	O = 399.9 C = 399.9	Steady State Voltage
1-FCV-068-0333	A	SS SS	C to O O to C	O = 412 C = 412	Steady State Voltage
1-FCV-070-0087	B	0 5 SS	O to C O to C C to O	C = 322 C = 391 O = 403.6	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-070-0089	B	0 5 SS	O to C O to C C to O	C = 322 C = 391.0 O = 426.4	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).

Calculation No.:
WBNEEBEDQ1999010001

ATTACHMENT 11.9

JOG Review Plan

Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

VAL/VID	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
1-FCV-070-0090	A	0 5 SS	O to C O to C C to O	C = 322 C = 398.5 O = 405.8	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-070-0092	A	0 5 SS	O to C O to C C to O	C = 322 C = 400.6 O = 428.0	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-070-0100	A	0 5 SS	O to C O to C C to O	C = 322 C = 393.4 O = 416.6	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-070-0133	A	0 12 SS	O to C O to C C to O	C = 322 C = 414 O = 414	Need 70% Voltage at t=0 sec, Need best Avail Voltage at t=12 sec forward from SI (Normally Open MOV)
1-FCV-070-0134	B	0 12 SS	O to C O to C C to O	C = 322 C = 414 O = 414	Need 70% Voltage at t=0 sec, Need best Avail Voltage at t=12 sec forward from SI (Normally Open MOV)
1-FCV-070-0140	B	0 5 SS	O to C O to C C to O	C = 322 C = 391.9 O = 427.4	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-070-0143	A	0 5 SS	O to C O to C C to O	C = 322 C = 398.5 O = 425.7	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-070-0153	B	SS SS	C to O O to C	O = 391.0 C = 391.0	Steady State Voltage; Active safety function is to operate from close/throttle position to open position.
1-FCV-070-0156	A	SS SS	C to O O to C	O = 434.8 C = 434.8	Steady State Voltage
1-FCV-070-0183	A	SS SS	O to C C to O	C = 395.1 O = 395.1	Steady State Voltage
1-FCV-070-0215	A	SS SS	O to C C to O	C = 395.4 O = 395.4	Steady State Voltage
1-FCV-072-0002	B	5 SS	C to O O to C	O = 412.7 C = 415	Time Delay added per DCN 52834, need best avail Voltage at t=5 sec from SI
1-FCV-072-0013	B	10 SS	C to O O to C	O = 414 C = 414	Need Best Avail Voltage at t= 10 sec from SI (MOV will not get a signal to open until after time delay per DCN 52834)
1-FCV-072-0021	B	SS SS	O to C C to O	C = 402.2 O = 402.2	Steady State Voltage

R73

Calculation No.:
WBNEEBEDQ1999010001

ATTACHMENT 11.9 Required Voltage 89-10 MOV's - Unit 1 Page 8 of 9
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Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

VALVEID	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
1-FCV-072-0022	A	SS SS	O to C C to O	C = 400.2 O = 400.2	Steady State Voltage
1-FCV-072-0034	A	10 SS	C to O O to C	O = 414 C = 414	Need Best Avail Voltage at t= 10 sec from SI (MOV will not get a signal to open until after time delay per DCN 52834)
1-FCV-072-0039	A	5 SS	C to O O to C	O = 411.3 C = 415	Time Delay added per DCN 52834, need best avail Voltage at t=5 sec from SI
1-FCV-072-0040	A	SS SS	C to O O to C	O = 405.7 C = 405.7	Steady State Voltage
1-FCV-072-0041	B	SS SS	C to O O to C	O = 396 C = 396	Steady State Voltage
1-FCV-072-0044	A	SS SS	C to O O to C	O = 414 C = 414	Steady State Voltage
1-FCV-072-0045	B	SS SS	C to O O to C	O = 414 C = 414	Steady State Voltage
1-FCV-074-0001	A	SS SS	O to C C to O	O = 414 C = 414	Steady State Voltage
1-FCV-074-0002	B	SS SS	C to O O to C	O = 414 C = 414	Steady State Voltage
1-FCV-074-0003	A	SS SS	O to C C to O	C = 424.2 O = 424.2	Steady State Voltage
1-FCV-074-0008	A	SS SS	O to C C to O	C = 414 O = 414	Steady State Voltage
1-FCV-074-0009	B	SS SS	O to C C to O	C = 419.4 O = 419.4	Steady State Voltage
1-FCV-074-0012	A	0 SS	C to O O to C	O = 345.4 C = 393.7	Need Best avail Voltage at t=0 sec from SI (OPEN); and SS (CLOSED)
1-FCV-074-0021	B	SS SS	O to C C to O	C = 422.3 O = 422.3	Steady State Voltage
1-FCV-074-0024	B	0 SS	C to O O to C	O = 347.2 C = 383.8	Need Best avail Voltage at t=0 sec from SI (OPEN); and SS (CLOSED)
1-FCV-074-0033	A	SS SS	O to C C to O	C = 394.6 O = 394.6	Steady State Voltage

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ATTACHMENT 11.9

JOG Review Plan

Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

The voltages listed in this Attachment must be met or exceeded.

R73 Prepared By William F. Colte Date: Reviewed By John V. Miller Date:

1873

1A BOARDS

ETAP Node ID	MOV	Available Voltage (New Analysis) Value from SS	Time from SI Signal (SS = steady state)	New Design Margin (using new Voltages) (open)	New Design Margin (using new Voltages) (closed)	Comments**
235-5B	RHR Sys Isln Vlv 1-FCV-74-1-A (2.6HP)	90.74*	SS	13.30%	18.80%	Acceptable Margin
235-6D	RCS Press Relief FCV 1-FCV-68-333-A (1.9HP)	89.20*	SS	19.90%	15.80%	Acceptable Margin
235-11B	RHR Hx A To CVCS Chrg Pmp 1-FCV-63-8-A (1.9HP)	87.48	SS	13.20%	124.60%	Acceptable Margin
235-12A	SIS Pmp 1A-A Inlet Vlv 1-FCV-63-47-A (1.9HP)	88.18*	SS	19.60%	16.10%	Acceptable Margin
235-12D	SIS To RCS Loops 2&3 FCV 1-FCV-63-93-A (1.6 HP)	88.65	SS	18.60%	140.30%	Acceptable Margin
235-12E	SIS Pmp 1A-A Outlet FCV 1-FCV-63-152-A (1.9HP)	88.48*	SS	29.50%	39.40%	Acceptable Margin
235-13A	SIS Pmp Out RCS Lp 1&3 Hot Leg 1-FCV-63-156-A (1.9HP)	89.28*	SS	15.40%	15.90%	Acceptable Margin
235-13B	Cntrmt Sump To Spray Hdr 1A FCV 1-FCV-72-44-A (3.2HP)	90.33*	SS	35.50%	105.93%	Acceptable Margin
235-14A	RHR Spray Hdr 1A Isln Vlv 1-FCV-72-40-A (1.9HP)	87.66	SS	75.20%	121.90%	Acceptable Margin
235-14E	RHR Hx 1A Bypass Vlv 1-FCV-74-33-A (2HP)	85.27	SS	79.30%	45.10%	Acceptable Margin
236-9D	Up Cntrmt Clr 1A Disc Iso Vlv 1-FCV-67-295 (0.13HP)	81.98	Not 89-10	28.96%	28.96%	Acceptable Margin
236-2D	AFWP Turb Stm Sup Fm Stm Gen 1 1-FCV-1-15-A (1HP)	92.47*	SS	14.50%	35.40%	Acceptable Margin
236-5E	Cntrmt Spray Hx 1A Sup Cont Vlv 1-FCV-67-125-A (0.33HP)	92.51*	SS	24.40%	24.40%	Acceptable Margin
236-5F	Cntrmt Spray Hx 1A Disch Vlv 1-FCV-67-126-A (0.33HP)	92.19*	SS	24.40%	24.40%	Acceptable Margin
236-6A	AFWP Turb St Sply Frm St gen 4 1-FCV-1-16-A (1HP)	92.52*	SS	14.50%	35.40%	Acceptable Margin
236-6D	RHR Sys Isln Bypass Vlv 1-FCV-74-8-A (1.6HP)	90.99*	SS	17.50%	42.40%	Acceptable Margin
236-11A	Cmpnt Clg Hx A Disch Cont Vlv 1-FCV-67-146-A (0.3HP)	87.97	SS	13.50%	13.50%	Acceptable Margin
236-17B	SFPCS Hx Sply Hdr Isln Vlv 0-FCV-70-197-A (0.3HP)	89.63	SS	28.10%	28.10%	Acceptable Margin
235-11A	SIS Pmp Inlet To CVCS Chrg Pmp 1-FCV-63-7-A (1.9HP)	88.21*	SS	9.40%	105.40%	Acceptable Margin
235-12B	Cntrmt Sump To RHR Pmp A-A 1-FCV-63-72-A (13HP)	85.00	SS	21.50%	1781.80%	Acceptable Margin
236-12B	SS&Con AirCpsr Sup Hdr A Iso V 0-FCV-67-205-A (0.33.9HP)	86.86	SS	78.40%	78.40%	Acceptable Margin
236-16E	RHR Hx A-A Outlet Vlv 1-FCV-70-156-A (0.33.9HP)	87.86	SS	24.40%	24.40%	Acceptable Margin
203-7D	RHR PMP 1A-A INLET FCV 1-FCV-74-3-A (5.2HP)	90.31	SS	125.80%	2250.80%	Acceptable Margin
203-7E	RWST TO SPRAY HDR 1A FCV 1-FCV-72-22-A (3.2HP)	85.27	SS	273.70%	266.60%	Acceptable Margin

* Calculated voltage considering Hammer Blow feature (using 50% LRC during unseating)

**Calculated voltages based on the new analysis have been reviewed and are considered acceptable based on the available margin.

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1B BOARDS

ETAP Node ID	MOV	Available Voltage (New Analysis)	Value from SS	Time from SI Signal (SS = steady state)	New Design Margin (using new Voltages) (open)	New Design Margin (using new Voltages) (closed)	Comments **
205-7D	RHR PMP 1B-B INLET FCV 1-FCV-74-21-B (5.2HP)	91.00	SS		107.10%	1705.70%	Acceptable Margin
237-5E	RCS Press Relief Flow Cont Vlv 1-FCV-68-332-B (1.9HP)	88.06*	SS		>21.7%	>13.5%	Acceptable Margin
237-9B	RHR To RCS H.L. 1&3 Flow Iso V 1-FCV-63-172-B (2.6HP)	85.99	SS		59.20%	87.40%	Acceptable Margin
237-11B	RHR Hx B To SIS Pmp 1-FCV-63-11-B (2HP)	85.71	SS		8.90%	124.60%	Acceptable Margin
237-13A	SIS Pmp 1B-B Outlet FCV 1-FCV-63-153-B (1.9HP)	88.75*	SS		19.90%	30.10%	Acceptable Margin
237-13B	SIS PMP OUT RCS LP 2& 4 H. LEG 1-FCV-63-157-B (1.9HP)	91.36*	SS		11.10%	11.50%	Acceptable Margin
237-13D	SIS 1B-B Dsh To RWST Shtrff Vlv 1-FCV-63-175-B (0.7HP)	84.70	SS		977.40%	77.10%	Acceptable Margin
237-14D	RHR Spray Hdr 1B Isln Vlv 1-FCV-72-41-B (1.9HP)	85.82	SS		66.90%	111.40%	Acceptable Margin
237-14E	Cntrmt Sump To Spray Hdr 1B FCV 1-FCV-72-45-B (3.2HP)	89.68*	SS		3.30%	57.00%	Acceptable Margin
238-2E	St Flow To AFWP Turb Isln Vlv 1-FCV-1-18-B (1HP)	92.50*	SS		95.80%	18.20%	Acceptable Margin
238-5F	Cntrmt Spray Hx 1B Disch Vlv 1-FCV-67-124-B (0.33HP)	91.73*	SS		24.40%	24.40%	Acceptable Margin
238-5E	Cntr Spray Hx 1B Sup Cont Vlv 1-FCV-67-123-B (0.33HP)	92.08*	SS		24.40%	24.40%	Acceptable Margin
205-7E	RWST TO SPRAY HDR 1B Vlv 1-FCV-72-22-B (3.3HP)	86.79	SS		291.10%	283.70%	Acceptable Margin
237-10A	SIS 1A-A DSH TO RWST SHTFF VLV 1-FCV-63-4-B (0.7HP)	84.57	SS		943.70%	76.10%	Acceptable Margin
237-10B	RWST To SIS Pump Flow Cont Vlv 1-FCV-63-5-B (1.9HP)	88.02*	SS		17.30%	38.60%	Acceptable Margin
237-11A	SIS PMP INLT TO CVCS CHRG PMP 1-FCV-63-6-B (1.9HP)	88.21*	SS		11.30%	118.70%	Acceptable Margin
237-12B	SIS Pmp 1B-B Inlet Vlv 1-FCV-63-48-B (1.9HP)	90.23 *	SS		39.00%	46.60%	Acceptable Margin
237-12D	CNTMT SUMP TO RHR PMP B-B 1-FCV-63-73-B (13HP)	88.03	SS		17.40%	2117.00%	Acceptable Margin
237-14A	Cntrmt Spray Hdr 1B Isln Vlv 1-FCV-72-2-B (3.2HP)	92.86*	5s		10.40%	359.00%	Acceptable Margin
238-3A	ERCW Hdr B Isln Vlv 1-FCV-3-179A-B (0.33HP)	83.46	SS		22.10%	19.00%	Acceptable Margin
238-17D	CCS HX B ERCW BYPASS FCV 0-FCV-67-144-B (0.13HP)	82.00	SS		110.40%	112.00%	Acceptable Margin
237-15D	RHR Hx 1B Bypass Vlv 1-FCV-74-35-B (1.9HP)	81.00	SS		64.30%	37.80%	Acceptable Margin
* Calculated voltage considering Hammer Blow feature (using 50% LRC during unseating)							
**Calculated voltages based on the new analysis have been reviewed and are considered acceptable based on the available margin.							

R2

VALVE ID	T(sec) from SI: 0, 5, or SS	MOV Position Change	Comments	OLD Min. Voltage Required to Achieve Position	Stroke Time (Secs)	NEW Min. Voltage Required to Achieve Position
2-FCV-1-15	SS	either	Steady State Voltage	O= 415 C= 415	20	O= 428.3 C= 428.3
2-FCV-1-16	SS	either	Steady State Voltage	O= 415 C= 415	20	O= 428.2 C= 428.2
2-FCV-1-17	SS	O to C	Steady State Voltage	O= 415 C= 415	16	O= 428.3 C= 428.3
2-FCV-1-18	SS	O to C	Steady State Voltage	O= 415 C= 415	16	O= 423.3 C= 423.3
2-FCV-1-51	0	C to O	125 VDC Motor, Need Best Avail Voltage at T=0 sec from SI	Not evaluated	16	O= 90V C= 90V
2-FCV-3-33	4	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=4 sec from SI (5.75 sec stroke time). Based on review of dP test MOV could become dP loaded just before 5 sec.	O- 390.3 C- 415.	6.5	O= 414 C= 414
2-FCV-3-47	4	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=4 sec from SI (5.75 sec stroke time). Based on review of dP test MOV could become dP loaded just before 5 sec.	O- 390.3 C- 415.	6.5	O= 414 C= 414
2-FCV-3-87	4	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=4 sec from SI (5.75 sec stroke time). Based on review of dP test MOV could become dP loaded just before 5 sec.	O- 376.9 C- 415.	6.5	O= 414 C= 414
2-FCV-3-100	4	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=4 sec from SI (5.75 sec stroke time). Based on review of dP test MOV could become dP loaded just before 5 sec.	O- 390.3 C- 415.	6.5	O= 414 C= 414
2-FCV-3-116A	SS	C to O	Steady State Voltage	O= 415 C= 415.	10	O= 413.3 C= 413.3
2-FCV-3-116B	SS	C to O	Steady State Voltage	O= 415 C= 415.	10	O= 413.2 C= 413.2
2-FCV-3-126A	SS	C to O	Steady State Voltage	O= 408 C= 408	10	O= 406.1 C= 406.1
2-FCV-3-126B	SS	C to O	Steady State Voltage	O= 408 C= 408	10	O= 406.1 C= 406.1
2-FCV-3-136A	SS	C to O	Steady State Voltage	O= 415 C= 415.	15	O= 412.2 C= 412.2
2-FCV-3-136B	SS	C to O	Steady State Voltage	O= 415 C= 415.	15	O= 412.3 C= 412.3
2-FCV-3-179A	SS	C to O	Steady State Voltage	O= 405 C= 405.	15	O= 409 C= 409
2-FCV-3-179B	SS	C to O	Steady State Voltage	O= 405 C= 405.	15	O= 409 C= 409
2-FCV-26-240	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (6.21 sec stroke time)	O= 408.7 C= 401.3	20	O= 430.6 C= 406.9
2-FCV-26-243	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (6.21 sec stroke time)	O= 408.7 C= 401.3	20	O= 426.5 C= 403
2-FCV-62-61	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (5.25 sec stroke time)	O= 415 C= 340.	10	O= 401.2 C= 401.2
2-FCV-62-63	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (5.25 sec stroke time)	O= 405 C= 378.5.	10	O= 380.5 C= 380.5
2-FCV-62-90	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (8.80 sec stroke time)	O= 415 C= 415.	10	O= 414 C= 414
2-FCV-62-91	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (8.25 sec stroke time)	O= 415 C= 415.	10	O= 414 C= 414

