## HANGER REPORT <br> Midland Plant Units 1 and 2

## August 9, 1982

# MIDLAND PLANT UNITS 1 AND 2 <br> HANGER REPORT 

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1. IOM, R. Tulloch to L. Curtis, 5/13/82 (Com 069863)
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# MIDLAND PLANT UNITS 1 AND 2 <br> FiANGER REPORT 

## I. INTRODUCTION

## A. Reason for Overinspection

The NRC conducted an inspection at the Midland jobsite from May 18 to 22,1981 . As a result of that inspection, two items of noncompliance were documented. Item 329/81-12-11; 330/81-12-12 states in part ". . . seven large bore pipe restraints, supports, and anchors were not installed in accordance with design drawing and specification requirements." Item 329/81-12-12; 330/81-12-13 states in part ". . . QC inspectors inspected and accepted 6 of 7 large bore pipe restraints, supports, and anchors that had not been installed in accordance with design drawings and specifications as determined by the NRC inspector."

In the Consumers Power Company response to those items of noncompliance (CPCo letter Serial $14601,10 / 30 / 81$ ), a commitment was made for the Midland Project Quality Assurance Department (MPQAD) to perform an overinspection of a sample of hangers installed before January 1981.

The purpose of the overinspection was to assess the acceptability of the installations and the adequacy of the original inspections performed by Bechtel Quality Control (QC).

## B. Overinspection Results

One hundred twenty-three hangers were overinspected by MPQAD. With one exception, all of the hangers were installed before January 1981.

The results of the $M P Q A D$ overinspection are summarized as follows:

| Hangers overinspected | 123 |
| :--- | ---: |
| Hangers acceptable (no nonconformances) | 68 (55\%) |
| Characteristics overinspected | 9,630 |
| Characteristics acceptable | $9,504 \quad(98.7 \%)$ |

The statistics given above, with some variances, were provided to the NRC during an exit meeting held on April 23, 1982 (see Attachment 15).

The nonconformances identified in the overinspection were documented on MPQAD Nonconformance Reports (NCRs) M-01-9-2-007, M-01-9-2-010, M-01-5-2-014, and M-01-5-2-017.

As issued in February 1982, the NCRs listed above identifed the 55 nonconforming hangers and grouped the 126 nonconforming characteristics into 88 items. (An item is one or more nonconforming characteristics of the same kind on a single hanger.)

## C. Corrective Action and Safety Evaluation of Identified Nonconformances

Upon receipt of the NCR, construction and QC reviewed each nonconforming characteristic and item and performed a reinspection to understand them more fully. On the basis of the review and reinspection, the items were dispositioned to perform one of the following:

- Rework them (Category A)
- Accept them as is, based on redline drawings approved by Field Engineering in acroordance with Field Procedure FIP-1. 112 (Citegory B)
- Accept them as is, based on the redline drawing approved by Project Engineering in accordance with Procedure EDPI 4.46 .9 (Category C)
- Reclassify them as conforming to requirements based on the reinspection results and based on agreements with MPQAD (Category D)
- Submit them for further dispositioning to project engineering (Category E)
The above dispositions were provided to the MPQAD as formal responses to the NCR (see Attachments 7 through 10).
The items dispositioned for Categories $A, B, C$, and $D$ above were evaluated by Project Engineering to have no impact on safety.


## D. Adjusted Reported Results and Dispositions

Based on the reinspection results concurred with by MPQAD and the disposition categories above, the 88 items were dispositioned as follows:

## Category

| A | 21 |
| :--- | :--- |
| B | 31 |
| C | 13 |
| D | 21 |
| E | $\underline{2}$ |

TOTAL 88

Based on the foregoing information, for the total number of hangers installed before January 1, 1981, there is $95 \%$ confidence that at least $97.5 \%$ of the characteristics of the hangers conform to the requirements.

## II. POTENTIAL GENERIC EVALUATION OF IDENTIFIED

## NONCONFORMANCES

## A. Introduction

The 67 nonconforming items remaining after adjusting the overinspection results have been categorized into 14 specific anomaly groups, as shown in Table 1 and further described in Table 2. Additionally, Table 1 provides a rationale as to the generic implications of each anomaly group and as to actions already taken and to be taken.

## B. Conclusions

Table 1 lists four anomaly groups that are of generic concern if they should occur elsewhere. To identify these occurrences, various examinations as described in Section IV will be utilized. Once identified during these examinations, any nonconformances will be properly dispositioned.

## C. Tables 1 and 2

Tables 1 and 2 categorize and describe the 14 specific anomaly groups. These tables are found on the following pages.

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Missing components could have an effect on the ability of the support to function properly.

Substituted material was found to be equal to or better

Review of existing conditions indicates conditions are acceptable because they are in accordance with the specifica. 5.10 of Specification 7220-M-326 when making material substitutions and ment. The four occurrences do is warranted.

## Action Required

a) Field Engineering and Quality Control are required to perform inspections of each hanger in accordance with the requirements of Specification 7220-M-326 and AAPD/PSP-G-11.1 prior to turnover. This is to verify the hanger configuration conforms to the latest design drawings.

These additional inspections will identify eny missing components as reguired by the design.

Records of completion will be secorded on the p-119 (small bore) and P-129 (large bore) form as required by Specification 7220-M-326.

Quality Control procedure AAPD/PSP G-11.1 will provide additional guidelines.

Field is to utilize field change procedures for future substitutions.


No further action beyond engineering analysis and a previous analysis and testing is required.

## Same as above

Revise Specification 7220-M-326 to define "member length" on bill of material as being provided to facilitate shop fabrication only.

|  | Anomaly | $\begin{gathered} \begin{array}{c} \text { Number } \\ \text { of } \\ \text { Sccurrences } \end{array} \\ \hline \end{gathered}$ | Generic Concern | Rationale | Action Required |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 5A. | Dimensional violations (other than anchors) | 11 | No | If the location of the member point of attachment to builcing structure and centerline of pipe are within tolerance. there is no effect on the design or structural capability of the support. | Revise Specification $7220-\mathrm{M}-326$ to clarify the tolerances. with this clarification, the previously identified nonconformances are eliminated. |
| 58. | ```Dimensional violations (anchors)``` | 2 |  | Same as above | Same as above |
|  | Clearance between pipe and support |  |  |  |  |
|  | A) Zero clearance | 5 | Yes | Binding of pipe by box or $U$ bolt does not allow pipe to move axially. | Zero clearance and excessive clearance are attributes checked during planned engineering functional stress walkdown. This walkdown will cover all Q supports where this condition could exist. |
|  | B) Excessive clearance | 4 | Yes | Clearance is greater than that specified in drawings, but this does not affect the structural integrity of the component. If a seisinic event occurs, the integrity of piping system could be compromised (additional impact loads). |  |
| Fixed component rotation |  |  |  |  |  |
|  | A) WF in tension rotated 90 degrees | 1 | Yes | As installed, the load (tension) carrying capability of the componint was not compromised. Th s may not be true for other pussible rotations of components. | These cases have been found acceptable. The inspections described in the "Action Required" for Anomaly 1 will address this anomaly as well. |
|  | B) Angle rotated 90 degrees (only equal leg angles) | 1 | Yes | An equal leg angle has equal moments of inertia when rotated in increments of 90 degrees. This would not be true for unequal leg angles. | Same as Anomaly 7A |

$\qquad$
11. Irregulairty in weld (grinding of weld)
12. Incorrect weld
A) Weld in wrong place instead of northsouth)
B) Rotated weld
$i$

Concern
No

Evaluation by engineering indicates that, as installed, this baseplate is acceptable; one occurrence in the total sample does not indicate this is of generic concern.

Hanger design normally pro$v i d e s$ for $\pm 5$ degrees rotation in the direction of least pipe movement. If rotating movement is larger, this could restrict pipe movement.
nt.
a) Weld is not undersized.
b) Structural integrity has not been violated.

Flared bevel groove weld used to hold a shim in place with very low weld loading.

Stress analysis required. Rotated welds may provide strength only in secondary axis.
Hanger location dimensions on hanger drawings are reference dimensions for small bore and are so noted on the drawings. The large bore hangers are controlled by hanger drawings. Conditions are unique to skewed pipe.
(20
axis.

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Action Required
Relocation of hangers to be consistent with the location of the pipe is not a problem for this type of occurrence.

Field will request design changes for all future occurrences.
Project Engineering will also
judge the acceptability of hanger location during functional walkdown.

Same as Anomaly 7A

Same as Anomaly 7A

Currently, Specification 7220-M-326(Q), Section 6.1, requires that Field Engineering observe pipe movement during plant heatup. Restricted motion would be noted at that time.

Project Engineering review of this case completed all required action.


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## TABLE 2

## DESCRIPTION OF ANOMALIES

## ANOMALY 1: MISSING COMPONENTS

## Description of Anomaly

Missing components, e.g., nuts, bolts, washers, cotter pins, lock nuts

Hanger No.
FSK-M-2ECB-4-4-H5, Rev 2 (Item a)

ESK-M-2EBB-3-4-H1,
Rev 1 (Item $a, b, c$ )

## No. of Occurrences

1

3

Ref: CPCo NCR

$$
M-01-5-2-014
$$

$$
\mathrm{M}-01-5-2-014
$$

Midland Plant Units 1 and 2 Hanger Report

TABLE 2 (continued)

## ANOMALY 2: MATERIAL SUBSTITUTION

## Description of Anomaly

a. The drawing requires the jam nuts to be $S A-307, G R B$. On the contrary, jam nuts SA-194, $2 H$ were used.
b. PGS 104 pipe strap specified; PGS 111 installed.
c. W5 I-beam specified; W6 I-beam installed.

| Hanger No. | No. of Occurrences | Ref: CPCo NCR |
| :---: | :---: | :---: |
| $\begin{aligned} & \text { FSK-M-1CCB-69-1-H1, } \\ & \text { Rev } 3 \text { (a) } \end{aligned}$ | 1 | M-01-5-2-017 |
| $\begin{aligned} & \text { FSK-M-1CCB-69-1-H2 } \\ & \text { Rev } 2 \text { (a) } \end{aligned}$ | 1 | M-01-5-2-017 |
| $\begin{aligned} & \text { FSK-M-2HBC-145-1-H5 } \\ & \text { Rev } 2 \text { (c) } \end{aligned}$ | 1 | M-01-5-2-014 |
| FSK-M-2GCB-21-1-H1, <br> (b) | 1 | M-01-9-2-010 |

TABLE 2 (continued)

## ANOMALY 3: UNDERSIZE WELDS

## Description of Anomaly

Undersize welds include: a) weld size which is either entirely or partially less than specified in the drawing, b) undercut (burnout), and c) noncontinuous weldment.

3A - Component Supports Other Than Anchors:

(a)

(b)

(c)

| Hanger No. |
| :--- |
| $1-610-4-27, \operatorname{Rev} 4(\mathrm{~b})$ |
| $2-604-3-18, \operatorname{Rev} 1(\mathrm{c})$ |
| $2-611-7-33, \operatorname{Rev} 1(\mathrm{a})$ |
| $2-611-6-5, \operatorname{Rev} 3(\mathrm{a})$ |
| $2-613-4-19, \operatorname{Rev} 3(\mathrm{a})$ |
| $2-619-6-11, \operatorname{Rev} 3(\mathrm{a})$ |
| $1-612-2-2, \operatorname{Rev} 1(\mathrm{a})$ |

No. of Occurrences
1
1
1

2

1
1

1
3B - Anchors (see Figure 3a above):

No. of Occurrences
1
1
1

Ref: CPCO NCR

$$
\begin{aligned}
& \mathrm{M}-01-9-2-007 \\
& \mathrm{M}-01-9-2-007 \\
& \mathrm{M}-01-9-2-010 \\
& \mathrm{M}-01-5-2-014 \\
& \mathrm{M}-01-5-2-014 \\
& \mathrm{M}-01-5-2-014 \\
& \mathrm{M}-01-5-2-014
\end{aligned}
$$

| Hanger No. | No. of Occurrences | Ref: CPCO NCR |
| :---: | :---: | :---: |
| 2-619-1-19, Rev 1(a) | 1 | M-01-9-2-010 |
| 1-612-4-33, Rev 1/F1 (a) | 1 | M-01-5-2-014 |
| 1-616-6-28, Rev 1(a) | 1 | M-01-9-2-007 |

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TABLE 2 (continued)
ANOMALY 4: BILL OF MATERIAL PROBLEM

## Description of Anomaly

Component dimensions are not in accordance with the dimensions listed on the bill of materials.


| Hanger No. | No. of Occurrences | Ref: CPCo NCR |
| :---: | :---: | :---: |
| 1-616-10-22, Rev 4 | 1 | M-01-9-2-007 |
| FSK-M-2HBC-216-5-H3, Rev | 1 | M-01-9-2-010 |
| 2-604-16-15, Rev 0/F1 | 2 | M-01-9-2-010 |
| 2-619-1-19, Rev 1 | 1 | M-01-9-2-010 |
| $\begin{aligned} & \text { FSK-M-2HBC-219-1-H1, } \\ & \text { Rev } 0 \end{aligned}$ | 1 | M-01-9-2-010 |
| $\begin{aligned} & \text { FSK-M-2HBC-144-1-H8, } \\ & \text { Rev } 1 \end{aligned}$ | 1 | M-01-5-2-014 |
| 2-619-6-11, Rev 3 | 2 | M-01-5-2-014 |
| $\begin{aligned} & \text { FSK-M-2GCB-22-1-H3, } \\ & \text { Rev } 0 \end{aligned}$ | 1 | M-01-5-2-014 |

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## TABLE 2 (continued)

## ANOMALY 5: DIMENSIONAL VIOLATION

## Description of Anomaly

Anqular and linear dimensions are not in accordance with the drawing.

5A - Component Supports Other Than Anchors:

(a)

| Hanger No. | No. of Occurrences | Ref: CPCo NCR |
| :---: | :---: | :---: |
| 2-611-6-5, Rev 3 | 1 | M-01-5-2-014 |
| 1-619-14-4, Rev 2 | 1 | M-01-9-2-007 |
| 1-610-4-27, Rev 4 | 1 | M-01-9-2-007 |
| 1-616-10-22, Rev 4 | 1 | M-01-9-2-007 |
| 1-612-2-3, Rev 1 | 1 | M-01-9-2-007 |
| FSK-M-1HBC-219-1-H1, Rev 2 | 1 | M-01-9-2-007 |
| 2-616-8-2, Rev 7 | 1 | M-01-9-2-010 |



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TABLE 2 (continued)

## ANOMALY 6: CLEARANCE BETWEEN PIPE AND SUPPORT

## Description of Anomaly

Clearances between pipe and support (strap, u-bolt, box) do not conform to the drawing/specification tolerances, e.g., zero clearance, excessive clearance.


ZERO CLEARANCE
(a)


EXCESSIVE CLEARANCE
(b)

Hanger No.
2-604-16-15, Rev 0/F1(a)
$2-657-43-6$, Rev 1 (b)
2-619-6-11, Rev 3(a)
FSK-M-1HBC-144-1-H3, Rev 1 (b)

1-648-7-58, Rev 1/F1 (b)
1-657-37-9, Rev 2(a)
FSK-M-OHBC-142-1-H1, Rev 4 (b)

No. of Occurrences
1
1
1

1

1

1
1

Ref: CPCO NCR

$$
\begin{aligned}
& M-01-9-2-010 \\
& M-01-9-2-010 \\
& M-01-5-2-014 \\
& M-01-5-2-017
\end{aligned}
$$

$$
M-01-5-2-017
$$

$$
M-01-5-2-017
$$

$$
M-01-5-2-017
$$

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TABLE 2 (continued)

| Hanger No. | No. of Occurrences | Ref: CPCo NCR |
| :---: | :---: | :---: |
| $\begin{aligned} & \text { FSK-M-1CCB-69-1-H2, } \\ & \text { Rev 2(a) } \end{aligned}$ | 1 | M-01-5-2-017 |
| $\begin{aligned} & \text { FSK-M-1HBC-145-1-H9, } \\ & \text { Rev 2(a) } \end{aligned}$ | 1 | M-01-5-2-017 |

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TABLE 2 (continued)
ANOMALY 7: FIXED COMPONENT ROTATION
Description of Anomaly
Support member rotated _ degrees from design sketch.

