



Tennessee Valley Authority, 1101 Market Street, Chattanooga, Tennessee 37402

CNL-14-077

June 13, 2014

10 CFR 50.4

ATTN: Document Control Desk
U.S. Nuclear Regulatory Commission
Washington, D.C. 20555-0001

Watts Bar Nuclear Plant, Unit 2
Construction Permit No. CPPR-92
NRC Docket No. 50-391

Watts Bar Nuclear Plant, Unit 1
Facility Operating License No. NPF-90
NRC Docket No. 50-390

Subject: Responses to Degraded Voltage Issue Requests for Additional Information

- References:
1. Letter from TVA to NRC, "Watts Bar Nuclear Plant (WBN) Unit 2 - Safety Evaluation Report Supplement 22 (SSER22) - Response to NRC Required Action Item, dated August 12, 2011 [ML11229A020]
 2. Letter from TVA to NRC, "Watts Bar Nuclear Plant, Unit 2 - NUREG-0847 Supplemental Safety Evaluation Report (SSER) Related to the Operation of Watts Bar Nuclear Plant, Unit 2, Appendix HH Open Item 30 - Power System Degraded Voltage," dated June 7, 2012 [ML12160A350]
 3. NRC Regulatory Issue Summary (RIS) 2011-12, Revision 1, "Adequacy of station Electrical Distribution System Voltages," dated December 29, 2011 [ML113050583]
 4. NRC Electronic Mail (email) from Siva Lingam to Gordon Arent, on Watts Bar 2 - Open Phase and Open Item 30 RAIs, dated February 27, 2014
 5. NRC Public Meeting Announcement with Tennessee Valley Authority (TVA) regarding Safety Evaluation Report electrical open items related to Watts Bar Nuclear Plant, Unit 2, April 24, 2014 [ML14100A313]
 6. Letter from NRC to TVA, "Watts Bar Nuclear Plant - NRC Integrated Inspection Report 05000390/2010005," dated January 28, 2011 [ML110280456]

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Page 2
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By letter dated August 12, 2011 (Reference 1), Tennessee Valley Authority (TVA) provided a response to NUREG-0847, Supplement 22, "Safety Evaluation Report Related to the Operation of Watts Bar Nuclear Plant, Unit 2," Appendix HH, Open Item 30.

By letter dated June 7, 2012 (Reference 2), TVA submitted updated information related to the offsite and onsite power system degraded voltage studies for safety-related electrical equipment. This submittal included excerpts from STUDY-EEB-WBN-12-001, "Sensitivity Study of Degraded Voltage Relay (DVR) Protection During Motor Starting," Revision 1. The information provided in Reference 2 demonstrated the impact of using a methodology meeting the intent of the guidance provided in Nuclear Regulatory Commission (NRC) Regulatory Issue Summary (RIS) 2011-12, "Adequacy of station Electrical Distribution System Voltages," Revision 1 (Reference 3).

On February 27, 2014, TVA received additional requests for information related to open phase and NUREG-0847, Open Item 30 (Reference 4), including questions associated with Watts Bar Nuclear Plant (WBN), Unit 2 Final Safety Analysis Report (FSAR) Section 8.3. The responses to these requests for additional information (RAIs) are included in this transmittal as Enclosure 1.

On April 24, 2014, the NRC conducted a public meeting with members of TVA (Reference 5). The purpose of the meeting was to discuss the status of electrical open items resulting from the NRC review of the FSAR for WBN Unit 2.

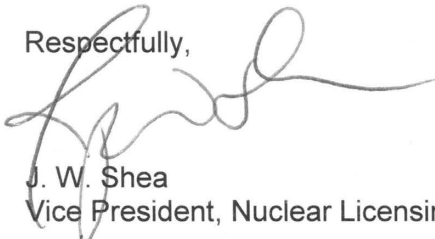
TVA addressed a non-cited violation (NCV) identified in Reference 6 by performing a motor starting analysis in the calculation of record at the DVR dropout analytical limit as opposed to the DVR reset. The analysis is provided in Appendix H of Enclosure 2.

Enclosure 1 to this letter also provides the TVA response to the information requested at the April 24, 2014 public meeting, including responses to the RAIs received in Reference 4. Enclosure 2 provides a copy of the Sensitivity Study of Degraded Voltage Relay (DVR) Protection During Motor Starting, Revision 2, performed by TVA to address the additional concerns with the DVR protection scheme at WBN.

Please address any questions regarding this submittal to Gordon Arent at (423) 365-2004.

I declare under penalty of perjury that the foregoing is true and correct. Executed on the 13th day of June 2014.

Respectfully,



J. W. Shea
Vice President, Nuclear Licensing

Enclosures
cc: See Page 2

ENCLOSURE 1

**TENNESSEE VALLEY AUTHORITY
RESPONSE TO REQUEST FOR ADDITIONAL INFORMATION FOR FSAR SECTION 8.3
ELECTRICAL OPEN ITEMS (TAC NO. ME2731)**

1.0 DESCRIPTION

This enclosure provides information related to degraded voltage protection at Watts Bar Nuclear Plant (WBN). The enclosure provides an overview of the licensing correspondence regarding degraded voltage as it applies to WBN Unit 2 licensing, findings, and remedial actions taken as a result of Nuclear Regulatory Commission (NRC) inspections of degraded voltage relays (DVRs).

2.0 BACKGROUND

TVA has performed calculations to evaluate and document the adequacy of the WBN auxiliary power system for two unit operation. Calculation WBN-EEB-EDQ000-999-2007-0002, "AC Auxiliary Power System Analysis," (Reference 1) verifies that adequate voltage is available for starting safety-related motors (individually) under degraded voltage conditions. Calculation WBN-EEB-MS-TI06-0029, "Degraded Voltage Analysis," (Reference 2) demonstrates that the WBN auxiliary power system complies with NRC Branch Technical Position PSB-1, establishes the basis for the degraded and loss of voltage relay setpoints and their associated time delays, ensures that the voltage level is adequate to allow required safety-related electrical equipment and devices to successfully complete their safety function, and ensures that the duration of the degraded voltage at a given voltage level does not result in thermal degradation or damage of the equipment. TVA Calculation EDQ00299920080003, "Class 1E MCC Control Circuit Voltage Analysis and Transformer Sizing," (Reference 3) and Calculation WBNEEBMSTI020020, "120V AC Class 1E Distribution Panel and Transformer Sizing and Voltage Drop Calculation," (Reference 4) evaluate the control circuits of the Class 1E loads to determine if the circuits will operate adequately, as intended under worst-case voltage drop conditions. In addition, TVA has performed STUDY-EEB-WBN-12-001, "Degraded Voltage Relay (DVR) Protection During Motor Starting," (Reference 5) to evaluate whether the existing DVR setpoint provides the minimum required voltages at the terminals of the Class 1E loads during motor starting (automatic start during a design basis event or individually) while still connected to the preferred offsite power source. A copy of STUDY-EEB-WBN-12-001, Revision 2 is provided in Enclosure 2.

In 2010, two independent but related events resulted in DVR settings at WBN requiring additional evaluation. First, NRC inspections (References 6 and 7) conducted at WBN identified conditions where the DVR setpoint value in the calculation of record was non-conservative with respect to the voltage specified in Technical Specifications (TS). Secondly, TVA submitted WBN Unit 2 Final Safety Analysis Report (FSAR) amendments addressing Section 8, "Electric Power."

On January 28, 2011, TVA received a non-cited violation (NCV) of low safety significance regarding the failure to use the DVR setpoint values specified in TS and configured in the 6.9 kV bus based on the electrical design calculation (Reference 6). The NRC concluded that the availability, reliability and operability of the 6.9 kV safety buses was impacted due to a non-conservative degraded voltage input being used in the safety related motor start and running calculations.

On January 31, 2011, the NRC issued NUREG-0847, Supplement 22, "Safety Evaluation Report, Related to the Operation of Watts Bar Nuclear Plant, Unit 2," Supplement 22, Appendix HH. Appendix HH contained Open Item 30, stating:

TVA should confirm that all safety-related equipment (in addition to the Class 1E motors) will have adequate starting and running voltage at the most limiting safety-related components (such as motor-operated valves (MOVs), contactors, solenoid valves or relays) at the DVR setpoint dropout setting. TVA should also confirm that (1) the motor starting transient studies are based on the dropout voltage value of DVR and time delay, (2) the steady-state voltage drop studies are carried out by maximizing running loads on the Class 1E distribution system (bounding combination of safety systems loads), with the voltage at 6.9 kV Class 1E buses (monitored by the DVRs) at or just above the DVR dropout setting, and (3) the DVR settings do not credit any equipment operation (such as LTC transformers) upstream of the 6.9-kV Class 1E buses. TVA should also confirm that the final technical specifications (TSs) are properly derived from these analytical values for the degraded voltage settings.

By letter dated August 12, 2011 (Reference 8), TVA provided a response to NUREG-0847, Supplement 22, Appendix HH, Open Item 30. In the enclosure to the letter, and in response to Open Item 30, TVA informed the NRC that it had performed a motor-starting transient study assuming the 6.9 kV Shutdown Boards were maintained at the DVR dropout setting and applied the worst-case accident block-start loading (bounding combination of safety system loads). Additionally, the response indicated that the analysis did not credit any non-Class 1E equipment upstream of the 6.9 kV Class 1E buses (such as automatic load tap changers (LTCs) or administratively controlled grid capacity). TVA confirmed that the Class 1E motors required to start and mitigate an accident would have adequate voltage.

On June 7, 2012, TVA submitted updated information related to the offsite and onsite power system degraded voltage studies for safety-related electrical equipment (Reference 9). In Reference 9, TVA submitted excerpts from the Reference 5 sensitivity study of motor starting relative to the existing DVR setpoint. The purpose of the study was to address issues concerning DVR protection at WBN as documented in 1) NRC NCV 05000390/2010005-003, "Failure to use Worst Case 6900 VAC Bus Voltage in design calculations," 2) NUREG-0847, Supplement 22, "Safety Evaluation Report Related to the Operation of Watts Bar Nuclear Plant, Unit 2," Appendix HH, Open Item 30, and 3) recent regulatory developments in the industry with respect to DVR protection and analysis including RIS 2011-12. The study was performed for both WBN Unit 1 and Unit 2.

Subsequently, on February 27, 2014, TVA received a request for additional information (RAI) via NRC Electronic Mail (Reference 10) related to certain aspects of the degraded voltage methodology used at WBN. Responses to these RAIs are provided in Section 3.0 of this enclosure.

On April 24, 2014, the NRC staff conducted a public meeting with members of TVA (Reference 11). The purpose of the meeting was to discuss the status of electrical open items resulting from the NRC review of the FSAR for WBN Unit 2 including the previous correspondence and the February 27, 2014 RAIs. The meeting allowed TVA to present the history of the regulatory guidance/industry events/actions implemented at WBN with regards to degraded voltage, highlights of the analysis performed by TVA on loss of voltage (LOV) and DVR settings, aspects of the TVA conformance with

Branch Technical Position PSB-1, and highlights of the TVA response to SSER Open Item 30.

3.0 RESPONSES TO REQUESTS FOR ADDITIONAL INFORMATION

By email dated February 27, 2014, the NRC forwarded a request for additional information. The NRC stated questions and TVA's responses are presented below.

NRC Request for Additional Information

The staff of the Electrical Engineering Branch (EEEB) of the Division of Engineering has previously requested information on open items associated with NUREG-0847, "Supplemental Safety Evaluation Report (SSER) Related to the Operation of Watts Bar Nuclear Plant, Unit 2." In order to complete the review and close these items, the staff requests additional information from the licensee, as described below:

BACKGROUND

In letter dated June 7, 2012, the Tennessee Valley Authority (TVA) provided a response to Open Item 30 (power system degraded voltage) with respect to SSER, Appendix HH.

The response states that the methodology used in the study was developed to meet the intent of Regulatory Issue Summary (RIS) 2011-12, "Adequacy of Station Electrical Distribution System Voltages".

The RIS states, "The licensee's voltage calculations should provide the basis for proper operation of the plant safety-related electrical distribution system, *when supplied from the offsite circuit(s) (from the transmission network). (emphasis added)* These calculations should demonstrate that the voltage requirements (both starting and running voltages) of all plant safety-related systems and components are satisfied based on operation of the transmission system (including the bounding transmission system single contingency in terms of voltage drop) and the plant onsite electric power system during all operating configurations of transmission network and plant systems."

The TVA response states that to perform the analysis, the 6.9 kV shutdown boards were disconnected from all offsite power source(s) and a dedicated fixed voltage source was added to each 6.9 kV shutdown board (6.9 kV shutdown board was used as a swing bus). The source voltage was set to the degraded voltage relay (DVR) analytical dropout limit of 6555 V.

RAI QUESTION 1

Based on the above statements:

- a) Please explain how disconnecting the shutdown boards from offsite power source(s) meets the intent of guidance provided in the RIS section cited above.
- b) Please explain how the voltage drop through station services transformers (CSST A, B, C and D) is accounted for during block starting or sequential starting of emergency loads in the analyses provided.

- c) If the shutdown bus is considered a 'dedicated fixed voltage source' or a swing bus, then please confirm that the calculation process assumes the swing bus to be an infinite source of real and reactive power. If not, provide basis for the assumption used.
- d) From bus voltage perspective, discuss how this simulation depicts the dynamic response capabilities of the shutdown boards compared to the real and reactive power demand of motor starts postulated during accident conditions with offsite source(s) supplying power through CSST A, B, C and D including all worst-case operating and loading configurations.

TVA Response

During discussions between the NRC and TVA at the April 24, 2014 public meeting, the NRC accepted the study case information presented by TVA and clarified that a response to Question 1 was no longer required. Enclosure 2, Appendix H includes the study cases presented and discussed during the April 24, 2014 public meeting.

RAI QUESTION 2

The analyses states that for contactors, relays and solenoid valves, adequacy of pickup voltage was performed as part of the Control Circuit Voltage Drop (CCVD) analysis. This analysis was performed considering a steady state minimum voltage of 432V at the motor control center (MCC) bus. Please confirm that 432V is the minimum voltage required for operability of all equipment (minimum voltage required at component terminal) with nominal operating voltage of 480V and lower (230/120V) voltage systems supplied from the 480V system.

TVA Response

432 V at the 480V AC Shutdown Boards and MCCs, ensures that the safety-related equipment connected to the Class 1E system is capable of performing their intended function. TVA's analysis of this is contained in Calculations EDQ00299920080003, "Class 1E MCC Control Circuit Voltage Analysis and Transformer Sizing," (Reference 3) and WBNEEBMSTI020020, "120V AC Class 1E Distribution Panel and Transformer Sizing and Voltage Drop Calculation," (Reference 4).

RAI QUESTION 3

The analyses states that the MCC transient bus voltage under degraded voltage conditions (at DVR dropout voltage of 6555V) drops below 432V due to starting of large motors on the 480V switchgear and recovers to a value of >432V within 4 seconds. Please confirm that the duration and magnitude of voltage drop and recovery during block starting of all safety related loads and sequenced start of loads remains within the acceptable range without actuating any protective devices (accident analyses perspective) if the 6.9kV busses remain connected to the 161kV offsite power source through the CSSTs.

TVA Response

The magnitude and duration of the < 4 second dip below 432V is acceptable for all equipment as discussed in TVA Calculation WBN-EEB-EDQ000-999-2007-0002, "AC Auxiliary Power

Systems Analysis,” and does not actuate any protective device, as discussed in TVA Calculation WBN-EEB-MS-TI06-0029, “Degraded Voltage Analysis.”

RAI QUESTION 4

Calculation Number WBN-EEB-EDQ000-999-2007-0002 1 submitted in response to preliminary request for additional information regarding Unit 2 licensing process states the following:

“One 161 kV transmission line and CSSTs A and D, or the other transmission line and CSSTs B and C, shall be capable of starting and running all required safety-related loads and powering all running BOP loads for a design basis accident in one unit and orderly shutdown of the other unit. The analysis for the Class 1 E power system shall evaluate all equipment that is started by a safety injection signal (SIS) as starting at the same time unless the load's control circuitry has sequential time delay, and that all continuous loads that could be operating as required by the process, whether safety-related or not, are running. The analyses in this calculation evaluate the starting of the equipment required to mitigate an accident in accordance with the above requirements for one Unit and simultaneous orderly shutdown of the other unit. The worst case bases for this evaluation is assuming a 161 kV grid pre-event voltage of 164kV and a subsequent 161 kV grid drop of 9kV at event initiation resulting in a post event 161kV grid voltage of 153kV. The analyses shows that all equipment required to start to mitigate an accident receive adequate starting voltage within the time period (5 seconds) of Reference 2.16 for the cases when both CSST C and D are available and also when only one CSST (either C or D) is available.”

Enclosure 1 attached to TVA letter dated July 31, 2010, provided similar information (reference pages E1-63 and 64) regarding the capability of the electrical power system described in FSAR Section 8.1. Please clarify that the impact of the voltage drop in the 161kV system coupled with the voltage drop in CSSTs during block loading of accident loads is accounted for in the degraded voltage relay setpoint calculation performed in accordance with the recommendations of RIS 2011-12.

TVA Response

During discussions between the NRC and TVA at the April 24, 2014 public meeting, the NRC accepted the study case information presented by TVA and clarified that a response to Question 4 was no longer required. Enclosure 2, Appendix H includes the study cases presented and discussed during the April 24, 2014 public meeting.

RAI QUESTION 5

- 1) In response to NRC letter dated December 20, 2013, for resolving open phase condition (OPC) design vulnerability within electric system at Watts Bar 2, TVA stated that:

Vulnerability studies of the OPC faults have been completed for WBN and additional operator meetings are being scheduled to communicate the results. For the analyzed configurations, the vulnerability studies showed existing protection automatically actuates and provides protection to the Class-1E system for grounded open phase

conditions. Vulnerability to an ungrounded open phase condition has been identified for some analyzed configurations.

The TVA nuclear fleet has endorsed the generic schedule provided in the Industry OPC Initiative.

To resolve the OPC design vulnerability at Watts Bar 2, staff requests that TVA provide design features and analyses information in the Final Safety Analysis Report to automatically detect and alarm in the main control room for OPC with and without a high impedance ground condition including two open phase condition on the high voltage side of a transformer connecting a credited GDC-17 offsite power circuit to the transmission system. For OPC, automatic detection and actuation circuits will transfer loads required to mitigate postulated accidents to an alternate power source and ensure that safety functions are preserved, as required by the current licensing bases. The OPC should be sensitive enough to identify an open phase condition under all operating electrical system configurations and loading conditions for which they are required to be operable and should minimize misoperation, maloperation, and spurious actuation. In addition, the staff requests TVA to address the limiting conditions of operation and surveillance requirements that must be added to the plant Technical Specifications to meet the provisions of 10CFR50.36 (c) (2) and c(3).

The above information is required from TVA for staff to reach the necessary safety conclusion that the electrical power system for Watts Bar Unit 2 design meets the 10 CFR Part 50, Appendix A, GDC 17, 10 CFR 50.55a(h)(2), and 10 CFR 50.36 requirements with respect to addressing electric power system design vulnerability due to OPC which could affect the safety functions of both onsite and offsite power systems.

TVA Response

As requested by the NRC staff during discussions with TVA on June 4, 2014, the response to Question 5 is being provided in a separate transmittal.

4.0 Non-cited Violation (NCV) 05000390/2010005-003

On January 28, 2011, TVA received a NCV of low safety significance (green) regarding the failure to use the DVR setpoint values specified in TS and configured in the 6.9 kV bus based on the electrical design calculation (Reference 6). The NRC concluded that the availability, reliability and operability of the 6.9 kV safety buses was impacted due to a non-conservative degraded voltage input being used in the safety related motor start and running calculations.

TVA STUDY-EEB-WBN-12-001, "Sensitivity Study of Degraded Voltage Relay (DVR) Protection During Motor Starting," (Reference 5) evaluates whether the DVR setpoint provides the minimum required voltages at the terminals of the Class 1E loads during motor starting (automatic start during a design basis event or individually) while still connected to the preferred offsite power source. The study concludes that adequate starting voltage is available to each Class 1E load when the 6.9 kV Shutdown Boards are at the DVR dropout setpoint for the following cases: 1) during a design basis event (all Class 1E loads that are automatically actuated for a safety injection (SI) signal), and 2) when individually starting a motor (all Class 1E loads, even if not SI actuated). Therefore, the existing DVR setpoints are adequate.

A copy of the study is provided in Enclosure 2 to address issues concerning DVR protection at WBN as documented in NRC NCV 05000390/2010005-003.

References

1. TVA Calculation WBN-EEB-EDQ000-999-2007-0002, AC Auxiliary Power Systems Analysis, Revision 38, May 28, 2014
2. TVA Calculation WBN-EEB-MS-TI06-0029, Degraded Voltage Analysis, Revision 36, March 13, 2014
3. TVA Calculation EDQ00299920080003, "Class 1E MCC Control Circuit Voltage Analysis and Transformer Sizing," Revision 10, dated February 1, 2014
4. TVA Calculation WBNEEBMSTI020020, "120V AC Class 1E Distribution Panel and Transformer Sizing and Voltage Drop Calculation," Revision 15, dated August 3, 2011
5. TVA STUDY-EEB-WBN-12-001, Degraded Voltage Relay (DVR) Protection During Motor Starting, Revision 001
6. Letter from NRC to TVA, "Watts Bar Nuclear Plant - NRC Integrated Inspection Report 05000390/2010005," dated January 28, 2011
7. Letter from NRC to TVA, "Watts Bar Nuclear Plant - NRC Component Design Bases Inspection - Inspection Report 05000390/2010006," dated June 11, 2010 [ML101620543]
8. Letter from TVA to NRC, "Watts Bar Nuclear Plant (WBN) Unit 2 - Safety Evaluation Report Supplement 22 (SSER22) - Response to NRC Required Action Item," dated August 12, 2011 [ML11229A020]
9. Letter from TVA to NRC, "Watts Bar Nuclear Plant, Unit 2 - NUREG-0847 Supplemental Safety Evaluation Report (SSER) Related to the Operation of Watts Bar Nuclear Plant, Unit 2, Appendix HH Open Item 30 - Power System Degraded Voltage," dated June 7, 2012 [ML12160A350]
10. NRC Electronic Mail (email) from Siva Lingam to Gordon Arent, on Watts Bar 2 - Open Phase and Open Item 30 RAIs, dated February 27, 2014
11. Summary of April 24, 2014 Meeting with Tennessee Valley Authority Regarding Watts Bar Nuclear Plant, Unit 2, Open Item for Licensing, May 29, 2014 [ML14118A201]

ENCLOSURE 2

**STUDY-EEB-WBN-12-001,
DEGRADED VOTAGE RECOVERY ANALYSIS for DBE,
Revision 2**

NPG CALCULATION COVERSHEET / CTS UPDATE

<u>REV 0 EDMS/RIMS NO.</u> T93120417020		<u>CTS TYPE:</u> Calculation		<u>EDMS TYPE:</u> CALCULATIONS (NUCLEAR)		<u>EDMS ACCESSION NO (N/A for REV. 0)</u>	
Calc Title: Sensitivity Study of Degraded Voltage Relay (DVR) Protection During Motor Starting							
<u>ORG</u>		<u>PLANT</u>		<u>BRANCH</u>		<u>NUMBER</u>	
CALC ID		NUC		WBN		EEB	
				STUDY-EEB-WBN-12-001		CUR REV 001	
						NEW REV 002	
CTS UPDATE ONLY <input type="checkbox"/> (Verifier and Approval Signatures Not Required)				NO CTS CHANGES <input checked="" type="checkbox"/> (For calc revision, CTS has been reviewed and no CTS changes required)			
<u>UNIT (check one)</u> 0 <input checked="" type="checkbox"/> 1 <input type="checkbox"/> 2 <input type="checkbox"/> 3 <input type="checkbox"/>		<u>SYSTEMS</u> N/A			<u>UNIDS</u> N/A		
<u>DCN.EDC.N/A</u> See Revision Log		<u>APPLICABLE DESIGN DOCUMENT(S)</u> See References				<u>CLASSIFICATION</u> FO	
<u>QUALITY RELATED?</u> Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	<u>SAFETY RELATED?</u> (If yes, QR = yes) Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	<u>UNVERIFIED ASSUMPTION</u> Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	<u>SPECIAL REQUIREMENTS AND/OR LIMITING CONDITIONS?</u> Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>		<u>DESIGN OUTPUT ATTACHMENT?</u> Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	<u>SAR/TS and/or ISFSI SAR/CoC AFFECTED</u> Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>	
<u>CALCULATION NUMBER REQUESTOR</u> Name: Anil Bangalore PHONE: 423 365 1610			<u>PREPARING DISCIPLINE</u> EEB		<u>VERIFICATION METHOD</u> DESIGN REVIEW		<u>NEW METHOD OF ANALYSIS</u> <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
<u>PREPARER (PRINT NAME AND SIGN)</u> Daljeet Bhatia <i>Daljeet Bhatia</i>		<u>DATE</u> 5/29/14	<u>CHECKER (PRINT NAME AND SIGN)</u> Vinu Patel <i>Vinupatel</i>			<u>DATE</u> 5/29/14	
<u>VERIFIER (PRINT NAME AND SIGN)</u> N/A		<u>DATE</u> 5/30/14	<u>APPROVAL (PRINT NAME AND SIGN)</u> Ronald E Cox <i>Ronald E. Cox</i>			<u>DATE</u> 6/3/14	
<u>STATEMENT OF PROBLEM/ABSTRACT</u> <i>ACB</i> <i>5/30/14</i>							
<u>Statement of problem</u> Issues were raised by the NRC concerning degraded voltage relay (DVR) protection which can be summarized as the need to determine if the DVR setpoint provides the minimum required voltages at the terminals of the Class 1E loads during motor starting (automatic starting during a DBE or individually) while still connected to the preferred offsite power source.							
<u>Abstract</u> This study is being performed as a sensitivity study to see the impact to the DVR setpoint and/or plant response if the current methodology is changed and determine if adequate starting voltage is available to each Class 1E load when the 6.9kV Shutdown Boards are at the DVR dropout setpoint (analytical limit) for the following cases: <ul style="list-style-type: none"> • During a design basis event (DBE): all Class 1E loads that are automatically actuated for a safety injection signal (SI-Phase A or SI-Phase B). • When individually starting a motor (single motor start): all Class 1E loads, even if not SI-actuated. <p>This study will also show that for a degraded voltage condition, overcurrent protective devices associated with Class 1E loads will not trip during SI-actuated motor starting and subsequent start on the emergency diesel generator. This analysis is performed for both Unit 1 and Unit 2.</p> <p>The study has a Compact Disk (CD) that contains Appendices C, D, E, F and G (ETAP output reports).</p>							
<u>MICROFICHE/EFICHE</u>		Yes <input type="checkbox"/> No <input checked="" type="checkbox"/>		<u>FICHE NUMBER(S)</u>			

LEGIBILITY EVALUATED AND
ACCEPTED FOR ISSUE, R002 (All Pages)
Initials: *ACB* Date: *5/30/14*

NPG CALCULATION COVERSHEET / CTS UPDATE

CALC ID	ORG	PLANT	BRANCH	NUMBER	REV
	NUC	WBN	EEB	STUDY-EEB-WBN-12-001	002
BUILDING N/A	ROOM N/A	ELEVATION N/A	COORD/AZIM N/A	FIRM BECHTEL	
CATEGORIES					

KEYWORDS (A-add, D-delete)

ACTION (A/D)	KEYWORD	A/D	KEYWORD

CROSS-REFERENCES (A-add, D-delete)

ACTION (A/D)	XREF CODE	XREF PLANT	XREF TYPE	XREF NUMBER	XREF REV
A	P	WBN	CALCULATION	EDX-000-999-2004-0002	

CTS ONLY UPDATES:

Following are required only when making keyword/cross reference CTS updates and page 1 of form NEDP-2-1 is not included:

PREPARER (PRINT NAME AND SIGN)	DATE	CHECKER (PRINT NAME AND SIGN)	DATE
PREPARER PHONE NO.	EDMS ACCESSION NO.		

NPG CALCULATION RECORD OF REVISION

CALCULATION IDENTIFIER		STUDY-EEB-WBN-12-001	Page 2
Title Sensitivity Study of Degraded Voltage Relay (DVR) Protection During Motor Starting			
Revision No.	DESCRIPTION OF REVISION		
000	<p>Initial issue. This sensitivity study also completes one of the corrective actions (298321-005) in PER 298321.</p> <p>Total number of pages: 127 This calculation also contains a CD which stores the ETAP output files and is stored in the calculation library for reference.</p> <p>Special Requirements/Limiting Conditions: None Successor Calculations: None</p>		
001	<p>Revised to incorporate comments from Licensing, revised section 7 to add analysis for Control Circuit Voltage Drop and added Introduction to Appendix A.</p> <p>Pages added: 13, Appendix A (page i, ii) Pages revised & replaced: 1, 2, 3, 5 thru 9, 11, Att. 4 (pages 10, 11), Att. 5 (pages 7, 8) Pages deleted: None</p> <p>Total number of pages: 130</p> <p>This study was prepared in accordance with procedure requirements, utilizing standard calculation format and forms. This study is a one-time sensitivity study to determine the impact, if any, to the plant if a new degraded voltage methodology is implemented.</p> <p>Special Requirements/Limiting Conditions: None Successor Calculations: None</p>		

NPG CALCULATION RECORD OF REVISION

CALCULATION IDENTIFIER STUDY-EEB-WBN-12-001

Page 2A

Title Sensitivity Study of Degraded Voltage Relay (DVR) Protection During Motor Starting

Revision No.

DESCRIPTION OF REVISION

002

This revision involves the following:

- Rerun Dynamic and Static Motor Starting analysis with the revised database incorporating all modifications performed to support U2 completion and ongoing modifications to the operating Unit 1.
- Perform additional degraded voltage analysis utilizing the offsite power as a swing source. This additional analysis is being performed in Appendix H..

Pages added: 2A, 4A, App. H (5 pages), Att. 5 (pages 8A, 8B, 8C, 8D)

Pages revised & replaced: 1, 1A, 3, 5, 6, 10, 13, App. A (pages 1 - 25), App. B (page 1),

Att. 4 (pages 10, 11), Att. 5 (pages 7, 8)

Pages deleted: Appendix A (pages 26-27)

This calculation contains a CD which stores the revised ETAP Reports for Appendices C, D, E, F and G.

Total number of pages for Calculation: $130 + 11 - 2 = 139$

This study was prepared in accordance with procedure requirements, utilizing standard calculation format and forms. This study determines the impact, if any, to the plant if a new degraded voltage methodology is implemented.

Special Requirements/Limiting Conditions: None

Successor Calculations: None

NPG CALCULATION TABLE OF CONTENTS

Calculation Identifier: STUDY-EEB-WBN-12-001

Revision: 002

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NPG COMPUTER INPUT FILE STORAGE INFORMATION SHEET			
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Subject: Sensitivity Study of Degraded Voltage Relay (DVR) Protection During Motor Starting			
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<input checked="" type="checkbox"/> Input files for this calculation have been stored electronically and sufficient identifying information is provided below for each input file. (Any retrieved file requires re-verification of its contents before use.)			
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Document Type	FILE		
Initiated Date	20120404		
Key Items	ELECTRICAL CALCULATION		
Equipment Name	ETAP		
Reference	STUDY-EEB-WBN-12-001 R0		
Description	Input Files for WBN CALC 12-001 R0		
Added By User	dsbhatia		
Property	BSL		
Data Added	04/04/2012 3.26.36 PM		
Document Category	FILEKEEPER		
Organization	NUCLEAR		
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Resp Org	WBNP		
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Document STUDY-EEB-WBN-12-001

Rev. 002

Plant: WBN

Subject:

Sensitivity Study of Degraded Voltage Relay (DVR) Protection During Motor Starting

 Electronic storage of the input files for this calculation is not required. Comments:

The Output files for the software ETAP are accessible in the EDMS System under Document Identifier STUDY-WBN-EEB-12-001.

 Input files for this calculation have been stored electronically and sufficient identifying information is provided below for each input file. (Any retrieved file requires re-verification of its contents before use.)

File Keeper Storage / Retrieval System

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Document Type	FILE
Initiated Date	20140523
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Equipment Name	ETAP
Reference	STUDY-EEB-WBN-12-001 R2
Description	Input Files for WBN CALC 12-001 R2
Added By User	dsbhatia
Property	BSL
Data Added	05/23/2014
Document Category	FILEKEEPER
Organization	NUCLEAR
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Resp Org	WBNP

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WBNDATA.PSO	07/13/2010 @ 10:05 AM	07/13/2010 @ 10:05 AM

Note: Additional copy of the input/output files are contained on server:

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SHEET 5

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1.0 Purpose

The purpose of this study is to address the issues concerning degraded voltage relay (DVR) protection at WBN as documented in:

1. WBN NCV 05000390/2010005-003 "Failure to Use Worst Case 6900 VAC Bus Voltage in Design Calculations"
2. Watts Bar (WBN) Unit 2 NUREG-0847, Supplement 22, RAI Item 30
3. Recent regulatory developments in the industry with respect to DVR protection and analysis including NRC Regulatory Issue Summary (RIS) 2011-12, "Adequacy of Station Electrical Distribution System Voltages"
4. Additional NRC comments received in public meeting

These issues can be summarized as the need to determine if the DVR setpoint provides the minimum required voltages at the terminals of the Class 1E loads during motor starting (automatic starting during a design basis event or individually) while still connected to the preferred offsite power source.

Currently, the DVR analytical limit is determined by the Degraded Voltage Analysis calculation (Ref. 2.1), using methodology consistent with industry standard IEEE Std. 741-1997 and station licensing basis. The DVR setpoint methodology has not previously considered motor starting voltage as a basis of the relay setpoint. This study is being performed as a sensitivity study to see the impact to the setpoint and/or plant response if the current methodology is changed.

1.1 Scope

This study determines if adequate starting voltage is available to each Class 1E load when the 6.9kV Shutdown Boards are at the DVR dropout setpoint (analytical limit) for the following cases:

- During a design basis event (DBE): all Class 1E loads that are automatically actuated for a safety injection signal (SI-Phase A or SI-Phase B).
- When individually starting a motor (single motor start): all Class 1E loads, even if not SI-actuated.

This study will also show that for a degraded voltage condition¹, overcurrent protective devices associated with Class 1E loads will not trip during SI-actuated motor starting and subsequent start on the emergency diesel generator.

This analysis is performed for both Unit 1 and Unit 2.

2.0 References

- 2.1 Calculation WBNEEBMSTI060029, Revision 33 "Degraded Voltage Analysis"
- 2.2 Calculation EDQ00099920070002, R37, "AC Auxiliary Power System Analysis (dual unit operation)"
- 2.3 Calculation WBNEEBEDQ1999010001, R75, "AC Auxiliary Power System Analysis"
- 2.4 NRC Regulatory Issue Summary (RIS) 2011-12, Revision 1, "Adequacy of Station Electrical Distribution System Voltages"
- 2.5 Watts Bar (WBN) Unit 1 NCV 05000390/2010005-03, "Failure to Use Worst Case 6900 VAC Bus Voltage in Design Calculations"
- 2.6 Watts Bar (WBN) Unit 2 NUREG-0847, Supplement 22, "Safety Evaluation Report Related to the operation of Watts Bar Nuclear Plant, Unit 2", RAI Item 30
- 2.7 Calculation WBNEEBMSTI060010, R76, "Auxiliary Power System Analysis on 1E Buses" (Historical Reference)

¹ A degraded voltage condition is when the 6.9kV Shutdown Board voltage drops below the DVR setpoint, but not below the loss of voltage (LOV) setpoint, and does not recover.

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- 2.8 Calculation WBPE2119202001, R8, "6.9kV Shutdown Logic Boards Undervoltage Relays Requirements/Demonstrated Accuracy Calculation"
- 2.9 Limitorque Maintenance Update 92-2 (RIMS L33930113 803) - Extract from Design Guide DG-E2.4.6
- 2.10 TVA General Engineering Specification DS-E9.4.1, R1, Selection and Specifications of Motors
- 2.11 NEMA MG-1-1998, Motors and Generators
- 2.12 PER 298321
- 2.13 Calculation EDX-000-999-2004-0002, R3, TSS Grid Voltage Study of WBN's Offsite Power System

3.0 Bases/Assumptions

- 3.1 The DVR dropout analytical limit (6555V) as determined in the Degraded Voltage Analysis calculation (Ref. 2.1) will be used to determine the available starting voltage.
- 3.2 The ETAP model used to perform offsite power analysis for dual unit operation (Ref. 2.2) is used to perform the motor starting analysis.
- 3.3 All process controlled loads (random loads) are conservatively considered to start at zero seconds in a DBE.
- 3.4 The Phase A Start Sequence evaluates a Safety Injection Initiation without receipt of a Phase B Containment Isolation (High Containment Pressure). The Phase B Start Sequence evaluates a Safety Injection Initiation with receipt of a Phase B Containment Isolation.

The short term steady state loading at the 480V level is higher during a Phase A start sequence than during a Phase B and results in a lower voltage at the 480V busses. However, piping breaks associated with a Phase A Start Sequence are small and will result in ECCS equipment being removed from service within a short period after the event (less than an hour). This will result in a much lower overall long term loading for a Phase A event when compared to a Phase B.

This study uses short term Phase A loading for the single motor start analysis since it is the most conservative loading. If, however the starting voltage (480V) is not acceptable using the Phase A loading, then Phase B loading is used provided:

- The load is only required for a Phase B event, or
- The load is required to be manually started at a time that is at least 2 hours after the initiation of a Phase A event.

This assumption is conservative since the long term 480V loading for a Phase B event is higher than for a Phase A event.

- 3.5 The 89-10 MOVs for WBN utilize motor actuators which have 'hammer-blow' feature, which allows the motor to start turning prior to engaging the mechanical load of the operator (i.e. start unloaded). The actual motor current draw is typically 50% of the full locked-rotor current (Ref. 2.9). Initially all MOVs are evaluated using full locked-rotor current but if the available voltage does not meet the required voltage criteria, the available voltage is re-calculated taking credit for the 'hammer-blow' feature. These MOVs are identified in Appendix A.

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4.0 Methodology/Approach

The methodology used in this study was developed to meet the intent of Regulatory Issue Summary (RIS) 2011-12, "Adequacy of Station Electrical Distribution System Voltages". The RIS states the protective function of the DVR setpoint is to ensure adequate starting voltage to all Class 1E equipment for all operating and accident conditions. Additionally, the RIS states that the DVR setpoint must be based on the starting voltage requirement at the terminal of the most limiting component and must account for the effect of all components which could affect voltage, this includes offsite power circuits, the plant distribution system, as well as all Class 1E and non-Class 1E loads.

However, the RIS does not prescribe the specific methodology to be used for the motor starting analysis, and there is no industry consensus on how to best address DVR protection for motor starting scenarios.² In actuality, the ability to start motors cannot be determined by monitoring voltage alone. The ability to start motors can only be determined by power system capacity, which is the ability to maintain voltage while providing the required starting current. Therefore, the very premise of using a voltage relay to protect motor starting ability requires an assumption of the power source capacity, which seems to violate the stated purpose of the DVR protective function.

An analytical approach is used in this study to determine the acceptability of the voltage during any Class 1E motor starting scenario that bounds any value of upstream capacity. This approach is based on the fact that for any Class 1E motor starting event (single motor or group of motors), the voltage at the DVR monitored bus can only respond in one of three ways:

1. The voltage decreases to the DVR setpoint, or above (i.e. DVR does not actuate)
2. The voltage decreases below the DVR setpoint and does not recover (i.e. DVR actuates and transfers loads to the DGs after the specified time)
3. The voltage decreases below the DVR setpoint and does recover (i.e. DVR actuates but does not initiate transfer since voltage remains above the LOV setpoint and recovers above the DVR reset value prior to timeout)

Analyses are performed for each of these situations as follows:

1. A starting voltage analysis is performed using a technique known as the "independent source" method. The voltage at the DVR monitored bus (i.e. 6.9kV Shutdown Board) is set at the DVR setpoint (dropout analytical limit) using an independent fixed voltage source. Since the initial DVR bus voltage prior to the event can be ignored, this simple technique produces correct voltages for downstream loads immediately after the initiation of the event. The analysis is performed for DBE motor starting (SI-actuated loads) as well as individual motor starts.
2. A protective device analysis is performed using a technique known as the "start-start" method. Since this is truly a degraded voltage situation, there is no need for a starting voltage analysis. However, an analysis should be performed to demonstrate that the Class 1E loads will be successfully transferred to the DG and started prior to their protective devices tripping. This "start-start" analysis was previously performed in the Degraded Voltage Analysis calculation (reference 2.1) and the results are reprinted in this study.
3. For DBE motor starting events, a bounding analysis is performed to demonstrate that any possible voltage transient caused by DBE motor starting, including drop to the LOV setpoint, will also result in successful recovery above DVR reset within 5 seconds (without crediting automatic load tap changers). For individual motor starting events, this situation is bounded by the starting voltage analysis from item 1 since the analysis at DVR dropout is more conservative than analysis at the DVR reset value.

These analyses bound any possible voltage outcome at the DVR monitored bus when starting any Class 1E motor required for any scenario.

² IEEE Power & Energy Society, Nuclear Power Engineering Committee (NPEC), Working Group 4.7 (Protection of Class 1E Power Systems and Equipment) meeting minutes of January 24, 2012, San Antonio, TX.

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5.0 Design Input Data

5.1 For individual minimum motor starting voltage requirements, see Appendix A.

5.2 The degraded voltage relay setpoints are as follows (Ref. 2.1, 2.8 & Att. 2 of this study):

	<u>Dropout (V)</u>	<u>Reset (V)</u>
Nominal Setpoint	6600	6642
Allowable Value	6570	6672
Analytical Limit	6555	N/A
Operational Limit	N/A	6681

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6.0 Computations and Analysis

The motor starting analysis is performed using ETAP V7.0.0N and the existing ETAP model used to perform offsite power system analysis for two unit operation (Ref. 2.2).

6.1 Starting Voltage Analysis

The 6.9kV shutdown boards were disconnected from all offsite power source(s) and a dedicated fixed voltage source was added to each 6.9kV shutdown board. The source voltage was set to the DVR dropout setting of 6555V (Section 5.2).

Using the load configuration in the existing Unit 1 & 2 ETAP model, the following analyses were performed:

- Dynamic Motor Starting – Safety Injection Signal Phase A (SIA)
- Dynamic Motor Starting – Safety Injection Signal Phase B (SIB)
- Static Motor Starting (starting individual motor): This analysis is performed with SIA since this provides the worst case voltages on the 480V system. For this analysis, motor starting study case is generated to individually start each Class 1E motor. Resolutions to loads requiring additional review are annotated in Appendix A. If the starting voltage using Phase A is not acceptable, analysis is performed using Phase B loading

DBE Motor Starting:

Each study case is run for a total simulation time of 15 seconds. Since it is considered that by this time all motors have been accelerated and the APS system has come to a steady state condition. ETAP reports provide terminal voltage and current for every motor which starts at 0+ second up to 15 seconds in steps of 0.1 second.

The output reports are saved as U1 sdbds at DVDO-Complete (Study Case U1-DV-SIBms, Config. DV-LOCA-U1), U2 sdbds at DVDO-Complete (Study Case U2SIB-DV(N), Config. DV-LOCA-U2) and U12 sdbds at DVDO-Complete (Study Case U1/2SIA, Config. Deg Volt SU) in folder J:\wbnp\DVR Analysis (Static) WBN\ETAP Reports - Dynamic Motor Analysis.

Single Motor Starting:

Each study case is run using 'Study Case ID U1/2SIA and Config. Deg Volt SU'.

The output reports, in pdf format, are saved in folders J:\wbnp\DVR Analysis (Static) WBN\ETAP Reports - Shutdown Boards 1A and 1B and J:\wbnp\DVR Analysis (Static) WBN\ETAP Reports Shutdown Boards 2A and 2B\New Reports. Due to the large number of output reports, the output report names are not listed. These analyses did not credit any non-Class 1E equipment upstream of the 6.9-kV Class 1E buses (such as LTC transformers or administratively controlled grid capacity). The available starting voltage for each motor is then documented and compared to the required starting voltage.

6.2 Protective Device Analysis (Start-Start scenario):

The scenario evaluated for the short time delay is an SI concurrent with the degraded voltage condition such that a block start attempt is made. A determination is made of the time permitted to allow voltage to return above the degraded voltage relay setpoint reset limit under block start transient conditions and still assure a subsequent start on the diesel if the voltage fails to recover, thus, making this a start-start evaluation. To evaluate the effect of the starting currents during the start-start scenario, the effect on overcurrent protective devices are considered. The board voltages at the onset of the event are, considered normal (i.e. no preheat). The degraded voltage condition presumes that the voltage does not recover but remains below the degraded voltage relay setpoint subjecting the SI initiated motors to starting currents for the time delay selected and then sequence onto the emergency diesel generators. The design calculated worst-case transient voltage dip during the accident loading sequence is used. This is conservative, because a lower voltage would produce less starting current for the motors.

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The above evaluation is performed for the safety related loads required for Units 1 and 2 which would be actuated for an SI as follows:

- Motor loads fed from 6.9kV and 480V Switchgear & MCCs, MOVs & Static loads fed from the MCCs are evaluated to determine the effect of the start-start heating of the overcurrent protective devices (breakers/TOLs), such that starting on the diesel without tripping can be assured.
- Protective devices are also evaluated for the 6.6kV and 460V safety-related motors that operate during non-accident conditions. The evaluation considers that the safety bus voltage is equivalent to operation at the lower boundary of the degraded voltage relay dropout. The protective devices are evaluated to ensure that operation of the safety-related loads can be sustained indefinitely at this voltage without protective device trip.
- SI actuated medium voltage (6.6kV) motor loads are evaluated to ensure that their thermal damage limits are not exceeded during the start-start event.
- 120VAC control power transformer (CPT) fuse time characteristics are evaluated to determine if the fuse could blow when carrying rated inrush current of the starter and any other normally energized devices for the safety analysis time of 11.5 seconds (upper boundary of the degraded voltage relay time delay, Attachment 2) or 12 seconds in the start-start scenario.
- MCC 120VAC distribution panel fuse time characteristics are evaluated to determine if the fuses melt during the start attempts. It is considered that circuit components required to pick-up during starting will be at inrush conditions.

6.3 Voltage Recovery Analysis:

See Appendix B for voltage recovery analysis for DBE for detailed purpose, approach, bases and assumptions and computations.