VALVE ID	T(sec) from SI: 0, 5, or SS	MOV Position Change	Comments	OLD Min. Voltage Required to Achieve Position	Stroke Time (Secs)	NEW Min. Voltage Required to Achieve Position
2-LCV-62-132	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (5.25 sec stroke time)	O= 390 C= 322	10	O= 417.8 C= 394.7
2-LCV-62-133	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (5.25 sec stroke time)	O= 390 C= 334	10	O= 418.7 C= 394.7
2-LCV-62-135	0	C to O	Need Best avail Voltage at t=0 sec from SI	O= 401.8 C= 409.3	15	O= 320.0 C= 396.3
2-LCV-62-136	0	C to O	Need Best avail Voltage at t=0 sec from SI	O= 376.3 C= 411.3	15	O= 342.9 C= 413.0
2-FCV-62-138	SS	C to O	Steady State Voltage	O= 384 C= 384	6	O= 421.4 C= 421.4
2-FCV-63-001	SS	O to C	Steady State Voltage	O= 413.5 C= 413.5	60	O= 364.2 C= 362.2
2-FCV-63-003	SS	O to C	Steady State Voltage	O= 401 C= 401	10	O= 426.3 C= 426.3
2-FCV-63-004	SS	O to C	Steady State Voltage	O= 390 C= 390	10	O= 416.4 C= 416.4
2-FCV-63-005	SS	O to C	Steady State Voltage	O= 395 C= 395	14	O= 404.4 C= 404.4
2-FCV-63-006	SS	C to O	Steady State Voltage	O= 395 C= 395	10	O= 396.7 C= 396.7
2-FCV-63-007	SS	C to O	Steady State Voltage	O= 399 C= 399	10	O= 396.5 C= 396.5
2-FCV-63-008	SS	C to O	Steady State Voltage	O= 415 C= 415	28	O= 430.7 C= 430.7
2-FCV-63-011	SS	C to O	Steady State Voltage	O= 415 C= 415	28	O= 429.6 C= 429.6
2-FCV-63-022	SS	O to C	Steady State Voltage	O= 407 C= 407	17	O= 408.6 C= 408.6
2-FCV-63-025	0	C to O	Need Best avail Voltage at t=0 sec from SI	O= 415 C= 415	12	O= 414 C= 414
2-FCV-63-026	0	C to O	Need Best avail Voltage at t=0 sec from SI	O= 415 C= 415	12	O= 414 C= 414
2-FCV-63-047	SS	O to C	Steady State Voltage	O= 400 C= 400.	15	O= 385.6 C= 385.6
2-FCV-63-048	SS	O to C	Steady State Voltage	O= 415 C= 415	15	O= 408.2 C= 408.2
2-FCV-63-067	SS	Open Only	Steady State Voltage		105	O = 322
2-FCV-63-072	SS	C to O	Steady State Voltage	O = 415 C = 415	60	O = 410 C = 410
2-FCV-63-073	SS	C to O	Steady State Voltage	O = 415 C = 415	60	O = 420 C = 420
2-FCV-63-080	SS	Open Only	Steady State Voltage		105	O = 322
2-FCV-63-093	SS	either	Steady State Voltage	O= 415 C= 415	40	O = 451.1 C = 451.1
2-FCV-63-094	SS	either	Steady State Voltage	O= 415 C= 415	40	O = 451.8 C = 451.8

AUXILIARY POWER SYSTEM ANALYSIS
 WBN-EEB-EDQ000-999-2007-0002,
 ATTACHMENT 11.5

WBN Unit 2 GL 89-10
Required Voltage Vs Time

VALVEID	T(sec) from SI: 0, 5, or SS	MOV Position Change	Comments	OLD Min. Voltage Required to Achieve Position	Stroke Time (Secs)	NEW Min. Voltage Required to Achieve Position
2-FCV-63-098	SS	Open Only	Steady State Voltage		105	O = 322
2-FCV-63-118	SS	Open Only	Steady State Voltage		105	O = 322
2-FCV-63-152	SS	O to C	Steady State Voltage	O= 415 C= 415	15	O = 414.6 C = 414.6
2-FCV-63-153	SS	O to C	Steady State Voltage	O= 415 C= 415	15	O = 415.7 C = 415.7
2-FCV-63-156	SS	C to O	Steady State Voltage	O= 415 C= 415	17	O = 414.4 C = 414.4
2-FCV-63-157	SS	C to O	Steady State Voltage	O= 415 C= 415	17	O = 428.6 C = 428.6
2-FCV-63-172	SS	either	Steady State Voltage	O= 394 C= 394	120	O = 395.2 C = 395.2
2-FCV-63-175	SS	O to C	Steady State Voltage	O= 400 C= 400	10	O = 419.5 C = 419.5
1-FCV-67-66	0	C to O	Need best voltage at T = 0 Secs from SI		66	O = 362.4 C = 362.4
1-FCV-67-67	0	C to O	Need best voltage at T = 0 Secs from SI		66	O = 361.9 C = 361.9
2-FCV-67-66	0	C to O	Need best voltage at T = 0 Secs from SI		66	O = 360.8 C = 360.8
2-FCV-67-67	0	C to O	Need best voltage at T = 0 Secs from SI		66	O = 363.8 C = 363.8
2-FCV-67-83	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 364	66	O = 434.8 C = 410.1
2-FCV-67-87	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 362	66	O = 431.5 C = 407
2-FCV-67-88	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 340	66	O = 422.5 C = 402.6
2-FCV-67-89	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 322	66	O = 322 C = 322
2-FCV-67-91	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 364	66	O = 433.9 C = 409.3
2-FCV-67-95	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 361	66	O = 430.7 C = 406.1
2-FCV-67-96	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 341	66	O = 423 C = 403.1
2-FCV-67-97	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 393.0 C=385.9	66	O = 322 C = 322
2-FCV-67-99	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 340	66	O = 422.5 C = 402.6
2-FCV-67-103	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 340	66	O = 422.4 C = 402.6
2-FCV-67-104	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 370	66	O = 441.7 C = 416.6
2-FCV-67-105	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 329	66	O = 322 C = 322

VALVED	T(sec) from SI: 0, 5, or SS	MOV Position Change	Comments	OLD Min. Voltage Required to Achieve Position	Stroke Time (Secs)	NEW Min. Voltage Required to Achieve Position
2-FCV-67-107	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 342	66	O = 424.1 C = 404.1
2-FCV-67-111	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 342	66	O = 424.3 C = 404.4
2-FCV-67-112	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 364	66	O = 434.8 C = 410.1
2-FCV-67-113	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 393.2 C= 386.1	66	O = 322 C = 322
2-FCV-67-123	SS	C to O	Steady State Voltage	O= 415 C= 415	70	O = 436.3 C = 436.3
2-FCV-67-124	SS	C to O	Steady State Voltage	O= 415 C= 415	70	O = 433 C = 433
2-FCV-67-125	SS	C to O	Steady State Voltage	O= 415 C= 415	70	O = 441.8 C = 441.8
2-FCV-67-126	SS	C to O	Steady State Voltage	O= 415 C= 415	70	O = 439.4 C = 439.4
2-FCV-67-130	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-131	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-133	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-134	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-138	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-139	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-141	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-142	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-143	SS	either	Steady State Voltage	O= 415 C= 415	180	O= 418.8 C= 418.8
2-FCV-67-295	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-296	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-297	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-298	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-148	SS	either	Steady State Voltage	O= 415 C= 415	60	O= 435.9 C= 435.9
2-FCV-68-332	SS	either	Steady State Voltage	O= 407 C= 407	20	O= 408.6 C= 408.6
2-FCV-68-333	SS	either	Steady State Voltage	O= 415 C= 415	20	O= 418.7 C= 418.7

VALVE ID	T(sec) from SI: 0, 5, or SS	MOV Position Change	Comments	OLD Min. Voltage Required to Achieve Position	Stroke Time (Secs)	NEW Min. Voltage Required to Achieve Position
2-FCV-70-087	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (24.04 sec stroke time)	O= 403.6 C= 396.2	66	O= 441.6 C= 420.8
2-FCV-70-089	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 400 C= 348	66	O= 406 C= 386.9
2-FCV-70-090	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (24.04 sec stroke time)	O= 415 C= 365	66	O= 436.1 C= 411.3
2-FCV-70-092	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 376	66	O= 449.2 C= 423.7
2-FCV-70-100	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 392.5 C= 385.4	66	O= 442.7 C= 417.5
2-FCV-70-133	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (16.8 sec stroke time)	O= 395.5 C= 415	66	O= 424.6 C= 400.4
2-FCV-70-134	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (16.8 sec stroke time)	O= 415 C= 415	66	O= 419.8 C= 400.1
2-FCV-70-140	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 327	66	O= 422.6 C= 402.7
2-FCV-70-143	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Closed Butterfly Valve, will close if opened, 62.65 sec stroke time. No opening accident requirement)	O= 415 C= 363	66	O= 432.7 C= 408.1
1-FCV-70-153	SS	C to O	Steady State Voltage		90	O= 416.76 C= 416.76
2-FCV-70-153	SS	C to O	Steady State Voltage		90	O= 434.2 C= 434.2
2-FCV-70-156	SS	C to O	Steady State Voltage	O= 415 C= 415	90	O= 443.3 C= 443.3
2-FCV-70-183	SS	O to C	Steady State Voltage	O= 415 C= 415	30	O= 425 C= 425
2-FCV-70-215	SS	O to C	Steady State Voltage	O= 415 C= 415	30	O= 425.7 C= 425.7
2-FCV-72-2	5	C to O	Need Best avail Voltage at t=0 sec from SI	O= 415 C= 415	28	O= 398.1 C= 398.1
2-FCV-72-13	10	C to O	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=10 sec from SI (10 sec time delay)	O= 410 C= 415	10	O= 396 C= 396
2-FCV-72-21	SS	O to C	Steady State Voltage	O= 415 C= 415	15	O= 423.7 C= 423.7
2-FCV-72-22	SS	O to C	Steady State Voltage	O= 402 C= 402	15	O= 406 C= 406
2-FCV-72-34	10	C to O	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=10 sec from SI (10 sec time delay)	O= 404 C= 404	10	O= 390.8 C= 390.8
2-FCV-72-39	5	C to O	Need Best avail Voltage at t=0 sec from SI	O= 415 C= 415	28	O= 399 C= 399
2-FCV-72-40	SS	C to O	Steady State Voltage	O= 415 C= 415	15	O= 427.6 C= 427.6
2-FCV-72-41	SS	C to O	Steady State Voltage	O= 415 C= 415	15	O= 427.6 C= 427.6
2-FCV-72-44	SS	C to O	Steady State Voltage	O= 400 C= 400	20	O= 405.4 C= 405.4
2-FCV-72-45	SS	C to O	Steady State Voltage	O= 400 C= 400	20	O= 412.8 C= 412.8

AUXILIARY POWER SYSTEM ANALYSIS
 WBN-EEB-EDQ000-999-2007-0002,
 ATTACHMENT 11.5

WBN Unit 2 GL 89-10
Required Voltage Vs Time

VALVEID	T(sec) from SI: 0, 5, or SS	MOV Position Change	Comments	OLD Min. Voltage Required to Achieve Position	Stroke Time (Secs)	NEW Min. Voltage Required to Achieve Position
2-FCV-74-01	SS	O to C	Steady State Voltage	O= 415 C= 415.	120	O= 414 C= 414
2-FCV-74-02	SS	C to O	Steady State Voltage	O= 415 C= 415.	120	O= 414 C= 414
2-FCV-74-03	SS	O to C	Steady State Voltage	O= 358 C= 358	60	O= 356.7 C= 356.7
2-FCV-74-08	SS	O to C	Steady State Voltage	O= 415 C= 415.	120	O= 425.8 C= 425.8
2-FCV-74-09	SS	O to C	Steady State Voltage	O= 415 C= 415.	120	O= 423.7 C= 423.7
2-FCV-74-12	0	C to O	Need Best avail Voltage at t=0 sec from SI	O= 386.6 C= 415	15	O= 337.3 C= 394.6
2-FCV-74-21	SS	O to C	Steady State Voltage	O= 392 C= 392	60	O= 393.3 C= 393.3
2-FCV-74-24	0	C to O	Need Best avail Voltage at t=0 sec from SI	O= 376.8 C= 415	15	O= 341.1 C= 387.2
2-FCV-74-33	SS	O to C	Steady State Voltage	O= 405 C= 405	15	O= 410 C= 410
2-FCV-74-35	SS	O to C	Steady State Voltage	O= 385 C= 385	15	O= 386.6 C= 386.6
Notes:						
1) The maximum required voltage for any GL 89-10 MOV is equal to or above 90% of 460 V (414 V). Guidance given in Design Standard DS-M18.2.21 states that for voltages 90% or greater the voltage factor is 1.0 (i.e. no degradation is required at 90% or above). Therefore, there will be no impact to any Mechanical MOV calculations as long as 90% of 460 V (414 V) is achieved.						
2) Required voltage for MOVs at T = 0, T = 4, T = 5 or T = 10 sec is the minimum available voltage from the time specified to any time forward during the SI. Example: If a 4 sec voltage was requested and voltage dropped at 5 sec, then the lower 5 sec voltage should be used to bound degraded voltage.						
3) For MOVs that are open and go closed upon receiving an SI signal, the required voltage at T = 0 is only 70% of 460 V (322 V) until the valve becomes loaded. MOVAT's differential pressure test traces were reviewed and conservative bounding times were determined for when the MOV becomes loaded. A 70% starting voltage is based on guidance provided in Limitorque Technical Update 98-01 in Vendor Manual WBN-VTD-L200-0460.						
The voltages listed in this Attachment must be met or exceeded.						
Prepared By:	J. Dwyer	Date: 5/1/11	Reviewed By:	M. R. Johnson	Date: 5/1/11	
	KARINA SORI					

2A BOARDS

ETAP Node ID	MOV	Available Voltage (New Analysis) Value from SS	Time from SI Signal (SS = steady state)	New Design Margin (using new Voltages) (open)	New Design Margin (using new Voltages) (closed)	Comments **
239-10B	SIS PMPS RECIRC TO RWST 2-FCV 63-3-A (0.7HP)	86.31	SS	975	47.8	Acceptable Margin
239-11A	SIS Pmp Inlet To CVCS Chrg Pmp 2-FCV 63-7-A (1.9HP)	80.28	SS	20	87	Acceptable Margin
239-14E	RHR Hx 2A Bypass Vlv 2-FCV 74-33-A (1.9HP)	82.97	SS	30	40	Acceptable Margin
239-11B	RHR Hx A To CVCS Chrg Pmp 2-FCV 63-8-A (1.9HP)	87.15	SS	13	135	Acceptable Margin
239-9F	RWST To Spray Hdr 2A FCV 2-FCV 72-22-A (3.2HP)	87.24	SS	288	272	Acceptable Margin
239-12A	SIS Pmp 2A A Inlet Vlv 2-FCV 63-47-A (1.9HP)	78.09	SS	108	26	Acceptable Margin
239-12D	SIS To RCS Loops 2&3 FCV 2-FCV 63-93-A (1.6HP)	91.22	SS	180	153	Acceptable Margin
239-12E	SIS Pmp 2A A Outlet FCV 2-FCV 63-152-A (1.9HP)	89.49*	SS	20	29	Acceptable Margin
239-13A	SIS Pmp Out RCS Lp 1&3 Hot Leg 2-FCV 63-156-A (1.9HP)	83.86	SS	15	28	Acceptable Margin
239-6D	RCS Press Relief FCV 2-FCV-68-333-A (1.9HP)	85.43	SS	22	19	Acceptable Margin
239-13B	Cntrnt Sump To Spray Hdr 2A FCV 2-FCV 72-44-A (3.2HP)	82	SS	17	43	Acceptable Margin
239-14A	RHR Spray Hdr 2A Isln Vlv 2-FCV 72-40-A (1.9HP)	86.5	SS	103	156	Acceptable Margin
239-13E	Cntrnt Spray Hdr 2A Isln Vlv 2-FCV-72-39-A (3.2HP)	79.41	5 sec	18.5	162.5	Acceptable Margin
240-15A	CCS HX B ERCW BYPASS FCV 2-FCV-67-143-A (0.13HP)	78.67	SS	222	270	Acceptable Margin
240-16E	RHR Hx A-A Outlet Vlv 2-FCV-70-156-A (0.33HP)	89.51	SS	14	14	Butterfly Valve & Acceptable Margin
240-17A	Sample Hx Hdr Outlet Vlv 2-FCV-70-183-A (0.13HP)	86.06	SS	134	147	Acceptable Margin
240-2A	ERCW Hdr A Isln Vlv 2-FCV-3-116A-A (0.25HP)	83.72	SS	99	115	Acceptable Margin
240-2B	ERCW Hdr A Isln Vlv 2-FCV-3-116B-A (0.25HP)	83.68	SS	86	115	Acceptable Margin
240-2D	AFWP Turb Stm Sup Fm Stm Gen 1 2-FCV-1-15-A (1HP)	91.15*	SS	25	45	Acceptable Margin
240-2E	St Flow To AFWP Turb Iso Vlv 2-FCV-1-17-A (1HP)	91.15*	SS	85	20	Acceptable Margin
240-3A	ERCW Hdr A Isln Vlv 2-FCV-3-136A-A (0.33HP)	83.49	SS	22	42	Acceptable Margin
240-3B	ERCW Hdr A Isln Vlv 2-FCV-3-136B-A (0.33HP)	83.5	SS	22	42	Acceptable Margin
240-5A	Sample Hx Isln Vlv 2-FCV-70-215-A (0.13HP)	86.16	SS	227	231	Acceptable Margin
240-5E	Cntrnt Spray Hx 2A Sup Cont Vlv 2-FCV-67-125-A (0.33HP)	89.4	SS	14	14	Butterfly Valve & Acceptable Margin
240-5F	Cntrnt Spray Hx 2A Disch Vlv 2-FCV-67-126-A (0.33HP)	88.91	SS	14	14	Butterfly Valve & Acceptable Margin
240-6A	AFWP Turb Stm Sup Fm Stm Gen 4 2-FCV-1-16-A (1HP)	91.14*	SS	25	31	Acceptable Margin
240-11A	Cmpnt Clg Hx A Disch Cont Vlv 2-FCV-67-146-A (0.33HP)	88.48	SS	9.4	9.4	Acceptable Margin

* Calculated voltage considering Hammer Blow feature (using 50% LRC during unseating)

**Calculated voltages based on the new analysis have been reviewed and are considered acceptable based on the available margin.