(7b)

| Hanger No. |
| :---: |
| $2-639-13-5, \operatorname{Rev} 2(a)$ |
| $2-604-17-2, \operatorname{Rev} 1(b)$ |

No. of Occurrences
1
1

Ref: CPCO NCR
M-01-9-2-010
M-01-9-2-010

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TABLE 2 (continued)

## ANOMALY 8: LOCATION OF HANGERS

Description of Anomaly
Hangers are not installed in accordance with the elevation and coordinates specified in the drawings. For example:


Hanger No.
FSK-M-2HBC-217-1-H2, Rev 1

1-612-2-2, Rev 1
2-619-6-11, Rev 3
1-612-3-12, Rev 1
2-619-1-20, Rev 1

No. of Occurrences
1

1
1
1
1

Ref: CPCO NCR

$$
M-01-9-2-010
$$

M-01-5-2-014
M-01-5-2-014
M-01-5-2-014
M-0. -5-2-014

TABLE 2 (continued)

## ANOMALY 9: GAP BETWEEN WALL AND BASEPLATE

Description of Anomaly
Lower right-hand corner of baseplate exceeds gap tolerance.


[^0]No. of Occurrences
Ref: CPCO NCR

1
M-01-9-2-010

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TABLE 2 (continued)

## ANOMALY 10: CLEVIS ROTATION

Description of Anomaly
Clevis rotated 90 degrees from drawing configuration.


| Hanger No. | No. of Occurrences |  | Ref: CPCO NCR |
| :---: | :---: | :---: | :---: |
| $2-604-2-35, ~ R e v ~ 1 ~$ | 1 | 1 | M-01-9-2-010 |
| $2-619-2-19$, Rev 1 |  |  | M-01-5-2-014 |

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## TABLE 2 (continued)

## ANOMALY 11: IRREGULARITY IN WELD

## Description of Anomaly

The vertical support weldment exhibits an approximately 2 -inchlong groove, creating a sharp edge.


| Hanger No. | No. of Occurrences |  |
| :--- | :---: | :---: | :---: |
| FSK-M-1HBC-219-1-H1 <br> Rev 2 | 1 | Ref: CPCo NCR |

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TABLE 2 (continued)

## ANOMALY 12: WELD IN WRONG PLACE

## Description of Anomaly

Field welds do not conform to drawing requirements, e.g., a, b) welds located at the ends instead of at the sides, c) weld configuration is not as shown on the drawing.

(c)

Hanger No.
0-618-1-6, Rev 0(b)
$2-617-8-5$, Rev 2(c)
FSK-M-2HBC-219-1-H1, Rev 0 (a)

No. of Occurrences
1

1

1

Ref: CPCO NCR

$$
\mathrm{M}-01-5-2-017
$$

$$
M-01-9-2-007
$$

$$
M-01-9-2-010
$$

TABLE 2 (continued)

## ANOMALY 13: THREAD ENGAGEMENT

## Description of Anomaly

At sight holes of support rod, no threads are visible. Thread engagement (at the lower end only) was 1 inch, instead of 1-1/2 inch.


Hanger No.
No. of Occurrences
Ref: CPCO NCR
1-616-8-2, Rev 7
1
M-01-9-2-010

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TABLE 2 (continued)

## ANOMALY 14: MISCELLANEOUS

Description of Anomaly
Angle clips are in wrong location.


Hanger No. 0-617-7-13, Rev 0

No. of Occurrences
1

Ref: CPCo NCR M-01-5-2-017

## III. PROCESS CORRECTIVE ACTION

## A. Completed Process Corrective Action

In January 1981 a QC Training Coordinator was appointed. The Training Coordinator's primary function is to arrange indoctrination and orientation training for new QC Engineers (QCEs). This training gives the QCE a betcer understanding of the Project Quality Assurance ( $Q A=/ \overline{ }$ C programs. The Training Coordinator reviews all training and certifications to ensure that the new QCE fulfills all requirements set forth in PSP G-8.1, which is Bechtel's procedure for complying with ANSI N45.2.6.

In addition to the Training Coordinator responsibilities, each discipline group supervisor (e.g., pipe supervisor) has created training programs for new QCEs. Training involves both classroom and on-the-job training (OJT). This training is then documented on standard training letters and OJT checklists (see Attachments 16 and 17). During training, each group supervisor tests the new QCE to determine areas in which the QCE needs additional training. In 1981 approximately 1,400 documented training sessions were performed by the pipe/mechanical discipline.

Audiovisual training programs have also been established to help familiarize new QCEs with the areas to which they will be assigned (e.g., pipe, hangers). Examples of audiovisual aids are: audioviewer projector, slide/tape programs, and overhead transparencies.

In early 1981, a formal Level II QCE training program was established to better familiarize the potential Level II QCE with QA/QC philosophy, organization, and program requirements. The program also instructs in evaluations, training, and reviewing documents for acceptance.

From February to March 1981 several pipe/mechanical discipline project QC instructions were changed to incorporate installation inspection records and welding inspection records. These changes were made to reduce the amount of paperwork and documentation errors. Other changes were made to replace surveillances with specific inspections on a characteristic-by-characteristic basis.
From November 1980 to January 1981, the project QC department underwent a management change. A new project field QCE and lead pipe/mechanical QCE were appointed during this period. Through their programatic and technical direction, the training and certification programs have improved the thoroughness and effectiveness of the QCE.

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## B. Planned Process Corrective Action

The following actions are to be taken in addition to the examinations and inspections described in Section IV.

1. Specification $7220-\mathrm{M}-326$ will be revised as described in Table 1 to provide additional direction to construction.
2. The $Q C$ instructions will be revised as necessary to reflect the specification changes.
3. Training will be provided as necessary to reflect the changes to both the specification and QC instructions.

## IV. SUMMARY AND CONCLUSIONS

As stated in Section I, deficiencies identified during the Consumers Power Company overinspection would not have had an impact on safety. Reasonable assurance, based on the confidence level described in Section I, has been provided that if the same deficiencies occurred in similar situations, there would be no impact on safety.

Section III describes process corrective actions taken after January 1981, which are applicable to this problem. Based on these actions, hangers installed after January 1981 should have fewer deficiencies and an even higher assurance that there would be no impact on safety.

However, additional inspections of hangers are planned by the project before fuel load in accordance with actions described as shown in Table 1 of Section II.

## Bechtel Power Corporation <br> Inter-office Memorandum

Date
May 13, 1982
From R. Tulloch
Bechtel Job 7220
Safety Evaluation of Large Bore Pipe Of
Hangers Discrepancies Identified in
CPCo NCRs
At
P. Corcoran w/a
R. Hollar w/a
D. Anderson w/a
D. Borlaza w/a
D. Lewis w/a
D. Loos w/a
B. Klein w/a
E. Hughes. $w / 2 / 3-x+\frac{1}{3}$

References: A) NCR M-01-9-2-007 AI: S-1261
B) NCR M-01-9-2-010 AI: S-1265
C) NCR M-01-5-2-014 AI: S-1267
D) NCR M-01-5-2-017 AI: S-1272
E) NCR M-01-5-2-015 AI: S-1268

This documents the safety evaluation performed by Plant Design Group on Large Bore Pipe Hangers discrepancies identified in the referenced CPCo NCRs. Only those hangers identified as requiring rework are the subject of this evaluation.

Detailed safety evaluation for these hangers are attached.

CPCO NCR M-01-9-2-007
CPCo NCR M-01-9-2-010

OPCO NCR M-01-5-2-014
*1-616-6-28

$$
2-619-1-19 \cdot 1
$$

$$
2-611-7-33
$$

$$
2-604-2-35
$$

$$
1-616-8-2
$$

- 2-657-43-6

2-604-16-15
2-619-6-11 • 14
*This item was field redlined. Status was changed to rework.
Results of the safety evaluation indicate that the identified deficiencies, were they to have remained uncorrected, could not have affected adversely the safety of operation of the plant.

# 69663 Bechtel Associates Professional Corporation 

IOM
Page 2

If there are any questions, please advise.


RT/LS/slm
Attachments
Written Response Requested: No
Com Use: N/A


NON-CONFORMING PART UNDERSIEED ZUECD.

PIPE SUPPQBT EVALUATION
Hge to Be peworbed
RATIOHALE FOR ACCEPTING

SAFETY EVALUATION

STRESS ENGIHEERS COMMENTS

PIPE SUPPORT ENGINEERS COMMENTS
ELTENSIVE REVIEZ BY IT-G PROVIDENCE HAS DETCNMINED


ilo Safedy wereto
STRESS ETHINEER DATE


PIPE SUFFgRT EVALUATION

RATIONALE FOR ACCEPTING

SAFETY EVALUATION

STRESS ENGINEERS COMMENTS

PIPE SUPPORT ENGINEERS COMMENTS
THE WLLD is QUESTION (BETWEEN ITEM NOS. 6 \& II) is vowLOAD BEARING. THEREFORE, UNDEESIZAK IT BY $1 / 3 Z^{\prime \prime}$ FOR LAT I" of wE WILL NT AFFECT THE DEJILN INTEGRITY कF THE STRUCTURE. $\therefore$ IT IS ACCEPTABLE .

No Sapketympar ITTGRUNEL


I REPLY TO NONCONFORMANCE REPORT


NON-CONFORMING PART
welds for tam 2 \& are unclesizod. H/"

PIPE SUPPORT EVALUATION
He marl be reworlcel.
RATIONALE FOR ACCEPTING

STRESS ENGINEERS CONTENTS

PIPE SUPPORT ENGINEERS COMMENTS
Section $\sqrt{11}$ Dimsian I Appenalices. App. XVIT Table xV11-245:-1-1 States minimum size welds $1 / 8^{\prime \prime}$ weld stateelin NCR Bifowninmums antononte for $1 / 2$ "plate and counidencel a "cold beveled".




REPLY TO NONCONFORMANCE REPORT


NON-CONFORMING PART $3 / 46^{\prime \prime}$ "Clearance exists Between Top of pipe \&U BOLT

PIPE SUPPORT EVALUATION
Tile Rcwntions support for sperefearneee
evaluate for safety unpoct only
RATIONALE FOR ACCEPTING

SAFETY EVALUATION

STRESS ENGINEERS COMMENTS

PIPE SUPPORT ENGINEERS COMMENTS
Wo Safety impart. The magnitude of lauds covid net eugene enough force to fail UBotr.

| STRESS ENGINEER | DATE |
| :--- | :---: |
| PIPE SUPPORT ENGINEER | DATE |
| Leckand Chicer | $4-14-8 \tau$ |

APPROVED


NOH-CONFORHING PART
U Bolt' O Clearance - Z DiRECTION one side of $U$ Bott

PIPE SUPPORT EVALUATION

RATIONALE FOR ACCEPTING
No Spec. U.olation

SAFETY EVALUATION

STRESS ENGINEERS COMMENTS

PIPE SUPPORT ENGILIEERS COMMENTS Pa EA 5.1 .3 (b)
Spec. $7220-1$. $32<Q$ ) Stater "When the component pipe sups't design shetch/Durg STATES the Clear. is " $1 /$ J2" inch typ. on poppas. 4 sates of thepipe or pipe lug, the actual clearances rial mot be lessthon $1 / 16$ "or more to on $1 / 8$ " in oh.... the actual indiuntwa! clearances may be dirtributed in amy manner, including a zero cleeramee on one side of thepige". Therofoue-Nospee Violation

No Safety inpzet.



NON－CONFORMING PART IGAPS NO CONGER E゙XIST BETTWE゙心次 PIPE゙ G HGR
2）We゙LDS MEASURE 3／16＂TTEN I TO ITEMZ QITEM 4
PIPE SUPPGBT EVALUATION

RATIONALE FOR ACCEPTING－Az Pcant Desigu Communt－

Resuctivg in a verr SmALC LOAD．FRICTIONAL EIFJ＝GUTS E×ISTING FROM $Y$ LOAD 15 MUCMGRENTER THAN LUAD DUETU RADIAL EXPAUSION TNEREFORE ITS CONTR，QUT：OW IS WEGGLGABLE RREIF LALEN SHC G19．6．1，＇
2）THE REQUIRED WELD PER CALCULATIONI，．O5＂TNENEFORW $3 / 16^{\prime} / 5$ «xCEPRABLE

SAFETY EVALUATION

STRESS ENGINEERS COMMENTS

PIPE SUPPORT ENGINEERS COHMENTS


AT PD SUPERUSOR R．TuLLOCN REPORTS NO SAFETT IMPNE DASER AN TAE DBOUE STATEO RATIONSLE，

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\mathrm{per}_{4}-2 \mathrm{~s}-8 \mathrm{C}
$$

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4-29-8
$$

| STRESS EMGINEER | DATE |
| :--- | :--- |
| PIPE SUPPORT ENGINEER | DATE |
|  | $4 \cdot 29-82$ |

APPROYED
DATE
Fon FTounoci $\quad 4-29-9=$

# Bechtel Power Corporation 

 Inter-office MemorandumL. E. Curtis

Subject
Midland Plant Onits 1 and 2
Bechtel Job 7220
Safety Evaluation of Small Pipe Hanger Discrepancies Identified in
Copies to CPCo NCRs

Date April 23, 1982

From D. Riat
Of Resident Ingineering
At Midland Jobsite
P. Corcoran w/a
R. Hollar w/a
R. Tulloch w/a
D. Anderson w/a
D. Borlaza w/a
D. Loos w/a
B. Klein w/a

References:

| A) | NCR | M-01-9-2-007 | AI: | S-1261 |
| :--- | :--- | :--- | :--- | :--- |
| B | NCR | M-01-9-2-010 | AI: | S-1265 |
| C | NCR | M-01-5-2-014 | AI: | S-1267 |
| D) | NCR | M-01-5-2-017 | AI: | S-1272 |

This documents the safety evaluation perfomed by the Small Pipe and Hanger Group (SPHG) on Small Pipe hangers discrepancies identified in the referenced CPCo NCRs. Only those hangers requiring rework, as determined by Construciion, were subjected to this evaluation.

Detailed safety evaluation for the following hangers are attached.


Results of the safety evaluation indicate that the identified deficiencies, were they to have remained uncorrected, could not have affected adversely the safety of operation of the plant.

IOM dated
D. Riat to
L. H. Curtis

Page 2


Reviewed by $\frac{05 \text { Renin }}{\begin{array}{l}\text { D. Fewis } \\ \text { Licensing Engineer }\end{array}}$


Attachments:
Written Response Requeated: No Com Use: N/A

REPLY TO NONCONFORMANCE REPORT
 RATIOTALE FOR ACCEPTING $\mathrm{N} / \mathrm{A}$

STRESS ENGIHEERS COMMENTS

$$
N / A
$$

PIPE SUPPORT ENGINEERS COMMENTS
RUSN IF EAFECTIUE WKLD $3 / z E$ WERE PEDUEED TO $1 / \mathrm{a}$ FILLET far $z^{*}$ LONG, THE WELD WOULD Qualirr for a 900- 1000 - (Two-dinercionnc) ON TWE PGS STRAP PER STD-CALC. 400-005 REV 2.

TNe MAT LOAD ON NI * 415*, WNiEN is Less
TNAN $900=$ (ALLOWABCK LOAD FOR YA FILCET), THEREARE TNE WELO IS JTLLC WITAIN DESION ALLOWABLES.

NO SAFETY MAPACT ON THE HANGER.


REPLY TO NONCONFORMANCE REPORT


RATIONALE FOR ACCEPTIIIO

SAFETY EVALUATION
ASSURING ONLY 3 BOLTS EXIST ON TN EASE PLATE, EVALUATE THE IMPACT ON THE SYSTEM.
STRESS ERIALHEERS COMMENTS

PIPE SUPPORT ENGINEERS COMMENTS
AN EUHLUTIION OF SUPPORT 2HBC-216-5-H3 (CL) ASSURING THE BOLT ON THE LOWER RIGHT HAND CORNER OF THE BASE PLATE IS NON-FUNCTIONAC, VERIFIES THAT HL THE STRESSES ARE WITHIN DESIGN PLCOWRBLES.

