

BRE Client Report

Calculations of data to support ECO4 scoring methodology

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1 Introduction

The fourth iteration of the Energy Company Obligation (ECO4) is expected to use a different scoring system from ECO3 to attribute credit for installed improvement measures against obligated suppliers' targets. The 'full project scores' (FPS) for packages of improvement measures applied to homes are to be based on the improvement in the EPC rating of the dwelling as a result of the package of measures installed, as measured by before and after EPC ratings and converted to a saving in annual fuel costs.

Additionally, 'partial project scores' (PPS) will be needed to evaluate the benefits associated with individual measures for various administrative purposes. These will also be expressed as annual fuel costs savings.

For the purposes of scoring, dwellings will be assigned to a size band based on their total floor area (TFA), so that homes in larger bands (where more energy can potentially be saved) can be attributed greater credit than those in smaller bands. Four size bands have been chosen for this purpose by BEIS and Ofgem: $TFA < 73m^2$, $73m^2 \leq TFA < 98m^2$, $98m^2 \leq TFA < 200m^2$, $200m^2 \leq TFA$.

On the basis of the overall approaches outlined above being used, BRE have undertaken some SAP modelling work on behalf of Ofgem to provide the formulae and tables needed to support the full and partial project scoring systems. This note describes the basis and assumptions used for this work.



2 Full project scoring method

A dwelling's EPC rating is produced using the SAP methodology¹, which calculates the energy requirements of the building, multiplies this by the relevant fuel prices to estimate its annual running costs, normalising by floor area, and then converts this to a rating between 1 and 100. This rating is then mapped to an A to G band according to Table 14 in the SAP specification:

Table 14: Rating bands

The rating is assigned to a rating band and the Environmental Impact rating.

| Rating | Band |
|------------|------|
| 1 to 20 | G |
| 21 to 38 | F |
| 39 to 54 | E |
| 55 to 68 | D |
| 69 to 80 | C |
| 81 to 91 | B |
| 92 or more | A |

For ECO4 purposes, it has been proposed by BEIS/Ofgem to divide the bands into low and high sub-bands, using the lower and upper half of each standard band, resulting in the sub-bands in Table 1:

Table 1 – Creation of sub-bands

| Band | From | Up to | Mid-point |
|--------|------|-------|-----------|
| High_A | 96 | 100+ | 98 |
| Low_A | 92 | 96 | 94 |
| High_B | 86 | 91 | 88.5 |
| Low_B | 81 | 86 | 83.5 |
| High_C | 74.5 | 80 | 77.25 |
| Low_C | 69 | 74.5 | 71.75 |
| High_D | 61.5 | 68 | 64.75 |
| Low_D | 55 | 61.5 | 58.25 |
| High_E | 46.5 | 54 | 50.25 |
| Low_E | 39 | 46.5 | 42.75 |
| High_F | 29.5 | 38 | 33.75 |
| Low_F | 21 | 29.5 | 25.25 |
| High_G | 10.5 | 20 | 15.25 |
| Low_G | 1 | 10.5 | 5.75 |

¹ https://www.bre.co.uk/filelibrary/SAP/2012/SAP-2012_9-92.pdf



Note that EPC ratings cannot be less than 1 (if the raw value is <1, it is reset to 1), but they can exceed 100 in rare cases.

Because a metric based on the cost per m² is used to generate the EPC rating, as long as the floor area is known it is possible to back-calculate the approximate running costs from an EPC rating. The proposed approach to scoring whole projects is therefore to use the EPC sub-band mid-points before and after the improvement measure, along with the average floor area for the applicable dwelling size band, to determine the improvement in SAP points and annual running costs. This can be illustrated by stepping through an example.

A. Input data

Actual floor area of dwelling = 90m²

EPC rating (band) before improvement package = 25 (F)

EPC rating (band) after improvement package = 65 (D)

B. Assign to ECO4 size and EPC bands

In this example the floor area falls into the 73m² ≤ TFA < 98m² band.

The 'before' EPC rating falls into the 'Low_F' band.

The 'after' EPC rating falls into the 'High_D' band.

C. Assign average floor area and SAP rating for ECO4 bands

The average total floor area for a home in this floor area band, according to data from the English Housing Survey (2017-18), is 83.9m². The EHS average areas for other bands are shown in Table A1 in Appendix A.

Assuming SAP ratings are evenly distributed through the bands, the mid-point can be assigned to homes falling within each band (as shown in Table 1). In the case of the Low_F band the mid-point is 25.25. In the case of the High_D band it is 64.75. The improvement in SAP points is therefore 64.75 - 25.25 = 39.5 SAP points.

D. Calculating the annual running cost saving

The SAP specification defines the procedure for calculating the SAP rating from the annual running costs using the following formulae (an extract from SAP 2012):

13 ENERGY COST RATING

The SAP rating is related to the total energy cost by the equations:

$$ECF = \text{deflator} \times \text{total cost} / (\text{TFA} + 45) \quad (9)$$

$$\text{if } ECF \geq 3.5, \quad \text{SAP 2012} = 117 - 121 \times \log_{10}(ECF) \quad (10)$$

$$\text{if } ECF < 3.5, \quad \text{SAP 2012} = 100 - 13.95 \times ECF \quad (11)$$

where the total cost is calculated at (255) or (355) and TFA is the total floor area of the dwelling at (4).



In SAP 2012, the 'deflator' term (used to keep ratings approximately comparable from one version of SAP to the next) is 0.42.

Rearranging to make running costs the subject of the equations, the following formulae can be used to calculate the annual running costs from a SAP rating:

If SAP rating <51.175, $Annual\ running\ cost = (10^{(117 - SAP\ rating)} / 121) / 0.42 * (TFA + 45)$

Otherwise, $Annual\ running\ cost = ((100 - SAP\ rating) / 13.95) / 0.42 * (TFA + 45)$

Applying these to the before and after mid-band SAP ratings (25.25 and 64.75) gives running costs of £1,759/yr and £775/yr, respectively. The annual saving attributed to this package of measure is therefore $1759 - 775 = £983/yr$.

The proposed scoring method therefore consists of the steps and equations described above. In practice, the first 2 steps (assigning to bands) may be done by the user of the scoring tool selecting the appropriate band from a drop-down menu, rather than entering the actual floor area and SAP rating. This should reduce the chance and impact of data entry errors.

Tables illustrating the savings for all combinations of floor area band and EPC rating sub-band are shown in Appendix B. These could potentially be used as look up tables by a scoring tool or implemented directly using the formulae and tables above.