In addition, Appendix H demonstrates the adequacy of the DVR protection scheme if the voltage source is placed at the switchyard bus and the grid voltage and capacity is set

1. Such that the DVR monitored bus voltage is at the DVR dropout analytical limit prior to DBE initiation
2. To support successful voltage recovery following DBE motor starting

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7.0 Summary of Results

7.1 Starting Voltage Analysis

See Appendix A for summary of the results. Based on a review of the results, all safety related loads have adequate starting voltage during DVR conditions and the existing setpoints for the degraded voltage relay are considered acceptable.

Note: ERCW Screen Wash Pumps are not assured to have adequate voltage as analyzed. However per N3-67-4002 this load is not required to be manually placed into service until 12 hours into a design basis event. This provides sufficient time to take corrective actions such as correcting the grid condition, adjusting the tap changers on the CSSTs or transferring the shutdown board(s) to the diesel generators.

Control Circuit Voltage Drop (CCVD) Analysis

With respect to the contactors, relays and solenoid valves, adequacy of pickup voltage for these control components (contactors, solenoid valves, relays) were performed as part of the Control Circuit Voltage Drop (CCVD) analysis. This analysis was performed considering a steady state minimum voltage of 432V at the MCC bus. All the components were determined to have adequate pickup voltage upon implementation of the issued design changes as identified in the CCVD calculation prior to Unit 2 fuel load.

The MCC transient bus voltage under degraded voltage conditions (at DVR dropout voltage of 6555V) drops below 432V due to starting of large motors on the 480V switchgear. This voltage, however, recovers to a value of >432V within 4 seconds. Since the startup of the safety related equipment may not have adequate starting voltage due to transient voltage conditions, Westinghouse evaluated the impact of additional 5 second delay for the startup of the safety injection pumps and feedwater isolation valves with offsite power available, and concluded the following: "This safety evaluation concludes that an additional five second delay for the startup of the safety injection pumps and an additional five second delay in the closure of the feedwater isolation valve does not impact the conclusions of the safety analysis that form the Watts Bar licensing basis (SECL-92-029; RIMS No. T33930330990)".

Based on the above, the analysis performed to verify adequacy of available voltage for the contactors, solenoid valves, relays is considered to be adequate and, therefore, no further analysis under the transient voltage conditions has been performed.

7.2 Protective Device Analysis

Motors Actuated by SI Signal:

As discussed in Attachment 7, there is no adverse effect of the start-start heating on the overcurrent devices on the safety related motors which would be actuated by safety injection signal and powered from safety related 6.9kV and 480V switchgears and 480V MCCs while operating at the lower boundary of the degraded voltage relay setting (6555V).

Non-Accident Safety Related Motors:

Based on the analysis, operation of safety-related loads with the 6.9kV Shutdown Board voltage operating at the lower boundary of the degraded voltage relay 6555V, will not cause tripping of protective devices. Static loads (constant impedance) are not considered, since operation at lower voltage results in less current. Therefore, operation at the lower boundary of the degraded voltage relay dropout setting would not trip the motors.

TOL Evaluation:

The generic evaluation of TOL's, in Attachment 7, showed that only motors having locked rotor current in excess of 850% are required to be evaluated further. A review of the WBN ETAP database, showed that four motors have a locked rotor current greater than 850% and start for an accident. An evaluation of those four loads shows that their TOL's are set at 115%. Therefore they would not be an issue, because it would increase their tolerance for tripping by an additional 15%.

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Fuse Evaluation for MCCs 120VAC CPT Circuits and 120VAC Distribution Panel Loads:
Based on the evaluation in Attachment 7, fuses for all the 120V AC CPT Circuits and 120V AC Distribution Panel Loads are considered acceptable, the fuses will carry inrush current and will not blow or melt for at least 12 seconds during a start-start scenario.

The upper boundary limit for the time delay is 11.5 seconds, which is the maximum total time allowed for loss of voltage detection and emergency diesel generator start in the WBN safety analysis as documented in the FSAR. Based on the evaluation performed in Attachment 7, it has been determined that protective devices will not trip prior to 12 seconds for start-start operation of motors at a degraded voltage at which time period disconnection from offsite power and reconnection to the emergency diesel generators occurs.

7.3 Voltage Recovery Analysis

The voltage recovery analysis shows that in all cases the voltage on the 6.9kV shutdown boards 1A, 1B, 2A and 2B recovers above the DVR reset value (operational limit of 6681V) within 4 seconds.

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8.0 Conclusions

- 8.1 This study determines that adequate starting voltage is available to each Class 1E load when the 6.9kV Shutdown Boards are at the DVR dropout setpoint (analytical limit) for the following cases:
- During a design basis event (DBE): all Class 1E loads that are automatically actuated for a safety injection signal (SI-Phase A or SI-Phase B).
 - When individually starting a motor (single motor start): all Class 1E loads, even if not SI-actuated.
- 8.2 This study shows that for a degraded voltage condition, overcurrent protective devices associated with Class 1E loads will not trip during SI-actuated motor starting and subsequent start on the emergency diesel generator.
- 8.3 The bounding voltage recovery analysis in Appendix B demonstrates that any possible voltage transient caused by DBE motor starting, including drop to the LOV setpoint, will also result in successful recovery above DVR reset within 4 seconds.
- 8.4 The outcome of the analysis in Appendix H demonstrates the adequacy of the DVR protection scheme.

Therefore, using motor starting voltage as a basis for the relay setpoint shows no impact to the DVR setpoint and/or the plant response.

Appendix A

Introduction

This appendix is a summary tabulation of the results for the various motor starting scenarios described in Section 6.0. The analyses in Appendix A were developed using the methodology and applicable inputs from References 2.2, and 2.3. Voltage values were obtained from the applicable ETAP files and output reports in this study. The key information and results are determined as follows:

A. Minimum Motor Starting Voltage

Minimum motor starting voltages are based on Attachments 1, 3 and 6 of this study. The minimum motor starting voltages used are:

6600 Volt Motors - 5280 Volts (80%)***

460 Volt Motors - 391 Volts (85%)**

460 Volt Air Compressors - 368 Volts (80%)**

89-10 MOVs - Valve thrust and torque design margin calculations/evaluations based on motor terminal voltage as documented in Attachments 4 and 5 of this study.

Non 89-10 MOVs - 368 Volts (80%)**

** Percentages are based on 460 Volt rated motor voltage. For motors rated other than 480V, the same percentages are applicable. The minimum starting voltage may be different from the above voltage if it is based on manufacturer's data or test report as documented in Attachments 3 and 6 of this study.

*** 80% for all motors except for the ERCW Pump motor which requires 90% and the Auxiliary Feedwater Pump motor which requires 85%

B. Motor Starting Evaluation Results

Individual motor starting evaluation results are tabulated for all class 1E safety-related motors and motor operated valves. As summarized in Section 6.1 of this study the following steps were performed:

1. Motor terminal voltage with Phase A loading is compared against the minimum motor starting requirements above. If acceptable voltage is obtained, no further action is required.
2. Motor terminal voltage with Phase B loading is compared against the minimum motor starting requirements above. If acceptable voltage is obtained, no further action is required.
3. Single motor start terminal voltage with Phase A loading or with Phase B loading provided the Phase B criteria in section 3.4 of this study applies is compared against the minimum motor starting requirements above. If acceptable voltage is obtained, no further action is required.

4. Individual circuit operating evaluations are performed based on when the motor is in service such as the ERCW Screen Wash Pump.
5. For 89-10 MOVs, See Section C below.

C. 89-10 Motor Operated Valve Evaluation Results

For Unit 1 and Unit 2 89-10 MOVs that did not meet the required valve motor starting voltage criteria, as a first step the calculated starting voltages for these MOVs were provided to Mechanical discipline (valve group) to evaluate if the revised voltages were acceptable. Based on the new thrust and torque calculations and calculated new design margins by mechanical valve group, the new available starting voltage for some MOVs was determined to be acceptable. However, some of the MOVs still did not meet either the required voltage or the minimum design margin criteria. Available voltage for these MOVs were re-evaluated further using the hammer-blow (HB) feature (see Section 3.5) which resulted in improved starting voltage available at the motor terminals. The available voltage with HB feature was again evaluated by the mechanical valve group and determined to be acceptable.

**Appendix A
1A Boards**

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)	SI Phase A	Terminal Voltage (%)	SI Phase B	Terminal Voltage (%)	Terminal Voltage V(%) 6.6kV/460V Base	Reference
6.9KV Shutdown Board 1A-A								
12-10 AFW	Aux Feedwater PMP 1A-A 1-MTR-3-118-A (600 HP)	99.09	Starts	99.09	Starts	99.07	85	Att. 3
12-13 CSP	CNTMT SPRAY PMP 1A-A 1-MTR-72-27-A (700 HP)	N/A	Not Running	98.80	Starts	98.79	80	Att. 3
12-14 RHR	RHR PUMP 1A-A 1-MTR-74-10-A (400 HP)	98.97	Starts	98.97	Starts	98.97	80	Att. 3
12-15 SI	SAFETY INJ PMP 1A-A 1-MTR-63-10-A (400 HP)	98.94	Starts	98.94	Starts	98.94	80	Att. 3
12-18 CCP	CNTFGL CHRNG PMP 1A-A 1-MTR-62-108-A (600 HP)	98.87	Starts	98.87	Starts	98.87	80	Att. 3
12-8 ERCW	ERCW PMP A-A 0-MTR-67-28-A (800 HP)	N/A	Starts (A-A or B-A start, but not both, other is not running)	N/A	Starts (A-A or B-A start, but not both, other is not running)	96.46	90	Att. 3
12-9 ERCW	ERCW PMP B-A 0-MTR-67-32-A (800 HP)	93.26	Starts (A-A or B-A start, but not both, other is not running)	93.26	Starts (A-A or B-A start, but not both, other is not running)	93.12	90	Same as ERCW Pmp A-A (Att. 3)
480V Shutdown Board 1A1-A								
125-3B	Comp Cooling Sys Pump 1A-A 1-MTR-70-46-A (350hp)	83.52 (8s)	Starts	84.13 (8s)	Starts	83.56	70	Att. 3
126-10C	Containment Air Rtn Fan 1A-A 1-MTR-30-38-A (100hp)	N/A	Not Running Starts @ 9 Min)	N/A	Not Running Starts @ 9 Min)	80.97 (SIB)	80	Att. 6
126-7C	Reac Lwr Compt Clr Fan 1A-A 1-MTR-30-74-A (60hp)	N/A	Running	N/A	Trips	81.73	80	Att. 3
126-9C	Elec Bd Rm AHU A-A 0-MTR-31-30B-A (50hp)	N/A	Running	N/A	Running	83.82	80	Att. 6
126-7A	Spent Fuel Pit Pump C-S 0-MTR-78-35-S (100hp)	N/A	Running	N/A	Running	80.77	80	Att. 6
480V Shutdown Board 1A2-A								
127-2C	Control Rm A/C A-A Compressor 0-MTR-31-80/2-A (250hp)	N/A	Running	N/A	Running	90.08	80	Att. 1
127-3B	Comp Cooling Sys Pump C-S 0-MTR-70-51-S (350hp)	81.61 (8s)	Starts	82.07 (8s)	Starts	80.61	70	Att. 3
128-7D	Reac Lwr Compt Clr Fan 1C-A 1-MTR-30-77-A (60hp)	N/A	Running	N/A	Trips	81.25	80	Att. 3
128-9D	480V SD Bd Rm AHU A-A 0-MTR-31-45-A (75hp)	N/A	Running	N/A	Running	87.36	85	Att. 1
480V C&A Vent Board 1A1-A								
203-12B	Cont Bldg Emerg Press Fan A-A 0-MTR-31-6-A (1hp)	85.89	Starts	87.23	Starts	87.60	85	Att. 1
203-13D	ERCW Scrn Wash Pump 1A-A 1-MTR-67-431-A (40hp)	N/A	N/A	N/A	N/A	73.63	75	Att. 3 See Sec. 7.1 for Justification

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**Appendix A
1A Boards**

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)	SI Phase A	Terminal Voltage (%)	SI Phase B	Terminal Voltage (%)	Terminal Voltage V(%) 6.6kV/460V Base	Reference
		6.6kV / 460V Base		6.6kV / 460V Base		6.6kV /460V Base		
203-2A	Cont Bldg Emerg Air CU Fan A-A 0-MTR-31-8-A (10hp)	86.39	Starts	87.73	Starts	89.23	85	Att. 1
203-3C	Cntrmt Spray Pump 1A-A Clr Fan 1-MTR-30-177-A (7.5hp)	N/A	Running	81.87	Starts	83.18	80	Att. 3
203-4D	Emerg Gas Trtmt Sys Fan A-A 0-MTR-65-23-A (20hp)	87.24	Starts	88.59	Starts	90.95	75	Att. 3
203-6B	ERCW Str 1A-A 1-MTR-67-9-A (3hp)	N/A	Running	N/A	Running	76.43	75	Att. 3
203-10A	Cntfg Chrg Pmp 1A-A Rm Clr Fan, 1-MTR-30-183-A, (5 HP)	84.47	Starts	85.79	Starts	86.76	80	Att. 3
203-10B	PEN RM EL 713 CLR FAN 1A-A, 1-MTR-30-196-A, (3HP)	86.68	Starts	88.03	Starts	90.30	80	Att. 3
203-10C	Pipe Chase Clr Fan 1A-A, 1-MTR-30-201-A, (3 HP)	85.43	Starts	86.76	Starts	88.55	80	Att. 3
203-11A	480V BD RM 1B PR SUP FAN 1B1-A 1-MTR-31-478-A, (3HP)	N/A	N/A	N/A	N/A	92.18	85	Att. 1
203-11C	480V Bd Rm 1A A/C Ahu 1A-A 1-MTR-31-461-A (15 HP)	N/A	N/A	N/A	N/A	90.06	85	Att. 1
203-11D	Cont Rm Ahu A-A 0-MTR-31-12-A (60 HP)	N/A	N/A	N/A	N/A	88.19	85	Att. 1
203-12A	125V Vtl Bat Rm II ExhFan 1B1-A 1-MTR-31-285-A (0.33 HP)	N/A	N/A	N/A	N/A	91.18	85	Att. 1
203-12C	480V Bd Rm 1A A/C Cond 1A-A 1-MTR-31-290-A, (15 HP)	N/A	N/A	N/A	N/A	90.76	85	Att. 1
203-12F1	Cntrmt Purge Air Radn Exh Mon 1-RE-90-130-A, (0.75 HP)	N/A	N/A	N/A	N/A	92.73	85	Att. 1
203-2C	PEN RM EL 692 CLR FAN 1A-A 1-MTR-30-186-A, (3HP)	86.13	Starts	87.47	Starts	90.42	80	Att. 3
203-4A	Btry Rm El 692 Exh Fan A-A 0-MTR-31-28-A (1.5HP)	N/A	N/A	N/A	N/A	88.45	85	Att. 1
203-4B	5TH VITL BATT.RM.EX. FAN 1B1-A 0-MTR-31-493B-A (0.25 HP)	N/A	N/A	N/A	N/A	94.40	85	Att. 1
203-5A	SFP Pmp A-A&TB Bst Pm SpClrFan 0-MTR-30-192-A (7.5HP)	86.00	Starts	87.34	Starts	89.67	80	Att. 3
203-5E	CCS & AFW PMPs SP CLR FAN A-A 1-MTR-30-190-A (20HP)	87.31	Starts	88.66	Starts	90.70	80	Att. 3
203-6A	Shutdown Bd Rm A Press Fan A-A 0-MTR-31-64-A (3HP)	N/A	N/A	N/A	N/A	92.71	85	Att. 1
203-6C	Traveling Scrn 1A-A 1-MTR-67-434-A (5HP)	N/A	N/A	N/A	N/A	80.36	80	Att. 3
203-6F1	Cntrmt Bldg Lwr Compt Air Mon 1-RE-90-106-A (3HP)	N/A	N/A	N/A	N/A	92.68	85	Att. 1
203-7B	125V Vtl Bat Rm I ExhFan 1A1-A 1-MTR-31-287-A (0.33HP)	N/A	N/A	N/A	N/A	91.40	85	Att. 1
203-8A	Safety Inj Pmp 1A-A Rm Clr Fan 1-MTR-30-180-A (5HP)	83.34	Starts	84.63	Starts	85.19	80	Att. 3
203-8B	Pen Rm El 737 Clr Fan 1A-A 1-MTR-30-194-A (3HP)	88.04	Starts	89.41	Starts	92.28	80	Att. 3
203-8C	480V Xfmr Rm 1A Exh Fan 1A2-A 1-MTR-30-244G-A (3HP)	N/A	N/A	N/A	N/A	89.57	80	Att. 3

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Appendix A
1A Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)	SI Phase A	Terminal Voltage (%)	SI Phase B	Terminal Voltage (%)	Terminal Voltage V(%)	Reference
		6.6kV / 460V Base		6.6kV / 460V Base		6.6kV / 460V Base	6.6kV/460V Base	
203-8D	480V Xfmr Rm 1A Exh Fan 1A3-A 1-MTR-30-244H-A (3HP)	N/A	N/A	N/A	N/A	91.34	80	Att. 3
203-8F1	CONT RM A/C A-A CONTROL/O.PMP 0-MTR-31-80/3-A (3.11 HP)	N/A	N/A	N/A	N/A	92.86	85	Att. 1
203-9A	RHR Pmp 1A-A Rm Clr Fan 1-MTR-30-175-A (5HP)	82.51	Starts	83.79	Starts	84.25	80	Att. 3
203-9B	Cont Rm A/C Circ Pmp A-A 0-MTR-31-80/1-A (15HP)	N/A	N/A	N/A	N/A	89.07	85	Att. 1
203-9C	480V Bd Rm 1A Pr Sup Fan 1A1-A 1-MTR-31-462-A (3HP)	N/A	N/A	N/A	N/A	92.92	85	Att. 1
203-9D	480V Xfmr Rm 1A Exh Fan 1A1-A 1-MTR-30-244F-A (3HP)	N/A	N/A	N/A	N/A	89.49	80	Att. 3
203-9F1	Cont Rm Intake Mon 0-RE-90-205-A (0.75HP)	N/A	N/A	N/A	N/A	93.17	85	Att. 1
203-4E	ERCW Str 1A-A Backwash Vlv 1-FCV-67-9A-A (0.33HP)	N/A	N/A	N/A	N/A	82.02	80	Att. 1
203-6E	ERCW Str 1A-A Flush Vlv 1-FCV-67-9B-A (0.33HP)	N/A	N/A	N/A	N/A	82.70	80	Att. 1
203-7D	RHR PMP 1A-A INLET FCV 1-FCV-74-3-A (5.2HP)	N/A	N/A	N/A	N/A	91.31	Pass	Att. 4 / Acceptable Margin
203-7E	RWST TO SPRAY HDR 1A FCV 1-FCV-72-22-A (3.2HP)	N/A	N/A	N/A	N/A	86.27	Pass	Att. 4 / Acceptable Margin
480V C&A Vent Board 1A2-A								
None								
480V Diesel Aux Board 1A1-A								
217-2B	DG 1A-A Rm Exh Fan 1-A 1-MTR-30-447-A (15hp)	91.83	Starts	92.48	Starts	92.64	85	Att. 1
217-3D	DG 1A-A Day Tk FO XFR PMP 1 1-MTR-18-55/1-A (1hp)	91.77	Random	92.43	Random	94.74	85	Att. 1
217-4B	DG 1A-A AUX LUBEOIL CIRC PMP A 1-MTR-82-AOPA1A (0.75hp)	92.10	Random	92.75	Random	94.57	85	Att. 1
217-4D	Dg Rm 1A-A Pnl Vent Fan 1-MTR-30-491-A (15HP)	N/A	N/A	N/A	N/A	92.14	85	Att. 1
217-4E	Dg 1A-A 480V Elec Bd Rm Ex Fan 1-MTR-30-459-A (2HP)	91.95	N/A	92.60	N/A	94.29	85	Att. 1
217-3A	EM DG HX 1A1 & 1A2 SPLY VLV 1-FCV-67-66-A (0.13HP)	82.50	N/A	83.08	N/A	85.85	Pass	Att. 5
217-6A	DG 1A-A Muffler Rm Exh Fan 1-MTR-30-463 (0.5hp)	91.88	Starts	92.54	Running	95.01	85	Att. 1
480V Diesel Aux Board 1A2-A								
218-2B	DG 1A-A Rm Exh Fan 2-A 1-MTR-30-451-A (15hp)	92.40	Starts	92.86	Running/ Starts	92.94	85	Att. 1
218-3D	DG 1A-A DAY TNK FO XFR PMP 2 1-MTR-18-54/1-A (1hp)	91.63	Random	92.08	Random	93.94	85	Att. 1
218-2A	DG 1A-A AUX LUBEOIL CIRC PMP B 1-MTR-82-AOPB1A (0.75HP)	N/A	N/A	N/A	N/A	93.76	85	Att. 1
218-2D	Dg 1A-A Lube Oil Circ Pmp 2 1-MTR-82-A2-A (1HP)	N/A	N/A	N/A	N/A	93.46	85	Att. 1
218-5F1	Dg Bldg Co2 Refrigeration Unit 0-PKG-39-37 (2HP)	N/A	N/A	N/A	N/A	94.53	85	Att. 1

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Appendix A
1A Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)	SI Phase A	Terminal Voltage (%)	SI Phase B	Terminal Voltage (%)	Terminal Voltage V(%)	Reference
		6.6kV / 460V Base		6.6kV / 460V Base		6.6kV /460V Base	6.6kV/460V Base	
480V RMOV Board 1A1-A								
235-5C	Lower CNTMT 1B CLRS ISLN VLV 1-FCV-67-97-A (0.13hp)	N/A	Not Running	81.71	Starts	85.11	Pass	Att. 4
235-7A	Seal Flow Ret Isln Vlv 1-FCV-62-63-A (1.9hp)	78.93	Closes on Ph A (Starts)	80.15	Closes on Ph B (Starts)	83.38	Pass	Att. 4
235-7B	CHARGING FLOW ISLN VLV 1-FCV-62-90-A (1.9hp)	85.86	Closes on SI (Starts)	87.20	Closes on SI (Starts)	90.69	Pass	Att. 4
235-8B	Vol Cont Tank Outlet Isln Vlv 1-LCV-62-132-A (1.9hp)	80.54	Closes on SI (Starts)	81.79	Closes on SI (Starts)	85.08	Pass	Att. 4
235-9A	RWST To Charging Pmp Vlv Cont 1-LCV-62-135-A (1.9hp)	83.79	Opens on SI (Starts)	85.09	Opens on SI (Starts)	88.51	Pass	Att. 4
235-9D	RCP Oil Lir Cntmt Iso Vlv 1-FCV-70-100 (0.13hp)	N/A	Not Running	81.60	Closes (Starts)	84.97	Pass	Att. 4
235-11A	SIS Pmp Inlet to CVCS Chrg Pmp 1-FCV-63-7 (1.9hp)	N/A	Not Running	N/A	Not Running	88.21*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
235-11D	SIS Boron Inj Tank Shutoff Vlv 1-FCV-63-26 (1.9hp)	86.95	Opens on SI (Starts)	88.30	Opens on SI (Starts)	91.83	Pass	Att. 4
235-12B	Cntmt Sump To RHR Pmp A-A 1-FCV-63-72-A (13hp)	N/A	Operate about 20 minutes after SI	N/A	Operate about 20 minutes after SI	86.95	Pass	Att. 4 / Acceptable Margin
235-13E	Cntmt Spray Hdr 1A Isln Vlv 1-FCV-72-39-A (3.2hp)	N/A	Not Running	89.45 (5s)	Opens on Ph B (Starts)	91.80*	Pass	Att. 4 (5 sec after SI) - Time Delay added per DCN 52834
235-14D	RHR Pmp 1A-A Min Flow Vlv 1-FCV-74-12-A (0.13hp)	80.60	Random	81.86	Random	85.24	Pass	Att. 4
235-15D	LWR CNTMT 1D CLRS ISLN VLV 1-FCV-67-89-A (0.13hp)	N/A	Not Running	81.83	Closes (Starts)	85.21	Pass	Att. 4
235-17B	Cntmt Standpipe Isln Vlv 1-FCV-26-240-A (0.67hp)	82.41	Close (Start)	83.69	Close (Start)	87.08	Pass	Att. 4
235-18E	RCP Spray Isln Vlv 1-FCV-26-243-A (0.67hp)	83.68	Close (Start)	84.98	Close (Start)	88.42	Pass	Att. 4
235-2E1	RWST To RHR Pmp Flow Cont Vlv 1-FCV-63-1-A (5.2HP)	N/A	N/A	N/A	N/A	92.09*	Pass	Att. 4
235-5B	RHR Sys Isln Vlv 1-FCV-74-1-A (2.6HP)	N/A	N/A	N/A	N/A	90.74*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
235-6D	RCS Press Relief FCV 1-FCV-68-333-A (1.9HP)	N/A	N/A	N/A	N/A	89.2*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
235-10B	SIS Pmp Recirc To RWST 1-FCV-63-3-A (0.7HP)	N/A	N/A	N/A	N/A	90.70*	Pass	Att. 4

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Appendix A
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EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)	SI Phase A	Terminal Voltage (%)	SI Phase B	Terminal Voltage (%)	Terminal Voltage V(%)	Reference
		6.6kV / 460V Base		6.6kV / 460V Base		6.6kV /460V Base	6.6kV/460V Base	
235-10F	Cont Spray Pmp 1A-A Recirc FCV 1-FCV-72-34-A (0.13HP)	N/A	N/A	N/A	N/A	89.39*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
235-11B	RHR Hx A To CVCS Chrg Pmp 1-FCV-63-8-A (1.9HP)	N/A	N/A	N/A	N/A	87.56	Pass	Att. 4 / Acceptable Margin
235-12A	SIS Pmp 1A-A Inlet Vlv 1-FCV-63-47-A (1.9HP)	N/A	N/A	N/A	N/A	88.18*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
235-12D	SIS To RCS Loops 2&3 FCV 1-FCV-63-93-A (1.6 HP)	N/A	N/A	N/A	N/A	90.73	Pass	Att. 4 / Acceptable Margin
235-12E	SIS Pmp 1A-A Outlet FCV 1-FCV-63-152-A (1.9HP)	N/A	N/A	N/A	N/A	88.48*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
235-13A	SIS Pmp Out RCS Lp 1&3 Hot Leg 1-FCV-63-156-A (1.9HP)	N/A	N/A	N/A	N/A	89.28*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
235-13B	Cntmt Sump To Spray Hdr 1A FCV 1-FCV-72-44-A (3.2HP)	N/A	N/A	N/A	N/A	90.33*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
235-14A	RHR Spray Hdr 1A Isln Vlv 1-FCV-72-40-A (1.9HP)	N/A	N/A	N/A	N/A	87.74	Pass	Att. 4 / Acceptable Margin
235-14E	RHR Hx 1A Bypass Vlv 1-FCV-74-33-A (2HP)	N/A	N/A	N/A	N/A	85.35	Pass	Att. 4 / Acceptable Margin
235-4E	AFW Pmp A-A Lube Oil Pmp A-A 1-MTR-3-118D-A (0.25HP)	N/A	Manual	N/A	Manual	89.80	85	Att. 1
480V RMOV Board 1A2-A								
236-17E	480V Bd Rm 1A A/C Compressor 1A-1 1-MTR-31-465-A (50hp)	N/A	Running	N/A	Running	91.94	85	Att. 1
236-2A	ERCW Hdr A Isln Vlv 1-FCV-3-116 (0.25hp)	N/A	Random	N/A	Random	84.14	Pass	Att. 4
236-3A	ERCW Hdr A Isln Vlv 1-FCV-3-136 (0.33hp)	N/A	Random	N/A	Random	84.72	Pass	Att. 4
236-3D	St Gen No 1 FW Isln Vlv 1-FCV-3-33-A (39.4hp)	81.97	Use 89-10 starts	82.77	Use 89-10 starts	82.79	Pass	Att. 4
236-4D	St Gen No 3 FW Isln Vlv 1-FCV-3-87 (39.4hp)	79.85	Use 89-10 starts	80.63	Use 89-10 starts	80.80	Pass	Att. 4
236-7D	Lwr Cntmt Clr 1A Disch Iso Vlv 1-FCV-67-87-A (0.13hp)	N/A	Not Running	84.74	Closes (Starts)	86.85	Pass	Att. 4
236-7F	Upr Cntm Vt Clr 1A Sup Iso Vlv 1-FCV-67-130-A (0.13hp)	N/A	Not Running	82.36	Closes (Starts)	84.42	Pass	Att. 1
236-8B	Lwr Cntmt 1A Clr Sply Isln Vlv 1-FCV-67-107-A (0.33hp)	N/A	Not Running	85.38	Closes (Starts)	87.49	Pass	Att. 4

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EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)	SI Phase A	Terminal Voltage (%)	SI Phase B	Terminal Voltage (%)	Terminal Voltage V(%)	Reference
		6.6kV / 460V Base		6.6kV / 460V Base		6.6kV /460V Base	6.6kV/460V Base	
236-8D	Lwr Cntmt 1C Clr Disch Iso Vlv 1-FCV-67-95-A (0.13hp)	N/A	Not Running	84.49	Closes (Starts)	86.59	Pass	Att. 4
236-8F	Upr Cntm Vt Clr 1C Sup Iso Vlv 1-FCV-67-133-A (0.13hp)	N/A	Not Running	81.29	Closes (Starts)	83.32	Pass	Att. 1
236-9A	Lwr Cntmt 1C Clr Sply Isln Vlv 1-FCV-67-99-A (0.33hp)	N/A	Not Running	85.07	Closes (Starts)	87.17	Pass	Att. 4
236-9B	Lwr CNTMT 1B CLR DISCH ISO VLV 1-FCV-67-104-A (0.33hp)	N/A	Not Running	85.41	Closes (Starts)	87.53	Pass	Att. 4
236-9D	Up Cntmt VT Clr 1A Disc Iso Vlv 1-FCV-67-295 (0.13hp)	N/A	Not Running	79.88	Closes (Starts)	81.87	Pass	Att. 4 / Acceptable Margin
236-9F	Upr Cntm Vt Clr 1B Sup Iso Vlv 1-FCV-67-139-A (0.13hp)	N/A	Not Running	81.29	Closes (Starts)	83.32	Pass	Att. 1
236-10A	Lwr Cntmt 1D Clr Disch Iso Vlv 1-FCV-67-112-A (0.33hp)	N/A	Not Running	85.46	Closes (Starts)	87.58	Pass	Att. 4
236-10D	UP CNTM VT CLR 1C DISH ISO VLV 1-FCV-67-296-A (0.13hp)	N/A	Not Running	81.33	Closes (Starts)	83.36	Pass	Att. 1
236-10F	UP CNTM VT CLR 1D DISH ISO VLV 1-FCV-67-142-A (0.13hp)	N/A	Not Running	82.36	Closes (Starts)	84.42	Pass	Att. 1
236-11D	RCP Thrn Barr Rtn Cntm Iso Vlv 1-FCV-70-90-A (0.7hp)	N/A	Not Running	86.05	Closes (Starts)	88.16	Pass	Att. 4
236-11E	RCP Thrn Barr Cntmt Isln Vlv 1-FCV-70-133-A (0.13hp)	N/A	Not Running	83.85	Closes (Starts)	85.94	Pass	Att. 4
236-12D	RCP Oil Clr Rtn Cntmt Isln Vlv 1-FCV-70-92-A (0.13hp)	N/A	Not Running	85.13	Closes (Starts)	87.25	Pass	Att. 4
236-16D	Excs Ltdn Hx Cont Inlt Iso Vlv 1-FCV-70-143-A (0.33hp)	83.86	Closes on Phase A	84.68	Closes on Phase A	86.78	Pass	Att. 4
236-2B	ERCW Hdr A Isln Vlv 1-FCV-3-116B-A (0.25HP)	N/A	N/A	N/A	N/A	84.13	Pass	Att. 4
236-2D	AFWP Turb Stm Sup Fm Stm Gen 1 1-FCV-1-15-A (1HP)	N/A	N/A	N/A	N/A	92.47*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
236-2E	St Flow To AFWP Turb Isln Vlv 1-FCV-1-17-A (1HP)	N/A	N/A	N/A	N/A	89.46	Pass	Att. 4
236-3B	ERCW Hdr A Isln Vlv 1-FCV-3-136B-A (0.33HP)	N/A	N/A	N/A	N/A	84.72	Pass	Att. 4
236-5A	Sample Hx Isln Vlv 1-FCV-70-215-A (0.13HP)	N/A	N/A	N/A	N/A	86.73	Pass	Att. 1
236-5E	Cntmt Spray Hx 1A Sup Cont Vlv 1-FCV-67-125-A (0.33HP)	N/A	N/A	N/A	N/A	92.51*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
236-5F	Cntmt Spray Hx 1A Disch Vlv 1-FCV-67-126-A (0.33HP)	N/A	N/A	N/A	N/A	92.19*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *

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**Appendix A
1A Boards**

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)	SI Phase A	Terminal Voltage (%)	SI Phase B	Terminal Voltage (%)	Terminal Voltage V(%)	Reference
		6.6kV / 460V Base		6.6kV / 460V Base		6.6kV /460V Base	6.6kV/460V Base	
236-6A	AFWP Turb St Sply Frm St gen 4 1-FCV-1-16-A (1HP)	N/A	N/A	N/A	N/A	92.52*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
236-6D	RHR Sys Isln Bypass Vlv 1-FCV-74-8-A (1.6HP)	N/A	N/A	N/A	N/A	90.99*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
236-11A	Cmpnt Clg Hx A Disch Cont Vlv 1-FCV-67-146-A (0.3HP)	N/A	N/A	N/A	N/A	88.07	Pass	Att. 4 / Acceptable Margin
236-12B	SS&Con AirCpsr Sup Hdr A Iso V 0-FCV-67-205-A (0.33HP)	N/A	N/A	N/A	N/A	87.86	Pass	Att. 4 / Acceptable Margin
236-15A	CCS HX A ERCW BYPASS FCV 1-FCV-67-143-A (0.13HP)	N/A	N/A	N/A	N/A	84.62	Pass	Att.4
236-16E	RHR Hx A-A Outlet Vlv 1-FCV-70-156-A (0.33HP)	N/A	N/A	N/A	N/A	88.86	Pass	Att. 4 / Acceptable Margin
236-17A	Sample Hx Hdr Outlet Vlv 1-FCV-70-183-A (0.13HP)	N/A	N/A	N/A	N/A	86.09	Pass	Att. 4
236-17B	SFPCS Hx Sply Hdr Isln Vlv 0-FCV-70-197-A (0.3HP)	N/A	N/A	N/A	N/A	89.74	Pass	Att. 4 / Acceptable Margin
480V Reac Vent Board 1A-A								
None								

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Appendix A
1B Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)	SI Phase A	Terminal Voltage (%)	SI Phase B	Terminal Voltage (%)	Terminal Voltage V(%)	Reference
		6.6kV / 460V Base		6.6kV / 460V Base		6.6kV / 460V Base	6.6kV / 460V Base	
6.9kV Shutdown Board 1B-B								
13-10 AFW	Aux Feedwater PMP 1B-B 1-MTR-3-128-B (600 HP)	99.01	Starts	99.01	Starts	98.98	85	Att. 3
13-13 CSP	CNTWMT SPRAY PMP 1B-B 1-MTR-72-10-B (700 HP)	N/A	Not Running	98.70	Start	98.69	80	Att. 3
13-14 RHR	RHR PUMP 1B-B 1-MTR-74-20-B (400 HP)	99.12	Starts	99.12	Starts	99.12	80	Att. 3
13-15 SI	SAFETY INJ PMP 1B-B 1-MTR-63-15-B (400 HP)	98.85	Starts	98.85	Starts	98.84	80	Att. 3
13-18 CCP	CNTFGL CHRGR PMP 1B-B 1-MTR-62-104-B (600 HP)	98.78	Starts	98.78	Starts	98.78	80	Att. 3
13-8 ERCW	ERCW PMP F-B 0-MTR-67-51-B (800 HP)	N/A	Starts (F-B or E-B start, but not both, other is not running)	N/A	Starts (F-B or E-B start, but not both, other is not running)	96.20	90	Att. 3
13-9 ERCW	ERCW PMP E-B 0-MTR-67-47-B (800 HP)	95.10	Starts (E-B or F-Bstart, but not both, other is not running)	95.10	Starts (E-B or F-Bstart, but not both, other is not running)	95.01	90	Same as ERCW Pmp F-B (Att. 3)
480V Shutdown Board 1B1-B								
129-3C	Comp Cooling Sys Pump 1B-B 1-MTR-70-38-B (350hp)	80.89 (8s)	Starts	81.53 (8s)	Starts	80.63	70	Att. 3
130-7A	Elec Bd Rm AHU C-B 0-MTR-31-31B-B (50hp)	N/A	Running	N/A	Running	90.28	80	Att. 6
130-7D	Reac Lwr Compt Cfr Fan 1B-B 1-MTR-30-75-B (60hp)	N/A	Running	N/A	Trips	82.24	80	Att. 3
480V Shutdown Board 1B2-B								
131-2B	Control Rm A/C B-B Compressor 0-MTR-31-96/2-B (250hp)	N/A	Running	N/A	Running	83.25	80	Att. 1
131-3C	SHDN BD RM CHLR PKG B-B Compressor 0-MTR-31-49/2-B (240hp)	N/A	Running	N/A	Running	87.92	85	Att. 1
132-7D	Reac Lwr Compt Cfr Fan 1D-B 1-MTR-30-78-B (60hp)	N/A	Running	N/A	Trips	82.33	80	Att. 3
132-9A	Spent Fuel Pit Pmp B-B 0-MTR-78-9-B (100hp)	N/A	Running	N/A	Running	83.47	80	Att. 6
132-9C	Cntmt Air Rtn Fan 1B-B 1-MTR-30-39-B (100hp)	N/A	Not Running Starts @ 9 Min)	N/A	Not Running Starts @ 9 Min)	80.27 (SIB)	80	Att. 6
132-9D	480V SD Bd Rm AHU C-B 0-MTR-31-55-B (75hp)	N/A	Running	N/A	Running	86.74	85	Att. 1
480V C&A Vent Board 1B1-B								
205-11A	Cont Bldg Emerg Press Fan B-B, 0-MTR-31-5-B (1hp)	89.06	Starts	90.34	Starts	91.38	85	Att. 1
205-13D	ERCW Scrn Wash Pump 1B-B 1-MTR-67-440-B (40hp)	N/A	N/A	N/A	N/A	73.47 (SIB)	75	Att. 3 See Sec. 7.1 for Justification

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Appendix A
1B Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
		SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%)	
ETAP Bus ID/ Compt No	Load Description	6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base	Reference
205-2A	Cont Bldg Em Air Clnup Fan B-B 0-MTR-31-7-B (10hp)	87.77	Starts	89.03	Starts	89.81	85	Att. 1
205-3C	Cntmt Spray Pump 1B-B Rm Clr Fan 1-MTR-30-178-B (7.5hp)	N/A	Random	87.96	Starts	89.52	80	Att. 3
205-4D	Emerg Gas Trmt Sys Fan B-B 0-MTR-65-42-B (20hp)	86.53	Starts	87.78	Starts	88.81	80	Att. 3
205-6B	ERCW Str 1B-B 1-MTR-67-10-B (3hp)	N/A	Running	N/A	Running	76.88	75	Att. 3
205-7E	RWST to Spray Hdr 1A Vlv 1-FCV-72-22 (3.2hp)	N/A	Stopped (No auto Start)	N/A	Stopped (No auto Start)	88.14 (SIB)	Pass	Att. 4 / Acceptable Margin
205-4E	ERCW Str 1B-B Backwash Vlv 1-FCV-67-10A-B (0.33HP)	N/A	N/A	N/A	N/A	82.31	80	Att. 1
205-6E	ERCW Str 1B-B Flush Vlv 1-FCV-67-10B-B (0.33HP)	N/A	N/A	N/A	N/A	82.32	80	Att. 1
205-7D	RHR PMP 1B-B INLET FCV 1-FCV-74-21-B (5.2HP)	N/A	N/A	N/A	N/A	91.09	Pass	Att. 4 / Acceptable Margin
205-2C	Pen Rm El 713 Clr Fan 1B-B 1-MTR-30-197-B (3HP)	87.64	Starts	88.90	Starts	90.90	80	Att. 3
205-3A	Shtdn Bd Rm Chlr CW Cir Pmp B-B 0-MTR-31-49/1-B (25HP)	N/A	N/A	N/A	N/A	90.61	85	Att. 1
205-3B	Pipe Chase Clr Fan 1B-B 1-MTR-30-202-B (3HP)	86.47	Starts	87.72	Starts	89.20	80	Att. 3
205-3F1	Cntmt Bldg Upper Compt Air Mon 1-RE-90-112-B (3HP)	N/A	N/A	N/A	N/A	89.78	85	Att. 1
205-4A	Battery Rm El 692 Exh Fan B-B 0-MTR-31-29-B (1.5HP)	N/A	N/A	N/A	N/A	87.82	85	Att. 1
205-4F1	CNTMT PURGE AIR EXH MON 1-RE-90-131-B (0.75HP)	N/A	N/A	N/A	N/A	92.86	85	Att. 1
205-5A	SFP PmpB-B&TB Bst Pmp SpClrFan 0-MTR-30-193-B (7.5HP)	86.27	Starts	87.51	Starts	88.78	80	Att. 3
205-5E	CCS & AFW Pumps Sp Clr Fan B-B 1-MTR-30-191-B (20HP)	86.59	Starts	87.83	Starts	88.44	80	Att. 3
205-6A	SHUTDOWN BD RM A PRESS FAN C-B 0-MTR-31-67-B (3HP)	N/A	N/A	N/A	N/A	91.61	85	Att. 1
205-6C	Traveling Scrn 1B-B 1-MTR-67-445-B (5HP)	N/A	N/A	N/A	N/A	80.61 (SIB)	80	Att.3
205-7B	125V Vtl Bat Rm I Ex Fan 1A2-B 1-MTR-31-288-B (0.33HP)	N/A	N/A	N/A	N/A	91.17	85	Att. 1
205-7C	High Press Fire Pmp Str B-B 0-MTR-26-14-B (0.75HP)	N/A	N/A	N/A	N/A	86.83	85	Att. 1
205-8A	Safety Inj Pmp 1B-B Rm Clr Fan 1-MTR-30-179-B (5HP)	N/A	N/A	N/A	N/A	86.06	80	Att.3
205-8B	Pen Rm El 692 Clr Fan 1B-B 1-MTR-30-187-B (3HP)	N/A	N/A	N/A	N/A	89.52	80	Att.3
205-8C	Shtdn Xfmr Rm 1B Exh Fan 1B2-B 1-MTR-30-248F-B (3HP)	N/A	N/A	N/A	N/A	89.94	80	Att.3
205-8D	Shtdn Xfmr Rm 1B Exh Fan 1B3- 1-MTR-30-248G-B (3HP)	N/A	N/A	N/A	N/A	89.89	80	Att.3

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**Appendix A
1B Boards**

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No		SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start Terminal Voltage (%)	Minimum Required Voltage Terminal Voltage V(%) 6.6kV / 460V Base	Bases for Minimum Required Voltage Reference
		Terminal Voltage (%)		Terminal Voltage (%)				
Load Description		6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base		
205-8E	Cont Rm A/C Cir Pmp B-B 0-MTR-31-96/1-B (15HP)	N/A	N/A	N/A	N/A	85.40	85	Att. 1
205-8F1	CONT RM A/C B-B CONTROL/O.PMP 0-MTR-31-96/3-B (3HP)	N/A	N/A	N/A	N/A	91.69	85	Att. 1
205-9A	RHR Pmp 1B-B Rm Clr Fan 1-MTR-30-176-B (5HP)	83.13	Starts	84.33	Starts	83.45	80	Att.3
205-9B	5th Vitl Batt Rm Exh Fan 1B2-B 0-MTR-31-496B-B (0.25HP)	N/A	N/A	N/A	N/A	93.69	85	Att. 1
205-9C	480V Bd Rm 1A Pr Sup Fan 1A2-B 1-MTR-31-463-B (3HP)	N/A	N/A	N/A	N/A	92.36	85	Att. 1
205-9D	Shtdn Xfmr Rm 1B Exh Fan 1B1-B 1-MTR-30-248E-B (3HP)	N/A	N/A	N/A	N/A	87.59	80	Att.3
205-9E	Pen Rm El 737 Clr Fan 1B-B 1-MTR-30-195-B (3HP)	87.45	Starts	88.71	Starts	89.63	80	Att.3
205-10A	Cntfg Chrg Pmp 1B-B Rm Clr Fan 1-MTR-30-182-B (5HP)	84.65	Starts	85.87	Starts	85.42	80	Att.3
205-10B	480V Bd Rm 1B Pr Sup Fan 1B2-B 1-MTR-31-477-B (3HP)	N/A	N/A	N/A	N/A	92.22	85	Att. 1
205-10C	125V VTL BAT RM II EXFAN 1B2-B 1-MTR-31-286-B (0.33HP)	N/A	N/A	N/A	N/A	91.01	85	Att. 1
205-10F1	Cont Rm Intake Mon 0-RE-90-206-B (0.75HP)	N/A	N/A	N/A	N/A	89.58	85	Att. 1
205-11B	480V Bd Rm 1B A/C Ahu 1B-B 1-MTR-31-475-B (20HP)	N/A	N/A	N/A	N/A	89.39	85	Att. 1
205-11C	480V Bd Rm 1B A/C Cond 1B-B 1-MTR-31-289-B (20HP)	N/A	N/A	N/A	N/A	91.40	85	Att. 1
205-11D	Cont Rm Ahu B-B 0-MTR-31-11-B (60HP)	N/A	N/A	N/A	N/A	87.63	85	Att. 1
480V C&A Vent Board 1B2-B								
None								
480V Diesel Aux Board 1B1-B								
219-2B	DG 1B-B RM EXH FAN 1-B 1-MTR-30-449-B (15hp)	90.80	Starts	91.41	Start	91.42	85	Att. 1
219-3D	DG 1B-B DAY TNK FO XFR PMP 1 1-MTR-18-55/2-B (1hp)	90.85	Random	91.46	Random	93.65	85	Att. 1
219-4B	Dg 1B-B Aux LubeOil Circ Pmp A 1-MTR-82-AOPA2B (0.75hp)	91.49	Starts	92.11	Starts	93.89	85	Att. 1
219-6A	DG 1B-B Muffler Rm Exh Fan 1-MTR-30-465 (0.5hp)	91.27	Starts	91.88	Starts	94.31	85	Att. 1
219-2D	Dg 1B-B Lube Oil Circ Pmp 1 1-MTR-82-B1-B (1HP)	N/A	N/A	N/A	N/A	93.79	85	Att. 1
219-4E	DG 1B-B 480V ELEC BD RM EX FAN 1-MTR-30-461-B (2HP)	N/A	N/A	N/A	N/A	93.52	85	Att. 1
480V Diesel Aux Board 1B2-B								
220-2B	DG 1B-B Rm Exh Fan 2-B 1-MTR-30-453-B (15hp)	91.32	Starts	91.79	Starts	92.60	85	Att. 1
220-3D	DG 1B-B DAY TNK FO XFR PMP 2 1-MTR-18-54/2-B (1HP)	91.14	Starts	91.60	Starts	94.85	85	Att. 1
220-2A	Dg 1B-B Aux LubeOil Circ Pmp B 1-MTR-82-AOPB2B (0.75HP)	N/A	N/A	N/A	N/A	94.33	85	Att. 1