THEREFORE THERE NO SAFETY IMPACT ON THE SUPPORT.


REPLY TO NONCONFORMANCE REPORT


NOH-CONFORMING PART
COTTER PIN IS MISSING ON LOWER END OF WEST SWAY STRUT.
PIPE SUPPORT EVALUATIO:
ACCEPTABLE- PROVIDE RATIONALE
NOT-ACCEPTABLE-PERFORM SAFETY EVALUATION
RATIONALE FOR ACCEPTING

SAFETY EVALUATION
ASSUIMIIVG THE VERTICAL RESTRAINT ON THE HANGER WILL
BE NONFUNCTIONAL.
STRESS ENGINEERS COMMENTS :
THERE IS ABSOLUTELY NO DANGER OR SAFETY HAZARD TO THE PIPING SYSTEM. THENDNLL STRESSES GRE ACTUALLY REDUCED, WEIGHT AND SEISMIC STRESSES ARE INCREASED, BIT ARE STLL WITHIN ASHE - SECTION TH CODE HILLCWADLE STRESS LEVELS.

LOADING ON DOUACENT RESTRAINTS INCREASE IF IT 15 ASSUMED THAT HANGER 2ECB-4-4-H5 (Q) IS NONFUNCTIONAL.

PIPE SUPPORT ENGINEERS COMMENTS
AN EvALUATION OF THE ADJACENT SUPPORTS, $2 E C B-4-4-H 4 Q)$ AND DECO-4-5-HI(Q), WITH THE INCREASED LOADS SHOWS THAT THEY ARE STILL WININ THE HCLETHOLE DESIGN FLLOWAGLES THEREFORE WHERE IS NC SAFETY UTINCT ON THE SYSTEM.

| STRESS EliA JEER | DATE |
| :--- | :--- |
| PIPE SUPPORT ENGINEER | $4.9-82$ |
| 1 | DATE |



## SAFETY EVALUATIO:i

ASSUMIING THE SUPPORA WILL BE NON-fUNCTIQNAIL.'

## STRESS ERGIMEERS CO:TMENTS

ADSUMING SUPPORT 2EBB-3-H-H/WWILL BE NON FUNCTIONAL, THE THE PIPING SYSTEM WQULD STILL QUALIIV PER SPEL. M-343; STILL WITHIN ACLEPTHOLE SEISITIC SPANS. THE ADTALENT SUPPORT ZEOD-3-4-HZLQ WOULD BE REQUIRED TO PICK UPTHE RDDITIONAL SEIDIMIC LOTO INCREASE FROM 14 lBS . To 82 lbS . FAVLTEO LOAD INCREASE FROM $42 \angle O S$ to 205 LOS .

## PIPE SUPPORT ELGGIHEERS COMMENTS

PIPE SUPPGRT ZEBD-3-4-HZLI WAS ORIGINALLY DESIGNED FOR A FAULTED. LOAD OF 345 LES. THIS IS GLEATER TMAIS TNG LOMD ARRIVED at oy tae stheis cugineedr evaluation, frerefoce the manler is STルL にITNIN DESICN ALLOWHOLES.

## NO SHFETY IMPACT ON THE SYSTEM.



REPLY TO NONCONFORMANCE REPORT


PIPE SUPPORT EVALUATIO:
ACCEPTABLE - PROVIDE RATIONALE
NOT-ACCEPTABLE-PERFORM SAFETY EVALUATION
RATIONALE FOR ACCEPTING*

SAFETY EVALUATION

STRESS ENGINEERS COMMENTS : THE ADDITIONAL $1 / 32^{\circ}$ CLEARANCE IS ACCEPTABLE FROM A SAFETY EVALUATION STAND POUT. IT DOES NOT INCREASE STRESSES ON THE PIPING SYSTEM. STRESSES ARE WITHIN CODE ALLOWARLES.

PIPE SUPPORT ENGINEERS COMMENTS

$$
N / A
$$

| STRESS EMÄINEER | DATE |
| :--- | :--- |
| thy Decanal | 4.14 .82 |
| PIPE SUPPORT ENGINEER. | DATE |

REPLY TO NONCONFORMANCE REPORT


NOH-CONFORMING PART
NO GAP EXISTS BETUZEN SIDES OF PGS $/ 13$ STRAD AND PIPE.
PIPE SUPPORT EVALUATIO:
$\square$ ACCEPTABLE- PROVIDE RATIONALE
区 NOT-ACCEPTABLE-PERFORM SAFETY EVALUATION
RATIOHALE FOR ACCEPTILİ

$$
N / A
$$

SAFETY EVALUATIOH
ASSUMING THE SUPPDRT IABC-IAS-AHQ LOCAS UP IN TWE ATIAC DNEFTINN, EUACUATE TNE IMPACT ONTNE SYSTEM.

STRESS ENGIIIEERS COMMENTS: ASSUHING TOTHL AXIAC RESTPAMT AT HANEER H9 RETCKTS IN THE




 DISRIBUTED BETWEEN SUPDNeTS H9 MND HIO.

PIPE SUPPORT ENGINEERS COMENTS :
SINCE THERE is $1 / 50^{\circ}$ CLCARANCE BETWORN THE LN ANO TNE PIPE ONNIO, MENGER AY OR NIO WOND aNLY BE REQUIRED To Deflect .0422*-.03125 $=.01095^{2}$. Nowever, wetve assumeo that twe ceemenacf is wot twere ino Hio is kso locieo. WIrN mis Assumprion twe Pokee Requraed to Derceer Nancer Ny .OYzz* in The $x$ aneccion is $F_{y}=600 \%$.

AN Evacuntion of suppoers He, Ho wirn NN ADDITIONAC LOAD of 600 THOWS THO TVE SUPDRETS ARE STILL wirvin desian milownaces.

NO SAFETY IMPACT ON TNE SYSTEN

PIDE SUPPORT ENGAFEEP. DATE


## REPLY TO NONCONFORMANCE REPORT



## PIPE SUPPORT ENGINEERS COMMENTS

## $N / A$

REPLY TO NONCONFORMANCE REPORT


NOH-CONFORMIHG PART
IS GAP EXST BETIZEEN PIFE CWAMP MND ITS SWHWOTTNG STPVETVRE
PIPE SUIPOR: EVALUATIO::
$\square$ ACCEPTABLE- PROVIDE RATIO:IALE

- NOT-ACCEPTABLE-PERFORR: SAFETY EVALUATION

RATIOLALE FOR ACCEPTII:

SAFETY EVALUATIO::
ASSUMING TNE SUPORT ICCO-69-ノAE LOCRS bP in TNREE DIRECTIONS, EVNLUTTE TNE ImPRCT ON TWE SysTED.









PIPE SUPPORT ENGINEERS CO:MENTS
AN EUNCVATION of Supports $1 C C 8-69-1-N 2(Q)$, ICCB-6GV-NI $Q$ W WD ICCA-69\%-NS WITN ADDITIONAL LOAOS CRUSGO a) SUPPORT /CCE-G-I-NEGQ BEING LOCAED IN TVREE DIRECTIONS verimes frier tre stresses on Twe Mancers ARE srich wrivin DESVEA RLCOWAOLES.

NO SAFETY IMPACT ON THE SYSTEM
$3 \ldots$.
$\because$ REPLY TO NONCONFORMANCE REPORT



PROJECTS, E:
QUALIT From: L. $\mathrm{H}_{\mathrm{C}}$ Curtis
 and inspected by Field angineering, turned over to quality control and inspected/accepted by quality control as evidenced by the completed P2. 10 document for each hanger.

1) FSK-M-1HBC-219-1-H1 - S/U-1GJA



|  | 23. WRITIEN REPLIY GEOUTRED BY: $2 / 22 / 82$ <br> To ESTABLISH CA COMPLITIOM DATE | 24. supervisg grsicaunminel 2/5/5/82 <br> 24. surzarisg imsicuatrmy paty |
| :---: | :---: | :---: |


Project Engineering's complete response is attached.
cc: D. Borlaza
D. Riat
W. Bind
D. Hollar
R. Tulloch
D. Taggart
L. Curtis
R. Myers
D. Tumbull
P. Corcoran
J. Horsch
B. Marguglio

| DESIGN/FRONECT SIG. NUTR. DISP. <br>  | 27. PRO SIG. ANTM. DISP.: | 28. PROCURDEAT SIG. CONC. DISP. : | 29. उIG. IF ORG. RİF. FOR C/A: <br> Pliguin fier A. liothes/2ič |
| :---: | :---: | :---: | :---: |
| FAB/CONST. SIG. NITR. DP. DISP. : | 31. SIG. OF TEST CROUP ACIOKN. COND ITIOA: | 32. POR MWTOR MOD - FLI. SUPZ. SIG. ANTR. DTSP.: | 33. AI AJPI. SIG. TO Derisicit disp.: |

[^1][^2]NONCONFORMANCE REPORT
company
3. A ASSESSICNT OF ROOT CALSEL (S):

Unknown, to be determined.


4. QA RECOMOEMDATION FOB PROCESS CA:

Uniknown, to be determined.


[^3]NCR MUL-Y-2-007
Page 3 of 5
Date: $2 / 4 / 82$
File: 16.0
12. "AS IS" NONCONFORMING CONDITION VERSUS "AS REQUIRED" CONDITION WITH REFS:
contrary to the above, the measured dimension is $6 \frac{1}{2}$ ".
b) The P2.10 for the subject hanger ( $\log 81753$ ) references $M-343$ for hanger fabrication. Paragraph 6.7.2 (Welding) envokes G-27 for welding and paragraph 4.4.8 of GWS-FM Rev 4 from G-27 states in part, ". . .each weld layer shall be free of porosity and excessive irregularities such as high spots and deep crevices."

Contrary to the above, the vertical support weldment exhibits an approximately $2^{\prime \prime}$ lung groove - creating a sharp edge.
2) $1-610-4-27-S / U-1 B C A$
a) The subjez* sketch requires a $9 / 16^{\prime \prime}$ length of support steel beyond the cross support weldment.

Contrary to the ${ }^{\prime}$ above, a length of $1 / 4^{\prime \prime}$ was measured.
b) The P2.10 for the subject hanger ( $\log 69498$ ) references M-326 for hanger installation. Paragraph 4.2.2 (Welding) states in part, "Urdercut shall not exceed $1 / 32$ "."

Contrary to the above, the angle flange to horizontal support beam weld exhitits a 5/32" undercut, (burnout).
3) 1-612-3-25-5/U-1 BKA
a) The P2.10 for the subject hanger (Log 76542) references $M-326$ for hanger installation. Paragraph 4.1 .2 (welding) envokes $G-27$ for welding and paragraph 4.4 .8 of GWS-FM Rev 4 from G-27 states in part, "...each weld layer shall be free of porosity and excessive irregularities such as high spots and deep crevices."

Contrary to the above, the vertical hanger support to support beam weld exhibits a grooved face $3 / 32^{\prime \prime}$ wide for approximately $l^{\prime \prime}$.
4) FSK-M-1HBC-204-1-H12 - S/U-1GJA
a) The bill of materials for the subject sketch specifies a $5 / 8^{\prime \prime}$ thickness for Item 6 .

Contrary to the above, several areas of the item noted measure $9 / 16^{\prime \prime}$.
5) $1-616-6-28-3 / U-1 E G A$
a) The subject sketch specifies a $1 / 2^{\prime \prime}$ weld for the stanchion to vertical support, (two sides).

Contrary to the above, a $3 / 8^{\prime \prime}$ weld was measured.
b) The subject sketch specifies an angle of $60^{\circ}$ between the angle support brace and vertical support.

Contrary to the above, an angle of $51^{\circ}$ was measured.
c) The subject sketch specifies stanchion heights of $20^{\circ}$ and $17 \mathrm{~h}^{\prime \prime}$.

Contrary to the above, stanchion heights of 22 h" and 18 " were measured respectively.
d) The subject sketch specifies $14^{\prime \prime}$ between the base of the angle support brace and the vertical support.

Contrary to the above, a 25h" dimension was measured.
6) $1-603-6-16-S / U-1$ BGC
a) The subject sket'ch specifies a gap between the ends of the two clamp halves of $4 "$.

Contrary to the above, a gap of $19 / 32^{\prime \prime}$ was measured.
h) The $P 2.10$ for the subject hanger (Log 81906) specifies $M-326$ for hanger installation. Paragraph 5.8 (Locking devices) of M-326 states in part, "...all threaded connections...shall be secured by....two jam nuts."