2B BOARDS

ETAP Node ID	MOV	Available Voltage (New Analysis)	Time from SI Signal (SS = steady state)	New Design Margin (using new Voltages) (open)	New Design Margin (using new Voltages) (closed)	Comments **
209-7E	RWST To Spray Hdr 2B FCV- 2-FCV-72-21-B (3.2 hp)	89.23	SS	211	295	Acceptable Margin
241-5E	RCS Press Relief FCV 2-FCV-68-332-B (2 hp)	83.26	SS	29	17	Acceptable Margin
241-9B	RHR To RCS H.L. 1&3 Flow Isol Vv 2-FCV-63-172-B (2.6 hp)	80.11	SS	45	69	Acceptable Margin
241-10A	SIS 2B-B Dsh To RWST Shlf Vv 2-FCV-63-4-B (0.66 hp)	84.47	SS	900	50	Acceptable Margin
241-10B	RWST To SIS Pump FCV 2-FCV-63-5-B (2 hp)	81.8	SS	45	23	Acceptable Margin
241-10F	RWST To Spray Hdr 2B FCV- 2-FCV-72-21-B (3.2 hp)	85.62	SS	260	250	Acceptable Margin
241-11A	SIS Pmp Inlet To CVCS Chrg Pmp 2-FCV-63-6-B (2 hp)	80.24	SS	16	86	Acceptable Margin
241-11B	RHR Hx-B to SIS Pmp 2-FCV-63-11-B (2 hp)	86.86	SS	13	134	Acceptable Margin
241-12B	SIS Pmp 2B-B Inlet Vlv 2-FCV-63-48-B (2 hp)	82.55	SS	130	40	Acceptable Margin
241-12D	Cntrmt Sump To RHR Pmp B-B 2-FCV-63-73-B (13.2 hp)	90.37	SS	36	2000	Acceptable Margin
241-12E	SIS To RCS Loops 1 & 4 FCV- 2-FCV-63-94-B (1.6 hp)	91.33	SS	187	157	Acceptable Margin
241-13A	SIS Pmp 2B-B Outlet FCV- 2-FCV-63-153-B (2 hp)	89.61*	SS	20	29	Acceptable Margin
241-13B	SIS pmp Out RCS Lp 2&4 Hot Leg 2-FCV-63-157-B (2 hp)	86.64	SS	13	26	Acceptable Margin
241-13D	SIS 2B-B Dsh to RWST Shlf Vv 2-FCV-63-175-B (0.66 hp)	84.87	SS	900	48	Acceptable Margin
241-14A	Cntrmt Spray Hdr 2B Isln Vlv 2-FCV-72-2-B (3.2 hp)	85.35	SS	28	185	Acceptable Margin
241-14D	RHR SPRAY HDR-2B-ISOL VLV 2-FCV-72-41-B (2 hp)	90.92*	SS	90	140	Acceptable Margin
241-14E	Cntrmt Sump To Spray Hdr 2B FCV 2-FCV-72-45-B (3.3 hp)	89.25*	SS	37	65	Acceptable Margin
241-15D	RHR Hx-2B Bypass Vlv 2-FCV-74-35-B (2 hp)	78.21	SS	20	29	Acceptable Margin
241-11E	SIS Boron Inj Tank Shutoff Vlv 2-FCV-63-25-B (1.9 hp)	82.51	5-sec	30.2	24.7	Acceptable Margin
241-15B	RHR Pmp 2B-B Min Flow Vlv 2-FCV-74-24-B (0.1 hp)	71.67	0 sec	290.2	48.5	Acceptable Margin
242-2B	ERCW Hdr-B Isln Vlv 2-FCV-3-126B-B (0.67 hp)	83.06	SS	86	115	Acceptable Margin
242-2E	St Flow To AFWP Turb Isln Vlv 2-FCV-1-18-B (1 hp)	90.84*	SS	85	20	Acceptable Margin
242-3A	ERCW Hdr-B Isln Vlv 2-FCV-3-179A-B (0.33 hp)	83.66	SS	19	39	Acceptable Margin
242-3B	ERCW Hdr-B Isln Vlv 2-FCV-3-179B-B (0.33 hp)	83.67	SS	19	39	Acceptable Margin
242-5E	Cntrmt Spray Hx 2B Sup Cont Vlv 2-FCV-67-123-B (0.33 hp)	89.15	SS	14	14	Butterfly Valve & Acceptable Margin
242-5F	Cntrmt Spray Hx 2B Sup Disch Vlv 2-FCV-67-124-B (0.33 hp)	88.5	SS	14	14	Butterfly Valve & Acceptable Margin
242-17A	SFPSCS Hx Sply Hdr Isln Vlv 0-FCV-70-194-B (0.33HP)	92.18*	SS	28.10%	28.10%	Acceptable Margin
242-15E	RHR Hx-B-B Outlet Vlv 2-FCV-70-153-B (0.33HP)	85	SS			Acceptable Margin

* Calculated voltage considering Hammer Blow feature (using 50% LRC during unseating)

**Calculated voltages based on the new analysis have been reviewed and are considered acceptable based on the available margin.

MOV UNIDs Minimum Voltage Required in Mechanical Calculations

2-FCV-01-015 (T = SS)	414
2-FCV-01-016 (T = SS)	414
2-FCV-01-017 (T = SS)	414
2-FCV-01-018 (T = SS)	414
2-FCV-03-116A (T = SS)	376
2-FCV-03-116B (T = SS)	376
2-FCV-03-126A (T = SS)	373
2-FCV-03-126B (T = SS)	373
2-FCV-03-136A (T = SS)	375
2-FCV-03-136B (T = SS)	374
2-FCV-03-179A (T = SS)	376
2-FCV-03-179B (T = SS)	376

PREPARER:

N.R. Bezwada

N.R. Bezwada
04-10-14

CHECKER:

Greg Lee

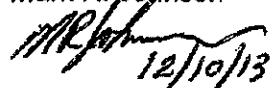
Greg Lee
4/10/14

MOV UNIDs Minimum Voltage Required in Mechanical Calculations

2-FCV-62-061	366
2-FCV-62-063	345
2-FCV-62-090 (T = 0 secs)	322
2-FCV-62-090 (T = 5 secs)	414
2-FCV-62-091 (T = 0 secs)	322
2-FCV-62-091 (T = 5 secs)	414
2-FCV-62-138	391
2-LCV-62-132	354
2-LCV-62-133	360
2-LCV-62-135	372
2-LCV-62-136	355

PREPARER:

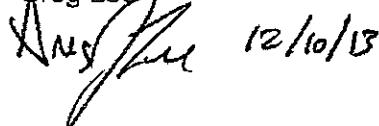
Mark R. Johnson



12/10/13

CHECKER:

Greg Lee

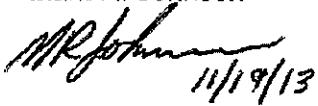


12/10/13

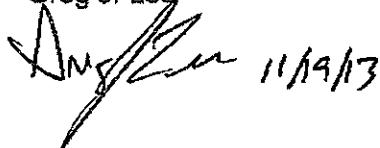
MOV UNIDs Minimum Voltage Required in Mechanical Calculations

2-FCV-63-1	413
2-FCV-63-3	386
2-FCV-63-4	379
2-FCV-63-5	367
2-FCV-63-6	360
2-FCV-63-7	361
2-FCV-63-8	392
2-FCV-63-11	390
2-FCV-63-22	383
2-FCV-63-47	351
2-FCV-63-48	371
2-FCV-63-67	401
2-FCV-63-72	413
2-FCV-63-73	407
2-FCV-63-80	406
2-FCV-63-93	411
2-FCV-63-94	411
2-FCV-63-98	394
2-FCV-63-118	401
2-FCV-63-152	389
2-FCV-63-153	390
2-FCV-63-156	377
2-FCV-63-157	371
2-FCV-63-172	359
2-FCV-63-175	381
2-FCV-63-25	414 (Test Condition)
2-FCV-63-26	414 (Test Condition)
2-FCV-63-25	372 (Accident Condition)
2-FCV-63-26	365 (Accident Condition)

PREPARER:
Mark R. Johnson


11/19/13

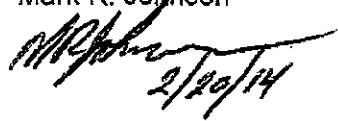
CHECKER:
Greg J. Lee


11/19/13

MOV UNIDs Minimum Voltage Required in Mechanical Calculations

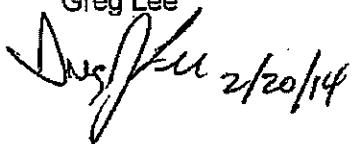
2-FCV-72-021 (T = 5 secs)	385
2-FCV-72-022 (T = 5 secs)	392
2-FCV-72-040 (T = 5 secs)	389
2-FCV-72-041 (T = 5 secs)	401
2-FCV-72-044 (T = 5 secs)	368
2-FCV-72-045 (T = 5 secs)	384
2-FCV-74-033 (T = 5 secs)	373
2-FCV-74-035 (T = 5 secs)	351

PREPARER:
Mark R. Johnson



2/20/14

CHECKER:
Greg Lee



2/20/14

WBN-VTD-R165-0140

AVING TRANSMITTAL

DATE FORMED

1/17/77

DATE

RECOMMENDED BY THE PROJECT TEAM.

NUCLEAR

ITEM NO.	TESTINERG E&G NO.	OPTIONAL SERVICES NO.	TESTINERG E&G NO.
10000	SY 417/3 06	10000	11770 12 14

TO/CC:

GOULDS PUMPS INC
NUCLEAR DIVISION, ROUTE
SENECA FALLS, N.Y. 13148

TELETYPE ADDRESS

THIS ARE:

FOR APPROVAL

Drawings are in compliance with your specified requirements. Drawings "Approved" or "Approved with Modifications" authorize Westinghouse proceed with manufacture. Modifications not in the contract or modifications made during or after drawing approval may result in a price change and/or shipment delay. To include shipping schedule, approved drawings must be received by Westinghouse no later than _____.

FOR CONSTRUCTION
OR INSTALLATION

FOR REPAIRS

The equipment shown on these drawing(s) has been released for manufacture, any modification may result in a price change and shipment delay.

ITEM: 1 SOG 77C12671

MARK: N229729

WBN REV 0
WBN PAGE 2

DESCRIPTION

KW:	100	FLN:	115	AMBIENT:	40 C
SPDN:	1770	ENCL:	DP	MOUNTING:	HORIZ.
FRAME:	414TS	TYPE:	LLT	CLSTY ECT:	FRONT-HOME REAR-STR. 100%
MODEL:	TBDP	HEAT DESIGN:	B	BUTY:	CONTINUOUS
VOLTAGE:	460	INSUL:	B	SPACE HEATERS:	none
PHASE:	3	SESV. FACTOR:	1.15	TERMAL PROV:	T.S.
HERTZ:	60	ASSTY:	F1		

ADDITIONAL FEATURES:

BEST AVAILABLE COPY

OUT DRAWING: 584D760 *Rev F*
+ I.L. 2930-11TD

EXCEPT- SCREENS & S.S. COND. SOG

1 DEPRO & 6 COPIES

MRS. FRAN CONLEY
GOULDS PUMPS, INC./SENECA FLS., NY, USA

1 COPY

SYRACUSE D.O. - ADIN BURROW

CARL CAROTHERS/ROUTE 1400,

CLEVELAND OHIO

1

THE REPORT CONTAINING THE ABOVE INFORMATION
MAY NOT BE COPIED OR REPRODUCED
Without Prior Written Consent Of The Project Team

WBN-VTD-R165-0140

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Westinghouse Electric Corporation

BUFFALO, N.Y.

Date 11/5/74

Purchaser GOULDS PUMPS D04883

Stock Order No. 73C74082

G.O. No. SY-44883 H.P. 100 Volts 230/460 Phase 3 Class B Insulation

Apparatus FR.404TS, TBDP, SQ. CAGE IND. MTR. Poles 4 R.P.M. 1770 Cycles 60

	1	2	3	COMMENTS
Amperes Per Terminal at no load	460	Volts	27.13	
Watts Input at no load			1694	
Stator Res. (T-T) at 75° C - ohms			.1323	
Starting Winding Res. at 75° C - ohms				
Rotor Res. (bet rings) at 75° C - ohms				

LOSSES IN WATTS AT FULL LOAD

Stray Load Loss	1012		
Stator I ² R Loss	2795		
Rotor I ² R Loss	1180		
Care Loss	1080		
Friction and Windage Loss	440		
% Efficiency - Full Load	92		
- $\frac{1}{4}$ Load	93.1		
- $\frac{1}{2}$ Load	93.2		
 % Power Factor Full Load	89.4		
- $\frac{1}{4}$ Load	88.7		
- $\frac{1}{2}$ Load	83.9		

n.r.M at Full Load	1772		
Amperes Per Term. at full load	113.82		
KW input at full load	81.11		
Amperes per Term.-Rotor locked	460 V	1546.7	
KW input - Rotor locked		215	
Max. Sec. Volts between rings	-		ON
Sec. Amps per ring at full load	-		
Full Load Torque (F.L.T.) in lb. ft.	296.2		
Max. Torque in % of F.L.T.	215.7		
Starting Torque in % of F.L.T.	168.6		
End Play Tested	OK		
Balance Tested	OK		
Stator Ins Tested	2100 V 60 Sec.	OK	
Rotor Ins Tested	V Sec.	-	

TEMPERATURE TESTS

Length of Test in hours	7.5	
Volts	1460	
% Normal Full Load Amp.	100	
Temp. Rise in degrees C	Stator Copper by Res.	78
	Stator Iron	48
	Rotor Copper	
	Rotor Iron	
Room temperature in °C	25	
Curve Nos.		

The above is a true and correct record of data obtained from tests made at the works of Westinghouse Electric Corporation.

3

REPORT OF TESTS ON INDUCTION MOTORS
 FORM 2956K

Signed *P. M. Sendibek* Engineer
 P. M. Sendibek

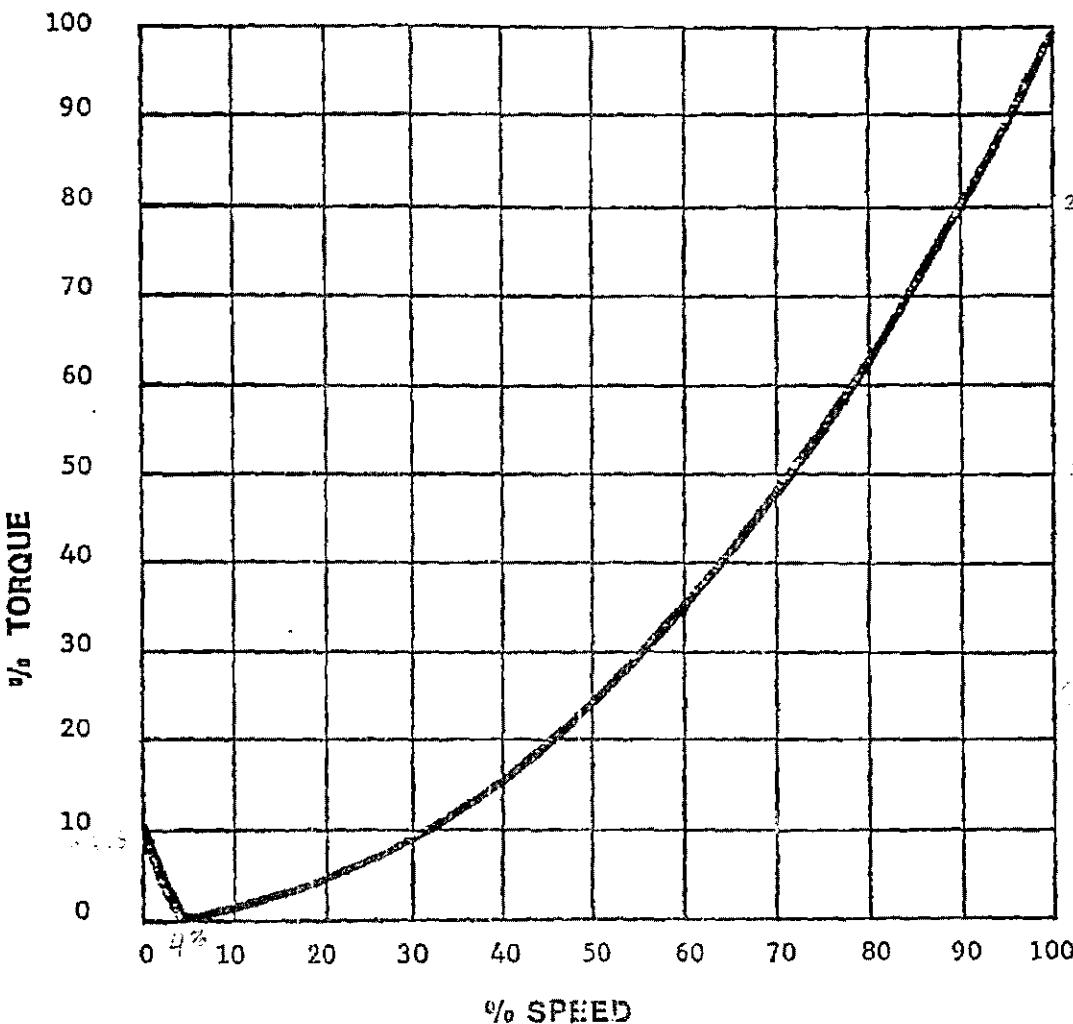
L. 16/01/77
N229739

SPEED - TORQUE CURVE

AT RATED ω of 1750 RPM @ 100% SPEED
100% TORQUE = 288.8 FT. LBS.