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Appendix A
1B Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
		SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%)	
ETAP Bus ID/ Compt No	Load Description	6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base	Reference
220-2D	Dg 1B-B Lube Oil Circ Pmp 2 1-MTR-82-82-B (1HP)	N/A	N/A	N/A	N/A	94.71	85	Att. 1
480V RMOV Board 1B1-B								
237-3F2	SIS ACCUM TANK FLOW ISOL VLV 1-FCV-63-98-B (6.6hp)	91.28	Opens on SI (Starts)	92.56	Opens on SI (Starts)	94.86	Pass	Att. 1
237-6D	Seal Flow Ret Isln Vlv 1-FCV-62-61-B (1.9hp)	81.68	Closes on Ph A (Starts)	82.82	Closes on Ph B (Starts)	85.18	Pass	Att. 4
237-7A	CHRG FLOW ISLN VLV 1-FCV-62-91-B (1.9hp)	86.42	Closes on SI (Starts)	87.63	Closes on SI (Starts)	90.11	Pass	Att. 4
237-8A	Vol Cont Tank Outlet Isln Vlv 1-LCV-62-133-B (1.9hp)	81.82	Closes on SI (Starts)	82.97	Closes on SI (Starts)	85.33	Pass	Att. 4
237-8B	RWST To Charging Pmp Vlv Cont 1-LCV-62-136-B (1.9hp)	79.51	Opens on SI (Starts)	80.63	Opens on SI (Starts)	82.92	Pass	Att. 4
237-10A	SIS 1A-A DSH TO RWST SHFFF VLV 1-FCV-63-4-B (0.7hp)	N/A	Not Running or Starting	N/A	Not Running or Starting	84.83	Pass	Att. 4/ Acceptable Margin
237-10B	RWST To SIS Pump Flow Cont Vlv 1-FCV-63-5-B (1.9hp)	N/A	Not Running or Starting	N/A	Not Running or Starting	88.02*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
237-11A	SIS PMP INLT TO CVCS CHRG PMP 1-FCV-63-6-B (1.9hp)	N/A	Not Running or Starting	N/A	Not Running or Starting	88.21*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
237-11E	SIS Boron Inj Tank Shutoff Vlv 1-FCV-63-25-B (1.9hp)	82.98	Opens on SI (Starts)	84.14	Opens on SI (Starts)	86.53	Pass	Att. 4
237-12B	SIS Pmp 1B-B Inlet Vlv 1-FCV-63-48-B (1.9hp)	N/A	Not Running or Starting	N/A	Not Running or Starting	90.23*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
237-12D	CNTMT SUMP TO RHR PMP B-B 1-FCV-63-73-B (13hp)	N/A	Opens at approx. 20 min	N/A	Opens at approx. 20 min	88.20	Pass	Att. 4/ Acceptable Margin
237-14A	Cntmt Spray Hdr 1B Isln Vlv 1-FCV-72-2-B (3.2hp)	N/A	Closed, Not Running	92.98* (5s)	Opens, Starting.	92.86*	Pass	Att. 4 (5 sec after SI) - Time Delay added per DCN 52834
237-15B	RHR Pmp 1B-B Min Flow Vlv 1-FCV-74-24-B (0.13hp)	79.61	Opens, Starting.	80.73	Opens, Starting.	83.12	Pass	Att. 4
237-17D	AFW Pmp B-B Lube Oil Pmp B-B 1-MTR-3-128D-B (0.25HP)	N/A	N/A	N/A	N/A	89.64	85	Att. 1
237-5E	RCS Press Relief Flow Cont Vlv 1-FCV-68-332-B (1.9HP)	N/A	N/A	N/A	N/A	88.06*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
237-9B	RHR To RCS H.L. 1&3 Flow Iso V 1-FCV-63-172-B (2.6HP)	N/A	N/A	N/A	N/A	86.20	Pass	Att. 4 / Acceptable Margin

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Appendix A
1B Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)	SI Phase A	Terminal Voltage (%)	SI Phase B	Terminal Voltage (%)	Terminal Voltage V(%)	Reference
		6.6kV / 460V Base		6.6kV / 460V Base		6.6kV / 460V Base	6.6kV / 460V Base	
237-9F	Cont Spray Pmp 1B-B Recirc FCV 1-FCV-72-13-B (0.13HP)	N/A	N/A	N/A	N/A	90.08*	Pass	Att. 4 (10 sec after SI) - Time Delay added per DCN 52834
237-11B	RHR Hx B To SIS Pmp 1-FCV-63-11-B (2HP)	N/A	N/A	N/A	N/A	85.98	Pass	Att. 4 / Acceptable Margin
237-12E	SIS To RCS Loops 1&4 FCV 1-FCV-63-94-B (1.6HP)	N/A	N/A	N/A	N/A	90.80	Pass	Att. 4
237-13A	SIS Pmp 1B-B Outlet FCV 1-FCV-63-153-B (1.9HP)	N/A	N/A	N/A	N/A	88.75*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
237-13B	SIS PMP OUT RCS LP 2&4 H. LEG 1-FCV-63-157-B (1.9HP)	N/A	N/A	N/A	N/A	91.36*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
237-13D	SIS 1B-B Dsh To RWST Shtff Vlv 1-FCV-63-175-B (0.7HP)	N/A	N/A	N/A	N/A	84.86	Pass	Att. 4 / Acceptable Margin
237-14D	RHR Spray Hdr 1B Isln Vlv 1-FCV-72-41-B (1.9HP)	N/A	N/A	N/A	N/A	85.82	Pass	Att. 4 / Acceptable Margin
237-14E	Cntmt Sump To Spray Hdr 1B FCV 1-FCV-72-45-B (3.2HP)	N/A	N/A	N/A	N/A	89.68*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
237-15D	RHR Hx 1B Bypass Vlv 1-FCV-74-35-B (1.9HP)	N/A	N/A	N/A	N/A	83.17	Pass	Att. 4 / Acceptable Margin
480V RMOV Board 1B2-B								
238-2A	ERCW Hdr B Isln Vlv 1-FCV-3-126A-B (0.25hp)	N/A	Random	N/A	Random	83.60	Pass	Att. 4
238-3A	ERCW Hdr B Isln Vlv 1-FCV-3-179A-B (0.33hp)	N/A	Random	N/A	Random	83.71	Pass	Att. 4/ Acceptable Margin
238-3D	ST GEN NO 2 FW ISLN VLV 1-FCV-3-47-B (39.4hp)	80.64	Starts	81.41	Starts	82.74	Pass	Att. 4
238-4D	St Gen No 4 FW Isln Vlv 1-FCV-3-100-B (39.4hp)	80.64	Use 89-10 start	81.41	Use 89-10 start	82.74	Pass	Att. 4
238-5C	LWR CNTMT 1A CLRS ISLN VLV 1-FCV-67-113-B (0.13hp)	N/A	Not Running	82.01	Closes (Starts)	85.62	Pass	Att. 4
238-6D	RCP Thrm Bar Rtn Cntmt Iso Vlv 1-FCV-70-87-B (0.7hp)	N/A	Not Running	84.16	Closes (Starts)	87.83	Pass	Att. 4
238-6E	RCP THRM BAR CNTMT ISO VLV 1-FCV-70-134-B (0.13hp)	N/A	Not Running	82.33	Closes (Starts)	85.96	Pass	Att. 4
238-7D	Lwr Cntmt 1B Clr Dish Iso Vlv 1-FCV-67-103-B (0.13hp)	N/A	Not Running	82.80	Closes (Starts)	86.22	Pass	Att. 4
238-7F	Up Cntm Vt Clr 1A Dish Iso Vlv 1-FCV-67-131-B (0.13hp)	N/A	Not Running	80.64	Closes (Starts)	83.98	Pass	Att. 1
238-8D	Lwr Cntmt 1D Clr Dish Iso Vlv 1-FCV-67-111-B (0.13hp)	N/A	Not Running	83.11	Closes (Starts)	86.55	Pass	Att. 4

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Appendix A
1B Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
		SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%)	
ETAP Bus ID/ Compt No	Load Description	6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base	Reference
238-8F	Up Cntm Vt Clr 1C Dish Iso Vlv 1-FCV-67-134-B (0.13hp)	N/A	Not Running	80.60	Closes (Starts)	83.93	Pass	Att. 1
238-9A	Lwr Cntmt 1A Clr Dish Iso Vlv 1-FCV-67-88-B (0.33hp)	N/A	Not Running	83.71	Closes (Starts)	87.16	Pass	Att. 4
238-9B	Lwr Cntmt 1C Clr Dish Iso Vlv 1-FCV-67-96-B (0.33hp)	N/A	Not Running	83.83	Closes (Starts)	87.28	Pass	Att. 4
238-9D	Up Cntm Vt Clr 1B Dish Iso Vlv 1-FCV-67-297-B (0.13hp)	N/A	Not Running	81.49	Closes (Starts)	84.87	Pass	Att. 1
238-9F	Up Cntm Vt Clr 1B Sup Iso Vlv 1-FCV-67-138-B (0.13hp)	N/A	Not Running	80.55	Closes (Starts)	83.88	Pass	Att. 1
238-10A	Lwr Cntmt 1B Clr Sply Isln Vlv 1-FCV-67-91-B (0.33hp)	N/A	Not Running	83.74	Closes (Starts)	87.21	Pass	Att. 4
238-10B	Lwr Cntmt 1D Clr Sply Isln Vlv 1-FCV-67-83-B (0.33hp)	N/A	Not Running	84.33	Closes (Starts)	87.82	Pass	Att. 4
238-10D	UP CNTM VT CLR 1D DIS ISO VLV 1-FCV-67-298-B (0.13hp)	N/A	Not Running	80.13	Closes (Starts)	83.46	Pass	Att. 1
238-10F	Up Cntm Vt Clr 1D Sup Iso Vlv 1-FCV-67-141-B (0.13hp)	N/A	Not Running	80.92	Closes (Starts)	84.29	Pass	Att. 1
238-11D	LWR CNTMT 1C CLRS ISLN VLV 1-FCV-67-105-B (0.13hp)	N/A	Not Running	81.77	Closes (Starts)	85.16	Pass	Att. 4
238-13D	RCP Oil Clr Rtn Cntmt Isln Vlv 1-FCV-70-89-B (0.13hp)	N/A	Not Running	83.44	Closes (Starts)	86.91	Pass	Att. 4
238-13F	RCP Oil Clr Hdr Cntmt Isln Vlv 1-FCV-70-140-B (0.33hp)	N/A	Not Running	83.64	Closes (Starts)	87.10	Pass	Att. 4
238-18D	480V Bd Rm 1B A/C Cprsr 1B-B 1-MTR-31-447-B (75HP)	N/A	N/A	N/A	N/A	89.30	85	Att. 1
238-2B	ERCW Hdr B Isln Vlv 1-FCV-3-126B-B (0.25HP)	N/A	N/A	N/A	N/A	83.62	Pass	Att. 4
238-2E	St Flow To AFWFP Turb Isln Vlv 1-FCV-1-18-B (1HP)	N/A	N/A	N/A	N/A	92.50*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
238-3B	ERCW Hdr B Isln Vlv 1-FCV-3-179B-B (0.33HP)	N/A	N/A	N/A	N/A	83.72	Pass	Att. 4
238-5E	Cntmt Spray Hx 1B Sup Cont Vlv 1-FCV-67-123-B (0.33HP)	N/A	N/A	N/A	N/A	92.08*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
238-5F	Cntmt Spray Hx 1B Disch Vlv 1-FCV-67-124-B (0.33HP)	N/A	N/A	N/A	N/A	91.73*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
238-11B	STA S & C AC SUP HDR B ISO VLV 0-FCV-67-208-B (0.33HP)	N/A	N/A	N/A	N/A	91.28*	Pass	Att. 4
238-17D	CCS HX B ERCW BYPASS FCV 0-FCV-67-144-B (0.13HP)	N/A	N/A	N/A	N/A	84.33	Pass	Att. 4 / Acceptable Margin
480V Reac Vent Board 1B-B								
None								

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Appendix A
1B Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
		SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%)	
ETAP Bus ID/ Compt No	Load Description	6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base	Reference

* This MOV terminal voltage is calculated taking credit for the hammer blow feature.

**Appendix A
2A Boards**

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
		SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%) 6.6kV / 460V Base	Reference
ETAP Bus ID/ Compt No	Load Description	6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base		
6.9KV Shutdown Board 2A-A								
14-10 AFW	AUX FEEDWTR PMP 2A-A 2-MTR-3-118-A (600hp)	98.98	Starts	98.98	Starts	98.94	85	Att. 3
14-13 CSP	CNTMT SPRAY PMP 2A-A 2-MTR-72-27-A (700hp)	N/A	Not Running	N/A	Starts	98.60	80	Based on Unit 1 motor data (Att. 3)
14-14 RHR	RHR PMP 2A-A 2-MTR-74-10-A (400hp)	99.08	Starts	99.08	Starts	99.08	80	Based on Unit 1 motor data (Att. 3)
14-15 SI	SAFETY INJ PMP 2A-A 2-MTR-63-10-A (400hp)	98.83	Starts	98.83	Starts	98.83	80	Based on Unit 1 motor data (Att. 3)
14-18 CCP	CNTFGL CHRNG PMP 2A-A 2-MTR-62-108-A (600hp)	98.98	Starts	98.98	Starts	98.97	80	Att. 3
14-8 ERCW	ERCW PMP D-A 0-MTR-67-40-A (800hp)	N/A	Starts (D-A or C-A start, but not both, other is not running)	N/A	Starts (D-A or C-A start, but not both, other is not running)	96.59	90	Att. 3
14-9 ERCW	ERCW PMP C-A 0-MTR-67-36-A (800hp)	96.67	Starts (D-A or C-A start, but not both, other is not running)	96.67	Starts (D-A or C-A start, but not both, other is not running)	96.61	90	Same as ERCW Pmp D-A (Att. 3)
480V Shutdown Board 2A1-A								
133-3B	Cmpnt Clg Sys Pmp 2A-A 2-MTR-70-59-A (350hp)	81.38 (8s)	Starts	81.78 (8s)	Starts	81.26	70	Att. 3
134-10C	Cntmt Air Rtn Fan 2A-A 2-MTR-30-38-A (100hp)	N/A	Not Running Starts @ 9 Min)	N/A	Not Running Starts @ 9 Min)	82.41 (SIB)	80	Att. 6
134-7C	Reac Lwr Compt Clr Fan 2A-A 2-MTR-30-74-A (60hp)	N/A	Running	N/A	Trips	83.31	80	Based on Unit 1 motor data (Att. 3)
134-9C	Elec Bd Rm AHU B-A 0-MTR-31-30D-A (50hp)	N/A	Running	N/A	Running	83.48	80	Att. 6
480V Shutdown Board 2A2-A								
135-2C	Elec Bd Rm A/C A-A Cprsr 0MTR-31-128/2-A (250hp)	N/A	Running	N/A	Running	86.06	85	Att. 1
135-3C	SHDN BD RM CHLR PKG A-A CPRSR 0-MTR-31-36/2-A (240hp)	N/A	Running	N/A	Running	91.51	85	Att. 1
136-7D	REAC LWR COMPT CLR FAN 2C-A 2-MTR-30-77-A (60hp)	N/A	Running	N/A	Trips	81.11	80	Based on Unit 1 motor data (Att. 3)
136-8D	480V SHUTDOWN BD RM AHU B-A 0-MTR-31-44-A (75hp)	N/A	Running	N/A	Running	86.84	85	Att. 1
136-9D	Spent Fuel Pil Pmp A-A 0-MTR-78-12-A (100hp)	N/A	Running	N/A	Running	82.29	80	Att. 6
480V Reactor Vent Board 2A-A								
None								
480V C&A Vent Board 2A1-A								
207-10A	Cntfg Chrg Pmp 2A-A Rm Clr Fan 2-MTR-30-183-A (5HP)	83.44	Starts on SI	84.19	Starts on SI	86.10	80	Based on Unit 1 motor data (Att. 3)

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**Appendix A
2A Boards**

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%) 6.6kV / 460V Base	Reference
		6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base		
207-10B	Pen Rm EI 713 Clr Fan 2A-A 2-MTR-30-196-A (3HP)	87.11	Starts on SI	87.89	Starts on SI	90.89	80	Based on Unit 1 motor data (Att. 3)
207-10C	Pipe Chase Clr Fan 2A-A 2-MTR-30-201-A (3HP)	84.55	Starts on SI	85.31	Starts on SI	86.93	80	Based on Unit 1 motor data (Att. 3)
207-10D	ABGTS HUM HTR A-A 0-HTR-30-147-A (50.008kW)	N/A	Starts on ABI (from SI)	N/A	Starts on ABI (from SI)	N/A	Static Load	N/A
207-11A	480V Bd Rm 2B Pr Sup Fan 2B1-A 2-MTR-31-478-A (3HP)	N/A	Running	N/A	Running	92.41	85	Att. 1
207-11C	480V Bd Rm 2A A/C Ahu 2A-A 2-MTR-31-461-A (10HP)	N/A	Running	N/A	Running	88.57	85	Att. 1
207-12A	125V Vital Bat Rm III Ex Fan 2B1-A 2-MTR-31-285-A (0.33HP)	N/A	Running	N/A	Running	91.84	85	Att. 1
207-12C	480V Bd Rm 2A A/C Cond 2A-A 2-MTR-31-290-A (15HP)	N/A	Running	N/A	Running	91.02	85	Att. 1
207-12F1	Cntmt Purge Air Radn Exh Mon 2-RE-90-130-A (0.75HP)	N/A	Running	N/A	Running	93.49	85	Att. 1
207-13D	ERCW SCREEN WASH PUMP 2A-A 2-MTR-67-437-A (40HP)	N/A	Running	N/A	Running	76.53	75	Att. 3 Also See Sec. 7.1
207-2A	AUX CONTROL AIR COMPRESSOR A-A 0-MTR-32-60-A (20hp)	N/A	Not Running	N/A	Not Running	84.61	80	Att. 1
207-2C	Pen Rm EI 692 Clr Fan 2A-A 2-MTR-30-186-A (3HP)	84.16	Starts on SI	84.92	Starts on SI	86.97	80	Based on Unit 1 motor data (Att. 3)
207-3A	Shdn Bd Rm Chlr CW Clr Pmp A-A 0-MTR-31-36/1-A (25HP)	N/A	Running	N/A	Running	86.75	85	Att. 1
207-3C	Cntrn Spray Pmp 2A-A Rm Clr Fan 2-MTR-30-177-A (7.5HP)	N/A	Running	84.21	Starts on Phase B	87.19	80	Based on Unit 1 motor data (Att. 3)
207-3D	Aux BIDG Gas Trtmt Sys Fan A-A 2-MTR-30-146-A (50hp)	83.76	Starts On ABI (from SI)	84.51	Starts On ABI (from SI)	89.53	80	Att. 3
207-4A	EG Trtmt Sys A-A Rm Clr Fan 2-MTR-30-200-A (3HP)	86.11	Starts on ABI (from SI)	86.89	Starts on ABI (from SI)	91.20	80	Att. 3
207-4E	ERCW Str 2A-A Backwash Vlv 2-FCV-67-9A-A (0.33HP)	N/A	N/A	N/A	N/A	83.90	80	Att. 1
207-5E	AFW & BA XFR SPACE CLR FAN A-A 2-MTR-30-184-A (15HP)	87.08	Starts on ABI (from SI)	87.87	Starts on ABI (from SI)	90.96	80	Based on Unit 1 motor data (Att. 3)
207-6B	ERCW Str 2A-A 2-MTR-67-9-A (3HP)	N/A	Running	N/A	Running	82.53	75	Att. 3
207-6C	Traveling Scrn 2A-A 2-MTR-67-439-A (5HP)	N/A	N/A	N/A	N/A	81.49	80	Att. 3
207-7B	125V VIT BAT RM IV EXFAN 2A1-A 2-MTR-31-287-A (0.33HP)	N/A	Running	N/A	Running	92.12	85	Att. 1
207-8A	Safety Inj Pmp 2A-A Rm Clr Fan 2-MTR-30-180-A (5HP)	84.46 (2s)	Starts on Pump Start	80.70	Starts on Pump Start	81.70	80	Based on Unit 1 motor data (Att. 3)
207-8B	Pen Rm EI 737 Clr Fan 2A-A 2-MTR-30-194-A (3HP)	87.66	Starts on ABI (from SI)	88.45	Starts on ABI (from SI)	92.45	80	Att. 3
207-8C	480V Xfmr Rm 2A Exh Fan 2A2-A 2-MTR-30-250F-A (3HP)	N/A	Running	N/A	Running	91.94	80	Att. 3
207-8D	480V Xfmr Rm 2A Exh Fan 2A3-A 2-MTR-30-250G-A (3HP)	N/A	Running	N/A	Running	91.94	80	Att. 3
207-8F1	EL BD RM A/C A-A CONTROL/O.PMP 0-MTR-31-128/3-A (3.11HP)	N/A	Running	N/A	Running	91.13	85	Att. 1

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Appendix A
2A Boards

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%) 6.6kV / 460V	Reference
		6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	Base	
207-9A	RHR Pmp 2A-A Rm Clr Fan 2-MTR-30-175-A (5HP)	84.23 (2s)	Starts on SI	80.47	Starts on SI	81.35	80	Based on Unit 1 motor data (Att. 3)
207-9B	C.BIDG Ele BdRm AC Clr Pmp A-A 0-MTR-31-128/1-A (20HP)	N/A	Running	N/A	Running	88.10	85	Att. 1
207-9C	480V Bd Rm 2A Pr Sup Fan 2A1-A 2-MTR-31-462-A (3HP)	N/A	Running	N/A	Running	92.31	85	Att. 1
207-9D	480V Xfmr Rm 2A Exh Fan 2A1-A 2-MTR-30-250E-A (3HP)	N/A	Running	N/A	Running	91.49	85	Att. 1
207-9F1	Cont Rm Intake Mon 0-RE-90-125-A (0.75HP)	N/A	Running	N/A	Running	93.16	85	Att. 1
207-7E	RWST To Spray Hdr 2A FCV 2-FCV-72-22-A (3.2HP)	N/A	N/A	N/A	N/A	86.30	Pass	Att. 5 / Acceptable Margin
480V C&A Vent Board 2A2-A								
None								
480V Diesel Aux Board 2A1-A								
221-2B	DG 2A-A RM EXH FAN 1-A 2-MTR-30-448-A (15hp)	92.28	Starts	92.66	Starts	93.44	85	Att. 3
221-2D	DG 2A-A Lube Oil Circ Pmp 1 2-MTR-82-A1-A (1hp)	N/A	Running	N/A	Running	94.72	85	Att. 1
221-3A	EM DG ENG HX 2A1 & 2A2 SUP VLV 2-FCV-67-66-A (0.13hp)	82.55	Starts	82.90	Starts	85.97	Pass	Att. 5
221-3D	DG 2A-A DAY TNK FO XFR PMP 1 2-MTR-18-55/3-A (1hp)	91.55	Random	91.94	Random	94.78	85	Att. 1
221-4B	DG 2A-A Aux LubeOil Circ Pmp A 2-MTR-82-AOPA1A (0.75hp)	N/A	Running	N/A	Running	94.97	85	Att. 1
221-6A	DG 2A-A Muffler Rm Exh Fan 2-MTR-30-464 (0.5hp)	91.99	Starts on Diesel Start from SI	92.37	Starts on Diesel Start from SI	94.90	85	Att. 3
221-4D	DG Rm 2A-A Pnl Vent Fan 2-MTR-30-492-A (15HP)	N/A	N/A	N/A	N/A	92.29	85	Att. 3
221-4E	2A-A 480V ELEC BD RM EX FAN 2-MTR-30-460-A (2HP)	N/A	N/A	N/A	N/A	95.16	85	Att. 1
480V Diesel Aux Board 2A2-A								
222-2A	DG 2A-A Aux LubeOil Circ Pmp B 2-MTR-82-AOPB1A (0.75hp)	N/A	Running	N/A	Running	94.93	85	Att. 1
222-2B	DG 2A-A RM EXH FAN 2-A 2-MTR-30-452-A (15hp)	92.59	Starts	92.85	Starts	93.29	85	Att. 3
222-2D	DG 2A-A Lube Oil Circ Pmp 2 2-MTR-82-A2-A (1hp)	N/A	Running	N/A	Running	94.98	85	Att. 1
222-3D	DG 2A-A DAY TNK FO XFR PMP 2 2-MTR-18-54/3-A (1hp)	92.18	Random	92.44	Random	94.94	85	Att. 1
480V RMOV Board 2A1-A								
239-10F	Cntm Spray Pmp 2A-A Recirc FCV 2-FCV-72-34-A (0.13hp)	N/A	Not Running	N/A	Closes 10s after Phase B	89.37	Pass	Att. 5
239-11D	SIS Boron Inj Tank Shutoff VLV 2-FCV-63-26-A (1.9hp)	86.11	Operate about 20 minutes after SI	86.83	Operate about 20 minutes after SI	92.06	Pass	Att. 5/ Acceptable Margin
239-12B	Cntmt Sump To RHR Pmp A-A 2-FCV-63-72-A (13hp)	N/A	Operate about 20 minutes after SI	N/A	Operate about 20 minutes after SI	91.21	Pass	Att. 5/ Acceptable Margin

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**Appendix A
2A Boards**

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%)	
		6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base	Reference
239-13E	Cntmt Spray Hdr 2A Isln Vlv 2-FCV-72-39-A (3.2hp)	N/A	Not Running	83.13	Opens on Ph B (Starts)	87.97	Pass	Att. 5/ Acceptable Margin
239-14D	RHR Pmp 2A-A Min Flow Vlv 2-FCV-74-12-A (0.13hp)	83.91	Random	84.61	Random	89.71	Pass	Att. 5
239-15D	LWR CNTMT 2A CLRS SUP ISLN VLV 2-FCV-67-89-A (0.33hp)	N/A	Not Running	87.91	Closes (Starts)	93.22	Pass	Att. 5
239-17B	Cntmt Standpipe Isln Vlv 2-FCV-26-240-A (0.67hp)	82.10	Close (Starts)	82.78	Close (Starts)	87.74	Pass	Att. 5
239-18E	RCP Spray Isln Vlv 2-FCV-26-243-A (0.67hp)	81.17	Close (Starts)	81.85	Close (Starts)	86.47	Pass	Att. 5
239-7A	Seal Flow Ret Isln Vlv 2-FCV-62-63-A (1.9hp)	77.85	Closes on Ph A (Starts)	78.50	Closes on Ph A (Starts)	83.16	Pass	Att. 5 / Acceptable Margin
239-7B	CHRG FLOW ISLN VLV 2-FCV-62-90-A (1.9hp)	85.16	Closes on SI	85.86	Closes on SI	90.94	Pass	Att. 5 / Acceptable Margin
239-8B	Vol Cont Tank Outlet Isln Vlv 2-LCV-62-132-A (1.9hp)	80.78	Closes on SI	81.45	Closes on SI	86.28	Pass	Att. 5
239-5C	LWR CNTMT 2C CLRS SUP ISLN VLV 2-FCV-67-97-A (0.33hp)	N/A	Not Running	87.71	Closes (Starts)	93.00	Pass	Att. 5
239-9A	RWST TO CHARGING PMPS CONT 2-LCV-62-135-A (1.9hp)	84.82	Opens on SI (Starts)	85.52	Opens on SI (Starts)	90.58	Pass	Att. 5 / Acceptable Margin
239-9D	2-FCV-70-100A (0.33hp)	N/A	Not Running	87.19	Closes on Phase B	92.46	Pass	Att. 5
239-10B	SIS PMPS RECIRC TO RWST 2-FCV-63-3-A (0.7HP)	N/A	N/A	N/A	N/A	89.43	Pass	Att. 5 / Acceptable Margin
239-2B	Boric Acid Transfer Pmp 2A-A 2-MTR-62-230-A (15HP)	N/A	N/A	N/A	N/A	92.42	85	Att. 1
239-11A	SIS Pmp Inlet To CVCS Chrg Pmp 2-FCV-63-7-A (1.9HP)	N/A	N/A	N/A	N/A	81.98	Pass	Att. 5 / Acceptable Margin
239-14E	RHR Hx 2A Bypass Vlv 2-FCV-74-33-A (1.9HP)	N/A	N/A	N/A	N/A	84.67	Pass	Att. 5 / Acceptable Margin
239-2C	THERM BAR SYS BSTR PMP 2A-A 2-MTR-70-131-A (10HP)	N/A	N/A	N/A	N/A	86.94	85	Att. 1
239-11B	RHR Hx A To CVCS Chgr Pmp 2-FCV-63-8-A (1.9HP)	N/A	N/A	N/A	N/A	89.05	Pass	Att. 5 / Acceptable Margin
239-2E1	RWST To RHR Pmp Flow Cont Vlv 2-FCV-63-1-A (5.2HP)	N/A	N/A	N/A	N/A	91.80	Pass	Att. 5/ Acceptable Margin
239-3E	Cntigl Chrg Pmp 2A-A AOP 2-MTR-62-AOP-A (2HP)	N/A	N/A	N/A	N/A	86.44	85	Att. 1
239-12A	SIS Pmp 2A-A Inlet Vlv 2-FCV-63-47-A (1.9HP)	N/A	N/A	N/A	N/A	79.72	Pass	Att. 5 / Acceptable Margin
239-4E	AFW Pmp A-A Lube Oil Pmp A-A 2-MTR-3-118D-A (0.25HP)	N/A	N/A	N/A	N/A	88.24	85	Att. 1
239-12D	SIS To RCS Loops 2&3 FCV 2-FCV-63-93-A (1.6HP)	N/A	N/A	N/A	N/A	93.00	Pass	Att. 5 / Acceptable Margin
239-12E	SIS Pmp 2A-A Outlet FCV 2-FCV-63-152-A (1.9HP)	N/A	N/A	N/A	N/A	85.61	Pass	Att. 5 / Acceptable Margin
239-13A	SIS Pmp Out RCS Lp 1&3 Hot Leg 2-FCV-63-156-A (1.9HP)	N/A	N/A	N/A	N/A	85.58	Pass	Att. 5 / Acceptable Margin

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**Appendix A
2A Boards**

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%) 6.6kV / 460V Base	Reference
		6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base		
239-6D	RCS Press Relief FCV 2-FCV-68-333-A (1.9HP)	N/A	N/A	N/A	N/A	86.46	Pass	Att. 5 / Acceptable Margin
239-13B	Cntmt Sump To Spray Hdr 2A FCV 2-FCV-72-44-A (3.2HP)	N/A	N/A	N/A	N/A	80.63	Pass	Att. 5 / Acceptable Margin
239-14A	RHR Spray Hdr 2A Isln Vlv 2-FCV-72-40-A (1.9HP)	N/A	N/A	N/A	N/A	88.31	Pass	Att. 5 / Acceptable Margin
480V RMOV Board 2A2-A								
240-10A	Lwr Cntm 2D Clr Dish Iso Vlv 2-FCV-67-112-A (0.33hp)	N/A	Not Running	89.57	Closes (Starts)	92.14	Pass	Att. 5
240-10D	Up Cntm Vt Clr 2C Dish Iso Vlv 2-FCV-67-296-A (0.13hp)	N/A	Not Running	88.24	Closes (Starts)	90.77	Pass	Att. 5
240-10F	Up Cntm Vt Clr 2D Dish Iso Vlv 2-FCV-67-142-A (0.13hp)	N/A	Not Running	89.61	Closes (Starts)	92.18	Pass	Att. 5
240-11D	RCP Thrm Barr Rtn Cntm Iso Vlv 2-FCV-70-90-A (0.7hp)	N/A	Not Running	87.25	Closes (Starts)	89.73	Pass	Att. 5
240-11E	RCP Thrm Barr Cntmt Isln Vlv 2-FCV-70-133-A (0.13hp)	N/A	Not Running	87.62	Closes (Starts)	90.14	Pass	Att. 5
240-12D	RCP Oil Clr Rtn Cntmt Isln Vlv 2-FCV-70-92-A (0.13hp)	N/A	Not Running	88.59	Closes (Starts)	91.77	Pass	Att. 5
240-16D	Excs Ltdn Hx Cont Init Iso Vlv 2-FCV-70-143-A (0.33hp)	88.49	Closes on Phase A	88.93	Closes on Phase A	91.48	Pass	Att. 5
240-3D	St Gen No 1 FW Isln Vlv 2-FCV-3-33-A (39.4hp)	85.33	Use 89-10 start	85.75	Use 89-10 start	86.38	Pass	Att. 5
240-4D	St Gen No 3 FW Isln Vlv 2-FCV-3-87-A (39.4hp)	87.00	Use 89-10 start	87.43	Use 89-10 start	88.05	Pass	Att. 5
240-7D	Lwr Cntm 2A Clr Dish Iso Vlv 2-FCV-67-87-A (0.13hp)	N/A	Not Running	89.73	Closes (Starts)	92.31	Pass	Att. 5
240-7F	Up Cntm Vt Clr 2A Sup Iso Vlv 2-FCV-67-130-A (0.13hp)	N/A	Not Running	89.63	Closes (Starts)	92.20	Pass	Att. 5
240-8B	Lwr Cntmt 2A Clr Sply Isln Vlv 2-FCV-67-107-A (0.33hp)	N/A	Not Running	89.57	Closes (Starts)	92.14	Pass	Att. 5
240-8D	Lwr Cntm 2C Clr Dish Iso Vlv 2-FCV-67-95-A (0.13hp)	N/A	Not Running	89.45	Closes (Starts)	92.02	Pass	Att. 5
240-8F	Up Cntm Vt Clr 2C Sup Iso Vlv 2-FCV-67-133-A (0.13hp)	N/A	Not Running	89.59	Closes (Starts)	92.16	Pass	Att. 5
240-9A	Lwr Cntmt 2C Clr Sply Isln Vlv 2-FCV-67-99-A (0.33hp)	N/A	Not Running	89.40	Closes (Starts)	91.97	Pass	Att. 5
240-9B	Lwr Cntm 2B Clr Dish Iso Vlv 2-FCV-67-104-A (0.33hp)	N/A	Not Running	89.40	Closes (Starts)	91.97	Pass	Att. 5
240-9D	Up Cntm Vt Clr 2A Dish Iso Vlv 2-FCV-67-295-A (0.13hp)	N/A	Not Running	88.06	Closes (Starts)	90.59	Pass	Att. 5
240-9F	Up Cntm Vt Clr 2B Dish Iso Vlv 2-FCV-67-139-A (0.13hp)	N/A	Not Running	89.61	Closes (Starts)	92.18	Pass	Att. 5
240-11A	Cmpnt Clg Hx A Disch Cont Vlv 2-FCV-67-146-A (0.3HP)	N/A	N/A	N/A	N/A	89.64	Pass	Att. 5 / Acceptable Margin
240-15A	CCS HX B ERCW BYPASS FCV 2-FCV-67-143-A (0.13HP)	N/A	N/A	N/A	N/A	92.44	Pass	Att. 5 / Acceptable Margin
240-16E	RHR Hx A-A Outlet Vlv 2-FCV-70-156-A (0.33HP)	N/A	N/A	N/A	N/A	89.63	Pass	Att. 5 / Acceptable Margin

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**Appendix A
2A Boards**

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%)	
		6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base	Reference
240-17A	Sample Hx Hdr Outlet Vlv 2-FCV-70-183-A (0.13HP)	N/A	N/A	N/A	N/A	90.15	Pass	Att. 5 / Acceptable Margin
240-17E	480V BD RM 2A A/C CPRSR 2A-A 2-MTR-31-465-A (50HP)	N/A	N/A	N/A	N/A	91.53	85	Att. 1
240-2A	ERCW Hdr A Isln Vlv 2-FCV-3-116A-A (0.25HP)	N/A	N/A	N/A	N/A	91.06	Pass	Att. 5 / Acceptable Margin
240-2B	ERCW Hdr A Isln Vlv 2-FCV-3-116B-A (0.25HP)	N/A	N/A	N/A	N/A	90.94	Pass	Att. 5 / Acceptable Margin
240-2D	AFWP Turb Stm Sup Fm Stm Gen 1 2-FCV-1-15-A (1HP)	N/A	N/A	N/A	N/A	91.38	Pass	Att. 5 / Acceptable Margin
240-3A	ERCW Hdr A Isln Vlv 2-FCV-3-136A-A (0.33HP)	N/A	N/A	N/A	N/A	90.06	Pass	Att. 5 / Acceptable Margin
240-3B	ERCW Hdr A Isln Vlv 2-FCV-3-136B-A (0.33HP)	N/A	N/A	N/A	N/A	90.07	Pass	Att. 5 / Acceptable Margin
240-5A	Sample Hx Isln Vlv 2-FCV-70-215-A (0.13HP)	N/A	N/A	N/A	N/A	90.31	Pass	Att. 5 / Acceptable Margin
240-5E	Cntmt Spray Hx 2A Sup Cont Vlv 2-FCV-67-125-A (0.33HP)	N/A	N/A	N/A	N/A	91.49	Pass	Att. 5 / Acceptable Margin
240-5F	Cntmt Spray Hx 2A Disch Vlv 2-FCV-67-126-A (0.33HP)	N/A	N/A	N/A	N/A	91.49	Pass	Att. 5 / Acceptable Margin
240-6A	AFWP Turb Stm Sup Fm Stm Gen 4 2-FCV-1-16-A (1HP)	N/A	N/A	N/A	N/A	91.37	Pass	Att. 5 / Acceptable Margin

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* This MOV terminal voltage is calculated taking credit for the hammer blow feature.

**Appendix A
2B Boards**

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%)	
		6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base	Reference
6.9kV Shutdown Board 2B-B								
15-10 AFW	Aux Feedwater PMP 2B-B 2-MTR-3-128-B (600 HP)	99.11	Starts	99.11	Starts	99.09	85	Att. 3
15-13 CSP	CNTMT SPRAY PMP 2B-B 2-MTR-72-10-B (700 HP)	N/A	Not Running	98.93	Starts	98.93	80	Based on Unit 1 motor data (Att. 3)
15-14 RHR	RHR PUMP 2B-B 2-MTR-74-20-B (400 HP)	99.03	Starts	99.03	Starts	99.03	80	Based on Unit 1 motor data (Att. 3)
15-15 SI	SAFETY INJ PMP 2B-B 2-MTR-63-15-B (400 HP)	99.05	Starts	99.05	Starts	99.05	80	Based on Unit 1 motor data (Att. 3)
15-18 CCP	CNTFGL CHRGR PMP 2B-B 2-MTR-62-104-B (500 HP)	99.00	Starts	99.00	Starts	98.99	80	Based on Unit 1 motor data (Att. 3)
15-8 ERCW	ERCW PMP H-B 0-MTR-67-59-B (800 HP)	N/A	Starts (H-B or G- B start, but not both, other is not running)	N/A	Starts (H-B or G-B start, but not both, other is not running)	96.05	90	Att. 3
15-9 ERCW	ERCW PMP G-B 0-MTR-67-55-B (800 HP)	96.72	Starts (H-B or G- B start, but not both, other is not running)	96.72	Starts (H-B or G-B start, but not both, other is not running)	6.66	90	Same as ERCW Pmp H-B (Att. 3)
480V Shutdown Board 2B1-B								
137-3C	Cmpnt Clg Sys Pmp 2B-B 2-MTR-70-33-B (350 hp)	81.40 (8s)	Starts	81.79 (8s)	Starts	81.19	70	Att. 3
138-7A	Elec Bd Rm AHU D-B 0-MTR-31-31D-B (50 hp)	N/A	Running	N/A	Running	85.53	80	Att. 6
138-7B	Spent Fuel Pit Pmp C-S ALT FDR 0-MTR-78-35-S (100 hp)	N/A	Running	N/A	Running	85.82	80	Att. 6
138-7D	Reac Lwr Compt Clr Fan 2B-B 2-MTR-30-75-B (60 hp)	N/A	Running	N/A	Trips	83.93	80	Based on Unit 1 motor data (Att. 3)
480V Shutdown Board 2B2-A								
139-2B	Elect Bd rm A/C B-B Cprsr 0-MTR-31-129/2-B (250 hp)	N/A	Running	N/A	Running	86.53	85	Att. 1
139-2D	Cmpnt Clg Sys Pmp C-5 0-MTR-70-51-S (350 hp)	N/A	Running	N/A	Running	69.99 (SIB)	70	Att. 3
140-7D	Reac Lwr Compt Clr Fan 2D-B 2-MTR-30-78-B (60 hp)	N/A	Running	N/A	Trips	86.42	80	Based on Unit 1 motor data (Att. 3)
140-9C	Cntmt Air Rtn Fan 2B-B 2-MTR-30-39-B (100 hp)	N/A	Not Running Starts @ 9 Min	N/A	Not Running Starts @ 9 Min	84.87	80	Att. 6
140-9D	480V Shutdown Bd Rm AHU D-B 0-MTR-31-61-B (75 hp)	N/A	Running	N/A	Running	88.06	85	Att. 1
480V CA Vent Board 2B1-B								
209-2A	Aux Cont Air Cprsr B-B 0-MTR-32-86-B (20 hp)	N/A	Not Running	N/A	Not Running	84.56	80	Att. 1
209-2C	Pen Rm EI713 Clr Fan 2B-B 2-MTR-30-197-B (3 hp)	87.20	Starts on ABI	88.00	Starts on ABI	91.06	80	Based on Unit 1 motor data (Att. 3)
209-3B	Pipe Chase Clr Fan 2B-B 2-MTR-30-202-B (3 hp)	87.25	Starts on ABI	88.06	Starts on ABI	91.11	80	Based on Unit 1 motor data (Att. 3)
209-3C	Cntm Spray Pmp 2B-B Rm Clr Fan 2-MTR-30-178-B (7.5 hp)	83.48	Random	84.25	Starts on Pump Start	86.17	80	Based on Unit 1 motor data (Att. 3)

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**Appendix A
2B Boards**

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A		SI Phase B		Individual Motor Start	Minimum Required Voltage	Bases for
		DBE Actuation		DBE Actuation		Terminal Voltage (%)	Terminal Voltage V(%)	Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	6.6kV / 460V	Reference
		6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	Base	
209-3D	Aux Bldg Gas Trtmt Sys Fan B-B 2-MTR-30-157-B (50 hp)	82.90	Starts on ABI	83.66	Starts on ABI	88.68	80	Same as Fan A-A (207-3D), Att 3
209-4A	BATTERY RM EL 692 EXH FAN C-B 0-MTR-31-27-B (2 hp)	N/A	Running	N/A	Running	89.95	85	Att. 1
209-5E	AFWP&BA XFR PMP SP CLR FAN B-B 2-MTR-30-185-B (15 hp)	87.24	Starts on ABI	88.05	Starts on ABI	88.81	80	Based on Unit 1 motor data (Att. 3)
209-6B	ERCW Str 2B-B 2-MTR-67-10-B (3 hp)	N/A	Running	N/A	Running	77.30	75	Att. 3
209-6C	Traveling Scrn 2B-B 2-MTR-67-10-B (5 hp)	N/A	Running	N/A	Running	81.68	80	Att. 3
209-7B	125V Vit Bat Rm IV ExFan 2A2-B 2-MTR-31-288-B (0.33 hp)	N/A	Running	N/A	Running	92.11	85	Att. 1
209-7D	RHR Pmp 2B-B Inlet FCV 2-FCV-74-21-B (5.2 hp)	N/A	Not Running	N/A	Not Running	93.70	Pass	Att. 5
209-8A	Safety Inj Pmp 2B-B Rm Clr Fan 2-MTR-30-179-B (5 hp)	84.79	Starts on Pump Start	85.58	Starts on Pump Start	87.41	80	Based on Unit 1 motor data (Att. 3)
209-8B	Pen Rm El 692 Clr Fan 2B-B 2-MTR-30-187-B (3 hp)	86.61	Starts on ABI	87.41	Starts on ABI	89.49	80	Based on Unit 1 motor data (Att. 3)
209-8C	Shtdn Xfrm Rm 2B Exh Fan 2B2-B 2-MTR-30-246G-B (3 hp)	N/A	Running	N/A	Running	91.83	80	Att. 3
209-8D	Shtdn Xfrm Rm 2B Exh Fan 2B3-B 2-MTR-30-246H-B (3 hp)	N/A	Running	N/A	Running	92.14	80	Att. 3
209-8E	C.Bldg Ele BdrM AC Clr Pmp B-B 0-MTR-31-129/1-B (20 hp)	N/A	Running	N/A	Running	88.44	85	Att. 1
209-8F1	EL BD RM A/C B-B CONTROL/O.PMP 0-MTR-31-129/3-B (3 hp)	N/A	Running	N/A	Running	92.33	85	Att. 1
209-9A	RHR Pmp 2B-B Rm Clr Fan 2-MTR-30-176-B (5 hp)	81.19	Starts on Pump Start	81.94	Starts on Pump Start	82.53	80	Based on Unit 1 motor data (Att. 3)
209-9C	480V Bd Rm 2A Pr Sup Fan 2A2-B 2-MTR-31-463-B (3 hp)	N/A	Running	N/A	Running	92.84	85	Att. 1
209-9D	Shtdn Xfrm Rm 2B Exh Fan 2B1-B 2-MTR-30-246F-B (3 hp)	N/A	Running	N/A	Running	92.45	80	Att. 3
209-9E	Pen Rm El 737 Clr Fan 2B-B 2-MTR-30-195-B (3 hp)	87.63	Starts on ABI	88.43	Starts on ABI	91.70	80	Att. 3
209-10A	Cntfg Chrg Pmp 2B-B Rm Clr Fan 2-MTR-30-182-B (5 hp)	86.12	Starts on Pump Start	86.91	Starts on Pump Start	89.04	80	Based on Unit 1 motor data (Att. 3)
209-10B	480V Bd Rm 2B Pr Sup Fan 2B2-B 2-MTR-31-477-B (3 hp)	N/A	Running	N/A	Running	93.15	85	Att. 1
209-10C	125V Vit BatRm III ExFan 2B2-B 2-MTR-31-286-B (0.33 hp)	N/A	Running	N/A	Running	91.90	85	Att. 1
209-10F1	Cont Rm Intake Mon 0-RE-90-126-B (0.75 hp)	N/A	Running	N/A	Running	93.11	85	Att. 1
209-11B	480V Bb Rm 2B A/C Ahu 2B-B 2-MTR-31-475-B (20 hp)	N/A	Running	N/A	Running	90.81	85	Att. 1
209-11C	480V Bd Rm 2B A/C cond 2B-B 2-MTR-31-289-B (20 hp)	N/A	Running	N/A	Running	90.23	85	Att. 1
209-12B	EG Trtmt Sys B-B Rm Clr Fan 2-MTR-30-207-B (3 hp)	87.39	Starts on ABI	88.20	Starts on ABI	91.70	80	Att. 3
209-13D	ERCW Scrn Wash Pmp 2B-B 2-MTR-67-447-B (40 hp)	N/A	N/A	N/A	N/A	74.69	75	Att. 3 Also See Sec. 7.1
209-7E	RWST To Spray Hdr 2B FCV 2-FCV-72-21-B (3.3 hp)	N/A	Not Running	N/A	Not Running	87.70	Pass	Att. 5 / Acceptable Margin
209-6E	ERCW Str 2B-B Flush Vlv 2-FCV-67-10B-B (0.33HP)	N/A	N/A	N/A	N/A	83.36	80	Att. 1
209-4E	ERCW Str 2B-B Backwash Vlv 2-FCV-67-10A-B (0.33HP)	N/A	N/A	N/A	N/A	83.62	80	Att. 1