Contrary to the above, one (outer) of the nuts was observed to be loose renderind the clamp insecure.
7) $1-612-2-3-5 / \mathrm{U}-1 \mathrm{BKA}$
a) The subject sketch specifies a support beam (w14 $\times 150$ ) to pipe dimension of 1'-114".
Contrary to the above, a dimension of $1^{\prime}-4$ " was measured.
8) $2-604-3-18-5 / \mathrm{U}-2 \mathrm{BGA}$
a) The subject sketch specifies a $h^{\prime \prime}$ fillet weld - all around for the horizontal support to support beam weldment (Item 1 to 7).
contrary to the above, a non-continuous weldment was observed in this location.
9) $1-616-10-22-S / U-1 E G A$
a) The subject sketch specifies a verticalsupport beam (Item 2) of $4^{\prime}-8 \frac{1}{\prime \prime}$ " in ienyth. Contrary to the above, the support beam measures $5^{\prime}-0^{\prime \prime}$.
b) The subject sketch specifies a vertical support beam to cross beam support length of $29^{\prime \prime}$.
Concrary to the above, the distance was measured to be $25^{\circ}$.

```
NCR MOL-9-2-007
Page 5 of 5
Date:
File: 16.0
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10) $2-617-8-5-S / U-2 E G A$
a) The P2. 10 for the subject hanger ( $\log 82242$ ) references $M-326$ for hanger installation. Paragraph 4.2 .5 (Welding) states in part, "Additional welds not shown in the design sketches/drawings require Project Engineering review and approval via field design change control procedure or nonconformance procedure as applicable."
Contrary to the above, several additionat filiet felds were observed at the vertical support to angle support union (Item 2 to 3 ).
11) $1-603-3-2-\mathrm{S} / \mathrm{U}-1 \mathrm{BGA}$
a) The subject sketch specifies a piping elevation of $634^{\prime \prime}-6^{\prime \prime}$. Contrary to the above, an elevation of $63^{\prime}$ 'il1t" was measured.
12) $1-619-14-4-S / U-1 E A C$
a) The subject sketch specifies a support beam to support beam dimension of $1^{\prime}-103 / 8^{\prime \prime}$.

Contrary to the above, this dimension measured $1^{\prime}-9 \mathrm{~m}$ ".


Project Mngineering's complete response is attached.
1
cc:

| D. Borlaza | D. Riat | W. . Bird |
| :--- | :--- | :--- |
| D. Hollar | R. Tulloch | D. Taggart |
| L. Curtis | R. Myers | D. Turnbull |
| P. Corcoran | J. Horsch | B. Marguglio |



Uniknown: To be determined.



## *1. Q fricomeride:ton por poczes Ca:

Unknown: To be determined.

43. Nemob of mocess ca vertrtentia:
compliance with the component pipe support design sketches/drawings."
Contrary to the above, the following hangers have violated this specification:
Hanger 2-604-17-2 P2. 10 log 476648; support angle welded to plate is reversed from design sketch. S/U: 2BGA

Hanger 2-639-13-5 P2. 10 log $\# 63333$; item $\# 1$ rotated $90^{\circ}$ from design sketch. S/U:2A.
Hanger 2-604-16-15 P2. 10 log 81811, pipe stanchion listed on bill of materials to be $1^{\prime}-713 / 16^{\prime \prime}$; actual? is $1^{\prime}-73 / 16^{\prime \prime}$. S/U: 2BGA

Hanger 2-604-2-35 P2.10 log \$59842; strut not located on $4^{\prime \prime} m$ beam as per drawing. S/U: 2BGE

Hanger 2-619-1-19 P2.10 log \#124673; item \#11 listed as $8^{\prime \prime} \times 12^{\prime \prime}$ actual as installed is $7^{\prime \prime} x 1^{\prime \prime}$. S/U: 2EAC

Hanger 2-GCB-21-1-H1 P2. 10 log 173127 ; gs 104 pipe strap specified, gs 111 installed. S/U 2BKA

Hanger 2-EBC-219-1-E1 P2. 10 log $\# 71982$; bill of materials lists item 02 as $3 / 8^{\prime \prime} \times 4^{\prime \prime} \times 4^{\prime \prime}$; actual as installed is $3 / 8^{\prime \prime} \times 4^{\prime \prime} \times 313 / 16^{\prime \prime}$. S/U: 2GJA

Hanger 2-HBC-216-5-\#3 P2. 10 log 472035 ; item $\# 5$ on bill of materials $1 \leq s^{*}-山$ as $3 / 4^{\prime \prime} \times 33 / 4^{\prime \prime}$; actual is $4^{\prime \prime} \times 4^{\prime \prime}$. S/U: 2GJA

Hanger 2-604-16-15 P2. 10 log \$81811 material lists item \#2 to be $3 / 8^{\prime \prime}$ thick; actual is $1 / 2^{\prime \prime}$ thick. S/U: 2BGA

Hanger 2-ABC-219-1-Z1 22. $10 \log 771982$ rev 5 item "3 to item $\# 2$ welded @ opposite sides than design sketc.. S/U: 2GJA

Hanger 2-611-4-4 P2. 10 log 42.41 , hanger clamp assembly indicates $13 / 8^{\prime \prime}$ clearance on sketch; actual is $11 / 2^{\prime \prime}$ typical on both sides. S/U:2BCA

Hanger 2-616-8-2 P2.: 0 log $\$ 63192$; centering of pipe to $=0$ of item 11 ( $4^{\prime} \mathrm{M}$ beam) not per drawing. S/U: 1EGA

Specification M-343 section 6.22 states in :art: "Acceptable Deviation Vertical
Piping: The design location of pip supports on vertical pipe may deviate
from the original approved location, in a direction parallel to the pipe centerline by 4 inches, provided it is not adjacent to an anchor, eçuipmert nozzle or valve, in which case prior approval from the engineer shall be required.

Contrary to the above:
Hanger 2-HBC-217-1-H2 P2. 10 log \#69460; sketch \& isometric calls for hanger to be centered e elevation $575^{\circ}-111 / 2^{\prime \prime}$; actually @ $575^{\prime}-53 / 4^{\prime \prime}$. S/U: 2GJA

Specification M-326 section 5.11 .1 states in part: "The clearance between the concrete walls and the structural attachment plates should not exceed $1 / 16^{\prime \prime}$ over a maximum of $20 \%$ of the bearing area;"

Contrary to the above:
Hanger 2-HBC-216-5-H3 $\quad 72305$ lower right hand corner of base plate exceeds gap tolerance. $S / U: \quad 2 G J A$

Specification $M-326$ section 4.2 .1 .9 states: "No undersize welds are permitted".
Contrary to the above:
Hanger 2-619-1-19 P2. 10 log $\# 124673$ undersize weld o item \#6 to item \#11. S/U: :
Hanger 2-604-2-35 P2. 10 log \#59842 undersize weld @ sway strut to $4^{\prime \prime} \mathrm{M}$ beam. $\mathrm{S} / \mathrm{U}$ :
Hanger 2-611-7-33 P2. 10 log \$135884 undersize weld @ item \#2 to item \#3. S/U: 2I
Hanger 2-639-13-5 log \#63333 insufficient welds for item f1. S/U: 2AEA
PQCI 7220-P2.10, 3.3 B states: 'Minimum thread engagement shall be that amount necessary to engage all the threads of the nut or threaded component. Hanger load devices which have internally threaded adjustable components are to have sight holes provided to verify adequate thread engagement where required."

Contrary to this:
Hanger 1-616-8-2 P2. 10 log $\$ 63192$; at sight holes of support rods, no threads are visible. S/U: LEGA

Specification N-326 section $5.1 .3 . b$ states: "When the component pipe support design sketch/drawing states the clearance is "1/32 inch typical" on cpposite sides of a pipe or $1 / 16$ inch on one side of a pipe or pipe lug, the sum of the actual clearances measured on the opposite sides of the pipe shall nc* be less than $1 / 16$ inch or more than $1 / 8$ inch. As long as the sum of these actual clearances falls wichin the above allowable limits, the actual. individual clearances may be distributed in any manner, including a zero clearance on one side of the pipe.

Contrary to the abcve;

```
Hanger 2-657-43-6 P2.10 log #84577; jesign sketch calls for 1/32" inch
clearance around "U bolt" and pipe: a total of 3/16" exists @ top side of
pipe and Elush on bottom. S/U: 2GJA
```


## 058510


#### Abstract

S-1265 M-Q1-2-2-010 Page 5 of 5 ```Hanger 2-604-16-15 log #81811 design sketch calls for 1/32 clearance dround pipe and "U bolt"; no clearance exists due to off set hoat holes. S/U: 2BGA Hanger 2-611-5-98 P2.10 log $70407; welds for 3/8" plates have buckled plates @ weld locations and corners. S/U: 2BNA NOTE 1: The preceeded conditions of all hangers identified, leave the integrity of hangers indeterminate. NOTE 2: All identified non-conforming hangers have been previously inspected & accepted by QC.```


        1
    To: M. Curland
(P) NONCONFORMANCE REPORT
farious
BPCo
Various

The following list of hangers do not conform to applicable requirerents as itemized below.

For all undersized welds see also M-326 4.2.1.a.1 which states, 'No undersized welds ar: permitted." For wrong material and material iimensions see M-326 5.1.1.

*i. en hrcomexta:ich fon frxeiss di:

Unknown: To be decermined.

b3. exext or procese an viotriantich


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NCR: M-01-5-2-01.4
Dàte: 2/3/82
Page 3 of 5
```

CONZINUED:
12. "AS IS" NONCONFORMTNG CONDITION VERSUS "AS REQUIRED" CONDITION WITH REFS:

## Hardware Discrepancy

1) 2-611-6-5 $(10-2 F L 3-35-H 5) \log \# 63225$ Rev $5 \mathrm{~S} / \mathrm{U}$ 2BCA
a) Where the sway strut fitting is welded to the vertical I-Beam, the welds are undersized both legs per the drawing.
b) Three of four welds attaching the horizontal I-Beam to the superstructure I-Beam are undersized on one leg per the drawinz
c) The beam to beam shop fabricated portion welds are undersized on one leg per the drawing.
d) The brace beam angle is supposed to be $44^{\circ} \pm 1^{*}$ per the drawing and it is installed at 46i'.
2) FSK-M-2HEC-145-1-HSQLog \#87879 Rev $5 \mathrm{~S} / \mathrm{U}$ 2EGA

Item \#1 in bill of materials is a W5 I-Beam and a W6 I-Seam was installed.
3) $\mathrm{FSK}-\mathrm{M}-2 \mathrm{HBC}-144-1-\mathrm{HEQ} \log \# 73182 \mathrm{Rev} 5 \mathrm{~S} / \mathrm{U}$ 2EGA
 however, a '" $^{\prime \prime} \times 3$ 3/4" $\times 33 / 4^{\prime \prime}$ plate was installed.
4) $1-612-3-12 Q\left(8^{\prime \prime}-1 G C B-16-H 1\right) \log \# 76107 \mathrm{ReV} 5 \mathrm{~S} / \mathrm{U}$ 1BKA

This hanger was installed 4 h" West of drawing coordinates perfendicular to the pipe. (Contrary to even the new Appendix K of M-326 allowance of $\pm 2^{\prime \prime}$ for a deviation of the pipe)
5) 2-613-4-19Qi12-2HBC-5-H1) Log * 68235 Rev $5 \mathrm{~S} / \mathrm{U}$ 2BCA
a) The two welds that attach the spring canister to the channels are undersized on one leg per the drawing.
b) The angle clips are attached to the wrong end of the channels per the drawing
c) Both bottom welds of the angle clips to the channel are undere: act on one leg per the drawing.
d) There is a gap between the angle clips and the channel and the drawing shows no gap.
Note:
Although the elip to main beam welds were changed from being an NF5 222 weld the detail indicates the elip to channel welds are :.... per NES222.

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Date: 2/3/82
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6) FSK-M-2-FCC-4-1-il $(Q) \log \# 64107 \mathrm{Rev} 5 \mathrm{~S} / \mathrm{U}$ 23BB

There is weld burn out causing reduced thickness of up to $3 / 32^{\prime \prime}$ at one end of one of the welds of strap to angle. This also makes the weld undersize
7) FSK-M-2ECS-8-3-H4 (Q) $\log \# 79652$ Rev $5 \mathrm{~S} / \mathrm{U}$ 2BHA
a) Item \#1 on the bill of material is 13 h" long, however, actual installed is 13 3/4" long.
b) The isometric drawing locates this hanger 11'-1 $11 / 16^{\prime \prime}$ East of reactor building centerline, however, measurement from a benchmark locates it at 11'-9 $\mathbf{h}^{\prime \prime}$ East of the reactor building centerline contrary to para 6.2 of $\mathrm{M}-343$.
8) ESK-M-2ECA-4-4-H5 (Q) Log \#60821 Rev $4 \mathrm{~S} / \mathrm{U}$ 23HA
a) There is a cotter pin missing on the lower end of the West sway strut.
b) The $\frac{1}{}$ " gap between the sway struts called for in view $c-c$ of the drawing is actually $\boldsymbol{r}^{\prime \prime}$.
9) $F S K-M-2 H B C-1-1-H 2(Q) \log \$ 78717 \mathrm{Rev} 5 \mathrm{~S} / \mathrm{U}$ 2JEA
a) The stiffener plate outer bottom edge thickness is reduced due to weld burn off resulting in an undersize weld.
b) The same condition occurs on three (3) places on the pipe strap (this was beveled and a full weld was not made).
10) FSK-M-2GCB-22-1-H3 (Q) Log \#68259 Rev $5 \mathrm{~S} / \mathrm{U}$ 2BKA

Item $\# 3$ on bill of material is $h^{\prime \prime} \times 23 / 4^{\prime \prime} \times 23 / 4^{\prime \prime}$ per drawing. Actual j. 5 女" $\times 33 / 4^{\prime \prime} \times 33 / 4^{\prime \prime}$.
11) 2-617-11-9 (5"-2HBC-149-H1)(Q) Log \#69494 Rev 5 STU 2EGA
a) Section AA of drawing requires $231 / 32^{n}$ offset between centerline of main beam and centerline of vertical beams of the hanger. Actual is 5/16" offset.
b) venterline of pips to centerline of vertical beams is actually " /4" and 12 s ", however, the drawing requires $12^{\prime \prime}$.
22) 2-619-1-20Rç(8"-2HRC-109-H20R) Log $* 64049$ Rev 5 STU 2EAC

The hanger is $5^{\prime \prime}$ west of drawing coordinates (perpendicular to the pipe) contrary to para 5.2 of $M-326$ (note the drawing states " $f$ in ld gut to $3 L:="$ fir 'tees 1 and 2 on the hill of material, however, material used $\because=$ longer than called for).

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13) 2-619-2-19 Q ( 10 "-2HBC-110-H19) Log \#103729 Rev 6 S/U 2EAC

The lugs attaching the sway strut to the vertical I-Beam are rotated 90. from the drawing configuration and contrary to M-326 5.2.1.d. Homper Do/ak
14) $2-619-6-118\left(10^{\prime \prime}-2 H B C-100-H 3\right) \frac{\log \# 76640}{\text { of } D 210} \frac{\text { Rev } 5}{L} S / U \frac{2 E A D}{P}$
a) Item \#8 on bill of material requires $1^{\prime \prime} \times 6^{\prime \prime} \times 4$ h", however, $1^{\prime \prime} \times 6$ r" $^{\prime} \times 5^{\prime \prime}$ was installed.
b) Item \#7 on bill of material requires $7 / 8^{\prime \prime} \times 6^{\prime \prime} \times 5^{\prime \prime}$, however, $7 / 8^{\prime \prime} \times 6^{\prime \prime} \times 4 h^{\prime \prime}$ was installed. (a later rev makes a \& b acceptable)
c) Vertical gap, both top and bottom, is not parallel with pipe. Gide pads top and bottom touch the pipe at one end and have gap exceeding the requirements of the drawirg and $1 /-326$ para $5.1 .3 . b$ at the other end.
d) The welds of the vertical hanger beams to the bottom horizontal beam are undersized per drawing.
e) The $1^{\prime}-71 / 8^{\prime \prime}$ distance between pipes per drawing was installed as 1'-10 1/8'.
15) FSK-M-2ESB-3-4-H1 (Q) Log \# 71689 Rev 5 S/U 2 SMA
a) The sway strut has a tie wrap (plastic) inscead of a bolt, nut and wasbers per the manufacturers drawing on one end.
b) A cotter pin is missing from the revaining pin at the other end of the sway strut contrary to the manufacturers drawing
e) Lock nuts missing on pipe clamp

1-612-2-2 Q (8"1GCE-16-H47) Log \#63197 Rev $5 \mathrm{~S} / \mathrm{U} \perp$ BKA
a) The $\mathbf{2 ' ~}^{\prime}-5 h^{\prime \prime}$ dimension from centerline of pipe to centerline of the W14 $\times 111$ I-Beam is $2^{\prime}-3^{\prime \prime}$ installed (this is perpendicular to the pipe)
b) The North and South end plates (Item 5) welded to angle have an undersized weld on one leg. Soth of these are on the West side,
17) 1-612-4-33(Q) (6"-1GCB-18-H10) Log \#65882 Rev $5 \mathrm{~S} / \mathrm{U}$ 1BCA

The small plate (\#l on bill of material) has reduced section and therefore undersized weld at the top.
company
wT io PRIORITY: 2 TREND: DST


Code 83
Mar $1 \pi$ ?


The following list of hangers do no: conform to the applicable requirements as itemized below:

It is noted that the identification of the nonconformances listed below was the result of an examination of hangers completely installed and inspected by Field Engineering, turned over to Quality Control and inspected/accepted by Quality Control as evidenced by the completed P2.10 document for each hanger.


1) Engineering to evaluate the acceptability of the hanger. (Curtis)
2) If rework/repair is required - implement rework/repair, document \& reinspect as required. (LEDavis, ESmith)
3) If acceptable, provide justification to use as is s revise the


LHCurtis
LEDavis
ESmith
spot curl:
WRBird RAWells
JWCook JLWood
MADietrich ALAB-2
Linnwell RDJohns:-
BWMarguglio
DBMiller
REMCCue/5FOI
BHPeck
DATaggart
nMTurnbull


5. mat a sisposimion, Jos fiction a condition sain:

Project Engineering's complete response is attached.
7
cc:
D. Borlaza
D. Rift
W. Bind
D. Molar
R. Tulloch
D. Taggart
L. Curtis
R. Myers
D. Tumbull
P. Corcoran
J. Borsch
B. Marguglio

4. named phat a nentiazion:
$\qquad$
campany

Unknown: To be determined.


*h. Qu Rrcomerdation Pas mocrss ci:

Unknown: To be determined.