3 Partial project scoring method

Tabulated scores (running cost savings) for individual improvement measures have been generated for each ECO4-applicable measure, for all floor area bands and each applicable² starting EPC sub-band. The resulting data table is too large to include in this report, containing around 9000 scores, so has been provided to Ofgem in a separate spreadsheet.

Regarding fuel prices, it was necessary to use the standard fuel prices that are used by SAP 2012 to calculate the EPC ratings for all ECO4 calculations to give consistency between partial and full project scores.

3.1 PPS for fabric improvement measures

The scores for fabric improvement measures were derived as follows:

- i) An archetype dwelling from Table A1 (Appendix A) was modelled with a wide range of fabric efficiency standards and features, designed to cover the range found in the GB housing stock, described in Table A2, with and without the improvement measure applied, allowing the running cost savings to be calculated. The specific before and after values used for modelling improvement measures are described in section 3.1.1.
- ii) This modelling generated multiple savings for each measure starting from a range of EPC sub-bands. The savings were averaged for all those starting in a particular sub-band to give a single figure for each sub-band.
- iii) Steps i) and ii) were repeated using each of the heating system types shown in Table A3.
- iv) The savings were then weighted by the heating system mix for homes in each EPC band – see Table A4. This step is significant because the heating system makes a big difference to the cost of a unit of heat and therefore to savings for fabric improvement measures, and because the heating system mix is substantially different in homes with high EPC ratings compared to those with low ones. This generally results in bigger savings for fabric improvement measures applied in homes in lower EPC bands.
- v) The above steps were repeated for each of the dwelling archetypes representing the four size bands (Table A1).
- vi) The resulting savings for each measure were plotted as a function of the starting SAP rating and a curve was fitted through them (see Figure 1). This was necessary because of the discontinuities in the modelled results caused by using a fixed set of fabric efficiencies to represent the continuum found in the real stock and (especially) the stepped change in heating fuel mix for each EPC band. Due to the high sensitivity of fabric savings to the heating system/fuel mix changing from one band to the next, this caused steps in the

² Figures were only required up to High D for most measures. Exceptions were ‘infill measures’, which need to be available up to High B (solid wall insulation, district heating and cavity wall insulation when delivered to flats)



modelled results which would not be found if we had modelled the results for every GB home individually and averaged.

- vii) The equations of the curves giving a smooth fit through the data were used to calculate the savings for each measure in each EPC starting band.

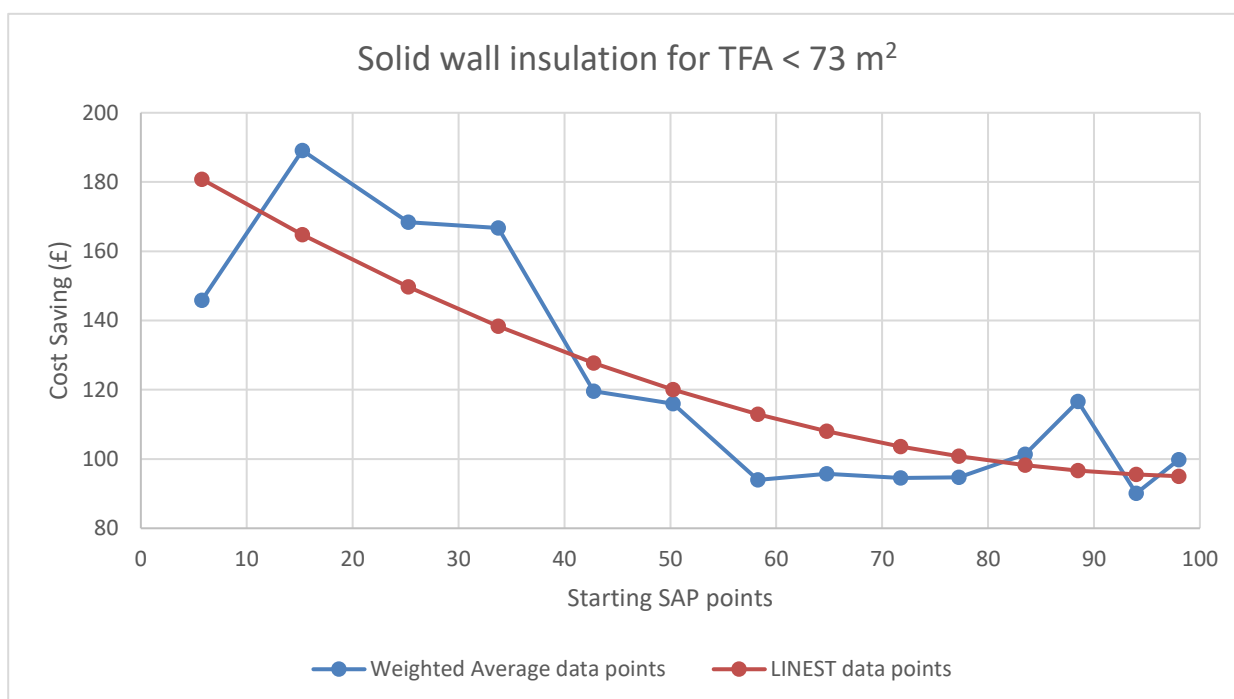


Figure 1: Example of comparison between the weighted average results and those generated from the curve fitting Excel function LINEST

To use the results of this modelling, the user could select the measure type, the starting EPC sub-band and the floor area band for the dwelling being assessed; then the scoring tool would look up the appropriate fuel cost saving from the tabulated data. This may have a reduction factor applied (see section 3.3) to give the deflated PPS. It can then be subtracted from the costs for the unimproved dwelling to give the running costs for the dwelling with the improvement applied. The post-improvement SAP rating and EPC sub-band can then be calculated using the standard SAP formulae described as part of the full project scoring method. The following example illustrates this process.

Example PPS

- Solid wall insulation is applied to a dwelling of floor area 90m² with a starting SAP rating of 25.
- The example dwelling is in the 73m²≤TFA<98m² size band and the Low_F EPC sub-band, for which a floor area of 83.9m² and a SAP rating of 25.25 are assumed. Using the reverse SAP equation described in section 1 for full project scoring, the running costs for a home of this SAP rating and floor area are calculated to be £1,759/yr.
- The pre-calculated running cost saving for the Low_F starting band for this measure is taken from the PPS table, giving a saving of £423/yr. This is multiplied by the reduction factor of, say, 0.75, giving a net PPS of £317/yr. Subtracting this from the running costs for the unimproved dwelling gives a post-improvement running cost of £1,441/yr. Using the standard SAP equations,



this is converted to a SAP rating of 35.70, which falls into the High_F sub-band, giving a SAP point saving of 10.45.

3.1.1 'Before' and 'after' values assumed for fabric measure savings

This section presents the 'before' and 'after' values for specific installations of measures used in the calculation of the PPS.