R2

**Appendix A
2B Boards**

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit) Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%)	Minimum Required Voltage
		6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base	Reference
480V CA Vent Board 2B2-B								
	None							
480V Diesel Aux Board 2B1-B								
223-2B	DG 2B-B RM EXH FAN 1B 2-MTR-30-450-B (15 hp)	92.48	Starts	92.88	Start	94.64	85	Att. 3
223-2D	DG 2B-B Lube Oil Circ Pmp 1 2-MTR-82-B1-B (1 hp)	N/A	Running	N/A	Running	95.14	85	Att. 1
223-3A	EM DG ENG SUP VLV FROM HDR 1B 2-FCV-67-67-B (0.13hp)	82.55	Open on Diesel Start	82.90	Open on Diesel Start	86.33	Pass	Att. 5
223-3D	DG 2B-B DAY TNK FO XFR PMP 1 2-MTR-18-55/4-B (1 hp)	92.31	Random	92.71	Random	95.03	85	Att. 1
223-4D	DG Rm 2B-B Pnl Vent Fan 2-MTR-30-494-B (15 hp)	N/A	Running	N/A	Running	92.52	85	Att. 3
223-4E	DG 2B-B 480V Elec Bd Rm Ex Fan 2-MTR-30-462-B (2 hp)	N/A	Running	N/A	Running	94.63	85	Att. 1
223-6A	Dg 2B-B Muffler Rm Exh Fan 2-MTR-30-466 (0.5HP)	92.72	Starts	93.11	Starts	95.56	85	Att. 3
480V Diesel Aux Board 2B2-B								
224-2A	DG 2B-B Aux Lube Oil Circ Pmp B 2-MTR-82-AOPB2B (0.75 hp)	N/A	Running	N/A	Running	94.71	85	Att. 1
224-2B	DG 2B-B RM EXH FAN 2-B 2-MTR-30-454-B (15 hp)	92.76	Starts	92.99	Starts	93.13	85	Att. 3
224-2D	DG 2B-B Lube Oil Circ Pmp 2 2-MTR-82-B2-B (1 hp)	N/A	Running	N/A	Running	94.83	85	Att. 1
224-3D	DG 2B-B DAY TNK FO XFR PMP 2 2-MTR-18-54/4-B (1 hp)	92.53	Random	92.76	Random	94.80	85	Att. 1
480V RMOV Board 2B1-B								
241-17D	AFW Pmp B-B Lube Oil Pmp B-B 2-MTR-3-128D-B (0.25 hp)	N/A	Running	N/A	Running	88.48	85	Att. 1
241-3F2	SIS Accum Tank Flow Isol Vlv 2-FCV-63-98-B (19.5 hp)	N/A	Not Running	N/A	Not Running	86.66	Pass	Att. 5 / Acceptable Margin
241-5A	HPPF Sys Low Level Intake Viv 0-FCV-26-8-B (0.13 hp)	N/A	Not Running	N/A	Not Running	80.91	80	Att. 1
241-5E	RCS Press Relief FCV 2-FCV-68-332-B (2 hp)	N/A	Not Running	N/A	Not Running	84.25	Pass	Att. 5 / Acceptable Margin
241-6D	Seal Flow Ret Isln Vlv 2-FCV-62-61-B (1.9 hp)	82.53	Closes on Ph A (Starts)	83.24	Not Running	87.63	Pass	Att. 5 / Acceptable Margin
241-7A	CHRG FLOW ISLN VLV 2-FCV-62-91-B (1.9 hp)	86.71	Closes on SI	87.45	Closes on SI	92.06	Pass	Att. 5 / Acceptable Margin
241-8A	Vol Cont Tank Outlet Isln Vlv 2-LCV-62-133-B (1.9 hp)	81.30	Closes on SI	82.00	Closes on SI	86.25	Pass	Att. 5 / Acceptable Margin
241-8B	RWST TO CHRG PMP VALVE CONT 2-LCV-62-136-B (1.9 hp)	80.20	Opens on SI	80.89	Opens on SI	85.08	Pass	Att. 5 / Acceptable Margin
241-9B	RHR To RCS H.L. 1&3 Flow Iso V 2-FCV-63-172-B (2.6 hp)	N/A	Not Running	N/A	Not Running	80.97	Pass	Att. 5 / Acceptable Margin
241-9F	Cntm spray Pmp 2B-B Recirc FCV 2-FCV-72-13-B (0.1 hp)	N/A	Not Running	N/A	Starts 10s after Phase B	89.77	Pass	Att. 5
241-10A	SIS 2B-B Dsh To RWST Shtff Vlv 2-FCV-63-4-B (0.66 hp)	N/A	Not Running	N/A	Not Running	89.02	Pass	Att. 5 / Acceptable Margin
241-10B	RWST To SIS Pump FCV 2-FCV-63-5-B (2 hp)	N/A	Not Running	N/A	Not Running	83.31	Pass	Att. 5 / Acceptable Margin
241-11A	SIS Pmp Inlet To CVCS Chrg Pmp 2-FCV-63-6-B (2 hp)	N/A	Not Running	N/A	Not Running	81.72	Pass	Att. 5 / Acceptable Margin

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**Appendix A
2B Boards**

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start Terminal Voltage (%)	Minimum Required Voltage Terminal Voltage V(%)	Bases for Minimum Required Voltage
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	6.6kV / 460V	Reference
		6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	Base	
241-11B	RHR Hx B to SIS Pmp 2-FCV-63-11-B (2 hp)	N/A	Not Running	N/A	Not Running	87.60	Pass	Att. 5 / Acceptable Margin
241-11E	SIS Boron Inj Tank Shutoff Vlv 2-FCV-63-25-B (1.9 hp)	86.65	Closes on SI	87.40	Closes on SI	91.98	Pass	Att. 5 / Acceptable Margin
241-12B	SIS Pmp 2B-B Inlet Vlv 2-FCV-63-48-B (2 hp)	N/A	Not Running	N/A	Not Running	84.14	Pass	Att. 5 / Acceptable Margin
241-12D	Cntmt Sump To RHR Pmp B-B 2-FCV-63-73-B (13.2 hp)	N/A	Open at 20 Min after SI	N/A	Open at 20 Min after SI	91.40	Pass	Att. 5 / Acceptable Margin
241-12E	SIS To RCS Loops 1 & 4 FCV 2-FCV-63-94-B (1.6 hp)	N/A	Not Running	N/A	Not Running	92.80	Pass	Att. 5 / Acceptable Margin
241-13A	SIS Pmp 2B-B Outlet FCV 2-FCV-63-153-B (2 hp)	N/A	Not Running	N/A	Not Running	85.71	Pass	Att. 5 / Acceptable Margin
241-13B	SIS pmp Out RCS Lp 2&4 Hot Leg 2-FCV-63-157-B (2 hp)	N/A	Not Running	N/A	Not Running	88.35	Pass	Att. 5 / Acceptable Margin
241-13D	SIS 2B-B Dsh to RWST Shdff Vlv 2-FCV-63-175-B (0.66 hp)	N/A	Not Running	N/A	Not Running	89.50	Pass	Att. 5 / Acceptable Margin
241-14A	Cntmt Spray Hdr 2B Isln Vlv 2-FCV-72-2-B (3.2 hp)	N/A	Not Running	85.96	Open on Phase B	90.37	Pass	Att. 5 / Acceptable Margin
241-14D	RHR SPRAY HDR 2B ISOL VLV 2-FCV-72-41-B (2 hp)	N/A	Not Running	N/A	Not Running	88.15	Pass	Att. 5 / Acceptable Margin
241-14E	Cntm Sump To Spray Hdr 2B FCV 2-FCV-72-45-B (3.3 hp)	N/A	Not Running	N/A	Not Running	82.22	Pass	Att. 5 / Acceptable Margin
241-15B	RHR Pmp 2B-B Min Flow Vlv 2-FCV-74-24-B (0.1 hp)	85.18	Start on RHR pump start on SI	85.91	Start on RHR pump start on SI	90.53	Pass	Att. 5 / Acceptable Margin
241-15D	RHR Hx 2B Bypass Vlv 2-FCV-74-35-B (2 hp)	N/A	Not Running	N/A	Not Running	79.68	Pass	Att. 5 / Acceptable Margin
480V RMOV Board 2B2-B								
242-18D	480V Bd Rm 2B A/C Cprsr 2B-B 2-MTR-31-447-B (75 hp)	N/A	Running	N/A	Running	90.83	85	Att. 1
242-2A	ERCW Hdr B Isln Vlv 2-FCV-3-126A-B (0.67 hp)	N/A	Not Running	N/A	Not Running	89.82	Pass	Att. 5 / Acceptable Margin
242-2B	ERCW Hdr B Isln Vlv 2-FCV-3-126B-B (0.67 hp)	N/A	Not Running	N/A	Not Running	89.81	Pass	Att. 5 / Acceptable Margin
242-2E	St Flow To AFWP Turb Isln Vlv 2-FCV-1-18-B (1 hp)	N/A	Running	N/A	Running	91.06	Pass	Att. 5 / Acceptable Margin
242-3A	ERCW Hdr B Isln Vlv 2-FCV-3-179A-B (0.33 hp)	N/A	Random	N/A	Random	90.39	Pass	Att. 5 / Acceptable Margin
242-3B	ERCW Hdr B Isln Vlv 2-FCV-3-179B-B (0.33 hp)	N/A	Random	N/A	Random	90.20	Pass	Att. 5 / Acceptable Margin
242-3D	St Gen No 2 FW Isln Vlv 2-FCV-3-47-B (39.4 hp)	85.16	Use 89-10 start	85.41	Use 89-10 start	87.81	Pass	Att. 5
242-4D	St Gen No 4 FW Isln Vlv 2-FCV-3-100-B (39.4 hp)	86.16	Use 89-10 start	86.41	Use 89-10 start	88.83	Pass	Att. 5
242-5C	LWR CNTMT 2A CLRS SUP ISLN VLV 2-FCV-67-113B (0.3 hp)	N/A	Not Running	88.43	Closes (Starts)	91.99	Pass	Att. 5
242-5E	Cntmt Spray Hx 2B Sup Cont Vlv 2-FCV-67-123-B (0.33 hp)	N/A	Not Running	N/A	Not Running	91.41	Pass	Att. 5 / Acceptable Margin
242-5F	Cntmt Spray Hx 2B Sup Disch Vlv 2-FCV-67-124-B (0.33 hp)	N/A	Not Running	N/A	Not Running	91.00	Pass	Att. 5 / Acceptable Margin
242-6D	RCP Thrm Barr Rtn Cntm Iso Vlv 2-FCV-70-87-B (0.7 hp)	N/A	Not Running	87.62	Closes (Starts)	91.14	Pass	Att. 5

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**Appendix A
2B Boards**

EVALUATION of CLASS 1E MOTOR STARTING VOLTAGES at DVR DROPOUT (Analytical Limit)								
Comparison of Minimum Available Starting Voltage v/s Required Starting Voltage								
Results Shown for DBE Actuation (SI-A or SI-B) and Individual Motor Starts								
ETAP Bus ID/ Compt No	Load Description	SI Phase A DBE Actuation		SI Phase B DBE Actuation		Individual Motor Start	Minimum Required Voltage	Bases for
		Terminal Voltage (%)		Terminal Voltage (%)		Terminal Voltage (%)	Terminal Voltage V(%)	Minimum Required Voltage
		6.6kV / 460V Base	SI Phase A	6.6kV / 460V Base	SI Phase B	6.6kV / 460V Base	6.6kV / 460V Base	Reference
242-6E	RCP Thrn Barr Cntmt Isln Vlv 2-FCV-70-134-B (0.1 hp)	N/A	Not Running	87.60	Closes (Starts)	91.14	Pass	Att. 5
242-7D	Lwr Cntmt 2B Clr Dish Isln Vlv 2-FCV-67-103-B (0.1 hp)	N/A	Not Running	87.51	Closes (Starts)	91.04	Pass	Att. 5
242-7F	Up Cntm Vt Clr 2A Dish Iso Vlv 2-FCV-67-131-B (0.1 hp)	N/A	Not Running	87.18	Closes (Starts)	90.69	Pass	Att. 5
242-8D	Lwr Cntm 2D Clr Dish Iso Vlv 2-FCV-67-111-B (0.1 hp)	N/A	Not Running	87.93	Closes (Starts)	91.48	Pass	Att. 5
242-8F	Up Cntm Vt Clr 2C dish Iso Vlv 2-FCV-67-134-B (0.1 hp)	N/A	Not Running	87.18	Closes (Starts)	85.63	Pass	Att. 5
242-9A	Lwr Cntm 2A Clr Dish Iso Vlv 2-FCV-67-88-B (0.3 hp)	N/A	Not Running	86.92	Closes (Starts)	90.43	Pass	Att. 5
242-9B	Lwr Cntm 2C Clr Dish Iso Vlv 2-FCV-67-96-B (0.3 hp)	N/A	Not Running	87.02	Closes (Starts)	90.53	Pass	Att. 5
242-9D	Up Cntm Vt Clr 2B Dish Iso Vlv 2-FCV-67-297-B (0.1 hp)	N/A	Not Running	86.19	Closes (Starts)	89.66	Pass	Att. 5
242-9F	Up Cntm Vt Clr 2B Sup Isln Vlv 2-FCV-67-138-B (0.1 hp)	N/A	Not Running	87.18	Closes (Starts)	90.69	Pass	Att. 5
242-10A	Lwr Cntmt 2B Clr Sply Isln Vlv 2-FCV-67-91-B (0.3 hp)	N/A	Not Running	86.93	Closes (Starts)	90.43	Pass	Att. 5
242-10B	Lwr Cntmt 2D Clr Sply Isln Vlv 2-FCV-67-83-B (0.3 hp)	N/A	Not Running	87.23	Closes (Starts)	90.75	Pass	Att. 5
242-10D	Up Cntm Vt Clr 2D Dish Iso Vlv 2-FCV-67-298-B (0.1 hp)	N/A	Not Running	86.87	Closes (Starts)	90.37	Pass	Att. 5
242-10F	Up Cntm Vt Clr 2D Sup Isln Vlv 2-FCV-67-141-B (0.1 hp)	N/A	Not Running	87.18	Closes (Starts)	90.69	Pass	Att. 5
242-11B	LWR CNTMT 2B CLRS SUP ISLN VLV 2-FCV-67-105-B (0.3 hp)	N/A	Not Running	88.09	Closes (Starts)	91.65	Pass	Att. 5
242-12B	CCS Hx C Dish Vlv To Hdr B 0-FCV-67-152-B (0.7 hp)	N/A	Running	N/A	Running	89.74	Pass	Att. 4
242-13D	RCP OIL CLR RTN CNTMT ISLN VLV 2-FCV-70-89-B (0.3 hp)	N/A	Not Running	88.11	Closes (Starts)	91.67	Pass	Att. 5
242-13F	RCP Oil Clr Hdr Cntmt Isln Vlv 2-FCV-70-140-B (0.3 hp)	N/A	Not Running	86.94	Closes (Starts)	90.45	Pass	Att. 5
242-17A	SFPCS Hx Sply Hdr Isln Vlv 0-FCV-70-194-B (0.33 hp)	N/A	Not Running	N/A	Not Running	92.18*	Pass	Att. 4 / Acceptable Margin with voltage based on Hammer Blow feature *
242-15E	RHR Hx B-B Outlet Vlv 2-FCV-70-153-B (0.33 hp)	N/A	Not Running	N/A	Not Running	91.47	Pass	Att 5
480V Reactor Vent Board 2B-B								
None								

* This MOV terminal voltage is calculated taking credit for the hammer blow feature.

Voltage Recovery Analysis for DBE

Purpose

The purpose of the attachment is to demonstrate that any possible voltage transient caused by motor starting during a DBE (SI with Phase A or Phase B isolation), including drop to the LOV setpoint, will also result in successful recovery above DVR reset within 5 seconds.

Approach

This transient voltage dip and recovery analysis is similar to that analyzed by the offsite power analysis (reference 2.2) which shows that the voltage recovers above the DVR reset within 5 seconds. However, the offsite power analysis credits the use of automatic load tap changers (LTC) for voltage recovery and also assumes minimum operable grid capacity. The offsite power analysis accounts for minimum operable grid capacity by using an extremely conservative technique of forcing the switchyard voltage to the minimum allowable post-event voltage. This technique ignores the voltage recovery that would occur once the larger motors accelerate.

In this analysis, the offsite power source has been modeled using a classical Thevenin equivalent impedance technique (fixed voltage source behind impedance). The impedance chosen is equivalent to that grid capacity that would result in the voltage at the 6.9kV Shutdown Boards dropping all the way to the loss of voltage (LOV) relay setpoint during initial DBE motor starting (block-start of ECCS loads).

Bases/Assumptions

- The offsite power LTCs (CSST C & D) are not allowed to correct the voltage during the motor starting event. However, they are allowed to adjust the voltage prior to the event. This is conservative because it will result in the worst-case voltage transient with no voltage recovery from the LTCs.
- The auxiliary power system is assumed to be in normal alignment prior to the event (Unit Boards and RCP Boards on USSTs, Common Boards on CSSTs A/B, Shutdown Boards on CSSTs C/D). This is conservative, because it puts the least amount of load on the offsite power source prior to the event and thereby results in a "stiffer" offsite power source impedance (i.e. less recovery). In addition, aligning the Shutdown Boards to CSSTs A/B would result in even greater recovery due to the Unit Board load shed feature.
- The 161kV Switchyard voltage is assumed to be at the minimum operable voltage prior to the event. This is conservative, because it will also result in a "stiffer" offsite power source impedance (i.e. less recovery).

Computations

Using the existing ETAP model used to perform offsite power analysis for two unit operation (Ref. 2.2), a dynamic motor starting analysis was performed for both SI-Phase A and SI-Phase B events on each unit. Using a trial and error technique, the switchyard source capacity (MVA_{sc}) was adjusted until the applicable 6.9kV Shutdown Board voltages just equaled the LOV setpoint (80% nominal) at $t=0+$ in the event being studied.

Each dynamic motor starting study case (SIA and SIB) was run for at least 5 seconds. The associated ETAP reports provide the voltage during the event in 0.1 second intervals for each 6.9kV Shutdown Board.

Results

A plot of the worst-case voltage recovery is shown for both U1 SIB and U2 SIB. The results show that in all cases the 6.9kV Shutdown Board voltage recovers above the DVR reset value (operational limit of 6681V) within 4 seconds.

Conclusions

This bounding analysis demonstrates that any possible voltage transient caused by DBE motor starting, including drop to the LOV setpoint, will also result in successful recovery above DVR reset within 5 seconds.

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Contract:
Engineer:

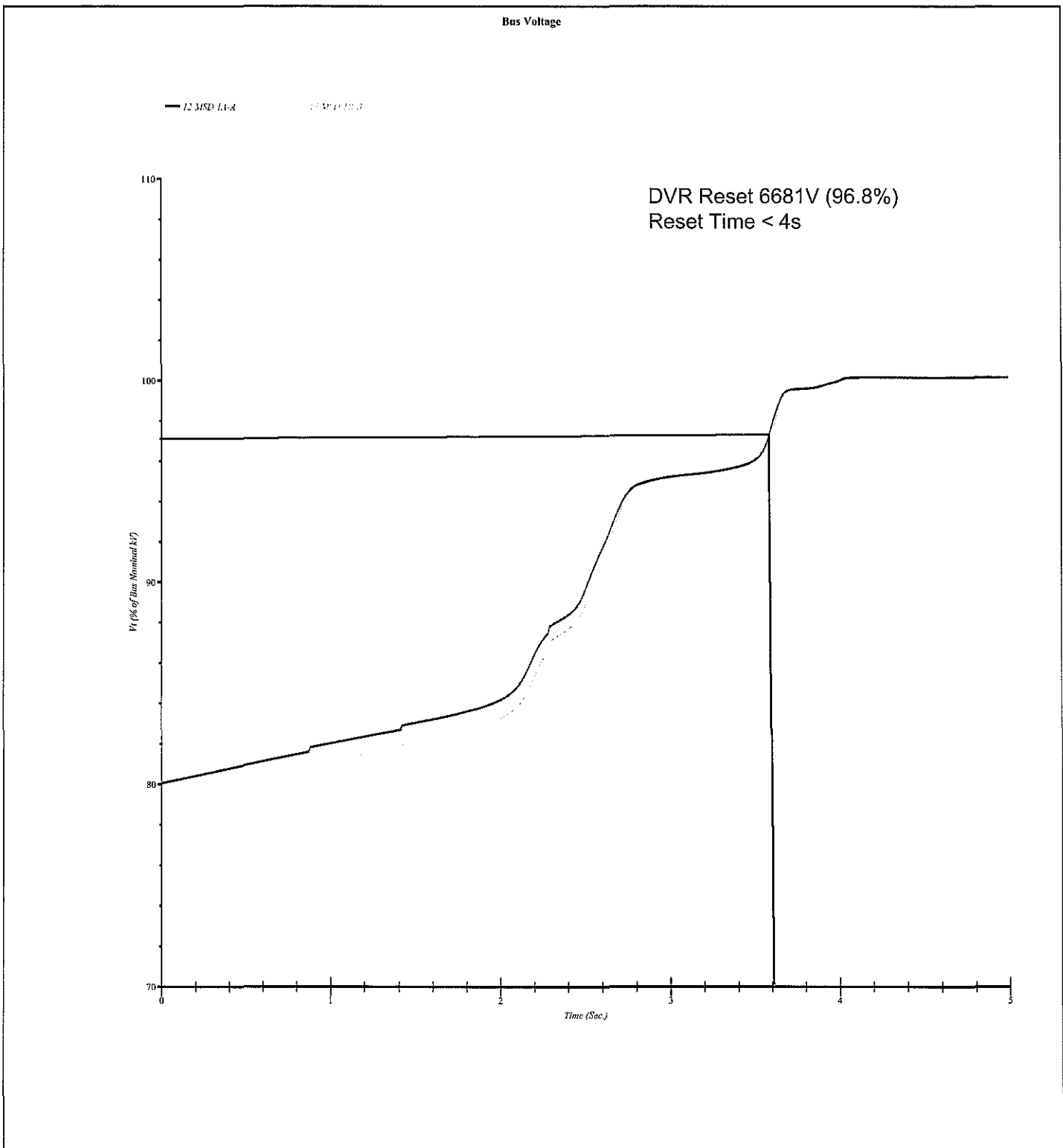
ETAP
7.0.0K
Study Case: U1 SIB-U2

Date: 03-21-2012
SN: 90TVA12DC2
Revision: Unit 1&2
Config.: N 4 CSST-U2

WBN-EEB-MS-TI06-0029
Unit 1 SI Phase B. Plant in normal alignment (4CSSTs) at lowest operable grid (161kV). No LTC during the event.

Project File: J:\wbnp\R0 EDQ00099920120004 (DVR Analysis)\DVR Analysis WBN\DVR LOV Recovery Analysis\WBNDATA
Output Report: UISIB-152MVA

MOTOR STARTING ANALYSIS



Project: Watts Bar Nuclear Plant
Location: //chachaapp5/etaps/wbnp/
Contract:
Engineer:

ETAP
7.0.0N

Study Case: U1/2 SIA

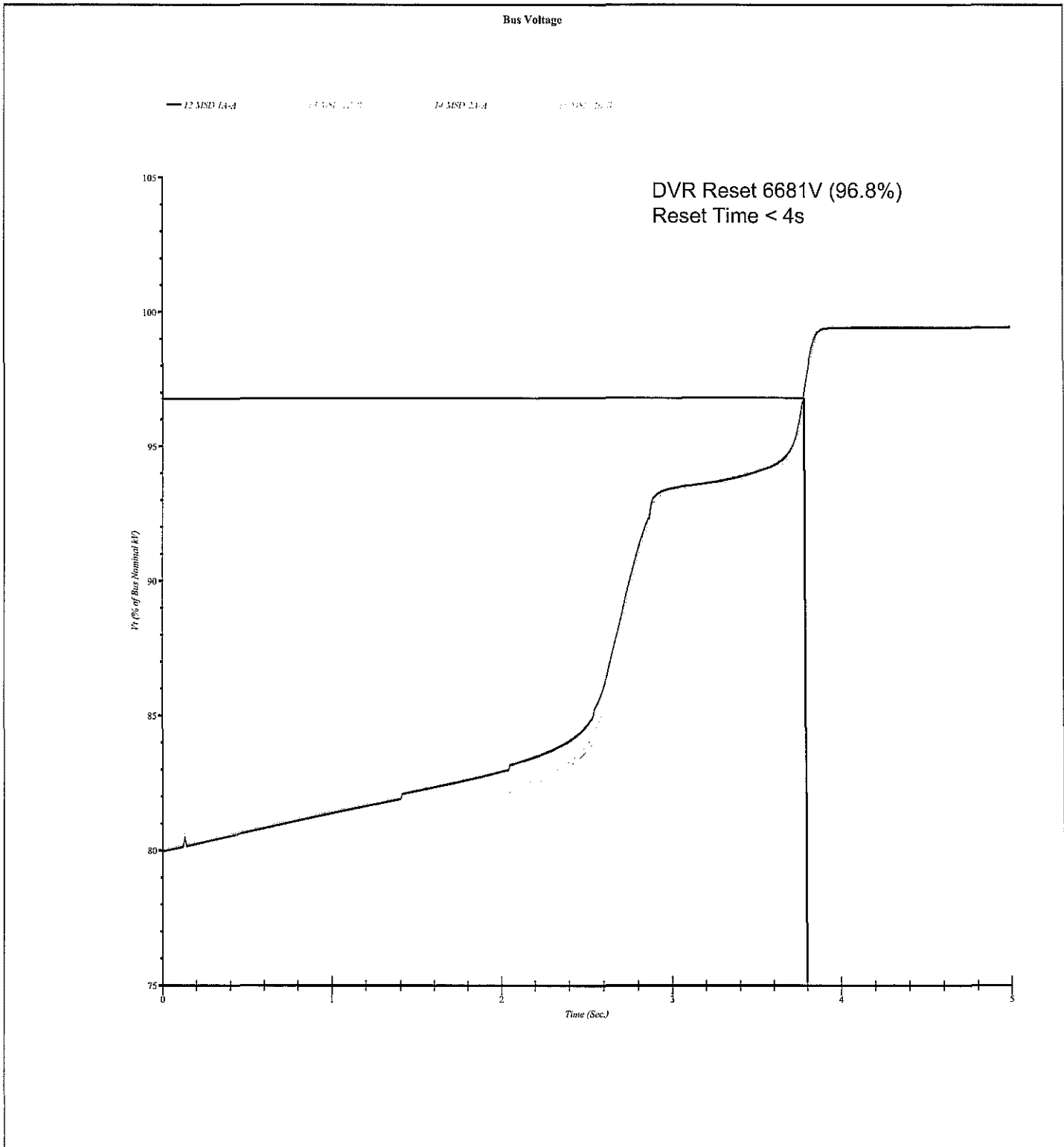
Date: 03-21-2012
SN: 90TVA12DC2
Revision: Unit 1&2
Config.: N 4 CSST-U2

WBN-EEB-MS-TI06-0029

Unit 1/2 SI Phase A. Plant in normal alignment (4CSSTs) at lowest operable grid (161kV). No LTC during the event.

Project File: J:\wbnp\RO EDQ00099920120004 (DVR Analysis)\DVR Analysis WBN\DVR LOV Recovery Analysis\WBNDATA
Output Report: U12-SIA

MOTOR STARTING ANALYSIS



Project: Watts Bar Nuclear Plant
Location: //chachaapp5/etaps/wbrp/
Contract:
Engineer:

ETAP
7.0.0N

Study Case: U2 SIB-U2

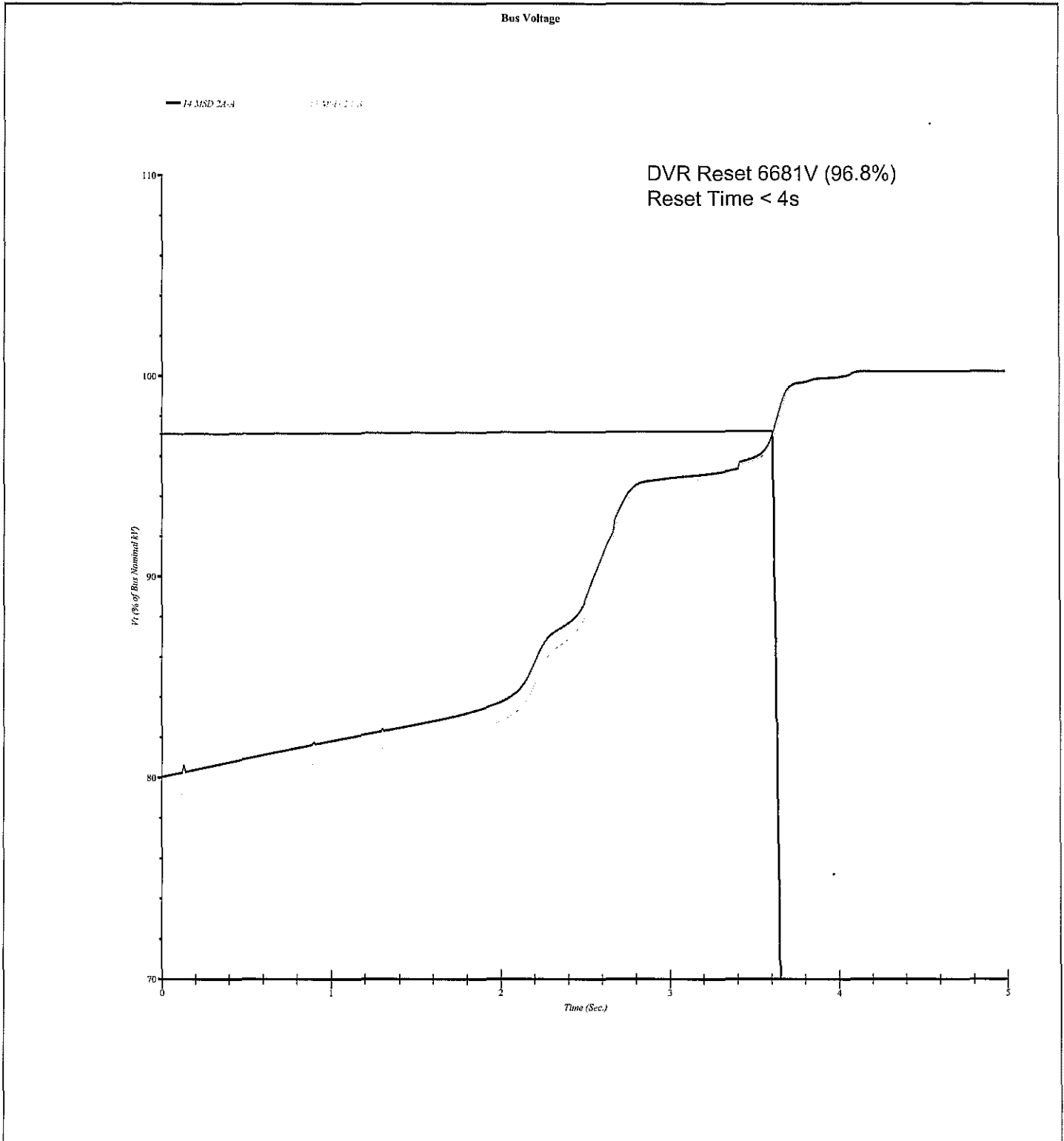
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SN: 90TVA12DC2
Revision: Unit 1&2
Config.: N 4 CSST-U2

WBN-EEB-MS-TI06-0029

Unit 2 SI Phase B. Plant in normal alignment (4CSSTs) at lowest operable grid (161kV). No LTC during the event.

Project File: J:\wbrp\R0 EDQ00099920120004 (DVR Analysis)\DVR Analysis WBN\DVR LOV Recovery Analysis\WBNDATA
Output Report: U2SIB-152MVA

MOTOR STARTING ANALYSIS



Degraded Voltage Recovery Analysis for DBE

Purpose

The purpose of this appendix is to address NRC comments concerning the adequacy of the analytical methodology for the motor starting cases previously analyzed in this study to support DBE. The nature of the comments concerned the initial voltage used in the analysis at the DVR monitored bus and fell into two general areas:

1. Demonstrate the adequacy of the DVR protection scheme if the voltage source is placed at the switchyard bus and the grid voltage is set such that the DVR monitored bus voltage is at the DVR dropout analytical limit prior to the DBE initiation.
2. Demonstrate the adequacy of the DVR protection scheme if the voltage source is placed at the switchyard bus and both grid voltage and capacity are adjusted to any value that will support successful voltage recovery following DBE motor starting (i.e. Class 1E loads remain on offsite power).

Approach

This appendix follows a similar analytical technique as described in Appendix B. Additional study cases were set up to address the NRC comments as follows:

Study Case 1: The grid is set to strongest capacity (maximum short-circuit strength) and grid voltage is lowered until the DVR monitored bus voltage reaches the DVR analytical limit prior to DBE initiation. The outcome of this evaluation should demonstrate that the Class 1E bus voltage will not be able to successfully recover (i.e. reset the DVR) following the DBE initiation.

Study Case 2: Grid voltage and capacity are adjusted until the lowest possible initial voltage is found (at the DVR monitored bus) that allows successful recovery following DBE motor starting (i.e. the resulting voltage dip recovers from the Loss of Voltage relay (LOV) and also resets the DVR in a bounding fashion). The outcome of this evaluation should demonstrate that any combination of initial grid voltage and capacity that results in successful recovery of the Class 1E bus voltage does so because of the proper acceleration of the accident initiated motors on the 6.9kV 1E buses.

Analysis is performed for each study case using normal offsite power alignment via CSSTs C & D as well as alignment via CSSTs A & B (Shutdown Boards aligned to Start Buses via Unit Boards).

Bases/Assumptions

All the bases and assumptions listed in Appendix B of this study are applicable to this appendix. (Ref. Attachment 2 for relay setpoints)

Computations

The existing ETAP model from offsite power analysis for two unit operation (Ref. 2.2) was used to perform dynamic motor starting analyses similar to Appendix B. The analysis was performed considering a DBE for Unit 1 (SI with Phase B isolation). Detailed evaluation was performed for 6.9kV Shutdown Board 1A-A only (aligned to CSSTs A, B, C, or D) as the results are considered to be representative of the other Shutdown Boards for the purposes of these analyses.

Study Case 1:

- 1) The utility source model was placed on the 161kV switchyard bus.
- 2) The applicable CSST automatic load tap changers (LTC) were placed in manual (i.e. not working).

- 3) Using normal plant operation loading, the source voltage was lowered until the voltage at the DVR monitored bus (6.9kV Shutdown Board) was exactly at 6555V (DVR dropout analytical limit).
- 4) The source capacity was set to the maximum short-circuit strength (Ref PSO Study), which allows the greatest ability of the grid to recover the Class 1E bus voltage above the DVR reset value following DBE motor starting.

Study Case 2:

- 1) The utility source model was placed on the 161kV switchyard bus.
- 2) The applicable CSST automatic load tap changers (LTC) were placed in manual (i.e. not working).
- 3) Normal plant operation loading was used prior to the DBE initiation.
- 4) The source voltage and capacity were adjusted as required to achieve all of the following criteria:
 - a) voltage at the 6.9kV Shutdown Board is not lower than 6555V (DVR dropout analytical limit) prior to DBE initiation.
 - b) if the voltage dip produced by DBE initiation (at the 6.9kV Shutdown Board) drops below the LOV relay setpoint, it also recovers above the setpoint within the relay timeout (nominal settings used for convenience)
 - c) the voltage at the 6.9kV Shutdown Board recovers to (exactly) the DVR reset point following the initial "block start" transient (nominal setting used for convenience).

Each dynamic motor starting study case was run for 5 seconds. The associated ETAP results provide the voltage profile in percent in 0.01 second intervals at the 6.9kV Shutdown Board. These values were plotted to evaluate the results. The existing offsite power analysis voltage profile for the same DBE (minimum grid capability) were also added on the same plots for general comparison (see Figures 1 and 2 of this appendix).

The following study cases have been run:

<u>Study Case</u>	<u>ETAP Configuration</u>	<u>ETAP MS Case</u>	<u>ETAP Report Name</u>
1	NCSSTABD-U2	U1SIB-U2	DVR DO AB
1	N4 CSST-U2	U1SIB-U2	DVR DO CD
2	NCSSTABD-U2	U1SIB-U2	WC Grid AB
2	N4 CSST-U2	U1SIB-U2	WC Grid CD

Results

Based on the study cases the results are summarized below:

Study Case 1 -

Voltage at the DVR monitored bus is at DVR dropout with a strong grid capacity. The evaluation shows (Ref. Figure 1) without the load tap changer, the DVR will not reset and Class 1E buses will disconnect from offsite power and transfer to the DGs as designed. Transfer to DG is acceptable because previous protective device analysis shows the successful transfer to the onsite power supply with all required Class 1E loads achieving adequate voltage for starting and running within required time limits.

Study Case 2 -

Voltage at the DVR monitored bus is at the lowest possible initial voltage that allows successful recovery. This case, while not representative of any actual postulated grid, results in the worst conceivable grid that allows Class 1E buses to remain on offsite power. The evaluation shows (Ref Figure 2) the DVR recovery time is not significantly different than that shown for offsite power analysis (minimum qualified grid). This case demonstrates that any conceivable voltage transient caused by motor starting, even at the threshold of LOV timeout and DVR timeout, will result in recovery of voltage (DVR reset or above) within 4 seconds.

Conclusions

The outcomes of these additional requested analysis demonstrate the adequacy of the DVR protection scheme based on:

- 1) If the LOV relay times out
 - a. Class 1E buses disconnect from offsite power and transfer to the DGs
 - b. Based on previous analysis, Class 1E components have adequate voltage for starting and running within analyzed time limits
- 2) If the LOV relay does not time out, then either:
 - a. The DVR times out
 - i. Class 1E buses disconnect from off site power and transfer to the DGs
 - ii. Based on previous analyses, Class 1E components have adequate voltage for starting and running within analyzed time limits
 - OR
 - b. The DVR does not time out
 - i. Class 1E buses remain connected to off site power
 - ii. Based on previous analyses, Class 1E components have adequate voltage for starting and running within analyzed time limits

DVR at Dropout Prior to LOCA, Shdn Bd 1A-A, U1 SIB

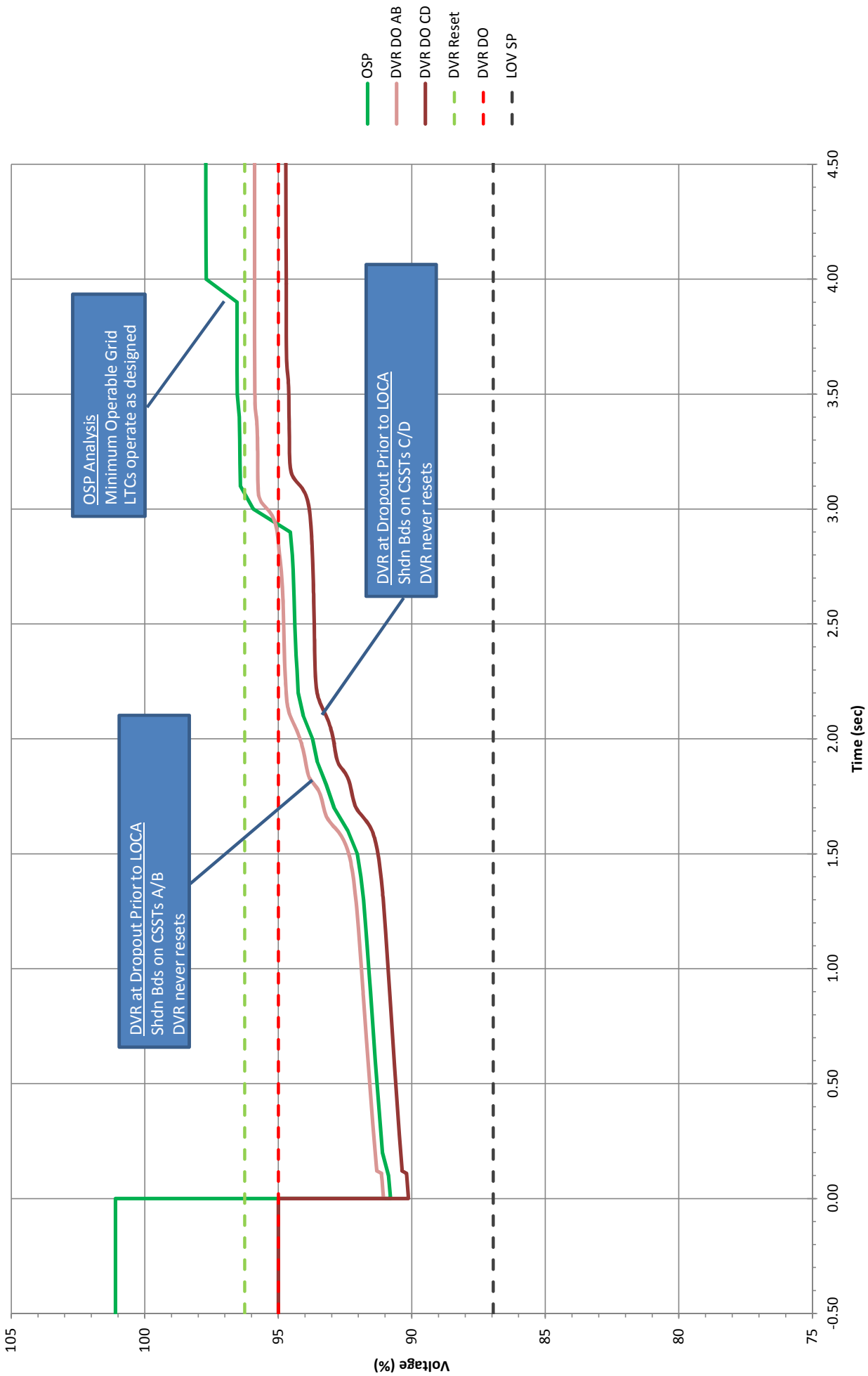


FIGURE 1
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Worst-Case Grid that Recovers, Shdn Bd 1A-A, U1 SIB

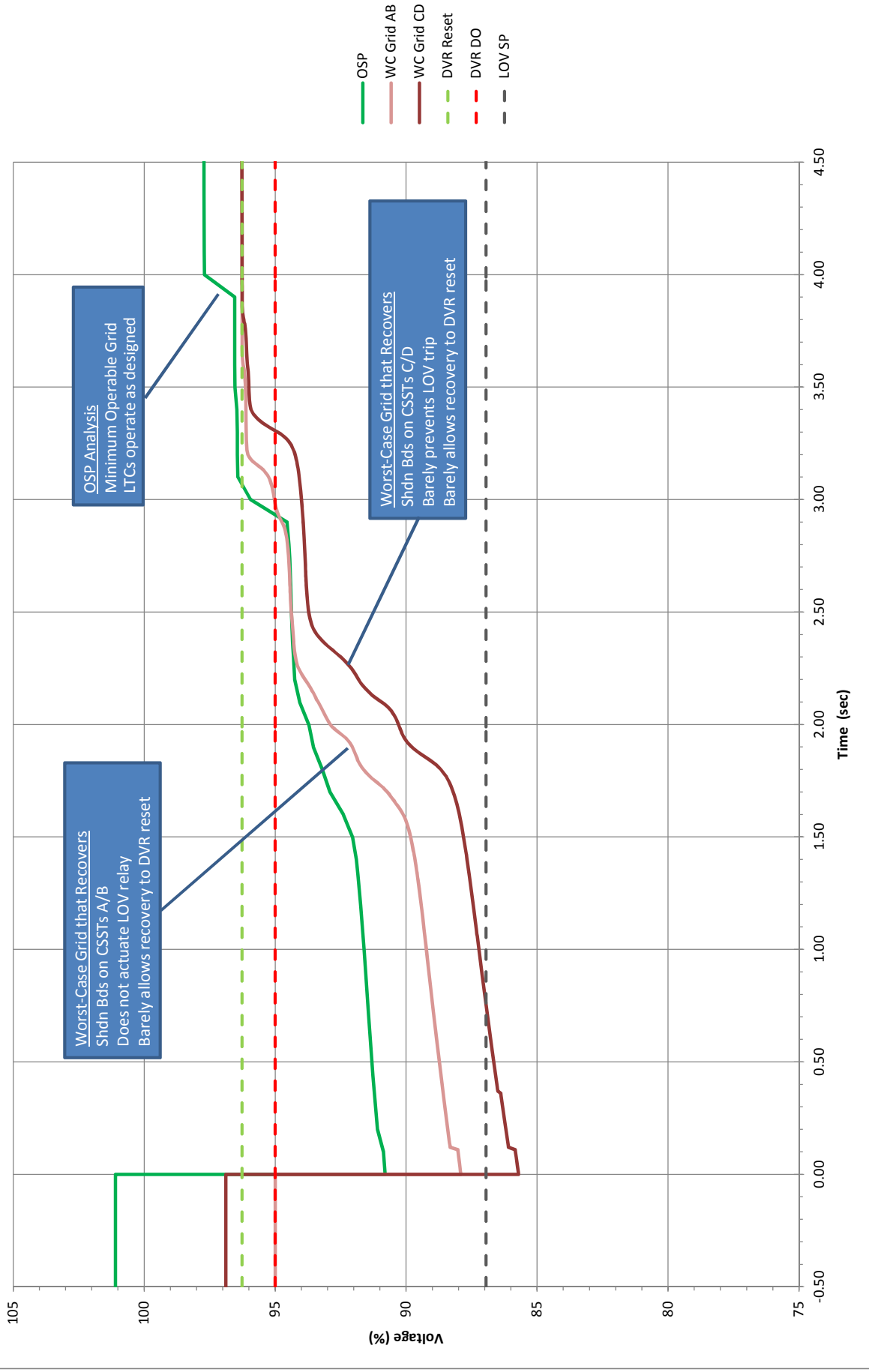


FIGURE 2
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CALCULATION SHEET

CALC NUMBER: WBN-EEB-EDQ000-999-2007-0002

REV. NO 20

SHEET NO. 11

3.0 DESIGN INPUT DATA & REQUIREMENTS

The evaluation documented in this calculation was previously performed and documented in the following calculations:

WBN EEB-MS-TI05-0001, Auxiliary Power System Database (TELAS)
WBN EEB-MS-TI06-0002, Auxiliary Power System Analysis (ELMS-NON1E),
WBN EEB-MS-TI06-0010, Auxiliary Power System Analysis on 1E Buses (ELMS-1E).