43. efice of phocess a mberpiatial

1) Clearances on the following hangers do not conform to the drawing/ specification tolerances :

| O-HBC-142-1-H1 | SUS : | 2-EAD |
| :---: | :---: | :---: |
| 1-HBC-145-1- H9 $^{\text {a }}$ | SUS: | $1-E G A$ |
| 1-657-37-9 | SUS: | 1-GJA |
| 1-657-37-22 | SUS: | 1-GJA |
| 1-648-7-58 | SUS: | 1-RAB |
| 1-HBC-144-1-H3 | SUS: | $1-E G A$ |
| 1-CCB-69-1-[2 | SUS: | 1-BGA |

NOTE: Items $b$ \& $f$ contain masking tape under the strap, preventing accurate measurement.
2) 0-617-7-13 SUS: 0-EGA

Item (I-BEAM) is not installed in accordance with the drawing. Angle clip \& field weld is located incorrectly.
3) 0-617-8-33 SUS: O-EGA
a) Field weld between items 2 S 3 does not conform to drawing requirements. West weld, south end, contains approximately h" of undersize weld.
4) 1-633-1-33 SUS: 1-BMA
a) Drawing requires the buttom plate, on one corner, to be jeveled $\zeta^{\prime \prime}$. Contrary to the above, the bevel was determined to be $3 / 16^{\prime \prime}$.
5) $1-C C B-69-1-\mathrm{H1}$ SUS: 1-BGA
a) PGS-114 requires the $f$ am nuts to be $S A-307, G R B$ Contrary to the above, the jam nuts are $\mathrm{SA}-194,2 \mathrm{H}$.
6) $1-C C B-69-1-\mathrm{H}_{2}$ SUS: 1-BGA
a) Same as 5.a above.
7) $0-618-1-6$

SUS: O-EAA
a) Field weids between 1 tems $2 \& 8$ do not conform to drawings requirements. Drawing requites the welds to be located on the sides of item 8 , the welds are located on the ends of 1 tem 8 .


$$
\begin{aligned}
& \text { CONSTRUC TION } \\
& \text { RFISPONSE }
\end{aligned}
$$

## QA AI $5-1261$

Item numbers listed in this response correspond to the item numbers listed in Block 12 of subject NCR. Information given , eflects investigation of actural field conditions and what, if any, construction action has been taken.

Item (1)
a) Redline SH-10111 has been issued to reflect existing field condition. Basic design of hgr not affected and PE approval is not required. No further action required.
b) Subject weld tas been damaged by grinding at the toe of the weld. Adequate weld size exists and will remain after ground area is faired-in Rework Package RSH-1105 issued to correct existing condition.

## Item (2)

a) Redline LH-10420 has been issued to reflect existing field condition. Basic design of hgr not affected and PE approval is not required. No further action required.
b) Subject condition listed on NCR has been documented on Bechtel NCR 4112. PE to evaluate.

## Item (3)

a) The condition stated on NCR has been evaluated by FE and QC. Condition conforms to requirements and no nonconforming condition exists. No further action required.

## Item (4)

a) Condition stated has been evaluated by $F E$ and $Q C$. Material installed conforms to dwg. requirements. No further action required.

## Item (5)

a) Redline has been submitted for evaluation to PE reflecting existing field condition.
b) Redline LH-4769 was issued and used as criteria for accept ance. Subject redline deleted angle requirements. No nonconforming condition exists. No further action required.
c) Redline has been made to reflect existing field condition. Basic design of hgr not affected and no PE approval required. No further action required.
d) Redline has been submitted to reflect existing field condition. Basic design of hgr not affected and PE approval not required. No further action required.

Item (6)
a) Redline LH-10579 has been issued to reflect existing field condition. Basic design not affected. PE approval not required. NOTE: Lower end of clamp measured $\mathrm{i}_{2}$, upper end $9 / 16^{\prime \prime}$. No further action required.
b) Condition stated is not a nonconformance. Securing of threaded fastners is a requirement of final walkdown and would hase been corrected at that time.

Item (7)
a) Condition stated, no longer exists. Subsequent revision of drawing reflects existing field condition. No further action required.

Item (8)
Redline has been submitted for evaluation to PE reflecting existing field condition.

It em (9)
a) Redline has been submitted for evaluation to PE reflecting existing field condition.
b) Redline has been made to reflect existing field condition. Basic design of hgr not affected and no PE approval required. No further action required.

Item (10)
Redline has been submitted for evaluation to PE reflecting existing field condition.

## Item (11)

a) Redline LH-10361 has been issued to reflect existing field condition. Actual existing elevation is within installation tolerances. No further action required.

Item (12)
a) Redline LH-10457 has been issued to reflect existing field condition. Basic design of hgr is not affected and PE ap proval is not required. No further action required.

NONCONFORMANCE REPORT


ie following list of hangers do not conform to the applicable require ints as itemized below:
I is noted that the identification of the nonconformances listed Blow was the result of an G:amination of hangers completely installed 2d inspected by Field Engineering, turned over to Quality Control and ispected/accepted by quality control as evidenced by the completed 2.10 document for each hanger.
) FSK-M-1HBC-219-1-H1 - S/U-1GJA
a) The subject sketch specifies a pipe to embecdonimension of 17 h "

Engineering to evaluate the acceptability of the as/is hanger.(Curtis If rework/repair is required - implement rework/repair, record, document and reinspect as required. (LEDavis, ESmith) and reyise the




PART CA IISPOSITION, JUSTIFICATION \& COMPLETHOA DATE:


[^4][^5]

Unknown, to be determined.


[^6]Contrary to the above, the measured dimension is $6 \frac{1}{2}$ ".
b) The P2.10 for the subject hanger (Log 81753) references M-343 for hanger fabrication. Paragraph 6.7.2 (Welding) envokes G-27 for welding and paragraph 4.4 .8 of GWS-FM Rev 4 from G-27 states in part, "...each weld layer shall be free of porosity and excessive irregularities such as high spots and deep crevices."

Contrary to the above, the vertical support weldment exhibits an approximately $2^{\prime \prime}$ ling groove - creating a sharp edge.
2) $\underline{1-610-4-27-S / U-1 B C A}$
a) The subjez+ sketch requires a $9 / 16^{\prime \prime}$ length of support steel beyond the cross support weldment.

Contrary to the above, a length of $1 / 4^{\prime \prime}$ was measured.
b) The P2.10 for the subject hanger (Log 69498) references M-326 for hanger installation. Paragraph 4.2.2 (Welding) states in part, "Undercut shall not exceed $1 / 32$ "."

Contrary to the above, the angle flange to horizontal support beam weld exhitits a 5/32" undercut, (burnout).
3) $1=612-3-25-S / U-1$ BKA
a) The P2.10 for the subject hanger (Log 76542) references M-326 for hanger installation. Paragraph 4.1 .2 (Welding) envokes G-27 for welding and paragraph 4.4.8 of GWS-FM Rev 4 from G-27 states in part, "...each weld layer shall be free of porosity and excessive irregularities such as high spots and deep crevices."

Contrary to the above, the vertical hanger support to support beam weld exhibits a grooved face $3 / 32^{\prime \prime}$ wide for approximately 1 ".
4) FSK-M-1HBC-204-1-H12 - S/U-1GJA
a) The bill of materials for the subject sketch specifies a $5 / 8^{\prime \prime}$ thickness for Item 6.

Contrary to the above, several areas of the item noted measure $9 / 16^{\prime \prime}$.
5) $1-616-6-28-9 / \mathrm{U}-1$ EGA
a) The subject sketch specifies a $1 / 2^{\prime \prime}$ weld for the stanchion to vertical support, (two sides).

Contrary to the above, a $3 / 8^{\prime \prime}$ weld was measured.
b) The subject sketch specifies an angle of $60^{\circ}$ between the angle support brace and vertical support.

Contrary to the above, an angle of $51^{\circ}$ was measured.
c) The subject sketch specifies stanchion heights of $20^{\prime \prime}$ and $17 \frac{1}{\prime \prime}$ ".

Contrary to the above, stanchion heights of $22 \frac{4}{}$ " and $185 / 8^{\prime \prime}$ were measured respectively.
d) The subject sketch specifies $14^{\prime \prime}$ between the base of the angle support brace and the vertical support.

Contracy to the above, a 25h" dimension was measured.
6) $1-603-6-16-S / U-1 B G C$
a) The subject sketch specifies a gap between the ends of the two clamp halves of $\frac{1}{2}$ ".

Contrary to the above, a gap of $19 / 32^{\prime \prime}$ was measured.
h) The P2.10 for the subject hanger (Log 81906) specifies M-326 for hanger installation. Paragrapi 5.8 (Locking devices) of M-326 states in part, "...all threaded connections...shall be secured by....two jam nuts."

Contrary to the above, one (outer) of the nuts was observed to be loose rendering theclamp insecure.
7) $1,-612-2-3-5 / U-1 B K A$
a) The subject sketch specifies a support beam (w14 $\times 150$ ) to pipe dimension of $1^{\prime}-11 \frac{1}{2}$.

Contrary to the above, a dimension of $1^{\prime}-4$ " was measured.
8) $2-604-3-18-S / \mathrm{U}-2 \mathrm{BGA}$
a) The subject sketch specifies $a$ " fillet weld - all around for the horizontal support to support beam weldment (Item 1 to 7 ).
Contrary to the above, a non-continuous weldment was observed in this location.
9) $1-616-10-22-5 / \mathrm{U}-1 E G A$
a) The subject sketch specifies a verticalsupport beam (Item 2) of $4^{\prime}-8$ h' in ienyth. Contrary to the above, the support beam measures $5^{\prime}-0^{\prime \prime}$.
b) The subject sketch specifies o vertical support beam to cross beam support length of $29^{\circ \prime}$.

Conurary to the above, the distance was measured to be $25^{\prime \prime}$.
401-9-2-007
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Date:
File: 16.0
10) 2-617-8-5 - S/U-2EGA
a) The P2.10 for the subject hanger (Log 82242) references M-326 for hanger installation. Paragraph 4.2.5 (Welding) states in part, "Additional welds not shown in the design sketches/drawings require Project Engineering review and approval via field design change control procedure or nonconformance procedure as applicable."

Contrary to the above, several additional h" fillet welds were observed at the vertical support to angle support union (Item 2 to 3 ).
11) $\mathrm{i}-603-3-2-\mathrm{S} / \mathrm{U}-1 \mathrm{BGA}$
a) The subject sketch specifies a piping elevation of 634'-6".

Contrary to the above, an elevation of $633^{\prime \prime} 111^{\prime \prime}$ " was measured.
12) $1-619-14-4-$ S/U-1EAC
a) The subject sketch specifies a support beam to support beam dimension of 1'-10 3/8".

Contrary to the above, this dimension measured l'-9 $\frac{1}{\mathbf{q}}$ ".

QC AI 1505
COCO $\mathrm{NCR}^{4}$ mol－9－2－OIC
QA AI $5-2 / 65$
Hangers listed in the response correspond to the hangers listed in Block 12 of subject NCR．Information given reflects investi－ gation of actual field conditions and what，if any，construction action has been taken．

Her 2－619－1－19
a）Subject weld is to be reworked under rework package RLH－626．
b）Redline LH－10448 has been issued to reflect existing field condition．Basic design of hgT is not affected and PE approval not required．No further action required．

Her 2－604－2－35
a）Subject weld was measured by $Q C$ and found to be acceptable， No further action required．
b）Subject condition no longer exist in field．Strut was re－ moved under rework package RLH－390．Strut to be reinstalled under rework package RLH－623．

Her 2－611 1－33
Subject weld is to be reworked under rework package RLH－618．
Note：Subject weld is a vendor supplied weld．
agr 2－639－13－5
a）Redline LH－10450 has been issued to reflect existing field condition．Welds are not insufficient（undersize），but are orientated incorrectly．
b）Redline has been submitted for evaluation to PE reflecting existing field condition．

Mgr 2－604－17－2
Redline LH－10437 has been issued to reflect existing field condition． Basic design of hor not affected and PE approval not required． No further action required．

Her 2－604－16－15
a）Redline LH－10438 has been issued to reflect existing field condition．Basic design of hor not affected．PE approval not required．No further action required．
b）Redline LH－10438 has been issued to reflect existing field
condition. Basic design of hgr not affected and PE approval is not required. No further action required.
c) Stated condition no longer exists in field. U-bolt is no longer installed. U-bolt to be reinstalled under rework package RLH-622.

## Hgr FSK-M-2GCB-21-1-H1

Redline SH-10112 has been issued to reflect existing field condition. Drafting error made, therefore PE approval not required. No further action required.

Hgr FSK M-2GCB-21-1-H1
a) Redline SH-10113 has been issued to reflect existing field condition. Basic design of hgr not affected and PE approval not required. No further action required.
b) Redline $\mathrm{SH}-10113$ has been issued to reflect existing field condition. Basic design not affected and PE approval not required. No further action required.

Hgr 2-611-4-4
Redline LH-10422 has been issued to reflect existing field condition. Basic design not affected and PE approval not required. No further action required.

Hgr 2-616-8-2
a) Redline LH-10431 has been issued to reflect existing field condition. Basic design not affected and PE approval is not required. No further action required.
b) Rework Package RLH-617 issued to correct tread engagement. Lower end is only nonconforming condition.

Hgr FSK-M-2HBC-217-1-H2
Redline SH-10115 has been issued to reflect existing field condition. FE determined no basic design change and PE approval not required. No further action required.

Hgr FSK-M-2HBC-216-5-H3
a) Rework Package RSH-1097 issued to correct existing field condition.
b) Redline SH-10114 issued to reflect existing field condition. Basic design not affected. PE approval not required. No further action required.

Hgr 2-657-43-6
Rework Package RLH-620 issued to correct existing field condition.
Hgr 2-611-5-98
Existing condition has been inspected and evaluated by FE and QC and is acceptable as is. No further action required.



|  |  |  | *To be determined. |
| :---: | :---: | :---: | :---: |
| 26. OESICN/PRCNTCT SIG. AUTM. DISP.: | 27. N0 SIG. NVITS. DISP,: | 28. PHoclrberer SIC. CONC. DISP. | 29. SIG. OF OLG. RESF. PCR C/A: |
| 30. PNB/CONST. SIG. AITRS. DEP. DISP.: | 31. STE. OF I2ST GROUP ACKMOH. CONDITION: | 32. POR MLIOR MOD , FLE. SUPT. SIG, AUTE, DISP.: | 33. Ci autis. Sic. To depieneat 215 |

34. METHOD OF PART CA VERITICATION:
35. SIE. OF ORG. RESP, TOR PNRT C/A
$\qquad$

Unknown: To be determined.



0 man
4. 2A RECOMEMAITON POR PROCESS CA:

Uniknown: To be determined.

43. vepiod or moczss a veriticatias:
compliance with the component pipe support design sketches/drawings."
Contrary to the above, the following hangers have violated this specification:
Hanger 2-604-17-2 P2. 10 log 476648 ; support angle welded to plaze is reversed from design sketch. S/U: 2BGA

Hanger 2-639-13-5 P2. 10 log 763333 ; 1tem $\# 1$ rotated $90^{\circ}$ from design sketch. S/U:2AE:
Eanger 2-604-16-15 P2.10 log " 81811, pipe stanchion listed on bill of materials to be $1^{\prime}-713 / 16^{\prime \prime}$; actua? is $1^{\prime}-73 / 16^{\prime \prime}$. S/U: 2BGA

Hanger 2-604-2-35 P2. 10 log 159842 ; strut not located on $4^{\prime \prime} m$ beam as per drawing. S/U: 2BGE

Hanger 2-619-1-19 P2.10 log 124673; item \#11 listed as $8^{\prime \prime} \times 12^{\prime \prime}$ actual as installed is $7^{\prime \prime} \times 11^{\prime \prime}$, S/U: 2EAC

Hanger 2-GCB-21-1-स1 P2. 10 log 773127; pgs 104 pipe strap specified, pgs 111 installed. S/U 2BKA

Hanger 2-ABC-219-1-Z1 P2.10 log \#71982; bill of materials lists item \#2 as $3 / 8^{\prime \prime} \times 4^{\prime \prime} \times 4^{\prime \prime}$; actual as installed is $3 / 8^{\prime \prime} \times 4^{\prime \prime} \times 313 / 16^{\prime \prime}$. S/U: 2GJA

Hanger 2-aBC-216-5-Z3 P2.10 log 472035 ; item 45 on bill of -dteriais lis as $33 / 4^{\prime \prime} \times 33^{\prime \prime}$; actual is $4^{\prime \prime} \times 4^{\prime \prime}$. S/U: 2GJA

Hanger 2-604-16-15 P2.10 log \#81811 material lists item $\# 2$ to be $3 / 8^{\prime \prime}$ thick; actual is $1 / 2^{\prime \prime}$ thick. S/U: 23GA
Hanger 2-ABC-219-1-\#1 P2.10 log $\# 71982$ rev 5 item $\# 3$ to item 72 welded © opposite sides than design sketc... S/U: 2GJA

Eanger 2-611-4-4 p2.10 log \#12.41 hanger clamp assembly indicates $13 / 8^{\prime \prime}$ clearance on sketch; actual is $1 / 2^{\prime \prime}$ typical on both sides. S/U:2BCA

Hanger 2-616-8-2 P2. 10 log $\# 63192$; centerline of pipe to top of item \#l ( $4^{\prime} \mathrm{M}$ beam) not per drawing. S/U: 1EGA

Specification M-343 section 6.22 states in :art: "Acceptable Deviation Vertical Piping: The design location of pipc supports on vertical pipe may deviate from the original approved location, in a direction parallel to the pipe centerline by 4 inches, provided it is not adjacent to al anchor, equipment nozzle or valve, in which case prior approval from the engineer shall be required.