E-2126

100% SPEED = 1750 R. P. M.



PUMP MODEL - 3405

PUMP SIZE - 8X10-12.2V

IMPELLER DWG. # - 80-45

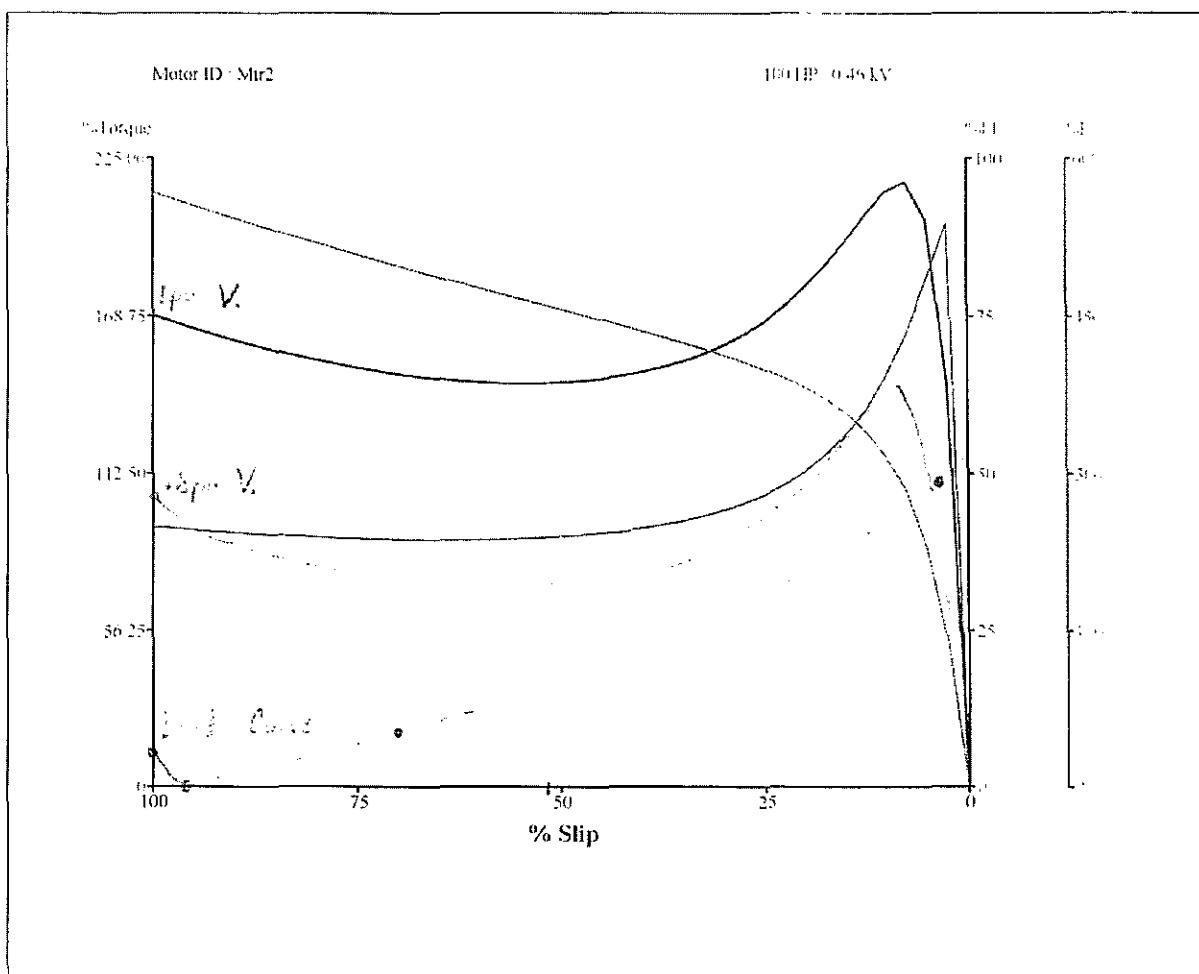
IMPELLER PATT. # - 52895

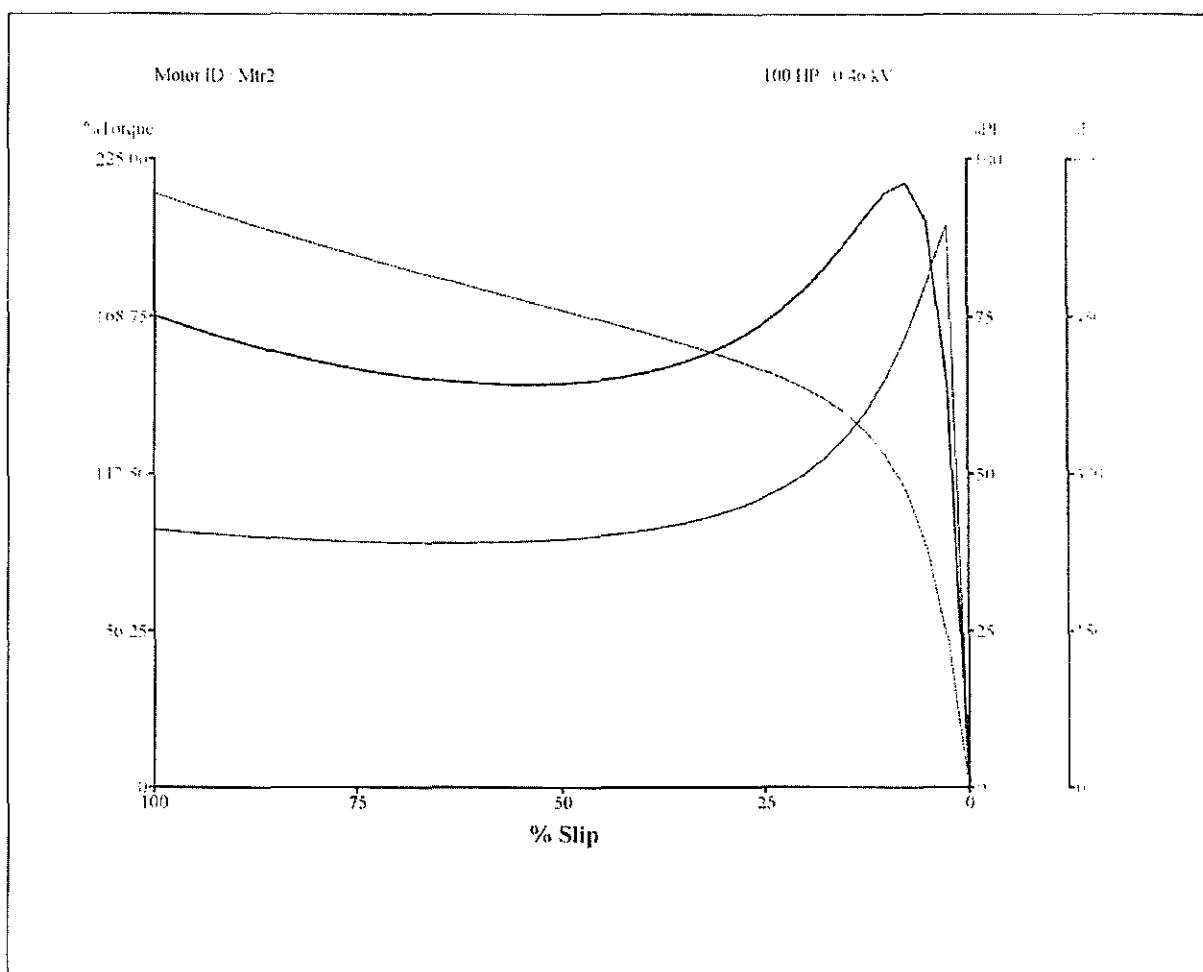
IMPELLER DIAMETER - 12"

$$100\% \text{ TORQUE} = \frac{\text{H. P.} \times 5250}{\text{R. P. M.}}$$

- Notes: A. H. P. is the shut-off H. P. at 100% speed with the rated impeller diameter.
B. Sleeve Bearing starting point is 15% not 10%.

PUMP WR² = 8.15 LB-FT² WBN REV 0
 WBN PAGE 8





CONTAINMENT AIR RETURN FAN 1A-A
I-MTR-030-0038-A

WBN-VTD-R165-0110

RELIANCE ELECTRIC COMPANY



24701 Euclid Avenue, Cleveland, Ohio 44117

Calc. STUDY-EEB-WBN-12-001
Attachment 6
Page 6 of 12

REPORT OF ROUTINE TESTS

Induction Motor

Purchaser Joy Manufacturing Co.
338 South Broadway
New Philadelphia, Ohio 44663

Date of Test

Manufacturer's
Order No. 1XF-882396

Purchaser's
Order No. NA2836

The air gap, condition of bearings and rotor balance were examined and found to be satisfactory.

Engineer P. Licuna Jr.
P. LICHUNA JR.

WBN REV 2
WBN PAGE 16

NAMEPLATE DATA

Hp	Service Factor	Rpm	Phase	Hertz	Volts	Amperes
100	1.0	1786	3	60	460	115

Type	Frame	Temp Rise by Method Indicated	Ambient Temp and Insulation Class	Time Rating	Design Letter	Code Letter for Locked Kva/Hp
P	444TCZ	-	50°C/H *	Cont.	-	J

TEST CHARACTERISTICS

Notes: * Type RN insulation. @ For 60 seconds.

Data on test from these motors.
(this or duplicate)

Approved by B. S. Bhandarkar, Date D.J.G.
(Engineer)

Issued: 8-12-77

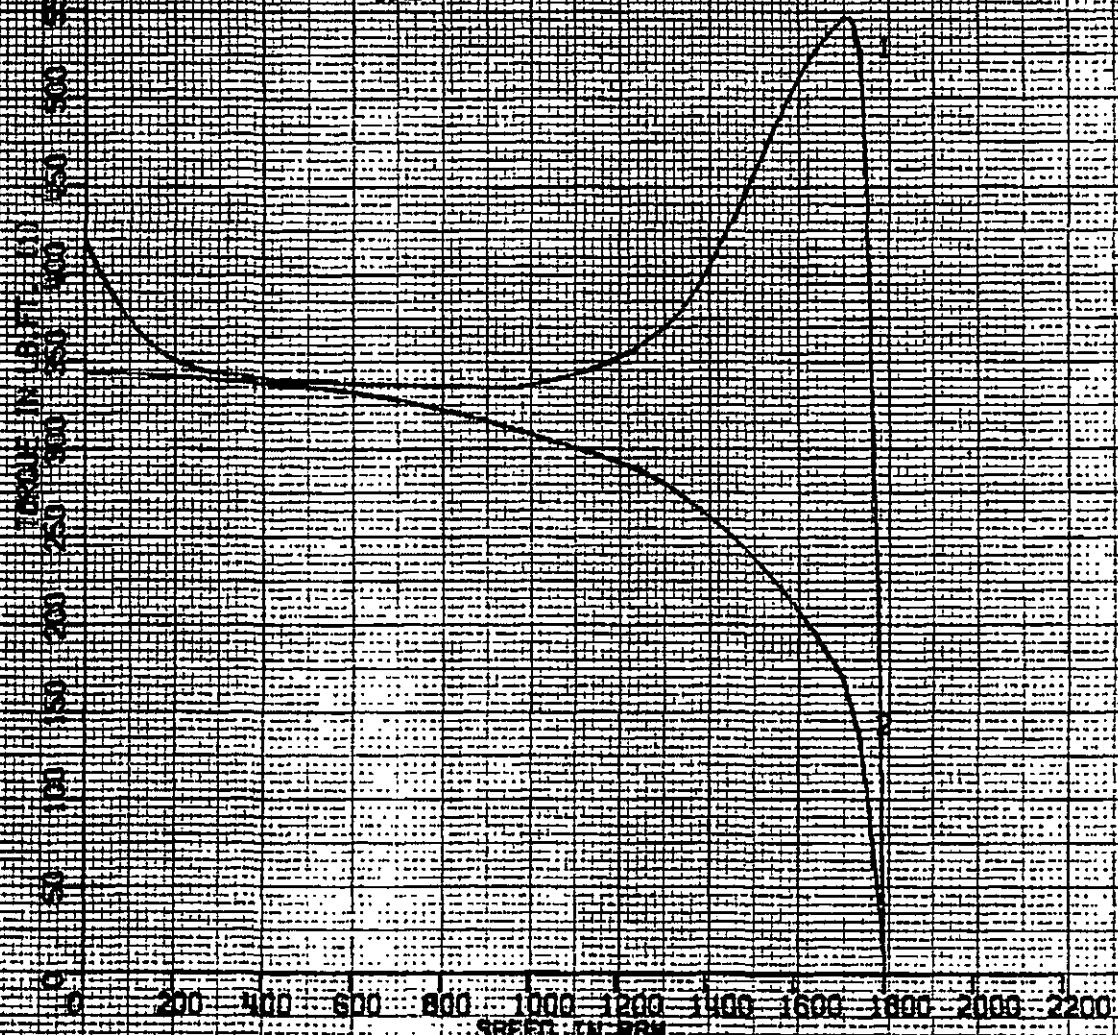
P. Licurs, Jr.

REL. S.O.	1XF-882396	RPM	1786	S.F.	1.0	ROTOR	604882-1RJ
FRAME	444TCZ	VOLTS	460	NEMA DESIGN	-	TEST S.O.	1XF-882396
HP	100	AMPS	115	CODE LETTER	J	TEST DATE	7-6-77
TYPE	P	DUTY	Cont.	ENCLOSURE	TEAO	STATOR RES. @ 25°C	.06439
PHASE/HERTZ	3/60	AMB°C/INSUL	50/H *	E/S	597617	OHMS (BETWEEN LINES)	

SPEED VS TORQUE AND CURRENT AT 460 VOLTS

WBN REV

WBN PAGE



DR. BY E.D.
CK. BY 227
APP. BY 227
DATE 8-22-77

A-C MOTOR
PERFORMANCE
CURVES

V29593.000

ISSUE DATE 8-22-77

AMPERES SHOWN FOR 460 Volt CONNECTION. IF OTHER VOLTAGE CONNECTIONS ARE AVAILABLE, THE AMPERES WILL VARY INVERSELY WITH THE RATED VOLTAGE. * Type RN insulation.

RE 1652V82 1 Ad In U.S.A.
RELIANCE 
ELECTRIC COMPANY
CLEVELAND, OHIO 44117 U.S.A.

6YF882998

CONTRACT #81K5-829093, CHG. #1
FOR: WATTS BAR NUCLEAR PLANT
HVAC EQUIPMENT
TRAVELING WATER SCREENS

(6)

ERCU TRAV. SCREEN 1B-B

1-MTR-067-0445-B

SPECIAL DATA SHEET

Calc. STUDY-EEB-WBN-12-001
Attachment 6
Page 8 of 12

- a. Manufacturer RELIANCE ELECTRIC COMPANY
- b. Application TRAVELING WATER SCREENS
- c. Rated horsepower 5
- d. Service factor 1.15
- e. Rated voltage 460
- f. Full load current per phase at the applicable rated voltage
6.8 AMPERES
- g. Locked rotor current at the applicable rated voltage
41.1 AMPERES AFC GPM
- h. Locked rotor power factor at rated voltage 61.2%
- * i. Full load current per phase at 80% of motor rated voltage
8.8 AMPERES
- J. Locked rotor current at 80% of motor rated voltage
30.6 AMPERES
- k. Locked rotor withstand time at rated voltage starting from ambient temperature
(3-ph motors only) 20 SECONDS
- l. Locked rotor withstand time at rated voltage starting from rated temperature
(3-ph motors only) 8 SECONDS
- m. Efficiency at 100%, 75% and 50% of rated horsepower
82.3%, 82.9%, 82.5%
- n. Power factor at 100%, 75% and 50% rated horsepower
83.9%, 79.8%, 70.6%
- * MOTOR NOT SUITABLE FOR CONTINUOUS OPERATION AT 80% VOLTAGE.