The design input data identified in these calculations are still valid and will not be repeated here. Only new and significant design input data will be identified here.

3.1 "WBN ETAP CONVERSION, Phase 1 - database Conversion", RIMS B43 990303 001

3.2 Not used

3.3 Acceptable Voltage Ranges

3.3.1 Steady State Board Voltages

	<u>6.9kV Switchgear</u>	<u>480V Switchgear/MCCs</u>
Max:	7260V (2)	508V (2)
Min:	6681V (1)	440V (2)

- (1) This is the reset operational limit for the degraded voltage relay (Sec. 3.12).
- (2) Per Table 1 of ANSI C84.1 (Ref. 2.23), Utilization Voltage Range B.

3.3.2 Minimum Operating Voltages

Running Motors

	<u>6.6kV**</u>	<u>460V*</u>
Max:	7260V	506V
Min:	5940V	414V

480V Static Loads

Max: 528V
Min: 432V (this voltage is conservative compared to the Range B utilization voltage of 424V in Ref. 2.23)

* NEMA MG1 Section 12.45 requires that motors shall operate with variation in voltage up to plus or minus 10% of rated voltage (Reference 2.24).

** Ref. 2.23, Utilization Voltage Range B.

3.3.3 Minimum Motor Starting Voltages

<u>6.6kV Motors</u>	<u>460V Motors</u>	<u>460V Air Comp</u>	<u>89-10 MOVs</u>	<u>Non 89-10 MOVs</u>
5280 (80%)*	391V (85%)**	368V (80%)**	Att. 11.5	368V (80%)**

** Percentages are based on 460V rated motor voltage. For motors rated other than 460V the same percentages are applicable. The minimum starting voltage for these motors may be different from the above voltage if it is based on manufacturer's data or test reports per Att. 11.4.

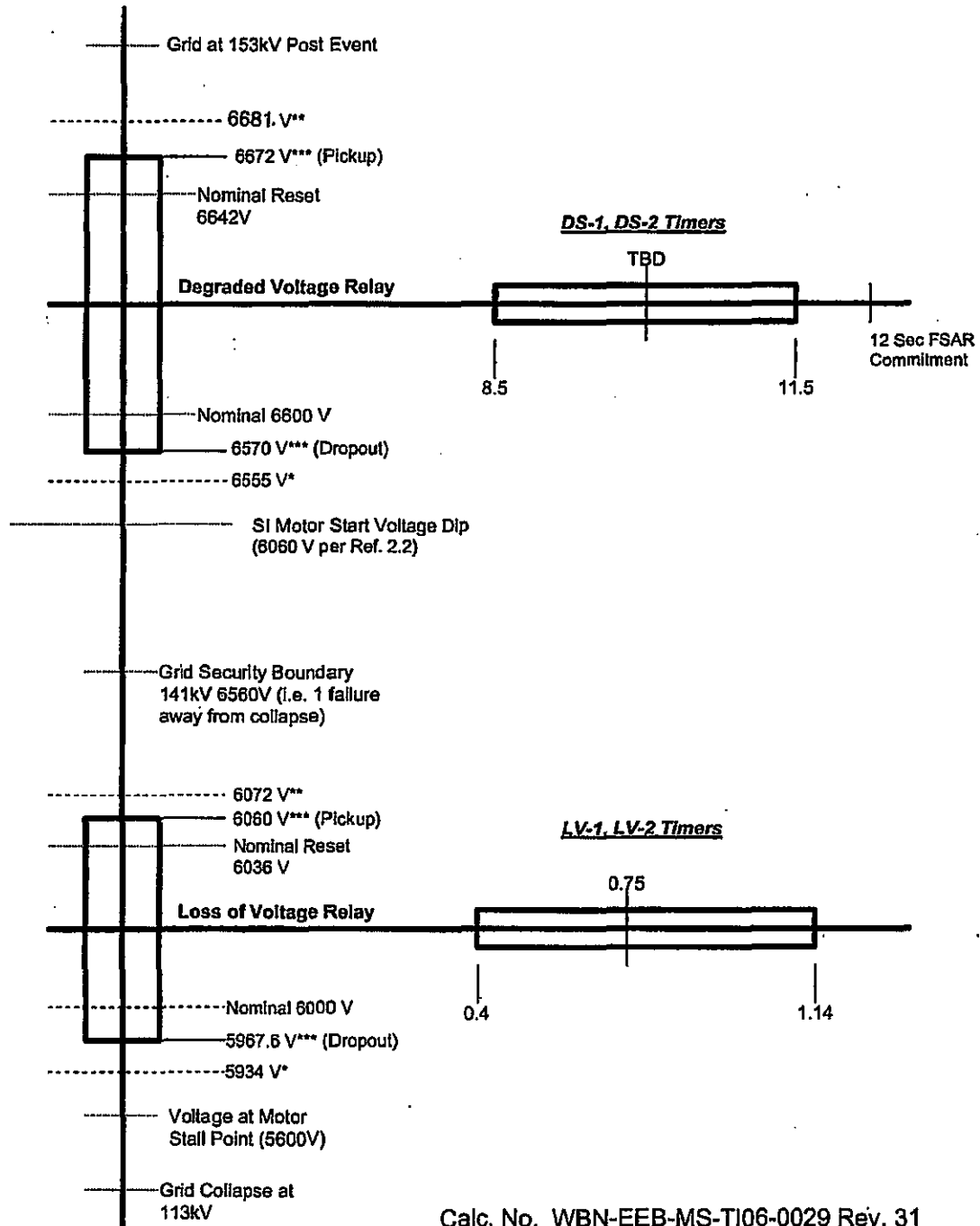
*** 80% for all motors except the for ERCW Pump motor which requires 90% and Aux Feedwater Pump motor which requires 85%. See Attachment 11.4 for motor starting voltage.

The minimum motor voltages for LV motors are based on the following:

Class 1E motors up to 30HP, NEMA Type B, provide 150 percent starting torque at full voltage which corresponds to close to 100 percent torque at 80 percent voltage (Ref. 2.24). For loads, such as fans, as the speed increases, so does the torque requirement. Other loads such as positive-displacement compressors start unloaded and do not require a

~~WBN-EEB-TI06-0029~~

Figure 8.3



Calc. No. WBN-EEB-MS-TI06-0029 Rev. 31
 This Sheet revised by Revision 31

Figure 8.3 - Degraded Voltage and Loss-of-Voltage Relay Setpoint

* Analytical Limit (Ref. 2.20)
 ** Operational Limit (Ref. 2.20)
 *** Allowable Value (Excludes PT accuracy - Ref. 2.16)

18-Feb-92

Attachment 10.5
Block Motor Start Data

17-Sep-92

WBN-EEB-MS-T106-0010 R0
ATTACHMENT 10.5 - BLOCK MOTOR START DATA

MOTOR NO.	BOARD NAME	COMP	MOTOR NAME	HP	FLI	LRA	LRF	MOTOR Zn	MOTOR Rn	MOTOR Jzn	CABLE NO.	CABLE SIZE	CABLE LENGTH	CABLE R	CABLE Jz	TOL NO.	TOL R	TOTAL R	TOTAL Jz	MIN START (Z)	ACCEL TIME SEC	VOLTAGE REQ	REV
*301	480V SDBD 2B1-B 3200	3C	CMPNT CL6 SYS PMP 2B-B	350.00	389.00	2084.0	0.30	0.1274	0.0382	0.1216	2PL4742B 2PL4743B	3-1C #500 3-1C #500	675	0.0314	0.0540			0.0106	0.0182	70	3.10	374.1	
*914	480V DSL AUX BD 2B1B	5A	DG 2B-B AIR CPRSR 2	5.00	7.10	44.5	0.62	5.9691	3.7002	4.6826	PL2225	1-3C #12	122	2.1500	0.0765	T39	0.0288	0.2911	0.0093	85		403.6	
*916	480V DSL AUX BD 2B1B	3A	EM DG ENG SUP VLV FROM HDR 1B	0.13	0.39	2.6	0.62	102.1466	63.3309	80.1444	PL2180B	1-3C #12	162	2.1500	0.0765	T8	13.9500	14.2983	0.0124	85		427.1	
*918	480V DSL AUX BD 2B1B	6A	DG 2B-B MUFFLER RM EXH FAN	1.50	2.65	20.0	0.62	13.2791	8.2330	10.4188	PL2255	1-3C #12	80	2.1500	0.0765	T29	0.2370	0.4090	0.0061	85		398.7	
921	480V DSL AUX BD 2B1B	2B	DG 2B-B RM EXH FAN FAN 1B	15.00	19.50	118.4	0.49	2.2427	1.0989	1.9550	PL2674B	1-3C #8	120	0.8490	0.0705	T49	0.0057	0.1076	0.0083	85		401.8	
*927	480V DSL AUX BD 2B1B	4D	DG RM 2B-B PNL VENT FAN	15.00	20.00	118.4	0.49	2.2427	1.0989	1.9550	PL3456B	1-3C #8	150	0.8490	0.0705	T48	0.0083	0.1357	0.0106	85		404.7	
928	480V CLA VT BD 2B1-B	3B	PIPE CHASE CLR FAN 2B-B	3.00	4.00	25.2	0.66	10.5389	5.9979	7.8803	2PL3081B	1-3C #10	460	1.3500	0.0705	T32	0.1000	0.7210	0.0324	85		410.1	
*931	480V CLA VT BD 2B1-B	5E	AFWPLBA XFR PMP SP CLR FAN B-B	15.00	19.00	133.5	0.49	1.9897	0.9749	1.7344	2PL3161B	1-3C #8	250	0.8490	0.0705	T49	0.0057	0.2180	0.0176	85		416.5	
*934	480V CLA VT BD 2B1-B	8B	PEN RM EL 692 CLR FAN 2B-B	3.00	4.30	26.7	0.62	9.9506	6.1694	7.8072	2PL3141B	1-3C #10	458	1.3500	0.0705	T32	0.1000	0.7183	0.0323	85		410.1	
935	480V CLA VT BD 2B1-B	2C	PEN RM EL 713 CLR FAN 2B-B	3.00	4.30	26.7	0.62	9.9506	6.1694	7.8072	2PL3121B	1-3C #10	306	1.3500	0.0705	T32	0.1000	0.5131	0.0216	85		404.5	
936	480V CLA VT BD 2B1-B	9E	PEN RM EL 737 CLR FAN 2B-B	3.00	4.00	24.6	0.66	10.7960	7.1361	8.1012	2PL3101B	1-3C #10	340	1.3500	0.0705	T32	0.1000	0.5590	0.0240	80	2.40	381.5	
942	480V CLA VT BD 2B1-B	12B	EG TRMT SYS B-B RM CLR FAN	3.00	4.10	27.0	0.53	9.8363	5.2133	8.3412	2PL3201B	1-3C #10	367	1.3500	0.0705	T32	0.1000	0.5955	0.0259	80	1.05	381.1	
*943	480V CLA VT BD 2B1-B	3D	AUX BLDG GAS TRTMT SYS FAN B-B	50.00	62.00	304.0	0.37	0.8736	0.3232	0.8116	2PL3768B	1-3C #2	350	0.2134	0.0615	T56	0.0012	0.0759	0.0215	75	9.10	364.8	
*1057	480V RX MOV BD 2B2-B	12B	CCS HX C DISCH VLV TO HDR B	0.67	1.90	7.6	0.60	35.1298	21.0779	28.1038	2V2791B	1-3C #12	342	2.1500	0.0765	T24	0.6320	1.3673	0.0262	85		400.5	
*1102	480V DSL AUX BD 2B2B	5A	DG 2B-B AIR CPRSR 1	5.00	7.25	44.5	0.62	5.9691	3.7002	4.6826	PL2230	1-3C #12	115	2.1500	0.0765	T39	0.0288	0.2760	0.0088	85		402.9	
*1104	480V DSL AUX BD 2B2B	2B	DG 2B-B RM EX FAN 2-B	15.00	19.50	118.4	0.49	2.2427	1.0989	1.9550	PL2683B	1-3C #8	114	0.8490	0.0705	T49	0.0057	0.1025	0.0080	85		401.3	
1119	480V RX MOV BD 1B2-B	5C	RCF DIL CLR SUP CNTMT ISOL VLV	0.13	0.60	3.5	0.60	75.8803	45.5282	60.7043	1VB808B 1VB918B	1-3C #10 1-3C #10	408 70	1.3500 1.3500	0.0705 0.0705	T11 T11	9.2500	9.8953	0.0337	85		423.7 IR4	
1120	480V RX MOV BD 1A1-A	9D	RCF DIL CLR SUP CNTMT ISOL VLV	0.13	0.60	3.5	0.60	75.8803	45.5282	60.7043	1VB15A 1VB17A	1-3C #12 1-3C #12	425 175	2.1500 2.1500	0.0765 0.0765	T11	9.2500	10.5400	0.0459	85		426.0 IR4	

THIS SHEET ADDED BY REV. 4

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401.3 IR4
426.0 IR4
2009-9-27-9

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18-Feb-92

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Attachment 10.6

480V Switchgear and Motor Control Center Motor Starting Voltages

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21-Sep-92

WBN-EEB-26-T106-0010 R0
 ATTACHMENT 10.6 - 10.6 VOLTAGE SWITCHgear MOTOR STARTING VOLTAGES

LINE TITLE	BOARD	COMP	EQUIPTD_NO	LOAD SF	FLI	LEN	LEFF	Zs	Rm	Xm	CABLE NO.	CABLE SIZE	LENG	Rc	Jsc	MOTOR MIN START VOLT SEC	ACCEL REMARKS	REV
LESS VOLTAGE =44.4V UNLESS NOTED OTHERWISE																		
Aux Blg 6th Exhaust Fan B	480V SKIN BD 282-B	7A	2-MTR-30-278	125.0	1.00	147.0	850	0.29	0.31245	0.09061	0.29002	2#15170	4/0	44	0.03059	0.02731	400.7	
Fuel Handling Exhaust Fan B	480V SKIN BD 282-B	7C	0-MTR-30-139	100.0	1.15	120.0	624	0.31	0.43581	0.13194	0.40464	2#15100	4/0	248	0.01709	0.01525	428.4	
480V Shutdown Bd RA ARI D-8	480V SKIN BD 282-B	9D	0-MTR-31-61-B	75.0	1.15	92.0	592	0.33	0.44862	0.14884	0.42349	2#15228	4/0	170	0.01171	0.01046	426.9	AMP FAIL
Station Fire Pmp 26-B	480V SKIN BD 282-B	4D	2-MTR-26-11-B	200.0	1.00	230.0	1179	0.27	0.22515	0.06079	0.21678	2#150178	500MCM	2889	0.04653	0.08070	323.4	PARALLEL COND
																		LESS VOLT=454.4

THIS SHEET ADDED BY REV 4

30-Oct-92

Prepared By G.C. P/RS Date 10-31-92
Checked By [Signature] Date 10-31-92

WBX-ZEB-M5-7106-0010 RD ATTACHMENT 10.6 - 480V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES
(TABLE 1) - UNIT 1 MCC MOTOR STARTING VOLTAGES FROM WBX-ZEB-M5-7106-0002 (R1)

Table with columns: ZAG_TITLE, NODE_NO, BOARD, COMPT NO, EQUIP19_NO, LOAD, FLI, LRA, LPP, Ia, Ra, jRa, OYR SIZE, Ktol, CABLE NO., CABLE SIZE LENG, Kc, jKc, IBD MOTOR START VOLT (140), BLOCK MOTOR START VOLT (432), MIN MOTOR START VOLT (5), ACCEL TIME (56), REMARKS, and XBY. The table lists various motor specifications and starting parameters for different equipment.

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[UNCOND] \$ MINIMUM MOTOR STARTING VOLTAGE = 15% OF 480V, EXCEPT NOTED. \$\$ ACCELERATION TIME IS AT 80% STARTING VOLTAGE, EXCEPT NOTED. * CABLE LENGTH USED IS DESIGN LENGTH PLUS 100 FEET. ** MAXIMUM CABLE LENGTH 1200 FEET

WBV-EEB-M5-Y106-0010 R0 ATTACHMENT 10.6 - 480V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES (TABLE 62 - UNIT 1 MCC MOTOR STARTING VOLTAGES FROM WBV-EEB-M5-Y106-0007 R10)

Table with columns: ENG Y1042, NODE_NO, BOARD, COMPT NO, EQUIP_ID_NO, LGAD, FLI, IFA, LPPF, Im, Km, Jm, OVAL, Ktel, CARC NO., CARC SIZE, KENG, Rc, jkc, IBS BLOCK MOTOR START VOLT, MIE MOTOR START VOLT, ACCEL TIME SEC, REMARKS, IIV. Rows include equipment like ERCK SCREEN WASH PUMP 1B-B, Toilet And Locker Rm Exh Fan, Dg 1A-1 Mtry Hood Exh Fan, etc.

(MINIMUM) \$ MINIMUM MOTOR STARTING VOLTAGE = 95% OF 480V, EXCEPT NOTED. \$€ ACCELERATION TIME IS AT 80% STARTING VOLTAGE, EXCEPT NOTED. * CABLE LENGTH USED IS DESIGN LENGTH PLUS 100 FEET. ** MAXIMUM CABLE LENGTH (1200 FEET)

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Pages 199 (Papers by Rad5)

EN-EEB-MS-7166-0010 R0 ATTACHMENT 10.6 - 480V SWITCHGEAR AND MOTOR CONTROL CIRCUIT MOTOR STARTING VOLTAGES
TABLE L2 - UNIT 1 MCC MOTOR STARTING VOLTAGES FROM WBN-EEB-MS-7166-0001 B10)

Table with columns: NG_TITLE, CODE_NO, BOARD, COMPT NO, EQUIP_ID_NO, LOAD, FLI, LRA, LRPV, Kc, Rn, jKc, OVLG SIZE, Stot, CABLE NO., CABLE SIZE LENG, Rr, jKc, MIN MOTOR START VOLT (440), MIN MOTOR START VOLT (437), MIN MOTOR START TIME (S), ACCCEL TIME (SS), REMARKS, REV.

WBN/EEB-ED-Q000-999-2007-0002, R0

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(DIM'ED) S MINIMUM MOTOR STARTING VOLTAGE = 85% OF 460V, EXCEPT NOTED. SS ACCELERATION TIME IS AT 80% STARTING VOLTAGE, EXCEPT NOTED. * CABLE LENGTHS USED IS DESIGN LENGTH PLUS 100 FEET. ** MAXIMUM CABLE LENGTH <1200 FEET

THIS SHEET ADDED BY REV 6

Page 18/4
(Added by R005)

Prepared By: S.C.P./R.S. Date: 10-31-02
Checked By: [Signature]

30-Oct-02

WBN-EEB-95-1100-0010 R0 ATTACHMENT 10.6 - 480V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES
(TABLE 12 - 480V 1 MCC MOTOR STARTING VOLTAGES FROM WBN-EEB-95-1100-0007 R10)

Table with columns: ZIG_VTYPE, MODEL_NO, BOARD, CODE, EQUIP_ID, LOAD, PUL, LBS, GRP, Ia, Ib, jIa, jIb, OVD, Rtd, CABLE TO, CABLE SIZE, CABLE SIZE, Kc, jlc, LEO, BLOCK, HIX, RECURS, MTR. Rows include equipment like RCP TRAN, XRES, RER, SPCS, etc.

UNCONNECTED \$ MINIMUM MOTOR STARTING VOLTAGE = 85% OF WVT, EXCEPT BUBBLE. \$\$ ACCELERATION TIME IS AT 80% STARTING VOLTAGE, EXCEPT BUBBLE. * CABLE LENGTH USED IS DESIGN LENGTH PLUS 100 FEET. ** MAXIMUM CABLE LENGTH C1200 FEET

EN-EEB-M5-7106-0010 R0 ATTACHMENT 10.6 - 480V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES
TABLE L2 - HWY 1 MCC MOTOR STARTING VOLTAGES FROM REF-EEB-M5-7106-0002 R18)

Table with columns: JO_TITLE, NODE_NO, BOARD, COMPT NO, EQUIP_ID_NO, LOAD, FLI, IRR, LRPP, Ia, Rn, jIc, OVID SIZE, Rto, CABLE NO., CABLE SIZE LENG, Rc, jIc, IFR MOTOR START (440), BLOCK MOTOR START (432), MIN MOTOR START (s), ACCEL TIME (SS), REMARKS, REV.

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MINIMUM MOTOR STARTING VOLTAGE = 85% OF 480V, EXCEPT NOTED. SS ACCELERATION TIME IS AT 80% STARTING VOLTAGE, EXCEPT NOTED. * CABLE LENGTHS USED IS DESIGN LENGTH PLUS 100 FEET. ** MAXIMUM CABLE LENGTHS <1000 FEET

THIS SHEET ADDED BY REV 6

PAGE 186A (ADDED BY REV 5)

30-Oct-12

ATTACHMENT 10.5 - 100V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES (TABLE 62 - GRAY 1 MCC MOTOR STARTING VOLTAGES FROM REV-RES-MS-VI06-Q002 21A)

Table with columns: TAG, VOLTAGE, BOARD, COMPT, EQUIP ID, NO, CORR, PH, WVA, LERP, Ia, Ra, jRa, OVL, PLO, CABLE NO, CABLE SIZE, LENO, BE, jbc, JTB BLOCK, MOTOR, MOTOR VOLT, REMAINS, VOLT, START, VOLT, SEC, VOLT, VOLT, VOLT, (4100) (432) (5) (58)

REVISION: Prepared By: GSP/RS Date: 10-31-12 Checked By: [Signature]

REVISION: \$ MINIMUM MOTOR STARTING VOLTAGE = 85% OF 480V, EXCEPT NOTED. \$\$ ACCELERATION TIME IS IN 60% STARTING VOLTAGE, EXCEPT NOTED. * CABLE LENGTH USED IS DESIGN LENGTH PLUS 100 FEET. ** MAXIMUM CABLE LENGTH 6140 FEET

WBNEEB-MS-T104-0010 R10 ATTACHMENT 10.6 - 480V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES (TABLE C3 - UNIT 2 MCC MOTOR STARTING VOLTAGES FROM WBNEEB-MS-T104-0002 R18)

Table with columns: ENG TITLE, NODE_NO, BOARD, COMPT NO, EQUIP_ID_NO, LOAD, FLI, LRA, LPPF, Zm, Rm, Xm, OALD SIZE, RunI, CABLE NO., CABLE SIZE LENG, Rr, Dc, IND MOTOR START VOLT (440) (A15) (\$)(%), BLOCK MIN MOTOR START SEC, ACCEL MOTOR START SEC, REMARKS, REV.

THIS SHEET ADDED BY REV. 4

WBNEEB-ED-Q000-999-2007-0002, R0

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Calc. STUDY-EEB-WBN-12-001 Attachment 3 Required Motor Starting Voltage Page 23 of 26

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WARNING: A MOTOR MUST START UNDER ONE OF THE FOLLOWING CONDITIONS: 1. ACCELERATION TIME IS AT OR ABOVE STARTING TIME. 2. EXCEEDS MOTOR RATED CURRENT. 3. CABLE LENGTH EXCEEDS 100 FEET. 4. MAXIMUM LENGTH PER 1000 FEET

WBN-EEB-MS-T106-0010 R10 ATTACHMENT 10.6 - 480V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES
(TABLE L3 - UNIT 2 MCC MOTOR STARTING VOLTAGES FROM WBN-EEB-MS-T106-0002 R10)

Table with columns: ENG TITLE, HOSE_NO, BOARD, COMPT NO, EQUIP_ID_NO, LOAD, FLI, LRA, LRF, Za, Rm, Dm, GFLD SIZE, Rvol, CABLE NO., CABLE SIZE LENG, Rc, Dxc, IND MOTOR START (440), BLOCK MOTOR START (415), MIN MOTOR START (400), ACCEL TIME (80%), REV, REMARKS. Rows include various equipment like Elec Bd Rm A/C Sys Oil Pmp, Dg 2A-A Btry Hood Exh Fan, Dg 2B-B Btry Hood Exh Fan, etc.

THIS SHEET ADDED BY REV. 4

WBN-EEB-ED-Q000-999-2007-0002, R0

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MINIMUM & MAXIMUM MOTOR STARTING VOLTAGE - 95% OF FLN CURRENT LIMITED BY MOTOR CAPACITY THE IS BY MOTOR STARTING VOLTAGE CURRENT LIMITED + FAN & PUMPS (USED TO DETERMINE LENGTH OF LINE TO MOTOR) MINIMUM LENGTH OF LINE TO MOTOR IS 100 FEET + MAXIMUM LENGTH OF LINE TO MOTOR IS 1000 FEET

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WBN-EEB-WB-T106-0010 R10 ATTACHMENT 10.6 - 480V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES (TABLE L3 - UNIT 2 REL MOTOR STARTING VOLTAGES FROM WBN-EEB-WB-T106-0002 R02)

15-Sep-72

Table with columns: ENG TITLE, MODE NO, BOARD, COPIED EQUIPID NO, LOAD, FLI, LBA, LRF, ZA, BA, JMA, OLD, ROL, CABLE NO., CABLE SIZE, CABLE LENGTH, BC, JAC, MOTOR START TIME, MIN, MAX, REMARKS, REV.

WBN-EEB-WB-T106-0010 R10 ATTACHMENT 10.6 - 480V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES. ** MAXIMUM LENGTH PLUS 1200 FEET.

THIS SHEET ADDED BY REV. 4

WBN-EEB-W5-T106-0010 R16 ATTACHMENT 10.6 - 480V SWITCHGEAR AND MOTOR CONTROL CENTER MOTOR STARTING VOLTAGES
(TABLE L3 - UNIT 2-MCC MOTOR STARTING VOLTAGES FROM WBN-EEB-W5-T106-0002 R16)

ENG TITLE	MODE NO	BOARD	COMPT NO	EQUIPID NO	LOAD	FLI	LRA	LRF	Z _s	R _s	X _s	DVLD SIZE	R ₁₀₁	CABLE NO.	CABLE SIZE LENG	R _c	J _{sc}	IND MOTOR START (440)	BLOCK MOTOR START (415)	MIN MOTOR START (\$)	ACCEL TIME SEC	REMARKS	REV
CCS Hr C Disch Vlv To Hdr B	242	RMOV BD 282-B	128	0-FCV-67-152-B	0.67	1.90	7.56	0.60	35.1298	21.0779	28.1038	T24	0.63200	2V2791B	#12	342	0.7353	0.0262	429.5	405.1		VALVE	
Annulus Spr Isln Vlv	242	RMOV BD 282-B	12F	2-FCV-26-244-B	0.67	2.80	16.0	0.60	16.5988	9.9593	13.2791	T24	0.63200	2V9170B	#14	700	2.3891	0.0578	392.4				
Sply Hdr 2B To Hdr 1A Isln Vlv	242	RMOV BD 282-B	13A	2-FCV-67-147-B	0.70	2.30	12.00	0.60	22.1318	13.2791	17.7054	T26	0.42100	2V2428B	#12	494	1.0621	0.0378	421.9				
CCS Hr B & C Inlet Isln Vlv	242	RMOV BD 282-B	13B	2-FCV-70-14-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	2V2526B	#12	572	1.2298	0.0438	416.3				
RHR Hr B Hdr Inlet Vlv	242	RMOV BD 282-B	14B	2-FCV-70-3-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	2V2466B	#12	386	0.8299	0.0295	418.6				
CCSP 2AA428B To C-5 Outl Iso V	242	RMOV BD 282-B	140	2-FCV-70-28-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	2V2532B	#12	566	1.2169	0.0433	416.4				
CCS Pmps 2A-A To 2B-B Isln Vlv	242	RMOV BD 282-B	145	2-FCV-70-39-B	0.67	1.90	7.56	0.60	35.1298	21.0779	28.1038	T24	0.63200	2V3228B	#12	566	1.2169	0.0433	425.8				TELAS R11
RHR Hr B Rtn Hdr Isln Vlv	242	RMOV BD 282-B	15A	2-FCV-70-75-B	0.33	0.75	5.70	0.60	46.5932	27.9559	37.2745	T14	4.72000	2V1970B	#12	704	1.5136	0.0539	405.0				
CCS Hr B & C Outlet Isln Vlv	242	RMOV BD 282-B	15B	2-FCV-70-196-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	2V2484B	#12	366	0.7869	0.0280	418.8				
CCSP 2AA428B To C-5 Inlt Iso V	242	RMOV BD 282-B	15D	2-FCV-70-78-B	0.67	1.90	7.56	0.60	35.1298	21.0779	28.1038	T24	0.63200	2V2544B	#12	570	1.2255	0.0436	425.7				TELAS R11
RHR Hr B-B Outlet Vlv	242	RMOV BD 282-B	15E	2-FCV-70-153-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	2V2556B	#12	470	1.0105	0.0360	417.5				
CCSP 2AA428B To C-5 Inlt Iso V	242	RMOV BD 282-B	16A	2-FCV-70-76-B	0.67	1.90	7.56	0.60	35.1298	21.0779	28.1038	T24	0.63200	2V2550B	#12	560	1.2040	0.0428	425.9				TELAS R11
SFPCS Hr Sply Hdr Isln Vlv	242	RMOV BD 282-B	17A	0-FCV-70-194-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	2V2514B	#12	416	0.8944	0.0318	418.2				
CCSP 2AA428B To C-5 Outl Iso V	242	RMOV BD 282-B	17B	2-FCV-70-29-B	0.33	0.95	5.70	0.60	46.5932	27.9559	37.2745	T16	2.95000	2V2538B	#12	556	1.1954	0.0425	416.5				
480V Bd Rn 2B A/C Crsr 2B-B	242	RMOV BD 282-B	180	2-HTR-31-447-B	75.00	90.00	526.2	0.33	0.5047	0.1666	0.4764			2PL3860B	#2	170	0.0363	0.0105	421.0				AMP FAIL
Waste Gas Crsr Pkg B	245	RX VENT BD 28-A	66	0-HTR-77-105	25.00	30.00	197.4	0.43	1.3454	0.5785	1.2147	T53	0.00226	2PL5460	#6	640	0.3416	0.0442	379.3				FAILED NON-IE
<u>Cont Bay Supp Pkg 1</u>	246	RX VENT BD 28-B	6F1	2-HTR-40-2	5.00	7.25	46.0	0.62	5.7735	3.5796	4.5299			2PL695	#10	976	1.3176	0.0688	378.1				FAILED NON-IE
COMPUTER ROOM AHU NO. 2	246	RX VENT BD 28-B	11B	0-HTR-31-498	7.50	9.60	60.0	0.57	4.4264	2.5230	3.6369	T41	0.01808	2PL3901	#6	1180	0.6299	0.0814	398.5				

THIS SHEET ADDED BY REV. 4

Calculation No.:

ATTACHMENT 11.9

Required Voltage 89-10 MOV's - Unit 1 Page 1 of 9

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Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

VALVEID	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
0-FCV-067-0144	B	SS SS	O to C C to O	C = 388.3 O = 388.3	Steady State Voltage
0-FCV-067-0152	B	0 SS	C to O O to C	O = 395.1 C = 414	Need Best avail Voltage at t=0 sec from SI
0-FCV-067-0205	A	SS SS	O to C C to O	C = 429.9 O = 429.9	Steady State Voltage
0-FCV-067-0208	B	SS SS	O to C C to O	C = 428.9 O = 428.9	Steady State Voltage
0-FCV-070-0194	B	SS SS	O to C C to O	C = 440.9 O = 440.9	Steady State Voltage
0-FCV-070-0197	A	SS SS	O to C C to O	C = 439.1 O = 439.1	Steady State Voltage
1-FCV-001-0015	A	SS SS	O to C C to O	C = 414 O = 414	Steady State Voltage
1-FCV-001-0016	A	SS SS	O to C C to O	C = 414 O = 414	Steady State Voltage
1-FCV-001-0017	A	SS SS	O to C C to O	C = 408.1 O = 408.1	Steady State Voltage
1-FCV-001-0018	B	SS SS	O to C C to O	C = 413.3 O = 413.3	Steady State Voltage
1-FCV-001-0051	S	0 SS	C to O O to C	O = 90.49 C = 90.49	125 V DC Motor, Need Best Avail Voltage at T=0 sec from SI
1-FCV-003-0033	A	0 4 SS	O to C O to C C to O	C = 322 C = 389.5 O = 414	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=4 sec forward from SI (normally open MOV). Need SS voltage for non-safety related opening stroke.
Motor Brake (1-FCV-003-0033)	A	0	energize	368	Needs 80% of 460 voltage @ T=0
1-FCV-003-0047	B	0 4 SS	O to C O to C C to O	C = 322 C = 381.5 O = 414	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=4 sec forward from SI (normally open MOV). Need SS voltage for non-safety related opening stroke.
Motor Brake (1-FCV-003-0047)	B	0	energize	368	Needs 80% of 460 voltage @ T=0

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Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

VALVEID	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
1-FCV-003-0087	A	0 4 SS	O to C O to C C to O	C = 322 C = 377.0 O = 403.0	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=4 sec forward from SI (normally open MOV). Need SS voltage for non-safety related opening stroke.
Motor Brake (1-FCV-003-0087)	A	0	energize	368	Needs 80% of 460 voltage @ T=0
1-FCV-003-0100	B	0 4 SS	O to C O to C C to O	C = 322 C = 381.5 O = 414	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=4 sec forward from SI (normally open MOV). Need SS voltage for non-safety related opening stroke.
Motor Brake (1-FCV-003-0100)	B	0	energize	368	Needs 80% of 460 voltage @ T=0
1-FCV-003-0116A	A	SS SS	C to O O to C	O = 383.6 C = 383.6	Steady State Voltage
1-FCV-003-0116B	A	SS SS	C to O O to C	O = 383.6 C = 383.6	Steady State Voltage
1-FCV-003-0126A	B	SS SS	C to O O to C	O = 381.9 C = 381.9	Steady State Voltage
1-FCV-003-0126B	B	SS SS	C to O O to C	O = 382 C = 382	Steady State Voltage
1-FCV-003-0136A	A	SS SS	C to O O to C	O = 386.3 C = 386.3	Steady State Voltage
1-FCV-003-0136B	A	SS SS	C to O O to C	O = 386.3 C = 386.3	Steady State Voltage
1-FCV-003-0179A	B	SS SS	C to O O to C	O = 384.5 C = 384.5	Steady State Voltage
1-FCV-003-0179B	B	SS SS	C to O O to C	O = 384.5 C = 384.5	Steady State Voltage
1-FCV-026-0240	A	0 5 SS	O to C O to C C to O	C = 322 C = 403.5 O = 427.2	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-026-0243	A	0 5 SS	O to C O to C C to O	C = 322 C = 409.7 O = 422.4	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-062-0061	B	0 5 SS	O to C O to C C to O	C = 322 C = 386.6 O = 393.7	Need 70% Voltage at t=0 sec Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).

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Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

VALVEID	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
1-FCV-062-0063	A	0 5 SS	O to C O to C C to O	C = 322 C = 381.1 O = 409.2	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-062-0090	A	0 5 SS	O to C O to C C to O	C = 322 C = 414 O = 414	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-062-0091	B	0 5 SS	O to C O to C C to O	C = 322 C = 414 O = 414	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-062-0138	B	SS SS	C to O O to C	O = 407.5 C = 407.5	Steady State Voltage
1-FCV-063-0001	A	SS SS	O to C C to O	C = 413.5 O = 413.5	Steady State Voltage
1-FCV-063-0003	A	SS SS	O to C C to O	C = 400.5 O = 400.5	Steady State Voltage
1-FCV-063-0004	B	SS SS	O to C C to O	C = 390 O = 390	Steady State Voltage
1-FCV-063-0005	B	SS SS	O to C C to O	C = 399.5 O = 399.5	Steady State Voltage
1-FCV-063-0006	B	SS SS	C to O O to C	O = 401.1 C = 401.1	Steady State Voltage
1-FCV-063-0007	A	SS SS	C to O O to C	O = 403.5 C = 403.5	Steady State Voltage
1-FCV-063-0008	A	SS SS	C to O O to C	O = 429.8 C = 429.8	Steady State Voltage
1-FCV-063-0011	B	SS SS	C to O O to C	O = 415.7 C = 415.7	Steady State Voltage
1-FCV-063-0022	B	SS SS	O to C C to O	C = 401.4 O = 401.4	Steady State Voltage
1-FCV-063-0025	B	0 SS	C to O O to C	O = 361.8 C = 414	Need Best avail Voltage at t=0 sec from SI for opening stroke, need steady state for closing stroke.

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Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

VALVEID	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
1-FCV-063-0026	A	0 SS	C to O O to C	O = 343.4 C = 414	Temporary minimum requirement in support of DCN 52837 Stage 2. Need Best avail Voltage at t=0 sec from SI for opening stroke, need steady state for closing stroke.
		0 SS	C to O O to C	O = 370 C = 414	Long term minimum requirement in support of DCN 52837 Stage 3. Need Best avail Voltage at t=0 sec from SI for opening stroke, need steady state for closing stroke.
1-FCV-063-0047	A	SS SS	O to C C to O	C = 403 O = 403	Steady State Voltage
1-FCV-063-0048	B	SS SS	O to C C to O	C = 418.8 O = 418.8	Steady State Voltage
1-FCV-063-0072	A	SS SS	C to O O to C	O = 404.3 C = 404.3	Steady State Voltage
1-FCV-063-0073	B	SS SS	C to O O to C	O = 408.7 C = 408.7	Steady State Voltage
1-FCV-063-0093	A	SS SS	C to O O to C	O = 419.6 C = 419.6	Steady State Voltage
1-FCV-063-0094	B	SS SS	C to O O to C	O = 418.2 C = 418.2	Steady State Voltage
1-FCV-063-0152	A	SS SS	O to C C to O	C = 405.8 C = 405.8	Steady State Voltage
1-FCV-063-0153	B	SS SS	O to C C to O	C = 405.8 O = 405.8	Steady State Voltage
1-FCV-063-0156	A	SS SS	C to O O to C	O = 412.7 C = 412.7	Steady State Voltage
1-FCV-063-0157	B	SS SS	C to O O to C	O = 414 C = 414	Steady State Voltage
1-FCV-063-0172	B	SS SS	C to O O to C	O = 396.7 C = 396.7	Steady State Voltage
1-FCV-063-0175	B	SS SS	O to C C to O	C = 390.7 O = 390.7	Steady State Voltage
1-FCV-067-0083	B	0 5 SS	O to C O to C C to O	C = 322 C = 395.1 O = 404.3	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).

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Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

VALVEID	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
1-FCV-067-0087	A	0 5 SS	O to C O to C C to O	C = 322 C = 392.4 O = 399.6	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0088	B	0 5 SS	O to C O to C C to O	C = 322 C = 392.2 O = 401.3	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0089	A	0 5 SS	O to C O to C C to O	C = 322 C = 386.7 O = 393.6	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0091	B	0 5 SS	O to C O to C C to O	C = 322 C = 392.4 O = 401.5	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0095	A	0 5 SS	O to C O to C C to O	C = 322 C = 391.6 O = 398.5	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0096	B	0 5 SS	O to C O to C C to O	C = 322 C = 392.8 O = 401.9	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0097	A	0 5 SS	O to C O to C C to O	C = 322 C = 385.9 O = 393	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0099	A	0 5 SS	O to C O to C C to O	C = 322 C = 393.9 O = 401.2	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0103	B	0 5 SS	O to C O to C C to O	C = 322 C = 388 O = 397	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0104	A	0 5 SS	O to C O to C C to O	C = 322 C = 394.3 O = 401.6	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0105	B	0 5 SS	O to C O to C C to O	C = 322 C = 383.1 O = 392	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0107	A	0 5 SS	O to C O to C C to O	C = 322 C = 395.3 O = 402.7	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).

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Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

VALVEID	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
1-FCV-067-0111	B	0 5 SS	O to C O to C C to O	C = 322 C = 389.4 O = 398.5	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0112	A	0 5 SS	O to C O to C C to O	C = 322 C = 395.7 O = 403.1	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0113	B	0 5 SS	O to C O to C C to O	C = 322 C = 384.3 O = 393.2	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-067-0123	B	SS SS	C to O O to C	O = 436.3 C = 436.3	Steady State Voltage
1-FCV-067-0124	B	SS SS	C to O O to C	O = 433.0 C = 433.0	Steady State Voltage
1-FCV-067-0125	A	SS SS	C to O O to C	O = 438.2 C = 438.2	Steady State Voltage
1-FCV-067-0126	A	SS SS	C to O O to C	O = 435.3 C = 435.3	Steady State Voltage
1-FCV-067-0143	A	SS SS	C to O O to C	O = 388.4 C = 388.4	Steady State Voltage
1-FCV-067-0146	A	SS SS	C to O O to C	O = 431 C = 431	Steady State Voltage
1-FCV-068-0332	B	SS SS	C to O O to C	O = 399.9 C = 399.9	Steady State Voltage
1-FCV-068-0333	A	SS SS	C to O O to C	O = 412 C = 412	Steady State Voltage
1-FCV-070-0087	B	0 5 SS	O to C O to C C to O	C = 322 C = 391 O = 403.6	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-070-0089	B	0 5 SS	O to C O to C C to O	C = 322 C = 391.0 O = 426.4	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).

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Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

VALVEID	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
1-FCV-070-0090	A	0 5 SS	O to C O to C C to O	C = 322 C = 398.5 O = 405.8	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-070-0092	A	0 5 SS	O to C O to C C to O	C = 322 C = 400.6 O = 428.0	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-070-0100	A	0 5 SS	O to C O to C C to O	C = 322 C = 393.4 O = 416.6	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-070-0133	A	0 12 SS	O to C O to C C to O	C = 322 C = 414 O = 414	Need 70% Voltage at t=0 sec, Need best Avail Voltage at t=12 sec forward from SI (Normally Open MOV)
1-FCV-070-0134	B	0 12 SS	O to C O to C C to O	C = 322 C = 414 O = 414	Need 70% Voltage at t=0 sec, Need best Avail Voltage at t=12 sec forward from SI (Normally Open MOV)
1-FCV-070-0140	B	0 5 SS	O to C O to C C to O	C = 322 C = 391.9 O = 427.4	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-070-0143	A	0 5 SS	O to C O to C C to O	C = 322 C = 398.5 O = 425.7	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
1-FCV-070-0153	B	SS SS	C to O O to C	O = 391.0 C = 391.0	Steady State Voltage; Active safety function is to operate from close/throttle position to open position.
1-FCV-070-0156	A	SS SS	C to O O to C	O = 434.8 C = 434.8	Steady State Voltage
1-FCV-070-0183	A	SS SS	O to C C to O	C = 395.1 O = 395.1	Steady State Voltage
1-FCV-070-0215	A	SS SS	O to C C to O	C = 395.4 O = 395.4	Steady State Voltage
1-FCV-072-0002	B	5 SS	C to O O to C	O = 412.7 C = 415	Time Delay added per DCN 52834, need best avail Voltage at t=5 sec from SI
1-FCV-072-0013	B	10 SS	C to O O to C	O = 414 C = 414	Need Best Avail Voltage at t= 10 sec from SI (MOV will not get a signal to open until after time delay per DCN 52834)
1-FCV-072-0021	B	SS SS	O to C C to O	C = 402.2 O = 402.2	Steady State Voltage

R73

Calculation No.:
WBNEEBEDQ1999010001

ATTACHMENT 11.9
JOG Review Plan

Required Voltage 89-10 MOV's - Unit 1
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Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

VALVEID	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
1-FCV-072-0022	A	SS SS	O to C C to O	C = 400.2 O = 400.2	Steady State Voltage
1-FCV-072-0034	A	10 SS	C to O O to C	O = 414 C = 414	Need Best Avail Voltage at t= 10 sec from SI (MOV will not get a signal to open until after time delay per DCN 52834)
1-FCV-072-0039	A	5 SS	C to O O to C	O = 411.3 C = 415	Time Delay added per DCN 52834, need best avail Voltage at t=5 sec from SI
1-FCV-072-0040	A	SS SS	C to O O to C	O = 405.7 C = 405.7	Steady State Voltage
1-FCV-072-0041	B	SS SS	C to O O to C	O = 396 C = 396	Steady State Voltage
1-FCV-072-0044	A	SS SS	C to O O to C	O = 414 C = 414	Steady State Voltage
1-FCV-072-0045	B	SS SS	C to O O to C	O = 414 C = 414	Steady State Voltage
1-FCV-074-0001	A	SS SS	O to C C to O	O = 414 C = 414	Steady State Voltage
1-FCV-074-0002	B	SS SS	C to O O to C	O = 414 C = 414	Steady State Voltage
1-FCV-074-0003	A	SS SS	O to C C to O	C = 424.2 O = 424.2	Steady State Voltage
1-FCV-074-0008	A	SS SS	O to C C to O	C = 414 O = 414	Steady State Voltage
1-FCV-074-0009	B	SS SS	O to C C to O	C = 419.4 O = 419.4	Steady State Voltage
1-FCV-074-0012	A	0 SS	C to O O to C	O = 345.4 C = 393.7	Need Best avail Voltage at t=0 sec from SI (OPEN); and SS (CLOSED)
1-FCV-074-0021	B	SS SS	O to C C to O	C = 422.3 O = 422.3	Steady State Voltage
1-FCV-074-0024	B	0 SS	C to O O to C	O = 347.2 C = 383.8	Need Best avail Voltage at t=0 sec from SI (OPEN); and SS (CLOSED)
1-FCV-074-0033	A	SS SS	O to C C to O	C = 394.6 O = 394.6	Steady State Voltage

Calculation No.:
 WBNEEBEDQ1999010001

ATTACHMENT 11.9
 JOG Review Plan

Mechanical Degraded Voltage Time Requirements for GL 89-10 MOVs

VALVEID	Train	T(sec) from SI: 0, 4, 5, 10 or SS See Notes	MOV Position Change	Required Voltage	Comments (also, see Notes Section)
1-FCV-074-0035	B	SS	O to C	C = 383	Steady State Voltage
		SS	C to O	O = 383	
1-LCV-062-0132	A	0	O to C	C = 322	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
		5	O to C	C = 394.3	
		SS	C to O	O = 414	
1-LCV-062-0133	B	0	O to C	C = 322	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec forward from SI (Normally open MOV).
		5	O to C	C = 401.6	
		SS	C to O	O = 414	
1-LCV-062-0135	A	0	C to O	O = 383	Need Best avail Voltage at t=0 sec from SI
		SS	O to C	C = 409.3	
1-LCV-062-0136	B	0	C to O	O = 343	Need Best avail Voltage at t=0 sec from SI
		SS	O to C	C = 383.3	
Notes:					
1) The maximum required voltage for any GL 89-10 MOV is equal to or above 90% of 460 v (414 v). Guidance given in Design Standard DS-M18.2.21 states that for voltages 90% or greater the voltage factor is 1.0 (i.e. no degradation is required at 90% or above). Therefore, there will be no impact to any Mechanical MOV calculations as long as 90% of 460 v (414 v) is met.					
2) Required voltage for MOVs at T = 0, T = 4, T = 5 or T = 10 sec is the minimum available voltage from the time specified to any time forward during the SI. Example: If a 4 sec voltage was requested and voltage dropped at 5 sec, then the lower 5 sec voltage should be used to bound degraded voltage.					
3) For MOVs that are open and go closed upon receiving an SI signal the required voltage at T = 0 is only 70% of 460 v (322 v) until the valve becomes loaded. MOVATs differential pressure test traces were reviewed and conservative bounding times were determined for when the MOV becomes loaded. A 70% starting voltage is based on guidance provided in Limitorque Technical Update 98-01 in Vendor Manual WBN-VTD-L200-0460.					
The voltages listed in this Attachment must be met or exceeded.					
R73	Prepared By: William F. Cetta	Date: 11/11/11	Reviewed By: Jerry V. Mills	Date: 11/11/11	R73

1A BOARDS

ETAP Node ID	MOV	Available Voltage (New Analysis) Value from SS	Time from SI Signal (SS = steady state)	New Design Margin (using new Voltages) (open)	New Design Margin (using new Voltages) (closed)	Comments**
235-5B	RHR Sys Isln Vlv 1-FCV-74-1-A (2.6HP)	90.74*	SS	13.30%	18.80%	Acceptable Margin
235-6D	RCS Press Relief FCV 1-FCV-68-333-A (1.9HP)	89.20*	SS	19.90%	15.80%	Acceptable Margin
235-11B	RHR Hx A To CVCS Chrgr Pmp 1-FCV-63-8-A (1.9HP)	87.48	SS	13.20%	124.60%	Acceptable Margin
235-12A	SIS Pmp 1A-A Inlet Vlv 1-FCV-63-47-A (1.9HP)	88.18*	SS	19.60%	16.10%	Acceptable Margin
235-12D	SIS To RCS Loops 2&3 FCV 1-FCV-63-93-A (1.6 HP)	88.65	SS	18.60%	140.30%	Acceptable Margin
235-12E	SIS Pmp 1A-A Outlet FCV 1-FCV-63-152-A (1.9HP)	88.48*	SS	29.50%	39.40%	Acceptable Margin
235-13A	SIS Pmp Out RCS Lp 1&3 Hot Leg 1-FCV-63-156-A (1.9HP)	89.28*	SS	15.40%	15.90%	Acceptable Margin
235-13B	Cntmt Sump To Spray Hdr 1A FCV 1-FCV-72-44-A (3.2HP)	90.33*	SS	35.50%	105.93%	Acceptable Margin
235-14A	RHR Spray Hdr 1A Isln Vlv 1-FCV-72-40-A (1.9HP)	87.66	SS	75.20%	121.90%	Acceptable Margin
235-14E	RHR Hx 1A Bypass Vlv 1-FCV-74-33-A (2HP)	85.27	SS	79.30%	45.10%	Acceptable Margin
236-9D	Up Cntmt Clr 1A Disc Iso Vlv 1-FCV-67-295 (0.13HP)	81.98	Not 89-10	28.96%	28.96%	Acceptable Margin
236-2D	AFWP Turb Stm Sup Fm Strm Gen 1 1-FCV-1-15-A (1HP)	92.47*	SS	14.50%	35.40%	Acceptable Margin
236-5E	Cntmt Spray Hx 1A Sup Cont Vlv 1-FCV-67-125-A (0.33HP)	92.51*	SS	24.40%	24.40%	Acceptable Margin
236-5F	Cntmt Spray Hx 1A Disch Vlv 1-FCV-67-126-A (0.33HP)	92.19*	SS	24.40%	24.40%	Acceptable Margin
236-6A	AFWP Turb St Sply Frm St gen 4 1-FCV-1-16-A (1HP)	92.52*	SS	14.50%	35.40%	Acceptable Margin
236-6D	RHR Sys Isln Bypass Vlv 1-FCV-74-8-A (1.6HP)	90.99*	SS	17.50%	42.40%	Acceptable Margin
236-11A	Cmpnt Clg Hx A Disch Cont Vlv 1-FCV-67-146-A (0.3HP)	87.97	SS	13.50%	13.50%	Acceptable Margin
236-17B	SFPCS Hx Sply Hdr Isln Vlv 0-FCV-70-197-A (0.3HP)	89.63	SS	28.10%	28.10%	Acceptable Margin
235-11A	SIS Pmp Inlet To CVCS Chrgr Pmp 1-FCV-63-7-A (1.9HP)	88.21*	SS	9.40%	105.40%	Acceptable Margin
235-12B	Cntmt Sump To RHR Pmp A-A 1-FCV-63-72-A (13HP)	85.00	SS	21.50%	1781.80%	Acceptable Margin
236-12B	SS&Con AirCpsr Sup Hdr A Iso V 0-FCV-67-205-A (0.33.9HP)	86.86	SS	78.40%	78.40%	Acceptable Margin
236-16E	RHR Hx A-A Outlet Vlv 1-FCV-70-156-A (0.33.9HP)	87.86	SS	24.40%	24.40%	Acceptable Margin
203-7D	RHR PMP 1A-A INLET FCV 1-FCV-74-3-A (5.2HP)	90.31	SS	125.80%	2250.80%	Acceptable Margin
203-7E	RWST TO SPRAY HDR 1A FCV 1-FCV-72-22-A (3.2HP)	85.27	SS	273.70%	266.60%	Acceptable Margin
* Calculated voltage considering Hammer Blow feature (using 50% LRC during unseating)						
** Calculated voltages based on the new analysis have been reviewed and are considered acceptable based on the available margin.						

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1B BOARDS

ETAP Node ID	MOV	Available Voltage (New Analysis) Value from SS	Time from Signal (SS = steady state)	New Design Margin (using new Voltages) (open)	New Design Margin (using new Voltages) (closed)	Comments **
205-7D	RHR PMP 1B-B INLET FCV 1-FCV-74-21-B (5.2HP)	91.00	SS	107.10%	1705.70%	Acceptable Margin
237-5E	RCS Press Relief Flow Cont Vlv 1-FCV-68-332-B (1.9HP)	88.06*	SS	>21.7%	>13.5%	Acceptable Margin
237-9B	RHR To RCS H.L. 1&3 Flow Iso V 1-FCV-63-172-B (2.6HP)	85.99	SS	59.20%	87.40%	Acceptable Margin
237-11B	RHR Hx B To SIS Pmp 1-FCV-63-11-B (2HP)	85.71	SS	8.90%	124.60%	Acceptable Margin
237-13A	SIS Pmp 1B-B Outlet FCV 1-FCV-63-153-B (1.9HP)	88.75*	SS	19.90%	30.10%	Acceptable Margin
237-13B	SIS PMP OUT RCS LP 2& 4 H. LEG 1-FCV-63-157-B (1.9HP)	91.36*	SS	11.10%	11.50%	Acceptable Margin
237-13D	SIS 1B-B Dsh To RWST Shtff Vlv 1-FCV-63-175-B (0.7HP)	84.70	SS	977.40%	77.10%	Acceptable Margin
237-14D	RHR Spray Hdr 1B Isln Vlv 1-FCV-72-41-B (1.9HP)	85.82	SS	66.90%	111.40%	Acceptable Margin
237-14E	Cntmt Sump To Spray Hdr 1B FCV 1-FCV-72-45-B (3.2HP)	89.68*	SS	3.30%	57.00%	Acceptable Margin
238-2E	St Flow To AFWP Turb Isln Vlv 1-FCV-1-18-B (1HP)	92.50*	SS	95.80%	18.20%	Acceptable Margin
238-5F	Cntmt Spray Hx 1B Disch Vlv 1-FCV-67-124-B (0.33HP)	91.73*	SS	24.40%	24.40%	Acceptable Margin
238-5E	Cntt Spray Hx 1B Sup Cont Vlv 1-FCV-67-123-B (0.33HP)	92.08*	SS	24.40%	24.40%	Acceptable Margin
205-7E	RWST TO SPRAY HDR 1B Vlv 1-FCV-72-22-B (3.3HP)	86.79	SS	291.10%	283.70%	Acceptable Margin
237-10A	SIS 1A-A DSH TO RWST SHTFF VLV 1-FCV-63-4-B (0.7HP)	84.57	SS	943.70%	76.10%	Acceptable Margin
237-10B	RWST To SIS Pump Flow Cont Vlv 1-FCV-63-5-B (1.9HP)	88.02*	SS	17.30%	38.60%	Acceptable Margin
237-11A	SIS PMP INLT TO CVCS CHR G PMP 1- FCV-63-6-B (1.9HP)	88.21*	SS	11.30%	118.70%	Acceptable Margin
237-12B	SIS Pmp 1B-B Inlet Vlv 1-FCV-63-48-B (1.9HP)	90.23*	SS	39.00%	46.60%	Acceptable Margin
237-12D	CNTMT SUMP TO RHR PMP B-B 1-FCV-63-73-B (13HP)	88.03	SS	17.40%	2117.00%	Acceptable Margin
237-14A	Cntmt Spray Hdr 1B Isln Vlv 1-FCV-72-2-B (3.2HP)	92.86*	5s	10.40%	359.00%	Acceptable Margin
238-3A	ERCW Hdr B Isln Vlv 1-FCV-3-179A-B (0.33HP)	83.46	SS	22.10%	19.00%	Acceptable Margin
238-17D	CCS HX B ERCW BYPASS FCV 0-FCV-67-144-B (0.13HP)	82.00	SS	110.40%	112.00%	Acceptable Margin
237-15D	RHR Hx 1B Bypass Vlv 1-FCV-74-35-B (1.9HP)	81.00	SS	64.30%	37.80%	Acceptable Margin
* Calculated voltage considering Hammer Blow feature (using 50% LRC during unseating)						
**Calculated voltages based on the new analysis have been reviewed and are considered acceptable based on the available margin.						

R2

**WBN Unit 2 GL 89-10
 Required Voltage Vs Time**

VALVEID	T(sec) from SI: 0, 5, or SS	MOV Position Change	Comments	OLD Min. Voltage Required to Achieve Position	Stroke Time (Secs)	NEW Min. Voltage Required to Achieve Position
2-FCV-1-15	SS	either	Steady State Voltage	O= 415 C= 415	20	O= 428.3 C= 428.3
2-FCV-1-16	SS	either	Steady State Voltage	O= 415 C= 415	20	O= 428.2 C= 428.2
2-FCV-1-17	SS	O to C	Steady State Voltage	O= 415 C= 415	16	O= 428.3 C= 428.3
2-FCV-1-18	SS	O to C	Steady State Voltage	O= 415 C= 415	16	O= 423.3 C= 423.3
2-FCV-1-51	0	C to O	125 VDC Motor, Need Best Avail Voltage at T=0 sec from SI	Not evaluated	16	O= 90V C= 90V
2-FCV-3-33	4	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=4 sec from SI (5.75 sec stroke time). Based on review of dP test MOV could become dP loaded just before 5 sec.	O= 390.3 C= 415.	6.5	O= 414 C= 414
2-FCV-3-47	4	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=4 sec from SI (5.75 sec stroke time). Based on review of dP test MOV could become dP loaded just before 5 sec.	O= 390.3 C= 415.	6.5	O= 414 C= 414
2-FCV-3-67	4	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=4 sec from SI (5.75 sec stroke time). Based on review of dP test MOV could become dP loaded just before 5 sec.	O= 376.9 C= 415.	6.5	O= 414 C= 414
2-FCV-3-100	4	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=4 sec from SI (5.75 sec stroke time). Based on review of dP test MOV could become dP loaded just before 5 sec.	O= 390.3 C= 415.	6.5	O= 414 C= 414
2-FCV-3-116A	SS	C to O	Steady State Voltage	O= 415 C= 415.	10	O= 413.3 C= 413.3
2-FCV-3-116B	SS	C to O	Steady State Voltage	O= 415 C= 415.	10	O= 413.2 C= 413.2
2-FCV-3-126A	SS	C to O	Steady State Voltage	O= 408 C= 408	10	O= 406.1 C= 406.1
2-FCV-3-126B	SS	C to O	Steady State Voltage	O= 408 C= 408	10	O= 406.1 C= 406.1
2-FCV-3-136A	SS	C to O	Steady State Voltage	O= 415 C= 415.	15	O= 412.2 C= 412.2
2-FCV-3-136B	SS	C to O	Steady State Voltage	O= 415 C= 415.	15	O= 412.3 C= 412.3
2-FCV-3-179A	SS	C to O	Steady State Voltage	O= 405 C= 405.	15	O= 409 C= 409
2-FCV-3-179B	SS	C to O	Steady State Voltage	O= 405 C= 405.	15	O= 409 C= 409
2-FCV-26-240	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (6.21 sec stroke time)	O= 408.7 C= 401.3	20	O= 430.6 C= 406.9
2-FCV-26-243	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (6.21 sec stroke time)	O= 408.7 C= 401.3	20	O= 426.5 C= 403
2-FCV-62-61	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (5.25 sec stroke time)	O= 415 C= 340.	10	O= 401.2 C= 401.2
2-FCV-62-63	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (5.25 sec stroke time)	O= 405 C= 378.5.	10	O= 380.5 C= 380.5
2-FCV-62-90	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (8.80 sec stroke time)	O= 415 C= 415.	10	O= 414 C= 414
2-FCV-62-91	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (8.25 sec stroke time)	O= 415 C= 415.	10	O= 414 C= 414

AUXILIARY POWER SYSTEM ANALYSIS
 WBN-EEB-EDQ000-999-2007-0002,
 ATTACHMENT 11.5

WBN Unit 2 GL 89-10
Required Voltage Vs Time

VALVEID	T(sec) from SF: 0, 5, or SS	MOV Position Change	Comments	OLD Min. Voltage Required to Achieve Position	Stroke Time (Sec)	NEW Min. Voltage Required to Achieve Position
2-LCV-82-132	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (5.25 sec stroke time)	O= 390 C= 322	10	O= 417.8 C= 394.7
2-LCV-82-133	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (5.25 sec stroke time)	O= 390 C= 334	10	O= 418.7 C= 394.7
2-LCV-82-135	0	C to O	Need Best avail Voltage at t=0 sec from SI	O= 401.8 C= 409.3	15	O= 320.0 C= 396.3
2-LCV-82-136	0	C to O	Need Best avail Voltage at t=0 sec from SI	O= 376.3 C= 411.3	15	O= 342.9 C= 413.0
2-FCV-82-136	SS	C to O	Steady State Voltage	O= 384 C= 384	6	O= 421.4 C= 421.4
2-FCV-83-001	SS	O to C	Steady State Voltage	O= 413.5 C= 413.5	60	O= 364.2 C= 362.2
2-FCV-83-003	SS	O to C	Steady State Voltage	O= 401 C= 401	10	O= 426.3 C= 426.3
2-FCV-83-004	SS	O to C	Steady State Voltage	O= 390 C= 390	10	O= 416.4 C= 416.4
2-FCV-83-005	SS	O to C	Steady State Voltage	O= 395 C= 395	14	O= 404.4 C= 404.4
2-FCV-83-006	SS	C to O	Steady State Voltage	O= 395 C= 395	10	O= 396.7 C= 396.7
2-FCV-83-007	SS	C to O	Steady State Voltage	O= 399 C= 399	10	O= 396.5 C= 396.5
2-FCV-83-008	SS	C to O	Steady State Voltage	O= 415 C= 415	28	O= 430.7 C= 430.7
2-FCV-83-011	SS	C to O	Steady State Voltage	O= 415 C= 415	28	O= 429.6 C= 429.6
2-FCV-83-022	SS	O to C	Steady State Voltage	O= 407 C= 407	17	O= 408.6 C= 408.6
2-FCV-83-025	0	C to O	Need Best avail Voltage at t=0 sec from SI	O= 415 C= 415	12	O= 414 C= 414
2-FCV-83-026	0	C to O	Need Best avail Voltage at t=0 sec from SI	O= 415 C= 415	12	O= 414 C= 414
2-FCV-83-047	SS	O to C	Steady State Voltage	O= 400 C= 400.	15	O= 385.6 C= 385.6
2-FCV-83-048	SS	O to C	Steady State Voltage	O= 415 C= 415	15	O= 408.2 C= 408.2
2-FCV-83-067	SS	Open Only	Steady State Voltage		105	O = 322
2-FCV-83-072	SS	C to O	Steady State Voltage	O = 415 C = 415	60	O = 410 C = 410
2-FCV-83-073	SS	C to O	Steady State Voltage	O = 415 C = 415	60	O = 420 C = 420
2-FCV-83-080	SS	Open Only	Steady State Voltage		105	O = 322
2-FCV-83-093	SS	either	Steady State Voltage	O= 415 C= 415	40	O = 451.1 C = 451.1
2-FCV-83-094	SS	either	Steady State Voltage	O= 415 C= 415	40	O = 451.8 C = 451.8

**WBN Unit 2 GL 89-10
Required Voltage Vs Time**

VALVE ID	T(sec) from SI: 0, 5, or SS	MOV Position Change	Comments	OLD Min. Voltage Required to Achieve Position	Stroke Time (Secs)	NEW Min. Voltage Required to Achieve Position
2-FCV-63-098	SS	Open Only	Steady State Voltage		105	O = 322
2-FCV-63-118	SS	Open Only	Steady State Voltage		105	O = 322
2-FCV-63-152	SS	O to C	Steady State Voltage	O= 415 C= 415	15	O = 414.6 C = 414.6
2-FCV-63-153	SS	O to C	Steady State Voltage	O= 415 C= 415	15	O = 415.7 C = 415.7
2-FCV-63-156	SS	C to O	Steady State Voltage	O= 415 C= 415	17	O = 414.4 C = 414.4
2-FCV-63-157	SS	C to O	Steady State Voltage	O= 415 C= 415	17	O = 428.6 C = 428.6
2-FCV-63-172	SS	either	Steady State Voltage	O= 394 C= 394	120	O = 395.2 C = 395.2
2-FCV-63-175	SS	O to C	Steady State Voltage	O= 400 C= 400	10	O = 419.5 C = 419.5
1-FCV-67-66	0	C to O	Need best voltage at T = 0 Secs from SI		66	O = 362.4 C = 362.4
1-FCV-67-67	0	C to O	Need best voltage at T = 0 Secs from SI		66	O = 361.9 C = 361.9
2-FCV-67-66	0	C to O	Need best voltage at T = 0 Secs from SI		66	O = 360.8 C = 360.8
2-FCV-67-67	0	C to O	Need best voltage at T = 0 Secs from SI		66	O = 363.8 C = 363.8
2-FCV-67-83	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 364	66	O = 434.8 C = 410.1
2-FCV-67-87	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 362	66	O = 431.5 C = 407
2-FCV-67-86	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 340	66	O = 422.5 C = 402.6
2-FCV-67-89	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 322	66	O = 322 C = 322
2-FCV-67-91	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 364	66	O = 433.9 C = 409.3
2-FCV-67-95	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 361	66	O = 430.7 C = 406.1
2-FCV-67-98	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 341	66	O = 423 C = 403.1
2-FCV-67-97	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 393.0 C=385.9	66	O = 322 C = 322
2-FCV-67-99	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 340	66	O = 422.5 C = 402.6
2-FCV-67-103	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 340	66	O = 422.4 C = 402.6
2-FCV-67-104	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 370	66	O = 441.7 C = 416.6
2-FCV-67-105	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 329	66	O = 322 C = 322

**WBN Unit 2 GL 89-10
Required Voltage Vs Time**

VALVEID	T(sec) from SI: 0, 5, or SS	MOV Position Change	Comments	OLD Min. Voltage Required to Achieve Position	Stroke Time (Secs)	NEW Min. Voltage Required to Achieve Position
2-FCV-67-107	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 342	66	O = 424.1 C = 404.1
2-FCV-67-111	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 342	66	O = 424.3 C = 404.4
2-FCV-67-112	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 364	66	O = 434.8 C = 410.1
2-FCV-67-113	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 393.2 C= 386.1	66	O = 322 C = 322
2-FCV-67-123	SS	C to O	Steady State Voltage	O= 415 C= 415	70	O = 436.3 C = 436.3
2-FCV-67-124	SS	C to O	Steady State Voltage	O= 415 C= 415	70	O = 433 C = 433
2-FCV-67-125	SS	C to O	Steady State Voltage	O= 415 C= 415	70	O = 441.8 C = 441.8
2-FCV-67-126	SS	C to O	Steady State Voltage	O= 415 C= 415	70	O = 439.4 C = 439.4
2-FCV-67-130	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-131	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-133	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-134	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-138	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-139	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-141	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-142	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-143	SS	either	Steady State Voltage	O= 415 C= 415	180	O= 418.8 C= 418.8
2-FCV-67-295	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-296	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-297	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-298	0	O to C	Need best voltage at T = 0 Secs from SI		66	O = 322 C = 322
2-FCV-67-146	SS	either	Steady State Voltage	O= 415 C= 415	60	O= 435.9 C= 435.9
2-FCV-68-332	SS	either	Steady State Voltage	O= 407 C= 407	20	O= 408.6 C= 408.6
2-FCV-68-333	SS	either	Steady State Voltage	O= 415 C= 415	20	O= 418.7 C= 418.7

**WBN Unit 2 GL 89-10
Required Voltage Vs Time**

VALVE ID	T(sec) from SI: O, 5, or SS	MOV Position Change	Comments	OLD Min. Voltage Required to Achieve Position	Stroke Time (Secs)	NEW Min. Voltage Required to Achieve Position
2-FCV-70-087	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (24.04 sec stroke time)	O= 403.6 C= 396.2	66	O= 441.6 C= 420.8
2-FCV-70-089	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 400 C= 348	66	O= 406 C= 386.9
2-FCV-70-090	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (24.04 sec stroke time)	O= 415 C= 365	66	O= 436.1 C= 411.3
2-FCV-70-092	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 376	66	O= 449.2 C= 423.7
2-FCV-70-100	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 392.5 C= 385.4	66	O= 442.7 C= 417.5
2-FCV-70-133	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (16.8 sec stroke time)	O= 395.5 C= 415	66	O= 424.6 C= 400.4
2-FCV-70-134	5	O to C	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=5 sec from SI (16.8 sec stroke time)	O= 415 C= 415	66	O= 419.8 C= 400.1
2-FCV-70-140	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Open Butterfly Valve, 62.65 sec stroke time)	O= 415 C= 327	66	O= 422.6 C= 402.7
2-FCV-70-143	5	O to C	Need 70% Voltage at t=0 & best avail at t=5 sec (Normally Closed Butterfly Valve, will close if opened, 62.65 sec stroke time. No opening accident requirement)	O= 415 C= 363	66	O= 432.7 C= 408.1
1-FCV-70-153	SS	C to O	Steady State Voltage		90	O= 416.76 C= 416.76
2-FCV-70-153	SS	C to O	Steady State Voltage		90	O= 434.2 C= 434.2
2-FCV-70-158	SS	C to O	Steady State Voltage	O= 415 C= 415	90	O= 443.3 C= 443.3
2-FCV-70-183	SS	O to C	Steady State Voltage	O= 415 C= 415	30	O= 425 C= 425
2-FCV-70-215	SS	O to C	Steady State Voltage	O= 415 C= 415	30	O= 425.7 C= 425.7
2-FCV-72-2	5	C to O	Need Best avail Voltage at t=0 sec from SI	O= 415 C= 415	28	O= 398.1 C= 398.1
2-FCV-72-13	10	C to O	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=10 sec from SI (10 sec time delay)	O= 410 C= 415	10	O= 396 C= 396
2-FCV-72-21	SS	O to C	Steady State Voltage	O= 415 C= 415	15	O= 423.7 C= 423.7
2-FCV-72-22	SS	O to C	Steady State Voltage	O= 402 C= 402	15	O= 406 C= 406
2-FCV-72-34	10	C to O	Need 70% Voltage at t=0 sec, Need Best Avail Voltage at t=10 sec from SI (10 sec time delay)	O= 404 C= 404	10	O= 390.8 C= 390.8
2-FCV-72-39	5	C to O	Need Best avail Voltage at t=0 sec from SI	O= 415 C= 415	28	O= 399 C= 399
2-FCV-72-40	SS	C to O	Steady State Voltage	O= 415 C= 415	15	O= 427.6 C= 427.6
2-FCV-72-41	SS	C to O	Steady State Voltage	O= 415 C= 415	15	O= 427.6 C= 427.6
2-FCV-72-44	SS	C to O	Steady State Voltage	O= 400 C= 400	20	O= 405.4 C= 405.4
2-FCV-72-45	SS	C to O	Steady State Voltage	O= 400 C= 400	20	O= 412.8 C= 412.8

**WBN Unit 2 GL 89-10
 Required Voltage Vs Time**

VALVEID	T(sec) from SI: 0, 5, or SS	MOV Position Change	Comments	OLD Min. Voltage Required to Achieve Position	Stroke Time (Secs)	NEW Min. Voltage Required to Achieve Position
2-FCV-74-01	SS	O to C	Steady State Voltage	O= 415 C= 415.	120	O= 414 C= 414
2-FCV-74-02	SS	C to O	Steady State Voltage	O= 415 C= 415.	120	O= 414 C= 414
2-FCV-74-03	SS	O to C	Steady State Voltage	O= 358 C= 358	60	O= 356.7 C= 356.7
2-FCV-74-08	SS	O to C	Steady State Voltage	O= 415 C= 415.	120	O= 425.8 C= 425.8
2-FCV-74-09	SS	O to C	Steady State Voltage	O= 415 C= 415.	120	O= 423.7 C= 423.7
2-FCV-74-12	0	C to O	Need Best avail Voltage at t=0 sec from SI	O= 386.6 C= 415	15	O= 337.3 C= 394.6
2-FCV-74-21	SS	O to C	Steady State Voltage	O= 392 C= 392	60	O= 393.3 C= 393.3
2-FCV-74-24	0	C to O	Need Best avail Voltage at t=0 sec from SI	O= 376.8 C= 415	15	O= 341.1 C= 387.2
2-FCV-74-33	SS	O to C	Steady State Voltage	O= 405 C= 405	15	O= 410 C= 410
2-FCV-74-35	SS	O to C	Steady State Voltage	O= 385 C= 385	15	O= 386.6 C= 386.6
Notes:						
1) The maximum required voltage for any GL 89-10 MOV is equal to or above 90% of 460 V (414 V). Guidance given in Design Standard DS-M18.2.21 states that for voltages 90% or greater the voltage factor is 1.0 (i.e. no degradation is required at 90% or above). Therefore, there will be no impact to any Mechanical MOV calculations as long as 90% of 460 V (414 V) is achieved.						
2) Required voltage for MOVs at T = 0, T = 4, T = 5 or T = 10 sec is the minimum available voltage from the time specified to any time forward during the SI. Example: If a 4 sec voltage was requested and voltage dropped at 5 sec, then the lower 5 sec voltage should be used to bound degraded voltage.						
3) For MOVs that are open and go closed upon receiving an SI signal, the required voltage at T = 0 is only 70% of 460 V (322 V) until the valve becomes loaded. MOVAT's differential pressure test traces were reviewed and conservative bounding times were determined for when the MOV becomes loaded. A 70% starting voltage is based on guidance provided in Limitorque Technical Update 98-01 in Vendor Manual WBN-VTD-L200-0460.						
The voltages listed in this Attachment must be met or exceeded.						
Prepared By:	<i>[Signature]</i>		Date:	5/11/11	Reviewed By:	<i>[Signature]</i>
	FAROOD SOFI					M.R. Johnson

2A BOARDS

ETAP Node ID	MOV	Available Voltage (New Analysis) Value from SS	Time from SI Signal (SS = steady state)	New Design Margin (using new Voltages) (open)	New Design Margin (using new Voltages) (closed)	Comments **
239-10B	SIS PMPs RECIRC TO RWST 2-FCV-62-3-A (0.7HP)	86.31	SS	975	47.8	Acceptable Margin
239-11A	SIS Pmp Inlet To CVCS Chrg Pmp 2-FCV-63-7-A (1.9HP)	80.28	SS	20	87	Acceptable Margin
239-14E	RHR Hx 2A Bypass Vlv 2-FCV-74-33-A (1.9HP)	82.97	SS	30	40	Acceptable Margin
239-11B	RHR Hx A To CVCS Chrg Pmp 2-FCV-63-8-A (1.9HP)	87.15	SS	13	135	Acceptable Margin
239-9F	RWST To Spray Hdr 2A FCV 2-FCV-72-22-A (3.2HP)	87.21	SS	288	272	Acceptable Margin
239-12A	SIS Pmp 2A A Inlet Vlv 2-FCV-63-47-A (1.9HP)	78.09	SS	108	26	Acceptable Margin
239-12D	SIS To RCS Loops 2&3 FCV 2-FCV-63-93-A (1.6HP)	91.22	SS	180	153	Acceptable Margin
239-12E	SIS Pmp 2A A Outlet FCV 2-FCV-63-152-A (1.9HP)	89.49*	SS	20	29	Acceptable Margin
239-13A	SIS Pmp Out RCS Lp 1&3 Hot Leg 2-FCV-63-156-A (1.9HP)	83.86	SS	15	28	Acceptable Margin
239-6D	RCS Press Relief FCV 2-FCV-68-333-A (1.9HP)	85.43	SS	22	19	Acceptable Margin
239-13B	Cntmt Sump To Spray Hdr 2A FCV 2-FCV-72-44-A (3.2HP)	82	SS	17	43	Acceptable Margin
239-14A	RHR Spray Hdr 2A Isln Vlv 2-FCV-72-40-A (1.9HP)	86.5	SS	103	156	Acceptable Margin
239-13E	Cntmt Spray Hdr 2A Isln Vlv 2-FCV-72-39-A (3.2HP)	79.41	5 sec	18.5	162.5	Acceptable Margin
240-15A	CCS HX B ERCW BYPASS FCV 2-FCV-67-143-A (0.13HP)	78.67	SS	222	270	Acceptable Margin
240-16E	RHR Hx A-A Outlet Vlv 2-FCV-70-156-A (0.33HP)	89.51	SS	14	14	Butterfly Valve & Acceptable Margin
240-17A	Sample Hx Hdr Outlet Vlv 2-FCV-70-183-A (0.13HP)	86.06	SS	134	147	Acceptable Margin
240-2A	ERCW Hdr A Isln Vlv 2-FCV-3-116A-A (0.25HP)	83.72	SS	99	115	Acceptable Margin
240-2B	ERCW Hdr A Isln Vlv 2-FCV-3-116B-A (0.25HP)	83.68	SS	86	115	Acceptable Margin
240-2D	AFWP Turb Stm Sup Fm Stm Gen-1 2-FCV-1-15-A (1HP)	91.15*	SS	25	45	Acceptable Margin
240-2E	St Flow To AFWP Turb Iso Vlv 2-FCV-1-17-A (1HP)	91.15*	SS	85	20	Acceptable Margin
240-3A	ERCW Hdr A Isln Vlv 2-FCV-3-126A-A (0.33HP)	83.49	SS	22	42	Acceptable Margin
240-3B	ERCW Hdr A Isln Vlv 2-FCV-3-126B-A (0.33HP)	83.5	SS	22	42	Acceptable Margin
240-5A	Sample Hx Isln Vlv 2-FCV-70-215-A (0.13HP)	86.16	SS	227	231	Acceptable Margin
240-5E	Cntmt Spray Hx 2A Sup Cont Vlv 2-FCV-67-125-A (0.33HP)	89.4	SS	14	14	Butterfly Valve & Acceptable Margin
240-5F	Cntmt Spray Hx 2A Disch Vlv 2-FCV-67-126-A (0.33HP)	88.91	SS	14	14	Butterfly Valve & Acceptable Margin
240-6A	AFWP Turb Stm Sup Fm Stm Gen-4 2-FCV-1-16-A (1HP)	91.14*	SS	25	31	Acceptable Margin
240-11A	Cmpnt Clg Hx A Disch Cont Vlv 2-FCV-67-146-A (0.33HP)	88.48	SS	9.4	9.4	Acceptable Margin

R2

R2

R2

* Calculated voltage considering Hammer Blow feature (using 50% LRC during unseating)

** Calculated voltages based on the new analysis have been reviewed and are considered acceptable based on the available margin.

2B BOARDS

ETAP Node ID	MOV	Available Voltage (New Analysis) Value from SS	Time from SI Signal (SS = steady state)	New Design Margin (using new Voltages) (open)	New Design Margin (using new Voltages) (closed)	Comments **
209-7E	RWST To Spray Hdr 2B FCV- 2 FCV 72-21-B (3.2 hp)	89.23	SS	211	295	Acceptable Margin
241-5E	RCS Press Relief FCV 2-FCV-68-332-B (2 hp)	83.26	SS	29	17	Acceptable Margin
241-9B	RHR To RCS H.L. 1&3 Flow-Isol V 2 FCV 63-172-B (2.6 hp)	80.11	SS	45	69	Acceptable Margin
241-10A	SIS 2B-B Dsh-To-RWST Shutoff Vlv 2 FCV 63-4-B (0.66 hp)	84.47	SS	900	50	Acceptable Margin
241-10B	RWST To SIS Pump FCV 2 FCV 63-5-B (2 hp)	81.8	SS	45	23	Acceptable Margin
241-10F	RWST To Spray Hdr 2B FCV- 2 FCV 72-21-B (3.2 hp)	85.62	SS	260	250	Acceptable Margin
241-11A	SIS Pmp-Inlet To CVCS Chrg Pmp 2 FCV 63-6-B (2 hp)	80.24	SS	16	86	Acceptable Margin
241-11B	RHR Hx-B to SIS Pmp 2 FCV 63-11-B (2 hp)	86.86	SS	13	134	Acceptable Margin
241-12B	SIS Pmp-2B-B Inlet Vlv 2 FCV 63-48-B (2 hp)	82.55	SS	130	40	Acceptable Margin
241-12D	Cntmt Sump To RHR Pmp B-B 2 FCV 63-73-B (13.2 hp)	90.37	SS	36	2000	Acceptable Margin
241-12E	SIS To RCS-Loops 1 & 4 FCV 2 FCV 63-94-B (1.6 hp)	91.33	SS	187	157	Acceptable Margin
241-13A	SIS Pmp-2B-B Outlet FCV 2 FCV 63-153-B (2 hp)	89.61*	SS	20	29	Acceptable Margin
241-13B	SIS pmp-Out RCS Lp 2&4 Hot Leg 2 FCV 63-157-B (2 hp)	86.64	SS	13	26	Acceptable Margin
241-13D	SIS 2B-B Dsh-to-RWST Shutoff Vlv 2 FCV 63-175-B (0.66 hp)	84.87	SS	900	48	Acceptable Margin
241-14A	Cntmt Spray Hdr 2B Isln Vlv 2-FCV-72-2-B (3.2 hp)	85.35	SS	28	185	Acceptable Margin
241-14D	RHR SPRAY HDR-2B-ISOL-VLV 2 FCV 72-41-B (2 hp)	90.92*	SS	90	140	Acceptable Margin
241-14E	Cntmt Sump To Spray Hdr 2B FCV 2 FCV 72-45-B (3.3 hp)	89.25*	SS	37	65	Acceptable Margin
241-15D	RHR Hx-2B Bypass Vlv 2 FCV 74-35-B (2 hp)	78.21	SS	20	29	Acceptable Margin
241-11E	SIS Boron Inj Tank Shutoff Vlv 2 FCV 63-25-B (1.9 hp)	82.51	5-sec	30.2	24.7	Acceptable Margin
241-15B	RHR Pmp 2B-B Min Flow Vlv 2-FCV-74-24-B (0.1 hp)	71.67	0 sec	290.2	48.5	Acceptable Margin
242-2B	ERCW Hdr-B Isln Vlv 2 FCV 3-126B-B (0.67 hp)	83.06	SS	86	115	Acceptable Margin
242-2E	St Flow To AFWP Turb Isln Vlv 2 FCV 1-18-B (1 hp)	90.84*	SS	85	20	Acceptable Margin
242-3A	ERCW Hdr-B Isln Vlv 2-FCV 3-179A-B (0.33 hp)	83.66	SS	19	39	Acceptable Margin
242-3B	ERCW Hdr-B Isln Vlv 2 FCV 3-179B-B (0.33 hp)	83.67	SS	19	39	Acceptable Margin
242-5E	Cntmt Spray Hx 2B Sup Cont Vlv 2-FCV-67-123-B (0.33 hp)	89.15	SS	14	14	Butterfly Valve & Acceptable Margin
242-5F	Cntmt Spray Hx 2B Sup Disch Vlv 2-FCV-67-124-B (0.33 hp)	88.5	SS	14	14	Butterfly Valve & Acceptable Margin
242-17A	SFPCS Hx Sply Hdr Isln Vlv 0-FCV-70-194-B (0.33HP)	92.18*	SS	28.10%	28.10%	Acceptable Margin
242-15E	RHR Hx B-B Outlet Vlv 2-FCV-70-153-B (0.33HP)	85	SS			Acceptable Margin

R2

R2

R2

R2

* Calculated voltage considering Hammer Blow feature (using 50% LRC during unseating)

** Calculated voltages based on the new analysis have been reviewed and are considered acceptable based on the available margin.

MOV UNIDs Minimum Voltage Required in Mechanical Calculations

2-FCV-01-015 (T = SS)	414
2-FCV-01-016 (T = SS)	414
2-FCV-01-017 (T = SS)	414
2-FCV-01-018 (T = SS)	414
2-FCV-03-116A (T = SS)	376
2-FCV-03-116B (T = SS)	376
2-FCV-03-126A (T = SS)	373
2-FCV-03-126B (T = SS)	373
2-FCV-03-136A (T = SS)	375
2-FCV-03-136B (T = SS)	374
2-FCV-03-179A (T = SS)	376
2-FCV-03-179B (T = SS)	376

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04-10-14

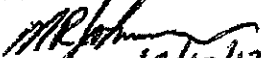
CHECKER:
Greg Lee

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4/10/14

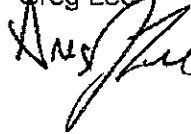
MOV UNIDs Minimum Voltage Required in Mechanical Calculations

2-FCV-62-061	366
2-FCV-62-063	345
2-FCV-62-090 (T = 0 secs)	322
2-FCV-62-090 (T = 5 secs)	414
2-FCV-62-091 (T = 0 secs)	322
2-FCV-62-091 (T = 5 secs)	414
2-FCV-62-138	391
2-LCV-62-132	354
2-LCV-62-133	360
2-LCV-62-135	372
2-LCV-62-136	355

PREPARER:
Mark R. Johnson



12/10/13

CHECKER:
Greg Lee

 12/10/13

MOV UNIDs	Minimum Voltage Required in Mechanical Calculations
2-FCV-63-1	413
2-FCV-63-3	386
2-FCV-63-4	379
2-FCV-63-5	367
2-FCV-63-6	360
2-FCV-63-7	361
2-FCV-63-8	392
2-FCV-63-11	390
2-FCV-63-22	383
2-FCV-63-47	351
2-FCV-63-48	371
2-FCV-63-67	401
2-FCV-63-72	413
2-FCV-63-73	407
2-FCV-63-80	406
2-FCV-63-93	411
2-FCV-63-94	411
2-FCV-63-98	394
2-FCV-63-118	401
2-FCV-63-152	389
2-FCV-63-153	390
2-FCV-63-156	377
2-FCV-63-157	371
2-FCV-63-172	359
2-FCV-63-175	381
2-FCV-63-25	414 (Test Condition)
2-FCV-63-26	414 (Test Condition)
2-FCV-63-25	372 (Accident Condition)
2-FCV-63-26	365 (Accident Condition)

PREPARER:
Mark R. Johnson


11/19/13

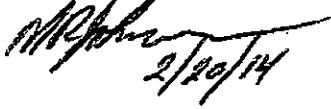
CHECKER:
Greg J. Lee


11/19/13

MOV UNIDs Minimum Voltage Required in Mechanical Calculations

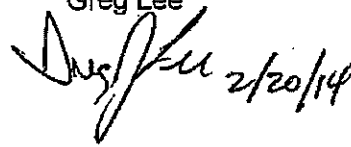
2-FCV-72-021 (T = 5 secs)	385
2-FCV-72-022 (T = 5 secs)	392
2-FCV-72-040 (T = 5 secs)	389
2-FCV-72-041 (T = 5 secs)	401
2-FCV-72-044 (T = 5 secs)	368
2-FCV-72-045 (T = 5 secs)	384
2-FCV-74-033 (T = 5 secs)	373
2-FCV-74-035 (T = 5 secs)	351

PREPARER:
Mark R. Johnson



2/20/14

CHECKER:
Greg Lee



2/20/14

WBN-VTD-R165-0140

AWING TRANSMITTAL



Washinghouse Inadequate Temperature

TEST NO.	VISITING UNIT NO.	UNIT OR REGISTERED NO.	COMPANY CODE
	SY 40779		11770
ISSUED TO GOULDS PUMPS INC NUCLEAR DIVISION; ROUTE SENECA FALLS, N.Y. 13148		PURPOSE OF ISSUE S.A.M.E.	

THIS AREA:

FOR APPROVAL

FOR CONSTRUCTION OR INSTALLATION

FOR REFERENCE

Drawings are in compliance with your specified requirements. Drawings "Approved" or "Approved with Modifications" authorize Washinghouse proceed with manufacture. Modifications not in the contract or modifications made during or after drawing approval may result in a price change and/or shipment delay. To maintain shipping schedule, approved drawings must be received by Washinghouse no later than _____.

The equipment shown on these drawing(s) has been released for manufacture, any modification may result in a price change and shipment delay.

ITEM: 1 SO# 77C12671

MARK: N229729

DESCRIPTION:

HP: 100	FLA: 115	AMBIENT: 40 C
YFD: 1770	ENCL: DP	MOUNTING: HORIZ.
FRAME: 4WAYS	TYPE: LLT	CHAST BOX: FRONT-HOME REAR-STATIONARY
MODEL: T80P	NEMA DESIGN: B	DUTY: CONTINUOUS
VOLTAGE: 480	INSUL: B	SPACE HEATERS: NONE
PHASE: 3	SERV. FACTOR: 1.15	THERMAL PROT: T.S.
HERTZ: 60	ASSY: F1	

ADDITIONAL FEATURES:

BEST AVAILABLE COPY

OUTLINE DWG: 584D760 *Sub 7*
+ I.L.L. 2930-117D

EXCEPT- SCREWS & S.S. COND. BOX

3 REPRO & 6 COPIES

MRS. FRAN CONLEY
GOULDS PUMPS, INC. SENECA PLD, N.Y. 13148

1 COPY

SYRACUSE D.D. - JOHN BURTON

CARL CAROTHERS - CHARGE - MGR.

SENECA FALLS

1

THIS DRAWING IS THE PROPERTY OF GOULDS PUMPS INC. IT IS TO BE KEPT IN THE OFFICE OF THE USER AND NOT TO BE REPRODUCED OR COPIED IN ANY MANNER WITHOUT THE WRITTEN PERMISSION OF GOULDS PUMPS INC.	DATE	BY	CHKD

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WBN REV Q
WBN PAGE 4



Westinghouse Electric Corporation

BUFFALO, N.Y.

Date 11/5/74

Purchaser GOULDS PUMPS D04883 Stock Order No. 73C74082
G.O. No. SY-44883 H.P. 100 Volts 230/460 Phase 3 Class B Insulation
Apparatus FR. 404TS, TBDP, SQ. GAGE IND. MTR. Poles 4 R.P.M. 1770 Cycles 60

	1	2	3	COMMENTS
Amperes Per Terminal at no load 460 Volts	27.13			
Watts Input at no load	1694			
Stator Res. (T-T) at 75° C - ohms	.1323			
Starting Winding Res. at 75° C - ohms				
Rotor Res. (bet rings) at 75° C - ohms				
LOSSES IN WATTS AT FULL LOAD				
Stray Load Loss	1012			
Stator I ² R Loss	2795			
Rotor I ² R Loss	1180			
Core Loss	1080			
Friction and Windage Loss	440			
% Efficiency - Full Load	92			
- ¾ Load	93.1			
- ½ Load	93.2			
% Power Factor Full Load	89.4			
- ¾ Load	88.7			
- ½ Load	83.9			
n _r H at Full Load	1772			
Amperes Per Term. at full load	113.82			
KW input at full load	81.11			
Amperes per Term-Rotor locked 460 V	646.7			
KW input - Rotor locked	215			
Max. Sec. Volts between rings	-			
Sec. Amps per ring at full load	-			
Full Load Torque (F.L.T.) in lb. ft.	296.2			
Max. Torque in % of F.L.T.	215.7			
Starting Torque in % of F.L.T.	168.6			
End Play Tested	OK			
Balance Tested	OK			
Stator Ins Tested 2100 V 60 Sec.	OK			
Rotor Ins Tested V Sec.	-			
TEMPERATURE TESTS				
Length of Test in hours	7.5			
Volts	460			
% Normal Full Load Amp.	100			
Temp. Rise in degrees C	Stator Copper by Res.	78		
	Stator Iron	48		
	Rotor Copper			
	Rotor Iron			
Room temperature in °C	26			
Curve Nos.				

06
WBN
WBN
WBN

The above is a true and correct record of data obtained from tests made at the works of Westinghouse Electric Corporation.

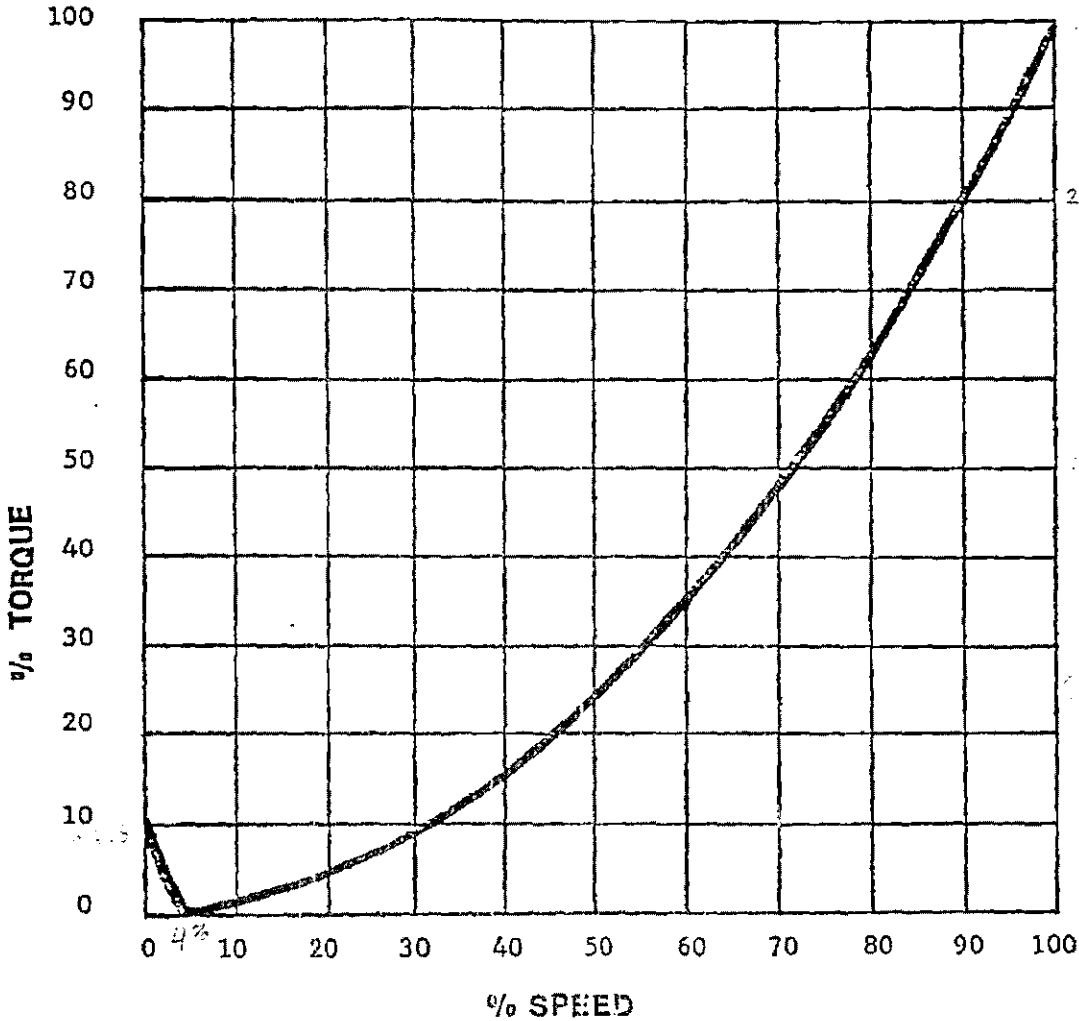
L. M. 01779
11229729

SPEED - TORQUE CURVE

AT RUNOUT OF
2750 GPM @ 132 feet
100% TORQUE = 288.8 FT. LBS.

E-2126

100% SPEED = 1750 R. P. M.



PUMP MODEL - 3405

PUMP SIZE - 8X10-12 DV

IMPELLER DWG. # - 80-45

IMPELLER PATT. # - 52895

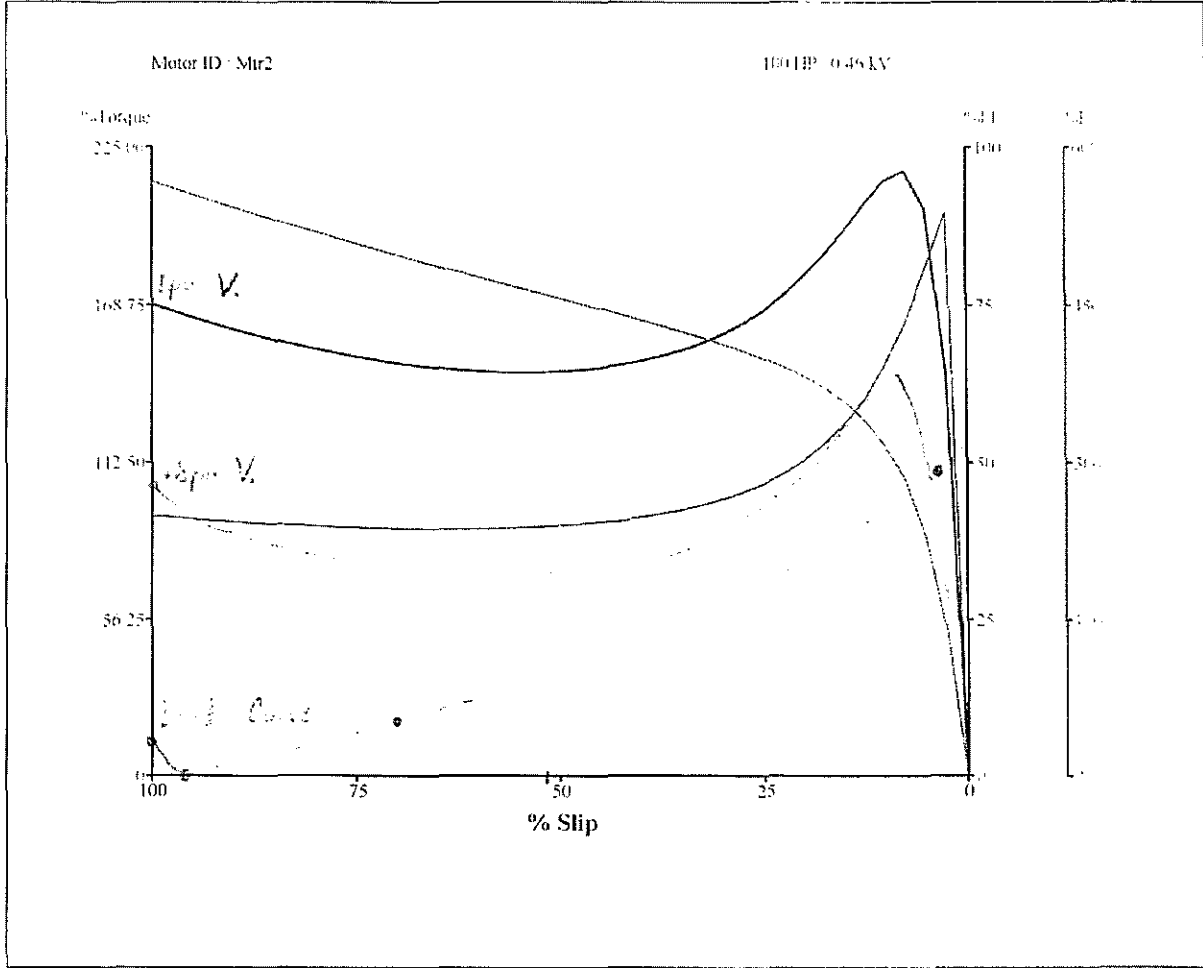
IMPELLER DIAMETER - 12"

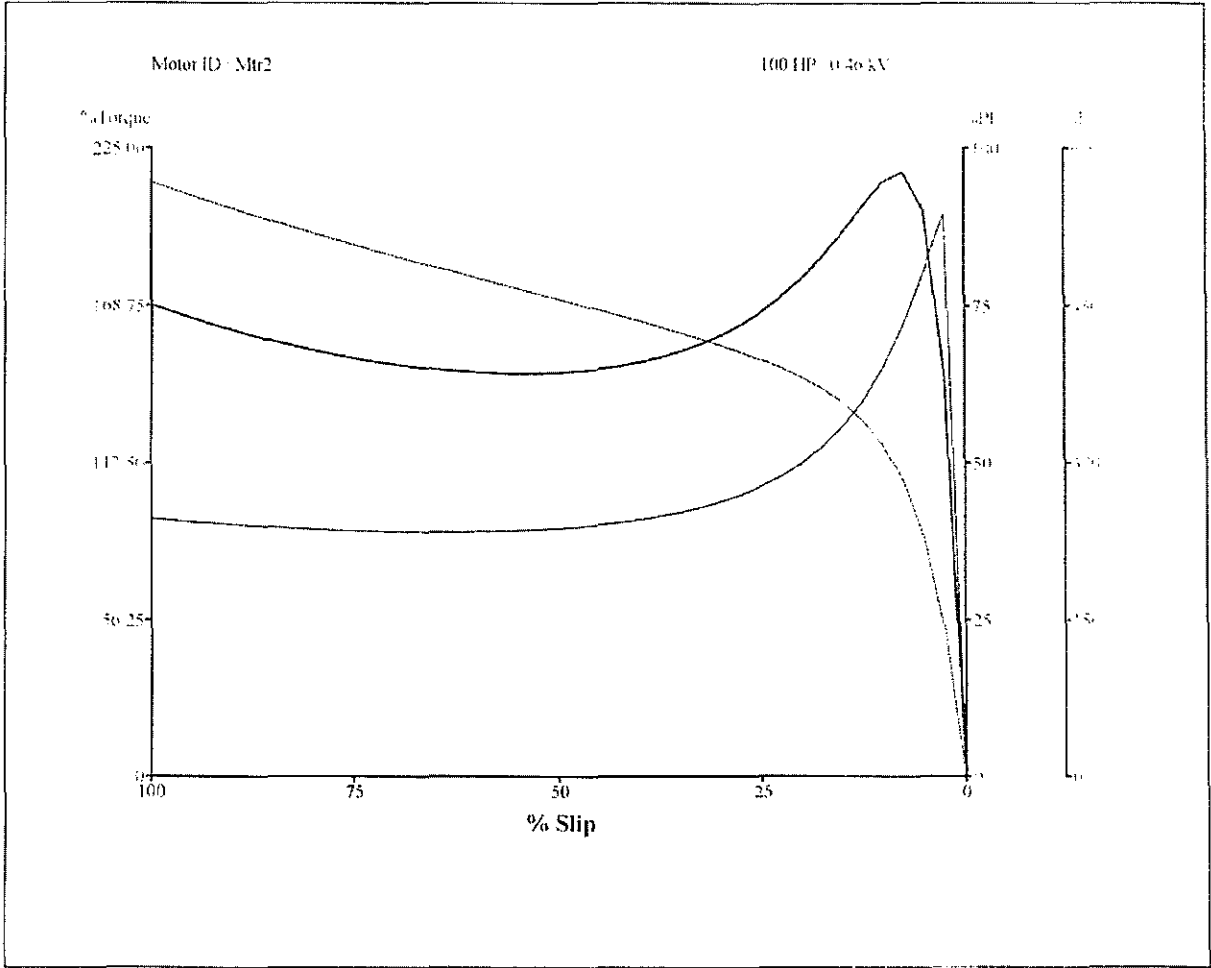
$$100\% \text{ TORQUE} = \frac{\text{H. P.} \times 5250}{\text{R. P. M.}}$$

- Notes:
- A. H. P. is the shut-off H. P. at 100% speed with the rated impeller diameter.
 - B. Sleeve Bearing starting point is 15% not 10%.

PUMP $WR^2 = 8.15$ LB.-FT²

WBN REV 0
WBN PAGE 8





1

CONTAINMENT AIR RETURN FAN 1A-A

1-MTR-030-0038-A

WBN-VTD-R165-0110

RELIANCE ELECTRIC COMPANY



24701 Euclid Avenue, Cleveland, Ohio 44117

Calc. STUDY-EEB-WBN-12-001
Attachment 6
Page 6 of 12

REPORT OF ROUTINE TESTS

Induction Motor

Purchaser Joy Manufacturing Co.
338 South Broadway
New Philadelphia, Ohio 44663

Date of Test

Manufacturer's Order No. 1XF-882396

Purchaser's Order No. NA2836

The air gap, condition of bearings and rotor balance were examined and found to be satisfactory.

Engineer P. Licurs, Jr.
P. Licurs, Jr.

WBN REV 2

WBN PAGE 16

NAMEPLATE DATA

Hp	Service Factor	Rpm	Phase	Hertz	Volts	Amperes
100	1.0	1786	3	60	460	115

Type	Frame	Temp Rise by Method Indicated	Ambient Temp and Insulation Class	Time Rating	Design Letter	Code Letter for Locked Kva/HP
P	444TCZ	-	50°C/H *	Cont.	-	J

TEST CHARACTERISTICS

Serial Number	No Load				Locked Rotor (Single Phase) (Three Phase)				Wound Rotor Open Circuit Volt.	@ High-potential Test Voltage	Date of Test
	Volts	Hertz	Rpm	Amperes	Volts	Hertz	Amperes				
A-1	460	60	1799	40.5	460	60	869		-	2000	7-6-77
A-2	460	60	1799	41.5	230	60	414		-	2000	7-7-77
A-3	460	60	1799	41.1	230	60	412		-	2000	7-7-77
A-4	460	60	1799	41.4	230	60	411		-	2000	7-7-77

Notes: * Type RN insulation. @ For 60 seconds.

Data on test from these (this or duplicate) motors -

Approved by P. Licurs, Jr. Data D.J.G.
(Engineer)

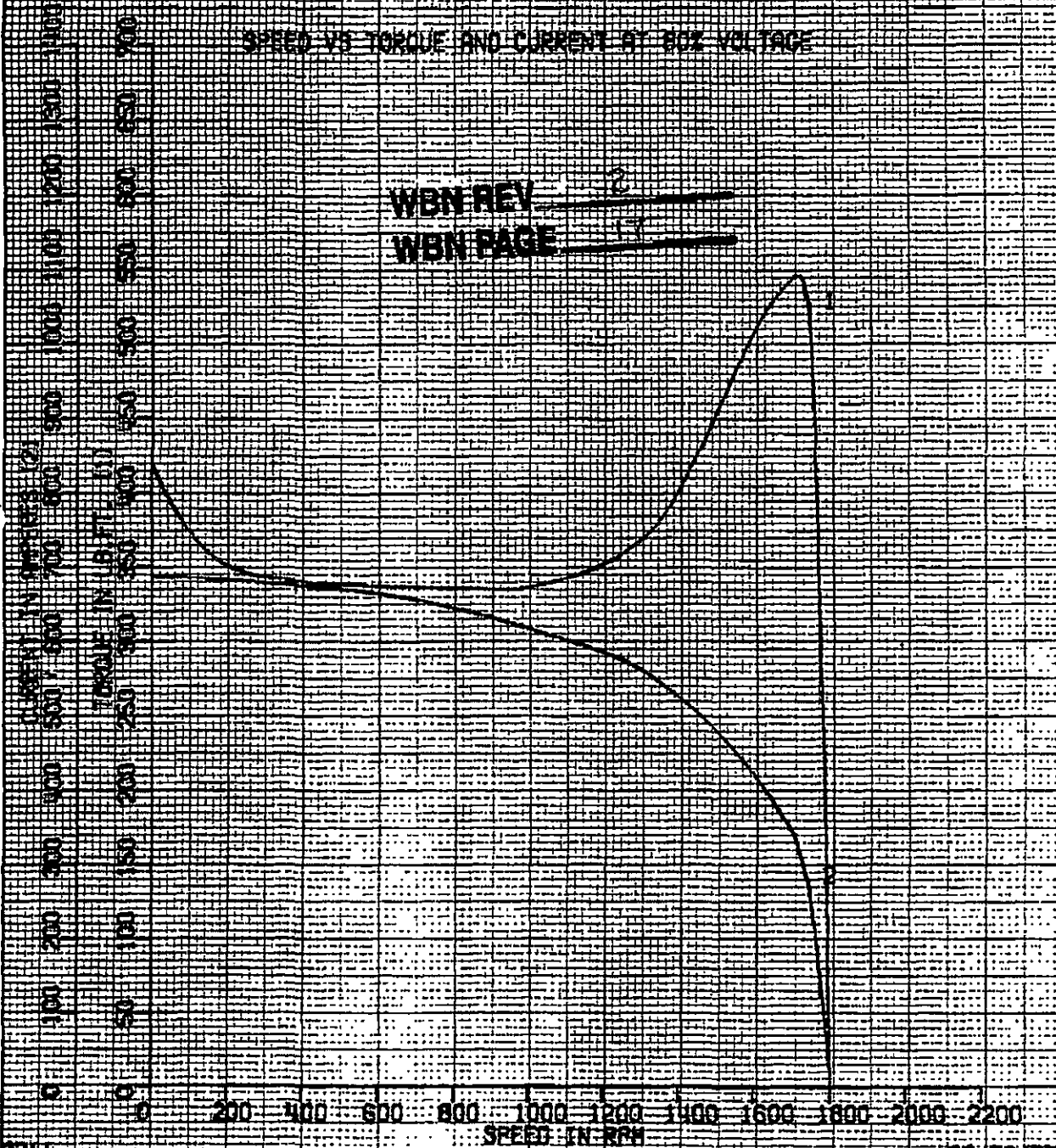
Issued: 8-12-77

P. Licurs, Jr.

REL. S.O. 1XF-882396	RPM 1786	S.F. 1.0	ROTOR 604882-1RJ
FRAME 444TCZ	VOLTS 460	NEMA DESIGN -	TEST S.O. 1XF-882396
HP 100	AMPS 115	CODE LETTER J	TEST DATE 7-6-77
TYPE P	DUTY Cont.	ENCLOSURE TEAO	STATOR RES. @ 25°C .06439
PHASE/HERTZ 3/60	AMB°C/INSUL 50/H *	E/S 597617	OHMS (BETWEEN LINES)

SPEED VS TORQUE AND CURRENT AT BOX VOLTAGE

WBN REV 2
WBN PAGE 13



AMPERES SHOWN FOR 460 Volt CONNECTION. IF OTHER VOLTAGE CONNECTIONS ARE AVAILABLE, THE AMPERES WILL VARY INVERSELY WITH THE RATED VOLTAGE. * Type RN insulation.

RELIANCE
ELECTRIC COMPANY
CLEVELAND, OHIO 44117 U.S.A.

DR. BY ED
CK. BY DEM
APP. BY DEM
DATE 8-22-77

**A-C MOTOR
PERFORMANCE
CURVES**

V29593.000
ISSUE DATE 8-22-77

RE 1572VB2 1 40 in U.S.A.

6YF882998
CONTRACT #81K5-829093, CHG. #1
FOR: WATTS BAR NUCLEAR PLANT
HVAC EQUIPMENT
TRAVELING WATER SCREENS

6

ERCW TRAV. SCREEN 1B-B

1-MTR-067-0445-B

SPECIAL DATA SHEET

Calc. STUDY-EEB-WBN-12-001
Attachment 6
Page 8 of 12

- a. Manufacturer RELIANCE ELECTRIC COMPANY
- b. Application TRAVELING WATER SCREENS
- c. Rated horsepower 5
- d. Service factor 1.15
- e. Rated voltage 460
- f. Full load current per phase at the applicable rated voltage
6.8 AMPERES
- g. Locked rotor current at the applicable rated voltage
41.1 AMPERES *AUC* *IBR*
- h. Locked rotor power factor at rated voltage 61.2%
- * i. Full load current per phase at 80% of motor rated voltage
8.8 AMPERES
- J. Locked rotor current at 80% of motor rated voltage
30.6 AMPERES
- k. Locked rotor withstand time at rated voltage starting from ambient temperature
(3-ph motors only) 20 SECONDS *M*
- l. Locked rotor withstand time at rated voltage starting from rated temperature
(3-ph motors only) 8 SECONDS
- m. Efficiency at 100%, 75% and 50% of rated horsepower
82.3%, 82.9%, 82.5%
- n. Power factor at 100%, 75% and 50% rated horsepower
83.9%, 79.8%, 70.6%
- * **MOTOR NOT SUITABLE FOR CONTINUOUS OPERATION AT 80% VOLTAGE.**

WATTS BAR
81-829093
6YF882998

M/A 112



ELLIS AND WATTS
CINCINNATI, OHIO 45244

DOCUMENT NO. N0055-4 REVISION 0 4/28/86

ISSUE NO. _____

TITLE: NUCLEAR ENVIRONMENTAL QUALIFICATION REPORT FOR
50 HP - 1800 RPM MOTOR

PART NO. _____

PART NAME _____

PREPARED BY: *K. Z. Wanky* 4/28/86
K.Z. Wanky

ENGINEERING APPROVAL: *M. J. Fox* 4/28/86
M.J. Fox

Q.A. APPROVAL: *R. R. Schertler* 4/28/86
R. R. Schertler
DATE

Tennessee Valley Authority
Watts Bar Generating Station
Contract No. 85PM8-451609

DOCUMENT NO. N0055-4

PAGE 1

DATE OF TEST) 01-15-80
MANUFACTURERS
ORDER NO. 6-150206
PURCHASERS
ORDER NO. 76013

REPORT OF TEST-INDUCTION MOTOR

PURCHASER ELLIS & WATTS

RATING

TYPE	FRAME	RATED H.P.	FULL LOAD R.P.M.	VOLTS	PH	HZ.	FULL LOAD AMPERES	SERVICE FACTOR	TIME RATING
COG6B	326T	50	1770	480	3	60	56.5	1.15	CONT.

CONDITIONS OF TEST

TEMPERATURE RISE-DEG. C

HOURS RUN	LINE VOLTS	LINE AMPERES	COOLING AIR DEG. C	STATOR			ROTOR		COLLECTOR RINGS
				CORE BY THERMO-COUPLE METHOD	WINDINGS (CROSS OUT THREE) BY RESISTANCE METHOD BY EMBEDDED DETECTOR BY THERMOCOUPLE METHOD BY THERMOMETER METHOD	CORE BY THERMO-METER METHOD	WINDINGS (CROSS OUT ONE) BY RESISTANCE METHOD BY THERMO-METER METHOD		
3.5	483	65.7	21	68	108.8	-----	-----	-----	

CHARACTERISTICS

SLIP-PERCENT	AMPERES RUNNING LIGHT	RESISTANCE IN OHMS AT 25°C (BETWEEN LINES)		SECONDARY VOLTS AT STANDSTILL	SECONDARY AMPERES PER RING AT FULL LOAD
		STATOR BETWEEN TERMINALS	ROTOR BETWEEN RINGS		
1.53	17.4	.159	-----	-----	-----

TORQUE AND STARTING CURRENT

HIGH-POTENTIAL TESTS

BREAK-DOWN TORQUE LBS. AT 1 FT. RADIUS	LOCKED ROTOR TORQUE LBS. AT 1 FT. RADIUS WITH-% VOLTS APPLIED	STARTING CURRENT AMPERES (LOCKED ROTOR) WITH-% VOLTS APPLIED	VOLTS A-C FOR 1 SEC.	
			STATOR	ROTOR
341.0 LB-FT	218-99.2%	334.7-99.2%	2400	-----

EFFICIENCIES AND POWER FACTOR

EFFICIENCY, PERCENT			POWER FACTOR, PERCENT		
FULL LOAD	3/4 LOAD	1/2 LOAD	FULL LOAD	3/4 LOAD	1/2 LOAD
93.1	93.9	94.0	83.4	81.8	75.8

NOTES: DATA FROM TEST ON THIS MOTOR. IN ACCORDANCE WITH IEEE 112-1984 (THIS OR DUPLICATE) FORM A-2.

THIS DATA FOR REFERENCE ONLY UNLESS OTHERWISE SPECIFIED

PREPARED BY C L MATTHEWS
APPROVED BY [Signature]
DATE 04-02-86



B32E04-050-731-C0

SHEET 1 OF 1

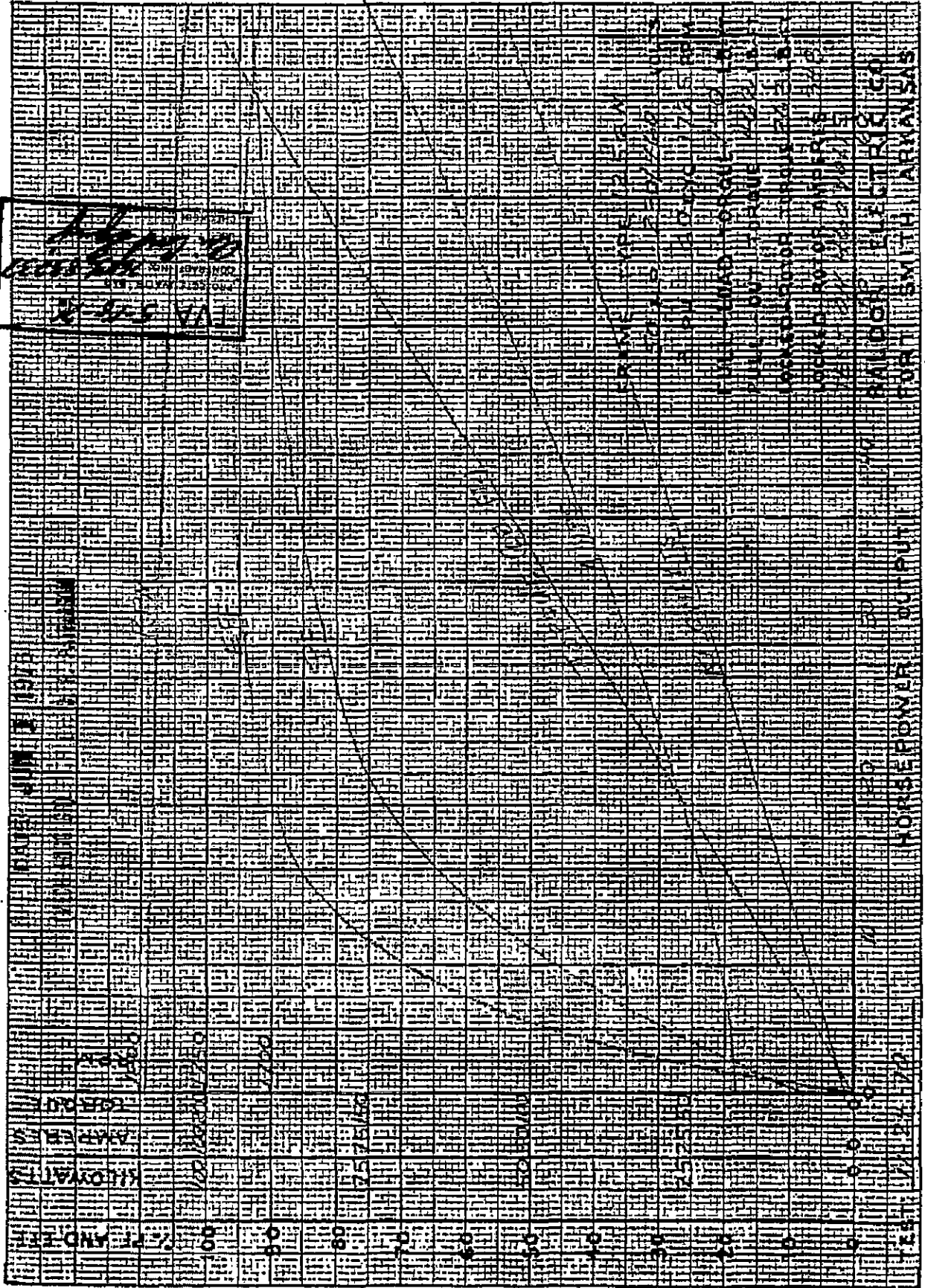
M 3126 2/84

11/22/07
BY GC 7/8 2:30 IN ALABAMA
KOPPEL & ESTER CO.

FOR INFORMATION ONLY

7

WINDING: 312-325



TVA P.O. 76K 36-83037
SCHEDULE II

1-11-71 WB

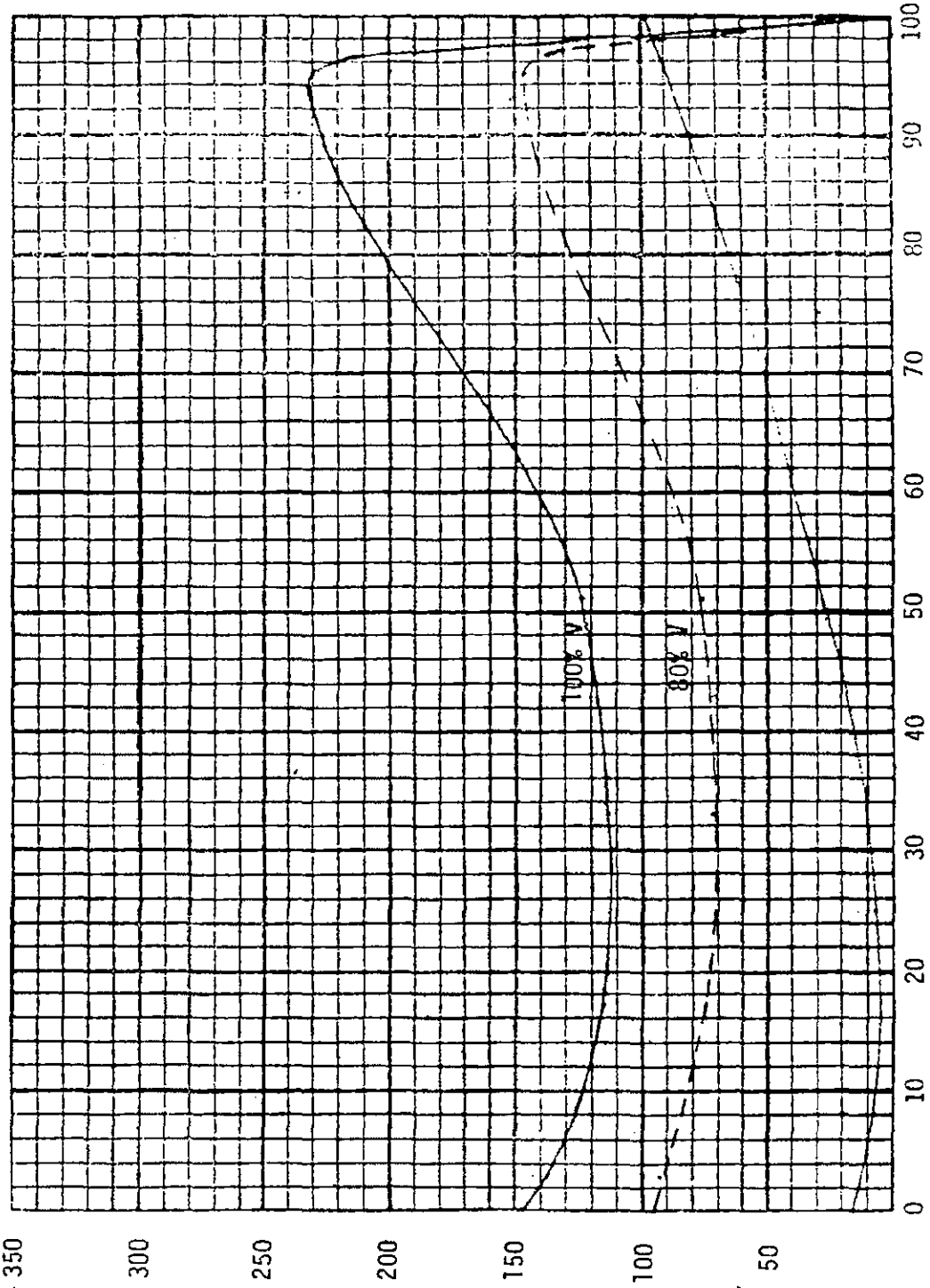
DATE OF TEST 01-16-86
 MANUFACTURERS
 ORDER NO. 6-150206
 PURCHASERS
 ORDER NO. 76013

SPEED-TORQUE & CURRENT CURVE

PURCHASER ELLIS & WATTS

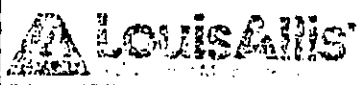
AMPERES IN % FULL-LOAD

TYPE COG6B FRAME 326T HP 50 F.L. RPM 1770
 VOLTAGE 480 PHASE/HERTZ 3/60 AMBIENT 40 SERVICE FACTOR 1.15
 F.L. AMPS 56.5 F.L. TORQUE 148.4 LBS. FT.
 INSULATION CLASS H DUTY CONT. ENCLOSURE O.D.P. MOUNTING F-1



THIS DATA FOR REFERENCE ONLY UNLESS OTHERWISE SPECIFIED TORQUE IN % OF FULL LOAD

PREPARED BY C. L. MATTHEWS
 APPROVED BY [Signature]
 DATE 04-02-86



B32E04-050-731-S0
 SHEET 1 OF

11 3181 2/82

5.2. Second Level Undervoltage (Degraded Voltage) Relay Reset Setpoint

An upper boundary should also be established for the reset setting of the degraded voltage relay. The tightest possible tolerance should be employed between the nominal dropout and reset setpoints. The upper boundary of the reset setting should be equal to the nominal setpoint plus all tolerances from any errors in accordance with Technical Instruction TI-28 (Ref. 2.13). Margin should exist between the upper boundary of the reset setting and the safety bus voltage equivalent to having the minimum allowable switchyard voltage during anticipated worst-case system operating conditions. If operation of the auxiliary power system under normal design transient (starting) conditions, with the safety-related bus voltage equivalent to having the minimum allowable switchyard voltage determines that the bus voltage drops below the dropout setting, then it must recover above the upper boundary of the reset setting prior to the lower boundary of the time delay selected in section 5.4.

The safety bus voltages associated with the upper boundary of the reset setting are evaluated to ensure adequate operation of the auxiliary power system under steady-state (starting) conditions and recovery (running) voltage conditions. The acceptance criteria and means of evaluation is as follows:

5.2.1. Induction motor starting analyses were performed at 6672V which bounds the operational limit of the degraded voltage relay reset setting upper boundary, 6681V (Section 3.9) to ensure that motors and motor-operated valves (MOVs) have adequate starting voltage as specified in section 3.8. Using 6672V provides conservative results for motor starting.

R31

5.2.2. All static loads are evaluated to ensure adequate operating voltages as specified in section 3.7

R31

5.3. Second Level Undervoltage (Degraded Voltage) - Long Time Delay

The long time delay specified in NRC Branch Technical Position PSB-1 is not used at WBN.

5.4. Second Level Undervoltage (Degraded Voltage)- Short Time Delay

5.4.1. The upper boundary of the time delay selected should be less than the safety analysis time allowed for the emergency diesel generators to come up to rated speed and voltage and be ready to accept load. The lower boundary of the time delay should be greater than the time it takes the safety bus voltage to recover above the upper boundary of the degraded voltage relay reset setting established in Section 5.2. The nominal setpoint should be selected considering all errors in accordance with Technical Instruction TI-28 (reference 2.13).

5.4.2. The scenario evaluated for the short time delay is an SI concurrent with the degraded voltage condition such that a block start attempt is made. A determination is made of the time permitted to allow voltage to return above the degraded voltage relay setpoint reset limit under block start transient conditions

and still assure a subsequent start on the diesel if the voltage fails to recover, thus, making this a start-start evaluation.

- 5.4.3. To evaluate the effect of the starting currents during the start-start scenario, the effect on overcurrent protective devices are considered. The board voltages at the onset of the event are, considered normal and are taken from Reference 2.2. The degraded voltage condition presumes that the voltage does not recover but remains below the degraded voltage relay setpoint subjecting the SI initiated motors to starting currents for the time delay selected and then sequence onto the emergency diesel generators. The design calculated worst-case transient voltage dip during the accident loading sequence (from reference 2.2) is used. This is conservative, because a lower voltage would produce less starting current for the motors.
- 5.4.4. Loads evaluated for this condition are safety-related loads required for Unit 1 which would be actuated for an SI. Load types considered are motor loads, vendor package loads, 120VAC motor control circuits, and MCC 120VAC distribution panel loads. The acceptance criteria and means of evaluation is as follows:
 - 5.4.4.1. Motor loads are evaluated to determine the effect of the start-start heating of the overcurrent protective devices, such that starting on the diesel without tripping can be assured.
 - 5.4.4.1.1. 6.9kV Switchgear Breakers - Motors fed from 6.9kV shutdown boards do not require analysis for starting immediately after running at degraded voltage. Overcurrent relays derive their input from current transformers. When power is lost, the relays reset to their normal state.
 - 5.4.4.1.2. 480V Switchgear Breakers - Motors supplied from the 480V Shutdown Boards do not require analysis for starting immediately after running at degraded voltage. Ampetector solid state overcurrent protective devices obtain their input from the current transformers. When the power is lost, the protective devices reset to their normal state.
 - 5.4.4.1.3. 480V MCC breakers feeding static loads - These loads are constant impedance loads and will have reduced current requirements at a degraded voltage, and therefore the reduced heating effect would not challenge their applicable protective devices.
 - 5.4.4.1.4. 480V MCC protective devices feeding MOV's - Thermal Overload Relays (TOL's) used in accident initiated MOV circuits have their trip function bypassed during an accident. The magnetic-only circuit breakers are set above the locked-rotor current of the MOV's and would not be affected by the operation of the MOV. Therefore the protective device heating effects during a degraded voltage for MOV's are not evaluated.
 - 5.4.4.1.5. 480V MCC protective devices feeding motor loads - Motor protective devices consist of a TOL in conjunction with a magnetic-only circuit breaker. The magnetic-only circuit

breakers are set above the locked-rotor current of the motor and would not be affected and therefore not analyzed.

The TOL's were evaluated as follows: The minimum terminal voltage of the enveloping safety-related MCC motor was determined from Reference 2.2. The minimum starting voltage at motor 203-12B is calculated as follows:

$$\begin{aligned} \%V_{st} @ 432 &= 83.77\% \text{ of } 480V \\ \%V_{st} @ 380 &= 83.77\% * \frac{380}{432} = 73.69\% \\ V_{st} &= \frac{73.69\%}{100} * 480 = 353.71V \end{aligned}$$

This is based on worst case voltage of 380V at t=0 for 480V C&A Vent Board 1A1-A with a grid voltage drop from 164kV to 153kV, concurrent with an SI accident.

For added margin, for conservatism 320 volts was used in this evaluation. Next, ETAP PowerStation was used to model a typical low voltage MCC motor in order to determine the total starting time during a degraded voltage event. The total starting time consists of an attempted start at a degraded voltage of 320 volts plus a re-start at rated 460 volts when applied to the diesel generator. The ETAP default dynamic model for a low voltage 50 HP motor was used as the typical WBN MCC motor. The 50 HP model has a higher power factor and efficiency than the smaller motor models. This produces a higher "%Start Load" for the connected mechanical load resulting in slower acceleration. In order to determine a conservatism value for the motor inertia constant "H", the motor acceleration simulation was performed several times at 80% rated voltage until it was found that an "H" value of 0.7 produced a 5 second acceleration time. The results of this simulation are given in output file **LV-H-7** (Attachment 1). Using this typical motor data, a simple three bus system was modeled which could be used to switch the motor from degraded voltage to rated voltage at a specified time (see Attachment 2).

Two cases were analyzed using this model. In the first case, the load was conservatively tripped from degraded voltage at 6 seconds and re-started at rated voltage at 10 seconds. This was conservative in that the load is given 4 seconds to slow down before it is re-energized at 10 seconds. In the second case, the load was tripped at 11.5 seconds and immediately re-started at rated voltage. The results of these cases are given in output files **LV-ACC-1** and **LV-ACC-2** (Attachment 2 and 3). Both acceleration cases show that a typical low voltage MCC motor will be fully accelerated in 12 seconds.

5.4.4.1.6. A generic review of MCC thermal overload (TOL) devices were evaluated to determine if they could trip during the 12 seconds of motor acceleration. The motor draws a reduced starting current during the degraded voltage period. For conservatism, the decay of starting current during motor acceleration has been ignored. For the ITE TOLs installed at WBN on safety-related loads, a starting current of 638% will trip the TOL in 12 seconds (see Reference 2.3). This is based on the TOL tripping in 12 seconds based on 555% of TOL 100% trip amps, which is a minimum of 115% of the motor current. The characteristic curve for size 0, 1 and 2 starters were conservatively used, since the current vs time for size 3 and 4 starters are significantly higher. Additionally, since the accident has just occurred, the equipment ambient temperatures are not elevated to 40°C, and there is an additional margin of 115% in the TOL trip time (see Reference 2.3). Therefore, at a reduced ambient temperature, the TOL would trip in 12 seconds for a starting current of 734%. Due to the reduced starting voltage available at the motors during the degraded condition, a voltage of 1% less than the minimum starting voltage of 85% will be conservatively used. This is based on reference 2.2 for the design calculated worst-case transient voltage dip during the accident loading sequence. This is conservative, because a lower voltage would produce less starting current for the motors. Therefore, this would be equivalent to a motor starting current of 851%. Therefore, the analysis will evaluate all TOL's for class 1E motors that start for an accident that have motor starting current greater than 850% of full load current.

5.4.4.1.7. Protective devices should also be evaluated for the 460V safety-related loads that operate during non-accident conditions. The evaluation should consider that the safety bus voltage is equivalent to operation at the lower boundary of the degraded voltage relay dropout. The protective devices should be evaluated to ensure that operation of the safety-related loads can be sustained indefinitely at this voltage without protective device trip.

5.4.4.2. SI actuated medium voltage motor loads are evaluated to ensure that their thermal damage limits are not exceeded during the start-start event.

This was determined not to be an issue. The medium voltage motors can start with 80 percent of motor rated voltage of 6600V (i.e. 76.5% of 6900V in ETAP). During the start-start scenario the voltage can not drop below 86% without actuating the loss-of-voltage relays, which will trip the offsite supply in no more than 1.14 seconds. Therefore the available voltages at the medium voltage motors will be adequate to ensure starting and accelerating of these loads and will not challenge the motor thermal limits during starting.

5.4.4.3. 120VAC control power transformer (CPT) fuse time characteristics are evaluated to determine if the fuse could blow when carrying rated inrush current of the starter and any other normally energized devices for the safety analysis time from 5.4.1 above. See reference 2.7.

5.4.4.4. MCC 120VAC distribution panel. Fuse time characteristics are evaluated to determine if the fuses melt during the start attempts. It is considered that circuit components required to pick-up during starting will be at inrush conditions.

5.5. Loss-of-Voltage (LOV) Relay Setpoint

The loss of voltage (LOV) relays are an integral part of the degraded voltage protection scheme, and their setting and time delay should be selected to limit the magnitude and duration of degraded voltage the safety buses will encounter. The LOV relay nominal setpoint and associated time delays should be selected considering all errors in accordance with Technical Instruction TI-28 (Ref. 2.13).

5.5.1. The LOV relay voltage setpoint upper boundary should be established to be less than, with some margin, the safety bus voltage equivalent to the design calculated worst-case transient voltage dip during the accident loading sequence. This setpoint should also be less than the TPS calculated security boundary voltage which is based on the grid voltage that is one failure away from failure (see reference 2.11).

5.5.2. The LOV relay voltage setpoint lower limit is selected by evaluating operation of the auxiliary power system under steady-state (running) conditions, with the 6.9-kV Shutdown Board voltage as low as possible while keeping all connected safety-related motor loads above their stall voltage (greater than 70.7 percent of rated motor voltage for NEMA Design "B" motors, see assumption 4.6). The lower limit must also be greater than the 6.9kV Shutdown Board voltage equivalent to having the lowest switchyard voltage that could be sustained without instability or collapse (see reference 2.11).

5.5.3. The lower boundary of the LOV voltage relay time delay should be long enough to ride through short-circuits and other short time system transients (lightning strikes, switching transients, etc.), taking into account the total sensing and clearing times for the above type of events. The time delay upper boundary should be less than the safety analysis time allowed for loss of voltage detection.

6. SUMMARY OF RESULTS

6.1. Degraded Voltage Relay Drop Out Setpoint

6.1.1. Table 1 in Section 9.0, shows the minimum calculated steady-state operating voltage for the boards when the 6.9kV Shutdown Boards are operating at the degraded voltage dropout lower boundary of 6555V. All 6.9kV switchgear and 480V switchgear voltages are equal to or greater than the ANSI C84.1 voltage range B service voltages of 6560V (5V difference is considered insignificant) and 440V, respectively, And 480V mccs are equal to or greater than the ANSI C84.1 voltage range B utilization voltages of 432V.

not need to be started during a time of voltage degradation. Therefore, the voltage is considered acceptable under those conditions.

Note 2 - Percent Required starting voltages were obtained from Att 10.7 of Ref 2.6 of Calculation WBN-EEB-EDQ1999-010001 (Ref 2.2).

6.3 Degraded Voltage Time Delays

6.3.1. Motor Protective Device Evaluation

Per section 5.4.4.1, the only issue requiring evaluation was TOL's protecting safety-related motors that start for an accident. The generic evaluation of TOL's, in section 5.4.4.1.6, showed that only motors having locked rotor current in excess of 850% would have to be evaluated further. A review of the WBN ETAP database, showed that the following motors in Table III have a locked rotor current greater than 850% and start for an accident:

Table III - Locked Rotor Current Summary

ID	Name	Percent
203-12B	Cont Bldg Emerg Press Fan A-A	882
203-2A	Cont Bldg Emerg Air CU Fan A-A	902
205-11A	Cont Bldg Emerg Press Fan B-B	882
205-2A	Cont Bldg Em Air Clnup Fan B-B	902

An evaluation of those four loads show that their TOL's are set at 115% (see reference 2.3). Therefore they would not be an issue, because it would increase their tolerance for tripping an additional 115%.