Contrary to the above:
Hanger 2-HBC-217-1-H2 P2. 10 log \#69460; sketch \& isometric calls for hanger to be centered @ elevation $575^{\prime}$ - $111 / 2^{\prime \prime}$; actually @ $575^{\prime}-53 / 4^{\prime \prime} . \mathrm{S} / \mathrm{U}: 2 \mathrm{GJA}$

Specification M-320 section 5.11 .1 states in part: "The clearance between the concrete walls and the structural attachment plates should not exceed $1 / 16^{\prime \prime}$ over a maximum of $20 \%$ of the bearing area;"

Contrary to the above:
Hanger $2-\mathrm{HBC}-216-5-\mathrm{H} 3$ \#72305 lower right hand corner of base plate exceeds gap tolerance. S/U: 2GJA

Specification $M-326$ section 4.2 .1.9 states: "No undersize welds are permitted".

Contrary to the above:
Hanger 2-619-1-19 P2. 10 log \#124673 undersi.e weld @ item \#6 to item \#11. S/U: 2E
Hanger 2-604-2-35 P2.10 log \#59842 undersize weld @ sway strut to $4^{\prime \prime} M$ beam. S/U:
Hanger 2-611-7-33 P2. 10 log $\$ 135884$ undersize weld @ item $\# 2$ to item \#3. $\mathrm{S} / \mathrm{U}: 2 \mathrm{CC}$
Hanger 2-639-13-5 log \#63333 insufficient welds for item \#1. S/U: 2AEA.
PQCI 7220-P2.10, 3.3 B states: 'Minimum thread engagement shall be that amount necessary to engage all the threads of the nut or threaded component. Hanger load devices which have internally threaded adjustable components are to have sight holes provided to verify adequate thread engagement where required."

Contrary to this:
Hanger $1-616-8-2$ P2. $10 \log$ \#63192; at sight holes of support rods, no threads are visible. S/U: IEGA

Specification M-326 section $5.1 .3 . b$ states: "When the component pipe support design sketch/drawing states the clearance is "1/32 inch typical" on spposite sides of a nipe or $1 / 16$ inch on one side of a pipe or pipe lug, the sum of the actual clearances measured on the opposite sides of the pipe shall nc* be less than $1 / 16$ inch or more than $1 / 8$ inch. As long as the sum of these actual clearances falls wichin the above allowable limits, the actual individual clearances may be distributed in any manner, including a zero clearance on one side of the pipe.

## Contrary to the above;

Hanger 2-657-43-6 P2.10 log \#84577; design sketch calls for $1 / 32^{\prime \prime}$ inch clearance aroind " $U$ bolt" and pipe: a total of $3 / 16$ " exists @ top side of pipe and flush on bottom. S/U: 2GJA

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    S-1265
    M-01-2-2-010
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Hanger 2-604-16-15 log \#81811 design sketch calls for $1 / 32$ clearance dround pipe and "U bolt"; no clearance exists due to off set bolt holes. S/U: 2BGA

Hanger 2-611-5-98 P2. 10 log "70407; welds for $3 / 8^{\prime \prime}$ plates have buckled plates weld locations and corners. S/U: 2BNA

NOTE 1: The preceeded conditions of all hangers identified, leave the integrity of hangers indeterminate.

NOTE 2: All identified non-conforming hangers have been previously inspected \& accepted by QC.

QC AI 1517
FE AI Ji 76 mol-5-2-014

## CONSTRUCTLON <br> RESPONSI.

QA AI S-1267
Items listed in this response correspond to the items listed in Block 12 of subject NCR. Information given reflects investigation of actual field conditions and what, if any, construction action has been taken.

Item (1)
a) Redline has been submitted fo: evaluation to PE reflecting existing field condition.
b) Redline has been submitted for evaluation to PE reflecting existing field cordition.
c) There are no shop fabricated welds. This is not a nonconforming condition. No further action required.
d) Redline has been submitted for evaluation to PE reflecting existing field condition.

Item (2)
Redline SH-10116 has been issued to reflect existing field condition. Basic design not affected and PE approval not required. No further action required.

Item (3)
Redline SH-10117 has been issued to reflect existing field condition. Basic design not affected. PE approval not required. No further action required.

Item (4)
Redline LH-10414 has been issued to reflect existing field condition. Basic design not affected. PE approval not required. No further action required.

Item (5)
a) Redline has been submitted for evaluation to PE reflecting existing field condition.
b) Angle clips are attached per Dwg. Nonconforming condition does not exist. No further action required.
c) Welds are not undersize. Nonconforming condition does not exist. No further action required.
d) No gap exists. Nonconforming condition does not exist. No further action required.

## Item (6)

The subject condition was inspected and evaluated by PE and QC and found to be acceptable as is. No further action required.

## Item (7)

a) Subject condition was inspected and evaluated by PF and QC. Pipe installed on item 1 per dwg the excess is non-critical dimension. Nonconforming condition does not exist. No further action required.
b) Hgr is installed within tolerance. Nonconforming condition does not exist. No further action required.

## Item (8)

a) Rework Package RSH-1098 issued to correct existing condition. Subject condition would not have gone undetected and would have been corrected on final walkdown inspection.
b) Condition stated was measured by PE and QC and found to be acceptable. No further action required.

## Item (9)

a) Subject condition does not exist. Nonconformance does not exist. No further action required.
b) Subject conditions do not exist. Nonconformance does not exist. No further action required.

## Item (10)

Redline SH-10120 has been issued to reflect existing field condition. Basic design not affected. PE approval not required. No further actinn required.

Item (11)
a) Redline LH-10432 has been issued to reflect existing field condition. Basic design not affected. PE approval not required. No further action required.
b) Rediine LH-10432 has been issued to reflect existing field condition. Basic design not affected. PE approval not required.

## Item (12)

Redline LH-10461 has been issued to reflect existing condition. Basic design not affected. PE approval not required. No further action required.

Redline has been submitted for evaluation to PE reflecting existing field condition.

Item (14)
(a) Based on subsequent specification changes and shim plate
(b) criteria clarification, FE and QC evaluated subject conditions to be used as is. No further action required.
c) Rework Package RLH-621 has been issued to correct deficiency.
d) Rework Package RLH-621 has been issued to correct weld deficiency.
e) Redline LH-10435 has been issued to reflect existing field condition. Basic design of hgr not affected and piping is installed within tolerance. RE approval not required. No further action required.

Item (15)
(a)(b) (c)

Rework Package RSH-1099 issued to correct existing conditiun. Existing condition would not have gone undetected and would have been corrected on final walkdown inspection.

Item (16)
a) Redline made to reflect the existing field condition. Basic design not affected by change. PE approval not required No further action required.
b) Redline has been submitted for evaluation to PE reflecting existing field condition.

Item (17)
Subject condition on NCR has been documented on Bechtel NCR 4113.





NCR: M-01-5-2-014
Date: 2/3/82
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## CONTINUED:

12. "AS IS" NONCONFORMING CONDITION VERSUS "AS REQUIRED" CONDITION WITH REFS:

## Hardware Discrepancy

1) 2-611-6-5 $Q(10-2 F L B-35-H 5) \log \# 63225$ Rev $5 \mathrm{~S} / \mathrm{U}$ 2BCA
a) Where the sway strut fitting is welded to the vertical I-Beam, the welds are undersized both legs per the drawing.
b) Three of four welds attaching the horizontal I-Beam to the superstructure I-Beam are undersized on one leg per the drawiuz
c) The beam to beam shop fabricated portion welds are undersized on one leg per the drawing.
d) The brace beam angle is supposed to be $44^{\circ} \pm 1^{\circ}$ per the drawing and it is installed at $46 \%^{\circ}$.
2) $\operatorname{FSK}-\mathrm{M}-2 \mathrm{HEC}-145-1-H S Q \log \# 87879 \mathrm{Rev} 5 \mathrm{~S} / \mathrm{U} 2 E G A$

Item \#1 in bill of materials is a W5 I-Beam and a W6 I-Beam was installed.
3) ESK-M-2HBC-144-1-HQQ Log $\# 73182$ Rev $5 \mathrm{~S} / \mathrm{U}$ 2EGA

Item \#3 per drawing bill of material is a plate $\frac{1}{\prime \prime} \times 23 / 4^{\prime \prime} \times 23 / 4^{\prime \prime}$ however, a $\frac{1}{\prime \prime \prime} \times 33 / 4^{\prime \prime} \times 33 / 4^{\prime \prime}$ plate was installed.
4) $1-612-3-12 Q\left(8^{\prime \prime}-1 G C B-16-H 1\right) \log \# 76107$ Rev $5 \mathrm{~S} / \mathrm{U}$ IBKA

This hanger was installed 4h" West of drawing coordinates perpendicular to the pipe. (Contrary to even the new Appendix $K$ of $M-326$ allowance of $\pm 2^{\prime \prime}$ for a deviation of the pipe)
5) 2-613-4-19 Q (12-2HEC-5-H1) Log \# $68235 \mathrm{Rev} 5 \mathrm{~S} / \mathrm{U}$ 2BCA
a) The two welds that attach the spring canister to the channels are undersized on one leg per the drawing.
b) The angle clips are attached to the wrong end of the channels per the drawing
c) Both bottom welds of the angle clips to the channel are undereized on one leg per the drawing.
d) There is a gap between the angle clips and the channel and the drawing shows no gap. Note:
Although the clip to main beam welds were changed from being an NFS 222 weld the detail indicates the clip to channel welds are still per NF5 222.

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6) FSK-M-2-FCC $-4-1$-H1 (Q) Log $\# 64107$ Rev $5 \mathrm{~S} / \mathrm{U} 2 \mathrm{EBB}$

There is weld burn out causing reduced thickness of up to $3 / 32^{\prime \prime}$ at one end of one of the welds of strap to angle. This also makes the weld undersize.
7) FSK-M-2ECB-8-3-H4 (Q) Log $\# 79652$ Rev $5 \mathrm{~S} / \mathrm{U}$ 2BHA
a) Item \#1 on the bill of material is 134 " long, however, actual installed is 13 3/4" long.
b) The isometric drawing locates this hanger $11^{\prime}-111 / 16^{\prime \prime}$ East of reactor building centerline, however, measurement from a benchmark locates it at $11^{\prime}-9 \mathrm{~h}^{\prime \prime}$ East of the reactor building centerline contrary to para 6.2 of $\mathrm{M}-343$.
8) FSK-M-2ECB-4-4-H5 (Q) Log $\# 60821$ Rev $4 \mathrm{~S} / \mathrm{U} 2 \mathrm{BHA}$
a) There is a cotter pin missing on the lower end of the West sway strut.
b) The h" gap between the sway struts called for an view $c-c$ of the drawing is actually $\boldsymbol{h}^{\prime \prime}$.
9) $\mathrm{FSK}-\mathrm{M}-2 \mathrm{HBC}-1-1-\mathrm{H} 2(Q) \log \# 78717 \mathrm{Rev} 5 \mathrm{~S} / \mathrm{U}$ 2JEA
a) The stiffener plate outer bottom edge thickness is reduced due to weld burn off resulting in an undersize weld.
b) The same condition occurs on three (3) places on the pipe strap (this was bevel ad and a full weld was not made).
10) FSK-M-2GCB-22-1-H3 (Q) Log \#68259 Rev $5 \mathrm{~S} / \mathrm{U}$ 2BKA

Item \#3 on bill of material is $4^{\prime \prime} \times 23 / 4^{\prime \prime} \times 23 / 4^{\prime \prime}$ per drawing. Actual is $4^{\prime \prime} \times 33 / 4^{\prime \prime} \times 33 / 4^{\prime \prime}$.
11) 2-61.7-11-9 ( $\left.6^{\prime \prime}-2 H B C-149-H 1\right)(Q) \log \# 69494$ Rev 5 S/U 2EGA
a) Section AA of drawing requires $231 / 32^{\prime \prime}$ offset between centerline of main bean and centerline of vertical beams of the hanger. Actual is $5 / 16^{\prime \prime}$ offset.
b) Centerline of pifs to centerline of vertical beams is actually 12 3/4" and $12 \mathrm{z} \mathrm{\prime}$, however, the drawing requires $12^{\prime \prime}$.
12) 2-519-1-20R $\left(8^{\prime \prime}-2 H E C-109-H 20 R\right) \log \# 64049$ Rev $5 \mathrm{~S} / \mathrm{U}$ 2EAC

The hanger is $5^{\circ}$ West of drawing coordinates (perpendicular to the pipe) contrary to para 5.2 of $M-226$ (note the drawing states "field cut to suit" for "tems 1 and 2 on the hill of material, however, material used vas longer znan called for).

NCR: M01-5-2-014
Date: $2 / 3 / 82$
Page 5 of 5
13) 2-619-2-19 Q ( 10 " $-2 \mathrm{HBC}-110-\mathrm{H} 19) \mathrm{Log} \# 103729$ Rev $6 \mathrm{~S} / \mathrm{U}$ 2EAC

The lugs attaching the sway strut to the vertical I-Beam are rotated $20^{\circ}$ from the drawing configuration and contrary to M-326 5.2.1.d.

Homier No/ Mk
14) $2-619-6-11$ Q $\left(10^{\prime \prime}-2 \mathrm{HBC}-100-H 3\right) \log 476640$ Rev $5 \mathrm{~S} / \mathrm{U}$ LEAD
a) Item \#8 on bill of material requires $1^{\prime \prime} \times 6^{\prime \prime} \times 4 \frac{h}{}{ }^{\prime \prime}$, however, $1^{\prime \prime} \times 6 h^{\prime \prime} \times 5^{\prime \prime}$ was installed.
b) Item $\# 7$ on bill of material requires $7 / 8^{\prime \prime} \times 6^{\prime \prime} \times 5^{\prime \prime}$, however, $7 / 8^{\prime \prime} \times 6^{\prime \prime} \times 4^{\prime \prime}$ " was installed. (a later rev makes a \& b acceptable)
c) Vertical gap, both top and bottom, is not parallel with pipe. Guide pads top and bottom touch the pipe at one end and have gap exceeding the requirements of the drawing and M-326 para $3.1 .3 . b$ at the other end.
d) The welds of the vertical hanger beams to the bottom horizontal beam are undersized per drawing.
e) The $1^{\prime}-71 / 8^{\prime \prime}$ distance between pipes per drawing was installed as $1^{\prime}-10 \quad 1 / 8^{\prime \prime}$.
15) FSK-M-2EBR-3-4-H1 (Q) Log \# 71689 Rev $5 \mathrm{~S} / \mathrm{U}$ 2BMA
a) The sway strut has a tie wrap (plastic) instead of a bolt, nut and washers per the manufacturers drawing on one end.
b) A cotter pin is missing from the retaining pin at the other end of the sway strut contrary to the manufacturers drawing
c) Lock nuts missing on pipe clamp
16) $1-612-2-2$ Q (8"IGCB-16-H47) $\mathrm{Log} \# 63197 \mathrm{Rev} 5 \mathrm{~S} / \mathrm{U}$ IBKA
a) The $2^{\prime \prime}-5 h^{\prime \prime}$ dimension from centerline of pipe to centerline of the W14 $\times 111$ I-Beam is $2^{\prime}-3^{\prime \prime}$ installed (this is perpendicular to the pipe)
b) The North and South end plates (Item 5) welded to angle have an undersized weld on one leg. Both of these are on the West side.
17) $1-612-4-33(Q)\left(6^{\prime \prime}-1 G C B-18-H 10\right) \log \# 65882 \mathrm{Rev} 5 \mathrm{~S} / \mathrm{U}$ 1BCA

The small plate (\#1 on bill of material) has reduced section and therefore undersized weld at the top.