3.1.1.1 Solid wall insulation

Savings were calculated for the improvements in U-value indicated in Table 2. These savings may be applied to internal, external or hybrid wall insulation on either solid or cavity walls. The before and after U-values are taken from Section S5.1 of RdSAP (SAP 2012 v9.94³) which assume a typical insulation material.

Table 2: Assumed U-values for solid wall insulation

| | Added Insulation thickness | | | To defined U-value | |
|---------------------------------------|-----------------------------------|-------|-------|------------------------|------------------------|
| | 50mm | 100mm | 150mm | 0.3 W/m ² K | 0.6 W/m ² K |
| Starting U-value (W/m ² K) | End U-values (W/m ² K) | | | | |
| 2.0 | 0.60 | 0.35 | 0.25 | 0.3 | 0.6 |
| 1.7 | 0.55 | - | 0.23 | 0.3 | 0.6 |
| 1.0 | 0.45 | - | - | 0.3 | 0.6 |
| 0.6 | - | 0.24 | - | 0.3 | - |
| 0.45 | - | 0.21 | - | - | - |

3.1.1.2 Cavity wall insulation

Savings were calculated for three construction age bands using standard a U-value calculation methodology applied to the relevant construction (e.g. brick/brick, brick/block with an average cavity width derived by BRE from installer data, as used for the CERT scheme). These age bands are associated with significant changes in wall U-values due to the introduction of successive new Building Regulations, and are not based on RdSAP assumptions for cavity walls. For cavity wall insulation with a standard thermal conductivity of 0.040 W/mK the U-values are as shown in Table 3.

³ https://www.bregroup.com/wp-content/uploads/2019/09/RdSAP_2012_9.94-20-09-2019.pdf

**Table 3: Assumed base U-values for cavity wall dwellings as used in the calculation of CWI savings**

| Year of construction | Uninsulated U-value (W/m ² K) | Insulated U-value (W/m ² K) | Weighting |
|----------------------|--|--|-----------|
| (1) Pre 1976 | 1.435 | 0.478 | 73% |
| (2) 1976 - 83 | 1.003 | 0.417 | 13% |
| (3) post 1983 | 0.694 | 0.343 | 15% |

The U-values for the three age bands are combined to give one uninsulated and one insulated U-value regardless of the age band of the wall. This is consistent with latest research which shows wide variation in measured U-values for each age band. The three values are averaged using the weightings in the table, which are derived from the number of uninsulated cavity wall dwellings for each age band in the national stock.

The method is then repeated using cavity wall insulation with a thermal conductivity of 0.033 W/mK and 0.027 W/mK. This results in the U-values in Table 8 below for all three cavity wall insulation deemed score variants. The resulting U-values after weighting by age band are also given in Table 4.

Table 4: U-values for Cavity Wall Insulation

| Thermal conductivity (W/mK) | Weighted average 'before' U-value (W/m ² K) | Weighted average 'after' U-value (W/m ² K) |
|-----------------------------|--|---|
| 0.040 | 1.272 | 0.451 |
| 0.033 | 1.272 | 0.393 |
| 0.027 | 1.272 | 0.338 |

A partial fill measure was also modelled with a before U-value 0.45 and an after U-value of 0.28.

Party cavity wall insulation savings were calculated using the standard RdSAP U-values. The U-value assumptions are shown in Table 5 below.

Table 5: U-values for Cavity Wall Insulation of party walls

| | 'before' U-value (W/m ² K) | 'after' U-value (W/m ² K) |
|------------------------------|---------------------------------------|--------------------------------------|
| Party wall insulation | 0.5 | 0.2 |

Note that flats and maisonettes are assumed to be constructed in such a way as to avoid a thermal bypass. Therefore, there are no scores for party cavity wall insulation for these property types.



3.1.1.3 Loft insulation

During the earlier CERT scheme, a case was made that during ‘top-up’ of loft insulation, the additional savings from correction of the existing insulation was not taken account of. A survey of 200 lofts was commissioned, collecting data on ‘disturbances’ such as missing or compressed insulation, and also the fraction of wood (the joists), area of loft hatches and water tanks. From this data, modified U-values were derived, resulting in an increase to the scores. These deemed scores are calculated using these modified U-values to take account of these additional savings, resulting in improved scores.

The starting U-values were determined from examination of English Housing Survey data, and assessment of the effect on the final U-value. This is shown in Figure 2 and Figure 3 below.

Figures 2 and 3 show:

- the reduction in savings with existing depth of insulation. This graph indicates very little increase in savings when insulating from a depth above about 125mm,
- the percentage of homes with different existing depths. This indicates a significant number with 100mm. This is a common depth, being the normal depth of joists, and so usually the maximum level while still allowing storage on the joists without compressing the insulation.

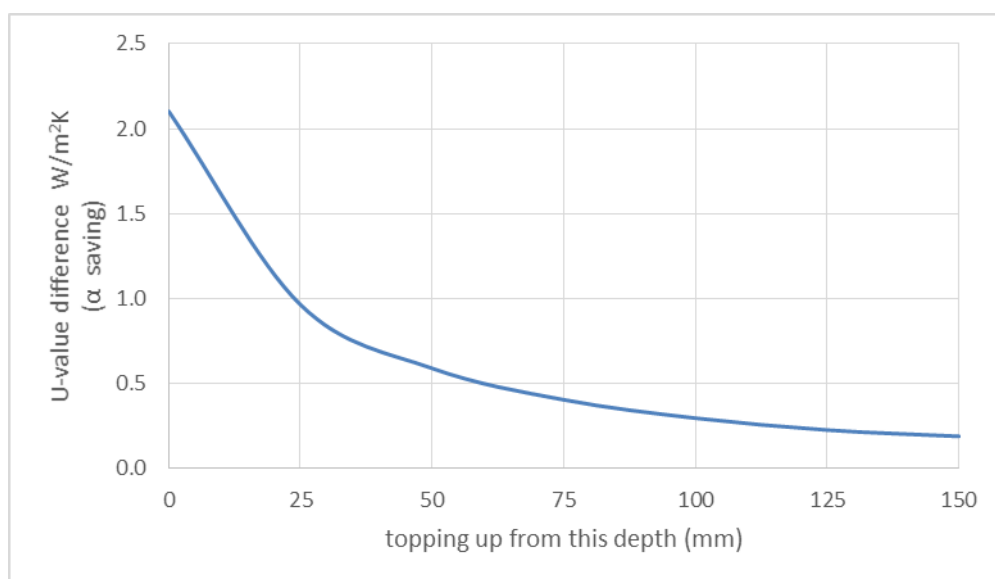


Figure 2: Difference in loft insulation U-value from topping up from different depths.