6.3.2. Fuse Evaluation for 120VAC CPT Circuits and MCC 120VAC Distribution Panel Loads

During the start-start scenario, MCC bus voltages are below the levels used in verifying adequate voltage in previous calculations. Control circuits for motors being started, or other loads being energized, may be at a sustained inrush for the duration of the start attempt (6 seconds) before going to the diesels. Consequently fuses for these circuits must be verified to not actuate for this condition.

Calculation WBNEEBMSTI020019 (Ref. 2.4) and its reference calculation WBPEVAR8909006, were reviewed to identify the typical circuit configurations, their worst case burden during inrush, and the fuse size and type presently required. The current for each circuit was calculated for the burden at rated voltage.

Calculation WBNEEBMSTI020020 (Ref. 2.5) was reviewed to identify the worst case inrush at rated voltage on each MCC 120VAC distribution panel. Each panel uses the same size and type fuse.

The inrush currents were then compared with the fuse melting time-current characteristic to determine the melt times. The results are tabulated in Tables 2, 3 and 4 in section 9.0. Use of inrush currents calculated at rated voltage is conservative for constant impedance devices as the current at degraded voltages will be less. The acceptance pass-fail criteria required for melting time is 12 seconds. From a review of Tables 2, 3, and 4 all fuses will carry inrush current for at least 12 seconds and are considered acceptable.

6.3.3. Non-Accident Degraded Voltage - Motor Protective Device Evaluation

Operation of safety-related loads with the 6.9kV Shutdown Board voltage operating at the lower boundary of the degraded voltage relay, 6555V, will not cause tripping of protective devices. Static loads are not considered, since operation at lower voltage results in less current. The evaluation was based on the following:

R31

6.6kV Motors - The voltage at the boards is 6555V (95% of nominal). The increased motor current would be approximately 105% of nominal. All of the protective relays are set to alarm only for overloads above 125% of nominal. Therefore, operation at the lower boundary of the degraded voltage relay dropout setting would not trip the motors.

R31

480V switchgear motors - The lowest voltage at the 480V Shutdown Boards would be 437 volts (Ref Table 1). The increased motor current would be approximately 110% of normal. All of the switchgear breakers are set above 115% of nominal, and most above 125% of nominal. Therefore, operation at the lower boundary of the degraded voltage relay dropout setting would not trip the motors.

R31

480V mcc motors - The lowest voltage at the 480V mccc would be 432 volts (Ref Table 1). The increased motor current would be approximately 110% of normal. All of the TOLs are set above 115% of nominal, and most above 125% of nominal. All motor breakers are magnetic only, and are not an issue. Therefore, operation at the lower boundary of the degraded voltage relay dropout setting would not trip the motors.

R31

6.3.4. The upper limit for the time delay is 11.5 seconds, which is the maximum total time allowed for loss of voltage detection and emergency diesel generator start in the WBN safety analysis as documented in the FSAR. Based on the above evaluations, it has been determined that protective devices will not trip prior to 12 seconds for operation at a degraded voltage for a period of time, disconnection from offsite power, and reconnection to the emergency diesel generators.

The bounding motor starting analysis from reference 2.2, assumes the plant being in a normal operating mode, with the grid at its expected grid schedule voltage of 165kV, followed by an accident concurrent with the grid falling to a voltage of 153kV. For this unlikely conservative drop in the grid, the degraded voltage relays can be reset in approximately 6 seconds. For conservatism and margin, the lower limit for the time delay is 8.5 seconds.

6.5 Loss of Voltage (LOV) Relay Setpoint and Time Delay

6.5.1. The LOV relay upper analytical limits were determined to be 6072 volts, which is the minimum voltage dip during any expected starting transient from reference 2.2 and 6560 volts which is the lowest 6.9kV Shutdown Board voltage when the grid is degraded down to the security boundary voltage of 141kV. See section 5.5.1. The upper boundary of the LOV relay is 6072 volts from reference 2.20. The current LOV setpoint meets the criteria in section 5.5.1. Table IV shows the 6.9kV Shutdown Board voltages when the grid is degraded down to the security boundary voltage of 141kV.

R32

R32

Calculation: WBN-EEB-MS-TI06-0029, R33

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PAGE 1

1.0 PURPOSE

The purpose of this appendix is as follows:

- Evaluate impact of the degraded voltage on the protective devices of safety related components and devices. This includes loads fed from 6.9kV and 480V switchgear, 480V MCCs, 120V CPT circuits and MCC 120VAC distribution panels. The equipment powered from Unit 2 boards required to support Unit 1 has been already analyzed in the main body of this calculation and therefore, not reviewed in this appendix.
- Ensure the duration of the degraded voltage at a given voltage level does not result in thermal degradation or damage of any required equipment.
- Verify that the existing setting of degraded voltage and loss of voltage relays, as stated in the main body, are acceptable for Unit 2

Analysis to verify adequacy of start and running voltages under degraded voltage conditions and stall voltage analysis is performed in calculation EDQ00099920070002 (Ref. 2.1).

2.0 SOURCES OF DESIGN INPUT/REFERENCES

References listed in Section 2.0 of the main body of this calculation, except references 2.2, 2.3, and 2.4, are also applicable to this appendix. Additional references are as follows:

- 2.1 Calculation EDQ000-999-2007-0002, R18 - Auxiliary Power System Analysis
- 2.2 Calculation EDQ002-999-2008-0004, R12 - 480V Class 1E Protection, Coordination and TOL Heater Calculation – Unit 2
- 2.3 Calculation EDQ002-999-2008-0003, R4 - 120VAC Class 1E MCC Control Circuit Voltage Analysis and Transformer Sizing
- 2.4 Calculation EDQ002-999-2008-0016, R2 – 6.9kV Protection and Coordination Calculation – Unit 2
- 2.5 Calculation WBNEEBMSTI070018, R80 – 120VAC Protection, Coordination and Short Circuit Study

3.0 Design Input and Requirements

- 3.1 Thermal overload heaters data is obtained from Appendix 8 of Reference 2.2.
- 3.2 MCC control circuit loads data is taken from Ref. 2.3.
- 3.3 Degraded Voltage and Loss of Voltage relays Setpoint (Sec 3.9 and Figure 8.3 of the main body)

Degraded Voltage Relay (27DAT, 27DBT, 27DCT)

Setpoint (Nominal) 6600V

Allowable Value: Dropout – 6570V Pickup – 6672V

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Analytical Limit: Dropout – 6555V Pickup – 6681V

Loss of Voltage Relay (27LVA, 27LVB, 27LVC)

Setpoint (Nominal) 6000V

Allowable Value: Dropout – 5967.6V Pickup – 6036V

Analytical Limit: Dropout – 5934V Pickup – 6072V

4.0 DOCUMENTATION OF ASSUMPTIONS AND JUSTIFICATION

Assumptions and justification listed in Sections 4.1 through 4.5 in the main body of this calculation are also applicable to this appendix. These are repeated below:

- 4.1 The resistive loads do not require protective device analysis for degraded voltage.

Justification: For a degraded voltage condition, the current for constant impedance devices decreases. Decreased current reduces the cumulative heating effect on thermal overloads, fuses or circuit breakers.

- 4.2 Motor operated valves do not require protective device analysis for degraded voltage.

Justification: The operation of the valve motors is intermittent and their overload relays are bypassed during accident conditions. Therefore the heating effect has no impact on this analysis.

- 4.3 Motors supplied from the 480V Shutdown Boards do not require protective device analysis for starting immediately after running at degraded voltage.

Justification: Amptector solid state overcurrent protective devices obtain their input from the current transformers. When the power is lost, the protective devices reset to their normal state.

- 4.4 Motors fed from 6.9kV shutdown boards do not require protective device analysis for starting immediately after running at degraded voltage.

Justification: Overcurrent relays derive their input from current transformers. When power is lost, the relays reset to their normal state.

- 4.5 A five second acceleration time is assumed for motors with no acceleration time.

Justification: IEEE-384-1977 (Ref. 2.18 of the main body), provides a typical motor acceleration time range from 2.5 to 4 seconds. Using 5 seconds is conservative.

5.0 COMPUTATIONS AND ANALYSIS

- 5.1 Degraded Voltage and Loss of Voltage Relays Settings

Degraded Voltage and Loss of Voltage relay setpoints are determined in the main body of this calculation and the currently installed settings are documented in Section 3.3 & Figure 8.3. These settings are reviewed to verify their acceptability for Unit 2 as follows:

- 5.1.1 Degraded Voltage relay

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From the auxiliary power system voltage analysis performed in Ref. 2.1, it is seen that under the worst case scenario of an accident with grid dropping from normal 164kV to the minimum of 153kV, the voltage on the 6.9kV shutdown boards will fall below the relay dropout level at $t=0+$ second but recovers to a level above the relay reset value in ≤ 5 seconds (Att. 11.3.b of Ref. 2.1). The minimum time to reset the degraded voltage relay so as not to isolate the shutdown boards from the offsite power is 8.5 second (Figure 8.3).

Also as per the analysis performed in Ref. 2.1, it is verified that all safety related equipment and devices will have adequate starting and running voltage under the degraded voltage reset and dropout conditions respectively, after the proposed modifications in Section 12.0 of Ref. 2.1 are implemented.

5.1.2 Loss of Voltage relay

From the auxiliary power system voltage analysis performed in Ref. 2.1, it is seen that under the worst case scenario of an accident with grid dropping from normal 164kV to the minimum of 153kV, the worst case voltage on the 6.9kV shutdown boards at $t=0+$ second is 88.85% of nominal voltage (Att. 11.3.b of Ref. 2.1) which is above the loss of voltage relay nominal setting of 87% (Figure 8.3).

Based on the above, the degraded voltage and loss of voltage relays existing settings, listed in Section 3.3, are acceptable for Unit 2.

5.2 Effect of the starting currents during the Start-Start scenario on the overcurrent protective devices

5.2.1 The effect of starting currents during Start-Start scenario on overcurrent protective devices for safety related loads required for Unit 1 which would be actuated for an SI are evaluated in Sections 5.4.3 and 5.4.4 in the main body of this calculation. Load types considered are motor loads, Static loads, 120VAC motor control circuits, and MCC 120VAC distribution panel loads. The evaluation performed in Sections 5.4.3 and 5.4.4 in the main body of this calculation is typical and, therefore, also applicable for Unit 2 loads except for the TOLs since the TOLs for Unit 2 loads have been replaced with new TOLs model AR supplied by Square D (Appendix 8 of Ref. 2.2). Unit 2 TOL evaluation is performed in Section 5.2.2 below.

5.2.2 Based on a worst case analysis performed for a 50 HP motor in Section 5.4.4.1.5 in the main body of this calculation, it was determined that a typical low voltage MCC motor will fully accelerate in 12 seconds during start-start scenario. This analysis is also applicable for Unit 2 based on similarity of U1 and U2 equipment.

A generic review of U2 MCC TOL devices (Square D type AR) is performed to determine if they could trip during the 12 seconds of motor acceleration. The motor draws a reduced starting current during the degraded voltage period. Since the motor starting analysis is performed with the worst case voltage dip of 320V at the bus, the reduced starting current is 70% ($320/460$) of the rated locked rotor current. For the replacement Square D type AR TOLs installed at WBN Unit 2 on safety-related loads, a starting current of 525% will trip the TOL in 12 seconds

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(see TOL Time-Current characteristics in Appendix 8 of Reference 2.2). The characteristic curve for size 0, 1 starters was conservatively used, since the current vs time for size 2, 3 and 4 starters are higher. Additionally, since the accident has just occurred, the equipment ambient temperatures are not elevated to 40°C, and there is an additional margin of 115% in the TOL trip time (see Reference 2.2). Therefore, at a reduced ambient temperature, the TOL would trip in 12 seconds for a starting current of 604% (525x1.15). The maximum motor starting current that would yield 604% at degraded voltage is 863% (604/0.7). Therefore, the analysis evaluates all TOL's for class 1E motors that start for an accident that have motor starting current greater than 850% of full load current.

- 5.2.3 Protective devices are also evaluated for the 6.6kV and 460V safety-related motors that operate during non-accident conditions. The evaluation considers that the safety bus voltage is equivalent to operation at the lower boundary of the degraded voltage relay dropout. The protective devices are evaluated to ensure that operation of the safety-related loads can be sustained indefinitely at this voltage without protective device trip.

6.6kV Motors - The lowest voltage at the boards is 6555V (95% of nominal 6900V). The increased motor current would be approximately 105% of nominal. All of the protective relays are set 115% nominal and most at 125% of nominal motor current (Ref. 2.4). The protective relay (51) is set to alarm only. Therefore, operation at the lower boundary of the degraded voltage relay dropout setting would not trip the motors.

480V switchgear motors - The lowest voltage at the 480V Shutdown Boards would be 441 volts or approximately 92% (Attachment 11.3.a of Ref. 2.1). The increased motor current would be approximately 110% of normal. All of the switchgear breakers for motors are set above 125% of nominal (Ref. 2.2). Therefore, operation at the lower boundary of the degraded voltage relay dropout setting would not trip the motors.

480V mcc motors - The lowest voltage at the 480V mccc would be 437 volts or approximately 91% (Attachment 11.3.a of Ref. 2.1). The increased motor current would be approximately 110% of normal. TOLs are set above 115% of nominal for motors with SF 1.0 and above 125% of nominal for motors with SF 1.15 (Ref. 2.2). All motor breakers are magnetic only, and are not an issue. Therefore, operation at the lower boundary of the degraded voltage relay dropout setting would not trip the motors.

- 5.2.4 SI actuated medium voltage (6.6kV) motor loads are evaluated to ensure that their thermal damage limits are not exceeded during the start-start event.

This was determined not to be an issue. The medium voltage motors can start with 80 percent of motor rated voltage of 6600V (i.e. 76.5% of 6900V in ETAP). During the start-start scenario the 6.9kV bus voltage cannot drop below 87% (Section 3.3) without actuating the loss-of-voltage relays, which will trip the offsite supply in no more than 1.14 seconds (Figure 8.3). Therefore, the available voltages at the medium

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voltage motors will be adequate to ensure starting and accelerating of these loads and will not challenge the motor thermal limits during starting.

- 5.2.5 120VAC control power transformer (CPT) fuse time characteristics are evaluated to determine if the fuse could blow when carrying rated inrush current of the starter and any other normally energized devices for the safety analysis time of 11.5 seconds (upper boundary of the degraded voltage relay time delay, Figure 8.3) or 12 seconds in the start-start scenario.

During the start-start scenario, MCC bus voltages are below the levels used in verifying adequate voltage in control circuit voltage drop calculation. Control circuits for motors being started, or other loads being energized, may be at a sustained inrush for the duration of the start attempt (6 seconds) before going to the diesels. Consequently fuses for these circuits must be verified to not actuate for this condition.

Calculation EDQ00299920080003 (Appendices J and K of Ref. 2.3) was reviewed to identify the typical circuit configurations, their worst case burden during inrush, and the fuse size and presently installed fuses of type TRM. The current for each circuit was calculated for the burden at rated voltage.

The inrush currents were then compared with the fuse melting time-current characteristic (page 8 of this appendix) to determine the melt times. The results are tabulated in Tables B-1 and B-2. Use of inrush currents calculated at rated voltage is conservative for constant impedance devices as the current at degraded voltages will be less. The acceptance pass-fail criteria required for melting time is 12 seconds. From a review of Table B-1 all fuses will carry inrush current for at least 12 seconds and are considered acceptable.

- 5.2.6 MCC 120VAC distribution panel fuse time characteristics are evaluated to determine if the fuses melt during the start attempts. It is considered that circuit components required to pick-up during starting will be at inrush conditions.

Calculation WBNEEBMSTI020020 (Attachment 10.1, 10.2 of R15 of Ref. 2.5 in the main body of this calculation) was reviewed to identify the worst case inrush at rated voltage on each MCC 120VAC distribution panel. Each panel uses KTK type fuses of the 5 amps size. From a review of Table B-2 all fuses will carry inrush current for at least 12 seconds and are considered acceptable.

6.0 SUMMARY OF RESULTS

Based on Section 5.0, following is the summary of results:

6.1 Degraded Voltage Relay and Loss of Voltage relay Setpoint

Existing setpoints for the degraded voltage relay and loss of voltage relay are acceptable.

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6.2 Protective Device Evaluation

6.2.1 Motors Actuated by SI Signal

As discussed in Section 5.2.1, there is no adverse effect of the start-start heating on the overcurrent devices on the safety related motors which would be actuated by safety injection signal and powered from safety related 6.9kV and 480V switchgears and 480V MCCs under the degraded voltage conditions.

6.2.2 Non-Accident Safety Related Motors

Based on the analysis in Section 5.2.3, operation of safety-related loads with the 6.9kV Shutdown Board voltage operating at the lower boundary of the degraded voltage relay, 6555V, will not cause tripping of protective devices. Static loads (constant impedance) are not considered, since operation at lower voltage results in less current.

6.2.3 TOL Evaluation

The generic evaluation of TOL's in Section 5.2.2, showed that only motors having locked rotor current in excess of 850% would have to be evaluated further. A review of the WBN ETAP database (Ref. 2.1) showed that there are **no** motors with a locked rotor current greater than 850% and start for an accident.

6.2.4 Fuse Evaluation for MCCs 120VAC CPT Circuits and 120VAC Distribution Panel Loads

Based on Sections 5.2.5 and 5.2.6, fuses for all 120VAC CPT Circuits and 120VAC Distribution Panel loads are acceptable and will not blow or melt during the 12 seconds criteria during a start-start scenario.

- 6.3 The upper boundary limit for the time delay is 11.5 seconds (Figure 8.3), which is the maximum total time allowed for loss of voltage detection and emergency diesel generator start. Based on the above evaluations, it has been determined that protective devices will not trip prior to 12 seconds for start-start operation of motors at a degraded voltage at which time disconnection from offsite power and reconnection to the emergency diesel generators occurs.

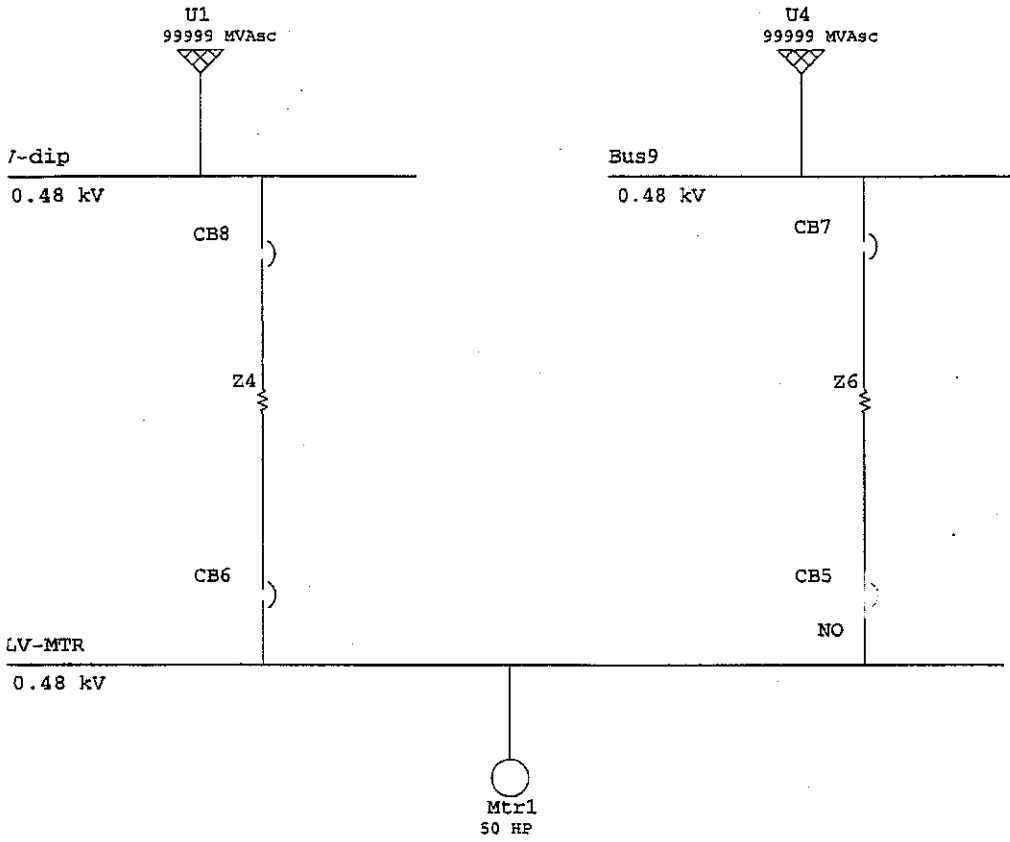
7.0 CONCLUSIONS

The above analyses have demonstrated that in the event of degraded voltage conditions, all safety related loads required for safe shutdown of the unit will be available and perform their intended safety function.

Acceleration of Typical Class 1E Motors (@ 80% MRV)

Appendix No. Attachment 1
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 1 of 16

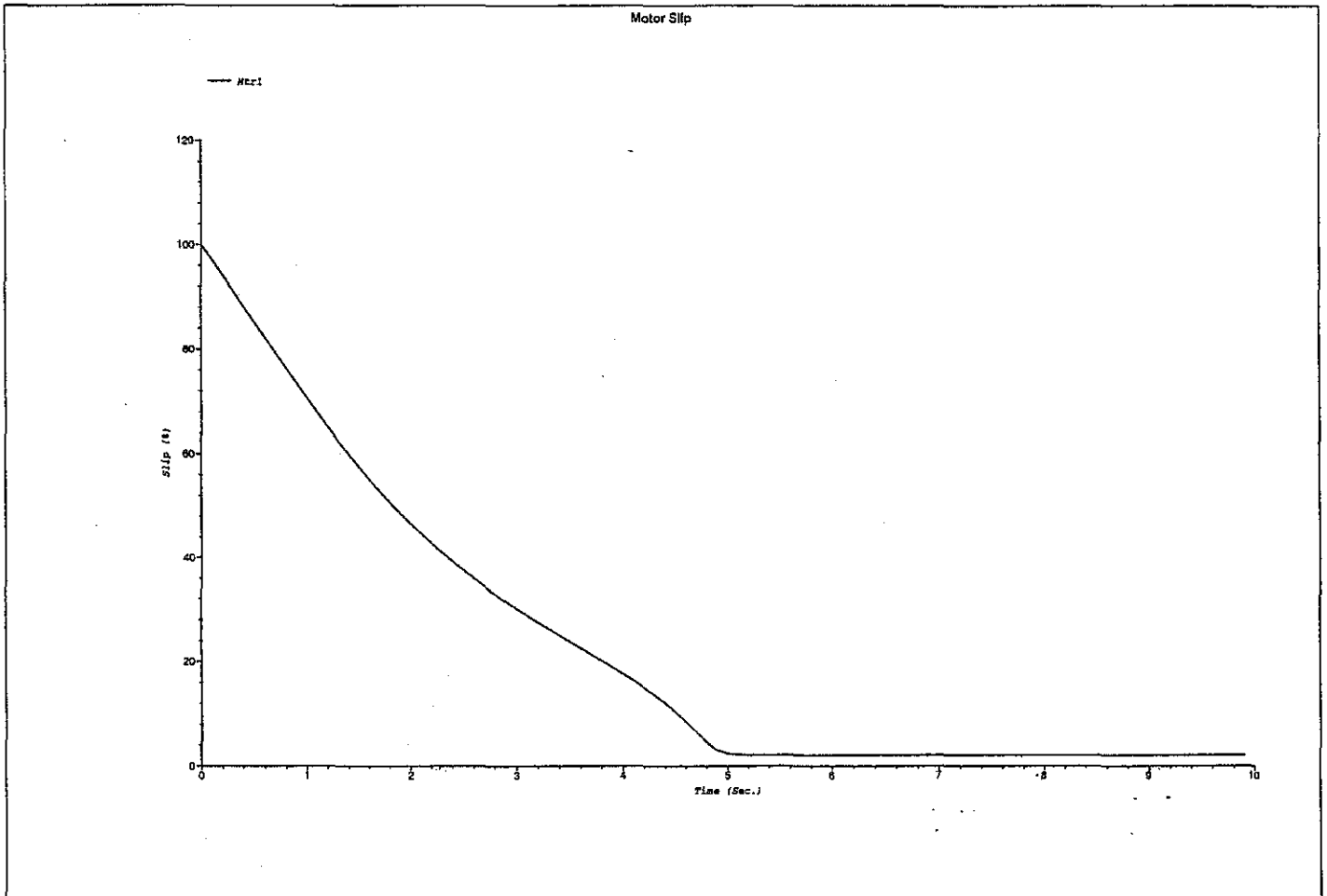
One-Line Diagram - OLV1



Appendix No. Attachment 1
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 2 of 16

May 26, 2000

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Location:
Contract:
Engineer:



Project File: DVMotorAcc

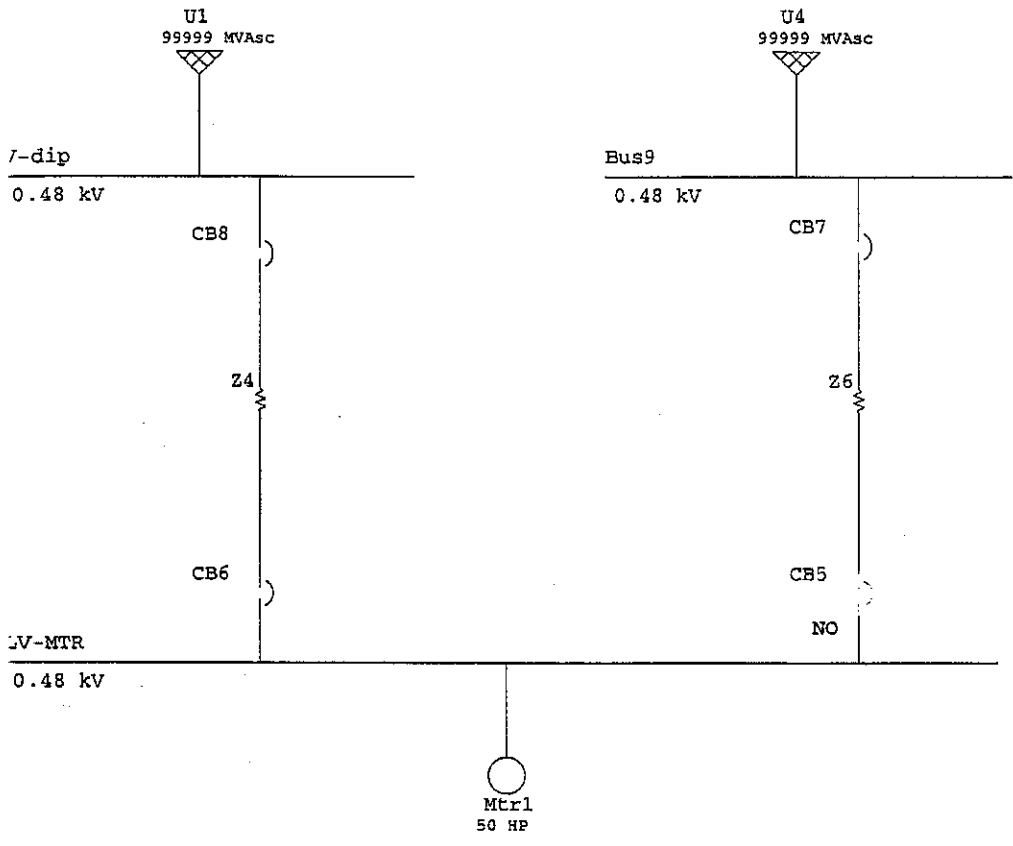
Output Report: Mtr1@80%

Appendix No. Attachment 1
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 3 of 16

Acceleration of Typical Class 1E Motors; Motor Voltage at 320 V
Diesel Generator Breaker Close @ 10 Sec.

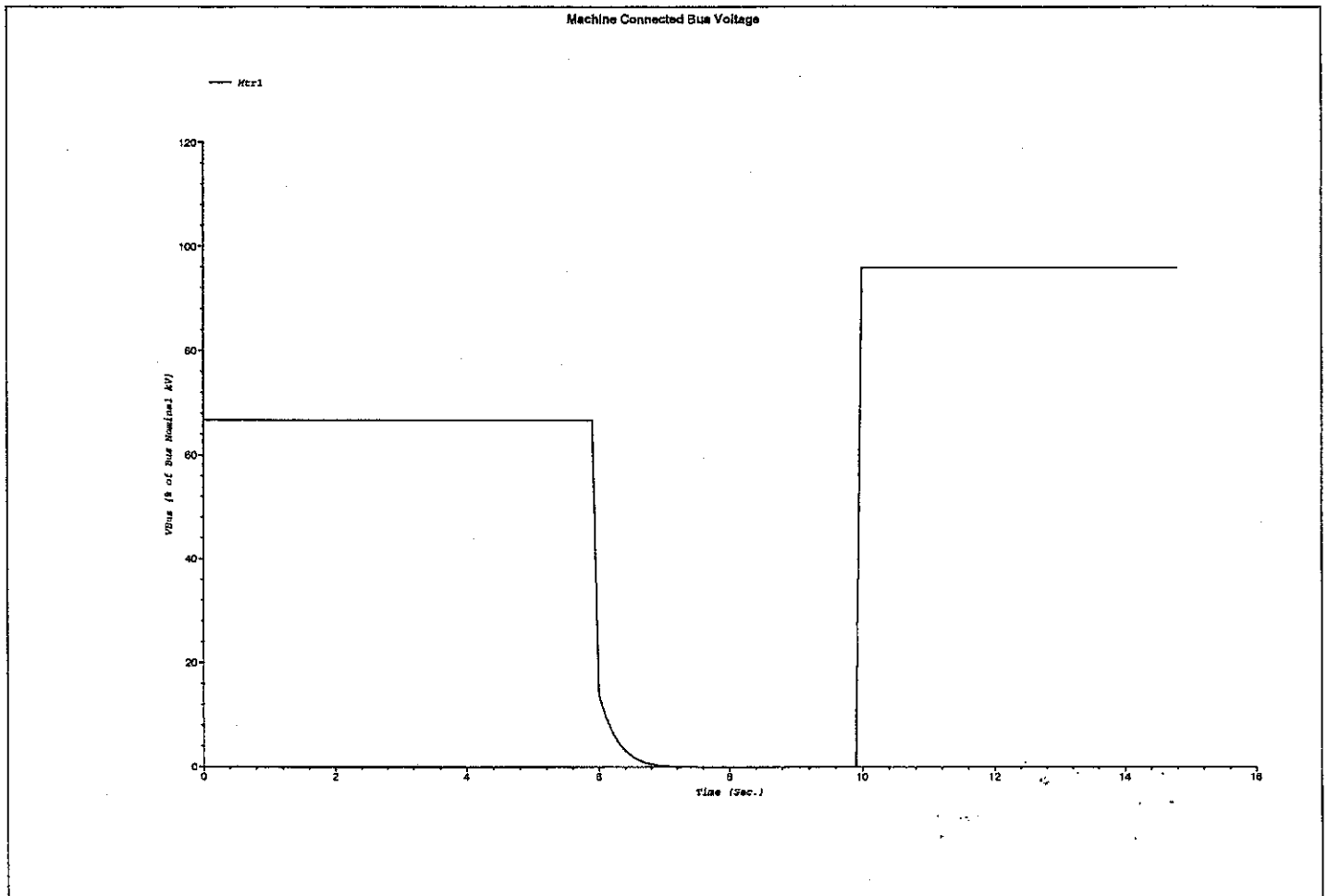
Appendix No. Attachment 2
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 1 of 23

One-Line Diagram - OLV1



Appendix No. Attachment 2
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 2 of 23

Project:
Location:
Contract:
Engineer:



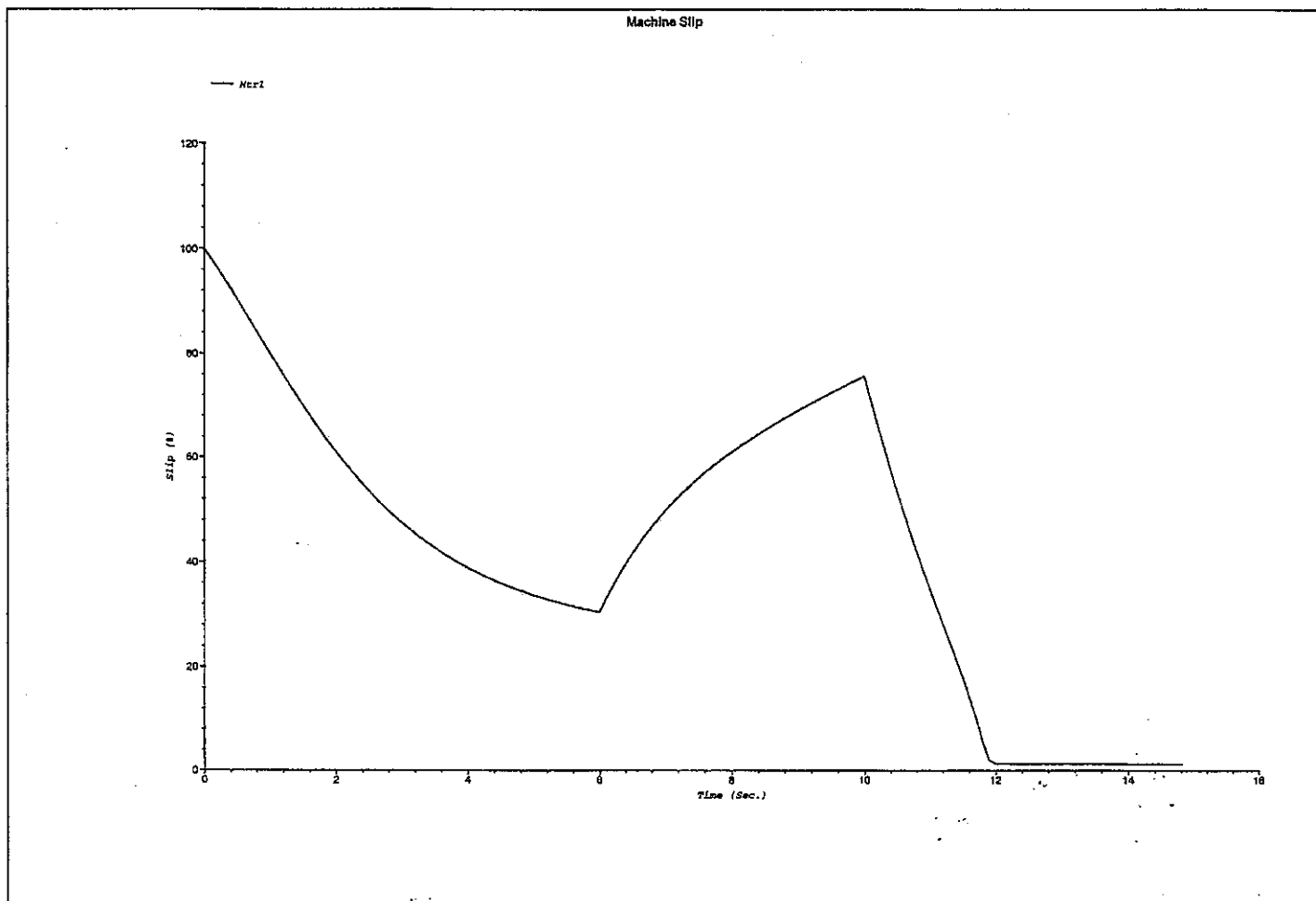
Project File: DVMotorAcc

Output Report: DV-Cas1

Appendix No. Attachment 2
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
Sheet No. 3 of 23

May 26, 2000

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Location:
Contract:
Engineer:



Project File: DVMotorAcc

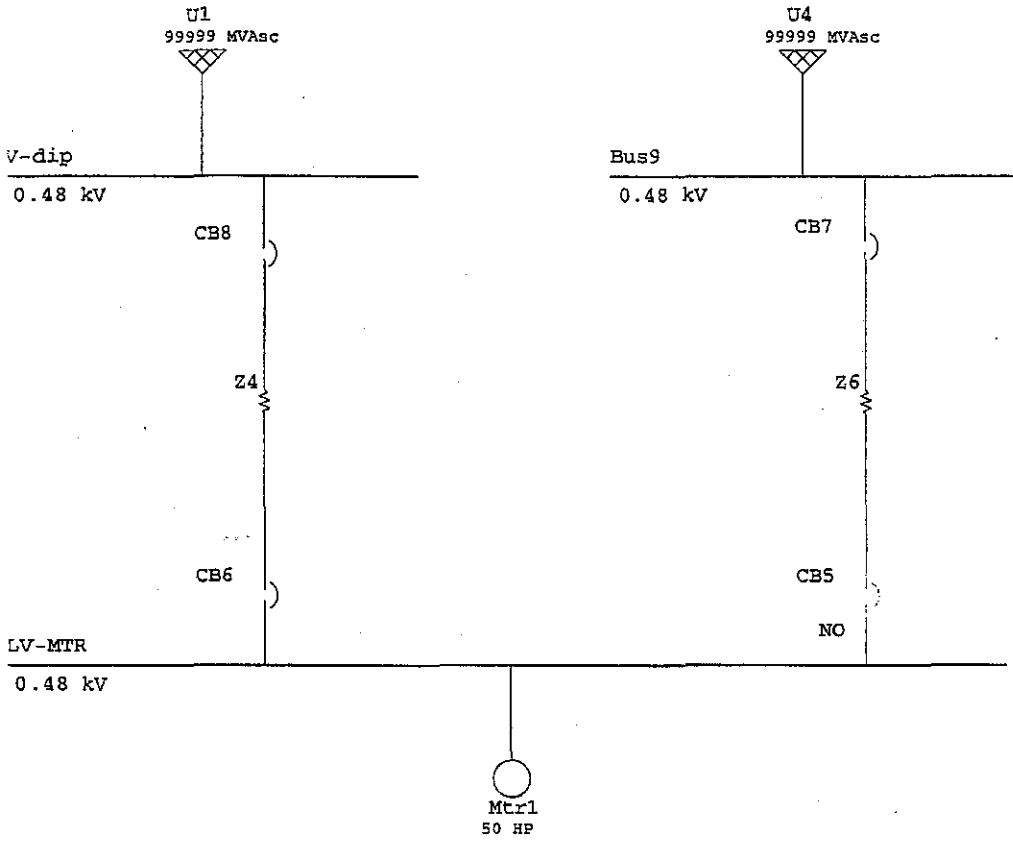
Output Report: DV-Cas1

Appendix No. Attachment 2
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
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Acceleration of Typical Class 1E Motors; Motor Voltage at 320 V
Diesel Generator Breaker Close @ 11.5 Sec.

Appendix No. Attachment 3
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
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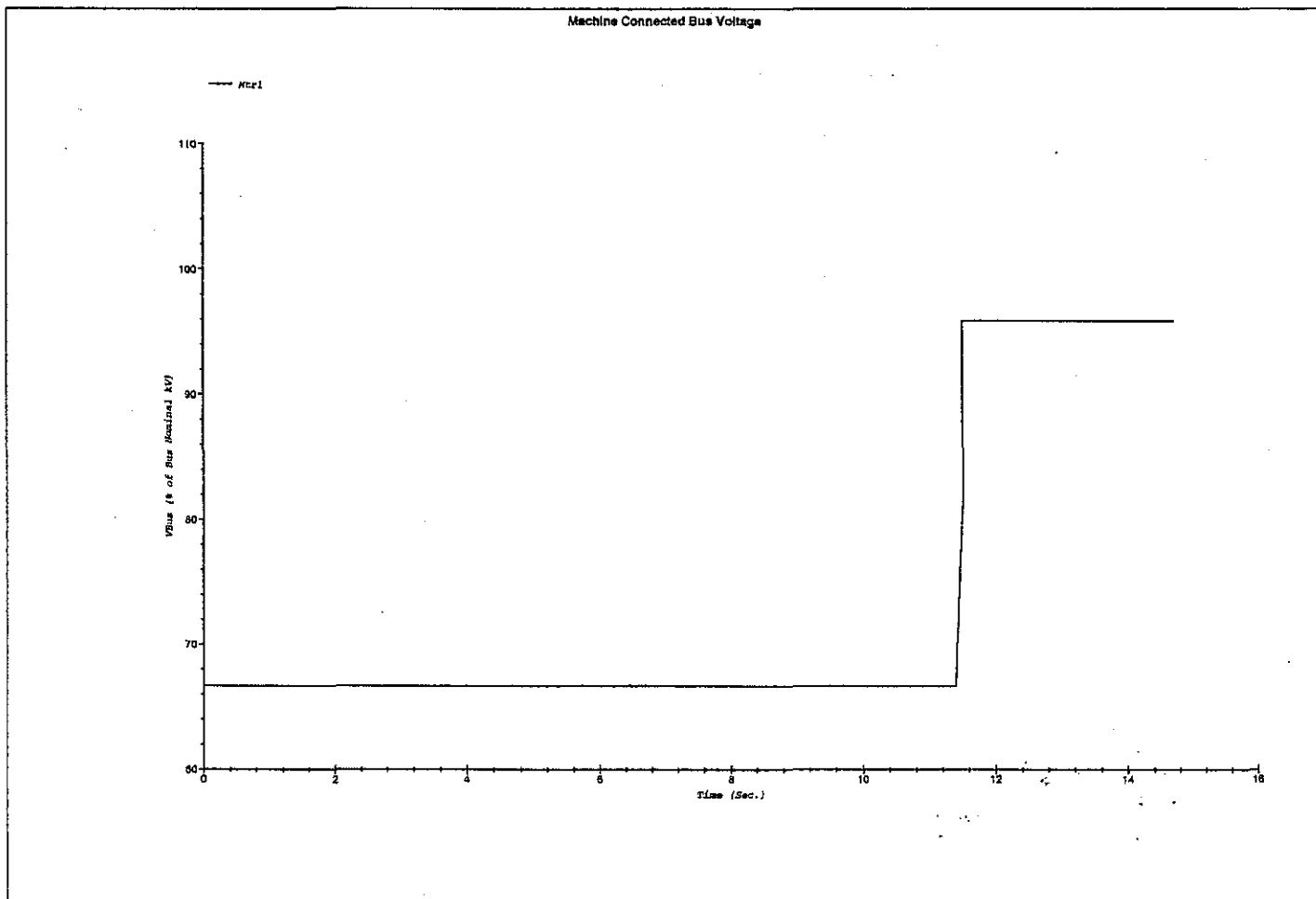
One-Line Diagram - OLV1



Appendix No. Attachment 3
Calc. No. WBN-EEB-MS-TI06-0029 Rev. 29
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May 26, 2000

Project:
Location:
Contract:
Engineer:



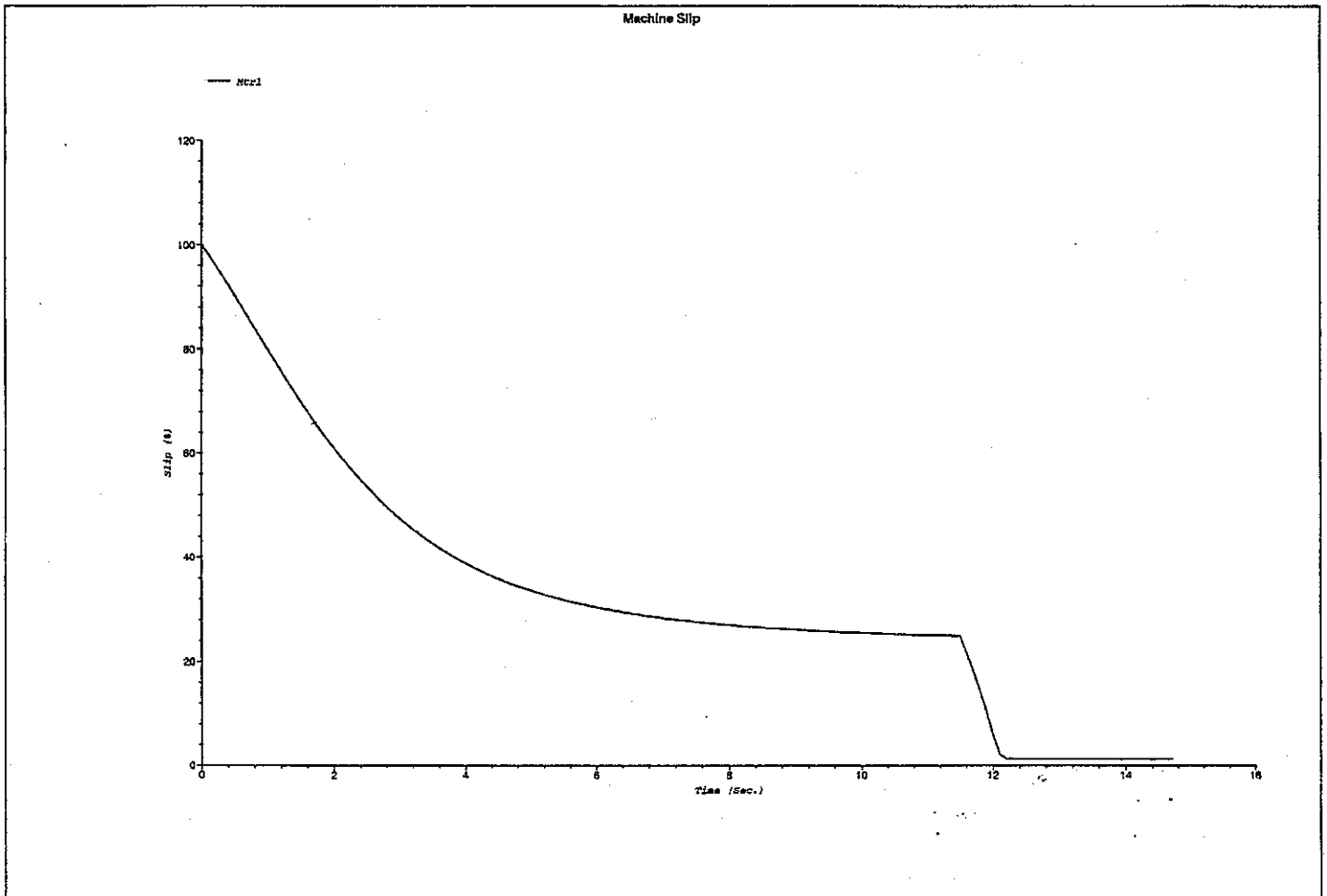
Project File: DVMotorAcc

Output Report: DV-Case2

Appendix No. Attachment 3
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May 26, 2000

Project:
Location:
Contract:
Engineer:



Project File: DVMotorAcc

Output Report: DV-Case2

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