WATTS BAR
81-829093
6YF882998
N/P 1/2



ELLIS AND WATTS
CINCINNATI, OHIO 45244

DOCUMENT NO. N0055-4 REVISION 0 4/28/86

ISSUE NO. _____

TITLE: NUCLEAR ENVIRONMENTAL QUALIFICATION REPORT FOR
50 HP - 1800 RPM MOTOR

PART NO. _____

PART NAME _____

PREPARED BY: Karl F. Vank 4/28/86
K.Z. Vank

ENGINEERING APPROVAL: M. J. Fox 4/28/86
M.J. Fox

Q.A. APPROVAL: Roger R. Schertler 4/28/86
R. R. Schertler

DATE

Tennessee Valley Authority
Watts Bar Generating Station
Contract No. 85PM8-451609

DOCUMENT NO. N0055-4

PAGE 1

REPORT OF TEST-INDUCTION MOTOR

PURCHASER ELLIS & WATTS

DATE OF TEST) 01-15-86

MANUFACTURERS
ORDER NO. 6-150206PURCHASERS
ORDER NO. 76013

RATING

TYPE	FRAME	RATED H.P.	FULL LOAD R.P.M.	VOLTS	PH	HZ.	FULL LOAD AMPERES	SERVICE FACTOR	TIME RATING
COG6B	326T	50	1770	480	3	60	56.5	1.15	CONT.

CONDITIONS OF TEST

TEMPERATURE RISE-DEG. C

HOURS RUN	LINE VOLTS	LINE AMPERES	COOLING AIR DEG. C	STATOR		ROTOR		COLLECTOR RINGS
				CORE BY THERMO- COUPLE METHOD	WINDINGS (CROSS OUT THREE) BY RESISTANCE METHOD BY EMBEDDED DETECTOR BY THERMOCOUPLE METHOD BY THERMOMETER METHOD	CORE BY THERMO- METER METHOD	WINDINGS (CROSS OUT ONE) BY RESISTANCE METHOD BY THERMO- METER METHOD	
3.5	483	65.7	21	68	108.8	-----	-----	-----

CHARACTERISTICS

SLIP-PERCENT	AMPERES RUNNING LIGHT	RESISTANCE IN OHMS AT 25°C (BETWEEN LINES)		SECONDARY VOLTS AT STANDSTILL	SECONDARY AMPERES PER RING AT FULL LOAD
		STATOR BETWEEN TERMINALS	ROTOR BETWEEN RINGS		
1.53	17.4	.159	-----	-----	-----

TORQUE AND STARTING CURRENT

HIGH-POTENTIAL TESTS

BREAK-DOWN TORQUE LBS. AT 1 FT. RADIUS	LOCKED ROTOR TORQUE LBS. AT 1 FT. RADIUS WITH-% VOLTS APPLIED	STARTING CURRENT AMPERES (LOCKED ROTOR) WITH-% VOLTS APPLIED	VOLTS A-C FOR 1 SEC.
			STATOR
341.0 LB-FT	218-99.2%	334.7-99.2%	2400

EFFICIENCIES AND POWER FACTOR

EFFICIENCY, PERCENT			POWER FACTOR, PERCENT		
FULL LOAD	3/4 LOAD	1/2 LOAD	FULL LOAD	3/4 LOAD	1/2 LOAD
93.1	93.9	94.0	83.4	81.8	75.8

NOTES: DATA FROM TEST ON THIS MOTOR. IN ACCORDANCE WITH IEEE 112-1984
(THIS OR DUPLICATE) FORM A-2.

THIS DATA FOR REFERENCE ONLY UNLESS OTHERWISE SPECIFIED

PREPARED BY C L MATTHEWS

APPROVED BY

DATE 04-02-86



B32E04-050-731-C0

SHEET 1 OF 1

1

WINNING: 312-325

FOR INFORMATION ONLY

SCAFFOLDING II

三

Digitized by srujanika@gmail.com

1-11-71 W/B

H 3164 2/82

Calc. STUDY-EEB-WBN-12-001
Attachment 6
Page 12 of 12

DATE OF TEST 01-16-86

MANUFACTURERS
ORDER NO. 6-150206

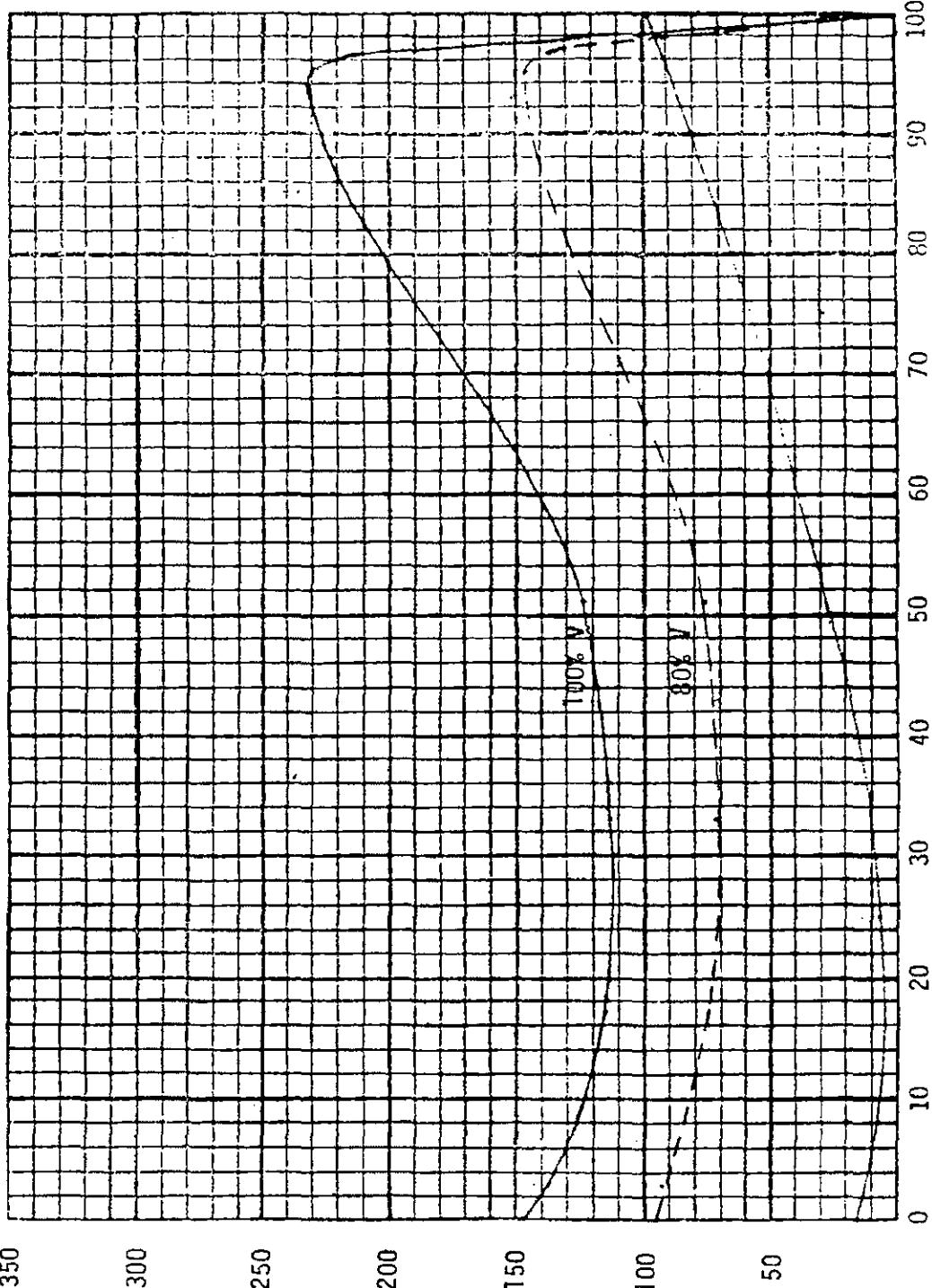
PURCHASERS
ORDER NO. 76013

SPINDLE-TORQUE & CURRENT CURVE

PURCHASER ELLIS & WATTS

AMPERES IN % FULL-LOAD

VOLTAGE	480	FRAME	326T	IP	50	F.I. RPM	1770
F.L. AMPS	55.5	PHASE/HERTZ	3/60	AMBIENT	40	SERVICE FACTOR	1.15
INSULATION CLASS	H	DUTY	CONT.	F.L. TORQUE	148.4	LBS. FT.	
				ENCLOSURE	0.D.P.	MOUNTING	F-1



THIS DATA FOR REFERENCE ONLY UNLESS OTHERWISE SPECIFIED

PREPARED BY C. L. MATTHEWS

APPROVED BY

DATE 04-02-86

Louisiana

B32E04-050-731-S0

SHEET 1 OF

5.2. Second Level Undervoltage (Degraded Voltage) Relay Reset Setpoint

An upper boundary should also be established for the reset setting of the degraded voltage relay. The tightest possible tolerance should be employed between the nominal dropout and reset setpoints. The upper boundary of the reset setting should be equal to the nominal setpoint plus all tolerances from any errors in accordance with Technical Instruction TI-28 (Ref. 2.13). Margin should exist between the upper boundary of the reset setting and the safety bus voltage equivalent to having the minimum allowable switchyard voltage during anticipated worst-case system operating conditions. If operation of the auxiliary power system under normal design transient (starting) conditions, with the safety-related bus voltage equivalent to having the minimum allowable switchyard voltage determines that the bus voltage drops below the dropout setting, then it must recover above the upper boundary of the reset setting prior to the lower boundary of the time delay selected in section 5.4.

The safety bus voltages associated with the upper boundary of the reset setting are evaluated to ensure adequate operation of the auxiliary power system under steady-state (starting) conditions and recovery (running) voltage conditions. The acceptance criteria and means of evaluation is as follows:

- 5.2.1. Induction motor starting analyses were performed at 6672V which bounds the operational limit of the degraded voltage relay reset setting upper boundary, 6681V (Section 3.9) to ensure that motors and motor-operated valves (MOVs) have adequate starting voltage as specified in section 3.8. Using 6672V provides conservative results for motor starting. R31
- 5.2.2. All static loads are evaluated to ensure adequate operating voltages as specified in section 3.7. R31

5.3. Second Level Undervoltage (Degraded Voltage) - Long Time Delay

The long time delay specified in NRC Branch Technical Position PSB-1 is not used at WBN.

5.4. Second Level Undervoltage (Degraded Voltage) - Short Time Delay

5.4.1. The upper boundary of the time delay selected should be less than the safety analysis time allowed for the emergency diesel generators to come up to rated speed and voltage and be ready to accept load. The lower boundary of the time delay should be greater than the time it takes the safety bus voltage to recover above the upper boundary of the degraded voltage relay reset setting established in Section 5.2. The nominal setpoint should be selected considering all errors in accordance with Technical Instruction TI-28 (reference 2.13).

5.4.2. The scenario evaluated for the short time delay is an SI concurrent with the degraded voltage condition such that a block start attempt is made. A determination is made of the time permitted to allow voltage to return above the degraded voltage relay setpoint reset limit under block start transient conditions

and still assure a subsequent start on the diesel if the voltage fails to recover, thus, making this a start-start evaluation.

- 5.4.3. To evaluate the effect of the starting currents during the start-start scenario, the effect on overcurrent protective devices are considered. The board voltages at the onset of the event are, considered normal and are taken from Reference 2.2. The degraded voltage condition presumes that the voltage does not recover but remains below the degraded voltage relay setpoint subjecting the SI initiated motors to starting currents for the time delay selected and then sequence onto the emergency diesel generators. The design calculated worst-case transient voltage dip during the accident loading sequence (from reference 2.2) is used. This is conservative, because a lower voltage would produce less starting current for the motors.
- 5.4.4. Loads evaluated for this condition are safety-related loads required for Unit 1 which would be actuated for an SI. Load types considered are motor loads, vendor package loads, 120VAC motor control circuits, and MCC 120VAC distribution panel loads. The acceptance criteria and means of evaluation is as follows:
 - 5.4.4.1. Motor loads are evaluated to determine the effect of the start-start heating of the overcurrent protective devices, such that starting on the diesel without tripping can be assured.
 - 5.4.4.1.1. 6.9kV Switchgear Breakers - Motors fed from 6.9kV shutdown boards do not require analysis for starting immediately after running at degraded voltage. Overcurrent relays derive their input from current transformers. When power is lost, the relays reset to their normal state.
 - 5.4.4.1.2. 480V Switchgear Breakers - Motors supplied from the 480V Shutdown Boards do not require analysis for starting immediately after running at degraded voltage. Ampmeter solid state overcurrent protective devices obtain their input from the current transformers. When the power is lost, the protective devices reset to their normal state.
 - 5.4.4.1.3. 480V MCC breakers feeding static loads - These loads are constant impedance loads and will have reduced current requirements at a degraded voltage, and therefore the reduced heating effect would not challenge their applicable protective devices.
 - 5.4.4.1.4. 480V MCC protective devices feeding MOV's - Thermal Overload Relays (TOL's) used in accident initiated MOV circuits have their trip function bypassed during an accident. The magnetic-only circuit breakers are set above the locked-rotor current of the MOV's and would not be affected by the operation of the MOV. Therefore the protective device heating effects during a degraded voltage for MOV's are not evaluated.
 - 5.4.4.1.5. 480V MCC protective devices feeding motor loads - Motor protective devices consist of a TOL in conjunction with a magnetic-only circuit breaker. The magnetic-only circuit

breakers are set above the locked-rotor current of the motor and would not be affected and therefore not analyzed.

The TOL's were evaluated as follows: The minimum terminal voltage of the enveloping safety-related MCC motor was determined from Reference 2.2. The minimum starting voltage at motor 203-12B is calculated as follows:

$$\begin{aligned} \%Vst @ 432 &= 83.77\% \text{ of } 480V \\ \%Vst @ 380 &= 83.77\% * \frac{380}{432} = 73.69\% \\ Vst &= \frac{73.69\%}{100} * 480 = 353.71V \end{aligned}$$

This is based on worst case voltage of 380V at t=0 for 480V C&A Vent Board 1A1-A with a grid voltage drop from 164kV to 153kV, concurrent with an SI accident.

For added margin, for conservatism 320 volts was used in this evaluation. Next, ETAP PowerStation was used to model a typical low voltage MCC motor in order to determine the total starting time during a degraded voltage event. The total starting time consists of an attempted start at a degraded voltage of 320 volts plus a re-start at rated 460 volts when applied to the diesel generator. The ETAP default dynamic model for a low voltage 50 HP motor was used as the typical WBN MCC motor. The 50 HP model has a higher power factor and efficiency than the smaller motor models. This produces a higher "%Start Load" for the connected mechanical load resulting in slower acceleration. In order to determine a conservatism value for the motor inertia constant "H", the motor acceleration simulation was performed several times at 80% rated voltage until it was found that an "H" value of 0.7 produced a 5 second acceleration time. The results of this simulation are given in output file **LV-H-7** (Attachment 1). Using this typical motor data, a simple three bus system was modeled which could be used to switch the motor from degraded voltage to rated voltage at a specified time (see Attachment 2).

Two cases were analyzed using this model. In the first case, the load was conservatively tripped from degraded voltage at 6 seconds and re-started at rated voltage at 10 seconds. This was conservative in that the load is given 4 seconds to slow down before it is re-energized at 10 seconds. In the second case, the load was tripped at 11.5 seconds and immediately re-started at rated voltage. The results of these cases are given in output files **LV-ACC-1** and **LV-ACC-2** (Attachment 2 and 3). Both acceleration cases show that a typical low voltage MCC motor will be fully accelerated in 12 seconds.

5.4.4.1.6. A generic review of MCC thermal overload (TOL) devices were evaluated to determine if they could trip during the 12 seconds of motor acceleration. The motor draws a reduced starting current during the degraded voltage period. For conservatism, the decay of starting current during motor acceleration has been ignored. For the ITE TOLs installed at WBN on safety-related loads, a starting current of 638% will trip the TOL in 12 seconds (see Reference 2.3). This is based on the TOL tripping in 12 seconds based on 555% of TOL 100% trip amps, which is a minimum of 115% of the motor current. The characteristic curve for size 0, 1 and 2 starters were conservatively used, since the current vs time for size 3 and 4 starters are significantly higher. Additionally, since the accident has just occurred, the equipment ambient temperatures are not elevated to 40°C, and there is an additional margin of 115% in the TOL trip time (see Reference 2.3). Therefore, at a reduced ambient temperature, the TOL would trip in 12 seconds for a starting current of 734%. Due to the reduced starting voltage available at the motors during the degraded condition, a voltage of 1% less than the minimum starting voltage of 85% will be conservatively used. This is based on reference 2.2 for the design calculated worst-case transient voltage dip during the accident loading sequence. This is conservative, because a lower voltage would produce less starting current for the motors. Therefore, this would be equivalent to a motor starting current of 851%. Therefore, the analysis will evaluate all TOL's for class 1E motors that start for an accident that have motor starting current greater than 850% of full load current.

- 5.4.4.1.7. Protective devices should also be evaluated for the 460V safety-related loads that operate during non-accident conditions. The evaluation should consider that the safety bus voltage is equivalent to operation at the lower boundary of the degraded voltage relay dropout. The protective devices should be evaluated to ensure that operation of the safety-related loads can be sustained indefinitely at this voltage without protective device trip.
- 5.4.4.2. SI actuated medium voltage motor loads are evaluated to ensure that their thermal damage limits are not exceeded during the start-start event.

This was determined not to be an issue. The medium voltage motors can start with 80 percent of motor rated voltage of 6600V (i.e. 76.5% of 6900V in ETAP). During the start-start scenario the voltage can not drop below 86% without actuating the loss-of-voltage relays, which will trip the offsite supply in no more than 1.14 seconds. Therefore the available voltages at the medium voltage motors will be adequate to ensure starting and accelerating of these loads and will not challenge the motor thermal limits during starting.

- 5.4.4.3. 120VAC control power transformer (CPT) fuse time characteristics are evaluated to determine if the fuse could blow when carrying rated inrush current of the starter and any other normally energized devices for the safety analysis time from 5.4.1 above. See reference 2.7.
- 5.4.4.4. MCC 120VAC distribution panel. Fuse time characteristics are evaluated to determine if the fuses melt during the start attempts. It is considered that circuit components required to pick-up during starting will be at inrush conditions.

5.5. Loss-of-Voltage (LOV) Relay Setpoint

The loss of voltage (LOV) relays are an integral part of the degraded voltage protection scheme, and their setting and time delay should be selected to limit the magnitude and duration of degraded voltage the safety buses will encounter. The LOV relay nominal setpoint and associated time delays should be selected considering all errors in accordance with Technical Instruction TI-28 (Ref. 2.13).

- 5.5.1. The LOV relay voltage setpoint upper boundary should be established to be less than, with some margin, the safety bus voltage equivalent to the design calculated worst-case transient voltage dip during the accident loading sequence. This setpoint should also be less than the TPS calculated security boundary voltage which is based on the grid voltage that is one failure away from failure (see reference 2.11).
- 5.5.2. The LOV relay voltage setpoint lower limit is selected by evaluating operation of the auxiliary power system under steady-state (running) conditions, with the 6.9-kV Shutdown Board voltage as low as possible while keeping all connected safety-related motor loads above their stall voltage (greater than 70.7 percent of rated motor voltage for NEMA Design "B" motors, see assumption 4.6). The lower limit must also be greater than the 6.9kV Shutdown Board voltage equivalent to having the lowest switchyard voltage that could be sustained without instability or collapse (see reference 2.11).
- 5.5.3. The lower boundary of the LOV voltage relay time delay should be long enough to ride through short-circuits and other short time system transients (lightning strikes, switching transients, etc.), taking into account the total sensing and clearing times for the above type of events. The time delay upper boundary should be less than the safety analysis time allowed for loss of voltage detection.

6. SUMMARY OF RESULTS

6.1. Degraded Voltage Relay Drop Out Setpoint

- 6.1.1. Table 1 in Section 9.0, shows the minimum calculated steady-state operating voltage for the boards when the 6.9kV Shutdown Boards are operating at the degraded voltage dropout lower boundary of 6555V. All 6.9kV switchgear and 480V switchgear voltages are equal to or greater than the ANSI C84.1 voltage range B service voltages of 6560V (5V difference is considered insignificant) and 440V, respectively. And 480V mucs are equal to or greater than the ANSI C84.1 voltage range B utilization voltages of 432V.

not need to be started during a time of voltage degradation. Therefore, the voltage is considered acceptable under those conditions.

Note 2 - Percent Required starting voltages were obtained from Att 10.7 of Ref 2.6 of Calculation WBN-EEB-EDQ1999-010001 (Ref 2.2).

6.3 Degraded Voltage Time Delays

6.3.1. Motor Protective Device Evaluation

Per section 5.4.4.1, the only issue requiring evaluation was TOL's protecting safety-related motors that start for an accident. The generic evaluation of TOL's, in section 5.4.4.1.6, showed that only motors having locked rotor current in excess of 850% would have to be evaluated further. A review of the WBN ETAP database, showed that the following motors in Table III have a locked rotor current greater than 850% and start for an accident:

Table III - Locked Rotor Current Summary

ID	Name	Percent
203-12B	Cont Bldg Emerg Press Fan A-A	882
203-2A	Cont Bldg Emerg Air CU Fan A-A	902
205-11A	Cont Bldg Emerg Press Fan B-B	882
205-2A	Cont Bldg Em Air Clnup Fan B-B	902

An evaluation of those four loads show that their TOL's are set at 115% (see reference 2.3). Therefore they would not be an issue, because it would increase their tolerance for tripping an additional 115%.

6.3.2. Fuse Evaluation for 120VAC CPT Circuits and MCC 120VAC Distribution Panel Loads

During the start-start scenario, MCC bus voltages are below the levels used in verifying adequate voltage in previous calculations. Control circuits for motors being started, or other loads being energized, may be at a sustained inrush for the duration of the start attempt (6 seconds) before going to the diesels. Consequently fuses for these circuits must be verified to not actuate for this condition.

Calculation WBNEEBMSTI020019 (Ref. 2.4) and its reference calculation WBPEVAR8909006, were reviewed to identify the typical circuit configurations, their worst case burden during inrush, and the fuse size and type presently required. The current for each circuit was calculated for the burden at rated voltage.

Calculation WBNEEBMSTI020020 (Ref. 2.5) was reviewed to identify the worst case inrush at rated voltage on each MCC 120VAC distribution panel. Each panel uses the same size and type fuse.

The inrush currents were then compared with the fuse melting time-current characteristic to determine the melt times. The results are tabulated in Tables 2, 3 and 4 in section 9.0. Use of inrush currents calculated at rated voltage is conservative for constant impedance devices as the current at degraded voltages will be less. The acceptance pass-fail criteria required for melting time is 12 seconds. From a review of Tables 2, 3, and 4 all fuses will carry inrush current for at least 12 seconds and are considered acceptable.

6.3.3. Non-Accident Degraded Voltage - Motor Protective Device Evaluation

Operation of safety-related loads with the 6.9kV Shutdown Board voltage operating at the lower boundary of the degraded voltage relay, 6555V, will not cause tripping of protective devices. Static loads are not considered, since operation at lower voltage results in less current. The evaluation was based on the following:

R31

6.6kV Motors - The voltage at the boards is 6555V (95% of nominal). The increased motor current would be approximately 105% of nominal. All of the protective relays are set to alarm only for overloads above 125% of nominal. Therefore, operation at the lower boundary of the degraded voltage relay dropout setting would not trip the motors.

R31

480V switchgear motors - The lowest voltage at the 480V Shutdown Boards would be 437 volts (Ref Table 1). The increased motor current would be approximately 110% of normal. All of the switchgear breakers are set above 115% of nominal, and most above 125% of nominal. Therefore, operation at the lower boundary of the degraded voltage relay dropout setting would not trip the motors.

R31

480V mcc motors - The lowest voltage at the 480V mucs would be 432 volts (Ref Table 1). The increased motor current would be approximately 110% of normal. All of the TOLs are set above 115% of nominal, and most above 125% of nominal. All motor breakers are magnetic only, and are not an issue. Therefore, operation at the lower boundary of the degraded voltage relay dropout setting would not trip the motors.

R31

6.3.4. The upper limit for the time delay is 11.5 seconds, which is the maximum total time allowed for loss of voltage detection and emergency diesel generator start in the WBN safety analysis as documented in the FSAR. Based on the above evaluations, it has been determined that protective devices will not trip prior to 12 seconds for operation at a degraded voltage for a period of time, disconnection from offsite power, and reconnection to the emergency diesel generators.

The bounding motor starting analysis from reference 2.2, assumes the plant being in a normal operating mode, with the grid at its expected grid schedule voltage of 165kV, followed by an accident concurrent with the grid falling to a voltage of 153kV. For this unlikely conservative drop in the grid, the degraded voltage relays can be reset in approximately 6 seconds. For conservatism and margin, the lower limit for the time delay is 8.5 seconds.

6.5 Loss of Voltage (LOV) Relay Setpoint and Time Delay

6.5.1. The LOV relay upper analytical limits were determined to be 6072 volts, which is the minimum voltage dip during any expected starting transient from reference 2.2 and 6560 volts which is the lowest 6.9kV Shutdown Board voltage when the grid is degraded down to the security boundary voltage of 141kV. See section 5.5.1. The upper boundary of the LOV relay is 6072 volts from reference 2.20. The current LOV setpoint meets the criteria in section 5.5.1. Table IV shows the 6.9kV Shutdown Board voltages when the grid is degraded down to the security boundary voltage of 141kV.

R32

R32

Calculation: WBN-EEB-MS-TI06-0029, R33

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1.0 PURPOSE

The purpose of this appendix is as follows:

- Evaluate impact of the degraded voltage on the protective devices of safety related components and devices. This includes loads fed from 6.9kV and 480V switchgear, 480V MCCs, 120V CPT circuits and MCC 120VAC distribution panels. The equipment powered from Unit 2 boards required to support Unit 1 has been already analyzed in the main body of this calculation and therefore, not reviewed in this appendix.
- Ensure the duration of the degraded voltage at a given voltage level does not result in thermal degradation or damage of any required equipment.
- Verify that the existing setting of degraded voltage and loss of voltage relays, as stated in the main body, are acceptable for Unit 2

Analysis to verify adequacy of start and running voltages under degraded voltage conditions and stall voltage analysis is performed in calculation EDQ00099920070002 (Ref. 2.1).

2.0 SOURCES OF DESIGN INPUT/REFERENCES

References listed in Section 2.0 of the main body of this calculation, except references 2.2, 2.3, and 2.4, are also applicable to this appendix. Additional references are as follows:

- 2.1 Calculation EDQ000-999-2007-0002, R18 - Auxiliary Power System Analysis
- 2.2 Calculation EDQ002-999-2008-0004, R12 - 480V Class 1E Protection, Coordination and TOL Heater Calculation – Unit 2
- 2.3 Calculation EDQ002-999-2008-0003, R4 - 120VAC Class 1E MCC Control Circuit Voltage Analysis and Transformer Sizing
- 2.4 Calculation EDQ002-999-2008-0016, R2 – 6.9kV Protection and Coordination Calculation – Unit 2
- 2.5 Calculation WBNEEBMSTI070018, R80 – 120VAC Protection, Coordination and Short Circuit Study

3.0 Design Input and Requirements

- 3.1 Thermal overload heaters data is obtained from Appendix 8 of Reference 2.2.
- 3.2 MCC control circuit loads data is taken from Ref. 2.3.
- 3.3 Degraded Voltage and Loss of Voltage relays Setpoint (Sec 3.9 and Figure 8.3 of the main body)

Degraded Voltage Relay (27DAT, 27DBT, 27DCT)

Setpoint (Nominal) 6600V

Allowable Value: Dropout – 6570V Pickup – 6672V

Calculation: WBN-EEB-MS-TI06-0029, R33

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Analytical Limit: Dropout – 6555V Pickup – 6681V

Loss of Voltage Relay (27LVA, 27LVB, 27LVC)

Setpoint (Nominal) 6000V

Allowable Value: Dropout – 5967.6V Pickup – 6036V

Analytical Limit: Dropout – 5934V Pickup – 6072V

4.0 DOCUMENTATION OF ASSUMPTIONS AND JUSTIFICATION

Assumptions and justification listed in Sections 4.1 through 4.5 in the main body of this calculation are also applicable to this appendix. These are repeated below:

- 4.1 The resistive loads do not require protective device analysis for degraded voltage.

Justification: For a degraded voltage condition, the current for constant impedance devices decreases. Decreased current reduces the cumulative heating effect on thermal overloads, fuses or circuit breakers.

- 4.2 Motor operated valves do not require protective device analysis for degraded voltage.

Justification: The operation of the valve motors is intermittent and their overload relays are bypassed during accident conditions. Therefore the heating effect has no impact on this analysis.

- 4.3 Motors supplied from the 480V Shutdown Boards do not require protective device analysis for starting immediately after running at degraded voltage.

Justification: Amptector solid state overcurrent protective devices obtain their input from the current transformers. When the power is lost, the protective devices reset to their normal state.

- 4.4 Motors fed from 6.9kV shutdown boards do not require protective device analysis for starting immediately after running at degraded voltage.

Justification: Overcurrent relays derive their input from current transformers. When power is lost, the relays reset to their normal state.

- 4.5 A five second acceleration time is assumed for motors with no acceleration time.

Justification: IEEE-384-1977 (Ref. 2.18 of the main body), provides a typical motor acceleration time range from 2.5 to 4 seconds. Using 5 seconds is conservative.

5.0 COMPUTATIONS AND ANALYSIS

- 5.1 Degraded Voltage and Loss of Voltage Relays Settings

Degraded Voltage and Loss of Voltage relay setpoints are determined in the main body of this calculation and the currently installed settings are documented in Section 3.3 & Figure 8.3. These setting are reviewed to verify their acceptability for Unit 2 as follow:

- 5.1.1 Degraded Voltage relay

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From the auxiliary power system voltage analysis performed in Ref. 2.1, it is seen that under the worst case scenario of an accident with grid dropping from normal 164kV to the minimum of 153kV, the voltage on the 6.9kV shutdown boards will fall below the relay dropout level at t=0+ second but recovers to a level above the relay reset value in ≤ 5 seconds (Att. 11.3.b of Ref. 2.1). The minimum time to reset the degraded voltage relay so as not to isolate the shutdown boards from the offsite power is 8.5 second (Figure 8.3).

Also as per the analysis performed in Ref. 2.1, it is verified that all safety related equipment and devices will have adequate starting and running voltage under the degraded voltage reset and dropout conditions respectively, after the proposed modifications in Section 12.0 of Ref. 2.1 are implemented.

5.1.2 Loss of Voltage relay

From the auxiliary power system voltage analysis performed in Ref. 2.1, it is seen that under the worst case scenario of an accident with grid dropping from normal 164kV to the minimum of 153kV, the worst case voltage on the 6.9kV shutdown boards at t=0+ second is 88.85% of nominal voltage (Att. 11.3.b of Ref. 2.1) which is above the loss of voltage relay nominal setting of 87% (Figure 8.3).

Based on the above, the degraded voltage and loss of voltage relays existing settings, listed in Section 3.3, are acceptable for Unit 2.

5.2 Effect of the starting currents during the Start-Start scenario on the overcurrent protective devices

5.2.1 The effect of starting currents during Start-Start scenario on overcurrent protective devices for safety related loads required for Unit 1 which would be actuated for an SI are evaluated in Sections 5.4.3 and 5.4.4 in the main body of this calculation. Load types considered are motor loads, Static loads, 120VAC motor control circuits, and MCC 120VAC distribution panel loads. The evaluation performed in Sections 5.4.3 and 5.4.4 in the main body of this calculation is typical and, therefore, also applicable for Unit 2 loads except for the TOLs since the TOLs for Unit 2 loads have been replaced with new TOLs model AR supplied by Square D (Appendix 8 of Ref. 2.2). Unit 2 TOL evaluation is performed in Section 5.2.2 below.

5.2.2 Based on a worst case analysis performed for a 50 HP motor in Section 5.4.4.1.5 in the main body of this calculation, it was determined that a typical low voltage MCC motor will fully accelerate in 12 seconds during start-start scenario. This analysis is also applicable for Unit 2 based on similarity of U1 and U2 equipment.

A generic review of U2 MCC TOL devices (Square D type AR) is performed to determine if they could trip during the 12 seconds of motor acceleration. The motor draws a reduced starting current during the degraded voltage period. Since the motor starting analysis is performed with the worst case voltage dip of 320V at the bus, the reduced starting current is 70% (320/460) of the rated locked rotor current. For the replacement Square D type AR TOLs installed at WBN Unit 2 on safety-related loads, a starting current of 525% will trip the TOL in 12 seconds

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(see TOL Time-Current characteristics in Appendix 8 of Reference 2.2). The characteristic curve for size 0, 1 starters was conservatively used, since the current vs time for size 2, 3 and 4 starters are higher. Additionally, since the accident has just occurred, the equipment ambient temperatures are not elevated to 40°C, and there is an additional margin of 115% in the TOL trip time (see Reference 2.2). Therefore, at a reduced ambient temperature, the TOL would trip in 12 seconds for a starting current of 604% (525x1.15). The maximum motor starting current that would yield 604% at degraded voltage is 863% (604/0.7). Therefore, the analysis evaluates all TOL's for class 1E motors that start for an accident that have motor starting current greater than 850% of full load current.

- 5.2.3 Protective devices are also evaluated for the 6.6kV and 460V safety-related motors that operate during non-accident conditions. The evaluation considers that the safety bus voltage is equivalent to operation at the lower boundary of the degraded voltage relay dropout. The protective devices are evaluated to ensure that operation of the safety-related loads can be sustained indefinitely at this voltage without protective device trip.

6.6kV Motors - The lowest voltage at the boards is 6555V (95% of nominal 6900V). The increased motor current would be approximately 105% of nominal. All of the protective relays are set 115% nominal and most at 125% of nominal motor current (Ref. 2.4). The protective relay (51) is set to alarm only. Therefore, operation at the lower boundary of the degraded voltage relay dropout setting would not trip the motors.

480V switchgear motors - The lowest voltage at the 480V Shutdown Boards would be 441 volts or approximately 92% (Attachment 11.3.a of Ref. 2.1). The increased motor current would be approximately 110% of normal. All of the switchgear breakers for motors are set above 125% of nominal (Ref. 2.2). Therefore, operation at the lower boundary of the degraded voltage relay dropout setting would not trip the motors.

480V mcc motors - The lowest voltage at the 480V mccs would be 437 volts or approximately 91% (Attachment 11.3.a of Ref. 2.1). The increased motor current would be approximately 110% of normal. TOLs are set above 115% of nominal for motors with SF 1.0 and above 125% of nominal for motors with SF 1.15 (Ref. 2.2). All motor breakers are magnetic only, and are not an issue. Therefore, operation at the lower boundary of the degraded voltage relay dropout setting would not trip the motors.

- 5.2.4 SI actuated medium voltage (6.6kV) motor loads are evaluated to ensure that their thermal damage limits are not exceeded during the start-start event.

This was determined not to be an issue. The medium voltage motors can start with 80 percent of motor rated voltage of 6600V (i.e. 76.5% of 6900V in ETAP). During the start-start scenario the 6.9kV bus voltage cannot drop below 87% (Section 3.3) without actuating the loss-of-voltage relays, which will trip the offsite supply in no more than 1.14 seconds (Figure 8.3). Therefore, the available voltages at the medium

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voltage motors will be adequate to ensure starting and accelerating of these loads and will not challenge the motor thermal limits during starting.

- 5.2.5 120VAC control power transformer (CPT) fuse time characteristics are evaluated to determine if the fuse could blow when carrying rated inrush current of the starter and any other normally energized devices for the safety analysis time of 11.5 seconds (upper boundary of the degraded voltage relay time delay, Figure 8.3) or 12 seconds in the start-start scenario.

During the start-start scenario, MCC bus voltages are below the levels used in verifying adequate voltage in control circuit voltage drop calculation. Control circuits for motors being started, or other loads being energized, may be at a sustained inrush for the duration of the start attempt (6 seconds) before going to the diesels. Consequently fuses for these circuits must be verified to not actuate for this condition.

Calculation EDQ00299920080003 (Appendices J and K of Ref. 2.3) was reviewed to identify the typical circuit configurations, their worst case burden during inrush, and the fuse size and presently installed fuses of type TRM. The current for each circuit was calculated for the burden at rated voltage.

The inrush currents were then compared with the fuse melting time-current characteristic (page 8 of this appendix) to determine the melt times. The results are tabulated in Tables B-1 and B-2. Use of inrush currents calculated at rated voltage is conservative for constant impedance devices as the current at degraded voltages will be less. The acceptance pass-fail criteria required for melting time is 12 seconds. From a review of Table B-1 all fuses will carry inrush current for at least 12 seconds and are considered acceptable.

- 5.2.6 MCC 120VAC distribution panel fuse time characteristics are evaluated to determine if the fuses melt during the start attempts. It is considered that circuit components required to pick-up during starting will be at inrush conditions.

Calculation WBNEEBMSTI020020 (Attachment 10.1, 10.2 of R15 of Ref. 2.5 in the main body of this calculation) was reviewed to identify the worst case inrush at rated voltage on each MCC 120VAC distribution panel. Each panel uses KTK type fuses of the 5 amps size. From a review of Table B-2 all fuses will carry inrush current for at least 12 seconds and are considered acceptable.

6.0 SUMMARY OF RESULTS

Based on Section 5.0, following is the summary of results:

6.1 Degraded Voltage Relay and Loss of Voltage relay Setpoint

Existing setpoints for the degraded voltage relay and loss of voltage relay are acceptable.

6.2 Protective Device Evaluation

6.2.1 Motors Actuated by SI Signal

As discussed in Section 5.2.1, there is no adverse effect of the start-start heating on the overcurrent devices on the safety related motors which would be actuated by safety injection signal and powered from safety related 6.9kV and 480V switchgears and 480V MCCs under the degraded voltage conditions.

6.2.2 Non-Accident Safety Related Motors

Based on the analysis in Section 5.2.3, operation of safety-related loads with the 6.9kV Shutdown Board voltage operating at the lower boundary of the degraded voltage relay, 6555V, will not cause tripping of protective devices. Static loads (constant impedance) are not considered, since operation at lower voltage results in less current.

6.2.3 TOL Evaluation

The generic evaluation of TOL's in Section 5.2.2, showed that only motors having locked rotor current in excess of 850% would have to be evaluated further. A review of the WBN ETAP database (Ref. 2.1) showed that there are no motors with a locked rotor current greater than 850% and start for an accident.

6.2.4 Fuse Evaluation for MCCs 120VAC CPT Circuits and 120VAC Distribution Panel Loads

Based on Sections 5.2.5 and 5.2.6, fuses for all 120VAC CPT Circuits and 120VAC Distribution Panel loads are acceptable and will not blow or melt during the 12 seconds criteria during a start-start scenario.

- 6.3 The upper boundary limit for the time delay is 11.5 seconds (Figure 8.3), which is the maximum total time allowed for loss of voltage detection and emergency diesel generator start. Based on the above evaluations, it has been determined that protective devices will not trip prior to 12 seconds for start-start operation of motors at a degraded voltage at which time disconnection from offsite power and reconnection to the emergency diesel generators occurs.

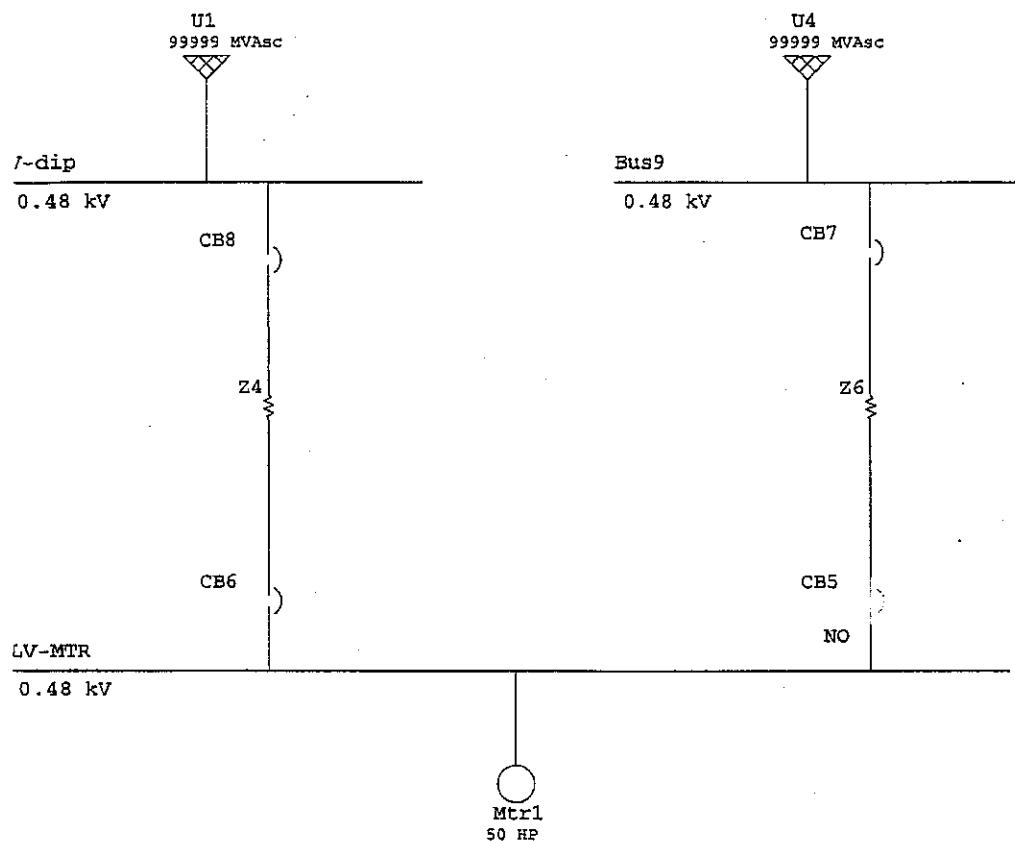
7.0 CONCLUSIONS

The above analyses have demonstrated that in the event of degraded voltage conditions, all safety related loads required for safe shutdown of the unit will be available and perform their intended safety function.

Acceleration of Typical Class 1E Motors (@ 80% MRV)

Appendix No. Attachment 1
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 1 of 16

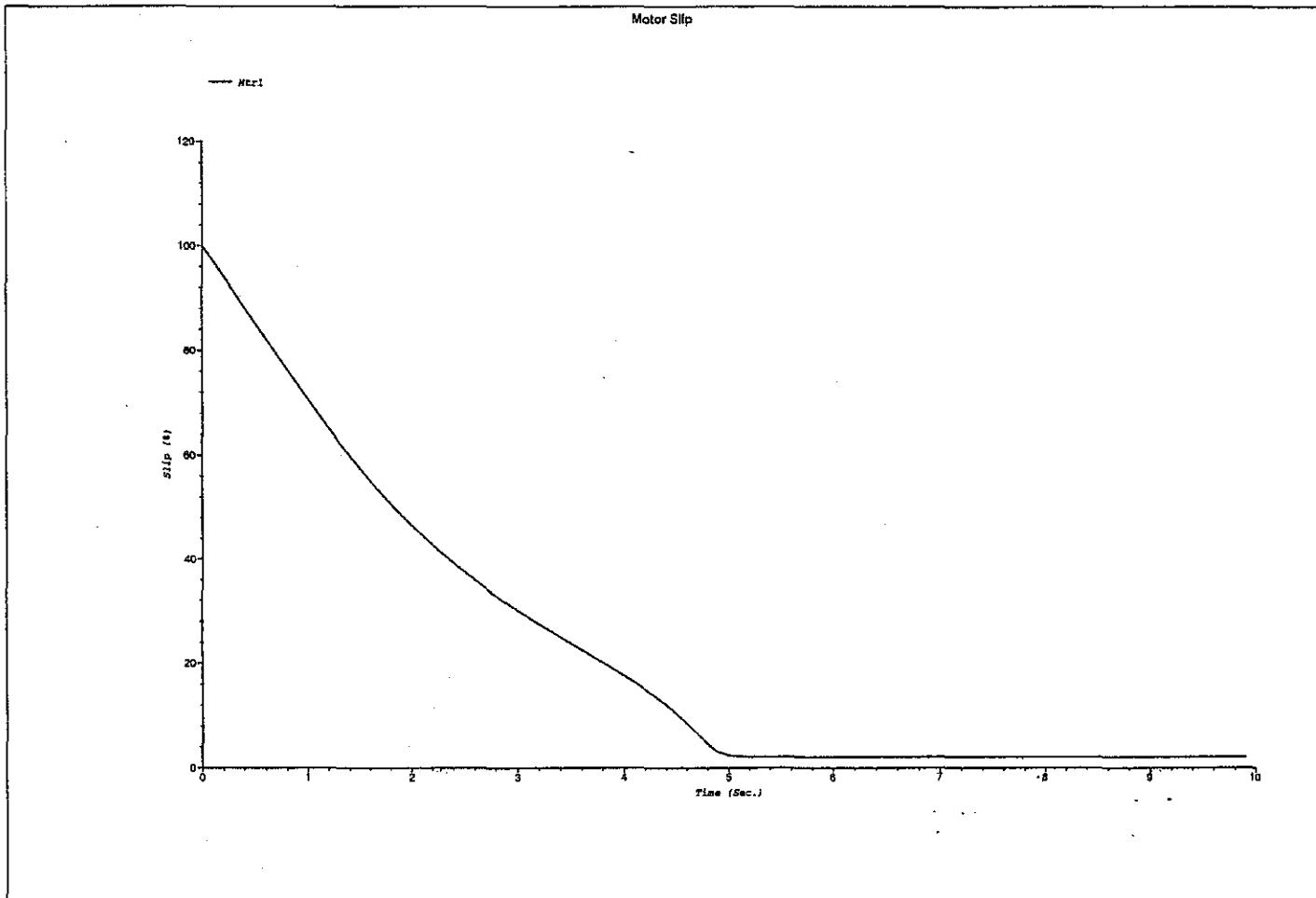
One-Line Diagram - OLVI



Appendix No. Attachment 1
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 2 of 16

Project:
Location:
Contract:
Engineer:

May 26, 2000



Project File: DVMotorAcc

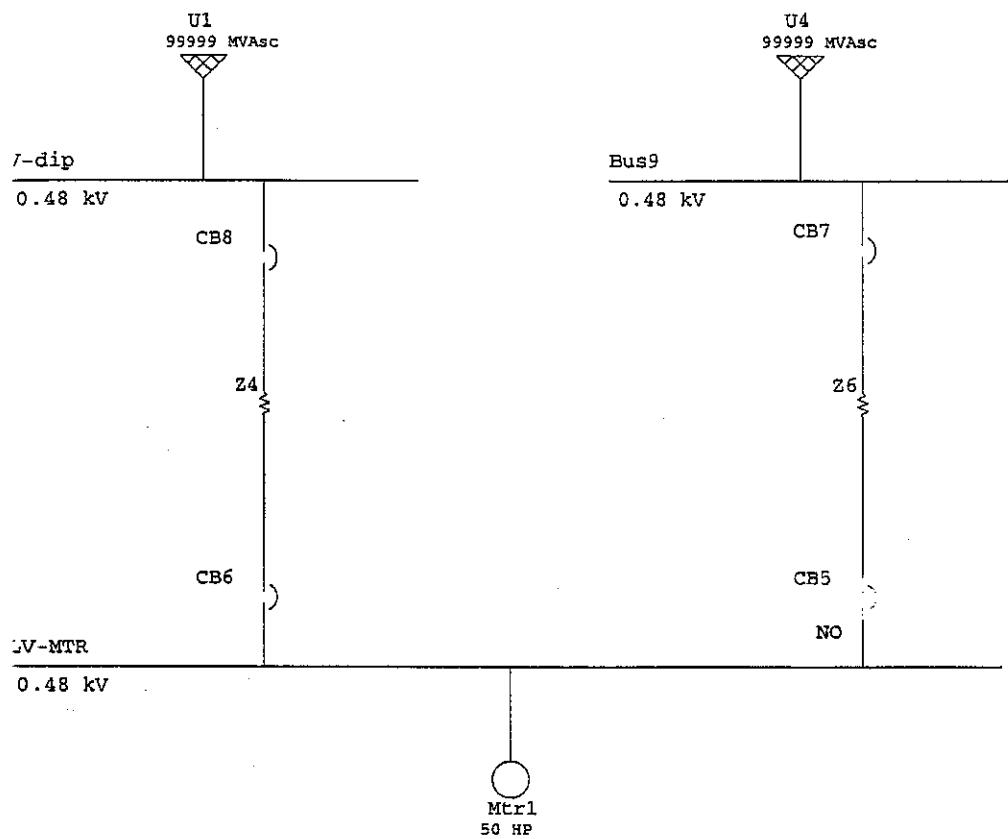
Output Report: Mtr1@80%

Appendix No. Attachment 1
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 3 of 16

Acceleration of Typical Class 1E Motors; Motor Voltage at 320 V
Diesel Generator Breaker Close @ 10 Sec.