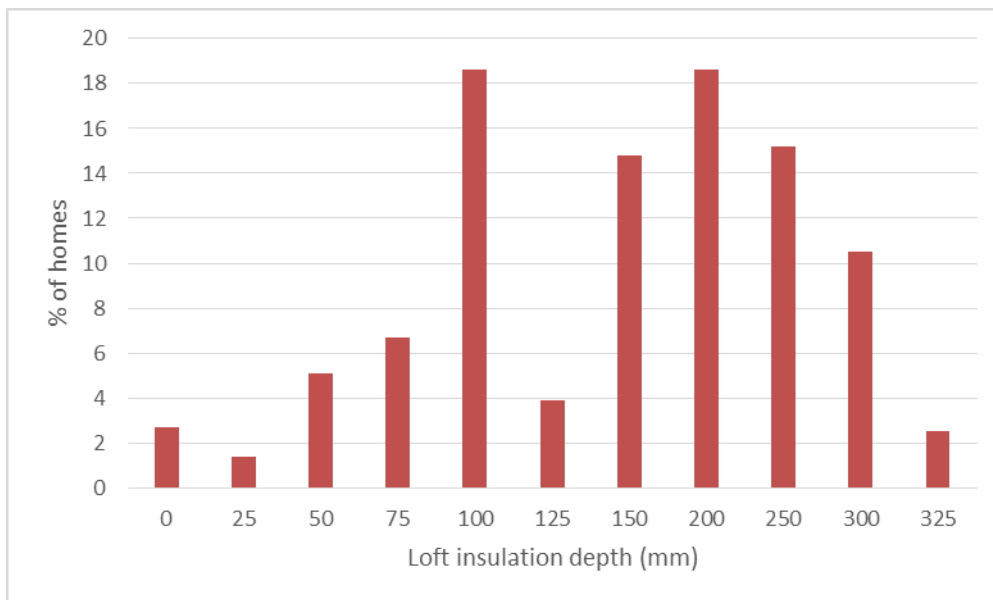


Figure 3: Distribution of loft insulation depths within England.

On the basis of this data, a weighted average U-value of depths in the stock of 100mm or less, and of 125mm to 200mm, were chosen as the ‘before’ cases (EHS data was recorded in 25mm intervals, any depths between were rounded). The post-insulation U-value assumes a thickness of 270mm, which reflects the requirements of Building Regulations. Table 6 shows the U-values used in the calculations.

Table 6: U-values for loft insulation measure variants

| | U-value before (W/m ² K) | U-value after (W/m ² K) |
|--------------------------------------|-------------------------------------|------------------------------------|
| 100mm or less of existing insulation | 0.727 | 0.185 |
| 125mm or more of existing insulation | 0.317 | 0.185 |

3.1.1.4 Room-in-roof insulation

For the ECO3 Deemed Scores, a review of ‘room in the roof’ (RiR) base assumptions was made. This review considered the different sizes of RiRs, and the base U-values of RiRs. The same assumption was made for ECO4, but the basis is repeated here for completeness.

The size of a RiR is constrained by the roof sloping on two, three or four sides. In order to calculate the size of each of the elements of a RiR, RdSAP requires the room floor area (as a minimum) to be measured, and a formula is applied based on this to estimate the areas of the other elements. However, measurement of the floor area is not considered suitable for deemed scores in ECO, and EHS and other data does not directly record the floor area of RiRs (only their presence and some information on their



type and age). Instead, data on the *type* of RiR, which is collected by the EHS, is used in order to estimate floor area.

Analysis of EHS data identified two different types of RiR:

- a) Those with no dormer windows (e.g. ‘Velux’ type conversions), or with small ‘standard’ dormer windows
- b) Those with large ‘Roof Extension’ or ‘Box Dormers’. Typically these would be at the rear of the property only, but in some cases they would also extend to the front elevation

It is then assumed that RiRs of type a) typically have a floor area of 50% of the floor below. Those of type b) are split into two categories, depending on whether there is a roof extension or box dormer on one or two elevations. RiRs with either of these elements on one elevation are assumed to have a floor area of 75% of the floor area below. RiRs with these on two elevations, are assumed to have a floor area of 95%.

Using these assumptions, and considering only RiRs built before 2002 (after this date, the performance of elements of the RiR are assumed to be equal to or better than an improved RiR), we can produce an estimate of the floor area of all RiRs using the EHS data on the distribution of these types of RiR in the stock as shown in Table 7. This produces an average floor area for RiRs of 59% of the area of the floor below.

Table 7: Assumptions used in estimating size of rooms-in-roof.

| Dormer type of room-in-roof | Distribution of room-in-roof type in housing stock (EHS data – pre-2002 room-in-roofs only) | Assumed proportion of floor area occupied by room-in-roof |
|---|--|--|
| No dormer or standard dormer | 70% | 50% |
| Front or back roof extension dormer | 21% | 75% |
| Front and back roof extension dormer | 9% | 95% |
| All pre-2002 room-in-roofs | 100% | Weighted average = 59% |

This value is used to calculate a RiR floor area for each dwelling archetype, which was then used within the RdSAP calculations to produce the areas of each of the RiR heat loss elements (RiR walls & roof).

EHS data on ages can also be used to assign U-values to these elements. The EHS collects data on the age of properties for ‘as-built’ RiRs, and an estimated age of loft conversions for converted RiRs. These two pieces of information are combined to produce the age of a RiR, which can then be matched with



the corresponding U-value for each element from the RdSAP table. A weighted average U-value, representative of RiRs built before 2002, is then produced using the EHS data on the distribution of RiRs in each age band. The results of this analysis are shown in Table 8 below.

Table 8: U-values for loft insulation

| Age of room in roof | Total number of dwellings | U-value of elements (using RdSAP Table S10) |
|------------------------|---------------------------|---|
| Pre 1966 | 1,068,000 | 2.30 |
| | 47.0% | |
| 1967 - 1975 | 233,000 | 1.50 |
| | 10.3% | |
| 1976 - 1982 | 160,000 | 0.80 |
| | 7.0% | |
| 1983 - 1990 | 274,000 | 0.50 |
| | 12.1% | |
| 1991 - 1995 | 214,000 | 0.35 |
| | 9.4% | |
| 1996 - 2002 | 324,000 | 0.35 |
| | 14.3% | |
| All dwellings with RIR | 2,273,000 | Weighted average 1.43 |
| | 100.0% ⁴ | |

Based on this analysis, the scores for RiR insulation have been produced using the U-values shown in Table 9 below. The 'after' U-values are based on Building Regulations Part L1B Table 3, assuming an insulation depth of 270mm at loft and ceiling (modified to allow for the 'disturbances' as described under 'Loft insulation').

⁴ This total percentage allows for a 0.01% error due to rounding

**Table 9: U-values for Room in Roof insulation.**

| | U-value (W/m ² K) | |
|----------|------------------------------|-------|
| | before | after |
| Ceiling | 1.43 | 0.185 |
| Walls | 1.43 | 0.3 |
| Residual | 0.36 | 0.36 |

3.1.1.5 Flat roof insulation

Savings were calculated using the standard SAP U-value for an uninsulated roof and insulating to Building Regulations Approved Document Part L1B Table 3 requirements. The U-values used for flat roof insulation are shown in Table 10 below.

Table 10: U-values for flat roof insulation.

| U-value before (W/m ² K) | U-value after (W/m ² K) |
|-------------------------------------|------------------------------------|
| 2.3 | 0.18 |

3.1.1.6 Pitched roof insulation

In the absence of specific data, the U-value achieved by pitched roof insulation was assumed to be the same as for loft insulation, being improved in both cases to a U-value of 0.185. This was based on starting U-values of 2 (for no previous insulation being present) and 1 (where there is some existing insulation present). However, to allow for the larger heat loss area of roofs insulated at rafter level compared to joist level, the horizontal roof area (before and after improvement) was multiplied by $1 / \cos 40^\circ = 1.3$.

3.1.1.7 Underfloor insulation

Savings were calculated for insulating a suspended wooden floor using the U-values shown in Table 11 below. The 'before' U-value for each of the dwelling types/sizes was derived from a standard calculation for wooden timber ground floors (derived from the floor area and perimeter of external walls). For the 'after' case the Building Regulations Part L1B Table 3 requirement of 0.25 W/m²K was used.

Table 11: U-values for floor insulation.

| U-value before (W/m ² K) | U-value after (W/m ² K) |
|---|------------------------------------|
| Suspended wooden floor U-value calculation (depends on the area and perimeter so is a different value for each dwelling type and size, varying from 0.46 to 0.66 W/m ² K for a suspended timber floor) | 0.25 |
| Solid floor U-value calculation (depends on the area and perimeter so is a different value for each dwelling type and size, varying from 0.48 to 0.67 W/m ² K for a suspended timber floor) | 0.25 |

3.1.1.8 Draught-proofing

Savings were calculated using a 'before' case of 0%, and an 'after' case of 100% draught-proofing.



3.1.1.9 Glazing

Savings from glazing were calculated for upgrading windows to a U-value of 1.6 W/m²K (the standard required in Building Regulations Approved Document Part L1B Table 1), from two base cases:

- (a) Single glazed windows
- (b) Double glazed windows, typical for the existing stock as defined in 'base cases' (table 2 in section 2.2).

The U-values used in these calculations are shown in Table 12 below.

Table 12: U-values for glazing upgrades

| Before | after |
|--|--|
| Single glazing U-value: 4.8 W/m ² K 0% draughtsealing | Double or triple glazing U-value: 1.6 W/m ² K 100% draughtsealing |
| Double glazing U-value: 2.2 W/m ² K 100% draughtsealing | Double or triple glazing U-value: 1.6 W/m ² K 100% draughtsealing |

3.1.1.10 High performing doors

Savings from high performing doors were calculated for improving the doors from a standard U-value as given in RdSAP for pre-1976 age bands, to that required by the Building Regulations Approved Document Part L during a refurbishment. This can be applied to doors with areas of glazing since the same Part L minimum requirements apply (n.b. the ECO2t measure distinguishes between doors with less than 60% and greater than 60% glazing, which give the same savings, but with different lifetimes). The U-value assumptions are shown in Table 13 below.

Table 13: U-values for door improvements

| U-value before (W/m ² K) | U-value after (W/m ² K) |
|-------------------------------------|------------------------------------|
| 3.0 | 1.8 |

3.1.1.11 Park home insulation

Although many sizes of Park Homes may be found, two common types are found which can be described as either "single" or "double" types. Both are typically 12 metres long and either 3 or 6 metres wide. Savings have been calculated for these two sizes as shown below in Table 14:

Table 14: Park Home dimensions

| | Size | Floor area (m ²) |
|------------|--------|------------------------------|
| Park Homes | single | 36 |
| | double | 72 |

Developing 'before' U-values for park home insulation measures required a different methodology than for other measures, as there is limited data available to come to a 'typical' park home. Combining data from the relevant British Standard for park homes (BS3632 Residential park homes – Specification), the RdSAP age bands and various studies and investigations of park homes suggest the 'before' U-values outlined in Table 15 are a reasonable approximation of a typical park home.



The 'after' position assumes an upgrade to add a thermal resistance of 0.695, a level which internal BRE work considers to be achievable, and which also brings the elemental U-values of the Park Home up to approximately the level of the BS3632:1995 standard. The floor U-values are dependent on whether the single or double park home is selected.

Table 15: U-values used for Park Home Insulation measures

| | U-value before (W/m ² K) | U-value after (W/m ² K) |
|-------|--|---------------------------------------|
| Roof | 0.6 | 0.42 |
| Wall | 1.2 | 0.65 |
| Floor | 0.73 (double)/0.92 (single) | 0.52 |

3.1.2 Photovoltaics

Although not a fabric improvement measure, PV savings were calculated in the same manner as the figures for fabric measures. Savings were derived using the configuration defined in SAP Appendix T 'Improvement measures for Energy Performance Certificates'. This identifies a solar panel as 2.5kWp, and located on a south facing roof on an incline of 30°, with modest overshadowing. Scores for specific areas of PV may be calculated by adjusting these values proportionately using the kWp of the individual installation.

3.2 PPS for heating system upgrades

The PPS for heating systems were calculated using a different method which is based on the fact that it is possible to calculate a 'cost of heat' for any heating system and use this to infer the dwelling's heat demand from the EPC rating and floor area. The following illustrative example demonstrates this process.

- A home of 90m² in EPC sub-band low-E is heated by an old gas boiler of 60% efficiency.
- The reverse SAP rating formula from section 1 can be used to calculate the approximate running costs of the dwelling from its EPC rating, in this case £1,759/yr. Subtracting the proportion of this cost which is for lighting, pumps and fans, and standing charges leaves £1,553/yr, which is the proportion used for space and water heating, provided by the boiler.
- In SAP 2012, the cost of gas is 3.48p per kWh, so the cost of heat would be $3.48 / 60\% = 5.8\text{p/kWh}$. Therefore, the heat requirement (for space and water heating) of this home must be $£1,553 / (5.8 / 100) = 26,776 \text{ kWh/yr}$.
- If the boiler is replaced by a new 90% efficient gas condensing boiler, the new cost of heat would be $3.48 / 90\% = 3.87\text{p/kWh}$.
- The cost of providing the same amount of heat would then be $26,776 \times (3.87 / 100) = £1,036/\text{yr}$. Adding back on the same amounts for other uses and the standing charge gives total costs of £1,242/yr. Thus, the saving for the improvement measure can be calculated as $1,759 - 1,242 = £517/\text{yr}$. The improved EPC rating can then be calculated from the running costs, if needed.

Using this process, and the assumptions about the cost of heat described in Table 16, the savings for going from and to all combinations of heating systems in ECO4 were calculated for each floor area band and each starting EPC sub-band.

**Table 16 – Key heating system assumptions**

| Heating type | Cost of fuel (p/kWh) | Efficiency | Cost of heat (p/kWh) |
|-------------------------------------|----------------------|------------|----------------------|
| Mains gas condensing boiler | 3.48 | 88% | 3.95 |
| Mains gas non-condensing boiler | 3.48 | 75% | 4.64 |
| Mains gas Back Boiler to radiators | 3.48 | 66% | 5.27 |
| Mains gas fire with back boiler | 3.48 | 50% | 6.96 |
| Mains gas room heaters | 3.48 | 60% | 5.80 |
| LPG condensing boiler | 7.6 | 88% | 8.64 |
| LPG non-condensing boiler | 7.6 | 75% | 10.13 |
| Bottled LPG boiler | 10.3 | 81% | 12.72 |
| LPG room heaters | 10.3 | 60% | 17.17 |
| Condensing oil boiler | 5.44 | 90% | 6.04 |
| Non-condensing oil boiler | 5.44 | 80% | 6.80 |
| Biomass Boiler | 3.07 | 65% | 4.72 |
| Solid fuel boiler | 3.67 | 60% | 6.12 |
| Solid fuel room heaters | 3.67 | 50% | 7.34 |
| Electric room heaters | 13.19 | 100% | 13.19 |
| Electric storage heaters | 5.5 | 85% | 6.47 |
| Electric boiler | 13.19 | 100% | 13.19 |
| High Heat Retention Storage Heaters | 5.5 | 95% | 5.79 |
| District heating system (non-CHP) | 4.24 | 100% | 4.24 |
| District heating system (CHP) | 2.97 | 100% | 2.97 |
| Ground source heat pump | 13.19 | 285% | 4.63 |
| Air source heat pump | 13.19 | 251% | 5.25 |
| mCHP(TFA<73) | 3.48 | 42% | 1.07 |
| mCHP(73≤TFA<98) | 3.48 | 48% | 1.48 |
| mCHP(98≤TFA<200) | 3.48 | 49% | 1.99 |
| mCHP(200≤TFA) | 3.48 | 54% | 2.99 |

In the case of storage heaters, an efficiency of <100% is used in Table 16 (despite their true efficiency of heat generation being 100%) to allow for their lower responsiveness compared to direct heating systems, which results in a higher heat demand.

In the case of micro CHP, which generates electricity as well as heat, the cost of heat figure in Table 16 accounts for the value of the electricity generated, as well as the cost of the fuel used – hence the cost of heat is lower than the cost of the gas used to generate it.

This approach requires the heating type before the improvement to be known (in contrast to the PPS for fabric measures which are averaged over all heating systems). The user of the scoring tool would therefore need to select the floor area band, the initial EPC rating sub-band and the initial heating system type to get the saving for a heating upgrade. This approach was taken because the savings from a heating upgrade are predominantly determined by what system was present before the upgrade.

The fuel costs needed for this approach were taken directly from SAP 2012 Table 12, unmodified, to give consistency with the FPS.



3.3 Reduction factor

A reduction factor can be applied to individual improvement measure scores to reduce the possibility of more credit being given for the installation of an individual measure than it would receive when part of a package of measures. This can occur because the interaction between measures is not included when scoring measures in isolation. For example, when a heating upgrade and an insulation upgrade are installed together the sum of their individually calculated savings will be less than their combined saving because installing insulation reduces the heating demand, so the saving achieved by the heating system falls; or, conversely, the saving for installing insulation is reduced when the heating system is more efficient. In practice the reduction caused by this interaction will vary with the measures being combined and the initial condition of the dwelling, but to keep things simple the use of a global reduction factor has been proposed. A set of illustrative examples for a few scenarios is shown in Appendix C, suggesting a factor of around 0.75, however a more detailed analysis considering the interaction for all possible combinations of measures will be used to determine the final reduction factor to be used.

In most cases, the PPS will be discarded for scoring purposes and the FPS method described in section 1 used instead, meaning the interaction between measures would be handled properly without the need for a correction factor. The correction factor would just be applied to PPS to avoid creating undue optimism when the impact of an individual measure is needed.

3.4 Scoring innovative measures

The scoring approach for innovative measures can be treated in a similar way to PPS, following the process described above to score an individual measure. Innovative measures can then be added to the PPS lookup tables as needed.

The notable difference in scoring innovative measures is that they are usually cannot be modelled using SAP, so in most cases the prior (and major) task needed to score them would be the creation of an evidence-based calculation methodology to establish running cost savings for a dwelling in each size band and each EPC sub-band. It may also be appropriate to apply a reduction factor relating to the uncertainty of the efficacy of the measure (e.g. based on the quality of evidence for the saving).

3.5 Proxy heating types

For ECO3, the savings for all measures depended on the heating system present prior to the improvement being made. To avoid the table of scores becoming unmanageably large, instead of providing scores for homes with rare heating systems, a proxy was assigned (e.g. homes with electric ceiling heaters would be assigned the savings calculated for homes with direct electric room heaters) on the basis of giving the closest match, taking account of the efficiency, fuel cost and responsiveness of the system.

For ECO4, PPS for fabric improvement measures are calculated as a weighted average over all heating systems types, so proxy heating types are not needed; but for heating measures the initial heating system type is still needed and therefore proxy heating types will be needed where rare heating systems are present, prior to improvement.

By calculating a typical cost of heat figure for each system type and comparing to the main heating types for which we do have PPS listed in Table 16, the closest match has been chosen as the proxy system of the same broad type (central heating or room heaters). These proxy systems are shown in Table 17.

**Table 17: Proxy heating systems to be used for rare heating types**

| Type | Rare heating types | Cost of fuel (p/kWh) | Efficiency | Cost of heat (p/kWh) | Proxy |
|------|--|----------------------|------------|----------------------|------------------------------------|
| CH | Air-oil hybrid heat pump | 13.19 | 251% | 5.25 | Air source heat pump |
| CH | Biomass/wood central heating | 5.26 | 60% | 8.77 | LPG condensing boiler |
| RH | Biomass/wood room heating | 4.61 | 50% | 9.22 | Solid fuel room heaters |
| CH | Bottled LPG back boiler to radiators | 10.3 | 66% | 15.61 | Electric boiler |
| CH | Bottled LPG central heating | 10.3 | 81% | 12.72 | Bottled LPG boiler |
| RH | Bottled LPG fire with back boiler | 10.3 | 50% | 20.60 | LPG room heaters |
| CH | Bottled LPG range cooker boiler | 10.3 | 61% | 16.89 | Electric boiler |
| RH | Bottled LPG room heaters | 10.3 | 60% | 17.17 | LPG room heaters |
| RH | Electric ceiling heaters | 13.19 | 100% | 13.19 | Electric room heaters |
| RH | Electric underfloor heaters | 13.19 | 95% | 13.88 | Electric room heaters |
| CH | Electric warm air system | 13.19 | 100% | 13.19 | Electric boiler |
| CH | Gas back boiler to radiators | 3.48 | 66% | 5.27 | Mains gas Back Boiler to radiators |
| CH | Gas fire with back boiler | 3.48 | 50% | 6.96 | Non-condensing oil boiler |
| CH | Gas range cooker boiler | 3.48 | 61% | 5.70 | Condensing oil boiler |
| CH | Gas warm air system | 3.48 | 70% | 4.97 | Biomass Boiler |
| CH | LPG back boiler to radiators | 7.6 | 66% | 11.52 | Bottled LPG boiler |
| CH | LPG boiler - Special Condition 18* | 3.48 | 81% | 4.30 | District heating system (non-CHP) |
| CH | LPG fire with back boiler | 7.6 | 50% | 15.20 | Electric boiler |
| CH | LPG range cooker boiler | 7.6 | 61% | 12.46 | Bottled LPG boiler |
| CH | LPG warm air system | 7.6 | 70% | 10.86 | LPG non-condensing boiler |
| RH | No heating present | 13.19 | 100% | 13.19 | Electric room heaters |
| CH | Oil range cooker boiler | 5.44 | 71% | 7.66 | LPG condensing boiler |
| RH | Oil room heaters | 5.44 | 55% | 9.89 | Solid fuel room heaters |
| CH | Oil warm air system | 5.44 | 70% | 7.77 | LPG condensing boiler |
| CH | Solid fossil fuel back boiler to radiators | 4.61 | 63% | 7.32 | Non-condensing oil boiler |
| RH | Solid fossil fuel fire with back boiler | 4.61 | 50% | 9.22 | Solid fuel room heaters |



Appendix A Modelling inputs

| Dwelling Archetype | Band | Average Area (m²) |
|---------------------------|----------------|-------------------------------------|
| Small 2 ext. Wall Flat | TFA < 73 | 56.1 |
| Medium Semi-detached 3 | 73 ≤ TFA < 98 | 83.9 |
| Medium Semi-detached 4 | 98 ≤ TFA < 200 | 127.6 |
| Large Detached | 200 ≤ TFA | 266.6 |

Table A1: Dwelling types and areas

| Roof U-value | Wall U-value | Window U-value | Floor U-value | PV fraction of main roof |
|---------------------|---------------------|-----------------------|----------------------|---------------------------------|
| 0.10 | 0.10 | 0.75 | 0.10 | 0.30 |
| 0.13 | 0.20 | 1.50 | 0.25 | 0.28 |
| 0.30 | 0.50 | 1.60 | 0.50 | 0.20 |
| 0.59 | 0.71 | 2.09 | 0.57 | 0.18 |
| 0.87 | 0.93 | 2.57 | 0.64 | 0.13 |
| 1.16 | 1.14 | 3.06 | 0.71 | 0.10 |
| 1.44 | 1.36 | 3.54 | 0.79 | 0.05 |
| 1.73 | 1.57 | 4.03 | 0.86 | 0.03 |
| 2.01 | 1.79 | 4.51 | 0.93 | 0.00 |
| 2.30 | 2.00 | 5.00 | 1.00 | 0.00 |

Table A2: Range of fabric and PV inputs

| Heating System | Efficiency | Responsiveness |
|------------------------------------|-------------------|-----------------------|
| Electric storage heater | 100% | 0.2 |
| LPG boiler non-condensing | 75% | 1 |
| Electric room heaters | 100% | 1 |
| Gas boiler 75 | 75% | 1 |
| Gas boiler 88 | 88% | 1 |
| Oil boiler condensing | 90% | 1 |
| LPG boiler condensing | 88% | 1 |
| Oil boiler non-condensing | 80% | 1 |
| Gas fire with back boiler | 50% | 1 |
| High heat retention storage heater | 100% | 0.8 |

Table A3: Range of heating systems modelled with the various fabric upgrade measures



| Proportion of heating systems by EPC band | | | | | | | |
|---|----------|-------|-------|-------|-------|-------|-------|
| Main heating system | EPC band | | | | | | |
| | A | B | C | D | E | F | G |
| Mains gas condensing boiler | 77.4% | 77.4% | 82.0% | 66.2% | 29.2% | 2.3% | 0.0% |
| Mains gas non-condensing boiler | 0.0% | 0.0% | 6.4% | 18.1% | 30.5% | 2.7% | 0.0% |
| Gas fire with back boiler | 0.0% | 0.0% | 0.0% | 1.0% | 2.0% | 5.0% | 1.0% |
| Oil condensing boiler | 0.6% | 0.6% | 0.4% | 1.4% | 5.1% | 7.1% | 1.1% |
| Oil non-condensing boiler | 0.0% | 0.0% | 0.0% | 1.0% | 6.9% | 15.7% | 5.5% |
| LPG condensing boiler | 0.0% | 0.0% | 1.0% | 5.0% | 7.0% | 8.0% | 8.9% |
| LPG non-condensing boiler | 0.0% | 0.0% | 0.0% | 1.0% | 2.0% | 9.0% | 8.4% |
| Electric storage heaters | 0.0% | 2.7% | 3.2% | 2.2% | 8.6% | 18.0% | 11.1% |
| Direct electric heaters | 0.0% | 0.0% | 1.0% | 1.0% | 3.2% | 20.1% | 42.5% |
| HHR electric storage heaters | 10.7% | 8.0% | 2.0% | 1.0% | 0.0% | 0.0% | 0.0% |
| Other | 11.3% | 11.3% | 4.0% | 2.1% | 5.5% | 12.1% | 21.5% |
| TOTAL | 100% | 100% | 100% | 100% | 100% | 100% | 100% |

Table A4: Mix of heating systems for homes in each starting EPC band, based on EHS 2017-18 data. Green rows required further assumptions to estimate their proportion. 'Other' was pro-rated into previous categories for the final weighting.



Appendix B Full project savings (£/yr) for all size and rating bands

| TFA<73 | | | | | | | | | | | | |
|----------------------|--------------------|--------|-------|--------|-------|--------|-------|--------|-------|--------|-------|--------|
| Starting EPC band √ | Finishing EPC band | | | | | | | | | | | |
| | Low_A | High_B | Low_B | High_C | Low_C | High_D | Low_D | High_E | Low_E | High_F | Low_F | High_G |
| High_B | 95 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Low_B | 181 | 86 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| High_C | 289 | 194 | 108 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Low_C | 384 | 289 | 203 | 95 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| High_D | 505 | 410 | 324 | 216 | 121 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Low_D | 617 | 522 | 436 | 328 | 233 | 112 | 0 | 0 | 0 | 0 | 0 | 0 |
| High_E | 754 | 659 | 573 | 465 | 370 | 249 | 137 | 0 | 0 | 0 | 0 | 0 |
| Low_E | 886 | 791 | 704 | 596 | 502 | 381 | 269 | 132 | 0 | 0 | 0 | 0 |
| High_F | 1070 | 975 | 889 | 781 | 686 | 565 | 453 | 316 | 185 | 0 | 0 | 0 |
| Low_F | 1276 | 1181 | 1095 | 987 | 892 | 772 | 659 | 522 | 391 | 206 | 0 | 0 |
| High_G | 1566 | 1471 | 1384 | 1277 | 1182 | 1061 | 949 | 812 | 680 | 495 | 289 | 0 |
| Low_G | 1896 | 1801 | 1715 | 1607 | 1512 | 1392 | 1279 | 1142 | 1011 | 826 | 620 | 331 |
| 73≤TFA<98 | | | | | | | | | | | | |
| Starting EPC band √ | Finishing EPC band | | | | | | | | | | | |
| | Low_A | High_B | Low_B | High_C | Low_C | High_D | Low_D | High_E | Low_E | High_F | Low_F | High_G |
| High_B | 121 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Low_B | 231 | 110 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| High_C | 368 | 247 | 137 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Low_C | 489 | 368 | 258 | 121 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| High_D | 643 | 522 | 412 | 275 | 154 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Low_D | 786 | 665 | 555 | 418 | 297 | 143 | 0 | 0 | 0 | 0 | 0 | 0 |
| High_E | 961 | 840 | 730 | 592 | 471 | 317 | 175 | 0 | 0 | 0 | 0 | 0 |
| Low_E | 1128 | 1007 | 898 | 760 | 639 | 485 | 342 | 168 | 0 | 0 | 0 | 0 |
| High_F | 1364 | 1243 | 1133 | 996 | 875 | 721 | 578 | 403 | 235 | 0 | 0 | 0 |
| Low_F | 1627 | 1506 | 1396 | 1258 | 1137 | 983 | 840 | 666 | 498 | 263 | 0 | 0 |
| High_G | 1995 | 1874 | 1764 | 1627 | 1506 | 1352 | 1209 | 1034 | 867 | 631 | 369 | 0 |
| Low_G | 2417 | 2296 | 2186 | 2048 | 1927 | 1773 | 1630 | 1456 | 1288 | 1053 | 790 | 421 |
| 98≤TFA<200 | | | | | | | | | | | | |
| Starting EPC band √ | Finishing EPC band | | | | | | | | | | | |
| | Low_A | High_B | Low_B | High_C | Low_C | High_D | Low_D | High_E | Low_E | High_F | Low_F | High_G |
| High_B | 162 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Low_B | 309 | 147 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| High_C | 493 | 331 | 184 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Low_C | 655 | 493 | 346 | 162 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| High_D | 862 | 700 | 552 | 368 | 206 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Low_D | 1053 | 891 | 744 | 560 | 398 | 191 | 0 | 0 | 0 | 0 | 0 | 0 |
| High_E | 1287 | 1125 | 977 | 793 | 631 | 425 | 234 | 0 | 0 | 0 | 0 | 0 |
| Low_E | 1511 | 1349 | 1202 | 1018 | 856 | 650 | 458 | 225 | 0 | 0 | 0 | 0 |
| High_F | 1827 | 1665 | 1517 | 1333 | 1171 | 965 | 774 | 540 | 315 | 0 | 0 | 0 |
| Low_F | 2178 | 2016 | 1869 | 1685 | 1523 | 1317 | 1125 | 892 | 667 | 352 | 0 | 0 |
| High_G | 2672 | 2510 | 2363 | 2179 | 2017 | 1810 | 1619 | 1385 | 1161 | 845 | 494 | 0 |
| Low_G | 3236 | 3074 | 2927 | 2743 | 2581 | 2375 | 2183 | 1950 | 1725 | 1410 | 1058 | 564 |



| 2005TFA | | | | | | | | | | | | |
|--------------------------------|--------------------|--------|-------|--------|-------|--------|-------|--------|-------|--------|-------|--------|
| Starting EPC band ^v | Finishing EPC band | | | | | | | | | | | |
| | Low_A | High_B | Low_B | High_C | Low_C | High_D | Low_D | High_E | Low_E | High_F | Low_F | High_G |
| High_B | 293 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Low_B | 558 | 266 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| High_C | 891 | 598 | 332 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Low_C | 1183 | 891 | 625 | 293 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| High_D | 1556 | 1263 | 997 | 665 | 372 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Low_D | 1902 | 1609 | 1343 | 1011 | 718 | 346 | 0 | 0 | 0 | 0 | 0 | 0 |
| High_E | 2324 | 2031 | 1765 | 1433 | 1140 | 768 | 422 | 0 | 0 | 0 | 0 | 0 |
| Low_E | 2729 | 2436 | 2171 | 1838 | 1546 | 1173 | 827 | 405 | 0 | 0 | 0 | 0 |
| High_F | 3298 | 3006 | 2740 | 2408 | 2115 | 1743 | 1397 | 975 | 569 | 0 | 0 | 0 |
| Low_F | 3934 | 3641 | 3375 | 3043 | 2750 | 2378 | 2032 | 1610 | 1205 | 635 | 0 | 0 |
| High_G | 4825 | 4532 | 4266 | 3934 | 3642 | 3269 | 2923 | 2501 | 2096 | 1527 | 891 | 0 |
| Low_G | 5844 | 5552 | 5286 | 4953 | 4661 | 4289 | 3943 | 3521 | 3115 | 2546 | 1911 | 1019 |