## CONSTRUCTION <br> RESPONSI

QC AI 1506
FE AI J-43
CPCO NCR MO1-5-2-017

QA AI S-1272
Item rumbers listed in this response correspond to the item numbers listed in Block 12 of subject NCR. Information given reflects investigation of actual field condition and what, if any, construction action has been taken.

## Item (1)

a) Rework Package RSH-1100 issued to correct existing field condition,
b) Rework Package RSH-1104 issued to correct existing field condition.
c) Redline has been submitted to PEreflecting existing field condition.
d) The clearances as installed are acceptable per requirements. Nonconforming condition does not exist. No further action required.
e) Redline has been submitted to PE reflecting existing fitld condition.
f) Rework Package RSH-1101 issued to field to correct existing condition.
g) Rework Package RSH-1102 issued to correct existing field condition.

Item (2)
Redline LH-10421 has been issued to reflect existing fiald condition. Basic design of hgr not affected by change. PE approval not required. No further action required.

Item (3)
Subject condition has been evaluated by FE and QC. Based on weld length and size existing condition is acceptable as is. No further action required.

## Item (4)

Rediine LH-10418 has been issued to reflect existing field condition. Basic design of hgr not affected. PE approval not required. No further action required.

Iten (5)
| Rework Package RSH-1103 issued to correct existing field condition. Item (6)

Rework Package RSH-1102 issued to correct existing field condition.
Item (7)
Redline has been submitted to PE reflecting existing field condition. (Redline \#LH-10449)

| $\qquad$ |  |  |  |
| :---: | :---: | :---: | :---: |
| 6. manct we: <br> MIDLAND | 7. NONCOMFCRMDN PANT No: VARIOUS (See Block 12) | 3. YOMCONFONLS: PART :WEVARIOUS  <br> (See Block 12) 2. $\frac{4 \pi}{2} \frac{\pi}{1} / 82$ |  |
| 9.VARIOUS (See Block 12) |  <br> BECHTEL CONSTRUCTION |  <br> (See Block 12) | $\begin{array}{\|lll\|} \hline \text { 3. SAII OF aIV: } & \\ \hline \text { 4. FILI so: } & 16.0 \\ \hline \end{array}$ |
| 12. "AS IS" NONCONFORMDN CONDITION VERSUS "AS REQUNED CONDITION =ITT RLTS: <br> The following list of hangers do not conform to the applicable requirements as itemized below: <br> It is noted that the identification of the nonconformances listed below was the result of an examination of hangers completely installed and inspected by Field Engineering, turned over to Quality Control and inspected/accepted by Quality Control as evidenced by the completed $P 2.10$ document for each hanger. |  |  | 5. DISRRZumtion  <br> Acrion copr:  <br> LHCurtis  <br> LEDavis  <br> ESmith  <br> nwo corr:  <br> WRBird RAnells <br> JWCook JLWood <br> MADietrich ALAB-2 <br> LRHowell RDJohnson <br> BWMarguglio  <br> DBMiller  <br> REMcCue/  <br> BHPeck  <br> DATaggart  <br> DMTurnbull  <br> JARutgers  |
| 14. HoL Sics NPM.IIP: <br> us $\square$ 50 $\square$ | $\qquad$ MPQAD Procedure F-7M Paragraph 5.1.1d |  |  |
|  |  |  |  |
|  |  | 17. is me reporviniz Pre 50.55(*): izs $\square$ * $\square$ * |  |
| 18. IS IC REPORTLALI FRR PNRT 21 : | ns <br> *o $\square$ |  |  |
|  |  |  |  |
|  |  |  | $\text { Clisor's simurne/Duz: } 2 / 5 / 82$ |
|  |  |  |  |
|  | 27. Po STG. NJTE. DISP.: | 25. Proctrwert SIG. COnc. Jisp.: | . SIE. OP ORE. RISE. ROE C/A: |
| 30. PMB/CONST. SIG. AUTR, DP. DISP.: | 31. SIG. of SST Grave nctown Condition: | 32. POR MeNOR MOD - PLI. SUFT. SIG, NUTE. DISP.: |  |

34. RE JHOD OF PRRT CA VEAIFICATION
35. S:Z. OF ORG. RES?. POR PANT C/A

36. A NSELSJVE: 27 ROOT CAUSELS:

Unknown: To be determined.

4. FROCISS $a$ RDQUTRED FRON:
xesian
-7צ2:
41. UA RECOI中ETDAITON FOR FMOCESS CA:

Unknown: To be determined.

43. vetsod of phocess an veriticatica

1) Clearances on the following hangers do not conform to the drawing/ specification tolerances:
a) 0- $\mathrm{HBC}-142-1-\mathrm{H1}$
SUS: 2-EAD
b) $1-\mathrm{HBC}-145-1-\mathrm{H9}$
SUS: $1-E G_{m}$
c) 1-657-37-9
SUS: 1-GJA
d) 1-657-37-22
SUS: 1-GJA
e) 1-648-7-58
SUS: $1-$ RAB
f) $1-\mathrm{HBC}-144-1-\mathrm{H} 3$
SUS: 1-EGA
g) $1-\mathrm{CCB}-69-1-\mathrm{H}_{2}$
SUS: $1-B G A$

NOTE: Items $b$ \& $f$ contain masking tape under the strap, preventing accurate measurement.
2) $0-617-7-13$

SUS: O-EGA
Item \#3 (I-BEAM) is not installed in accordance with the drawing. Angle clip \& field weld is located incorrectly.
3) $0-617-8-33$

SUS: 0-EGA
a) Field weld between items $2 \& 3$ does not conform to drawing requirements. West weld, south end, contains approximately $\frac{\hbar}{2}^{\prime \prime}$ of undersize weld.
4) 1-633-1-33 SUS: 1-BMA
a) Drawing requires the bottom plate, on one corner, to be oeveled そ". Contrary to the above, the bevel was determined to be $3 / 16^{\prime \prime}$.
5) $1-\mathrm{CCB}-69-1-\mathrm{HI}$ SUS: 1-BGA
a) PGS-114 requires the $j$ am nuts to be SA-307, GR B

Contrary to the above, the $j a m$ nuts are $\mathrm{SA}-194,2 \mathrm{H}$.
6) $1-\mathrm{CCB}-69-1-\mathrm{H}_{2}$

SUS: 1-BGA
a) Same as $5 . a$ above.
7) $0-618-1-6$

SUS: O-EAA
a) Field welds between items $2 \& 8$ do not conform to drawings requirements. Drawing requires the welds to be located on the sides of 1tem 8 , the welds are located on the ends of item 8 .

## PROJECT ENGINEERTNG'S COMPLETE HESPONSE

TO CPCO NONCONFORMANCE REIPORT M-01-9-2-007, AI: S-1261

This response supplements Construction and Quality Control's response to the subject SCR. The condition of the discrepancies requiring rework were evaluated for safety while redlined items (to reflect existing condition) submitted for Project Engineering approval were reviewed for acceptability. One discrepancy was also documented on Bechtel NCR number 4112.

Results of the safety evaluation indicate that the identified discrepancies (requiring rework), were they to have remained uncorrected, could not have affected adversely the safety of operation of the plant.

Field Redlined drawings that were submitted by Construction for FE approval were found acceptable. Bechtel NCR 4112 was dispositioned "use as is".

Details are shown below.

1. 1HBC-219-1-H1 (Q), HEV. $2-\mathrm{HEWOHK}$

Safety Evaluation: A groove $1^{\prime \prime}$ long $\times 1 / 32^{\prime \prime} \times 1 / 16^{\prime \prime}$ deep exists at the top of the west weld on the pgs-113 strap. A $5 / 16^{\prime \prime}$ filled is required. The wel.d is large enough to achieve $5 / 16^{\prime \prime}$ fillet beyond grooved area. The remainder of weld (1") is acceptable. Even if effective weld size were reduced to $1 / 4$ fillet for $2^{\prime \prime}$ long, the weld would quallfy for a 900 pound load (two-directional) * on the pgs strap per standard calculation $400-005$, HEV.2. The maximum load on H1 - 415 pounds, which is less than 900 pounds (allowable load for $1 / 4^{\prime \prime}$ fillet), hence the weld is atill within design allowables. Therefore, there is no safety impact. (Ref. Bechtel calc. mumber 400-3-208(Q))
2. 1-610-4-27(Q), HEV. 4 --BEGETEL NCR 4112 WAS ISSUERD

Acceptability: This NCR was dispositioned "use as is". The gouge in the support has caused very minimal loss of cross sectional area and will not affect the structural integrity of the support, therefore, acceptable.
3. 1-616-6-28(Q), REV. 1 - HEWORK (THIS WAS ORTGINALLY REDLINED FOR PE APPROVAL)

Safety Evaluation: Undersized weld exdsts. Bxtensive review by ITT-Grinnel Providence has determined that the $3 / 8^{\prime \prime}$ weld will accomodate the loading conditions. Therefore, there is no safety firpact. However, ITT Grinnell prefers to have the weld reworked. (Ref. ITT Grinnell calc. mumber Z-351)
4. 2-60L-3-18(Q), HEV. 1 --RENLINE FOR FE APPROVAL

Acceptability: A non-continuous weldment exists (item 1 to 7). There is a small difference in weld properties from an all around weld to what was made on the support. Based on load and span of the braced cantilevers, the weld that was not made on the edges of the flange willnnot affect the design, therefore, acceptable. (Ref. ITT Grinnell calc. number 2-356)
5. 1-616-10-22(Q), REV. $4--$ REDLINE FOR PE APPROVAL

Acceptability: Item 2 is $5^{\prime}-0^{\prime \prime}$ instead of $4^{\prime}-8 \quad 1 / 2^{\prime \prime}$. After reviewing the forces and stresses from STRUDL analysis, the change in dimension (elevation) will not affect the stability of the structure, therefore, acceptable. (Ref. IT T Grinnell call. number 2-355)
6. 2-617-8-5(Q), RIEV. $2-$ REDLINE FOR PE APPROVAL

Acceptability: Several additional $1 / 4^{\prime \prime}$ fillet welds were observed at the vertical support to angle support union. These additional welds at the joint has no adverse effect on the design, therefore, acceptable. (Ref. Bechtel call. number LBSE 1-617-8)


Reviewed by: $\frac{\text { AşcrlazN }}{\text { D. S. Borlaza }}$ Resident Q. E.

D. Riat

Resident Small Pipe and Hanger


PROJECT ENGINEERTING'S COMPLETE RESPONSE
TO CPCO NONCONFORMANCE REPORT M-01-9-2-010, AI: S1265

This response supplements Construction and Quality Control's response to the subject NCR. The condition of the discrepancies requiring rework were evaluated for safety while redlined items (to reflect existing condition) submisted for Project Engineering approval were reviewed for acceptability.

Results of the safety evaluation indicate that the identified discrepancies (requiring rework), were they to have remained uncorrected, could not have affected adversely the safety of operation of the plant.

Field redlined drawings that were submitted by Construction for PE approval were found acceptable.

Details are shown below.

1. 2-619-1-19 (Q), REV. 1 --REWORK

Safety Evaluation: Weld for item 6 to 11 is undersized by $1 / 32^{\prime \prime}$ for last $1^{\prime \prime}$ of weld. The weld in question is non-load bearing. Therefore, undersizing it by $1 / 32^{\prime \prime}$ for the last $1^{\prime \prime}$ of weld will not affect the design integrity of the structure. There is no safety impact. (Ref. ITT Grinnell call. number 2-361)
2. 2-604-2-35(Q), HEV. 1 -REWORK

Safety Evaluation: Rear bracket was rotated $90^{\circ} . \mathrm{Z}$ - and X -movement is zero. Therefore, rotation of rear bracket has no effect on hanger design. There is no safety impact. (Ref. Bechtel call. number LBSE 1-601-2)
3. 2-611-7-33(Q), RETV. 1 - HEWORIX

Safety Evaluation: Welds for items 2 and 3 are undersized. Section III, Division I Appendices, Appendix XVII, Table XVII-2452.1-1 states minimum size welds. The $1 / 8^{\prime \prime}$ weld stated in NCR is below minimum for $1 / 2^{\prime \prime}$ plate and considered a "cold weld". Based on load and the amount of weld at $1 / 8 " f i l l e t$, this weld is within the weld allowable. Therefore, there is no safety impact. (Ref. ITP Grimell call. muser 2-354)
4. 2-639-13-5(Q), RET 2 --REDIIIS FOR FE $\angle P P R O T A L$

Acceptability: Item 1 was rotated $90^{\circ}$. Also, welds for item 1 is insufficient. Item 1 rotated has no effect on design. Y-load is transmitted lengthwise in the beam. The component forces due to the movement of the pipe are small, therefore the forces will have negligible effect on the welds. Weld is sufficient. This is acceptable. (Ref. ITT Grinnell call. number 2-353)
5. 2-60L-16-15 (Q), REV.0/FT --HEWURK

Safety Evaluation: No clearance exists due to offset "J-bolt" holes. Specification $7220-\mathrm{M}-326$ (Q) paragraph 5.1 .3 (b) states, when the component pipe support design sketch/drawing states the clearance is $1 / 32^{\prime \prime}$ typical on opposite sides of the pipe or pipe lug, the actual clearances shall not be less than $1 / 16^{\prime \prime}$ or more than $1 / 8^{\prime \prime}$ inclusive... the actual individual clearances may be distributed in any manner, including a zero clearance on one-side of the pipe. Therefore, there is no specification violation.
6. 1-616-8-2(Q), HBV. 7 - HENOHX

Safety Evaluation: At sight holes of support rods, no threads are visible. Thread engagement on lower end of extension does not meet requirements. Measured ingagement is $1^{\prime \prime}$, minimum required is $11 / 2^{\prime \prime}$. Based on calculation, $1^{\prime \prime}$ thread engagement is sufficient. Therefore, there is no safety impact. (Ref. ITT Grinnell call. number 2-360)
7. $2 \mathrm{HBC}-216-5-\mathrm{H} 3(Q)$, HIST. $0-\mathrm{HEWORK}$

Safety Evaluation: Approximately $24 \%$ of the bearing surface exceeds gap requirements of spec. $7220-\mathrm{M}-326(\mathrm{Q})$. All of lower right hand anchor bolt and lower $1 / 4$ of plate has slightly greater than $1 / 16^{\prime \prime}$ gap. An evaluation of support $2 \mathrm{HBC}-216-5-\mathrm{H} 3(Q)$, assuming the bolt on the lower right hand corner of the base plate is nonfunctional, verifies that all the stresses are within design allowables. Therefore, there is no safety impact. (Ref. Bechtel call. number 400-3-209(Q))
8. 2-657-43-6(Q), RIEV. 1 -- REWORK

Safety Evaluation: $3 / 16^{\prime \prime}$ clearance exists between top of pipe and J-bolt. The magnitude of loads could not create enough force to fail 0 -bolt. Therefore, there is no safety impact. (Ref. Bechtel call. member. LBSE 1-657-43)


Reviewed by:

D. Fiat

Resident Small Pipe and Hangers


## PROJECT ENGINEERRING'S COMPLETE RESPONSE



This response supplements Construction and Quality Control's response to the subject NCR. The condition of the discrepancies requiring rework were evaluated for safety while redined items (to reflect existing condition) submitted for Project Zngineering approval were reviewed for acceptability. One discrepancy was also documented on Bechtel NCR 4113.

Results of the safety evaluation indicate that the identified discrepancies (requiring rework), were they to have remained uncorrected, could not have affected adversely the safety of operation of the plant.

Field redlined drawings that were submitted by Construction for approval were found acceptable. Bechtel NCR 4113 was dispositioned "use as is".

Details are shown below.