Appendix No. Attachment 2
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 1 of 23

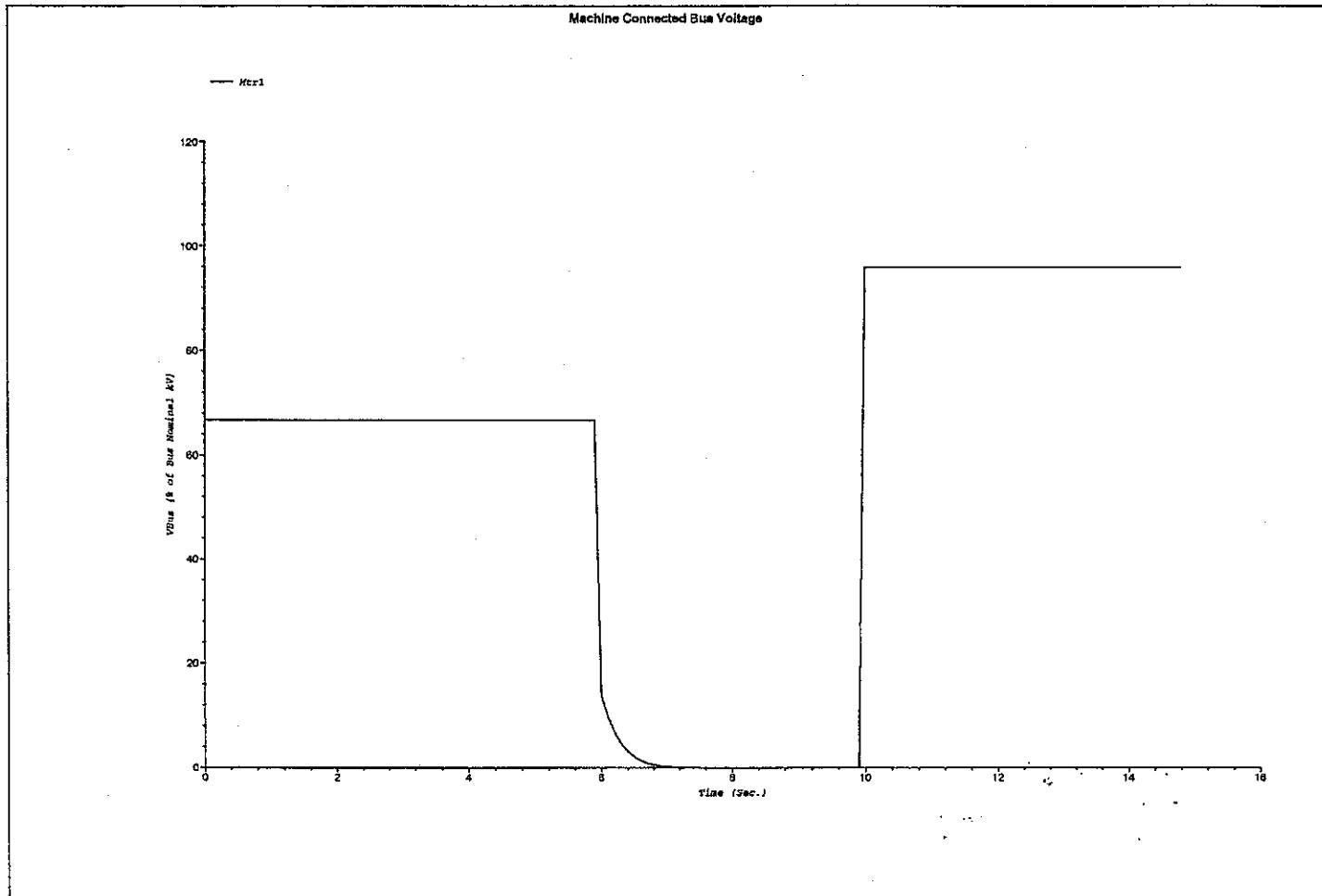
One-Line Diagram - OLV1



Appendix No. Attachment 2
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 2 of 23

Project:
Location:
Contract:
Engineer:

May 26, 2000



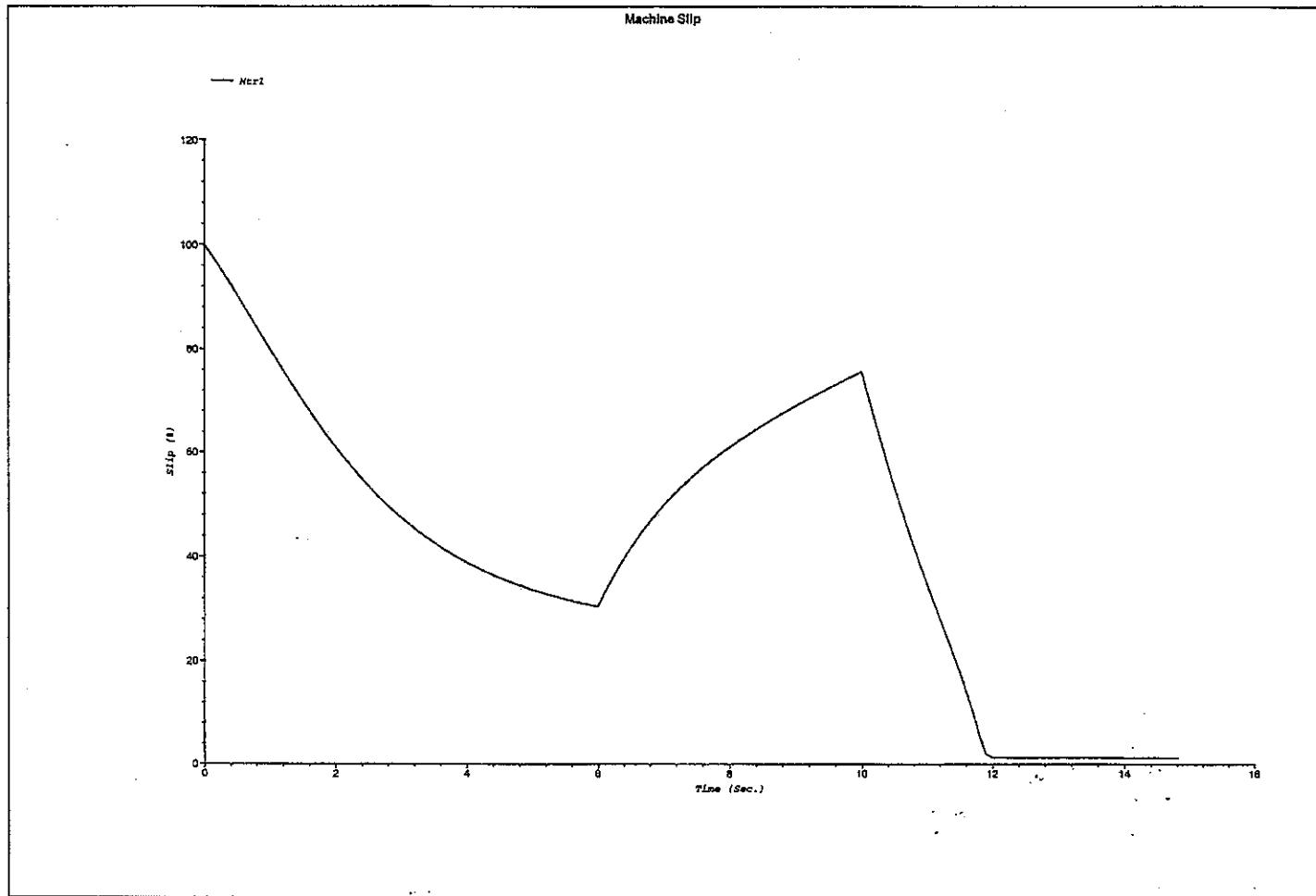
Project File: DVMotorAcc

Output Report: DV-Case1

Appendix No. Attachment 2
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 3 of 23

Project:
Location:
Contract:
Engineer:

May 26, 2000



Project File: DVMotorAcc

Output Report: DV-Casel

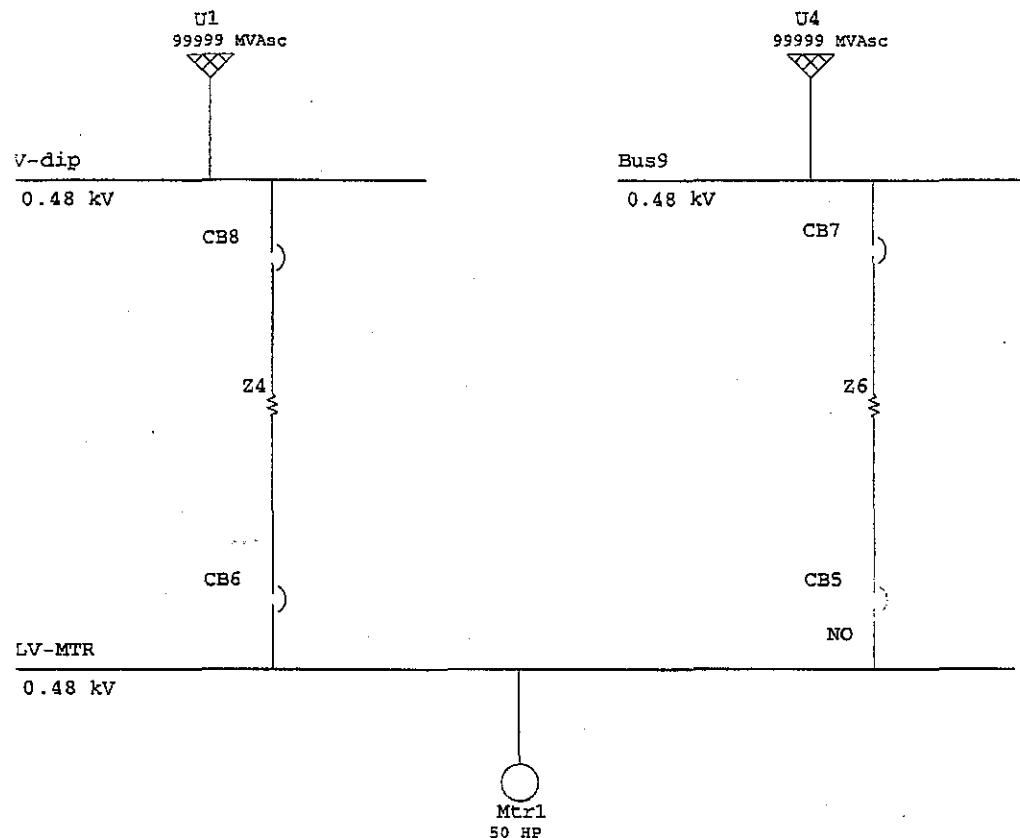
Appendix No. Attachment 2
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 4 of 23

Acceleration of Typical Class 1E Motors; Motor Voltage at 320 V
Diesel Generator Breaker Close @ 11.5 Sec.

Appendix No. Attachment 3
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 1 of 23

One-Line Diagram

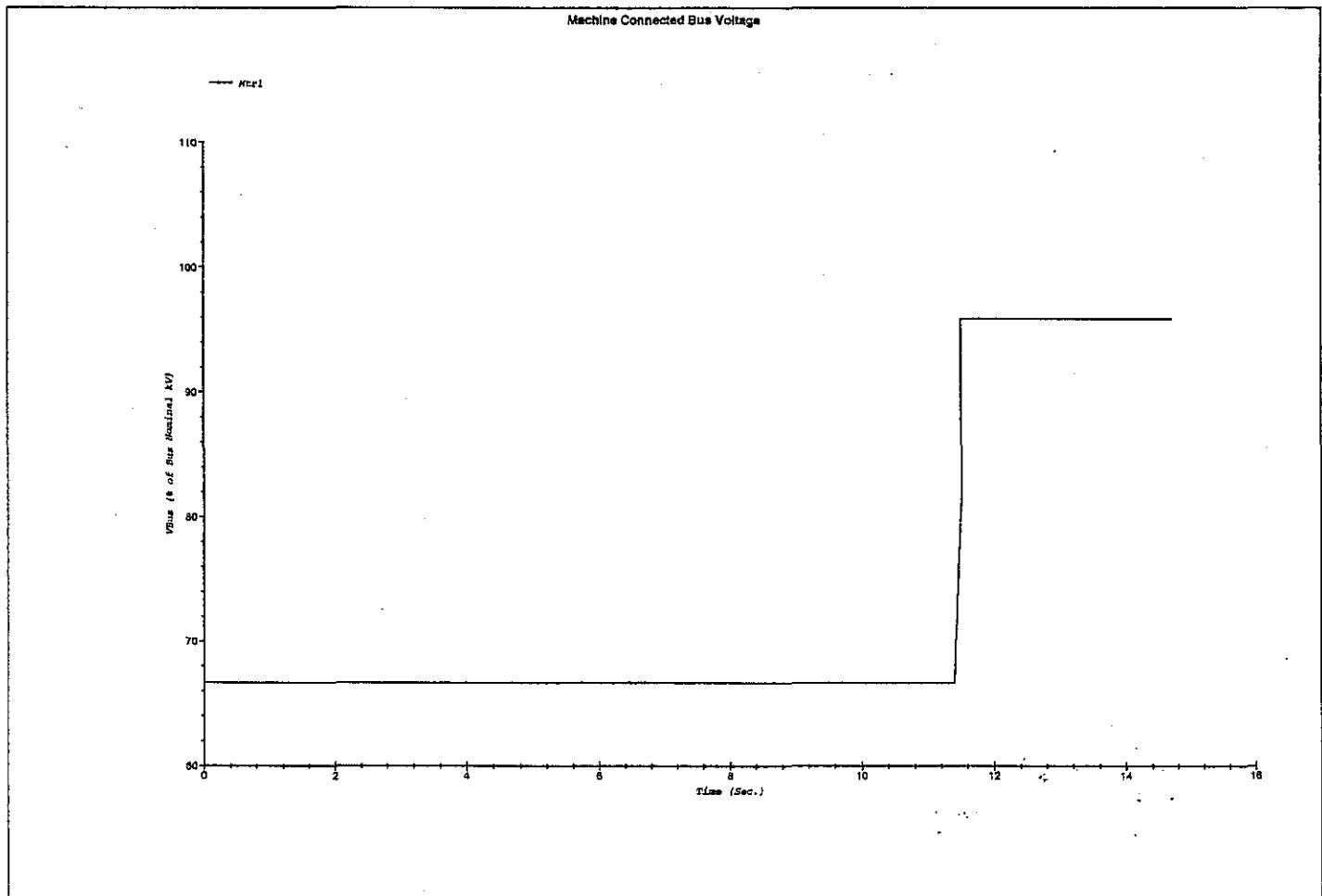
OLV1



Appendix No. Attachment 3
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 2 of 23

Project:
Location:
Contract:
Engineer:

May 26, 2000



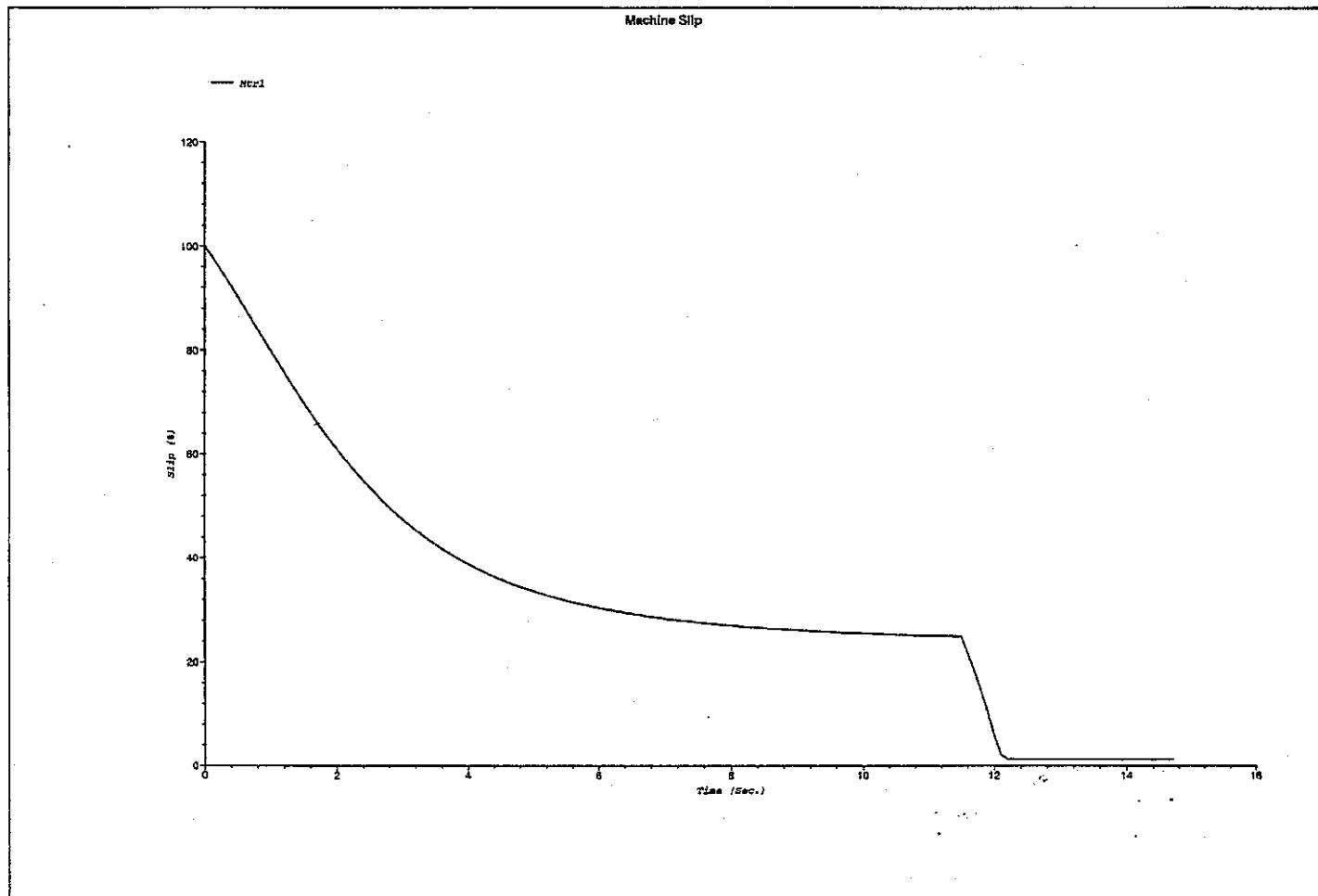
Project File: DVMotorAcc

Output Report: DV-Case2

Appendix No. Attachment 3
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 3 of 23

Project:
Location:
Contract:
Engineer:

May 26, 2000



Project File: DVMotorAcc

Output Report: DV-Case2

Appendix No. Attachment 3
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 4 of 23