1. 2-611-6-5(Q), REV. 3 -- RRELINE FOR FE APPROVAL

Acceptability: Undersized welds and wider brace beam angle was observed. The $3 / 16^{\prime \prime}$ weld on figure 211 rear bracket to item number 2 is well within the allowables. The $3 / 16^{\prime \prime}$ fillet weld is oufficient for the connection of item number 3 to existing steel based on brief calculation. Therefore, it is acceptable. (Ref. IIT Grinnell calc. number 2-352)
2. 2-613-4-19(Q), REV. $3-\mathrm{HEDLINE}$ FOR FE APPROVAL

Acceptability: Undersized weld of $3 / 16^{\prime \prime}$ fillet at connection of item number 3 and number 2 is sufficient since subject weld is not a stressed weld. It is only used to stabilize item number 3. Therefore, it is acceptable. (Ref. ITT Grinnell calc. number 2-358)
3. $2 E C B-4-4-\mathrm{H} 5$ (Q), HEV. 2 - HEWORE

Safety Evaluation: Cotter pin is missing on lower end of west sway strut. In this evaluation, the vertical restraint on the hanger will be non-functional.

There is absolutely no danger or safety hazzard to the piping system. Thermal stresses are actually reduced, weight and seismic stresses are increased, but are still within ASME-Section III Code allowable stress levels. Loading on adjacent restraints increase if it is assumed that hanger $2 E C B-L-4-H 5(Q)$ is nonfunctional.

An evaluation of the adjacent supports, $2 E C B-4-4-H_{4}(Q)$ and $2 E C B-$ 4-5-H! (Q), with the increased loads shows that they are still within the acceptable design allowables, therefore, there is no safety impact on the system. (Ref. Bechtel calc, numbers $400-3-201(Q)$ and $: 00-3-202(Q))$
4. 2-619-2-19(Q), HEV. 1 --BRDLINE FOR PE APPROVAL

Acceptability: Rear end brackat of sway strut was rotated $90^{\circ}$. Review of thermal and seismic movepents show that there is no restraint with end bracket rotat.od. (Ref. Bechtel calc. no. LBSE1-619-2)
5. 2-619-6-11(Q), HEV. 3 --REWORX

Safety Evaluation: No gap exist between pipe and hanger. Also, undersized welds were roted on the vertical hanger beams to the bottom horizontal beam.

The radial expansion of the pipe is less than $0.001^{\prime \prime}$ resulting in a very small load. Frictional effects existing from $Y$-load is very much greater than load due to radial expansion, therefore, its contribution is negligible.

The required weld (per calculation) is $0.05^{\prime \prime}$. Therefore, the $3 / 16^{\prime \prime}$ weld is acceptable.
Based on the abovs, there is no safety impact. (Ref. Bechtel Ic. mumber SHC-619-6-1 (Q))
6. 2EBB-3-4-H1 (Q), REV. 1 -REWORK

Safety Evaluation: It was observed that plastic tie wrap was used instead of a bolt. Also, lock nuts and cotter pins are missing.

Assuming support $2 \mathrm{EBB}-3-4-\mathrm{H} 1(Q)$ will be non-functional, the piping system would still qualify per spec. M-343, i.e. still within acceptable seismic spans. The adjacent support 2 EBBB-3-4H2 (Q) would be required to pick up the additional seismic load increase from 14 pounds to 82 pounds. Failled load increase from 42 pounds to 205 pounds.

Pipe support 2 EBBB-3-4-H2 (Q) was originally designed for a faulted load of 345 pounds. This is greater than the load arrived at by the stress engineer's evaluation, therefore, the hanger is still (Ref. Bechtel calc. number 400-3-200(Q))
7. 1-612-2-2(Q), REV. 1 - REDLINE FOR PE APPROVAL

Acceptability: Undersized weld on one leg was noted. The $1 / 4^{\prime \prime}$ fillet weld at all shim plates are sufficient and are well within the limits of the welding allowables, therefore, acceptable. (Ref. ITM Grimell calc. number 2-359)
8. 1-612-4-33(Q), REV. 1/F1 ---BECEIIEL NCR L113 WAS ISSUED

Acceptability: Plate number 1 has reduced section and undersized weld. In accordance with Civil calculation $23 c 6(Q)$, the weld is acceptable. This NCR was dispositioned "use as is". (Ref. Bechtel calc. number $23 \operatorname{c} 6(Q)$ )

Reviewed by: $\frac{\text { Aspoclaza }}{\frac{\text { D. Borlaza }}{\text { Resident Q. E. }} \text {. }}$
1 Rif
D. Riant

Resident Small Pipe and Hangers


## PROJECT ENGINEERTNG'S COMPLETE RESPONSE TO

CPCo NONCONFORMANCE REPORT M-01-5-2-017, AI: 1272

This response supplements Construction and Quality Control's response to the subject NCR. The condition of the discrepancies requiring rework were evaluated for safety while Redlined items (to reflect existing condition) submitted for Project Engineering approval were reviewed for acceptability.

Results of the safety evaluation indicate that the identified deficiencies (requiring rework), were they to have remained uncorrected, could not have affected adversely the safety of operation of the plant.

Field Redlined Hanger drawings that were submitted by construction for Project Engineering's approval were found acceptable. Details are shown below.

1. OHBC-142-1-H1 (Q), REV. 4 --REWORK

Safety Evaluation: The actual total clearance between pipe and pga104 strap is $3 / 32^{\prime \prime}$. The additional $1 / 32^{\prime \prime}$ clearance is acceptable from a safety stand point. It does not increase stresses on the piping system. Stresses are within code allowables. (Ref. Bechtel call. number 439-3-1 (Q))
2. $1 \mathrm{HBD}-145-1-\mathrm{H} 9(Q)$, REV. 2 - HEWORK

Safety Evaluation: No gap exists between sides of pgs-113 strap and pipe. In this evaluation, it is assumed that the total axial restraint at hanger $\# 9$ results in the $6^{\prime}-11^{\prime \prime}$ span between $\mathrm{H}_{9}$ and H10 being totally restrained.

Although the compressive stress is not required to be evaluated by code, this was done. At a maximum temperature of $150^{\circ} \mathrm{F}$ as listed in spec. $\mathrm{M}-480$, compressive stress is well within the yield strength of the pipe material. Also, the critical buckling load for the span is not developed, and the piping system remains operable. however, a total deflection of $0.0422^{\prime \prime}$ will be distributed between supports E 9 and H10.

Since there is $1 / 32^{\prime \prime}$ clearance between the lug and the pipe on H10, Hanger H9 and H10 would only be required to deflect $0.01095^{\prime \prime}$. However, since it was assumed that the clearance is not there and E10 is also locked, the force required to deflect $\# 9\left(0.0422^{\prime \prime}\right)$ in the X -direction is $\mathrm{Fx}=600$ pounds.

An evaluation of supports H 9 and H 10 with an additional load of 600 pounds shows that the supports are still within design allowabies. Therefore, there is no safety impact. (Ref. Bechtel call. numbers 400-3-204(Q) and 400-3-205(Q))
3. 1-657-37-9(Q), REV. $2-$ HEDDITNE FOR PE APPROVAL

Acceptability: The clearance in the Z-direction is within specification tolerance. Total movement in Y-direction is $\pm 0.66^{\prime \prime}$, therefore the 0.78 clearance is acceptable. (Ref. Bechtel calc. no. LBSE 1-657-37)
4. 1-648-7-58(Q), HEV. 1/F1 -- REDLINE FOR PE APPROVAL

Acceptability: The relationship of forces indicate that support surface in the positive direction will never oome into play. Clearance is not critical to design. Therefore, it is acceptable. (Ref. Bechtel calc. number LBSE 1-648-7)
5. 1HBC-14 $1-\mathrm{H} 3$ (Q), HEV. 2 - HEWORIK

Safety Evaluation: There is only a $1 / 32^{\prime \prime}$ clearance between side of pgs113 strap and pipe. The radial expansion of the pipe at maximum temperature of $115^{\circ} \mathrm{F}$ (listed in spec. M-480) is equal to $0.00067^{\prime \prime}$ which is less than $1 / 32^{\prime \prime}$. This qualifies the piping and has no effect on the hanger. Therefore, no safety impact. (Ref. Bechtel calc. number 400-3-203(Q))
6. 1CCB-69-1-H2 (Q) HEV. 2 ---REWORI

Safety Evaluation: No gap exists between pipe clamp and its supporting structire. In this evaluation, it is assumed that the support 1CCB- ${ }^{2}-1-H_{2}$ locks up in three directions.

Ada , ional restraint for weight and seismic load cases will aid in the pipe stress equations and additional loads will be minimal due to relative locations of adjacent supports. The unrestrained displacements for thermal and seismic anchor movement load cases at H2 (per $\triangle A O$ analysis) -are used to approximate additional loads. If these displacements were restrained, the additional pipe stress would be approximately $1 / 4$ the allowable of equations \#10 and \#11, which is conservatively based on a guided cantilever beam. Therefore, the pipe system would still be operable.

Additional loads on H2 from all load cases combined would be conservatively 200 pounds $X$-direction and 200 pounds Z-direction. Additional loads on hangers 1CCB-66-1-स1 and 1CCB-69-1- स3 will be approximately 100 pounds in the $X$ - and 2-directions.

An evaluation of the above hangers with the additional loads caused by support $1 \mathrm{CCB}-69-1-\mathrm{H}_{2}$ being locked in three directions verifies that se stresses on the hangers are still within design allowables. Therefire, there is no safety impact. (Ref. Bechtel calc. number 400-3-206(Q))
. 7. 1 CCB-69-1-H1 (Q), REV. 3 and $1 \operatorname{CCB}-69-1-\mathrm{H} 2(Q)$, HEV. 2 --REWORK
Safety Evaluation: Pgs-114 requires the jam nuts to be SA-307, GR.B, however, SA-194, 2H was used. Although SA-307, GR.B nut is a standard callout for these support assemblies, the SA-194, 2 H nuts have a higher proof load rating per $A S M E$ Code. This substitution will have no safety impact on the support.
8. $0-618-1-6(Q)$, HEV. $0-$ - RIBDLINE FOR FE APPROVAL

Acceptability: Field welds between items 2 and 8 do not conform to drawing. The existing welds are within the welding allowables, therefore, welds are sufficient. (Ref. ITT Grinnell calc. number 2-357)


A TACHMENH

Midland Project: PO Box 1983, Midland, MI 48840 • (517) 631-0981

May 5, 1982

Messes W R Bird and B W Marguglio
Consumers Power Co
1945 Parnall Road
Jackson, MI 49201

Mr MA Dietrich
Bechtel Power Corp
PO Box 2167
Midland, MI 48640
MIDLAND PROJECT - USNRC EXIT MEETING (Isa Yin) OF APRIL 23, 1982
File 0.4.2 Serial 17009

An unannounced NRC inspection by Mr I T Yin took place from April 21 through April 23, 1982. Entrance and exit meetings were held on April 21 and April 23 respectively. The lists of attendees for each of those meetings are attached to this letter.

The stated (by Mr Yin) purpose of this inspection was to close infractions and unresolved items from the 81-12 inspection and other older items, if time permitted.
I. The following old items were addressed:

1. Infraction 81-12-11/12 Large Bore Pipe Supports Not Installed Per Drawings/Specifications. This item remains open and is the subject of an additional violation (See Section II on the following page for details).
2. Infraction 81-12-12/13 Pipe Hanger Inspection and Acceptance by Quality Control. This item remains open and is the subject of an additional violation (See Section II on the following page for details).
3. Infraction 81-12-13/14 Installation of Small Bore Pipe Without Committed Preliminary Design Calculations. Closed.
4. Infraction 81-12-14/15 Small Bore Pipe Design Document Control Not Maintained. Closed.
5. Infraction 81-12-16/17 Inadequate QA Audits. Closed.
6. Infraction 81-14-01 Inadequate Design Control (Redlines). Closed.
7. URI 81-12-10/11 Bechtel Specification Applicability. Closed.
8. URI 81-12-15/16 Mechanical Rework Controls. Closed.

## II. New Items

1. Infraction - Severity Level IV. Piping Suspension QC Inspection Breakdown. In view of the large number of hangers ( $43.9 \%$ of sample) identified as nonconforming in MPQAD NCRs as a result of the MPQAD overinspection of hangers which had been previously inspected and accepted by Bechtel QC, Mr Yin determined that there was breakdown in Quality Control in 1980 and that MPQAD had failed to report this as required by 10 CTR 50.55 (e). He noted that a deficiency in 127 of 9401 characteristics served only to demonstrate the complexity of the hangers, not the overall acceptability of the installed condition. Review of the records indicated that 1649 hangers were inspected/ accepted in 1980,3270 in 1981 and 789 to date (ihrough March) in 1982.

The NRC has determined that they will require the licensee to do a 100\% (re)inspection of the hangers installed in 1980 and a sample (undetermined size) of those inspected/accepted in 1981 and 1982. Any alternate proposals by MPQAD should be discussed with USNRC Region III management.
2. Unresolved item. Design of large bore hangers and other mechanical items. Mr Yin plans to visit Ann Arbor in the near future to review the design process and records in these areas.


R E Whitaker, Section Head Fluids and Mechanical Midland Project QA Department

REW/lrb

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CC BJCole, Midland
    JWCook, P26-336B
    MLOurland, Midland
    LHOurtis, Bechtel-Ann Arbor
    LEDavis, Bechtel-Midl and
    WDGreenwall, Bechtel-Ann Arbor
    DEHorn, Midland
    JAHorsch, Midland
    GSKeeley, P14-113B
    HPLeonard, Midland
    REMcase, Midl and
    DBMiller, Midland
    JARistgers, Bechtel-AA
    MJSchaeffer, Midland
    RAWells, P14-113A
    REWhitaker, Midland
    JlWood, P14-416
    Great Lakes QA Managers
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# Bechtel Power Corporation 

 Inter-office Memorandum| To | Training File | Date | June 28, 1982 |
| :--- | :--- | :--- | :--- |
| Subject | Job 7220 Midland Project | From | J. E. Studs |
|  | Training Session BT-429 | Of | Construction |
| Copies to |  | At | Midland, MI |

On Thursday, May 13, 1982, a one hour training session was held on hanger inspection. The instructors were: Rick Shaw, Mechanical Field Engineering, Ed UrDanawiz, Q.C., John Low and Ron Cable, Welding Field Engineering. A question and answer period was ir.-luded.

Those in attendance were:


J. E. Stabs

JES/kls

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John，Doboie If Johnson，Kevin 万ßJ Foris，Vurrey rire
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$\therefore \because$ ：ここ：

Masont Katema．


Mille Jeff，Jm Moore，Dick］i，David May 13， 1982 osmansxi，albert dute Hanges Insp．Trainin Mech．Rep．Rict Shaw QC Ref．Ed Urbanawi welding Rep．John Low／

OJT Checklist \& Field Training Summary
(1) PQCI:


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## INSTRUCTIONS

1. Enter the PQCI number, title, and revision.
2. Enter the generic training activites, ie. Activity No. or Subject.
3. Enter the name of the QCE in training.
4. Enter the date that the QCE commences training.
5. The level I or II QCE shall enter a checkmark (V) in the appropriate block to identify that training was conducted in a specific area.
6. Enter the signature of the Level I, II, or III QCE conducting the training
7. Enter the level of certification of the training OCE.
8. Enter the date training is conducted.
9. Enter the duration of training in hours.
10. Enter the total number of training hours.

11 . Enter specific training which is not catagorized in the activites listed in block 2 . Additionally enter the duration of this training.
Attachment 18
SPECIFICATION 7220-M-326(Q)
$\Delta$ APPE $\cdot$

SPECIFICATION 7220-M-326(Q) 1
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[^0]:    Hanger No.
    FSK-M-2HBC-216-5-H3, Rev 0

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[^2]:    Siv. of Qulg. Me:P. FOK thil C/a
    

[^3]:    

[^4]:    WEZOD OF YANT CA FRDFICATION:

[^5]:    7. ACTVAL AOOT CAUSE(S), Z DIFTERENT FROM ABOVE (TD AE COMPLITD 3Y ORG. RESPONSTBLE FOR PROCESS CA):
[^6]:    CETHOD OF PROCESS CA "ERTP"ATION:

