# All-Island Ten-Year Transmission Forecast Statement

2020





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This document incorporates the Transmission System Capacity Statement for Northern Ireland and the Transmission Forecast Statement for Ireland. For queries relating to this document or to request a copy contact :

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# All-Island Ten-Year Transmission Forecast Statement 2020

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# **Document Structure**

This document contains an Abbreviations and Terms section, an Executive Summary, eight main sections and eight appendices. The structure of the document is as follows:

Abbreviations and Terms provides a list of abbreviations and terms used in the document.

The **Executive Summary** gives an overview of the main highlights of the document.

#### Chapter 1: Introduction

Presents the purpose and context of the All-Island Transmission Forecast Statement. Our statutory and legal obligations are also introduced.

#### Chapter 2: The Electricity Transmission System

Describes the existing all-island transmission system. A brief outline of transmission system development plans for both Ireland and Northern Ireland is also given.

#### Chapter 3: Demand

Describes the demand forecast assumptions over the study period of 2020 – 2029.

#### **Chapter 4: Generation**

Describes the projected generation connection assumptions over the study period of 2020 – 2029.

#### Chapter 5: Transmission System Performance

Provides information on power flow and short circuit study results.

#### Chapter 6: Overview of Transmission System Capability Analysis

Outlines the analysis methods used to carry out the demand and generation opportunities' analyses.

#### Chapter 7: Transmission System Capability for New Generation

Describes the opportunities for connection of new generation on the all-island transmission system.

#### **Chapter 8: Transmission System Capability for New Demand**

Describes the opportunities for connection of new demand on the all-island transmission system.

Appendix A: Maps and Schematic Diagrams

Appendix B: Transmission System Characteristics

**Appendix C:** Demand Forecasts at Individual Transmission Interface Stations

Appendix D: Generation Capacity and Dispatch Details

Appendix E: Short Circuit Currents

Appendix F: Approaches to Consultation for Developing the Grid

Appendix G: References

Appendix H: Power Flow Tables

# Abbreviations and Terms

# Abbreviations

| Abbreviation | Explanation   |
|--------------|---|
| AC           | Alternating Current   |
| ACS          | Average Cold Spell  |
| ATR          | Associated Transmission Reinforcement                         |
| BETTA        | The British Electricity Trading and Transmission Arrangements |
| BSP          | Bulk Supply Point   |
| CCGT         | Combined Cycle Gas Turbine                                    |
| CHP          | Combined Heat and Power                                       |
| CRU          | Commission for the Regulation of Utilities                    |
| DC           | Direct Current/Double Circuit                                 |
| DCCAE        | Department of Communications, Climate Action and Environment  |
| DfE          | Department for the Economy                                    |
| DO           | Distillate Oil  |
| DSM          | Demand Side Management  |
| DSO          | Distribution System Operator                                  |
| EIDAC        | EirGrid Interconnector DAC                                    |
| ESB          | Electricity Supply Board                                      |
| ESRI         | Economic and Social Research Institute                        |
| EU           | European Union  |
| FAQ          | Firm Access Quantity  |
| GCS          | Generation Capacity Statement                                 |
| GIS          | Gas Insulated Switchgear                                      |
| HFO          | Heavy Fuel Oil  |
| HVDC         | High Voltage Direct Current                                   |
| IA           | Interconnector Administrator                                  |
| IME          | Internal Market for Electricity                               |
| IMP          | Independent Market Participant                                |
| IPP          | Independent Power Producer                                    |
| IRL          | Ireland   |
| ITC          | Incremental Transfer Capability                               |
| kV           | Kilo Volts  |
| LFG          | Land Fill Gas   |
| MIL          | Moyle Interconnector Limited                                  |
| MCR          | Maximum Continuous Rating                                     |
| MEC          | Maximum Export Capacity                                       |
| MIC          | Maximum Import Capacity                                       |
| MVA          | Megavolt-Amperes  |

| Abbreviation | Explanation                                    |
|--------------|--|
| MW           | Megawatt                                       |
| NI           | Northern Ireland                               |
| NIEN         | Northern Ireland Electricity Networks          |
| NTC          | Net Transfer Capacity                          |
| PPB          | Power Procurement Business                     |
| PU           | Per Unit                                       |
| PST          | Phase Shifting Transformer                     |
| RES          | Renewable Energy Schemes                       |
| RIDP         | Renewable Integration Development Project      |
| RMS          | Root Mean Square                               |
| RP           | Review Period                                  |
| SEM          | Single Electricity Market                      |
| SONI         | System Operator for Northern Ireland           |
| SPS          | Special Protection Scheme                      |
| SVC          | Static Var Compensator                         |
| SP           | Summer Peak                                    |
| SS           | Substation                                     |
| SV           | Summer Valley                                  |
| TDP          | Transmission Development Plan                  |
| TDPNI        | Transmission Development Plan Northern Ireland |
| TYTFS        | Ten Year Transmission Forecast Statement       |
| TRM          | Transfer Reserve Margin                        |
| TSO          | Transmission System Operator                   |
| TTC          | Total Transfer Capacity                        |
| ТΧ           | Transformer                                    |
| WFPS         | Wind Farm Power Station                        |
| WP           | Winter Peak                                    |

# Terms

| Abbreviation                             | Explanation   |
|--|---|
| Active Power                             | The product of voltage and the in-phase component of alternating<br>current measured in Megawatts (MW). When compounded with the<br>flow of 'reactive power', measured in Megavolt-Amperes Reactive<br>(Mvar), the resultant is measured in Megavolt-Amperes (MVA).                       |
| Autumn Peak                              | This is the maximum Northern Ireland demand in the period September to October inclusive.   |
| Associated Transmission<br>Reinforcement | Associated Transmission Reinforcements (ATRs) are all of the transmission reinforcements that must be completed in order for a generator to be allocated FAQ. ATRs include reinforcements such as line and busbar upratings, new stations and new lines.                                  |
| Bulk Supply Point                        | A point at which the Northern Ireland transmission system is connected to the distribution system.  |
| Busbar                                   | The common connection point of two or more circuits.  |
| Capacitor                                | An item of plant normally utilised on the electrical network to supply reactive power to loads (generally locally) and thereby supporting the local area voltage.   |
| Circuit                                  | An element of the transmission system that carries electrical power.  |
| Combined Cycle Gas Turbine               | A collection of gas turbines and steam units; waste heat from the gas turbine(s) is passed through a heat recovery boiler to generate steam for the steam turbine(s).   |
| Combined Heat and Power                  | A plant designed to produce both heat and electrical power from a single heat source.   |
| Constraint                               | A transfer limit imposed by finite network capacity.  |
| Contingency                              | The unexpected failure or outage of a system component, such as<br>a generation unit, transmission line, transformer or other electrical<br>element. A contingency may also include multiple components,<br>which are related by situations leading to simultaneous<br>component outages. |
| Commission for Regulation of Utilities   | The Commission for Regulation of Utilities (CRU) is the regulator for the electricity, natural gas and public water sectors in Ireland.   |
| Data Freeze Date                         | The dates on which the Transmission Forecast Statement data<br>was effectively "frozen" for both EirGrid and SONI. Changes to<br>transmission system characteristics made after these dates do not<br>feature in the analyses carried out for this Transmission Forecast<br>Statement.    |
| Deep Reinforcement                       | Refers to transmission system reinforcement additional to the shallow connection that is required to allow a new generator or demand to operate at maximum capacity.  |
| Demand                                   | The peak demand figures in Table 3-1 in the introduction refer to<br>the power that must be transported from transmission system-<br>connected generation stations to meet all customers' electricity<br>requirements. These figures include transmission losses.                         |
| Demand-Side Management                   | The modification of normal demand patterns usually through the use of financial incentives.   |
| EirGrid                                  | EirGrid plc is the state-owned company established to take on<br>the role and responsibilities of Transmission System Operator in<br>Ireland as well as market operator of the wholesale trading system.  |

| Abbreviation                       | Explanation  |
|------------------------------------|--|
| EirGrid Interconnector DAC         | EIDAC is an organisation that is part of the EirGrid Group. EIDAC<br>owns the East West Interconnector linking the electricity grids<br>in Ireland and Wales. EIDAC sell capacity on the East West<br>Interconnector through auctions.   |
| Embedded Generation                | Refers to generation that is connected to the distribution system or at a customer's site.   |
| Firm Access Quantity               | The level of firm financial access available in the transmission<br>network for a generator is that generator's Firm Access Quantity or<br>'FAQ'. Firm financial access means that if a generator is constrained<br>on or off, it is eligible for compensation in the manner set out in<br>the Trading & Settlement Code.  |
| Gate 2                             | The term given to the group-processing scheme that applies to approximately 1,300 MW of renewable generation seeking connection to the transmission and distribution systems.  |
| Gate 3                             | The term given to the group-processing scheme that applies to approximately 10,000 MW of generation seeking connection to the transmission and distribution systems.   |
| Generation Dispatch                | The configuration of outputs from the connected generation units.  |
| Grid Code (EirGrid)                | The EirGrid Grid Code is designed to cover all material technical<br>aspects to the operation and use of the transmission system of<br>Ireland. The code was prepared by the TSO (pursuant to Section 33<br>of the Electricity Regulation Act, 1999) and approved by the CER.<br>The Grid Code is available on www.eirgrid.com.  |
| Grid Code (SONI)                   | The SONI Grid Code is designed to permit the development,<br>maintenance and operation of an efficient, co-ordinated and<br>economical transmission system in Northern Ireland. It is prepared<br>by the TSO (SONI) pursuant to condition 16 of SONI's Licence. The<br>SONI Grid Code is available at www.soni.ltd.uk.   |
| Interconnector<br>Administrator    | An Interconnector Administrator (IA) facilitates the allocation<br>of capacity and energy trading. Trading is carried out using an<br>Auction Management Platform (AMP) for the Moyle and East West<br>Interconnectors.  |
| Incremental Transfer<br>Capability | A measure of the transfer capability remaining in the physical transmission system for further commercial activity over and above anticipated uses.  |
| Interconnector                     | The tie line, facilities and equipment that connect the transmission system of one independently supplied transmission system to that of another.  |
| Loadflow                           | Study carried out to simulate the flow of power on the transmission system given a generation dispatch and system load.  |
| Maximum Continuous<br>Rating       | The maximum capacity (MVA) modified for ambient temperature conditions that the circuit can sustain indefinitely without degradation of equipment life.  |
|                                    | The MCR of a generator is the maximum capacity (MW) modified<br>for ambient temperature conditions that the generation unit can<br>sustain indefinitely without degradation of equipment life. All<br>generation capacity figures in this Transmission Forecast Statement<br>are maximum continuous ratings (defined as its MCR at 10°C),<br>expressed in exported terms i.e., generation unit output less the<br>unit's own load. |

| Maximum Export Capacity The maximum export value (MW) prov<br>generator's connection agreement. Th<br>which the generator chooses to cater<br>conditions that are not normally achie<br>CCGT plant can produce greater outpu   | ne MECs are contract values<br>for peaking under certain<br>evable or sustainable e.g., a<br>at at lower temperatures.<br>cuits meet. Node and station |
|--|--|
|  |  |
| Node Connecting point at which several circ<br>are used interchangeably in this Trans  | smission Forecast Statement.   |
| Parametric Analysis (P-V)A parametric study involves a series o<br>the changes in one set of power flow v<br>another in a systematic fashion. In thi<br>Statement the two variables are voltage  | variables with respect to<br>is Transmission Forecast  |
| Per Unit (pu.) Ratio of the actual electrical quantity to The base quantity used here for calculis 100 MVA.  |  |
| Phase Shifting Transformer An item of plant employed on the elec<br>flow of active power.  | ctrical network to control the   |
| Power Factor The power factor of a load is a ratio of to the reactive power requirement of t   | • •  |
| Reactive Compensation The process of supplying reactive pow  | ver to the network.  |
| ReactorAn item of plant employed on the elect<br>limit short circuit levels or prevent vol<br>installation and configuration.  |  |
| Shallow Connection Shallow Connection means the local of connect a customer to the Transmission the specific benefit of that particular of the specific benefit b | on System and which are for  |
| Single Electricity Market The Single Electricity Market (SEM) is market operating in Ireland and North information is available at www.semcommittee.com.   | ern Ireland. Further   |
| SONI System Operator for Northern Ireland<br>EirGrid plc. SONI ensures the safe, see<br>of the high-voltage electricity system i<br>cooperation with EirGrid is also respo<br>island wholesale market for electricity  | cure and economic operation<br>in Northern Ireland and in<br>nsible for running the all-   |
| Split BusbarRefers to the busbar(s) at a given sub-<br>electrically separated. Busbars are no<br>circuit levels or to maintain security of   | ormally split to limit short   |
| Static Var Compensator Device which provides fast and contin<br>inductive reactive power supply to the   | •  |
| Summer Valley This is the minimum system demand.<br>to September, inclusive in Ireland and<br>Northern Ireland.  |  |
| Summer Peak This is the maximum system demand<br>September, inclusive in Ireland and M<br>Northern Ireland.  |  |
| Tee ConnectionUn-switched connection into existing<br>stations.  | line between two other   |

| Abbreviation                      | Explanation   |
|-----------------------------------|---|
| Total Transfer Capability         | The total capacity available on cross-border circuits between<br>Ireland and Northern Ireland for all flows, including emergency<br>flows that occur after a contingency in either system.  |
| Transformer                       | An item of equipment connecting busbars at different nominal voltages. (see also Phase Shifting Transformer).   |
| Transmission Interface<br>Station | A station that is a point of connection between the transmission system and the distribution system or directly-connected customers.  |
| Transmission Losses               | A small proportion of energy is lost mainly as heat whilst<br>transporting electricity on the transmission system. These<br>are known as transmission losses. As the amount of energy<br>transmitted increases, losses also increase.   |
| Transmission Peak                 | The peak demand that is transported on the transmission system.<br>The transmission peak includes an estimate of transmission<br>losses.  |
| Transmission Planning<br>Criteria | The set of standards that the transmission system of Ireland is designed to meet.   |
| Transmission System               | The transmission system is a meshed network of high-voltage<br>lines and cables (400 kV, 275 kV, 220 kV and 110 kV) for the<br>transmission of bulk electricity supply around Ireland and<br>Northern Ireland. The transmission system and network are used<br>interchangeably in this Transmission Forecast Statement. |
| Uprating                          | To increase the rating of a circuit. This is achieved by increasing ground clearances and/or replacing conductor, together with any changes to terminal equipment and support structures.   |
| Utility Regulator (UR)            | UR is an independent non-ministerial government department set<br>up to ensure the effective regulation of the Electricity, Gas and<br>Water and Sewerage industries in Northern Ireland.   |
| Winter Peak                       | This is the maximum annual system demand. It occurs in the period October to February, inclusive in Ireland and in the Period November to February in Northern Ireland.   |

# **Executive Summary**

The All-Island Ten-Year Transmission Forecast Statement (TYTFS) 2020 provides the following information:

- Network models and data for the all-island transmission system;
- Forecast generation capacity and demand growth;
- Maximum and minimum fault levels at transmission system stations;
- Predicted transmission system power flows at different points in time; and
- Demand and generation opportunities on the transmission system.

TYTFS 2020 is prepared in accordance with the statutory regulations outlined in Table S-1.

# Table S-1: Statutory Regulations requiring the TSOs to produce a Transmission Forecast Statement

| Ireland   | Northern Ireland  |
|---|---|
| Section 38 of the Electricity Regulation Act 1999<br>(as amended) | Condition 33 of the Licence to participate in the Transmission of Electricity |

TYTFS 2020 describes the transmission system on the island of Ireland from 2020 to 2029. EirGrid and SONI have jointly prepared TYTFS 2020. This document supersedes the All-Island Ten-Year Transmission Forecast Statement 2019-2028.

This document presents information available for the all-island transmission system at the data freeze date of January 2020. Where applicable we provide information on transmission system projects under development. Where multiple solutions are presented for a transmission system project, no preference is given to one solution<sup>1</sup>.

In recent years there has been an increase in activity in the demand sector in Ireland. The demand forecast used in our analysis is the median all-island transmission peak demand forecast which is taken from the All-Island Generation Capacity Statement 2020-2029 (GCS)<sup>2</sup>. The demand forecast represents an average annual increase in all-island winter peak demand of 1.8% over the period of GCS 2020-2029<sup>3</sup>. This represented a decrease in the demand forecast relative to GCS 2019-2028, when the forecast average annual increase in all-island winter peak demand was 2.4%<sup>4</sup>.

This TYTFS shows that large energy users currently represent significant demand connections in Ireland and are expected to represent significant demand requirements into the future. New large energy users are expected to comprise data centres primarily. A large portion of these data centres are connected or plan to connect in the Dublin area. Depending on the level of demand connections, new large-scale generation, transmission solutions, demand side response and/or storage will be required to maintain security of supply in the area.

The system needs in the Dublin area are dynamic due to the connection of these new large-scale demand customers combined with potential changes in the connected generation portfolio.

<sup>1</sup> In line with our strategy to consider all practical technology options for network development.

<sup>2</sup> http://www.eirgridgroup.com/site-files/library/EirGrid/All-Island-Generation-Capacity-Statement-2020-2029.pdf

<sup>3</sup> The cumulative forecast increase in demand over the period of GCS 2020-2029 is 19.6%.

<sup>4</sup> The cumulative forecast increase in demand over the period of GCS 2019-2028 was 27%.

In response to this we have confirmed the need for investment in the greater Dublin area. We are progressing two projects: Kildare-Meath Grid Upgrade (also known as Capital Project 966) and CP1021 East Meath/North Dublin Network Reinforcement, which together help transfer power into and around the Dublin region. We are progressing these projects in line with our process for developing the grid which is outlined in our Have Your Say brochure. This is available on the EirGrid website<sup>5</sup>.

The generation portfolio assumed in this statement is based on connected generation and generation that had contracts in place, at the data freeze date, to connect to the transmission or distribution system.

In addition, in June 2019 the Irish Government launched its Climate Action Plan 2019<sup>6</sup>. The Action Plan sets out an ambitious course of action over the coming years. Specifically, it sets a target that 70% of electricity will come from renewable energy sources by 2030. It is important to note that the Climate Action Plan will be updated annually.

For Northern Ireland, the United Kingdom's Committee on Climate Change advised that it is necessary, feasible and cost-effective for the UK to set a target of net zero Green House Gas (GHG) emissions by 2050. The Climate Change Act 2008 (2050 Target Amendment) Order 2019 came into effect on the 27 June 2019. The revised legally binding target towards net zero emissions covers all sectors of the economy. This update to the Order demonstrates the UK's commitment to targeting a challenging ambition in line with the requirements of the Paris Agreement on climate change.

Energy Policy is a devolved matter for Northern Ireland and the Department for the Economy (DfE) is currently working with stakeholders to develop a Future Energy Strategy. This is likely to be published at the end of 2021. SONI is providing input to this important work, which will inform future renewable targets, and the approach to facilitating growth in renewable electricity generation. We are encouraged by the Economy Minister's aspiration for a renewable target of no less than 70% by 2030.

In order to meet Ireland's and Northern Ireland's commitments, investment will be needed in new renewable generation capacity and electricity networks. The transition to low-carbon and renewable energy will have widespread consequences; it will require a significant transformation of the electricity system.

In 2019 EirGrid and SONI launched new corporate Strategies 2020-2025 which are shaped by two factors: climate change and the impending transformation of the electricity sector. Together, EirGrid and SONI are committed to leading the change towards a carbon-free electricity system and achieving the renewable energy ambitions of both jurisdictions.

To realise these ambitions and the enabling transformation of the electricity system, we launched a public consultation on the future of the electricity system. We sought feedback on Shaping Our Electricity Future; a new report that details innovative approaches to developing the grid in order to meet the ambitious 2030 renewable energy targets. The report outlines the many network, operational and market requirements which need to be put in place by 2030. This work includes network development, technology and innovation, system operation and market development.

Extensive stakeholder engagement in relation to this work ran for a 14-week period beginning Monday 8 March 2021, including a formal consultation process.

It is important to note that the TYTFS is based on contracted customer connections and approved transmission reinforcements at the data freeze date. Therefore, future iterations of the TYTFS will take the outcome and progress of Shaping Our Electricity Future into account, including new customer connections and transmission reinforcements that are contracted and approved in the coming years.

<sup>5</sup> http://www.eirgridgroup.com/\_\_uuid/7d658280-91a2-4dbb-b438-ef005a857761/EirGrid-Have-Your-Say\_May-2017.pdf 6 https://www.gov.ie/en/publication/ccb2e0-the-climate-action-plan-2019/

TYTFS 2020 includes maximum and minimum short circuit current levels at transmission system stations. This information is given at each 110 kilovolt (kV), 220 kV, 275 kV and 400 kV transmission system station. Short circuit levels at each transmission system station are provided for the following years: 2020; 2023; and 2026.

Results show that several stations on the island are approaching, or have the potential to exceed, their rated short circuit current level. This can be seen in the maximum short circuit current level analysis, when there are high generation levels on the system. We manage the transmission system to mitigate possible risks while investment plans are in place to resolve these issues. Information on short circuit current levels is presented in Chapter 5.

Ireland and Northern Ireland are currently connected to Great Britain though the Moyle and East-West Interconnector (EWIC) high voltage direct current (HVDC) interconnectors. Interconnection with neighbouring countries offers many benefits, which include:

- Enhancing the security of supply of the transmission system;
- Facilitating the integration of variable renewable generation; and
- Facilitating greater competition and the potential for wholesale electricity prices to be reduced.

Our analyses include the Moyle and EWIC interconnectors. In addition, for the purpose of our analysis we assume the planned Greenlink Interconnector is in place in winter 2023. These interconnectors connect the all-island transmission system to the Great Britain transmission system. The connection application for the proposed Celtic Interconnector between Ireland and France is currently being processed. Once a signed connection agreement is in place it will be included in future forecast statements' analyses.

This document is based on an information freeze date of January 2020. At that time, it was considered that the North South Interconnector would be operational by 2023. Our analyses consequently assumed the planned North South Interconnector is in place in winter 2023. The reinforcement will increase security of supply, support the development of renewable power generation and provide economic benefits to customers in both jurisdictions. Since the data freeze, we have revised the likely energisation date for the North South Interconnector to 2025. This is due to delays in the receipt of planning approval in Northern Ireland and subsequent legal challenge. We will assume 2025 as the year for energisation of the North South Interconnector in our analyses for the next TYTFS.

TYTFS 2020 includes information on generation and demand opportunities for interested parties. This information is based on assessments and studies carried out on an all-island basis. The methodologies applied to the all-island opportunity analyses are presented in Chapter 6. Information on opportunities is presented in Chapter 7 and Chapter 8.

The all-island generation opportunities assessment in Chapter 7 provides information for generators wishing to connect to the transmission system. Generator opportunity is assessed at a number of 110 kV, 220 kV, 275 kV and 400 kV nodes across the all-island transmission system. The results show that there are opportunities for new generation of significant scale in the east of the island, in particular in the east of Northern Ireland and in north Dublin. The results also show that future generation connections in the North-West, West and South-West regions would require network reinforcements.

Regional changes in locational tariff signals are also described in Chapter 7. This information is provided to help network users make informed decisions when exploring potential transmission network connection locations. Regions with generation capacity in excess of local demand in the South West, West and North West of Ireland have lower Transmission Loss Adjustment Factors and higher Generator Transmission Use of System charges than Eastern regions with higher demand levels and less surplus generation.

The all-island demand opportunity results, based on the 2025 transmission system, are presented in Chapter 8. The study indicates that a significant number of stations across the island have the capability to accommodate demand connections, some to a lesser degree than others. The planned North South Interconnector improves generation adequacy across the island. It is also an important factor when considering the capacity of the system to connect significant amounts of additional demand in Ireland and Northern Ireland.

Chapter 8 also includes a qualitative assessment of the demand capability in the Dublin area. This assessment has been included as a result of the large volume of connections and enquires from data centres and other large energy users in the Dublin area.

It should be noted that, as mentioned above and in Chapter 4, a significant amount of conventional generation in Ireland and Northern Ireland is expected to close over the period covered by this statement. For the purpose of the TYTFS 2020 analysis, it is assumed that the Capacity Market, which is overseen by the SEM Committee, will deliver sufficient power in appropriate locations to ensure generation adequacy and security of supply are maintained. It is important to note that we are currently working with CRU and the Department of the Environment, Climate and Communications (DECC) to address short to medium term generation adequacy concerns in Ireland. Current analysis and projections for Northern Ireland indicate there is sufficient capacity in the short to medium term to meet system needs.

The results of demand and generation opportunity analyses are based on high level transmission network assessments. The results provide guidance, the actual connection capacity and possible connection solutions can only be determined following detailed individual connection studies. We will continue to examine innovative solutions and technologies in response to future connection enquiries.

Those who are considering connecting generation or demand to the transmission systems of Ireland or Northern Ireland should contact us. It is advisable to consult us early in the project process. In Ireland customers can contact us at info@eirgrid.com while in Northern Ireland customers can contact us at info@soni.ltd.uk.



# 1. Introduction





# 1. Introduction

The transmission system is a network of 400 kV, 275 kV, 220 kV and 110 kV high-voltage lines and cables. It is the backbone of the power system, efficiently delivering large amounts of power from where it is generated to where it is needed.

EirGrid is the Transmission System Operator (TSO) in Ireland, while SONI is the TSO in Northern Ireland. As TSOs, we jointly prepare and publish the All-Island Ten Year Transmission Forecast Statement (TYTFS) each year.

EirGrid plans and develops the transmission system in Ireland to ensure it meets forecast transmission system operating conditions. SONI is responsible for planning and operating the transmission system in Northern Ireland within defined security standards.

The TYTFS 2020 provides the following information:

- Network models and data of the all-island transmission system;
- Forecast generation capacity and demand growth;
- Maximum and minimum fault levels at transmission system stations;
- Predicted transmission system power flows at different points in time; and
- Demand and generation opportunities on the transmission system.

The TYTFS is designed to assist users and potential users of the transmission system to identify opportunities to connect to and make use of the transmission system. The appendices provide further information and transmission system data to enable the reader to perform power flow analysis.

When using data provided in the TYTFS 2020, readers should consider other documents we produce, or are involved in producing, including<sup>7</sup>:

- All-Island Generation Capacity Statement (GCS);
- Shaping Our Electricity Future consultation;
- EirGrid's Transmission Development Plan for Ireland;
- SONI's Transmission Development Plan for Northern Ireland;
- EirGrid's Tomorrow's Energy Scenarios for Ireland;
- SONI's Tomorrow's Energy Scenarios for Northern Ireland; and
- European Network of Transmission System Operators for Electricity's (ENTSO-E's) Ten Year Network Development Plan for Europe.

Each year EirGrid and SONI jointly prepare the All-Island Generation Capacity Statement. The GCS outlines demand forecasts and assesses the generation adequacy of the island of Ireland over the ten year period covered by the GCS. The TYTFS complements the demand information presented in the GCS.

Each year EirGrid and SONI publish Transmission Development Plans (TDP) for Ireland and Northern Ireland respectively. The TDPs are available on the EirGrid and SONI websites. The TDPs for Ireland and Northern Ireland provide details of the transmission system developments expected to be progressed in Ireland and Northern Ireland in the coming 10 years. These transmission system developments are also included in the data, assumptions and analyses in the TYTFS.

<sup>7</sup> Our publications are available at www.eirgridgroup.com and www.soni.ltd.uk. EirGrid Group All-Island Ten-Year Transmission Forecast Statement • 2020

To cater for the increased level of uncertainty over the future usage of the grid EirGrid and SONI have introduced scenario planning for Ireland and Northern Ireland respectively. We call our scenarios Tomorrow's Energy Scenarios (TES). These acknowledge that there is no single pathway to a low carbon future.

The European Network of Transmission System Operators for Electricity (ENTSO-E), of which EirGrid and SONI are members, publishes a Ten Year Network Development Plan (TYNDP) every two years. The TYNDP outlines projects of European significance.

# 1.1. Governing Arrangements

# 1.1.1. Roles and Responsibilities (Governance)

### **Northern Ireland**

Under our licence in Northern Ireland, held by SONI, we are required to plan<sup>8</sup> and operate the Northern Ireland transmission system.

In doing so we must comply with both the SONI Transmission System Security and Planning Standards (TSSPS) and the SONI Grid Code.

### Ireland

Under our licence in Ireland, held by EirGrid, we are required to operate, develop and ensure the maintenance of the Irish transmission system.

In doing so we must comply with both the EirGrid TSSPS and the EirGrid Grid Code.

# 1.1.2. Duty to Prepare a Statement

EirGrid and SONI are each required to publish a Transmission Forecast Statement in line with the Statutory Regulations in Table 1-1. Since 2012 we have jointly prepared and produced an allisland document, following an agreement with the Regulatory Authorities in Ireland<sup>9</sup> and Northern Ireland<sup>10</sup>.

# Table 1-1: Statutory Regulations requiring the TSOs to produce a Transmission Forecast Statement

| Ireland   | Northern Ireland                                  |
|---|---|
| Section 38 of the Electricity Regulation Act 1999 | Condition 33 of the Licence to participate in the |
| (as amended)                                      | Transmission of Electricity                       |

TYTFS 2020 has been prepared in accordance with and in fulfilment of these obligations. The format was approved by the Commission for Regulation of Utilities (CRU) and the Utility Regulator (UR).

9 The Commission for Regulation of Utilities is the Regulatory Authority in Ireland. 10 The Utility Regulator is the Regulatory Authority in Northern Ireland.

<sup>8</sup> Under the direction of the Utility Regulator (NI), investment planning functions are the responsibility of SONI as of May 2014 (ref: Commission Decisions 12.4.2013 pursuant to Article 3(1) of Regulation (EC) No 714/2009 and Article 10(6) of Directive 2009/72/EC – United Kingdom (Northern Ireland) – SONI / NIE).

# 1.1.3. Single Electricity Market

The Single Electricity Market (SEM) has been operating on the island of Ireland since 2007. The all-island wholesale electricity market allows consumers in both Ireland and Northern Ireland to benefit from increased competition. This in turn allows consumers to benefit from reduced energy costs and improved reliability of supply.

The model of the SEM changed considerably on 1 October 2018 to take account of the requirements of the European Network Codes<sup>11</sup> and the Target Model<sup>12</sup>. The project to develop and realise the new market was called the Integrated - Single Electricity Market (I-SEM). The market remains the Single Electricity Market (SEM<sup>13</sup>).

The transmission systems of Ireland and Northern Ireland are electrically connected by means of a 275 kV tie-line. This tie-line connects Louth station in Co. Louth (Ireland) to Tandragee station, in Co. Armagh (Northern Ireland).

There are also two 110 kV connections between Ireland and Northern Ireland:

- Letterkenny station in Co. Donegal (Ireland) and Strabane station in Co. Tyrone (Northern Ireland); and
- Corraclassy station in Co. Cavan (Ireland) and Enniskillen station in Co. Fermanagh (Northern Ireland).

Generation on the transmission systems of Ireland and Northern Ireland is dispatched on an all-island basis. The TYTFS transmission network models are also dispatched in this manner, to reflect how the all-island transmission system is operated.

# 1.2. Data Management

Transmission system development is continuously evolving. A data freeze date of January 2020 applies to TYTFS 2020. All data for system model files, and sequence data for use with short circuit current level analysis, was collected on this date. A data freeze date enables us to:

- Perform analyses;
- Update system models; and
- Update the appendices of TYTFS 2020.

# 1.3. Other Information

Potential users of the transmission system should also be aware of the following key documents:

- SONI Grid Code<sup>14</sup>;
- EirGrid Grid Code<sup>15</sup>;
- SONI Transmission System Security and Planning Standards<sup>16</sup>;
- The Electricity Safety, Quality and Continuity Regulations<sup>17</sup> (Northern Ireland) 2012;
- EirGrid Transmission System Security and Planning Standards<sup>18</sup>;

<sup>11</sup> https://www.entsoe.eu/major-projects/network-code-development/Pages/default.aspx

 $<sup>{\</sup>tt 12}\ {\tt https://www.entsoe.eu/about-entso-e/market/long-term-market-design/Pages/default.aspx}$ 

<sup>13</sup> Further information on the SEM is available on https://www.sem-o.com/

<sup>14</sup> http://www.soni.ltd.uk/customer-and-industry/general-customer-information/grid-code/

 $<sup>{\</sup>tt 15}\ {\tt http://www.eirgridgroup.com/customer-and-industry/general-customer-information/grid-code-info/index.xml}$ 

<sup>16</sup> http://www.soni.ltd.uk/media/Northern-Ireland-TSSPS-September-2015.pdf

<sup>17</sup> http://www.legislation.gov.uk/nisr/2012/381/pdfs/nisr\_20120381\_en.pdf

<sup>18</sup> http://www.eirgridgroup.com/site-files/library/EirGrid/EirGrid-Transmission-System-Security-and-Planning-Standards-TSSPS-Final-May-2016-APPROVED.pdf

- EirGrid Operating Security Standards<sup>19</sup>;
- SONI Transmission Connection Charging Methodology Statement<sup>20</sup>;
- EirGrid Transmission Connection Charging Methodology Statement 2008<sup>21</sup>;
- EirGrid Statement of Charges 2020/2021<sup>22</sup>;
- Statement of Charges For Use of Northern Ireland Electricity Ltd Transmission System<sup>23</sup>;
- EirGrid Transmission Loss Adjustment Factors 2021-2022<sup>24</sup>
- SONI Transmission Loss Adjustment Factors 2021-2022<sup>25</sup>
- All-Island Generation Capacity Statement 2020-2029<sup>26</sup>;
- EirGrid Transmission Development Plan for Ireland 2019-2028<sup>27</sup>;
- SONI Transmission Development Plan for Northern Ireland 2019-2028<sup>28</sup>; and
- SONI Transmission Development Plan for Northern Ireland 2020-2029<sup>29</sup>.

# 1.4. Publication

The TYTFS 2020 is available in pdf format on our websites:

- www.eirgridgroup.com; and
- www.soni.ltd.uk

For a hard-copy version, please send a request to info@eirgrid.com or info@soni.ltd.uk. Transmission system model files are also available on both websites.

21 http://www.eirgridgroup.com/site-files/library/EirGrid/Connection-Charging-Statement.pdf

<sup>19</sup> http://www.eirgridgroup.com/site-files/library/EirGrid/Operating-Security-Standards-December-2011.pdf

<sup>20</sup> http://www.soni.ltd.uk/media/SONI-Transmission-Connection-Charging-Methodology-Statement-Effective-1-Sept-2016-Approved-by-UR.pdf

<sup>22</sup> http://www.eirgridgroup.com/site-files/library/EirGrid/Statement-of-Charges-2020\_21-\_final.pdf

<sup>23</sup> http://www.soni.ltd.uk/customer-and-industry/general-customer-information/transmission-use-of-system-charges%20TUoS/?\_\_\_\_\_toolbar=1

<sup>24</sup> http://www.eirgridgroup.com/site-files/library/EirGrid/Approved-2021-2022-Transmission-Loss-Adjustment-Factors-(TLAFs)-Accompanying-Note-v1.o.pdf

<sup>25</sup> https://www.soni.ltd.uk/media/documents/Approved-2021-2022-Transmission-Loss-Adjustment-Factors-(TLAFs)-Accompanying-Note-v1.0.pdf

<sup>26</sup> https://www.eirgridgroup.com/site-files/library/EirGrid/All-Island-Generation-Capacity-Statement-2020-2029.pdf

<sup>27</sup> https://www.eirgridgroup.com/site-files/library/EirGrid/TDP-2019-2028-Final-For-Publication.pdf

<sup>28</sup> http://www.soni.ltd.uk/media/documents/SONI-TDPNI-2019-2028.pdf

<sup>29</sup> https://www.soni.ltd.uk/media/documents/SONI-Transmission-Development-Plan-Northern-Ireland-2020-2029.pdf

# 2. The Electricity Transmission System





# 2. The Electricity Transmission System

# 2.1. Overview of the All-Island Electricity Transmission System

The transmission system in Ireland and Northern Ireland plays a vital role in the supply of electricity. It provides the means to transport energy from generators to demand centres across the island.

The transmission system in Northern Ireland is operated at 275 kV and 110 kV. The transmission system in Ireland is operated at 400 kV, 220 kV and 110 kV. The two transmission systems are connected by means of a 275 kV double circuit from Louth station in Co. Louth (Ireland/IE) to Tandragee station in Co. Armagh (Northern Ireland/NI). There are also two 110 kV connections:

- Letterkenny station in Co. Donegal (IE) to Strabane station in Co. Tyrone (NI); and
- Corraclassy station in Co. Cavan (IE) to Enniskillen station in Co. Fermanagh (NI).

See Section 2.2 below for further information on the existing transmission connections between Ireland and Northern Ireland.

EirGrid and SONI together operate the transmission systems - North and South - on an all-island basis.

The 400 kV, 275 kV and 220 kV networks form the backbone of the transmission system. They have higher power carrying capacity and lower losses than the 110 kV network.

In Ireland, the 400 kV network provides a high capacity link between the Moneypoint generation station on the west coast and Dublin on the east. We are planning a new 400 kV interconnector between Ireland and Northern Ireland called the North South Interconnector.

In Northern Ireland the 275 kV network is comprised of:

- A double circuit ring;
- A double circuit spur to Coolkeeragh Power Station; and
- A double circuit spur southwards into Co. Louth, in Ireland.

In Ireland the transmission network is comprised of single circuit lines which are interconnected to cover the wider geographical distances between stations. Typically large generation stations (greater than 200 MW) are connected to the 220 kV or 400 kV networks.

The 110 kV<sup>30</sup> circuits provide parallel paths to the 220 kV, 275 kV and 400 kV networks and are the most extensive element of the all-island transmission system, reaching into every county on the island of Ireland.

The all-island transmission system is generally comprised of overhead lines. There are exceptions to this, such as in the city centres of Belfast, Cork and Dublin, where underground cables are used. Table 2-1 presents the total lengths of overhead lines<sup>31</sup> and cables at the different voltage levels. Revision of individual line lengths may change following completion of network development projects.

30 A number of radial 110 kV circuits in Ireland and the 110 kV lines and cables within Dublin City are operated by the Distribution System Operator (DSO). The DSO licence is held by ESB Networks. Details of the distribution network in Dublin are not included in this All-Island Ten Year Transmission Forecast Statement. 31 Some lines may contain short sections of cable.

# Table 2-1: Total Length of Existing Transmission System Circuitsas at the Data Collection Freeze Date (January 2020)

| Voltage Level (kV) | Total Circuit Lengths (km) |  |
|--------------------|----------------------------|--|
| 400                | 439                        |  |
| 275                | 825                        |  |
| 220                | 1,966                      |  |
| 110                | 6,777                      |  |

Transformers are located at substations that link the different voltage networks together, providing paths for power flow between voltage levels. The total transformer capacity between the different voltage levels on the all-island system is presented in Table 2-2.

# Table 2-2: Total Transmission System Transformer MVA Capacityas at the Data Collection Freeze Date32 (January 2020)

| Voltage Levels (kV) | Capacity (MVA) | Number of transformers |
|---------------------|----------------|------------------------|
| 400/220             | 4,050          | 8                      |
| 275/220             | 1,200          | 3                      |
| 275/110             | 4,080          | 17                     |
| 220/110             | 13,799         | 66                     |
| 110/3333            | 5,740          | 79                     |

Reactive compensation devices are used to improve transmission system voltages in local areas. Existing reactive compensation devices connected to the transmission system include shunt capacitors, static var compensators (SVCs) and shunt reactors.

Capacitors and SVCs help to support local voltages in areas where low voltages may otherwise occur. Shunt reactors suppress voltages in areas where they would otherwise be too high, most likely during periods of low demand and/or high wind. Table 2-3 displays the reactive compensation on the all-island transmission system.

| Voltage Level<br>(kV) | Туре                                    | Capacity<br>(Mvar) | Number of Devices |
|-----------------------|---|--------------------|-------------------|
| (                     | Line Shunt Reactor                      | 160                | 2                 |
| 400                   | Voltage Source Converter Interconnector | +/- 175            | 1                 |
| 275                   | Shunt Capacitor                         | 236                | 4                 |
| 220                   | Shunt Reactor                           | 200                | 3                 |
| 110                   | Static Var Compensator                  | 90                 | 2                 |
|                       | Shunt Capacitor                         | 961                | 44                |
| 38                    | Shunt Reactor                           | 100                | 5                 |
| 33                    | Shunt Capacitor                         | 29                 | 5                 |
|                       | Shunt Reactor                           | 210                | 7                 |
| 22                    | Shunt Capacitor                         | 125                | 5                 |
| 20                    | Shunt Capacitor                         | 92                 | 14                |
|                       | Shunt Reactor                           | 9                  | 1                 |

Table 2-3: Total Reactive Compensation<sup>34</sup> as at the Data Collection Freeze Date (January 2020)

 $_{\rm 32}$  Transformer details are provided in Tables B-4 and B-5 in Appendix B.

33 In Northern Ireland, 110/33 kV transformers are formally part of the transmission system. In Ireland, 110/38 kV transformers are part of the distribution system.

34 Details of existing reactive compensation devices are provided in Table B-6 in Appendix B. This table also includes reactive compensation devices at lower voltage levels that are modelled in the TYTFS studies.

# 2.2. Existing Connections between Ireland and Northern Ireland Transmission Systems

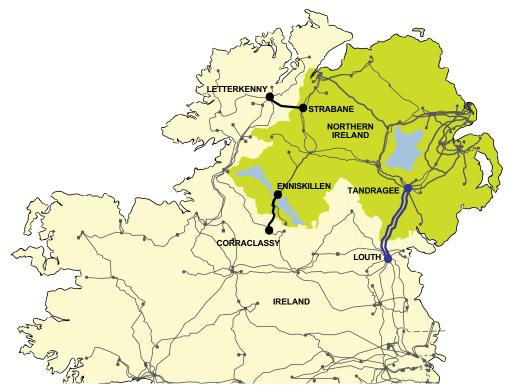


Figure 2-1: Existing Cross-Border Circuits

As illustrated in Figure 2-1, the transmission systems of Ireland and Northern Ireland are connected via a double circuit 275 kV line. This line connects the Northern Irish transmission system at Tandragee to the Irish transmission system in Louth. There are three 275/220 kV transformers in Louth station, one 600 MVA unit and two ganged<sup>35</sup> 300 MVA units.

The design capacity of each of the 275/220 kV cross-border circuits is 600 MVA. However, the actual capacity of the circuits to accommodate transfers between the two systems at any time depends on the prevailing system conditions on either side of the border. This includes the ability to deal with system separation.

In addition to the main 275/220 kV double circuit, there are two 110 kV connections:

- One between Letterkenny, Co. Donegal and Strabane, Co. Tyrone; and
- One between Corraclassy, Co. Cavan and Enniskillen, Co. Fermanagh.

The purpose of these 110 kV circuits is to provide support to either system in certain system conditions. Phase shifting transformers (PSTs) in Strabane and Enniskillen are used to control the power flow under normal conditions.

<sup>35</sup> Plant connected in parallel through common switchgear.

# 2.3. Interconnection with Great Britain and Europe

Transmission grids are often interconnected so that energy can flow from one country to another. By linking to other transmission systems, we can:

- Increase the diversity and security of energy supplies;
- Facilitate competition in the European market; and
- Aid the transition to a low carbon energy sector by integrating renewable sources.

This helps provide a safe, secure, reliable and affordable energy supply for everybody.

The East West Interconnector links the electricity grids in Ireland and Wales, while the Moyle Interconnector links the electricity grids in Northern Ireland and Scotland. Further interconnectors are planned, see Section 2.3.3 Future European Interconnection.

Power can be either imported or exported on the interconnectors. Interconnector power flows have system impacts that need to be managed operationally. For example, during times of import conventional generation is displaced by these non-synchronous power sources. This reduces the all-island system inertia<sup>36</sup>. Interconnector flows can also have implications for the system frequency and transmission system stability and operation. Frequency changes are faster in transmission systems with low rotational inertia, making frequency control and system operation more challenging.

The Moyle Interconnector also increases the dynamic reactive support required by the transmission system as the link does not have dynamic reactive power export capability<sup>37</sup>.

SONI acts as Interconnector Administrator (IA) for the East West and Moyle interconnectors<sup>38</sup>.

Interconnector capacity is auctioned by the IA on behalf of EirGrid Interconnector DAC (EIDAC)<sup>39</sup> and Moyle Interconnector Limited (MIL)<sup>40</sup>. The capacity is purchased by market participants and utilised in the wholesale electricity markets on the islands of Ireland and Great Britain. Figure 2-2 shows the location of the Moyle Interconnector and EirGrid East-West Interconnector.

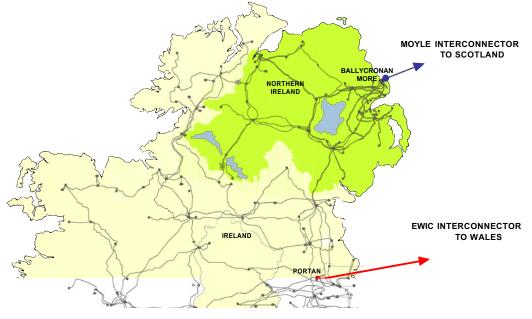


Figure 2-2: Existing Interconnectors

<sup>36</sup> System inertia is also reduced by the increased wind penetration (another form of non-synchronous generation).

<sup>37</sup> Unlike Moyle the East West Interconnector has dynamic reactive power export capability.

<sup>38</sup> http://www.soni.ltd.uk/customer-and-industry/interconnection/

<sup>39</sup> http://www.eirgridgroup.com/customer-and-industry/interconnection/

<sup>40</sup> http://www.mutual-energy.com/electricity-business/

The amount of power that is permitted to be traded between Ireland and Wales across the East-West Interconnector is detailed in Table 2-4.

The available capacity is measured at the SEM and BETTA market reference point in Deeside 400 kV station in Wales.

| Direction        | Summer (MW) | Winter (MW) |
|------------------|-------------|-------------|
| Wales to Ireland | 500         | 500         |
| Ireland to Wales | 500         | 500         |

### Table 2-4: Contracted Capacity on EWIC Interconnector

The amount of power that can be traded between Northern Ireland and Scotland across the Moyle Interconnector is detailed in Table 2-5.

| Direction              | Dates                                | Firm capacity<br>available<br>(MW) | Additional<br>Capacity<br>Potentially<br>Available (MW)42 | Potential Total<br>Capacity Available<br>(MW) |
|------------------------|--------------------------------------|------------------------------------|---|---|
| Northern               | 1 December 2020 – 31<br>October 2021 | 250                                | 150   | 400   |
| Ireland to<br>Scotland | 1 November 2021 – 31<br>March 2022   | 160                                | 240   | 400   |
|                        | 1 April 2022 onwards                 | 400 <sup>43</sup>                  | 0   | 400   |
| Scotland to            | 1 April – 31 October                 | 410 <sup>44</sup>                  | 40  | 450   |
| Northern<br>Ireland    | 1 November – 31 March                | 450                                | 0   | 450   |

# Table 2-5: Capacity on Moyle Interconnector<sup>41</sup>

# 2.3.1. Moyle Interconnector

The Northern Ireland transmission system is currently connected to Scotland via a 500 MW High Voltage Direct Current (HVDC) link, the Moyle Interconnector. It is a Line Commutated Converter (LCC) HVDC link, which commenced full commercial operation in 2002.

It is constructed as a dual monopole HVDC link with two coaxial sub-sea cables from Ballycronan More in Islandmagee, Northern Ireland to Auchencrosh in Ayrshire, Scotland. The link has a physical installed capacity of 500 MW. The link has the capacity to provide reserve of up to 75 MW should the frequency on the island drop below 49.4 Hz.

The converter station at Ballycronan More is looped into one of the 275 kV Ballylumford to Hannahstown circuits. The Moyle link is self-compensating for reactive power losses. There are 4 x 59 Mvar capacitor banks at the Ballycronan More converter station with three of these capacitor banks acting as filters.

Where there are faults on the transmission system, effects are limited to a brief distortion of the HVDC 50 Hz AC synchronous waveform in import mode. The rapid response means that the HVDC link can have a net stabilising effect on the transmission system in the event of generation loss.

<sup>41</sup> http://www.mutual-energy.com/trading-across-the-moyle-interconnector-isem/

<sup>42</sup> This capacity is assessed day-ahead by National Grid based on flows in Scotland.

<sup>43</sup> Maximum Northern Ireland to Scotland flows are limited by constraints on the Northern Ireland network.

<sup>44</sup> May be reduced from 450 MW to 410 MW under certain system outage conditions.

# 2.3.2. East-West Interconnector

The East-West Interconnector is a 500 MW HVDC link which runs between Woodland, County Meath in Ireland and Deeside in North Wales. The link comprises approximately 186 km of sub-sea cable and 76 km of land underground cable.

The East-West Interconnector uses Voltage Source Converter (VSC) technology. VSC technology offers independent and rapid control of active and reactive power. It does not suffer from commutation failures, and is capable of offering emergency power control in the event of low or high frequency events.

In addition, due to the VSC technology, the East-West Interconnector provides black start capability. The link can operate in either voltage control or reactive power control mode independently in both converter stations. It can supply or absorb up to 175 Mvar at Portan 400 kV station which is connected directly to Woodland 400 kV station. The East-West Interconnector commenced commercial operation in December 2012.

# 2.3.3. Future European Interconnection

Currently, there are two proposed interconnectors that are deemed Projects of Common Interest (PCIs) by the European Commission. PCIs are intended to help the EU achieve its energy policy and climate objectives: affordable, secure and sustainable energy for all citizens. At the TYTFS data freeze date the planned Greenlink Interconnector, connecting Great Island in Co. Wexford to Pembrokeshire in Wales, was expected to be completed in winter 2023. The connection application for the proposed Celtic Interconnector between Ireland and France is currently being processed. Once a signed connection agreement is in place it will be included in future forecast statements' analyses.

In Northern Ireland there is potential for new interconnection (LirIC) to Scotland, with one potential operator receiving an interconnector license from Ofgem. This would provide an additional connection between Northern Ireland and Scotland. SONI have not yet received a connection application for this interconnector, and any future developments will be reflected in future versions of TYTFS.

# 2.4. Transmission Development Plans

EirGrid's Transmission Development Plan (TDP)<sup>45</sup> and SONI's Transmission Development Plan Northern Ireland (TDPNI)<sup>46</sup> detail the transmission system development projects that have been initiated by EirGrid and SONI respectively. They also discuss further developments that may arise in the period of the plans. The TDP and TDPNI describe projects that are required to:

- Facilitate demand growth;
- Provide new generation and demand connections<sup>47</sup>;
- Ensure the transmission system is in compliance with the EirGrid Transmission System Security and Planning Standards (TSSPS) and SONI TSSPS;
- Provide interconnection capacity; and
- Refurbish or replace existing assets.

The planned transmission system developments presented in this statement are based on those projects that have received internal approval by the data freeze date<sup>48</sup>. Appendix B outlines these developments. These projects are currently scheduled to be completed at various stages

<sup>45</sup> The latest TDP can be found on the EirGrid website http://www.eirgridgroup.com/how-the-grid-works/tso-regulatory-publicatio/ 46 The latest TDPNI can be found on the SONI website http://www.soni.ltd.uk/the-grid/projects/tdpni/the-project/ 47 For example data centres or large industrial sites.

<sup>48 01</sup> January 2020

between now and 2029. It should be noted that the information presented in later chapters on transmission system transfer capabilities and opportunities is dependent on the completion of these development projects in the assumed timeframe.

Information presented in the TDP, TDPNI and TYTFS documents represent a snapshot of an evolving transmission system development plan. While we are considering other reinforcements, these are not at the stage of maturity required for inclusion in this statement.

The Transmission Development Plans include details of major transmission system developments planned for the transmission system of Ireland and Northern Ireland. Each planned development is illustrated in the maps and schematics in Appendix A. New generation connections and new transmission interface stations are described in Sections 2.8 and 2.9 respectively.

# 2.5. Ireland Transmission System Developments

This section details the transmission system projects that are planned to take place in Ireland over the period covered by this forecast statement. Project completion dates in the TYTFS are forecasts based on the best project information available at the time of the data freeze date (January 2020).

# 2.5.1. Grid Development Strategy

EirGrid published the updated Grid Development Strategy (GDS) "Your Grid, Your Tomorrow<sup>49</sup>" in 2017. The GDS documents our strategy for the long-term development of the network and includes three strategy statements:

- Inclusive consultation with local communities and stakeholders will be central to our approach;
- We will consider all practical technology options; and
- We will optimise the existing grid to minimise the need for new infrastructure.

The GDS aims to achieve a balance between the costs and impact of new infrastructure, while maximising the capability of the existing network.

# 2.5.2. Our Public Consultation Process

Our approach to developing the grid and how the public can engage with us at each stage of project development is outlined in our Have Your Say<sup>50</sup> brochure.

Our approach comprises a six-step process that provides an "end-to-end" structure for all our grid projects. It ensures an appropriate balance between technical, economic, environmental, social and community considerations, with significant provision for stakeholder engagement at all stages. A general structure of the process is set out in Figure 2-3 below.



Figure 2-3: General structure of the six-step process for our grid projects

<sup>49</sup> http://www.eirgridgroup.com/the-grid/irelands-strategy/

<sup>50</sup> http://www.eirgridgroup.com/site-files/library/EirGrid/EirGrid-Have-Your-Say\_May-2017.pdf

# 2.5.3. Tomorrow's Energy Scenarios

In 2017, to cater for the increased level of uncertainty over the future usage of the grid, we introduced scenario planning into our grid development process. We call our scenarios Tomorrow's Energy Scenarios<sup>51</sup> (TES).

Our scenarios detail credible futures for the electricity sector in Ireland, with specific focus on what this means for the electricity transmission system over the next twenty years and beyond. The underlying assumptions in the scenarios are validated using feedback received from policy makers, industry and the general public as part of an open consultation.

When the scenarios are finalised, we use them to test the performance of the electricity transmission grid and publish the results in the TES System Needs Assessment (SNA)<sup>52</sup>. The TES process occurs every two years.

The needs identified in the TES process are brought through our six-step process for developing the grid. As needs and projects progress through the six-step process they are included in the TDP and TYTFS.

# 2.5.4. Descriptions of Ireland Development Projects

### Aghada 220 kV Redevelopment

The 220 kV busbar in Aghada 220 kV station will be reconfigured from the existing double busbar into a 'C' configuration. The 110 kV busbar will also be uprated. The project will increase security of supply, increase operational flexibility and improve maintainability of station equipment. At the TYTFS data freeze date this project was expected to be completed in 2021.

### **Ballynahulla Station STATCOM**

A new ±100 Mvar STATCOM will be installed and commissioned on the 110 kV busbar at Ballynahulla. At the TYTFS data freeze date this project was expected to be completed in 2022.

### **Ballyvouskill Temporary Shunt Reactor**

A 50 Mvar shunt reactor will be installed temporarily at Ballyvouskill 220 kV station to address existing voltage support needs before construction of the STATCOM at this site. At the TYTFS data freeze date this project was expected to be completed in 2020.

# **Ballyvouskill Station STATCOM**

A new ±100 Mvar STATCOM will be installed and commissioned on the 110 kV busbar at Ballyvouskill. At the TYTFS data freeze date this project was expected to be completed in 2022.

### Belcamp Phase 1 220 kV Development<sup>53</sup>

Belcamp 220 kV station, in north Co. Dublin, will be connected to the 220 kV network by an underground cable from Finglas in order to facilitate new demand connections to the system in the North East Dublin area. At the TYTFS data freeze date this project was expected to be completed in 2020.

http://www.eirgridgroup.com/customer-and-industry/energy-future/

52 TES 2017 System Needs Assessment Report:

<sup>51</sup> The latest Tomorrow's Energy Scenarios information is available at the following link:

http://www.eirgridgroup.com/site-files/library/EirGrid/TES-2017-System-Needs-Assessment-Final.pdf TES 2019 System Needs Assessment Report:

http://www.eirgridgroup.com/site-files/library/EirGrid/EirGrid-TES-2019-System-Needs-Assessment-Report\_Final.pdf 53 http://www.eirgridgroup.com/the-grid/projects/dublin-north-fringe/the-project/

## Belcamp Phase 2 220/110 kV Development

A 220 kV cable will connect Shellybanks station to Belcamp station, by utilising the existing Finglas - Shellybanks and Dardistown - Finglas cables, and continuing the cable connection to Belcamp. This will lead to a revision in the feeding arrangements of the underlying Finglas and Belcamp 110 kV network. At the TYTFS data freeze date this project was expected to be completed in 2022.

## Bracklone 110 kV Station

A new 110 kV substation will be constructed near Portarlington. It will be looped into the existing Newbridge – Portlaoise 110 kV circuit. It will facilitate more demand in the area and also improve security of supply. At the TYTFS data freeze date this project was expected to be completed in 2023.

### Carrickmines 220/110 kV Redevelopment

This project involves installation of a fourth 220/110 kV transformer at Carrickmines 220 kV station as well as upgrading to Gas Insulated Switchgear (GIS) and reconfiguration of the existing busbar. At the TYTFS data freeze date this project was expected to be completed in 2020.

### Castlebagot 220/110 kV Development

Castlebagot 220/110 kV station<sup>54</sup>, in west Co. Dublin, will be connected into the existing Inchicore-Maynooth No. 1 and No. 2 220 kV lines. A number of the existing 110 kV circuits in the area will be connected to the new Castlebagot station. This development will offload demand from Inchicore 220 kV station. It will also ensure compliance with the distribution system planning standards as new demand connects to the system in the West Dublin area. At the TYTFS data freeze date this project was expected to be completed in 2020.

## Castlebar 110 kV Busbar Uprate

The busbar at Castlebar will be uprated to accommodate increased power flows arising from an increase in wind generation in the area. At the TYTFS data freeze date this project was expected to be completed in 2021.

# Clashavoon – Dunmanway 110 kV Circuit

A new 110 kV circuit will be constructed between Clashavoon and Dunmanway substations to improve security of supply and accommodate increased power flows arising from an increase in wind generation. At the TYTFS data freeze date this project was expected to be completed in 2020.

# Clashavoon – Macroom Second 110 kV Circuit

A new 110 kV circuit will be constructed between Clashavoon and Macroom substations. The existing 220/110 kV transformer at Clashavoon substation will be replaced with one of higher capacity. At the TYTFS data freeze date this project was expected to be completed in 2020.

# Clashavoon – Tarbert 220 kV Uprate

This 220 kV circuit is being uprated to accommodate increased power flows arising from an increase in wind generation. The uprated circuit will enable the export of wind power out of the southwest. Following the connection of four 220 kV stations, the original Clashavoon – Tarbert 220 kV circuit became five circuits: Tarbert – Kilpaddoge, Kilpaddoge – Knockanure, Knockanure – Ballynahulla, Ballynahulla – Ballyvouskil, and Ballyvouskil – Clashavoon. At the TYTFS data freeze date this project was expected to be completed in 2021.

<sup>54</sup> Formerly known as West Dublin 220/110 kV station.

## Coolnabacky – Portlaoise 110 kV Uprate

The 110 kV circuit between Coolnabacky and Portlaoise will be uprated due to higher power flows arising once the Coolnabacky 400/110 kV station has been looped into the existing Athy – Portlaoise 110 kV circuit. The higher flows occur during high renewable generation in the south west which flows towards the east. At the TYTFS data freeze date this project was expected to be completed in 2023.

### Corderry – Srananagh 110 kV Uprate

The 110 kV circuit between Corderry and Srananagh will be uprated to accommodate increased wind generation in the northwest. At the TYTFS data freeze date this project was expected to be completed in 2020.

### Corduff – Ryebrook 110 kV Uprate

The 110 kV circuit between Corduff and Ryebrook will be uprated due to increases in demand and an increase in flows on the overlying 220 kV network. At the TYTFS data freeze date this project was expected to be completed in 2020.

### Finglas 220 kV and 110 kV Redevelopment

The 220 kV and 110 kV busbars in the existing Finglas 220 kV station will be reconfigured and redeveloped into a ring busbar arrangement. This project will address the following issues: ability to accommodate future load growth; security of supply to north Dublin; asset condition of existing equipment; inadequate circuit breaker ratings and the need to upgrade the protection systems. The project will also increase operational flexibility and improve maintainability of station equipment. At the TYTFS data freeze date this project was expected to be completed in 2023.

### Galway 110 kV Station Redevelopment

The existing Galway 110 kV station will be replaced with a GIS station in order to accommodate increased power flows due to an increase in wind generation. The project will also increase operational flexibility and improve maintainability of station equipment. At the TYTFS data freeze date this project was expected to be completed in 2023.

### **Greenlink Interconnector**

The Greenlink Interconnector, connecting Great Island in Co. Wexford to Pembrokeshire in Wales, will have an import and export capacity of 500 MW. The project to facilitate the connection of the interconnector to the transmission system will consist of the construction of a new 220 kV GIS station 'Loughtown'. Loughtown will connect to Great Island 220 kV GIS station via approximately 400m of underground cable. At the TYTFS data freeze date this project was expected to be completed in 2023.

### Inchicore 220 kV Redevelopment

The oldest section of the existing Inchicore 220 kV station, in Co. Dublin will be replaced with a new GIS compound. This project will address issues with the condition of existing equipment, inadequate circuit breaker ratings, and the need to upgrade the protection systems. The new GIS compound will increase operational flexibility, improve maintainability of station equipment and allow for future 220 kV expansion. At the TYTFS data freeze date this project was expected to be completed in 2025.

## Kildare-Meath Grid Upgrade (Capital Project 966)

This project will involve reinforcement of the network between Dunstown and Woodland 400 kV stations.

We are progressing this project in line with our six-step process for our grid projects. The sixstep process is introduced above and outlined in our Have Your Say<sup>55</sup> brochure. In spring 2021 the project completed Step 3 and moved into Step 4. For the most up to date information on the project please visit the project page on the EirGrid website<sup>56</sup>.

## New 110 kV Station close to Kilbarry 110 kV Station

A new 110 kV substation will be constructed adjacent to the existing station. This will facilitate more demand in the area and also improve security of supply. Some of the existing circuits connecting into the existing Kilbarry 110 kV station will be transferred into the new station. At the TYTFS data freeze date this project was expected to be completed in 2023.

## Killonan 220/110 kV Redevelopment

The existing Killonan 220/110 kV station, in Co. Limerick will be replaced with a new GIS compound. This project will address issues with the condition of existing equipment, inadequate circuit breaker ratings, and the need to upgrade the protection systems as well as to accommodate increased power flows. The new GIS compound will increase operational flexibility and improve maintainability of station equipment. At the TYTFS data freeze date this project was expected to be completed in 2027.

## **Knockanure Station Reactor**

A new 50 Mvar reactor will be installed on the 220 kV busbar at Knockanure. At the TYTFS data freeze date this project was expected to be completed in 2020.

## Knockraha 220 kV Reconfiguration

The 220 kV busbar in Knockraha 220 kV station will be reconfigured from the existing double busbar configuration to a ring busbar arrangement. The third Knockraha 220/110 kV transformer will be decommissioned resulting in the station having two 220/110 kV transformers. The project will resolve issues regarding security of supply, operational flexibility and improve maintainability of station equipment. At the TYTFS data freeze date this project was expected to be completed in 2021.

## Lanesboro 110 kV Station Redevelopment

The existing Lanesboro 110 kV station will be replaced with a GIS station in order to accommodate increased power flows due to an increase in wind generation in the north-west. The project will also increase operational flexibility and improve maintainability of station equipment. At the TYTFS data freeze date this project was expected to be completed in 2024.

## Laois-Kilkenny Reinforcement Project<sup>57</sup>

This project involves a new 400/110 kV station at Coolnabacky near Portlaoise, Co. Laois, with an associated 110 kV circuit to Kilkenny 110 kV station via a new 110/38 kV station at Ballyragget. The 400/110 kV station will be looped into the existing Dunstown-Moneypoint 400 kV line and the existing Athy-Portlaoise 110 kV line. The proposed infrastructure will improve quality of supply to the south-east and midlands. It will also increase capacity in the region. At the TYTFS data freeze date this project was expected to be completed in 2023.

<sup>55</sup> http://www.eirgridgroup.com/the-grid/have-your-say/

<sup>56</sup> http://www.eirgridgroup.com/the-grid/projects/capital-project-966/the-project/

<sup>57</sup> http://www.eirgridgroup.com/the-grid/projects/laois-kilkenny/the-project/

## **Louth Station Redevelopment**

Louth station comprises three voltage levels, 275 kV, 220 kV and 110 kV. The station will undergo a major refurbishment of assets at all three voltage levels. The 110 kV busbar will be reconfigured from the existing double busbar configuration to ring busbar arrangement. At the TYTFS data freeze date this project was expected to be completed in 2023.

## **Maynooth Station Redevelopment**

This project involves refurbishment and reconfiguration of the entire 220 kV and 110 kV busbars, and an increase in the short circuit rating of both busbars. Series reactors will be incorporated to manage short circuit levels within limits. At the TYTFS data freeze date this project was expected to be completed in 2027.

## Maynooth – Woodland 220 kV Refurbishment and Uprate

The 220 kV circuit between Maynooth and Woodland will be refurbished and uprated to facilitate increased power flows arising from an increase in demand. At the TYTFS data freeze date this project was expected to be completed in 2022.

## Moneypoint – Kilpaddoge – Knockanure 220 kV Development

There is a planned new 220 kV cable from Moneypoint in Co. Clare to Knockanure in north Co. Kerry, via Kilpaddoge also in north Co. Kerry. This will create a new path for power out of the South West to the existing 400 kV network. The project comprises a 220 kV submarine cable under the Shannon between Moneypoint and Kilpaddoge and a 21 km 220 kV land cable between Kilpaddoge and Knockanure. The submarine cable has been completed. At the TYTFS data freeze date the land cable part of the project was expected to be completed in 2020.

## **Moneypoint Station Redevelopment**

The entire Moneypoint 400/220/110 kV station will be replaced with a new GIS station including two 400/220 kV transformers and one 220/110 kV transformer. This project is required to address voltage issues, replace ageing assets, and increase transmission capacity in the area. At the TYTFS data freeze date this project was expected to be completed in 2020.

## Moy 110 kV Busbar Uprate

The 110 kV busbar in Moy station will be reconfigured and uprated to accommodate power flows arising due to increases in wind generation in Co. Mayo and also to facilitate refurbishment of key components. At the TYTFS data freeze date this project was expected to be completed in 2020.

## Mount Lucas – Thornsberry New 110 kV Circuit

A new 110 kV circuit will be constructed between Mount Lucas and Thornsberry stations to improve security of supply. At the TYTFS data freeze date this project was expected to be completed in 2020.

## North Connacht 110 kV Reinforcement

This project includes a new 110 kV circuit from Moy station in Co. Mayo to Tonroe station in Co. Roscommon. The new circuit will facilitate the connection of renewable generation in Co. Mayo. For the most up to date information on the project please visit the project website on the EirGrid website<sup>58</sup>. At the TYTFS data freeze date this project was expected to be completed in 2024.

<sup>58</sup> http://www.eirgridgroup.com/the-grid/projects/north-connacht/the-project/

## **North-West Project**

The cross-border Renewable Integration Development Project (RIDP)<sup>59</sup> identified that the existing network in the north west of the island is insufficient to accommodate the future wind generation in the area. The North-West project is one element of the original RIDP solution. We are reviewing the need, solutions, technology and timing of this work in line with our six-step process for developing the grid.

Should the North-West Project progress, an investigation of overhead and underground options utilising various technologies will be undertaken.

## **Regional Solution**

The Regional Solution is made up of a number of projects, with the objective of improving security of supply in the south-east and facilitating connection of generation in the south-west.

## (i) Cross-Shannon 400 kV Cable

A 400 kV cable crossing the Shannon estuary will be installed between Kilpaddoge and Moneypoint stations. The cable length is estimated at approximately 6 km consisting of approximately 3 km land cable and approximately 3 km submarine cable. A new 400/220 kV 500 MVA transformer will also be required at Kilpaddoge station. At the TYTFS data freeze date this project was expected to be completed in 2022.

## (ii) Great Island – Kilkenny 110 kV Line Uprate

At the TYTFS data freeze date this project was expected to be completed in 2021.

## (iii) Wexford 110 kV Busbar Uprate

At the TYTFS data freeze date this project was expected to be completed in 2021.

## (iv) Dunstown, Moneypoint and Oldstreet Series Compensation

Series compensation will be installed at Dunstown, Moneypoint and Oldstreet 400 kV stations to compensate the Coolnabacky-Moneypoint, Coolnabacky - Dunstown and Oldstreet-Woodland 400 kV lines. At the TYTFS data freeze date these projects were expected to be completed in 2022.

## **Thornsberry Busbar Uprate**

The 110 kV busbar at Thornsberry will be uprated to accommodate increased power flows arising due to increases in demand and generation in the midlands. At the TYTFS data freeze date this project was expected to be completed in 2020.

## **Thurles Station STATCOM**

One of the existing 15 Mvar capacitor banks on the 110 kV busbar at Thurles will be removed and replaced with a new ±30 Mvar STATCOM. At the TYTFS data freeze date this project was expected to be completed in 2022.

<sup>59</sup> http://www.eirgridgroup.com/how-the-grid-works/ridp/

## 2.6. Northern Ireland Transmission System Developments

This section details the transmission system projects that are planned to take place in Northern Ireland over the period covered by this forecast statement. Projects have been included using completion dates assessed to be appropriate at the time of the data freeze (January 2020).

## 2.6.1. Grid Development Process

SONI recently updated the Northern Ireland Grid Development Process<sup>60</sup>. This is a three part process which includes stakeholder and public participation (as appropriate) in the development of projects, see Figure 2-4.

## SONI's Grid Development Process



Figure 2-4: SONI's Grid Development Process

The approach taken to developing the grid is described by the following:

- The projects listed here have all progressed through either the SONI approval and governance process or have been identified to SONI by NIE Networks. In cases where the project is at an early stage, i.e. Part 1, this approval may be limited to the investigation of feasibility of several options prior to shortlisting and selection of preferred option and identification of study areas. Therefore, the outline design that progresses to the consents stage may vary from that assumed in the forecast statement study files;
- Developments are based on assumptions relating to the forecast change in demand and generation; and
- Studies have concluded that the following projects are required to address forecast noncompliance with standards, subject to the forecast change in demand and generation. However, further cost benefit analysis may result, in some cases, in the identification of alternative solutions or operational interventions.

Further projects for which a need has been identified but approval has not yet been granted have not been included in the TYTFS analysis. These are discussed in more detail in Transmission Development Plan Northern Ireland 2020 - 2029<sup>61</sup> (TDPNI).

<sup>60</sup> http://www.soni.ltd.uk/media/SONIs-Powering-The-Future-Grid-Development-Process-brochure.pdf 61 https://www.soni.ltd.uk/media/documents/SONI-Transmission-Development-Plan-Northern-Ireland-2020-2029.pdf

SONI published its first 'Tomorrow's Energy Scenarios Northern Ireland' (TESNI) which outlines three possible energy futures<sup>62</sup>. These acknowledge that there is no single pathway to a low carbon future. We also analysed how the existing and planned transmission grid performs under each of the scenarios over a range of timeframes. The results of this analysis, known as TESNI 2020 System Needs Assessment, are also available on the SONI website<sup>63</sup>.

## 2.6.2. Descriptions of Northern Ireland Development Projects

## **Additional Shunt Reactors**

With an increase in small scale generation and increasing energy efficiency, the minimum load seen on the NI transmission system has dropped, leading to an increased need to reduce system voltages during these periods. Shunt reactors suppress system voltages. This project involves installation of two new shunt reactors at Castlereagh, and one at each of Tandragee and Tamnamore, connected to tertiary windings of interbus transformers. At the TYTFS data freeze date this project was expected to be completed by summer 2022.

## **Banbridge Transformer Replacement**

The 30 MVA 110/33 kV transformers T1 – T4 at Banbridge are to be replaced by two new 90 MVA units. At the TYTFS data freeze date this project was expected to be completed by winter 2024.

## **Ballymena Transformer Replacement**

The 60 MVA 110/33 kV transformers T3 and T4 at Ballymena are to be replaced by new 90 MVA units. At the TYTFS data freeze date this project was expected to be completed by winter 2020.

## **Enniskillen Transformer Replacement**

The 45 MVA 110/33 kV transformers T1 and T2 at Enniskillen are to be replaced by new 90 MVA units. At the TYTFS data freeze date this project was expected to be completed by winter 2024.

## Donegall Main (North) Transformer Replacement

The 60 MVA 110/33 kV transformer TxB at Donegall North is to be replaced by a new 90 MVA unit. At the TYTFS data freeze date this project was expected to be completed by summer 2021.

## **Glengormley Transformer Replacement**

The 60 MVA 110/33 kV transformer TxB at Glengormley is to be replaced by a new 90 MVA unit. At the TYTFS data freeze date this project was expected to be completed by winter 2021.

## Omagh Main – Dromore 110 kV Circuit Uprate

With the connection of Drumquin cluster substation to Dromore it will be necessary to restring the Omagh Main – Dromore tower line with a higher capacity conductor. At the TYTFS data freeze date this project was expected to be completed by 2022.

## **Airport Road Main**

It is planned to construct a new 110/33 kV substation including 2 x 60 MVA transformers and a 33 kV switchboard in the Belfast Harbour Estate, close to Airport Road. The substation will be connected as a teed transformer feeder arrangement from Rosebank Main 110 kV. The substation will supply both Airport Road and Queens Road 33 kV substations which are to be transferred from Cregagh Main. At the TYTFS data freeze date this project was expected to be completed by winter 2022.

<sup>62</sup> https://www.soni.ltd.uk/customer-and-industry/energy-future/

<sup>63</sup> https://www.soni.ltd.uk/media/documents/TESNI-SNA-2020.pdf

## Ballylumford - Eden 110 kV Circuit Uprate

The conductor on the existing tower line will be replaced and uprated. At the TYTFS data freeze date this project was expected to be completed by winter 2022.

## **Ballylumford Switchgear**

The existing 110 kV switchgear at Ballylumford is to be replaced with a new 110 kV GIS double busbar and the 110 kV circuits diverted accordingly. At the TYTFS data freeze date this project was expected to be completed by winter 2021. Currently one 275/110 kV interbus transformer at Ballylumford is operated out of service to ensure the fault level is kept within existing switchgear fault rating. After this work is completed, this restriction can be removed.

## Castlereagh IBTx 1

The interbus transformer IBTX 1 at Castlereagh is to be replaced. The replacement transformer will have a 240 MVA primary winding and a 60 MVA tertiary winding. At the TYTFS data freeze date this project was expected to be completed by 2024.

## Castlereagh – Knock 110 kV Cable Uprate

The cable sealing ends at Castlereagh will be replaced along with a section of cable in order to improve capacity and fault rating. At the TYTFS data freeze date this project was expected to be completed by 2021.

## Coolkeeragh-Magherafelt 275 kV Circuits

It is planned to replace the conductor on the existing double circuit tower line. The rating of the replacement conductor will be defined as part of the redesign of the circuit. At the TYTFS data freeze date this project was expected to be completed by winter 2022.

## Kells-Rasharkin New 110 kV Circuit

As a result of increasing growth in renewable generation there will be a need to construct a second 110 kV circuit between Kells and Rasharkin 110/33 kV cluster substations. This circuit will be required to have a minimum rating of approximately 190 MVA. At the TYTFS data freeze date this project was expected to be completed by 2024.

## Windfarm Clusters Development

## (i) Agivey 110 kV Cluster

It is planned to establish a 110/33 kV cluster substation at Agivey, near Garvagh, connected to the Rasharkin cluster via a portal overhead line. At the TYTFS data freeze date this project was expected to be completed by winter 2021.

## (ii) Kells 110/33 kV Cluster

It is planned to establish a 110/33 kV cluster substation near Kells, connected to the existing Kells station via an overhead line. At the TYTFS data freeze date this project was expected to be completed by 2022.

## (iii) Gort Main 2nd Transformer

It is planned to install a 2nd 110/33 kV transformer at Gort Main cluster substation, allowing the transfer of a nearby wind farm from the Omagh distribution system to a more direct connection to the transmission system. At the TYTFS data freeze date this project was expected to be completed by winter 2022.

## 2.6.3. Projects Not Included in the 2020 TYTFS Analysis

A number of projects have not been included in the TYTFS analysis due to uncertainty at this time over either:

- The case of need; and/or
- Scope; and/or
- Timescales.

These projects are described in more detail in TDPNI which is available on the SONI website<sup>64</sup>.

## 2.7. Joint Ireland and Northern Ireland Approved Transmission System Developments

This section includes transmission system developments which both EirGrid and SONI have identified the need for.

We are proposing a new 400 kV circuit which will connect Woodland 400/220 kV station in County Meath (Ireland) and Turleenan 400/275 kV station in County Tyrone (Northern Ireland). A new 400 kV station at Turleenan is required.

At present, the transmission transfer capacity between Ireland and Northern Ireland is not sufficient. Due to the risk of a forced outage, we must limit power flows across the border to prevent stress on the grid and risk to security of supply. The North South Interconnector will deliver a more secure and reliable electricity supply throughout the island of Ireland. It will bring about major cost savings and address significant issues around the security of electricity supply.

A key benefit is that it will remove bottlenecks between the two systems. This will enable the two systems to work together as a single network. This will benefit residents and businesses on both sides of the border. Other benefits will include cost savings for consumers, as larger electricity systems operate more efficiently than smaller ones.

The North South Interconnector will also allow for greater connection of renewable generation. This will help Ireland and Northern Ireland achieve future renewable energy targets.

At the TYTFS data freeze date this project was expected to be completed by the end of 2023. Since the data freeze, we have revised the likely energisation date for the North South Interconnector to 2025. This is due to delays in the receipt of planning approval in Northern Ireland and subsequent legal challenge. We will assume 2025 as the year for energisation of the North South Interconnector in our analyses for the next TYTFS.

Once this connection is established, the constraints on the existing Tandragee-Louth 275 kV double circuit will be significantly reduced.

## 2.8. Connection of New Generation Stations

New generators will connect over the period covered by this statement. Table 2-6 lists the transmission system developments associated with future generation. New generators are included in the appropriate network models according to their expected connection date. Details of these generators and their expected connected dates are given in Section B.2 in Appendix B.

<sup>64</sup> http://www.soni.ltd.uk/the-grid/projects/tdpni/the-project/

## Table 2-6: Transmission System Station Developmentto Facilitate the Connection of Future Generation

| Generator  | Planned Connection Method  | Location         |  |  |
|--|--|------------------|--|--|
| Agivey Cluster                                   | Future Agivey 110/33 kV cluster substation is planned to be connected via a loop in to the Rasharkin – Brockaghboy 110 kV circuit. | Northern Ireland |  |  |
| Kells Cluster                                    | Future Kells 110/33 kV cluster substation is planned to be tail-connected into Kells 275/110 kV switching station at 110 kV.       | Northern Ireland |  |  |
| Ardderoo Wind Farm                               | New Buffy 110 kV station, connected into<br>Knockranny 110 kV station.   | Ireland          |  |  |
| Ballinknockane Solar Park                        | Ballinknockane Solar Park New Ballinknockane 110 kV station, connected into the existing Aughinish-Kilpaddoge 110 kV circuit.      |                  |  |  |
| Blundlestown Solar Park                          | New Blundelstown 110 kV station, connected into the existing Corduff-Mullingar 110 kV circuit.                                     | Ireland          |  |  |
| Croaghonagh Wind Farm <sup>65</sup>              | New Croaghonagh 110 kV station, connected into<br>Clogher 110 kV station.  | Ireland          |  |  |
| Carrigdangan Wind Farm<br>(formerly Barnadivane) | New Carrigdangan 110 kV station, connected into<br>Dunmanway 110 kV station.   | Ireland          |  |  |
| Drombeg Solar Park                               | New Drombeg 110 kV station, connected into the existing Kilpaddoge-Tralee 110 kV circuit.  | Ireland          |  |  |
| Gallanstown Solar Park                           | New Gallanstown 110 kV station, connected into the existing Corduff-Platin 110 kV circuit.   | Ireland          |  |  |
| Harristown Solar Park                            | New Harristown 110 kV station, connected into<br>the existing Kinnegad-Dunfirth/Rinawade 110 kV<br>circuit.                        | Ireland          |  |  |
| Lumcloon Energy Storage                          | New Derrycarney 110 kV station, connected into<br>the existing Portlaoise-Dallow/Shannonbridge<br>110 kV circuit.                  | Ireland          |  |  |
| Monatooreen Solar Park                           | New Monatooreen 110 kV station, connected into<br>Knockraha 220/110 kV station.  | Ireland          |  |  |
| Oriel Wind Farm                                  | New Oriel 220 kV station, connected into the existing Louth-Woodland 220 kV circuit.   | Ireland          |  |  |
| Rosspile Solar Park                              | New Rosspile 110 kV station, connected into the existing Great Island-Wexford 110 kV circuit.                                      | Ireland          |  |  |
| Shantallow Solar Park                            |  |                  |  |  |
| Timahoe North Solar Park                         | New Timahoe North 110 kV station, connected into the existing Derryiron-Maynooth 110 kV circuit.                                   | Ireland          |  |  |
| Tullabeg Solar Park                              | New Tullabeg 110 kV station, connected into the existing Banoge-Crane 110 kV circuit.  | Ireland          |  |  |

<sup>65</sup> Formed by the merger of Carrickaduff and Carrickalangan windfarms.

## 2.9. Connection of New Interface Stations

Transmission interface stations are the points of connection between the transmission system and the distribution system or large energy users connecting directly to the transmission system.

The planned new interface stations, for the period covered by this statement, are listed in Table 2-7. These stations are included in the network models according to their expected connection date. Details of the connections and dates are given in Section B.2, Appendix B.

| Station                          | Nearest Main Town or Load Centre | County   |
|----------------------------------|----------------------------------|----------|
| Airport Road 110 kV station      | Belfast                          | Down     |
| Ballyragget 110 kV station       | Ballyragget                      | Kilkenny |
| Barnageeragh 110 kV station      | Transmission connected demand    | Dublin   |
| Bracetown 220 kV station         | Transmission connected demand    | Meath    |
| Bracklone 110 kV station         | Portarlington                    | Laois    |
| Darndale 110 kV station          | Transmission connected demand    | Dublin   |
| Kellystown 220 kV station        | Transmission connected demand    | Kildare  |
| New 110 kV station near Kilbarry | Cork                             | Cork     |

## Table 2-7: Planned Transmission Interface Stations

## 2.10. Detailed Transmission Network Information

Appendix A includes geographical maps and network schematic diagrams of the existing and planned all-island transmission system.

The maps and schematic diagrams show snapshots of the all-island transmission system at January 2020 and the planned transmission system expected by the end of 2029. The diagrams indicate stations, circuits, transformers, generation, reactive devices and phase shifting transformers.

The electrical characteristics and capacity ratings of the existing and planned transmission system are included in Appendix B. Characteristics of existing and planned overhead lines, underground cables, transformers and reactive compensation devices are provided.



# 3. Demand





# 3. Demand

This chapter provides information on the all-island, Ireland and Northern Ireland demand forecasts.

The forecasts are taken from the All-Island Generation Capacity Statement 2020-2029 (GCS)<sup>66</sup> which was published by EirGrid and SONI in August 2020. GCS 2020 contains forecasts of future energy consumption and demand levels between 2020 and 2029.

This chapter also provides an introduction to the anticipated large demand increase in the Dublin area. This anticipated demand increase is associated primarily with the connection of new large energy users such as data centres. The impact of these data centres on the future all-island demand forecast is also discussed.

## 3.1. All-Island, Ireland and Northern Ireland Peak Transmission Demand

Table 3-1 presents the median all-island, Ireland and Northern Ireland, winter peak demand forecasts over the period 2020-2029, as published in the GCS.

It is difficult to accurately predict a peak demand figure for a particular year in the future. This is due to a number of factors that can cause fluctuations in the forecast. These factors include weather conditions, economic activity, electricity usage patterns and government policy.

The annual peak demand figures listed in Table 3-1 are expected to occur during the winter period of each year. For example, we would expect that the 2020 peak demand forecast of 6.95 gigawatts (GW) would occur in winter 2020/2021. In Ireland and Northern Ireland, the winter peak demand usually occurs between 17:00 and 19:00 on a weekday evening. However, the peak demand in each jurisdiction generally does not occur on the same day.

The demand forecast represents an average annual increase in all-island winter peak demand of 1.8% over the period of GCS 2020-2029<sup>67</sup>. This represents a decrease in demand forecast relative to GCS 2019-2028, when the forecast average annual increase in all-island winter peak demand between was 2.4%<sup>68</sup>.

|                          | 2019 | 2020 | 2021 | 2022 | 2023 | 2024 | 2025 | 2026 | 2027 | 2028 | 2029 |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|
| Northern Ireland<br>(GW) | 1.71 | 1.72 | 1.72 | 1.73 | 1.74 | 1.75 | 1.76 | 1.77 | 1.78 | 1.79 | 1.80 |
| Ireland (GW)             | 5.14 | 5.32 | 5.46 | 5.63 | 5.77 | 5.91 | 6.01 | 6.09 | 6.18 | 6.28 | 6.37 |
| All-island (GW)          | 6.76 | 6.95 | 7.11 | 7.29 | 7.44 | 7.59 | 7.69 | 7.79 | 7.89 | 7.99 | 8.09 |

Table 3-1: All-island, Ireland and Northern Ireland Peak Demand Forecast

As well as winter peak forecasts, we also develop summer peak and summer valley forecasts for Ireland and Northern Ireland, and autumn peak forecasts for Northern Ireland only.

The summer peak refers to the average peak demand levels that are forecast to occur during the summer period of each year. The Ireland and Northern Ireland summer peaks are combined to produce an all-island summer peak.

<sup>66</sup> http://www.eirgridgroup.com/site-files/library/EirGrid/All-Island-Generation-Capacity-Statement-2020-2029.pdf

<sup>67</sup> The cumulative forecast increase in demand over the period of GCS 2020-2029 is 19.6%.

<sup>68</sup> The cumulative forecast increase in demand over the period of GCS 2019-2028 was 27%.

The overall transmission system power flows are usually lower in summer than in winter. However, this may not be the case for flows on all circuits. The capacity of overhead lines is lower during the summer period because of higher ambient temperatures. Network maintenance is also usually carried out during the summer/autumn period. Both of these factors can restrict the network, reducing its capability to transport power.

The annual minimum expected demand is referred to as the summer valley. It represents the lowest annual demand that is forecast, and is expected to occur during the summer period of each year. The Ireland and Northern Ireland summer valley demands are combined to produce an all-island summer valley demand. The summer valley cases examine the impact of the combination of low demand and low levels of conventional generation on the transmission system.

This minimum condition is of particular interest when assessing the capability of the transmission system to connect new generation. This is because with local demand at a minimum, the connecting generator will export more of its power across the transmission system.

The summer peak and valley demands occur between May and August. The autumn peak demand refers to the peak demand value expected in September and October.

Summer peak, summer valley and autumn peak demand forecasts can be expressed in terms of percentage of winter peak demand. These are shown in Table 3-2.

## Table 3-2: Ireland and Northern Ireland Seasonal Demand Forecast as a Percentage of Winter Peak Demand

| Season        |     | Northern Ireland Seasonal Demand<br>Forecast as a Percentage of Winter Peak (%) |
|---------------|-----|---|
| Winter Peak   | 100 | 100   |
| Autumn Peak   | N/A | 87  |
| Summer Peak   | 80  | 79  |
| Summer Valley | 35  | 29  |

These figures are consistent with historical demand data.

## 3.1.1. Large Demand Increases in the Dublin Area

## Background

In recent years there has been an increase in the level of connections and enquiries for connection to the transmission system in the Dublin area. This document includes information on both current demand connections and future demand opportunities at the freeze date of January 2020. Our assessment of demand opportunities is presented in Chapter 8 and includes a section focused on the Dublin area.

The level of enquiries in the Dublin area is principally driven by the need for Information, Communications and Technology (ICT) industries and high-tech manufacturing companies to connect to a high quality power supply in the Dublin area.

## **Data Centres**

Ireland is an attractive business location and continues to attract world-class investments. Industrial Development Authority (IDA) Ireland has cited access to a high-quality electricity grid as critically important for attracting new investment. This is particularly important in the ICT and high-tech manufacturing sectors.

Some of the world's best known companies have chosen Ireland as the location for their European data centre operations. Factors such as a temperate climate, stable power sources, internet connectivity and a skilled workforce have influenced their decisions. This is emphasised by nine out of the top 10 global software companies and US ICT companies locating strategic business activities in Ireland<sup>69</sup>.

In 2020, connected data centres had a combined total power demand of approximately 400 MVA. The total contracted maximum import capacity (MIC) for these sites is 961 MVA. This includes connections to the transmission and distribution systems. In addition to the connected sites, a further 589 MVA of contracts are in place for new data centre connections. Applications are being processed for a further 660 MVA of data centre contracts in the Dublin region. There continues to be ongoing enquiries regarding further large demand connections in the Dublin region.

To put this in context, the 2029 winter peak demand forecast on the all-island transmission system is 8,090 MW. If all applicants currently being processed were to connect, the data centre load could account for approximately 27% of the all-island system peak demand in 2029.

## What is a data centre?

A data centre is a facility used to house computer systems and associated components, such as telecommunications and storage systems. They underpin the operations of companies in the broad ICT sector, particularly those in social media and cloud computing. The size of the individual electricity demand connections depends on the scale of the business operation. These have varied from 20 MW with some possibly extending to 250 MW in the final stages of development. Their use of electricity tends to be constant throughout the year. The modern world increasingly requires the retention and use of vast volumes of data, so this trend is likely to continue for the foreseeable future.

## Impact on the System Demand Forecast

The potential connection of data centre demand on the scale discussed represents significant demand growth. This is having an impact on the all island system demand forecast and generation capacity adequacy. Generation adequacy is assessed and discussed in the GCS.

The focus of the majority of the connection enquiries have been in the greater Dublin area. Depending on the number and scale of projects that materialise, new transmission solutions will be required to strengthen the grid to facilitate these connections. These transmission solutions are under investigation and could vary from short lead-time to longer lead-time developments. The impact of these Dublin demand connections are described in greater detail in Chapter 8, Section 8.3.

SONI is preparing a connection offer for a data centre in the North West which is expected to connect at Coolkeeragh 110kV. If this offer is accepted, this might have an impact on the generation and demand opportunities in the North West.

<sup>69</sup> https://www.idaireland.com/doing-business-here/industry-sectors/ict

## 3.2. Demand Data

Electricity usage follows some generally accepted patterns. For example, annual peak demand occurs between 17:00 - 19:00 hrs on winter weekday evenings. Minimum usage usually occurs during summer weekend night-time hours.

## 3.2.1. Generated Peak Demand Profiles

Figure 3-1 shows the generated peak demand profiles of Ireland and Northern Ireland on the day of the 2019 all-island winter peak on 17 December 2019. The individual peaks for Ireland and Northern Ireland did not occur on the same day. Peak demand for Ireland occurred on 17 December 2019, while peak demand occurred in Northern Ireland on 31 January 2019.

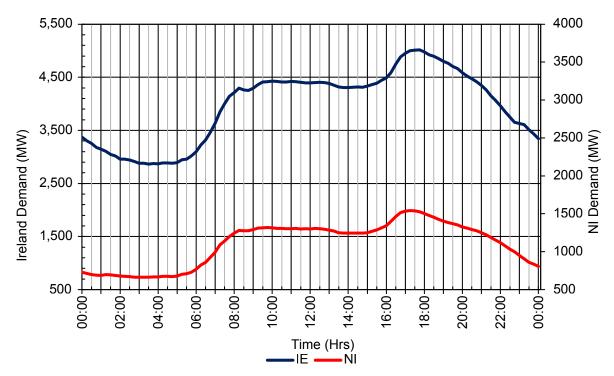


Figure 3-1: Generated Peak Demand Profiles for 2019

## 3.2.2. All-Island Demand Profiles

Figure 3-2 shows the profiles of the 2019 all-island winter peak, summer peak and summer valley. The percentage demand attributable to each jurisdiction during the peak and valley scenarios is also shown.

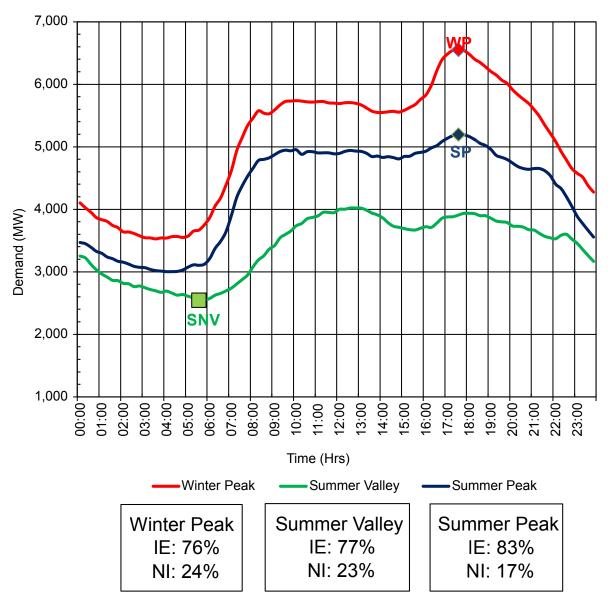


Figure 3-2: All-Island Daily Demand Profiles for Year 2019

|                | Irelan           | d           | Northern Ireland |             |  |  |
|----------------|------------------|-------------|------------------|-------------|--|--|
| 2019           | Date and Time    | Demand (MW) | Date and Time    | Demand (MW) |  |  |
| Winter Peak    | 17/12/2019 17:45 | 5015        | 31/01/2019 18:00 | 1598        |  |  |
| Summer Peak    | 08/05/2019 17:45 | 3991        | 07/05/2019 17:30 | 1225        |  |  |
| Minimum Demand | 05/08/2019 05:45 | 2052        | 18/08/2019 04:00 | 429         |  |  |

Minimum demand is normally seen during the summer. The demand reported here is that which was seen at the transmission system Bulk Supply Points (BSP), which does not count the effect of small scale generation such as rooftop solar panels. These are not metered in the same way as larger sources of generation and serve to reduce the demand observed rather than increasing the generation.

## 3.2.3. All-Island Weekly Demand Peaks

Figure 3-3 shows the profile for the all-island, Northern Ireland and Ireland weekly peaks across the year for 2019.

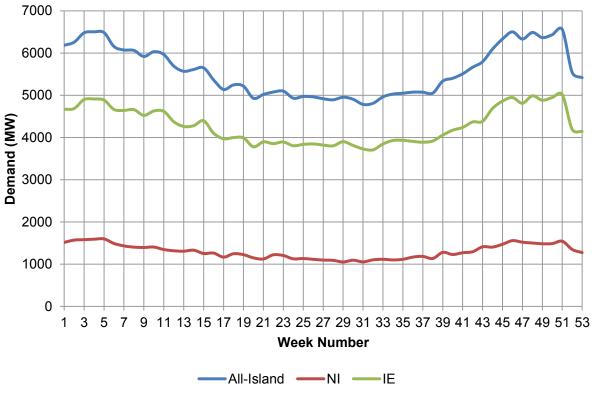


Figure 3-3: Weekly Demand Peak Values for Year 2019

## 3.2.4. Load Duration Curves

Figures 3-4 and 3-5 show the Ireland and Northern Ireland 2019 load duration curves, respectively. The curves show the percentage of time in the year that a particular demand value was exceeded. For example, demand exceeded 3,000 MW for 66% of the year in Ireland. Demand in Northern Ireland exceeded 1,000 MW for 36% of the year.

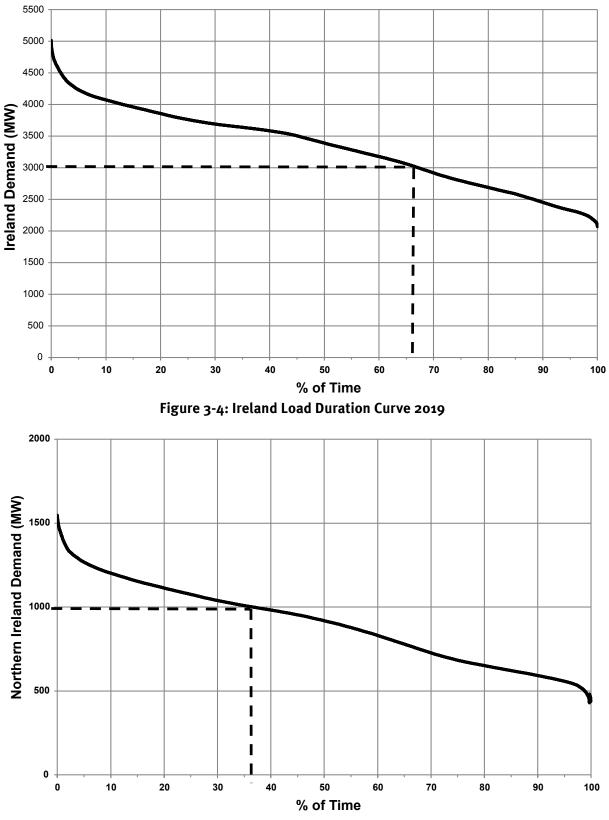


Figure 3-5: Northern Ireland Load Duration Curve 2019

## 3.3. Forecast Demand at Transmission Interface Stations in Ireland

Transmission interface stations are the points of connection to the transmission system. These interfaces include:

- Connections between the transmission and the distribution systems; and
- Customers connected directly to the transmission system at 220 kV or 110 kV.

The interfaces are mostly 110 kV stations. In Dublin city, where the Distribution System Operator (DSO) operates the 110 kV network, the interface is usually at 220 kV stations.

Appendix C lists forecast demands at each transmission interface station. The forecast demands are given for winter peak, summer peak and summer valley for all years from 2020-2029. Demand projections at individual transmission stations are developed from the system demand forecasts on a top-down<sup>70</sup> basis.

The forecasting process includes regular monitoring and review of consumption trends in all parts of the country. The allocation of the system demand forecast to each station is pro-rata. This is based on an up-to-date measurement of actual peak demand at each station. Account is taken of planned transfers of demand between stations, as agreed with ESB Networks<sup>71</sup>. In this way, changes in the location of electricity consumption are captured. This process provides a station demand forecast and by extension a regional demand forecast for the short to medium term.

The system-wide demand forecasts, presented in Table 3-1, include transmission losses whereas the individual station demand forecasts do not. Transmission losses therefore account for the difference between system-wide demand and the sum of the demand at each interface station. The demand at each interface is given in Appendix C.

Demand forecasts in Appendix C include the small number of directly-connected customers. The values in Appendix C were the best estimates of requirements at the data freeze date and do not reflect contractual status or the level of firm capacity that may be available in the network. In some cases, the estimates may be less than contracted maximum import capacity (MIC) values. These values are chosen to give a better projection of expected demand on a system-wide basis. When analysing the capacity for new demand in a particular area, the MIC values of local directly-connected and contracted customers are used. It is important to note that some contracted MIC is non-firm and subject to flexible demand arrangements.

A demand-side unit (DSU) consists of one or more demand sites that can be instructed by EirGrid and SONI to reduce electricity demand. DSUs are usually medium to large industrial premises. A DSU uses a combination of on-site generation or plant shutdown to deliver a demand reduction. Providing this dispatch availability means that the DSU is eligible for capacity payments in the Single Electricity Market (SEM).

It is noted that DSUs may reduce some customers' demands from time to time over winter peak hours. However, normal demand levels are included in the winter peak demand forecasts shown in Table C-1 in Appendix C. Normal demand levels are also used in the power flow tables in Appendix H. These normal demand levels are used since they are more indicative of general power flows.

<sup>70</sup> This approach takes the overall demand forecast and breaks it down - using transmission system information, including historical data - to gain better knowledge of the sub-components of the demand forecast. 71 ESB Networks is the Distribution System Operator (DSO) in Ireland.

## 3.4. Forecast Demand at Northern Ireland Bulk Supply Points (BSP)

The 110/33 kV BSP demand forecasts are provided by NIE Networks<sup>72</sup>. These forecasts are based on demand trends at an individual nodal level and adjusted to align with system average cold spell (ACS<sup>73</sup>) forecasts. Consideration is also given to future block load transfers from one BSP to another. Tables and information relating to demand forecasts are contained in Appendix C.

<sup>72</sup> NIE Networks is the DSO in Northern Ireland.

<sup>73</sup> Demand trends are based on historical information. ACS analysis produces a peak demand which would have occurred had conditions been averagely cold for the time of year. This ACS adjustment to each winter peak seeks to remove any sudden changes caused by extremely cold or unusually mild weather conditions.



# 4. Generation





# 4. Generation

This chapter gives information about existing generation capacity. This chapter also defines future projections for the next ten years from 2020 to 2029. All generation capacity and dispatch figures given in this statement are expressed in exported or net terms. This is the generation unit output less the unit's own auxiliary load.

In June 2019 the Irish Government launched its Climate Action Plan 2019. The Action Plan sets out an ambitious course of action over the coming years. Specifically for the electricity sector it sets a target that 70% of electricity will come from renewable energy sources by 2030. In order to meet this target, investment will be needed in new renewable generation capacity, system service infrastructure and electricity networks. The Climate Action Plan 2019 was complemented by the Programme for Government in 2020. A Climate Action Plan 2021 is currently being drafted, following a consultation in the 1st half of 2021.

In Northern Ireland, the United Kingdom's Committee on Climate Change advised that it is necessary, feasible and cost-effective for the UK to set a target of net zero Green House Gas (GHG) emissions by 2050. The Climate Change Act 2008 (2050 Target Amendment) Order 2019 came into effect on 27 June 2019. The revised legally binding target towards net zero emissions covers all sectors of the economy. This update to the Order demonstrates the UK's commitment to targeting a challenging ambition in line with the requirements of the Paris Agreement on climate change.

Energy Policy is a devolved matter for Northern Ireland and the DfE is currently working with stakeholders to develop the next Strategic Energy Framework for Northern Ireland. SONI is providing input to this important work, which will inform future renewable targets and the approach to facilitating growth in renewable electricity generation.

A freeze date for data was applied when compiling this TYTFS. A freeze date enables transmission system analyses to be carried out for inclusion in the document. The data freeze date for TYTFS 2020 is January 2020.

## 4.1. Generation in Ireland

At the data freeze date 10,692 MW of generation capacity was installed in Ireland, as detailed in Table 4-1.

| Transmission System | Distribution System Connected | Total Generation Capacity |
|---------------------|-------------------------------|---------------------------|
| Connected (MW)      | (MW)                          | (MW)                      |
| 8,157 <sup>74</sup> | 2,535                         |                           |

## Table 4-1: Installed Generation Capacity in Ireland

<sup>74</sup> Please note this figure does not include the East West Interconnector.

## 4.1.1. Existing and Planned Transmission Connected Generation

Table 4-2 lists planned generators that have signed transmission connection agreements in place, along with their expected energisation dates if available, at the data freeze date. It should be noted that this position has changed somewhat since the data freeze date and a number of projects have decided not to proceed – a more up to date picture will be presented in the Generation Capacity Statement 2021 to 2030.

| Generator                                | Generation Type | Generation Capacity<br>(MW) | Expected Energisation Date |
|--|-----------------|-----------------------------|----------------------------|
| Ardderoo (formerly Buffy)                | Wind            | 91.20                       | 2020                       |
| Beenanaspock and<br>Tobertooreen         | Battery         | 11                          | 2020                       |
| Ballinknockane                           | Solar           | 50                          | 2021                       |
| Banemore                                 | Solar           | 34                          | Date unavailable           |
| Blundlestown                             | Solar           | 80                          | 2021                       |
| Carrigdangan (formerly<br>Barnadivane)   | Wind            | 60                          | 2020                       |
| Croaghonagh <sup>75</sup>                | Wind            | 138.10                      | Date unavailable           |
| Drombeg                                  | Solar           | 50                          | 2021                       |
| Gallanstown                              | Solar           | 85                          | 2021                       |
| Gorman Energy Storage                    | Battery         | 50                          | Date unavailable           |
| Harristown                               | Solar           | 42.3                        | 2022                       |
| Kelwin Phase 2                           | Battery         | 20                          | 2020                       |
| Knocknamona                              | Wind            | 34                          | 2020                       |
| Loughteague                              | Solar           | 55                          | Date unavailable           |
| Lumcloon Energy Storage<br>(Derrycarney) | Battery         | 100                         | 2020                       |
| Monatooreen                              | Solar           | 25.7                        | Date unavailable           |
| North Wall 4                             | OCGT            | 120                         | Date unavailable           |
| Oriel                                    | Wind            | 210                         | Date unavailable           |
| Oweninny Power 2                         | Wind            | 83                          | Date unavailable           |
| Oweninny 3                               | Wind            | 50                          | Date unavailable           |
| Poolbeg Energy Storage                   | Battery         | 75                          | Date unavailable           |
| Poolbeg Flexgen                          | OCGT            | 70                          | Date unavailable           |
| Porterstown                              | Battery         | 30                          | Date unavailable           |
| Rosspile                                 | Solar           | 95                          | 2021                       |
| Shannonbridge A                          | Battery         | 100                         | 2021                       |
| Shannonbridge B                          | Battery         | 63.2                        | Date unavailable           |
| Shantallow                               | Solar           | 35                          | 2021                       |
| Timahoe North                            | Solar           | 70                          | 2021                       |
| Tullabeg                                 | Solar           | 50                          | 2021                       |

## Table 4-2: Contracted Transmission Generation at data freeze date

<sup>75</sup> Formed by the merger of Carrickaduff and Carrickalangan wind farms.

## 4.1.2. Planned Closure of Generation Plant

The closure of generation plant could have a significant impact on the ability of the transmission system to comply with standards. The EirGrid Grid Code specifies the minimum length of notice a generator must give the TSO before retirement or divestiture. The closure of a generator with capacity less than or equal to 50 MW requires at least 24 months' notice. Generators with larger capacity than this must give at least 36 months' notice.

Some older generators will come to the end of their lifetimes over the next ten years. Some generators are also assumed to close as they don't comply with the carbon limits imposed by the Clean Energy Package. These generators are noted in All-Island Generation Capacity Statement 2020-2029 (GCS) and are listed in Table 4-3.

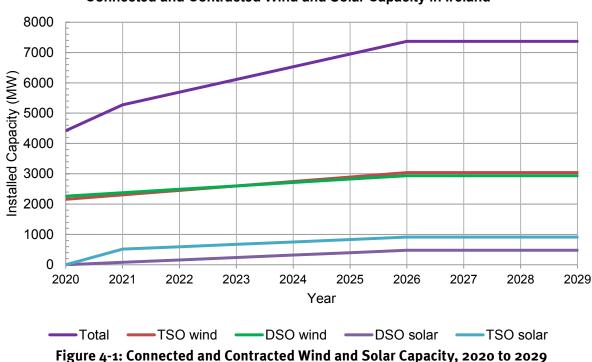
| Generator          | Generation Capacity (MW) | Expected to close by end of year |
|--------------------|--------------------------|----------------------------------|
| Lough Ree          | 91                       | Closed                           |
| West Offaly        | 137                      | Closed                           |
| Aghada (AT1)       | 90                       | 2023                             |
| Edenderry          | 118                      | 2023                             |
| Tarbert 1, 2, 3, 4 | 590                      | 2023                             |
| Moneypoint         | 885                      | 2025                             |

## Table 4-3: Closure of Conventional Generation

## 4.1.3. Wind and Solar Generation

Over the past two decades wind power generation in Ireland has increased significantly. The level of wind generation in Ireland is expected to continue to grow over the period of this TYTFS.

While there is currently no grid scale solar generation connected, solar connections are expected to increase significantly over the course of this TYTFS. The information presented in Figure 4-1 is a combination of connected and contracted wind and solar generation as of data freeze date<sup>76</sup>.



Connected and Contracted Wind and Solar Capacity in Ireland

76 Detailed information on these figures is presented in Tables D-2 and D-3 in Appendix D.

Table 4-4 shows the existing and committed wind and solar generation capacity totals expected to be connected by the end of each year<sup>77</sup>. These generators have signed connection agreements and are committed to connecting to either the transmission or distribution system over the next few years. Generators with no estimated connection dates were assumed to connect at a steady rate from 2021 onwards.

| Connection           | 2020  | 2021  | 2022  | 2023  | 2024  | 2025  | 2026  | 2027  | 2028  | 2029  |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Wind (Transmission)  | 2,158 | 2,305 | 2,452 | 2,599 | 2,745 | 2,892 | 3,039 | 3,039 | 3,039 | 3,039 |
| Wind (Distribution)  | 2,264 | 2,376 | 2,489 | 2,601 | 2,713 | 2,826 | 2,938 | 2,938 | 2,938 | 2,938 |
| Solar (Transmission) | 0     | 515   | 594   | 673   | 753   | 832   | 911   | 911   | 911   | 911   |
| Solar (Distribution) | 0     | 80    | 159   | 239   | 318   | 398   | 477   | 477   | 477   | 477   |
| Total                | 4,422 | 5,276 | 5,694 | 6,112 | 6,529 | 6,948 | 7,365 | 7,365 | 7,365 | 7,365 |

## 4.1.4. Offshore Generation

In 2014, the Irish Government published an Offshore Renewable Energy Development Plan (OREDP)<sup>78</sup>. The plan was reviewed in 2018. The OREDP provides a framework for the sustainable development of Ireland's offshore renewable energy sources. The OREDP identifies three high level goals:

- 1. That Ireland harnesses the market opportunities presented by offshore renewable energy to achieve economic development, growth and jobs;
- 2. To increase awareness of the value, opportunities and societal benefits of developing offshore renewable energy; and
- **3.** That offshore renewable energy development does not adversely impact our rich marine environment and its living and non-living resources.

The Department of the Environment, Climate and Communications is leading the implementation of the OREDP.

In 2019, the Irish Government launched the Climate Action Plan 2019. The Action Plan sets out an ambitious course of action over the coming years. Specifically, it sets a target that 70% of electricity will come from renewable energy sources by 2030.

In order to meet the Climate Action Plan target, investment will be needed in new renewable generation capacity. Offshore wind will be a significant part of the renewable generation mix in the future. Currently there is one 25 MW offshore wind farm in Ireland. The Action Plan outlines that at least 3.5 GW of offshore wind will be connected to the grid by 2030. This was complemented by the 2020 Programme for Government which outlined that at least 5 GW of offshore wind will be connected to the grid by 2030. As connection agreements are put in place to meet this level of capacity, we will include them in future TYTFS analyses.

## 4.1.5. Demand Side Units

In 2020, demand side units (DSUs) in Ireland had a combined dispatchable capacity of 571 MW.

<sup>77</sup> The individual wind farm details are included in Tables D-2 and D-3 of Appendix D.

<sup>78</sup> https://www.gov.ie/en/publication/e13f49-offshore-renewable-energy-development-plan/

## 4.1.6. Distribution-Connected Generation

Table 4-5 details the existing distribution-connected generation capacity by generation type. This generation plant comprises of small conventional and renewable units. Conventional units include CHP schemes and small industrial thermal units. Renewable generation consists of:

- Wind;
- Small Hydro;
- Land-fill gas (LFG);
- Biogas; and
- Biomass.

## Table 4-5: Existing Distribution-Connected Generation in Ireland

|                   | Wind <sup>79</sup> | Small Hydro | Biomass/ LFG | СНР | Diesel | Solar | Total |
|-------------------|--------------------|-------------|--------------|-----|--------|-------|-------|
| Net Capacity (MW) | 2,264              | 27          | 101          | 125 | 18     | <1    | 2,535 |

Distribution-connected generators reduce the demand supplied through Transmission Interface Stations. Forecasts of demand levels at individual Transmission Interface Stations are presented in Appendix C. These forecasts take account of the contribution of the existing non-wind distribution-connected generators<sup>80</sup>.

## 4.2. Generation in Northern Ireland

At the data freeze date 3,833 MW of generation capacity was installed in Northern Ireland, as detailed in Table 4-6.

## Table 4-6: Northern Ireland Installed Generation Capacity

| Transmission System | Distribution System Connected | Total Generation Capacity |  |  |
|---------------------|-------------------------------|---------------------------|--|--|
| Connected (MW)      | (MW)                          | (MW)                      |  |  |
| 2,208 <sup>81</sup> | 1,625                         | 3,833                     |  |  |

The 2,208 MW connected to the transmission system consists of:

- Conventional generation;
- Brockaghboy Wind Farm; and
- Slieve Kirk Wind Farm.

<sup>79</sup> Table D-3 in Appendix D provides details of the existing distribution-connected wind farms and their capacities. 80 Because of the variability of wind, a fixed contribution from distribution-connected wind farms is not taken into account in the calculation of the peak transmission flow forecasts. Rather a number of wind scenarios are considered in the TYTFS analyses. 81 Please note this figure does not include the Moyle Interconnector capacity.

## 4.2.1. Existing and Planned Transmission Connected Generation

## **Existing Conventional Generation**

In Northern Ireland, until September 2018, conventional thermal generation plant were split into two contractual categories:

- Plant contracted to Power NI Energy Limited via their Power Procurement Business (PPB) (Contracted Plant); and
- Independent Market Participants (IMP) (Non-Contracted Plant).

There was a total of 593 MW of plant contracted to PPB under pre-vesting contracts, or contracts negotiated thereafter. Since September 2018, all conventional generation in Northern Ireland have been Independent Market Participants.

## 4.2.2. Planned Closure of Generation Plant

The generation output of Kilroot ST1 and ST2 is anticipated to be restricted. The restriction is due to the Industrial Emissions Directive (IED)<sup>82</sup>. The restriction includes limited emissions each year from 2016-2020, followed by severely restricted running hours in subsequent years. As noted in GCS 2020 Kilroot ST1 and ST2 are assumed unavailable after 2023.

## 4.2.3. Northern Ireland Renewable Generation

## **Existing/Approved Renewable Generation**

Existing and approved renewable generation in NI is shown geographically in Figure 4-2. The totals are derived from locational and capacity information<sup>83</sup> on:

- Large scale renewable generation schemes that are connected to the Northern Ireland network;
- Small scale renewable generation schemes with installed capacity at each Bulk Supply Point (BSP) greater than 0.5 MW;
- Large scale schemes that are currently in construction; and
- Schemes approved by the planning service.

<sup>82</sup> http://ec.europa.eu/environment/industry/stationary/ied/legislation.htm 83 As at data freeze date – January 2020.

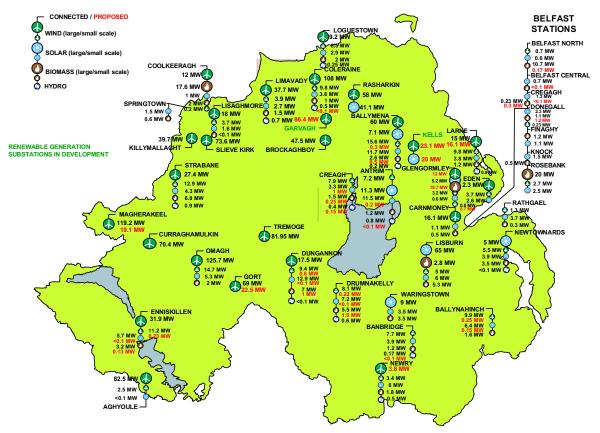
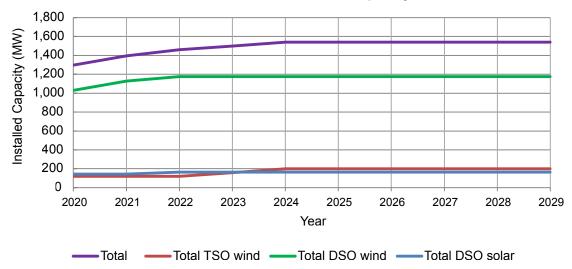


Figure 4-2: Existing and Committed Northern Ireland Renewable Generation

The map indicates points at which renewable generation is connected to or is assumed to connect to. These points include 110/33 kV Bulk Supply Points and 110/33 kV Cluster substations<sup>84</sup>.

Figure 4-3 shows the expected change in wind and solar generation in Northern Ireland. Only committed generators are included.



Connected and Contracted Wind and Solar Capacity in Northern Ireland



<sup>84</sup> A Cluster substation is a 110/33 kV substation in the vicinity of a number of wind farms. It acts as a local hub to group or "cluster" the wind farms. The wind farms are connected by short individual 33 kV lines to the Cluster substation. Cluster substations already exist at Magherakeel, Tremoge, Gort, Rasharkin and Curraghmulkin, with a further two planned at Agivey and Kells (see Chapter 2). SONI is responsible for the delivery of the transmission elements of the Cluster substation, in line with the criteria set out in 'Statement of Charges for Connection to the Northern Ireland Electricity Networks' Distribution System': https://www.nienetworks.co.uk/ statementofcharges

Table 4-7 shows the existing and committed wind and solar generation capacity totals expected to be connected by the end of each year<sup>85</sup>. These wind and solar farms have signed connection agreements and are committed to connecting to either the transmission or distribution system over the next few years.

| Connection           | 2020  | 2021  | 2022  | 2023  | 2024  | 2025  | 2026  | 2027  | 2028  | 2029  |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Wind (Transmission)  | 121   | 121   | 121   | 159   | 201   | 201   | 201   | 201   | 201   | 201   |
| Wind (Distribution)  | 1,031 | 1,129 | 1,175 | 1,175 | 1,175 | 1,175 | 1,175 | 1,175 | 1,175 | 1,175 |
| Solar (Distribution) | 144   | 144   | 164   | 164   | 164   | 164   | 164   | 164   | 164   | 164   |
| Total                | 1,296 | 1,394 | 1,460 | 1,498 | 1,540 | 1,540 | 1,540 | 1,540 | 1,540 | 1,540 |

Table 4-7: Existing and Committed Wind and Solar Capacity Totals (MW)

## Offshore Renewable Generation

Our assumptions regarding the level and location of offshore renewable generation connected to the NI transmission system are based on best information available at the data freeze date.

For the purpose of this TYTFS analyses we assumed that there will not be any offshore renewable generation connected as at present there are no connection agreements in place. However, development rights are in place for tidal sites in Northern Ireland's coastal waters. We will continue to monitor progress with a view to incorporating offshore renewable generation in future TYTFS analyses.

## 4.2.4. Demand Side Units

In 2020, demand side units (DSUs) in Northern Ireland had a combined dispatchable capacity of 135 MW.

## 4.2.5. Distribution-Connected Generation

## **Existing Distribution-Connected Generation**

Table 4-8 shows a breakdown of the existing Northern Ireland distribution-connected generation.

## Table 4-8: Northern Ireland Distribution-Connected Generation

| Generation                                | Net Capacity (MW)     |  |  |  |
|---|-----------------------|--|--|--|
| Large Scale Wind                          | 996                   |  |  |  |
| Small Scale Wind                          | 163                   |  |  |  |
| Large Scale Biomass                       | 22                    |  |  |  |
| Small Scale Biomass, CHP and Landfill Gas | 69                    |  |  |  |
| Large Scale Solar                         | 144                   |  |  |  |
| Small Scale Solar                         | 124                   |  |  |  |
| Small Scale Hydro                         | 6                     |  |  |  |
| Large Scale Landfill Gas                  | 3                     |  |  |  |
| СНР                                       | 27                    |  |  |  |
| AGU                                       | 71 (83) <sup>86</sup> |  |  |  |
| Total                                     | 1,625                 |  |  |  |

<sup>85</sup> The individual wind farm details are included in Tables D-2 and D-3 of Appendix D.

<sup>86</sup> There is 83 MW of AGU capacity in Northern Ireland. However, this includes 12 MW at Contour Global in Lisburn, which is a CHP plant. To avoid double counting of generation, only 71 MW of AGU capacity is included in the total figure.

There is a total of 83 MW of Aggregated Generating Units (AGUs) in Northern Ireland registered in the SEM by three parties. Two of these AGUs, iPower and EmPower, consist of mostly distribution connected diesel generator sets located around Northern Ireland. The third, ContourGlobal, consists of CHP gas generation. These units currently participate in the SEM.

There is currently 6 MW of small-scale hydro generation installed on the waterways of Northern Ireland. This is a mature technology. Due to the lack of suitable new locations, limited increase in the small-scale hydro is expected in the foreseeable future.



# 5. Transmission System Performance





# 5. Transmission System Performance

This chapter describes the future performance of the transmission system in terms of compliance with planning standards<sup>87</sup>. System performance levels are assessed using:

- Forecast power flows; and
- Short circuit<sup>88</sup> current levels.

The power flow and short circuit analyses results presented in this document are based on updated information, which includes changes to:

- The existing and planned transmission system;
- Demand projections; and
- Generation connections.

This updated information is based on the best information available at the data freeze date, January 2020.

### **5.1. Forecast Power Flows**

The power flows on the all-island transmission system, at any given time, depend on a number of factors, such as:

- The transmission system configuration;
- The level of demand; and
- The power output from each generator.

There are many possible combinations of generator dispatches that can meet the demand requirements. There are also many demand scenarios that may occur on the transmission system.

Renewable generation connected to the all-island transmission and distribution system has the effect of altering power flows. The increase in renewable generation<sup>89</sup> is one of the main factors behind recent changes to power flows on the transmission system.

When examining transmission system performance a range of economic generation dispatches are considered. The generation dispatches used in our power flow analysis are prepared on an all-island basis<sup>90</sup>. Power flows across the existing 275 kV and planned 400 kV internal<sup>91</sup> interconnectors are modelled to operate within transfer limits. The dispatch scenarios also consider imports and exports of power across the existing Moyle and East-West interconnectors.

Transmission system power flows are described in Appendix H. The power flow tables show the flow of real power on the transmission system under normal conditions.

As can be seen in Appendix H, the level of renewable generation increases over the ten year period. As renewable generation increases, power flows from the West of the Island to the East can be seen to increase. This is because renewable power generated in the Western regions is supplying the larger demand levels in the East (Belfast and Dublin). These increased power flows are more significant at times of minimum demand and high renewable generation output.

<sup>87</sup> Please note that different planning standards are applied in Ireland and Northern Ireland.

<sup>88</sup> Short circuit analysis was carried out on both the Ireland and Northern Ireland transmission systems.

<sup>89</sup> Projected levels of renewable generation connections are detailed in Tables D-2 and D-3 in Appendix D.

<sup>90</sup> This is reflective of how generation is dispatched in the Single Electricity Market.

<sup>91</sup> Internal to the all-island transmission system. These are the interconnectors between Ireland and Northern Ireland. This type of interconnector is also known as a tie line.

Another effect that can be seen in Appendix H is the effect of increased renewable generation levels on reactive power requirements on the transmission system. At high levels of renewable generation, reactive power support is needed to keep voltages within planning standard limits.

# 5.2. Compliance with Planning Standards

The transmission system is planned and operated to technical requirements and standards in Ireland and Northern Ireland. These requirements are laid out in the Transmission System Security and Planning Standards (TSSPS<sup>92</sup>) documents. These standards are in line with international standards.

The standards are deterministic<sup>93</sup> – as are those generally used throughout the world in transmission planning. They set out an objective standard which delivers an acceptable compromise between the cost of development and service delivered. Rather than conducting subjective benefit analysis in each case, it is preferable to plan to meet an objective standard and carry out analysis of the options available to meet the standard.

The need for transmission system development is identified when the simulation of future conditions indicates that the TSSPS would be breached.

#### 5.2.1. Ireland

Our view of future transmission needs and our plan to develop the Irish network through specific projects to meet these needs over the next ten years is presented in our Transmission Development Plan (TDP<sup>94</sup>). The TDP presents the projects which are currently being advanced to solve the needs of the transmission network. In addition, future needs that drive future potential projects are also discussed. We issue the TDP annually.

It is possible that changes will occur in the need for; scope of; and timing of the developments in the TDP. Similarly, it is likely, given the continuously changing nature of electricity requirements, that new developments will emerge that could impact the plan as presented. The long-term development of the network is under review on an on-going basis.

TYTFS 2020 includes transmission system development projects that have received capital approval.

#### 5.2.2. Northern Ireland

The Northern Ireland transmission projects included in TYTFS 2020 are based on the Transmission Development Plan Northern Ireland (TDPNI<sup>95</sup>). The TDPNI is issued annually. Capital projects are mainly driven by increases in Northern Ireland demand levels and renewable generation connections. Planned developments also include load related and asset replacement projects. These projects mainly impact on the rating of switchgear<sup>96</sup> and circuits.

It is possible that changes will occur in the need for; scope of; and timing of the developments in the TDPNI. Similarly, it is likely, given the continuously changing nature of electricity requirements, that new developments will emerge that could impact the plan as presented. The long-term development of the network is under review on an on-going basis.

TYTFS 2020 includes transmission system development projects that have received capital approval.

<sup>92</sup> The Irish transmission system is developed in accordance with the TSSPS Ireland: http://www.eirgridgroup.com/site-files/library/ EirGrid/EirGrid-Transmission-System-Security-and-Planning-Standards-TSSPS-Final-May-2016-APPROVED.pdf

The Northern Irish transmission system is developed in accordance with the TSSPS Northern Ireland: http://www.soni.ltd.uk/media/ Northern-Ireland-TSSPS-September-2015.pdf

<sup>93</sup> The deterministic methodology is often referred to as the N-1 criterion. The system must have sufficient capacity so that in the eventuality of a probable system outage, there are no resulting system problems such as overloading, under-voltage, over-voltage or instability.

<sup>94</sup> The latest version of the Transmission Development Plan for Ireland is available at www.eirgridgroup.com.

<sup>95</sup> The latest version of TDPNI is available at www.soni.ltd.uk.

<sup>96</sup> Devices used to control, protect and isolate electrical equipment.

# 5.3. Short Circuit Current Levels<sup>97</sup>

Short circuit currents<sup>98</sup> occur during a fault condition on the transmission system. Depending on the type of fault, these short circuit currents can be very high. All transmission system equipment must be capable of carrying these very high currents.

Protection devices, in particular circuit breakers, must be capable of closing onto high currents created by a fault on the transmission system. They must also be capable of interrupting high currents to isolate a fault. Correct operation is essential for minimising risk to personnel and preventing damage to transmission equipment. Correct operation of protection devices is also necessary for maintaining system stability, security and quality of supply.

Short circuit current levels must be considered as the transmission system is developed and as new generation or demand is connected. In Ireland the EirGrid Grid Code specifies short circuit current levels; these values are shown in Table 5-1. Users connecting to the transmission system are required to design their plant and apparatus to these specified levels. Equipment at lower voltage levels must also be designed to withstand short circuit current levels.

| Voltage Level (kV) | Short Circuit Current Levels (kA) |      |                  |  |
|--------------------|-----------------------------------|------|------------------|--|
|                    | Ireland                           |      | Northern Ireland |  |
| 400                | 50                                |      | 50               |  |
| 275                | n/a                               |      | 40               |  |
| 220                | 40                                |      | n/a              |  |
| 110                | Countrywide                       | 25   | 40               |  |
|                    | Designated sites                  | 31.5 |                  |  |

#### Table 5-1: Short Circuit Current Levels

Table 5-1 also includes short circuit requirements for new users connecting to the Northern Ireland transmission system. Northern Ireland system users are recommended to design their plant and apparatus to withstand short circuit current levels set out in Table 5-1, as a minimum. The design of a user's plant is also subject to detailed short circuit current level assessment.

Changes to the transmission system or the addition of generation can increase the short circuit current levels at nearby<sup>99</sup> stations. Forecast increases in short circuit current levels can indicate transmission system equipment at risk of having its rating exceeded. Should this be the case, it may be necessary to replace this equipment with higher rated plant. Risk mitigation measures may also be implemented to reduce short circuit current levels. Short circuit current levels are calculated for all transmission system nodes in accordance with engineering recommendation G74<sup>100</sup>. Engineering recommendation G74 is based on international standards.

The analysis was carried out for single and three phase faults, for winter peak and summer valley studies. Short circuit current levels were assessed for the years 2020, 2023 and 2026, and the results are presented in Section 5.3.1. A description of the calculation methods used are given in Appendix E. Appendix E also provides the results of the short circuit analysis alongside an explanation of the terms used in short circuit discussions in this document.

Winter peak analysis is carried out to represent the most onerous transmission system conditions, where maximum short circuit currents on the transmission system are most likely to occur.

<sup>97</sup> Short circuit currents are also known as "fault levels".

<sup>98</sup> A short circuit current is an abnormal current that flows along an unintended, low resistance path. Short circuit currents can be extremely high and may cause harm to personnel or damage equipment.

<sup>99</sup> This means stations that are electrically nearby, which does not necessarily mean those geographically closest.

<sup>100</sup> IEC 60909 was an international standard issued in 1988 which provided guidance on the manual calculation of short circuit currents in a three phase AC system. The conservative results produced by this method could result in over investment and Engineering Recommendation G74 was introduced by Electricity Networks Association (ENA) as an outline procedure for computer-based derivation of short circuit currents.

During winter peak analysis, generators that are not providing real or reactive power are switched on in the study and dispatched at o MW. This measure ensures short circuit current contributions from all generator sources are considered in the studies. This ensures the most onerous, but credible, conditions are used for the calculation of short circuit current levels at each bus.

Analysis of summer valley is carried out to indicate minimum short circuit currents on the transmission system based on intact network conditions. The minimum short circuit current at each bus is dependent on generation dispatch and transmission system conditions. Those requiring the expected minimum short circuit current level at a particular bus are advised to contact us directly. During summer valley analysis, generators that were not dispatched were not connected to the system.

Both the maximum and minimum short circuit current level studies assume that the transmission system is in the normal intact condition. The economic generation dispatches for the winter peak and summer valley studies are presented in Appendix D.

The results presented in Section 5.3.1 are the total busbar short circuit current levels. Short circuit current that could flow through each individual circuit breaker may be less than the total busbar short circuit current. This is dependent on network configuration and conditions.

#### 5.3.1. Assessment of Short Circuit Current Levels in Ireland

The transmission system in Ireland is designed and operated to maintain short circuit current levels below the levels in Table 5-1. In planning the system a 10% margin is applied (for example 220 kV short circuit currents will be kept below 36 kA). This is done for security reasons.

As Table 5-1 indicates, while most 110 kV stations in Ireland are designated as 25 kA, the EirGrid Grid Code stipulates that certain 110 kV stations may be designated as 31.5 kA. A new station could be designated as 31.5 kA from the start, or an existing 25 kA station may be changed to 31.5 kA. When a station changes from 25 kA to 31.5 kA, the equipment at that station may need to be modified. Station equipment at lower voltages also needs to be replaced in order to comply with this design rating.

Short circuit current results are presented in Appendix E. The results for Ireland include X/R ratios, transient AC (Ik') and subtransient AC (Ik'') currents. These results provide an indication of the strength of the transmission system.

#### 5.3.2. Assessment of Short Circuit Current Levels in Northern Ireland

The Northern Ireland transmission system is designed and operated to maintain short circuit current levels below equipment ratings. These ratings are listed in the tables in Appendix E, Section E.6.3. The individual substation ratings are based on the lowest rated equipment at each substation.

The Northern Ireland results in Appendix E include transmission substation ratings for:

- AC & DC X/R Ratios;
- Initial Short Circuit Current (I");
- Peak Make Current (ip); and
- RMS Break Current (IB).

The I" and ip values are used to assess the necessary rating of electrical equipment required to close onto short circuit currents.

The IB values are used to assess the capability of electrical equipment required to open and break short circuit current.

#### 5.3.3. Maximum Short Circuit Current Results

Short circuit current results show that a number of Ireland and Northern Ireland transmission nodes have short circuit current levels with the potential to be close to or exceed acceptable levels. Careful management of these issues is needed to ensure short circuit currents remain within acceptable levels.

Figure 5-1 indicates the locations where short circuit current levels are high in 2026. In Ireland the short circuit current level results are represented as a percentage of the levels specified in the Grid Code which are outlined in Table 5.1.

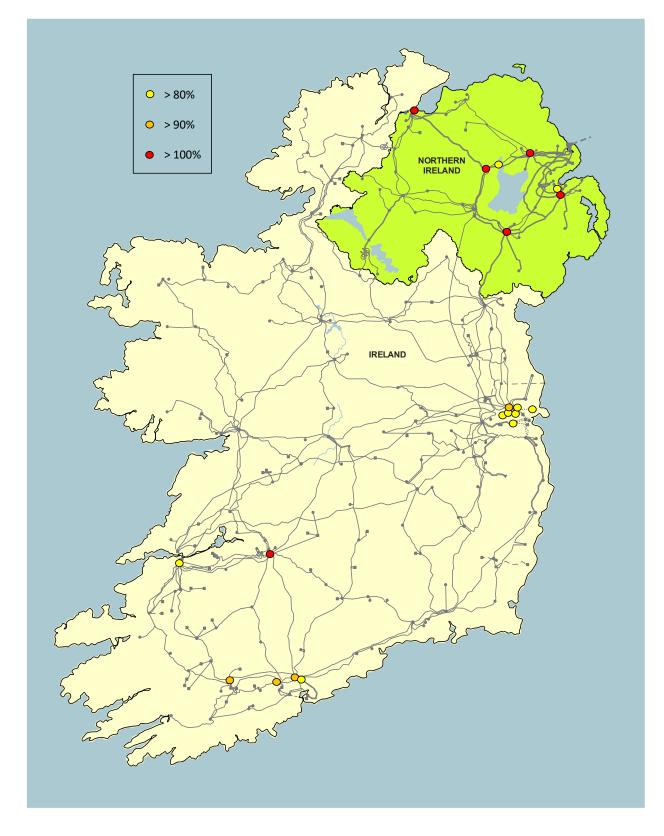
In Northern Ireland the short circuit level results are represented as a percentage of actual equipment ratings.

Three short circuit level ranges are represented in Figure 5-1:

- Yellow dots represent substations where short circuit current results are between 80% and 90% of the ratings;
- Orange dots represent substations where short circuit current results are between 90% and 100% of the ratings; and
- Red dots indicate substations where the short circuit current results exceed ratings.

There are a number of stations where short circuit current levels are anticipated to be above 80% of standard levels and these are indicated in Figure 5-1. We continue to monitor short circuit current levels at all stations and if required we will put mitigation plans and measures in place to ensure that they remain within safety standards. Mitigations include operational measures such as sectionalising parts of the network and investing in new equipment.

The short circuit ratings of Castlereagh, Kells, Magherafelt, Tandragee and Coolkeeragh 275 kV substations in Northern Ireland have been reduced to 10 kA following a review by NIE Networks of the ability of concrete structures at these substations to withstand mechanical forces arising from fault conditions. SONI and NIE Networks will be bringing forward projects to address this issue.



#### Figure 5-1: Short Circuit Current Levels for Winter Peak 2026

Table 5-2 below provides information on the transmission nodes for 2020; 2023; and 2026 where the short circuit current level is above 90% of the relevant level<sup>101</sup>.

<sup>101</sup> In Ireland these results are presented as a percentage of the short circuit current levels specified in the Grid Code which are outlined in Table 5.1, with the exception of KLN/Killonan 110 kV which is presented as a percentage of actual equipment ratings. In Northern Ireland they are a percentage of actual equipment ratings. Please note the Northern Ireland results in 2022 and 2025 take account of planned switchgear upratings in deriving this percentage.

| Rating (%)     | 2020       | 2023       | 2026       |
|----------------|------------|------------|------------|
| >100           | BPS 110 kV | KLN 110 kV | KLN 110 kV |
|                | KLN 110 kV | CAS 275 kV | CAS 275 kV |
|                | CAS 275 kV | CPS 275 kV | CPS 275 kV |
|                | CPS 275 kV | KEL 275 kV | KEL 275 kV |
|                | KEL 275 kV | MAG 275 kV | MAG 275 kV |
|                | MAG 275 kV | TAN 275 kV | TAN 275 kV |
|                | TAN 275 kV |            |            |
| <b>&gt;</b> 90 | CLA 110 kV | CLA 110 kV | CLA 110 kV |
|                | KBY 110 kV | CDU 110 kV | CDU 110 kV |
|                | KRA 110 kV | CPS 110 kV | CPS 110 kV |
|                | STR 110 kV | KBY 110 kV | KBY 110 kV |
|                |            | KRA 110 kV | KRA 110 kV |
|                |            | MEN 110 kV | TAN 110 kV |
|                |            | STR 110 kV |            |
|                |            | TAN 110 kV |            |

Table 5-2: Nodes Approaching or Exceeding Short Circuit Current Levels

#### **Stations Where the Rating Has Been Exceeded**

#### Ireland Transmission Stations Where the Rating Has the Potential to be Exceeded

#### i. Killonan 110 kV (KLN 110 kV)

Studies indicate that the short circuit current level at Killonan 110 kV station has the potential to exceed 100% of the existing substation ratings.

The existing substation is being refurbished to a 220 kV and 110 kV GIS station. The existing AIS station will be decommissioned. This work is due to be completed in 2027. In the interim, we will continue to monitor and manage this risk. If required we will put mitigation plans and measures in place to ensure that the short circuit current level remains within safety standards.

#### Northern Ireland Stations Where the Rating Has Been Exceeded

#### i. Castlereagh, Coolkeeragh, Kells, Magherafelt and Tandragee 275 kV

The short circuit rating of these stations have been reduced to 10 kA following a review by NIE Networks of the ability of concrete structures at these stations to withstand mechanical forces arising from fault currents. SONI and NIE Networks will bring forward projects to address these issues, and will continue to monitor the risk on-site in the meantime.

#### Northern Ireland Stations Where the Rating Has the Potential to be Exceeded

#### ii. Ballylumford 110 kV

Short circuit current level at the Ballylumford 110 kV node has the potential to exceed the existing substation ratings. This occurs under maximum generation conditions when both of the 275/110 kV interbus transformers are in service.

The existing substation is programmed to be replaced with a substation incorporating a new 110 kV GIS switchboard. This work is planned to be completed by 2021. In the interim, we manage this risk by operating with one interbus transformer out of service. This reduces the short circuit current level below the equipment rating.

#### 5.3.4. Minimum Short Circuit Current Results

The minimum short circuit current results are presented in Appendix E. These results indicate minimum short circuit currents on the transmission system based on intact network conditions. These results are representative of the assumed generation dispatch and transmission system conditions.

Any parties requiring the expected minimum short circuit current level at a particular bus are advised to contact us directly.

The Moyle Interconnector has a minimum operating requirement of 1,500 MVA. This is equivalent to a short circuit current level of 3.15 kA. Below this short circuit current level the high voltage direct current (HVDC) interconnector fails to commutate<sup>102</sup>. However, as shown in Appendix E, this is not an issue over the period covered by this TYTFS.

<sup>102</sup> Commutation is the process of reversing the direction of electric current. It is commonly used when turning alternating current to a direct current.

# 6. Overview of Transmission System Capability Analyses





# 6. Overview of Transmission System Capability Analyses

This chapter describes analyses carried out to determine the capability of the transmission system to accommodate additional demand and generation. The results of these analyses<sup>103</sup> provide the basis for the statements of opportunity<sup>104</sup> discussed in Chapter 7 and Chapter 8.

# 6.1. All-Island Demand Opportunity Analysis

This section describes the demand opportunity analysis performed on the Ireland and Northern Ireland power systems. This analysis is used to determine the capability of the transmission system to accommodate additional demand connections at the defined areas. The statements of opportunity presented in Chapter 8 are a result of this demand opportunity analysis.

The all-island demand opportunity analysis is carried out for a single year, 2025. This year gives developers a useful indication as to the demand opportunities that exist in the medium-term on the transmission system. Studies are carried out for the summer period and the winter period of 2025/2026.

In Northern Ireland the demand opportunity analysis provides an indication of capability of the backbone<sup>105</sup> transmission network to accommodate additional demand. In Ireland, the locations analysed for new demand have been carefully chosen based on feedback from industry sources. The chosen stations have been tailored to align with potential areas that are of interest to customers seeking connection to the transmission system.

It should be noted that the results of these studies are dependent on:

- Generation assumptions;
- Demand assumptions; and
- Completion dates of transmission system development projects.

Factors that may influence the results are discussed in Section 6.3.

#### 6.1.1. Approach for Calculation of Demand Opportunity

The transmission system is planned to meet forecast demand levels at all stations in Ireland and Northern Ireland. The demand forecast for each 110 kV station is a proportion of the overall system demand forecast. This forecast is based on historical demand distributions. Future demand customers that have signed connection agreements are also included in station demand forecasts as presented in Chapter 3.

Additional demand connections above the forecast levels are not explicitly catered for in transmission system development plans. However, capacity for additional demand on the transmission system may exist at certain locations. For example, the addition of transmission system infrastructure generally provides a step increase in transmission system capacity. This addition may permit demand connections higher than forecast levels, as illustrated in Figure 6-1.

<sup>103</sup> It is important to note that the statements of opportunity are not only based on these analyses, but also on information presented in other chapters of this document.

<sup>104</sup> Information on how to become a customer can be accessed at the EirGrid and SONI websites as follows: http://www.eirgridgroup.com/customer-and-industry/becoming-a-customer/

http://www.soni.ltd.uk/customer-and-industry/becoming-a-customer/

<sup>105</sup> The backbone transmission system connects local area networks together, enabling the efficient bulk transfer of electricity around the country and beyond.

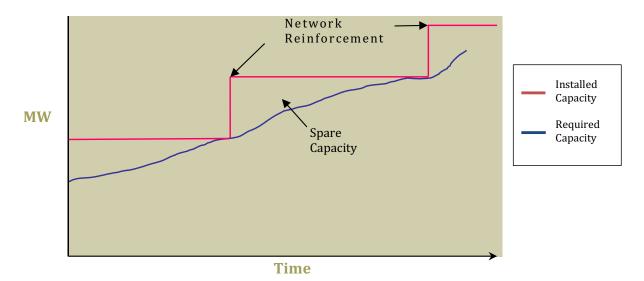
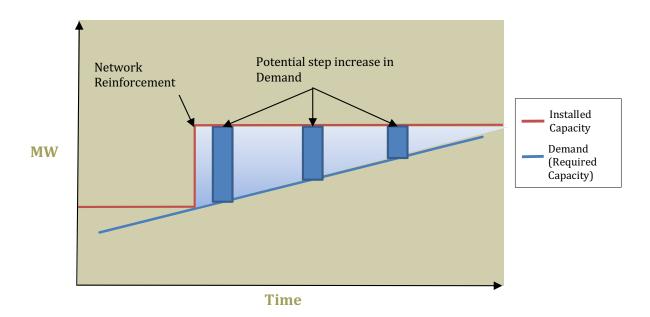


Figure 6-1: Illustration of Typical Step Change in System Capacity Due to the Addition of Transmission System Infrastructure

In Figure 6-1 the blue line represents the required MW capacity at a particular location on the transmission system. The red line represents the installed transmission system capacity. As Figure 6-1 shows, changes in installed capacity generally appear as a step increase following completion of a network reinforcement project. Therefore, following a network reinforcement project there is spare capacity available on the transmission system for a period of time.

In general, demand for electricity increases over time. Figure 6-2 below displays the typical demand growth profile of a typical station. The blue line represents the demand forecast at the station. The blue bars represent potential new step increases in demand that could potentially be accommodated at this typical station.





The analysis examines the transmission system's capability to accept such increased demand above forecast levels. Capability to accept additional demand is examined at a number of 110 kV, 220 kV and 275 kV stations. The stations analysed are distributed throughout Ireland and Northern Ireland, as shown in Figure 8-1 in Chapter 8. The results of this analysis are useful in identifying opportunities for the connection of new or increased demand.

The opportunity value calculated is a measure of the transfer capability remaining in the physical transmission system. It provides an indication of the flexibility of the transmission system to accommodate future demand increases before additional reinforcements are required.

The transfer analysis is intended as a pre-feasibility indication of opportunity for increased demands. The method for determining capacity closely aligns with pre-feasibility study techniques.

In Ireland, the Ireland Transmission System Security and Planning Standards (TSSPS)<sup>106</sup> have been applied in the analyses of demand opportunities. The transmission system is assessed for the loss of any single item of plant (N-1). Unlike generators, demand stations are typically not dispatchable. It is therefore necessary to assess the transmission system performance against standards for maintenance-trip contingencies (N-1-1) in the analysis of increased demand in Ireland.

In Northern Ireland, the Northern Ireland Transmission System Security and Planning Standards (TSSPS)<sup>107</sup> have been applied for analyses of demand opportunities. The transmission system is assessed for loss of any single item of transmission plant (N-1) and loss of a double circuit (N-DCT) all year round. During the summer season the Northern Ireland transmission system is also assessed for maintenance-trip (N-1-1) contingencies for specific cases.

Voltage analysis is performed as part of the demand capacity studies in both Ireland and Northern Ireland. This is because the addition of demand is likely to impact on local voltage levels.

#### 6.1.2. Method for Calculating Limits for Increased Demand Connections

An AC load flow linear algorithm is used to screen critical contingencies for thermal overloads or voltage limitations.

#### What is a load flow?

A load flow is a numerical analysis of the flow of electric power in an interconnected system. Load flow analysis is performed on a power system model to determine steady-state (normal operation) values such as voltages, voltage angles, real power and reactive power.

#### What is a linear algorithm?

A linear algorithm uses an interactive approach to find the solution to a numerical problem, such as determining voltages on the power system. A linear algorithm is a simple and robust method of finding a solution.

Power transfers are considered using dispatch scenarios typically experienced on the transmission system. While these dispatches are typical, we choose them for our analysis to stress the network in terms of power transfers.

By analysing different scenarios that stress the transmission system, we can reasonably ensure that the demand opportunities reported in our analysis will not breach our Transmission System Security and Planning Standards.

The conventional units selected for each dispatch scenario align with market projections for the study year 2025.

**106** http://www.eirgridgroup.com/site-files/library/EirGrid/EirGrid/Transmission-System-Security-and-Planning-Standards-TSSPS-Final-May-2016-APPROVED.pdf

107 http://www.soni.ltd.uk/media/Northern-Ireland-TSSPS-September-2015.pdf

#### **Modelling Details**

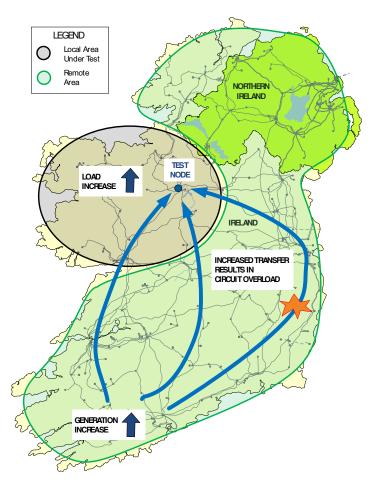
#### For single (N-1) and double circuit (N-DC) contingency studies

- Generators are modelled with their maximum output equivalent to their Maximum Export Capacity (MEC); and
- Local wind generation is switched out in the vicinity of the test station<sup>108</sup>.

#### For maintenance-trip studies (N-1-1)

- Generators are modelled with their maximum output equivalent to their Maximum Export Capacity (MEC); and
- Some centrally-dispatchable generation local to the test station is maximised to its MEC value<sup>109</sup>.

To calculate the opportunity, demand at 0.95 power factor is added to a test station in increasing amounts. This is balanced by an increase in generation<sup>110</sup> outside the local test area. This is illustrated in Figure 6-3 below.



#### Figure 6-3: Illustration of Incremental Transfer Capability Study Method for Demand

The limit for increased transfers to the test station is then established. This is achieved by checking the post-contingency performance of the transmission system against thermal and voltage standards. This process is carried out for each dispatch scenario studied. Issues on the transmission system are not considered limiting unless they are sensitive to the incremental transfers under examination.

<sup>108</sup> As renewable generation is classified as an intermittent energy source, it cannot be relied upon to serve demand. 109 This is implemented to create a more favourable dispatch for the maintenance case. 110 Generation increased as per merit order.

#### **Calculation of Results**

As noted above we undertake a range of contingency studies (N-1, N-1-1, N-DCT) to calculate the capability for increased demand at each station studied.

For the maintenance-trip studies (N-1-1) in Ireland, less onerous generation dispatches can be scheduled to accommodate maintenance outages.

The results of this analysis are reported in Chapter 8. The demand opportunity reported is the lowest demand increase achieved from the range of studies undertaken. It is important to note that results of the demand opportunity analysis are indicative only. Demand opportunity is tested at each station on an individual basis. As such, the opportunities presented are not cumulative. If new demand connects in an area that is currently shown to have capacity, this will then use up some or all of the available capacity in that area.

Potential demand customers should not be discouraged by choosing a site in which there appears to be a lack of transmission system capacity. The actual transmission capacity can only be determined during the connection offer process. Early consultation with us is encouraged so that we can work jointly to explore options relating to any potential proposals and enable timely decision making. Customers considering connecting demand to the transmission system are advised to contact us as early in the project as possible.

#### 6.1.3. Calculation of Capability for Demand in Dublin

The Dublin region is the largest demand centre on the all-island transmission system. Dublin has been and remains the focus of continued interest for the connection of new large demand.

There has been a significant increase in the number of enquiries and applications for new demand connections in the Dublin region and its environs in recent years. Many of these requests are for data centres. Data centres present relatively flat load profiles that impact on both the minimum and maximum demand requirements in the region.

The Dublin 220 kV transmission network is operated by EirGrid, the transmission system operator (TSO). The radial 110 kV circuits are operated by ESB Networks, the distribution system operator (DSO). System development and operation in the area requires both system operators to work closely together. This is to ensure power flows are optimised and to facilitate new connections.

Due to the volume of demand enquiries and applications received for the Dublin area, and their potential impact, Section 8.3 of this document focuses on the demand opportunities in the Dublin region.

The Dublin region has been divided into three geographic zones (see Figure 8-3 in Chapter 8), namely the North, West and South. This is aimed at providing a more detailed insight into the available connection capacity. This takes into account the three main corridors servicing the main bulk supply points<sup>111</sup>.

The methodology used to consider demand opportunities in the Dublin region is based on the existing transmission system. It also includes criteria, such as:

- How each zone is expected to develop; and
- The associated lead times for project delivery.

<sup>111</sup> These main bulk supply points act as the transmission to distribution interfaces in the region.

#### 6.1.4. Calculation of Capability for Demand at Any Station Outside Dublin

This section provides a general example of the analysis of the capability of any station studied in Chapter 8 to accept additional new demand.

The assessment is carried out by simulating the transmission system for summer peak 2025. The station is tested to accommodate increased demand. The relevant demand forecasts and generator dispatches are used.

Due to its variable nature, wind generation cannot be relied on to meet the demand at all times. Therefore, all wind generation in the vicinity of the test station is switched off. Studies are carried out according to the dispatch scenario assumed. The extra demand in each study is met by increasing generation according to the merit order. For each study in turn, a test demand (for example 100 MW) is added to the station under study. The power system is then analysed using an AC load flow linear algorithm.

The analysis tests an exhaustive range of N-1 contingencies (individual circuit/transformer or generator outages) to identify any resultant TSSPS violations. Thus TSSPS violations identify a capacity limit. Some contingencies cause violations of thermal overload or voltage standards at the maximum capacity. In these cases, the analysis reverts to o MW and performs the test in increasing steps, 10 MW in size. The test runs in increasing steps until a violation of thermal overload or voltage standards occurs. The preceding step value is then the calculated capacity value.

In assessing opportunities for new demand, the TYTFS considers the capability of the transmission system only. The capability of the distribution system is not addressed in Ireland or Northern Ireland. The implications for generation adequacy of demand growth above the median forecast levels are dealt with separately in the All-Island Generation Capacity Statement 2020-2029 (GCS) which is available on the EirGrid and SONI websites.

## 6.2. All-Island Generator Opportunity Analysis

This section describes the generation opportunity analysis performed on the Ireland and Northern Ireland power systems. This analysis is used to determine the capability of the transmission system to accommodate additional generation connections at the defined areas. The statements of opportunity presented in Chapter 7 are a result of this generation opportunity analysis.

The generation opportunity for a selection of nodes across the all-island transmission network is presented in Chapter 7. The final year of this forecast statement, 2029, is used in the analysis. The analysis is performed using an AC load flow linear algorithm, the same approach used in the demand opportunity analysis.

In Chapter 7 we also include information on the harmonised all-island Transmission Use of System (TUoS) tariffs and Transmission Loss Adjustment Factor (TLAF) arrangements in the SEM. The all-island TUoS and TLAF arrangements have an objective to provide locational signals to generators that reflect the costs they impose on the transmission system<sup>112</sup>.

This information is provided to help generators make informed decisions when exploring potential transmission network connection locations.

All information relating to generation opportunity presented in Chapter 7 is indicative only. The actual transmission system capacity can only be determined during the connection offer process.

<sup>112</sup> This is not the only objective of the charges and losses arrangements in SEM.

#### 6.2.1. Approach for Calculation of Generation Opportunity

Generation opportunity at a node is assessed via the use of an AC load flow linear algorithm. It is based on the premise that new generation at a particular point on the network will displace generation at a different point on the network. Figure 6-4 presents a simple illustration of the calculation methodology used for the generator opportunity analysis.

All existing generation, and all generation planned to connect in Ireland and Northern Ireland during the period covered by the TYTFS, is considered for dispatch before assessing any further generation opportunity on the all-island transmission network.



Figure 6-4: Generator Opportunities Analysis Methodology

We compiled a list of 110 kV, 220 kV, 275 kV and 400 kV nodes for generation opportunity analysis. These nodes are distributed across the all-island network so that potential users can understand how opportunities vary across the network.

When testing a node, existing generation in the area around the node is maximised; this group of generators is referred to as the source region. The remaining generation required to meet the demand is dispatched based on a merit order. Finally, the test generator is then dispatched.

As the output of the test generator increases, the output from other generation in a separate area of the network - the sink area - is reduced. This forces power flows along specific corridors of the transmission network.

For each incremental increase in new generation capacity at the test node, an AC load flow linear algorithm is used to test the network for compliance with the TSSPS. The generation opportunity is determined once overloads are detected on the network.

For the generation opportunity analysis, single (N-1) and double circuit (N-DCT) contingency studies only are considered.

For each node assessed, three different analyses are performed. Figure 6-5 demonstrates an example of this approach.

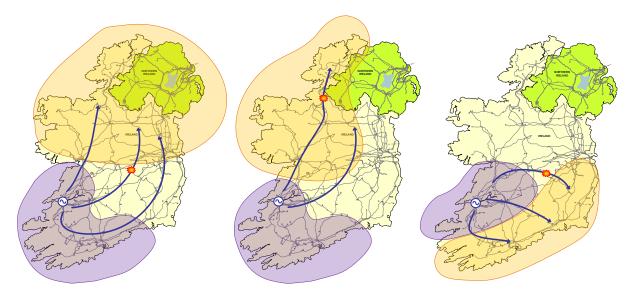


Figure 6-5: Illustration of Incremental Transfer Capability Study Method for Generation

For each scenario in the illustration, the purple area represents the source region where generation is maximised. The test generator is then increased, and generation in the orange area - the sink region - is reduced. The blue arrows represent the resulting power flows. These three scenarios are then repeated for the following network demand scenarios:

- Winter peak;
- Autumn peak (Northern Ireland only);
- Summer peak; and
- Summer valley.

The lowest result from all of the scenarios analysed is used to determine the capacity of the node under test. By analysing several scenarios across different demand scenarios that stress the transmission system, we can reasonably ensure that the generation opportunities reported in our analysis will not breach our Transmission System Security and Planning Standards.

It is important to note that results of the generation opportunity analysis are indicative only. The results of the analysis are not cumulative, as the capability of a node to accept new generation capacity is tested individually.

The transmission system is planned to meet forecast generation levels at all stations in Ireland and Northern Ireland. Additional generation connections above the forecast levels are not explicitly catered for in transmission system development plans. However, capacity for additional generation on the transmission system may exist at certain locations.

Because of the relative size of individual generators, changes in generation installations, whether new additions or closures can have a more significant impact on power flows than demand. New generation capacity will inevitably alter the power flows across the network, which has the potential to create overload problems deep into the network. Problems deep into the network are resolved by network reinforcements known as deep reinforcements.

The generation opportunity analysis presents the level of generation that can be accommodated on the planned transmission system without the need for deep reinforcements to allow full network access.

# 6.3. Factors Impacting On Results

The results of the analyses<sup>113</sup> described in this chapter are based on a set of assumptions. These assumptions are associated with:

- Future demand growth;
- Generation connections; and
- Transmission system developments.

The key forecast factors on which the results depend are dynamic. Therefore, the reality that emerges will not exactly match the forecasts. Consequently, the results, while reasonably indicative, should not be interpreted as definitive projections.

The factors likely to have an impact on the outcomes include:

- The signing of a connection agreement by a new generator;
- Delays in connection of committed new generation stations;
- Closure of existing generation stations;
- Changes in the economy which give rise to consequential changes in the overall demand for electricity;
- Changes in demand in a particular region or area, arising from new industry developments or closures;
- Delays in the provision of transmission system reinforcements; and
- Selection and construction of new transmission system reinforcement developments which may significantly increase transmission system capacity.

<sup>113</sup> The results are presented in Chapter 7 and Chapter 8.



# 7. Transmission System Capability for New Generation





# 7. Transmission System Capability for New Generation

# 7.1. Summary of analysis

The results of the generation opportunity analysis for this statement show that generation opportunities have reduced since the previous statement. With significant quantities of renewable generation connected across the island, future generation connections in the North-West, West and South-West regions would require network reinforcements.

The areas with the greatest opportunity for additional generation are at nodes on the 275 kV ring in Northern Ireland, and 220 kV stations in the Dublin area.

## 7.2. Background

In this chapter we provide the results of the detailed generation capacity opportunity analysis, of which the calculation methodology is described in Chapter 6.

The analysis considers the final year of this statement – 2029 – and details the opportunity for connecting further generation beyond the assumed installed generation portfolio. The results provide potential network users with a guide to the ability of the all-island transmission system to accept new generation. It must be stressed that this analysis is indicative only; the actual transmission network capacity can only be determined during the connection offer process. This process requires detailed network assessments to determine the optimal connection arrangement that complies with the Transmission System Security and Planning Standards (TSSPS) in Ireland and Northern Ireland.

Changes to generation dispatch patterns and the geographical location of generation can have an impact on all-island transmission network power flows. As a consequence, Generator Transmission Use of System (GTUoS) tariffs and Transmission Loss Adjustment Factors (TLAFs) can change, resulting in an impact on the economics of power generation. Resulting regional changes in GTUoS and TLAFs are described to help generators make informed decisions when exploring potential transmission network connection locations.

# 7.3. New Generation Capacity

The level of generation expected to connect to the all-island transmission system is described in detail in Chapter 4 of this statement.

The largest recent generation capacity increase has been wind generation. At the freeze date of January 2020 there was about 5,400 MW connected to the all-island transmission system.

This generation is mainly connected in remote locations in the South-West, West and North-West of the island of Ireland. At times of high wind generation, this can result in very high power flows on transmission circuits supplying power to the large demand centres on the East coast of Ireland and Northern Ireland.

Currently there is a relatively small amount of solar generation capacity connected to the all-island transmission system.

In contrast, there are a number of large conventional power stations due to retire or to have restricted output due to the EU Industrial Emissions Directive. These are detailed in All-Island Generation Capacity Statement 2020-2029<sup>114</sup> and noted in Chapter 4 of this document.

<sup>114</sup> http://www.eirgridgroup.com/site-files/library/EirGrid/All-Island-Generation-Capacity-Statement-2020-2029.pdf

# 7.4. Generation Opportunity

#### 7.4.1. At Selected 220 kV, 275 kV and 400 kV Stations

This section provides the opportunities for additional generation on the 220 kV, 275 kV and 400 kV networks in 2029. For these high voltage stations, new generation of up to 550 MW in size was considered for assessment. Figure 7-1 illustrates the stations selected across the all-island network, and their resultant generation opportunity. It is important to note that the results are not cumulative, as the opportunity at each station is assessed individually. The capacities shown are relevant to the station tested, but also provide an indication of the opportunities available at neighbouring stations.

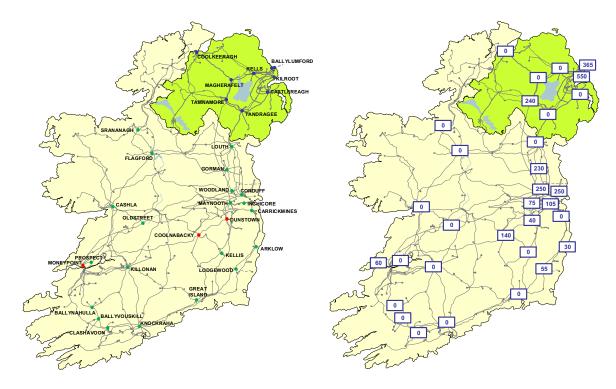


Figure 7-1: Generation opportunity at 220 kV, 275 kV and 400 kV stations in 2029

In general, there is no opportunity for new generation in the North, West and South of Ireland. The transmission network in these areas has significant levels of connected and planned renewable generation, and also in the south there are efficient conventional gas generators and plans for further interconnection. As a result, there is little to no additional capacity available. In the East and to a lesser extent South-East regions, there is opportunity for new generation, being located closer to the large demand centres.

With the potential development of large data centres in the Dublin area, there will be increased generation opportunities at stations around Dublin beyond that indicated in this analysis.

In Northern Ireland, there is currently very little opportunity for new generation in the North-West region, although this may change in future. Similar to Ireland, this area has significant levels of renewable generation, both connected and planned, and the transmission network is almost entirely comprised of 110 kV circuits. There is currently no capacity for new synchronous generation to be directly connected at Coolkeeragh, Magherafelt, Tandragee, Castlereagh and Kells 275 kV stations. This is because the mechanical forces created by the additional fault current of directly connected generation would exceed the original design specification. SONI and NIE Networks will be bringing forward projects to address this issue, however these are at an early stage. The fault contribution from non-synchronous connections such as wind farms and data centres tend to be significantly smaller, particularly those likely to connect at 110 kV. Any such potential connection at these nodes would be assessed based on its fault current contribution.

#### 7.4.2. At Selected 110 kV Stations

A number of 110 kV stations were also analysed to complement the higher voltage stations analysed in Section 7.4.1. For these stations, new generation of up to 200 MW in size was considered for assessment. The stations, and their resultant generation opportunity, are displayed in Figure 7-2.

As in the previous section, the results are not cumulative, as the opportunity at each station is assessed individually. The capacities shown are relevant to the station tested, but also provide an indication of the opportunities available at neighbouring stations.

As expected, there is very little opportunity for generation connection at 110 kV. By 2029 in Ireland, there is a high level of renewable generation connected to both the transmission and distribution systems. This is concentrated in the North-West, West and South-West, and the installed capacities exceed the demand in these areas.

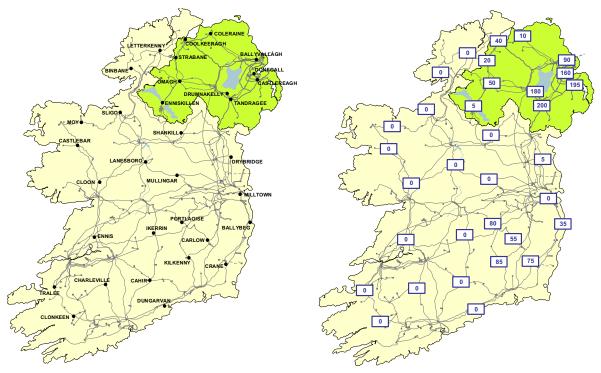


Figure 7-2: Generation opportunity at 110 kV stations in 2029

In the South-East and East of Ireland, there is opportunity available at some 110 kV nodes. The largest demand centres are located in these areas, and the transmission network is stronger. Additionally, renewable generation penetration is lower in these areas. Connection studies would be required to determine the available capacity and connection arrangements.

Not dissimilar to Ireland, Northern Ireland is connecting high levels of renewable generation, with more planning to connect to the transmission and distribution systems by 2029. This generation in the North and West of Northern Ireland is greater than local demand and causes congestion on the transmission network.

In the East of Northern Ireland, opportunities for generation connection are possible, with a less congested transmission network and higher demand density. Again, detailed connection studies would be required to determine the available capacity and connection arrangements.

# 7.5. Generation Locational Tariff Signals and Their Impact on Transmission Network Capacity

Harmonised transmission arrangements provide locational signals to users reflecting the costs they impose on the transmission system. TLAFs and GTUoS tariffs, as part of harmonised transmission arrangements, can provide generators with locational signals informing their decision on where to connect to the grid and incentivise efficient generation dispatch.

Electrical losses, which occur as electricity is transported along transmission circuits, are accounted for in the settlement process with the application of TLAFs. Some units are responsible for proportionally more transmission losses than others, depending on their point of connection to the grid and use of transmission network capacity.

The methodology used by the transmission system operators (TSOs) to calculate the TLAFs has been approved by the regulatory authorities<sup>115</sup>.

The most efficient way to transfer power in terms of losses is to minimise the distance between generation and demand, and not to heavily load lines. Due to the location and amount of demand and generation, power can be transmitted over sizeable distances. If the power generated in a region is in excess of the demand in that region, the excess generation will be utilised some distance away from the source.

The transmission network consists of high voltage overhead lines and cables ranging from 110 kV to 400 kV. When current flows across these circuits, some energy is lost as heat. The higher the power transmitted on a line, the higher the current. Current has a squared relationship to power losses, therefore if the power on a line is doubled, the losses will increase by a factor of four.

In general, transmitting power on a higher voltage level will lower the associated current. The associated losses will be dependent on how congested the line is; increasing power on an already congested line will result in greater losses than increasing power on a similar less congested line.

The Transmission Use of System (TUoS) tariff is the main tariff for transporting power in bulk across the power system. Generator Transmission Use of System (GTUoS) tariffs contains a locational component, which provides a signal of the costs associated with a generator's use of the transmission network.

Such signals provide a commercial incentive for generators to make informed decisions (both siting/entry and exit decisions) concerning their use of the transmission system. This is intended to improve efficiency in respect of both the use of, and investment in, the transmission system.

#### 7.5.1. TLAFs

Generator TLAFs are reflective of their contribution to transmission losses. The principle is that market participants that contribute more to transmission losses, due to their location, should have a lower TLAF, than those generators who contribute less to transmission losses. The regional average 2020/21 TLAF values are shown in Figure 7-3, and are based on the published approved 2020/21 TLAF values<sup>116</sup>.

<sup>115</sup> http://www.eirgridgroup.com/site-files/library/EirGrid/TLAF-Methodology-Explanatory-Paper-v1.o.pdf 116 http://www.eirgridgroup.com/site-files/library/EirGrid/Approved-TLAFs-2020-2021-v0-1.pdf http://www.soni.ltd.uk/media/documents/Approved-TLAFs-2020-2021-v0-1.pdf

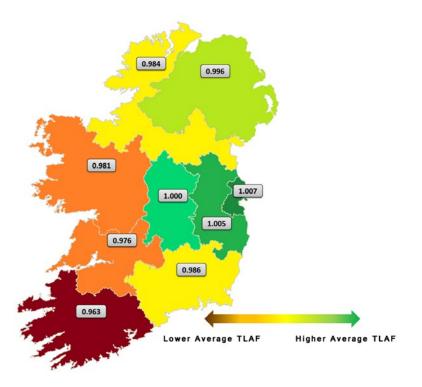


Figure 7-3: All-island 2020/21 regional average TLAF values

Figure 7-4 shows the change in TLAFs between 2019/20 and 2020/21. These changes are influenced by yearly dispatch, demand and topology changes.

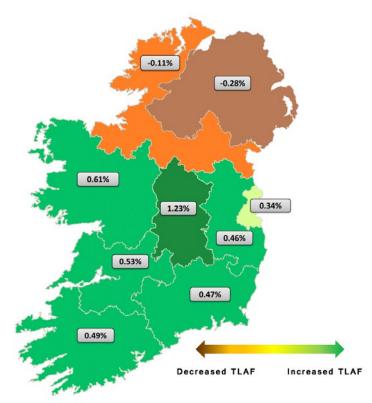


Figure 7-4: Percent (%) TLAF Change between 2019/20 & 2020/21

The information presented in Figures 7-3 and 7-4 should be used as regional indicators. For the 2020/21 tariff year the average all-island TLAF has increased by 0.26%. In the Northern Ireland area, Figure 7-4 shows the average TLAF value has decreased slightly between 2019/20 and 2020/21; however, as shown in Figure 7-3, the average TLAF value remains high and above average when considering all-island TLAFs. TLAFs for the Dublin region are relatively high as there tends to be local use of generation, with an increasing demand. Local use of generation also typically supports the relatively high Northern Ireland TLAFs. Further information on the 2020/21 TLAFs can be found on the EirGrid and SONI websites<sup>117</sup>.

#### 7.5.2. GTUoS

The regional average 2020/21 GTUoS tariffs are shown in Figure 7-5, and are based on the approved 2020/21 GTUoS tariffs. Higher GTUoS tariffs are reflective of transmission investment costs linked to a generator's use of the system. This promotes efficient use of the transmission system by generators, which should, in turn, facilitate efficient investment in the transmission system.

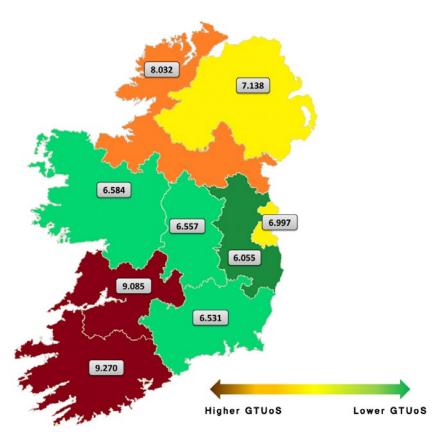


Figure 7-5: All-Island 2020/21 regional average GTUoS values

<sup>117</sup> http://www.eirgridgroup.com/site-files/library/EirGrid/Approved-2020-2021-Transmission-Loss-Adjustment-Factors-(TLAFs)-Accompanying-Note.pdf

Figure 7-6 shows the change in GTUoS tariffs between 2019/20 and 2020/21.

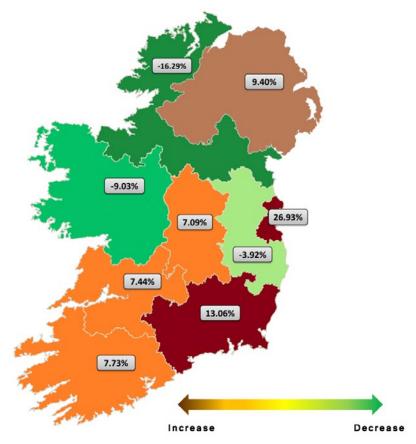


Figure 7-6: Percent (%) GTUoS change between 2019/20 & 2020/21

For 2020/21, there is an overall increase in tariffs due to a 4% increase in the all-island revenue; regional changes are attributed to changes in network flows and local reinforcements. The annual revenue is the amount allowed to build, operate and maintain the transmission network, and this has increased in Ireland and decreased in Northern Ireland for 2020/21.

GTUoS tariffs have increased on average by 4.79% from those of 2019/20, which is higher than the revenue change, as there are fewer MWs in the model to spread the cost around, due to two conventional units having now closed. The base flows are relatively similar to those of 2019/20and as a result there are similar trends to those of 2019/20. Significant changes in some areas are due to reinforcements joining or leaving the 12 year cost window. As shown in Figure 7-6, GTUoS tariffs for Northern Ireland are 9.4% higher than those of 2019/20 but are still around 5.9% lower than the average Ireland GTUoS tariff for  $2020/21^{118}$ .

**<sup>118</sup>** http://www.eirgridgroup.com/site-files/library/EirGrid/2021-Approved-GTUoS-Tariffs.pdf http://www.soni.ltd.uk/media/documents/2021-Approved-GTUoS-Tariffs.pdf

# 7.6. Assumptions behind the TLAF and GTUoS models

#### 7.6.1. TLAFs

The assumptions used to determine TLAFs are from the Imperfections Forecast model, and essentially are a snapshot of a particular study year, comprised of complex and detailed data. This data is collected up to a data freeze point just before the calculation process; this ensures they are as reflective as reasonably practicable for the study year.

For the level of detail involved specifically for calculating TLAFs, the assumptions are only valid for the study year.

Due to the complexity and variability of these assumptions, their collective impact on TLAFs is neither predictable nor forecastable. Looking beyond the study year, assumption data becomes increasingly speculative and could not be considered as reasonable data for the TLAF model.

#### 7.6.2. GTUoS

The GTUoS model includes an element of 'looking to the future' by incorporating the future network. Looking at the future network involves including the next five years of network files in the model. The network files are consistent with the information published in the latest version of this document available at the time of calculation.

Indicative asset costs for a 12 year window are also included in the GTUoS model (looking five years forward and seven years back). Under normal circumstances this starts when the asset first appears in the 'Year+5' network file, until seven years post-commissioning.

GTUoS tariffs are calculated on an all-island basis, and assumptions or network changes from one jurisdiction can have an impact on the other. For example, if the revenue to recover in Ireland significantly increased, and the revenue to recover in Northern Ireland remained the same as the previous year, the average all-island tariff would increase as there is a greater all-island revenue to recover. Local variations would then be related to changes in network flows. Another example could be interconnector flows, where an assumption for Moyle impacts flows in Ireland, and an assumption for EWIC impacts flows in Northern Ireland.

Although there is an element of forecasting in the GTUoS model by looking at the future network and associated costs, alongside this are many assumptions and variables that only apply for the study year.

## 7.7. How to Use the Information for Generation

Generation developers wishing to use the information contained within this section when considering where to connect should follow these steps:

- Consult the maps in Appendix A to find the nearest transmission station to the proposed development. Also, consider the regions and nodes identified in Section 7.4 which are indicating opportunity for generation connections.
- Consult the forecast increase and retirement of generation within a region. Consider the impact of changes to the transmission system since the analysis was carried out. Consider short circuit current levels at the nearest transmission station.
- Discuss your project with EirGrid or SONI as early as possible.
- If seeking to apply for a connection, refer to the EirGrid connection application process or the SONI connection application process.

# 8. Transmission System Capability for New Demand





# 8. Transmission System Capability for New Demand<sup>119</sup>

This chapter presents demand opportunity analysis which assesses the capability of the existing and planned transmission system to accommodate increased demand. Opportunities for further demand connections in Ireland and Northern Ireland are discussed.

A significant amount of conventional generation in Ireland and Northern Ireland is expected to close over the period covered by this statement. For the purpose of the TYTFS 2020 analysis, it is assumed that the Capacity Market, which is overseen by the SEM Committee, will deliver sufficient power in appropriate locations to ensure generation adequacy and security of supply are maintained.

It is important to note that we are currently working with CRU and the Department of the Environment, Climate and Communications (DECC) to address short to medium term generation adequacy concerns in Ireland. In Northern Ireland, we are mindful that the Capacity Market will ensure adequate generation until the North South Interconnector is delivered. Current analysis and projections for Northern Ireland indicate there is sufficient capacity in the short to medium term to meet system needs.

There continues to be a significant volume of enquiries and applications for the connection of large energy users such as data centres in the Dublin region (see Chapter 3). This is addressed in Section 8.3, in which a qualitative approach to describe demand opportunities in the Dublin area is presented.

## 8.1. Transmission System Demand Capability Obligations

This chapter of the TYTFS is published in order to meet the requirements of EirGrid's Section 38 of the 1999 Electricity Act and Condition 33 of SONI's TSO licence.

The analysis illustrated in Chapter 8 is presented to provide a high-level indication of transmission network capacity for developers. Results from demand capability studies are based on a specific set of assumptions (see Chapter 6) which may be subject to change. Developers wishing to connect to the transmission system will therefore require further detailed studies.

The TYTFS is not intended to have any legal effect on the negotiation of contractual terms for transmission system connections. Before making any commercial decisions developers should contact us for discussions on their proposed developments.

## 8.2. All-Island Transmission System Capability for New Demand

As detailed in Chapter 6, the transmission system's capability to accommodate new demand is assessed using demand opportunity analysis. The study was performed for 2025 winter and summer peaks.

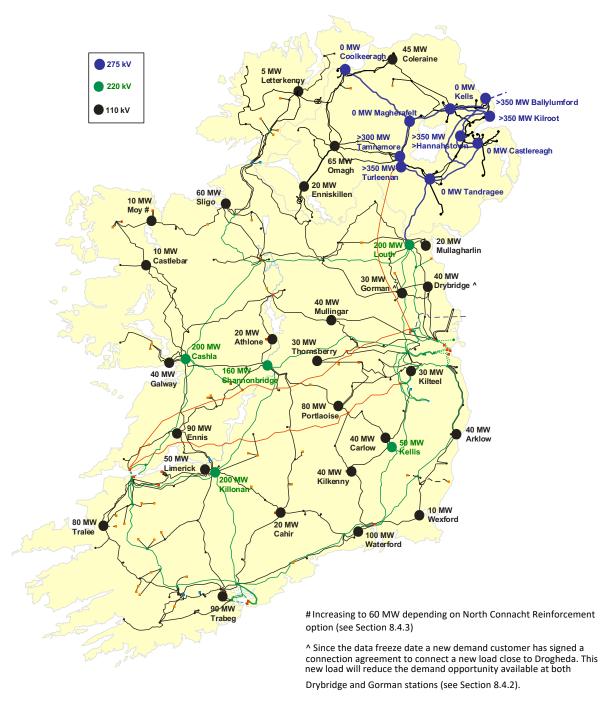
Data used for the demand opportunity analysis is based on the best available information at the January 2020 data freeze date. The results of the demand opportunity analysis presented in this chapter are based on the following assumptions:

119 Information for potential demand connections can be accessed at the following addresses: http://www.eirgridgroup.com/\_\_uuid/463e7512-d115-4d94-b1ab-79b8cb366f73/index.xml and http://www.soni.ltd.uk/\_\_uuid/463e7512-d115-4d94-b1ab-79b8cb366f73/index.xml

- Year 2025 demand forecast was used (see Appendix C);
- Only transmission reinforcements with capital approval which were planned to be completed by 2025 at the data freeze date were included in the analysis);
- Planned generation up until 2025 at the data freeze date was included in the analysis
- Variable generation cannot be relied upon to serve demand. As such, variable generation local to the test station was switched out; and
- The 2025 transmission system was assessed for the loss of a single transmission asset (N-1), maintenance-trip (N-1-1) and loss of a double transmission circuit (N-DC, Northern Ireland) contingencies.

We analysed 41 transmission stations throughout Ireland (excluding Dublin) and Northern Ireland. These consisted of twenty-six 110 kV stations, five 220 kV stations and ten 275 kV stations. These stations were analysed to help identify locations that are potentially suitable for major industrial load centres with large power requirements. The stations examined and their accompanying results are shown in Figure 8-1. Opportunities in Dublin are discussed separately in Section 8.3.

It should be noted that demand opportunity is tested at each station on an individual basis. As such, the opportunities presented are not cumulative. If new demand connects in an area that is currently shown to have capacity, this will then use up some or all of the available capacity in that area.



#### Figure 8-1: Capability for Additional Demand at 275 kV, 220 kV and 110 kV Stations in 2025

As a general rule, demand opportunity at a particular station would tend to reduce over time. This is due to normal demand growth using up available capacity. Yet, in many cases demand opportunities can improve as a result of planned transmission system or generation developments.

The results of the analysis are presented on a regional basis below. The results indicate that in 2025 there will be opportunities at all the stations examined.

# 8.3. Opportunities for New Demand in the Dublin Area

#### 8.3.1. Context

Dublin is the largest load centre on the island of Ireland. We include this section due to the considerable interest and number of enquiries for connection to the grid around Dublin (see Chapter 3 Demand). The volume of enquiries and the uncertainty of their final power requirements require us to make a qualitative assessment of demand opportunities for the future.

The scale of individual demand connection enquiries to the transmission system vary from 20 MW to some possibly extending to over 250 MW in the final stages of development. The enquiries are mainly comprised of data centres that support the information, communications and technology (ICT) infrastructure of large multinational companies.

#### 8.3.2. The Dublin Network

The diagram in Figure 8-2 represents the 220 kV backbone transmission system in the greater Dublin area. There also exists a 110 kV network in the Dublin area. However, for clarity we have not shown it in Figure 8-2.



Figure 8-2: Dublin Area 220 kV Transmission System

Electricity is supplied within Dublin via a 220 kV network arranged in a figure of eight. A combination of operational arrangements and network devices can create open points that effectively divide the Dublin 220 kV network into north and south rings as required.

This network configuration is primarily used to maintain fault currents at safe levels should a network fault occur. It also prevents excessive power flows through the Dublin region. Dublin is then fed via the underlying 110 kV distribution infrastructure which is mainly arranged radially from transmission bulk supply point (BSP) interface stations (220/110 kV).

The larger Dublin power stations are located at Huntstown, which is made up of two separate generators, in North Dublin and one each at Irishtown and Shellybanks in Dublin Bay. The combined capacity of these four stations is approximately 1,600 MW. The 500 MW East West Interconnector is connected to Woodland 400 kV station on the periphery of North Dublin.

Analysis is carried out to ensure compliance with the Transmission System Security and Planning Standards (TSSPS) for all new connections to the transmission system.

This ensures the co-ordinated development of a reliable, efficient, and economical system for transmission system users. EirGrid must ensure the performance requirements of the TSSPS are met. For example, the thermal capacity limits of equipment must be maintained for all operating conditions.

To ensure the optimised, efficient and economic development of the network, EirGrid aims to make maximum use of existing assets. This can be achieved by using generation output to help offset power flows on the network and avoid the need for reinforcement. The cost of using generation in this way is compared to the cost of new network reinforcements.

There are primarily three limitations that can restrict the availability of transmission capacity in Dublin:

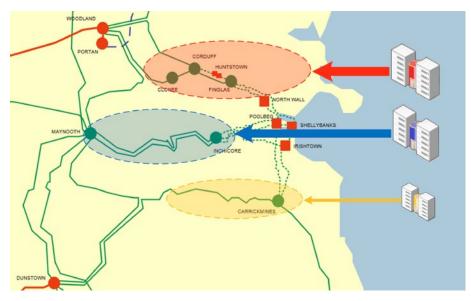
- 1. Limitations at the 220/110 kV interface stations, these can include restrictions due to the 220/110 kV transformers or spatial constraints;
- 2. Power flow limitations on local transmission circuits within Dublin; and
- **3.** Limited capacity on circuits outside Dublin in terms of facilitating large power flows across the transmission network.

Generation dispatch is critical in assessing the capability of the network and can have a significant impact on (2) and (3) above, especially in the case of Dublin.

The power delivered to Dublin demand centres can originate from power sources located within or outside Dublin or a combination of both. This is dependent on wholesale electricity market generation costs in the Single Electricity Market (SEM) as well as network or system issues.

#### 8.3.3. Dublin Transmission Development Plans

Figure 8-3 below describes the areas of focus for demand connections in Dublin and the scale of interest in each zone. The connections fall into three zones: North, West and South Dublin.



#### Figure 8-3: Dublin Potential Demand Connections

Depending on the level of future demand connections, new large scale generation, transmission solutions, demand side response and/or storage will be required to ensure continued security of supply.

Each zone is described below with consideration given to existing transmission infrastructure, transmission network projects and lead-times.

Should the reader require more detailed transmission network project information please read our latest Transmission Development Plan and Associated Transmission Reinforcement (ATR) update, both of which are available on the EirGrid website.

#### 8.3.4. North Dublin

North Dublin has two 220/110 kV interface stations at Corduff and Finglas with another planned at Belcamp. In addition, there is a 220 kV directly connected customer interface station at Clonee. The level of interest for connection in North Dublin is the highest of all Dublin areas.

A number of transmission projects are in place to increase the network capacity and security of supply in this area. They are summarised in Table 8-1 below.

| North Dublin             |  |   |
|--------------------------|--|---|
| Project Name/Number      | Project Description                                  | Estimated Delivery Date at<br>Data Freeze |
| Belcamp (CPo437)         | New 220/110 kV station                               | 2020                                      |
| Belcamp Phase 2 (CPo984) | Additional 220/110 kV transformer and second circuit | 2022                                      |
| Finglas (CPo646)         | 110 kV station redevelopment                         | 2023                                      |
| Finglas (CP0792)         | 220 kV station redevelopment                         | 2023                                      |

#### Table 8-1: North Dublin Projects

As noted in our Transmission Development Plan we have confirmed the need for further investment in north Dublin. In response, we are progressing the East Meath-North Dublin Network Reinforcement (CP1021). This could be in the form of increased network connectivity between Woodland 400 kV station and a transmission station in North Dublin. Typically, such major projects delivering additional network capacity have significant lead times (five to ten years or more) which are dependent on the chosen technology.

#### 8.3.5. West Dublin

West Dublin has one main 220/110 kV interface station at Inchicore with another planned at Castlebagot<sup>120</sup>. These stations are supported by the Maynooth 220/110 kV station on the outer rim of the Dublin region.

A number of transmission projects are in place to increase the network capacity and security of supply in this area. They are summarised in Table 8-2 below.

| West Dublin                   |                                  |   |
|-------------------------------|----------------------------------|---|
| Project Name/Number           | Project Description              | Estimated Delivery Date at<br>Data Freeze |
| Ryebrook-Corduff (CPo668)     | Uprate 110 kV line               | 2020                                      |
| Castlebagot (CPo872)          | New 220/110 kV station           | 2020                                      |
| Maynooth-Woodland<br>(CPo869) | Uprate 220 kV line               | 2022                                      |
| Inchicore (CPo692)            | 220 kV station upgrade           | 2025                                      |
| Maynooth (CPo8o8)             | 220/110 kV station redevelopment | 2027                                      |

#### Table 8-2: West Dublin Projects

<sup>120</sup> Formerly known as West Dublin 220/110 kV station.

As noted in our Transmission Development Plan we have confirmed the need for further investment in this area. In response, we are progressing the Kildare-Meath Grid Upgrade (also known as Capital Project 966) which seeks to increase the strength of the link between two existing 400 kV stations at Dunstown and Woodland.

#### 8.3.6. South Dublin

South Dublin has one main 220/110 kV interface station at Carrickmines. Carrickmines is connected at 220 kV to Dunstown 400/220 kV station and Arklow 220/110 kV station.

A transmission project was being progressed, at the data freeze date, to increase the network capacity and ensure continued security of supply in this area. It is summarised in Table 8-3 below.

#### Table 8-3: South Dublin Projects

| South Dublin          |   |   |
|-----------------------|---|---|
| Project Name/Number   | Project Description                                     | Estimated Delivery Date at<br>Data Freeze |
| Carrickmines (CP0580) | New 220/110 kV 250 MVA<br>transformer & GIS development | 2020                                      |

## 8.3.7. Impact of Additional Generation & Flexible Demand on North, West and South Dublin

As described in Chapter 7, there are generation opportunities in the Dublin region, particularly in north Dublin. If additional generation was to locate in the Dublin area this would generally improve the network capacity available for transmission system users in North, West and South Dublin zones.

However, the specific location of any proposed additional generation would have to be assessed to fully understand its full impact on the network.

Similarly, if major demand customers can ensure demand side flexibility during low probability system events this would also improve the capability of the network to accommodate further demand increases.

#### 8.3.8. Looking Forward

In January 2017 we published an updated grid development strategy for the long-term development of the network. In the strategy paper<sup>121</sup>, we explain the role of electricity transmission infrastructure in supporting new investments and jobs as well as ensuring competitiveness by offering cost-effective power capacity.

The strategy puts forward a number of major projects to upgrade the transmission network. The Regional Solution (see Chapter 2) and the Kildare-Meath Grid Upgrade (Capital Project 966) have many system benefits, which include providing additional network capacity and improving security of supply for the eastern side of Ireland.

The Regional Solution involves a new circuit across the Shannon Estuary and the installation of series compensation equipment on the 400 kV circuits that extend from Moneypoint 400 kV power station in the West of Ireland towards Woodland and Dunstown 400 kV stations located on the western outskirts of Dublin.

This project will greatly enhance the capability of the existing 400 kV circuits to transfer bulk power generated in the South-West and West to Dublin and other demand centres in the East as illustrated in Figure 8-4.

<sup>121</sup> http://www.eirgridgroup.com/the-grid/irelands-strategy/

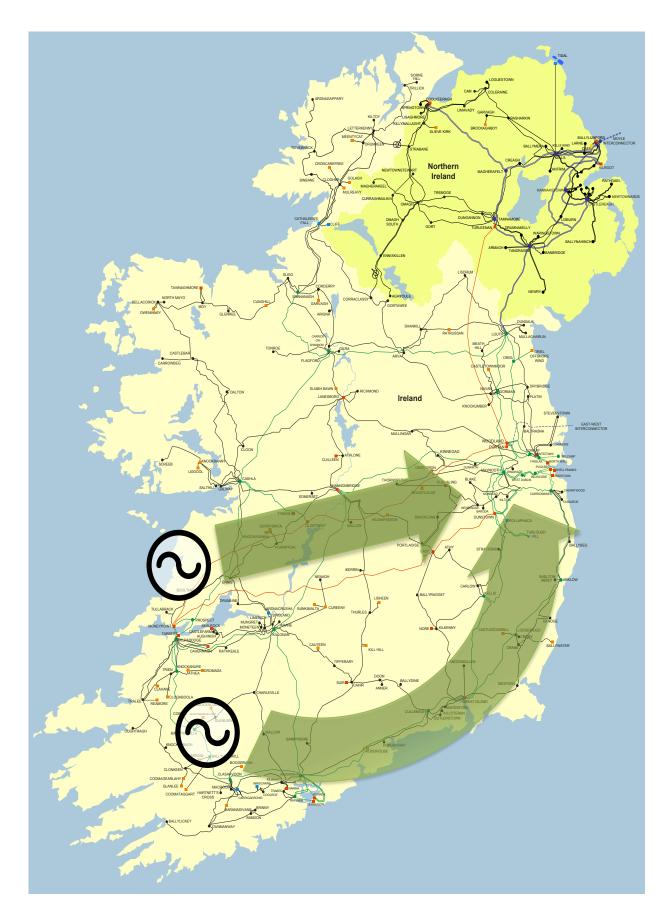


Figure 8-4: Transfer of Power Generated in the West and South-West Regions to the East

The Kildare-Meath Grid Upgrade is at an early point in the project life-cycle. The project will increase the strength of the link between two 400 kV stations at Dunstown and Woodland. This will provide benefits by reducing power flows that pass through the Dublin 220 kV transmission network.

To maintain system stability and facilitate significant inter-regional power flows we are also developing a number of voltage support solutions across Ireland.

In addition, as noted in our Transmission Development Plan, we have confirmed the need for investment in north Dublin. The future project is called the East Meath-North Dublin Network Reinforcement (CP1021).

#### 8.3.9. Summary

New transmission solutions will be required to strengthen the grid. These solutions are being progressed.

We continue to apply a strategic approach to network development and we are continuously considering the approach to the level of demand enquires. Our strategic approach takes account of the following:

- Companies developing data centres operate in a rapid and dynamic environment. Their business requires connection timescales that are short relative to time taken for transmission reinforcement. Most are considering being operational within two to three years and growing their power usage rapidly thereafter.
- We are working to understand the needs of these developers and their impact in terms of our grid development strategy. We are publishing information on the system adequacy, grid needs and opportunities to ensure transparency so that the impacts of this sector and its developments are known.
- We will continue to examine innovative solutions and technologies in response to future requests. However, as interest in connecting additional demand has developed into contracted connections, the available capacity on the existing transmission network for further large scale demand connections has been depleted.

It is advised that any potential new demand consumers contact EirGrid early so that the available connection options can be considered.

### 8.4. Transmission System Capability for New Demand in Ireland

Demand opportunities available on an Ireland regional basis are discussed below. Results presented in this section are based on the assumptions detailed in Chapter 6.

#### 8.4.1. Opportunities for New Demand in the Midlands and West

The demand opportunities available in the Midlands and West are shown in Figure 8-5. It is shown that there are potential demand opportunities available for new customers at stations examined in the region<sup>122</sup>. In particular, Cashla and Shannonbridge 220 kV stations would be suitable connection points for major industrial load centres. Both of these stations are capable of accommodating significant additional demand without additional network reinforcements.

<sup>122</sup> Please note that the demand opportunities results are not cumulative. Each station is assessed individually, taking account of forecast demand growth only at stations outside of the test node. These figures are indicative only, with further detailed assessment of each station required. Customers considering connecting demand to the Irish transmission system are advised to contact EirGrid as early in the project as possible.

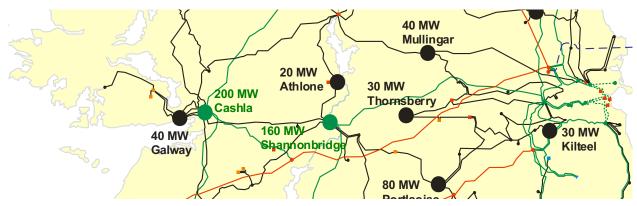


Figure 8-5: Capability for Additional Demand in Midlands and West Regions

#### 8.4.2. Opportunities for New Demand in the North-East

The demand opportunities available for the North-East region are shown in Figure 8-6. It is shown that there are potential demand opportunities available for industrial customers at stations examined in the region. The delivery of the North South interconnector aids demand opportunity in the North-East. The North South interconnector provides a route for large power transfers to flow between Northern Ireland and Ireland via the North-East region of Ireland. The North South interconnector will benefit potential demand customers connecting in this region by releasing more capacity on the underlying 110 kV network.

Potential overloading of the Louth – Mullagharlin and Dundalk – Louth 110 kV lines is responsible for limiting the opportunity at Mullagharlin. The overload occurs during winter and summer peaks for single circuit outage conditions. This is a local issue as only two circuits supply the load at Mullagharlin. Drybridge is more interconnected with four circuits supplying the station. Thus, it has a higher demand opportunity. It should be noted that since the data freeze date a new demand customer has signed a connection agreement to connect a new load close to Drogheda. This new load will reduce the demand opportunity available at both Drybridge and Gorman stations.

Demand opportunity studies were performed at Louth 220/110 kV station. Louth is capable of accommodating significant additional demand without additional network reinforcements.

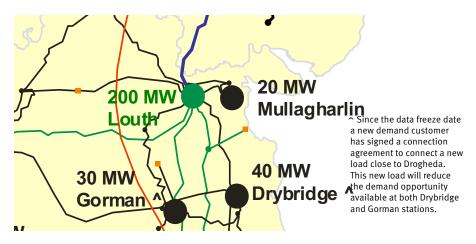


Figure 8-6: Capability for Additional Demand in North-East Region

#### 8.4.3. Opportunities for New Demand in the North-West

The demand opportunities available for the North-West region are shown in Figure 8-7. It shows that there are potential demand opportunities available for industrial customers at all stations examined in the region. The potential demand opportunity at Castlebar is 10 MW. Analysis has shown that the 110 kV lines supplying Castlebar could overload under certain maintenance-trip scenarios (see Chapter 6).

Demand opportunity studies were performed at Moy 110 kV station. In our studies we identified an opportunity for 10 MW. However, depending on the North Connacht Reinforcement solution option this could increase to 60 MW.

Demand opportunity studies were performed at Letterkenny 110 kV station. In our studies we identified an opportunity for 5 MW. Analysis has shown that the 110 kV lines supplying Donegal could overload under certain maintenance-trip scenarios. Under certain circumstances and in co-ordination with SONI the existing Letterkenny – Strabane 110 kV line can be used to support the network in Donegal.

We have confirmed the need, and are progressing projects through our six-step process for developing the grid, to increase transmission capacity in Mayo and Donegal. These investments will increase capacity for demand in both counties. As these investments progress and get approval they will be included in future forecast statements' analyses.

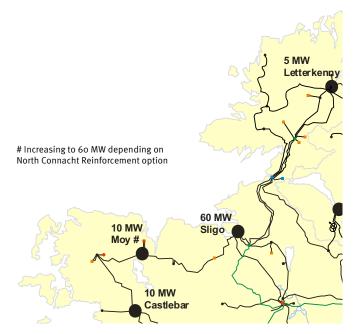


Figure 8-7: Capability for Additional Demand in North-West Region

#### 8.4.4. Opportunities for New Demand in the South-East

The demand opportunities available for the South-East region are shown in Figure 8-8. It is shown that there are potential opportunities available for industrial customers at all stations examined in the region.

The demand opportunity at Kellis 220 kV station is limited to 50 MW due to the maintenancetrip scenario (see Chapter 6) where both 220 kV lines supplying Kellis are assumed to be out of service. This scenario means that demand at Kellis 220 kV station must be supplied by the underlying 110 kV network, which does not have the capacity to carry as much power as the 220 kV network. Demand opportunity studies were performed at Wexford 110 kV station. In our studies we identified an opportunity for 10 MW. Analysis has shown that voltage violations could occur under certain maintenance-trip scenarios.

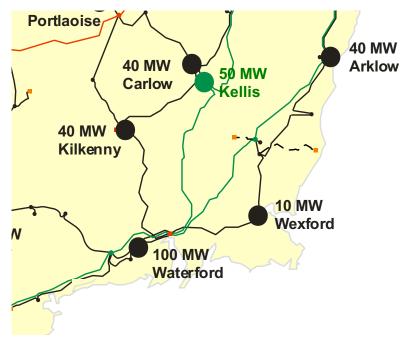


Figure 8-8: Capability for Additional Demand in the South-East Region

#### 8.4.5. Opportunities for New Demand in the South-West

The demand opportunities available for the South-West region are shown in Figure 8-9. It can be seen that there are potential opportunities available for industrial customers at all stations examined in the region.

In particular the Killonan 220 kV station would be a suitable connection point for a major industrial load centre, with the capability of accommodating in excess of 200 MW without additional network reinforcements.

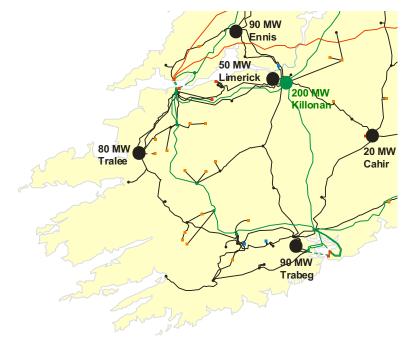


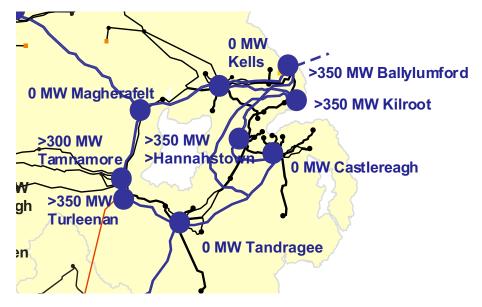
Figure 8-9: Capability for Additional Demand in South-West Region

# 8.5. Transmission System Capability for New Demand in Northern Ireland

Section 8.5.1 discusses the demand opportunities available in the South-Eastern region of Northern Ireland. Section 8.5.2 discusses the demand opportunities available in the Northern and Western region. These results are based on the assumptions detailed in Chapter 6.

#### 8.5.1. Opportunities for New Demand in South-East of Northern Ireland

The demand opportunities available in the South-Eastern region are shown in Figure 8-10.



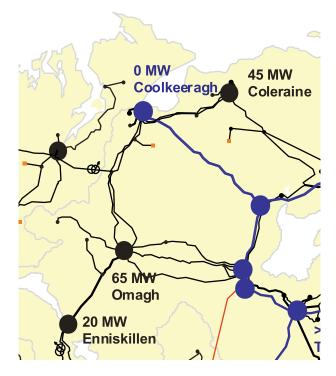
#### Figure 8-10: Capability for Additional Demand (MW) in the East of Northern Ireland

It can be seen that there are potential opportunities available for industrial customers at most stations examined in the region. Those stations with capacity are capable of accommodating approximately 350 MW<sup>123</sup> of additional demand without additional network reinforcements. Those 275 kV stations with an identified capacity of 0 MW are restricted by the ability of the structures and busbars to withstand mechanical forces arising from potential faults. SONI and NIEN will be bringing forward projects to address this issue however these are at an early stage and no additional capacity can as yet be identified in 2029. The fault contributions from non-synchronous connections such as data centres tend to be significantly smaller, particularly those likely to connect at 110 kV. Any such potential connection at these nodes would be assessed based on its fault current contribution.

<sup>123</sup> Please note that the demand opportunities results are not cumulative. Each station is assessed individually, taking account of forecast demand growth only at stations outside of the test node. These figures are indicative only, with further detailed assessment of each station required. Customers considering connecting demand to the NI transmission system are advised to contact SONI as early in the project as possible.

#### 8.5.2. Opportunities for New Demand in North and West of Northern Ireland

The demand opportunities available for the North and West of Northern Ireland are shown in Figure 8-11.



#### Figure 8-11: Capability for Additional Demand in the North and West of Northern Ireland

It can be seen that there are potential opportunities available for industrial customers at all stations examined in the region except Coolkeeragh. It should be noted that the North-West of Northern Ireland requires specific assessment in line with the TSSPS (see Chapter 6). As the North-West is connected by a single double circuit 275 kV spur, an N-1-1 contingency is performed as a credible contingency:

- The loss of the Coolkeeragh-Magherafelt 275 kV double circuit; and
- Coolkeeragh steam and gas units are out on maintenance.

However, the capacity at Coolkeeragh is limited by the ability of the 275 kV structures to withstand mechanical loading from potential faults. SONI and NIEN will be bringing forward projects to address this issue however these are at an early stage.

Enniskillen station represents the second lowest capability of the 110 kV nodes assessed. Enniskillen 110 kV is connected to Dromore 110 kV station via two 110 kV circuits. The loss of one of these circuits creates a thermal overload on the other. This limits demand connection capability.

### 8.6. How to Use the Information for Demand

Although not every station was considered, the results presented can be regarded as a guide to opportunities at other stations in the same area.

Customers wishing to use the demand opportunity results described in this chapter when considering where to connect should follow these steps:

- 1. Consult the maps in Appendix A to find the nearest transmission station to the proposed development. Also, the nearest station for which opportunity has been assessed should be identified, where it differs from the nearest transmission station.
- 2. The anticipated demand growth at the relevant station can be obtained from the demand forecasts presented in Appendix C. The transmission system is being planned to meet this level of demand increase.
- 3. Consider the impact of changes to the transmission system since the analysis was carried out.
- **4.** Consult with EirGrid and SONI on the proposed location as early as possible as well as consulting the EirGrid application process<sup>124</sup> and SONI application process<sup>125</sup>.

Early consultation with us is encouraged so that we can work jointly to explore options relating to any potential proposals and enable timely decision making.

<sup>124</sup> http://www.eirgridgroup.com/customer-and-industry/becoming-a-customer/

<sup>125</sup> http://www.soni.ltd.uk/Customers/howconnected/



# Appendices





## Appendix A Maps and Schematic Diagrams

Appendix A contains geographical maps of the All-Island Transmission System and short bus codes for every transmission voltage node on the island. Geographical maps are presented illustrating the All-Island Transmission System in 2020 and as planned for in 2029.

#### A.1. Network Maps

This section includes two network maps:

- Figure A-1 is a map of the All-Island Transmission System as at January 2020; and
- Figure A-2 is a map of the planned All-Island Transmission System in 2029.

Note: There are a number of network reinforcement projects that do not have a finalised reinforcement solution. They are shown on the Transmission System Map as a transparent bubble in Figure A-2. The solutions that will be used for these projects have not yet been finalised.



Figure A-1: All-Island Transmission System as at January 2020

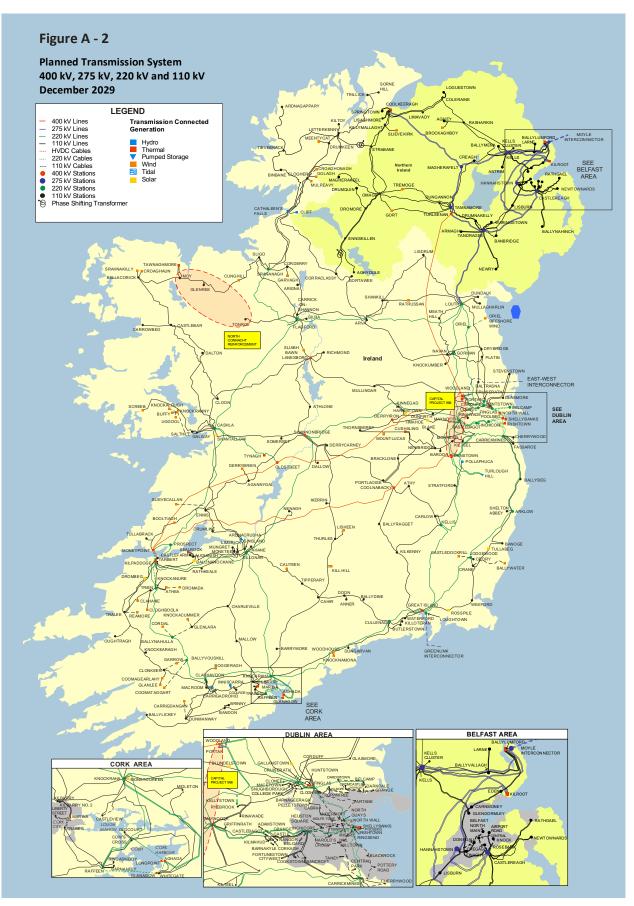


Figure A-2: All-Island Transmission System as at December 2029

### A.2. Short Bus Codes

The following table associates full station names with the two or three letter codes used in the schematic diagrams in Section A.3, in the tables in Appendices B and C, and the power flow tables in Appendix H. Stations in Northern Ireland and Ireland with the same three letter bus code are distinguished with (N) for Northern Ireland and (I) for Ireland.

| Short   | Full Name      |
|---------|----------------|
| Bus     |                |
| Code    |                |
| AA      | Ardnacrusha    |
| AD      | Aghada         |
| ADM     | Adamstown      |
| AGH     | Aghyoule       |
| AGL     | Agannygal      |
| AGI     | Agivey Cluster |
| AGY     | Ardnagappary   |
| AHA     | Ahane          |
| AIR     | Airport Road   |
| ANR     | Anner          |
| ANT     | Antrim         |
| ARI     | Arigna         |
| ARK     | Arklow         |
| ARM     | Armagh         |
| ART     | Artane         |
| ARV     | Arva           |
| ATE     | Athea          |
| ATH     | Athlone        |
| ATY     | Athy           |
| AUG     | Aughinish      |
| BAG     | Barnageeragh   |
| BAL     | Baltrasna      |
| BAN (I) | Bandon         |
| BAN (N) | Banbridge      |
| BAR     | Barrymore      |
| ВСМ     | Ballycummin    |
| ВСТ     | Bancroft       |
| BDA     | Baroda         |
| BDN     | Ballydine      |
| BDV     | Barnadivane    |
| BEG     | Ballybeg       |
| BFP     | Belfast Power  |
|         | Station        |
| BGD     | Belgard Road   |
| BGH     | Boggeragh      |

#### Table A-1: Short Bus Codes

| Short | Full Name                     |  |
|-------|-------------------------------|--|
| Bus   |                               |  |
| Code  |                               |  |
| BGT   | Ballyragget                   |  |
| BIN   | Binbane                       |  |
| BK    | Bellacorick                   |  |
| BKM   | Bunkimalta                    |  |
| BKY   | Barnakyle                     |  |
| BLA   | Blackrock                     |  |
| BLC   | Belcamp                       |  |
| BLE   | Ballinknockane                |  |
| BLI   | Ballylickey                   |  |
| BLK   | Blake                         |  |
| BLU   | Blundelstown                  |  |
| BMA   | Ballymena                     |  |
| BNH   | Ballynahinch                  |  |
| BNM   | Belfast North                 |  |
| BOG   | Banoge                        |  |
| BOL   | Booltiagh                     |  |
| BPS   | Ballylumford<br>Power Station |  |
| BRA   | Bracklone                     |  |
| BRI   | Brinny                        |  |
| BRO   | Brockaghboy                   |  |
| BRT   | Bracetown                     |  |
| BRY   | Barnahely                     |  |
| BUF   | Buffy                         |  |
| BUT   | Butlerstown                   |  |
| BVG   | Ballyvallagh                  |  |
| BVK   | Ballyvouskill                 |  |
| BWR   | Ballywater                    |  |
| BYC   | Ballycronan More<br>(Moyle)   |  |
| ВҮН   | Ballynahulla                  |  |
| CAB   | Cabra                         |  |
| CAE   | CAES                          |  |
| CAG   | Carrickalangan                |  |
| CAU   | Cahir                         |  |
| САП   | Callii                        |  |

| Short | Full Name        |  |
|-------|------------------|--|
| Bus   |                  |  |
| Code  |                  |  |
| CAM   | Cam Cluster      |  |
| CAR   | Carnmoney        |  |
| CAS   | Castlereagh      |  |
| CBG   | Carrowbeg        |  |
| CBL   | Cloghboola       |  |
| CBR   | Castlebar        |  |
| CBT   | Castlebagot      |  |
| CD    | Carrigadrohid    |  |
| CDN   | Carrigdangan     |  |
| CDF   | Carrickaduff     |  |
| CDK   | Castledockrill   |  |
| CDL   | Cordal           |  |
| CDU   | Corduff          |  |
| CDY   | Corderry         |  |
| CEN   | Belfast Central  |  |
| CF    | Cathaleen's Fall |  |
| CFM   | Castlefarm       |  |
| CGL   | Coomagearlahy    |  |
| СН    | Cahernagh        |  |
| CHA   | Charleville      |  |
| CHE   | Cherrywood       |  |
| CHR   | Cahernagh        |  |
| CKG   | Corkagh          |  |
| СКМ   | Carrickmines     |  |
| CKN   | Clonkeen         |  |
| CL    | Cliff            |  |
| CLA   | Clashavoon       |  |
| CLE   | Clonee           |  |
| CLG   | Cloghran         |  |
| CLH   | Clahane          |  |
| CLN   | Cloon            |  |
| CLO   | Clogher          |  |
| CLS   | Clonshaugh       |  |
| CLW   | Carlow           |  |
| CNB   | Coolnabacky      |  |

#### Table A-1: Short Bus Codes

| Short   | Full Name     |
|---------|---------------|
| Bus     |               |
| Code    |               |
| CNF     | Caraunduff    |
| CNN     | Croaghnagawna |
| COL (I) | College Park  |
| COL (N) | Coleraine     |
| C00     | Cookstown     |
| COR     | Corraclassy   |
| COS     | Carrick-on-   |
|         | Shannon       |
| COW     | Cow Cross     |
| СРК     | Central Park  |
| CPS     | Coolkeeragh   |
|         | Power Station |
| CRA     | Crane         |
| CRD     | Croaghonagh   |
| CRE     | Cregagh       |
| CRG     | Creagh        |
| CRH     | Cruiserath    |
| CRM     | Cromcastle    |
| CRN     | Croaghaun     |
| CRO     | Coolroe       |
| CRY     | Crory         |
| CSH     | Cashla        |
| CTG     | Coomataggart  |
| CTN     | Cauteen       |
| CTY     | City West     |
| CUL     | Cullenagh     |
| CUN     | Cunghill      |
| CUR     | Cureeny       |
| CUS     | Cushaling     |
| CVW     | Castleview    |
| DAL     | Dallow        |
| DRN     | Darndale      |
| DDK     | Dundalk       |
| DER     | Derryiron     |
| DEY     | Derrycarney   |
| DFR     | Dunfirth      |
| DGN     | Dungarvan     |
| DJG     | Drombeg       |
| DLN     | Derrylyn      |
| DLT     | Dalton        |

| Short   | Full Name        |
|---------|------------------|
| Bus     |                  |
| Code    |                  |
| DMY     | Dunmanway        |
| DON     | Donegall         |
| D00     | Doon             |
| DRM     | Drumkeen         |
| DRN     | Darndale         |
| DRO     | Dromada          |
| DRO (N) | Dromore          |
| DRQ     | Drumquin Cluster |
| DRU (I) | Drumline         |
| DRU (N) | Drumnakelly      |
| DRY     | Drybridge        |
| DSN     | Dunstown         |
| DTN     | Dardistown       |
| DUN     | Dungannon        |
| DYN     | Derrybrien       |
| EDE     | Eden             |
| ENN (I) | Ennis            |
| ENN (N) | Enniskillen      |
| FAS     | Fassaroe         |
| FAS E   | Fassaroe East    |
| FIN (I) | Finglas          |
| FIN (N) | Finaghy          |
| FLA     | Flagford         |
| FNT     | Finnstown        |
| FRN     | Francis Street   |
| GAE     | Glanlee          |
| GAL     | Galway           |
| GAR     | Garvagh          |
| GCA     | Grange Castle    |
| GGO     | Glanagow         |
| GI      | Great Island     |
| GIL     | Gilra            |
| GLA     | Glasmore         |
| GLE (I) | Glenlara         |
| GLE (N) | Glengormley      |
| GLN     | Gallanstown      |
| GLR     | Glenree          |
| GOL     | Golagh           |
| GOR (I) | Gorman           |
| GOR (N) | Gort Cluster     |

| <u> </u> |                |  |
|----------|----------------|--|
| Short    | Full Name      |  |
| Bus      |                |  |
| Code     |                |  |
| GRA      | Grange         |  |
| GRI      | Griffinrath    |  |
| GRO      | Garrow         |  |
| GWE      | Gortawee       |  |
| HAN      | Hannastown     |  |
| HAR      | Harolds Cross  |  |
| HEU      | Heuston Square |  |
| HN       | Huntstown      |  |
| HRR      | Harristown     |  |
| IA       | Inniscarra     |  |
| IKE      | Ikerrin        |  |
| INC      | Inchicore      |  |
| ISH      | Irishtown      |  |
| KBY      | Kilbarry       |  |
| KBY2     | Kilbarry No. 2 |  |
| KCR      | Knockacummer   |  |
| KDN      | Kildonan       |  |
| KEL      | Kells          |  |
| KLC      | Kells Cluster  |  |
| KER      | Knockearagh    |  |
| KHL      | Kill Hill      |  |
| KIN      | Kinnegad       |  |
| ККҮ      | Kilkenny       |  |
| KLH      | Knockalough    |  |
| KLM      | Kilmore        |  |
| KLN      | Killonan       |  |
| KLS      | Kellis         |  |
| КМА      | Knocknamona    |  |
| КМТ      | Killymallaght  |  |
| KNO      | Knock          |  |
| KNR      | Knockanure     |  |
| KNV      | Knockavanna    |  |
| KNY      | Knockranny     |  |
| KPG      | Kilpaddoge     |  |
| KPN      | Killinaparson  |  |
| KPS      | Kilroot Power  |  |
|          | Station        |  |
| KRA      | Knockraha      |  |
| KTL      | Kilteel        |  |
| KTN      | Killoteran     |  |
|          |                |  |

| Short   | Full Name      |
|---------|----------------|
| Bus     |                |
| Code    |                |
| KUD     | Kilmahud       |
| KUR     | Knockumber     |
| КҮТ     | Kellystown     |
| LA      | Lanesboro      |
| LAR     | Larne          |
| LET     | Letterkenny    |
| LIB     | Liberty Street |
| LIM (I) | Limerick       |
| LIM (N) | Limavady       |
| LIS (I) | Lisdrum        |
| LIS (N) | Lisburn        |
| LMR     | Lisaghmore     |
| LOG     | Loguestown     |
| LOU     | Louth          |
| LPT     | Longpoint      |
| LSN     | Lisheen        |
| LUM     | Lumcloon       |
| LWD     | Lodgewood      |
| MAC     | Macroom        |
| MAG     | Magherafelt    |
| MAL     | Mallow         |
| MAY     | Maynooth       |
| MCD     | McDermott      |
| MCE     | Macetown       |
| MEE     | Meentycat      |
| MEN     | Monatooreen    |
| MHL     | Misery Hill    |
| MID     | Midleton       |
| MIL     | Milltown       |
| MKL     | Magherakeel    |
|         | Cluster        |
| MLC     | Mountlucas     |
| MLN     | Mullagharlin   |
| MON     | Monread        |
| MOY     | Моу            |
| MP      | Moneypoint     |
| MR      | Marina         |
| MRY     | Mulreavy       |
| MTH     | Meath Hill     |
| MTN     | Moneteen       |

#### Table A-1: Short Bus Codes

| Short   | Full Name         |
|---------|-------------------|
| Bus     |                   |
| Code    |                   |
| MUC     | Muckerstown       |
| MUL     | Mullingar         |
| MUN     | Mungret           |
| NAN (I) | Nangor            |
| NAR     | Newtownards       |
| NAV     | Navan             |
| NBY     | Newbury           |
| NEN     | Nenagh            |
| NEW (I) | Newbridge         |
| NEW (N) | Newry             |
| NQS     | North Quays       |
| NW      | North Wall        |
| OLD     | Oldcourt          |
| OMA     | Omagh             |
| ORL     | Oriel             |
| OST     | Oldstreet         |
| OUG     | Oughtragh         |
| PA      | Pollaphuca        |
| PB      | Poolbeg           |
| PLA     | Platin            |
| PLS     | Portlaoise        |
| POP     | Poppintree        |
| POT     | Pottery Road      |
| PRO     | Prospect          |
| PRT     | Portan            |
| PTN     | Pelletstown       |
| RAF     | Raffeen           |
| RAT (I) | Rathkeale         |
| RAT (N) | Rathgael          |
| RE      | Ringsend          |
| REM     | Reamore           |
| RIC     | Richmond          |
| RNW     | Rinawade          |
| ROP     | Rosspile          |
| ROS     | Rosebank          |
| RRU     | Ratrussan         |
| RSK     | Rasharkin Cluster |
| RSY     | Ringaskiddy       |
| RYB     | Ryebrook          |
| SAL     | Salthill          |

| Short   | Full Name           |
|---------|---------------------|
| Bus     | rutt Name           |
|         |                     |
| Code    | Current harmonica h |
| SBH     | Snughborough        |
| SCR     | Screeb              |
| SH      | Shannonbridge       |
| SHE     | Shelton Abbey       |
| SHL     | Shellybanks         |
| SK      | Sealrock            |
| SKL     | Shankill            |
| SKY     | Srahnakilly         |
| SLB     | Sliabh Bawn         |
| SLC     | Slievecallan        |
| SLI     | Sligo               |
| SLK     | Slieve Kirk         |
| SNG     | Singland            |
| SOM     | Somerset            |
| SOR     | Sorne Hill          |
| SPR     | Springtown          |
| SRA     | Srananagh           |
| STR (I) | Stratford           |
| STR (N) | Strabane            |
| SVN     | Stevenstown         |
| SXH     | Shantallow          |
| TAN     | Tandragee           |
| TAW     | Tawnaghmore         |
| ТВ      | Tarbert             |
| TBG     | Trabeg              |
| ТВК     | Tullabrack          |
| TEN     | Timahoe             |
| TH      | Turlough Hill       |
| THU     | Thurles             |
| TIP     | Tipperary           |
| TIV     | Tievebrack          |
| TLK     | Trillick            |
| TLY     | Tanley              |
| TMN     | Tamnamore           |
| TON     | Tonroe              |
| TRE     | Tremoge Cluster     |
| TRI     | Trien               |
| TRN     | Trinity             |
| TSB     | Thornsberry         |
| TTU     | Tullabeg            |
| 110     | ιαπαρέξ             |

#### Table A-1: Short Bus Codes

| Short | Full Name |
|-------|-----------|
| Bus   |           |
| Code  |           |
| TUR   | Turleenan |
| TYN   | Tynagh    |
| UGL   | Uggool    |

| Short<br>Bus<br>Code | Full Name   |
|----------------------|-------------|
| WAR                  | Waringstown |
| WAT                  | Waterford   |
| WEX                  | Wexford     |

| Short<br>Bus<br>Code | Full Name  |
|----------------------|------------|
| WH                   | Woodhouse  |
| WHI                  | Whitegate  |
| WOL                  | Wolfe Tone |

## A.3. Schematic Diagrams of the All-Island Transmission System

Schematic diagrams of the All-Island Transmission System are included to assist users in understanding the transmission system and in the identification of the changes outlined in Appendix B. Lines, cables, transformers, station busbars and reactive compensation devices are illustrated in the diagrams. The type of generation (thermal, wind, hydro or solar) at a station is also displayed. Table A-2 indicates the diagram conventions.

The schematic diagram for 2020 shows the transmission system as of January 2020. The schematic diagram for 2029 shows the planned transmission system due to be completed by the end of 2029.

| Symbol     | Network Element Represented             |
|------------|---|
|            | 110 kV circuit                          |
|            | 220 kV circuit                          |
|            | 275 kV circuit                          |
|            | 400 kV circuit                          |
|            | System Link                             |
| $\bigcirc$ | 110 kV Busbar                           |
| $\bigcirc$ | 220 kV Busbar                           |
| $\bigcirc$ | 275 kV Busbar                           |
|            | 400 kV Busbar                           |
| $\bigcirc$ | Busbar with Thermal Generation          |
|            | Busbar with Wind Generation (>5 MW)     |
|            | Busbar with Hydro Generation            |
|            | Busbar with Solar Generation (>5 MW)    |
|            | Busbar with Wind and Thermal Generation |
|            | Busbar with Wind and Hydro Generation   |
|            | Busbar with Wind and Solar Generation   |
| ÷          | Capacitor                               |
| <u>_</u>   | Static Var Compensator/STATCOM          |
| ٥          | Reactor                                 |
| PST        | Phase Shifting Transformer              |
| <u> </u>   | Transformer                             |
| NO         | Normally Open Point                     |
| SC         | Series Compensation                     |

#### Table A-2: Schematic Legend

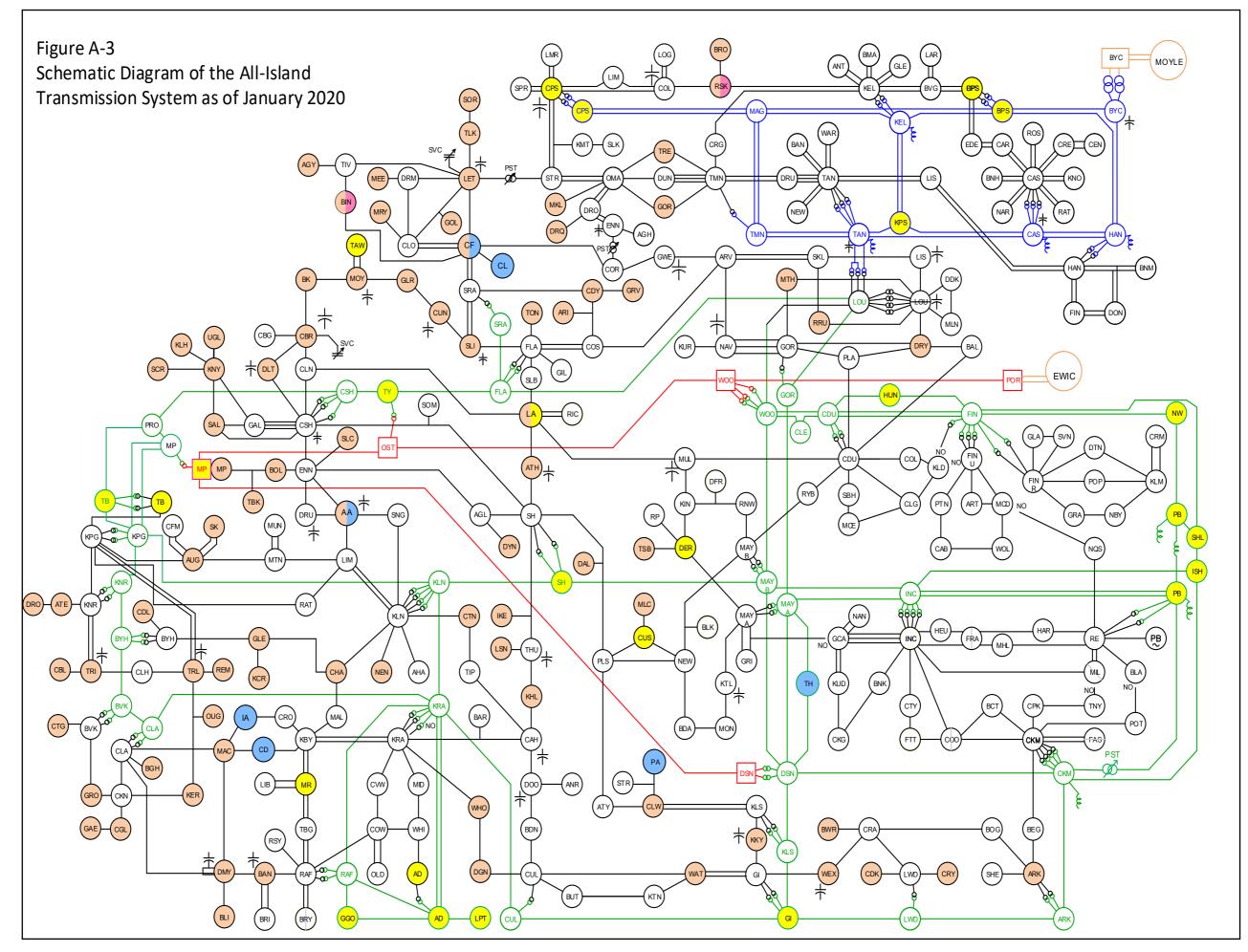


Figure A-3: Schematic Diagram of the All-Island Transmission System as of January 2020

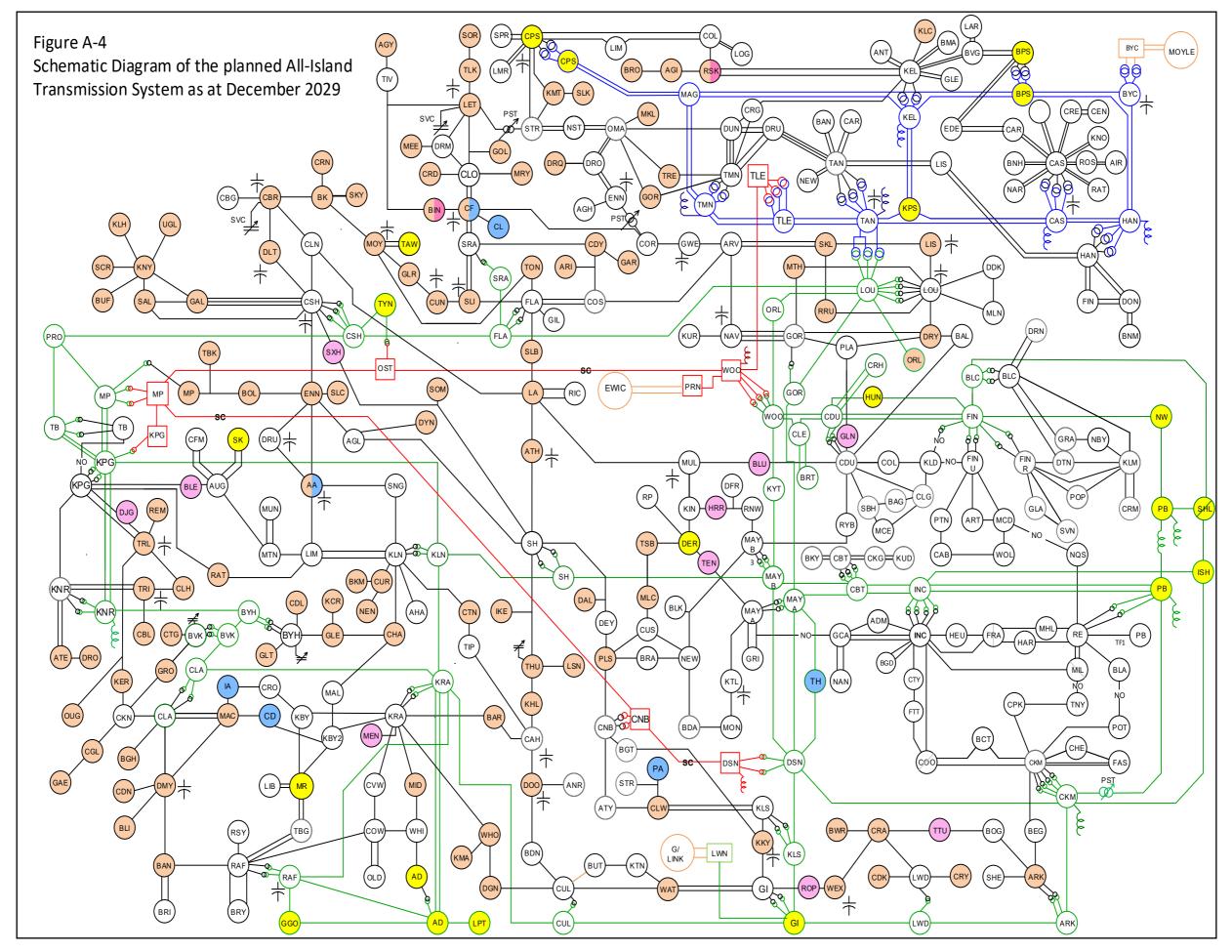


Figure A-4: Schematic Diagram of the planned All-Island Transmission System as of December 2029

## Appendix B Transmission System Characteristics

This appendix presents details of the physical and electrical characteristics of the all-island transmission system in tabular form:

- Section B.1 details the data for the existing<sup>126</sup> transmission system; and
- Section B.2 details the data for planned transmission system developments<sup>127</sup>.

The following is a list of tables in Section B.1:

- Table B-2 Characteristics of Existing Transmission Circuits;
- Table B-3 Characteristics of Existing Transformers in Ireland;
- Table B-4 Characteristics of Existing 3 Winding Transformers in Northern Ireland;
- Table B-5 Characteristics of Existing 2 Winding Transformers in Northern Ireland;
- Table B-6 Characteristics of Existing Power Flow Controllers; and
- Table B-7 Characteristics of Existing Reactive Compensation.

The following is a list of tables in Section B.2:

- Table B-8 Expected Changes in Transmission Circuits;
- Table B-9 Expected Changes in Transformers in Ireland;
- Table B-10 Expected Changes in 3 Winding Transformers in Northern Ireland;
- Table B-11 Expected Changes in 2 Winding Transformers in Northern Ireland; and
- Table B-12 Expected Changes in Reactive Compensation.

Tables B-2 and B-8 include the ratings for lines and cables in MVA for winter and summer reference temperature conditions at 1 per unit (pu) voltage. The higher ambient temperature in summer dictates a reduced thermal rating for overhead lines. The rating is the maximum permissible power that the circuit can transport on a continuous basis.

Reference ambient temperatures are:

- winter: 11°C<sup>128</sup>; and
- summer: 25°C.

The electrical characteristics of the all-island transmission system at the four nominal voltage levels are documented. They are represented in per unit values, with a 100 MVA base, and the applicable reference voltage. Table B-1 below displays the four nominal and reference voltage levels on the all-island transmission system.

126 As at January 2020.

<sup>127</sup> Includes transmission system reinforcement projects and developments necessary to connect new generation and demand. 128 ESB Networks previously calculated winter ratings based on an assumed winter temperature of 5°C. In 2018 this was changed to 11°C.

| Nominal Voltage Level (kV) | Reference Voltage (kV) |
|----------------------------|------------------------|
| 400                        | 400                    |
| 275                        | 275                    |
| 220                        | 220                    |
| 110                        | 110                    |

#### Table B-1: Nominal and Reference Voltage Levels

In some cases equipment associated with a line or cable may be lower rated than the circuit or line. However, this equipment<sup>129</sup> is easier to upgrade than lines and cables and is therefore not expected to restrict access to the transmission system.

A small number of 110 kV stations are connected to the transmission system via a tee. A tee is an un-switched connection into an existing line between two other stations. For the purposes of describing the various sections of lines in the following tables, tee points are identified by the name of the tee'd 110 kV station with a suffix "T" added.

# B.1. Characteristics of the Existing Transmission System (January 2020)

|         |      |     |     |        | Impedan | ce on 100 l | NVA Base |              |        |        |
|---------|------|-----|-----|--------|---------|-------------|----------|--------------|--------|--------|
| Voltage |      |     |     | Length |         | (pu)        |          | Rating (MVA) |        |        |
| (kV)    | From | То  | No. | (km)   | R       | X           | В        | Summer       | Autumn | Winter |
| 400     | DSN  | MP  | 1   | 208.5  | 0.0041  | 0.0436      | 1.1397   | 1283         | 1331   | 1454   |
| 400     | MP   | OST | 1   | 104.1  | 0.0037  | 0.0266      | 0.4885   | 1283         | 1331   | 1454   |
| 400     | OST  | WOO | 1   | 126    | 0.0044  | 0.0323      | 0.5715   | 1577         | 1749   | 1944   |
| 275     | LOU  | TAN | 1   | 50     | 0.0026  | 0.021       | 0.1269   | 710          | 820    | 881    |
| 275     | LOU  | TAN | 2   | 50     | 0.0026  | 0.021       | 0.1269   | 710          | 820    | 881    |
| 275     | BPS  | HAN | 2   | 45.5   | 0.002   | 0.0191      | 0.1141   | 710          | 820    | 881    |
| 275     | BPS  | KEL | 1   | 34.5   | 0.0016  | 0.0145      | 0.0889   | 710          | 820    | 881    |
| 275     | BPS  | MAG | 1   | 65.5   | 0.0029  | 0.0274      | 0.1688   | 710          | 820    | 881    |
| 275     | CAS  | HAN | 1   | 18.4   | 0.0008  | 0.0077      | 0.0461   | 710          | 820    | 881    |
| 275     | CAS  | HAN | 2   | 18.4   | 0.0008  | 0.0077      | 0.0461   | 710          | 820    | 881    |
| 275     | CAS  | KPS | 1   | 66.8   | 0.003   | 0.028       | 0.171    | 710          | 820    | 881    |
| 275     | CAS  | TAN | 1   | 45.6   | 0.002   | 0.0192      | 0.1143   | 710          | 820    | 881    |
| 275     | CPS  | MAG | 1   | 56.2   | 0.0059  | 0.0245      | 0.1512   | 412          | 477    | 513    |
| 275     | CPS  | MAG | 2   | 56.2   | 0.0059  | 0.0245      | 0.1512   | 412          | 477    | 513    |
| 275     | HAN  | BYC | 1   | 44.7   | 0.002   | 0.0188      | 0.1121   | 710          | 820    | 881    |
| 275     | KEL  | KPS | 1   | 29     | 0.0013  | 0.0121      | 0.0747   | 710          | 820    | 881    |
| 275     | KEL  | KPS | 2   | 29     | 0.0013  | 0.0121      | 0.0747   | 710          | 820    | 881    |
| 275     | KEL  | MAG | 1   | 31.1   | 0.0014  | 0.013       | 0.0801   | 710          | 820    | 881    |
| 275     | KPS  | TAN | 1   | 80.8   | 0.0036  | 0.0339      | 0.2061   | 710          | 820    | 881    |

Table B-2: Characteristics of Existing Transmission Circuits

129 For example, current transformers.

|         |         |         |     |        | Impedan | ce on 100 <b>I</b> | NVA Base |        |           |        |
|---------|---------|---------|-----|--------|---------|--------------------|----------|--------|-----------|--------|
| Voltage |         |         |     | Length |         | (pu)               |          | Ra     | ting (MVA | )      |
| (kV)    | From    | То      | No. | (km)   | R       | X                  | В        | Summer | Autumn    | Winter |
| 275     | MAG     | TMN     | 1   | 25.7   | 0.0012  | 0.011              | 0.0654   | 710    | 820       | 881    |
| 275     | MAG     | TMN     | 2   | 25.7   | 0.0012  | 0.011              | 0.0654   | 710    | 820       | 881    |
| 275     | TAN     | TMN     | 1   | 25.7   | 0.0012  | 0.0109             | 0.0647   | 710    | 820       | 881    |
| 275     | TAN     | TMN     | 2   | 25.7   | 0.0012  | 0.0109             | 0.0647   | 710    | 820       | 881    |
| 220     | AD      | KRA     | 1   | 25.6   | 0.003   | 0.0219             | 0.0345   | 393    | 429       | 468    |
| 220     | AD      | RAF     | 1   | 14.4   | 0.0011  | 0.0091             | 0.2518   | 434    | 481       | 513    |
| 220     | AD      | GGO     | 1   | 3.8    | 0.0002  | 0.0015             | 0.1035   | 573    | 536       | 573    |
| 220     | AD      | KRA     | 2   | 25.6   | 0.0013  | 0.0089             | 0.0335   | 393    | 429       | 468    |
| 220     | ARK     | СКМ     | 1   | 53.6   | 0.0062  | 0.0456             | 0.0814   | 434    | 481       | 513    |
| 220     | ARK     | LWD     | 1   | 39     | 0.0046  | 0.0338             | 0.051    | 434    | 481       | 513    |
| 220     | BVK     | CLA     | 1   | 16.8   | 0.002   | 0.0145             | 0.025    | 740    | 769       | 792    |
| 220     | BVK     | BYH     | 1   | 28.6   | 0.0035  | 0.0246             | 0.0503   | 434    | 473       | 513    |
| 220     | BLC     | FIN (I) | 1   | 10     | 0.0004  | 0.0015             | 0.332    | 570    | 570       | 570    |
| 220     | CLE     | CDU     | 1   | 5.1    | 0.0006  | 0.0044             | 0.0067   | 434    | 481       | 513    |
| 220     | CLE     | WOO     | 1   | 13.5   | 0.0016  | 0.0117             | 0.0177   | 434    | 473       | 513    |
| 220     | CLA     | KRA     | 1   | 42.9   | 0.005   | 0.0372             | 0.0574   | 646    | 704       | 751    |
| 220     | CSH     | FLA     | 1   | 88.1   | 0.0103  | 0.0763             | 0.1152   | 350    | 393       | 436    |
| 220     | CSH     | PRO     | 1   | 88.5   | 0.0103  | 0.0767             | 0.1158   | 392    | 429       | 468    |
| 220     | CSH     | TYN     | 1   | 39.9   | 0.0046  | 0.0337             | 0.058    | 761    | 777       | 792    |
| 220     | СКМ     | DSN     | 1   | 41.6   | 0.0049  | 0.0361             | 0.109    | 434    | 481       | 513    |
| 220     | СКМ     | ISH     | 1   | 11.9   | 0.0003  | 0.0046             | 0.3255   | 593    | 593       | 593    |
| 220     | CUL     | GI      | 1   | 23.3   | 0.0034  | 0.0198             | 0.0445   | 746    | 746       | 793    |
| 220     | CUL     | KRA     | 1   | 86     | 0.0117  | 0.0735             | 0.1168   | 646    | 704       | 765    |
| 220     | CDU     | FIN (I) | 1   | 3.7    | 0.0005  | 0.0033             | 0.0049   | 434    | 481       | 513    |
| 220     | CDU     | HN      | 1   | 3.7    | 0.0001  | 0.0014             | 0.1338   | 555    | 555       | 555    |
| 220     | CDU     | FIN (I) | 2   | 3.7    | 0.0005  | 0.0033             | 0.0049   | 434    | 481       | 513    |
| 220     | CDU     | WOO     | 2   | 17.8   | 0.0021  | 0.0155             | 0.0234   | 434    | 481       | 513    |
| 220     | DSN     | KLS     | 1   | 59.3   | 0.0069  | 0.0514             | 0.0776   | 393    | 429       | 468    |
| 220     | DSN     | MAY     | 1   | 36.3   | 0.0043  | 0.0317             | 0.0479   | 350    | 393       | 436    |
| 220     | DSN     | MAY     | 2   | 30.5   | 0.0036  | 0.0265             | 0.04     | 350    | 393       | 436    |
| 220     | DSN     | TH      | 1   | 26.6   | 0.003   | 0.0221             | 0.1443   | 351    | 351       | 351    |
| 220     | FLA     | LOU     | 1   | 110.1  | 0.0129  | 0.0976             | 0.1452   | 384    | 430       | 475    |
| 220     | FLA     | SRA     | 1   | 56     | 0.0065  | 0.047              | 0.0768   | 434    | 481       | 513    |
| 220     | FIN (I) | SHL     | 1   | 13.4   | 0.0005  | 0.0053             | 0.3668   | 536    | 557       | 557    |
| 220     | FIN (I) | NW      | 1   | 11.9   | 0.0006  | 0.0036             | 0.6702   | 332    | 332       | 332    |
| 220     | GI      | KLS     | 1   | 70.4   | 0.0081  | 0.0608             | 0.101    | 393    | 429       | 468    |
| 220     | GI      | LWD     | 1   | 48.1   | 0.0056  | 0.0416             | 0.0705   | 434    | 481       | 513    |
| 220     | GOR     | LOU     | 1   | 32.4   | 0.0038  | 0.0281             | 0.0424   | 434    | 473       | 476    |
| 220     | GOR     | MAY     | 1   | 42.2   | 0.0049  | 0.0366             | 0.0552   | 350    | 393       | 436    |

|         |      |         |     |        | Impedan | ce on 100 <b>I</b> | NVA Base |        |           |        |
|---------|------|---------|-----|--------|---------|--------------------|----------|--------|-----------|--------|
| Voltage |      |         |     | Length |         | (pu)               |          | Ra     | ting (MVA | )      |
| (kV)    | From | То      | No. | (km)   | R       | X                  | В        | Summer | Autumn    | Winter |
| 220     | GGO  | RAF     | 1   | 9.5    | 0.0003  | 0.0049             | 0.4139   | 570    | 570       | 570    |
| 220     | INC  | ISH     | 1   | 12.1   | 0.0003  | 0.0047             | 0.3302   | 562    | 582       | 634    |
| 220     | KNR  | BYH     | 1   | 37.8   | 0.0045  | 0.0326             | 0.0607   | 434    | 473       | 513    |
| 220     | KNR  | KPG     | 1   | 21.4   | 0.0027  | 0.0146             | 0.0543   | 731    | 750       | 762    |
| 220     | KNR  | KPG     | 2   | 20     | 0.0004  | 0.0096             | 0.9709   | 731    | 750       | 762    |
| 220     | KRA  | KLN     | 1   | 82.2   | 0.013   | 0.069              | 0.107    | 512    | 536       | 564    |
| 220     | KRA  | RAF     | 1   | 19.3   | 0.0023  | 0.0167             | 0.0257   | 353    | 405       | 454    |
| 220     | KLN  | SH      | 1   | 89.7   | 0.0144  | 0.0795             | 0.1203   | 269    | 322       | 354    |
| 220     | KLN  | KPG     | 1   | 70.6   | 0.0085  | 0.0609             | 0.1136   | 434    | 481       | 513    |
| 220     | KPG  | MP      | 1   | 5.4    | 0.0001  | 0.0017             | 0.2362   | 660    | 660       | 660    |
| 220     | KPG  | MP      | 2   | 5.4    | 0.0001  | 0.0017             | 0.2362   | 660    | 660       | 660    |
| 220     | KPG  | TB      | 1   | 2.8    | 0.0003  | 0.0022             | 0.0257   | 350    | 393       | 436    |
| 220     | LOU  | WOO     | 1   | 61.2   | 0.0071  | 0.053              | 0.08     | 350    | 393       | 436    |
| 220     | MAY  | TH      | 1   | 53.1   | 0.0058  | 0.0442             | 0.1839   | 325    | 351       | 351    |
| 220     | MAY  | SH      | 1   | 105.6  | 0.0169  | 0.0936             | 0.1417   | 269    | 322       | 354    |
| 220     | MAY  | WOO     | 1   | 22.3   | 0.0027  | 0.0195             | 0.0295   | 350    | 393       | 436    |
| 220     | MP   | PRO     | 1   | 12.7   | 0.0015  | 0.0108             | 0.0173   | 537    | 600       | 663    |
| 220     | NW   | PB      | 1   | 4.5    | 0.0003  | 0.0013             | 0.2612   | 332    | 332       | 332    |
| 220     | OST  | TYN     | 1   | 10     | 0.0012  | 0.0085             | 0.0137   | 434    | 481       | 513    |
| 220     | PB   | СКМ     | 1   | 14.5   | 0.0012  | 0.0049             | 0.579    | 267    | 267       | 267    |
| 220     | PB   | INC     | 1   | 12.5   | 0.001   | 0.0043             | 0.498    | 267    | 267       | 267    |
| 220     | PB   | INC     | 2   | 11.3   | 0.0005  | 0.0032             | 0.7216   | 351    | 351       | 351    |
| 220     | PRO  | ТВ      | 1   | 10.2   | 0.0012  | 0.0072             | 0.1732   | 467    | 467       | 467    |
| 220     | TB   | KPG     | 2   | 2.8    | 0.0003  | 0.0019             | 0.028    | 350    | 393       | 436    |
| 110     | AA   | DRU     | 1   | 18.2   | 0.0274  | 0.0631             | 0.0061   | 99     | 110       | 121    |
| 110     | AA   | ENN (I) | 1   | 32.3   | 0.0484  | 0.1108             | 0.012    | 99     | 110       | 121    |
| 110     | AA   | LIM (I) | 1   | 11.7   | 0.0071  | 0.037              | 0.0116   | 178    | 194       | 209    |
| 110     | AD   | WHI     | 1   | 3.1    | 0.0049  | 0.0107             | 0.001    | 99     | 110       | 121    |
| 110     | AGL  | DYN     | 1   | 8      | 0.0125  | 0.0276             | 0.0026   | 105    | 116       | 123    |
| 110     | AGL  | ENN (I) | 1   | 38.2   | 0.0594  | 0.1314             | 0.0123   | 99     | 110       | 121    |
| 110     | AGL  | SH      | 1   | 45.9   | 0.0685  | 0.1571             | 0.0169   | 104    | 113       | 119    |
| 110     | AHA  | KLN     | 1   | 3.8    | 0.0039  | 0.0123             | 0.0035   | 112    | 112       | 112    |
| 110     | ADM  | INC     | 1   | 10.5   | 0.0091  | 0.0273             | 0.0237   | 103    | 123       | 134    |
| 110     | ADM  | KUD     | 1   | 0      | 0.0008  | 0.0016             | 0.0105   | 140    | 140       | 140    |
| 110     | ANR  | DOO     | 1   | 2      | 0.0031  | 0.0069             | 0.0006   | 105    | 116       | 123    |
| 110     | ARK  | BEG     | 1   | 21.9   | 0.0102  | 0.0787             | 0.0071   | 99     | 111       | 122    |
| 110     | ARK  | BOG     | 1   | 29     | 0.0207  | 0.0952             | 0.0102   | 178    | 197       | 210    |
| 110     | ARK  | SHE     | 2   | 2.2    | 0.0035  | 0.0077             | 0.0008   | 34     | 46        | 57     |
| 110     | ATE  | DRO     | 1   | 5.5    | 0.0012  | 0.0057             | 0.0602   | 120    | 124       | 140    |
| 110     | ATE  | KNR     | 1   | 6.7    | 0.0042  | 0.0208             | 0.0068   | 178    | 197       | 210    |

| Voltogo |      |         |     | Longth | Impedan | ce on 100 l | NVA Base | De     |           | •      |
|---------|------|---------|-----|--------|---------|-------------|----------|--------|-----------|--------|
| Voltage | -    | -       |     | Length |         | (pu)        |          |        | ting (MVA |        |
| (kV)    | From | То      | No. | (km)   | R       | X           | B        | Summer | Autumn    | Winter |
| 110     | ATH  | LA      | 1   | 35.8   | 0.054   | 0.123       | 0.0116   | 99     | 110       | 121    |
| 110     | ATH  | SH      | 1   | 21.6   | 0.0135  | 0.0696      | 0.0113   | 178    | 190       | 190    |
| 110     | AUG  | CFM     | 1   | 0.6    | 0.001   | 0.002       | 0.0011   | 96     | 96        | 96     |
| 110     | AUG  | KPG     | 1   | 32.8   | 0.0207  | 0.1067      | 0.0116   | 178    | 197       | 210    |
| 110     | AUG  | MTN     | 1   | 27.5   | 0.0173  | 0.0894      | 0.0097   | 178    | 197       | 210    |
| 110     | AUG  | SK      | 3   | 1      | 0.0006  | 0.0012      | 0.0061   | 120    | 120       | 120    |
| 110     | AUG  | SK      | 4   | 1      | 0.0006  | 0.0012      | 0.0061   | 120    | 120       | 120    |
| 110     | AUG  | CFM     | 2   | 0.7    | 0.001   | 0.0021      | 0.0012   | 96     | 96        | 96     |
| 110     | ARV  | COS     | 1   | 43     | 0.0666  | 0.1479      | 0.0138   | 104    | 113       | 123    |
| 110     | ARV  | GWE     | 1   | 30.6   | 0.0193  | 0.0994      | 0.0108   | 178    | 197       | 210    |
| 110     | ARV  | NAV     | 1   | 65.5   | 0.0412  | 0.2128      | 0.0231   | 178    | 197       | 210    |
| 110     | ARV  | SKL     | 1   | 18.5   | 0.0117  | 0.0602      | 0.0066   | 178    | 197       | 210    |
| 110     | ARV  | SKL     | 2   | 23.6   | 0.0148  | 0.0763      | 0.0097   | 178    | 197       | 210    |
| 110     | ART  | FIN (I) | 1   | 9      | 0.0047  | 0.0101      | 0.0548   | 120    | 120       | 131    |
| 110     | ART  | MCD     | 1   | 4.9    | 0.0026  | 0.0055      | 0.0298   | 120    | 120       | 131    |
| 110     | BVK  | GRO     | 1   | 4.9    | 0.0021  | 0.0025      | 0.0541   | 195    | 201       | 220    |
| 110     | ATY  | CLW     | 1   | 24.2   | 0.0363  | 0.0833      | 0.0081   | 99     | 110       | 121    |
| 110     | ATY  | PLS     | 1   | 25.5   | 0.0382  | 0.0876      | 0.0085   | 99     | 110       | 121    |
| 110     | BWR  | CRA     | 1   | 22.4   | 0.008   | 0.0235      | 0.1366   | 115    | 115       | 115    |
| 110     | BOL  | ENN (I) | 1   | 24.7   | 0.0156  | 0.0802      | 0.0087   | 178    | 197       | 210    |
| 110     | BOL  | ТВК Т   | 1   | 18.3   | 0.0115  | 0.0594      | 0.0065   | 178    | 197       | 210    |
| 110     | BAL  | CDU     | 1   | 15.9   | 0.0106  | 0.0546      | 0.006    | 178    | 194       | 209    |
| 110     | BAL  | DRY     | 1   | 20     | 0.0126  | 0.065       | 0.0071   | 178    | 197       | 210    |
| 110     | BLI  | DMY     | 1   | 27.6   | 0.0426  | 0.0943      | 0.0098   | 105    | 116       | 123    |
| 110     | BEG  | СКМ     | 1   | 32.3   | 0.0148  | 0.1159      | 0.0104   | 136    | 150       | 159    |
| 110     | CDL  | BYH     | 1   | 9.5    | 0.002   | 0.0109      | 0.1055   | 195    | 201       | 220    |
| 110     | BLK  | BLK     | 1   | 0.5    | 0.0006  | 0.0017      | 0.0002   | 136    | 150       | 159    |
| 110     | BIN  | CF      | 1   | 34.3   | 0.0533  | 0.1178      | 0.011    | 99     | 110       | 121    |
| 110     | BIN  | TIV     | 1   | 23.2   | 0.0242  | 0.0774      | 0.0079   | 136    | 150       | 159    |
| 110     | BDA  | MON     | 1   | 11.2   | 0.0102  | 0.0304      | 0.0294   | 99     | 110       | 121    |
| 110     | BDA  | NEW (I) | 1   | 7.2    | 0.006   | 0.0171      | 0.0281   | 122    | 122       | 122    |
| 110     | BDN  | CUL     | 1   | 21.8   | 0.0312  | 0.0751      | 0.0073   | 196    | 216       | 217    |
| 110     | BDN  | DOO     | 1   | 11.3   | 0.0071  | 0.0368      | 0.004    | 178    | 197       | 210    |
| 110     | BRY  | RAF     | 1   | 1.7    | 0.0027  | 0.0059      | 0.0006   | 63     | 82        | 92     |
| 110     | BRY  | RAF     | 2   | 1.8    | 0.0021  | 0.0061      | 0.0007   | 99     | 110       | 121    |
| 110     | BK   | CBR     | 1   | 37.4   | 0.0533  | 0.1284      | 0.0143   | 195    | 202       | 221    |
| 110     | BK   | MOY     | 1   | 27     | 0.017   | 0.0877      | 0.0096   | 178    | 197       | 210    |
| 110     | BGD  | INC     | 1   | 6.5    | 0.0047  | 0.0097      | 0.0652   | 140    | 140       | 140    |
| 110     | BGD  | INC     | 2   | 6.5    | 0.0047  | 0.0097      | 0.0652   | 140    | 140       | 140    |
| 110     | BLA  | RE      | 1   | 7.7    | 0.003   | 0.006       | 0.1362   | 119    | 119       | 119    |

#### Impedance on 100 MVA Base Rating (MVA) Voltage Length (pu) Winter Summer Autumn (kV) From То No. (km) R Х В BAN BRI 110 1 2.6 0.004 0.009 0.0009 105 116 123 110 BAN DMY 0.0403 0.0891 0.0083 110 121 1 25.9 99 110 BAN RAF 1 26.9 0.0413 0.0914 0.0115 99 110 121 BAN BRI 110 2 2.5 0.0039 0.0086 0.0008 99 110 121 CDU 110 CLG 1 0.0006 0.0028 0.0276 187 206 2.5 219 110 CLG FIN (I) 1 3.6 0.0035 0.0111 124 0.0073 124 124 BAR BAR 110 0.3 0.0004 0.0011 0.0002 136 1 150 159 BLC DRN 0.0257 110 1 0 0.0004 0.0021 228 228 228 BLC DRN 110 2 0 0.0004 0.0021 0.0257 228 228 228 BUT 178 CUL 0.0078 110 1 12.3 0.038 0.013 192 192 110 BUT KTN 1 2.7 0.0038 0.0099 0.001 200 209 216 KNG TRI 0.0067 110 1 13.6 0.0195 0.0989 124 124 124 BOG CRA 110 1 24.7 0.0179 0.0811 0.0087 178 197 210 110 BGH CLA 0.0081 0.0401 0.027 178 210 1 13.5 197 110 AGY TIV 1 0.0544 0.1204 0.0112 105 116 123 35 CAB PTN 80 110 1 2.7 0.0024 0.0072 0.0053 105 119 CAB WOL 110 1 4.7 0.0025 0.0053 0.0286 120 120 131 CLA CKN 0.0188 110 1 30 0.0963 0.0147 178 190 190 110 CLA DMY 1 38.8 0.0243 0.1257 0.0152 178 197 210 CLA MAC 161 110 0.0036 0.0184 0.002 176 1 5.7 191 KER 110 CKN 1 20.3 0.0128 0.066 0.0072 178 197 210 110 CRO IA 1 2.7 0.004 0.0101 0.001 196 216 217 110 CRO KBY 1 0.02 0.049 0.005 178 200 14.4 194 CDY GRV 5.8 0.0188 110 1 0.0037 0.0033 132 137 150 CDY SRA 110 1 12.7 0.0198 0.0437 0.0041 99 110 121 CDY ARI T 0.0049 0.0086 178 210 110 1 0.0445 13.7 197 110 CSH CLN 1 22.8 0.0144 0.0741 0.0081 178 197 210 CSH DLT 60.8 110 1 0.0745 0.2049 0.0202 110 99 121 110 CSH ENN (I) 1 0.0336 0.1737 0.0189 178 210 53.5 197 CSH GAL 13.8 0.0215 110 1 0.0475 0.0045 99 110 121 CSH GAL 110 2 11.3 0.0176 0.0389 0.0037 99 110 121 CSH GAL 0.0176 0.0389 110 3 11.3 0.0037 99 110 121 CSH SAL 110 1 24.9 0.0236 0.0738 0.0678 97 97 97 CSH SOM 0.0778 110 1 50 0.172 0.0161 99 110 121 CLH TRI 110 1 9 0.014 0.031 0.0029 99 110 121 CLH TRL 110 1 13.5 0.02 0.0449 0.0132 105 114 123 CBR CLN 110 1 57.5 0.0893 0.1978 0.0195 110 121 99 CBR CBG 26.7 0.0586 110 1 0.035 0.0779 110 121 99 CBR DLT 110 1 27.8 0.0432 0.0955 0.0089 99 110 121

|         |         |         |     |        | Impedan | ce on 100 <b>I</b> | NVA Base |        | •         |        |
|---------|---------|---------|-----|--------|---------|--------------------|----------|--------|-----------|--------|
| Voltage |         |         |     | Length |         | (pu)               |          | Ra     | ting (MVA | )      |
| (kV)    | From    | То      | No. | (km)   | R       | Х                  | В        | Summer | Autumn    | Winter |
| 110     | CD      | KBY     | 1   | 32.1   | 0.0202  | 0.1043             | 0.0113   | 178    | 197       | 210    |
| 110     | CD      | MAC     | 1   | 2.4    | 0.0016  | 0.0079             | 0.0009   | 178    | 197       | 210    |
| 110     | СРК     | TNY     | 1   | 5.6    | 0.0029  | 0.0056             | 0.0725   | 100    | 100       | 100    |
| 110     | СРК     | СРК     | 1   | 3.4    | 0.0018  | 0.0037             | 0.0247   | 100    | 100       | 100    |
| 110     | CF      | CL      | 1   | 5.5    | 0.0058  | 0.0184             | 0.0019   | 136    | 150       | 159    |
| 110     | CF      | COR     | 1   | 61.3   | 0.0385  | 0.1992             | 0.0216   | 178    | 194       | 209    |
| 110     | CF      | SRA     | 1   | 53     | 0.0649  | 0.1787             | 0.0211   | 196    | 214       | 234    |
| 110     | CF      | CLO     | 2   | 25.7   | 0.0386  | 0.0884             | 0.0095   | 178    | 194       | 209    |
| 110     | CRM     | KLM     | 2   | 1.4    | 0.001   | 0.0021             | 0.0136   | 140    | 140       | 140    |
| 110     | CAH     | DOO     | 1   | 15.7   | 0.0099  | 0.0511             | 0.0056   | 178    | 197       | 210    |
| 110     | CAH     | KHL     | 1   | 18     | 0.0113  | 0.0584             | 0.0064   | 178    | 197       | 210    |
| 110     | CAH     | TIP     | 1   | 18.1   | 0.0114  | 0.0587             | 0.0064   | 178    | 197       | 210    |
| 110     | CAH     | BAR     | 1   | 43.7   | 0.0653  | 0.1497             | 0.0141   | 105    | 116       | 123    |
| 110     | CRM     | KLM     | 1   | 1.4    | 0.001   | 0.0021             | 0.0136   | 140    | 140       | 140    |
| 110     | СКМ     | CHE     | 1   | 4      | 0.0038  | 0.0081             | 0.0295   | 105    | 116       | 123    |
| 110     | СКМ     | POT     | 1   | 3.2    | 0.0013  | 0.0025             | 0.0566   | 119    | 119       | 119    |
| 110     | BRA     | NEW (I) | 1   | 9.3    | 0.0097  | 0.031              | 0.0032   | 136    | 150       | 159    |
| 110     | BRA     | PLS     | 1   | 19.3   | 0.03    | 0.0665             | 0.0062   | 99     | 110       | 121    |
| 110     | CO0     | BCT     | 1   | 15.1   | 0.0136  | 0.045              | 0.0272   | 130    | 130       | 130    |
| 110     | C00     | СКМ     | 2   | 16     | 0.0134  | 0.0417             | 0.0604   | 130    | 130       | 130    |
| 110     | CLN     | LA      | 1   | 64.8   | 0.0951  | 0.2216             | 0.021    | 99     | 110       | 121    |
| 110     | SCR     | KNY     | 1   | 33.3   | 0.0311  | 0.1082             | 0.0398   | 135    | 147       | 159    |
| 110     | CRA     | LWD     | 1   | 6.7    | 0.0042  | 0.0216             | 0.0035   | 178    | 197       | 210    |
| 110     | CRA     | WEX     | 1   | 22.8   | 0.0238  | 0.0761             | 0.0077   | 99     | 110       | 113    |
| 110     | COS     | FLA     | 1   | 3.4    | 0.0053  | 0.0117             | 0.0011   | 99     | 110       | 121    |
| 110     | COS     | FLA     | 2   | 3.3    | 0.0052  | 0.0114             | 0.0011   | 99     | 110       | 121    |
| 110     | COS     | ARI T   | 1   | 20.7   | 0.013   | 0.0647             | 0.007    | 178    | 197       | 210    |
| 110     | COL (I) | FIN (I) | 1   | 5      | 0.0034  | 0.0127             | 0.0373   | 104    | 124       | 124    |
| 110     | COL (I) | CDU     | 1   | 2.7    | 0.0009  | 0.0043             | 0.0196   | 143    | 143       | 143    |
| 110     | CHA     | GLE     | 1   | 28.1   | 0.042   | 0.0965             | 0.009    | 99     | 110       | 121    |
| 110     | CHA     | KLN     | 1   | 36.9   | 0.0385  | 0.1231             | 0.0126   | 136    | 150       | 159    |
| 110     | CHA     | MAL     | 1   | 22.5   | 0.0142  | 0.0731             | 0.008    | 178    | 197       | 210    |
| 110     | CLW     | KLS     | 1   | 5.4    | 0.0084  | 0.0186             | 0.0018   | 99     | 110       | 121    |
| 110     | CLW     | KLS     | 2   | 5.3    | 0.0082  | 0.0186             | 0.0017   | 99     | 110       | 121    |
| 110     | CLW     | STR     | 1   | 17.6   | 0.0274  | 0.0606             | 0.0057   | 105    | 116       | 123    |
| 110     | COW     | CVW     | 1   | 17.2   | 0.0245  | 0.0543             | 0.0182   | 99     | 110       | 121    |
| 110     | COW     | OLD     | 1   | 2.3    | 0.0035  | 0.0079             | 0.0008   | 105    | 116       | 123    |
| 110     | COW     | OLD     | 2   | 2.2    | 0.0033  | 0.0076             | 0.0007   | 105    | 116       | 123    |
| 110     | COW     | RAF     | 1   | 6.9    | 0.01    | 0.0236             | 0.0033   | 99     | 110       | 121    |

#### Impedance on 100 MVA Base Rating (MVA) Voltage Length (pu) Winter Summer Autumn (kV) From То No. (km) R Х В COW WHI 17.8 110 1 0.0272 0.0615 0.0058 110 121 99 26.3 110 CUN GLR 0.0904 0.0087 178 1 0.0394 194 209 110 CUN SLI 1 21.1 0.0302 0.0727 0.0071 178 194 209 CUS MLC 110 1 13.7 0.0151 0.0483 0.005 136 150 159 CUS NEW (I) 24.6 0.0257 0.0821 0.0084 110 1 134 147 152 CUS PLS 1 0.0436 0.1396 110 42.1 0.0143 136 150 159 CVW KRA 110 7.6 0.0117 0.0035 110 121 1 0.0259 99 CGL CKN 110 1 6.3 0.004 0.0205 0.0028 178 190 190 COR GWE 0.0039 110 1 10.9 0.0069 0.0355 178 197 210 COR ENN (N) 110 1 27.5 0.0412 0.0946 0.0092 99 110 121 110 CDK LWD 1 8.4 0.003 0.0088 0.0512 115 115 115 CUL DGN 178 110 1 0.0215 0.1093 0.0203 34.2 192 192 CUL WAT 110 1 13.1 0.0073 0.0298 0.0548 178 200 194 110 CTY INC 8.9 0.0111 0.0301 0.003 103 116 1 123 110 CDU MUL 1 0.0933 0.2415 0.0376 104 114 122 73.3 PLA CDU 110 1 37 0.0233 0.1202 0.0131 178 197 210 CDU RYB 110 1 13 0.0135 0.0434 0.0045 178 197 219 KNY UGL 110 1 3.4 0.0007 0.0041 0.0402 201 220 195 110 KNY GAL 1 26.5 0.005 0.031 0.1376 110 121 99 KNY KLH 110 0.0027 0.015 190 1 11.7 0.107 190 190 110 KNY SAL 1 22.7 0.0189 0.0634 0.0814 195 201 220 110 DDK MLN 1 7.5 0.0117 0.0258 0.0025 99 110 121 110 DDK LOU 1 16.8 0.0262 0.0582 0.0054 110 121 99 DRU ENN (I) 0.027 0.0601 121 110 1 17.4 0.0063 99 110 DGN WHO 8.6 110 1 0.0055 0.0281 0.0031 178 210 197 DRY 0.0063 GOR 0.0293 0.0667 110 1 19.4 99 110 121 110 DRY LOU 1 31.9 0.0201 0.1037 0.0113 99 110 121 DRY PLA 110 1 0.0082 0.0182 0.0017 110 121 5.3 99 110 DMY MAC 1 26.2 0.0393 0.0901 0.0087 196 217 213 DAL DAL 12.2 0.019 0.042 110 1 0.004 105 116 123 DTN FIN (I) 110 1 9.2 0.0017 0.0144 0.1108 140 140 140 DTN KLM 0.0048 110 1 3.2 0.0023 0.0321 140 140 140 DER KIN 0.0123 110 1 15.1 0.0498 0.0053 99 110 121 DER TSB 0.0308 0.0681 110 1 19.7 0.0064 110 121 99 LET 110 DRM 1 8.3 0.0125 0.0276 0.0026 99 110 123 DRM MEE 0.0078 0.0172 110 1 5 0.0016 99 110 121 DRM CLO 110 1 27 0.0386 0.0909 0.0152 103 116 123 ENN (I) SLC 0.0032 110 1 31 0.0475 0.271 201 220 195 0.0075 KHL THU 110 1 21.2 0.0134 0.069 178 197 210 MLC TSB 18.3 0.016 110 1 0.0561 0.0277 135 147 159

| N 11    |         |     |     |        | Impedan | ce on 100 l | MVA Base |        |           | ,      |
|---------|---------|-----|-----|--------|---------|-------------|----------|--------|-----------|--------|
| Voltage | _       | _   |     | Length |         | (pu)        |          |        | ting (MVA |        |
| (kV)    | From    | То  | No. | (km)   | R       | X           | В        | Summer | Autumn    | Winter |
| 110     | CKG     | BKY | 1   | 3      | 0.0007  | 0.0033      | 0.033    | 187    | 206       | 223    |
| 110     | FAS     | FAS | 1   | 5      | 0.0078  | 0.0172      | 0.0016   | 105    | 116       | 123    |
| 110     | FAS     | СКМ | 1   | 7.5    | 0.0117  | 0.0258      | 0.0024   | 105    | 116       | 123    |
| 110     | FLA     | GIL | 1   | 10.6   | 0.0165  | 0.0365      | 0.0034   | 105    | 116       | 123    |
| 110     | FLA     | SLI | 1   | 50.5   | 0.0785  | 0.1737      | 0.0162   | 99     | 110       | 121    |
| 110     | FLA     | TON | 1   | 32.3   | 0.0502  | 0.1111      | 0.0104   | 98     | 111       | 126    |
| 110     | FLA     | SLB | 1   | 21.7   | 0.0337  | 0.0747      | 0.007    | 99     | 110       | 123    |
| 110     | FRA     | HAR | 1   | 2.3    | 0.0018  | 0.004       | 0.03     | 107    | 107       | 107    |
| 110     | FRA     | TRN | 1   | 2.8    | 0.002   | 0.0042      | 0.0281   | 140    | 140       | 140    |
| 110     | FRA     | HEU | 1   | 2.4    | 0.0017  | 0.0036      | 0.0241   | 140    | 140       | 140    |
| 110     | FRA     | INC | 1   | 5.6    | 0.0044  | 0.0098      | 0.0727   | 107    | 107       | 107    |
| 110     | FIN (I) | MCD | 1   | 7.9    | 0.003   | 0.0069      | 0.1412   | 119    | 119       | 119    |
| 110     | FIN (I) | PTN | 1   | 3.5    | 0.0033  | 0.0099      | 0.0061   | 80     | 105       | 119    |
| 110     | FIN (I) | GLA | 1   | 14     | 0.0218  | 0.0482      | 0.0047   | 105    | 116       | 123    |
| 110     | FIN (I) | GRA | 1   | 13.2   | 0.005   | 0.0115      | 0.2359   | 119    | 119       | 119    |
| 110     | FIN (I) | POP | 1   | 4.3    | 0.0023  | 0.0048      | 0.0262   | 120    | 120       | 131    |
| 110     | FIN (I) | SVN | 1   | 32.2   | 0.0394  | 0.104       | 0.0564   | 105    | 115       | 115    |
| 110     | FTT     | CO0 | 1   | 4.4    | 0.004   | 0.0106      | 0.0193   | 124    | 124       | 132    |
| 110     | GLA     | SVN | 1   | 18     | 0.0173  | 0.0552      | 0.0517   | 136    | 150       | 154    |
| 110     | GRI     | GRI | 1   | 1      | 0.0016  | 0.0035      | 0.0004   | 105    | 116       | 123    |
| 110     | GI      | ККҮ | 1   | 49.2   | 0.0765  | 0.1692      | 0.0158   | 99     | 110       | 121    |
| 110     | GI      | WAT | 1   | 11.7   | 0.0074  | 0.0381      | 0.0042   | 178    | 197       | 210    |
| 110     | GI      | WAT | 2   | 12.9   | 0.0082  | 0.042       | 0.0046   | 178    | 197       | 210    |
| 110     | GI      | WEX | 1   | 34.5   | 0.0217  | 0.1121      | 0.0122   | 178    | 197       | 210    |
| 110     | GRA     | NBY | 1   | 5.1    | 0.002   | 0.0046      | 0.0887   | 119    | 119       | 119    |
| 110     | GRO     | CKN | 1   | 15.2   | 0.0094  | 0.0085      | 0.137    | 120    | 120       | 120    |
| 110     | GAL     | SAL | 1   | 6.1    | 0.0026  | 0.0027      | 0.0675   | 99     | 106       | 106    |
| 110     | GOL     | GLT | 1   | 3.9    | 0.0061  | 0.0135      | 0.0013   | 105    | 116       | 123    |
| 110     | GOR     | MTH | 1   | 26.4   | 0.0264  | 0.0871      | 0.0123   | 99     | 110       | 121    |
| 110     | GOR     | NAV | 1   | 5.3    | 0.0079  | 0.0187      | 0.0018   | 99     | 110       | 121    |
| 110     | GOR     | NAV | 2   | 6.3    | 0.0089  | 0.0217      | 0.0021   | 99     | 110       | 121    |
| 110     | GOR     | NAV | 3   | 5.5    | 0.0054  | 0.017       | 0.007    | 99     | 110       | 121    |
| 110     | GOR     | PLA | 1   | 19.7   | 0.0302  | 0.0681      | 0.0064   | 99     | 110       | 121    |
| 110     | GCA     | INC | 1   | 8.1    | 0.0079  | 0.0246      | 0.0091   | 103    | 123       | 134    |
| 110     | GCA     | INC | 2   | 8.1    | 0.0079  | 0.0246      | 0.0091   | 103    | 123       | 134    |
| 110     | GCA     | KUD | 2   | 2.1    | 0.0015  | 0.0032      | 0.0211   | 140    | 140       | 140    |
| 110     | GCA     | NAN | 1   | 1.8    | 0.001   | 0.0021      | 0.0111   | 120    | 120       | 131    |
| 110     | GCA     | NAN | 2   | 1.7    | 0.0009  | 0.002       | 0.0106   | 120    | 120       | 131    |
| 110     | CLO     | MRY | 1   | 7.7    | 0.002   | 0.009       | 0.0895   | 136    | 136       | 136    |
| 110     | CLO     | CF  | 1   | 26.1   | 0.0163  | 0.0884      | 0.0158   | 178    | 194       | 209    |

#### Impedance on 100 MVA Base Rating (MVA) Voltage Length (pu) Winter Autumn (kV) From То No. (km) R Х В Summer HAR RE 5.6 0.0045 110 1 0.0098 0.0728 107 107 107 INC 3.6 HEU 0.0026 0.0362 110 1 0.0054 140 140 140 110 IA MAC 1 18.2 0.0273 0.0625 0.006 196 213 217 INC MIL 110 1 8.4 0.0044 0.0094 0.0511 120 120 131 INC BKY 1 10 0.0023 0.011 0.11 187 206 110 223 KNR KPG 0.0152 0.0498 0.0051 110 1 14.9 136 150 159 KNR TRI 110 2 0.0035 110 121 4.2 0.0035 0.0133 99 KNR TRI 110 1 4.3 0.0026 0.0131 0.0053 178 194 209 KRA KBY 110 1 11.9 0.0075 0.0387 0.0042 178 197 210 KRA BAR 110 1 19.5 0.0203 0.0649 0.0067 136 150 159 110 KRA MID 1 10.7 0.0167 0.0368 0.0035 99 110 121 KRA WHO 110 1 0.0261 0.1347 0.0146 178 210 41.5 197 KRA KBY 110 2 12.5 0.0183 0.0428 0.0041 99 110 121 110 KTL MAY 0.0223 0.0716 0.0073 110 121 1 21.4 99 110 KTL MON 1 8.9 0.0093 0.0297 0.0031 136 150 159 REM TRL 110 1 12 0.0053 0.003 0.1099 125 130 141 KKY KLS 110 1 34.3 0.0534 0.118 0.011 99 110 121 KLN LIM (I) 0.0029 110 1 9 0.014 0.031 121 99 110 110 KLN CUR 1 14.8 0.0109 0.0484 0.0052 136 150 159 KLN SNG 110 0.0026 0.0026 178 209 1 4.1 0.0131 194 110 KER OUG T 1 22.6 0.0142 0.0735 0.008 178 197 210 110 KUR NAV 1 6.1 0.0095 0.021 0.002 99 110 123 110 BYH GLE 1 19.1 0.0055 0.022 0.186 124 124 124 KIN MUL 178 110 1 24.9 0.0155 0.0773 0.0227 197 210 KIN DFR 110 1 29.3 0.0213 0.0957 0.0103 110 121 99 KCR GLE 0.003 122 110 1 11.3 0.013 0.1239 122 122 110 KTN WAT 1 0.0007 0.0034 0.0386 99 110 121 3.3 KLM NBY 110 1 1.2 0.0006 0.0012 0.0199 119 119 119 110 KLM POP 1 6 0.0031 0.0067 0.0365 120 120 131 KPG RAT (I) 0.1067 110 1 32.4 0.0332 0.0183 136 150 159 KPG TRL 110 1 39.4 0.0602 0.0127 99 110 121 0.1354 KPG TRL 2 190 110 43.6 0.0271 0.1405 0.0231 178 190 KPG СН 110 1 22.6 0.0236 0.0754 0.0077 136 150 159 LA MUL 110 1 46.3 0.0719 0.1595 0.0149 110 121 99 LA RIC 110 1 15.7 0.0242 0.0535 0.0068 99 110 123 LA RIC 2 110 12.5 0.0195 0.043 0.0051 99 110 123 LA SLB 110 1 9.1 0.0141 0.0313 0.003 99 110 123 LOU MLN 0.0203 110 13 0.0447 0.0042 110 121 1 99 LOU RRU 110 1 38.8 0.058 0.133 0.0142 95 103 112 LIM (I) MTN 0.0027 178 110 1 6.5 0.0053 0.0245 197 210

|         |         |         |     |        | Impedan | ce on 100 l | MVA Base |        | •         |        |
|---------|---------|---------|-----|--------|---------|-------------|----------|--------|-----------|--------|
| Voltage |         |         |     | Length |         | (pu)        |          | Ra     | ting (MVA | )      |
| (kV)    | From    | То      | No. | (km)   | R       | X           | В        | Summer | Autumn    | Winter |
| 110     | LIM (I) | RAT (I) | 1   | 28.4   | 0.0413  | 0.0963      | 0.0124   | 99     | 110       | 121    |
| 110     | LIM (I) | KLN     | 2   | 11.7   | 0.0179  | 0.0396      | 0.0089   | 80     | 95        | 110    |
| 110     | LIS     | SKL     | 1   | 39.3   | 0.0611  | 0.1352      | 0.0126   | 99     | 110       | 123    |
| 110     | LIS     | LOU     | 1   | 40.4   | 0.0628  | 0.1389      | 0.013    | 99     | 110       | 123    |
| 110     | LET     | TIV     | 1   | 45.2   | 0.0471  | 0.1508      | 0.0154   | 136    | 150       | 159    |
| 110     | LET     | TLK     | 1   | 34     | 0.051   | 0.117       | 0.0119   | 105    | 116       | 123    |
| 110     | LET     | GLT     | 1   | 38.4   | 0.0577  | 0.1316      | 0.0136   | 99     | 110       | 121    |
| 110     | LET     | STR (N) | 1   | 22.3   | 0.0346  | 0.0765      | 0.0072   | 99     | 110       | 123    |
| 110     | LIB     | MR      | 1   | 2.7    | 0.0014  | 0.0031      | 0.0165   | 100    | 100       | 100    |
| 110     | LIB     | MR      | 2   | 2.7    | 0.0015  | 0.0031      | 0.0167   | 99     | 110       | 119    |
| 110     | LSN     | THU     | 1   | 10.4   | 0.0162  | 0.0358      | 0.0034   | 104    | 113       | 122    |
| 110     | CUR     | NEN     | 1   | 18.8   | 0.0293  | 0.0648      | 0.0061   | 105    | 116       | 123    |
| 110     | CUR     | BKM     | 1   | 17.3   | 0.0039  | 0.0189      | 0.1921   | 190    | 190       | 190    |
| 110     | MHL     | RE      | 1   | 3      | 0.0022  | 0.0045      | 0.0301   | 140    | 140       | 140    |
| 110     | MHL     | TRN     | 1   | 1.4    | 0.001   | 0.0021      | 0.0141   | 140    | 140       | 140    |
| 110     | MCE     | SBH     | 1   | 4.7    | 0.0047  | 0.0151      | 0.0054   | 99     | 110       | 121    |
| 110     | MCE     | CDU     | 1   | о      | 0.0027  | 0.0099      | 0.0163   | 98     | 111       | 124    |
| 110     | MCD     | WOL     | 1   | 1.4    | 0.0008  | 0.0016      | 0.0086   | 120    | 120       | 131    |
| 110     | MID     | WHI     | 1   | 20     | 0.0303  | 0.0691      | 0.0065   | 99     | 110       | 121    |
| 110     | MTH     | LOU     | 1   | 15.1   | 0.0235  | 0.052       | 0.0049   | 99     | 110       | 121    |
| 110     | MAY     | GRI     | 1   | 2.2    | 0.0022  | 0.0069      | 0.0019   | 99     | 110       | 120    |
| 110     | MAY     | GRI     | 1   | 2.2    | 0.003   | 0.0087      | 0.0008   | 105    | 116       | 123    |
| 110     | MAY     | RYB     | 1   | 9      | 0.0092  | 0.0303      | 0.0052   | 178    | 197       | 219    |
| 110     | MAY     | RNW     | 1   | 7.1    | 0.0082  | 0.0239      | 0.0024   | 80     | 92        | 103    |
| 110     | MAY     | BLK     | 1   | 30.9   | 0.0322  | 0.1031      | 0.0106   | 99     | 110       | 121    |
| 110     | MIL     | RE      | 1   | 4.9    | 0.0026  | 0.0047      | 0.0746   | 100    | 100       | 100    |
| 110     | MIL     | RE      | 2   | 5.6    | 0.0029  | 0.0062      | 0.0338   | 120    | 120       | 131    |
| 110     | MAC     | CLA     | 2   | 5.7    | 0.0021  | 0.0099      | 0.0993   | 161    | 176       | 192    |
| 110     | MTN     | MUN     | 1   | 0.7    | 0.0011  | 0.0025      | 0.0003   | 105    | 116       | 123    |
| 110     | MTN     | MUN     | 2   | 0.7    | 0.0011  | 0.0024      | 0.0002   | 105    | 116       | 123    |
| 110     | MP      | ТВК Т   | 1   | 7.3    | 0.0046  | 0.0237      | 0.0026   | 178    | 197       | 210    |
| 110     | MR      | TBG     | 1   | 3.3    | 0.0014  | 0.0016      | 0.0358   | 178    | 198       | 219    |
| 110     | MR      | TBG     | 2   | 2.8    | 0.0012  | 0.0014      | 0.0309   | 178    | 206       | 219    |
| 110     | MR      | KBY     | 1   | 4      | 0.0041  | 0.0134      | 0.0028   | 109    | 119       | 130    |
| 110     | MR      | KBY     | 2   | 4      | 0.0041  | 0.0134      | 0.0028   | 103    | 119       | 130    |
| 110     | MAL     | KBY     | 1   | 29.2   | 0.0184  | 0.0949      | 0.0103   | 134    | 147       | 159    |
| 110     | MOY     | GLR     | 1   | 14     | 0.0216  | 0.048       | 0.0045   | 105    | 116       | 123    |
| 110     | MOY     | TAW     | 1   | 8.4    | 0.013   | 0.028       | 0.0036   | 99     | 110       | 123    |
| 110     | MOY     | TAW     | 2   | 8.3    | 0.0125  | 0.0286      | 0.0038   | 99     | 110       | 121    |
| 110     | BCT     | СКМ     | 1   | 3.1    | 0.0022  | 0.0047      | 0.0311   | 140    | 140       | 140    |

#### Impedance on 100 MVA Base Rating (MVA) Voltage Length (pu) (kV) From То No. (km) R Х В Summer Autumn Winter NEW (I) BLK 0.0042 110 1 12.2 0.0128 0.0407 136 150 159 0.0376 NQS RE 0.0008 0.0019 110 1 2.1 119 119 119 110 OUG OUG T 1 11 0.0171 0.0379 0.0036 105 116 123 PA STR 110 1 22.4 0.0349 0.0771 0.0072 105 116 123 PΒ RE 0.0002 0.002 0.0463 269 269 269 110 3 1.4 PB RE 0.0002 269 269 269 110 4 1.4 0.002 0.0463 RE PΒ 110 1.2 0.0005 0.0011 0.0157 112 112 112 1 RAF TBG 11 110 1 0.0164 0.0374 0.0048 195 201 220 RAF RSY 92 110 1 2.1 0.0033 0.0073 0.0007 63 82 RAF TBG 110 2 0.006 0.0306 0.0047 178 209 9.5 194 110 RNW DFR 1 25.9 0.0202 0.085 0.009 99 110 121 RRU SKL 110 1 12.7 0.0197 0.0436 0.0042 112 95 103 DAL 0.0069 110 SH 1 12 0.0075 0.0388 178 210 197 110 SH IKE T 0.019 178 210 1 53.9 0.0339 0.1752 197 110 SH SOM 1 13.8 0.0212 0.0468 0.0062 105 116 123 SLI SRA 110 1 11.1 0.0173 0.0382 0.0036 99 110 121 SLI SRA 110 2 12 0.0187 0.0413 0.0039 99 110 121 SOR TLK 0.0015 110 1 4.4 0.0069 0.0152 105 116 123 110 SOM SOM 1 2 0.0032 0.0069 0.0007 105 116 123 SRA CF 110 2 0.0309 178 49.2 0.1599 0.0174 197 210 110 STR STR 1 2 0.0032 0.0069 0.0007 105 116 123 110 SNG AA 5.5 0.0033 0.0171 0.0069 145 161 1 177 110 SBH CDU 1 1.8 0.0002 0.0027 0.0155 238 238 238 TBK TBK T 2.9 0.0046 0.01 116 110 1 0.001 105 123 CTN KLN 110 1 29.2 0.0184 0.095 0.0103 178 210 197 TIP 0.0428 CTN 0.0083 178 110 1 13.1 0.0047 210 197 110 TRL OUG T 1 11.3 0.0071 0.0368 0.004 178 197 210 THU IKE T 110 1 0.0162 0.0834 0.0091 178 25.7 197 210 110 CTG BVK 0.006 0.0358 0.3856 228 228 228 1 31.7 ΒK SKY 0.0044 187 110 1 4 0.001 0.044 206 223 CKM FAS 110 2.9 0.0046 0.01 0.001 105 116 123 1 CUR BKM 0.0038 0.0069 110 1 7.3 0.0722 120 120 120 AGH ENN (N) 110 1 31.1 0.0395 0.0947 0.019 109 114 124 ANT KEL 82 110 1 8.9 0.0116 0.0299 0.003 95 103 110 ANT KEL 2 8.9 0.0116 0.0299 0.003 82 95 103 BPS BVG 0.0226 0.0582 82 110 1 17.3 0.0059 95 103 BPS BVG 110 2 17.3 0.0226 0.0582 0.0059 82 103 95 BPS EDE 0.0228 80 86 110 15.1 0.0536 0.0049 69 1 BPS EDE 110 2 15.1 0.0227 0.0529 0.0049 70 81 87 **BMA** KEL 0.0345 110 1 10 0.0131 0.0033 109 119 124

|         |         |         |     |        | Impedan | ce on 100 l | NVA Base |        |           |        |  |  |
|---------|---------|---------|-----|--------|---------|-------------|----------|--------|-----------|--------|--|--|
| Voltage |         |         |     | Length |         | (pu)        |          | Ra     | ting (MVA | )      |  |  |
| (kV)    | From    | То      | No. | (km)   | R       | X           | В        | Summer | Autumn    | Winter |  |  |
| 110     | BMA     | KEL     | 2   | 11.5   | 0.015   | 0.0397      | 0.0038   | 109    | 119       | 124    |  |  |
| 110     | BAN     | TAN     | 1   | 18.4   | 0.024   | 0.0624      | 0.0062   | 82     | 95        | 103    |  |  |
| 110     | BAN     | TAN     | 2   | 18.4   | 0.0185  | 0.049       | 0.0047   | 82     | 95        | 103    |  |  |
| 110     | BVG     | KEL     | 1   | 21.2   | 0.0277  | 0.073       | 0.0071   | 109    | 119       | 124    |  |  |
| 110     | BVG     | KEL     | 2   | 20.3   | 0.0265  | 0.0699      | 0.0068   | 109    | 119       | 124    |  |  |
| 110     | BVG     | LAR     | 1   | 7.1    | 0.0071  | 0.0234      | 0.0025   | 79     | 79        | 113    |  |  |
| 110     | BVG     | LAR     | 2   | 7.1    | 0.0071  | 0.0234      | 0.0025   | 79     | 79        | 113    |  |  |
| 110     | BNH     | CAS     | 1   | 21.2   | 0.0277  | 0.0713      | 0.0072   | 82     | 95        | 103    |  |  |
| 110     | BNH     | CAS     | 2   | 21.2   | 0.0277  | 0.0713      | 0.0072   | 82     | 95        | 103    |  |  |
| 110     | BNM     | DON     | 1   | 6      | 0.0048  | 0.0046      | 0.0531   | 75     | 75        | 82     |  |  |
| 110     | BNM     | DON     | 2   | 5.8    | 0.0048  | 0.0046      | 0.0531   | 75     | 75        | 82     |  |  |
| 110     | BRO     | RSK     | 1   | 17.4   | 0.01    | 0.062       | 0.02     | 144    | 144       | 144    |  |  |
| 110     | CAR     | CAS     | 1   | 24.7   | 0.0371  | 0.0875      | 0.008    | 69     | 80        | 86     |  |  |
| 110     | CAR     | EDE     | 1   | 12.4   | 0.0187  | 0.0435      | 0.004    | 69     | 80        | 86     |  |  |
| 110     | CAR     | CAS     | 2   | 24.7   | 0.0369  | 0.0864      | 0.008    | 70     | 81        | 87     |  |  |
| 110     | CAR     | EDE     | 2   | 12.4   | 0.0188  | 0.044       | 0.004    | 69     | 80        | 86     |  |  |
| 110     | CAS     | CRE     | 1   | 3      | 0.0012  | 0.0036      | 0.0608   | 132    | 132       | 145    |  |  |
| 110     | CAS     | CRE     | 2   | 3      | 0.0012  | 0.0036      | 0.0609   | 132    | 132       | 145    |  |  |
| 110     | CAS     | KNO     | 1   | 4.6    | 0.0053  | 0.0045      | 0.0442   | 66     | 66        | 73     |  |  |
| 110     | CAS     | KNO     | 2   | 4.5    | 0.0052  | 0.0044      | 0.0435   | 66     | 66        | 73     |  |  |
| 110     | CAS     | NAR     | 1   | 18     | 0.0152  | 0.0403      | 0.0714   | 109    | 109       | 124    |  |  |
| 110     | CAS     | NAR     | 2   | 19.8   | 0.0177  | 0.0461      | 0.0705   | 109    | 124       | 124    |  |  |
| 110     | CAS     | RAT (N) | 1   | 18.9   | 0.0247  | 0.0636      | 0.0064   | 82     | 95        | 103    |  |  |
| 110     | CAS     | RAT (N) | 2   | 18.9   | 0.0247  | 0.0636      | 0.0064   | 82     | 95        | 103    |  |  |
| 110     | CAS     | ROS     | 1   | 1.8    | 0.0006  | 0.0025      | 0.0154   | 144    | 144       | 152    |  |  |
| 110     | CAS     | ROS     | 2   | 1.8    | 0.0006  | 0.0025      | 0.0154   | 144    | 144       | 152    |  |  |
| 110     | CEN     | CRE     | 1   | 3.2    | 0.0011  | 0.0044      | 0.0303   | 144    | 144       | 144    |  |  |
| 110     | CEN     | CRE     | 2   | 3.2    | 0.0011  | 0.0044      | 0.0303   | 144    | 144       | 144    |  |  |
| 110     | COL (N) | CPS     | 1   | 46.7   | 0.0609  | 0.1606      | 0.0155   | 82     | 95        | 103    |  |  |
| 110     | COL (N) | LIM (N) | 1   | 18.6   | 0.0243  | 0.0643      | 0.0062   | 82     | 95        | 103    |  |  |
| 110     | COL (N) | LOG     | 1   | 8.1    | 0.0106  | 0.0272      | 0.0028   | 82     | 95        | 103    |  |  |
| 110     | COL (N) | LOG     | 2   | 8.1    | 0.0106  | 0.0272      | 0.0028   | 82     | 95        | 103    |  |  |
| 110     | COL (N) | RSK     | 1   | 20     | 0.0237  | 0.0691      | 0.0066   | 186    | 191       | 193    |  |  |
| 110     | CPS     | КМТ     | 1   | 14.5   | 0.0108  | 0.0482      | 0.0051   | 143    | 158       | 166    |  |  |
| 110     | CPS     | LIM (N) | 1   | 29.5   | 0.0385  | 0.1014      | 0.0098   | 82     | 95        | 103    |  |  |
| 110     | CPS     | LMR     | 1   | 9      | 0.0117  | 0.0303      | 0.0031   | 82     | 95        | 103    |  |  |
| 110     | CPS     | LMR     | 2   | 9      | 0.0117  | 0.0303      | 0.0031   | 82     | 95        | 103    |  |  |
| 110     | CPS     | SPR     | 1   | 9.2    | 0.0107  | 0.0289      | 0.0116   | 82     | 95        | 103    |  |  |
| 110     | CPS     | SPR     | 2   | 9.4    | 0.0107  | 0.0291      | 0.0126   | 82     | 95        | 103    |  |  |
| 110     | CPS     | STR (N) | 1   | 27     | 0.0181  | 0.0529      | 0.0169   | 109    | 119       | 124    |  |  |

### Table B-2: Characteristics of Existing Transmission Circuits

| Voltage |         |         |     | Length | Impedan | ce on 100 l<br>(pu) | MVA Base | Ra     | ting (MVA | )      |
|---------|---------|---------|-----|--------|---------|---------------------|----------|--------|-----------|--------|
| (kV)    | From    | То      | No. | (km)   | R       | X                   | В        | Summer | Autumn    | Winter |
| 110     | CRG     | KEL     | 1   | 23.1   | 0.0293  | 0.0767              | 0.0129   | 82     | 95        | 103    |
| 110     | CRG     | TMN     | 1   | 36.2   | 0.0448  | 0.1191              | 0.0218   | 109    | 114       | 124    |
| 110     | DON     | HAN     | 1   | 6.1    | 0.0016  | 0.0045              | 0.1397   | 144    | 144       | 158    |
| 110     | DON     | HAN     | 2   | 5.9    | 0.0016  | 0.0045              | 0.1397   | 144    | 144       | 158    |
| 110     | DON     | FIN (N) | 1   | 3.7    | 0.0044  | 0.011               | 0.0076   | 69     | 81        | 86     |
| 110     | DON     | FIN (N) | 2   | 3.7    | 0.0045  | 0.0112              | 0.0075   | 69     | 80        | 86     |
| 110     | DRO (N) | DRQ     | 1   | 0      | 0.0072  | 0.0449              | 0.0043   | 187    | 200       | 200    |
| 110     | DRO (N) | ENN (N) | 1   | 0      | 0.0257  | 0.0663              | 0.0067   | 82     | 95        | 103    |
| 110     | DRO (N) | ENN (N) | 2   | 0      | 0.0257  | 0.0663              | 0.0067   | 82     | 95        | 103    |
| 110     | DRO (N) | OMA     | 1   | 0      | 0.0183  | 0.0471              | 0.0048   | 82     | 95        | 103    |
| 110     | DRO (N) | OMA     | 2   | 0      | 0.0183  | 0.0471              | 0.0048   | 82     | 95        | 103    |
| 110     | DRU (N) | TAN     | 1   | 4.4    | 0.0044  | 0.0145              | 0.0015   | 79     | 96        | 113    |
| 110     | DRU (N) | TAN     | 2   | 4.4    | 0.0044  | 0.0145              | 0.0015   | 79     | 96        | 113    |
| 110     | DRU (N) | TAN     | 3   | 4.1    | 0.0048  | 0.0136              | 0.0014   | 108    | 119       | 126    |
| 110     | DRU (N) | TMN     | 1   | 22.7   | 0.0294  | 0.0755              | 0.0077   | 109    | 119       | 124    |
| 110     | DRU (N) | TMN     | 2   | 21.5   | 0.0279  | 0.0726              | 0.012    | 109    | 119       | 124    |
| 110     | DUN     | TMN     | 1   | 6.5    | 0.0043  | 0.0171              | 0.005    | 157    | 171       | 178    |
| 110     | DUN     | TMN     | 2   | 5.8    | 0.0091  | 0.0234              | 0.0024   | 144    | 144       | 144    |
| 110     | DUN     | OMA     | 1   | 36.1   | 0.0419  | 0.1238              | 0.012    | 186    | 191       | 193    |
| 110     | DUN     | TMN     | 3   | 6      | 0.0037  | 0.0198              | 0.0186   | 186    | 191       | 193    |
| 110     | FIN (N) | HAN     | 1   | 3      | 0.0008  | 0.0032              | 0.0224   | 144    | 144       | 144    |
| 110     | FIN (N) | HAN     | 2   | 3.2    | 0.0008  | 0.0032              | 0.0224   | 144    | 144       | 144    |
| 110     | GLE (N) | KEL     | 1   | 21.4   | 0.0273  | 0.0683              | 0.0272   | 82     | 82        | 90     |
| 110     | GLE (N) | KEL     | 2   | 21.4   | 0.0273  | 0.0683              | 0.0273   | 82     | 82        | 90     |
| 110     | GOR (N) | OMA     | 1   | 17.1   | 0.0106  | 0.0657              | 0.0063   | 200    | 200       | 200    |
| 110     | GOR (N) | TMN     | 1   | 34.8   | 0.0212  | 0.1313              | 0.0126   | 200    | 200       | 200    |
| 110     | HAN     | LIS (N) | 1   | 9.2    | 0.0097  | 0.0265              | 0.0182   | 82     | 95        | 103    |
| 110     | HAN     | LIS (N) | 2   | 9.2    | 0.0086  | 0.0263              | 0.018    | 80     | 93        | 100    |
| 110     | KEL     | RSK     | 1   | 25.9   | 0.0391  | 0.133               | 0.0132   | 185    | 190       | 193    |
| 110     | KMT     | SLK     | 1   | 6.2    | 0.0073  | 0.0182              | 0.0061   | 109    | 119       | 124    |
| 110     | KMT     | STR (N) | 1   | 11.2   | 0.0082  | 0.0367              | 0.0039   | 143    | 158       | 166    |
| 110     | LIS (N) | TAN     | 1   | 31     | 0.0405  | 0.1059              | 0.0104   | 82     | 95        | 103    |
| 110     | LIS (N) | TAN     | 2   | 29.2   | 0.0339  | 0.1002              | 0.0087   | 80     | 93        | 100    |
| 110     | MKL     | OMA     | 1   | 37.5   | 0.0278  | 0.1132              | 0.0146   | 139    | 150       | 157    |
| 110     | NEW (N) | TAN     | 1   | 24.1   | 0.0312  | 0.0804              | 0.0081   | 82     | 95        | 103    |
| 110     | NEW (N) | TAN     | 2   | 24     | 0.0312  | 0.0804              | 0.0081   | 82     | 95        | 103    |
| 110     | OMA     | STR (N) | 1   | 35.5   | 0.0464  | 0.1226              | 0.0118   | 109    | 119       | 124    |
| 110     | OMA     | STR (N) | 2   | 35.5   | 0.0472  | 0.1247              | 0.012    | 82     | 95        | 103    |
| 110     | OMA     | TRE     | 1   | 21.4   | 0.0253  | 0.0734              | 0.0071   | 186    | 191       | 193    |
| 110     | TAN     | WAR     | 1   | 12.9   | 0.0129  | 0.0424              | 0.0045   | 79     | 96        | 113    |
| 110     | TAN     | WAR     | 2   | 12.9   | 0.0129  | 0.0424              | 0.0045   | 79     | 96        | 113    |
| 110     | TRE     | TMN     | 1   | 42.9   | 0.0254  | 0.082               | 0.0245   | 186    | 191       | 193    |

# Table B-2: Characteristics of Existing Transmission Circuits

|         |             |                 |            | I                   |         | Malta a        | - Datia            |
|---------|-------------|-----------------|------------|---------------------|---------|----------------|--------------------|
|         |             | Deting          |            | Impeda<br>100 MVA I |         | Voltage        | e Ratio<br>g Range |
| Station | Transformer | Rating<br>(MVA) | HV/LV (kV) | R                   |         | - Tapping<br>+ |                    |
| DSN     | T4201       | 500             | 400/220    | 0.0002              | 0.0317  | 0.01           | 0.15               |
| DSN     | T4201       | 500             | 400/220    | 0.0002              | 0.027   | 0.01           | 0.07               |
| MP      | T4202       | 500             | 400/220    | 0.0003              | 0.027   | 0.1            | 0.07               |
| MP      | T4201       | 500             | 400/220    | 0.0002              | 0.0329  | 0.03           | 0.13               |
| OST     | T4202       | 500             | 400/220    | 0.0002              | 0.027   | 0.05           | 0.07               |
| WOO     | T4201       | 500             | 400/220    | 0.0002              | 0.0316  | 0.07           | 0.09               |
| WOO     | T4201       | 550             | 400/220    | 0.0002              | 0.0316  | 0.07<br>N/     | -                  |
| WOO     | T4202       | 500             | 400/220    | 0.0002              | 0.027   | 0.07           | 0.09               |
| LOU     | AT1         | 300             | 275/220    | 0.0002              | 0.0303  | 0.15           | 0.09               |
| LOU     | AT2         | 600             | 220/275    | 0.0008              | 0.03    | 0.15           | 0.15               |
| LOU     | AT3         | 300             | 220/275    | 0.0008              | 0.015   | 0.15           | 0.15               |
| AD      | T2101       | 125             | 220/2/5    | 0.000               | 0.124   | 0.1            | 0.15               |
| ARK     | T2101       | 63              | 220/110    | 0.007               | 0.124   | 0.23           | 0.10               |
| ARK     | T2101       | 125             | 220/110    | 0.0021              | 0.1237  | 0.11           | 0.16               |
| BYH     | T2102       | 250             | 220/110    | 0.0021              | 0.064   | 0.09           | 0.17               |
| BVS     | T2101       | 250             | 220/110    | 0.001               | 0.064   | 0.09           | 0.17               |
| BVS     | T2101       | 250             | 220/110    | 0.001               | 0.064   | 0.09           | 0.17               |
| BYB     | T2102       | 250             | 220/110    | 0.001               | 0.064   | 0.09           | 0.17               |
| BLC     | T2102       | 250             | 220/110    | 0.001               | 0.0646  | 0.1            | 0.18               |
| CBT     | T2101       | 250             | 220/110    | 0.001               | 0.0646  | 0.1            | 0.18               |
| CBT     | T2102       | 250             | 220/110    | 0.001               | 0.0646  | 0.1            | 0.1                |
| CBT     | T2103       | 250             | 220/110    | 0.001               | 0.0646  | 0.1            | 0.1                |
| CBT     | T2104       | 250             | 220/110    | 0.001               | 0.0646  | 0.1            | 0.1                |
| CDU     | T2101       | 250             | 220/110    | 0.00093             | 0.06152 | 0.09           | 0.17               |
| CDU     | T2102       | 250             | 220/110    | 0.00066             | 0.061   | 0.09           | 0.17               |
| СКМ     | T2101       | 250             | 220/110    | 0.001               | 0.0646  | 0.09           | 0.17               |
| СКМ     | T2102       | 250             | 220/110    | 0.001               | 0.0646  | 0.09           | 0.17               |
| СКМ     | T2103       | 250             | 220/110    | 0.001               | 0.0646  | 0.09           | 0.17               |
| СКМ     | T2104       | 250             | 220/110    | 0.0004              | 0.0631  | 0.09           | 0.18               |
| CLA     | T2101       | 250             | 220/110    | 0.0013              | 0.0647  | 0.1            | 0.09               |
| CLA     | T2102       | 250             | 220/110    | 0.0013              | 0.0647  | 0.09           | 0.17               |
| CSH     | T2101       | 238             | 220/110    | 0.0004              | 0.0631  | 0.09           | 0.18               |
| CSH     | T2102       | 250             | 220/110    | 0.0004              | 0.0631  | 0.09           | 0.18               |
| CSH     | T2104       | 175             | 220/110    | 0.0021              | 0.1332  | 0.22           | 0.18               |
| CUL     | T2101       | 250             | 220/110    | 0.0005              | 0.064   | 0.09           | 0.18               |
| FIN     | T2101       | 250             | 220/110    | 0.0013              | 0.0651  | 0.09           | 0.18               |
| FIN     | T2102       | 250             | 220/110    | 0.0013              | 0.0648  | 0.09           | 0.18               |
| FIN     | T2103       | 250             | 220/110    | 0.001               | 0.064   | 0.09           | 0.17               |
| FIN     | T2104       | 250             | 220/110    | 0.001               | 0.0638  | 0.09           | 0.17               |
| FIN     | T2105       | 250             | 220/110    | 0.001               | 0.064   | 0.09           | 0.17               |

### Table B-3: Characteristics of Existing Transformers in Ireland

|         |             |        |            | Impeda    |           | Voltag  |         |
|---------|-------------|--------|------------|-----------|-----------|---------|---------|
|         |             | Rating |            | 100 MVA E | Base (pu) | Tapping | g Range |
| Station | Transformer | (MVA)  | HV/LV (kV) | R         | X         | +       | -       |
| FLA     | T2101       | 125    | 220/110    | 0.0027    | 0.128     | 0.09    | 0.18    |
| FLA     | T2102       | 125    | 220/110    | 0.0008    | 0.1331    | 0.09    | 0.18    |
| GI      | T2101       | 125    | 220/110    | 0.0026    | 0.1331    | 0.09    | 0.18    |
| GI      | T2102       | 125    | 220/110    | 0.0023    | 0.1237    | 0.22    | 0.18    |
| GOR     | T2101       | 250    | 220/110    | 0.001     | 0.064     | 0.09    | 0.18    |
| INC     | T2101       | 250    | 220/110    | 0.001     | 0.0564    | 0.09    | 0.17    |
| INC     | T2102       | 250    | 220/110    | 0.001     | 0.0564    | 0.09    | 0.17    |
| INC     | T2103       | 250    | 220/110    | 0.0001    | 0.06      | 0.09    | 0.18    |
| INC     | T2104       | 250    | 220/110    | 0.0001    | 0.06      | 0.09    | 0.18    |
| KLN     | T2103       | 250    | 220/110    | 0.0004    | 0.0631    | 0.09    | 0.18    |
| KLN     | T2104       | 120    | 220/110    | 0.0004    | 0.0631    | 0.12    | 0.15    |
| KLS     | T2101       | 125    | 220/110    | 0.00132   | 0.1237    | 0.12    | 0.15    |
| KLS     | T2102       | 125    | 220/110    | 0.0008    | 0.1237    | 0.12    | 0.15    |
| KNR     | T2101       | 250    | 220/110    | 0.001     | 0.064     | 0.09    | 0.17    |
| KNR     | T2102       | 250    | 220/110    | 0.001     | 0.064     | 0.09    | 0.17    |
| KPG     | T2101       | 250    | 220/110    | 0.0004    | 0.0631    | 0.09    | 0.18    |
| KPG     | T2102       | 250    | 220/110    | 0.0004    | 0.0631    | 0.09    | 0.18    |
| KRA     | T2101       | 250    | 220/110    | 0.0013    | 0.0652    | 0.09    | 0.17    |
| KRA     | T2102       | 250    | 220/110    | 0.0013    | 0.0647    | 0.09    | 0.17    |
| KRA     | T2103       | 250    | 220/110    | 0.0013    | 0.0652    | 0.09    | 0.17    |
| LDW     | T2101       | 250    | 220/110    | 0.001     | 0.064     | 0.09    | 0.18    |
| LOU     | T2101       | 125    | 220/110    | 0.0022    | 0.1331    | 0.26    | 0.14    |
| LOU     | T2102       | 125    | 220/110    | 0.0023    | 0.1324    | 0.26    | 0.14    |
| LOU     | T2103       | 125    | 220/110    | 0.0022    | 0.1324    | 0.26    | 0.14    |
| LOU     | T2104       | 250    | 220/110    | 0.001     | 0.064     | 0.09    | 0.17    |
| MAY     | T2101       | 125    | 220/110    | 0.0021    | 0.1339    | 0.22    | 0.18    |
| MAY     | T2102       | 238    | 220/110    | 0.001     | 0.064     | 0.09    | 0.17    |
| MAY     | T2103       | 125    | 220/110    | 0.0021    | 0.1324    | 0.22    | 0.18    |
| MAY     | T2104       | 250    | 220/110    | 0.001     | 0.064     | 0.09    | 0.17    |
| MP      | T2101       | 250    | 220/110    | 0.001     | 0.064     | 0.09    | 0.17    |
| PB      | T2103       | 250    | 220/110    | 0.0013    | 0.059     | 0.08    | 0.17    |
| PB      | T2104       | 250    | 220/110    | 0.0013    | 0.0609    | 0.08    | 0.17    |
| RAF     | T2101       | 238    | 220/110    | 0.001     | 0.064     | 0.09    | 0.17    |
| RAF     | T2102       | 250    | 220/110    | 0.00045   | 0.0558    | 0.09    | 0.17    |
| SH      | T2101       | 125    | 220/110    | 0.00131   | 0.1237    | 0.09    | 0.18    |
| SH      | T2102       | 125    | 220/110    | 0.00574   | 0.1237    | 0.09    | 0.18    |
| SRA     | T2101       | 250    | 220/110    | 0.001     | 0.064     | 0.09    | 0.18    |
| TB      | T2101       | 238    | 220/110    | 0.00099   | 0.0554    | 0.09    | 0.17    |
| TB      | T2102       | 238    | 220/110    | 0.00099   | 0.0554    | 0.09    | 0.17    |

# Table B-3: Characteristics of Existing Transformers in Ireland

|             |          |       | Impedan | ce pu on : | 100 MVA | oase |        |      |        |     | Off No | minal | No.  |
|-------------|----------|-------|---------|------------|---------|------|--------|------|--------|-----|--------|-------|------|
| Substation/ | HV/LV    | W     | 1-2     | W:         | 2-3     |      | W3-1   | Rati | ing (M | VA) | Ratio  | (pu)  | of   |
| Transformer | (kV)     | R     | X       | R          | X       | R    | X      | W1   | W2     | W3  | Upper  | Lower | Taps |
| BPS IBTx 1  | 275/110  | 0.002 | 0.064   | 0.002      | 0.209   | 0    | 0.133  | 240  | 240    | 30  | 1.15   | 0.85  | 19   |
| BPS IBTx 2  | 275/110  | 0.002 | 0.064   | 0.002      | 0.206   | 0    | 0.128  | 240  | 240    | 30  | 1.15   | 0.85  | 19   |
| CAS IBTx 1  | 275/110  | 0.002 | 0.064   | 0.002      | 0.209   | 0    | 0.133  | 240  | 240    | 60  | 1.15   | 0.85  | 19   |
| CAS IBTx 2  | 275/110  | 0.001 | 0.064   | 0.001      | 0.224   | 0    | 0.145  | 240  | 240    | 30  | 1.15   | 0.85  | 19   |
| CAS IBTx 3  | 275/110  | 0.002 | 0.066   | 0.002      | 0.238   | 0    | 0.159  | 240  | 240    | 30  | 1.15   | 0.85  | 19   |
| CPS IBTx 1  | 275/110  | 0.002 | 0.061   | 0.002      | 0.127   | 0    | 0.057  | 240  | 240    | 60  | 1.15   | 0.85  | 19   |
| CPS IBTx 2  | 275/110  | 0.001 | 0.064   | 0.001      | 0.224   | 0    | 0.145  | 240  | 240    | 30  | 1.15   | 0.85  | 19   |
| HAN IBTx 1  | 275/110  | 0.002 | 0.059   | 0.002      | 0.126   | 0    | 0.056  | 240  | 240    | 45  | 1.15   | 0.85  | 19   |
| HAN IBTx 2  | 275/110  | 0.002 | 0.059   | 0.002      | 0.126   | 0    | 0.056  | 240  | 240    | 45  | 1.15   | 0.85  | 19   |
| HAN IBTx 3  | 275/110  | 0.001 | 0.064   | 0.001      | 0.224   | 0    | 0.145  | 240  | 240    | 60  | 1.15   | 0.85  | 19   |
| KEL IBTx 1  | 275/110  | 0.002 | 0.061   | 0.002      | 0.127   | 0    | 0.057  | 240  | 240    | 45  | 1.15   | 0.85  | 19   |
| KEL IBTx 2  | 275/110  | 0.002 | 0.061   | 0.002      | 0.132   | 0    | 0.057  | 240  | 240    | 45  | 1.15   | 0.85  | 19   |
| TAN IBTx 1  | 275/110  | 0.002 | 0.064   | 0.002      | 0.209   | 0    | 0.133  | 240  | 240    | 30  | 1.15   | 0.85  | 19   |
| TAN IBTx 2  | 275/110  | 0.002 | 0.064   | 0.002      | 0.209   | 0    | 0.133  | 240  | 240    | 30  | 1.15   | 0.85  | 19   |
| TAN IBTx 3  | 275/110  | 0.001 | 0.064   | 0.002      | 0.238   | 0    | 0.158  | 240  | 240    | 60  | 1.15   | 0.85  | 19   |
| TMN IBTx 1  | 275/110  | 0.001 | 0.064   | 0.004      | 0.224   | 0    | 0.151  | 240  | 240    | 60  | 1.15   | 0.85  | 19   |
| TMN IBTx 2  | 275/110  | 0.001 | 0.064   | 0.004      | 0.232   | 0    | 0.15   | 240  | 240    | 60  | 1.15   | 0.85  | 19   |
| KPS IBTx 1  | 275/11.5 | 0     | 0.164   | 0          | 0.304   | 0    | 0.164  | 110  | 55     | 55  | 1.15   | 0.938 | 33   |
| KPS IBTx1   | 275/11.5 | 0     | 0.1635  | 0          | 0.3040  | 0    | 0.1635 | 110  | 55     | 55  | 1.15   | 0.938 | 33   |

# Table B-4: Characteristics of Existing 3 Winding Transformers in Northern Ireland

|         |            |        | Impedar | ice pu on   |         |            |             |
|---------|------------|--------|---------|-------------|---------|------------|-------------|
|         |            | Rating | 1       | ,<br>g base | Off nom | inal ratio |             |
| Station | HV/LV (kV) | (MVA)  | R       | X           | Upper   | Lower      | No. of taps |
| AGH     | 110/33     | 90     | 0.0039  | 0.2464      | 1.1     | 0.8        | 19          |
| ANT     | 110/33     | 90     | 0.0039  | 0.2464      | 1.1     | 0.8        | 19          |
| ANT     | 110/33     | 90     | 0.0039  | 0.2473      | 1.1     | 0.8        | 19          |
| BMA     | 110/33     | 90     | 0.0039  | 0.2447      | 1.1     | 0.8        | 19          |
| BMA     | 110/33     | 60     | 0.0065  | 0.2893      | 1.1     | 0.8        | 19          |
| BMA     | 110/33     | 90     | 0.0039  | 0.2463      | 1.1     | 0.8        | 19          |
| BMA     | 110/33     | 60     | 0.0065  | 0.2867      | 1.1     | 0.8        | 19          |
| BAN (N) | 110/33     | 30     | 0.0171  | 0.4133      | 1.1     | 0.8        | 15          |
| BAN (N) | 110/33     | 30     | 0.019   | 0.414       | 1.1     | 0.8        | 15          |
| BAN (N) | 110/33     | 30     | 0.019   | 0.4167      | 1.1     | 0.8        | 15          |
| BAN (N) | 110/33     | 30     | 0.019   | 0.415       | 1.1     | 0.8        | 15          |
| BNH     | 110/33     | 90     | 0.0037  | 0.2419      | 1.1     | 0.8        | 19          |
| BNH     | 110/33     | 90     | 0.0038  | 0.2413      | 1.1     | 0.8        | 19          |
| BNM     | 110/33     | 90     | 0.0039  | 0.2461      | 1.1     | 0.8        | 19          |
| BNM     | 110/33     | 90     | 0.0039  | 0.2461      | 1.1     | 0.8        | 19          |
| BRO     | 110/33     | 100    | 0.0035  | 0.16        | 1.1     | 0.9        | 33          |
| CAR     | 110/33     | 90     | 0.0039  | 0.248       | 1.1     | 0.8        | 19          |
| CAR     | 110/33     | 90     | 0.0039  | 0.248       | 1.1     | 0.8        | 19          |
| CEN     | 110/33     | 90     | 0.0037  | 0.2422      | 1.1     | 0.8        | 19          |
| CEN     | 110/33     | 90     | 0.0038  | 0.2419      | 1.1     | 0.8        | 19          |
| COL (N) | 110/33     | 60     | 0.0074  | 0.2512      | 1.1     | 0.8        | 19          |
| COL (N) | 110/33     | 60     | 0.0075  | 0.2508      | 1.1     | 0.8        | 19          |
| CPS     | 110/33     | 90     | 0.0087  | 0.2559      | 1.1     | 0.8        | 19          |
| CPS     | 110/33     | 90     | 0.0087  | 0.2573      | 1.1     | 0.8        | 19          |
| CRG     | 110/33     | 60     | 0.0074  | 0.2515      | 1.1     | 0.8        | 19          |
| CRG     | 110/33     | 60     | 0.0074  | 0.2508      | 1.1     | 0.8        | 19          |
| CRE     | 110/33     | 75     | 0.0091  | 0.1953      | 1.1     | 0.8        | 19          |
| CRE     | 110/33     | 75     | 0.0091  | 0.1967      | 1.1     | 0.8        | 19          |
| DON     | 110/33     | 90     | 0.004   | 0.2403      | 1.1     | 0.8        | 19          |
| DON     | 110/33     | 60     | 0.0119  | 0.3658      | 1.1     | 0.8        | 19          |
| DON     | 110/33     | 60     | 0.0119  | 0.3607      | 1.1     | 0.8        | 19          |
| DON     | 110/33     | 60     | 0.0119  | 0.3658      | 1.1     | 0.8        | 19          |
| DRU (N) | 110/33     | 90     | 0.0061  | 0.2423      | 1.1     | 0.8        | 19          |
| DRU (N) | 110/33     | 90     | 0.0061  | 0.2426      | 1.1     | 0.8        | 19          |
| DRQ     | 110/33     | 90     | 0.0039  | 0.2461      | 1.1     | 0.8        | 19          |
| DUN     | 110/33     | 90     | 0.0087  | 0.2566      | 1.1     | 0.8        | 19          |
| DUN     | 110/33     | 90     | 0.0087  | 0.2599      | 1.1     | 0.8        | 19          |
| EDE     | 110/33     | 45     | 0.0125  | 0.2733      | 1.1     | 0.8        | 19          |

#### Table B-5: Characteristics of Existing 2 Winding Transformers in Northern Ireland<sup>130</sup>

130 110/33 kV transformers in Northern Ireland are included here as these are controlled by SONI. 110/38 kV transformers in Ireland are not included here as these are controlled by ESB Networks.

# Table B-5: Characteristics of Existing 2 Winding Transformers in Northern Ireland

|         |            |        | Impedan | ice pu on |          |            |             |
|---------|------------|--------|---------|-----------|----------|------------|-------------|
|         |            | Rating | -       | ,<br>base | Off nomi | inal ratio |             |
| Station | HV/LV (kV) | (MVA)  | R       | X         | Upper    | Lower      | No. of taps |
| EDE     | 110/33     | 45     | 0.0123  | 0.2738    | 1.1      | 0.8        | 19          |
| ENN (N) | 110/33     | 45     | 0.0126  | 0.272     | 1.1      | 0.8        | 19          |
| ENN (N) | 110/33     | 45     | 0.0126  | 0.2733    | 1.1      | 0.8        | 19          |
| ENN (N) | 110/33     | 45     | 0.0078  | 0.2512    | 1.1      | 0.8        | 19          |
| FIN (N) | 110/33     | 45     | 0.0076  | 0.2533    | 1.1      | 0.8        | 19          |
| FIN (N) | 110/33     | 45     | 0.0076  | 0.2549    | 1.1      | 0.8        | 19          |
| GLE (N) | 110/33     | 60     | 0.0119  | 0.2692    | 1.1      | 0.8        | 19          |
| GOR (N) | 110/33     | 90     | 0.0039  | 0.2461    | 1.1      | 0.8        | 19          |
| КМТ     | 110/33     | 90     | 0.0039  | 0.2461    | 1.1      | 0.8        | 19          |
| KNO     | 110/33     | 90     | 0.0039  | 0.2461    | 1.1      | 0.8        | 19          |
| KNO     | 110/33     | 90     | 0.0039  | 0.2461    | 1.1      | 0.8        | 19          |
| LAR     | 110/33     | 45     | 0.0116  | 0.2778    | 1.1      | 0.8        | 15          |
| LAR     | 110/33     | 45     | 0.0116  | 0.2771    | 1.1      | 0.8        | 15          |
| LIM (N) | 110/33     | 45     | 0.0125  | 0.2809    | 1.1      | 0.8        | 15          |
| LIM (N) | 110/33     | 45     | 0.0122  | 0.2764    | 1.1      | 0.8        | 15          |
| LIS (N) | 110/33     | 90     | 0.0087  | 0.254     | 1.1      | 0.8        | 19          |
| LIS (N) | 110/33     | 90     | 0.0086  | 0.2569    | 1.1      | 0.8        | 19          |
| LMR     | 110/33     | 45     | 0.0076  | 0.254     | 1.1      | 0.8        | 19          |
| LMR     | 110/33     | 45     | 0.0076  | 0.2533    | 1.1      | 0.8        | 19          |
| LOG     | 110/33     | 45     | 0.0126  | 0.2738    | 1.1      | 0.8        | 19          |
| LOG     | 110/33     | 45     | 0.0128  | 0.28      | 1.1      | 0.8        | 19          |
| MKL     | 110/33     | 90     | 0.0039  | 0.2502    | 1.1      | 0.8        | 19          |
| MKL     | 110/33     | 90     | 0.0039  | 0.2502    | 1.1      | 0.8        | 19          |
| NAR     | 110/33     | 60     | 0.0075  | 0.2505    | 1.1      | 0.8        | 19          |
| NAR     | 110/33     | 60     | 0.0073  | 0.25      | 1.1      | 0.8        | 19          |
| NEW (N) | 110/33     | 90     | 0.0038  | 0.2427    | 1.1      | 0.8        | 19          |
| NEW (N) | 110/33     | 90     | 0.0038  | 0.2419    | 1.1      | 0.8        | 19          |
| OMA     | 110/33     | 90     | 0.0039  | 0.2481    | 1.1      | 0.8        | 19          |
| OMA     | 110/33     | 90     | 0.0039  | 0.249     | 1.1      | 0.8        | 19          |
| RSK     | 110/33     | 90     | 0.0039  | 0.2461    | 1.1      | 0.8        | 19          |
| RAT (N) | 110/33     | 90     | 0.0087  | 0.2549    | 1.1      | 0.8        | 19          |
| RAT (N) | 110/33     | 90     | 0.0046  | 0.2402    | 1.1      | 0.8        | 19          |
| ROS     | 110/33     | 90     | 0.0087  | 0.2576    | 1.1      | 0.8        | 19          |
| ROS     | 110/33     | 90     | 0.0087  | 0.2533    | 1.1      | 0.8        | 19          |
| SPR     | 110/33     | 90     | 0.0039  | 0.247     | 1.1      | 0.8        | 19          |
| SPR     | 110/33     | 90     | 0.0039  | 0.2471    | 1.1      | 0.8        | 19          |
| STR (N) | 110/33     | 45     | 0.0076  | 0.2522    | 1.1      | 0.8        | 19          |
| STR (N) | 110/33     | 45     | 0.0076  | 0.2516    | 1.1      | 0.8        | 19          |
| TRE     | 110/33     | 90     | 0.0039  | 0.2461    | 1.1      | 0.8        | 19          |
| WAR     | 110/33     | 90     | 0.0039  | 0.2481    | 1.1      | 0.8        | 19          |
| WAR     | 110/33     | 90     | 0.0039  | 0.2488    | 1.1      | 0.8        | 19          |

### Table B-6: Characteristics of Existing Power Flow Controllers

|         | Voltage |               | Rating    | Impedance on<br>100 MVA Base (pu) |        | Phase Angle Range<br>electrical degrees) |      |  |
|---------|---------|---------------|-----------|-----------------------------------|--------|--|------|--|
| Station | (kV)    | Circuit       | (MVA) R X |                                   | +      | -  |      |  |
| СКМ     | 220     | CKM – PB      | 350       | 0.000                             | 0.029  | 15.3                                     | 15.3 |  |
| ENN (N) | 110     | ENN (N) – COR | 125       | 0.000                             | 0.0213 | 45                                       | 45   |  |
| STR (N) | 110     | STR (N) – LET | 125       | 0.000                             | 0.0213 | 45                                       | 45   |  |

#### Table B-7: Characteristics of Existing Reactive Compensation

|         |              |                                  | Capabilit | y (Mvar) |
|---------|--------------|----------------------------------|-----------|----------|
| Station | Voltage (kV) | Plant                            | Generate  | Absorb   |
| AA      | 110          | 1 Capacitor                      | 30        |          |
| ATH     | 110          | 3 Capacitors (1 Mobile)          | 90        |          |
| BAN (I) | 110          | 1 Capacitor                      | 15        |          |
| BYC     | 275          | 4 Capacitors (4 x 59)            | 236       |          |
| CAH     | 110          | 4 Capacitors (4 x 15)            | 60        |          |
| CAS     | 22           | 3 Capacitors (3 x 25)            | 75        |          |
| CAS     | 22           | 1 Shunt Reactor                  |           | 30       |
| CBR     | 110          | 1 Capacitor                      | 30        |          |
| CBR     | 110          | 1 Static Var Compensator         | 60        | 10       |
| CF      | 110          | 1 Capacitor                      | 15        |          |
| CGL     | 20           | 3 Capacitors (3 x 1)             | 3         |          |
| СКМ     | 220          | 1 Shunt Reactor                  |           | 100      |
| СКМ     | 38           | 1 Shunt Reactor                  |           | 20       |
| COL (N) | 110          | 1 Capacitor                      | 36        |          |
| CPS     | 110          | 1 Capacitor                      | 40        |          |
| CSH     | 110          | 2 Capacitors (2 x 40)            | 80        |          |
| CUN     | 20           | 2 Capacitors (2 x 4)             | 8         |          |
| DLN     | 33           | 1 Capacitor                      | 5         |          |
| DLT     | 110          | 1 Capacitor                      | 15        |          |
| DMY     | 110          | 1 Capacitor                      | 15        |          |
| DOO     | 110          | 1 Capacitor                      | 15        |          |
| DRU (I) | 110          | 1 Capacitor                      | 15        |          |
| DYN     | 20           | 2 Capacitors (2 x 3.25)          | 6.5       |          |
| FIN (I) | 38           | 1 Shunt Reactor                  |           | 20       |
| GAR     | 20           | 2 Capacitors (1 x 12.4, 1 x 1.5) | 13.9      |          |
| GAR     | 20           | 1 Shunt Reactor                  |           | 9        |
| GAR     | 20           | 1 STATCOM                        | 3         | 7.5      |
| GIL     | 20           | 1 Capacitor                      | 12        |          |
| GWE     | 110          | 1 Capacitor                      | 15        |          |
| HAN     | 22           | 2 Shunt Reactors (2 x 30)        |           | 60       |
| INC     | 38           | 2 Shunt Reactors (2 x 20)        |           | 40       |
| KEL     | 22           | 2 Shunt Reactors (2 x 30)        |           | 60       |
| KNR     | 220          | 1 Shunt Reactor                  |           | 50       |

|         |              |                           | Capabilit | y (Mvar) |
|---------|--------------|---------------------------|-----------|----------|
| Station | Voltage (kV) | Plant                     | Generate  | Absorb   |
| KNY     | 110          | 1 Capacitor               | 30        |          |
| ККҮ     | 110          | 2 Capacitor (2 x 15)      | 30        |          |
| KTL     | 10           | 1 Capacitor               | 30        |          |
| LET     | 110          | 2 Capacitor (1 Mobile)    | 45        |          |
| LET     | 110          | 1 Static Var Compensator  | 30        |          |
| LIS (I) | 110          | 2 Capacitors (2 x 15)     | 30        |          |
| LOU     | 110          | 1 Capacitor               | 30        |          |
| LSN     | 20           | 1 Capacitor               | 4         |          |
| MOY     | 110          | 2 Capacitors (2 x 15)     | 30        |          |
| MRY     | 20           | 1 Capacitor               | 4         |          |
| MUL     | 110          | 2 Capacitors (2 x 15)     | 30        |          |
| NAV     | 110          | 1 Capacitor (1 Mobile)    | 30        |          |
| PB      | 220          | 2 Shunt Reactors (2 x 50) |           | 100      |
| POR     | 400          | EWIC HVDC                 | 175       | 175      |
| RAF     | 110          | 1 Capacitor               | 60        |          |
| RE      | 38           | 1 Shunt Reactor           |           | 20       |
| SKL     | 110          | 1 Capacitor (1 Mobile)    | 30        |          |
| SLB     | 20           | 1 Capacitor               | 15        |          |
| SLI     | 110          | 1 Capacitor               | 15        |          |
| SLK     | 20           | 1 Capacitor               | 13        |          |
| TAN     | 22           | 2 Capacitors (2 x 25)     | 50        |          |
| TAN     | 22           | 2 Shunt Reactors (2 x 30) |           | 60       |
| THU     | 110          | 2 Capacitors (2 x 15)     | 30        |          |
| TRI     | 110          | 1 Capacitor               | 30        |          |
| TRL     | 110          | 1 Capacitor               | 30        |          |
| WEX     | 110          | 2 Capacitors (2 x 15)     | 30        |          |

#### Table B-7: Characteristics of Existing Reactive Compensation

# **B.2. Transmission System Developments**

Future developments of the transmission system are listed in this section according to the year in which they are expected to be completed. The physical and electrical characteristics of future transmission plant or changes to the characteristics brought about by planned developments are listed in the tables. These characteristics are indicative at this stage and will be reviewed when the item of plant is commissioned.

### Table B-8: Expected Changes in Transmission Circuits

|        |         |      |     |     |        | Im     | pedance  | on     |        |        |      |
|--------|---------|------|-----|-----|--------|--------|----------|--------|--------|--------|------|
|        | Voltage |      |     |     | Length | 100    | MVA Base | (pu)   | Rating | (MVA)  |      |
| Action | (kV)    | From | То  | No. | (km)   | R      | X        | В      | Summer | Winter | Year |
| Add    | 110     | BGT  | ККҮ | 1   | 22     | 0.0139 | 0.0715   | 0.0078 | 178    | 210    | 2020 |
| Add    | 110     | CKG  | CBT | 1   | 1      | 0.0002 | 0.0009   | 0.0083 | 187    | 223    | 2020 |
| Add    | 110     | DMY  | CDN | 1   | 11     | 0.0155 | 0.0397   | 0.0036 | 211    | 217    | 2020 |
| Add    | 220     | INC  | CBT | 2   | 14     | 0.0020 | 0.0123   | 0.0195 | 761    | 794    | 2020 |
| Add    | 220     | CBT  | MAY | 1   | 12     | 0.0019 | 0.0115   | 0.0183 | 761    | 794    | 2020 |
| Add    | 220     | CBT  | MAY | 2   | 12     | 0.0016 | 0.0100   | 0.0159 | 761    | 794    | 2020 |
| Add    | 220     | CBT  | INC | 1   | 14     | 0.0015 | 0.0091   | 0.0144 | 761    | 794    | 2020 |
| Add    | 110     | DEY  | PLS | 1   | 48     | 0.0305 | 0.1574   | 0.0171 | 178    | 210    | 2020 |
| Add    | 110     | DEY  | DAL | 1   | 6      | 0.0040 | 0.0207   | 0.0023 | 178    | 210    | 2020 |
| Add    | 110     | CNN  | CLO | 1   | 18     | 0.0114 | 0.0585   | 0.0064 | 178    | 210    | 2020 |
| Add    | 110     | CNN  | CAG | 1   | 7      | 0.0017 | 0.0085   | 0.0772 | 140    | 140    | 2020 |
| Add    | 110     | CNN  | CDF | 1   | 6      | 0.0013 | 0.0067   | 0.0607 | 140    | 140    | 2020 |
| Add    | 110     | WHO  | КМА | 1   | 2      | 0.0011 | 0.0023   | 0.0151 | 124    | 124    | 2020 |
| Add    | 110     | BK   | CRN | 1   | 3      | 0.0021 | 0.0108   | 0.0012 | 178    | 210    | 2020 |
| Amend  | 110     | CDY  | SRA | 1   | 13     | 0.0198 | 0.0437   | 0.0041 | 178    | 210    | 2020 |
| Amend  | 110     | CLN  | LA  | 1   | 65     | 0.0951 | 0.2216   | 0.0210 | 99     | 121    | 2020 |
| Amend  | 110     | CDU  | RYB | 1   | 13     | 0.0135 | 0.0434   | 0.0045 | 178    | 219    | 2020 |
| Remove | 110     | ADM  | KUD | 1   |        |        |          |        |        |        | 2021 |
| Remove | 110     | AUG  | KPG | 1   |        |        |          |        |        |        | 2021 |
| Remove | 110     | BOG  | CRA | 1   |        |        |          |        |        |        | 2021 |
| Remove | 110     | CSH  | SOM | 1   |        |        |          |        |        |        | 2021 |
| Remove | 110     | CDU  | MUL | 1   |        |        |          |        |        |        | 2021 |
| Remove | 110     | CDU  | PLA | 1   |        |        |          |        |        |        | 2021 |
| Remove | 110     | CKG  | ВКҮ | 1   |        |        |          |        |        |        | 2021 |
| Remove | 110     | GI   | WEX | 1   |        |        |          |        |        |        | 2021 |
| Remove | 110     | GCA  | KUD | 2   |        |        |          |        |        |        | 2021 |
| Remove | 110     | INC  | ВКҮ | 1   |        |        |          |        |        |        | 2021 |
| Remove | 110     | KIN  | DFR | 1   |        |        |          |        |        |        | 2021 |
| Remove | 110     | KPG  | TRL | 2   |        |        |          |        |        |        | 2021 |
| Remove | 110     | BRO  | RSK | 1   |        |        |          |        |        |        | 2021 |
| Add    | 110     | ADM  | GCA | 1   | 3      | 0.0018 | 0.0038   | 0.0251 | 140    | 140    | 2021 |
| Add    | 110     | BLE  | AUG | 1   | 5      | 0.0029 | 0.0149   | 0.0017 | 178    | 210    | 2021 |
| Add    | 110     | BLE  | KPG | 1   | 28     | 0.0178 | 0.0917   | 0.0100 | 178    | 210    | 2021 |
| Add    | 110     | BLU  | CDU | 1   | 18     | 0.0168 | 0.0557   | 0.0308 | 130    | 130    | 2021 |
| Add    | 110     | BLU  | MUL | 1   | 56     | 0.0790 | 0.1906   | 0.0250 | 105    | 123    | 2021 |
| Add    | 110     | BLC  | DTN | 2   | 8      | 0.0041 | 0.0089   | 0.0486 | 140    | 143    | 2021 |
| Add    | 110     | BLC  | GRA | 1   | 4      | 0.0025 | 0.0053   | 0.0309 | 140    | 140    | 2021 |
| Add    | 110     | BLC  | KLM | 1   | 4      | 0.0023 | 0.0050   | 0.0291 | 140    | 140    | 2021 |
| Add    | 220     | CLE  | BRT | 1   | 3      | 0.0001 | 0.0004   | 0.0830 | 570    | 570    | 2021 |

#### Impedance on 100 MVA Base (pu) Rating (MVA) Voltage Length Action (kV) From То No. (km) R Х В Summer Winter Year Add CLE 220 BRT 2 0.0001 0.0004 0.0830 2021 3 570 570 Add BOG TTU 0.0070 0.0362 0.0045 110 1 11 178 210 2021 Add CSH SXH 0.0015 110 0.0073 0.0160 105 2021 1 5 123 Add CRA TTU 110 1 14 0.0110 0.0452 0.0054 178 210 2021 Add 110 CDU GLN 0.0070 0.0359 0.0039 178 210 2021 1 11 Add 0.0000 0.0415 CDU CRH 0.0002 220 1 0 570 570 2021 Add CDU CRH 570 220 2 0 0.0000 0.0002 0.0415 570 2021 Add KNY BUF 0.0056 110 1 1 0.0002 0.0007 140 140 2021 Add KPG DJG 110 1 0.0081 0.0452 0.0104 178 2021 14 210 Add DJG TRL 0.0203 0.0138 178 110 1 32 0.1047 210 2021 Add DER TEN 0.0817 0.0089 178 110 25 0.0158 210 2021 1 Add CKG CBT 110 2 1 0.0002 0.0009 0.0083 187 223 2021 Add 110 GI ROP 1 22 0.0141 0.0725 0.0079 178 210 2021 Add GLN MUC 178 110 0.0020 0.0102 0.0012 210 2021 1 3 Add GCA INC 8 110 3 0.0047 0.0044 0.0939 124 124 2021 Add MEN KRA 110 0.0017 0.0016 0.0341 124 124 2021 1 3 Add KUD CBT 0.0002 0.0009 0.0083 187 2021 110 1 1 223 Add 110 CBT BKY 0.0003 0.0011 0.0110 187 2021 1 1 223 Add 0.0011 CBT BKY 0.0110 187 110 2 1 0.0003 223 2021 Add MAY TEN 110 1 19 0.0118 0.0605 0.0093 112 112 2021 PLA Add MUC 0.0084 178 110 1 24 0.0149 0.0771 210 2021 Add SXH SOM 0.0146 110 1 0.0707 0.1563 105 2021 45 123 Add ROP WEX 110 1 13 0.0081 0.0416 0.0046 178 210 2021 Add BRO AGI 0.0047 0.0027 0.0164 2021 110 1 3 144 144 Add 0.0167 AGI RSK 187 110 1 20 0.0098 0.0590 200 2021 Amend 220 **BVK** BYH 15 0.0020 0.0126 0.0193 761 2021 1 794 Amend GI KKY 110 1 0.0309 0.1599 0.0174 178 210 2021 49 Amend BYH KNR 38 0.0326 0.0607 220 1 0.0045 740 792 2021 Remove 110 CLG FIN (I) 2022 1 FIN (I) Remove SHL 220 1 2022 LOU Remove WOO 220 1 2022 MCE SBH Remove 110 1 2022 MAY Remove W00 220 1 2022 Add BAG CLG 0.0002 0.0010 0.0094 110 1 1 192 192 2022 Add BAG SBH 0.0014 0.0133 2022 110 1 1 0.0003 192 192 Add BLC SHL 0.0010 220 1 23 0.0034 0.7769 570 570 2022 Add 110 FIN (I) MCE 8 0.0081 0.0262 0.0127 2022 1 124 124 Add HWN KIN 6 0.0060 110 1 0.0192 0.0034 136 140 2022

0.0064

0.0307

Add

HWN

110

DFR

1

9

#### Table B-8: Expected Changes in Transmission Circuits

0.0034

104

157

2022

### Table B-8: Expected Changes in Transmission Circuits

|        |         |         |     |     |        | Im     | pedance  | on     |        |        |      |
|--------|---------|---------|-----|-----|--------|--------|----------|--------|--------|--------|------|
|        | Voltage |         |     |     | Length |        | MVA Base |        | Rating | (MVA)  |      |
| Action | (kV)    | From    | То  | No. | (km)   | R      | X        | B      | Summer | Winter | Year |
| Add    | 220     | КҮТ     | MAY | 1   | 14     | 0.0030 | 0.0106   | 0.1120 | 761    | 746    | 2022 |
| Add    | 220     | КҮТ     | WOO | 1   | 14     | 0.0030 | 0.0109   | 0.1124 | 761    | 746    | 2022 |
| Add    | 400     | KPG     | MP  | 1   | 6      | 0.0008 | 0.0002   | 0.5489 | 1210   | 1210   | 2022 |
| Add    | 220     | LOU     | ORL | 1   | 15     | 0.0017 | 0.0126   | 0.0190 | 434    | 513    | 2022 |
| Add    | 220     | WOO     | ORL | 1   | 49     | 0.0058 | 0.0427   | 0.0644 | 434    | 513    | 2022 |
| Add    | 220     | ORL     | ORL | 1   | 20     | 0.0007 | 0.0079   | 0.5502 | 593    | 593    | 2022 |
| Add    | 220     | ORL     | ORL | 1   | 16     | 0.0007 | 0.0023   | 0.5279 | 570    | 570    | 2022 |
| Add    | 110     | AIR     | ROS | 1   | 5      | 0.0131 | 0.0341   | 0.0034 | 82     | 103    | 2022 |
| Add    | 110     | AIR     | ROS | 1   | 5      | 0.0131 | 0.0341   | 0.0034 | 82     | 103    | 2022 |
| Amend  | 400     | OST     | WOO | 1   | 125    | 0.0024 | 0.0080   | 0.6309 | 1577   | 1944   | 2022 |
| Amend  | 110     | BPS     | EDE | 1   | 15     | 0.0228 | 0.0536   | 0.0049 | 143    | 166    | 2022 |
| Amend  | 110     | BPS     | EDE | 2   | 15     | 0.0227 | 0.0529   | 0.0049 | 143    | 166    | 2022 |
| Amend  | 275     | CPS     | MAG | 1   | 56     | 0.0021 | 0.0236   | 0.1404 | 811    | 905    | 2022 |
| Amend  | 275     | CPS     | MAG | 2   | 56     | 0.0021 | 0.0236   | 0.1404 | 811    | 905    | 2022 |
| Amend  | 110     | DRO (N) | OMA | 1   | 9      | 0.0183 | 0.0471   | 0.0048 | 199    | 225    | 2022 |
| Amend  | 110     | DRO (N) | OMA | 2   | 9      | 0.0183 | 0.0471   | 0.0048 | 199    | 225    | 2022 |
| Remove | 110     | ATY     | PLS | 1   |        |        |          |        |        |        | 2023 |
| Remove | 110     | DRY     | PLA | 1   |        |        |          |        |        |        | 2023 |
| Remove | 400     | DSN     | MP  | 1   |        |        |          |        |        |        | 2023 |
| Remove | 110     | CKG     | KUD | 1   |        |        |          |        |        |        | 2023 |
| Remove | 275     | TAN     | TMN | 1   |        |        |          |        |        |        | 2023 |
| Remove | 275     | TAN     | TMN | 2   |        |        |          |        |        |        | 2023 |
| Add    | 110     | ATY     | CNB | 1   | 22     | 0.0138 | 0.0713   | 0.0078 | 178    | 210    | 2023 |
| Add    | 110     | BGT     | CNB | 1   | 28     | 0.0176 | 0.0910   | 0.0099 | 178    | 210    | 2023 |
| Add    | 110     | CLU     | KUD | 1   | 0      | 0.0001 | 0.0002   | 0.0012 | 187    | 223    | 2023 |
| Add    | 110     | CLU     | CBT | 1   | 1      | 0.0003 | 0.0014   | 0.0138 | 187    | 223    | 2023 |
| Add    | 110     | DRY     | RMN | 1   | 3      | 0.0042 | 0.0093   | 0.0038 | 105    | 123    | 2023 |
| Add    | 400     | DSN     | CNB | 1   | 45     | 0.0009 | 0.0030   | 0.2260 | 1577   | 1944   | 2023 |
| Add    | 220     | GI      | LWN | 1   | 1      | 0.0001 | 0.0002   | 0.0110 | 593    | 593    | 2023 |
| Add    | 110     | CNB     | PLS | 1   | 8      | 0.0051 | 0.0261   | 0.0083 | 178    | 210    | 2023 |
| Add    | 400     | CNB     | MP  | 1   | 170    | 0.0033 | 0.0113   | 0.8580 | 1577   | 1944   | 2023 |
| Add    | 110     | PLA     | RMN | 1   | 3      | 0.0043 | 0.0096   | 0.0038 | 105    | 123    | 2023 |
| Add    | 400     | WOO     | TUR | 1   | 135    | 0.0027 | 0.0311   | 0.7066 | 1424   | 1731   | 2023 |
| Add    | 110     | DRQ     | PT  | 1   | 2      | 0.0017 | 0.0036   | 0.0241 | 124    | 124    | 2023 |
| Add    | 275     | TAN     | TUR | 1   | 22     | 0.0009 | 0.0086   | 0.0514 | 710    | 881    | 2023 |
| Add    | 275     | TAN     | TUR | 2   | 22     | 0.0009 | 0.0086   | 0.0514 | 710    | 881    | 2023 |
| Add    | 275     | TMN     | TUR | 1   | 4      | 0.0002 | 0.0023   | 0.0135 | 710    | 881    | 2023 |
| Add    | 275     | TMN     | TUR | 2   | 4      | 0.0002 | 0.0023   | 0.0135 | 710    | 881    | 2023 |
| Amend  | 110     | CSH     | GAL | 1   | 14     | 0.0215 | 0.0475   | 0.0045 | 105    | 123    | 2023 |

|        |         |      |     |     |        | Impedance on<br>ength 100 MVA Base (pu) |          |        |        |        |       |
|--------|---------|------|-----|-----|--------|---|----------|--------|--------|--------|-------|
|        | Voltage |      |     |     | Length | 100 l                                   | MVA Base | (pu)   | Rating | (MVA)  |       |
| Action | (kV)    | From | То  | No. | (km)   | R                                       | X        | В      | Summer | Winter | Year  |
| Amend  | 110     | CSH  | GAL | 2   | 11     | 0.0176                                  | 0.0389   | 0.0037 | 105    | 123    | 2023  |
| Amend  | 110     | CSH  | GAL | 3   | 11     | 0.0176                                  | 0.0389   | 0.0037 | 105    | 123    | 2023  |
| Amend  | 110     | KNY  | GAL | 1   | 27     | 0.0051                                  | 0.0310   | 0.1376 | 228    | 228    | 2023  |
| Remove | 110     | ARK  | SHE | 2   |        |   |          |        |        |        | >2023 |
| Remove | 220     | DSN  | MAY | 2   |        |   |          |        |        |        | >2023 |
| Add    | 110     | ARK  | PHY | 1   | 2      | 0.0015                                  | 0.0074   | 0.0008 | 178    | 210    | >2023 |
| Add    | 110     | ARK  | PHY | 2   | 2      | 0.0015                                  | 0.0078   | 0.0009 | 178    | 210    | >2023 |
| Add    | 220     | DSN  | MAY | 2   | 31     | 0.0036                                  | 0.0265   | 0.0400 | 434    | 513    | >2023 |
| Add    | 110     | MOY  | TON | 1   | 58     | 0.0365                                  | 0.1884   | 0.0205 | 178    | 210    | >2023 |
| Add    | 110     | PHY  | SHE | 1   | 0      | 0.0003                                  | 0.0013   | 0.0002 | 178    | 210    | >2023 |
| Add    | 110     | KEL  | RSK | 2   |        | 0.0217                                  | 0.1344   | 0.0129 | 188    | 213    | >2023 |
| Amend  | 220     | DSN  | MAY | 1   | 31     | 0.0036                                  | 0.0265   | 0.0399 | 434    | 513    | >2023 |
| Amend  | 110     | FLA  | TON | 1   | 32     | 0.0203                                  | 0.1050   | 0.0114 | 178    | 210    | >2023 |
| Amend  | 110     | MR   | KBY | 1   | 4      | 0.0026                                  | 0.0130   | 0.0015 | 178    | 210    | >2023 |

Table B-8: Expected Changes in Transmission Circuits

Table B-9: Expected Changes in Transformers in Ireland

|        |         |             | Rating | HV/LV   | Impedance on<br>100 MVA Base (pu) |        |      | e Ratio<br>g Range |       |
|--------|---------|-------------|--------|---------|-----------------------------------|--------|------|--------------------|-------|
| Action | Station | Transformer | (MVA)  | (kV)    | R                                 | X      | +    | -                  | Year  |
| Add    | CBT     | T2101       | 250    | 220/110 | 0.001                             | 0.0646 | 0.1  | 0.18               | 2020  |
| Add    | CBT     | T2102       | 250    | 220/110 | 0.001                             | 0.0646 | 0.1  | 0.1                | 2020  |
| Add    | CBT     | T2103       | 250    | 220/110 | 0.001                             | 0.0646 | 0.1  | 0.1                | 2020  |
| Add    | CBT     | T2104       | 250    | 220/110 | 0.001                             | 0.0646 | 0.1  | 0.1                | 2020  |
| Remove | KRA     | T2103       | 250    | 220/110 | 0.0013                            | 0.0652 | 0.1  | 0.18               | 2020  |
| Add    | BLC     | T2102       | 250    | 220/110 | 0.001                             | 0.0646 | 0.1  | 0.1                | 2022  |
| Add    | KPG     | T4201       | 500    | 400/220 | 0.0003                            | 0.027  | 0.11 | 0.08               | 2022  |
| Add    | CNB     | T4102       | 500    | 400/110 | 0.00048                           | 0.072  | 0.16 | 0.16               | 2023  |
| Add    | CNB     | T4101       | 500    | 400/110 | 0.00048                           | 0.072  | 0.16 | 0.16               | 2023  |
| Remove | KLN     | T2101       | 63     | 220/110 | 0.0065                            | 0.2453 | 0.09 | 0.18               | >2023 |
| Remove | KLN     | T2102       | 63     | 220/110 | 0.0095                            | 0.2473 | 0.09 | 0.18               | >2023 |
| Amend  | KLN     | T2104       | 250    | 220/110 | 0.0004                            | 0.0631 | 0.1  | 0.18               | >2023 |

#### Table B-10: Expected Changes in 3 Winding Transformers in Northern Ireland

|        | Substa-    |         | h      | mpedanc | e on 100 l | MVA Ba | se (pu)      |     |      |       |     | 0   | ff   |      |      |
|--------|------------|---------|--------|---------|------------|--------|--------------|-----|------|-------|-----|-----|------|------|------|
|        | tion/      |         | W      | l-2     | W2-        | 3      | <b>W</b> 3-1 | L   | Rati | ng (M | VA) | Nom | inal | No.  |      |
|        | Trans-     | Voltage |        |         |            |        |              |     |      |       |     |     |      | of   |      |
| Action | former     | (kV)    | R      | Х       | R          | X      | R            | X   | W1   | W2    | W3  | Upr | Lwr  | Taps | Year |
| Add    | TUR IBTx 1 | 400/275 | 0.0003 | 0.026   | 0.0001     | 0.18   | 0.0001       | 0.2 | 500  | 500   | 60  | 1.1 | 0.9  | 15   | 2023 |
| Add    | TUR IBTx 2 | 400/275 | 0.0003 | 0.026   | 0.0001     | 0.18   | 0.0001       | 0.2 | 500  | 500   | 60  | 1.1 | 0.9  | 15   | 2023 |
| Add    | TUR IBTx 3 | 400/275 | 0.0003 | 0.026   | 0.0001     | 0.18   | 0.0001       | 0.2 | 500  | 500   | 60  | 1.1 | 0.9  | 15   | 2023 |

|        |         | HV/LV  | Rating | Impedance pu<br>on rating base |        | Off nomi | inal ratio | No. of |      |
|--------|---------|--------|--------|--------------------------------|--------|----------|------------|--------|------|
| Action | Station | (kV)   | (MVA)  | R                              | X      | Upper    | Lower      | taps   | Year |
| Add    | AGI     | 110/33 | 90     | 0.0035                         | 0.16   | 1.1      | 0.8        | 19     | 2021 |
| Add    | TAN     | 110/33 | 60     | 0                              | 0.0213 | 1.1      | 0.8        | 33     | 2021 |
| Add    | TMN     | 110/33 | 60     | 0.0039                         | 0.2461 | 1.1      | 0.8        | 19     | 2021 |
| Amend  | DON     | 110/33 | 90     | 0.0119                         | 0.3658 | 1.1      | 0.8        | 19     | 2021 |
| Add    | AIR     | 110/33 | 60     | 0.0039                         | 0.2464 | 1.1      | 0.8        | 19     | 2022 |
| Add    | AIR     | 110/33 | 60     | 0.0039                         | 0.2464 | 1.1      | 0.8        | 19     | 2022 |
| Add    | KEL     | 110/33 | 90     | 0.0039                         | 0.2461 | 1.1      | 0.8        | 19     | 2022 |
| Add    | CAS     | 110/33 | 60     | 0.0039                         | 0.248  | 1.1625   | 0.9125     | 21     | 2023 |
| Add    | KEL     | 110/33 | 60     | 0.0039                         | 0.2461 | 1.1      | 0.8        | 19     | 2023 |
| Add    | KPS     | 275/19 | 500    | 0.0007                         | 0.0488 | 1.1375   | 0.8625     | 23     | 2023 |
| Add    | KPS     | 275/19 | 500    | 0.0007                         | 0.0488 | 1.144    | 0.856      | 17     | 2023 |

#### Table B-11: Expected Changes in 2 Winding Transformers in Northern Ireland

Table B-12: Expected Changes in Reactive Compensation

|        |         |              |           | Mvar Ca  | pability |      |
|--------|---------|--------------|-----------|----------|----------|------|
| Action | Station | Voltage (kV) | Plant     | Generate | Absorb   | Year |
| Add    | KNR     | 220          | Reactor   |          | 50       | 2020 |
| Add    | BVK     | 110          | Reactor   |          | 50       | 2020 |
| Remove | THU     | 110          | Capacitor | 15       |          | 2021 |
| Add    | BVK     | 110          | STATCOM   | 100      | 100      | 2022 |
| Add    | BYH     | 110          | STATCOM   | 100      | 100      | 2022 |
| Add    | THU     | 110          | STATCOM   | 30       | 30       | 2022 |
| Add    | CAS     | 22           | Reactor   |          | 30       | 2022 |
| Add    | CAS     | 22           | Reactor   |          | 30       | 2022 |
| Add    | TAN     | 22           | Reactor   |          | 30       | 2022 |
| Add    | TMN     | 22           | Reactor   |          | 30       | 2022 |

# Appendix C Demand Forecasts at Individual Transmission Interface Stations

Transmission Interface Stations and Bulk Supply Points are connection points to the transmission system. These connection points include transmission system connections to the distribution system or directly-connected customers. Table C-1 to Table C-4 list the demand forecasts at each Transmission Interface Station and Bulk Supply Point. The forecasts are noted for each node between 2020 and 2029 at the winter peak, summer peak, and summer valley. The autumn peak forecasts are also given for Northern Ireland.

The station demand values do not include transmission losses. Demand values at stations that interface with the distribution system do include distribution losses.

Transmission Interface Stations are generally 110 kV stations. The exceptions to this are six 220/110 kV interface stations that supply the Dublin network. These interface stations are Belcamp, Carrickmines, Castlebagot, Finglas, Inchicore and Poolbeg.

Only stations feeding demand are included in the tables below, generation stations are not included.

| Bus        |                              | Power  | Demand Forecast (MW) |      |      |      |      |      |      |      |       |          |  |
|------------|------------------------------|--------|----------------------|------|------|------|------|------|------|------|-------|----------|--|
| Code       | Bus Name                     | Factor | 2020                 | 2021 | 2022 | 2023 | 2024 | 2025 | 2026 | 2027 | 2028  | 2029     |  |
| AA         | Ardnacrusha                  | 0.993  | 71.7                 | 72.7 | 72.2 | 73.0 | 73.8 | 74.4 | 74.6 | 75.0 | 75.6  | 76.0     |  |
| AGH        | Aghyoule                     | 0.998  | 13.9                 | 14.1 | 14.4 | 14.3 | 14.7 | 14.9 | 15.0 | 15.2 | 15.3  | 15.3     |  |
| AGY        | Ardnagappary                 | 0.985  | 16.2                 | 16.4 | 16.3 | 16.5 | 16.7 | 16.8 | 16.8 | 16.9 | 17.0  | 17.1     |  |
| AHA        | Ahane                        | 0.991  | 5.2                  | 5.2  | 5.2  | 5.2  | 5.3  | 5.3  | 5.4  | 5.4  | 0.0   | ,<br>5.5 |  |
| AIR        | Airport Road                 | 0.990  | -                    | -    | -    | 28.2 | 30.5 | 31.9 | 33.5 | 37.4 | 37.6  | 37.8     |  |
|            | (Belfast)                    |        |                      |      |      |      |      |      |      | 5, 1 | 5,    |          |  |
| ANR        | Anner                        | 0.897  | 14.0                 | 14.0 | 14.0 | 14.0 | 14.0 | 14.0 | 14.0 | 14.0 | 14.0  | 14.0     |  |
| ANT        | Antrim                       | 0.991  | 41.7                 | 41.8 | 42.6 | 42.2 | 43.1 | 43.4 | 43.7 | 43.9 | 44.1  | 44.4     |  |
| ARI        | Arigna                       | 0.965  | 2.5                  | 2.5  | 2.5  | 2.5  | 2.5  | 2.5  | 2.6  | 2.6  | 2.6   | 2.6      |  |
| ARK        | Arklow                       | 0.997  | 28.1                 | 28.5 | 28.3 | 28.6 | 28.9 | 29.1 | 29.2 | 29.4 | 29.6  | 29.7     |  |
| ATH        | Athlone                      | 0.976  | 69.4                 | 70.3 | 69.8 | 70.6 | 71.4 | 72.0 | 72.2 | 72.6 | 73.1  | 73.5     |  |
| ATY        | Athy                         | 0.989  | 22.1                 | 22.4 | 22.2 | 22.5 | 22.7 | 22.9 | 23.0 | 23.1 | 23.3  | 23.4     |  |
| BAL        | Baltrasna                    | 0.983  | 13.6                 | 13.8 | 13.7 | 13.8 | 14.0 | 14.1 | 14.1 | 14.2 | 14.3  | 14.4     |  |
| BAH        | Barnageeragh                 | 0.952  | -                    | -    | -    | 3.0  | 5.0  | 8.0  | 10.0 | 13.0 | 15.0  | 18.0     |  |
| BAN (I)    | Bandon                       | 0.977  | 55.0                 | 55.8 | 55.4 | 56.0 | 56.6 | 57.0 | 57.2 | 57.5 | 57.9  | 58.2     |  |
| BAN (N)    | Banbridge                    | 0.979  | 39.1                 | 39.2 | 40.0 | 39.6 | 40.4 | 40.7 | 40.9 | 41.1 | 46.7  | 41.6     |  |
| BAR        | Barrymore                    | 0.994  | 33.6                 | 34.1 | 33.9 | 34.2 | 34.6 | 34.9 | 35.0 | 35.2 | 35.4  | 35.6     |  |
| BDA        | Baroda                       | 0.988  | 5.3                  | 5.3  | 5.3  | 5.3  | 5.3  | 5.3  | 5.3  | 5.3  | 5.3   | 5.3      |  |
| BDN        | Ballydine                    | 0.971  | 17.8                 | 18.0 | 17.9 | 18.0 | 18.2 | 18.3 | 18.3 | 18.4 | 18.5  | 18.5     |  |
| BEG        | Ballybeg                     | 0.997  | 14.7                 | 14.9 | 14.8 | 14.9 | 15.1 | 15.2 | 15.3 | 15.4 | 15.5  | 15.6     |  |
| BLC        | Belcamp                      | 0.951  | 43.0                 | 51.0 | 59.0 | 67.0 | 75.0 | 83.0 | 91.0 | 99.0 | 107.0 | 115.0    |  |
| BGD        | Belgard Road                 | 0.950  | 29.5                 | 37.0 | 44.7 | 53.2 | 53.2 | 53.2 | 53.2 | 53.2 | 53.2  | 53.2     |  |
| BGT        | Ballyragget                  | 0.977  | 26.5                 | 26.9 | 26.7 | 27.0 | 27.3 | 27.5 | 27.6 | 27.8 | 28.0  | 28.1     |  |
| BIN        | Binbane                      | 0.974  | 14.2                 | 14.4 | 14.3 | 14.4 | 14.6 | 14.7 | 14.7 | 14.8 | 14.9  | 15.0     |  |
| BK         | Bellacorick                  | 0.979  | 6.0                  | 6.1  | 6.0  | 6.1  | 6.2  | 6.2  | 6.2  | 6.3  | 6.3   | 6.4      |  |
| ВКҮ        | Barnakyle                    | 0.951  | 10.3                 | 34.5 | 38.4 | 42.5 | 46.6 | 50.7 | 54.8 | 58.8 | 61.9  | 67.0     |  |
| BLI        | Ballylickey                  | 0.977  | 15.0                 | 15.2 | 15.1 | 15.3 | 15.5 | 15.6 | 15.6 | 15.7 | 15.8  | 15.9     |  |
| BLK        | Blake                        | 0.993  | 12.6                 | 12.8 | 12.7 | 12.9 | 13.0 | 13.1 | 13.2 | 13.2 | 13.3  | 13.4     |  |
| BMA        | Ballymena                    | 0.979  | 83.3                 | 83.6 | 85.2 | 84.4 | 86.2 | 86.8 | 87.3 | 87.6 | 88.1  | 88.6     |  |
| BNH        | Ballynahinch                 | 0.991  | 56.7                 | 57.0 | 58.0 | 57.4 | 58.7 | 59.0 | 59.3 | 59.6 | 59.9  | 60.3     |  |
| BNM        | Belfast North                | 0.990  | 49.9                 | 50.1 | 51.0 | 50.6 | 51.7 | 52.0 | 52.3 | 52.5 | 52.8  | 53.1     |  |
| BOG        | Banoge                       | 0.983  | 22.7                 | 23.1 | 22.9 | 23.1 | 23.4 | 23.6 | 23.7 | 23.8 | 24.0  | 24.1     |  |
| BRA        | Bracklone                    | 0.978  | 14.1                 | 14.3 | 14.2 | 14.4 | 14.6 | 14.7 | 14.7 | 14.8 | 14.9  | 15.0     |  |
| BRI        | Brinny                       | 0.971  | 4.0                  | 4.0  | 4.0  | 4.0  | 4.0  | 4.0  | 4.0  | 4.0  | 4.0   | 4.0      |  |
| BRY        | Barnahely                    | 0.988  | 30.6                 | 31.1 | 30.8 | 31.2 | 31.5 | 31.8 | 31.9 | 32.1 | 32.3  | 32.5     |  |
| BUT        | Butlerstown                  | 0.995  | 41.1                 | 41.7 | 41.4 | 41.8 | 42.3 | 42.7 | 42.8 | 43.0 | 43.3  | 43.6     |  |
| BVG        | Ballyvallagh                 | 0.972  | 15.1                 | 15.1 | 15.4 | 15.3 | 15.6 | 15.7 | 15.8 | 15.8 | 15.9  | 16.0     |  |
| CAH        | Cahir                        | 0.982  | 27.7                 | 28.1 | 27.9 | 28.2 | 28.5 | 28.7 | 28.8 | 29.0 | 29.2  | 29.4     |  |
| CAR        | Carnmoney                    | 0.996  | 25.4                 | 25.1 | 25.2 | 24.6 | 24.7 | 24.5 | 24.3 | 24.0 | 24.2  | 24.3     |  |
| CBG        | Carrowbeg                    | 0.985  | 19.2                 | 19.4 | 19.3 | 19.5 | 19.7 | 19.9 | 20.0 | 20.1 | 20.2  | 20.3     |  |
| CBR<br>CEN | Castlebar<br>Bolfast Control | 0.992  | 35.7                 | 36.2 | 35.9 | 36.3 | 36.7 | 37.0 | 37.1 | 37.3 | 37.6  | 37.8     |  |
| CEN        | Belfast Central              | 0.999  | 52.8                 | 53.2 | 54.2 | 53.8 | 55.1 | 55.5 | 55.9 | 56.3 | 56.6  | 56.9     |  |
|            | Cathaleen's<br>Fall          | 0.995  | 19.2                 | 19.4 | 19.3 | 19.5 | 19.7 | 19.9 | 19.9 | 20.0 | 20.2  | 20.3     |  |
| CFM        | Castlefarm                   | 0.901  | 50.8                 | 50.8 | 50.8 | 50.8 | 50.8 | 50.8 | 50.8 | 50.8 | 50.8  | 50.8     |  |

| Bus                |                        | Power          |              |       |              | De           | mand Fo      | recast (N    | W)           |              |              |              |
|--------------------|------------------------|----------------|--------------|-------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| Code               | Bus Name               | Factor         | 2020         | 2021  | 2022         | 2023         | 2024         | 2025         | 2026         | 2027         | 2028         | 2029         |
| СНА                | Charleville            | 0.980          | 16.7         | 16.9  | 16.8         | 17.0         | 17.2         | 17.3         | 17.4         | 17.5         | 17.6         | 17.7         |
| CKG                | Corkagh                | 0.950          | 46.6         | 54.2  | 64.1         | 74.1         | 84.1         | 94.1         | 104.5        | 114.0        | 124.5        | 134.0        |
| СКМ                | Carrickmines           | 0.987          | 379.0        | 387.6 | 385.4        | 388.8        | 392.6        | 395.0        | 396.0        | 397.7        | 400.2        | 401.9        |
| CLE                | Clonee                 | 0.950          | 67.5         | 86.5  | 105.5        | 124.5        | 142.5        | 142.5        | 142.5        | 142.5        | 142.5        | 142.5        |
| CLG                | Cloghran               | 0.952          | 67.5         | 75.0  | 79.8         | 79.8         | 79.8         | 79.8         | 79.8         | 79.8         | 79.8         | 79.8         |
| CLN                | Cloon                  | 0.977          | 32.7         | 33.2  | 32.9         | 33.3         | 33.7         | 33.9         | 34.0         | 34.2         | 34.5         | 34.7         |
| CLU                | Clutterland            | 0.952          | -            | -     | -            | 3.8          | 9.5          | 14.3         | 20.0         | 24.7         | 30.4         | 35.2         |
| CLW                | Carlow                 | 0.989          | 65.3         | 66.2  | 65.7         | 66.4         | 67.2         | 67.7         | 67.9         | 68.3         | 68.8         | 69.2         |
| COL (I)            | College Park           | 0.988          | 27.1         | 27.5  | 27.3         | 27.6         | 27.9         | 28.1         | 28.2         | 28.3         | 28.6         | 28.7         |
| COL (N)            | Coleraine              | 0.991          | 42.6         | 42.7  | 43.5         | 43.1         | 44.0         | 44.3         | 44.5         | 44.7         | 45.0         | 45.2         |
| COS                | Carrick-on-            | 0.993          | 29.6         | 30.0  | 29.8         | 30.1         | 30.4         | 30.7         | 30.8         | 30.9         | 31.2         | 31.3         |
|                    | Shannon                |                |              |       |              |              |              |              |              |              |              |              |
| COW                | Cow Cross              | 0.997          | 13.4         | 13.6  | 13.5         | 13.7         | 13.9         | 14.0         | 14.0         | 14.1         | 14.2         | 14.3         |
| CPS                | Cool                   | 0.989          | 25.3         | 25.4  | 25.8         | 25.6         | 26.1         | 26.3         | 26.4         | 26.6         | 26.7         | 26.9         |
| CRA                | Crane                  | 0.988          | 35.7         | 36.2  | 36.0         | 36.4         | 36.8         | 37.1         | 37.2         | 37.4         | 37.7         | 37.9         |
| CRE                | Cregagh                | 0.986          | 85.8         | 86.2  | 72.5         | 71.9         | 73.6         | 74.2         | 74.7         | 75.2         | 75.6         | 76.0         |
| CRG                | Creagh                 | 0.991          | 24.8         | 24.9  | 25.3         | 25.1         | 25.6         | 25.8         | 25.9         | 26.1         | 26.2         | 26.3         |
| CRH                | Cruiserath             | 0.953          | -            | 3.8   | 9.0          | 14.3         | 19.5         | 24.7         | 29.9         | 35.2         | 40.4         | 45.6         |
| CRO                | Coolroe                | 0.986          | 12.6         | 12.8  | 12.7         | 12.8         | 13.0         | 13.1         | 13.1         | 13.2         | 13.3         | 13.4         |
| CVW                | Castleview             | 0.986          | 26.6         | 26.9  | 26.7         | 27.0         | 27.4         | 27.6         | 27.6         | 27.8         | 28.0         | 28.2         |
| DAL                | Dallow                 | 0.996          | 18.3         | 18.6  | 18.5         | 18.7         | 18.9         | 19.0         | 19.1         | 19.2         | 19.3         | 19.4         |
| DDK                | Dundalk                | 0.980          | 75.5         | 76.6  | 76.1         | 76.9         | 77.8         | 78.4         | 78.6         | 79.0         | 79.6         | 80.1         |
| DFR                | Dunfirth               | 0.996          | 10.4         | 10.5  | 10.4         | 10.6         | 10.7         | 10.8         | 10.8         | 10.9         | 10.9         | 11.0         |
| DGN                | Dungarvan              | 0.987          | 47.1         | 47.8  | 47.5         | 48.0         | 48.5         | 48.9         | 49.1         | 49.3         | 49.7         | 49.9         |
| DLT                | Dalton                 | 0.986          | 26.8         | 27.2  | 27.0         | 27.3         | 27.6         | 27.8         | 27.9         | 28.0         | 28.3         | 28.4         |
| DMY                | Dunmanway              | 0.978          | 26.1         | 26.5  | 26.3         | 26.6         | 26.9         | 27.1         | 27.2         | 27.3         | 27.5         | 27.7         |
| DON                | Donegall               | 1.000          | 92.6         | 91.4  | 91.5         | 89.1         | 89.5         | 88.6         | 87.7         | 86.7         | 87.1         | 87.6         |
| D00                | Doon                   | 0.979          | 32.1         | 32.5  | 32.3         | 32.6         | 33.0         | 33.3         | 33.4         | 33.6         | 33.8         | 34.0         |
| DRU (I)            | Drumline               | 0.979          | 31.3         | 31.8  | 31.5         | 31.9         | 32.3         | 32.5         | 32.6         | 32.8         | 33.0         | 33.2         |
| DRU (N)            | Drumnakelly            | 0.988          | 91.3         | 91.6  | 93.4         | 92.5         | 94.5         | 95.2         | 95.9         | 96.4         | 97.0         | 97.5         |
| DRY                | Drybridge              | 0.989          | 91.3         | 92.5  | 91.9         | 92.9         | 94.0         | 94.7         | 95.0         | 95.5         | 96.2         | 96.7         |
| DUN                | Dungannon              | 0.970          | 96.6         | 97.0  | 98.8         | 97.9         | 100.0        | 100.6        | 101.2        | 101.7        | 102.2        | 102.8        |
| EDE                | Eden                   | 0.984          | 34.5         | 34.6  | 35.2         | 34.9         | 35.7         | 35.9         | 36.1         | 36.2         | 36.4         | 36.6         |
| ENN (I)            | Ennis                  | 0.981          | 61.3         | 62.1  | 61.7         | 62.4         | 63.1         | 63.6         | 63.8         | 64.1         | 64.6         | 64.9         |
| ENN (N)            | Enniskillen            | 0.984          | 58.3         | 58.6  | 59.7         | 59.2         | 60.4         | 60.8         | 61.2         | 61.5         | 61.8         | 62.2         |
| FIN (I)            | Finglas                | 0.986          | 478.6        | 484.6 | 481.6        | 486.4        | 491.5        | 494.9        | 496.3        | 498.7        | 502.1        | 504.5        |
| FIN (N)            | Finaghy                | 0.994          | 30.8         | 31.0  | 31.5         | 31.2         | 31.9         | 32.1         | 32.3         | 32.4         | 32.6         | 32.8         |
| FTT<br>GAL         | Fortunestown<br>Galway | 0.970          | 10.9         | 11.0  | 11.0         | 11.1         | 11.2         | 11.3         | 11.3         | 11.4         | 11.5         | 11.5         |
| GAL                | Great Island           | 0.991          | 71.9         | 47.6  | 72.4         | 47.8         | 54.2         | 54.6         | 74.8         | 75.2         | 75.8         | 76.1         |
| GIL                | Gilra                  | 0.950          | 14.2         | 14.4  | 14.3         | 14.5         | 14.6         | 14.7         | 14.8         | 14.9         | 15.0         | 15.0         |
| GLE (I)            | Glenlara               | 0.971<br>0.989 | 11.4         | 11.4  | 11.4<br>17.8 | 11.4<br>18.0 | 11.4<br>18.2 | 11.4<br>18.3 | 11.4<br>18.4 | 11.4<br>18.5 | 11.4<br>18.6 | 11.4<br>18.7 |
| GLE (I)<br>GLE (N) | Glengormley            | 0.989          | 17.7         | 17.9  | 31.8         |              |              |              |              |              |              |              |
| GRI                | Griffinrath            |                | 31.4         | 31.4  |              | 31.4         | 32.0<br>60.0 | 32.1         | 32.1         | 32.2         | 32.3         | 32.5<br>61.8 |
| GWE                | Gortawee               | 0.994          | 58.3<br>21.1 | 59.1  | 58.7         | 59.3         | 32.6         | 60.5         | 60.7         | 61.0         | 61.5         |              |
| GWE                | JUILAWEE               | 0.953          | 21.1         | 32.4  | 32.4         | 32.5         | 2.0          | 32.7         | 32.7         | 32.8         | 32.9         | 33.0         |

| Bus     |              | Power  | wer Demand Forecast (MW) |              |       |              |       |              |              |              |       |       |  |
|---------|--------------|--------|--------------------------|--------------|-------|--------------|-------|--------------|--------------|--------------|-------|-------|--|
| Code    | Bus Name     | Factor | 2020                     | 2021         | 2022  | 2023         | 2024  | 2025         | 2026         | 2027         | 2028  | 2029  |  |
| IKE     | Ikerrin      | 0.966  |                          |              |       | _            | -     |              |              |              |       |       |  |
| INC     | Inchicore    | -      | 31.5                     | 32.0         | 31.7  | 32.1         | 32.5  | 32.7         | 32.8         | 33.0         | 33.2  | 33.4  |  |
| KBY     |              | 0.990  | 271.2                    | 290.1        | 269.5 | 305.5        | 306.4 | 312.1        | 296.1        | 301.1        | 305.5 | 310.3 |  |
|         | Kilbarry     | 0.992  | 96.0                     | 97.4         | 96.7  | 97.8         | 98.9  | 99.6         | 99.9         | 100.5        | 101.2 | 101.8 |  |
| KER     | Knockearagh  | 0.990  | 42.0                     | 42.6         | 42.3  | 42.8         | 43.3  | 43.6         | 43.7         | 43.9         | 44.3  | 44.5  |  |
| KIL     | Kildare      | 0.951  | -                        | -            | -     | -            | 7.6   | 15.2         | 22.8         | 30.4         | 38.0  | 45.6  |  |
| KIN     | Kinnegad     | 0.973  | 10.2                     | 10.2         | 10.2  | 10.2         | 10.2  | 10.2         | 10.2         | 10.2         | 10.2  | 10.2  |  |
| ККҮ     | Kilkenny     | 0.966  | 55.8                     | 56.6         | 56.2  | 56.8         | 57.5  | 57.9         | 58.1         | 58.4         | 58.8  | 59.1  |  |
| KNO     | Knock        | 0.981  | 51.0                     | 51.3         | 45.6  | 45.2         | 46.2  | 46.6         | 46.9         | 47.1         | 47.4  | 47.6  |  |
| KTL     | Kilteel      | 0.972  | 51.4                     | 52.1         | 51.7  | 52.3         | 52.9  | 53.3         | 53.5         | 53.7         | 54.2  | 54.4  |  |
| KTN     | Killoteran   | 0.973  | 11.4                     | 11.6         | 11.5  | 11.6         | 11.8  | 11.9         | 11.9         | 12.0         | 12.0  | 12.1  |  |
| KUD     | Kilmahud     | 0.951  | 17.1                     | 17.1         | 20.9  | 24.7         | 28.5  | 32.3         | 36.1         | 39.9         | 43.7  | 47.5  |  |
| KUR     | Knockumber   | 0.907  | 23.7                     | 23.7         | 23.7  | 23.7         | 23.7  | 23.7         | 23.7         | 23.7         | 23.7  | 23.7  |  |
| KYN     | Kellystown   | 0.950  | -                        | -            | 125.0 | 125.0        | 125.0 | 125.0        | 125.0        | 125.0        | 125.0 | 125.0 |  |
| LA      | Lanesboro    | 0.986  | 16.9                     | 17.1         | 17.0  | 17.2         | 17.4  | 17.5         | 17.6         | 17.7         | 17.8  | 17.9  |  |
| LAR     | Larne        | 0.972  | 28.5                     | 28.7         | 29.2  | 28.9         | 29.5  | 29.7         | 29.9         | 30.0         | 30.1  | 30.3  |  |
| LET     | Letterkenny  | 0.984  | 78.0                     | 79.1         | 78.5  | 79.4         | 80.3  | 80.9         | 81.2         | 81.6         | 82.2  | 82.6  |  |
| LIB     | Liberty      | 0.989  | 21.6                     | 21.9         | 21.7  | 21.9         | 22.2  | 22.4         | 22.4         | 22.6         | 22.7  | 22.8  |  |
| LIM (I) | Limerick     | 0.987  | 80.8                     | 81.9         | 81.4  | 82.3         | 83.2  | 83.8         | 84.1         | 84.6         | 85.2  | 85.6  |  |
| LIM (N) | Limavady     | 0.977  | 24.7                     | 24.8         | 25.2  | 25.0         | 25.5  | 25.6         | 25.8         | 25.9         | 26.0  | 26.2  |  |
| LIS (I) | Lisdrum      | 0.969  | 26.4                     | 26.8         | 26.6  | 26.9         | 27.2  | 27.4         | 27.5         | 27.7         | 27.9  | 28.0  |  |
| LIS (N) | Lisburn      | 0.992  | 73.7                     | 74.0         | 75.4  | 74.7         | 76.3  | 76.8         | 77.2         | 77.6         | 78.0  | 78.5  |  |
| LMR     | Lisaghmore   | 0.980  | 32.7                     | 32.9         | 33.5  | 33.2         | 33.9  | 34.1         | 34.3         | 34.4         | 34.6  | 34.8  |  |
| LOG     | Loguestown   | 0.977  | 38.9                     | 39.0         | 39.7  | 39.4         | 40.2  | 40.4         | 40.7         | 40.8         | 41.1  | 41.3  |  |
| MAC     | Macroom      | 0.949  | 12.5                     | 12.7         | 12.6  | 12.7         | 12.9  | 13.0         | 13.0         | 13.1         | 13.2  | 13.2  |  |
| MAL     | Mallow       | 0.980  | 23.1                     | 23.4         | 23.3  | 23.5         | 23.8  | 24.0         | 24.1         | 24.2         | 24.4  | 24.5  |  |
| MCE     | Macetown     | 0.978  | 34.0                     | 34.4         | 34.2  | 34.5         | 34.9  | 35.1         | 35.2         | 35.4         | 35.6  | 35.8  |  |
| MID     | Midleton     | 0.985  | 42.8                     | 43.4         | 43.1  | 43.6         | 44.1  | 44.4         | 44.6         | 44.8         | 45.1  | 45.4  |  |
| MLN     | Mullagharlin | 0.958  | 4.5                      | 4.5          | 4.5   | 4.5          | 4.5   | 4.5          | 4.5          | 4.5          | 4.5   | 4.5   |  |
| MON     | Monread      | 0.989  | 13.8                     | 14.0         | 13.9  | 14.0         | 14.2  | 14.3         | 14.3         | 14.4         | 14.5  | 14.6  |  |
| MOY     | Моу          | 0.990  | 28.6                     | 29.0         | 28.8  | 29.1         | 29.5  | 29.7         | 29.8         | 29.9         | 30.2  | 30.3  |  |
| MR      | Marina       | 0.997  | 15.8                     | 16.0         | 15.9  | 16.1         | 16.3  | 16.4         | 16.5         | 16.6         | 16.7  | 16.8  |  |
| МТН     | Meathhill    | 0.965  | 56.4                     | 57.2         | 56.8  | 57.4         | 58.1  | 58.5         | 58.7         | 59.0         | 59.4  | 59.8  |  |
| MUL     | Mullingar    | 0.983  | 47.7                     | 48.4         | 48.0  | 48.5         | 49.1  | 49.5         | 49.6         | 49.9         | 50.3  | 50.5  |  |
| MUN     | Mungret      | 0.871  | 21.5                     | 21.5         | 21.5  | 21.5         | 21.5  | 21.5         | 21.5         | 21.5         | 21.5  | 21.5  |  |
| NAR     | Newtownards  | 1.000  | 45.2                     | 45.4         | 46.2  | 45.8         | 46.7  | 47.0         | 47.3         | 47.5         | 47.7  | 48.0  |  |
| NAV     | Navan        | 0.980  | 64.4                     | 65.3         | 64.8  | 65.5         | 66.3  | 66.8         | 67.0         | 67.3         | 67.9  | 68.2  |  |
| NEN     | Nenagh       | 0.967  | 22.5                     | 22.8         | 22.7  | 22.9         | 23.2  | 23.4         | 23.4         | 23.6         | 23.7  | 23.9  |  |
| NEW (I) | Newbridge    | 0.992  | 28.9                     |              | 29.1  |              | 29.8  |              | 1            |              |       | 30.6  |  |
| NEW (N) | Newry        | 0.992  |                          | 29.3<br>80.0 | 81.5  | 29.4<br>80.7 | 82.5  | 30.0<br>82.0 | 30.1<br>82.5 | 30.2<br>82.0 | 30.5  | 84.8  |  |
| OLD     | Oldcourt     |        | 79.7                     |              |       |              |       | 83.0         | 83.5         | 83.9         | 84.3  |       |  |
|         |              | 0.949  | 0.3                      | 0.3          | 0.3   | 0.3          | 0.3   | 0.3          | 0.3          | 0.3          | 0.3   | 0.3   |  |
| OMA     | Omagh        | 0.993  | 60.4                     | 60.7         | 61.8  | 61.2         | 62.5  | 62.8         | 63.2         | 63.5         | 63.8  | 64.2  |  |
| OUG     | Oughtragh    | 0.994  | 26.9                     | 27.3         | 27.1  | 27.4         | 27.8  | 28.0         | 28.0         | 28.2         | 28.4  | 28.6  |  |
| PB      | Poolbeg      | 0.989  | 210.0                    | 213.0        | 211.5 | 213.8        | 216.3 | 217.9        | 218.6        | 219.8        | 221.4 | 222.6 |  |
| PLA     | Platin       | 0.950  | 18.0                     | 18.0         | 18.0  | 18.0         | 18.0  | 18.0         | 18.0         | 18.0         | 18.0  | 18.0  |  |

| Bus     |              | Power  |       |       |       | De    | mand Fo | recast (N | IW)   |       |       |       |
|---------|--------------|--------|-------|-------|-------|-------|---------|-----------|-------|-------|-------|-------|
| Code    | Bus Name     | Factor | 2020  | 2021  | 2022  | 2023  | 2024    | 2025      | 2026  | 2027  | 2028  | 2029  |
| PLS     | Portlaoise   | 0.990  | 41.8  | 42.4  | 42.1  | 42.5  | 43.0    | 43.4      | 43.5  | 43.7  | 44.1  | 44.3  |
| RAT (I) | Rathkeale    | 0.989  | 29.2  | 29.6  | 29.4  | 29.7  | 30.0    | 30.3      | 30.4  | 30.5  | 30.7  | 30.9  |
| RAT (N) | Rathgael     | 0.997  | 57.6  | 57.9  | 58.9  | 58.4  | 59.6    | 60.0      | 60.3  | 60.6  | 60.9  | 61.2  |
| RIC     | Richmond     | 0.977  | 37.0  | 37.5  | 37.3  | 37.7  | 38.1    | 38.4      | 38.5  | 38.7  | 39.0  | 39.2  |
| RMN     | Rathmullan   | 0.950  | -     | -     | -     | 3.8   | 9.5     | 14.3      | 20.0  | 24.7  | 30.4  | 35.2  |
| RNW     | Rinawade     | 0.988  | 9.1   | 9.1   | 9.1   | 9.1   | 9.1     | 9.1       | 9.1   | 9.1   | 9.1   | 9.1   |
| ROS     | Rosebank     | 0.979  | 30.3  | 30.4  | 27.8  | 27.6  | 28.2    | 28.4      | 28.5  | 28.7  | 28.8  | 29.0  |
| RSY     | Ringaskiddy  | 0.996  | 4.1   | 4.2   | 4.2   | 4.2   | 4.3     | 4.3       | 4.3   | 4.3   | 4.4   | 4.4   |
| RYB     | Ryebrook     | 0.928  | 104.5 | 104.5 | 104.5 | 104.5 | 104.5   | 104.5     | 104.5 | 104.5 | 104.5 | 104.5 |
| SAL     | Salthill     | 0.995  | 55.5  | 56.2  | 55.8  | 56.5  | 57.1    | 57.5      | 57.7  | 58.0  | 58.5  | 58.8  |
| SBH     | Snughborough | 0.951  | 7.6   | 11.4  | 14.3  | 17.1  | 19.0    | 21.9      | 23.8  | 26.6  | 28.5  | 31.4  |
| SCR     | Screeb       | 0.972  | 29.2  | 29.6  | 29.4  | 29.7  | 30.1    | 30.3      | 30.4  | 30.6  | 30.8  | 31.0  |
| SHE     | Shelton      | 0.956  | 2.3   | 2.3   | 2.3   | 2.3   | 2.3     | 2.3       | 2.3   | 2.3   | 2.3   | 2.3   |
| SKL     | Shankill     | 0.966  | 60.0  | 60.8  | 60.4  | 61.1  | 61.8    | 62.3      | 62.4  | 62.8  | 63.3  | 63.6  |
| SLI     | Sligo        | 0.987  | 57.5  | 58.3  | 57.9  | 58.6  | 59.2    | 59.7      | 59.9  | 60.2  | 60.6  | 61.0  |
| SNG     | Singland     | 0.976  | 11.6  | 11.8  | 11.7  | 11.8  | 12.0    | 12.1      | 12.1  | 12.2  | 12.3  | 12.3  |
| SOM     | Somerset     | 0.990  | 22.4  | 22.7  | 22.6  | 22.8  | 23.1    | 23.2      | 23.3  | 23.4  | 23.6  | 23.7  |
| SPR     | Springtown   | 0.994  | 47.4  | 47.6  | 48.4  | 48.0  | 49.0    | 49.3      | 49.5  | 49.7  | 50.0  | 50.3  |
| STR     | Stratford    | 0.990  | 22.0  | 22.3  | 22.2  | 22.4  | 22.7    | 22.9      | 22.9  | 23.1  | 23.2  | 23.3  |
| STR (N) | Strabane     | 0.968  | 42.2  | 42.3  | 43.1  | 42.7  | 43.6    | 43.8      | 44.1  | 44.3  | 44.5  | 44.8  |
| TBG     | Trabeg       | 0.993  | 76.1  | 77.1  | 76.6  | 77.4  | 78.3    | 78.9      | 79.2  | 79.6  | 80.2  | 80.6  |
| ТВК     | Tullabrack   | 0.980  | 11.6  | 11.8  | 11.7  | 11.9  | 12.0    | 12.1      | 12.1  | 12.2  | 12.3  | 12.3  |
| THU     | Thurles      | 0.976  | 29.7  | 30.1  | 29.9  | 30.2  | 30.6    | 30.8      | 30.9  | 31.1  | 31.3  | 31.5  |
| TIP     | Tipperary    | 0.979  | 21.9  | 22.2  | 22.1  | 22.3  | 22.6    | 22.7      | 22.8  | 22.9  | 23.1  | 23.2  |
| TLK     | Trillick     | 0.989  | 21.4  | 21.7  | 21.6  | 21.8  | 22.0    | 22.2      | 22.3  | 22.4  | 22.6  | 22.7  |
| TON     | Tonroe       | 0.993  | 16.3  | 16.5  | 16.4  | 16.6  | 16.8    | 16.9      | 16.9  | 17.0  | 17.1  | 17.2  |
| TRI     | Trien        | 0.957  | 25.5  | 25.9  | 25.7  | 26.0  | 26.3    | 26.5      | 26.6  | 26.7  | 26.9  | 27.1  |
| TRL     | Tralee       | 0.995  | 58.7  | 59.6  | 59.1  | 59.8  | 60.5    | 60.9      | 61.1  | 61.5  | 61.9  | 62.2  |
| TSB     | Thornsberry  | 0.982  | 33.9  | 34.3  | 34.1  | 34.5  | 34.9    | 35.1      | 35.2  | 35.4  | 35.7  | 35.9  |
| WAR     | Waringstown  | 0.986  | 66.0  | 66.2  | 67.4  | 66.8  | 68.2    | 68.6      | 69.0  | 69.2  | 69.6  | 70.0  |
| WAT     | Waterford    | 0.978  | 57.9  | 58.7  | 58.3  | 58.9  | 59.6    | 60.1      | 60.3  | 60.6  | 61.0  | 61.4  |
| WEX     | Wexford      | 0.968  | 60.2  | 61.0  | 60.6  | 61.3  | 62.0    | 62.5      | 62.6  | 63.0  | 63.5  | 63.8  |
| WHI     | Whitegate    | 0.870  | 9.0   | 9.0   | 9.0   | 9.0   | 9.0     | 9.0       | 9.0   | 9.0   | 9.0   | 9.0   |

| _          |                           | _      | Demand Forecast (MW) |      |      |      |      |      |      |      |       |           |  |  |
|------------|---------------------------|--------|----------------------|------|------|------|------|------|------|------|-------|-----------|--|--|
| Bus        | DecoNorma                 | Power  | 2020                 | 2024 | 2022 | 1    | I    |      |      | 2027 | 2020  | 2020      |  |  |
| Code       | Bus Name                  | Factor | 2020                 | 2021 | 2022 | 2023 | 2024 | 2025 | 2026 | 2027 | 2028  | 2029      |  |  |
| AA         | Ardnacrusha               | 0.993  | 55.1                 | 55.6 | 54.5 | 54.9 | 55.3 | 55.6 | 55.6 | 55.7 | 55.9  | 56.1      |  |  |
| AGH        | Aghyoule                  | 1.000  | 11.0                 | 11.1 | 11.3 | 11.3 | 11.6 | 11.7 | 11.8 | 11.9 | 12.0  | 12.1      |  |  |
| AGY        | Ardnagappary              | 0.985  | 12.4                 | 12.5 | 12.3 | 12.4 | 12.5 | 12.5 | 12.5 | 12.6 | 12.6  | 12.6      |  |  |
| AHA        | Ahane                     | 0.991  | 4.0                  | 4.0  | 3.9  | 3.9  | 4.0  | 4.0  | 4.0  | 4.0  | 4.0   | 4.0       |  |  |
| AIR        | Airport Road<br>(Belfast) | 0.990  | -                    | -    | -    | 22.2 | 24.0 | 25.1 | 26.3 | 29.4 | 29.6  | 29.7      |  |  |
| ANR        | Anner                     | 0.897  | 14.0                 | 14.0 | 14.0 | 14.0 | 14.0 | 14.0 | 14.0 | 14.0 | 14.0  | 14.0      |  |  |
| ANT        | Antrim                    | 0.990  | 32.7                 | 32.9 | 33.5 | 33.2 | 33.9 | 34.1 | 34.3 | 34.5 | 34.7  | 34.9      |  |  |
| ARI        | Arigna                    | 0.967  | 1.9                  | 1.9  | 1.9  | 1.9  | 1.9  | 1.9  | 1.9  | 1.9  | 1.9   | 1.9       |  |  |
| ARK        | Arklow                    | 0.997  | 21.6                 | 21.8 | 21.3 | 21.5 | 21.7 | 21.8 | 21.8 | 21.8 | 21.9  | 21.9      |  |  |
| ATH        | Athlone                   | 0.976  | 53.3                 | 53.8 | 52.7 | 53.1 | 53.5 | 53.8 | 53.7 | 53.9 | 54.1  | 54.2      |  |  |
| ATY        | Athy                      | 0.989  | 16.9                 | 17.1 | 16.8 | 16.9 | 17.0 | 17.1 | 17.1 | 17.1 | 17.2  | 17.2      |  |  |
| BAL        | Baltrasna                 | 0.983  | 10.4                 | 10.5 | 10.3 | 10.4 | 10.5 | 10.5 | 10.5 | 10.5 | 10.6  | 10.6      |  |  |
| BAH        | Barnageeragh              | 0.952  | -                    | -    | -    | 3.0  | 5.0  | 8.0  | 10.0 | 13.0 | 15.0  | 18.0      |  |  |
| BAN (I)    | Bandon                    | 0.977  | 42.7                 | 43.1 | 42.3 | 42.6 | 42.9 | 43.1 | 43.1 | 43.2 | 43.4  | 43.4      |  |  |
| BAN<br>(N) | Banbridge                 | 0.969  | 30.7                 | 30.8 | 31.4 | 31.1 | 31.8 | 32.0 | 32.2 | 32.3 | 32.5  | 32.7      |  |  |
| BAR        | Barrymore                 | 0.994  | 25.8                 | 26.1 | 25.6 | 25.7 | 25.9 | 26.1 | 26.0 | 26.1 | 26.2  | 26.3      |  |  |
| BDA        | Baroda                    | 0.988  | 5.3                  | 5.3  | 5.3  | 5.3  | 5.3  | 5.3  | 5.3  | 5.3  | 5.3   | 5.3       |  |  |
| BDN        | Ballydine                 | 0.970  | 15.1                 | 15.2 | 15.0 | 15.0 | 15.1 | 15.2 | 15.2 | 15.2 | 15.2  | 15.2      |  |  |
| BEG        | Ballybeg                  | 0.997  | 11.3                 | 11.4 | 11.2 | 11.2 | 11.3 | 11.4 | 11.4 | 11.4 | 11.5  | 11.5      |  |  |
| BGD        | Belgard Road              | 0.950  | 29.5                 | 37.0 | 44.7 | 53.2 | 53.2 | 53.2 | 53.2 | 53.2 | 53.2  | 53.2      |  |  |
| BGT        | Ballyragget               | 0.977  | -                    | 20.6 | 20.2 | 20.3 | 20.5 | 20.6 | 20.6 | 20.6 | 20.7  | 20.8      |  |  |
| BIN        | Binbane                   | 0.974  | 10.9                 | 11.0 | 10.8 | 10.8 | 10.9 | 11.0 | 11.0 | 11.0 | 11.0  | 11.1      |  |  |
| ВК         | Bellacorick               | 0.979  | 4.6                  | 4.6  | 4.6  | 4.6  | 4.6  | 4.6  | 4.6  | 4.7  | 4.7   | 4.7       |  |  |
| BKY        | Barnakyle                 | 0.951  | 7.9                  | 32.0 | 35.9 | 39.9 | 44.0 | 48.0 | 52.0 | 56.0 | 59.1  | 64.1      |  |  |
| BLI        | Ballylickey               | 0.977  | 11.5                 | 11.7 | 11.4 | 11.5 | 11.6 | 11.6 | 11.6 | 11.7 | 11.7  | 11.7      |  |  |
| BLC        | Belcamp                   | 0.951  | 43.0                 | 51.0 | 59.0 | 67.0 | 75.0 | 83.0 | 91.0 | 99.0 | 107.0 | 115.0     |  |  |
| BLK        | Blake                     | 0.993  | 9.7                  | 9.8  | 9.6  | 9.7  | 9.8  | 9.8  | 9.8  | 9.8  | 9.9   | 9.9       |  |  |
| BMA        | Ballymena                 | 0.969  | 65.5                 | 65.7 | 67.0 | 66.3 | 67.8 | 68.2 | 68.6 | 68.9 | 69.3  | 69.7      |  |  |
| BNH        | Ballynahinch              | 0.985  | 44.6                 | 44.8 | 45.6 | 45.2 | 46.1 | 46.4 | 46.6 | 46.8 | 47.1  | 47.4      |  |  |
| BNM        | Belfast North             | 0.990  | 39.2                 | 39.4 | 40.1 | 39.7 | 40.6 | 40.8 | 41.1 | 41.3 | 41.5  | 41.7      |  |  |
| BOG        | Banoge                    | 0.983  | 17.5                 | 17.6 | 17.3 | 17.4 | 17.5 | 17.6 | 17.6 | 17.7 | 17.7  | 17.8      |  |  |
| BRA        | Bracklone                 | 0.978  | 10.9                 | 11.0 | 10.8 | 10.8 | 10.9 | 11.0 | 11.0 | 11.0 | 11.0  | 11.1      |  |  |
| BRI        | Brinny                    | 0.971  | 4.0                  | 4.0  | 4.0  | 4.0  | 4.0  | 4.0  | 4.0  | 4.0  | 4.0   | 4.0       |  |  |
| BRY        | Barnahely                 | 0.988  | 23.5                 | 23.8 | 23.3 | 23.5 | 23.6 | 23.7 | 23.7 | 23.8 | 23.9  | 23.9      |  |  |
| BUT        | Butlerstown               | 0.995  | 31.6                 | 31.9 | 31.3 | 31.5 | 31.7 | 31.9 | 31.9 | 31.9 | 32.1  | 32.2      |  |  |
| BVG        | Ballyvallagh              | 0.934  | 11.9                 | 11.9 | 12.1 | 12.0 | 12.3 | 12.3 | 12.4 | 12.4 | 12.5  | 12.6      |  |  |
| CAH        | Cahir                     | 0.982  | 21.3                 | 21.5 | 21.1 | 21.2 | 21.4 | 21.5 | 21.5 | 21.5 | 21.6  | 21.7      |  |  |
| CAR        | Carnmoney                 | 1.000  | 20.0                 | 19.8 | 19.8 | 19.3 | 19.5 | 19.3 | 19.1 | 18.9 | 19.0  | ,<br>19.1 |  |  |
| CBG        | Carrowbeg                 | 0.985  | 14.7                 | 14.9 | 14.6 | 14.7 | 14.8 | 14.9 | 14.8 | 14.9 | 15.0  | 15.0      |  |  |
| CBR        | Castlebar                 | 0.992  | 27.4                 | 27.7 | 27.1 | 27.3 | 27.5 | 27.6 | 27.6 | 27.7 | 27.8  | 27.9      |  |  |
| CEN        | Belfast Central           |        |                      | 41.8 |      |      |      |      |      |      |       |           |  |  |
| CEN        | Belfast Central           | 0.994  | 41.5                 | 41.8 | 42.6 | 42.3 | 43.3 | 43.6 | 44.0 | 44.2 | 44.5  | 44.7      |  |  |

| Bus     |                        | Douror | Power Demand Forecast (MW) |       |       |       |       |       |       |       |       |       |  |  |
|---------|------------------------|--------|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--|--|
| Code    | Bus Name               |        | 2020                       | 2021  | 2022  | 2023  | 2024  | 2025  | 2026  | 2027  | 2028  | 2029  |  |  |
| CF      | Cathaleen's            | Factor |                            |       |       |       |       |       |       |       |       |       |  |  |
| CF      | Fall                   | 0.995  | 14.7                       | 14.9  | 14.6  | 14.7  | 14.8  | 14.8  | 14.8  | 14.9  | 14.9  | 15.0  |  |  |
| CFM     | Castlefarm             | 0.901  | 50.8                       | 50.8  | 50.8  | 50.8  | 50.8  | 50.8  | 50.8  | 50.8  | 50.8  | 50.8  |  |  |
| CHA     | Charleville            | 0.980  | 12.8                       | 12.9  | 12.7  | 12.8  | 12.9  | 12.9  | 12.9  | 13.0  | 13.0  | 13.0  |  |  |
| CKG     | Corkagh                | 0.950  | 46.6                       | 54.2  | 64.1  | 74.1  | 84.1  | 94.1  | 104.5 | 114.0 | 124.5 | 134.0 |  |  |
| СКМ     | Carrickmines           | 0.986  | 306.4                      | 313.1 | 308.3 | 309.9 | 311.7 | 312.8 | 312.8 | 313.3 | 314.5 | 315.0 |  |  |
| CLE     | Clonee                 | 0.950  | 67.5                       | 86.5  | 105.5 | 124.5 | 142.5 | 142.5 | 142.5 | 142.5 | 142.5 | 142.5 |  |  |
| CLG     | Cloghran               | 0.952  | 67.5                       | 75.0  | 79.8  | 79.8  | 79.8  | 79.8  | 79.8  | 79.8  | 79.8  | 79.8  |  |  |
| CLN     | Cloon                  | 0.977  | 25.1                       | 25.4  | 24.9  | 25.0  | 25.2  | 25.4  | 25.3  | 25.4  | 25.5  | 25.6  |  |  |
| CLU     | Clutterland            | 0.952  | -                          | -     | -     | 3.8   | 9.5   | 14.3  | 20.0  | 24.7  | 30.4  | 35.2  |  |  |
| CLW     | Carlow                 | 0.989  | 50.1                       | 50.6  | 49.6  | 50.0  | 50.4  | 50.6  | 50.6  | 50.7  | 50.9  | 51.0  |  |  |
| COL (I) | College Park           | 0.988  | 20.8                       | 21.0  | 20.6  | 20.7  | 20.9  | 21.0  | 21.0  | 21.0  | 21.1  | 21.2  |  |  |
| COL (N) | Coleraine              | 0.969  | 33.5                       | 33.6  | 34.2  | 33.9  | 34.6  | 34.8  | 35.0  | 35.1  | 35.3  | 35.5  |  |  |
| COS     | Carrick-on-<br>Shannon | 0.993  | 22.7                       | 22.9  | 22.5  | 22.6  | 22.8  | 22.9  | 22.9  | 23.0  | 23.1  | 23.1  |  |  |
| COW     | Cow Cross              | 0.997  | 10.3                       | 10.4  | 10.2  | 10.3  | 10.4  | 10.4  | 10.4  | 10.4  | 10.5  | 10.5  |  |  |
| CPS     | Cool                   | 0.997  | 19.8                       | 19.9  | 20.3  | 20.1  | 20.5  | 20.7  | 20.8  | 20.9  | 21.0  | 21.1  |  |  |
| CRA     | Crane                  | 0.988  | 27.4                       | 27.7  | 27.2  | 27.4  | 27.6  | 27.7  | 27.7  | 27.8  | 27.9  | 27.9  |  |  |
| CRE     | Cregagh                | 0.986  | 67.4                       | 67.7  | 57.0  | 56.5  | 57.8  | 58.3  | 58.7  | 59.1  | 59.4  | 59.8  |  |  |
| CRG     | Creagh                 | 0.984  | 19.5                       | 19.6  | 19.9  | 19.7  | 20.2  | 20.3  | 20.4  | 20.5  | 20.6  | 20.7  |  |  |
| CRH     | Cruiserath             | 0.953  |                            |       | 9.0   | 14.3  | 19.5  | 24.7  | 29.9  | 35.2  | 40.4  | 45.6  |  |  |
| CRO     | Coolroe                | 0.986  | 9.7                        | 9.8   | 9.6   | 9.7   | 9.7   | 9.8   | 9.8   | 9.8   | 9.8   | 9.9   |  |  |
| CVW     | Castleview             | 0.986  | 20.4                       | 20.6  | 20.2  | 20.3  | 20.5  | 20.6  | 20.6  | 20.6  | 20.7  | 20.8  |  |  |
| DAL     | Dallow                 | 0.996  | 14.1                       | 14.2  | 13.9  | 14.0  | 14.1  | 14.2  | 14.2  | 14.2  | 14.3  | 14.3  |  |  |
| DDK     | Dundalk                | 0.980  | 58.0                       | 58.6  | 57.5  | 57.8  | 58.3  | 58.6  | 58.5  | 58.7  | 58.9  | 59.1  |  |  |
| DFR     | Dunfirth               | 0.996  | 8.0                        | 8.1   | 7.9   | 7.9   | 8.0   | 8.0   | 8.0   | 8.1   | 8.1   | 8.1   |  |  |
| DGN     | Dungarvan              | 0.987  | 36.2                       | 36.6  | 35.8  | 36.1  | 36.4  | 36.5  | 36.5  | 36.6  | 36.8  | 36.9  |  |  |
| DLT     | Dalton                 | 0.986  | 20.6                       | 20.8  | 20.4  | 20.5  | 20.7  | 20.8  | 20.8  | 20.8  | 20.9  | 21.0  |  |  |
| DMY     | Dunmanway              | 0.978  | 20.1                       | 20.3  | 19.9  | 20.0  | 20.2  | 20.2  | 20.2  | 20.3  | 20.4  | 20.4  |  |  |
| DON     | Donegall               | 1.000  | 72.8                       | 71.8  | 71.9  | 70.0  | 70.4  | 69.6  | 68.9  | 68.1  | 68.5  | 68.9  |  |  |
| D00     | Doon                   | 0.979  | 24.6                       | 24.9  | 24.4  | 24.6  | 24.7  | 24.9  | 24.8  | 24.9  | 25.0  | 25.1  |  |  |
| DRU (I) | Drumline               | 0.979  | 24.0                       | 24.3  | 23.8  | 24.0  | 24.2  | 24.3  | 24.3  | 24.3  | 24.4  | 24.5  |  |  |
| DRU (N) | Drumnakelly            | 0.988  | 71.7                       | 72.0  | 73.4  | 72.7  | 74.3  | 74.8  | 75.3  | 75.8  | 76.2  | 76.7  |  |  |
| DRY     | Drybridge              | 0.989  | 70.1                       | 70.8  | 69.4  | 69.9  | 70.4  | 70.7  | 70.7  | 70.9  | 71.2  | 71.4  |  |  |
| DUN     | Dungannon              | 0.970  | 75.9                       | 76.2  | 77.7  | 76.9  | 78.6  | 79.1  | 79.5  | 79.9  | 80.4  | 80.8  |  |  |
| EDE     | Eden                   | 0.969  | 27.1                       | 27.2  | 27.7  | 27.4  | 28.0  | 28.2  | 28.4  | 28.5  | 28.6  | 28.8  |  |  |
| ENN (I) | Ennis                  | 0.981  | 47.1                       | 47.5  | 46.6  | 46.9  | 47.3  | 47.5  | 47.5  | 47.6  | 47.8  | 47.9  |  |  |
| ENN (N) | Enniskillen            | 0.939  | 45.9                       | 46.1  | 46.9  | 46.5  | 47.5  | 47.8  | 48.1  | 48.3  | 48.6  | 48.9  |  |  |
| FIN (I) | Finglas                | 0.985  | 377.7                      | 381.2 | 374.6 | 376.8 | 379.4 | 380.9 | 380.7 | 381.5 | 383.1 | 383.8 |  |  |
| FIN (N) | Finaghy                | 0.984  | 24.2                       | 24.3  | 24.8  | 24.6  | 25.1  | 25.2  | 25.4  | 25.5  | 25.6  | 25.8  |  |  |
| FTT     | Fortunestown           | 0.970  | 8.4                        | 8.4   | 8.3   | 8.3   | 8.4   | 8.4   | 8.4   | 8.5   | 8.5   | 8.5   |  |  |
| GAL     | Galway                 | 0.990  | 55.2                       | 55.7  | 54.7  | 55.0  | 55.4  | 55.7  | 55.7  | 55.8  | 56.1  | 56.2  |  |  |
| GI      | Great Island           | 0.950  | 10.1                       | 11.0  | 10.8  | 10.9  | 11.0  | 11.0  | 11.0  | 11.0  | 11.1  | 11.1  |  |  |
| GIL     | Gilra                  | 0.971  | 11.4                       | 11.4  | 11.4  | 11.4  | 11.4  | 11.4  | 11.4  | 11.4  | 11.4  | 11.4  |  |  |

| Bus     |              | Power  |       |       |       | De    | mand Fo | recast (M | W)    |       |       |       |
|---------|--------------|--------|-------|-------|-------|-------|---------|-----------|-------|-------|-------|-------|
| Code    | Bus Name     | Factor | 2020  | 2021  | 2022  | 2023  | 2024    | 2025      | 2026  | 2027  | 2028  | 2029  |
| GLE (I) | Glenlara     | 0.989  | 13.6  | 13.7  | 13.4  | 13.5  | 13.6    | 13.7      | 13.7  | 13.7  | 13.8  | 13.8  |
| GLE (N) | Glengormley  | 0.976  | 24.6  | 24.7  | 25.0  | 24.7  | 25.1    | 25.2      | 25.2  | 25.3  | 25.4  | 25.6  |
| GRI     | Griffinrath  | 0.994  | 44.8  | 45.2  | 44.3  | 44.6  | 45.0    | 45.2      | 45.2  | 45.3  | 45.5  | 45.6  |
| GWE     | Gortawee     | 0.950  | 29.7  | 29.8  | 29.6  | 29.7  | 29.7    | 29.8      | 29.8  | 29.8  | 29.8  | 29.8  |
| IKE     | Ikerrin      | 0.966  | 24.2  | 24.5  | 24.0  | 24.1  | 24.3    | 24.4      | 24.4  | 24.5  | 24.6  | 24.6  |
| INC     | Inchicore    | 0.989  | 208.1 | 211.7 | 214.5 | 223.8 | 229.0   | 233.5     | 236.7 | 240.9 | 244.3 | 248.3 |
| КВҮ     | Kilbarry     | 0.992  | 73.7  | 74.5  | 73.0  | 73.5  | 74.1    | 74.4      | 74.4  | 74.6  | 74.9  | 75.1  |
| KER     | Knockearagh  | 0.990  | 32.3  | 32.6  | 32.0  | 32.2  | 32.4    | 32.6      | 32.5  | 32.6  | 32.8  | 32.8  |
| KIL     | Kildare      | 0.951  | -     | -     | -     | -     | 7.6     | 15.2      | 22.8  | 30.4  | 38.0  | 45.6  |
| KIN     | Kinnegad     | 0.973  | 10.2  | 10.2  | 10.2  | 10.2  | 10.2    | 10.2      | 10.2  | 10.2  | 10.2  | 10.2  |
| ККҮ     | Kilkenny     | 0.966  | 51.8  | 43.3  | 42.4  | 42.7  | 43.1    | 43.3      | 43.2  | 43.3  | 43.5  | 43.6  |
| КNО     | Knock        | 0.978  | 40.1  | 40.3  | 35.9  | 35.6  | 36.3    | 36.6      | 36.8  | 37.0  | 37.2  | 37.4  |
| KTL     | Kilteel      | 0.972  | 39.4  | 39.8  | 39.1  | 39.3  | 39.6    | 39.8      | 39.8  | 39.9  | 40.1  | 40.2  |
| KTN     | Killoteran   | 0.973  | 8.8   | 8.9   | 8.7   | 8.7   | 8.8     | 8.9       | 8.9   | 8.9   | 8.9   | 8.9   |
| KUD     | Kilmahud     | 0.951  | 17.1  | 17.1  | 20.9  | 24.7  | 28.5    | 32.3      | 36.1  | 39.9  | 43.7  | 47.5  |
| KUR     | Knockumber   | 0.907  | 23.7  | 23.7  | 23.7  | 23.7  | 23.7    | 23.7      | 23.7  | 23.7  | 23.7  | 23.7  |
| KYN     | Kellystown   | 0.950  | -     | -     | 125.0 | 125.0 | 125.0   | 125.0     | 125.0 | 125.0 | 125.0 | 125.0 |
| LA      | Lanesboro    | 0.986  | 13.0  | 13.1  | 12.8  | 12.9  | 13.0    | 13.1      | 13.1  | 13.1  | 13.2  | 13.2  |
| LAR     | Larne        | 0.934  | 22.4  | 22.5  | 22.9  | 22.7  | 23.2    | 23.3      | 23.5  | 23.6  | 23.7  | 23.8  |
| LET     | Letterkenny  | 0.984  | 59.9  | 60.5  | 59.3  | 59.7  | 60.2    | 60.4      | 60.4  | 60.6  | 60.9  | 61.0  |
| LIB     | Liberty      | 0.990  | 16.6  | 16.7  | 16.4  | 16.5  | 16.6    | 16.7      | 16.7  | 16.8  | 16.8  | 16.9  |
| LIM (I) | Limerick     | 0.987  | 62.1  | 62.7  | 61.5  | 61.9  | 62.4    | 62.6      | 62.6  | 62.8  | 63.1  | 63.2  |
| LIM (N) | Limavady     | 0.980  | 19.4  | 19.5  | 19.8  | 19.6  | 20.0    | 20.2      | 20.3  | 20.3  | 20.5  | 20.6  |
| LIS (I) | Lisdrum      | 0.969  | 20.3  | 20.5  | 20.1  | 20.2  | 20.4    | 20.5      | 20.5  | 20.5  | 20.6  | 20.7  |
| LIS (N) | Lisburn      | 0.985  | 57.9  | 58.2  | 59.3  | 58.7  | 60.0    | 60.4      | 60.7  | 61.0  | 61.3  | 61.7  |
| LMR     | Lisaghmore   | 0.980  | 25.7  | 25.8  | 26.3  | 26.1  | 26.6    | 26.8      | 26.9  | 27.1  | 27.2  | 27.4  |
| LOG     | Loguestown   | 0.973  | 30.5  | 30.7  | 31.2  | 30.9  | 31.6    | 31.8      | 32.0  | 32.1  | 32.3  | 32.5  |
| MAC     | Macroom      | 0.949  | 9.6   | 9.7   | 9.5   | 9.6   | 9.6     | 9.7       | 9.7   | 9.7   | 9.7   | 9.8   |
| MAL     | Mallow       | 0.980  | 17.8  | 17.9  | 17.6  | 17.7  | 17.8    | 17.9      | 17.9  | 18.0  | 18.0  | 18.1  |
| MCE     | Macetown     | 0.979  | 27.2  | 27.4  | 27.0  | 27.1  | 27.3    | 27.4      | 27.4  | 27.4  | 27.5  | 27.6  |
| MID     | Midleton     | 0.985  | 32.9  | 33.2  | 32.6  | 32.8  | 33.0    | 33.2      | 33.2  | 33.3  | 33.4  | 33.5  |
| MLN     | Mullagharlin | 0.958  | 4.5   | 4.5   | 4.5   | 4.5   | 4.5     | 4.5       | 4.5   | 4.5   | 4.5   | 4.5   |
| MON     | Monread      | 0.989  | 10.6  | 10.7  | 10.5  | 10.6  | 10.6    | 10.7      | 10.7  | 10.7  | 10.8  | 10.8  |
| MOY     | Моу          | 0.990  | 22.0  | 22.2  | 21.8  | 21.9  | 22.1    | 22.2      | 22.2  | 22.2  | 22.3  | 22.4  |
| MR      | Marina       | 0.997  | 12.1  | 12.3  | 12.0  | 12.1  | 12.2    | 12.3      | 12.3  | 12.3  | 12.3  | 12.4  |
| MTH     | Meathhill    | 0.965  | 43.3  | 43.8  | 42.9  | 43.2  | 43.5    | 43.7      | 43.7  | 43.8  | 44.0  | 44.1  |
| MUL     | Mullingar    | 0.983  | 36.6  | 37.0  | 36.3  | 36.5  | 36.8    | 37.0      | 37.0  | 37.0  | 37.2  | 37.3  |
| MUN     | Mungret      | 0.871  | 21.5  | 21.5  | 21.5  | 21.5  | 21.5    | 21.5      | 21.5  | 21.5  | 21.5  | 21.5  |
| NAR     | Newtownards  | 1.000  | 35.5  | 35.7  | 36.3  | 36.0  | 36.7    | 37.0      | 37.2  | 37.3  | 37.5  | 37.7  |
| NAV     | Navan        | 0.980  | 49.4  | 49.9  | 49.0  | 49.3  | 49.7    | 49.9      | 49.9  | 50.0  | 50.2  | 50.3  |
| NEN     | Nenagh       | 0.967  | 17.3  | 17.5  | 17.1  | 17.2  | 17.4    | 17.4      | 17.4  | 17.5  | 17.6  | 17.6  |
| NEW (I) | Newbridge    | 0.992  | 22.2  | 22.4  | 22.0  | 22.1  | 22.3    | 22.4      | 22.4  | 22.4  | 22.5  | 22.6  |
| NEW (N) | Newry        | 0.992  | 62.6  | 62.9  | 64.1  | 63.5  | 64.8    | 65.2      | 65.6  | 65.9  | 66.3  | 66.7  |
| OLD     | Oldcourt     | 0.949  | 0.3   | 0.3   | 0.3   | 0.3   | 0.3     | 0.3       | 0.3   | 0.3   | 0.3   | 0.3   |

| Bus     |              | Power  |       |       |       | De    | mand Fo | recast (M | W)    |       |       |       |
|---------|--------------|--------|-------|-------|-------|-------|---------|-----------|-------|-------|-------|-------|
| Code    | Bus Name     | Factor | 2020  | 2021  | 2022  | 2023  | 2024    | 2025      | 2026  | 2027  | 2028  | 2029  |
| OMA     | Omagh        | 0.961  | 47.5  | 47.7  | 48.6  | 48.1  | 49.1    | 49.4      | 49.7  | 49.9  | 50.2  | 50.4  |
| OUG     | Oughtragh    | 0.994  | 20.7  | 20.9  | 20.5  | 20.6  | 20.8    | 20.9      | 20.9  | 20.9  | 21.0  | 21.1  |
| PB      | Poolbeg      | 0.989  | 161.3 | 163.0 | 159.8 | 160.8 | 162.1   | 162.8     | 162.7 | 163.1 | 163.9 | 164.2 |
| PLA     | Platin       | 0.950  | 18.0  | 18.0  | 18.0  | 18.0  | 18.0    | 18.0      | 18.0  | 18.0  | 18.0  | 18.0  |
| PLS     | Portlaoise   | 0.990  | 43.5  | 32.4  | 31.8  | 32.0  | 32.2    | 32.4      | 32.4  | 32.5  | 32.6  | 32.7  |
| RAT (I) | Rathkeale    | 0.989  | 22.4  | 22.6  | 22.2  | 22.3  | 22.5    | 22.6      | 22.6  | 22.6  | 22.8  | 22.8  |
| RAT (N) | Rathgael     | 1.000  | 45.3  | 45.5  | 46.3  | 45.9  | 46.9    | 47.1      | 47.4  | 47.6  | 47.9  | 48.1  |
| RIC     | Richmond     | 0.977  | 28.4  | 28.7  | 28.1  | 28.3  | 28.5    | 28.7      | 28.7  | 28.7  | 28.9  | 28.9  |
| RMN     | Rathmullan   | 0.950  | -     | -     | -     | 3.8   | 9.5     | 14.3      | 20.0  | 24.7  | 30.4  | 35.2  |
| RNW     | Rinawade     | 0.988  | 9.1   | 9.1   | 9.1   | 9.1   | 9.1     | 9.1       | 9.1   | 9.1   | 9.1   | 9.1   |
| ROS     | Rosebank     | 0.975  | 23.8  | 23.9  | 21.9  | 21.7  | 22.2    | 22.3      | 22.4  | 22.5  | 22.7  | 22.8  |
| RSY     | Ringaskiddy  | 0.996  | 3.2   | 3.2   | 3.1   | 3.2   | 3.2     | 3.2       | 3.2   | 3.2   | 3.2   | 3.2   |
| RYB     | Ryebrook     | 0.928  | 104.5 | 104.5 | 104.5 | 104.5 | 104.5   | 104.5     | 104.5 | 104.5 | 104.5 | 104.5 |
| SAL     | Salthill     | 0.995  | 42.6  | 43.0  | 42.2  | 42.5  | 42.8    | 43.0      | 43.0  | 43.1  | 43.3  | 43.4  |
| SBH     | Snughborough | 0.951  | 7.6   | 11.4  | 14.3  | 17.1  | 19.0    | 21.9      | 23.8  | 26.6  | 28.5  | 31.4  |
| SCR     | Screeb       | 0.972  | 22.4  | 22.7  | 22.2  | 22.4  | 22.5    | 22.6      | 22.6  | 22.7  | 22.8  | 22.8  |
| SHE     | Shelton      | 0.956  | 2.3   | 2.3   | 2.3   | 2.3   | 2.3     | 2.3       | 2.3   | 2.3   | 2.3   | 2.3   |
| SKL     | Shankill     | 0.966  | 46.1  | 46.5  | 45.6  | 45.9  | 46.3    | 46.5      | 46.5  | 46.6  | 46.8  | 46.9  |
| SLI     | Sligo        | 0.987  | 44.2  | 44.6  | 43.7  | 44.0  | 44.4    | 44.6      | 44.6  | 44.7  | 44.9  | 45.0  |
| SNG     | Singland     | 0.976  | 8.9   | 9.0   | 8.8   | 8.9   | 9.0     | 9.0       | 9.0   | 9.0   | 9.1   | 9.1   |
| SOM     | Somerset     | 0.990  | 17.2  | 17.4  | 17.0  | 17.2  | 17.3    | 17.4      | 17.4  | 17.4  | 17.5  | 17.5  |
| SPR     | Springtown   | 0.995  | 37.2  | 37.4  | 38.1  | 37.7  | 38.5    | 38.7      | 38.9  | 39.1  | 39.3  | 39.5  |
| STR     | Stratford    | 0.991  | 16.9  | 17.1  | 16.8  | 16.9  | 17.0    | 17.1      | 17.1  | 17.1  | 17.2  | 17.2  |
| STR (N) | Strabane     | 0.965  | 33.1  | 33.3  | 33.9  | 33.5  | 34.3    | 34.5      | 34.6  | 34.8  | 35.0  | 35.2  |
| WAR     | Waringstown  | 0.972  | 51.8  | 52.0  | 53.0  | 52.5  | 53.6    | 53.9      | 54.2  | 54.4  | 54.7  | 55.0  |
| TBG     | Trabeg       | 0.993  | 58.4  | 59.0  | 57.8  | 58.2  | 58.7    | 58.9      | 58.9  | 59.1  | 59.3  | 59.5  |
| TBK     | Tullabrack   | 0.980  | 8.9   | 9.0   | 8.9   | 8.9   | 9.0     | 9.0       | 9.0   | 9.0   | 9.1   | 9.1   |
| THU     | Thurles      | 0.976  | 22.8  | 23.0  | 22.6  | 22.7  | 22.9    | 23.0      | 23.0  | 23.1  | 23.2  | 23.2  |
| TIP     | Tipperary    | 0.979  | 16.8  | 17.0  | 16.7  | 16.8  | 16.9    | 17.0      | 17.0  | 17.0  | 17.1  | 17.1  |
| TLK     | Trillick     | 0.989  | 16.4  | 16.6  | 16.3  | 16.4  | 16.5    | 16.6      | 16.6  | 16.6  | 16.7  | 16.7  |
| TON     | Tonroe       | 0.993  | 12.5  | 12.6  | 12.4  | 12.5  | 12.6    | 12.6      | 12.6  | 12.6  | 12.7  | 12.7  |
| TRI     | Trien        | 0.957  | 19.6  | 19.8  | 19.4  | 19.5  | 19.7    | 19.8      | 19.8  | 19.8  | 19.9  | 20.0  |
| TRL     | Tralee       | 0.995  | 45.1  | 45.6  | 44.7  | 45.0  | 45.3    | 45.5      | 45.5  | 45.6  | 45.8  | 45.9  |
| TSB     | Thornsberry  | 0.982  | 26.0  | 26.3  | 25.7  | 25.9  | 26.1    | 26.2      | 26.2  | 26.3  | 26.4  | 26.5  |
| WAT     | Waterford    | 0.978  | 45.3  | 44.9  | 44.0  | 44.3  | 44.7    | 44.9      | 44.9  | 45.0  | 45.2  | 45.3  |
| WEX     | Wexford      | 0.968  | 46.2  | 46.7  | 45.8  | 46.1  | 46.4    | 46.7      | 46.6  | 46.7  | 47.0  | 47.1  |
| WHI     | Whitegate    | 0.870  | 9.0   | 9.0   | 9.0   | 9.0   | 9.0     | 9.0       | 9.0   | 9.0   | 9.0   | 9.0   |

| Bus     |                     | Power  |      |      |      | De   | mand Fo | recast (N | IW)  |      |       |       |
|---------|---------------------|--------|------|------|------|------|---------|-----------|------|------|-------|-------|
| Code    | Bus Name            | Factor | 2020 | 2021 | 2022 | 2023 | 2024    | 2025      | 2026 | 2027 | 2028  | 2029  |
| AA      | Ardnacrusha         | 0.988  | 27.3 | 27.3 | 27.2 | 27.1 | 27.1    | 27.0      | 27.0 | 27.0 | 27.0  | 26.9  |
| AGH     | Aghyoule            | 1.000  | 4.1  | 4.1  | 4.2  | 4.2  | 4.3     | 4.4       | 4.4  | 4.4  | 4.5   | 4.5   |
| AGY     | Ardnagappary        | 0.985  | 4.8  | 4.8  | 4.7  | 4.7  | 4.7     | 4.7       | 4.7  | 4.7  | 4.7   | 4.7   |
| AHA     | Ahane               | 0.951  | 1.0  | 1.0  | 1.0  | 1.0  | 1.0     | 1.0       | 1.0  | 1.0  | 1.0   | 1.0   |
| AIR     | Airport Road        | 0.990  |      | -    | -    | 8.9  | 8.9     | 9.4       | 9.8  | 11.0 | 11.0  | 11.1  |
|         | (Belfast)           |        |      |      |      |      |         |           |      |      |       |       |
| ANR     | Anner               | 0.897  | 14.0 | 14.0 | 14.0 | 14.0 | 14.0    | 14.0      | 14.0 | 14.0 | 14.0  | 14.0  |
| ANT     | Antrim              | 0.991  | 12.2 | 12.3 | 12.5 | 12.4 | 12.6    | 12.7      | 12.8 | 12.9 | 12.9  | 13.0  |
| ARI     | Arigna              | 0.955  | 1.4  | 1.4  | 1.4  | 1.4  | 1.4     | 1.4       | 1.4  | 1.4  | 1.4   | 1.4   |
| ARK     | Arklow              | 0.960  | 4.8  | 4.8  | 4.8  | 4.8  | 4.8     | 4.8       | 4.8  | 4.8  | 4.7   | 4.7   |
| ATH     | Athlone             | 0.998  | 24.7 | 24.7 | 24.6 | 24.5 | 24.5    | 24.5      | 24.4 | 24.4 | 24.4  | 24.3  |
| ATY     | Athy                | 0.997  | 6.6  | 6.6  | 6.6  | 6.5  | 6.5     | 6.5       | 6.5  | 6.5  | 6.5   | 6.5   |
| BAH     | Barnageeragh        | 0.952  | -    | -    | -    | 3.0  | 5.0     | 8.0       | 10.0 | 13.0 | 15.0  | 18.0  |
| BAL     | Baltrasna           | 0.980  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3     | 4.3       | 4.3  | 4.3  | 4.3   | 4.3   |
| BAN (I) | Bandon              | 0.981  | 21.9 | 21.9 | 21.8 | 21.8 | 21.8    | 21.7      | 21.7 | 21.7 | 21.7  | 21.6  |
| BAN (N) | Banbridge           | 0.965  | 11.4 | 11.5 | 11.7 | 11.6 | 11.8    | 11.9      | 12.0 | 12.0 | 12.1  | 12.2  |
| BAR     | Barrymore           | 0.988  | 12.2 | 12.2 | 12.1 | 12.1 | 12.1    | 12.1      | 12.1 | 12.1 | 12.0  | 12.0  |
| BDA     | Baroda              | 0.988  | 5.3  | 5.3  | 5.3  | 5.3  | 5.3     | 5.3       | 5.3  | 5.3  | 5.3   | 5.3   |
| BDN     | Ballydine           | 0.972  | 9.0  | 8.9  | 8.9  | 8.9  | 8.9     | 8.9       | 8.9  | 8.9  | 8.9   | 8.9   |
| BEG     | Ballybeg            | 0.997  | 4.0  | 4.0  | 4.0  | 4.0  | 4.0     | 4.0       | 4.0  | 4.0  | 4.0   | 4.0   |
| BGD     | Belgard Road        | 0.950  | 29.5 | 37.0 | 44.7 | 53.2 | 53.2    | 53.2      | 53.2 | 53.2 | 53.2  | 53.2  |
| BGT     | Ballyragget         | 0.977  | -    | 0.0  | 0.0  | 7.8  | 7.8     | 7.7       | 7.7  | 7.7  | 7.7   | 7.7   |
| BIN     | Binbane             | 0.962  | 5.7  | 5.7  | 5.7  | 5.7  | 5.7     | 5.6       | 5.6  | 5.6  | 5.6   | 5.6   |
| ВК      | Bellacorick         | 0.993  | 1.9  | 1.9  | 1.9  | 1.9  | 1.9     | 1.8       | 1.8  | 1.8  | 1.8   | 1.8   |
| ВКҮ     | Barnakyle           | 0.950  | 3.0  | 25.8 | 29.6 | 33.4 | 37.2    | 41.0      | 44.8 | 48.6 | 51.5  | 56.2  |
| BLC     | Belcamp             | 0.950  | -    | 48.5 | 56.1 | 63.7 | 71.3    | 78.8      | 86.5 | 94.1 | 101.7 | 109.3 |
| BLI     | Ballylickey         | 0.960  | 4.6  | 4.6  | 4.6  | 4.6  | 4.6     | 4.5       | 4.5  | 4.5  | 4.5   | 4.5   |
| BLK     | Blake               | 0.992  | 5.3  | 5.3  | 5.2  | 5.2  | 5.2     | 5.2       | 5.2  | 5.2  | 5.2   | 5.2   |
| BMA     | Ballymena           | 0.965  | 24.4 | 24.5 | 25.0 | 24.7 | 25.3    | 25.4      | 25.6 | 25.7 | 25.8  | 26.0  |
| BNH     | Ballynahinch        | 0.995  | 16.6 | 16.7 | 17.0 | 16.8 | 17.2    | 17.3      | 17.4 | 17.5 | 17.6  | 17.7  |
| BNM     | Belfast North       | 0.990  | 14.6 | 14.7 | 15.0 | 14.8 | 15.1    | 15.2      | 15.3 | 15.4 | 15.5  | 15.6  |
| BOG     | Banoge              | 0.984  | 7.6  | 7.5  | 7.5  | 7.5  | 7.5     | 7.5       | 7.5  | 7.5  | 7.5   | 7.4   |
| BRA     | Bracklone           | 0.978  | 4.2  | 4.2  | 4.1  | 4.1  | 4.1     | 4.1       | 4.1  | 4.1  | 4.1   | 4.1   |
| BRI     | Brinny              | 0.971  | 4.0  | 4.0  | 4.0  | 4.0  | 4.0     | 4.0       | 4.0  | 4.0  | 4.0   | 4.0   |
| BRY     | Barnahely           | 0.984  | 23.0 | 22.9 | 22.9 | 22.8 | 22.8    | 22.8      | 22.7 | 22.7 | 22.7  | 22.7  |
| BUT     | Butlerstown         | 1.000  | 11.9 | 11.8 | 11.8 | 11.8 | 11.8    | 11.7      | 11.7 | 11.7 | 11.7  | 11.7  |
| BVG     | Ballyvallagh        | 0.881  | 4.4  | 4.4  | 4.5  | 4.5  | 4.6     | 4.6       | 4.6  | 4.6  | 4.7   | 4.7   |
| CAH     | Cahir               | 0.999  | 8.3  | 8.2  | 8.2  | 8.2  | 8.2     | 8.2       | 8.2  | 8.2  | 8.2   | 8.1   |
| CAR     | Carnmoney           | 0.993  | 7.4  | 7.4  | 7.4  | 7.2  | 7.3     | 7.2       | 7.1  | 7.0  | 7.1   | 7.1   |
| CBG     | Carrowbeg           | 0.992  | 9.0  | 9.0  | 8.9  | 8.9  | 8.9     | 8.9       | 8.9  | 8.9  | 8.9   | 8.9   |
| CBR     | Castlebar           | 0.987  | 11.5 | 11.5 | 11.5 | 11.4 | 11.4    | 11.4      | 11.4 | 11.4 | 11.4  | 11.4  |
| CEN     | Belfast Central     | 0.999  | 15.5 | 15.6 | 15.9 | 15.8 | 16.1    | 16.3      | 16.4 | 16.5 | 16.6  | 16.7  |
| CF      | Cathaleen's<br>Fall | 0.965  | 6.0  | 6.0  | 5.9  | 5.9  | 5.9     | 5.9       | 5.9  | 5.9  | 5.9   | 5.9   |
| CFM     | Castlefarm          | 0.901  | 50.8 | 50.8 | 50.8 | 50.8 | 50.8    | 50.8      | 50.8 | 50.8 | 50.8  | 50.8  |

| Bus     |              | Power          | Pr Demand Forecast (MW) |       |       |       |       |       |       |       |       |       |
|---------|--------------|----------------|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Code    | Bus Name     | Factor         | 2020                    | 2021  | 2022  | 2023  | 2024  | 2025  | 2026  | 2027  | 2028  | 2029  |
| CHA     | Charleville  | 1              |                         |       |       |       | -     | _     |       | -     |       | -     |
| CKG     | Corkagh      | 0.998<br>0.687 | 5.1                     | 5.1   | 5.1   | 5.1   | 5.0   | 5.0   | 5.0   | 5.0   | 5.0   | 5.0   |
| СКМ     | Carrickmines | 1              | 46.6                    | 54.2  | 64.1  | 74.1  | 84.1  | 94.1  | 104.5 | 114.0 | 124.5 | 134.0 |
|         |              | 0.980          | 160.4                   | 164.2 | 163.9 | 163.7 | 163.6 | 163.5 | 163.4 | 163.2 | 163.1 | 163.0 |
| CLE     | Clonee       | 0.950          | 67.5                    | 86.5  | 105.5 | 124.5 | 142.5 | 142.5 | 142.5 | 142.5 | 142.5 | 142.5 |
| CLG     | Cloghran     | 0.951          | 67.5                    | 75.0  | 79.8  | 79.8  | 79.8  | 79.8  | 79.8  | 79.8  | 79.8  | 79.8  |
| CLN     | Cloon        | 0.995          | 8.9                     | 8.9   | 8.9   | 8.9   | 8.9   | 8.9   | 8.8   | 8.8   | 8.8   | 8.8   |
| CLU     | Clutterland  | 0.950          | -                       | -     | -     | 3.8   | 9.5   | 14.3  | 20.0  | 24.7  | 30.4  | 35.2  |
| CLW     | Carlow       | 0.986          | 17.7                    | 17.7  | 17.7  | 17.6  | 17.6  | 17.6  | 17.6  | 17.5  | 17.5  | 17.5  |
| COL (I) | College Park | 0.987          | 13.9                    | 13.9  | 13.8  | 13.8  | 13.8  | 13.7  | 13.7  | 13.7  | 13.7  | 13.7  |
| COL (N) | Coleraine    | 0.973          | 12.5                    | 12.5  | 12.8  | 12.6  | 12.9  | 13.0  | 13.0  | 13.1  | 13.2  | 13.3  |
| COS     | Carrick-on-  | 0.994          | 8.9                     | 8.9   | 8.8   | 8.8   | 8.8   | 8.8   | 8.8   | 8.8   | 8.8   | 8.8   |
|         | Shannon      |                |                         |       |       |       |       |       |       |       |       |       |
| COW     | Cow Cross    | 0.970          | 1.7                     | 1.7   | 1.7   | 1.7   | 1.7   | 1.7   | 1.7   | 1.7   | 1.7   | 1.7   |
| CPS     | Cool         | 0.988          | 7.4                     | 7.4   | 7.6   | 7.5   | 7.7   | 7.7   | 7.8   | 7.8   | 7.8   | 7.9   |
| CRA     | Crane        | 1.000          | 5.9                     | 5.9   | 5.9   | 5.9   | 5.9   | 5.8   | 5.8   | 5.8   | 5.8   | 5.8   |
| CRE     | Cregagh      | 0.970          | 25.1                    | 25.2  | 21.2  | 21.1  | 21.6  | 21.7  | 21.9  | 22.0  | 22.1  | 22.3  |
| CRG     | Creagh       | 0.972          | 7.3                     | 7.3   | 7.4   | 7.4   | 7.5   | 7.6   | 7.6   | 7.6   | 7.7   | 7.7   |
| CRH     | Cruiserath   | 0.950          | -                       | -     | 9.0   | 14.3  | 19.5  | 24.7  | 29.9  | 35.2  | 40.4  | 45.6  |
| CRO     | Coolroe      | 1.000          | 5.5                     | 5.5   | 5.5   | 5.5   | 5.5   | 5.5   | 5.4   | 5.4   | 5.4   | 5.4   |
| CVW     | Castleview   | 0.994          | 9.3                     | 9.3   | 9.3   | 9.2   | 9.2   | 9.2   | 9.2   | 9.2   | 9.2   | 9.2   |
| DAL     | Dallow       | 0.993          | 4.8                     | 4.8   | 4.7   | 4.7   | 4.7   | 4.7   | 4.7   | 4.7   | 4.7   | 4.7   |
| DDK     | Dundalk      | 1.000          | 17.4                    | 17.4  | 17.3  | 17.3  | 17.3  | 17.3  | 17.3  | 17.2  | 17.2  | 17.2  |
| DFR     | Dunfirth     | 1.000          | 3.0                     | 3.0   | 3.0   | 3.0   | 3.0   | 3.0   | 3.0   | 2.9   | 2.9   | 2.9   |
| DGN     | Dungarvan    | 0.999          | 12.8                    | 12.8  | 12.7  | 12.7  | 12.7  | 12.7  | 12.6  | 12.6  | 12.6  | 12.6  |
| DLT     | Dalton       | 1.000          | 8.4                     | 8.4   | 8.4   | 8.3   | 8.3   | 8.3   | 8.3   | 8.3   | 8.3   | 8.3   |
| DMY     | Dunmanway    | 0.961          | 9.1                     | 9.1   | 9.0   | 9.0   | 9.0   | 9.0   | 9.0   | 9.0   | 9.0   | 9.0   |
| DON     | Donegall     | 0.992          | 27.1                    | 26.8  | 26.8  | 26.1  | 26.2  | 26.0  | 25.7  | 25.4  | 25.5  | 25.7  |
| D00     | Doon         | 0.994          | 8.9                     | 8.9   | 8.9   | 8.8   | 8.8   | 8.8   | 8.8   | 8.8   | 8.8   | 8.8   |
| DRU (I) | Drumline     | 0.956          | 12.0                    | 12.0  | 11.9  | 11.9  | 11.9  | 11.9  | 11.9  | 11.9  | 11.8  | 11.8  |
| DRU (N) | Drumnakelly  | 0.999          | 26.7                    | 26.8  | 27.4  | 27.1  | 27.7  | 27.9  | 28.1  | 28.3  | 28.4  | 28.6  |
| DRY     | Drybridge    | 0.995          | 25.6                    | 25.5  | 25.4  | 25.4  | 25.4  | 25.3  | 25.3  | 25.3  | 25.2  | 25.2  |
| DUN     | Dungannon    | 0.970          | 28.3                    | 28.4  | 28.9  | 28.7  | 29.3  | 29.5  | 29.7  | 29.8  | 29.9  | 30.1  |
| EDE     | Eden         | 0.965          | 10.1                    | 10.1  | 10.3  | 10.2  | 10.4  | 10.5  | 10.6  | 10.6  | 10.7  | 10.7  |
| ENN (I) | Ennis        | 0.997          | 18.6                    | 18.6  | 18.5  | 18.5  | 18.4  | 18.4  | 18.4  | 18.4  | 18.3  | 18.3  |
| ENN (N) | Enniskillen  | 0.981          | 17.1                    | 17.2  | 17.5  | 17.3  | 17.7  | 17.8  | 17.9  | 18.0  | 18.1  | 18.2  |
| FIN (I) | Finglas      | 0.982          | 159.4                   | 176.1 | 175.7 | 175.4 | 158.5 | 158.3 | 158.2 | 158.1 | 174.6 | 174.5 |
| FIN (N) | Finaghy      | 0.986          | 9.0                     | 9.1   | 9.2   | 9.2   | 9.4   | 9.4   | 9.5   | 9.5   | 9.6   | 9.6   |
| FTT     | Fortunestown | 0.970          | 3.2                     | 3.2   | 3.2   | 3.2   | 3.2   | 3.2   | 3.2   | 3.2   | 3.2   | 3.2   |
| GAL     | Galway       | 1.000          | 28.3                    | 28.2  | 28.1  | 20.3  | 28.0  | 28.0  | 28.0  | 27.9  | 27.9  | 27.9  |
| GI      | Great Island | 0.950          | 4.8                     | 5.1   | 5.1   | 5.1   | 5.1   | 5.1   | 5.1   | 5.1   | 5.0   | 5.0   |
| GIL     | Gilra        | 0.971          | 11.4                    | 11.4  | 11.4  | 11.4  | 11.4  | 11.4  | 11.4  | 11.4  | 11.4  | 11.4  |
| GLE (I) | Glenlara     | 0.956          | 5.0                     | 5.0   | 5.0   | 5.0   | 5.0   | 5.0   | 5.0   | 5.0   | 5.0   | 5.0   |
| GLE (N) | Glengormley  | 0.976          | 9.2                     | 9.2   | 9.3   | 9.2   | 9.4   | 9.4   | 9.4   | 9.4   | 9.5   | 9.5   |
| GOR (N) | Gort         | 1.000          | 0.4                     | 0.4   | 0.4   | 0.4   | 0.4   | 0.4   | 0.4   | 0.4   | 0.4   | 0.4   |

| Bus     |              | Power  |       |             |       | De    | mand Fo | recast (N | IW)   |       |       |       |
|---------|--------------|--------|-------|-------------|-------|-------|---------|-----------|-------|-------|-------|-------|
| Code    | Bus Name     | Factor | 2020  | 2021        | 2022  | 2023  | 2024    | 2025      | 2026  | 2027  | 2028  | 2029  |
| GRI     | Griffinrath  | 0.948  | 17.0  | 16.9        | 16.9  | 16.9  | 16.8    | 16.8      | 16.8  | 16.8  | 16.8  | 16.7  |
| GWE     | Gortawee     | 0.940  | 27.8  | 27.8        | 27.8  | 27.7  | 27.7    | 27.7      | 27.7  | 27.7  | 27.7  | 27.7  |
| IKE     | Ikerrin      | 0.947  | 7.6   | 7.6         | 7.6   | 7.6   | 7.5     | 7.5       | 7.5   | 7.5   | 7.5   | 7.5   |
| INC     | Inchicore    | 0.997  | 138.2 | 122.8       | 128.5 |       | 156.6   | 160.2     | 163.1 | 166.7 |       |       |
| КВҮ     | Kilbarry     |        |       |             |       | 144.1 |         |           |       | -     | 152.3 | 155.7 |
| KER     | -            | 0.995  | 17.5  | 17.4        | 17.4  | 17.4  | 17.3    | 17.3      | 17.3  | 17.3  | 17.3  | 17.2  |
|         | Knockearagh  | 0.994  | 13.5  | 13.5        | 13.4  | 13.4  | 13.4    | 13.4      | 13.4  | 13.4  | 13.3  | 13.3  |
| KIL     | Kildare      | 0.950  | -     | -           | -     | -     | 7.6     | 15.2      | 22.8  | 30.4  | 38.0  | 45.6  |
| KIN     | Kinnegad     | 0.973  | 10.2  | 10.2        | 10.2  | 10.2  | 10.2    | 10.2      | 10.2  | 10.2  | 10.2  | 10.2  |
| KKY     | Kilkenny     | 1.000  | 17.1  | 17.1        | 17.0  | 13.6  | 13.6    | 13.6      | 13.5  | 13.5  | 13.5  | 13.5  |
| KNO     | Knock        | 0.975  | 15.0  | 15.0        | 13.4  | 13.3  | 13.5    | 13.6      | 13.7  | 13.8  | 13.9  | 14.0  |
| KTL     | Kilteel      | 0.988  | 14.9  | 14.9        | 14.8  | 14.8  | 14.8    | 14.8      | 14.8  | 14.7  | 14.7  | 14.7  |
| KTN     | Killoteran   | 0.977  | 4.9   | 4.8         | 4.8   | 4.8   | 4.8     | 4.8       | 4.8   | 4.8   | 4.8   | 4.8   |
| KUR     | Knockumber   | 0.907  | 23.7  | 23.7        | 23.7  | 23.7  | 23.7    | 23.7      | 23.7  | 23.7  | 23.7  | 23.7  |
| KYN     | Kellystown   | 0.950  | -     | -           | 125.0 | 125.0 | 125.0   | 125.0     | 125.0 | 125.0 | 125.0 | 125.0 |
| KUD     | Kilmahud     | 0.950  | 17.1  | 17.1        | 20.9  | 24.7  | 28.5    | 32.3      | 36.1  | 39.9  | 43.7  | 47.5  |
| LA      | Lanesboro    | 0.978  | 4.4   | 4.4         | 4.4   | 4.3   | 4.3     | 4.3       | 4.3   | 4.3   | 4.3   | 4.3   |
| LAR     | Larne        | 0.881  | 8.4   | 8.4         | 8.6   | 8.5   | 8.6     | 8.7       | 8.7   | 8.8   | 8.8   | 8.9   |
| LET     | Letterkenny  | 0.975  | 16.9  | 16.9        | 16.9  | 16.8  | 16.8    | 16.8      | 16.8  | 16.7  | 16.7  | 16.7  |
| LIB     | Liberty      | 0.981  | 7.5   | 7.5         | 7.5   | 7.5   | 7.5     | 7.5       | 7.5   | 7.5   | 7.4   | 7.4   |
| LIM (I) | Limerick     | 1.000  | 28.9  | 28.9        | 28.8  | 28.8  | 28.7    | 28.7      | 28.6  | 28.6  | 28.6  | 28.5  |
| LIM (N) | Limavady     | 0.989  | 7.2   | 7.3         | 7.4   | 7.3   | 7.5     | 7.5       | 7.6   | 7.6   | 7.6   | 7.7   |
| LIS (I) | Lisdrum      | 0.988  | 9.2   | 9.1         | 9.1   | 9.1   | 9.1     | 9.1       | 9.1   | 9.1   | 9.0   | 9.0   |
| LIS (N) | Lisburn      | 0.995  | 21.6  | 21.7        | 22.1  | 21.9  | 22.4    | 22.5      | 22.6  | 22.7  | 22.9  | 23.0  |
| LMR     | Lisaghmore   | 0.980  | 9.6   | 9.6         | 9.8   | 9.7   | 9.9     | 10.0      | 10.0  | 10.1  | 10.1  | 10.2  |
| LOG     | Loguestown   | 0.994  | 11.4  | 11.4        | 11.6  | 11.5  | 11.8    | 11.8      | 11.9  | 12.0  | 12.0  | 12.1  |
| MAC     | Macroom      | 0.990  | 8.1   | 8.1         | 8.1   | 8.1   | 8.1     | 8.1       | 8.1   | 8.1   | 8.0   | 8.0   |
| MAL     | Mallow       | 0.989  | 7.2   | 7.1         | 7.1   | 7.1   | 7.1     | 7.1       | 7.1   | 7.1   | 7.1   | 7.1   |
| MCE     | Macetown     | 0.999  | 15.0  | 14.9        | 14.9  | 14.9  | 14.9    | 14.9      | 14.8  | 14.8  | 14.8  | 14.8  |
| MID     | Midleton     | 0.988  | 19.3  | 19.3        | 19.2  | 19.2  | 19.1    | 19.1      | 19.1  | 19.1  | 19.0  | 19.0  |
| MLN     | Mullagharlin | 0.958  | 4.5   | 4.5         | 4.5   | 4.5   | 4.5     | 4.5       | 4.5   | 4.5   | 4.5   | 4.5   |
| MON     | Monread      | 0.993  | 4.4   | 4.4         | 4.4   | 4.4   | 4.4     | 4.4       | 4.4   | 4.4   | 4.4   | 4.4   |
| MOY     | Моу          | 1.000  | 8.1   | 8.1         | 8.0   | 8.0   | 8.0     | 8.0       | 8.0   | 8.0   | 8.0   | 8.0   |
| MR      | Marina       | 1.000  | 4.5   | 4.5         | 4.5   | 4.5   | 4.5     | 4.5       | 4.5   | 4.5   | 4.5   | 4.5   |
| MTH     | Meathhill    | 0.977  | 16.2  | 16.2        | 16.1  | 16.1  | 16.1    | 16.1      | 16.1  | 16.0  | 16.0  | 16.0  |
| MUL     | Mullingar    | 0.971  | 12.2  | 12.2        | 12.2  | 12.1  | 12.1    | 12.1      | 12.1  | 12.1  | 12.1  | 12.1  |
| MUN     | Mungret      | 0.871  | 21.5  | 21.5        | 21.5  | 21.5  | 21.5    | 21.5      | 21.5  | 21.5  | 21.5  | 21.5  |
| NAR     | Newtownards  | 0.954  | 13.2  | 13.3        | 13.5  | 13.4  | 13.7    | 13.8      | 13.8  | 13.9  | 14.0  | 14.1  |
| NAV     | Navan        | 1.000  | 15.2  | 15.2        | 15.1  | 15.1  | 15.1    | 15.1      | 15.1  | 15.0  | 15.0  | 15.0  |
| NEN     | Nenagh       | 0.986  | 10.4  | 10.4        | 10.4  | 10.4  | 10.3    | 10.3      | 10.3  | 10.3  | 10.3  | 10.3  |
| NEW (I) | Newbridge    | 0.992  | 5.4   | 5.4         | 5.4   | 5.4   | 5.4     | 5.4       | 5.4   | 5.4   | 5.4   | 5.4   |
| NEW (N) | Newry        | 0.990  | 23.3  | 23.4        | 23.9  | 23.7  | 24.2    | 24.3      | 24.5  | 24.6  | 24.7  | 24.8  |
| OLD     | Oldcourt     | 0.949  | 0.3   | 0.3         | 0.3   | 0.3   | 0.3     | 0.3       | 0.3   | 0.3   | 0.3   | 0.3   |
| ОМА     | Omagh        | 0.970  | 17.7  | 17.8        | 18.1  | 17.9  | 18.3    | 18.4      | 18.5  | 18.6  | 18.7  | 18.8  |
| OUG     | Oughtragh    | 0.996  | 9.6   | <i>9</i> .6 | 9.5   | 9.5   | 9.5     | 9.5       | 9.5   | 9.5   | 9.5   | 9.5   |
| РВ      | Poolbeg      | 0.995  | 72.7  | 72.6        | 72.4  | 72.2  | 72.1    | 72.1      | 72.0  | 71.9  | 71.8  | 71.7  |

| Bus     |              | Power  |       |       |       | De    | mand Fo | recast (N | IW)   |       |       |       |
|---------|--------------|--------|-------|-------|-------|-------|---------|-----------|-------|-------|-------|-------|
| Code    | Bus Name     | Factor | 2020  | 2021  | 2022  | 2023  | 2024    | 2025      | 2026  | 2027  | 2028  | 2029  |
| PLA     | Platin       | 0.950  | 18.0  | 18.0  | 18.0  | 18.0  | 18.0    | 18.0      | 18.0  | 18.0  | 18.0  | 18.0  |
| PLS     | Portlaoise   | 0.999  | 15.0  | 15.0  | 15.0  | 10.6  | 10.6    | 10.6      | 10.6  | 10.5  | 10.5  | 10.5  |
| RAT (I) | Rathkeale    | 0.989  | 26.0  | 26.0  | 25.9  | 25.8  | 25.8    | 25.8      | 25.7  | 25.7  | 25.7  | 25.6  |
| RAT (N) | Rathgael     | 0.995  | 16.9  | 16.9  | 17.3  | 17.1  | 17.5    | 17.6      | 17.7  | 17.7  | 17.8  | 17.9  |
| RIC     | Richmond     | 1.000  | 10.7  | 10.7  | 10.7  | 10.6  | 10.6    | 10.6      | 10.6  | 10.6  | 10.6  | 10.6  |
| RMN     | Rathmullan   | 0.950  | -     | -     | -     | 3.8   | 9.5     | 14.3      | 20.0  | 24.7  | 30.4  | 35.2  |
| RNW     | Rinawade     | 0.988  | 9.1   | 9.1   | 9.1   | 9.1   | 9.1     | 9.1       | 9.1   | 9.1   | 9.1   | 9.1   |
| ROS     | Rosebank     | 0.971  | 8.9   | 8.9   | 8.2   | 8.1   | 8.3     | 8.3       | 8.4   | 8.4   | 8.4   | 8.5   |
| RSY     | Ringaskiddy  | 0.993  | 1.0   | 1.0   | 1.0   | 1.0   | 1.0     | 1.0       | 1.0   | 1.0   | 1.0   | 1.0   |
| RYB     | Ryebrook     | 0.928  | 104.5 | 104.5 | 104.5 | 104.5 | 104.5   | 104.5     | 104.5 | 104.5 | 104.5 | 104.5 |
| SAL     | Salthill     | 0.998  | 18.3  | 18.3  | 18.2  | 18.2  | 18.2    | 18.2      | 18.1  | 18.1  | 18.1  | 18.1  |
| SBH     | Snughborough | 0.950  | 7.6   | 11.4  | 14.3  | 17.1  | 19.0    | 21.9      | 23.8  | 26.6  | 28.5  | 31.4  |
| SCR     | Screeb       | 0.971  | 10.1  | 10.0  | 10.0  | 10.0  | 10.0    | 10.0      | 9.9   | 9.9   | 9.9   | 9.9   |
| SHE     | Shelton      | 0.956  | 2.3   | 2.3   | 2.3   | 2.3   | 2.3     | 2.3       | 2.3   | 2.3   | 2.3   | 2.3   |
| SKL     | Shankill     | 0.997  | 15.5  | 15.5  | 15.4  | 15.4  | 15.4    | 15.4      | 15.4  | 15.3  | 15.3  | 15.3  |
| SLI     | Sligo        | 1.000  | 18.1  | 18.1  | 18.0  | 18.0  | 18.0    | 18.0      | 18.0  | 17.9  | 17.9  | 17.9  |
| SNG     | Singland     | 0.970  | 3.6   | 3.6   | 3.6   | 3.6   | 3.6     | 3.6       | 3.6   | 3.6   | 3.6   | 3.6   |
| SOM     | Somerset     | 0.999  | 4.6   | 4.6   | 4.5   | 4.5   | 4.5     | 4.5       | 4.5   | 4.5   | 4.5   | 4.5   |
| SPR     | Springtown   | 0.995  | 13.9  | 13.9  | 14.2  | 14.0  | 14.3    | 14.4      | 14.5  | 14.6  | 14.6  | 14.7  |
| STR     | Stratford    | 1.000  | 4.8   | 4.8   | 4.8   | 4.8   | 4.8     | 4.8       | 4.8   | 4.8   | 4.8   | 4.8   |
| STR (N) | Strabane     | 0.920  | 12.4  | 12.4  | 12.6  | 12.5  | 12.8    | 12.8      | 12.9  | 13.0  | 13.0  | 13.1  |
| TBG     | Trabeg       | 0.988  | 30.9  | 30.9  | 30.8  | 30.7  | 30.7    | 30.6      | 30.6  | 30.6  | 30.5  | 30.5  |
| ТВК     | Tullabrack   | 0.972  | 4.2   | 4.2   | 4.2   | 4.2   | 4.2     | 4.2       | 4.2   | 4.1   | 4.1   | 4.1   |
| THU     | Thurles      | 0.998  | 10.2  | 10.2  | 10.1  | 10.1  | 10.1    | 10.1      | 10.1  | 10.1  | 10.1  | 10.1  |
| TIP     | Tipperary    | 0.995  | 7.2   | 7.1   | 7.1   | 7.1   | 7.1     | 7.1       | 7.1   | 7.1   | 7.1   | 7.1   |
| TLK     | Trillick     | 0.953  | 5.7   | 5.7   | 5.7   | 5.7   | 5.7     | 5.7       | 5.7   | 5.7   | 5.7   | 5.7   |
| TON     | Tonroe       | 0.975  | 5.8   | 5.8   | 5.8   | 5.8   | 5.8     | 5.8       | 5.8   | 5.8   | 5.8   | 5.8   |
| TRI     | Trien        | 0.972  | 14.0  | 14.0  | 14.0  | 13.9  | 13.9    | 13.9      | 13.9  | 13.9  | 13.8  | 13.8  |
| TRL     | Tralee       | 0.981  | 14.1  | 14.1  | 14.0  | 14.0  | 14.0    | 14.0      | 13.9  | 13.9  | 13.9  | 13.9  |
| TSB     | Thornsberry  | 0.959  | 9.9   | 9.9   | 9.9   | 9.9   | 9.8     | 9.8       | 9.8   | 9.8   | 9.8   | 9.8   |
| WAR     | Waringstown  | 0.980  | 19.3  | 19.4  | 19.8  | 19.6  | 20.0    | 20.1      | 20.2  | 20.3  | 20.4  | 20.5  |
| WAT     | Waterford    | 1.000  | 25.1  | 24.7  | 24.7  | 24.6  | 24.6    | 24.6      | 24.5  | 24.5  | 24.5  | 24.4  |
| WEX     | Wexford      | 0.998  | 18.9  | 18.8  | 18.8  | 18.7  | 18.7    | 18.7      | 18.7  | 18.7  | 18.6  | 18.6  |
| WHI     | Whitegate    | 0.870  | 9.0   | 9.0   | 9.0   | 9.0   | 9.0     | 9.0       | 9.0   | 9.0   | 9.0   | 9.0   |

| Bus     |                 | Power  |      |      |      | De   | mand Fo | recast (N | IW)  | •    |      |      |
|---------|-----------------|--------|------|------|------|------|---------|-----------|------|------|------|------|
| Code    | Bus Name        | Factor | 2020 | 2021 | 2022 | 2023 | 2024    | 2025      | 2026 | 2027 | 2028 | 2029 |
| AGH     | Aghyoule        | 0.998  | 12.1 | 12.2 | 12.5 | 12.5 | 12.8    | 12.9      | 13.1 | 13.2 | 13.3 | 13.3 |
| AIR     | Airport Road    | 0.990  | -    | -    | -    | 24.5 | 26.5    | 27.7      | 29.1 | 32.5 | 32.7 | 32.9 |
|         | (Belfast)       |        |      |      |      |      | _       |           |      |      |      |      |
| ANT     | Antrim          | 0.991  | 36.2 | 36.4 | 37.0 | 36.7 | 37.5    | 37.7      | 37.9 | 38.1 | 38.3 | 38.5 |
| BAN (N) | Banbridge       | 0.979  | 33.9 | 34.1 | 34.7 | 34.4 | 35.1    | 35.3      | 35.6 | 35.7 | 35.9 | 36.1 |
| ВМА     | Ballymena       | 0.979  | 72.4 | 72.7 | 74.0 | 73.3 | 74.9    | 75.4      | 75.8 | 76.2 | 76.6 | 77.0 |
| BNH     | Ballynahinch    | 0.991  | 49.3 | 49.5 | 50.4 | 49.9 | 51.0    | 51.3      | 51.6 | 51.8 | 52.1 | 52.4 |
| BNM     | Belfast North   | 0.990  | 43.4 | 43.5 | 44.4 | 43.9 | 44.9    | 45.2      | 45.4 | 45.6 | 45.9 | 46.1 |
| BVG     | Ballyvallagh    | 0.972  | 13.1 | 13.2 | 13.4 | 13.3 | 13.6    | 13.6      | 13.7 | 13.8 | 13.8 | 13.9 |
| CAR     | Carnmoney       | 0.996  | 22.1 | 21.8 | 21.9 | 21.4 | 21.5    | 21.3      | 21.1 | 20.9 | 21.0 | 21.1 |
| CEN     | Belfast Central | 0.999  | 45.9 | 46.2 | 47.1 | 46.8 | 47.9    | 48.2      | 48.6 | 48.9 | 49.2 | 49.4 |
| COL (N) | Coleraine       | 0.991  | 37.0 | 37.1 | 37.8 | 37.5 | 38.3    | 38.5      | 38.7 | 38.9 | 39.1 | 39.3 |
| CPS     | Cool            | 0.989  | 21.9 | 22.0 | 22.4 | 22.2 | 22.7    | 22.9      | 23.0 | 23.1 | 23.2 | 23.3 |
| CRE     | Cregagh         | 0.987  | 74.5 | 74.9 | 63.0 | 62.5 | 64.0    | 64.4      | 64.9 | 65.3 | 65.7 | 66.1 |
| CRG     | Creagh          | 0.991  | 21.5 | 21.6 | 22.0 | 21.8 | 22.3    | 22.4      | 22.5 | 22.6 | 22.8 | 22.9 |
| DON     | Donegall        | 1.000  | 80.4 | 79.4 | 79.5 | 77.4 | 77.8    | 77.0      | 76.2 | 75.3 | 75.7 | 76.2 |
| DRU (N) | Drumnakelly     | 0.988  | 79.3 | 79.6 | 81.1 | 80.4 | 82.2    | 82.7      | 83.3 | 83.8 | 84.3 | 84.7 |
| DUN     | Dungannon       | 0.970  | 83.9 | 84.3 | 85.9 | 85.1 | 86.9    | 87.4      | 87.9 | 88.3 | 88.8 | 89.3 |
| EDE     | Eden            | 0.984  | 29.9 | 30.1 | 30.6 | 30.3 | 31.0    | 31.2      | 31.4 | 31.5 | 31.7 | 31.8 |
| ENN (N) | Enniskillen     | 0.984  | 50.7 | 50.9 | 51.9 | 51.4 | 52.5    | 52.9      | 53.2 | 53.4 | 53.7 | 54.0 |
| FIN (N) | Finaghy         | 0.994  | 26.8 | 26.9 | 27.4 | 27.2 | 27.7    | 27.9      | 28.1 | 28.2 | 28.3 | 28.5 |
| GLE (N) | Glengormley     | 0.976  | 27.3 | 27.3 | 27.7 | 27.3 | 27.8    | 27.9      | 27.9 | 27.9 | 28.1 | 28.3 |
| КНО     | Knock           | 0.981  | 44.4 | 44.5 | 39.6 | 39.3 | 40.2    | 40.5      | 40.7 | 40.9 | 41.2 | 41.4 |
| LAR     | Larne           | 0.972  | 24.8 | 24.9 | 25.4 | 25.1 | 25.6    | 25.8      | 25.9 | 26.0 | 26.2 | 26.3 |
| LIM (N) | Limavady        | 0.977  | 21.4 | 21.5 | 21.9 | 21.7 | 22.2    | 22.3      | 22.4 | 22.5 | 22.6 | 22.7 |
| LIS (N) | Lisburn         | 0.992  | 64.1 | 64.3 | 65.5 | 64.9 | 66.3    | 66.7      | 67.1 | 67.4 | 67.8 | 68.2 |
| LMR     | Lisaghmore      | 0.980  | 28.4 | 28.6 | 29.1 | 28.8 | 29.4    | 29.6      | 29.8 | 29.9 | 30.1 | 30.3 |
| LOG     | Loguestown      | 0.977  | 33.8 | 33.9 | 34.5 | 34.2 | 34.9    | 35.1      | 35.3 | 35.5 | 35.7 | 35.9 |
| NAR     | Newtownards     | 1.000  | 39.3 | 39.4 | 40.2 | 39.8 | 40.6    | 40.9      | 41.1 | 41.3 | 41.5 | 41.7 |
| NEW (N) | Newry           | 0.990  | 69.2 | 69.5 | 70.8 | 70.2 | 71.7    | 72.1      | 72.6 | 72.9 | 73.3 | 73.7 |
| ОМА     | Omagh           | 0.993  | 52.5 | 52.7 | 53.7 | 53.2 | 54.3    | 54.6      | 54.9 | 55.1 | 55.4 | 55.8 |
| RAT (N) | Rathgael        | 0.997  | 50.1 | 50.3 | 51.2 | 50.7 | 51.8    | 52.1      | 52.4 | 52.6 | 52.9 | 53.2 |
| ROS     | Rosebank        | 0.979  | 26.3 | 26.4 | 24.2 | 24.0 | 24.5    | 24.6      | 24.8 | 24.9 | 25.0 | 25.2 |
| SPR     | Springtown      | 0.994  | 41.2 | 41.3 | 42.1 | 41.7 | 42.6    | 42.8      | 43.0 | 43.2 | 43.5 | 43.7 |
| STR (N) | Strabane        | 0.968  | 36.6 | 36.8 | 37.4 | 37.1 | 37.9    | 38.1      | 38.3 | 38.5 | 38.7 | 38.9 |
| WAR     | Waringstown     | 0.986  | 57.3 | 57.5 | 58.6 | 58.0 | 59.3    | 59.6      | 59.9 | 60.2 | 60.5 | 60.8 |

#### Table C-4: Demand Forecasts at Time of Autumn Peak – Northern Ireland only

# Appendix D Generation Capacity Details

# **D.1. Generation Capacity Details**

Table D-1 lists existing and committed future transmission connected generation, their connection details and the Registered Capacity<sup>131</sup> of each unit as at the data freeze date. All generation capacity figures in Table D-1 are expressed in exported terms. Exported terms are given by the generation unit output less the unit's own auxiliary load. The units are grouped in these tables on a geographical basis. Generation capacity figures are rounded to the nearest MW.

Table D-2 lists the existing and committed future wind generation. The wind generation included in this table is wind generation that feeds into each 110 kV transmission station, from the distribution system. The respective MW capacity over the period of the statement is included. Table D-2 is based on the wind farms that had connection agreements with the DSO at the data freeze date.

Table D-3 lists the existing and committed distribution connected generation, excluding wind generation, as at the data freeze date. Their respective MW capacity over the period of the statement is included.

<sup>131</sup> The Registered Capacity of future units will not be known until the unit enters the Integrated Single Electricity Market. Therefore, for future units the Maximum Export Capacity of the unit appears in Table D-1.

| Area   | Generation<br>Station   | Unit ID | Connected At     | Fuel   | l Туре  | Connection<br>Year (if<br>future) | Maximum<br>Export<br>Capacity<br>(MW) |
|--------|-------------------------|---------|------------------|--------|---------|-----------------------------------|---------------------------------------|
|        | Carrickaduff            |         | Croaghnagawna    | 110 kV | Wind    | 2022                              | 66                                    |
|        | Carrickalangan          |         | Croaghnagawna    | 110 kV | Wind    | 2022                              | 72                                    |
|        | Erne                    | ER3     | Cathaleen's Fall | 110 kV | Hydro   |                                   | 22                                    |
|        | Erne                    | ER4     | Cathaleen's Fall | 110 kV | Hydro   |                                   | 23                                    |
|        | Erne                    | ER1     | Cliff            | 110 kV | Hydro   |                                   | 10                                    |
|        | Erne                    | ER2     | Cliff            | 110 kV | Hydro   |                                   | 10                                    |
|        | Garvagh - Glebe         |         | Garvagh          | 110 kV | Wind    |                                   | 26                                    |
|        | Garvagh -<br>Tullynahaw |         | Garvagh          | 110 kV | Wind    |                                   | 22                                    |
|        | Golagh                  |         | Golagh           | 110 kV | Wind    |                                   | 15                                    |
| Border | Kingsmountain (1)       |         | Cunghill         | 110 kV | Wind    |                                   | 24                                    |
|        | Kingsmountain (2)       |         | Cunghill         | 110 kV | Wind    |                                   | 11                                    |
|        | Lisdrumdoagh            |         | Lisdrum          | 110 kV | Battery | 2024                              | 60                                    |
|        | Meentycat (1)           |         | Meentycat        | 110 kV | Wind    |                                   | 71                                    |
|        | Meentycat (2)           |         | Meentycat        | 110 kV | Wind    |                                   | 14                                    |
|        | Mountain Lodge          |         | Ratrussan        | 110 kV | Wind    |                                   | 31                                    |
|        | Mulreavy                |         | Mulreavy         | 110 kV | Wind    |                                   | 82                                    |
|        | Mulreavy Ext            |         | Mulreavy         | 110 kV | Wind    |                                   | 13                                    |
|        | Oriel                   |         | Oriel            | 110 kV | Wind    | 2022                              | 210                                   |
|        | Ratrussan               |         | Ratrussan        | 110 kV | Wind    |                                   | 48                                    |
|        |                         |         | Border Area T    | otal   |         |                                   | 829                                   |
|        | Dublin Bay Power        | DB1     | Irishtown        | 220 kV | Gas/DO  |                                   | 422                                   |
|        | Gallanstown             |         | Gallanstown      | 110 kV | Solar   | 2021                              | 85                                    |
| Dublin | Harristown              |         | Harristown       | 110 kV | Solar   | 2022                              | 42                                    |
| Bubun  | Huntstown               | HNC     | Huntstown A      | 220 kV | Gas/DO  |                                   | 359                                   |
|        | Huntstown               | HN2     | Huntstown B      | 220 kV | Gas/DO  |                                   | 412                                   |
|        | Poolbeg                 | PBC     | Shellybanks      | 220 kV | Gas/DO  |                                   | 473                                   |
|        |                         |         | Dublin Area T    | otal   |         |                                   | 1793                                  |

|             |                       |         |                 |        |            |            | Maximum  |
|-------------|-----------------------|---------|-----------------|--------|------------|------------|----------|
|             |                       |         |                 |        |            | Connection | Export   |
|             | Generation            |         |                 |        |            | Year (if   | Capacity |
| Area        | Station               | Unit ID | Connected At    | Fuel   | Туре       | future)    | (MW)     |
|             | Blundelstown          |         | Blundelstown    | 110 kV | Solar      | 2021       | 80       |
|             | Gorey BES             |         | Gorman          | 110 kV | Battery    | 2022       | 50       |
|             | Porterstown BES       |         | Kilteel         | 110 kV | Battery    | 2024       | 60       |
|             | Liffey Hydro          | Ll1     | Pollaphuca      | 110 kV | Hydro      |            | 15       |
|             | Liffey Hydro          | LI2     | Pollaphuca      | 110 kV | Hydro      |            | 15       |
| Mid-East    | Liffey Hydro          | LI4     | Pollaphuca      | 110 kV | Hydro      |            | 15       |
| initia Eust | Muckerstown           |         | Muckerstown     | 110 kV | Solar      | 2021       | 34       |
|             | Timahoe               |         | Timahoe         | 110 kV | Solar      | 2021       | 70       |
|             | Turlough Hill         | TH1     | Turlough Hill   | 220 kV | Hydro      |            | 73       |
|             | Turlough Hill         | TH2     | Turlough Hill   | 220 kV | Hydro      |            | 73       |
|             | Turlough Hill         | TH3     | Turlough Hill   | 220 kV | Hydro      |            | 73       |
|             | Turlough Hill         | TH4     | Turlough Hill   | 220 kV | Hydro      |            | 73       |
|             |                       |         | Mid-East Area T | otal   |            |            | 631      |
|             | Edenderry Peaking     | ED3     | Cushaling       | 110 kV | Distillate | 2025       | 117      |
|             | Edenderry Power       | ED1     | Cushaling       | 110 kV | Peat       |            | 134      |
|             | Lough Ree Power       | LR4     | Lanesboro       | 110 kV | Peat       |            | 103      |
| Midlands    | Loughteague           |         | Coolnabacky     | 110 kV | Solar      | 2023       | 55       |
| micianus    | Lumcloon              |         | Lumcloon        | 110 kV | Battery    | 2021       | 100      |
|             | Mountlucas            |         | Mountlucas      | 110 kV | Wind       |            | 79       |
|             | Rhode PCP (1)         | RP1     | Derryiron       | 110 kV | Distillate |            | 52       |
|             | Rhode PCP (2)         | RP2     | Derryiron       | 110 kV | Distillate |            | 52       |
|             |                       |         | Midlands Area 1 | Total  |            |            | 692      |
|             | Aughinish             | SK3     | Aughinish       | 110 kV | Gas/DO     |            | 86       |
|             | Aughinish             | SK4     | Aughinish       | 110 kV | Gas/DO     |            | 86       |
|             | Ardnacrusha Hydro (1) | AA1     | Ardnacrusha     | 110 kV | Hydro      |            | 21       |
|             | Ardnacrusha Hydro (2) | AA2     | Ardnacrusha     | 110 kV | Hydro      |            | 22       |
|             | Ardnacrusha Hydro (3) | AA3     | Ardnacrusha     | 110 kV | Hydro      |            | 19       |
|             | Ardnacrusha Hydro (4) | AA4     | Ardnacrusha     | 110 kV | Hydro      |            | 24       |
|             | Boolinrudda           |         | Ennis           | 110 kV | Wind       |            | 46       |
|             | Booltiagh             |         | Booltiagh       | 110 kV | Wind       |            | 19       |
|             | Booltiagh Ext.        |         | Booltiagh       | 110 kV | Wind       |            | 12       |
| Mid-West    | Knockalassa           |         | Ennis           | 110 kV | Wind       |            | 27       |
|             | Dromada (1)           |         | Dromada         | 110 kV | Wind       |            | 29       |
|             | Dromada (1a)          |         | Dromada         | 110 kV | Wind       |            | 18       |
|             | Kill Hill             |         | Kill Hill       | 110 kV | Wind       |            | 36       |
|             | Lisheen (1)           |         | Lisheen         | 110 kV | Wind       |            | 36       |
|             | Lisheen (1a)          |         | Lisheen         | 110 kV | Wind       |            | 19       |
|             | Moneypoint (1)        | MP1     | Moneypoint      | 400 kV | Coal       |            | 302      |
|             | Moneypoint (2)        | MP2     | Moneypoint      | 400 kV | Coal       |            | 305      |
|             | Moneypoint (3)        | MP3     | Moneypoint      | 400 kV | Coal       |            | 302      |
|             | Moneypoint Wind       |         | Moneypoint      | 110 kV | Wind       |            | 18       |
|             |                       |         | Mid-West Area   | Fotal  |            |            | 1427     |

|             | Generation        |         |                    |           |                        | Connection<br>Year (if | Maximum<br>Export<br>Capacity |
|-------------|-------------------|---------|--------------------|-----------|------------------------|------------------------|-------------------------------|
| Area        | Station           | Unit ID | Connected At       | Fue       | l Type                 | future)                | (MW)                          |
|             | Ballylumford B10  | B10     | Ballylumford       | 110 kV    | Gas                    |                        | 100                           |
|             | Ballylumford GT7  | BGT1    | Ballylumford       | 110 kV    | DO                     |                        | 58                            |
|             | Ballylumford GT8  | BGT2    | Ballylumford       | 110 kV    | DO                     |                        | 58                            |
|             | Ballylumford B20  | BGT20   | Ballylumford       | 275 kV    | Gas                    |                        | 500                           |
|             | Brockaghboy       |         | Brockaghboy        | 110 kV    | Wind                   |                        | 48                            |
|             | Castlereagh BES   |         | Castlereagh        | 110 kV    | Battery                | 2023                   | 50                            |
|             | Coolkeeragh GT8   | CGT8    | Coolkeeragh        | 110 kV    | Oil                    |                        | 53                            |
|             | Coolkeeragh GT    | C30 GT  | Coolkeeragh        | 275 kV    | Gas/DO                 |                        | 260                           |
|             | Coolkeeragh ST    | C30 GS  | Coolkeeragh        | 110 kV    | Gas/DO                 |                        | 170                           |
| Northern    | Kilroot OCGT6     |         | Kilroot            | 275 kV    | Gas                    | 2023                   | 458                           |
| Ireland     | Kilroot OCGT7     |         | Kilroot            | 275 kV    | Gas                    | 2023                   | 302                           |
|             | Kilroot ST1       | K1      | Kilroot            | 275 kV    | Coal/ <mark>Oil</mark> |                        | 195                           |
|             | Kilroot ST2       | K2      | Kilroot            | 275 kV    | Coal/ <mark>Oil</mark> |                        | 195                           |
|             | Kilroot GT1       | KGT1    | Kilroot            | 275 kV    | DO                     |                        | 29                            |
|             | Kilroot GT2       | KGT2    | Kilroot            | 275 kV    | DO                     |                        | 29                            |
|             | Kilroot GT3       | KGT3    | Kilroot            | 275 kV    | DO                     |                        | 42                            |
|             | Kilroot GT4       | KGT4    | Kilroot            | 275 kV    | DO                     |                        | 42                            |
|             | Slieve Kirk       | SLK     | Killymallaght      | 110 kV    | Wind                   |                        | 74                            |
|             | Tandragee BES     |         | Tandragee          | 110 kV    | Battery                | 2021                   | 50                            |
|             | Tamnamore BES     |         | Tamnamore          | 110 kV    | Battery                | 2021                   | 50                            |
|             |                   |         | Northern Ireland A | rea Total |                        |                        | 2763                          |
|             | Ballywater        |         | Ballywater         | 110 kV    | Wind                   |                        | 42                            |
|             | Castledockrell    |         | Castledockrell     | 110 kV    | Wind                   |                        | 42                            |
| South-East  | Great Island CCGT | GI4     | Great Island       | 220 kV    | Gas                    |                        | 439                           |
| JUULII-East | Knocknamona       |         | Dungarvan          | 110 kV    | Wind                   |                        | 34                            |
|             | Rosspile          |         | Rosspile           | 110 kV    | Solar                  | 2021                   | 95                            |
|             | Woodhouse         |         | Woodhouse          | 110 kV    | Wind                   |                        | 20                            |
|             |                   |         | South-East Area    | Total     |                        |                        | 672                           |
|             | Aghada            | AT1     | Aghada             | 220 kV    | Gas/DO                 |                        |                               |
|             | Aghada            | AT2     | Aghada             | 220 kV    | Gas/DO                 |                        |                               |
|             | Aghada            | AT4     | Aghada             | 220 kV    | Gas/DO                 |                        |                               |
|             | Athea             |         | Athea              | 110 kV    | Wind                   |                        |                               |
|             | Tobertoreen       |         | Athea              | 110 kV    | Wind                   | 2021                   |                               |
|             | Balinknockane     |         | Balinknockane      | 110 kV    | Solar                  | 2021                   |                               |
| South-West  | Barnadivane       |         | Barnadivine        | 110 kV    | Wind                   |                        |                               |
| South-west  | Boggeragh         |         | Boggeragh          | 110 kV    | Wind                   |                        |                               |
|             | Boggeragh (2)     |         | Boggeragh          | 110 kV    | Wind                   |                        |                               |
|             | Killavoy          |         | Boggeragh          | 110 kV    | Wind                   |                        |                               |
|             | Lee Hydro         | LE1     | Carrigadrohid      | 110 kV    | Hydro                  |                        |                               |
|             | Banemore          |         | Clahane            | 110 kV    | Solar                  | 2021                   |                               |
|             | Clahane           |         | Clahane            | 110 kV    | Wind                   |                        |                               |
|             | Clahane (2)       |         | Clahane            | 110 kV    | Wind                   | 2021                   |                               |

|            |                    |         |                 |        |        |            | Maximum  |
|------------|--------------------|---------|-----------------|--------|--------|------------|----------|
|            |                    |         |                 |        |        | Connection | Export   |
|            | Generation         |         |                 |        |        | Year (if   | Capacity |
| Area       | Station            | Unit ID | Connected At    | Fue    | l Type | future)    | (MW)     |
|            | Cloghboola         |         | Cloghboola      | 110 kV | Wind   | _          | 46       |
|            | Cloghboola         |         | Cloghboola      | 110 kV | Wind   |            | 46       |
|            | Coomagearlahy      |         | Coomagearlahy   | 110 kV | Wind   |            | 43       |
|            | Coomagearlahy ext. |         | Coomagearlahy   | 110 kV | Wind   |            | 39       |
|            | Coomataggart       |         | Coomataggart    | 110 kV | Wind   | _          | 114      |
|            | Grousemount        |         | Coomataggart    | 110 kV | Wind   |            | 114      |
|            | Cordal             |         | Cordal          | 110 kV | Wind   |            | 90       |
|            | Drombeg            |         | Drombeg         | 110 kV | Solar  | 2021       | 50       |
|            | Coomacheo          |         | Garrow          | 110 kV | Wind   |            | 41       |
| South-West | Coomacheo (2)      |         | Garrow          | 110 kV | Wind   |            | 18       |
| Julii-West | Whitegen CCGT      | WG      | Glanagow        | 220 kV | Gas/DO |            | 449      |
|            | Glanlee (1)        |         | Glanlee         | 110 kV | Wind   |            | 30       |
|            | Lee Hydro          | LE2     | Inniscarra      | 110 kV | Hydro  |            | 15       |
|            | Lee Hydro          | LE3     | Inniscarra      | 110 kV | Hydro  |            | 15       |
|            | Kelwin Power Plant |         | Kilpaddoge      | 110 kV | Hybrid | 2021       | 44       |
|            | Knockacummer       |         | Knockacummer    | 110 kV | Wind   |            | 105      |
|            | Aghada CCGT        | AD2     | Longpoint       | 220 kV | Gas    |            | 442      |
|            | Tarbert            | TB1     | Tarbert         | 110 kV | HFO    |            | 57       |
|            | Tarbert            | TB2     | Tarbert         | 110 kV | HFO    |            | 57       |
|            | Tarbert            | TB3     | Tarbert         | 220 kV | HFO    |            | 256      |
|            |                    |         | South-West Area | Total  |        |            | 3043     |
|            | Ardderoo           |         | Screeb          | 110 kV | Wind   | 2021       | 27       |
|            | Oweninney (1)      |         | Bellacorick     | 110 kV | Wind   |            | 89       |
|            | Oweninney (2)      |         | Bellacorick     | 110 kV | Wind   |            | 83       |
|            | Oweninney (3)      |         | Bellacorick     | 110 kV | Wind   | 2022       | 50       |
|            | Sheskin            |         | Bellacorick     | 110 kV | Wind   | 2021       | 17       |
|            | Buffy              |         | Buffy           | 110 kV | Wind   | 2021       | 91       |
|            | Carrigdangan       |         | Carrigdangan    | 110 kV | Wind   |            | 60       |
|            | Derrybrien         |         | Derrybrien      | 110 kV | Wind   |            | 60       |
|            | Knockalough        |         | Knockalough     | 110 kV | Wind   |            | 34       |
| West       | Seecon             |         | Knockranny      | 110 kV | Wind   |            | 108      |
| West       | West Offaly Power  | WO4     | Shannonbridge   | 110 kV | Peat   |            | 154      |
|            | Shantallow         |         | Shantallow      | 110 kV | Solar  | 2021       | 35       |
|            | Sliabh Bawn        |         | Sliabh Bawn     | 110 kV | Wind   |            | 58       |
|            | Tawnaghmore        | TP1     | Tawnaghmore     | 110 kV | DO     |            | 52       |
|            | Peaking Plant      |         |                 |        |        |            |          |
|            | Tawnaghmore        | TP2     | Tawnaghmore     | 110 kV | DO     |            | 52       |
|            | Peaking Plant      |         |                 |        |        |            |          |
|            | Tynagh             | TY1     | Tynagh          | 220 kV | Gas    |            | 268      |
|            | Tynagh             | TY2     | Tynagh          | 220 kV | Gas    |            | 142      |
|            | Ugool              |         | Ugool           | 110 kV | Wind   |            | 66       |

|                |                     |       | -     |       | Maximu | m Expor | t Capaci | ty (MEC) |       |       |       |
|----------------|---------------------|-------|-------|-------|--------|---------|----------|----------|-------|-------|-------|
| Area           | 110 kV Station      | 2020  | 2021  | 2022  | 2023   | 2024    | 2025     | 2026     | 2027  | 2028  | 2029  |
|                | Ardnagappary        | 22.9  | 22.9  | 22.9  | 22.9   | 22.9    | 22.9     | 22.9     | 22.9  | 22.9  | 22.9  |
|                | Binbane             | 61.3  | 102.0 | 102.0 | 102.0  | 102.0   | 108.0    | 108.0    | 108.0 | 108.0 | 108.0 |
|                | Cath_Fall           | 29.4  | 29.4  | 29.4  | 29.4   | 29.4    | 29.4     | 29.4     | 29.4  | 29.4  | 29.4  |
|                | Corderry            | 75.2  | 75.2  | 75.2  | 75.2   | 75.2    | 75.2     | 75.2     | 75.2  | 75.2  | 75.2  |
|                | Crane               | 7.5   | 15.5  | 15.5  | 15.5   | 15.5    | 15.5     | 15.5     | 15.5  | 15.5  | 15.5  |
|                | Drybridge           | 6.7   | 10.6  | 10.6  | 10.6   | 10.6    | 10.6     | 10.6     | 10.6  | 10.6  | 10.6  |
|                | Dundalk             | 0.5   | 15.5  | 15.5  | 15.5   | 15.5    | 15.5     | 15.5     | 15.5  | 15.5  | 15.5  |
|                | Garvagh             | 34.0  | 34.0  | 34.0  | 34.0   | 34.0    | 34.0     | 34.0     | 34.0  | 34.0  | 34.0  |
|                | Glenree             | 36.8  | 64.8  | 64.8  | 77.3   | 77.3    | 77.3     | 77.3     | 77.3  | 77.3  | 77.3  |
|                | Gortawee            | 3.0   | 3.0   | 3.0   | 3.0    | 3.0     | 3.0      | 3.0      | 3.0   | 3.0   | 3.0   |
| Border         | Letterkenny         | 51.1  | 85.5  | 85.5  | 85.5   | 85.5    | 85.5     | 85.5     | 85.5  | 85.5  | 85.5  |
|                | Lisdrum             | 49.2  | 49.2  | 49.2  | 49.2   | 49.2    | 49.2     | 49.2     | 49.2  | 49.2  | 49.2  |
|                | Meath Hill          | 43.0  | 74.6  | 74.6  | 107.6  | 107.6   | 107.6    | 107.6    | 107.6 | 107.6 | 107.6 |
|                | Моу                 | 6.5   | 6.5   | 6.5   | 6.5    | 6.5     | 6.5      | 6.5      | 6.5   | 6.5   | 6.5   |
|                | Mulreavy            | 33.1  | 33.1  | 33.1  | 33.1   | 33.1    | 33.1     | 33.1     | 33.1  | 33.1  | 33.1  |
|                | Shankill            | 25.7  | 29.7  | 29.7  | 29.7   | 29.7    | 29.7     | 29.7     | 29.7  | 29.7  | 29.7  |
|                | Sligo               | 13.7  | 13.7  | 13.7  | 13.7   | 13.7    | 13.7     | 13.7     | 13.7  | 13.7  | 13.7  |
|                | Somerset            | 19.5  | 19.5  | 19.5  | 19.5   | 19.5    | 19.5     | 19.5     | 19.5  | 19.5  | 19.5  |
|                | Sorne Hill          | 63.9  | 63.9  | 63.9  | 68.9   | 68.9    | 68.9     | 68.9     | 68.9  | 68.9  | 68.9  |
|                | Trien               | 88.8  | 88.8  | 88.8  | 88.8   | 88.8    | 88.8     | 88.8     | 88.8  | 88.8  | 88.8  |
|                | Trillick            | 44.7  | 44.7  | 44.7  | 44.7   | 44.7    | 44.7     | 44.7     | 44.7  | 44.7  | 44.7  |
|                | Border Area Total   | 716.4 | 882.0 | 882.0 | 932.5  | 932.5   | 938.5    | 938.5    | 938.5 | 938.5 | 938.5 |
|                | Glasmore            | 0.8   | 0.8   | 0.8   | 0.8    | 0.8     | 0.8      | 0.8      | 0.8   | 0.8   | 0.8   |
| Dublin         | Nangor              | 13.4  | 13.4  | 13.4  | 13.4   | 13.4    | 13.4     | 13.4     | 13.4  | 13.4  | 13.4  |
|                | Poppintree          | 4     | 4     | 4     | 4      | 4       | 4        | 4        | 4     | 4     | 4     |
|                | Dublin Area Total   | 18.2  | 18.2  | 18.2  | 18.2   | 18.2    | 18.2     | 18.2     | 18.2  | 18.2  | 18.2  |
|                | Arklow              | 79.7  | 85.7  | 85.7  | 85.7   | 85.7    | 85.7     | 85.7     | 85.7  | 85.7  | 85.7  |
|                | Dunfirth            | 0.0   | 4.0   | 4.0   | 4.0    | 4.0     | 4.0      | 4.0      | 4.0   | 4.0   | 4.0   |
| Mid-East       | Kilteel             | 0.0   | 15.0  | 15.0  | 15.0   | 15.0    | 15.0     | 15.0     | 15.0  | 15.0  | 15.0  |
|                | Monread             | 0.0   | 4.0   | 4.0   | 4.0    | 4.0     | 4.0      | 4.0      | 4.0   | 4.0   | 4.0   |
|                | Newbridge           | 0.0   | 4.0   | 4.0   | 4.0    | 4.0     | 4.0      | 4.0      | 4.0   | 4.0   | 4.0   |
|                | Mid-East Area Total | 79.7  | 112.7 | 112.7 | 112.7  | 112.7   | 112.7    | 112.7    | 112.7 | 112.7 | 112.7 |
|                | Blake               | 5.0   | 5.0   | 5.0   | 5.0    | 5.0     | 5.0      | 5.0      | 5.0   | 5.0   | 5.0   |
|                | Dallow              | 31.0  | 31.0  | 31.0  | 17.7   | 17.7    | 17.7     | 17.7     | 17.7  | 17.7  | 17.7  |
| Midlands       | Lanesboro           | 4.6   | 8.6   | 8.6   | 13.6   | 13.6    | 13.6     | 13.6     | 13.6  | 13.6  | 13.6  |
| - intertunites | Mullingar           | 0.0   | 4.0   | 4.0   | 8.0    | 8.0     | 8.0      | 8.0      | 8.0   | 8.0   | 8.0   |
|                | Navan               | 4.0   | 4.0   | 4.0   | 8.0    | 8.0     | 8.0      | 8.0      | 8.0   | 8.0   | 8.0   |
|                | Thornsberry         | 0.0   | 4.0   | 4.0   | 4.0    | 4.0     | 4.0      | 4.0      | 4.0   | 4.0   | 4.0   |
|                | Midlands Area Total | 44.6  | 56.6  | 56.6  | 56.2   | 56.2    | 56.2     | 56.2     | 56.2  | 56.2  | 56.2  |

# Table D-2: Existing and Committed Distribution-Connected Wind Farm Capacity

|                     |                                |        |        |        | Maximu | m Expor | t Capaci | ty (MEC) |        |        |        |
|---------------------|--------------------------------|--------|--------|--------|--------|---------|----------|----------|--------|--------|--------|
| Area                | 110 kV Station                 | 2020   | 2021   | 2022   | 2023   | 2024    | 2025     | 2026     | 2027   | 2028   | 2029   |
| Mid-West            | Ardnacrusha                    | 8.2    | 8.2    | 8.2    | 8.2    | 8.2     | 8.2      | 8.2      | 8.2    | 8.2    | 8.2    |
|                     | Ballydine                      | 0.0    | 28.0   | 28.0   | 28.0   | 28.0    | 28.0     | 28.0     | 28.0   | 28.0   | 28.0   |
|                     | Booltiagh                      | 96.0   | 109.4  | 109.4  | 109.4  | 109.4   | 109.4    | 109.4    | 109.4  | 109.4  | 109.4  |
|                     | Bunkimalta                     | 46.5   | 46.5   | 46.5   | 46.5   | 46.5    | 46.5     | 46.5     | 46.5   | 46.5   | 46.5   |
|                     | Cahir                          | 0.0    | 4.0    | 4.0    | 4.0    | 4.0     | 4.0      | 4.0      | 4.0    | 4.0    | 4.0    |
|                     | Cauteen                        | 178.1  | 182.1  | 182.1  | 182.1  | 182.1   | 182.1    | 182.1    | 182.1  | 182.1  | 182.1  |
|                     | Charleville                    | 84.7   | 84.7   | 84.7   | 84.7   | 84.7    | 84.7     | 84.7     | 84.7   | 84.7   | 84.7   |
|                     | Cureeny T                      | 94.0   | 94.0   | 94.0   | 94.0   | 94.0    | 94.0     | 94.0     | 94.0   | 94.0   | 94.0   |
|                     | Drumline                       | 0.0    | 4.0    | 4.0    | 4.0    | 4.0     | 4.0      | 4.0      | 4.0    | 4.0    | 4.0    |
|                     | Ikerrin                        | 36.0   | 36.0   | 36.0   | 36.0   | 36.0    | 36.0     | 36.0     | 36.0   | 36.0   | 36.0   |
|                     | Lisheen                        | 39.6   | 39.6   | 39.6   | 39.6   | 39.6    | 39.6     | 39.6     | 39.6   | 39.6   | 39.6   |
|                     | Nenagh                         | 14.0   | 14.0   | 14.0   | 14.0   | 14.0    | 14.0     | 14.0     | 14.0   | 14.0   | 14.0   |
|                     | Rathkeale                      | 30.0   | 30.0   | 30.0   | 30.0   | 30.0    | 30.0     | 30.0     | 30.0   | 30.0   | 30.0   |
|                     | Thurles                        | 41.8   | 41.8   | 41.8   | 41.8   | 41.8    | 41.8     | 41.8     | 41.8   | 41.8   | 41.8   |
|                     | Tipperary                      | 3.0    | 3.0    | 3.0    | 3.0    | 3.0     | 3.0      | 3.0      | 3.0    | 3.0    | 3.0    |
|                     | Tullabrack                     | 31.0   | 31.0   | 31.0   | 31.0   | 31.0    | 31.0     | 31.0     | 31.0   | 31.0   | 31.0   |
|                     | Mid-West Area Total            | 702.7  | 756.1  | 756.1  | 756.1  | 756.1   | 756.1    | 756.1    | 756.1  | 756.1  | 756.1  |
|                     | Aghyoule                       | 82.5   | 82.5   | 82.5   | 82.5   | 82.5    | 82.5     | 82.5     | 82.5   | 82.5   | 82.5   |
|                     | Agivey                         | 15.0   | 15.0   | 15.0   | 15.0   | 15.0    | 15.0     | 15.0     | 15.0   | 15.0   | 15.0   |
|                     | Antrim                         | 0.0    | 48.3   | 48.3   | 48.3   | 48.3    | 48.3     | 48.3     | 48.3   | 48.3   | 48.3   |
|                     | Ballymena                      | 56.3   | 56.3   | 56.3   | 56.3   | 56.3    | 56.3     | 56.3     | 56.3   | 56.3   | 56.3   |
|                     | Carnmoney                      | 13.8   | 13.8   | 13.8   | 13.8   | 13.8    | 13.8     | 13.8     | 13.8   | 13.8   | 13.8   |
|                     | Coleraine                      | 108.0  | 108.0  | 108.0  | 108.0  | 108.0   | 108.0    | 108.0    | 108.0  | 108.0  | 108.0  |
|                     | Coolkeeragh                    | 12.0   | 12.0   | 12.0   | 12.0   | 12.0    | 12.0     | 12.0     | 12.0   | 12.0   | 12.0   |
|                     | Creagh                         | 5.0    | 5.0    | 5.0    | 5.0    | 5.0     | 5.0      | 5.0      | 5.0    | 5.0    | 5.0    |
|                     | Drumnakelly                    | 2.6    | 2.6    | 2.6    | 2.6    | 2.6     | 2.6      | 2.6      | 2.6    | 2.6    | 2.6    |
|                     | Drumquin                       | 67.9   | 67.9   | 67.9   | 119.5  | 119.5   | 119.5    | 119.5    | 119.5  | 119.5  | 119.5  |
| Northern<br>Ireland | Dungannon                      | 17.5   | 17.5   | 17.5   | 17.5   | 17.5    | 17.5     | 17.5     | 17.5   | 17.5   | 17.5   |
|                     | Eden                           | 2.3    | 2.3    | 2.3    | 2.3    | 2.3     | 2.3      | 2.3      | 2.3    | 2.3    | 2.3    |
|                     | Enniskillen                    | 34.4   | 34.4   | 34.4   | 34.4   | 34.4    | 34.4     | 34.4     | 34.4   | 34.4   | 34.4   |
|                     | Gort                           | 67.5   | 67.5   | 90.0   | 90.0   | 90.0    | 90.0     | 90.0     | 90.0   | 90.0   | 90.0   |
|                     | Kells                          | 0.0    | 0.0    | 75.0   | 75.0   | 75.0    | 75.0     | 75.0     | 75.0   | 75.0   | 75.0   |
|                     | Killymallaght                  | 35.7   | 35.7   | 35.7   | 35.7   | 35.7    | 35.7     | 35.7     | 35.7   | 35.7   | 35.7   |
|                     | Larne                          | 20.0   | 20.0   | 20.0   | 20.0   | 20.0    | 20.0     | 20.0     | 20.0   | 20.0   | 20.0   |
|                     | Limavady                       | 37.7   | 37.7   | 37.7   | 37.7   | 37.7    | 37.7     | 37.7     | 37.7   | 37.7   | 37.7   |
|                     | Lismore                        | 17.5   | 17.5   | 17.5   | 17.5   | 17.5    | 17.5     | 17.5     | 17.5   | 17.5   | 17.5   |
|                     | Loguestown                     | 9.2    | 9.2    | 9.2    | 9.2    | 9.2     | 9.2      | 9.2      | 9.2    | 9.2    | 9.2    |
|                     | Magherakeel                    | 208.6  | 208.6  | 208.6  | 208.6  | 208.6   | 208.6    | 208.6    | 208.6  | 208.6  | 208.6  |
|                     | Newry                          | 23.0   | 23.0   | 23.0   | 23.0   | 23.0    | 23.0     | 23.0     | 23.0   | 23.0   | 23.0   |
|                     | Omagh                          | 140.2  | 140.2  | 140.2  | 140.2  | 140.2   | 140.2    | 140.2    | 140.2  | 140.2  | 140.2  |
|                     | Rasharkin                      | 54.8   | 54.8   | 54.8   | 54.8   | 54.8    | 54.8     | 54.8     | 54.8   | 54.8   | 54.8   |
|                     | Strabane                       | 28.5   | 28.5   | 28.5   | 28.5   | 28.5    | 28.5     | 28.5     | 28.5   | 28.5   | 28.5   |
|                     | Tremogue                       | 68.3   | 68.3   | 68.3   | 68.3   | 68.3    | 68.3     | 68.3     | 68.3   | 68.3   | 68.3   |
|                     | Northern Ireland<br>Area Total | 1128.3 | 1176.6 | 1274.1 | 1325.7 | 1325.7  | 1325.7   | 1325.7   | 1325.7 | 1325.7 | 1325.7 |

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| Table D-2: Existing and Committed Distribution-Connected Wind Farm Capacity |
|---|
|---|

|            |                       | Maximum Export Capacity (MEC) |       |       |       |       |       |       |       |       |       |
|------------|-----------------------|-------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Area       | 110 kV Station        | 2020                          | 2021  | 2022  | 2023  | 2024  | 2025  | 2026  | 2027  | 2028  | 2029  |
| South-East | Banoge                | 0.0                           | 0.0   | 0.0   | 9.0   | 9.0   | 9.0   | 9.0   | 9.0   | 9.0   | 9.0   |
|            | Barrymore             | 32.4                          | 32.4  | 32.4  | 32.4  | 32.4  | 32.4  | 32.4  | 32.4  | 32.4  | 32.4  |
|            | Butlerstown           | 1.7                           | 5.7   | 5.7   | 5.7   | 5.7   | 5.7   | 5.7   | 5.7   | 5.7   | 5.7   |
|            | Carlow                | 39.4                          | 39.4  | 39.4  | 39.4  | 39.4  | 39.4  | 39.4  | 39.4  | 39.4  | 39.4  |
|            | Doon                  | 0.0                           | 21.0  | 21.0  | 21.0  | 21.0  | 21.0  | 21.0  | 21.0  | 21.0  | 21.0  |
|            | Dungarvan             | 9.2                           | 9.2   | 9.2   | 9.2   | 9.2   | 9.2   | 9.2   | 9.2   | 9.2   | 9.2   |
|            | Great Island          | 0.0                           | 12.0  | 12.0  | 12.0  | 12.0  | 12.0  | 12.0  | 12.0  | 12.0  | 12.0  |
|            | Lodgewood             | 60.1                          | 64.1  | 64.1  | 64.1  | 64.1  | 64.1  | 64.1  | 64.1  | 64.1  | 64.1  |
|            | Portlaoise            | 54.2                          | 54.2  | 54.2  | 58.2  | 58.2  | 58.2  | 58.2  | 58.2  | 58.2  | 58.2  |
|            | Waterford             | 18.3                          | 22.2  | 22.2  | 22.2  | 22.2  | 22.2  | 22.2  | 22.2  | 22.2  | 22.2  |
|            | Wexford               | 38.9                          | 42.9  | 42.9  | 42.9  | 42.9  | 42.9  | 42.9  | 42.9  | 42.9  | 42.9  |
|            | South-East Area Total | 254.1                         | 303.0 | 303.0 | 316.0 | 316.0 | 316.0 | 316.0 | 316.0 | 316.0 | 316.0 |
| South-West | Athea                 | 3.6                           | 41.5  | 41.5  | 41.5  | 41.5  | 41.5  | 41.5  | 41.5  | 41.5  | 41.5  |
|            | Ballylickey           | 54.0                          | 54.0  | 54.0  | 54.0  | 54.0  | 54.0  | 54.0  | 54.0  | 54.0  | 54.0  |
|            | Bandon                | 26.6                          | 32.6  | 32.6  | 32.6  | 32.6  | 32.6  | 32.6  | 32.6  | 32.6  | 32.6  |
|            | Boggeragh             | 20.0                          | 31.9  | 31.9  | 44.0  | 44.0  | 44.0  | 44.0  | 44.0  | 44.0  | 44.0  |
|            | Castleview            | 2.0                           | 2.0   | 2.0   | 2.0   | 2.0   | 2.0   | 2.0   | 2.0   | 2.0   | 2.0   |
|            | Cloghboola            | 54.5                          | 54.5  | 54.5  | 54.5  | 54.5  | 54.5  | 54.5  | 54.5  | 54.5  | 54.5  |
|            | Coomataggart          | 64.2                          | 64.2  | 64.2  | 64.2  | 64.2  | 64.2  | 64.2  | 64.2  | 64.2  | 64.2  |
|            | Cordal                | 75.8                          | 75.8  | 75.8  | 75.8  | 75.8  | 75.8  | 75.8  | 75.8  | 75.8  | 75.8  |
|            | Dunmanway             | 45.4                          | 65.4  | 65.4  | 65.4  | 65.4  | 65.4  | 65.4  | 65.4  | 65.4  | 65.4  |
|            | Garrow                | 15.0                          | 15.0  | 15.0  | 15.0  | 15.0  | 15.0  | 15.0  | 15.0  | 15.0  | 15.0  |
|            | Glenlara              | 53.0                          | 53.0  | 53.0  | 53.0  | 53.0  | 53.0  | 53.0  | 53.0  | 53.0  | 53.0  |
|            | Kilbarry              | 0.8                           | 5.8   | 5.8   | 5.8   | 5.8   | 5.8   | 5.8   | 5.8   | 5.8   | 5.8   |
|            | Kilpaddoge            | 18.0                          | 18.0  | 18.0  | 18.0  | 18.0  | 18.0  | 18.0  | 18.0  | 18.0  | 18.0  |
|            | Knockeragh            | 15.1                          | 15.1  | 15.1  | 15.1  | 15.1  | 15.1  | 15.1  | 15.1  | 15.1  | 15.1  |
|            | Limerick              | 0.0                           | 4.0   | 4.0   | 4.0   | 4.0   | 4.0   | 4.0   | 4.0   | 4.0   | 4.0   |
|            | Macroom               | 34.1                          | 34.1  | 34.1  | 34.1  | 34.1  | 34.1  | 34.1  | 34.1  | 34.1  | 34.1  |
|            | Mallow                | 0.0                           | 9.0   | 9.0   | 9.0   | 9.0   | 9.0   | 9.0   | 9.0   | 9.0   | 9.0   |
|            | Midleton              | 1.6                           | 5.6   | 5.6   | 5.6   | 5.6   | 5.6   | 5.6   | 5.6   | 5.6   | 5.6   |
|            | Oughtragh             | 9.0                           | 13.0  | 13.0  | 13.0  | 13.0  | 13.0  | 13.0  | 13.0  | 13.0  | 13.0  |
|            | Reamore               | 57.9                          | 71.4  | 96.7  | 96.7  | 96.7  | 96.7  | 96.7  | 96.7  | 96.7  | 96.7  |
|            | Trabeg                | 0.0                           | 0.0   | 5.0   | 5.0   | 5.0   | 5.0   | 5.0   | 5.0   | 5.0   | 5.0   |
|            | Tralee                | 47.6                          | 51.6  | 51.6  | 51.6  | 51.6  | 51.6  | 51.6  | 51.6  | 51.6  | 51.6  |
|            | South-West Area Total | 598.1                         | 717.2 | 747-4 | 759.5 | 759.5 | 759.5 | 759.5 | 759.5 | 759.5 | 759.5 |

|      |                    | Maximum Export Capacity (MEC) |       |       |       |       |       |       |       |       |       |  |
|------|--------------------|-------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--|
| Area | 110 kV Station     | 2020                          | 2021  | 2022  | 2023  | 2024  | 2025  | 2026  | 2027  | 2028  | 2029  |  |
|      | Arigna             | 15.6                          | 15.6  | 15.6  | 15.6  | 15.6  | 15.6  | 15.6  | 15.6  | 15.6  | 15.6  |  |
|      | Bellacorick        | 9.0                           | 9.0   | 68.2  | 68.2  | 68.2  | 68.2  | 68.2  | 68.2  | 68.2  | 68.2  |  |
|      | Carrick on Shannon | 0.0                           | 8.3   | 8.3   | 8.3   | 8.3   | 8.3   | 8.3   | 8.3   | 8.3   | 8.3   |  |
|      | Castlebar          | 46.0                          | 46.0  | 46.0  | 46.0  | 46.0  | 46.0  | 46.0  | 46.0  | 46.0  | 46.0  |  |
| West | Cloon              | 4.3                           | 8.3   | 8.3   | 8.3   | 8.3   | 8.3   | 8.3   | 8.3   | 8.3   | 8.3   |  |
| west | Dalton             | 43.4                          | 43.4  | 43.4  | 43.4  | 43.4  | 43.4  | 43.4  | 43.4  | 43.4  | 43.4  |  |
|      | Salthill           | 46.1                          | 46.1  | 46.1  | 46.1  | 46.1  | 46.1  | 46.1  | 46.1  | 46.1  | 46.1  |  |
|      | Screeb             | 3.0                           | 3.0   | 3.0   | 3.0   | 3.0   | 3.0   | 3.0   | 3.0   | 3.0   | 3.0   |  |
|      | Tawnaghmore        | 19.2                          | 19.2  | 19.2  | 19.2  | 19.2  | 19.2  | 19.2  | 19.2  | 19.2  | 19.2  |  |
|      | Tonroe             | 12.5                          | 14.0  | 14.0  | 14.0  | 14.0  | 14.0  | 14.0  | 14.0  | 14.0  | 14.0  |  |
|      | West Area Total    | 199.1                         | 212.8 | 272.0 | 272.0 | 272.0 | 272.0 | 272.0 | 272.0 | 272.0 | 272.0 |  |

# Table D-2: Existing and Committed Distribution-Connected Wind Farm Capacity

# Table D-3: Existing and Committed Distribution-Connected Generation (excluding wind)

|        |                         |              |       |       | l        | Maximur | m Export | Capacit | ty (MEC) |          |       |          |
|--------|-------------------------|--------------|-------|-------|----------|---------|----------|---------|----------|----------|-------|----------|
| Area   | 110 kV Station          | Туре         | 2020  | 2021  | 2022     | 2023    | 2024     | 2025    | 2026     | 2027     | 2028  | 2029     |
|        | Binbane                 | Hydro        | 4.3   | 4.3   | 4.3      | 4.3     | 4.3      | 4.3     | 4.3      | 4.3      | 4.3   | 4.3      |
|        | Crane                   | Battery      | -     | -     | -        | -       | 16       | 16      | 16       | 16       | 16    | 16       |
|        | Crane                   | PV           | -     | -     | -        | -       | 4        | 4       | 4        | 4        | 4     | 4        |
|        | Crane                   | PV           | -     | -     | -        | -       | 4        | 4       | 4        | 4        | 4     | 4        |
|        | Drybridge               | LFG          | 1.274 | 1.274 | 1.274    | 1.274   | 1.274    | 1.274   | 1.274    | 1.274    | 1.274 | 1.274    |
|        | Drybridge               | Biogas       | 3     | 3     | 3        | 3       | 3        | 3       | 3        | 3        | 3     | 3        |
|        | Drybridge               | Solar        | -     | 4     | 4        | 4       | 4        | 4       | 4        | 4        | 4     | 4        |
| Border | Drybridge               | Conventional | 20    | 20    | 20       | 20      | 20       | 20      | 20       | 20       | 20    | 20       |
|        | Drybridge               | LFG          | 3.525 | 3.525 | 3.525    | 3.525   | 3.525    | 3.525   | 3.525    | 3.525    | 3.525 | 3.525    |
|        | Drybridge               | LFG          | 1.43  | 1.43  | 1.43     | 1.43    | 1.43     | 1.43    | 1.43     | 1.43     | 1.43  | 1.43     |
|        | Meath Hill              | СНР          | 1     | 1     | 1        | 1       | 1        | 1       | 1        | 1        | 1     | 1        |
|        | Shankill                | LFG          | 0.7   | 0.7   | 0.7      | 0.7     | 0.7      | 0.7     | 0.7      | 0.7      | 0.7   | 0.7      |
|        | Somerset                | Solar        | 4     | 4     | 4        | 4       | 4        | 4       | 4        | 4        | 4     | 4        |
|        | Trien                   | Solar        | -     | -     | -        | -       | 4        | 4       | 4        | 4        | 4     | 4        |
|        | Border Total Are        | a            | 39.2  | 43.2  | 43.2     | 43.2    | 71.2     | 71.2    | 71.2     | 71.2     | 71.2  | 71.2     |
|        | Blackrock               | СНР          | 0.22  | 0.22  | 0.22     | 0.22    | 0.22     | 0.22    | 0.22     | 0.22     | 0.22  | 0.22     |
|        | Blackrock               | СНР          | 0.33  | 0.33  | 0.33     | 0.33    | 0.33     | 0.33    | 0.33     | 0.33     | 0.33  | 0.33     |
|        | Fin_rural               | СНР          | 1.6   | 1.6   | 1.6      | 1.6     | 1.6      | 1.6     | 1.6      | 1.6      | 1.6   | 1.6      |
|        | <br>Finglas             | Solar        | 3.96  | 3.96  | 3.96     | 3.96    | 3.96     | 3.96    | 3.96     | 3.96     | 3.96  | 3.96     |
| Dublin | Finglas                 | Solar        | 3.96  | 3.96  | 3.96     | 3.96    | 3.96     | 3.96    | 3.96     | 3.96     | 3.96  | 3.96     |
|        | Glasmore                | СНР          | 1.7   | 1.7   | 1.7      | 1.7     | 1.7      | 1.7     | 1.7      | 1.7      | 1.7   | 1.7      |
|        | Ringsend                | Diesel       | 2.5   | 2.5   | 2.5      | 2.5     | 2.5      | 2.5     | 2.5      | 2.5      | 2.5   | 2.5      |
|        | Ringsend                | Waste to     | 72    | 72    | 72       | 72      | 72       | 72      | 72       | 72       | 72    | 72       |
|        | 5                       | Energy       | ,     | ,<br> | <b>`</b> | ,       | ĺ        | ,<br>   | ĺ        | <u> </u> | ,<br> | <u> </u> |
|        | Dublin Total Are        | a            | 86.3  | 86.3  | 86.3     | 86.3    | 86.3     | 86.3    | 86.3     | 86.3     | 86.3  | 86.3     |
|        | Arklow                  | Biomass      | 1     | 1     | 1        | 1       | 1        | 1       | 1        | 1        | 1     | 1        |
|        | Arklow                  | Solar        | 1     | 1     | 1        | 1       | 1        | 1       | 1        | 1        | 1     | 1        |
|        | Arklow                  | Solar        | -     | 4     | 4        | 4       | 4        | 4       | 4        | 4        | 4     | 4        |
| Mid-   | Baltrasna               | Solar        | -     | 10    | 10       | 10      | 10       | 10      | 10       | 10       | 10    | 10       |
| East   | Griffinrath             | Hydro        | 4     | 4     | 4        | 4       | 4        | 4       | 4        | 4        | 4     | 4        |
|        | Griffinrath             | Solar        | -     | 4     | 4        | 4       | 4        | 4       | 4        | 4        | 4     | 4        |
|        | Kilteel                 | LFG          | 9.77  | 9.77  | 9.77     | 9.77    | 9.77     | 9.77    | 9.77     | 9.77     | 9.77  | 9.77     |
|        | Stratford               | Solar        | -     | -     | -        | 4       | 4        | 4       | 4        | 4        | 4     | 4        |
|        | Mid-East Total A        | Area         | 15.8  | 33.8  | 33.8     | 37.8    | 37.8     | 37.8    | 37.8     | 37.8     | 37.8  | 37.8     |
|        | Athlone                 | Solar        | -     | -     | -        | -       | -        | 4       | 4        | 4        | 4     | 4        |
|        | Athlone                 | LFG          | 0.75  | 0.75  | 0.75     | 0.75    | 0.75     | 0.75    | 0.75     | 0.75     | 0.75  | 0.75     |
|        | Mullingar               | Solar        | 4     | 4     | 4        | 4       | 4        | 4       | 4        | 4        | 4     | 4        |
|        | Navan                   | Solar        | -     | -     | -        | -       | -        | 4       | 4        | 4        | 4     | 4        |
| Mid-   | Navan                   | Solar        | -     | 4.999 | 4.999    | 4.999   | 4.999    | 4.999   | 4.999    | 4.999    | 4.999 | 4.999    |
| lands  | Navan                   | СНР          | 13    | 13    | 13       | 13      | 13       | 13      | 13       | 13       | 13    | 13       |
|        | Richmond                | Solar        | -     | 4     | 4        | 4       | 4        | 4       | 4        | 4        | 4     | 4        |
|        |                         | CUD          | -     | -     | -        | -       | 5        | 5       | 5        | 5        | 5     | 5        |
|        | Richmond                | СНР          | -     |       |          |         |          |         | -        |          | -     | -        |
|        | Richmond<br>Thornsberry | СНР          | -     | 10    | 10       | 10      | 10       | 10      | 10       | 10       | 10    | 10       |
|        |                         |              |       | 10    | 10       | 10      |          |         |          |          |       |          |

# Table D-3: Existing and Committed Distribution-Connected Generation (excluding wind)

|                |  |   |  |  | I  | Maximu   | m Export  | Capacit   | y (MEC)  |   |  |   |
|----------------|--|---|--|--|--|--|---|---|--|---|--|---|
| Area           | 110 kV Station   | Туре  | 2020   | 2021   | 2022   | 2023   | 2024  | 2025  | 2026   | 2027  | 2028   | 2029  |
|                | Ballydine  | Biogas  | 0.44   | 0.44   | 0.44   | 0.44   | 0.44  | 0.44  | 0.44   | 0.44  | 0.44   | 0.44  |
|                | Cahir  | Solar   | 8  | 8  | 8  | 8  | 8   | 8   | 8  | 8   | 8  | 8   |
|                | Cahir  | Solar   | -  | 4  | 4  | 4  | 4   | 4   | 4  | 4   | 4  | 4   |
|                | Drumline   | Solar   | -  | -  | -  | -  | 8   | 8   | 8  | 8   | 8  | 8   |
| Mid-<br>West   | Rathkeale  | CHP   | 6.5  | 6.5  | 6.5  | 6.5  | 6.5   | 6.5   | 6.5  | 6.5   | 6.5  | 6.5   |
| west           | Rathkeale  | LFG   | 3.2  | 3.2  | 3.2  | 3.2  | 3.2   | 3.2   | 3.2  | 3.2   | 3.2  | 3.2   |
|                | Rathkeale  | Biogas  | 3.2  | 3.2  | 3.2  | 3.2  | 3.2   | 3.2   | 3.2  | 3.2   | 3.2  | 3.2   |
|                | Thurles  | Solar   | -  | -  | -  | -  | 4   | 4   | 4  | 4   | 4  | 4   |
|                | Tullabrack   | Wave  | 5.4  | 5.4  | 5.4  | 5.4  | 5.4   | 5.4   | 5.4  | 5.4   | 5.4  | 5.4   |
|                | Mid-West Total   | Area  | 26.7   | 30.7   | 30.7   | 30.7   | 42.7  | 42.7  | 42.7   | 42.7  | 42.7   | 42.7  |
|                | Antrim   | Solar   | 29.8   | 29.8   | 29.8   | 29.8   | 29.8  | 29.8  | 29.8   | 29.8  | 29.8   | 29.8  |
|                | Ballymena  | Solar   | 6  | 6  | 6  | 6  | 6   | 6   | 6  | 6   | 6  | 6   |
|                | Coolkeeragh  | Biomass   | 17.6   | 17.6   | 17.6   | 17.6   | 17.6  | 17.6  | 17.6   | 17.6  | 17.6   | 17.6  |
|                | Dungannon  | Solar   | -  | 4  | 4  | 4  | 4   | 4   | 4  | 4   | 4  | 4   |
|                | Glengormley  | Solar   | 2.3  | 2.3  | 2.3  | 2.3  | 2.3   | 2.3   | 2.3  | 2.3   | 2.3  | 2.3   |
| Northern       | Kells  | Battery   | -  | -  | -  | 50   | 50  | 50  | 50   | 50  | 50   | 50  |
| Ireland        | Lisburn  | Solar   | 58.9   | 58.9   | 58.9   | 58.9   | 58.9  | 58.9  | 58.9   | 58.9  | 58.9   | 58.9  |
|                | Newtownards  | Solar   | 5  | 5  | 5  | 5  | 5   | 5   | 5  | 5   | 5  | 5   |
|                | Rasharkin  | Solar   | 35   | 35   | 35   | 35   | 35  | 35  | 35   | 35  | 35   | 35  |
|                | Rosebank   | Biomass   | 10   | 10   | 10   | 10   | 10  | 10  | 10   | 10  | 10   | 10  |
|                | Tremogue   | Solar   | 5  | 5  | 5  | 5  | 5   | 5   | 5  | 5   | 5  | 5   |
|                | Waringstown  | Solar   | 9  | 9  | 9  | 9  | 9   | 9   | 9  | 9   | 9  | 9   |
|                | -  |   | -  | -  | 9  | -  | -   | -   | -  | 9   | 9  | -   |
|                | Northern Ireland   | Total Area  | -  | 182.6  | 182.6  | 232.6  | 232.6   | 232.6   | 232.6  | 232.6   | 232.6  | 232.6   |
|                | Athy   | Total Area<br>Solar   | -  |  |  | 232.6<br>4.99  | <b>232.6</b><br>4.99  | 232.6<br>4.99   | <b>232.6</b><br>4.99   | 232.6<br>4.99   | <b>232.6</b><br>4.99   | 232.6<br>4.99   |
|                | Athy<br>Athy   | Solar<br>Battery  | 178.6  | 182.6  | 182.6  | 232.6<br>4.99<br>8   | 232.6   | 232.6<br>4.99<br>8  | 232.6  | 232.6   | 232.6  | 232.6   |
|                | Athy   | Solar<br>Battery<br>Solar   | 178.6  | <b>182.6</b><br>4.99   | <b>182.6</b><br>4.99<br>4<br>4   | 232.6<br>4.99<br>8<br>8  | 232.6<br>4.99<br>8<br>8   | 232.6<br>4.99<br>8<br>8   | 232.6<br>4.99<br>8<br>8  | 232.6<br>4.99<br>8<br>8   | 232.6<br>4.99<br>8<br>8  | 232.6<br>4.99   |
|                | Athy<br>Athy<br>Athy<br>Ballybeg   | Solar<br>Battery<br>Solar<br>Solar  | 178.6<br>-   | <b>182.6</b><br>4.99<br>4  | <b>182.6</b><br>4.99<br>4  | 232.6<br>4.99<br>8   | 232.6<br>4.99<br>8  | 232.6<br>4.99<br>8  | 232.6<br>4.99<br>8   | 232.6<br>4.99<br>8  | 232.6<br>4.99<br>8   | 232.6<br>4.99<br>8  |
|                | Athy<br>Athy<br>Athy<br>Ballybeg<br>Ballybeg   | Solar<br>Battery<br>Solar<br>Solar<br>LFG   | 178.6<br>-<br>-  | <b>182.6</b><br>4.99<br>4  | <b>182.6</b><br>4.99<br>4<br>4   | 232.6<br>4.99<br>8<br>8  | 232.6<br>4.99<br>8<br>8   | 232.6<br>4.99<br>8<br>8   | 232.6<br>4.99<br>8<br>8  | 232.6<br>4.99<br>8<br>8   | 232.6<br>4.99<br>8<br>8  | 232.6<br>4.99<br>8<br>8   |
|                | Athy<br>Athy<br>Athy<br>Ballybeg<br>Ballybeg<br>Ballybeg   | Solar<br>Battery<br>Solar<br>Solar<br>LFG<br>LFG  | 178.6<br>-<br>-<br>-   | 182.6         4.99         4         4         -   | 182.6         4.99         4         4         8   | 232.6<br>4.99<br>8<br>8<br>8<br>8  | 232.6<br>4.99<br>8<br>8<br>8<br>8   | 232.6<br>4.99<br>8<br>8<br>8<br>8   | 232.6<br>4.99<br>8<br>8<br>8<br>8  | 232.6<br>4.99<br>8<br>8<br>8<br>8   | 232.6<br>4.99<br>8<br>8<br>8<br>8  | 232.6<br>4.99<br>8<br>8<br>8<br>8   |
|                | Athy<br>Athy<br>Athy<br>Ballybeg<br>Ballybeg<br>Ballybeg<br>Banoge   | Solar<br>Battery<br>Solar<br>Solar<br>LFG<br>LFG<br>Solar   | 178.6<br>-<br>-<br>-<br>0.75<br>3.51<br>-  | 182.6         4.99         4         -         0.75         3.51         4   | 182.6         4.99         4         8         0.75         3.51         4   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4  | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4  | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4  | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4  |
|                | Athy<br>Athy<br>Athy<br>Ballybeg<br>Ballybeg<br>Ballybeg<br>Banoge<br>Barrymore  | Solar<br>Battery<br>Solar<br>Solar<br>LFG<br>LFG<br>Solar<br>CHP  | 178.6<br>-<br>-<br>-<br>-<br>0.75  | 182.6         4.99         4         -         0.75         3.51   | 182.6         4.99         4         8         0.75         3.51   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51  | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51  | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51  | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51   |
|                | Athy<br>Athy<br>Athy<br>Ballybeg<br>Ballybeg<br>Ballybeg<br>Banoge<br>Barrymore<br>Barrymore   | Solar<br>Battery<br>Solar<br>Solar<br>LFG<br>Solar<br>CHP<br>Solar  | 178.6<br>-<br>-<br>-<br>0.75<br>3.51<br>-<br>4.8<br>-  | 182.6         4.99         4         -         0.75         3.51         4   | 182.6         4.99         4         8         0.75         3.51         4         4.8         -   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4  | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4  | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4  | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4  |
| South-         | Athy<br>Athy<br>Athy<br>Ballybeg<br>Ballybeg<br>Ballybeg<br>Banoge<br>Barrymore<br>Barrymore<br>Doon   | Solar<br>Battery<br>Solar<br>LFG<br>LFG<br>Solar<br>CHP<br>Solar<br>Hydro   | 178.6<br>-<br>-<br>-<br>0.75<br>3.51<br>-<br>4.8<br>-<br>1   | 182.6         4.99         4         -         0.75         3.51         4         4.8         -         1   | 182.6         4.99         4         8         0.75         3.51         4         4.8         -         1   | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1  | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1  | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1   | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1   | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1   |
| South-<br>East | Athy<br>Athy<br>Athy<br>Ballybeg<br>Ballybeg<br>Ballybeg<br>Banoge<br>Barrymore<br>Barrymore<br>Doon<br>Doon   | Solar<br>Battery<br>Solar<br>LFG<br>LFG<br>Solar<br>CHP<br>Solar<br>Hydro<br>Solar  | 178.6<br>-<br>-<br>-<br>0.75<br>3.51<br>-<br>4.8<br>-  | 182.6         4.99         4         -         0.75         3.51         4         4.8         -   | 182.6         4.99         4         8         0.75         3.51         4         4.8         -   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17                                       | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17  | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95  | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17  | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95  | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95   |
|                | Athy<br>Athy<br>Athy<br>Ballybeg<br>Ballybeg<br>Ballybeg<br>Banoge<br>Barrymore<br>Barrymore<br>Doon<br>Doon<br>Great Island                           | Solar<br>Battery<br>Solar<br>LFG<br>LFG<br>Solar<br>CHP<br>Solar<br>Hydro<br>Solar<br>Solar   | 178.6<br>-<br>-<br>-<br>0.75<br>3.51<br>-<br>4.8<br>-<br>1   | 182.6         4.99         4         -         0.75         3.51         4         4.8         -         1   | 182.6         4.99         4         8         0.75         3.51         4         4.8         -         1   | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1  | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1  | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1   | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1   | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1   | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1   |
|                | Athy<br>Athy<br>Athy<br>Ballybeg<br>Ballybeg<br>Ballybeg<br>Banoge<br>Barrymore<br>Barrymore<br>Doon<br>Doon<br>Great Island<br>Kilkenny               | Solar<br>Battery<br>Solar<br>LFG<br>Solar<br>CHP<br>Solar<br>Hydro<br>Solar<br>Solar<br>CHP   | 178.6<br>-<br>-<br>-<br>0.75<br>3.51<br>-<br>4.8<br>-<br>1<br>-<br>7.5   | 182.6         4.99         4         -         0.75         3.51         4         4.8         -         1         17         4.99         7.5   | 182.6         4.99         4         8         0.75         3.51         4         4.8         -         1         17         4.99         7.5   | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5                             | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5                                       | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5                                      | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5                                       | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5                                      | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5                                  | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5                                  |
|                | Athy<br>Athy<br>Athy<br>Ballybeg<br>Ballybeg<br>Ballybeg<br>Banoge<br>Barrymore<br>Barrymore<br>Doon<br>Doon<br>Great Island<br>Kilkenny<br>Kilkenny   | Solar<br>Battery<br>Solar<br>LFG<br>LFG<br>Solar<br>CHP<br>Solar<br>Hydro<br>Solar<br>Solar<br>CHP<br>Biogas  | 178.6<br>-<br>-<br>-<br>0.75<br>3.51<br>-<br>4.8<br>-<br>1<br>-<br>7.5<br>7.5  | 182.6         4.99         4         -         0.75         3.51         4         4.8         -         1         17         4.99         7.5         7.5   | 182.6         4.99         4         8         0.75         3.51         4         4.8         -         1         17         4.99         7.5         7.5   | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5                      | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5                                | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5                               | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5                           | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5                               | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5                           | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5                           |
|                | Athy<br>Athy<br>Athy<br>Ballybeg<br>Ballybeg<br>Ballybeg<br>Ballybeg<br>Barrymore<br>Barrymore<br>Doon<br>Doon<br>Great Island<br>Kilkenny<br>Kilkenny | Solar<br>Battery<br>Solar<br>LFG<br>Solar<br>CHP<br>Solar<br>Hydro<br>Solar<br>Solar<br>CHP<br>Biogas   | 178.6<br>-<br>-<br>-<br>0.75<br>3.51<br>-<br>4.8<br>-<br>1<br>-<br>7.5<br>7.5<br>4   | 182.6         4.99         4         -         0.75         3.51         4         4.8         -         1         17         4.99         7.5         7.5         4   | 182.6         4.99         4         8         0.75         3.51         4         4.8         -         1         17         4.99         7.5         7.5         4   | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4                 | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4                           | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4                          | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4                      | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4                          | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4                      | 232.6<br>4.99<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4                           |
|                | AthyAthyAthyBallybegBallybegBallybegBanogeBarrymoreBarrymoreDoonDoonGreat IslandKilkennyKilkennyKilkennyPortlaoise                                     | Solar<br>Battery<br>Solar<br>LFG<br>LFG<br>Solar<br>CHP<br>Solar<br>Hydro<br>Solar<br>Solar<br>CHP<br>Biogas<br>Solar<br>Biogas                                     | 178.6<br>-<br>-<br>-<br>0.75<br>3.51<br>-<br>4.8<br>-<br>1<br>-<br>7.5<br>7.5<br>4<br>1<br>1   | 182.6         4.99         4         -         0.75         3.51         4         4.8         -         1         17         4.99         7.5         7.5   | 182.6         4.99         4         8         0.75         3.51         4         4.8         -         1         17         4.99         7.5         7.5         4         1   | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1            | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5                                | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1                     | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1                 | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1                     | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1                 | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1                 |
|                | AthyAthyAthyAthyBallybegBallybegBallybegBanogeBarrymoreBarrymoreDoonDoonGreat IslandKilkennyKilkennyKilkennyPortlaoisePortlaoise                       | Solar<br>Battery<br>Solar<br>LFG<br>Solar<br>CHP<br>Solar<br>Hydro<br>Solar<br>Solar<br>CHP<br>Biogas<br>Solar<br>Biogas  | 178.6<br>-<br>-<br>-<br>0.75<br>3.51<br>-<br>4.8<br>-<br>1<br>-<br>7.5<br>7.5<br>4<br>1<br>-<br>-<br>7.5<br>4<br>1<br>-                                  | 182.6         4.99         4         -         0.75         3.51         4         4.8         -         1         17         4.99         7.5         7.5         4         1         -   | 182.6         4.99         4         8         0.75         3.51         4         4.8         -         1         17         4.99         7.5         7.5         4         1         -         1         -   | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>-  | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>-                 | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>4<br>4      | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>4<br>4       | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>4<br>4      | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>4<br>4       | 232.6<br>4.99<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4                           |
|                | AthyAthyAthyBallybegBallybegBallybegBanogeBarrymoreBarrymoreDoonDoonGreat IslandKilkennyKilkennyKilkennyPortlaoisePortlaoiseWexford                    | Solar<br>Battery<br>Solar<br>LFG<br>LFG<br>Solar<br>CHP<br>Solar<br>Solar<br>Solar<br>CHP<br>Biogas<br>Solar<br>Biogas<br>Solar<br>Biogas                           | 178.6<br>-<br>-<br>-<br>0.75<br>3.51<br>-<br>4.8<br>-<br>1<br>-<br>7.5<br>7.5<br>4<br>1<br>1   | 182.6         4.99         4         -         0.75         3.51         4         4.8         -         1         17         4.99         7.5         7.5         4   | 182.6         4.99         4         8         0.75         3.51         4         4.8         -         1         17         4.99         7.5         7.5         4         1   | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1            | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4                           | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1                     | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1                 | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1                     | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1                 | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1                 |
|                | AthyAthyAthyAthyBallybegBallybegBallybegBanogeBarrymoreBarrymoreDoonDoonGreat IslandKilkennyKilkennyKilkennyPortlaoisePortlaoiseWexfordWexford         | Solar<br>Battery<br>Solar<br>LFG<br>Solar<br>CHP<br>Solar<br>Solar<br>Solar<br>CHP<br>Biogas<br>Solar<br>Biogas<br>Solar<br>Solar<br>Solar                          | 178.6<br>-<br>-<br>-<br>0.75<br>3.51<br>-<br>4.8<br>-<br>1<br>-<br>7.5<br>7.5<br>4<br>1<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>- | 182.6         4.99         4         -         0.75         3.51         4         4.8         -         1         17         4.99         7.5         7.5         4         1         -         -         -         -         -         -         -         -         -         -         -         - | 182.6         4.99         4         8         0.75         3.51         4         4.8         -         1         17         4.99         7.5         7.5         4         1         -         -         -         -         -         -         -         -         -         -         -         - | 232.6<br>4.99<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>-<br>12<br>- | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>-<br>12<br>4 | 232.6<br>4.99<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>4<br>12<br>4     | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>4<br>12<br>4 | 232.6<br>4.99<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>4<br>12<br>4     | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>4<br>12<br>4 | 232.6<br>4.99<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>4<br>12<br>4 |
|                | AthyAthyAthyBallybegBallybegBallybegBanogeBarrymoreBarrymoreDoonDoonGreat IslandKilkennyKilkennyKilkennyPortlaoisePortlaoiseWexford                    | Solar<br>Battery<br>Solar<br>LFG<br>LFG<br>Solar<br>CHP<br>Solar<br>Solar<br>Solar<br>CHP<br>Biogas<br>Solar<br>Biogas<br>Solar<br>Solar<br>Solar<br>Solar<br>Solar | 178.6<br>-<br>-<br>-<br>0.75<br>3.51<br>-<br>4.8<br>-<br>1<br>-<br>7.5<br>7.5<br>4<br>1<br>-<br>-<br>7.5<br>4<br>1<br>-                                  | 182.6         4.99         4         -         0.75         3.51         4         4.8         -         1         17         4.99         7.5         7.5         4         1         -   | 182.6         4.99         4         8         0.75         3.51         4         4.8         -         1         17         4.99         7.5         7.5         4         1         -         -         -   | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>-  | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>-<br>12      | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>4<br>1<br>2 | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>4<br>12 | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>4<br>1<br>2 | 232.6<br>4.99<br>8<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>4<br>12 | 232.6<br>4.99<br>8<br>8<br>8<br>0.75<br>3.51<br>4<br>4.8<br>4.95<br>1<br>17<br>4.99<br>7.5<br>7.5<br>4<br>1<br>1<br>4<br>12 |

|        |                       |               | Maximum Export Capacity (MEC) |      |      |      |      |      |      |      |      |      |
|--------|-----------------------|---------------|-------------------------------|------|------|------|------|------|------|------|------|------|
| Area   | 110 kV Station        | Туре          | 2020                          | 2021 | 2022 | 2023 | 2024 | 2025 | 2026 | 2027 | 2028 | 2029 |
|        | Bandon                | Solar         | -                             | -    | -    | 3.99 | 3.99 | 3.99 | 3.99 | 3.99 | 3.99 | 3.99 |
|        | Barnahely             | Solar         | 5                             | 5    | 5    | 5    | 5    | 5    | 5    | 5    | 5    | 5    |
|        | Castleview            | СНР           | 2                             | 2    | 2    | 2    | 2    | 2    | 2    | 2    | 2    | 2    |
|        | Dunmanway             | Gas           | 6                             | 6    | 6    | 6    | 6    | 6    | 6    | 6    | 6    | 6    |
| South- | Knockeragh            | Solar         | -                             | -    | -    | 8.99 | 8.99 | 8.99 | 8.99 | 8.99 | 8.99 | 8.99 |
| West   | Knockeragh            | Biogas<br>DSO | 3                             | 3    | 3    | 3    | 3    | 3    | 3    | 3    | 3    | 3    |
|        | Midleton              | Solar         | -                             | -    | -    | -    | -    | 3.95 | 3.95 | 3.95 | 3.95 | 3.95 |
|        | Reamore               | Battery       | -                             | -    | -    | 8    | 8    | 8    | 8    | 8    | 8    | 8    |
|        | Tralee                | Solar         | -                             | -    | -    | -    | -    | 4    | 4    | 4    | 4    | 4    |
|        | South-West Tota       | al Area       | 16.0                          | 16.0 | 16.0 | 37.0 | 37.0 | 44.9 | 44.9 | 44.9 | 44.9 | 44.9 |
|        | Bellacorick           | Wave          | 10                            | 10   | 10   | 10   | 10   | 10   | 10   | 10   | 10   | 10   |
| West   | Carrick on<br>Shannon | Solar         | -                             | 4    | 4    | 4    | 4    | 4    | 4    | 4    | 4    | 4    |
|        | Dalton                | Battery       | -                             | -    | -    | 12   | 12   | 12   | 12   | 12   | 12   | 12   |
|        | Tawnaghmore           | Biomass       | 54                            | 54   | 54   | 54   | 54   | 54   | 54   | 54   | 54   | 54   |
|        | West Total Area       |               | 64.0                          | 68.0 | 68.0 | 80.0 | 80.0 | 80.0 | 80.0 | 80.0 | 80.0 | 80.0 |

# Table D-3: Existing and Committed Distribution-Connected Generation (excluding wind)

# Appendix E Short Circuit Currents

# E.1. Background of Short Circuit Currents

The main driver for calculating short circuit current levels is safety. All transmission system equipment must be capable of carrying very high currents. These high currents typically occur in the event of a short circuit fault. In particular, circuit breakers must be capable of closing onto a fault and opening to isolate a fault.

Their correct operation minimises risk to human life and prevents damage to transmission system equipment. It is also crucial for maintaining transmission system stability, security and quality of supply.

Short circuit current levels also give an indication of the electrical strength of the transmission system at each station. This provides an indication of the suitability of a station for connection of 'voltage sensitive' equipment.

A station with a high short circuit current level will be more attractive to these types of load. This is due to strong generation infeeds minimising distortions in voltage and frequency caused by transmission system disturbances. Similarly, generators will have less difficulty to ride through faults and maintain stability when connected to stations with high short circuit current levels.

Short circuit current levels vary across the transmission system. They are affected by the transmission system topology, system impedance and the available short circuit contribution from rotating machines (i.e. generators and large motors). Changes in the transmission system topology or the addition/retirement of generation units can bring about an increase/reduction in the short circuit current levels on the transmission system. Similarly, seasonal variations in generation dispatches and demand levels combined with possible transmission system sectionalising or plant outages will result in variations of short circuit current levels at different locations. To ensure safe and reliable operation of the transmission system and customer's equipment at all times, two types of short circuit current level calculations are carried out:

- Maximum short circuit current levels are required for the specification of transmission system equipment and for connections to the transmission system. Plant in substations is typically subjected to the most onerous short circuit currents. The high capital costs of HV equipment means that it is important to predict the maximum short circuit current the equipment may see in its lifetime, and this must be specified to a rating above the maximum expected short circuit current level. Also, for customers, the design and specification of equipment at lower voltage levels will depend on the short circuit level at the transmission connection point.
- Minimum short circuit current levels are required to guarantee reliable and coordinated operation of protection systems or to assess the suitability of a station for the connection of 'voltage sensitive' equipment. Minimum short circuit current levels are also required at the design stage of generation plants to ensure fault ride through capabilities are in accordance with Grid Code requirements.

### E.1.1. The Nature of Short Circuit Currents

The plot in Figure E-1 shows a typical short circuit current waveform. Short circuit current is normally made up of a symmetrical AC component, with a decay rate, and a DC offset component, which has a much faster decay rate. The combination of AC and DC components results in an asymmetrical current waveform.

While the AC component is always present in the short circuit current, the DC offset is dependent on the instant that the fault occurs within the voltage waveform. For the purposes of this document, it is assumed that the fault occurs at the instant of maximum DC offset in the short circuit current.

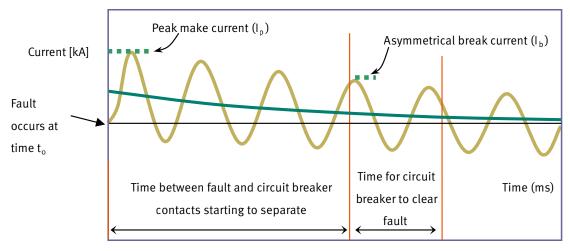


Figure E-1: Typical Short Circuit Current

The DC component of a short circuit current decays exponentially. Its rate of decay is influenced by the individual ratios of the reactance (X) to the resistance (R) of the paths back to the generators feeding power to the fault (the X/R ratio). Transmission nodes where large generators can have high X/R ratios, may have a slower decay time for the DC component of the short circuit current.

The AC component of a short circuit current also decays with time. This is due to the changes in the synchronous generators internal reactance and, thus, the AC reduction effect is more pronounced in the vicinity of large generation plants. The internal impedance of a synchronous generator is not constant after the start of the fault. It increases progressively and the short circuit current contribution becomes weaker, passing through three characteristic stages:

- Subtransient: (approx. 0.01 to 0.1 sec). Short-circuit current (RMS value of the AC component) is high: 5 to 10 times permanent rated current. This is called sub-transient short-circuit current, Ik''.
- Transient: (between 0.1 and 1 sec). Short-circuit current (RMS value of the AC component) drops to between 2 and 6 times rated current. This is called transient short-circuit current, Ik'.
- Continuous: Short-circuit current (RMS value of the AC component) drops to between 0.5 and 2 times rated current. This is called steady-state short-circuit current, Ik.

### E.1.2. Duty of Circuit Breakers

Over the duration of a fault the switchgear has to be able to withstand two events, namely the fault initiation and then the fault clearance. The short circuit currents at these two instances are referred to as the make current and the break current respectively.

i. The make current (Ip) is the maximum instantaneous current that the circuit breaker is called to withstand. The initiation of a fault causes an instantaneous peak current which results in the generation of electromechanical forces along the busbars and transmission lines. An example of such a fault initiation would be a circuit breaker energising a line that is still earthed following maintenance, hence the term make current.

Make current is expressed in peak values and is comprised of an AC and a DC component. Essentially, the make current is the maximum instantaneous peak of the short circuit current waveform. This will occur at approximately 10 milliseconds (ms) after the instant of fault (see Figure E-1), whether the fault is energised through a circuit breaker or it spontaneously occurs on the transmission system. Circuit breakers are typically rated approximately 2.5 times higher for make duty than for break duty, as per IEC 62271-100 standard.

**ii.** After the fault initiation, there is a time period during which the protection scheme will identify the fault, make a decision and then instruct the relevant circuit breaker to open to interrupt the fault. This could take anything from 10 ms in modern fast protection systems to 60 ms in older systems. At this point the circuit breaker begins to open and it takes a certain time period before the contacts actually separate, normally around two cycles or 40 ms in modern switchgear equipment. The total time from the start of the fault until the breaker opening or fault clearance time can vary from 50 ms to 120 ms, depending on the protection system. In some cases, if main protection fails and back-up main protection is not installed, clearance times can be considerably longer than 120 ms.

At the point of physical separation, the short circuit current forms an arc and the thermal energy generated by this arc has to be dissipated as the short circuit current is interrupted. The short circuit current when this interruption occurs is referred to as the break current, lb. This value is expressed in RMS (root mean square) terms and is comprised of an AC component and a DC component. Circuit breakers designed and tested in accordance with the IEC 62271-100 standard can interrupt any short circuit current up to its rated breaking current containing any AC component up to the rated value and, associated with it, any percentage DC component up to that specified (typically 30%).

The duty of the circuit breaker is calculated from the make and break current as a percentage of the circuit breaker rating.

# E.2. Short Circuit Current Calculation Methodology

Engineering Recommendation G74 has been applied to all short circuit studies reported in this document. Some of the general assumptions applied include:

- Short circuit level contribution from loads has been considered following G74 recommendations. The demand at each node is assumed to contribute 1 MVA of induction motor fault infeed per MW of load. A constant X/R ratio of 2.76 is assumed for all of the loads; and
- A break time of 50 ms is assumed typical for the circuit breakers at 110 kV, 220 kV, 275 kV and 400 kV. A break time of 80 ms is used for the circuit breakers at 110 kV stations in Ireland.

**Winter Peak** study results give an indication of the maximum prospective short circuit current levels on the transmission system. For winter peak studies, all generators have been included in the calculations. A merit order economic dispatch has been used, and to enable maximum short circuit current level to be calculated, any generators that were not dispatched have been switched in with o MW output, thus contributing to short circuit current levels.

**Summer Night Valley** study results give an indication of the minimum short circuit current levels to be expected on the transmission system under normal transmission system operating conditions (i.e. maintenance outages are not considered in this section<sup>132</sup>). For summer night valley studies, only generators dispatched on a merit order are considered in the model.

# E.3. Short Circuit Currents in Ireland

### E.3.1. Methodology used in Ireland

Short circuit current levels are calculated in accordance with the UK Engineering Recommendation G74, which is a computer based analysis, based on the International Standard IEC60909. Compliance with G74 includes:

- Short circuit contributions from rotating plant, including induction motors embedded in the general load;
- Comprehensive plant parameters including impedances, transformer winding and earthing configurations;
- Pre-fault voltage levels at each node which should be obtained from a credible, pre-fault load flow study; and
- Pre-fault transformer tap settings should also be obtained from the load flow study.

The short circuit current level network model includes the following component parameters:

- Transformer impedance variation with tap position;
- Zero sequence mutual coupling effect;
- Saturated generator reactance values; and
- Power station auxiliaries short circuit current level contributions.

The calculation of the X/R ratios, used by EirGrid, is undertaken in accordance with IEC60909-0 Method B. Method B is currently considered to be the most appropriate general purpose method for calculating DC short circuit currents in the transmission system of Ireland.

The transmission system of Ireland is designed and operated to maintain RMS break short circuit levels in accordance with EirGrid Grid Code CC.8.6. A summary of these requirements is set out in Table E-1. In designing the system, a 10% safety margin is applied.

It should be noted that the EirGrid Grid Code stipulates that short circuit current levels at designated stations in Ireland may be allowed to increase to 31.5 kA. If necessary, the equipment at these stations is to be modified or replaced in order to comply with this new rating.

Circuit breakers with a higher rating than the current levels may be necessary for a number of reasons, including, but not limited to the need to provide an adequate safety margin or to cater for a high DC component in the short circuit current.

<sup>132</sup> Minimum fault levels including maintenance outages are currently provided to generator applicants wishing to connect to the transmission system as part of the connection offer process to allow developers to design the plant in accordance with the Grid Code requirements.

#### Table E-1: Ireland Short Circuit Current Levels Specified in the Grid Code

| Volt | age Level (kV)   | Short Circuit Current Levels (kA) |
|------|------------------|-----------------------------------|
|      | 400              | 50                                |
|      | 220              | 40                                |
| 110  | Countrywide      | 25                                |
| 110  | Designated sites | 31.5                              |

#### E.3.2. Analysis

The total RMS break current at a busbar is an indication of the short circuit current level that one could expect at that point in the transmission system. However, they do not necessarily represent the short circuit current that could flow through each individual breaker, which may be lower.

#### E.3.3. Analysis

Tables E-2 to E-4 list subtransient (Ik"), transient (Ik') currents and X/R ratios for single-phase to earth and balanced three-phase faults for transmission system busbars of Ireland. These are presented for maximum winter peak and minimum summer valley intact system demand conditions for 2020, 2023 and 2026. From these values, the relevant currents required to assess circuit breaker duty can be derived using the following equations:

• Peak make current (I<sub>n</sub>)

$$I_{p} = \sqrt{2} \cdot \left[ 1.02 + 0.98 \cdot e^{-3 \cdot \frac{R}{X}} \right] \cdot I_{k}^{"}$$

AC component (I<sub>RMS\_AC\_b</sub>) of short-circuit current at a selected time of break (t<sub>b</sub>)

$$I_{RMS\_AC\_b} = I_{k}' + (I_{k}'' - I_{k}') \cdot e^{-\frac{t_{b}}{40ms}}$$

• DC component  $(I_{DC_b})$  of short-circuit current at a selected time of break  $(t_b)$ 

$$I_{DC_b} = \sqrt{2} \cdot I_k'' \cdot e^{-2 \cdot \pi \cdot 50t_b \cdot \frac{R}{X}}$$

• Break current  $(I_{h})$  at a selected time of break  $(t_{h})$ 

$$I_b = \sqrt{I_{DC_b}^2 + I_{RMS_AC_b}^2}$$

|                      |              |            | Sum         | nmer         |             |             |              |             | Wi          | nter         |             |             |
|----------------------|--------------|------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|
|                      | Th           | ree pha    | se          | Si           | ngle Pha    | ase         | Th           | ree pha     | se          | Si           | ngle Ph     | ase         |
| Station              | X/R<br>Ratio | k"<br>[kA] | lk'<br>[kA] | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] | X/R<br>Ratio | Ik"<br>[kA] | lk'<br>[kA] | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] |
| Adamstown 110 kV     | 16.58        | 11.20      | 10.21       | 10.54        | 12.58       | 12.13       | 15.69        | 13.27       | 11.75       | 10.06        | 14.30       | 13.66       |
| Agannygal 110 kV     | 2.83         | 4.75       | 4.64        | 3.86         | 4.10        | 4.08        | 2.97         | 6.43        | 5.80        | 4.24         | 4.94        | 4.81        |
| Aghada 110 kV        | 5.19         | 8.03       | 7.81        | 6.14         | 9.56        | 9.45        | 4.63         | 9.93        | 9.53        | 5.68         | 11.31       | 11.13       |
| Aghada A 220 kV      | 13.70        | 10.63      | 10.30       | 14.89        | 13.98       | 13.78       | 14.72        | 20.64       | 19.08       | 16.00        | 25.48       | 24.63       |
| Aghada B 220 kV      | 13.37        | 11.17      | 10.71       | 12.18        | 14.52       | 14.25       | 14.72        | 20.64       | 19.08       | 16.00        | 25.48       | 24.63       |
| Aghada C 220 kV      | 13.31        | 10.40      | 10.08       | 13.56        | 13.66       | 13.47       | 13.81        | 19.80       | 18.36       | 12.89        | 24.46       | 23.68       |
| Aghada D 220 kV      | 13.31        | 10.40      | 10.08       | 13.56        | 13.66       | 13.47       | 14.72        | 20.64       | 19.08       | 16.00        | 25.48       | 24.63       |
| Ahane 110 kV         | 5.54         | 10.63      | 10.05       | 6.03         | 9.37        | 9.22        | 4.94         | 15.32       | 14.15       | 5.77         | 11.46       | 11.22       |
| Anner 110 kV         | 4.07         | 5.88       | 5.64        | 4.52         | 4.51        | 4.46        | 4.03         | 7.33        | 6.78        | 4.54         | 5.01        | 4.92        |
| Ardnacrusha 110 kV   | 6.05         | 11.56      | 10.80       | 7.12         | 13.08       | 12.74       | 5.96         | 18.71       | 16.79       | 7.61         | 18.31       | 17.65       |
| Ardnagappary 110 kV  | 2.75         | 1.89       | 1.84        | 3.92         | 1.22        | 1.21        | 2.95         | 2.52        | 2.30        | 4.27         | 1.34        | 1.31        |
| Arigna 110 kV        | 4.38         | 6.21       | 5.97        | 5.40         | 5.20        | 5.14        | 4.54         | 8.54        | 7.77        | 5.74         | 6.13        | 5.99        |
| Arklow 110 kV        | 10.90        | 7.64       | 7.43        | 11.57        | 9.38        | 9.27        | 10.85        | 9.57        | 9.01        | 11.65        | 11.27       | 11.00       |
| Arklow 220 kV        | 9.42         | 7.03       | 6.82        | 10.66        | 6.66        | 6.60        | 9.07         | 8.44        | 8.09        | 10.47        | 7.57        | 7.47        |
| Artane 110 kV        | 13.58        | 10.00      | 9.47        | 6.25         | 12.19       | 11.92       | 13.17        | 12.87       | 11.83       | 5.73         | 15.04       | 14.53       |
| Arva 110 kV          | 3.90         | 8.06       | 7.64        | 4.96         | 6.60        | 6.50        | 3.92         | 10.73       | 9.43        | 5.17         | 7.62        | 7.38        |
| Athea 110 kV         | 10.12        | 6.19       | 6.06        | 10.72        | 6.73        | 6.68        | 11.25        | 10.70       | 8.99        | 12.18        | 9.55        | 9.03        |
| Athlone 110 kV       | 4.05         | 6.34       | 6.08        | 5.27         | 5.23        | 5.17        | 4.05         | 8.28        | 7.79        | 5.51         | 6.07        | 5.98        |
| Athy 110 kV          | 3.35         | 5.53       | 5.37        | 4.43         | 4.71        | 4.67        | 3.19         | 6.75        | 6.38        | 4.40         | 5.37        | 5.29        |
| Aughinish 110 kV     | 8.99         | 9.33       | 8.48        | 10.93        | 10.48       | 10.10       | 7.90         | 10.65       | 9.77        | 9.96         | 11.22       | 10.88       |
| Ballybeg 110 kV      | 10.00        | 6.01       | 5.85        | 10.15        | 7.16        | 7.08        | 9.94         | 7.07        | 6.75        | 10.14        | 8.18        | 8.03        |
| Ballydine 110 kV     | 4.10         | 6.54       | 6.30        | 3.80         | 5.37        | 5.32        | 4.01         | 8.03        | 7.49        | 3.74         | 6.01        | 5.91        |
| Ballylickey 110 kV   | 2.81         | 2.96       | 2.90        | 3.93         | 1.92        | 1.91        | 2.97         | 3.99        | 3.71        | 4.05         | 2.25        | 2.22        |
| Ballynahulla 110 kV  | 13.29        | 7.03       | 6.86        | 11.86        | 7.71        | 7.65        | 16.27        | 11.90       | 10.61       | 12.67        | 10.91       | 10.51       |
| Ballynahulla 220 kV  | 8.53         | 5.94       | 5.75        | 8.48         | 6.83        | 6.75        | 9.40         | 10.73       | 9.89        | 9.09         | 10.32       | 10.04       |
| Ballyvouskill 110 kV | 13.82        | 7.20       | 7.03        | 13.47        | 8.66        | 8.58        | 14.63        | 12.48       | 10.97       | 13.72        | 12.92       | 12.33       |
| Ballyvouskill 220 kV | 8.73         | 6.25       | 6.05        | 9.28         | 7.95        | 7.84        | 9.27         | 10.95       | 10.05       | 10.03        | 12.31       | 11.90       |
| Ballywater 110 kV    | 5.60         | 5.38       | 5.28        | 3.47         | 5.63        | 5.60        | 5.46         | 6.80        | 6.39        | 3.30         | 6.52        | 6.39        |
| Baltrasna 110 kV     | 6.38         | 9.57       | 9.08        | 7.40         | 7.62        | 7.51        | 5.89         | 10.87       | 10.30       | 7.11         | 8.29        | 8.18        |
| Bancroft 110 kV      | 13.27        | 11.34      | 10.69       | 7.17         | 13.36       | 13.04       | 12.39        | 13.01       | 12.13       | 6.81         | 14.97       | 14.56       |
| Bandon 110 kV        | 3.35         | 5.78       | 5.56        | 4.37         | 5.74        | 5.67        | 3.12         | 7.80        | 7.15        | 4.32         | 7.01        | 6.82        |
| Banoge 110 kV        | 6.52         | 5.48       | 5.36        | 7.13         | 5.03        | 5.00        | 6.22         | 6.62        | 6.25        | 6.97         | 5.66        | 5.56        |
| Barnahealy A 110 kV  | 5.38         | 10.56      | 10.16       | 5.96         | 11.41       | 11.25       | 4.52         | 13.83       | 13.01       | 5.31         | 13.83       | 13.54       |
| Barnahealy B 110 kV  | 7.33         | 10.34      | 9.95        | 7.74         | 11.02       | 10.86       | 6.24         | 13.91       | 13.00       | 6.95         | 13.54       | 13.23       |
| Barnakyle 110 kV     | 20.53        | 11.36      | 10.36       | 12.69        | 12.49       | 12.07       | 19.42        | 13.47       | 11.94       | 12.10        | 14.20       | 13.58       |
| Baroda 110 kV        | 3.97         | 7.32       | 7.01        | 4.63         | 8.67        | 8.52        | 3.99         | 9.53        | 8.91        | 4.80         | 10.68       | 10.41       |
| Barrymore 110 kV     | 3.98         | 6.81       | 6.60        | 4.95         | 4.30        | 4.27        | 3.73         | 8.72        | 8.27        | 4.91         | 4.82        | 4.77        |
| Belcamp 110 kV       | 33.61        | 6.64       | 6.30        | 34.01        | 8.24        | 8.06        | 35.74        | 7.48        | 7.14        | 35.59        | 9.20        | 9.02        |
| Belcamp 220 kV       | 12.63        | 14.99      | 13.69       | 10.67        | 18.95       | 18.21       | 11.49        | 21.00       | 19.11       | 9.53         | 25.00       | 24.04       |
| Belgard 110 kV       | 12.83        | 11.56      | 10.90       | 6.97         | 14.24       | 13.89       | 12.13        | 13.27       | 12.31       | 6.65         | 16.03       | 15.54       |
| Bellacorick 110 kV   | 3.40         | 3.41       | 3.25        | 3.77         | 4.23        | 4.15        | 5.16         | 6.73        | 5.80        | 5.69         | 7.15        | 6.76        |
| Binbane 110 kV       | 3.16         | 3.52       | 3.39        | 4.28         | 3.46        | 3.42        | 3.57         | 5.66        | 4.99        | 5.30         | 4.56        | 4.40        |

|                                   |               |               | Sum           | mer           |               |                |              |                | Wi            | nter         |               |               |
|-----------------------------------|---------------|---------------|---------------|---------------|---------------|----------------|--------------|----------------|---------------|--------------|---------------|---------------|
|                                   | ты            | iree pha      |               |               | ngle Pha      |                | тн           | ree pha        |               |              | ngle Ph       | 250           |
|                                   |               |               | 1             |               | -             |                |              |                |               |              | , <b>-</b>    |               |
| Station                           | X/R<br>Ratio  | lk"<br>[kA]   | lk'<br>[kA]   | X/R<br>Ratio  | lk"<br>[kA]   | lk'<br>[kA]    | X/R<br>Ratio | lk"<br>[kA]    | lk'<br>[kA]   | X/R<br>Ratio | lk"<br>[kA]   | lk'<br>[kA]   |
| Brinny B 110 kV                   | 3.21          | 5.25          | 5.07          | 4.22          | 4.82          | 4.77           | 2.99         | 6.89           | 6.37          | 4.16         | 5.71          | 5.58          |
| Bunkimalta 110 kV                 | 5.27          | 5.09          | 4.93          | 5.50          | 5.35          | 5.29           | 6.57         | 8.12           | 7.14          | 6.41         | 7.47          | 7.16          |
| Butlerstown 110 kV                | 6.77          | 9.59          | 9.27          | 6.89          | 10.06         | 9.94           | 6.13         | 11.91          | 11.02         | 6.45         | 11.69         | 11.39         |
| Cabra 110 kV                      | 12.59         | 9.69          | 9.18          | 5.07          | 11.01         | 10.79          | 12.10        | 12.40          | 11.41         | 4.65         | 13.37         | 12.97         |
| Cahir 110 kV                      | 4.42          | 7.27          | 6.96          | 5.37          | 6.28          | 6.20           | 4.58         | 10.29          | 9.29          | 5.72         | 7.43          | 7.24          |
| Carlow 110 kV                     | 5.33          | 7.30          | 7.05          | 6.03          | 8.09          | 7.99           | 5.28         | 9.45           | 8.74          | 6.10         | 9.74          | 9.48          |
| Carrickalangan 110 kV             | 4.25          | 3.24          | 3.14          | 5.18          | 2.55          | 2.53           | 5.01         | 4.53           | 4.07          | 5.88         | 2.95          | 2.88          |
| Carrickmines 220 kV               | 17.28         | 16.94         | 15.52         | 9.74          | 21.18         | 20.39          | 14.52        | 21.06          | 19.15         | 8.46         | 25.11         | 24.13         |
| Carrickmines A 110 kV             | 33.55         | 11.20         | 10.63         | 24.39         | 12.41         | 12.17          | 31.70        | 12.97          | 12.03         | 23.35        | 13.92         | 13.54         |
| Carrickmines B 110 kV             | 27.40         | 12.53         | 11.79         | 21.58         | 15.16         | 14.79          | 25.32        | 14.52          | 13.49         | 20.25        | 17.17         | 16.66         |
| Carrick-on-Shannon 110 kV         | 4.42          | 9.43          | 8.91          | 5.06          | 10.56         | 10.33          | 4.20         | 13.18          | 11.94         | 5.05         | 13.43         | 12.97         |
| Carrigadrohid 110 kV              | 6.90          | 10.34         | 9.92          | 7.04          | 10.62         | 10.47          | 6.59         | 15.66          | 14.31         | 6.87         | 13.76         | 13.39         |
| Carrigdangan 110 kV               | 3.44          | 4.39          | 4.29          | 4.39          | 3.30          | 3.28           | 4.11         | 6.91           | 6.01          | 5.15         | 7.26          | 6.89          |
| Carrowbeg 110 kV                  | 2.72          | 2.54          | 2.44          | 3.59          | 2.40          | 2.37           | 2.72         | 3.30           | 3.02          | 3.76         | 2.80          | 2.74          |
| Cashla 110 kV                     | 7.70          | 12.97         | 12.14         | 7.98          | 16.74         | 16.26          | 7.28         | 19.47          | 17.68         | 7.67         | 23.42         | 22.50         |
| Cashla 220 kV                     | 8.57          | 8.75          | 8.27          | 9.53          | 9.30          | 9.11           | 8.49         | 12.18          | 11.54         | 9.66         | 11.71         | 11.50         |
| Castlebagot 110 kV                | 22.62         | 17.46         | 16.50         | 22.94         | 11.48         | 11.34          | 20.97        | 20.26          | 19.27         | 22.17        | 12.63         | 12.50         |
| Castlebagot 220 kV                | 13.35         | 18.59         | 16.90         | 10.43         | 20.35         | 19.62          | 11.04        | 24.08          | 21.89         | 9.07         | 24.62         | 23.80         |
| Castlebar 110 kV                  | 3.14          | 4.16          | 3.96          | 3.71          | 4.67          | 4.59           | 3.40         | 6.38           | 5.62          | 4.16         | 6.17          | 5.91          |
| Castledockrill 110 kV             | 7.74          | 6.55          | 6.42          | 4.58          | 7.70          | 7.64           | 7.56         | 8.39           | 7.89          | 4.30         | 9.07          | 8.86          |
| Castlefarm A 110 kV               | 8.09          | 9.00          | 8.20          | 9.49          | 9.76          | 9.43           | 7.14         | 10.24          | 9.42          | 8.69         | 10.44         | 10.13         |
| Castlefarm B 110 kV               | 8.10          | 8.99          | 8.19          | 9.50          | 9.75          | 9.41           | 7.15         | 10.23          | 9.40          | 8.70         | 10.43         | 10.12         |
| Castleview 110 kV                 | 4.46          | 10.45         | 10.06         | 4.85          | 8.25          | 8.17           | 3.78         | 13.81          | 12.95         | 4.50         | 9.61          | 9.46          |
| Cathaleen's Fall 110 kV           | 4.22          | 6.43          | 6.10          | 4.85          | 7.30          | 7.15           | 5.21         | 12.06          | 10.20         | 6.20         | 11.11         | 10.51         |
| Cauteen 110 kV                    | 5.37          | 6.24          | 6.03          | 6.28          | 4.30          | 4.26           | 5.93         | 9.37           | 8.57          | 6.74         | 5.09          | 5.00          |
| Central Park 110 kV               | 15.31         | 10.27         | 9.78          | 7.84          | 11.14         | 10.95          | 14.55        | 11.81          | 11.00         | 7.56         | 12.42         | 12.10         |
| Charleville 110 kV                | 4.58          | 5.50          | 5.33          | 5.94          | 5.23          | 5.17           | 4.76         | 7.68           | 7.00          | 6.50         | 6.49          | 6.32          |
| Cherrywood 110 kV                 | 10.83         | 9.53          | 9.09          | 7.65          | 9.81          | 9.65           | 10.33        | 10.85          | 10.16         | 7.42         | 10.83         | 10.59         |
| City West 110 kV                  | 6.22          | 7.39          | 6.92          | 6.12          | 5.62          | 5.52           | 5.93         | 8.55           | 7.73          | 5.97         | 6.12          | 5.96          |
| Clahane 110 kV                    | 4.31          | 6.24          | 6.00          | 5.23          | 5.97          | 5.90           | 4.03         | 8.55           | 7.82          | 5.15         | 7.18          | 7.00          |
| Clashavoon 220 kV                 | 9.03          | 7.17          | 6.91          | 9.64          | 8.88          | 8.75           | 9.28         | 11.98          | 11.08         | 10.08        | 13.08         | 12.69         |
| Clashavoon A 110 kV               | 7.77          | 11.68         | 11.16         | 8.03          | 15.44         | 15.12          | 7.92         | 19.14          | 17.16         | 8.23         | 23.00         | 21.97         |
| Clashavoon B 110 kV               | 7.77          | 11.68         | 11.16         | 8.03          | 15.44         | 15.12          | 7.92         | 19.14          | 17.16         | 8.23         | 23.00         | 21.97         |
| Cliff 110 kV<br>Cloghboola 110 kV | 3.99          | 5.26          | 5.04          | 4.92          | 5.40          | 5.32           | 4.55         | 8.71           | 7.70          | 5.93         | 7.27<br>8.50  | 7.01          |
| Cloghboola 110 kV                 | 7.18          | 5.44          | 5.34          | 9.15          | 5.90          | 5.86           | 7.75         | 9.71           | 7.94          | 11.19        | 8.50          | 7.97          |
| Clogher 110 kV                    | 7.18          | 5.44          | 5.34          | 9.15          | 5.90          | 5.86<br>6.06   | 7.75<br>4.89 | 9.71           | 7.94<br>8.30  | 11.19        | 8.50          | 7.97<br>8.05  |
| Cloghran 110 kV                   | 3.82<br>9.48  | 5.35<br>17.65 | 5.10<br>15.98 | 4.36          | 6.17<br>20.59 |                | 4.89<br>8.45 | 10.37<br>20.90 | 8.30<br>19.12 | 5.76<br>8.64 | 9.66<br>23.46 | 8.95<br>22.67 |
| Clonee 220 kV                     | 9.40<br>13.82 | 17.05         | 15.98         | 9.43<br>10.37 | 15.58         | 19.79<br>15.10 | 12.12        | 20.90          | 19.12         | 9.27         | 19.24         | 18.72         |
| Clonkeen A 110 kV                 | -             | 5.41          | 5.26          | 6.77          | 4.12          | 4.09           | 5.56         | 6.70           | 6.33          | 9.27<br>6.76 |               |               |
| Clonkeen B 110 kV                 | 5.74<br>5.07  | 5.41<br>6.19  | 6.07          | 4.45          | 7.39          | 7.33           | 4.70         | 10.40          | 9.14          | 4.05         | 4.59<br>10.77 | 4.53<br>10.28 |
| Cloon 110 kV                      | 4.51          | 6.65          | 6.37          | 4.45<br>5.81  | 7.39<br>5.98  | 7.33<br>5.91   | 4.17         | 8.58           | 9.14<br>8.01  | 5.70         | 7.01          | 6.88          |
|                                   | 4·ɔ¹          | 0.05          | /ز.ب          | 0.01          | 2.20          | J·YI           | 4.1/         | 0.50           | 0.01          | 5./0         | /.01          | 0.00          |

|                      | Summer |         |       |       |          |       |       |         | Wi    | nter  |         |       |
|----------------------|--------|---------|-------|-------|----------|-------|-------|---------|-------|-------|---------|-------|
|                      | Th     | ree pha | se    | Si    | ngle Pha | ise   | Th    | ree pha | se    | Si    | ngle Ph | ase   |
|                      | X/R    | lk"     | lk'   | X/R   | lk"      | lk'   | X/R   | lk"     | lk'   | X/R   | lk"     | lk'   |
| Station              | Ratio  | [kA]    | [kA]  | Ratio | [kA]     | [kA]  | Ratio | [kA]    | [kA]  | Ratio | [kA]    | [kA]  |
| College Park 110 kV  | 9.15   | 16.92   | 15.41 | 6.48  | 20.39    | 19.61 | 8.18  | 19.97   | 18.36 | 5.91  | 23.33   | 22.55 |
| Cookstown 110 kV     | 7.54   | 8.04    | 7.72  | 6.01  | 6.89     | 6.81  | 7.17  | 9.02    | 8.58  | 5.85  | 7.52    | 7.42  |
| Cookstown A 110 kV   | 5.07   | 6.32    | 5.96  | 5.25  | 4.53     | 4.46  | 4.86  | 7.28    | 6.59  | 5.15  | 4.89    | 4.78  |
| Coolroe 110 kV       | 3.94   | 8.38    | 8.10  | 5.06  | 8.33     | 8.24  | 3.48  | 11.23   | 10.52 | 4.86  | 10.05   | 9.85  |
| Coomagearlahy 110 kV | 5.08   | 5.04    | 4.96  | 5.51  | 6.09     | 6.05  | 5.21  | 8.31    | 7.22  | 5.87  | 8.94    | 8.48  |
| Coomataggart 110 kV  | 9.70   | 4.90    | 4.82  | 7.00  | 3.48     | 3.47  | 10.04 | 7.97    | 7.08  | 6.65  | 4.16    | 4.07  |
| Cordal 110 kV        | 11.27  | 6.18    | 6.05  | 7.98  | 6.75     | 6.70  | 12.95 | 10.25   | 9.14  | 7.56  | 9.40    | 9.06  |
| Corderry 110 kV      | 4.01   | 6.37    | 6.11  | 4.95  | 6.33     | 6.25  | 4.21  | 9.71    | 8.55  | 5.50  | 8.13    | 7.83  |
| Corduff 110 kV       | 10.45  | 19.24   | 17.34 | 11.23 | 23.58    | 22.56 | 9.23  | 23.06   | 20.98 | 10.18 | 27.31   | 26.28 |
| Corduff 220 kV       | 16.19  | 17.17   | 15.55 | 14.67 | 21.65    | 20.72 | 14.72 | 24.29   | 21.95 | 13.22 | 28.64   | 27.47 |
| Corkagh 110 kV       | 19.13  | 11.39   | 10.37 | 12.61 | 12.71    | 12.25 | 18.15 | 13.53   | 11.95 | 12.05 | 14.47   | 13.81 |
| Corraclassy 110 kV   | 4.27   | 5.94    | 5.63  | 5.38  | 4.78     | 4.72  | 4.32  | 7.42    | 6.85  | 5.60  | 5.31    | 5.21  |
| Cow Cross 110 kV     | 4.91   | 10.58   | 10.18 | 5.15  | 9.48     | 9.37  | 4.12  | 13.89   | 13.05 | 4.68  | 11.21   | 11.02 |
| Crane 110 kV         | 7.87   | 7.16    | 6.98  | 7.51  | 7.95     | 7.88  | 7.75  | 9.47    | 8.68  | 7.34  | 9.57    | 9.29  |
| Croaghaun 110 kV     | 3.47   | 3.19    | 3.05  | 3.98  | 3.66     | 3.60  | 5.15  | 5.94    | 5.20  | 5.80  | 5.68    | 5.43  |
| Croaghnagawna 110 kV | 4.21   | 3.41    | 3.30  | 5.21  | 2.83     | 2.81  | 5.02  | 4.88    | 4.35  | 6.04  | 3.34    | 3.25  |
| Cromcastle A 110 kV  | 12.24  | 9.84    | 9.16  | 7.49  | 11.13    | 10.82 | 11.27 | 12.18   | 10.92 | 7.02  | 13.10   | 12.57 |
| Cromcastle B 110 kV  | 12.24  | 9.84    | 9.16  | 7.49  | 11.13    | 10.82 | 11.27 | 12.18   | 10.92 | 7.02  | 13.10   | 12.57 |
| Crory 110 kV         | 9.68   | 7.38    | 7.22  | 9.77  | 9.32     | 9.24  | 9.66  | 9.65    | 8.99  | 9.63  | 11.30   | 10.98 |
| Cullenagh 110 kV     | 8.39   | 11.44   | 11.02 | 8.83  | 13.57    | 13.37 | 7.50  | 14.59   | 13.45 | 8.14  | 16.37   | 15.86 |
| Cullenagh 220 kV     | 9.14   | 8.14    | 7.97  | 9.27  | 8.48     | 8.42  | 8.25  | 9.93    | 9.58  | 8.67  | 9.75    | 9.64  |
| Cunghill 110 kV      | 3.24   | 4.56    | 4.38  | 3.72  | 4.45     | 4.39  | 3.16  | 6.44    | 5.97  | 3.78  | 5.47    | 5.35  |
| Cureeny 110 kV       | 4.73   | 4.75    | 4.62  | 5.31  | 5.11     | 5.05  | 5.93  | 7.62    | 6.69  | 6.53  | 7.21    | 6.90  |
| Cureeny T 110 kV     | 5.38   | 6.20    | 5.97  | 5.22  | 6.08     | 6.01  | 6.16  | 9.59    | 8.54  | 5.57  | 8.14    | 7.87  |
| Cushaling 110 kV     | 3.80   | 6.01    | 5.81  | 4.38  | 7.71     | 7.59  | 5.30  | 9.50    | 8.83  | 6.56  | 11.06   | 10.74 |
| Dallow 110 kV        | 3.44   | 4.53    | 4.42  | 4.52  | 3.02     | 3.00  | 3.51  | 5.70    | 5.43  | 4.71  | 3.38    | 3.35  |
| Dalton 110 kV        | 3.09   | 3.70    | 3.56  | 4.12  | 3.26     | 3.22  | 3.28  | 5.21    | 4.71  | 4.56  | 3.87    | 3.78  |
| Dardistown 110 kV    | 15.54  | 9.97    | 9.27  | 12.20 | 11.53    | 11.21 | 14.38 | 12.37   | 11.08 | 11.57 | 13.65   | 13.09 |
| Darndale 110 kV      | 31.77  | 6.56    | 6.23  | 33.88 | 8.20     | 8.02  | 33.52 | 7.39    | 7.04  | 35.43 | 9.14    | 8.96  |
| Derrybrien 110 kV    | 2.68   | 3.76    | 3.70  | 3.74  | 3.65     | 3.63  | 3.00  | 5.17    | 4.57  | 4.45  | 4.57    | 4.40  |
| Derryiron 110 kV     | 4.71   | 6.77    | 6.52  | 5.75  | 7.22     | 7.12  | 4.87  | 7.09    | 6.81  | 6.33  | 7.19    | 7.09  |
| Doon 110 kV          | 4.37   | 6.39    | 6.11  | 4.68  | 5.04     | 4.98  | 4.38  | 8.12    | 7.46  | 4.73  | 5.66    | 5.54  |
| Dromada 110 kV       | 9.46   | 5.82    | 5.70  | 6.69  | 6.22     | 6.18  | 10.23 | 9.84    | 8.29  | 6.26  | 8.66    | 8.20  |
| Drumkeen 110 kV      | 3.47   | 4.87    | 4.64  | 4.16  | 5.09     | 5.00  | 3.96  | 8.70    | 7.22  | 5.03  | 7.24    | 6.85  |
| Drumline 110 kV      | 3.63   | 7.21    | 6.90  | 4.75  | 6.31     | 6.23  | 3.22  | 9.65    | 8.92  | 4.60  | 7.38    | 7.23  |
| Drybridge 110 kV     | 5.86   | 12.26   | 11.45 | 6.70  | 10.49    | 10.28 | 5.16  | 14.82   | 13.58 | 6.27  | 11.86   | 11.57 |
| Dundalk 110 kV       | 3.75   | 7.99    | 7.63  | 4.70  | 7.43     | 7.32  | 3.41  | 9.74    | 8.92  | 4.51  | 8.49    | 8.27  |
| Dunfirth 110 kV      | 4.67   | 5.85    | 5.66  | 6.17  | 4.70     | 4.66  | 4.53  | 6.48    | 6.27  | 6.13  | 5.02    | 4.98  |
| Dungarvan 110 kV     | 6.06   | 5.66    | 5.52  | 7.75  | 4.83     | 4.80  | 6.34  | 7.67    | 6.86  | 8.32  | 5.75    | 5.59  |
| Dunmanway 110 kV     | 4.14   | 6.71    | 6.47  | 5.20  | 6.25     | 6.18  | 4.39  | 10.69   | 9.38  | 5.39  | 9.47    | 9.09  |
| Dunstown 220 kV      | 12.60  | 16.03   | 14.94 | 12.12 | 19.03    | 18.49 | 10.90 | 20.48   | 19.23 | 10.82 | 23.15   | 22.59 |
| Dunstown 400 kV      | 17.58  | 6.14    | 5.86  | 19.93 | 6.92     | 6.80  | 16.13 | 7.71    | 7.43  | 18.85 | 8.26    | 8.15  |

|                         |              |             | Sum         | mer          |             |             |              |             | Wi          | nter         |             |             |
|-------------------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|
|                         | ты           | iree pha    |             |              | ngle Pha    |             | ты           | ree pha     |             | <u> </u>     | ngle Pha    | 250         |
|                         |              |             | 1           |              | -<br>-      |             |              |             | 1           |              | _           |             |
| Station                 | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] |
| Ennis 110 kV            | 4.51         | 9.10        | 8.65        | 5.64         | 8.49        | 8.36        | 4.48         | 14.27       | 12.52       | 5.98         | 10.94       | 10.56       |
| Fassaroe East 110 kV    | 5.36         | 7.54        | 7.25        | 5.41         | 5.83        | 5.77        | 5.12         | 8.50        | 8.05        | 5.29         | 6.35        | 6.26        |
| Fassaroe West 110 kV    | 5.52         | 7.70        | 7.40        | 5.51         | 6.02        | 5.96        | 5.26         | 8.68        | 8.22        | 5.38         | 6.56        | 6.47        |
| Finglas 220 kV          | 15.93        | 16.41       | 14.88       | 15.48        | 21.43       | 20.49       | 15.40        | 23.70       | 21.35       | 14.73        | 29.14       | 27.85       |
| Finglas A 110 kV        | 29.89        | 11.38       | 10.52       | 28.17        | 12.98       | 12.59       | 28.34        | 14.48       | 12.83       | 27.80        | 15.64       | 14.94       |
| Finglas B 110 kV        | 29.91        | 11.13       | 10.50       | 28.35        | 14.17       | 13.81       | 33.43        | 14.54       | 13.29       | 30.25        | 17.87       | 17.21       |
| Flagford 110 kV         | 4.70         | 9.81        | 9.25        | 5.40         | 12.07       | 11.78       | 4.48         | 13.83       | 12.51       | 5.40         | 15.84       | 15.23       |
| Flagford 220 kV         | 7.08         | 6.24        | 5.95        | 8.98         | 6.07        | 5.98        | 7.40         | 8.15        | 7.74        | 9.71         | 7.21        | 7.10        |
| Fortunestown 110 kV     | 5.81         | 7.28        | 6.82        | 5.69         | 5.55        | 5.45        | 5.55         | 8.42        | 7.61        | 5.56         | 6.04        | 5.89        |
| Francis Street A 110 kV | 11.04        | 11.95       | 11.17       | 5.27         | 14.32       | 13.93       | 10.51        | 14.04       | 12.61       | 5.06         | 16.27       | 15.58       |
| Francis Street B 110 kV | 13.54        | 11.58       | 10.93       | 6.82         | 14.20       | 13.86       | 12.79        | 13.31       | 12.36       | 6.51         | 16.00       | 15.52       |
| Galway 110 kV           | 5.11         | 10.08       | 9.50        | 4.66         | 12.41       | 12.10       | 5.12         | 15.03       | 13.58       | 4.52         | 16.95       | 16.29       |
| Garrow 110 kV           | 10.30        | 6.96        | 6.80        | 10.30        | 8.41        | 8.33        | 10.39        | 12.01       | 10.55       | 10.33        | 12.55       | 11.97       |
| Garvagh 110 kV          | 4.17         | 5.22        | 5.04        | 5.31         | 5.08        | 5.02        | 4.61         | 7.72        | 6.80        | 6.15         | 6.33        | 6.11        |
| Gilra 110 kV            | 3.26         | 5.77        | 5.54        | 4.05         | 4.64        | 4.59        | 3.01         | 6.98        | 6.59        | 3.96         | 5.16        | 5.09        |
| Glanagow 220 kV         | 14.00        | 11.39       | 10.91       | 13.89        | 14.93       | 14.64       | 14.34        | 19.77       | 18.34       | 13.99        | 24.45       | 23.67       |
| Glanlee 110 kV          | 4.96         | 4.99        | 4.91        | 5.17         | 6.01        | 5.97        | 5.04         | 8.19        | 7.13        | 5.35         | 8.78        | 8.33        |
| Glasmore A 110 kV       | 4.93         | 6.26        | 5.93        | 5.31         | 4.57        | 4.51        | 4.66         | 7.53        | 6.81        | 5.19         | 5.03        | 4.92        |
| Glenlara A 110 kV       | 3.07         | 2.69        | 2.63        | 4.32         | 2.35        | 2.34        | 3.26         | 3.44        | 3.16        | 4.77         | 2.75        | 2.68        |
| Glenlara B 110 kV       | 8.76         | 5.47        | 5.37        | 6.55         | 6.21        | 6.17        | 9.11         | 8.69        | 7.78        | 6.11         | 8.58        | 8.26        |
| Glenree 110 kV          | 3.31         | 3.77        | 3.59        | 4.04         | 3.68        | 3.62        | 3.72         | 6.01        | 5.58        | 4.66         | 4.85        | 4.75        |
| Golagh 110 kV           | 3.51         | 4.68        | 4.48        | 4.11         | 4.68        | 4.62        | 3.94         | 8.15        | 6.77        | 4.77         | 6.43        | 6.10        |
| Gorman 110 kV           | 6.79         | 12.96       | 12.08       | 7.66         | 14.48       | 14.10       | 6.02         | 16.05       | 14.63       | 7.09         | 17.00       | 16.44       |
| Gorman 220 kV           | 9.42         | 10.16       | 9.55        | 10.10        | 8.72        | 8.56        | 8.43         | 12.40       | 11.76       | 9.54         | 9.88        | 9.74        |
| Gortawee 110 kV         | 4.38         | 5.77        | 5.45        | 5.82         | 4.87        | 4.80        | 4.47         | 7.04        | 6.45        | 6.13         | 5.35        | 5.23        |
| Grange 110 kV           | 13.17        | 10.05       | 9.34        | 4.53         | 10.63       | 10.36       | 12.11        | 12.53       | 11.19       | 4.23         | 12.42       | 11.94       |
| Grange Castle 110 kV    | 17.52        | 11.34       | 10.33       | 11.67        | 12.75       | 12.30       | 16.80        | 13.50       | 11.93       | 11.20        | 14.55       | 13.88       |
| Great Island 110 kV     | 8.34         | 11.32       | 10.95       | 9.14         | 14.94       | 14.72       | 7.49         | 14.19       | 13.12       | 8.38         | 17.99       | 17.39       |
| Great Island 220 kV     | 11.81        | 10.25       | 10.08       | 13.21        | 12.74       | 12.66       | 10.48        | 12.30       | 11.88       | 12.01        | 14.42       | 14.22       |
| Griffinrath A 110 kV    | 7.31         | 9.41        | 9.03        | 7.56         | 9.70        | 9.57        | 7.49         | 10.07       | 9.59        | 7.73         | 10.29       | 10.11       |
| Griffinrath B 110 kV    | 7.86         | 9.71        | 9.31        | 7.72         | 9.70        | 9.57        | 8.07         | 10.39       | 9.88        | 7.89         | 10.27       | 10.10       |
| Harolds Cross 110 kV    | 11.23        | 11.99       | 11.21       | 4.97         | 14.28       | 13.89       | 10.70        | 14.08       | 12.65       | 4.78         | 16.20       | 15.52       |
| Heuston 110 kV          | 14.69        | 11.80       | 11.13       | 8.23         | 14.61       | 14.26       | 13.87        | 13.58       | 12.60       | 7.85         | 16.51       | 16.00       |
| Huntstown A 220 kV      | 15.09        | 15.81       | 14.39       | 13.48        | 20.64       | 19.77       | 14.90        | 22.87       | 20.68       | 12.74        | 28.09       | 26.90       |
| Huntstown B 220 kV      | 16.35        | 16.22       | 14.80       | 11.97        | 20.42       | 19.62       | 14.90        | 22.24       | 20.30       | 10.52        | 26.35       | 25.37       |
| Ikerrin 110 kV          | 5.08         | 4.02        | 3.91        | 5.89         | 3.20        | 3.17        | 5.72         | 5.77        | 5.22        | 6.46         | 3.82        | 3.73        |
| Inchicore 220 kV        | 16.94        | 19.43       | 17.50       | 11.50        | 24.39       | 23.29       | 13.89        | 25.05       | 22.36       | 9.73         | 29.81       | 28.41       |
| Inchicore A 110 kV      | 31.45        | 12.95       | 12.15       | 27.23        | 16.42       | 15.98       | 29.57        | 15.02       | 13.85       | 25.73        | 18.71       | 18.07       |
| Inchicore B 110 kV      | 48.98        | 12.99       | 11.81       | 37.60        | 16.62       | 15.94       | 45.54        | 15.64       | 13.77       | 35.02        | 19.47       | 18.42       |
| Inniscarra 110 kV       | 3.90         | 8.15        | 7.88        | 4.93         | 7.93        | 7.84        | 3.49         | 10.99       | 10.30       | 4.80         | 9.53        | 9.35        |
| Irishtown 220 kV        | 18.74        | 19.02       | 17.26       | 13.40        | 24.38       | 23.34       | 15.51        | 23.47       | 21.20       | 11.45        | 28.69       | 27.46       |
| Kellis 110 kV           | 6.38         | 7.83        | 7.57        | 7.30         | 9.47        | 9.34        | 6.16         | 9.99        | 9.29        | 7.22         | 11.48       | 11.16       |

|                     | Summer Winter |         |       |       |          |       |       |         | nter  |       |         |       |
|---------------------|---------------|---------|-------|-------|----------|-------|-------|---------|-------|-------|---------|-------|
|                     | Tł            | ree pha | se    | Si    | ngle Pha | ase   | Th    | ree pha | se    | Si    | ngle Ph | ase   |
| Station             | X/R           | lk"     | lk'   | X/R   | lk"      | lk'   | X/R   | lk"     | lk'   | X/R   | lk"     | lk'   |
|                     | Ratio         | [kA]    | [kA]  | Ratio | [kA]     | [kA]  | Ratio | [kA]    | [kA]  | Ratio | [kA]    | [kA]  |
| Kellis 220 kV       | 8.12          | 7.12    | 6.93  | 9.75  | 6.34     | 6.29  | 7.76  | 8.50    | 8.21  | 9.59  | 7.13    | 7.06  |
| Kilbarry 110 kV     | 7.56          | 14.87   | 14.03 | 8.07  | 16.61    | 16.24 | 6.31  | 23.01   | 20.48 | 7.21  | 22.45   | 21.58 |
| Kildonan 110 kV     | 7.55          | 14.95   | 13.74 | 6.29  | 14.85    | 14.43 | 6.82  | 17.39   | 16.14 | 5.88  | 16.59   | 16.19 |
| Kilgarvan 110 kV    | 9.70          | 4.90    | 4.82  | 7.00  | 3.48     | 3.47  | 10.04 | 7.97    | 7.08  | 6.65  | 4.16    | 4.07  |
| Kilkenny 110 kV     | 3.03          | 4.70    | 4.58  | 4.25  | 4.34     | 4.30  | 2.99  | 5.66    | 5.25  | 4.31  | 4.85    | 4.74  |
| Kill Hill 110 kV    | 4.80          | 4.97    | 4.81  | 5.80  | 4.63     | 4.58  | 5.59  | 7.57    | 6.70  | 6.78  | 5.89    | 5.70  |
| Killonan 110 kV     | 7.26          | 14.16   | 13.15 | 8.16  | 16.53    | 16.05 | 6.99  | 23.73   | 21.08 | 8.38  | 23.98   | 23.00 |
| Killonan 220 kV     | 8.09          | 8.33    | 7.92  | 9.88  | 8.50     | 8.35  | 7.97  | 12.47   | 11.80 | 10.42 | 11.00   | 10.82 |
| Killoteran 110 kV   | 7.52          | 10.37   | 10.00 | 7.64  | 11.84    | 11.68 | 6.76  | 13.03   | 11.99 | 7.09  | 14.02   | 13.60 |
| Kilmahud 110 kV     | 18.90         | 11.43   | 10.40 | 12.81 | 12.88    | 12.42 | 17.95 | 13.58   | 11.99 | 12.24 | 14.69   | 14.02 |
| Kilmore 110 kV      | 15.04         | 10.26   | 9.52  | 9.67  | 11.67    | 11.33 | 13.89 | 12.81   | 11.43 | 9.10  | 13.83   | 13.25 |
| Kilpaddoge 110 kV   | 11.14         | 12.94   | 12.15 | 11.64 | 16.77    | 16.31 | 11.94 | 20.13   | 18.26 | 12.72 | 24.03   | 23.07 |
| Kilpaddoge 220 kV   | 11.12         | 10.16   | 9.59  | 10.90 | 13.89    | 13.52 | 15.39 | 22.73   | 20.52 | 13.98 | 27.86   | 26.66 |
| Kilteel 110 kV      | 4.40          | 6.87    | 6.60  | 5.38  | 6.43     | 6.35  | 4.42  | 8.32    | 7.82  | 5.51  | 7.28    | 7.14  |
| Kinnegad 110 kV     | 4.43          | 6.95    | 6.66  | 5.22  | 6.57     | 6.48  | 4.37  | 7.68    | 7.34  | 5.30  | 7.01    | 6.91  |
| Knockacummer 110 kV | 7.83          | 4.85    | 4.77  | 7.01  | 5.24     | 5.21  | 8.00  | 7.38    | 6.71  | 6.91  | 7.11    | 6.89  |
| Knockalough 110 kV  | 3.98          | 3.99    | 3.87  | 3.61  | 4.05     | 4.01  | 4.35  | 5.26    | 4.82  | 3.72  | 4.84    | 4.70  |
| Knockanure 220 kV   | 8.75          | 7.57    | 7.26  | 6.36  | 10.21    | 10.01 | 13.14 | 17.99   | 16.27 | 7.59  | 22.01   | 21.08 |
| Knockanure A 110 kV | 14.77         | 8.09    | 7.86  | 12.29 | 9.75     | 9.64  | 21.87 | 15.28   | 12.79 | 16.82 | 15.61   | 14.62 |
| Knockanure B 110 kV | 5.03          | 7.05    | 6.77  | 5.91  | 6.20     | 6.12  | 4.63  | 9.58    | 8.83  | 5.79  | 7.34    | 7.19  |
| Knockearagh 110 kV  | 5.48          | 4.99    | 4.82  | 7.17  | 4.41     | 4.37  | 5.43  | 6.38    | 5.85  | 7.38  | 5.12    | 5.00  |
| Knocknamona 110 kV  | -             | -       | -     | -     | -        | -     | 6.45  | 7.77    | 6.84  | 7.17  | 5.04    | 4.90  |
| Knockraha A 110 kV  | 9.36          | 15.99   | 15.13 | 9.86  | 17.18    | 16.83 | 7.98  | 24.29   | 21.96 | 8.92  | 22.71   | 21.97 |
| Knockraha A 220 kV  | 12.41         | 11.87   | 11.34 | 12.29 | 14.22    | 13.95 | 11.60 | 20.04   | 18.51 | 11.44 | 20.77   | 20.18 |
| Knockraha B 110 kV  | 9.36          | 15.99   | 15.13 | 9.86  | 17.18    | 16.83 | 7.98  | 24.29   | 21.96 | 8.92  | 22.71   | 21.97 |
| Knockraha B 220 kV  | 12.41         | 11.87   | 11.34 | 12.29 | 14.22    | 13.95 | 11.60 | 20.04   | 18.51 | 11.44 | 20.77   | 20.18 |
| Knockranny 110 kV   | 5.44          | 6.40    | 6.16  | 4.97  | 8.37     | 8.23  | 6.15  | 9.06    | 8.51  | 5.27  | 11.22   | 10.93 |
| Knockranny A 110 kV | 3.85          | 4.48    | 4.33  | 3.51  | 4.44     | 4.39  | 4.12  | 5.95    | 5.44  | 3.59  | 5.29    | 5.14  |
| Knockranny B 110 kV | 5.44          | 6.40    | 6.16  | 4.97  | 8.37     | 8.23  | 6.15  | 9.06    | 8.51  | 5.27  | 11.22   | 10.93 |
| Knockumber 110 kV   | 3.89          | 7.86    | 7.45  | 4.67  | 6.00     | 5.92  | 3.58  | 9.01    | 8.44  | 4.50  | 6.50    | 6.39  |
| Lanesboro 110 kV    | 3.22          | 7.73    | 7.39  | 3.97  | 8.71     | 8.56  | 3.69  | 11.77   | 10.84 | 4.92  | 11.75   | 11.42 |
| Letterkenny110 kV   | 3.75          | 5.59    | 5.28  | 4.40  | 6.49     | 6.35  | 4.37  | 10.50   | 8.55  | 5.47  | 9.96    | 9.28  |
| Liberty A 110 kV    | 6.23          | 13.09   | 12.42 | 5.27  | 15.52    | 15.19 | 5.13  | 19.03   | 17.22 | 4.48  | 20.49   | 19.73 |
| Liberty B 110 kV    | 6.14          | 13.08   | 12.41 | 5.12  | 15.49    | 15.16 | 5.04  | 19.00   | 17.20 | 4.35  | 20.42   | 19.68 |
| Limerick 110 kV     | 5.73          | 12.63   | 11.71 | 6.33  | 12.63    | 12.30 | 4.99  | 19.39   | 17.39 | 5.98  | 16.50   | 15.98 |
| Lisdrum 110 kV      | 2.89          | 4.76    | 4.60  | 4.15  | 4.20     | 4.16  | 2.80  | 5.79    | 5.29  | 4.24  | 4.65    | 4.54  |
| Lisheen 110 kV      | 3.93          | 3.18    | 3.10  | 3.93  | 4.78     | 4.72  | 5.05  | 5.49    | 4.63  | 5.01  | 8.07    | 7.39  |
| Lodgewood 110 kV    | 9.68          | 7.38    | 7.22  | 9.77  | 9.32     | 9.24  | 9.66  | 9.65    | 8.99  | 9.63  | 11.30   | 10.98 |
| Lodgewood 220 kV    | 9.12          | 6.66    | 6.52  | 10.14 | 6.62     | 6.57  | 8.90  | 8.10    | 7.78  | 9.97  | 7.57    | 7.47  |
| Longpoint 220 kV    | 13.59         | 10.56   | 10.24 | 13.61 | 13.79    | 13.60 | 14.03 | 20.20   | 18.72 | 12.22 | 24.55   | 23.77 |
| Louth 220 kV        | 10.51         | 13.82   | 12.59 | 11.36 | 16.25    | 15.64 | 9.16  | 18.95   | 17.37 | 10.41 | 20.55   | 19.89 |
| Louth A 110 kV      | 7.35          | 11.46   | 10.82 | 8.31  | 13.96    | 13.63 | 6.33  | 14.13   | 12.97 | 7.48  | 16.46   | 15.91 |

|                      |       |          | Sum   | mer   |          |       | Winter |          |       |       |         |       |  |
|----------------------|-------|----------|-------|-------|----------|-------|--------|----------|-------|-------|---------|-------|--|
|                      | Th    | iree pha |       | 1     | ngle Pha | ise   | Th     | iree pha |       |       | ngle Ph | ase   |  |
|                      | X/R   | lk"      | lk'   | X/R   | lk"      | lk'   | X/R    | lk"      | lk'   | X/R   | lk"     | lk'   |  |
| Station              | Ratio | [kA]     | [kA]  | Ratio | [kA]     | [kA]  | Ratio  | [kA]     | [kA]  | Ratio | [kA]    | [kA]  |  |
| Louth A 275 kV       | 12.03 | 8.59     | 7.90  | 11.74 | 10.41    | 10.05 | 10.94  | 11.53    | 10.76 | 10.89 | 13.13   | 12.78 |  |
| Louth B 110 kV       | 7.89  | 12.34    | 11.60 | 8.66  | 15.40    | 15.00 | 6.70   | 15.39    | 14.14 | 7.67  | 18.43   | 17.80 |  |
| Louth B 275 kV       | 11.38 | 8.62     | 7.92  | 10.47 | 10.56    | 10.19 | 10.31  | 11.46    | 10.70 | 9.60  | 13.29   | 12.93 |  |
| Macetown 110 kV      | 7.88  | 15.53    | 14.24 | 7.49  | 16.39    | 15.88 | 7.10   | 18.19    | 16.81 | 6.96  | 18.45   | 17.95 |  |
| Macroom 110 kV       | 7.08  | 11.33    | 10.83 | 7.00  | 13.10    | 12.87 | 6.88   | 18.22    | 16.38 | 6.82  | 18.29   | 17.62 |  |
| Mallow 110 kV        | 5.27  | 5.90     | 5.73  | 6.86  | 5.27     | 5.22  | 5.16   | 7.49     | 7.02  | 7.01  | 6.11    | 6.00  |  |
| Marina 110 kV        | 7.29  | 14.24    | 13.46 | 8.09  | 17.11    | 16.72 | 6.04   | 21.48    | 19.22 | 7.12  | 23.29   | 22.33 |  |
| Maynooth A 110 kV    | 11.30 | 11.58    | 11.03 | 11.87 | 14.42    | 14.13 | 11.80  | 12.39    | 11.72 | 12.40 | 15.26   | 14.91 |  |
| Maynooth A 220 kV    | 11.00 | 15.56    | 14.40 | 10.32 | 15.47    | 15.07 | 9.30   | 19.43    | 18.11 | 9.25  | 18.06   | 17.65 |  |
| Maynooth B 110 kV    | 8.77  | 15.71    | 14.58 | 9.97  | 15.54    | 15.15 | 8.00   | 18.24    | 17.13 | 9.48  | 17.33   | 16.98 |  |
| Maynooth B 220 kV    | 11.73 | 17.44    | 15.97 | 10.44 | 17.57    | 17.04 | 9.84   | 22.94    | 21.18 | 9.28  | 21.30   | 20.76 |  |
| McDermott 110 kV     | 16.00 | 10.27    | 9.71  | 6.34  | 12.26    | 11.98 | 16.17  | 13.34    | 12.21 | 5.84  | 15.17   | 14.65 |  |
| Meath Hill 110 kV    | 4.12  | 8.18     | 7.80  | 5.23  | 6.93     | 6.84  | 3.81   | 10.03    | 9.21  | 5.12  | 7.83    | 7.66  |  |
| Meentycat 110 kV     | 3.22  | 4.19     | 4.02  | 4.07  | 4.25     | 4.19  | 3.67   | 7.09     | 5.99  | 5.02  | 5.85    | 5.57  |  |
| Midleton 110 kV      | 4.04  | 9.01     | 8.69  | 5.07  | 8.08     | 7.99  | 3.46   | 11.47    | 10.79 | 4.69  | 9.35    | 9.19  |  |
| Milltown A 110 kV    | 15.67 | 12.95    | 12.06 | 6.90  | 15.73    | 15.27 | 14.89  | 15.29    | 13.67 | 6.61  | 17.97   | 17.16 |  |
| Milltown B 110 kV    | 9.28  | 10.48    | 9.94  | 4.20  | 12.63    | 12.36 | 8.81   | 12.01    | 11.18 | 4.02  | 14.15   | 13.75 |  |
| Misery Hill 110 kV   | 13.95 | 12.64    | 11.78 | 7.61  | 15.49    | 15.04 | 13.26  | 14.92    | 13.34 | 7.30  | 17.72   | 16.92 |  |
| Moneteen 110 kV      | 5.86  | 9.70     | 9.06  | 6.52  | 7.71     | 7.57  | 5.23   | 12.63    | 11.71 | 6.23  | 8.84    | 8.68  |  |
| Moneypoint 110 kV    | 12.88 | 7.72     | 7.48  | 15.23 | 8.16     | 8.07  | 15.08  | 10.67    | 10.06 | 18.04 | 10.13   | 9.94  |  |
| Moneypoint 220 kV    | 11.23 | 10.14    | 9.57  | 10.96 | 13.86    | 13.49 | 15.68  | 22.47    | 20.34 | 13.96 | 27.59   | 26.43 |  |
| Moneypoint G1 400 kV | 13.50 | 5.91     | 5.63  | 15.18 | 7.31     | 7.17  | 20.94  | 10.81    | 10.22 | 23.62 | 11.74   | 11.50 |  |
| Moneypoint G2 400 kV | 23.08 | 2.74     | 2.67  | 24.62 | 3.51     | 3.47  | 51.58  | 4.95     | 4.73  | 49.42 | 5.67    | 5.57  |  |
| Moneypoint G3 400 kV | 13.50 | 5.91     | 5.63  | 15.18 | 7.31     | 7.17  | 20.94  | 10.81    | 10.22 | 23.62 | 11.74   | 11.50 |  |
| Monread 110 kV       | 4.08  | 6.75     | 6.49  | 4.87  | 6.97     | 6.87  | 4.05   | 8.40     | 7.89  | 4.96  | 8.13    | 7.96  |  |
| Mount Lucas 110 kV   | 3.68  | 5.12     | 4.96  | 4.58  | 5.20     | 5.15  | 4.53   | 7.26     | 6.79  | 5.73  | 6.60    | 6.46  |  |
| Moy 110 kV           | 3.62  | 3.79     | 3.57  | 4.29  | 4.49     | 4.39  | 5.37   | 6.98     | 6.32  | 6.65  | 6.98    | 6.75  |  |
| Mullagharlin 110 kV  | 3.86  | 8.13     | 7.77  | 4.87  | 7.95     | 7.84  | 3.47   | 9.68     | 8.97  | 4.60  | 8.97    | 8.76  |  |
| Mullingar 110 kV     | 3.55  | 6.33     | 6.09  | 4.45  | 6.21     | 6.13  | 3.39   | 7.34     | 6.93  | 4.39  | 6.87    | 6.75  |  |
| Mulreavy 110 kV      | 3.86  | 4.92     | 4.71  | 4.47  | 5.80     | 5.70  | 5.09   | 9.37     | 7.47  | 6.20  | 9.07    | 8.37  |  |
| Mungret A 110 kV     | 5.50  | 9.26     | 8.67  | 6.19  | 7.20     | 7.07  | 4.89   | 11.91    | 11.08 | 5.91  | 8.18    | 8.04  |  |
| Mungret B 110 kV     | 5.49  | 9.27     | 8.68  | 6.18  | 7.20     | 7.08  | 4.88   | 11.93    | 11.10 | 5.90  | 8.19    | 8.05  |  |
| Nangor 110 kV        | 15.37 | 11.09    | 10.11 | 9.52  | 12.43    | 12.00 | 14.78  | 13.16    | 11.66 | 9.14  | 14.16   | 13.52 |  |
| Navan 110 kV         | 5.83  | 11.56    | 10.81 | 6.55  | 11.57    | 11.31 | 5.26   | 14.18    | 12.96 | 6.18  | 13.34   | 12.96 |  |
| Nenagh 110 kV        | 3.34  | 3.50     | 3.40  | 4.06  | 2.46     | 2.45  | 3.30   | 4.55     | 4.18  | 4.13  | 2.77    | 2.72  |  |
| Newbridge 110 kV     | 4.03  | 8.07     | 7.70  | 4.65  | 8.65     | 8.50  | 4.16   | 11.02    | 10.20 | 4.93  | 10.82   | 10.55 |  |
| Newbury 110 kV       | 14.18 | 10.18    | 9.45  | 7.25  | 11.34    | 11.01 | 13.07  | 12.69    | 11.33 | 6.79  | 13.37   | 12.82 |  |
| North Quays 110 kV   | 19.51 | 13.21    | 12.29 | 6.42  | 15.75    | 15.30 | 18.53  | 15.63    | 13.95 | 6.15  | 17.98   | 17.17 |  |
| North Wall 220 kV    | 14.93 | 15.24    | 13.92 | 9.41  | 18.00    | 17.34 | 13.73  | 21.10    | 19.24 | 8.25  | 23.12   | 22.31 |  |
| Oldcourt A 110 kV    | 4.25  | 9.05     | 8.76  | 4.70  | 7.34     | 7.28  | 3.64   | 11.46    | 10.89 | 4.36  | 8.44    | 8.33  |  |
| Oldcourt B 110 kV    | 4.29  | 9.10     | 8.81  | 4.73  | 7.41     | 7.35  | 3.67   | 11.54    | 10.96 | 4.38  | 8.53    | 8.41  |  |
| Oldstreet 220 kV     | 15.42 | 9.30     | 8.85  | 13.20 | 10.51    | 10.31 | 14.64  | 11.37    | 10.96 | 12.48 | 12.36   | 12.19 |  |

|                      |       |         | Sum   | nmer  |          |       |       |         | Wi    | nter  |          |       |
|----------------------|-------|---------|-------|-------|----------|-------|-------|---------|-------|-------|----------|-------|
|                      | Th    | ree pha | se    | Si    | ngle Pha | ise   | Th    | ree pha | se    | Si    | ngle Pha | ase   |
|                      | X/R   | lk"     | lk'   | X/R   | lk"      | lk'   | X/R   | lk"     | lk'   | X/R   | lk"      | lk'   |
| Station              | Ratio | [kA]    | [kA]  | Ratio | [kA]     | [kA]  | Ratio | [kA]    | [kA]  | Ratio | [kA]     | [kA]  |
| Oldstreet 400 kV     | 13.77 | 6.06    | 5.78  | 10.78 | 6.20     | 6.09  | 12.40 | 8.22    | 7.94  | 9.78  | 7.70     | 7.62  |
| Oughtragh 110 kV     | 3.77  | 4.08    | 3.95  | 4.81  | 2.84     | 2.81  | 3.60  | 5.06    | 4.68  | 4.78  | 3.11     | 3.05  |
| Pelletstown 110 kV   | 14.02 | 9.77    | 9.27  | 8.10  | 10.80    | 10.59 | 13.55 | 12.49   | 11.51 | 7.58  | 13.09    | 12.70 |
| Platin 110 kV        | 5.21  | 11.35   | 10.64 | 5.79  | 8.82     | 8.67  | 4.61  | 13.39   | 12.41 | 5.45  | 9.74     | 9.56  |
| Pollaphuca 110 kV    | 2.78  | 2.42    | 2.39  | 3.98  | 2.25     | 2.24  | 3.22  | 3.08    | 3.00  | 4.66  | 2.59     | 2.57  |
| Poolbeg A 110 kV     | 29.38 | 13.79   | 12.80 | 23.08 | 17.30    | 16.76 | 27.92 | 16.35   | 14.59 | 22.03 | 19.96    | 19.01 |
| Poolbeg A 220 kV     | 15.97 | 15.44   | 14.09 | 8.15  | 17.21    | 16.60 | 14.66 | 21.32   | 19.42 | 7.07  | 21.83    | 21.10 |
| Poolbeg B 110 kV     | 29.34 | 13.77   | 12.79 | 23.06 | 17.28    | 16.74 | 27.88 | 16.33   | 14.57 | 22.02 | 19.94    | 18.99 |
| Poolbeg B 220 kV     | 16.20 | 18.28   | 16.55 | 11.05 | 21.39    | 20.53 | 13.54 | 23.35   | 20.96 | 9.58  | 25.80    | 24.73 |
| Poolbeg C 110 kV     | 22.29 | 13.49   | 12.53 | 7.49  | 16.12    | 15.64 | 21.16 | 15.99   | 14.24 | 7.16  | 18.45    | 17.61 |
| Poppintree 110 kV    | 15.92 | 10.53   | 9.77  | 9.86  | 11.96    | 11.62 | 14.76 | 13.21   | 11.78 | 9.29  | 14.23    | 13.63 |
| Portan 260 kV        | 22.24 | 8.48    | 8.12  | 86.66 | 2.96     | 2.95  | 19.72 | 11.05   | 10.71 | 86.99 | 3.12     | 3.11  |
| Portan 400 kV        | 18.69 | 6.79    | 6.45  | 17.95 | 7.91     | 7.75  | 16.07 | 8.92    | 8.58  | 15.97 | 10.02    | 9.87  |
| Portlaoise 110 kV    | 3.79  | 7.15    | 6.87  | 4.91  | 7.03     | 6.94  | 4.01  | 9.94    | 9.19  | 5.43  | 8.71     | 8.51  |
| Pottery 110 kV       | 18.62 | 10.62   | 10.10 | 5.76  | 10.94    | 10.75 | 17.66 | 12.23   | 11.38 | 5.56  | 12.15    | 11.86 |
| Prospect 220 kV      | 10.26 | 9.20    | 8.73  | 8.52  | 11.08    | 10.84 | 11.48 | 17.91   | 16.55 | 8.15  | 18.22    | 17.71 |
| Raffeen 220 kV       | 13.55 | 11.28   | 10.82 | 13.16 | 14.77    | 14.50 | 13.16 | 18.43   | 17.11 | 10.98 | 22.07    | 21.40 |
| Raffeen A 110 kV     | 6.66  | 12.06   | 11.55 | 7.41  | 14.80    | 14.54 | 5.54  | 16.38   | 15.27 | 6.43  | 18.84    | 18.32 |
| Raffeen B 110 kV     | 9.17  | 11.80   | 11.29 | 9.91  | 14.43    | 14.17 | 7.80  | 16.49   | 15.25 | 8.74  | 18.73    | 18.16 |
| Rathkeale 110 kV     | 3.72  | 6.53    | 6.23  | 4.85  | 5.42     | 5.35  | 3.46  | 8.22    | 7.73  | 4.82  | 6.11     | 6.02  |
| Ratrussan 110 kV     | 3.26  | 6.03    | 5.80  | 4.07  | 6.81     | 6.71  | 3.95  | 9.19    | 7.26  | 5.09  | 8.90     | 8.19  |
| Reamore 110 kV       | 3.89  | 6.82    | 6.53  | 4.26  | 6.40     | 6.31  | 3.73  | 9.94    | 8.77  | 4.23  | 7.95     | 7.67  |
| Richmond A 110 kV    | 2.88  | 5.66    | 5.46  | 3.81  | 5.51     | 5.45  | 3.01  | 7.71    | 7.21  | 4.22  | 6.76     | 6.62  |
| Richmond B 110 kV    | 2.88  | 5.66    | 5.46  | 3.81  | 5.51     | 5.45  | 3.01  | 7.71    | 7.21  | 4.22  | 6.76     | 6.62  |
| Rinawade 110 kV      | 5.12  | 9.99    | 9.49  | 5.99  | 7.40     | 7.31  | 4.82  | 11.28   | 10.80 | 5.86  | 8.03     | 7.94  |
| Ringaskiddy 110 kV   | 6.42  | 10.06   | 9.69  | 6.57  | 10.26    | 10.13 | 5.42  | 13.40   | 12.56 | 5.89  | 12.45    | 12.20 |
| Ringsend 110 kV      | 29.91 | 13.89   | 12.88 | 24.43 | 17.43    | 16.87 | 28.41 | 16.53   | 14.68 | 23.31 | 20.17    | 19.17 |
| Ryebrook 110 kV      | 6.10  | 14.50   | 13.21 | 6.76  | 12.91    | 12.55 | 5.24  | 15.03   | 13.94 | 6.20  | 13.09    | 12.79 |
| Salthill 110 kV      | 4.61  | 9.69    | 9.15  | 3.82  | 11.70    | 11.42 | 4.52  | 14.31   | 12.94 | 3.57  | 15.74    | 15.15 |
| Screeb 110 kV        | 3.66  | 2.38    | 2.31  | 4.27  | 1.60     | 1.59  | 3.83  | 2.88    | 2.65  | 4.41  | 1.72     | 1.69  |
| Seal Rock A 110 kV   | 8.66  | 9.19    | 8.36  | 10.30 | 10.35    | 9.97  | 7.60  | 10.46   | 9.61  | 9.36  | 11.07    | 10.73 |
| Seal Rock B 110 kV   | 8.66  | 9.19    | 8.36  | 10.30 | 10.35    | 9.97  | 7.60  | 10.46   | 9.61  | 9.36  | 11.07    | 10.73 |
| Shankill 110 kV      | 3.72  | 7.20    | 6.85  | 4.71  | 6.88     | 6.77  | 3.88  | 10.35   | 8.60  | 5.12  | 8.53     | 8.08  |
| Shannonbridge 110 kV | 5.01  | 10.66   | 10.14 | 5.87  | 13.01    | 12.75 | 5.57  | 16.69   | 15.83 | 7.28  | 18.59    | 18.22 |
| Shannonbridge 220 kV | 6.57  | 5.97    | 5.77  | 8.68  | 5.52     | 5.46  | 7.00  | 7.58    | 7.39  | 9.68  | 6.39     | 6.35  |
| Shellybanks A 220 kV | 15.78 | 15.42   | 14.07 | 8.14  | 19.33    | 18.58 | 14.47 | 21.28   | 19.40 | 6.93  | 25.10    | 24.15 |
| Shellybanks B 220 kV | 17.99 | 18.49   | 16.81 | 11.45 | 23.32    | 22.36 | 14.93 | 22.64   | 20.51 | 9.87  | 27.23    | 26.11 |
| Shelton Abbey 110 kV | 7.83  | 6.85    | 6.67  | 7.76  | 7.31     | 7.24  | 7.49  | 8.40    | 7.96  | 7.55  | 8.51     | 8.35  |
| Singland 110 kV      | 6.60  | 12.02   | 11.25 | 7.37  | 12.59    | 12.29 | 6.36  | 18.84   | 17.04 | 7.50  | 16.81    | 16.30 |
| Sliabh Bawn 110 kV   | 3.14  | 7.14    | 6.86  | 3.95  | 7.33     | 7.22  | 3.45  | 10.46   | 9.59  | 4.58  | 9.39     | 9.15  |
| Slievecallan 110 kV  | 6.51  | 5.11    | 4.96  | 8.65  | 2.21     | 2.21  | 7.81  | 7.79    | 6.77  | 9.40  | 2.43     | 2.39  |
| Sligo 110 kV         | 3.94  | 7.35    | 6.97  | 4.52  | 7.41     | 7.27  | 3.60  | 10.80   | 9.72  | 4.41  | 9.42     | 9.12  |
| -                    |       |         |       |       |          |       | -     | 1       |       | 1 1 1 |          | · ·   |

|                      |              | •           | Sum         | nmer         |             |             |              |             | Wi          | nter         |             |             |
|----------------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|
|                      | Th           | ree pha     | se          | Sir          | igle Pha    | ase         | Th           | ree pha     | se          | Si           | ngle Pha    | ase         |
| Station              | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] |
| Snugborough 110 kV   | 10.50        | 17.67       | 16.04       | 9.79         | 18.97       | 18.30       | 9.38         | 20.95       | 19.21       | 9.04         | 21.43       | 20.78       |
| Somerset 110 kV      | 3.12         | 6.32        | 6.13        | 4.00         | 4.50        | 4.47        | 2.89         | 8.14        | 7.82        | 3.96         | 5.11        | 5.07        |
| Sorne Hill 110 kV    | 2.74         | 2.32        | 2.25        | 3.39         | 2.67        | 2.64        | 3.51         | 3.81        | 3.33        | 4.45         | 3.68        | 3.51        |
| Srahnakilly 110 kV   | 3.42         | 3.31        | 3.17        | 3.80         | 4.14        | 4.06        | 5.25         | 6.57        | 5.66        | 5.86         | 7.04        | 6.65        |
| Srananagh 110 kV     | 4.78         | 8.30        | 7.85        | 5.46         | 9.51        | 9.31        | 4.56         | 12.75       | 11.35       | 5.53         | 12.89       | 12.37       |
| Srananagh 220 kV     | 6.63         | 4.01        | 3.87        | 8.68         | 3.43        | 3.40        | 7.32         | 5.12        | 4.89        | 9.67         | 3.93        | 3.88        |
| Stevenstown 110 kV   | 4.76         | 5.29        | 5.06        | 5.13         | 3.62        | 3.59        | 4.52         | 6.16        | 5.69        | 5.03         | 3.93        | 3.86        |
| Stratford 110 kV     | 3.18         | 3.68        | 3.61        | 4.14         | 3.00        | 2.98        | 3.32         | 4.58        | 4.36        | 4.34         | 3.38        | 3.33        |
| Taney 110 kV         | 9.20         | 9.21        | 8.81        | 3.29         | 9.19        | 9.06        | 8.79         | 10.49       | 9.83        | 3.19         | 10.10       | 9.89        |
| Tarbert 110 kV       | 18.24        | 9.96        | 9.61        | 20.92        | 11.26       | 11.11       | 30.20        | 13.89       | 13.34       | 32.60        | 14.26       | 14.06       |
| Tarbert 220 kV       | 10.87        | 9.89        | 9.34        | 10.96        | 13.34       | 13.00       | 14.78        | 21.82       | 19.77       | 14.32        | 26.15       | 25.08       |
| Tawnaghmore A 110 kV | 3.26         | 3.12        | 2.97        | 4.06         | 3.36        | 3.30        | 4.47         | 5.47        | 5.07        | 5.86         | 4.86        | 4.75        |
| Tawnaghmore B 110 kV | 3.73         | 3.39        | 3.18        | 4.54         | 3.96        | 3.87        | 5.04         | 5.74        | 5.31        | 6.59         | 5.79        | 5.64        |
| Thornsberry 110 kV   | 3.61         | 5.11        | 4.94        | 4.58         | 5.06        | 5.01        | 4.04         | 6.33        | 5.96        | 5.23         | 5.97        | 5.86        |
| Thurles 110 kV       | 4.99         | 4.12        | 3.99        | 5.36         | 4.78        | 4.73        | 6.15         | 7.04        | 5.99        | 6.47         | 6.98        | 6.59        |
| Tievebrack 110 kV    | 3.36         | 3.35        | 3.23        | 4.50         | 2.67        | 2.64        | 3.69         | 5.03        | 4.49        | 5.12         | 3.18        | 3.10        |
| Tipperary 110 kV     | 5.02         | 6.05        | 5.84        | 6.02         | 4.26        | 4.23        | 5.30         | 8.40        | 7.75        | 6.33         | 4.91        | 4.83        |
| Tonroe 110 kV        | 2.69         | 3.11        | 3.03        | 3.74         | 1.98        | 1.97        | 2.69         | 3.69        | 3.46        | 3.83         | 2.13        | 2.11        |
| Trabeg 110 kV        | 7.23         | 14.20       | 13.42       | 7.94         | 17.05       | 16.66       | 5.95         | 21.37       | 19.13       | 6.96         | 23.18       | 22.23       |
| Tralee 110 kV        | 5.07         | 7.20        | 6.88        | 5.97         | 6.80        | 6.70        | 5.10         | 10.67       | 9.37        | 6.20         | 8.52        | 8.22        |
| Trien A 110 kV       | 4.79         | 6.62        | 6.36        | 5.88         | 6.19        | 6.11        | 4.44         | 9.08        | 8.30        | 5.81         | 7.46        | 7.27        |
| Trien B 110 kV       | 11.18        | 6.77        | 6.62        | 9.22         | 6.10        | 6.06        | 12.88        | 12.37       | 10.27       | 9.21         | 8.29        | 7.92        |
| Trillick 110 kV      | 2.78         | 2.49        | 2.41        | 3.48         | 2.70        | 2.67        | 3.62         | 4.19        | 3.61        | 4.56         | 3.68        | 3.52        |
| Trinity 110 kV       | 12.26        | 12.30       | 11.48       | 6.34         | 14.93       | 14.51       | 11.66        | 14.48       | 12.98       | 6.08         | 17.03       | 16.28       |
| Tullabrack 110 kV    | 6.65         | 6.03        | 5.86        | 7.24         | 4.97        | 4.93        | 6.56         | 8.11        | 7.65        | 7.30         | 5.80        | 5.71        |
| Turlough 220 kV      | 11.51        | 10.90       | 10.44       | 12.66        | 10.39       | 10.25       | 10.29        | 12.44       | 12.00       | 11.79        | 11.22       | 11.10       |
| Tynagh 220 kV        | 16.18        | 10.06       | 9.49        | 17.48        | 11.87       | 11.59       | 14.99        | 12.21       | 11.67       | 16.43        | 13.69       | 13.45       |
| Uggool 110 kV        | 5.47         | 6.11        | 5.89        | 5.22         | 8.02        | 7.89        | 6.26         | 8.64        | 8.14        | 5.69         | 10.77       | 10.50       |
| Waterford 110 kV     | 7.71         | 10.80       | 10.40       | 8.07         | 12.27       | 12.10       | 6.91         | 13.65       | 12.54       | 7.48         | 14.59       | 14.14       |
| Wexford 110 kV       | 5.71         | 5.86        | 5.71        | 6.92         | 5.71        | 5.66        | 5.77         | 7.73        | 6.84        | 7.17         | 6.72        | 6.48        |
| Whitebank 110 kV     | 26.39        | 13.85       | 12.84       | 21.06        | 17.35       | 16.79       | 24.98        | 16.46       | 14.62       | 20.07        | 20.04       | 19.06       |
| Whitegate 110 kV     | 4.88         | 8.59        | 8.32        | 5.54         | 9.13        | 9.02        | 4.28         | 10.74       | 10.24       | 5.11         | 10.70       | 10.52       |
| Wolfe Tone 110 kV    | 14.34        | 10.07       | 9.53        | 5.80         | 11.89       | 11.63       | 14.16        | 13.03       | 11.94       | 5.33         | 14.64       | 14.15       |
| Woodhouse 110 kV     | 6.03         | 5.60        | 5.47        | 7.29         | 4.29        | 4.27        | 6.71         | 7.97        | 7.02        | 7.98         | 5.14        | 4.99        |
| Woodland 220 kV      | 14.30        | 17.42       | 15.93       | 13.47        | 19.69       | 19.01       | 11.86        | 23.49       | 21.68       | 11.74        | 24.89       | 24.16       |
| Woodland 400 kV      | 19.83        | 6.82        | 6.47        | 19.32        | 7.95        | 7.78        | 17.13        | 8.97        | 8.62        | 17.24        | 10.10       | 9.95        |

|                       |       |         | Sum   | mer   | -        | -     |       |         | Wi    | nter  |          |       |
|-----------------------|-------|---------|-------|-------|----------|-------|-------|---------|-------|-------|----------|-------|
|                       | Th    | ree pha | se    | Si    | ngle Pha | ase   | Th    | ree pha | se    | Si    | ngle Pha | ase   |
| <u> </u>              | X/R   | lk"     | lk'   | X/R   | lk"      | lk'   | X/R   | lk"     | lk'   | X/R   | lk"      | lk'   |
| Station               | Ratio | [kA]    | [kA]  | Ratio | [kA]     | [kA]  | Ratio | [kA]    | [kA]  | Ratio | [kA]     | [kA]  |
| Adamstown 110 kV      | 12.29 | 11.26   | 10.30 | 6.53  | 13.53    | 13.03 | 11.47 | 13.41   | 12.09 | 6.11  | 15.65    | 15.00 |
| Agannygal 110 kV      | 2.83  | 4.74    | 4.60  | 3.87  | 4.09     | 4.05  | 2.97  | 6.36    | 5.70  | 4.24  | 4.90     | 4.76  |
| Aghada 110 kV         | 5.16  | 7.67    | 7.21  | 6.09  | 9.11     | 8.88  | 4.57  | 9.95    | 9.46  | 5.62  | 11.27    | 11.05 |
| Aghada A 220 kV       | 11.27 | 10.06   | 8.99  | 12.12 | 13.43    | 12.74 | 13.52 | 20.52   | 18.22 | 14.72 | 24.51    | 23.30 |
| Aghada B 220 kV       | 11.27 | 10.06   | 8.99  | 12.12 | 13.43    | 12.74 | 13.52 | 20.52   | 18.22 | 14.72 | 24.51    | 23.30 |
| Aghada C 220 kV       | 11.05 | 9.84    | 8.81  | 11.11 | 13.12    | 12.46 | 12.80 | 19.69   | 17.55 | 12.15 | 23.57    | 22.44 |
| Aghada D 220 kV       | 11.27 | 10.06   | 8.99  | 12.12 | 13.43    | 12.74 | 13.52 | 20.52   | 18.22 | 14.72 | 24.51    | 23.30 |
| Ahane 110 kV          | 5.51  | 10.57   | 9.80  | 6.05  | 9.28     | 9.07  | 4.85  | 15.52   | 14.35 | 5.72  | 11.51    | 11.28 |
| Anner 110 kV          | 4.07  | 5.85    | 5.54  | 4.54  | 4.48     | 4.42  | 3.99  | 7.67    | 7.12  | 4.56  | 5.07     | 4.99  |
| Ardnacrusha 110 kV    | 6.03  | 11.52   | 10.56 | 7.17  | 12.94    | 12.51 | 5.91  | 19.05   | 17.06 | 7.57  | 18.34    | 17.68 |
| Ardnagappary 110 kV   | 2.77  | 1.88    | 1.83  | 3.93  | 1.22     | 1.22  | 2.90  | 2.61    | 2.43  | 4.26  | 1.35     | 1.34  |
| Arigna 110 kV         | 4.42  | 6.16    | 5.88  | 5.44  | 5.17     | 5.10  | 4.46  | 8.53    | 7.84  | 5.69  | 6.13     | 6.00  |
| Arklow 110 kV         | 10.71 | 7.72    | 7.40  | 11.57 | 9.41     | 9.25  | 10.30 | 10.27   | 9.68  | 11.50 | 11.83    | 11.56 |
| Arklow 220 kV         | 9.31  | 7.16    | 6.79  | 10.71 | 6.69     | 6.57  | 8.98  | 8.92    | 8.58  | 10.55 | 7.73     | 7.64  |
| Artane 110 kV         | 13.36 | 10.17   | 9.47  | 6.20  | 12.29    | 11.93 | 13.09 | 12.59   | 11.41 | 5.84  | 14.70    | 14.13 |
| Arva 110 kV           | 3.95  | 7.93    | 7.44  | 5.00  | 6.53     | 6.41  | 3.84  | 10.59   | 9.62  | 5.13  | 7.61     | 7.43  |
| Athea 110 kV          | 11.21 | 6.75    | 6.50  | 11.91 | 7.10     | 7.01  | 11.74 | 11.31   | 9.76  | 12.48 | 10.06    | 9.60  |
| Athlone 110 kV        | 4.05  | 6.32    | 6.02  | 5.29  | 5.21     | 5.14  | 3.84  | 7.75    | 7.21  | 5.22  | 5.66     | 5.56  |
| Athy 110 kV           | 3.37  | 5.61    | 5.41  | 4.50  | 4.74     | 4.69  | 4.73  | 8.25    | 7.92  | 5.97  | 6.50     | 6.43  |
| Aughinish 110 kV      | 9.13  | 9.58    | 8.49  | 11.12 | 10.57    | 10.08 | 8.33  | 12.35   | 11.34 | 10.64 | 12.32    | 11.96 |
| Ballinknockane 110 kV | 8.36  | 8.87    | 8.01  | 8.87  | 8.16     | 7.90  | 8.04  | 12.10   | 11.31 | 8.75  | 9.71     | 9.53  |
| Ballybeg 110 kV       | 9.91  | 6.05    | 5.84  | 10.15 | 7.17     | 7.07  | 9.65  | 7.25    | 6.93  | 9.98  | 8.30     | 8.16  |
| Ballydine 110 kV      | 4.11  | 6.51    | 6.19  | 3.82  | 5.34     | 5.27  | 3.94  | 8.33    | 7.81  | 3.73  | 6.07     | 5.97  |
| Ballylickey 110 kV    | 2.83  | 2.90    | 2.82  | 3.85  | 1.96     | 1.95  | 2.96  | 4.01    | 3.75  | 4.05  | 2.25     | 2.22  |
| Ballynahulla 110 kV   | 14.55 | 7.59    | 7.27  | 13.05 | 8.10     | 7.98  | 16.72 | 12.43   | 11.02 | 13.34 | 11.47    | 11.03 |
| Ballynahulla 220 kV   | 9.01  | 6.77    | 6.36  | 9.17  | 7.63     | 7.45  | 9.20  | 11.83   | 10.85 | 9.22  | 11.46    | 11.13 |
| Ballyragget 110 kV    | 4.53  | 2.97    | 2.89  | 5.96  | 2.14     | 2.12  | 5.50  | 7.36    | 7.02  | 6.55  | 4.96     | 4.91  |
| Ballyvouskill 110 kV  | 14.32 | 7.42    | 7.09  | 13.93 | 8.77     | 8.61  | 15.06 | 12.93   | 11.38 | 14.01 | 13.34    | 12.74 |
| Ballyvouskill 220 kV  | 8.88  | 6.71    | 6.29  | 9.51  | 8.36     | 8.13  | 9.17  | 11.96   | 10.92 | 9.97  | 13.29    | 12.83 |
| Ballywater 110 kV     | 5.56  | 5.41    | 5.25  | 3.47  | 5.62     | 5.57  | 5.31  | 7.48    | 7.18  | 3.17  | 6.91     | 6.82  |
| Baltrasna 110 kV      | 6.44  | 9.56    | 8.92  | 7.46  | 7.57     | 7.43  | 5.84  | 11.50   | 10.98 | 7.14  | 8.50     | 8.41  |
| Bancroft 110 kV       | 13.20 | 11.56   | 10.65 | 7.17  | 13.44    | 13.01 | 12.00 | 13.37   | 12.42 | 6.65  | 15.21    | 14.77 |
| Bandon 110 kV         | 3.38  | 5.60    | 5.29  | 4.36  | 5.62     | 5.51  | 3.09  | 7.92    | 7.26  | 4.33  | 7.07     | 6.88  |
| Banoge 110 kV         | 6.35  | 5.55    | 5.38  | 7.10  | 5.04     | 5.00  | 6.55  | 7.72    | 7.41  | 7.39  | 6.13     | 6.06  |
| Barnageeragh 110 kV   | 10.25 | 18.04   | 15.83 | 10.17 | 21.43    | 20.30 | 9.05  | 23.86   | 21.85 | 9.18  | 26.71    | 25.82 |
| Barnahealy A 110 kV   | 5.28  | 9.92    | 9.18  | 5.86  | 10.76    | 10.45 | 4.44  | 13.90   | 12.94 | 5.25  | 13.79    | 13.46 |
| Barnahealy B 110 kV   | 7.05  | 9.75    | 9.03  | 7.50  | 10.43    | 10.14 | 6.11  | 14.01   | 12.97 | 6.86  | 13.53    | 13.18 |
| Barnakyle 110 kV      | 20.22 | 18.31   | 16.26 | 21.00 | 13.00    | 12.62 | 18.24 | 21.46   | 19.74 | 19.81 | 14.23    | 13.96 |
| Baroda 110 kV         | 3.96  | 7.32    | 6.94  | 4.65  | 8.64     | 8.45  | 3.80  | 9.93    | 9.37  | 4.63  | 10.93    | 10.70 |
| Barrymore 110 kV      | 3.98  | 6.63    | 6.29  | 4.95  | 4.23     | 4.18  | 3.68  | 8.79    | 8.33  | 4.89  | 4.81     | 4.76  |
| Belcamp 110 kV        | 17.98 | 16.73   | 14.80 | 13.68 | 19.49    | 18.54 | 17.30 | 21.51   | 19.07 | 12.84 | 23.93    | 22.83 |
| Belcamp 220 kV        | 13.38 | 16.65   | 14.38 | 11.72 | 20.49    | 19.20 | 12.01 | 24.50   | 21.62 | 10.18 | 28.16    | 26.75 |

|                              |              |             | Sum         | mer          |             |             |              |             | Wi          | nter         |             |             |
|------------------------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|
|                              | Th           | ree pha     |             |              | ngle Pha    |             | Th           | iree pha    |             | 1            | ngle Pha    |             |
|                              |              | -           | 1           |              | , <b>-</b>  |             |              |             | 1           |              |             |             |
| Station                      | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] |
| Belgard 110 kV               | 12.76        | 11.90       | 10.88       | 6.96         | 14.48       | 13.94       | 11.83        | 13.74       | 12.59       | 6.52         | 16.45       | 15.86       |
| Bellacorick 110 kV           | 3.42         | 3.41        | 3.24        | 3.74         | 4.41        | 4.31        | 5.88         | 8.60        | 7.12        | 6.49         | 9.27        | 8.62        |
| Binbane 110 kV               | 3.20         | 3.48        | 3.34        | 4.32         | 3.44        | 3.40        | 3.81         | 6.73        | 6.21        | 5.82         | 5.00        | 4.89        |
| Blackrock 110 kV             | 10.45        | 12.07       | 11.12       | 2.49         | 11.64       | 11.33       | 9.82         | 14.29       | 12.79       | 2.38         | 13.01       | 12.56       |
| Blake 110 kV                 | 3.95         | 6.95        | 6.61        | 4.92         | 5.10        | 5.04        | 3.79         | 8.84        | 8.43        | 4.90         | 5.80        | 5.74        |
| Blundestown 110 kV           | 4.19         | 7.44        | 7.05        | 4.87         | 4.92        | 4.86        | 4.30         | 9.61        | 9.34        | 5.01         | 5.62        | 5.59        |
| Boggeragh 110 kV             | 6.19         | 6.09        | 5.83        | 7.26         | 6.71        | 6.60        | 6.66         | 9.32        | 8.52        | 7.99         | 8.96        | 8.70        |
| Booltiagh 110 kV             | 6.15         | 6.27        | 6.02        | 7.69         | 5.53        | 5.46        | 6.67         | 9.26        | 8.44        | 8.54         | 6.88        | 6.72        |
| Bracetown 220 kV             | 12.60        | 16.19       | 14.09       | 9.15         | 15.72       | 14.97       | 11.04        | 22.84       | 20.58       | 8.02         | 20.00       | 19.36       |
| Bracklone 110 kV             | 3.68         | 6.72        | 6.40        | 4.60         | 6.69        | 6.58        | 3.59         | 9.67        | 9.19        | 4.68         | 8.54        | 8.41        |
| Brinny A 110 kV              | 3.24         | 5.08        | 4.82        | 4.21         | 4.70        | 4.62        | 2.96         | 6.95        | 6.43        | 4.17         | 5.70        | 5.58        |
| Brinny B 110 kV              | 3.24         | 5.10        | 4.84        | 4.21         | 4.73        | 4.65        | 2.96         | 6.98        | 6.46        | 4.17         | 5.75        | 5.62        |
| Buffy 110 kV                 | 3.84         | 4.46        | 4.29        | 4.14         | 5.45        | 5.37        | 5.34         | 7.99        | 6.80        | 5.56         | 8.56        | 8.05        |
| Bunkimalta 110 kV            | 5.26         | 5.06        | 4.86        | 5.52         | 5.31        | 5.24        | 6.51         | 8.14        | 7.17        | 6.38         | 7.48        | 7.17        |
| Butlerstown 110 kV           | 6.94         | 9.59        | 9.08        | 7.05         | 9.99        | 9.79        | 6.22         | 12.66       | 11.79       | 6.53         | 12.04       | 11.77       |
| Cabra 110 kV                 | 12.39        | 9.84        | 9.18        | 5.04         | 11.09       | 10.80       | 12.07        | 12.14       | 11.02       | 4.75         | 13.10       | 12.63       |
| Cahir 110 kV                 | 4.39         | 7.22        | 6.82        | 5.41         | 6.21        | 6.11        | 4.56         | 10.78       | 9.75        | 5.80         | 7.51        | 7.33        |
| Carlow 110 kV                | 5.66         | 7.42        | 7.08        | 6.41         | 8.15        | 8.01        | 5.75         | 10.32       | 9.62        | 6.60         | 10.31       | 10.06       |
| Carrickaduff 110 kV          | 4.29         | 3.24        | 3.13        | 5.22         | 2.59        | 2.57        | 7.40         | 7.39        | 5.84        | 7.03         | 3.57        | 3.42        |
| Carrickalangan 110 kV        | 4.30         | 3.21        | 3.10        | 5.21         | 2.54        | 2.52        | 7.35         | 7.25        | 5.75        | 6.96         | 3.47        | 3.33        |
| Carrickmines 220 kV          | 17.20        | 18.04       | 15.60       | 9.73         | 21.69       | 20.36       | 13.39        | 23.12       | 20.64       | 7.90         | 26.53       | 25.33       |
| Carrickmines A 110 kV        | 34.08        | 11.40       | 10.59       | 24.57        | 12.47       | 12.13       | 31.29        | 13.27       | 12.25       | 22.93        | 14.07       | 13.67       |
| Carrickmines B 110 kV        | 27.63        | 12.79       | 11.75       | 21.77        | 15.28       | 14.75       | 24.54        | 14.98       | 13.85       | 19.70        | 17.49       | 16.95       |
| Carrick-on-Shannon 110<br>kV | 4.47         | 9.33        | 8.71        | 5.13         | 10.45       | 10.17       | 4.15         | 13.25       | 12.05       | 5.01         | 13.47       | 13.02       |
| Carrigadrohid 110 kV         | 6.94         | 10.04       | 9.33        | 7.10         | 10.28       | 10.01       | 6.54         | 16.03       | 14.60       | 6.85         | 13.92       | 13.53       |
| Carrigdangan 110 kV          | 3.46         | 4.30        | 4.14        | 4.12         | 5.11        | 5.03        | 4.12         | 7.03        | 6.12        | 5.20         | 7.35        | 6.98        |
| Carrowbeg 110 kV             | 2.72         | 2.53        | 2.43        | 3.59         | 2.38        | 2.35        | 2.68         | 3.41        | 3.15        | 3.74         | 2.86        | 2.80        |
| Cashla 110 kV                | 7.85         | 13.13       | 12.06       | 8.17         | 16.75       | 16.14       | 7.23         | 21.45       | 19.34       | 7.69         | 25.27       | 24.22       |
| Cashla 220 kV                | 8.67         | 9.04        | 8.33        | 9.71         | 9.39        | 9.12        | 8.56         | 12.94       | 12.20       | 9.79         | 12.13       | 11.90       |
| Castlebagot 110 kV           | 22.00        | 18.68       | 16.55       | 23.62        | 13.35       | 12.95       | 19.85        | 21.92       | 20.14       | 22.26        | 14.63       | 14.34       |
| Castlebagot 220 kV           | 12.67        | 19.88       | 16.96       | 10.40        | 21.09       | 19.83       | 9.75         | 27.01       | 24.03       | 8.47         | 26.54       | 25.48       |
| Castlebar 110 kV             | 3.15         | 4.15        | 3.94        | 3.70         | 4.66        | 4.57        | 3.35         | 6.86        | 6.08        | 4.13         | 6.48        | 6.23        |
| Castledockrill 110 kV        | 7.69         | 6.60        | 6.38        | 4.59         | 7.71        | 7.61        | 7.41         | 9.18        | 8.80        | 4.13         | 9.66        | 9.52        |
| Castlefarm A 110 kV          | 8.18         | 9.24        | 8.21        | 9.60         | 9.84        | 9.41        | 7.35         | 11.81       | 10.87       | 9.05         | 11.38       | 11.07       |
| Castlefarm B 110 kV          | 8.19         | 9.23        | 8.20        | 9.62         | 9.83        | 9.40        | 7.37         | 11.78       | 10.85       | 9.06         | 11.36       | 11.05       |
| Castleview 110 kV            | 4.45         | 9.88        | 9.17        | 4.86         | 7.92        | 7.75        | 3.70         | 13.94       | 12.96       | 4.48         | 9.59        | 9.43        |
| Cathaleen's Fall 110 kV      | 4.30         | 6.30        | 5.93        | 4.93         | 7.19        | 7.02        | 5.15         | 13.53       | 11.64       | 6.21         | 11.88       | 11.34       |
| Cauteen 110 kV               | 5.35         | 6.20        | 5.92        | 6.30         | 4.27        | 4.22        | 5.91         | 9.55        | 8.72        | 6.74         | 5.11        | 5.02        |
| Central Park 110 kV          | 15.26        | 10.44       | 9.75        | 7.83         | 11.19       | 10.91       | 14.24        | 12.06       | 11.19       | 7.44         | 12.54       | 12.21       |
| Charleville 110 kV           | 4.56         | 5.42        | 5.18        | 5.93         | 5.15        | 5.08        | 4.77         | 7.77        | 7.07        | 6.53         | 6.52        | 6.35        |
| Cherrywood 110 kV            | 10.75        | 9.67        | 9.06        | 7.65         | 9.84        | 9.62        | 10.11        | 11.07       | 10.32       | 7.31         | 10.94       | 10.68       |

|                      |       |         | Sum   | mer   |          |       |       |         | Wi    | nter  |         |       |
|----------------------|-------|---------|-------|-------|----------|-------|-------|---------|-------|-------|---------|-------|
|                      | Th    | ree pha | se    | Si    | ngle Pha | ase   | Th    | ree pha | se    | Si    | ngle Ph | ase   |
| Station              | X/R   | lk"     | lk'   | X/R   | lk"      | lk'   | X/R   | lk"     | lk'   | X/R   | lk"     | lk'   |
| Station              | Ratio | [kA]    | [kA]  | Ratio | [kA]     | [kA]  | Ratio | [kA]    | [kA]  | Ratio | [kA]    | [kA]  |
| City West 110 kV     | 6.17  | 7.36    | 6.89  | 6.12  | 5.59     | 5.49  | 5.84  | 8.59    | 7.82  | 5.93  | 6.14    | 6.00  |
| Clahane 110 kV       | 4.28  | 6.26    | 5.96  | 5.23  | 5.96     | 5.86  | 4.09  | 9.70    | 9.05  | 5.33  | 7.67    | 7.53  |
| Clashavoon 220 kV    | 8.94  | 7.23    | 6.71  | 9.65  | 8.75     | 8.48  | 9.14  | 12.60   | 11.59 | 10.01 | 13.52   | 13.10 |
| Clashavoon A 110 kV  | 7.85  | 11.39   | 10.50 | 8.16  | 14.84    | 14.32 | 7.90  | 19.76   | 17.65 | 8.26  | 23.53   | 22.45 |
| Clashavoon B 110 kV  | 7.85  | 11.39   | 10.50 | 8.16  | 14.84    | 14.32 | 7.90  | 19.76   | 17.65 | 8.26  | 23.53   | 22.45 |
| Cliff 110 kV         | 4.05  | 5.18    | 4.93  | 4.98  | 5.35     | 5.26  | 4.48  | 9.49    | 8.49  | 5.92  | 7.61    | 7.38  |
| Cloghboola 110 kV    | 7.44  | 5.86    | 5.67  | 9.66  | 6.16     | 6.09  | 7.52  | 9.67    | 8.20  | 10.87 | 8.66    | 8.21  |
| Cloghboola 110 kV    | 7.44  | 5.86    | 5.67  | 9.66  | 6.16     | 6.09  | 7.52  | 9.67    | 8.20  | 10.87 | 8.66    | 8.21  |
| Clogher 110 kV       | 3.89  | 5.25    | 4.98  | 4.43  | 6.08     | 5.95  | 5.34  | 12.75   | 10.19 | 6.30  | 10.97   | 10.22 |
| Cloghran 110 kV      | 10.17 | 18.16   | 15.91 | 10.49 | 21.65    | 20.50 | 8.96  | 24.05   | 21.99 | 9.51  | 27.04   | 26.12 |
| Clonee 220 kV        | 12.92 | 16.40   | 14.25 | 10.04 | 16.04    | 15.26 | 11.36 | 23.23   | 20.89 | 8.85  | 20.48   | 19.81 |
| Clonkeen A 110 kV    | 5.75  | 5.33    | 5.11  | 6.79  | 4.06     | 4.01  | 5.58  | 6.87    | 6.53  | 6.80  | 4.64    | 4.59  |
| Clonkeen B 110 kV    | 5.03  | 6.33    | 6.09  | 4.42  | 7.43     | 7.31  | 4.63  | 10.71   | 9.43  | 3.97  | 11.04   | 10.54 |
| Cloon 110 kV         | 4.54  | 6.67    | 6.34  | 5.85  | 5.98     | 5.89  | 4.07  | 8.80    | 8.21  | 5.65  | 7.10    | 6.97  |
| Clutterland 110 kV   | 20.23 | 18.27   | 16.22 | 20.01 | 13.01    | 12.63 | 18.26 | 21.40   | 19.69 | 18.87 | 14.24   | 13.97 |
| College Park 110 kV  | 9.32  | 16.81   | 14.89 | 6.53  | 20.10    | 19.11 | 8.20  | 21.91   | 20.20 | 5.70  | 24.96   | 24.18 |
| Cookstown 110 kV     | 7.48  | 8.14    | 7.69  | 6.01  | 6.91     | 6.80  | 7.01  | 9.18    | 8.72  | 5.78  | 7.56    | 7.45  |
| Cookstown A 110 kV   | 5.03  | 6.30    | 5.94  | 5.26  | 4.51     | 4.45  | 4.79  | 7.32    | 6.67  | 5.13  | 4.92    | 4.81  |
| Coolnabacky 110 kV   | -     | -       | -     | -     | -        | -     | 7.70  | 16.15   | 15.33 | 8.16  | 19.44   | 19.03 |
| Coolnabacky 400 kV   | -     | -       | -     | -     | -        | -     | 8.39  | 11.64   | 11.00 | 8.72  | 10.43   | 10.25 |
| Coolroe 110 kV       | 3.97  | 8.09    | 7.60  | 5.10  | 8.08     | 7.91  | 3.46  | 11.40   | 10.60 | 4.85  | 10.10   | 9.88  |
| Coomagearlahy 110 kV | 5.05  | 5.10    | 4.94  | 5.51  | 6.08     | 6.00  | 5.15  | 8.51    | 7.40  | 5.81  | 9.12    | 8.65  |
| Coomataggart 110 kV  | 9.79  | 4.96    | 4.81  | 7.01  | 3.44     | 3.41  | 10.06 | 8.13    | 7.24  | 6.64  | 4.20    | 4.12  |
| Coomataggart 110 kV  | 9.79  | 4.96    | 4.81  | 7.01  | 3.44     | 3.41  | 10.06 | 8.13    | 7.24  | 6.64  | 4.20    | 4.12  |
| Cordal 110 kV        | 11.91 | 6.54    | 6.31  | 8.28  | 6.99     | 6.89  | 13.01 | 10.60   | 9.43  | 7.62  | 9.80    | 9.43  |
| Corderry 110 kV      | 4.05  | 6.31    | 6.01  | 5.00  | 6.28     | 6.18  | 4.11  | 9.70    | 8.66  | 5.42  | 8.14    | 7.88  |
| Corduff 110 kV       | 10.74 | 19.30   | 16.83 | 11.62 | 23.42    | 22.10 | 9.46  | 26.03   | 23.71 | 10.57 | 29.89   | 28.81 |
| Corduff 220 kV       | 15.25 | 18.42   | 15.77 | 14.16 | 22.49    | 21.00 | 14.00 | 27.51   | 24.20 | 12.59 | 31.10   | 29.53 |
| Corkagh 110 kV       | 20.83 | 18.39   | 16.31 | 21.32 | 13.03    | 12.64 | 18.80 | 21.55   | 19.82 | 20.11 | 14.26   | 13.99 |
| Corraclassy 110 kV   | 4.35  | 5.81    | 5.47  | 5.43  | 4.72     | 4.64  | 4.28  | 7.48    | 7.01  | 5.58  | 5.32    | 5.24  |
| Cow Cross 110 kV     | 4.85  | 9.95    | 9.21  | 5.13  | 9.03     | 8.81  | 4.05  | 13.97   | 12.99 | 4.64  | 11.18   | 10.96 |
| Crane 110 kV         | 7.80  | 7.21    | 6.94  | 7.54  | 7.94     | 7.83  | 7.93  | 10.92   | 10.28 | 7.49  | 10.52   | 10.31 |
| Croaghaun 110 kV     | 3.50  | 3.19    | 3.04  | 3.90  | 4.03     | 3.95  | 5.98  | 7.59    | 6.36  | 6.83  | 7.96    | 7.45  |
| Croaghnagawna 110 kV | 4.26  | 3.37    | 3.26  | 5.25  | 2.82     | 2.79  | 7.34  | 7.81    | 6.16  | 7.32  | 3.99    | 3.81  |
| Cromcastle A 110 kV  | 11.13 | 15.26   | 13.62 | 6.84  | 17.56    | 16.78 | 10.22 | 19.32   | 17.28 | 6.23  | 21.26   | 20.36 |
| Cromcastle B 110 kV  | 11.13 | 15.26   | 13.62 | 6.84  | 17.56    | 16.78 | 10.22 | 19.32   | 17.28 | 6.23  | 21.26   | 20.36 |
| Crory 110 kV         | 9.62  | 7.44    | 7.17  | 9.83  | 9.33     | 9.18  | 9.76  | 10.73   | 10.21 | 9.82  | 12.27   | 12.04 |
| Cruiserath 220 kV    | 14.98 | 18.30   | 15.69 | 13.76 | 22.31    | 20.84 | 13.68 | 27.26   | 24.01 | 12.17 | 30.77   | 29.23 |
| Cullenagh 110 kV     | 8.59  | 11.41   | 10.71 | 9.08  | 13.40    | 13.07 | 7.66  | 15.51   | 14.40 | 8.28  | 16.88   | 16.41 |
| Cullenagh 220 kV     | 9.19  | 8.15    | 7.70  | 9.41  | 8.36     | 8.19  | 8.50  | 10.68   | 10.27 | 8.81  | 9.90    | 9.78  |
| Cunghill 110 kV      | 3.27  | 4.55    | 4.34  | 3.74  | 4.43     | 4.36  | 3.12  | 6.71    | 6.21  | 3.78  | 5.62    | 5.50  |
| Cureeny 110 kV       | 4.72  | 4.74    | 4.56  | 5.32  | 5.07     | 5.00  | 5.88  | 7.65    | 6.72  | 6.50  | 7.22    | 6.91  |

|                         |              |             | Sum         | imer         |             |             |              |             | Wi          | nter         |             |             |
|-------------------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|
|                         | ты           | raa nha     |             |              | ngle Pha    |             | ты           | raa nha     |             |              | ngle Ph     | 250         |
|                         |              | ree pha     | 1           |              |             |             |              | ree pha     |             |              |             |             |
| Station                 | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] |
| Cureeny T 110 kV        | 5.36         | 6.17        | 5.87        | 5.23         | 6.04        | 5.94        | 6.09         | 9.64        | 8.59        | 5.54         | 8.16        | 7.88        |
| Cushaling 110 kV        | 3.79         | 6.02        | 5.77        | 4.40         | 7.70        | 7.56        | 3.94         | 8.49        | 8.13        | 4.76         | 10.18       | 10.00       |
| Dallow 110 kV           | 3.43         | 4.52        | 4.38        | 4.52         | 3.01        | 2.99        | 3.49         | 5.70        | 5.42        | 4.67         | 3.35        | 3.32        |
| Dalton 110 kV           | 3.09         | 3.70        | 3.55        | 4.13         | 3.25        | 3.21        | 3.42         | 5.63        | 5.17        | 4.80         | 4.02        | 3.94        |
| Dardistown 110 kV       | 14.10        | 15.75       | 14.02       | 10.54        | 18.51       | 17.65       | 13.22        | 20.08       | 17.90       | 9.77         | 22.60       | 21.60       |
| Darndale 110 kV         | 16.95        | 16.21       | 14.38       | 13.84        | 18.52       | 17.65       | 16.19        | 20.70       | 18.41       | 13.06        | 22.56       | 21.57       |
| Derrybrien 110 kV       | 2.68         | 3.76        | 3.67        | 3.74         | 3.64        | 3.61        | 3.01         | 5.14        | 4.51        | 4.44         | 4.56        | 4.38        |
| Derryiron 110 kV        | 4.72         | 6.98        | 6.65        | 5.81         | 7.36        | 7.24        | 5.55         | 10.80       | 10.19       | 7.12         | 9.75        | 9.58        |
| Doon 110 kV             | 4.36         | 6.35        | 6.01        | 4.71         | 5.01        | 4.93        | 4.36         | 8.54        | 7.88        | 4.76         | 5.74        | 5.64        |
| Dromada 110 kV          | 10.27        | 6.30        | 6.09        | 6.93         | 6.53        | 6.45        | 10.44        | 10.28       | 8.92        | 6.20         | 9.05        | 8.66        |
| Drombeg 110 kV          | 7.45         | 7.34        | 6.97        | 7.48         | 6.22        | 6.13        | 7.38         | 10.77       | 10.27       | 7.46         | 7.67        | 7.59        |
| Drumkeen 110 kV         | 3.53         | 4.77        | 4.53        | 4.22         | 5.02        | 4.93        | 3.81         | 9.52        | 8.10        | 4.97         | 7.65        | 7.30        |
| Drumline 110 kV         | 3.62         | 7.20        | 6.81        | 4.77         | 6.28        | 6.18        | 3.18         | 9.74        | 9.03        | 4.59         | 7.41        | 7.26        |
| Drybridge 110 kV        | 5.91         | 12.15       | 11.13       | 6.74         | 10.37       | 10.10       | 5.02         | 15.89       | 14.68       | 6.22         | 12.26       | 12.01       |
| Dundalk 110 kV          | 3.79         | 7.85        | 7.41        | 4.74         | 7.33        | 7.19        | 3.40         | 10.00       | 9.25        | 4.51         | 8.62        | 8.43        |
| Dunfirth 110 kV         | 4.58         | 6.53        | 6.23        | 5.91         | 5.38        | 5.31        | 4.60         | 8.31        | 8.03        | 6.16         | 6.17        | 6.12        |
| Dungarvan 110 kV        | 6.06         | 5.59        | 5.37        | 7.77         | 4.78        | 4.72        | 6.28         | 7.70        | 6.90        | 8.29         | 5.76        | 5.60        |
| Dunmanway 110 kV        | 4.18         | 6.53        | 6.17        | 4.93         | 6.87        | 6.73        | 4.42         | 10.97       | 9.63        | 5.47         | 9.62        | 9.24        |
| Dunstown 220 kV         | 12.23        | 16.87       | 14.90       | 12.10        | 19.37       | 18.41       | 9.62         | 24.44       | 22.53       | 9.88         | 26.17       | 25.39       |
| Dunstown 400 kV         | 17.17        | 6.39        | 5.89        | 19.87        | 7.03        | 6.82        | 8.71         | 11.26       | 10.65       | 10.89        | 11.22       | 11.01       |
| Ennis 110 kV            | 4.51         | 9.12        | 8.55        | 5.69         | 8.46        | 8.29        | 4.41         | 14.25       | 12.63       | 5.95         | 10.96       | 10.61       |
| Fassaroe East 110 kV    | 5.31         | 7.63        | 7.22        | 5.40         | 5.84        | 5.76        | 5.00         | 8.63        | 8.17        | 5.23         | 6.37        | 6.28        |
| Fassaroe West 110 kV    | 5.47         | 7.79        | 7.37        | 5.51         | 6.03        | 5.94        | 5.14         | 8.82        | 8.34        | 5.33         | 6.59        | 6.49        |
| Finglas 220 kV          | 15.13        | 17.56       | 15.08       | 14.98        | 22.23       | 20.74       | 14.56        | 26.59       | 23.29       | 13.92        | 31.49       | 29.77       |
| Finglas A 110 kV        | 18.31        | 16.71       | 14.81       | 13.61        | 19.47       | 18.54       | 17.76        | 21.72       | 19.21       | 12.85        | 24.09       | 22.96       |
| Finglas B 110 kV        | 29.38        | 11.34       | 10.50       | 27.98        | 14.30       | 13.83       | 32.64        | 14.24       | 12.82       | 29.63        | 17.47       | 16.71       |
| Flagford 110 kV         | 4.76         | 9.71        | 9.05        | 5.47         | 11.93       | 11.58       | 4.42         | 13.88       | 12.60       | 5.34         | 15.86       | 15.27       |
| Flagford 220 kV         | 7.17         | 6.18        | 5.81        | 9.10         | 6.01        | 5.89        | 7.30         | 8.26        | 7.88        | 9.64         | 7.26        | 7.16        |
| Fortunestown 110 kV     | 5.76         | 7.25        | 6.79        | 5.69         | 5.52        | 5.43        | 5.46         | 8.46        | 7.70        | 5.52         | 6.06        | 5.92        |
| Francis Street A 110 kV | 10.97        | 12.08       | 11.13       | 5.26         | 14.35       | 13.88       | 10.30        | 14.30       | 12.80       | 4.99         | 16.44       | 15.73       |
| Francis Street B 110 kV | 13.47        | 11.87       | 10.90       | 6.82         | 14.38       | 13.88       | 12.48        | 13.74       | 12.63       | 6.39         | 16.36       | 15.80       |
| Gallanstown 110 kV      | 6.72         | 10.44       | 9.69        | 7.01         | 7.66        | 7.52        | 6.66         | 13.86       | 13.27       | 7.03         | 8.92        | 8.83        |
| Galway 110 kV           | 5.14         | 10.15       | 9.44        | 4.67         | 12.48       | 12,11       | 5.19         | 16.79       | 14.98       | 4.47         | 18.64       | 17.83       |
| Garrow 110 kV           | 10.48        | 7.16        | 6.85        | 10.49        | 8.51        | 8.36        | 10.43        | 12.43       | 10.94       | 10.34        | 12.94       | 12.35       |
| Garvagh 110 kV          | 4.20         | 5.18        | 4.97        | 5.35         | 5.05        | 4.98        | 4.51         | 7.67        | 6.86        | 6.07         | 6.33        | 6.13        |
| Gilra 110 kV            | 3.28         | 5.74        | 5.47        | 4.07         | 4.62        | 4.56        | 2.99         | 6.99        | 6.61        | 3.94         | 5.16        | 5.08        |
| Glanagow 220 kV         | 11.62        | 10.08       | 9.00        | 11.91        | 13.41       | 12.71       | 13.39        | 19.78       | 17.61       | 13.21        | 23.66       | 22.52       |
| Glanlee 110 kV          | 4.93         | 5.05        | 4.89        | 5.16         | 6.00        | 5.92        | 4.98         | 8.39        | 7.30        | 5.29         | 8.96        | 8.50        |
| Glasmore A 110 kV       | 4.00         | 7.49        | 7.02        | 4.55         | 5.13        | 5.05        | 3.76         | 8.97        | 8.23        | 4.43         | 5.66        | 5.56        |
| Glenlara A 110 kV       | 3.07         | 2.66        | 2.59        | 4.33         | 2.33        | 2.32        | 3.25         | 3.45        | 3.17        | 4.77         | 2.75        | 2.69        |
| Glenlara B 110 kV       | 8.98         | 5.71        | 5.53        | 6.61         | 6.37        | 6.29        | 9.20         | 9.05        | 8.03        | 6.05         | 8.94        | 8.57        |
| Glenree 110 kV          | 3.34         | 3.78        | 3.57        | 4.06         | 3.68        | 3.61        | 3.82         | 6.73        | 6.14        | 4.89         | 5.21        | 5.08        |

|                      |       |         | Sum   | mer   |          |       |       |         | Wi    | nter  |          |       |
|----------------------|-------|---------|-------|-------|----------|-------|-------|---------|-------|-------|----------|-------|
|                      | Th    | ree pha | se    | Si    | ngle Pha | ise   | Th    | ree pha | se    | Si    | ngle Pha | ase   |
|                      | X/R   | lk"     | lk'   | X/R   | lk"      | lk'   | X/R   | lk"     | lk'   | X/R   | lk"      | lk'   |
| Station              | Ratio | [kA]    | [kA]  | Ratio | [kA]     | [kA]  | Ratio | [kA]    | [kA]  | Ratio | [kA]     | [kA]  |
| Golagh 110 kV        | 3.57  | 4.60    | 4.39  | 4.16  | 4.63     | 4.56  | 3.99  | 9.51    | 7.97  | 4.90  | 6.98     | 6.66  |
| Gorman 110 kV        | 6.88  | 12.88   | 11.75 | 7.77  | 14.36    | 13.86 | 6.42  | 17.95   | 16.34 | 7.55  | 18.26    | 17.67 |
| Gorman 220 kV        | 9.52  | 10.07   | 9.24  | 10.20 | 8.63     | 8.41  | 8.66  | 13.15   | 12.52 | 9.69  | 10.15    | 10.02 |
| Gortawee 110 kV      | 4.45  | 5.66    | 5.31  | 5.88  | 4.80     | 4.72  | 4.42  | 7.04    | 6.56  | 6.10  | 5.35     | 5.26  |
| Grange 110 kV        | 13.71 | 16.04   | 14.25 | 6.94  | 18.21    | 17.37 | 12.78 | 20.56   | 18.26 | 6.29  | 22.19    | 21.21 |
| Grange Castle 110 kV | 15.01 | 11.96   | 10.88 | 9.60  | 14.75    | 14.17 | 14.07 | 14.37   | 12.88 | 8.97  | 17.27    | 16.49 |
| Great Island 110 kV  | 8.94  | 11.42   | 10.77 | 9.84  | 14.89    | 14.50 | 8.49  | 16.00   | 14.93 | 9.46  | 19.60    | 19.04 |
| Great Island 220 kV  | 12.23 | 10.58   | 9.92  | 13.74 | 12.76    | 12.42 | 12.38 | 14.45   | 13.81 | 13.31 | 15.51    | 15.26 |
| Griffinrath A 110 kV | 7.26  | 9.49    | 8.96  | 7.57  | 9.71     | 9.52  | 6.43  | 11.86   | 11.30 | 6.98  | 11.44    | 11.26 |
| Griffinrath B 110 kV | 7.81  | 9.80    | 9.24  | 7.73  | 9.71     | 9.52  | 6.92  | 12.31   | 11.71 | 7.12  | 11.43    | 11.25 |
| Harolds Cross 110 kV | 11.17 | 12.11   | 11.16 | 4.96  | 14.31    | 13.84 | 10.48 | 14.33   | 12.84 | 4.71  | 16.37    | 15.67 |
| Harristown 110 kV    | 4.43  | 6.82    | 6.48  | 5.44  | 5.73     | 5.65  | 4.63  | 9.27    | 8.91  | 5.82  | 6.81     | 6.75  |
| Heuston 110 kV       | 14.63 | 12.10   | 11.10 | 8.23  | 14.82    | 14.28 | 13.53 | 14.03   | 12.88 | 7.69  | 16.89    | 16.30 |
| Huntstown A 220 kV   | 14.36 | 16.88   | 14.57 | 13.08 | 21.37    | 19.99 | 14.09 | 25.55   | 22.48 | 12.03 | 30.27    | 28.67 |
| Huntstown B 220 kV   | 15.47 | 17.34   | 15.00 | 11.62 | 21.17    | 19.86 | 14.24 | 24.86   | 22.14 | 10.00 | 28.33    | 27.03 |
| Ikerrin 110 kV       | 5.08  | 4.00    | 3.87  | 5.90  | 3.18     | 3.16  | 5.63  | 5.63    | 5.13  | 6.39  | 3.77     | 3.69  |
| Inchicore 220 kV     | 16.81 | 20.84   | 17.62 | 11.56 | 25.11    | 23.32 | 12.63 | 27.83   | 24.30 | 9.03  | 31.83    | 30.10 |
| Inchicore A 110 kV   | 31.84 | 13.33   | 12.13 | 27.55 | 16.71    | 16.04 | 29.00 | 15.59   | 14.19 | 25.12 | 19.24    | 18.49 |
| Inchicore B 110 kV   | 50.43 | 12.89   | 11.69 | 37.79 | 16.29    | 15.61 | 45.07 | 15.61   | 13.94 | 33.79 | 19.28    | 18.37 |
| Inniscarra 110 kV    | 3.93  | 7.88    | 7.42  | 4.97  | 7.71     | 7.56  | 3.48  | 11.17   | 10.38 | 4.79  | 9.59     | 9.38  |
| Irishtown 220 kV     | 18.77 | 20.59   | 17.45 | 13.47 | 25.16    | 23.37 | 14.32 | 26.08   | 22.91 | 10.65 | 30.51    | 28.90 |
| Kellis 110 kV        | 6.99  | 7.96    | 7.60  | 8.04  | 9.55     | 9.37  | 6.72  | 10.93   | 10.25 | 7.93  | 12.22    | 11.92 |
| Kellis 220 kV        | 8.25  | 7.23    | 6.87  | 9.96  | 6.35     | 6.25  | 7.91  | 8.93    | 8.64  | 9.78  | 7.23     | 7.16  |
| Kellystown 220 kV    | 7.69  | 15.72   | 13.81 | 6.56  | 13.23    | 12.72 | 6.15  | 21.12   | 19.43 | 5.72  | 16.08    | 15.72 |
| Kilbarry 110 kV      | 7.25  | 13.84   | 12.46 | 7.83  | 15.47    | 14.85 | 6.18  | 23.42   | 20.60 | 7.13  | 22.53    | 21.57 |
| Kildonan 110 kV      | 7.07  | 13.40   | 12.15 | 5.37  | 12.50    | 12.11 | 6.24  | 16.67   | 15.65 | 4.91  | 14.54    | 14.27 |
| Kilkenny 110 kV      | 4.20  | 4.92    | 4.74  | 5.65  | 4.48     | 4.43  | 4.75  | 8.30    | 7.81  | 6.35  | 6.65     | 6.54  |
| Kill Hill 110 kV     | 4.78  | 4.94    | 4.75  | 5.83  | 4.60     | 4.54  | 5.59  | 7.60    | 6.80  | 6.81  | 5.85     | 5.68  |
| Killonan 110 kV      | 7.19  | 14.07   | 12.74 | 8.19  | 16.26    | 15.63 | 6.78  | 24.22   | 21.54 | 8.21  | 24.22    | 23.25 |
| Killonan 220 kV      | 8.06  | 8.26    | 7.64  | 9.96  | 8.35     | 8.12  | 7.75  | 12.57   | 11.88 | 10.22 | 11.01    | 10.83 |
| Killoteran 110 kV    | 7.78  | 10.38   | 9.79  | 7.90  | 11.75    | 11.48 | 7.06  | 14.03   | 13.01 | 7.31  | 14.63    | 14.24 |
| Kilmahud 110 kV      | 20.45 | 18.30   | 16.24 | 21.24 | 13.06    | 12.68 | 18.46 | 21.43   | 19.72 | 20.03 | 14.29    | 14.02 |
| Kilmore 110 kV       | 15.03 | 16.31   | 14.46 | 10.28 | 18.98    | 18.07 | 14.16 | 20.94   | 18.57 | 9.49  | 23.27    | 22.21 |
| Kilpaddoge 110 kV    | 11.67 | 13.39   | 12.28 | 12.32 | 17.05    | 16.42 | 10.91 | 22.95   | 21.12 | 11.93 | 26.59    | 25.72 |
| Kilpaddoge 220 kV    | 11.33 | 11.32   | 10.30 | 11.43 | 14.99    | 14.35 | 12.70 | 24.05   | 22.00 | 12.09 | 28.88    | 27.82 |
| Kilpaddoge 400 kV    | 9.70  | 6.70    | 6.13  | 8.83  | 7.44     | 7.18  | 7.73  | 14.46   | 13.44 | 7.12  | 12.77    | 12.48 |
| Kilteel 110 kV       | 4.38  | 6.88    | 6.54  | 5.40  | 6.41     | 6.31  | 4.22  | 8.91    | 8.39  | 5.38  | 7.56     | 7.43  |
| Kinnegad 110 kV      | 4.45  | 7.36    | 6.97  | 5.29  | 6.93     | 6.81  | 4.66  | 10.22   | 9.74  | 5.67  | 8.45     | 8.34  |
| Knockacummer 110 kV  | 7.94  | 5.00    | 4.86  | 7.06  | 5.37     | 5.31  | 8.12  | 7.74    | 6.91  | 6.86  | 7.32     | 7.05  |
| Knockalough 110 kV   | 3.98  | 3.99    | 3.86  | 3.79  | 4.86     | 4.79  | 5.50  | 6.79    | 5.87  | 4.55  | 7.35     | 6.95  |
| Knockanure 220 kV    | 11.01 | 9.72    | 8.95  | 8.34  | 12.79    | 12.31 | 11.75 | 18.94   | 17.36 | 7.11  | 22.83    | 22.01 |
| Knockanure A 110 kV  | 19.74 | 9.10    | 8.67  | 16.83 | 10.67    | 10.47 | 21.76 | 15.80   | 13.63 | 16.30 | 16.16    | 15.31 |

|                     |       |         | Sum   | imer  |          |       |       |         | Wi    | nter  |         |         |
|---------------------|-------|---------|-------|-------|----------|-------|-------|---------|-------|-------|---------|---------|
|                     | Th    | ree pha |       |       | ngle Pha | ISP   | Th    | ree pha |       | 1     | ngle Ph | <br>ase |
|                     | X/R   | Ik"     | Ik'   | X/R   | lk"      | lk'   | X/R   | Ik"     | Ik'   | X/R   | lk"     | lk'     |
| Station             | Ratio | [kA]    | [kA]  | Ratio | [kA]     | [kA]  | Ratio | [kA]    | [kA]  | Ratio | [kA]    | [kA]    |
| Knockanure B 110 kV | 5.02  | 7.13    | 6.76  | 5.94  | 6.20     | 6.10  | 4.47  | 10.45   | 9.80  | 5.74  | 7.67    | 7.55    |
| Knockearagh 110 kV  | 5.46  | 4.92    | 4.71  | 7.17  | 4.35     | 4.29  | 5.51  | 6.66    | 6.20  | 7.56  | 5.24    | 5.14    |
| Knocknamona 110 kV  | 5.77  | 5.38    | 5.18  | 6.63  | 4.16     | 4.12  | 6.38  | 7.79    | 6.86  | 7.14  | 5.03    | 4.89    |
| Knockraha A 110 kV  | 8.65  | 14.75   | 13.27 | 9.21  | 15.81    | 15.20 | 7.67  | 24.61   | 21.94 | 8.63  | 22.51   | 21.70   |
| Knockraha A 220 kV  | 10.66 | 10.35   | 9.28  | 10.73 | 12.10    | 11.56 | 10.99 | 20.17   | 18.09 | 10.74 | 19.89   | 19.14   |
| Knockraha B 110 kV  | 8.65  | 14.75   | 13.27 | 9.21  | 15.81    | 15.20 | 7.67  | 24.61   | 21.94 | 8.63  | 22.51   | 21.70   |
| Knockraha B 220 kV  | 10.66 | 10.35   | 9.28  | 10.73 | 12.10    | 11.56 | 10.99 | 20.17   | 18.09 | 10.74 | 19.89   | 19.14   |
| Knockranny 110 kV   | 5.47  | 6.43    | 6.14  | 4.96  | 8.37     | 8.20  | 6.22  | 9.57    | 8.96  | 5.21  | 11.76   | 11.44   |
| Knockranny A 110 kV | 3.85  | 4.49    | 4.32  | 4.12  | 5.48     | 5.39  | 5.34  | 8.04    | 6.84  | 5.51  | 8.60    | 8.08    |
| Knockranny B 110 kV | 5.47  | 6.43    | 6.14  | 4.96  | 8.37     | 8.20  | 6.22  | 9.57    | 8.96  | 5.21  | 11.76   | 11.44   |
| Knockumber 110 kV   | 3.91  | 7.83    | 7.32  | 4.70  | 5.98     | 5.87  | 3.53  | 9.50    | 8.92  | 4.51  | 6.61    | 6.51    |
| Lanesboro 110 kV    | 3.24  | 7.74    | 7.33  | 4.02  | 8.69     | 8.51  | 3.07  | 10.34   | 9.51  | 4.00  | 10.70   | 10.39   |
| Letterkenny110 kV   | 3.84  | 5.45    | 5.13  | 4.47  | 6.37     | 6.22  | 4.23  | 11.62   | 9.73  | 5.43  | 10.70   | 10.09   |
| Liberty A 110 kV    | 6.09  | 12.24   | 11.13 | 5.27  | 14.51    | 13.95 | 5.03  | 19.28   | 17.26 | 4.44  | 20.54   | 19.71   |
| Liberty B 110 kV    | 6.01  | 12.23   | 11.12 | 5.13  | 14.49    | 13.93 | 4.95  | 19.25   | 17.24 | 4.31  | 20.47   | 19.65   |
| Limerick 110 kV     | 5.72  | 12.61   | 11.44 | 6.38  | 12.50    | 12.09 | 4.91  | 19.94   | 17.94 | 5.94  | 16.70   | 16.19   |
| Lisdrum 110 kV      | 2.91  | 4.70    | 4.52  | 4.17  | 4.17     | 4.12  | 2.78  | 5.76    | 5.33  | 4.22  | 4.61    | 4.51    |
| Lisheen 110 kV      | 3.93  | 3.17    | 3.08  | 3.94  | 4.75     | 4.68  | 4.93  | 5.29    | 4.61  | 4.94  | 7.93    | 7.38    |
| Lodgewood 110 kV    | 9.62  | 7.44    | 7.17  | 9.83  | 9.33     | 9.18  | 9.76  | 10.73   | 10.21 | 9.82  | 12.27   | 12.04   |
| Lodgewood 220 kV    | 9.10  | 6.77    | 6.47  | 10.23 | 6.63     | 6.53  | 9.13  | 8.71    | 8.42  | 10.26 | 7.76    | 7.68    |
| Longpoint 220 kV    | 11.27 | 10.06   | 8.99  | 12.12 | 13.43    | 12.74 | 13.52 | 20.52   | 18.22 | 14.72 | 24.51   | 23.30   |
| Loughtown 220 kV    | -     | -       | -     | -     | -        | -     | 11.89 | 14.31   | 13.69 | 10.71 | 15.12   | 14.88   |
| Louth 220 kV        | 10.59 | 13.00   | 11.56 | 11.22 | 15.63    | 14.87 | 9.51  | 21.27   | 19.68 | 10.43 | 22.92   | 22.27   |
| Louth A 110 kV      | 7.39  | 11.23   | 10.43 | 8.37  | 13.69    | 13.28 | 6.36  | 14.40   | 13.46 | 7.49  | 16.78   | 16.34   |
| Louth A 275 kV      | 12.53 | 7.96    | 7.20  | 12.18 | 9.79     | 9.37  | 11.22 | 12.41   | 11.86 | 10.93 | 14.02   | 13.77   |
| Louth B 110 kV      | 7.88  | 12.04   | 11.14 | 8.66  | 15.05    | 14.56 | 6.76  | 15.99   | 14.89 | 7.70  | 19.07   | 18.53   |
| Louth B 275 kV      | 11.81 | 7.98    | 7.22  | 10.75 | 9.97     | 9.53  | 10.51 | 12.38   | 11.83 | 9.39  | 14.33   | 14.07   |
| Lumcloon 110 kV     | 4.95  | 6.43    | 6.18  | 6.05  | 4.79     | 4.74  | 5.46  | 8.76    | 8.42  | 6.54  | 5.62    | 5.58    |
| Macetown 110 kV     | 7.60  | 14.78   | 13.27 | 7.00  | 15.16    | 14.58 | 6.66  | 18.78   | 17.47 | 6.35  | 18.05   | 17.63   |
| Macroom 110 kV      | 7.14  | 11.00   | 10.16 | 7.10  | 12.63    | 12.24 | 6.84  | 18.75   | 16.79 | 6.81  | 18.59   | 17.89   |
| Mallow 110 kV       | 5.24  | 5.77    | 5.51  | 6.83  | 5.17     | 5.10  | 5.24  | 7.69    | 7.17  | 7.14  | 6.18    | 6.07    |
| Marina 110 kV       | 7.00  | 13.25   | 11.96 | 7.80  | 15.91    | 15.24 | 5.90  | 21.80   | 19.28 | 7.02  | 23.36   | 22.30   |
| Maynooth A 110 kV   | 11.25 | 11.72   | 10.95 | 11.92 | 14.46    | 14.05 | 9.98  | 15.27   | 14.43 | 10.82 | 18.10   | 17.68   |
| Maynooth A 220 kV   | 10.76 | 16.27   | 14.33 | 10.34 | 15.69    | 15.02 | 8.77  | 21.82   | 20.09 | 8.95  | 19.26   | 18.78   |
| Maynooth B 110 kV   | 8.78  | 15.56   | 14.05 | 10.08 | 15.33    | 14.81 | 7.43  | 19.34   | 18.20 | 9.03  | 17.92   | 17.58   |
| Maynooth B 220 kV   | 10.03 | 18.23   | 15.80 | 9.27  | 17.78    | 16.90 | 7.82  | 25.17   | 22.91 | 7.77  | 22.32   | 21.67   |
| McDermott 110 kV    | 15.74 | 10.44   | 9.71  | 6.30  | 12.35    | 11.99 | 15.67 | 13.02   | 11.75 | 5.93  | 14.81   | 14.21   |
| Meath Hill 110 kV   | 4.16  | 8.06    | 7.60  | 5.27  | 6.86     | 6.74  | 3.89  | 10.48   | 9.75  | 5.22  | 7.98    | 7.84    |
| Meentycat 110 kV    | 3.27  | 4.12    | 3.94  | 4.11  | 4.21     | 4.15  | 3.53  | 7.60    | 6.57  | 4.94  | 6.11    | 5.86    |
| Midleton 110 kV     | 4.05  | 8.57    | 8.00  | 5.07  | 7.76     | 7.60  | 3.43  | 11.53   | 10.78 | 4.67  | 9.33    | 9.16    |
| Milltown A 110 kV   | 15.63 | 13.10   | 12.01 | 6.90  | 15.77    | 15.21 | 14.57 | 15.60   | 13.90 | 6.50  | 18.18   | 17.35   |
| Milltown B 110 kV   | 9.20  | 10.71   | 9.91  | 4.18  | 12.76    | 12.35 | 8.60  | 12.34   | 11.39 | 3.95  | 14.41   | 13.96   |

|                      |       |         | Sum   | mer   |          |       |       |         | Wi    | nter  |         |       |
|----------------------|-------|---------|-------|-------|----------|-------|-------|---------|-------|-------|---------|-------|
|                      | Th    | ree pha | se    | Si    | ngle Pha | ise   | Th    | ree pha | se    | Si    | ngle Ph | ase   |
|                      | X/R   | lk"     | lk'   | X/R   | lk"      | lk'   | X/R   | lk"     | lk'   | X/R   | lk"     | lk'   |
| Station              | Ratio | [kA]    | [kA]  | Ratio | [kA]     | [kA]  | Ratio | [kA]    | [kA]  | Ratio | [kA]    | [kA]  |
| Misery Hill 110 kV   | 13.89 | 12.78   | 11.73 | 7.61  | 15.53    | 14.98 | 12.98 | 15.21   | 13.56 | 7.18  | 17.93   | 17.10 |
| Monatooreen 110 kV   | 6.47  | 14.01   | 12.67 | 6.53  | 14.91    | 14.36 | 5.25  | 22.67   | 20.38 | 5.69  | 20.80   | 20.10 |
| Moneteen 110 kV      | 5.85  | 9.73    | 8.93  | 6.55  | 7.68     | 7.50  | 5.17  | 13.08   | 12.18 | 6.21  | 8.97    | 8.82  |
| Moneypoint 110 kV    | 13.29 | 7.89    | 7.53  | 15.82 | 8.24     | 8.10  | 14.83 | 10.76   | 10.22 | 17.78 | 10.20   | 10.03 |
| Moneypoint 220 kV    | 11.40 | 11.19   | 10.20 | 11.41 | 14.84    | 14.21 | 12.91 | 23.58   | 21.62 | 12.10 | 28.42   | 27.40 |
| Moneypoint G1 400 kV | 12.27 | 6.76    | 6.18  | 14.34 | 8.02     | 7.73  | 12.62 | 14.76   | 13.70 | 15.79 | 14.52   | 14.16 |
| Moneypoint G2 400 kV | 24.59 | 2.85    | 2.73  | 26.49 | 3.60     | 3.54  | 45.43 | 5.06    | 4.82  | 44.84 | 5.73    | 5.62  |
| Moneypoint G3 400 kV | 12.27 | 6.76    | 6.18  | 14.34 | 8.02     | 7.73  | 12.62 | 14.76   | 13.70 | 15.79 | 14.52   | 14.16 |
| Monread 110 kV       | 4.07  | 6.75    | 6.43  | 4.89  | 6.95     | 6.83  | 3.90  | 8.82    | 8.33  | 4.85  | 8.33    | 8.18  |
| Mount Lucas 110 kV   | 3.66  | 5.14    | 4.95  | 4.59  | 5.21     | 5.14  | 3.97  | 7.26    | 6.93  | 5.16  | 6.48    | 6.39  |
| Moy 110 kV           | 3.67  | 3.81    | 3.55  | 4.32  | 4.50     | 4.38  | 5.71  | 7.98    | 7.02  | 7.09  | 7.66    | 7.33  |
| Muckerstown 110 kV   | 6.42  | 9.69    | 9.04  | 6.82  | 6.87     | 6.76  | 6.32  | 12.66   | 12.17 | 6.84  | 7.91    | 7.84  |
| Mullagharlin 110 kV  | 3.90  | 7.99    | 7.55  | 4.91  | 7.85     | 7.70  | 3.44  | 9.88    | 9.27  | 4.58  | 9.11    | 8.93  |
| Mullingar 110 kV     | 3.58  | 6.43    | 6.13  | 4.48  | 6.27     | 6.17  | 3.52  | 8.09    | 7.68  | 4.55  | 7.28    | 7.16  |
| Mulreavy 110 kV      | 3.93  | 4.84    | 4.60  | 4.54  | 5.71     | 5.60  | 5.43  | 11.05   | 8.92  | 6.73  | 10.13   | 9.42  |
| Mungret A 110 kV     | 5.49  | 9.29    | 8.55  | 6.22  | 7.17     | 7.01  | 4.83  | 12.31   | 11.50 | 5.89  | 8.29    | 8.16  |
| Mungret B 110 kV     | 5.48  | 9.31    | 8.57  | 6.21  | 7.18     | 7.02  | 4.82  | 12.33   | 11.52 | 5.88  | 8.30    | 8.17  |
| Nangor 110 kV        | 13.32 | 11.67   | 10.64 | 7.91  | 14.33    | 13.78 | 12.54 | 13.99   | 12.56 | 7.41  | 16.72   | 15.98 |
| Navan 110 kV         | 5.90  | 11.50   | 10.55 | 6.63  | 11.49    | 11.15 | 5.41  | 15.56   | 14.23 | 6.36  | 14.04   | 13.66 |
| Nenagh 110 kV        | 3.34  | 3.48    | 3.37  | 4.06  | 2.45     | 2.43  | 3.29  | 4.56    | 4.20  | 4.13  | 2.77    | 2.72  |
| Newbridge 110 kV     | 4.02  | 8.06    | 7.61  | 4.67  | 8.61     | 8.43  | 3.92  | 11.54   | 10.83 | 4.72  | 11.10   | 10.88 |
| Newbury 110 kV       | 13.62 | 16.03   | 14.23 | 6.86  | 18.11    | 17.28 | 12.70 | 20.50   | 18.22 | 6.23  | 22.03   | 21.07 |
| North Quays 110 kV   | 19.51 | 13.37   | 12.24 | 6.42  | 15.80    | 15.24 | 18.15 | 15.95   | 14.19 | 6.05  | 18.19   | 17.36 |
| North Wall 220 kV    | 14.17 | 16.25   | 14.09 | 9.20  | 18.58    | 17.52 | 12.53 | 23.38   | 20.78 | 7.74  | 24.60   | 23.53 |
| Oldcourt A 110 kV    | 4.25  | 8.59    | 8.03  | 4.70  | 7.07     | 6.94  | 3.59  | 11.51   | 10.84 | 4.33  | 8.42    | 8.29  |
| Oldcourt B 110 kV    | 4.28  | 8.64    | 8.07  | 4.73  | 7.13     | 7.00  | 3.62  | 11.59   | 10.91 | 4.36  | 8.51    | 8.38  |
| Oldstreet 220 kV     | 16.52 | 10.38   | 9.47  | 13.70 | 11.13    | 10.75 | 14.95 | 12.94   | 12.25 | 12.41 | 13.37   | 13.11 |
| Oldstreet 400 kV     | 12.97 | 7.62    | 6.94  | 10.25 | 7.02     | 6.80  | 9.48  | 12.02   | 11.43 | 8.24  | 9.47    | 9.34  |
| Oriel 220 kV         | 9.73  | 10.51   | 9.60  | 8.31  | 10.91    | 10.56 | 9.28  | 15.97   | 14.72 | 7.66  | 14.61   | 14.24 |
| Oughtragh 110 kV     | 3.75  | 4.04    | 3.89  | 4.80  | 2.81     | 2.78  | 3.59  | 5.32    | 4.99  | 4.82  | 3.17    | 3.13  |
| Pelletstown 110 kV   | 13.80 | 9.93    | 9.26  | 8.05  | 10.88    | 10.60 | 13.56 | 12.24   | 11.13 | 7.70  | 12.84   | 12.40 |
| Platin 110 kV        | 5.24  | 11.23   | 10.33 | 5.75  | 8.68     | 8.49  | 4.51  | 14.31   | 13.37 | 5.37  | 9.93    | 9.78  |
| Pollaphuca 110 kV    | 2.80  | 2.43    | 2.39  | 4.02  | 2.25     | 2.24  | 3.27  | 3.18    | 3.07  | 4.73  | 2.58    | 2.55  |
| Poolbeg A 110 kV     | 29.65 | 13.96   | 12.75 | 23.29 | 17.36    | 16.69 | 27.41 | 16.71   | 14.85 | 21.60 | 20.23   | 19.25 |
| Poolbeg A 220 kV     | 14.47 | 16.51   | 14.28 | 7.83  | 17.75    | 16.77 | 12.49 | 23.69   | 21.01 | 6.50  | 23.16   | 22.20 |
| Poolbeg B 110 kV     | 29.61 | 13.94   | 12.73 | 23.28 | 17.34    | 16.68 | 27.37 | 16.68   | 14.83 | 21.59 | 20.20   | 19.22 |
| Poolbeg B 220 kV     | 16.11 | 19.49   | 16.65 | 11.11 | 21.93    | 20.56 | 12.41 | 25.68   | 22.62 | 8.99  | 27.25   | 25.97 |
| Poolbeg C 110 kV     | 22.35 | 13.65   | 12.48 | 7.48  | 16.17    | 15.58 | 20.73 | 16.32   | 14.49 | 7.04  | 18.67   | 17.80 |
| Poppintree 110 kV    | 12.17 | 15.67   | 13.97 | 7.11  | 18.10    | 17.28 | 11.28 | 20.06   | 17.86 | 6.48  | 22.09   | 21.12 |
| Portan 260 kV        | 18.27 | 9.51    | 8.79  | 79.27 | 3.08     | 3.05  | 15.88 | 14.72   | 14.13 | 95.45 | 3.40    | 3.39  |
| Portan 400 kV        | 14.99 | 7.89    | 7.18  | 15.25 | 8.91     | 8.58  | 11.76 | 13.44   | 12.73 | 11.82 | 14.14   | 13.86 |
| Portlaoise 110 kV    | 3.79  | 7.16    | 6.82  | 4.94  | 6.98     | 6.87  | 5.61  | 14.35   | 13.52 | 6.68  | 12.96   | 12.72 |

|                      |              |             | C           | mer          |                         |             |              |             | 14/:        | nter         |             |             |
|----------------------|--------------|-------------|-------------|--------------|-------------------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|
|                      |              |             |             |              |                         |             | TL           |             |             |              |             |             |
|                      |              | ree pha     | 1           |              | n <mark>gle Ph</mark> a | 1           |              | iree pha    |             |              | ngle Ph     |             |
| Station              | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] | X/R<br>Ratio | lk"<br>[kA]             | lk'<br>[kA] | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] |
| Pottery 110 kV       | 18.62        | 10.79       | 10.06       | 5.74         | 10.99                   | 10.72       | 17.31        | 12.49       | 11.58       | 5.47         | 12.27       | 11.96       |
| Prospect 220 kV      | 10.31        | 10.04       | 9.23        | 8.61         | 11.67                   | 11.28       | 10.11        | 18.46       | 17.25       | 7.67         | 18.49       | 18.05       |
| Raffeen 220 kV       | 11.20        | 9.64        | 8.65        | 10.54        | 12.54                   | 11.93       | 12.38        | 18.45       | 16.54       | 10.56        | 21.47       | 20.53       |
| Raffeen A 110 kV     | 6.39         | 11.24       | 10.30       | 7.09         | 13.74                   | 13.24       | 5.41         | 16.49       | 15.18       | 6.31         | 18.78       | 18.18       |
| Raffeen B 110 kV     | 8.56         | 11.04       | 10.13       | 9.25         | 13.45                   | 12.97       | 7.59         | 16.63       | 15.21       | 8.55         | 18.72       | 18.08       |
| Rathkeale 110 kV     | 3.71         | 6.54        | 6.18        | 4.87         | 5.40                    | 5.32        | 3.40         | 8.42        | 7.94        | 4.78         | 6.17        | 6.08        |
| Rathmullan 110 kV    | 5.34         | 11.43       | 10.51       | 5.94         | 9.12                    | 8.91        | 4.56         | 14.65       | 13.64       | 5.51         | 10.52       | 10.34       |
| Ratrussan 110 kV     | 3.30         | 5.95        | 5.68        | 4.10         | 6.73                    | 6.61        | 3.68         | 8.52        | 7.29        | 4.87         | 8.72        | 8.25        |
| Reamore 110 kV       | 3.84         | 6.79        | 6.43        | 4.25         | 6.34                    | 6.23        | 3.72         | 11.16       | 10.06       | 4.29         | 8.45        | 8.22        |
| Richmond A 110 kV    | 2.90         | 5.68        | 5.44        | 3.85         | 5.51                    | 5.44        | 2.75         | 7.10        | 6.61        | 3.81         | 6.42        | 6.28        |
| Richmond B 110 kV    | 2.90         | 5.68        | 5.44        | 3.85         | 5.51                    | 5.44        | 2.75         | 7.10        | 6.61        | 3.81         | 6.42        | 6.28        |
| Rinawade 110 kV      | 5.16         | 10.13       | 9.44        | 6.02         | 7.49                    | 7.36        | 4.70         | 12.13       | 11.64       | 5.78         | 8.35        | 8.27        |
| Ringaskiddy 110 kV   | 6.25         | 9.50        | 8.82        | 6.46         | 9.75                    | 9.50        | 5.32         | 13.49       | 12.53       | 5.83         | 12.44       | 12.15       |
| Ringsend 110 kV      | 30.19        | 14.06       | 12.82       | 24.67        | 17.49                   | 16.80       | 27.88        | 16.89       | 14.94       | 22.84        | 20.44       | 19.41       |
| Rosspile 110 kV      | 6.05         | 6.27        | 6.05        | 6.84         | 5.21                    | 5.15        | 6.25         | 8.95        | 8.48        | 7.14         | 6.29        | 6.21        |
| Ryebrook 110 kV      | 5.79         | 13.21       | 11.80       | 6.62         | 12.01                   | 11.59       | 5.01         | 15.78       | 14.67       | 6.06         | 13.45       | 13.17       |
| Salthill 110 kV      | 4.63         | 9.76        | 9.09        | 3.87         | 11.81                   | 11.46       | 4.68         | 16.09       | 14.34       | 3.60         | 17.43       | 16.69       |
| Screeb 110 kV        | 3.66         | 2.37        | 2.30        | 4.60         | 1.72                    | 1.70        | 4.57         | 3.54        | 3.15        | 5.35         | 2.04        | 1.99        |
| Seal Rock A 110 kV   | 8.77         | 9.44        | 8.37        | 10.45        | 10.43                   | 9.96        | 7.90         | 12.09       | 11.11       | 9.85         | 12.12       | 11.77       |
| Seal Rock B 110 kV   | 8.81         | 9.45        | 8.37        | 10.47        | 10.44                   | 9.96        | 7.93         | 12.10       | 11.11       | 9.86         | 12.13       | 11.77       |
| Shankill 110 kV      | 3.77         | 7.08        | 6.68        | 4.75         | 6.80                    | 6.67        | 3.79         | 10.00       | 8.74        | 5.05         | 8.49        | 8.16        |
| Shannonbridge 110 kV | 5.00         | 10.63       | 9.96        | 5.91         | 12.90                   | 12.56       | 4.72         | 14.67       | 13.66       | 5.84         | 16.65       | 16.20       |
| Shannonbridge 220 kV | 6.55         | 5.96        | 5.65        | 8.71         | 5.47                    | 5.38        | 6.34         | 7.39        | 7.16        | 8.78         | 6.29        | 6.24        |
| Shantallow 110 kV    | 4.67         | 10.09       | 9.46        | 4.96         | 9.03                    | 8.85        | 4.05         | 14.60       | 13.66       | 4.63         | 11.23       | 11.04       |
| Shellybanks A 220 kV | 14.25        | 16.49       | 14.27       | 9.67         | 18.83                   | 17.74       | 12.28        | 23.66       | 20.99       | 8.07         | 24.85       | 23.76       |
| Shellybanks B 220 kV | 18.01        | 19.99       | 17.01       | 11.46        | 24.05                   | 22.40       | 13.82        | 25.07       | 22.11       | 9.21         | 28.85       | 27.39       |
| Shelton Abbey 110 kV | 7.72         | 6.91        | 6.65        | 7.75         | 7.33                    | 7.23        | 7.08         | 8.92        | 8.47        | 7.36         | 8.80        | 8.65        |
| Singland 110 kV      | 6.56         | 11.96       | 10.96       | 7.41         | 12.44                   | 12.05       | 6.25         | 19.16       | 17.33       | 7.42         | 16.91       | 16.39       |
| Sliabh Bawn 110 kV   | 3.16         | 7.14        | 6.79        | 3.99         | 7.31                    | 7.18        | 3.19         | 9.79        | 8.96        | 4.22         | 9.00        | 8.75        |
| Slievecallan 110 kV  | 6.53         | 5.11        | 4.93        | 8.68         | 2.21                    | 2.20        | 7.72         | 7.64        | 6.77        | 9.39         | 2.43        | 2.39        |
| Sligo 110 kV         | 3.99         | 7.28        | 6.84        | 4.57         | 7.34                    | 7.19        | 3.53         | 11.03       | 10.02       | 4.36         | 9.55        | 9.27        |
| Snugborough 110 kV   | 10.60        | 18.16       | 15.93       | 10.19        | 21.44                   | 20.31       | 9.39         | 24.06       | 22.02       | 9.21         | 26.73       | 25.84       |
| Somerset 110 kV      | 3.12         | 6.32        | 6.07        | 4.01         | 4.49                    | 4.44        | 2.86         | 7.79        | 7.43        | 3.90         | 4.98        | 4.93        |
| Sorne Hill 110 kV    | 2.76         | 2.30        | 2.23        | 3.42         | 2.66                    | 2.63        | 3.44         | 3.90        | 3.46        | 4.38         | 3.74        | 3.60        |
| Srahnakilly 110 kV   | 3.44         | 3.31        | 3.15        | 3.76         | 4.27                    | 4.18        | 5.94         | 8.26        | 6.87        | 6.52         | 8.83        | 8.23        |
| Srananagh 110 kV     | 4.85         | 8.19        | 7.68        | 5.53         | 9.40                    | 9.16        | 4.47         | 13.04       | 11.75       | 5.45         | 13.11       | 12.65       |
| Srananagh 220 kV     | 6.69         | 3.98        | 3.81        | 8.75         | 3.41                    | 3.36        | 7.26         | 5.18        | 4.97        | 9.64         | 3.95        | 3.91        |
| Stevenstown 110 kV   | 3.99         | 6.15        | 5.83        | 4.54         | 3.96                    | 3.92        | 3.78         | 7.12        | 6.67        | 4.44         | 4.31        | 4.25        |
| Stratford 110 kV     | 3.22         | 3.71        | 3.62        | 4.20         | 3.01                    | 2.99        | 3.36         | 4.78        | 4.55        | 4.41         | 3.41        | 3.37        |
| Taney 110 kV         | 9.13         | 9.34        | 8.78        | 3.28         | 9.22                    | 9.03        | 8.60         | 10.69       | 9.99        | 3.15         | 10.20       | 9.97        |
| Tarbert 110 kV       | 19.17        | 10.44       | 9.89        | 22.20        | 11.56                   | 11.32       | 26.18        | 14.07       | 13.61       | 29.08        | 14.36       | 14.20       |
| Tarbert 220 kV       | 11.03        | 10.97       | 10.01       | 11.43        | 14.35                   | 13.76       | 11.81        | 22.45       | 20.65       | 12.00        | 26.49       | 25.59       |

|                      |              |             | Sum         | mer          |             |             |              |             | Wi          | nter         |             |             |
|----------------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|
|                      | Th           | iree pha    | se          | Si           | ngle Pha    | ise         | Th           | ree pha     | se          | Si           | ngle Ph     | ase         |
| Station              | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] |
| Tawnaghmore A 110 kV | 3.29         | 3.13        | 2.96        | 4.08         | 3.36        | 3.29        | 4.53         | 6.07        | 5.48        | 5.97         | 5.16        | 5.01        |
| Tawnaghmore B 110 kV | 3.79         | 3.41        | 3.17        | 4.58         | 3.97        | 3.85        | 5.16         | 6.39        | 5.74        | 6.75         | 6.20        | 5.98        |
| Thornsberry 110 kV   | 3.59         | 5.16        | 4.96        | 4.59         | 5.09        | 5.02        | 3.72         | 7.29        | 6.91        | 5.00         | 6.47        | 6.37        |
| Thurles 110 kV       | 4.98         | 4.10        | 3.95        | 5.38         | 4.75        | 4.68        | 6.13         | 6.84        | 5.95        | 6.45         | 6.90        | 6.57        |
| Tievebrack 110 kV    | 3.40         | 3.31        | 3.18        | 4.52         | 2.66        | 2.63        | 3.73         | 5.51        | 5.09        | 5.23         | 3.31        | 3.26        |
| Timahoe 110 kV       | 6.25         | 6.92        | 6.62        | 6.83         | 5.39        | 5.33        | 6.25         | 9.61        | 9.30        | 6.95         | 6.45        | 6.40        |
| Tipperary 110 kV     | 5.00         | 6.01        | 5.73        | 6.04         | 4.23        | 4.19        | 5.29         | 8.59        | 7.92        | 6.36         | 4.93        | 4.85        |
| Tonroe 110 kV        | 2.70         | 3.10        | 3.01        | 3.75         | 1.98        | 1.97        | 2.72         | 3.80        | 3.50        | 3.85         | 2.14        | 2.11        |
| Trabeg 110 kV        | 6.93         | 13.21       | 11.92       | 7.67         | 15.85       | 15.19       | 5.82         | 21.69       | 19.19       | 6.86         | 23.24       | 22.20       |
| Tralee 110 kV        | 5.00         | 7.17        | 6.78        | 5.94         | 6.73        | 6.60        | 5.11         | 12.01       | 10.79       | 6.34         | 9.07        | 8.81        |
| Trien A 110 kV       | 4.78         | 6.67        | 6.34        | 5.91         | 6.19        | 6.09        | 4.32         | 9.96        | 9.28        | 5.81         | 7.84        | 7.69        |
| Trien B 110 kV       | 12.85        | 7.45        | 7.16        | 9.79         | 6.39        | 6.31        | 12.68        | 12.56       | 10.77       | 9.06         | 8.48        | 8.16        |
| Trillick 110 kV      | 2.82         | 2.47        | 2.39        | 3.50         | 2.68        | 2.65        | 3.53         | 4.30        | 3.77        | 4.49         | 3.75        | 3.60        |
| Trinity 110 kV       | 12.19        | 12.43       | 11.43       | 6.33         | 14.96       | 14.45       | 11.42        | 14.76       | 13.18       | 5.99         | 17.22       | 16.44       |
| Tullabeg 110 kV      | 6.39         | 5.81        | 5.63        | 6.59         | 5.17        | 5.12        | 7.12         | 8.93        | 8.57        | 7.03         | 6.57        | 6.51        |
| Tullabrack 110 kV    | 6.66         | 6.10        | 5.88        | 7.29         | 4.98        | 4.93        | 6.53         | 8.15        | 7.74        | 7.28         | 5.82        | 5.75        |
| Turlough 220 kV      | 11.59        | 11.68       | 10.54       | 12.79        | 10.60       | 10.25       | 9.84         | 13.84       | 12.93       | 11.44        | 11.74       | 11.51       |
| Tynagh 220 kV        | 17.31        | 11.19       | 10.04       | 18.46        | 12.50       | 11.98       | 15.21        | 13.68       | 12.74       | 16.49        | 14.57       | 14.19       |
| Uggool 110 kV        | 5.50         | 6.14        | 5.87        | 5.20         | 8.02        | 7.86        | 6.33         | 9.10        | 8.54        | 5.65         | 11.25       | 10.95       |
| Waterford 110 kV     | 8.01         | 10.81       | 10.17       | 8.38         | 12.17       | 11.89       | 7.28         | 14.80       | 13.70       | 7.78         | 15.29       | 14.87       |
| Wexford 110 kV       | 5.71         | 5.85        | 5.64        | 6.94         | 5.67        | 5.60        | 5.74         | 8.60        | 7.95        | 7.36         | 7.17        | 7.01        |
| Whitebank 110 kV     | 26.52        | 14.02       | 12.78       | 21.22        | 17.40       | 16.72       | 24.46        | 16.82       | 14.88       | 19.67        | 20.31       | 19.29       |
| Whitegate 110 kV     | 4.85         | 8.17        | 7.65        | 5.52         | 8.71        | 8.50        | 4.22         | 10.77       | 10.18       | 5.06         | 10.66       | 10.46       |
| Wolfe Tone 110 kV    | 14.12        | 10.24       | 9.53        | 5.76         | 11.98       | 11.64       | 13.90        | 12.72       | 11.50       | 5.42         | 14.30       | 13.75       |
| Woodhouse 110 kV     | 6.02         | 5.51        | 5.31        | 7.30         | 4.24        | 4.20        | 6.64         | 7.99        | 7.04        | 7.95         | 5.13        | 4.99        |
| Woodland 220 kV      | 12.42        | 18.66       | 16.16       | 12.08        | 20.47       | 19.34       | 10.55        | 27.61       | 24.98       | 10.58        | 27.92       | 26.94       |
| Woodland 400 kV      | 15.86        | 7.93        | 7.21        | 16.35        | 8.96        | 8.63        | 12.72        | 13.55       | 12.83       | 13.04        | 14.32       | 14.04       |

|                       |              |          | Sum   | mer          |          |       |              |         | Wi    | nter         |          |       |
|-----------------------|--------------|----------|-------|--------------|----------|-------|--------------|---------|-------|--------------|----------|-------|
|                       | Th           | iree pha |       | -            | ngle Pha |       | Th           | ree pha |       |              | ngle Pha |       |
|                       |              | lk"      | lk'   |              | lk"      | lk'   |              | lk"     | Ik'   |              | lk"      | lk'   |
| Station               | X/R<br>Ratio | [kA]     | [kA]  | X/R<br>Ratio | [kA]     | [kA]  | X/R<br>Ratio | [kA]    | [kA]  | X/R<br>Ratio | [kA]     | [kA]  |
| Adamstown 110 kV      | 12.11        | 11.49    | 10.57 | 6.44         | 13.75    | 13.28 | 11.49        | 13.48   | 12.10 | 6.11         | 15.73    | 15.05 |
| Agannygal 110 kV      | 2.82         | 4.79     | 4.66  | 3.86         | 4.11     | 4.08  | 2.98         | 6.29    | 5.66  | 4.24         | 4.82     | 4.69  |
| Aghada 110 kV         | 5.11         | 7.72     | 7.29  | 6.03         | 9.17     | 8.96  | 4.57         | 9.89    | 9.39  | 5.61         | 11.22    | 11.00 |
| Aghada A 220 kV       | 10.97        | 10.19    | 9.17  | 11.78        | 13.62    | 12.96 | 12.96        | 19.70   | 17.49 | 14.13        | 23.76    | 22.58 |
| Aghada B 220 kV       | 10.97        | 10.19    | 9.17  | 11.78        | 13.62    | 12.96 | 12.96        | 19.70   | 17.49 | 14.13        | 23.76    | 22.58 |
| Aghada C 220 kV       | 10.77        | 9.97     | 8.99  | 10.82        | 13.30    | 12.67 | 12.34        | 18.93   | 16.88 | 11.85        | 22.88    | 21.78 |
| Aghada D 220 kV       | 10.97        | 10.19    | 9.17  | 11.78        | 13.62    | 12.96 | 12.96        | 19.70   | 17.49 | 14.13        | 23.76    | 22.58 |
| Ahane 110 kV          | 5.43         | 10.74    | 10.02 | 6.00         | 9.38     | 9.19  | 4.86         | 15.42   | 14.22 | 5.73         | 11.46    | 11.23 |
| Anner 110 kV          | 4.04         | 5.88     | 5.60  | 4.52         | 4.50     | 4.44  | 3.99         | 7.68    | 7.12  | 4.56         | 5.08     | 4.99  |
| Ardnacrusha 110 kV    | 5.93         | 11.70    | 10.82 | 7.08         | 13.11    | 12.72 | 5.93         | 18.98   | 16.94 | 7.58         | 18.30    | 17.61 |
| Ardnagappary 110 kV   | 2.75         | 1.90     | 1.86  | 3.92         | 1.24     | 1.23  | 2.90         | 2.62    | 2.43  | 4.26         | 1.35     | 1.34  |
| Arigna 110 kV         | 4.38         | 6.17     | 5.93  | 5.40         | 5.20     | 5.14  | 4.53         | 8.66    | 7.97  | 5.76         | 6.17     | 6.04  |
| Arklow 110 kV         | 10.63        | 7.78     | 7.50  | 11.48        | 9.48     | 9.33  | 10.32        | 10.36   | 9.78  | 11.53        | 11.93    | 11.66 |
| Arklow 220 kV         | 9.18         | 7.27     | 6.93  | 10.60        | 6.75     | 6.65  | 9.07         | 9.00    | 8.65  | 10.64        | 7.77     | 7.68  |
| Artane 110 kV         | 13.75        | 11.55    | 10.81 | 5.86         | 13.61    | 13.25 | 13.09        | 13.40   | 12.18 | 5.63         | 15.44    | 14.86 |
| Arva 110 kV           | 3.88         | 8.10     | 7.66  | 4.96         | 6.62     | 6.52  | 3.87         | 10.86   | 9.87  | 5.18         | 7.67     | 7.49  |
| Athea 110 kV          | 11.07        | 6.94     | 6.72  | 11.79        | 7.25     | 7.17  | 11.49        | 11.11   | 9.52  | 12.28        | 9.98     | 9.49  |
| Athlone 110 kV        | 4.06         | 6.39     | 6.13  | 5.31         | 5.23     | 5.17  | 3.85         | 7.81    | 7.27  | 5.24         | 5.71     | 5.61  |
| Athy 110 kV           | 5.08         | 6.91     | 6.68  | 6.13         | 5.82     | 5.76  | 4.71         | 8.28    | 7.94  | 5.96         | 6.51     | 6.44  |
| Aughinish 110 kV      | 8.99         | 9.68     | 8.62  | 10.97        | 10.65    | 10.19 | 8.33         | 12.30   | 11.27 | 10.63        | 12.28    | 11.92 |
| Ballinknockane 110 kV | 8.25         | 8.98     | 8.15  | 8.79         | 8.22     | 7.97  | 8.03         | 12.04   | 11.23 | 8.74         | 9.68     | 9.50  |
| Ballybeg 110 kV       | 9.85         | 6.10     | 5.90  | 10.09        | 7.21     | 7.12  | 9.65         | 7.28    | 6.96  | 9.99         | 8.34     | 8.20  |
| Ballydine 110 kV      | 4.07         | 6.56     | 6.26  | 3.80         | 5.37     | 5.30  | 3.95         | 8.34    | 7.81  | 3.73         | 6.07     | 5.97  |
| Ballylickey 110 kV    | 2.82         | 2.92     | 2.84  | 3.84         | 1.97     | 1.95  | 2.96         | 4.01    | 3.74  | 4.06         | 2.25     | 2.22  |
| Ballynahulla 110 kV   | 14.38        | 7.74     | 7.45  | 12.93        | 8.23     | 8.12  | 16.43        | 12.28   | 10.84 | 13.24        | 11.38    | 10.92 |
| Ballynahulla 220 kV   | 8.79         | 7.00     | 6.62  | 8.98         | 7.85     | 7.68  | 9.12         | 11.50   | 10.49 | 9.17         | 11.24    | 10.89 |
| Ballyragget 110 kV    | 5.76         | 6.27     | 6.07  | 6.66         | 4.57     | 4.54  | 5.48         | 7.39    | 7.04  | 6.54         | 4.97     | 4.91  |
| Ballyvouskill 110 kV  | 14.15        | 7.54     | 7.24  | 13.78        | 8.90     | 8.75  | 14.93        | 12.82   | 11.25 | 13.94        | 13.25    | 12.64 |
| Ballyvouskill 220 kV  | 8.67         | 6.89     | 6.50  | 9.31         | 8.57     | 8.36  | 9.16         | 11.71   | 10.65 | 9.95         | 13.08    | 12.60 |
| Ballywater 110 kV     | 5.52         | 5.45     | 5.31  | 3.46         | 5.65     | 5.60  | 5.37         | 7.83    | 7.57  | 3.15         | 7.12     | 7.05  |
| Baltrasna 110 kV      | 6.35         | 9.77     | 9.18  | 7.41         | 7.66     | 7.54  | 5.82         | 11.53   | 11.00 | 7.13         | 8.50     | 8.40  |
| Bancroft 110 kV       | 13.04        | 11.73    | 10.89 | 7.08         | 13.61    | 13.21 | 12.04        | 13.42   | 12.45 | 6.66         | 15.26    | 14.82 |
| Bandon 110 kV         | 3.36         | 5.63     | 5.35  | 4.34         | 5.65     | 5.55  | 3.10         | 7.90    | 7.22  | 4.34         | 7.05     | 6.86  |
| Banoge 110 kV         | 6.31         | 5.58     | 5.43  | 7.08         | 5.07     | 5.02  | 6.57         | 7.87    | 7.58  | 7.41         | 6.20     | 6.14  |
| Barnageeragh 110 kV   | 10.56        | 19.14    | 16.94 | 10.36        | 22.44    | 21.35 | 9.05         | 24.10   | 21.99 | 9.18         | 26.88    | 25.95 |
| Barnahealy A 110 kV   | 5.21         | 10.00    | 9.30  | 5.80         | 10.85    | 10.56 | 4.45         | 13.79   | 12.80 | 5.24         | 13.74    | 13.39 |
| Barnahealy B 110 kV   | 6.96         | 9.83     | 9.16  | 7.40         | 10.55    | 10.28 | 6.11         | 13.90   | 12.84 | 6.83         | 13.54    | 13.18 |
| Barnakyle 110 kV      | 19.75        | 19.29    | 17.06 | 20.72        | 13.33    | 12.94 | 18.21        | 21.90   | 19.85 | 19.79        | 14.41    | 14.09 |
| Baroda 110 kV         | 4.02         | 8.07     | 7.70  | 4.77         | 9.33     | 9.16  | 3.99         | 11.08   | 10.32 | 4.93         | 11.75    | 11.46 |
| Barrymore 110 kV      | 3.95         | 6.67     | 6.36  | 4.93         | 4.26     | 4.22  | 3.69         | 8.77    | 8.29  | 4.88         | 4.83     | 4.78  |
| Belcamp 110 kV        | 20.48        | 18.61    | 16.57 | 16.94        | 22.38    | 21.32 | 17.94        | 22.05   | 19.42 | 15.32        | 26.02    | 24.69 |
| Belcamp 220 kV        | 15.31        | 20.89    | 18.01 | 12.42        | 24.58    | 23.08 | 12.57        | 25.72   | 22.52 | 10.47        | 29.26    | 27.71 |

|                           |       |          | Sum   | mer   |          |       |       |          | Wi    | nter  |          |       |
|---------------------------|-------|----------|-------|-------|----------|-------|-------|----------|-------|-------|----------|-------|
|                           | Th    | iree pha | se    | Si    | ngle Pha | ise   | Th    | iree pha | se    | Si    | ingle Ph | ase   |
|                           | X/R   | lk"      | lk'   |
| Station                   | Ratio | [kA]     | [kA]  |
| Belgard 110 kV            | 12.57 | 12.12    | 11.17 | 6.85  | 14.70    | 14.21 | 11.85 | 13.78    | 12.60 | 6.53  | 16.48    | 15.88 |
| Bellacorick 110 kV        | 3.36  | 3.53     | 3.42  | 3.68  | 4.55     | 4.49  | 5.90  | 8.97     | 7.51  | 6.51  | 9.57     | 8.94  |
| Binbane 110 kV            | 3.17  | 3.52     | 3.40  | 4.29  | 3.45     | 3.41  | 3.81  | 6.73     | 6.21  | 5.82  | 5.00     | 4.90  |
| Blackrock 110 kV          | 10.33 | 12.25    | 11.38 | 2.46  | 11.75    | 11.48 | 9.84  | 14.34    | 12.82 | 2.38  | 13.03    | 12.58 |
| Blake 110 kV              | 3.96  | 7.45     | 7.13  | 4.96  | 5.28     | 5.23  | 3.83  | 9.30     | 8.84  | 4.97  | 5.92     | 5.85  |
| Blundestown 110 kV        | 4.14  | 7.61     | 7.26  | 4.85  | 4.97     | 4.92  | 4.29  | 9.62     | 9.34  | 5.00  | 5.61     | 5.58  |
| Boggeragh 110 kV          | 6.15  | 6.15     | 5.91  | 7.22  | 6.77     | 6.67  | 6.67  | 9.29     | 8.48  | 8.00  | 8.94     | 8.68  |
| Booltiagh 110 kV          | 6.09  | 6.37     | 6.15  | 7.65  | 5.59     | 5.53  | 6.65  | 9.19     | 8.37  | 8.52  | 6.84     | 6.68  |
| Bracetown 220 kV          | 13.64 | 19.25    | 16.81 | 9.13  | 17.52    | 16.76 | 11.28 | 23.40    | 20.96 | 8.06  | 20.26    | 19.58 |
| Bracklone 110 kV          | 3.85  | 7.95     | 7.61  | 4.83  | 7.54     | 7.43  | 3.65  | 10.39    | 9.83  | 4.81  | 8.88     | 8.73  |
| Brinny A 110 kV           | 3.22  | 5.11     | 4.87  | 4.20  | 4.72     | 4.65  | 2.97  | 6.93     | 6.40  | 4.17  | 5.69     | 5.57  |
| Brinny B 110 kV           | 3.22  | 5.13     | 4.89  | 4.20  | 4.75     | 4.68  | 2.97  | 6.96     | 6.43  | 4.17  | 5.74     | 5.61  |
| Buffy 110 kV              | 3.82  | 4.48     | 4.33  | 4.12  | 5.47     | 5.40  | 5.35  | 7.98     | 6.78  | 5.56  | 8.55     | 8.04  |
| Bunkimalta 110 kV         | 5.22  | 5.11     | 4.92  | 5.49  | 5.35     | 5.28  | 6.52  | 8.09     | 7.12  | 6.39  | 7.40     | 7.10  |
| Butlerstown 110 kV        | 6.91  | 9.80     | 9.33  | 7.03  | 10.14    | 9.97  | 6.22  | 12.70    | 11.83 | 6.53  | 12.07    | 11.80 |
| Cabra 110 kV              | 12.57 | 11.13    | 10.44 | 4.74  | 12.15    | 11.86 | 11.99 | 12.90    | 11.74 | 4.57  | 13.69    | 13.22 |
| Cahir 110 kV              | 4.36  | 7.27     | 6.90  | 5.38  | 6.25     | 6.15  | 4.57  | 10.79    | 9.75  | 5.80  | 7.52     | 7.33  |
| Carlow 110 kV             | 5.92  | 8.07     | 7.76  | 6.66  | 8.68     | 8.56  | 5.72  | 10.33    | 9.61  | 6.57  | 10.31    | 10.06 |
| Carrickaduff 110 kV       | 4.24  | 3.28     | 3.19  | 5.19  | 2.62     | 2.60  | 7.40  | 7.39     | 5.84  | 7.03  | 3.57     | 3.42  |
| Carrickalangan 110 kV     | 4.24  | 3.25     | 3.16  | 5.18  | 2.56     | 2.54  | 7.35  | 7.25     | 5.75  | 6.96  | 3.47     | 3.33  |
| Carrickmines 220 kV       | 16.59 | 19.03    | 16.64 | 9.35  | 22.68    | 21.41 | 13.63 | 23.12    | 20.58 | 7.97  | 26.57    | 25.32 |
| Carrickmines A 110 kV     | 33.91 | 11.58    | 10.84 | 24.36 | 12.62    | 12.31 | 31.67 | 13.31    | 12.27 | 23.08 | 14.11    | 13.70 |
| Carrickmines B 110 kV     | 27.46 | 13.00    | 12.03 | 21.55 | 15.49    | 15.01 | 24.76 | 15.03    | 13.88 | 19.81 | 17.55    | 17.00 |
| Carrick-on-Shannon 110 kV | 4.42  | 9.55     | 8.98  | 5.07  | 10.67    | 10.42 | 4.25  | 14.02    | 12.80 | 5.13  | 14.03    | 13.59 |
| Carrigadrohid 110 kV      | 6.85  | 10.16    | 9.51  | 7.04  | 10.38    | 10.14 | 6.56  | 15.92    | 14.45 | 6.87  | 13.86    | 13.46 |
| Carrigdangan 110 kV       | 3.44  | 4.33     | 4.18  | 4.10  | 5.12     | 5.06  | 4.13  | 6.99     | 6.09  | 5.21  | 7.29     | 6.93  |
| Carrowbeg 110 kV          | 2.70  | 2.54     | 2.46  | 3.57  | 2.39     | 2.36  | 2.67  | 3.42     | 3.16  | 3.74  | 2.87     | 2.80  |
| Cashla 110 kV             | 7.66  | 13.25    | 12.29 | 7.99  | 16.92    | 16.37 | 7.20  | 21.29    | 19.14 | 7.68  | 25.13    | 24.06 |
| Cashla 220 kV             | 8.33  | 9.23     | 8.58  | 9.42  | 9.56     | 9.31  | 8.56  | 12.72    | 11.96 | 9.79  | 11.99    | 11.76 |
| Castlebagot 110 kV        | 21.51 | 19.69    | 17.38 | 23.31 | 13.70    | 13.29 | 19.82 | 22.39    | 20.26 | 22.23 | 14.82    | 14.48 |
| Castlebagot 220 kV        | 11.90 | 21.57    | 18.55 | 9.88  | 22.34    | 21.11 | 9.71  | 27.33    | 24.15 | 8.44  | 26.72    | 25.59 |
| Castlebar 110 kV          | 3.10  | 4.19     | 4.03  | 3.65  | 4.68     | 4.61  | 3.33  | 6.89     | 6.11  | 4.12  | 6.48     | 6.23  |
| Castledockrill 110 kV     | 7.64  | 6.65     | 6.46  | 4.56  | 7.76     | 7.67  | 7.51  | 9.54     | 9.20  | 4.10  | 9.95     | 9.82  |
| Castlefarm A 110 kV       | 8.06  | 9.33     | 8.33  | 9.49  | 9.91     | 9.50  | 7.36  | 11.76    | 10.80 | 9.05  | 11.35    | 11.03 |
| Castlefarm B 110 kV       | 8.08  | 9.32     | 8.32  | 9.50  | 9.90     | 9.49  | 7.37  | 11.74    | 10.78 | 9.06  | 11.33    | 11.02 |
| Castleview 110 kV         | 4.40  | 9.96     | 9.30  | 5.40  | 10.19    | 9.94  | 3.72  | 13.84    | 12.84 | 4.96  | 12.79    | 12.49 |
| Cathaleen's Fall 110 kV   | 4.21  | 6.36     | 6.04  | 4.85  | 7.23     | 7.09  | 5.16  | 13.55    | 11.66 | 6.22  | 11.89    | 11.34 |
| Cauteen 110 kV            | 5.31  | 6.25     | 6.00  | 6.28  | 4.29     | 4.25  | 5.92  | 9.54     | 8.70  | 6.75  | 5.10     | 5.02  |
| Central Park 110 kV       | 15.09 | 10.59    | 9.96  | 7.75  | 11.32    | 11.07 | 14.31 | 12.10    | 11.21 | 7.46  | 12.58    | 12.24 |
| Charleville 110 kV        | 4.52  | 5.46     | 5.24  | 5.89  | 5.16     | 5.10  | 4.77  | 7.75     | 7.04  | 6.53  | 6.51     | 6.33  |
| Cherrywood 110 kV         | 10.62 | 9.80     | 9.24  | 7.57  | 9.94     | 9.74  | 10.14 | 11.11    | 10.34 | 7.32  | 10.96    | 10.70 |
| City West 110 kV          | 6.10  | 7.44     | 7.00  | 6.08  | 5.61     | 5.53  | 5.84  | 8.63     | 7.84  | 5.94  | 6.16     | 6.02  |

|                      |              |             | Sum         | mer          |             |             | Winter                   |             |             |              |             |             |  |  |
|----------------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------------------|-------------|-------------|--------------|-------------|-------------|--|--|
|                      | ты           | roo nha     |             |              | aglo Dha    |             | Three phase Single Phase |             |             |              |             |             |  |  |
|                      |              | ree pha     |             |              | ngle Pha    |             |                          | <u> </u>    | 1           |              |             |             |  |  |
| Station              | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] | X/R<br>Ratio             | lk"<br>[kA] | lk'<br>[kA] | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] |  |  |
| Clahane 110 kV       | 4.23         | 6.37        | 6.10        | 5.20         | 6.02        | 5.94        | 4.10                     | 9.63        | 8.96        | 5.34         | 7.62        | 7.47        |  |  |
| Clashavoon 220 kV    | 8.74         | 7.39        | 6.91        | 9.45         | 8.92        | 8.67        | 9.16                     | 12.39       | 11.34       | 10.02        | 13.35       | 12.91       |  |  |
| Clashavoon A 110 kV  | 7.74         | 11.55       | 10.73       | 8.06         | 15.05       | 14.56       | 7.91                     | 19.59       | 17.42       | 8.27         | 23.35       | 22.24       |  |  |
| Clashavoon B 110 kV  | 7.74         | 11.55       | 10.73       | 8.06         | 15.05       | 14.56       | 7.91                     | 19.59       | 17.42       | 8.27         | 23.35       | 22.24       |  |  |
| Cliff 110 kV         | 3.98         | 5.23        | 5.01        | 4.92         | 5.37        | 5.29        | 4.49                     | 9.50        | 8.50        | 5.92         | 7.62        | 7.38        |  |  |
| Cloghboola 110 kV    | 7.33         | 6.00        | 5.84        | 9.57         | 6.27        | 6.21        | 7.49                     | 9.51        | 8.01        | 10.80        | 8.55        | 8.09        |  |  |
| Cloghboola 110 kV    | 7.33         | 6.00        | 5.84        | 9.57         | 6.27        | 6.21        | 7.49                     | 9.51        | 8.01        | 10.80        | 8.55        | 8.09        |  |  |
| Clogher 110 kV       | 3.82         | 5.32        | 5.08        | 4.36         | 6.12        | 6.02        | 5.34                     | 12.75       | 10.19       | 6.30         | 10.97       | 10.22       |  |  |
| Cloghran 110 kV      | 10.47        | 19.27       | 17.03       | 10.73        | 22.68       | 21.56       | 8.96                     | 24.28       | 22.13       | 9.50         | 27.21       | 26.25       |  |  |
| Clonee 220 kV        | 14.10        | 19.54       | 17.04       | 10.14        | 17.92       | 17.12       | 11.63                    | 23.80       | 21.29       | 8.92         | 20.75       | 20.04       |  |  |
| Clonkeen A 110 kV    | 5.70         | 5.38        | 5.18        | 6.76         | 4.08        | 4.04        | 5.59                     | 6.85        | 6.50        | 6.80         | 4.63        | 4.58        |  |  |
| Clonkeen B 110 kV    | 4.97         | 6.42        | 6.20        | 4.37         | 7.52        | 7.42        | 4.65                     | 10.63       | 9.34        | 3.98         | 10.98       | 10.47       |  |  |
| Cloon 110 kV         | 4.48         | 6.66        | 6.38        | 5.79         | 5.98        | 5.90        | 4.07                     | 8.77        | 8.17        | 5.65         | 7.07        | 6.94        |  |  |
| Clutterland 110 kV   | 19.77        | 19.25       | 17.02       | 19.74        | 13.35       | 12.96       | 18.23                    | 21.85       | 19.80       | 18.85        | 14.42       | 14.10       |  |  |
| College Park 110 kV  | 9.50         | 17.75       | 15.87       | 6.49         | 20.99       | 20.04       | 8.19                     | 22.09       | 20.31       | 5.69         | 25.09       | 24.28       |  |  |
| Cookstown 110 kV     | 7.40         | 8.23        | 7.82        | 5.97         | 6.96        | 6.85        | 7.01                     | 9.21        | 8.74        | 5.78         | 7.59        | 7.48        |  |  |
| Cookstown A 110 kV   | 4.98         | 6.35        | 6.02        | 5.23         | 4.53        | 4.47        | 4.79                     | 7.35        | 6.69        | 5.13         | 4.94        | 4.83        |  |  |
| Coolnabacky 110 kV   | 7.90         | 12.16       | 11.50       | 8.27         | 15.30       | 14.94       | 7.57                     | 16.43       | 15.56       | 8.07         | 19.68       | 19.26       |  |  |
| Coolnabacky 400 kV   | 10.03        | 8.02        | 7.33        | 9.89         | 8.09        | 7.83        | 8.81                     | 10.46       | 9.86        | 8.95         | 9.77        | 9.59        |  |  |
| Coolroe 110 kV       | 3.93         | 8.16        | 7.71        | 5.06         | 8.12        | 7.97        | 3.48                     | 11.35       | 10.52       | 4.86         | 10.08       | 9.85        |  |  |
| Coomagearlahy 110 kV | 5.00         | 5.16        | 5.02        | 5.46         | 6.14        | 6.08        | 5.17                     | 8.47        | 7.35        | 5.83         | 9.08        | 8.61        |  |  |
| Coomataggart 110 kV  | 9.70         | 5.02        | 4.88        | 6.98         | 3.46        | 3.44        | 10.05                    | 8.09        | 7.19        | 6.64         | 4.19        | 4.10        |  |  |
| Coomataggart 110 kV  | 9.70         | 5.02        | 4.88        | 6.98         | 3.46        | 3.44        | 10.05                    | 8.09        | 7.19        | 6.64         | 4.19        | 4.10        |  |  |
| Cordal 110 kV        | 11.78        | 6.66        | 6.44        | 8.19         | 7.08        | 7.00        | 12.91                    | 10.49       | 9.31        | 7.62         | 9.74        | 9.36        |  |  |
| Corderry 110 kV      | 4.01         | 6.28        | 6.02        | 4.96         | 6.28        | 6.19        | 4.16                     | 9.78        | 8.74        | 5.48         | 8.18        | 7.92        |  |  |
| Corduff 110 kV       | 11.15        | 20.56       | 18.09       | 12.01        | 24.62       | 23.34       | 9.46                     | 26.31       | 23.88       | 10.58        | 30.10       | 28.97       |  |  |
| Corduff 220 kV       | 18.38        | 23.03       | 19.69       | 15.69        | 26.78       | 25.06       | 14.68                    | 28.63       | 25.00       | 12.96        | 32.00       | 30.31       |  |  |
| Corkagh 110 kV       | 20.35        | 19.38       | 17.12       | 21.04        | 13.36       | 12.96       | 18.76                    | 22.01       | 19.93       | 20.09        | 14.44       | 14.12       |  |  |
| Corraclassy 110 kV   | 4.26         | 5.92        | 5.62        | 5.38         | 4.72        | 4.66        | 4.29                     | 7.50        | 7.03        | 5.60         | 5.25        | 5.18        |  |  |
| Cow Cross 110 kV     | 4.80         | 10.02       | 9.34        | 5.10         | 9.29        | 9.08        | 4.06                     | 13.86       | 12.85       | 4.65         | 11.43       | 11.19       |  |  |
| Crane 110 kV         | 7.74         | 7.27        | 7.03        | 7.49         | 8.00        | 7.90        | 8.46                     | 11.71       | 11.11       | 7.80         | 11.02       | 10.84       |  |  |
| Croaghaun 110 kV     | 3.44         | 3.30        | 3.20        | 3.85         | 4.15        | 4.10        | 5.98                     | 7.88        | 6.66        | 6.85         | 8.17        | 7.68        |  |  |
| Croaghnagawna 110 kV | 4.21         | 3.41        | 3.31        | 5.21         | 2.85        | 2.82        | 7.34                     | 7.81        | 6.16        | 7.32         | 3.99        | 3.81        |  |  |
| Cromcastle A 110 kV  | 11.46        | 16.79       | 15.11       | 6.50         | 19.72       | 18.88       | 10.33                    | 19.73       | 17.55       | 6.01         | 22.67       | 21.63       |  |  |
| Cromcastle B 110 kV  | 11.46        | 16.79       | 15.11       | 6.50         | 19.72       | 18.88       | 10.33                    | 19.73       | 17.55       | 6.01         | 22.67       | 21.63       |  |  |
| Crory 110 kV         | 9.55         | 7.50        | 7.26        | 9.77         | 9.40        | 9.27        | 10.12                    | 11.23       | 10.76       | 10.15        | 12.73       | 12.52       |  |  |
| Cruiserath 220 kV    | 17.87        | 22.85       | 19.55       | 15.09        | 26.52       | 24.84       | 14.31                    | 28.37       | 24.80       | 12.49        | 31.65       | 29.99       |  |  |
| Cullenagh 110 kV     | 8.55         | 11.63       | 10.99       | 9.04         | 13.62       | 13.32       | 7.66                     | 15.56       | 14.43       | 8.28         | 16.92       | 16.45       |  |  |
| Cullenagh 220 kV     | 9.17         | 8.26        | 7.85        | 9.38         | 8.44        | 8.29        | 8.53                     | 10.69       | 10.28       | 8.84         | 9.92        | 9.80        |  |  |
| Cunghill 110 kV      | 3.16         | 4.49        | 4.34        | 3.64         | 4.40        | 4.35        | 3.09                     | 6.79        | 6.29        | 3.75         | 5.67        | 5.55        |  |  |
| Cureeny 110 kV       | 4.68         | 4.77        | 4.61        | 5.29         | 5.11        | 5.05        | 5.89                     | 7.59        | 6.67        | 6.51         | 7.14        | 6.84        |  |  |
| Cureeny T 110 kV     | 5.31         | 6.23        | 5.96        | 5.20         | 6.09        | 6.00        | 6.10                     | 9.58        | 8.53        | 5.55         | 8.08        | 7.81        |  |  |

|                         |       |         | Sum   | mer   |          |       |       |         | Wi    | nter         |       |       |  |
|-------------------------|-------|---------|-------|-------|----------|-------|-------|---------|-------|--------------|-------|-------|--|
|                         | Th    | ree pha | se    | Si    | ngle Pha | ise   | Th    | ree pha | se    | Single Phase |       |       |  |
|                         | X/R   | lk"     | lk'   | X/R   | lk"      | lk'   | X/R   | lk"     | lk'   | X/R          | lk"   | lk'   |  |
| Station                 | Ratio | [kA]    | [kA]  | Ratio | [kA]     | [kA]  | Ratio | [kA]    | [kA]  | Ratio        | [kA]  | [kA]  |  |
| Cushaling 110 kV        | 3.98  | 6.78    | 6.53  | 4.68  | 8.50     | 8.36  | 5.27  | 11.35   | 10.53 | 6.56         | 12.47 | 12.12 |  |
| Dallow 110 kV           | 3.47  | 4.65    | 4.53  | 4.56  | 3.06     | 3.05  | 3.49  | 5.67    | 5.37  | 4.68         | 3.32  | 3.29  |  |
| Dalton 110 kV           | 3.06  | 3.71    | 3.59  | 4.10  | 3.25     | 3.22  | 3.42  | 5.63    | 5.18  | 4.79         | 4.01  | 3.93  |  |
| Dardistown 110 kV       | 15.11 | 17.39   | 15.60 | 9.94  | 20.85    | 19.93 | 13.50 | 20.52   | 18.19 | 9.14         | 24.12 | 22.95 |  |
| Darndale 110 kV         | 18.94 | 17.97   | 16.04 | 15.94 | 20.87    | 19.94 | 16.71 | 21.20   | 18.73 | 14.53        | 24.13 | 22.97 |  |
| Derrybrien 110 kV       | 2.67  | 3.79    | 3.71  | 3.74  | 3.65     | 3.62  | 3.01  | 5.08    | 4.48  | 4.45         | 4.45  | 4.29  |  |
| Derrycarney_ 110 kV     | 5.08  | 10.90   | 10.29 | 6.01  | 13.18    | 12.87 | 4.73  | 14.64   | 13.63 | 5.85         | 16.58 | 16.13 |  |
| Derryiron 110 kV        | 4.66  | 7.23    | 6.93  | 5.78  | 7.55     | 7.44  | 5.44  | 11.11   | 10.49 | 7.07         | 9.85  | 9.68  |  |
| Doon 110 kV             | 4.33  | 6.39    | 6.07  | 4.69  | 5.03     | 4.96  | 4.36  | 8.55    | 7.88  | 4.76         | 5.74  | 5.64  |  |
| Dromada 110 kV          | 10.13 | 6.47    | 6.28  | 6.84  | 6.66     | 6.59  | 10.29 | 10.12   | 8.72  | 6.19         | 8.98  | 8.57  |  |
| Drombeg 110 kV          | 7.38  | 7.50    | 7.17  | 7.44  | 6.31     | 6.23  | 7.30  | 10.62   | 10.11 | 7.42         | 7.62  | 7.53  |  |
| Drumkeen 110 kV         | 3.47  | 4.84    | 4.63  | 4.17  | 5.08     | 5.00  | 3.81  | 9.50    | 8.09  | 4.97         | 7.62  | 7.28  |  |
| Drumline 110 kV         | 3.58  | 7.28    | 6.93  | 4.74  | 6.33     | 6.24  | 3.21  | 9.75    | 9.03  | 4.62         | 7.45  | 7.30  |  |
| Drybridge 110 kV        | 5.70  | 12.36   | 11.38 | 6.59  | 10.48    | 10.23 | 4.98  | 16.04   | 14.77 | 6.19         | 12.29 | 12.03 |  |
| Dundalk 110 kV          | 3.73  | 8.07    | 7.68  | 4.70  | 7.47     | 7.35  | 3.35  | 10.08   | 9.33  | 4.48         | 8.65  | 8.46  |  |
| Dunfirth 110 kV         | 4.51  | 6.66    | 6.39  | 5.87  | 5.44     | 5.38  | 4.56  | 8.36    | 8.08  | 6.13         | 6.18  | 6.13  |  |
| Dungarvan 110 kV        | 6.03  | 5.62    | 5.43  | 7.74  | 4.80     | 4.75  | 6.29  | 7.71    | 6.90  | 8.29         | 5.77  | 5.61  |  |
| Dunmanway 110 kV        | 4.15  | 6.58    | 6.25  | 4.90  | 6.89     | 6.77  | 4.44  | 10.91   | 9.56  | 5.48         | 9.58  | 9.19  |  |
| Dunstown 220 kV         | 11.32 | 17.73   | 15.82 | 11.39 | 20.22    | 19.31 | 9.76  | 22.49   | 20.74 | 10.01        | 24.51 | 23.77 |  |
| Dunstown 400 kV         | 10.80 | 8.02    | 7.33  | 12.69 | 8.71     | 8.42  | 9.26  | 10.29   | 9.70  | 11.29        | 10.54 | 10.32 |  |
| Ennis 110 kV            | 4.46  | 9.25    | 8.73  | 5.64  | 8.55     | 8.39  | 4.42  | 14.18   | 12.55 | 5.96         | 10.92 | 10.57 |  |
| Fassaroe East 110 kV    | 5.26  | 7.71    | 7.34  | 5.37  | 5.87     | 5.80  | 5.01  | 8.67    | 8.19  | 5.24         | 6.39  | 6.30  |  |
| Fassaroe West 110 kV    | 5.41  | 7.87    | 7.49  | 5.47  | 6.07     | 5.99  | 5.14  | 8.86    | 8.36  | 5.33         | 6.61  | 6.51  |  |
| Finglas 220 kV          | 19.40 | 22.53   | 19.26 | 17.78 | 27.25    | 25.44 | 15.60 | 27.95   | 24.28 | 14.62        | 32.76 | 30.87 |  |
| Finglas A 110 kV        | 21.04 | 18.55   | 16.58 | 12.13 | 21.91    | 20.92 | 18.44 | 22.22   | 19.54 | 11.08        | 25.60 | 24.30 |  |
| Finglas B 110 kV        | 37.45 | 13.02   | 12.10 | 32.89 | 16.02    | 15.54 | 35.35 | 15.23   | 13.75 | 31.12        | 18.45 | 17.67 |  |
| Flagford 110 kV         | 4.73  | 9.98    | 9.36  | 5.43  | 12.25    | 11.93 | 4.59  | 14.84   | 13.52 | 5.57         | 16.78 | 16.18 |  |
| Flagford 220 kV         | 6.98  | 6.23    | 5.91  | 8.90  | 6.07     | 5.96  | 7.59  | 8.34    | 7.97  | 9.95         | 7.32  | 7.21  |  |
| Fortunestown 110 kV     | 5.70  | 7.33    | 6.90  | 5.65  | 5.54     | 5.46  | 5.46  | 8.50    | 7.72  | 5.52         | 6.08  | 5.94  |  |
| Francis Street A 110 kV | 10.84 | 12.25   | 11.38 | 5.19  | 14.52    | 14.09 | 10.32 | 14.36   | 12.83 | 4.99         | 16.49 | 15.76 |  |
| Francis Street B 110 kV | 13.27 | 12.09   | 11.20 | 6.71  | 14.61    | 14.15 | 12.51 | 13.78   | 12.64 | 6.39         | 16.39 | 15.82 |  |
| Gallanstown 110 kV      | 6.67  | 10.75   | 10.04 | 6.98  | 7.77     | 7.64  | 6.64  | 13.90   | 13.29 | 7.02         | 8.91  | 8.82  |  |
| Galway 110 kV           | 5.06  | 10.22   | 9.58  | 4.64  | 12.65    | 12.31 | 5.19  | 16.72   | 14.88 | 4.52         | 18.74 | 17.90 |  |
| Garrow 110 kV           | 10.35 | 7.27    | 6.99  | 10.37 | 8.62     | 8.49  | 10.41 | 12.33   | 10.81 | 10.33        | 12.86 | 12.25 |  |
| Garvagh 110 kV          | 4.17  | 5.17    | 4.99  | 5.30  | 5.05     | 5.00  | 4.56  | 7.71    | 6.91  | 6.12         | 6.35  | 6.15  |  |
| Gilra 110 kV            | 3.25  | 5.85    | 5.60  | 4.06  | 4.69     | 4.64  | 3.00  | 7.21    | 6.84  | 3.96         | 5.24  | 5.17  |  |
| Glanagow 220 kV         | 11.31 | 10.22   | 9.18  | 11.58 | 13.59    | 12.93 | 12.93 | 19.06   | 16.96 | 12.86        | 23.01 | 21.89 |  |
| Glanlee 110 kV          | 4.88  | 5.11    | 4.97  | 5.12  | 6.06     | 5.99  | 5.00  | 8.34    | 7.25  | 5.30         | 8.92  | 8.45  |  |
| Glasmore A 110 kV       | 3.89  | 7.82    | 7.39  | 4.41  | 5.26     | 5.20  | 3.74  | 9.05    | 8.28  | 4.33         | 5.73  | 5.62  |  |
| Glenlara A 110 kV       | 3.06  | 2.67    | 2.61  | 4.32  | 2.34     | 2.33  | 3.25  | 3.45    | 3.16  | 4.77         | 2.75  | 2.68  |  |
| Glenlara B 110 kV       | 8.88  | 5.80    | 5.63  | 6.55  | 6.45     | 6.38  | 9.19  | 8.98    | 7.94  | 6.06         | 8.89  | 8.52  |  |
| Glenree 110 kV          | 3.17  | 3.89    | 3.77  | 3.90  | 3.79     | 3.75  | 3.69  | 7.22    | 6.64  | 4.80         | 5.43  | 5.31  |  |

|                      |              |                          | Sum   | mer   |       |          | Winter     |       |         |       |       |       |  |
|----------------------|--------------|--------------------------|-------|-------|-------|----------|------------|-------|---------|-------|-------|-------|--|
|                      | Th           | Three phase Single Phase |       |       | Th    | iree pha | se         | Si    | ngle Ph | ase   |       |       |  |
| Station              | X/R          | lk"                      | lk'   | X/R   | lk"   | lk'      | X/R        | lk"   | lk'     | X/R   | lk"   | lk'   |  |
|                      | Ratio        | [kA]                     | [kA]  | Ratio | [kA]  | [kA]     | Ratio      | [kA]  | [kA]    | Ratio | [kA]  | [kA]  |  |
| Golagh 110 kV        | 3.51         | 4.66                     | 4.48  | 4.11  | 4.67  | 4.61     | 3.99       | 9.51  | 7.97    | 4.90  | 6.98  | 6.66  |  |
| Gorman 110 kV        | 6.80         | 13.26                    | 12.19 | 7.72  | 14.67 | 14.22    | 6.38       | 18.15 | 16.50   | 7.53  | 18.41 | 17.81 |  |
| Gorman 220 kV        | 9.37         | 10.65                    | 9.87  | 10.10 | 8.94  | 8.74     | 8.69       | 13.31 | 12.67   | 9.70  | 10.23 | 10.10 |  |
| Gortawee 110 kV      | 4.37         | 5.76                     | 5.45  | 5.83  | 4.82  | 4.74     | 4.44       | 7.07  | 6.60    | 6.14  | 5.33  | 5.23  |  |
| Grange 110 kV        | 14.63        | 17.75                    | 15.88 | 6.86  | 20.64 | 19.73    | 13.04      | 21.03 | 18.57   | 6.32  | 23.87 | 22.71 |  |
| Grange Castle 110 kV | 14.81        | 12.22                    | 11.19 | 9.46  | 15.02 | 14.47    | 14.11      | 14.45 | 12.89   | 8.98  | 17.36 | 16.55 |  |
| Great Island 110 kV  | 9.13         | 11.90                    | 11.28 | 10.07 | 15.43 | 15.07    | 8.49       | 16.09 | 15.02   | 9.47  | 19.67 | 19.11 |  |
| Great Island 220 kV  | 12.29        | 10.78                    | 10.16 | 13.80 | 12.96 | 12.65    | 12.49      | 14.51 | 13.87   | 13.44 | 15.57 | 15.32 |  |
| Griffinrath A 110 kV | 7.15         | 9.84                     | 9.37  | 7.48  | 9.99  | 9.82     | 6.36       | 12.41 | 11.76   | 6.94  | 11.76 | 11.56 |  |
| Griffinrath B 110 kV | 7.70         | 10.17                    | 9.67  | 7.65  | 10.00 | 9.83     | 6.86       | 12.91 | 12.22   | 7.10  | 11.76 | 11.56 |  |
| Harolds Cross 110 kV | 11.04        | 12.29                    | 11.42 | 4.90  | 14.48 | 14.06    | 10.50      | 14.39 | 12.87   | 4.71  | 16.42 | 15.70 |  |
| Harristown 110 kV    | 4.37         | 6.97                     | 6.67  | 5.41  | 5.81  | 5.74     | 4.58       | 9.36  | 9.00    | 5.79  | 6.83  | 6.76  |  |
| Heuston 110 kV       | 14.42        | 12.33                    | 11.41 | 8.10  | 15.05 | 14.57    | 13.57      | 14.07 | 12.89   | 7.70  | 16.93 | 16.32 |  |
| Huntstown A 220 kV   | 18.56        | 21.81                    | 18.72 | 15.02 | 26.35 | 24.65    | 14.94      | 26.78 | 23.38   | 12.42 | 31.41 | 29.67 |  |
| Huntstown B 220 kV   | 18.23        | 21.19                    | 18.35 | 12.03 | 24.76 | 23.30    | 14.85      | 25.75 | 22.80   | 10.13 | 29.06 | 27.67 |  |
| Ikerrin 110 kV       | 5.07         | 4.03                     | 3.91  | 5.90  | 3.20  | 3.18     | 5.63       | 5.61  | 5.11    | 6.39  | 3.74  | 3.66  |  |
| Inchicore 220 kV     | 16.07        | 22.48                    | 19.21 | 10.99 | 26.72 | 24.96    | 12.74      | 28.10 | 24.40   | 9.06  | 32.06 | 30.25 |  |
| Inchicore A 110 kV   | 31.68        | 13.61                    | 12.49 | 27.27 | 17.00 | 16.39    | 29.22      | 15.64 | 14.21   | 25.25 | 19.29 | 18.52 |  |
| Inchicore B 110 kV   | 50.77        | 13.18                    | 12.04 | 37.56 | 16.61 | 15.97    | 45.63      | 15.69 | 13.95   | 34.03 | 19.37 | 18.42 |  |
| Inniscarra 110 kV    | 3.89         | 7.95                     | 7.53  | 4.93  | 7.74  | 7.60     | 3.49       | 11.12 | 10.31   | 4.80  | 9.57  | 9.35  |  |
| Irishtown 220 kV     | 18.01        | 21.91                    | 18.76 | 12.87 | 26.51 | 24.76    | 14.52      | 26.21 | 22.93   | 10.73 | 30.65 | 28.98 |  |
| Kellis 110 kV        | 7.13         | 8.67                     | 8.32  | 8.22  | 10.23 | 10.06    | 6.67       | 10.93 | 10.24   | 7.88  | 12.22 | 11.92 |  |
| Kellis 220 kV        | 8.35         | 7.44                     | 7.11  | 10.05 | 6.47  | 6.38     | 7.94       | 8.86  | 8.56    | 9.79  | 7.19  | 7.12  |  |
| Kellystown 220 kV    | 7.33         | 16.58                    | 14.74 | 6.38  | 13.48 | 13.03    | 6.16       | 20.20 | 18.55   | 5.76  | 15.48 | 15.12 |  |
| Kilbarry 110 kV      | 7.12         | 13.98                    | 12.70 | 7.69  | 15.64 | 15.07    | 6.19       | 23.19 | 20.32   | 7.10  | 22.46 | 21.47 |  |
| Kildonan 110 kV      | 7.07         | 14.00                    | 12.79 | 5.33  | 12.84 | 12.48    | 6.23       | 16.77 | 15.70   | 4.90  | 14.56 | 14.28 |  |
| Kilkenny 110 kV      | 5.00         | 6.89                     | 6.65  | 6.46  | 5.96  | 5.90     | 4.74       | 8.32  | 7.82    | 6.35  | 6.66  | 6.55  |  |
| Kill Hill 110 kV     | 4.76         | 4.97                     | 4.79  | 5.81  | 4.62  | 4.57     | 5.59       | 7.61  | 6.81    | 6.81  | 5.86  | 5.69  |  |
| Killonan 110 kV      | 7.06         | 14.35                    | 13.11 | 8.06  | 16.53 | 15.95    | 6.78       | 23.99 | 21.25   | 8.20  | 24.05 | 23.05 |  |
| Killonan 220 kV      | 7.87         | 8.49                     | 7.90  | 9.79  | 8.52  | 8.31     | 7.75       | 12.32 | 11.60   | 10.18 | 10.87 | 10.67 |  |
| Killoteran 110 kV    | 7.80         | 10.65                    | 10.10 | 7.91  | 11.98 | 11.74    | 7.06       | 14.09 | 13.06   | 7.31  | 14.68 | 14.29 |  |
| Kilmahud 110 kV      | ,<br>19.98   | 19.28                    | 17.05 | 20.95 | 13.40 | 13.01    | ,<br>18.42 | 21.88 | 19.83   | 20.01 | 14.48 | 14.16 |  |
| Kilmore 110 kV       | 16.36        | 18.07                    | 16.14 | 10.15 | 21.54 | 20.55    | 14.52      | 21.43 | 18.90   | 9.30  | 25.00 | 23.74 |  |
| Kilpaddoge 110 kV    | 11.68        | 13.96                    | 12.90 | 12.33 | 17.71 | 17.12    | 10.15      | 22.20 | 20.32   | 11.17 | 25.91 | 25.00 |  |
| Kilpaddoge 220 kV    | 10.78        | 12.58                    | 11.50 | 10.83 | 16.62 | 15.94    | 10.32      | 20.60 | 18.82   | 10.20 | 25.62 | 24.64 |  |
| Kilpaddoge 400 kV    | 7.76         | 8.19                     | 7.48  | 7.16  | 9.04  | 8.73     | 7.26       | 11.39 | 10.68   | 6.63  | 11.56 | 11.30 |  |
| Kilteel 110 kV       | 4.35         | 7.24                     | 6.93  | 5.40  | 6.63  | 6.54     | 5.13       | 10.83 | 9.76    | 6.27  | 8.25  | 8.03  |  |
| Kinnegad 110 kV      |              | 7.56                     | 7.20  |       | 7.05  | 6.94     | 4.60       | 10.33 | 9.70    | 5.63  | 8.49  | 8.38  |  |
| Knockacummer 110 kV  | 4.39<br>7.86 | 5.06                     |       | 5.25  |       |          | 8.12       | 7.68  | 6.84    | 6.87  | 7.28  |       |  |
| Knockalough 110 kV   |              | -                        | 4.94  | 7.00  | 5.42  | 5.37     |            | -     | -       |       | 1     | 7.01  |  |
|                      | 3.96         | 4.01                     | 3.89  | 3.77  | 4.88  | 4.82     | 5.51       | 6.78  | 5.86    | 4.55  | 7.34  | 6.94  |  |
| Knockanure 220 kV    | 10.58        | 10.56                    | 9.78  | 7.88  | 13.86 | 13.38    | 10.37      | 17.06 | 15.57   | 6.81  | 21.06 | 20.25 |  |
| Knockanure A 110 kV  | 19.67        | 9.46                     | 9.06  | 16.62 | 11.03 | 10.84    | 19.62      | 15.33 | 13.13   | 15.42 | 15.84 | 14.96 |  |

|                     |              |            | Sum         | mer          |             |             |              |            | Wi          | nter         |             |             |
|---------------------|--------------|------------|-------------|--------------|-------------|-------------|--------------|------------|-------------|--------------|-------------|-------------|
|                     | Th           | ree pha    | se          | Si           | ngle Pha    | ase         | Th           | ree pha    | se          | Si           | ngle Pha    | ase         |
| Station             | X/R<br>Ratio | k"<br>[kA] | lk'<br>[kA] | X/R<br>Ratio | Ik"<br>[kA] | lk'<br>[kA] | X/R<br>Ratio | k"<br>[kA] | lk'<br>[kA] | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] |
| Knockanure B 110 kV | 4.96         | 7.28       | 6.94        | 5.90         | 6.28        | 6.20        | 4.47         | 10.34      | 9.67        | 5.73         | 7.62        | 7.49        |
| Knockearagh 110 kV  | 5.42         | 4.97       | 4.78        | 7.14         | 4.38        | 4.33        | 5.52         | 6.64       | 6.17        | 7.56         | 5.23        | 5.13        |
| Knocknamona 110 kV  | 5.74         | 5.41       | 5.23        | 5.74         | 5.41        | 5.23        | 6.39         | 7.79       | 6.85        | 6.39         | 7.79        | 6.85        |
| Knockraha A 110 kV  | 8.48         | 14.91      | 13.52       | 9.04         | 16.33       | 15.74       | 7.64         | 24.32      | 21.62       | 8.56         | 23.09       | 22.21       |
| Knockraha A 220 kV  | 10.37        | 10.51      | 9.49        | 10.53        | 12.33       | 11.82       | 10.83        | 19.55      | 17.50       | 10.74        | 19.63       | 18.87       |
| Knockraha B 110 kV  | 8.48         | 14.91      | 13.52       | 9.04         | 16.33       | 15.74       | 7.64         | 24.32      | 21.62       | 8.56         | 23.09       | 22.21       |
| Knockraha B 220 kV  | 10.37        | 10.51      | 9.49        | 10.53        | 12.33       | 11.82       | 10.83        | 19.55      | 17.50       | 10.74        | 19.63       | 18.87       |
| Knockranny 110 kV   | 5.41         | 6.46       | 6.20        | 4.88         | 8.43        | 8.28        | 6.22         | 9.56       | 8.93        | 5.17         | 11.77       | 11.44       |
| Knockranny A 110 kV | 3.82         | 4.50       | 4.35        | 4.10         | 5.50        | 5.42        | 5.34         | 8.02       | 6.82        | 5.51         | 8.58        | 8.07        |
| Knockranny B 110 kV | 5.41         | 6.46       | 6.20        | 4.88         | 8.43        | 8.28        | 6.22         | 9.56       | 8.93        | 5.17         | 11.77       | 11.44       |
| Knockumber 110 kV   | 3.86         | 7.98       | 7.50        | 4.67         | 6.05        | 5.95        | 3.52         | 9.54       | 8.96        | 4.50         | 6.62        | 6.52        |
| Lanesboro 110 kV    | 3.22         | 7.80       | 7.44        | 4.00         | 8.75        | 8.59        | 3.11         | 10.48      | 9.63        | 4.06         | 10.76       | 10.44       |
| Letterkenny110 kV   | 3.76         | 5.54       | 5.26        | 4.40         | 6.44        | 6.31        | 4.23         | 11.62      | 9.73        | 5.43         | 10.70       | 10.09       |
| Liberty A 110 kV    | 5.99         | 12.35      | 11.32       | 5.19         | 14.65       | 14.13       | 5.04         | 19.11      | 17.05       | 4.45         | 20.43       | 19.58       |
| Liberty B 110 kV    | 5.91         | 12.34      | 11.31       | 5.06         | 14.62       | 14.11       | 4.96         | 19.08      | 17.03       | 4.31         | 20.37       | 19.52       |
| Limerick 110 kV     | 5.61         | 12.83      | 11.74       | 6.30         | 12.67       | 12.29       | 4.93         | 19.80      | 17.75       | 5.94         | 16.63       | 16.11       |
| Lisdrum 110 kV      | 2.88         | 4.78       | 4.63        | 4.15         | 4.22        | 4.18        | 3.65         | 7.29       | 6.39        | 5.39         | 5.08        | 4.92        |
| Lisheen 110 kV      | 3.92         | 3.19       | 3.10        | 3.93         | 4.77        | 4.71        | 4.93         | 5.28       | 4.61        | 4.94         | 7.92        | 7.37        |
| Lodgewood 110 kV    | 9.55         | 7.50       | 7.26        | 9.77         | 9.40        | 9.27        | 10.12        | 11.23      | 10.76       | 10.15        | 12.73       | 12.52       |
| Lodgewood 220 kV    | 9.01         | 6.86       | 6.58        | 10.16        | 6.69        | 6.60        | 9.33         | 8.83       | 8.55        | 10.44        | 7.83        | 7.76        |
| Longpoint 220 kV    | 10.70        | 10.04      | 9.04        | 10.46        | 13.27       | 12.65       | 12.58        | 19.34      | 17.21       | 11.38        | 22.99       | 21.88       |
| Loughtown 220 kV    | 11.80        | 10.68      | 10.08       | 11.13        | 12.64       | 12.34       | 11.99        | 14.37      | 13.75       | 10.79        | 15.18       | 14.94       |
| Louth 220 kV        | 10.68        | 14.45      | 13.01       | 11.35        | 16.90       | 16.19       | 9.53         | 21.22      | 19.65       | 10.46        | 22.90       | 22.25       |
| Louth A 110 kV      | 7.33         | 11.63      | 10.91       | 8.34         | 14.09       | 13.72       | 6.24         | 14.53      | 13.59       | 7.38         | 16.89       | 16.45       |
| Louth A 275 kV      | 12.35        | 9.16       | 8.39        | 11.99        | 10.92       | 10.53       | 11.32        | 12.22      | 11.70       | 11.01        | 13.89       | 13.65       |
| Louth B 110 kV      | 7.93         | 12.56      | 11.74       | 8.74         | 15.58       | 15.14       | 6.66         | 16.44      | 15.27       | 7.64         | 19.44       | 18.87       |
| Louth B 275 kV      | 11.69        | 9.17       | 8.40        | 10.53        | 11.12       | 10.72       | 10.59        | 12.19      | 11.67       | 9.46         | 14.19       | 13.94       |
| Lumcloon 110 kV     | 5.28         | 6.81       | 6.57        | 6.29         | 4.97        | 4.93        | 5.46         | 8.74       | 8.38        | 6.54         | 5.58        | 5.53        |
| Macetown 110 kV     | 7.63         | 15.51      | 14.04       | 6.98         | 15.65       | 15.12       | 6.65         | 18.91      | 17.54       | 6.34         | 18.11       | 17.66       |
| Macroom 110 kV      | 7.04         | 11.15      | 10.37       | 7.02         | 12.78       | 12.42       | 6.86         | 18.59      | 16.59       | 6.82         | 18.48       | 17.76       |
| Mallow 110 kV       | 5.20         | 5.81       | 5.57        | 6.79         | 5.20        | 5.13        | 5.25         | 7.67       | 7.13        | 7.14         | 6.17        | 6.05        |
| Marina 110 kV       | 6.88         | 13.37      | 12.17       | 7.67         | 16.06       | 15.45       | 5.91         | 21.59      | 19.02       | 7.00         | 23.22       | 22.14       |
| Maynooth A 110 kV   | 11.21        | 12.26      | 11.54       | 11.93        | 15.08       | 14.71       | 10.17        | 16.23      | 15.21       | 11.08        | 19.00       | 18.52       |
| Maynooth A 220 kV   | 10.74        | 18.45      | 16.32       | 10.31        | 17.90       | 17.15       | 9.23         | 23.72      | 21.66       | 9.22         | 21.38       | 20.78       |
| Maynooth B 110 kV   | 8.24         | 16.01      | 14.61       | 9.61         | 15.59       | 15.12       | 7.09         | 19.28      | 18.13       | 8.70         | 17.83       | 17.48       |
| Maynooth B 220 kV   | 8.62         | 17.77      | 15.70       | 8.30         | 16.65       | 15.97       | 7.23         | 22.16      | 20.23       | 7.36         | 19.51       | 18.97       |
| McDermott 110 kV    | 17.08        | 11.93      | 11.14       | 5.98         | 13.71       | 13.34       | 16.21        | 13.92      | 12.59       | 5.74         | 15.58       | 14.98       |
| Meath Hill 110 kV   | 4.10         | 8.27       | 7.85        | 5.24         | 6.97        | 6.87        | 3.84         | 10.57      | 9.83        | 5.19         | 7.99        | 7.85        |
| Meentycat 110 kV    | 3.22         | 4.18       | 4.02        | 4.07         | 4.26        | 4.20        | 3.53         | 7.57       | 6.55        | 4.94         | 6.06        | 5.82        |
| Midleton 110 kV     | 4.01         | 8.63       | 8.10        | 5.01         | 7.83        | 7.68        | 3.45         | 11.48      | 10.71       | 4.67         | 9.34        | 9.16        |
| Milltown A 110 kV   | 15.49        | 13.31      | 12.30       | 6.80         | 15.98       | 15.47       | 14.62        | 15.67      | 13.93       | 6.50         | 18.24       | 17.39       |
| Milltown B 110 kV   | 9.06         | 10.89      | 10.15       | 4.12         | 12.93       | 12.57       | 8.61         | 12.38      | 11.40       | 3.95         | 14.44       | 13.97       |

|                      |              |                          | Sum         | \ <b>\</b> /i | inter       |             |                          |             |             |              |             |             |  |  |
|----------------------|--------------|--------------------------|-------------|---------------|-------------|-------------|--------------------------|-------------|-------------|--------------|-------------|-------------|--|--|
|                      | ты           | Three phase Single Phase |             |               |             |             | Three phase Single Phase |             |             |              |             |             |  |  |
|                      |              |                          |             |               |             |             |                          |             |             |              |             |             |  |  |
| Station              | X/R<br>Ratio | lk"<br>[kA]              | lk'<br>[kA] | X/R<br>Ratio  | lk"<br>[kA] | lk'<br>[kA] | X/R<br>Ratio             | lk"<br>[kA] | lk'<br>[kA] | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] |  |  |
| Misery Hill 110 kV   | 13.75        | 12.98                    | 12.02       | 7.51          | 15.72       | 15.23       | 13.02                    | 15.28       | 13.59       | 7.18         | 17.99       | 17.14       |  |  |
| Monatooreen 110 kV   | 6.35         | 14.16                    | 12.90       | 6.39          | 15.38       | 14.85       | 5.26                     | 22.42       | 20.10       | 5.62         | 21.29       | 20.53       |  |  |
| Moneteen 110 kV      | 5.77         | 9.86                     | 9.11        | 6.50          | 7.75        | 7.58        | 5.18                     | 13.02       | 12.09       | 6.21         | 8.95        | 8.79        |  |  |
| Moneypoint 110 kV    | 13.31        | 8.11                     | 7.79        | 15.94         | 8.42        | 8.30        | 13.95                    | 10.51       | 9.94        | 16.98        | 10.05       | 9.87        |  |  |
| Moneypoint 220 kV    | 10.84        | 12.44                    | 11.38       | 10.93         | 16.46       | 15.80       | 10.40                    | 20.09       | 18.41       | 10.32        | 25.11       | 24.18       |  |  |
| Moneypoint G1 400 kV | 10.04        | 8.31                     | 7.57        | 11.65         | 9.95        | 9.57        | 9.67                     | 11.57       | 10.84       | 11.51        | 12.98       | 12.66       |  |  |
| Moneypoint G2 400 kV | 24.72        | 2.98                     | 2.87        | 25.60         | 3.93        | 3.86        | 30.72                    | 3.58        | 3.48        | 30.74        | 4.62        | 4.57        |  |  |
| Moneypoint G3 400 kV | 10.04        | 8.31                     | 7.57        | 11.65         | 9.95        | 9.57        | 9.67                     | 11.57       | 10.84       | 11.51        | 12.98       | 12.66       |  |  |
| Monread 110 kV       | 4.07         | 7.23                     | 6.92        | 4.93          | 7.28        | 7.17        | 4.25                     | 10.06       | 9.29        | 5.28         | 8.93        | 8.72        |  |  |
| Mount Lucas 110 kV   | 3.73         | 5.53                     | 5.36        | 4.72          | 5.47        | 5.42        | 4.32                     | 8.34        | 7.87        | 5.64         | 7.09        | 6.97        |  |  |
| Moy 110 kV           | 3.48         | 4.10                     | 3.96        | 4.10          | 4.83        | 4.77        | 5.82                     | 9.43        | 8.36        | 7.23         | 8.71        | 8.38        |  |  |
| Kildare 110 kV       | 29.60        | 6.59                     | 6.32        | -             | -           | -           | 29.57                    | 7.13        | 6.92        | -            | -           | -           |  |  |
| Muckerstown 110 kV   | 6.36         | 9.94                     | 9.33        | 6.79          | 6.96        | 6.85        | 6.30                     | 12.69       | 12.18       | 6.83         | 7.90        | 7.83        |  |  |
| Mullagharlin 110 kV  | 3.84         | 8.22                     | 7.82        | 4.87          | 8.00        | 7.87        | 3.40                     | 9.95        | 9.34        | 4.55         | 9.15        | 8.98        |  |  |
| Mullingar 110 kV     | 3.55         | 6.54                     | 6.27        | 4.46          | 6.35        | 6.26        | 3.50                     | 8.12        | 7.70        | 4.55         | 7.31        | 7.19        |  |  |
| Mulreavy 110 kV      | 3.86         | 4.90                     | 4.70        | 4.47          | 5.75        | 5.66        | 5.44                     | 11.05       | 8.92        | 6.73         | 10.12       | 9.42        |  |  |
| Mungret A 110 kV     | 5.42         | 9.41                     | 8.72        | 6.17          | 7.23        | 7.08        | 4.84                     | 12.25       | 11.42       | 5.89         | 8.27        | 8.13        |  |  |
| Mungret B 110 kV     | 5.41         | 9.42                     | 8.73        | 6.16          | 7.23        | 7.09        | 4.83                     | 12.28       | 11.44       | 5.89         | 8.28        | 8.14        |  |  |
| Nangor 110 kV        | 13.13        | 11.92                    | 10.93       | 7.79          | 14.58       | 14.06       | 12.56                    | 14.07       | 12.58       | 7.41         | 16.80       | 16.03       |  |  |
| Navan 110 kV         | 5.82         | 11.81                    | 10.91       | 6.58          | 11.70       | 11.39       | 5.38                     | 15.72       | 14.37       | 6.35         | 14.15       | 13.76       |  |  |
| Nenagh 110 kV        | 3.32         | 3.51                     | 3.40        | 4.05          | 2.46        | 2.45        | 3.29                     | 4.55        | 4.18        | 4.13         | 2.76        | 2.71        |  |  |
| Newbridge 110 kV     | 4.16         | 9.16                     | 8.69        | 4.86          | 9.43        | 9.26        | 4.12                     | 12.96       | 12.02       | 4.98         | 11.87       | 11.60       |  |  |
| Newbury 110 kV       | 14.52        | 17.73                    | 15.86       | 6.57          | 20.45       | 19.55       | 12.95                    | 20.97       | 18.52       | 6.06         | 23.58       | 22.45       |  |  |
| North Quays 110 kV   | 19.39        | 13.58                    | 12.55       | 6.33          | 16.01       | 15.50       | 18.23                    | 16.02       | 14.22       | 6.05         | 18.25       | 17.40       |  |  |
| North Wall 220 kV    | 15.87        | 20.07                    | 17.41       | 9.00          | 21.67       | 20.50       | 13.62                    | 24.82       | 21.83       | 7.83         | 25.58       | 24.38       |  |  |
| Oldcourt A 110 kV    | 4.20         | 8.65                     | 8.13        | 4.67          | 7.23        | 7.11        | 3.60                     | 11.43       | 10.74       | 4.33         | 8.56        | 8.42        |  |  |
| Oldcourt B 110 kV    | 4.24         | 8.70                     | 8.17        | 4.70          | 7.30        | 7.17        | 3.63                     | 11.51       | 10.81       | 4.36         | 8.65        | 8.51        |  |  |
| Oldstreet 220 kV     | 16.06        | 10.99                    | 10.09       | 13.29         | 11.68       | 11.31       | 14.65                    | 12.63       | 11.93       | 12.26        | 13.12       | 12.86       |  |  |
| Oldstreet 400 kV     | 11.02        | 9.11                     | 8.30        | 9.12          | 7.95        | 7.73        | 9.34                     | 11.46       | 10.86       | 8.16         | 9.24        | 9.10        |  |  |
| Oriel 220 kV         | 9.57         | 11.21                    | 10.36       | 9.57          | 11.21       | 10.36       | 9.30                     | 15.95       | 14.70       | 9.30         | 15.95       | 14.70       |  |  |
| Oughtragh 110 kV     | 3.72         | 4.08                     | 3.95        | 4.79          | 2.83        | 2.80        | 3.59                     | 5.30        | 4.97        | 4.82         | 3.16        | 3.12        |  |  |
| Pelletstown 110 kV   | 14.13        | 11.22                    | 10.52       | 7.76          | 11.88       | 11.60       | 13.47                    | 12.99       | 11.84       | 7.49         | 13.39       | 12.95       |  |  |
| Platin 110 kV        | 5.12         | 11.48                    | 10.61       | 5.68          | 8.79        | 8.61        | 4.48                     | 14.43       | 13.44       | 5.35         | 9.94        | 9.78        |  |  |
| Pollahoney 110 kV    | 10.05        | 7.37                     | 7.11        | 10.42         | 8.42        | 8.31        | 9.66                     | 9.67        | 9.16        | 10.29        | 10.35       | 10.15       |  |  |
| Pollaphuca 110 kV    | 2.78         | 2.51                     | 2.47        | 4.02          | 2.28        | 2.28        | 3.27                     | 3.18        | 3.07        | 4.73         | 2.58        | 2.55        |  |  |
| Poolbeg A 110 kV     | 29.69        | 14.20                    | 13.09       | 23.15         | 17.60       | 17.00       | 27.64                    | 16.78       | 14.89       | 21.71        | 20.30       | 19.30       |  |  |
| Poolbeg A 220 kV     | 15.88        | 20.33                    | 17.61       | 7.45          | 20.46       | 19.41       | 13.31                    | 25.01       | 21.99       | 6.49         | 23.93       | 22.88       |  |  |
| Poolbeg B 110 kV     | 29.65        | 14.18                    | 13.07       | 23.13         | 17.58       | 16.98       | 27.60                    | 16.76       | 14.87       | 21.69        | 20.28       | 19.28       |  |  |
| Poolbeg B 220 kV     | 15.64        | 20.97                    | 18.11       | 10.69         | 23.18       | 21.86       | 12.56                    | 25.93       | 22.73       | 9.04         | 27.44       | 26.09       |  |  |
| Poolbeg C 110 kV     | 22.24        | 13.87                    | 12.79       | 7.38          | 16.39       | 15.85       | 20.85                    | 16.40       | 14.53       | 7.05         | 18.73       | 17.84       |  |  |
| Poppintree 110 kV    | 12.72        | 17.29                    | 15.54       | 6.51          | 20.27       | 19.41       | 11.44                    | 20.49       | 18.15       | 6.02         | 23.45       | 22.33       |  |  |
| Portan 260 kV        | 19.28        | 11.78                    | 10.86       | 99.20         | 3.22        | 3.19        | 16.26                    | 14.51       | 13.90       | 95.82        | 3.35        | 3.34        |  |  |

|                      |              | •<br>•      | Sum         | mer          | •           | •           |              |             | Wi          | nter         |             |             |
|----------------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|
|                      | Th           | ree pha     | se          | Si           | ngle Pha    | ase         | Th           | ree pha     | se          | Single Phase |             |             |
| Station              | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] | X/R<br>Ratio | Ik"<br>[kA] | lk'<br>[kA] | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] |
| Portan 400 kV        | 15.09        | 10.12       | 9.15        | 14.35        | 11.12       | 10.69       | 12.12        | 13.07       | 12.34       | 12.08        | 13.80       | 13.52       |
| Portlaoise 110 kV    | 5.81         | 10.81       | 10.25       | 6.69         | 10.72       | 10.53       | 5.58         | 15.08       | 14.16       | 6.70         | 13.33       | 13.08       |
| Pottery 110 kV       | 18.43        | 10.95       | 10.29       | 5.68         | 11.11       | 10.87       | 17.41        | 12.54       | 11.60       | 5.48         | 12.31       | 11.99       |
| Prospect 220 kV      | 9.83         | 10.96       | 10.13       | 8.21         | 12.58       | 12.19       | 9.09         | 16.42       | 15.30       | 7.35         | 17.11       | 16.67       |
| Raffeen 220 kV       | 10.91        | 9.77        | 8.82        | 10.29        | 12.71       | 12.13       | 12.04        | 17.84       | 15.99       | 10.45        | 20.97       | 20.03       |
| Raffeen A 110 kV     | 6.29         | 11.33       | 10.46       | 6.98         | 13.87       | 13.41       | 5.40         | 16.33       | 14.99       | 6.28         | 18.68       | 18.06       |
| Raffeen B 110 kV     | 8.42         | 11.13       | 10.28       | 9.10         | 13.65       | 13.21       | 7.55         | 16.48       | 15.03       | 8.49         | 18.77       | 18.10       |
| Rathkeale 110 kV     | 3.67         | 6.63        | 6.31        | 4.85         | 5.43        | 5.35        | 3.40         | 8.37        | 7.87        | 4.78         | 6.17        | 6.08        |
| Rathmullan 110 kV    | 5.19         | 11.68       | 10.78       | 5.84         | 9.23        | 9.03        | 4.53         | 14.81       | 13.72       | 5.49         | 10.55       | 10.35       |
| Ratrussan 110 kV     | 3.25         | 6.07        | 5.83        | 4.07         | 6.84        | 6.74        | 3.65         | 8.73        | 7.49        | 4.86         | 8.86        | 8.39        |
| Reamore 110 kV       | 3.79         | 6.92        | 6.59        | 4.21         | 6.42        | 6.32        | 3.74         | 11.06       | 9.95        | 4.30         | 8.41        | 8.18        |
| Richmond A 110 kV    | 2.88         | 5.72        | 5.51        | 3.83         | 5.55        | 5.48        | 2.81         | 7.20        | 6.69        | 3.91         | 6.47        | 6.33        |
| Richmond B 110 kV    | 2.88         | 5.72        | 5.51        | 3.83         | 5.55        | 5.48        | 2.81         | 7.20        | 6.69        | 3.91         | 6.47        | 6.33        |
| Rinawade 110 kV      | 5.01         | 10.34       | 9.71        | 5.92         | 7.56        | 7.45        | 4.63         | 12.13       | 11.63       | 5.73         | 8.34        | 8.26        |
| Ringaskiddy 110 kV   | 6.17         | 9.58        | 8.94        | 6.49         | 10.10       | 9.85        | 5.32         | 13.39       | 12.41       | 5.91         | 12.82       | 12.50       |
| Ringsend 110 kV      | 30.23        | 14.30       | 13.16       | 24.53        | 17.73       | 17.11       | 28.11        | 16.97       | 14.98       | 22.96        | 20.51       | 19.46       |
| Rossiple 110 kV      | 6.04         | 6.37        | 6.17        | 6.84         | 5.25        | 5.21        | 6.24         | 9.06        | 8.61        | 7.14         | 6.33        | 6.25        |
| Ryebrook 110 kV      | 5.63         | 13.61       | 12.27       | 6.50         | 12.22       | 11.83       | 4.94         | 15.78       | 14.66       | 6.01         | 13.43       | 13.14       |
| Salthill 110 kV      | 4.56         | 9.82        | 9.23        | 3.90         | 11.98       | 11.67       | 4.69         | 16.02       | 14.24       | 3.70         | 17.57       | 16.79       |
| Screeb 110 kV        | 3.65         | 2.38        | 2.32        | 4.59         | 1.72        | 1.71        | 4.57         | 3.53        | 3.15        | 5.35         | 2.04        | 1.99        |
| Seal Rock A 110 kV   | 8.64         | 9.53        | 8.49        | 10.31        | 10.51       | 10.06       | 7.91         | 12.04       | 11.04       | 9.85         | 12.09       | 11.73       |
| Seal Rock B 110 kV   | 8.67         | 9.54        | 8.50        | 10.33        | 10.52       | 10.06       | 7.93         | 12.05       | 11.05       | 9.86         | 12.09       | 11.73       |
| Shankill 110 kV      | 3.71         | 7.23        | 6.87        | 4.71         | 6.90        | 6.79        | 3.83         | 10.44       | 9.10        | 5.13         | 8.65        | 8.32        |
| Shannonbridge 110 kV | 5.08         | 10.90       | 10.29       | 6.01         | 13.18       | 12.87       | 4.73         | 14.64       | 13.63       | 5.85         | 16.58       | 16.13       |
| Shannonbridge 220 kV | 6.53         | 6.05        | 5.77        | 8.71         | 5.53        | 5.45        | 6.35         | 7.30        | 7.07        | 8.80         | 6.23        | 6.17        |
| Shantallow 110 kV    | 4.60         | 10.17       | 9.60        | 4.91         | 9.09        | 8.94        | 4.06         | 14.51       | 13.55       | 4.63         | 11.18       | 10.98       |
| Shellybanks A 220 kV | 15.59        | 20.32       | 17.59       | 9.48         | 21.97       | 20.76       | 13.01        | 24.97       | 21.96       | 8.16         | 25.80       | 24.59       |
| Shellybanks B 220 kV | 17.25        | 21.22       | 18.23       | 10.96        | 25.25       | 23.65       | 13.99        | 25.20       | 22.13       | 9.26         | 28.99       | 27.47       |
| Shelton Abbey 110 kV | 9.82         | 7.24        | 6.99        | 9.96         | 8.09        | 7.99        | 9.41         | 9.45        | 8.96        | 9.78         | 9.88        | 9.69        |
| Singland 110 kV      | 6.45         | 12.16       | 11.24       | 7.32         | 12.60       | 12.25       | 6.26         | 19.04       | 17.17       | 7.43         | 16.84       | 16.31       |
| Sliabh Bawn 110 kV   | 3.14         | 7.21        | 6.89        | 3.96         | 7.37        | 7.26        | 3.20         | 9.92        | 9.08        | 4.25         | 9.03        | 8.79        |
| Slievecallan 110 kV  | 6.49         | 5.16        | 4.99        | 8.67         | 2.22        | 2.21        | 7.73         | 7.62        | 6.75        | 9.39         | 2.42        | 2.39        |
| Sligo 110 kV         | 3.87         | 7.11        | 6.76        | 4.45         | 7.23        | 7.11        | 3.54         | 11.06       | 10.03       | 4.37         | 9.56        | 9.29        |
| Snugborough 110 kV   | 10.95        | 19.27       | 17.05       | 10.39        | 22.45       | 21.36       | 9.39         | 24.30       | 22.16       | 9.20         | 26.89       | 25.96       |
| Somerset 110 kV      | 3.11         | 6.40        | 6.18        | 4.01         | 4.52        | 4.49        | 2.86         | 7.74        | 7.37        | 3.90         | 4.92        | 4.87        |
| Sorne Hill 110 kV    | 2.74         | 2.33        | 2.27        | 3.40         | 2.69        | 2.66        | 3.44         | 3.90        | 3.46        | 4.38         | 3.74        | 3.60        |
| Srahnakilly 110 kV   | 3.38         | 3.43        | 3.33        | 3.70         | 4.40        | 4.34        | 5.94         | 8.59        | 7.22        | 6.54         | 9.09        | 8.51        |
| Srananagh 110 kV     | 4.72         | 8.07        | 7.64        | 5.39         | 9.30        | 9.11        | 4.50         | 13.09       | 11.80       | 5.49         | 13.15       | 12.68       |
| Srananagh 220 kV     | 6.48         | 3.97        | 3.83        | 8.54         | 3.42        | 3.38        | 7.39         | 5.20        | 4.99        | 9.77         | 3.96        | 3.92        |
| Stevenstown 110 kV   | 3.90         | 6.36        | 6.08        | 4.43         | 4.04        | 4.01        | 3.77         | 7.16        | 6.70        | 4.37         | 4.34        | 4.29        |
| Stratford 110 kV     | 3.20         | 3.88        | 3.80        | 4.20         | 3.08        | 3.06        | 3.35         | 4.79        | 4.55        | 4.41         | 3.41        | 3.37        |
| Taney 110 kV         | 9.02         | 9.46        | 8.95        | 3.25         | 9.31        | 9.14        | 8.62         | 10.73       | 10.01       | 3.15         | 10.23       | 10.00       |

|                      |              | Summer      |             |              |             |             |              |             | Winter      |              |             |             |  |  |  |  |
|----------------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------|-------------|-------------|--|--|--|--|
|                      | Th           | Three phase |             |              | igle Pha    | ise         | Th           | ree pha     | se          | Si           | ngle Ph     | ase         |  |  |  |  |
| Station              | X/R<br>Ratio | lk"<br>[kA] | lk'<br>[kA] |  |  |  |  |
| Tarbert 110 kV       | 19.05        | 10.95       | 10.42       | 22.14        | 11.99       | 11.78       | 21.78        | 13.38       | 12.89       | 24.97        | 13.96       | 13.78       |  |  |  |  |
| Tarbert 220 kV       | 10.49        | 12.14       | 11.12       | 10.86        | 15.79       | 15.18       | 9.92         | 19.42       | 17.84       | 10.28        | 23.69       | 22.85       |  |  |  |  |
| Tawnaghmore A 110 kV | 3.14         | 3.34        | 3.24        | 3.93         | 3.54        | 3.50        | 4.35         | 6.78        | 6.19        | 5.83         | 5.54        | 5.40        |  |  |  |  |
| Tawnaghmore B 110 kV | 3.18         | 3.33        | 3.24        | 3.85         | 3.88        | 3.84        | 4.94         | 7.13        | 6.47        | 6.56         | 6.70        | 6.49        |  |  |  |  |
| Thornsberry 110 kV   | 3.60         | 5.42        | 5.23        | 4.64         | 5.25        | 5.20        | 3.83         | 7.81        | 7.39        | 5.19         | 6.73        | 6.62        |  |  |  |  |
| Thurles 110 kV       | 4.97         | 4.12        | 3.99        | 5.37         | 4.78        | 4.72        | 6.12         | 6.84        | 5.95        | 6.45         | 6.89        | 6.56        |  |  |  |  |
| Tievebrack 110 kV    | 3.36         | 3.35        | 3.24        | 4.50         | 2.68        | 2.66        | 3.73         | 5.52        | 5.09        | 5.23         | 3.31        | 3.26        |  |  |  |  |
| Timahoe 110 kV       | 6.17         | 7.12        | 6.86        | 6.79         | 5.49        | 5.44        | 6.17         | 9.85        | 9.52        | 6.92         | 6.51        | 6.46        |  |  |  |  |
| Tipperary 110 kV     | 4.97         | 6.05        | 5.80        | 6.02         | 4.26        | 4.21        | 5.29         | 8.58        | 7.91        | 6.36         | 4.93        | 4.85        |  |  |  |  |
| Tonroe 110 kV        | 4.72         | 4.38        | 4.24        | 5.80         | 3.24        | 3.22        | 5.34         | 6.08        | 5.65        | 6.41         | 3.75        | 3.69        |  |  |  |  |
| Trabeg 110 kV        | 6.81         | 13.33       | 12.13       | 7.54         | 16.00       | 15.39       | 5.82         | 21.48       | 18.93       | 6.84         | 23.11       | 22.03       |  |  |  |  |
| Tralee 110 kV        | 4.93         | 7.31        | 6.95        | 5.89         | 6.81        | 6.71        | 5.12         | 11.90       | 10.66       | 6.35         | 9.02        | 8.76        |  |  |  |  |
| Trien A 110 kV       | 4.72         | 6.80        | 6.50        | 5.87         | 6.27        | 6.18        | 4.33         | 9.88        | 9.18        | 5.81         | 7.79        | 7.64        |  |  |  |  |
| Trien B 110 kV       | 12.69        | 7.69        | 7.42        | 9.69         | 6.51        | 6.45        | 12.27        | 12.27       | 10.46       | 8.99         | 8.36        | 8.04        |  |  |  |  |
| Trillick 110 kV      | 2.79         | 2.50        | 2.43        | 3.48         | 2.71        | 2.69        | 3.53         | 4.30        | 3.77        | 4.49         | 3.75        | 3.60        |  |  |  |  |
| Trinity 110 kV       | 12.06        | 12.61       | 11.70       | 6.25         | 15.15       | 14.68       | 11.44        | 14.82       | 13.21       | 5.99         | 17.27       | 16.48       |  |  |  |  |
| Tullabeg 110 kV      | 6.35         | 5.85        | 5.69        | 6.56         | 5.20        | 5.15        | 7.18         | 9.22        | 8.89        | 7.06         | 6.68        | 6.63        |  |  |  |  |
| Tullabrack 110 kV    | 6.60         | 6.23        | 6.02        | 7.26         | 5.05        | 5.00        | 6.49         | 8.03        | 7.61        | 7.25         | 5.77        | 5.69        |  |  |  |  |
| Turlough 220 kV      | 11.07        | 11.86       | 10.79       | 12.40        | 10.71       | 10.39       | 9.98         | 13.36       | 12.47       | 11.54        | 11.49       | 11.26       |  |  |  |  |
| Tynagh 220 kV        | 16.49        | 11.66       | 10.53       | 17.71        | 12.96       | 12.45       | 15.03        | 13.31       | 12.39       | 16.32        | 14.17       | 13.80       |  |  |  |  |
| Uggool 110 kV        | 5.44         | 6.17        | 5.93        | 5.13         | 8.07        | 7.93        | 6.33         | 9.09        | 8.52        | 5.60         | 11.26       | 10.95       |  |  |  |  |
| Waterford 110 kV     | 8.04         | 11.11       | 10.52       | 8.41         | 12.43       | 12.17       | 7.28         | 14.87       | 13.75       | 7.79         | 15.34       | 14.92       |  |  |  |  |
| Wexford 110 kV       | 5.69         | 5.91        | 5.72        | 6.94         | 5.71        | 5.65        | 5.72         | 8.79        | 8.15        | 7.37         | 7.27        | 7.11        |  |  |  |  |
| Whitebank 110 kV     | 26.45        | 14.25       | 13.12       | 21.05        | 17.64       | 17.03       | 24.63        | 16.90       | 14.92       | 19.75        | 20.39       | 19.34       |  |  |  |  |
| Whitegate 110 kV     | 4.81         | 8.23        | 7.74        | 5.47         | 8.78        | 8.58        | 4.23         | 10.70       | 10.10       | 5.05         | 10.63       | 10.43       |  |  |  |  |
| Wolfe Tone 110 kV    | 14.84        | 11.66       | 10.90       | 5.44         | 13.25       | 12.90       | 14.11        | 13.57       | 12.30       | 5.23         | 15.02       | 14.46       |  |  |  |  |
| Woodhouse 110 kV     | 5.99         | 5.55        | 5.36        | 7.27         | 4.26        | 4.22        | 6.65         | 7.99        | 7.03        | 7.95         | 5.14        | 4.99        |  |  |  |  |
| Woodland 220 kV      | 13.56        | 21.72       | 18.92       | 12.80        | 22.96       | 21.78       | 10.79        | 27.54       | 24.82       | 10.78        | 27.80       | 26.78       |  |  |  |  |
| Woodland 400 kV      | 16.31        | 10.19       | 9.21        | 15.86        | 11.22       | 10.79       | 13.12        | 13.18       | 12.44       | 13.34        | 13.98       | 13.69       |  |  |  |  |

# E.4. Short Circuit Currents in Northern Ireland

# E.4.1. Methodology used in Northern Ireland

Short circuit current levels are calculated in accordance with the UK Engineering Recommendation G74, which is a computer based analysis, based on the International Standard IEC60909. Compliance with G74 includes:

- Short circuit current contributions from all synchronous and non-synchronous rotating plant including induction motors embedded in the general load;
- Comprehensive plant parameters including time-dependent impedances, transformer winding and earthing configurations;
- Pre-fault voltage levels at each node which should be obtained from a credible, pre-fault load flow study; and
- Pre-fault transformer tap settings should also be obtained from the load flow study.
- The short circuit current level network model includes the following component parameters:
- Transformer impedance variation with tap position;
- Zero sequence mutual coupling effect;
- Unsaturated generator reactance values; and
- Power station auxiliaries fault level contributions.

The calculation of the X/R ratios, used by SONI, is undertaken in accordance with IEC60909o Method C, which is known as the equivalent frequency method. The equivalent frequency method is considered to be the most appropriate general purpose method for calculating the DC component of short circuit currents on the Northern Ireland transmission system.

The Northern Ireland transmission system is designed and operated to maintain short circuit current levels below the ratings of equipment at each substation. Table E-5 below, indicates the range of circuit breaker RMS ratings that are currently installed on the Northern Ireland transmission system, for the respective voltage levels currently operated.

Table E-5 Northern Ireland Station Equipment Rating Range by Voltage Level

| Voltage Level (kV) | Short Circuit Current Levels (kA) |
|--------------------|-----------------------------------|
| 275 <sup>133</sup> | 31.5 – 40                         |
| 275                | 31.5 – 40                         |

# E.4.2. Analysis

The total RMS break current at a busbar is an indication of the short circuit current level that one could expect at that point in the transmission system. However, they do not necessarily represent the short circuit current that could flow through each individual breaker, which may be lower.

<sup>133</sup> The switchgear ratings at Castlereagh, Coolkeeragh, Magherafelt, Tandragee and Kells 275 kV substations have been temporarily reduced to 10 kA by NIE Networks following review of the capability of concrete structures to withstand mechanical loading under fault conditions. This is under constant review and projects will be brought forward to address this issue.

### E.4.3. Northern Ireland Short Circuit Current Level Results

Tables E-6 to E-11 contain the following three-phase and single-phase short circuit current level results for maximum winter peak and minimum summer valley system demand conditions for 2020, 2023 and 2026:

#### • Initial Short Circuit Current (I")

This is the initial RMS value of the AC component of the short circuit current, prior to contact separation time. It is calculated using generator sub-transient reactances.

#### • Peak Make Current (ip)

The largest peak current occurs around 10ms, and is the short circuit current that equipment must be able to withstand, for example, when a circuit breaker is closed directly onto an earthed section of network, thus energising a fault. All equipment in the fault current path will be subjected to the peak make current, and therefore should be rated to withstand this.

#### • RMS Break Current (IB)

This is the RMS value of the AC component of the short circuit current at the time of circuit breaker contact separation. The break time at which contact separation occurs varies from circuit to circuit, and depends on protection settings, fault location, circuit breaker design etc. For the purposes of this report, we have used a short circuit current break time of 50ms for all 275 kV and 110 kV calculations.

In the Northern Ireland results tables, the RMS Break and Peak Make ratings of the existing nodes are shown. It should be noted that the Ballylumford 110 kV node (highlighted in the tables with \*) currently has separate ratings for three-phase and single-phase faults; these are indicated in the tables. All ratings are in kA.

Single phase to earth short circuit currents tend to be larger than three phase short circuit currents in heavily meshed transmission networks. This is due to the multiplicity of zero phase sequence paths available to earth fault currents. In all tables, any nodes where short circuit currents exceed 90% of the corresponding existing rating are highlighted in orange. Any nodes where short circuit currents currents exceed the corresponding existing ratings are highlighted in red.

The results presented in the following section are indicative only. They are based on intact network conditions and are representative of the assumed generation dispatch and transmission system conditions.

|                 | Northe            | rn Irelar | nd Short      | Circuit       | Currents | s for Mir | nimum D | emand         | in 2020       |          |       |       |
|-----------------|-------------------|-----------|---------------|---------------|----------|-----------|---------|---------------|---------------|----------|-------|-------|
|                 | Rat               | ing       |               | Th            | ree Pha  | se        |         |               | Sir           | ngle Pha | ase   |       |
|                 | RMS               | Peak      | X/R           | X/R           | l.       | ip        | IB      | X/R           | X/R           | - P      | ip    | IB    |
| Node            | [kA]              | [kA]      | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]      | [kA]    | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]  | [kA]  |
| 275 kV          |                   |           |               |               |          |           |         |               |               |          |       |       |
| Ballylumford    | 31.5              | 79        | 11.58         | 16.75         | 8.97     | 22.53     | 7.97    | 12.30         | 18.35         | 11.62    | 29.38 | 10.75 |
| Castlereagh     | 10 <sup>134</sup> | 79        | 10.46         | 14.93         | 7.90     | 19.60     | 7.05    | 10.78         | 15.88         | 9.46     | 23.58 | 8.82  |
| Coolkeeragh     | 10 <sup>134</sup> | 79        | 10.27         | 18.11         | 7.74     | 19.17     | 7.04    | 11.57         | 20.57         | 8.86     | 22.26 | 8.42  |
| Hannahstown     | 31.5              | 79        | 10.59         | 15.14         | 8.11     | 20.17     | 7.24    | 10.96         | 16.47         | 9.91     | 24.74 | 9.22  |
| Kells           | 10 <sup>134</sup> | 79        | 12.55         | 18.93         | 10.38    | 26.30     | 9.13    | 11.84         | 18.04         | 12.20    | 30.72 | 11.31 |
| Kilroot         | 31.5              | 79        | 13.99         | 22.60         | 10.71    | 27.44     | 9.37    | 13.84         | 23.27         | 12.48    | 31.92 | 11.57 |
| Magherafelt     | 10 <sup>134</sup> | 79        | 11.78         | 16.41         | 10.66    | 26.84     | 9.42    | 9.52          | 12.19         | 11.10    | 27.24 | 10.39 |
| Moyle           | 31.5              | 79        | 11.52         | 16.60         | 8.87     | 22.28     | 7.89    | 12.20         | 18.08         | 11.46    | 28.94 | 10.61 |
| Tandragee       | 10 <sup>134</sup> | 79        | 10.80         | 14.64         | 10.93    | 27.25     | 9.70    | 10.63         | 15.40         | 12.66    | 31.50 | 11.78 |
| Tamnamore       | 40                | 100       | 11.14         | 15.20         | 10.59    | 26.50     | 9.39    | 11.17         | 16.90         | 11.97    | 29.94 | 11.16 |
| 110 kV          |                   |           |               |               |          |           |         |               |               |          |       |       |
| Aghyoule        | 40                | 100       | 2.95          | 3.14          | 3.10     | 6.02      | 3.01    | 3.99          | 5.03          | 3.33     | 6.97  | 3.27  |
| Antrim          | 40                | 100       | 4.67          | 7.50          | 8.23     | 17.87     | 7.82    | 4.78          | 9.44          | 8.65     | 18.87 | 8.40  |
| Ballylumford    | 21.9              | 55        | 10.24         | 20.51         | 14.80    | 36.65     | 13.56   |               |               |          |       |       |
|                 | 26.2              | 65        |               |               |          |           |         | 10.08         | 24.37         | 16.19    | 40.01 | 15.27 |
| Ballymena       | 40                | 100       | 4.79          | 8.40          | 7.47     | 16.31     | 7.12    | 5.00          | 11.39         | 7.43     | 16.36 | 7.23  |
| Banbridge       | 18.4              | 46.8      | 4.14          | 6.43          | 6.04     | 12.77     | 5.82    | 5.09          | 9.79          | 6.17     | 13.63 | 6.04  |
| Ballyvallagh    | 21.9              | 46.8      | 5.38          | 6.61          | 11.92    | 26.66     | 11.09   | 4.94          | 6.61          | 12.11    | 26.61 | 11.66 |
| Ballynahinch    | 18.4              | 46.8      | 4.25          | 7.04          | 5.02     | 10.68     | 4.81    | 4.97          | 9.95          | 5.24     | 11.53 | 5.11  |
| Belfast Central | n/a               | n/a       | 8.01          | 12.09         | 10.70    | 25.64     | 9.85    | 5.43          | 11.28         | 13.64    | 30.55 | 12.87 |
| Belfast North   | n/a               | n/a       | 5.01          | 7.68          | 10.46    | 23.04     | 9.75    | 3.26          | 11.53         | 11.63    | 23.20 | 11.15 |
| Brockaghboy     | 40                | 100       | 4.68          | 5.63          | 3.52     | 7.66      | 3.44    | 4.14          | 5.61          | 2.97     | 6.28  | 2.93  |
| Carnmoney       | 31.5              | 79        | 4.07          | 6.54          | 7.23     | 15.22     | 6.86    | 4.58          | 8.86          | 7.59     | 16.41 | 7.37  |
| Castlereagh     | 31.5              | 79        | 10.21         | 17.99         | 12.65    | 31.32     | 11.50   | 10.96         | 19.04         | 17.00    | 42.45 | 15.85 |
| Coleraine       | 40                | 100       | 3.77          | 4.46          | 6.61     | 13.67     | 6.27    | 4.36          | 5.73          | 8.02     | 17.16 | 7.74  |
| Coolkeeragh     | 31.5              | 79        | 10.76         | 22.01         | 16.13    | 40.17     | 14.54   | 11.42         | 23.29         | 20.96    | 52.58 | 19.64 |
| Creagh          | 31.5              | 79        | 3.65          | 4.14          | 7.24     | 14.85     | 6.92    | 4.40          | 6.61          | 7.83     | 16.79 | 7.63  |
| Cregagh         | 26.2              | 65        | 8.78          | 14.03         | 11.68    | 28.36     | 10.68   | 7.23          | 13.08         | 15.24    | 35.93 | 14.30 |
| Donegall North  | 31.5              | 79        | 7.93          | 12.57         | 11.67    | 27.93     | 10.81   | 5.69          | 10.45         | 15.19    | 34.34 | 14.37 |
| Donegall South  | n/a               | n/a       | 6.06          | 8.62          | 9.62     | 22.00     | 9.02    | 5.08          | 8.81          | 11.14    | 24.63 | 10.69 |
| Dromore         | 40                | 100       | 3.88          | 4.53          | 7.98     | 16.63     | 7.56    | 4.12          | 5.02          | 8.73     | 18.44 | 8.45  |
| Drumnakelly     | 31.5              | 79        | 7.76          | 11.88         | 15.19    | 36.22     | 13.93   | 7.61          | 12.52         | 17.58    | 41.78 | 16.64 |
| Dungannon       | 40                | 100       | 7.21          | 12.79         | 13.52    | 31.87     | 12.52   | 7.10          | 13.36         | 16.05    | 37.72 | 15.27 |

#### Table E-6 Northern Ireland Short Circuit Currents for Minimum Demand in 2020

<sup>134</sup> The switchgear ratings at Castlereagh, Coolkeeragh, Magherafelt, Tandragee and Kells 275 kV substations have been temporarily reduced to 10 kA by NIE Networks following review of the capability of concrete structures to withstand mechanical loading under fault conditions. This is under constant review and projects will be brought forward to address this issue.

|                     | Northe | rn Irelar | nd Short      | t Circuit     | Currents         | s for Mir | nimum C | emand         | in 2020       |          |       |       |
|---------------------|--------|-----------|---------------|---------------|------------------|-----------|---------|---------------|---------------|----------|-------|-------|
|                     | Rat    | ing       |               | Th            | ree Pha          | se        |         |               | Sir           | ngle Pha | ase   |       |
|                     | RMS    | Peak      | X/R           | X/R           | - P <sup>i</sup> | ip        | IB      | X/R           | X/R           | - P      | ip    | IB    |
| Node                | [kA]   | [kA]      | ratio<br>(AC) | Ratio<br>(DC) | [kA]             | [kA]      | [kA]    | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]  | [kA]  |
| 110 kV              |        |           |               |               |                  |           |         |               |               |          |       |       |
| Eden                | 25     | 62.5      | 4.20          | 6.26          | 7.99             | 16.95     | 7.57    | 4.62          | 8.43          | 8.33     | 18.05 | 8.09  |
| Enniskillen         | 31.5   | 79        | 3.58          | 3.97          | 6.35             | 12.97     | 6.04    | 4.32          | 5.47          | 7.53     | 16.08 | 7.29  |
| Finaghy             | 31.5   | 79        | 8.81          | 14.51         | 12.03            | 29.20     | 11.12   | 6.82          | 11.83         | 16.04    | 37.45 | 15.13 |
| Glengormley         | 18.4   | 46.8      | 3.41          | 3.92          | 5.02             | 10.14     | 4.85    | 4.11          | 6.93          | 5.06     | 10.69 | 4.97  |
| Gort Cluster        | 40     | 100       | 5.99          | 7.21          | 6.69             | 15.26     | 6.42    | 5.80          | 10.93         | 6.67     | 15.12 | 6.52  |
| Hannahstown         | 31.5   | 79        | 9.69          | 17.28         | 12.95            | 31.85     | 11.91   | 10.29         | 18.37         | 17.59    | 43.59 | 16.52 |
| Kells               | 40     | 100       | 9.40          | 19.46         | 14.98            | 36.69     | 13.73   | 10.04         | 20.64         | 19.54    | 48.28 | 18.41 |
| Killymallaght       | 40     | 100       | 6.01          | 7.63          | 9.79             | 22.36     | 9.19    | 5.66          | 9.40          | 9.86     | 22.26 | 9.55  |
| Knock               | n/a    | n/a       | 5.24          | 7.83          | 11.25            | 25.02     | 10.32   | 3.37          | 10.97         | 12.70    | 25.54 | 12.05 |
| Larne               | 18.4   | 46.8      | 4.54          | 5.53          | 7.92             | 17.09     | 7.53    | 5.15          | 8.45          | 7.98     | 17.69 | 7.77  |
| Limavady            | 18.4   | 46.8      | 3.62          | 4.09          | 6.10             | 12.49     | 5.83    | 4.28          | 6.17          | 6.88     | 14.66 | 6.69  |
| Lisburn             | 18.4   | 46.8      | 5.90          | 8.23          | 9.92             | 22.59     | 9.31    | 5.45          | 9.57          | 10.42    | 23.35 | 10.03 |
| Lisaghmore          | 31.5   | 79        | 4.70          | 7.20          | 8.58             | 18.65     | 8.09    | 4.86          | 9.45          | 8.74     | 19.13 | 8.49  |
| Loguestown          | 26.2   | 65        | 3.46          | 4.23          | 4.97             | 10.05     | 4.77    | 4.05          | 5.78          | 5.64     | 11.86 | 5.49  |
| Magherakeel Cluster | 40     | 100       | 4.25          | 4.59          | 3.28             | 6.97      | 3.21    | 5.40          | 6.23          | 3.86     | 8.63  | 3.80  |
| Newtownards         | 40     | 100       | 4.79          | 7.09          | 6.67             | 14.57     | 6.32    | 5.72          | 9.74          | 6.74     | 15.26 | 6.54  |
| Newry               | 18.4   | 46.8      | 3.95          | 6.64          | 5.14             | 10.74     | 4.96    | 4.86          | 9.69          | 5.22     | 11.44 | 5.12  |
| Omagh               | 40     | 100       | 4.66          | 6.03          | 10.54            | 22.87     | 9.85    | 4.98          | 7.81          | 12.08    | 26.60 | 11.58 |
| Rasharkin           | 40     | 100       | 4.02          | 5.37          | 5.87             | 12.33     | 5.65    | 4.53          | 8.17          | 6.13     | 13.22 | 5.98  |
| Rathgael            | 26.2   | 65        | 4.31          | 6.80          | 5.35             | 11.41     | 5.11    | 4.98          | 9.71          | 5.54     | 12.19 | 5.40  |
| Rosebank            | 40     | 100       | 9.44          | 15.56         | 11.96            | 29.31     | 10.92   | 10.48         | 17.34         | 15.81    | 39.26 | 14.80 |
| Slieve Kirk         | 40     | 100       | 4.48          | 5.24          | 7.29             | 15.69     | 6.95    | 5.27          | 9.70          | 6.43     | 14.31 | 6.29  |
| Springtown          | n/a    | n/a       | 4.92          | 7.61          | 8.78             | 19.28     | 8.26    | 5.03          | 9.63          | 9.10     | 20.06 | 8.83  |
| Strabane            | 18.4   | 46.8      | 5.23          | 6.71          | 11.67            | 25.94     | 10.83   | 5.43          | 9.16          | 12.61    | 28.24 | 12.10 |
| Tandragee           | 31.5   | 79        | 9.68          | 17.40         | 16.55            | 40.69     | 15.08   | 10.45         | 19.47         | 20.91    | 51.90 | 19.61 |
| Tremoge             | 40     | 100       | 4.20          | 5.25          | 7.38             | 15.66     | 7.06    | 4.52          | 8.29          | 7.40     | 15.96 | 7.22  |
| Tamnamore           | 40     | 100       | 8.56          | 18.08         | 15.55            | 37.61     | 14.28   | 9.33          | 19.73         | 20.63    | 50.49 | 19.42 |
| Waringstown         | 18.4   | 46.8      | 5.11          | 7.61          | 7.49             | 16.57     | 7.15    | 5.66          | 10.32         | 7.49     | 16.91 | 7.30  |

#### Table E-6 Northern Ireland Short Circuit Currents for Minimum Demand in 2020

|                 | Northe            | rn Irelar | d Short       | Circuit       | Currents         | for Ma | ximum [ | Demand        | in 2020       | )        |       |       |
|-----------------|-------------------|-----------|---------------|---------------|------------------|--------|---------|---------------|---------------|----------|-------|-------|
|                 | Rat               | ing       |               | Th            | ree Pha          | se     |         |               | Sir           | ngle Pha | ase   |       |
| Nodo            | RMS               | Peak      | X/R           | X/R           | - P <sup>i</sup> | ip     | IB      | X/R           | X/R           | - P      | ip    | IB    |
| Node            | [kA]              | [kA]      | ratio<br>(AC) | Ratio<br>(DC) | [kA]             | [kA]   | [kA]    | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]  | [kA]  |
| 275 kV          |                   |           |               |               |                  |        |         |               |               |          |       |       |
| Ballylumford    | 31.5              | 79        | 13.12         | 20.82         | 17.08            | 43.47  | 15.01   | 14.16         | 23.60         | 19.37    | 49.66 | 17.92 |
| Castlereagh     | 10 <sup>135</sup> | 79        | 10.45         | 15.14         | 15.18            | 37.69  | 13.32   | 10.50         | 16.01         | 15.76    | 39.14 | 14.60 |
| Coolkeeragh     | 10 <sup>135</sup> | 79        | 8.65          | 13.65         | 12.04            | 29.16  | 10.95   | 10.31         | 16.96         | 12.26    | 30.39 | 11.67 |
| Hannahstown     | 31.5              | 79        | 10.68         | 15.50         | 14.89            | 37.05  | 13.12   | 10.97         | 17.38         | 15.66    | 39.11 | 14.54 |
| Kells           | 10 <sup>135</sup> | 79        | 12.34         | 18.25         | 17.26            | 43.66  | 15.17   | 11.39         | 17.25         | 17.57    | 44.06 | 16.36 |
| Kilroot         | 31.5              | 79        | 13.63         | 21.10         | 17.03            | 43.50  | 14.97   | 13.62         | 22.63         | 17.46    | 44.59 | 16.31 |
| Magherafelt     | 10 <sup>135</sup> | 79        | 11.34         | 15.75         | 17.29            | 43.32  | 15.26   | 8.81          | 11.04         | 15.28    | 37.10 | 14.38 |
| Moyle           | 31.5              | 79        | 12.95         | 20.25         | 16.74            | 42.56  | 14.74   | 13.91         | 22.73         | 18.91    | 48.40 | 17.52 |
| Tandragee       | 10 <sup>135</sup> | 79        | 10.26         | 14.20         | 18.17            | 45.01  | 15.98   | 9.95          | 14.91         | 18.69    | 46.13 | 17.37 |
| Tamnamore       | 40                | 100       | 10.61         | 14.46         | 16.96            | 42.19  | 15.00   | 10.63         | 16.68         | 16.72    | 41.60 | 15.64 |
| 110 kV          |                   |           |               |               |                  |        |         |               |               |          |       |       |
| Aghyoule        | 40                | 100       | 3.86          | 8.29          | 4.34             | 9.03   | 3.91    | 5.32          | 11.80         | 4.09     | 9.13  | 3.89  |
| Antrim          | 40                | 100       | 4.28          | 7.49          | 10.08            | 21.47  | 9.53    | 4.55          | 9.69          | 9.90     | 21.38 | 9.54  |
| Dellulumeferrel | 21.9              | 55        | 10.26         | 24.43         | 22.51            | 55.76  | 20.51   |               |               |          |       |       |
| Ballylumford    | 26.2              | 65        |               |               |                  |        |         | 11.77         | 28.08         | 26.28    | 66.13 | 22.41 |
| Ballymena       | 40                | 100       | 4.38          | 8.18          | 8.98             | 19.22  | 8.54    | 4.74          | 11.42         | 8.42     | 18.36 | 8.07  |
| Banbridge       | 18.4              | 46.8      | 3.77          | 6.03          | 6.81             | 14.07  | 6.53    | 4.83          | 9.55          | 6.64     | 14.53 | 6.48  |
| Ballyvallagh    | 21.9              | 46.8      | 4.53          | 5.38          | 16.04            | 34.60  | 14.86   | 4.42          | 5.88          | 14.55    | 31.22 | 13.96 |
| Ballynahinch    | 18.4              | 46.8      | 3.91          | 6.67          | 5.79             | 12.07  | 5.49    | 4.78          | 9.83          | 5.76     | 12.56 | 5.57  |
| Belfast Central | n/a               | n/a       | 7.20          | 11.24         | 15.07            | 35.50  | 13.57   | 4.70          | 10.95         | 17.89    | 38.90 | 16.55 |
| Belfast North   | n/a               | n/a       | 4.38          | 6.96          | 13.16            | 28.18  | 12.16   | 2.91          | 11.37         | 13.51    | 26.17 | 12.85 |
| Brockaghboy     | 40                | 100       | 5.36          | 6.87          | 5.04             | 11.27  | 4.43    | 4.20          | 5.92          | 3.31     | 7.03  | 3.19  |
| Carnmoney       | 31.5              | 79        | 3.62          | 6.21          | 8.72             | 17.86  | 8.27    | 4.29          | 8.72          | 8.56     | 18.24 | 8.30  |
| Castlereagh     | 31.5              | 79        | 9.83          | 19.84         | 19.31            | 47.59  | 17.00   | 10.81         | 20.91         | 24.50    | 61.08 | 22.18 |
| Coleraine       | 40                | 100       | 3.93          | 5.39          | 9.64             | 20.14  | 8.49    | 4.70          | 7.19          | 10.49    | 22.81 | 9.72  |
| Coolkeeragh     | 31.5              | 79        | 8.77          | 17.85         | 22.96            | 55.73  | 20.32   | 9.75          | 19.72         | 27.93    | 68.74 | 25.85 |
| Creagh          | 31.5              | 79        | 3.31          | 4.01          | 8.47             | 16.96  | 8.04    | 4.18          | 6.68          | 8.71     | 18.47 | 8.42  |
| Cregagh         | 26.2              | 65        | 8.02          | 13.62         | 17.13            | 41.04  | 15.24   | 6.43          | 12.73         | 20.91    | 48.33 | 19.14 |
| Drumquin        | 40                | 100       | 5.29          | 7.58          | 6.75             | 15.05  | 6.18    | 5.78          | 11.92         | 6.22     | 14.09 | 5.95  |
| Donegall North  | 31.5              | 79        | 7.34          | 12.24         | 15.20            | 35.92  | 13.91   | 5.09          | 9.98          | 18.81    | 41.60 | 17.59 |
| Donegall South  | n/a               | n/a       | 5.48          | 7.95          | 11.87            | 26.64  | 11.05   | 4.65          | 8.41          | 12.95    | 28.10 | 12.34 |
| Dromore         | 40                | 100       | 4.05          | 5.94          | 12.27            | 25.81  | 10.96   | 4.32          | 6.16          | 11.59    | 24.74 | 10.92 |
| Drumnakelly     | 31.5              | 79        | 6.58          | 10.69         | 21.96            | 50.97  | 19.79   | 6.70          | 11.68         | 23.20    | 54.00 | 21.71 |

#### Table E-7 Northern Ireland Short Circuit Currents for Maximum Demand in 2020

<sup>135</sup> The switchgear ratings at Castlereagh, Coolkeeragh, Magherafelt, Tandragee and Kells 275 kV substations have been temporarily reduced to 10 kA by NIE Networks following review of the capability of concrete structures to withstand mechanical loading under fault conditions. This is under constant review and projects will be brought forward to address this issue.

|                     | Northe | rn Irelan | d Short       | Circuit       | Currents | for Ma | ximum I | Demand        | in 2020       |          | •     | •     |
|---------------------|--------|-----------|---------------|---------------|----------|--------|---------|---------------|---------------|----------|-------|-------|
|                     | Rat    | ing       |               | Th            | ree Pha  | se     |         |               | Sir           | igle Pha | ase   |       |
|                     | RMS    | Peak      | X/R           | X/R           | - P      | ip     | IB      | X/R           | X/R           | - P      | ip    | IB    |
| Node                | [kA]   | [kA]      | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]   | [kA]    | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]  | [kA]  |
| 110 kV              |        |           |               |               |          |        |         |               |               |          |       |       |
| Dungannon           | 40     | 100       | 6.18          | 11.04         | 19.28    | 44.25  | 17.61   | 6.43          | 12.46         | 20.94    | 48.41 | 19.74 |
| Eden                | 25     | 62.5      | 3.71          | 5.76          | 9.81     | 20.20  | 9.30    | 4.29          | 8.18          | 9.47     | 20.19 | 9.20  |
| Enniskillen         | 31.5   | 79        | 3.85          | 5.13          | 9.69     | 20.14  | 8.57    | 4.93          | 7.46          | 10.26    | 22.54 | 9.57  |
| Finaghy             | 31.5   | 79        | 8.31          | 14.70         | 15.78    | 38.02  | 14.42   | 6.20          | 11.46         | 20.14    | 46.27 | 18.77 |
| Glengormley         | 18.4   | 46.8      | 3.13          | 3.53          | 5.62     | 11.10  | 5.40    | 3.94          | 6.64          | 5.46     | 11.41 | 5.32  |
| Gort Cluster        | 40     | 100       | 6.29          | 8.18          | 8.70     | 20.02  | 8.20    | 5.87          | 12.39         | 7.86     | 17.87 | 7.57  |
| Hannahstown         | 31.5   | 79        | 9.35          | 18.76         | 17.40    | 42.60  | 15.79   | 10.11         | 20.16         | 22.70    | 56.12 | 21.02 |
| Kells               | 40     | 100       | 8.36          | 18.52         | 21.42    | 51.62  | 19.42   | 9.25          | 20.27         | 26.44    | 64.63 | 24.35 |
| Killymallaght       | 40     | 100       | 5.64          | 7.98          | 13.04    | 29.42  | 12,10   | 5.38          | 9.85          | 11.80    | 26.38 | 11.38 |
| Knock               | n/a    | n/a       | 4.26          | 6.72          | 16.07    | 34.20  | 14.39   | 2.89          | 10.97         | 16.02    | 30.97 | 14.96 |
| Larne               | 18.4   | 46.8      | 4.03          | 4.83          | 9.60     | 20.17  | 9.11    | 4.83          | 8.07          | 9.00     | 19.67 | 8.73  |
| Limavady            | 18.4   | 46.8      | 3.58          | 4.34          | 8.06     | 16.47  | 7.30    | 4.41          | 7.06          | 8.28     | 17.75 | 7.84  |
| Lisburn             | 18.4   | 46.8      | 5.24          | 7.54          | 12.17    | 27.07  | 11.36   | 5.04          | 9.30          | 11.88    | 26.23 | 11.40 |
| Lisaghmore          | 31.5   | 79        | 4.15          | 6.50          | 10.31    | 21.81  | 9.66    | 4.51          | 9.04          | 9.79     | 21.10 | 9.48  |
| Loguestown          | 26.2   | 65        | 3.47          | 4.74          | 6.59     | 13.35  | 5.97    | 4.21          | 6.69          | 6.83     | 14.50 | 6.46  |
| Magherakeel Cluster | 40     | 100       | 5.17          | 9.26          | 4.47     | 9.92   | 4.31    | 6.89          | 12.14         | 4.80     | 11.23 | 4.67  |
| Newtownards         | 40     | 100       | 4.28          | 6.64          | 8.10     | 17.26  | 7.60    | 5.42          | 9.64          | 7.59     | 17.00 | 7.32  |
| Newry               | 18.4   | 46.8      | 3.78          | 7.14          | 5.81     | 12.01  | 5.53    | 4.79          | 10.40         | 5.64     | 12.30 | 5.48  |
| Omagh               | 40     | 100       | 4.72          | 7.08          | 16.88    | 36.73  | 15.01   | 5.13          | 9.45          | 16.74    | 37.07 | 15.64 |
| Rasharkin           | 40     | 100       | 4.30          | 6.43          | 8.32     | 17.74  | 7.43    | 4.72          | 9.70          | 7.31     | 15.92 | 6.93  |
| Rathgael            | 26.2   | 65        | 3.92          | 6.36          | 6.21     | 12.96  | 5.87    | 4.74          | 9.51          | 6.11     | 13.32 | 5.91  |
| Rosebank            | 40     | 100       | 8.86          | 15.90         | 17.72    | 43.08  | 15.75   | 10.25         | 18.23         | 22.06    | 54.63 | 20.15 |
| Slieve Kirk         | 40     | 100       | 4.35          | 6.39          | 9.20     | 19.67  | 8.72    | 5.38          | 11.45         | 7.39     | 16.53 | 7.22  |
| Springtown          | n/a    | n/a       | 4.27          | 6.67          | 10.48    | 22.32  | 9.83    | 4.60          | 8.98          | 10.19    | 22.05 | 9.86  |
| Strabane            | 18.4   | 46.8      | 4.57          | 6.05          | 16.69    | 36.07  | 15.12   | 5.02          | 9.12          | 15.95    | 35.16 | 15.17 |
| Tandragee           | 31.5   | 79        | 8.22          | 16.89         | 23.94    | 57.57  | 21.43   | 9.26          | 19.41         | 28.19    | 68.91 | 26.08 |
| Tremoge             | 40     | 100       | 4.05          | 5.76          | 9.60     | 20.19  | 9.05    | 4.46          | 9.23          | 8.71     | 18.74 | 8.44  |
| Tamnamore           | 40     | 100       | 7.37          | 16.29         | 23.34    | 55.21  | 21.12   | 8.36          | 18.37         | 29.16    | 70.28 | 27.09 |
| Waringstown         | 18.4   | 46.8      | 4.59          | 7.13          | 8.73     | 18.89  | 8.30    | 5.33          | 10.09         | 8.26     | 18.43 | 8.02  |

#### Table E-7 Northern Ireland Short Circuit Currents for Maximum Demand in 2020

|                 | Northe            | rn Irelaı | nd Short      | Circuit       | Currents | s for Mir | nimum C | emand         | in 2023       |          |       |       |
|-----------------|-------------------|-----------|---------------|---------------|----------|-----------|---------|---------------|---------------|----------|-------|-------|
|                 | Rat               | ing       |               | Th            | ree Pha  | se        |         |               | Sir           | ngle Pha | ase   |       |
|                 | RMS               | Peak      | X/R           | X/R           | - P      | ip        | IB      | X/R           | X/R           | - P      | ір    | IB    |
| Node            | [kA]              | [kA]      | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]      | [kA]    | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]  | [kA]  |
| 275 kV          |                   |           |               |               |          |           |         |               |               |          |       |       |
| Ballylumford    | 31.5              | 79        | 11.70         | 19.31         | 8.31     | 20.91     | 7.31    | 12.36         | 20.76         | 10.79    | 27.31 | 9.85  |
| Castlereagh     | 10 <sup>136</sup> | 79        | 10.38         | 16.05         | 7.94     | 19.70     | 6.99    | 10.46         | 16.45         | 9.68     | 24.04 | 8.87  |
| Coolkeeragh     | 10 <sup>136</sup> | 79        | 13.21         | 21.59         | 7.81     | 19.90     | 6.95    | 13.97         | 23.87         | 8.98     | 22.99 | 8.37  |
| Hannahstown     | 31.5              | 79        | 10.55         | 16.39         | 7.84     | 19.49     | 6.91    | 10.76         | 17.39         | 9.61     | 23.95 | 8.82  |
| Kells           | 10 <sup>136</sup> | 79        | 10.97         | 17.11         | 8.20     | 20.47     | 7.22    | 10.75         | 16.81         | 10.04    | 25.02 | 9.22  |
| Kilroot         | 31.5              | 79        | 10.73         | 16.02         | 7.66     | 19.07     | 6.80    | 11.13         | 17.26         | 9.48     | 23.70 | 8.73  |
| Magherafelt     | 10 <sup>136</sup> | 79        | 11.59         | 18.79         | 8.99     | 22.58     | 7.87    | 9.72          | 13.82         | 9.90     | 24.35 | 9.13  |
| Moyle           | 31.5              | 79        | 11.65         | 19.08         | 8.23     | 20.70     | 7.25    | 12.27         | 20.40         | 10.65    | 26.93 | 9.73  |
| Tandragee       | 10 <sup>136</sup> | 79        | 10.46         | 16.16         | 9.48     | 23.53     | 8.28    | 10.12         | 15.93         | 11.43    | 28.26 | 10.43 |
| Tamnamore       | 40                | 100       | 10.83         | 16.86         | 8.99     | 22.41     | 7.88    | 10.89         | 18.34         | 10.52    | 26.25 | 9.66  |
| 110 kV          |                   |           |               |               |          |           |         |               |               |          |       |       |
| Aghyoule        | 40                | 100       | 2.98          | 3.20          | 3.05     | 5.94      | 2.95    | 3.99          | 5.00          | 3.32     | 6.95  | 3.25  |
| Antrim          | 40                | 100       | 4.75          | 7.76          | 7.65     | 16.67     | 7.21    | 4.84          | 9.62          | 8.20     | 17.94 | 7.91  |
| Ballylumford    | 40                | 100       | 10.49         | 22.30         | 13.90    | 34.53     | 12.62   | 11.51         | 24.57         | 17.69    | 44.42 | 16.57 |
| Ballymena       | 40                | 100       | 4.87          | 8.62          | 7.00     | 15.34     | 6.62    | 5.07          | 11.54         | 7.10     | 15.70 | 6.87  |
| Banbridge       | 18.4              | 46.8      | 4.17          | 6.61          | 5.84     | 12.36     | 5.57    | 5.10          | 9.91          | 5.98     | 13.24 | 5.82  |
| Ballyvallagh    | 21.9              | 46.8      | 5.51          | 7.04          | 11.06    | 24.84     | 10.20   | 5.05          | 6.86          | 11.46    | 25.30 | 10.94 |
| Ballynahinch    | 18.4              | 46.8      | 4.30          | 7.15          | 4.97     | 10.59     | 4.73    | 5.00          | 10.08         | 5.19     | 11.44 | 5.04  |
| Belfast Central | n/a               | n/a       | 8.15          | 12.57         | 10.60    | 25.45     | 9.67    | 5.48          | 11.64         | 13.51    | 30.33 | 12.63 |
| Belfast North   | n/a               | n/a       | 5.20          | 8.16          | 9.83     | 21.83     | 9.08    | 3.35          | 11.84         | 10.98    | 22.06 | 10.44 |
| Brockaghboy     | 40                | 100       | 4.59          | 4.95          | 3.08     | 6.66      | 3.00    | 5.01          | 6.59          | 3.20     | 7.06  | 3.15  |
| Carnmoney       | 31.5              | 79        | 4.13          | 6.66          | 7.03     | 14.85     | 6.64    | 4.62          | 8.96          | 7.39     | 16.02 | 7.15  |
| Castlereagh     | 31.5              | 79        | 10.45         | 19.10         | 12.54    | 31.13     | 11.28   | 11.15         | 20.01         | 16.92    | 42.34 | 15.59 |
| Coleraine       | 40                | 100       | 3.81          | 4.27          | 6.17     | 12.80     | 5.81    | 4.33          | 5.47          | 7.54     | 16.11 | 7.23  |
| Coolkeeragh     | 31.5              | 79        | 11.54         | 25.01         | 14.51    | 36.43     | 12.98   | 12.09         | 26.07         | 19.05    | 48.07 | 17.65 |
| Creagh          | 31.5              | 79        | 3.73          | 4.37          | 6.81     | 14.05     | 6.46    | 4.45          | 6.77          | 7.46     | 16.03 | 7.22  |
| Cregagh         | 26.2              | 65        | 8.96          | 14.70         | 11.57    | 28.16     | 10.48   | 7.32          | 13.54         | 15.13    | 35.74 | 14.04 |
| Drumquin        | 40                | 100       | 4.59          | 5.15          | 4.70     | 10.16     | 4.51    | 5.14          | 8.19          | 4.94     | 10.95 | 4.82  |
| Donegall North  | 31.5              | 79        | 8.15          | 13.48         | 10.92    | 26.22     | 10.01   | 5.87          | 11.07         | 14.15    | 32.18 | 13.27 |
| Donegall South  | n/a               | n/a       | 6.24          | 9.13          | 9.08     | 20.87     | 8.44    | 5.21          | 9.14          | 10.54    | 23.41 | 10.04 |
| Dromore         | 40                | 100       | 3.94          | 4.70          | 7.64     | 15.97     | 7.16    | 4.15          | 5.12          | 8.44     | 17.86 | 8.10  |
| Drumnakelly     | 31.5              | 79        | 7.72          | 12.61         | 14.49    | 34.52     | 13.06   | 7.51          | 12.92         | 16.98    | 40.27 | 15.83 |
| Dungannon       | 40                | 100       | 7.01          | 12.89         | 12.79    | 30.01     | 11.67   | 6.95          | 13.40         | 15.27    | 35.78 | 14.35 |

#### Table E-8 Northern Ireland Short Circuit Currents for Minimum Demand in 2023

<sup>136</sup> The switchgear ratings at Castlereagh, Coolkeeragh, Magherafelt, Tandragee and Kells 275 kV substations have been temporarily reduced to 10 kA by NIE Networks following review of the capability of concrete structures to withstand mechanical loading under fault conditions. This is under constant review and projects will be brought forward to address this issue.

|                     | Northe | rn Irelar | nd Short      | t Circuit     | Currents | s for Mir | nimum C | emand         | in 2023       |          | •     | •     |
|---------------------|--------|-----------|---------------|---------------|----------|-----------|---------|---------------|---------------|----------|-------|-------|
|                     | Rat    | ing       |               | Th            | iree Pha | se        |         |               | Si            | ngle Pha | ase   |       |
| Node                | RMS    | Peak      | X/R           | X/R           | - I''    | ip        | IB      | X/R           | X/R           | - P'     | ip    | IB    |
| Node                | [kA]   | [kA]      | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]      | [kA]    | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]  | [kA]  |
| 110 kV              |        |           |               |               |          |           |         |               |               |          |       |       |
| Enniskillen         | 31.5   | 79        | 3.63          | 4.10          | 6.16     | 12.62     | 5.81    | 4.35          | 5.55          | 7.37     | 15.75 | 7.08  |
| Finaghy             | 31.5   | 79        | 9.00          | 15.52         | 11.23    | 27.35     | 10.28   | 7.01          | 12.52         | 14.89    | 34.94 | 13.93 |
| Glengormley         | 18.4   | 46.8      | 3.48          | 4.06          | 4.78     | 9.70      | 4.59    | 4.15          | 7.01          | 4.88     | 10.32 | 4.77  |
| Gort Cluster        | 40     | 100       | 5.96          | 7.37          | 6.43     | 14.65     | 6.11    | 5.83          | 10.99         | 6.49     | 14.73 | 6.31  |
| Hannahstown         | 31.5   | 79        | 9.87          | 18.53         | 12.04    | 29.68     | 10.96   | 10.40         | 19.50         | 16.25    | 40.33 | 15.12 |
| Kells               | 40     | 100       | 8.80          | 18.09         | 13.25    | 32.17     | 12.04   | 9.37          | 19.16         | 17.46    | 42.74 | 16.25 |
| Killymallaght       | 40     | 100       | 6.23          | 8.06          | 9.18     | 21.09     | 8.53    | 5.82          | 9.75          | 9.43     | 21.41 | 9.07  |
| Knock               | n/a    | n/a       | 5.31          | 8.12          | 11.13    | 24.82     | 10.12   | 3.42          | 11.32         | 12.55    | 25.33 | 11.80 |
| Larne               | 18.4   | 46.8      | 4.65          | 5.80          | 7.51     | 16.29     | 7.09    | 5.23          | 8.60          | 7.71     | 17.14 | 7.46  |
| Limavady            | 18.4   | 46.8      | 3.70          | 4.14          | 5.78     | 11.91     | 5.47    | 4.33          | 6.17          | 6.57     | 14.03 | 6.35  |
| Lisburn             | 18.4   | 46.8      | 5.92          | 8.38          | 9.24     | 21.03     | 8.58    | 5.48          | 9.62          | 9.76     | 21.91 | 9.33  |
| Lisaghmore          | 31.5   | 79        | 4.95          | 7.57          | 8.09     | 17.78     | 7.57    | 5.03          | 9.74          | 8.37     | 18.46 | 8.07  |
| Loguestown          | 26.2   | 65        | 3.49          | 4.12          | 4.71     | 9.57      | 4.49    | 4.06          | 5.62          | 5.40     | 11.35 | 5.23  |
| Magherakeel Cluster | 40     | 100       | 4.26          | 4.67          | 3.20     | 6.81      | 3.11    | 5.38          | 6.24          | 3.79     | 8.48  | 3.73  |
| Newtownards         | 40     | 100       | 4.83          | 7.24          | 6.60     | 14.43     | 6.21    | 5.71          | 9.87          | 6.68     | 15.11 | 6.45  |
| Newry               | 18.4   | 46.8      | 4.00          | 6.80          | 5.00     | 10.48     | 4.78    | 4.90          | 9.81          | 5.13     | 11.24 | 4.99  |
| Omagh               | 40     | 100       | 4.70          | 6.24          | 9.92     | 21.56     | 9.16    | 5.00          | 7.92          | 11.52    | 25.38 | 10.93 |
| Rasharkin           | 40     | 100       | 3.89          | 4.39          | 5.37     | 11.20     | 5.13    | 4.38          | 6.22          | 6.01     | 12.87 | 5.84  |
| Rathgael            | 26.2   | 65        | 4.35          | 6.91          | 5.28     | 11.30     | 5.02    | 4.99          | 9.82          | 5.49     | 12.09 | 5.32  |
| Rosebank            | 40     | 100       | 9.65          | 16.40         | 11.85    | 29.13     | 10.72   | 10.43         | 17.50         | 15.75    | 39.10 | 14.58 |
| Slieve Kirk         | 40     | 100       | 4.64          | 5.48          | 6.93     | 15.03     | 6.56    | 5.38          | 9.84          | 6.25     | 13.97 | 6.08  |
| Springtown          | n/a    | n/a       | 5.19          | 8.00          | 8.26     | 18.35     | 7.72    | 5.20          | 9.94          | 8.70     | 19.32 | 8.38  |
| Strabane            | 18.4   | 46.8      | 5.42          | 7.11          | 10.84    | 24.28     | 9.96    | 5.55          | 9.43          | 11.92    | 26.83 | 11.33 |
| Tandragee           | 31.5   | 79        | 9.21          | 17.75         | 15.40    | 37.63     | 13.81   | 9.84          | 19.38         | 19.58    | 48.24 | 18.08 |
| Tremoge             | 40     | 100       | 4.17          | 5.14          | 7.00     | 14.82     | 6.63    | 4.50          | 8.09          | 7.12     | 15.35 | 6.91  |
| Tamnamore           | 40     | 100       | 8.21          | 17.86         | 14.68    | 35.29     | 13.25   | 8.89          | 19.36         | 19.52    | 47.46 | 18.09 |
| Waringstown         | 18.4   | 46.8      | 5.12          | 7.82          | 7.19     | 15.91     | 6.79    | 5.67          | 10.46         | 7.25     | 16.39 | 7.02  |

#### Table E-8 Northern Ireland Short Circuit Currents for Minimum Demand in 2023

|                 | Northe            | r <mark>n Irela</mark> r | d Short       | Circuit       | Currents | for Max | ximum [ | Demand        | in 2023       |          |       |       |
|-----------------|-------------------|--------------------------|---------------|---------------|----------|---------|---------|---------------|---------------|----------|-------|-------|
|                 | Rat               | ing                      |               | Th            | ree Pha  | se      |         |               | Sir           | ngle Pha | ase   |       |
| Nede            | RMS               | Peak                     | X/R           | X/R           | - P      | ір      | IB      | X/R           | X/R           | - I''    | ip    | IB    |
| Node            | [kA]              | [kA]                     | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]    | [kA]    | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]  | [kA]  |
| 275 kV          |                   |                          |               |               |          |         |         |               |               |          |       |       |
| Ballylumford    | 31.5              | 79                       | 13.48         | 19.41         | 20.19    | 51.52   | 18.33   | 14.44         | 22.39         | 21.89    | 56.21 | 20.73 |
| Castlereagh     | 10 <sup>137</sup> | 79                       | 10.68         | 14.37         | 18.03    | 44.88   | 16.33   | 10.59         | 15.45         | 17.72    | 44.06 | 16.79 |
| Coolkeeragh     | 10 <sup>137</sup> | 79                       | 12.87         | 16.90         | 13.51    | 34.31   | 12.61   | 13.98         | 20.91         | 13.21    | 33.82 | 12.77 |
| Hannahstown     | 31.5              | 79                       | 10.85         | 14.58         | 17.46    | 43.54   | 15.87   | 11.04         | 16.69         | 17.46    | 43.62 | 16.56 |
| Kells           | 10 <sup>137</sup> | 79                       | 13.70         | 18.83         | 22.16    | 56.65   | 20.15   | 11.69         | 16.95         | 20.67    | 51.98 | 19.73 |
| Kilroot         | 31.5              | 79                       | 17.42         | 27.16         | 23.92    | 62.41   | 21.65   | 15.14         | 25.21         | 21.73    | 56.06 | 20.80 |
| Magherafelt     | 10 <sup>137</sup> | 79                       | 12.47         | 16.29         | 21.59    | 54.67   | 19.72   | 8.75          | 10.64         | 17.34    | 42.07 | 16.68 |
| Moyle           | 31.5              | 79                       | 13.26         | 18.85         | 19.72    | 50.26   | 17.94   | 14.14         | 21.53         | 21.31    | 54.63 | 20.21 |
| Tandragee       | 10 <sup>137</sup> | 79                       | 11.05         | 14.35         | 23.05    | 57.58   | 20.90   | 9.83          | 14.41         | 21.80    | 53.72 | 20.74 |
| Tamnamore       | 40                | 100                      | 11.63         | 14.97         | 22.25    | 55.92   | 20.30   | 10.71         | 17.66         | 20.00    | 49.81 | 19.13 |
| 110 kV          |                   |                          |               |               |          |         |         |               |               |          |       |       |
| Aghyoule        | 40                | 100                      | 3.85          | 8.28          | 4.38     | 9.10    | 3.96    | 5.31          | 11.80         | 4.11     | 9.18  | 3.92  |
| Agivey          | 40                | 100                      | 5.84          | 9.04          | 5.70     | 12.95   | 4.97    | 6.38          | 12.57         | 5.03     | 11.61 | 4.75  |
| Antrim          | 40                | 100                      | 4.17          | 7.17          | 10.56    | 22.37   | 10.13   | 4.46          | 9.41          | 10.18    | 21.89 | 9.89  |
| Ballylumford    | 40                | 100                      | 10.03         | 23.77         | 24.02    | 59.34   | 22.35   | 11.65         | 27.43         | 27.45    | 69.00 | 26.29 |
| Ballymena       | 40                | 100                      | 4.30          | 8.01          | 9.38     | 20.00   | 9.02    | 4.70          | 11.33         | 8.65     | 18.82 | 8.34  |
| Banbridge       | 18.4              | 46.8                     | 3.73          | 5.95          | 7.00     | 14.43   | 6.78    | 4.82          | 9.50          | 6.78     | 14.82 | 6.65  |
| Ballyvallagh    | 21.9              | 46.8                     | 4.38          | 5.10          | 17.00    | 36.41   | 16.04   | 4.34          | 5.71          | 15.07    | 32.20 | 14.60 |
| Ballynahinch    | 18.4              | 46.8                     | 3.86          | 6.58          | 5.93     | 12.33   | 5.67    | 4.72          | 9.76          | 5.86     | 12.75 | 5.69  |
| Belfast Central | n/a               | n/a                      | 7.08          | 10.92         | 16.04    | 37.70   | 14.65   | 4.59          | 10.74         | 18.91    | 40.91 | 17.72 |
| Belfast North   | n/a               | n/a                      | 4.27          | 6.77          | 13.78    | 29.35   | 12.95   | 2.87          | 11.36         | 13.93    | 26.89 | 13.40 |
| Brockaghboy     | 40                | 100                      | 6.00          | 8.80          | 5.15     | 11.75   | 4.47    | 5.76          | 9.85          | 4.14     | 9.38  | 3.92  |
| Carnmoney       | 31.5              | 79                       | 3.55          | 6.08          | 8.98     | 18.30   | 8.61    | 4.24          | 8.62          | 8.73     | 18.56 | 8.52  |
| Castlereagh     | 31.5              | 79                       | 9.83          | 19.95         | 20.95    | 51.63   | 18.73   | 10.90         | 20.96         | 26.51    | 66.13 | 24.32 |
| Coleraine       | 40                | 100                      | 3.94          | 5.44          | 9.89     | 20.67   | 8.78    | 4.68          | 7.33          | 10.77    | 23.41 | 10.03 |
| Coolkeeragh     | 31.5              | 79                       | 9.51          | 20.72         | 23.85    | 58.51   | 21.47   | 10.50         | 22.60         | 28.80    | 71.53 | 26.97 |
| Creagh          | 31.5              | 79                       | 3.24          | 3.87          | 8.77     | 17.48   | 8.44    | 4.14          | 6.57          | 8.92     | 18.86 | 8.69  |
| Cregagh         | 26.2              | 65                       | 7.92          | 13.32         | 18.39    | 43.99   | 16.61   | 6.31          | 12.39         | 22.32    | 51.42 | 20.70 |
| Drumquin        | 40                | 100                      | 5.53          | 8.54          | 7.18     | 16.14   | 6.64    | 5.86          | 12.49         | 6.35     | 14.44 | 6.12  |
| Donegall North  | 31.5              | 79                       | 7.28          | 11.96         | 16.04    | 37.85   | 14.95   | 4.99          | 9.81          | 19.64    | 43.26 | 18.63 |
| Donegall South  | n/a               | n/a                      | 5.38          | 7.69          | 12.36    | 27.64   | 11.69   | 4.57          | 8.24          | 13.31    | 28.76 | 12.82 |
| Dromore         | 40                | 100                      | 4.10          | 6.32          | 12.81    | 27.02   | 11.60   | 4.32          | 6.27          | 11.84    | 25.27 | 11.24 |
| Drumnakelly     | 31.5              | 79                       | 6.58          | 10.42         | 24.37    | 56.55   | 22.51   | 6.65          | 11.59         | 24.86    | 57.81 | 23.67 |

#### Table E-9 Northern Ireland Short Circuit Currents for Maximum Demand in 2023

<sup>137</sup> The switchgear ratings at Castlereagh, Coolkeeragh, Magherafelt, Tandragee and Kells 275 kV substations have been temporarily reduced to 10 kA by NIE Networks following review of the capability of concrete structures to withstand mechanical loading under fault conditions. This is under constant review and projects will be brought forward to address this issue.

|                     | Northe | rn Irelan | d Short       | Circuit       | Currents | s for Ma | ximum D                               | Demand        | in 2023       | 5        |       |       |
|---------------------|--------|-----------|---------------|---------------|----------|----------|---------------------------------------|---------------|---------------|----------|-------|-------|
|                     | Rat    | ing       |               | Th            | iree Pha | se       | · · · · · · · · · · · · · · · · · · · |               | Sir           | ngle Pha | ase   |       |
|                     | RMS    | Peak      | X/R           | X/R           | - In     | ip       | IB                                    | X/R           | X/R           | - P      | ip    | IB    |
| Node                | [kA]   | [kA]      | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]     | [kA]                                  | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]  | [kA]  |
| 110 kV              |        |           |               |               |          |          |                                       |               |               |          |       |       |
| Dungannon           | 40     | 100       | 6.13          | 10.94         | 20.92    | 47.96    | 19.55                                 | 6.41          | 12.46         | 22.16    | 51.19 | 21.21 |
| Eden                | 25     | 62.5      | 3.63          | 5.62          | 10.11    | 20.71    | 9.70                                  | 4.24          | 8.07          | 9.66     | 20.54 | 9.45  |
| Enniskillen         | 31.5   | 79        | 3.84          | 5.18          | 9.90     | 20.57    | 8.84                                  | 4.92          | 7.49          | 10.39    | 22.80 | 9.74  |
| Finaghy             | 31.5   | 79        | 8.29          | 14.38         | 16.69    | 40.18    | 15.54                                 | 6.08          | 11.13         | 21.09    | 48.26 | 19.94 |
| Glengormley         | 18.4   | 46.8      | 3.08          | 3.43          | 5.78     | 11.37    | 5.60                                  | 3.90          | 6.62          | 5.54     | 11.54 | 5.42  |
| Gort Cluster        | 40     | 100       | 6.36          | 8.45          | 9.02     | 20.81    | 8.57                                  | 5.90          | 12.71         | 8.01     | 18.24 | 7.75  |
| Hannahstown         | 31.5   | 79        | 9.39          | 18.59         | 18.53    | 45.38    | 17.15                                 | 10.14         | 19.92         | 23.91    | 59.15 | 22.49 |
| Kells               | 40     | 100       | 8.59          | 19.15         | 23.90    | 57.84    | 22.16                                 | 9.55          | 20.84         | 28.94    | 71.04 | 27.03 |
| Killymallaght       | 40     | 100       | 5.66          | 7.90          | 13.30    | 30.04    | 12.50                                 | 5.38          | 9.83          | 11.94    | 26.69 | 11.59 |
| Knock               | n/a    | n/a       | 4.09          | 6.37          | 17.19    | 36.24    | 15.63                                 | 2.77          | 10.64         | 16.81    | 32.13 | 15.89 |
| Larne               | 18.4   | 46.8      | 3.95          | 4.68          | 9.94     | 20.77    | 9.54                                  | 4.78          | 7.96          | 9.19     | 20.06 | 8.98  |
| Limavady            | 18.4   | 46.8      | 3.57          | 4.30          | 8.18     | 16.69    | 7.46                                  | 4.40          | 7.07          | 8.37     | 17.95 | 7.97  |
| Lisburn             | 18.4   | 46.8      | 5.14          | 7.27          | 12.69    | 28.11    | 12.04                                 | 4.97          | 9.14          | 12.17    | 26.77 | 11.79 |
| Lisaghmore          | 31.5   | 79        | 4.18          | 6.51          | 10.47    | 22.18    | 9.90                                  | 4.54          | 9.09          | 9.88     | 21.31 | 9.61  |
| Loguestown          | 26.2   | 65        | 3.47          | 4.76          | 6.70     | 13.57    | 6.11                                  | 4.21          | 6.77          | 6.94     | 14.71 | 6.58  |
| Magherakeel Cluster | 40     | 100       | 5.27          | 9.80          | 4.60     | 10.24    | 4.46                                  | 7.04          | 12.85         | 4.97     | 11.67 | 4.83  |
| Newtownards         | 40     | 100       | 4.20          | 6.49          | 8.38     | 17.77    | 7.94                                  | 5.31          | 9.50          | 7.77     | 17.33 | 7.53  |
| Newry               | 18.4   | 46.8      | 3.75          | 7.07          | 5.93     | 12.26    | 5.70                                  | 4.79          | 10.38         | 5.72     | 12.50 | 5.59  |
| Omagh               | 40     | 100       | 4.69          | 7.12          | 17.69    | 38.45    | 16.00                                 | 5.11          | 9.51          | 17.23    | 38.12 | 16.25 |
| Rasharkin           | 40     | 100       | 4.47          | 7.35          | 8.83     | 18.99    | 7.92                                  | 4.86          | 9.57          | 8.26     | 18.10 | 7.82  |
| Rathgael            | 26.2   | 65        | 3.85          | 6.23          | 6.36     | 13.21    | 6.06                                  | 4.66          | 9.41          | 6.18     | 13.41 | 6.01  |
| Rosebank            | 40     | 100       | 8.80          | 15.73         | 19.12    | 46.42    | 17.23                                 | 9.98          | 17.27         | 23.75    | 58.63 | 21.96 |
| Slieve Kirk         | 40     | 100       | 4.34          | 6.32          | 9.32     | 19.91    | 8.91                                  | 5.39          | 11.40         | 7.45     | 16.67 | 7.31  |
| Springtown          | n/a    | n/a       | 4.31          | 6.70          | 10.65    | 22.72    | 10.09                                 | 4.63          | 9.06          | 10.28    | 22.29 | 10.01 |
| Strabane            | 18.4   | 46.8      | 4.53          | 5.92          | 17.22    | 37.14    | 15.86                                 | 4.99          | 9.07          | 16.26    | 35.82 | 15.61 |
| Tandragee           | 31.5   | 79        | 8.50          | 17.50         | 26.94    | 65.08    | 24.74                                 | 9.40          | 19.82         | 30.75    | 75.32 | 28.99 |
| Tremoge             | 40     | 100       | 3.99          | 5.64          | 9.86     | 20.67    | 9.41                                  | 4.43          | 9.17          | 8.84     | 18.98 | 8.62  |
| Tamnamore           | 40     | 100       | 7.45          | 16.93         | 25.97    | 61.51    | 24.11                                 | 8.55          | 19.25         | 31.77    | 76.83 | 30.10 |
| Waringstown         | 18.4   | 46.8      | 4.55          | 7.06          | 9.04     | 19.53    | 8.70                                  | 5.33          | 10.12         | 8.44     | 18.83 | 8.25  |

#### Table E-9 Northern Ireland Short Circuit Currents for Maximum Demand in 2023

|                 | Northe            | rn Irelar | nd Short      | Circuit       | Currents | s for Mir | nimum D | emand         | in 2026       |          |       |       |
|-----------------|-------------------|-----------|---------------|---------------|----------|-----------|---------|---------------|---------------|----------|-------|-------|
|                 | Rat               | ing       |               | Th            | ree Pha  | se        |         |               | Siı           | ngle Pha | ase   |       |
|                 | RMS               | Peak      | X/R           | X/R           | - P      | ip        | IB      | X/R           | X/R           | I.       | ip    | IB    |
| Node            | [kA]              | [kA]      | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]      | [kA]    | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]  | [kA]  |
| 400 kV          |                   |           |               |               |          |           |         |               |               |          |       |       |
| Turleenan       | 50                | 125       | 14.29         | 19.32         | 7.62     | 19.56     | 6.97    | 12.75         | 18.93         | 8.93     | 22.67 | 8.43  |
| 275 kV          |                   |           |               |               |          |           |         |               |               |          |       |       |
| Ballylumford    | 31.5              | 79        | 13.46         | 20.59         | 11.07    | 28.26     | 9.91    | 14.19         | 22.55         | 13.79    | 35.35 | 12.81 |
| Castlereagh     | 10 <sup>138</sup> | 79        | 11.32         | 15.97         | 10.17    | 25.47     | 9.13    | 11.21         | 16.54         | 11.84    | 29.65 | 11.05 |
| Coolkeeragh     | 10 <sup>138</sup> | 79        | 14.00         | 20.20         | 9.37     | 23.99     | 8.53    | 14.72         | 23.09         | 10.29    | 26.47 | 9.75  |
| Hannahstown     | 31.5              | 79        | 11.56         | 16.42         | 10.06    | 25.28     | 9.06    | 11.59         | 17.67         | 11.77    | 29.58 | 11.00 |
| Kells           | 10 <sup>138</sup> | 79        | 12.13         | 17.11         | 10.63    | 26.85     | 9.57    | 11.51         | 16.72         | 12.38    | 31.07 | 11.57 |
| Kilroot         | 31.5              | 79        | 11.71         | 15.75         | 9.70     | 24.41     | 8.81    | 12.03         | 17.38         | 11.48    | 28.96 | 10.78 |
| Magherafelt     | 10 <sup>138</sup> | 79        | 13.05         | 19.01         | 12.00    | 30.54     | 10.72   | 9.87          | 12.87         | 12.16    | 29.98 | 11.42 |
| Moyle           | 31.5              | 79        | 13.34         | 20.22         | 10.93    | 27.86     | 9.80    | 14.00         | 21.96         | 13.55    | 34.70 | 12.61 |
| Tandragee       | 10 <sup>138</sup> | 79        | 11.68         | 16.49         | 12.69    | 31.92     | 11.29   | 10.65         | 16.02         | 14.34    | 35.69 | 13.32 |
| Tamnamore       | 40                | 100       | 12.39         | 17.70         | 12.54    | 31.72     | 11.17   | 11.54         | 19.15         | 13.65    | 34.27 | 12.73 |
| Turleenan       | 40                | 100       | 12.37         | 17.68         | 12.74    | 32.24     | 11.35   | 10.96         | 17.28         | 13.78    | 34.39 | 12.85 |
| 110 kV          |                   |           |               |               |          |           |         |               |               |          |       |       |
| Aghyoule        | 40                | 100       | 2.94          | 3.13          | 3.11     | 6.04      | 3.02    | 4.03          | 5.00          | 3.33     | 6.99  | 3.27  |
| Agivey          | 40                | 100       | 5.46          | 6.70          | 4.16     | 9.33      | 4.07    | 6.14          | 10.14         | 4.42     | 10.13 | 4.35  |
| Antrim          | 40                | 100       | 4.56          | 7.35          | 8.39     | 18.12     | 8.03    | 4.71          | 9.37          | 8.76     | 19.06 | 8.54  |
| Airport Road    | 40                | 100       | 4.81          | 7.11          | 7.42     | 16.21     | 7.08    | 5.24          | 9.84          | 7.59     | 16.88 | 7.38  |
| Ballylumford    | 40                | 100       | 10.74         | 23.15         | 16.16    | 40.24     | 14.98   | 11.92         | 25.84         | 20.10    | 50.65 | 19.13 |
| Ballymena       | 40                | 100       | 4.69          | 8.24          | 7.61     | 16.54     | 7.29    | 4.96          | 11.35         | 7.52     | 16.53 | 7.33  |
| Banbridge       | 18.4              | 46.8      | 3.79          | 5.68          | 5.99     | 12.40     | 5.80    | 3.76          | 4.77          | 4.74     | 9.80  | 4.67  |
| Ballyvallagh    | 21.9              | 46.8      | 5.24          | 6.38          | 12.52    | 27.84     | 11.77   | 4.85          | 6.46          | 12.45    | 27.25 | 12.03 |
| Ballynahinch    | 18.4              | 46.8      | 4.19          | 6.93          | 5.25     | 11.12     | 5.06    | 4.93          | 9.95          | 5.40     | 11.86 | 5.28  |
| Belfast Central | n/a               | n/a       | 8.26          | 12.19         | 11.91    | 28.66     | 11.08   | 5.30          | 11.34         | 14.97    | 33.38 | 14.20 |
| Belfast North   | n/a               | n/a       | 4.97          | 7.64          | 11.09    | 24.40     | 10.45   | 3.21          | 11.75         | 12.07    | 24.00 | 11.63 |
| Brockaghboy     | 40                | 100       | 5.53          | 6.63          | 3.69     | 8.30      | 3.62    | 5.61          | 8.37          | 3.67     | 8.27  | 3.62  |
| Carnmoney       | 31.5              | 79        | 3.98          | 6.44          | 7.60     | 15.92     | 7.28    | 4.54          | 8.87          | 7.85     | 16.94 | 7.65  |
| Castlereagh     | 31.5              | 79        | 11.18         | 19.94         | 14.42    | 36.07     | 13.23   | 11.93         | 20.89         | 19.24    | 48.49 | 18.01 |
| Coleraine       | 40                | 100       | 3.97          | 4.61          | 7.24     | 15.17     | 6.89    | 4.55          | 6.04          | 8.66     | 18.71 | 8.36  |
| Coolkeeragh     | 31.5              | 79        | 11.47         | 24.11         | 16.17    | 40.57     | 14.74   | 12.09         | 25.35         | 20.98    | 52.94 | 19.71 |
| Creagh          | 31.5              | 79        | 3.57          | 4.03          | 7.35     | 15.00     | 7.07    | 4.35          | 6.47          | 7.93     | 16.95 | 7.74  |
| Cregagh         | 26.2              | 65        | 9.23          | 14.53         | 13.15    | 32.15     | 12.15   | 7.26          | 13.26         | 16.97    | 40.03 | 15.99 |
| Drumquin        | 40                | 100       | 4.54          | 5.01          | 4.85     | 10.47     | 4.70    | 5.20          | 8.15          | 5.03     | 11.18 | 4.94  |

#### Table E-10 Northern Ireland Short Circuit Currents for Minimum Demand in 2026

<sup>138</sup> The switchgear ratings at Castlereagh, Coolkeeragh, Magherafelt, Tandragee and Kells 275 kV substations have been temporarily reduced to 10 kA by NIE Networks following review of the capability of concrete structures to withstand mechanical loading under fault conditions. This is under constant review and projects will be brought forward to address this issue.

|                     | Northe | rn Irelar | nd Short      | Circuit       | Currents | s for Mir | nimum D | emand         | in 2026       | ,        |       |       |
|---------------------|--------|-----------|---------------|---------------|----------|-----------|---------|---------------|---------------|----------|-------|-------|
|                     | Rat    | ing       |               | Th            | ree Pha  | se        | •       |               | Sir           | ngle Pha | ase   |       |
| Node                | RMS    | Peak      | X/R           | X/R           | 1"       | ip        | IB      | X/R           | X/R           | - P'     | ip    | IB    |
| Node                | [kA]   | [kA]      | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]      | [kA]    | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]  | [kA]  |
| 110 kV              |        |           |               |               |          |           |         |               |               |          |       |       |
| Donegall North      | 31.5   | 79        | 8.22          | 13.10         | 12.48    | 30.02     | 11.69   | 5.69          | 10.63         | 16.03    | 36.23 | 15.25 |
| Donegall South      | n/a    | n/a       | 6.09          | 8.61          | 10.13    | 23.20     | 9.59    | 5.06          | 8.87          | 11.55    | 25.50 | 11.13 |
| Dromore             | 40     | 100       | 3.83          | 4.47          | 8.10     | 16.81     | 7.69    | 4.15          | 5.17          | 8.53     | 18.04 | 8.26  |
| Drumnakelly         | 31.5   | 79        | 7.80          | 12.14         | 17.20    | 41.02     | 15.84   | 7.52          | 12.63         | 19.29    | 45.76 | 18.28 |
| Dungannon           | 18.4   | 46.8      | 7.10          | 12.84         | 14.85    | 34.90     | 13.81   | 7.02          | 13.52         | 17.19    | 40.35 | 16.38 |
| Eden                | 25     | 62.5      | 4.11          | 6.11          | 8.39     | 17.70     | 8.02    | 4.56          | 8.36          | 8.58     | 18.53 | 8.36  |
| Enniskillen         | 31.5   | 79        | 3.56          | 3.97          | 6.43     | 13.10     | 6.13    | 4.26          | 5.99          | 6.74     | 14.35 | 6.55  |
| Finaghy             | 31.5   | 79        | 9.25          | 15.40         | 12.89    | 31.51     | 12.05   | 6.91          | 12.15         | 16.98    | 39.74 | 16.11 |
| Glengormley         | 18.4   | 46.8      | 3.35          | 3.82          | 5.06     | 10.16     | 4.91    | 4.07          | 6.84          | 5.07     | 10.67 | 4.98  |
| Gort Cluster        | 40     | 100       | 5.92          | 7.10          | 6.80     | 15.49     | 6.55    | 5.81          | 10.91         | 6.73     | 15.27 | 6.59  |
| Hannahstown         | 31.5   | 79        | 10.37         | 19.06         | 13.97    | 34.66     | 13.00   | 10.98         | 20.20         | 18.76    | 46.84 | 17.71 |
| Kells               | 21.9   | 55.9      | 9.01          | 18.38         | 15.63    | 38.08     | 14.50   | 9.63          | 19.60         | 20.29    | 49.86 | 19.18 |
| Killymallaght       | 40     | 100       | 6.05          | 7.59          | 9.78     | 22.36     | 9.24    | 5.69          | 9.45          | 9.85     | 22.28 | 9.56  |
| Knock               | n/a    | n/a       | 5.10          | 7.53          | 12.60    | 27.88     | 11.68   | 3.23          | 11.11         | 13.80    | 27.47 | 13.16 |
| Larne               | 18.4   | 46.8      | 4.45          | 5.38          | 8.14     | 17.50     | 7.81    | 5.08          | 8.37          | 8.10     | 17.90 | 7.91  |
| Limavady            | 18.4   | 46.8      | 3.66          | 4.05          | 6.32     | 12.98     | 6.06    | 4.33          | 6.23          | 7.04     | 15.04 | 6.86  |
| Lisburn             | 18.4   | 46.8      | 5.83          | 8.10          | 10.39    | 23.60     | 9.84    | 5.40          | 9.61          | 10.70    | 23.94 | 10.34 |
| Lisaghmore          | 31.5   | 79        | 4.76          | 7.19          | 8.57     | 18.68     | 8.13    | 4.90          | 9.48          | 8.70     | 19.09 | 8.47  |
| Loguestown          | 26.2   | 65        | 3.56          | 4.32          | 5.31     | 10.82     | 5.10    | 4.16          | 5.99          | 5.93     | 12.54 | 5.78  |
| Magherakeel Cluster | 40     | 100       | 4.22          | 4.55          | 3.27     | 6.95      | 3.21    | 5.34          | 6.10          | 3.88     | 8.67  | 3.83  |
| Newtownards         | 40     | 100       | 4.70          | 6.90          | 7.09     | 15.42     | 6.77    | 5.64          | 9.68          | 7.02     | 15.84 | 6.84  |
| Newry               | 18.4   | 46.8      | 3.89          | 6.58          | 5.26     | 10.96     | 5.10    | 4.88          | 9.68          | 5.30     | 11.62 | 5.20  |
| Omagh               | 40     | 100       | 4.58          | 5.90          | 10.78    | 23.30     | 10.12   | 4.97          | 7.77          | 12.20    | 26.84 | 11.70 |
| Rasharkin           | 40     | 100       | 5.08          | 7.24          | 7.64     | 16.90     | 7.34    | 5.24          | 9.22          | 8.26     | 18.37 | 8.03  |
| Rathgael            | 26.2   | 65        | 4.24          | 6.66          | 5.60     | 11.90     | 5.39    | 4.92          | 9.68          | 5.72     | 12.55 | 5.59  |
| Rosebank            | 40     | 100       | 10.11         | 16.55         | 13.52    | 33.42     | 12.47   | 10.94         | 17.78         | 17.74    | 44.29 | 16.68 |
| Slieve Kirk         | 40     | 100       | 4.50          | 5.20          | 7.27     | 15.65     | 6.96    | 5.30          | 9.60          | 6.43     | 14.34 | 6.31  |
| Springtown          | n/a    | n/a       | 4.99          | 7.61          | 8.77     | 19.31     | 8.31    | 5.07          | 9.67          | 9.06     | 20.02 | 8.80  |
| Strabane            | 18.4   | 46.8      | 5.22          | 6.63          | 11.68    | 25.96     | 10.91   | 5.44          | 9.11          | 12.63    | 28.30 | 12.13 |
| Tandragee           | 31.5   | 79        | 9.71          | 18.49         | 18.51    | 45.53     | 16.96   | 10.37         | 20.36         | 22.64    | 56.15 | 21.28 |
| Tremoge             | 40     | 100       | 4.12          | 5.14          | 7.56     | 15.97     | 7.26    | 4.49          | 8.25          | 7.50     | 16.15 | 7.33  |
| Tamnamore           | 40     | 100       | 8.60          | 19.06         | 17.47    | 42.28     | 16.10   | 9.41          | 20.93         | 22.78    | 55.82 | 21.45 |
| Waringstown         | 18.4   | 46.8      | 5.00          | 7.58          | 7.79     | 17.17     | 7.48    | 5.60          | 10.39         | 7.66     | 17.26 | 7.48  |

#### Table E-10 Northern Ireland Short Circuit Currents for Minimum Demand in 2026

|                 | Northe            | rn Irelar | d Short       | Circuit       | Currents | for Ma | kimum [ | Demand        | in 2026       | 5        |       |       |
|-----------------|-------------------|-----------|---------------|---------------|----------|--------|---------|---------------|---------------|----------|-------|-------|
|                 | Rat               | ing       |               | Th            | ree Pha  | se     |         |               | Siı           | ngle Pha | ase   |       |
|                 | RMS               | Peak      | X/R           | X/R           | - In     | ip     | IB      | X/R           | X/R           | - In-    | ip    | IB    |
| Node            | [kA]              | [kA]      | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]   | [kA]    | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]  | [kA]  |
| 400 kV          |                   |           |               |               |          |        |         |               |               |          |       |       |
| Turleenan       | 50                | 125       | 15.21         | 19.34         | 10.69    | 27.57  | 10.07   | 12.72         | 18.56         | 11.59    | 29.40 | 11.20 |
| 275 kV          |                   |           |               |               |          |        |         |               |               |          |       |       |
| Ballylumford    | 31.5              | 79        | 13.46         | 20.59         | 19.19    | 48.94  | 17.34   | 14.24         | 22.61         | 21.12    | 54.18 | 19.91 |
| Castlereagh     | 10 <sup>139</sup> | 79        | 11.32         | 15.97         | 17.15    | 42.65  | 15.46   | 10.53         | 15.58         | 17.27    | 42.91 | 16.27 |
| Coolkeeragh     | 10 <sup>139</sup> | 79        | 14.00         | 20.20         | 13.23    | 33.61  | 12.30   | 13.95         | 21.10         | 13.04    | 33.39 | 12.57 |
| Hannahstown     | 31.5              | 79        | 11.56         | 16.42         | 16.68    | 41.55  | 15.08   | 10.94         | 16.76         | 16.97    | 42.36 | 16.02 |
| Kells           | 10 <sup>139</sup> | 79        | 12.13         | 17.11         | 20.16    | 51.33  | 18.30   | 11.48         | 16.77         | 19.52    | 49.00 | 18.55 |
| Kilroot         | 31.5              | 79        | 11.71         | 15.75         | 20.18    | 52.02  | 18.40   | 13.93         | 22.26         | 19.60    | 50.17 | 18.71 |
| Magherafelt     | 10 <sup>139</sup> | 79        | 13.05         | 19.01         | 20.52    | 51.92  | 18.65   | 8.79          | 10.85         | 16.89    | 41.01 | 16.18 |
| Moyle           | 31.5              | 79        | 13.34         | 20.22         | 18.78    | 47.80  | 16.99   | 13.96         | 21.76         | 20.58    | 52.70 | 19.42 |
| Tandragee       | 10 <sup>139</sup> | 79        | 11.68         | 16.49         | 22.01    | 54.97  | 19.86   | 9.76          | 14.57         | 21.08    | 51.89 | 19.96 |
| Tamnamore       | 40                | 100       | 12.39         | 17.70         | 21.29    | 53.49  | 19.32   | 10.70         | 17.84         | 19.48    | 48.49 | 18.55 |
| Turleenan       | 40                | 100       | 12.37         | 17.68         | 21.63    | 54.33  | 19.63   | 10.00         | 15.64         | 19.61    | 48.42 | 18.68 |
| 110 kV          |                   |           |               |               |          |        |         |               |               |          |       |       |
| Aghyoule        | 40                | 100       | 2.94          | 3.13          | 4.38     | 9.10   | 3.96    | 5.42          | 12.02         | 4.06     | 9.09  | 3.87  |
| Agivey          | 40                | 100       | 5.46          | 6.70          | 6.32     | 14.59  | 5.60    | 6.75          | 13.36         | 5.46     | 12.74 | 5.19  |
| Antrim          | 40                | 100       | 4.56          | 7.35          | 10.66    | 22.55  | 10.18   | 4.44          | 9.37          | 10.26    | 22.03 | 9.94  |
| Airport Road    | 40                | 100       | 4.81          | 7.11          | 8.76     | 18.64  | 8.27    | 4.86          | 9.48          | 8.44     | 18.50 | 8.16  |
| Ballylumford    | 40                | 100       | 10.74         | 23.15         | 23.71    | 58.54  | 21.96   | 11.56         | 27.47         | 27.19    | 68.29 | 25.95 |
| Ballymena       | 40                | 100       | 4.69          | 8.24          | 9.46     | 20.16  | 9.07    | 4.69          | 11.29         | 8.71     | 18.94 | 8.39  |
| Banbridge       | 18.4              | 46.8      | 3.79          | 5.68          | 6.71     | 13.62  | 6.50    | 3.62          | 4.60          | 5.03     | 10.30 | 4.96  |
| Ballyvallagh    | 21.9              | 46.8      | 5.24          | 6.38          | 16.97    | 36.33  | 15.94   | 4.33          | 5.73          | 15.07    | 32.19 | 14.56 |
| Ballynahinch    | 18.4              | 46.8      | 4.19          | 6.93          | 5.93     | 12.33  | 5.65    | 4.72          | 9.77          | 5.86     | 12.76 | 5.69  |
| Belfast Central | n/a               | n/a       | 8.26          | 12.19         | 15.92    | 37.37  | 14.46   | 4.56          | 10.73         | 18.82    | 40.66 | 17.55 |
| Belfast North   | n/a               | n/a       | 4.97          | 7.64          | 13.67    | 29.14  | 12.81   | 2.86          | 11.29         | 13.85    | 26.71 | 13.30 |
| Brockaghboy     | 40                | 100       | 5.53          | 6.63          | 5.61     | 12.98  | 4.94    | 5.94          | 10.01         | 4.42     | 10.08 | 4.22  |
| Carnmoney       | 31.5              | 79        | 3.98          | 6.44          | 8.95     | 18.25  | 8.56    | 4.25          | 8.64          | 8.72     | 18.54 | 8.50  |
| Castlereagh     | 31.5              | 79        | 11.18         | 19.94         | 20.72    | 50.94  | 18.40   | 10.69         | 20.74         | 26.32    | 65.52 | 24.01 |
| Coleraine       | 40                | 100       | 3.97          | 4.61          | 10.54    | 22.05  | 9.45    | 4.73          | 7.19          | 11.35    | 24.71 | 10.63 |
| Coolkeeragh     | 31.5              | 79        | 11.47         | 24.11         | 23.85    | 58.42  | 21.47   | 10.36         | 22.55         | 28.83    | 71.48 | 26.97 |
| Creagh          | 31.5              | 79        | 3.57          | 4.03          | 8.80     | 17.53  | 8.44    | 4.14          | 6.58          | 8.96     | 18.93 | 8.70  |
| Cregagh         | 26.2              | 65        | 9.23          | 14.53         | 18.22    | 43.51  | 16.36   | 6.24          | 12.35         | 22.19    | 51.02 | 20.47 |
| Drumquin        | 40                | 100       | 4.54          | 5.01          | 7.18     | 16.15  | 6.64    | 5.98          | 12.65         | 6.28     | 14.34 | 6.05  |

#### Table E-11 Northern Ireland Short Circuit Currents for Maximum Demand in 2026

<sup>139</sup> The switchgear ratings at Castlereagh, Coolkeeragh, Magherafelt, Tandragee and Kells 275 kV substations have been temporarily reduced to 10 kA by NIE Networks following review of the capability of concrete structures to withstand mechanical loading under fault conditions. This is under constant review and projects will be brought forward to address this issue.

|                     | Northe | rn Irelan | d Short       | Circuit       | Currents | for Ma | ximum C | Demand        | in 2026       | ;        |       |       |
|---------------------|--------|-----------|---------------|---------------|----------|--------|---------|---------------|---------------|----------|-------|-------|
|                     | Rat    | ing       |               | Th            | iree Pha | se     | •       |               | Sir           | ngle Pha | ase   |       |
| Node                | RMS    | Peak      | X/R           | X/R           | - I''    | ip     | IB      | X/R           | X/R           | - P      | ip    | IB    |
| Node                | [kA]   | [kA]      | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]   | [kA]    | ratio<br>(AC) | Ratio<br>(DC) | [kA]     | [kA]  | [kA]  |
| 110 kV              |        |           |               |               |          |        |         |               |               |          |       |       |
| Donegall North      | 31.5   | 79        | 8.22          | 13.10         | 15.87    | 37.46  | 14.75   | 4.99          | 9.80          | 19.47    | 42.89 | 18.41 |
| Donegall South      | n/a    | n/a       | 6.09          | 8.61          | 12.27    | 27.46  | 11.58   | 4.57          | 8.22          | 13.24    | 28.62 | 12.73 |
| Dromore             | 40     | 100       | 3.83          | 4.47          | 12.81    | 27.03  | 11.58   | 4.42          | 6.60          | 11.28    | 24.20 | 10.72 |
| Drumnakelly         | 31.5   | 79        | 7.80          | 12.14         | 24.01    | 55.74  | 22.09   | 6.64          | 11.59         | 24.42    | 56.77 | 23.18 |
| Dungannon           | 40     | 100       | 7.10          | 12.84         | 20.77    | 47.63  | 19.34   | 6.42          | 12.49         | 22.07    | 51.00 | 21.06 |
| Eden                | 25     | 62.5      | 4.11          | 6.11          | 10.06    | 20.63  | 9.63    | 4.24          | 8.10          | 9.64     | 20.50 | 9.41  |
| Enniskillen         | 31.5   | 79        | 3.56          | 3.97          | 9.92     | 20.61  | 8.85    | 4.72          | 7.97          | 8.71     | 18.96 | 8.24  |
| Finaghy             | 31.5   | 79        | 9.25          | 15.40         | 16.51    | 39.73  | 15.32   | 6.10          | 11.18         | 20.89    | 47.83 | 19.70 |
| Glengormley         | 18.4   | 46.8      | 3.35          | 3.82          | 5.83     | 11.45  | 5.63    | 3.89          | 6.61          | 5.57     | 11.61 | 5.44  |
| Gort Cluster        | 40     | 100       | 5.92          | 7.10          | 9.02     | 20.81  | 8.56    | 5.92          | 12.72         | 8.02     | 18.26 | 7.75  |
| Hannahstown         | 31.5   | 80        | 10.37         | 19.06         | 18.29    | 44.77  | 16.88   | 10.09         | 19.90         | 23.64    | 58.45 | 22.17 |
| Kells               | 40     | 100       | 9.01          | 18.38         | 24.28    | 58.66  | 22.31   | 9.37          | 20.19         | 29.39    | 71.96 | 27.28 |
| Killymallaght       | 40     | 100       | 6.05          | 7.59          | 13.31    | 30.04  | 12.50   | 5.37          | 9.84          | 11.95    | 26.71 | 11.59 |
| Knock               | n/a    | n/a       | 5.10          | 7.53          | 17.03    | 35.92  | 15.40   | 2.77          | 10.65         | 16.73    | 31.97 | 15.75 |
| Larne               | 18.4   | 46.8      | 4.45          | 5.38          | 9.94     | 20.78  | 9.51    | 4.77          | 7.97          | 9.20     | 20.08 | 8.98  |
| Limavady            | 18.4   | 46.8      | 3.66          | 4.05          | 8.35     | 17.02  | 7.66    | 4.40          | 7.00          | 8.51     | 18.23 | 8.12  |
| Lisburn             | 18.4   | 46.8      | 5.83          | 8.10          | 12.61    | 27.95  | 11.93   | 4.96          | 9.08          | 12.11    | 26.64 | 11.71 |
| Lisaghmore          | 31.5   | 79        | 4.76          | 7.19          | 10.48    | 22.20  | 9.91    | 4.53          | 9.10          | 9.89     | 21.34 | 9.62  |
| Loguestown          | 26.2   | 65        | 3.56          | 4.32          | 6.98     | 14.14  | 6.43    | 4.22          | 6.68          | 7.16     | 15.20 | 6.83  |
| Magherakeel Cluster | 40     | 100       | 4.22          | 4.55          | 4.58     | 10.18  | 4.44    | 7.03          | 12.74         | 4.92     | 11.55 | 4.79  |
| Newtownards         | 40     | 100       | 4.70          | 6.90          | 8.36     | 17.74  | 7.89    | 5.31          | 9.52          | 7.77     | 17.33 | 7.52  |
| Newry               | 18.4   | 46.8      | 3.89          | 6.58          | 5.96     | 12.33  | 5.72    | 4.85          | 10.40         | 5.76     | 12.61 | 5.62  |
| Omagh               | 40     | 100       | 4.58          | 5.90          | 17.65    | 38.38  | 15.94   | 5.20          | 9.65          | 17.02    | 37.79 | 16.04 |
| Rasharkin           | 40     | 100       | 5.08          | 7.24          | 11.19    | 24.85  | 10.17   | 5.22          | 10.06         | 10.27    | 22.84 | 9.78  |
| Rathgael            | 26.2   | 65        | 4.24          | 6.66          | 6.35     | 13.20  | 6.04    | 4.66          | 9.43          | 6.18     | 13.42 | 6.00  |
| Rosebank            | 40     | 100       | 10.11         | 16.55         | 18.93    | 45.89  | 16.96   | 9.86          | 17.23         | 23.61    | 58.20 | 21.71 |
| Slieve Kirk         | 40     | 100       | 4.50          | 5.20          | 9.32     | 19.92  | 8.91    | 5.39          | 11.42         | 7.46     | 16.69 | 7.32  |
| Springtown          | n/a    | n/a       | 4.99          | 7.61          | 10.66    | 22.74  | 10.10   | 4.62          | 9.06          | 10.30    | 22.31 | 10.02 |
| Strabane            | 40     | 100       | 5.22          | 6.63          | 17.22    | 37.13  | 15.84   | 5.00          | 9.08          | 16.26    | 35.82 | 15.59 |
| Tandragee           | 31.5   | 79        | 9.71          | 18.49         | 26.44    | 63.86  | 24.17   | 9.36          | 19.78         | 29.84    | 73.06 | 28.06 |
| Tremoge             | 40     | 100       | 4.12          | 5.14          | 9.84     | 20.62  | 9.38    | 4.41          | 9.10          | 8.80     | 18.88 | 8.57  |
| Tamnamore           | 40     | 100       | 8.60          | 19.06         | 25.68    | 60.83  | 23.74   | 8.52          | 19.22         | 31.50    | 76.15 | 29.73 |
| Waringstown         | 18.4   | 46.8      | 5.00          | 7.58          | 9.03     | 19.50  | 8.67    | 5.30          | 10.04         | 8.41     | 18.75 | 8.21  |

#### Table E-11 Northern Ireland Short Circuit Currents for Maximum Demand in 2026

## Appendix F Approaches to Consultation for Developing the Grid

### F.1. EirGrid Approach to Consultation

In December 2016 EirGrid launched Have Your Say<sup>140</sup>, which outlines our approach to consultation. It followed a review of our consultation activities, after which, we made a commitment to improve the way we engage with the public and stakeholders.

Have Your Say outlines the way we develop our projects and how the public can engage with us at each stage of project development.

### F.2. SONI Approach to Consultation

SONI has reviewed its approach to engaging and consulting with the public and stakeholders, this included independent analysis by The Consultation Institute (TCI) which made a number of recommendations. Following engagement with a range of stakeholders and in line with TCI's recommendations, SONI has developed a new Grid Development Process<sup>141</sup>.

This three part process puts stakeholders and the community at the heart of what we do. To find out more visit www.soni.ltd.uk and if you have any queries you can contact us at info@soni.ltd.uk.

140 http://www.eirgridgroup.com/the-grid/have-your-say/ 141 http://www.soni.ltd.uk/media/SONIs-Powering-The-Future-Grid-Development-Process-brochure.pdf

# Appendix G References

The following documents are referenced in this All-Island Ten Year Transmission Forecast Statement:

- All-Island Generation Capacity Statement 2020-2029. EirGrid and SONI issued this report in August 2020. Its main purpose is to inform market participants, regulatory agencies and policy makers of the likely minimum generation capacity required to achieve an adequate supply and demand balance for electricity for the period 2020 to 2029. Available on: http://www.eirgridgroup.com/site-files/library/EirGrid/All-Island-Generation-Capacity-Statement-2020-2029.pdf.
- Transmission Development Plan Ireland 2019-2028, CRU approved version published in July 2020. The main purpose of this document is to document the plan for the development of the Irish transmission system and interconnection for the following 10 year period. Available on: https://www.eirgridgroup.com/site-files/library/EirGrid/TDP-2019-2028-Final-For-Publication. pdf.
- Transmission Development Plan Northern Ireland 2019-2028, UR approved version published in May 2020. The main purpose of this document is to document the plan for the development of the Northern Ireland transmission system and interconnection for the following 10 year period. Available on: https://www.soni.ltd.uk/media/documents/SONI-TDPNI-2019-2028.pdf.
- Transmission Development Plan Northern Ireland 2020-2029, UR approved version published in March 2021. The main purpose of this document is to document the plan for the development of the Northern Ireland transmission system and interconnection for the following 10 year period. Available on https://www.soni.ltd.uk/media/documents/SONI-Transmission-Development-Plan-Northern-Ireland-2020-2029.pdf.
- EirGrid Grid Code Version 9.0, December 2020. The EirGrid Grid Code covers technical aspects relating to the operation and use of the transmission system, and to plant and apparatus connected to the transmission system or to the distribution system. Available on: http://www.eirgridgroup.com/site-files/library/EirGrid/GridCodeVersion9.pdf.
- SONI Grid Code, October 2020. The SONI Grid Code is designed to permit the development, maintenance and operation of an efficient, co-ordinated and economical Transmission System in Northern Ireland. The grid code is prepared by SONI pursuant to condition 16 of SONI's Licence. Available on: https://www.soni.ltd.uk/media/documents/SONI-Grid-Code-8th-October-2020.pdf.
- Transmission System Security and Planning Standards Ireland, May 2016. This document sets out the technical standards by which the adequacy of the grid in Ireland is determined. Available on: http://www.eirgridgroup.com/site-files/library/EirGrid/EirGrid-Transmission-System-Security-and-Planning-Standards-TSSPS-Final-May-2016-APPROVED.pdf.
- Transmission System Security and Planning Standards Northern Ireland, September 2015. This document sets out the technical standards by which the adequacy of the grid in Northern Ireland is determined. Available on: https://www.soni.ltd.uk/media/Northern-Ireland-TSSPS-September-2015.pdf.

- Electricity Regulation Act, 1999. This act provides the regulatory framework for the introduction of competition in the generation and supply of electricity in Ireland. The Act provided for the establishment of the Commission for Regulation of Utilities (CRU) (previously called the Commission for Energy Regulation) and gave it the necessary powers to licence and regulate the generation, distribution, transmission and supply of electricity. Available on: www.cru.ie.
- EirGrid's TSO Licence. On June 29 2006, the CER issued a Transmission System Operator (TSO) Licence to EirGrid plc. pursuant to Section 14(1)(e) of the Electricity Regulation Act, 1999, as inserted by Regulation 32 of S.I. No. 445 of 2000 – European Communities (Internal Market in Electricity) Regulations 2001. The most recent update was issued in Mach 2017. Available on: www.cru.ie.
- SONI's Licence to Participate in the Transmission of Electricity, updated to February 2019. Available on: www.uregni.gov.uk. Condition 33 requires SONI to prepare a statement (in a form; in consultation with EirGrid; and based on methodologies approved by UREGNI) showing in respect of each of the ten succeeding financial years; circuit capacity; forecast electrical flows and loading on each part of the transmission system; and fault levels for each transmission node.
- Ireland's Climate Action Plan, June 2019, published by the Department of Communications, Climate Action and Environment. Available on: www.dccae.gov.ie.

# Appendix H Power Flows

This appendix presents sample power flows for summer valley and winter peak for the years 2020 and 2029 based on a particular set of assumptions. Table H-1 shows the MW and MVAR flows on all lines in the transmission system and the percentage loading of the lines relative to their seasonal rating. The flows shown are based on the following assumptions:

- Wind generation operating at 30% of capacity at the winter peak, and 0% at the summer valley;
- Solar power operating at o% at both the winter peak and summer valley (as both occur at night); and
- Power stations dispatched according to system constraints and merit order.

Indeed the transmission system needs to be capable of accommodating a diverse range of power flows as they can vary greatly throughout the day and year. Power flows depend on system conditions, such as the level of demand, generation and interconnection, and the availability of plant which can be out of service unexpectedly or due to planned maintenance.

Data fields without data (but with a hyphen) denote lines which do not exist in the associated case, due to either being decommissioned or not yet constructed.

| Image: consistant con |      |     |     |     |        |             | 20   | 2020   |                    |      |        |             | 20   | 2029   |                    |      |
|---|------|-----|-----|-----|--------|-------------|------|--------|--------------------|------|--------|-------------|------|--------|--------------------|------|
| To         No.  |      |     | ЭГ  |     | SI     | ummer Valle | ey ( |        | <b>Ninter Peak</b> |      | Sı     | Immer Valle | ey   |        | <b>Winter Peak</b> |      |
| CWB         400         1         ····         ···         ···         ····         ····         ····         ····         ·····         ·····         ·····         ·····         ······         ·······         ·······         ···········         ····································  | From | To  | kv  | No. | MW     | MVAR        | %    | MM     | MVAR               | %    | MM     | MVAR        | %    | MM     | MVAR               | %    |
| MP         400         1         ···  | DSN  | CNB | 400 | 1   |        | -           | -    |        |                    |      | -186.7 | -67.2       | 12.6 | -202.5 | -9.2               | 10.4 |
| MP         400         1         ····         ····         ····         ····         ····         ····         ····         ····         ·····         ·····         ·····         ·····         ······         ·····         ······  | KPG  | МР  | 400 | 1   |        |             |      |        |                    |      | 138.5  | 4.7         | 11.5 | 215.6  | -14.4              | 17.9 |
| 05T         q00         1         559         81.2         51.4         52.4<   | CNB  | МР  | 400 | 1   |        |             | •    |        |                    |      | -194.9 | -122.6      | 14.6 | -291.6 | -79.4              | 15.5 |
| W 00         400         1         62.6         34.4         7.2         91.0         91.7         13.6         23.4         91.4         91.1           PKT         400         11         100.0         96.6         20.3         100.0         31.4         15.3         100.0         157.4         28.5         499.8         97.5           TN         700         11         10.0         96.6         20.3         100.0         15.4         12.6         13.6  | MP   | 0ST | 400 | 1   | -55.9  | 58.2        | 8.1  | 5.4    | 30.8               | 3.1  | 9.5    | 52.0        | 5.3  | 58.7   | 69.0               | 9.1  |
| PFT         400         11         -100.0         96.6         20.3         100.0         31.4         15.3         160.4         369.8         37.5           TNR         400         1         ····     ···         ·   | OST  | MOO | 400 | 1   | 62.6   | 34.4        | 7.2  | 191.0  | 91.7               | 21.3 | 218.2  | 43.6        | 22.3 | 234.8  | 191.1              | 30.4 |
| IUR         400         1         ····         ····         ····         ····         ····         ····         ····         ····         ····         ····         ·····         ······         ····     <   | MOO  | PRT | 400 | 1   | -100.0 | 96.6        | 20.3 | -100.0 | -31.4              | 15.3 | -100.0 | 167.4       | 28.5 | -499.8 | 97.5               | 74.3 |
|   | MOO  | TUR | 400 | 1   |        | -           | -    | -      |                    |      | -43.6  | -100.9      | 2.7  | 166.1  | -50.7              | 10.0 |
| NM $275$ $2$ $780$ $5.8$ $11.0$ $6.0$ $1.6$ $0.7$ $0.12$ $0.12$ $0.3.6$ $0.3.$  | LOU  | TAN | 275 | 1   | -77.5  | 4.5         | 10.9 | 5.9    | 0.5                | 0.7  | -91.1  | 3.5         | 12.8 | -33.8  | 4.7                | 3.9  |
| HAN $275$ $2$ $49.1$ $2.4$ $6.9$ $183.4$ $17.5$ $20.9$ $95.4$ $6.0$ $13.5$ $18.8$ $12.5$ $18.8$ $12.5$ $13.6$ $12.3$ KEL $275$ $1$ $5.0$ $1$ $5.0$ $13.0$ $2.0$ $4.13$ $9.1$ $86.5$ $88.8$ $12.5$ $30.8$ $37.1$ $6.1$ MAG $275$ $1$ $5.0$ $13.0$ $2.0$ $40.6$ $7.4$ $4.7$ $37.5$ $5.7$ $5.4$ $11.6$ $6.8$ WA $275$ $1$ $1.8$ $1.80$ $1.83$ $3.6$ $40.7$ $12.0$ $6.9$ $2.44$ $4.2$ $10.7$ $6.8$ WA $275$ $1$ $1.8$ $1.8$ $1.20$ $1.8$ $12.0$ $5.7$ $5.4$ $11.6$ $6.8$ $3.17$ WA $275$ $1$ $1.8$ $1.8$ $1.20$ $1.94$ $12.0$ $6.9$ $8.9$ $11.6$ $6.8$ $3.17$ WA $275$ $1$ $1.8$ $3.16$ $3.12$ $2.12$ $4.2$ $10.7$ $6.3$ $2.20$ $9.6$ $6.8$ $3.17$ WA $275$ $1$ $1$ $5.9$ $3.12$ $3.2$ $12.10$ $2.11$ $3.7$ $12.10$ $9.2$ WA $275$ $1$ $1$ $1$ $1$ $1.20$ $13.7$ $12.10$ $12.7$ $12.10$ $12.2$ $12.10$ $12.2$ WA $275$ $1$ $1$ $1$ $10.7$ $2.21$ $10.7$ $2.21$ $12.10$ $12.2$ <td>LOU</td> <td>TAN</td> <td>275</td> <td>2</td> <td>-78.0</td> <td>5.8</td> <td>11.0</td> <td>6.0</td> <td>1.6</td> <td>0.7</td> <td>-91.2</td> <td>4.5</td> <td>12.9</td> <td>-33.6</td> <td>5.3</td> <td>3.9</td>   | LOU  | TAN | 275 | 2   | -78.0  | 5.8         | 11.0 | 6.0    | 1.6                | 0.7  | -91.2  | 4.5         | 12.9 | -33.6  | 5.3                | 3.9  |
| KEL $275$ $1$ $12.5$ $31.4$ $4.8$ $69.1$ $41.3$ $91.7$ $86.5$ $18.8$ $12.5$ $30.8$ $35.1$ MAG $275$ $1$ $50$ $13.0$ $2.0$ $40.6$ $7.4$ $47$ $375$ $5.7$ $5.4$ $10.6$ $6.8$ BYC $275$ $1$ $-293$ $32.3$ $6.1$ $104.9$ $13.4$ $12.0$ $16.9$ $5.4$ $10.7$ $6.8$ $31.7$ HN $275$ $1$ $-18.0$ $-88.3$ $3.6$ $83.7$ $42.7$ $10.7$ $63.8$ $-22.0$ $9.5$ $80.8$ $31.7$ HN $275$ $1$ $-18.0$ $-88.3$ $3.6$ $83.7$ $42.7$ $10.7$ $63.8$ $22.0$ $9.6$ $31.7$ HN $275$ $1$ $1$ $-63.8$ $3.7$ $83.7$ $12.10$ $27.7$ $11.7$ $22.0$ $9.6$ $9.8$ HN $275$ $1$ $1$ $-63.8$ $3.7$ $12.7$ $10.7$ $63.8$ $22.0$ $10.6$ MAG $275$ $1$ $1$ $-7$ $22.8$ $12.10$ $21.7$ $11.3$ $11.2$ $11.2$ MAG $275$ $1$ $1$ $-7$ $22.8$ $10.9$ $10.7$ $10.7$ $10.7$ $10.7$ $10.7$ MAG $275$ $1$ $1$ $-7$ $22.8$ $10.9$ $22.9$ $10.6$ $10.7$ $10.7$ $10.7$ MAG $275$ $10$ $10.9$ $21.9$ $10.7$ $22.9$ $10.7$ $10.7$ <   | BPS  | HAN | 275 | 2   | 49.1   | -2.4        | 6.9  | 183.4  | 17.5               | 20.9 | 95.4   | 6.0         | 13.5 | 185.8  | 12.3               | 21.1 |
| MAG         Z75         1         5,0         13,0         2,0         40,6         7,4         4,7         3,75         5,4         11.6         6,8         17.3           BYC         Z75         1         -293         32.3         6.1         104,9         -13.4         12.0         16.9         -24.4         4.2         107.3         -17.3           HAN         Z75         1         -18.0         -18.3         3.6         -83.7         -42.7         10.7         63.8         -22.0         95.7         -80.8         -31.7           HAN         Z75         1         -58.4         3.7         -27.2         13.7         -52.0         95.7         -80.8         -31.7           HAN         Z75         1         -58.4         3.7         -27.2         13.7         -27.9         95.7         -11.3         -25.0         95.4         -11.3         -36.7         -11.3         -11.3         -11.3         -11.2         -11.4         -14.5         -14.6         -14.5         -14.6         -14.5         -14.6         -14.5         -14.6         -14.5         -14.5         -14.5         -14.5         -14.5         -14.5         -14.5         -14.5         -1   | BPS  | KEL | 275 | 1   | -12.5  | 31.4        | 4.8  | 69.1   | 41.3               | 9.1  | 86.5   | 18.8        | 12.5 | 30.8   | 35.1               | 5.3  |
| BYC $275$ $1$ $-29.3$ $32.3$ $6.1$ $104.9$ $13.4$ $12.0$ $16.9$ $-24.4$ $4.2$ $1073$ $17.3$ HAN $275$ $1$ $18.0$ $18.3$ $3.6$ $83.7$ $42.7$ $10.7$ $63.8$ $22.0$ $9.5$ $80.8$ $31.7$ HAN $275$ $1$ $18.0$ $18.3$ $3.6$ $83.7$ $42.7$ $10.7$ $65.8$ $22.0$ $9.5$ $80.8$ $31.7$ HAN $275$ $1$ $58.4$ $3.7$ $8.3$ $-121.0$ $2.7$ $10.7$ $65.8$ $22.0$ $9.5$ $80.8$ $31.7$ KPS $275$ $1$ $-58.4$ $3.7$ $8.3$ $-121.0$ $2.7$ $10.7$ $63.8$ $22.0$ $9.5$ $80.8$ $31.7$ MAG $275$ $1$ $-58.4$ $3.7$ $8.3$ $-121.0$ $2.7$ $10.7$ $22.1$ $113.2$ $113.2$ MAG $275$ $1$ $-59.4$ $3.7$ $8.3$ $-10.9$ $21.3$ $108.6$ $52.6$ $74.4$ $61.3$ $9.4$ MAG $275$ $1$ $-59.5$ $10.9$ $38.7$ $10.9$ $21.3$ $108.6$ $52.6$ $113.2$ $119.2$ MAG $275$ $1$ $-59.5$ $10.6$ $61.6$ $61.6$ $61.6$ $61.3$ $64.6$ $61.3$ $64.6$ MAG $275$ $1$ $-59.7$ $10.7$ $22.9$ $22.1$ $108.6$ $-22.6$ $13.4$ $119.2$ MAG $275$ $1$ $-22.9$  | BPS  | MAG | 275 | 1   | 5.0    | 13.0        | 2.0  | 40.6   | 7.4                | 4.7  | 37.5   | 5.7         | 5.4  | 11.6   | 6.8                | 1.5  |
| HAN $275$ $1.8$ $1.8.0$ $1.8.3$ $3.6$ $8.3.7$ $4.2.7$ $10.7$ $63.8$ $2.2.0$ $9.5$ $80.8$ $3.1.7$ HAN $275$ $2$ $1.8.0$ $1.8.3$ $3.6$ $83.7$ $4.27$ $10.7$ $63.8$ $22.0$ $9.5$ $80.8$ $31.7$ KPS $275$ $1$ $58.4$ $3.7$ $8.3$ $121.0$ $2.7$ $10.7$ $63.8$ $22.0$ $9.6$ $8.9.8$ $31.7$ KPS $275$ $1$ $58.4$ $3.7$ $8.3$ $121.0$ $2.7$ $13.7$ $21.3$ $21.461$ $3.8$ MAG $275$ $1$ $-59.4$ $-7$ $0.8$ $-10.9$ $21.3$ $108.6$ $21.4$ $113.2$ $119.6$ MAG $275$ $1$ $-7$ $-7$ $23.8$ $108.7$ $21.9$ $21.4$ $113.2$ $119.6$ MAG $275$ $1$ $-7$ $-7$ $21.8$ $21.9$ $21.3$ $108.6$ $-21.2$ $113.2$ $119.6$ MAG $275$ $1$ $-7$ $-7$ $21.6$ $22.9$ $12.4$ $22.6$ $12.4$ $113.2$ $119.6$ MAG $275$ $1$ $-7$ $21.6$ $22.7$ $22.9$ $22.3$ $34.5$ $6.9$ $50.6$ $23.7$ $14.8$ MAG $275$ $1$ $21.6$ $21.7$ $22.9$ $22.2$ $22.4$ $22.6$ $24.7$ $10.7$ $10.7$ MAG $275$ $1$ $21.6$ $22.7$ $22.7$ $22.9$ $22.7$ $22.9$ <  | BPS  | ВҮС | 275 | 1   | -29.3  | -32.3       | 6.1  | 104.9  | -13.4              | 12.0 | 16.9   | -24.4       | 4.2  | 107.3  | -17.3              | 12.3 |
| HAN         275         2         -18.0         -18.3         3.6         -83.7         -42.7         10.7         65.8         -22.0         9.5         -80.8         -31.7           KPS         275         1         -58.4         3.7         8.3         -1210         2.7         13.7         -13.9         3.6         -1461         3.8           TAN         275         1         -58.4         3.7         8.3         -10.9         2.7         13.7         -13.9         3.6         -1461         3.8           MAG         275         1         -         -         -         -108.5         -10.9         21.3         108.6         -2.2         13.4         113.2         -11.9           MAG         275         2         154.2         -10.0         7.3         108.5         -2.2         13.4         113.2         -11.9           MAG         275         1         -5.0         -10.0         7.3         -184.1         -16.6         -14.3         -14.3         -14.3           MAG         275         1         -5         13.4         13.2         21.4         13.2         13.4         113.2         14.8         -14.9 <t< td=""><td>CAS</td><td>HAN</td><td>275</td><td>1</td><td>-18.0</td><td>-18.3</td><td></td><td>-83.7</td><td>-42.7</td><td>10.7</td><td>-63.8</td><td>-22.0</td><td>9.5</td><td>-80.8</td><td>-31.7</td><td>9.9</td></t<>  | CAS  | HAN | 275 | 1   | -18.0  | -18.3       |      | -83.7  | -42.7              | 10.7 | -63.8  | -22.0       | 9.5  | -80.8  | -31.7              | 9.9  |
| KPS2751-58.43.78.3-121.02.713.7-23.111.33.6146.13.83.6TAN2751 <t< td=""><td>CAS</td><td>HAN</td><td>275</td><td>2</td><td>-18.0</td><td>-18.3</td><td>3.6</td><td>-83.7</td><td>-42.7</td><td>10.7</td><td>-63.8</td><td>-22.0</td><td>9.5</td><td>-80.8</td><td>-31.7</td><td>9.9</td></t<>  | CAS  | HAN | 275 | 2   | -18.0  | -18.3       | 3.6  | -83.7  | -42.7              | 10.7 | -63.8  | -22.0       | 9.5  | -80.8  | -31.7              | 9.9  |
| TAN2751··   | CAS  | KPS | 275 | 1   | -58.4  | 3.7         | 8.3  | -121.0 | 2.7                | 13.7 | -23.1  | -11.3       | 3.6  | -146.1 | 3.8                | 16.6 |
| MAG275110108.5108.6-2.213.4113.2119.5119.5MAG2752154.2154.237.138.5108.5108.5108.6-2.213.4113.2119.5119.5BYC2751-50.510.07.3184.123.921.196.613.813.813.211.9119.5BYC2751-50.510.07.3184.123.921.196.67.613.4113.211.9BYC2751-31.62.74.522.922.33.634.56.95.033.314.8MAG275124.22.13.486.620.33.634.56.95.033.314.8MAG275124.22.110.581.714.83.634.56.95.05.314.8MAG275124.22.110.581.714.83.634.55.023.314.8MAG275174.32.110.581.714.89.445.95.023.314.8MAG275174.321.110.5132.484.415.1118.825.517.1113.921.9MAG275191.07.612.9132.484.415.1118.825.517.1113.921.5MAG<  | CAS  | TAN | 275 | 1   | -      | 1           | 1    | -32.8  | -1.1               | 3.7  | 47.5   | 22.6        | 7.4  | -61.3  | 9.4                | 7.0  |
| MAG         275         154.2         -37.1         38.5         108.5         -10.9         12.2         13.4         113.2         -11.9           BYC         275         1         -50.5         -10.0         7.3         -184.1         -23.9         21.1         -96.6         -16.8         13.8         -186.5         -18.6           BYC         275         1         -31.6         -2.7         4.5         -22.9         22.3         3.6         34.5         6.9         5.0         -33.3         14.8         14.8           KPS         275         2         -31.6         -22.9         22.3         3.6         34.5         6.9         5.0         -33.3         14.8         14.8           MAG         275         1         24.2         2.1         3.4         8.6         5.0         5.0         -33.3         14.8         14.8           MAG         275         1         24.2         21.1         34.5         6.6         5.0         5.3         14.8         14.8         14.8         14.8         14.8         14.8         14.8         14.8         14.8         14.8         14.8         14.8         14.9         14.9         14.9  | CPS  | MAG | 275 | 1   | -      | -           | -    | 108.5  | -10.9              | 21.3 | 108.6  | -2.2        | 13.4 | 113.2  | -11.9              | 12.6 |
| BYC         275         1         -50.5         -10.0         7.3         -184,1         -23.9         21.1         -96.6         -16.8         13.8         -186.5         -18.6 <td>CPS</td> <td>MAG</td> <td>275</td> <td>2</td> <td>154.2</td> <td>-37.1</td> <td>38.5</td> <td>108.5</td> <td>-10.9</td> <td>21.3</td> <td>108.6</td> <td>-2.2</td> <td>13.4</td> <td>113.2</td> <td>-11.9</td> <td>12.6</td>  | CPS  | MAG | 275 | 2   | 154.2  | -37.1       | 38.5 | 108.5  | -10.9              | 21.3 | 108.6  | -2.2        | 13.4 | 113.2  | -11.9              | 12.6 |
| KPS         275         1         -31.6         -2.7         4.5         -22.9         22.3         3.6         34.5         -6.9         5.0         -33.3         14.8           KPS         275         2         -31.6         -2.7         4.5         -22.9         22.3         3.6         34.5         -6.9         5.0         -33.3         14.8           MAG         275         1         24.2         2.1         4.5         -22.9         22.3         3.6         34.5         -6.9         5.0         -33.3         14.8           MAG         275         1         24.2         2.1         10.5         81.7         -14.8         2.6         7.8         6.6         86.2         -9.3           IMN         275         1         91.0         7.6         12.9         132.4         8.4         15.1         118.8         25.5         17.1         113.9         9.1           IMN         275         2         91.0         7.8         15.1         113.9         9.1  | HAN  | ВҮС | 275 | 1   | -50.5  | -10.0       | 7.3  | -184.1 | -23.9              | 21.1 | -96.6  | -16.8       | 13.8 | -186.5 | -18.6              | 21.3 |
| KPS         275         2         -31.6         -2.7         4.5         -22.9         22.3         3.6         34.5         -6.9         5.0         -33.3         14.8           MAG         275         1         24.2         2.1         3.4         8.6         -20.8         2.6         76.6         -33.3         14.8         14.8           MAG         275         1         24.2         2.1         3.4         8.6         -20.8         2.6         76.8         0.5         2.4         9.7         15.0           TAN         275         1         74.3         2.1         10.5         81.7         14.8         9.4         45.9         7.8         6.6         86.2         9.3           TMN         275         1         91.0         7.6         12.9         132.4         8.4         15.1         118.8         25.5         17.1         113.9         9.1           TMN         275         2         91.0         7.6         132.4         8.4         15.1         118.8         25.5         17.1         113.9         9.1  | KEL  | KPS | 275 | 1   | -31.6  | -2.7        | 4.5  | -22.9  | 22.3               | 3.6  | 34.5   | -6.9        | 5.0  | -33.3  | 14.8               | 4.1  |
| MAG         275         1         24.2         2.1         3.4         8.6         -20.8         2.6         -16.8         0.5         2.4         -9.7         -15.0           TAN         275         1         74.3         2.1         10.5         81.7         -14.8         9.4         45.9         7.8         6.6         86.2         -9.3           TAN         275         1         91.0         7.6         12.9         132.4         8.4         15.1         118.8         25.5         17.1         113.9         9.1           TAN         275         2         91.0         7.6         12.9         132.4         8.4         15.1         118.8         25.5         17.1         113.9         9.1   | KEL  | KPS | 275 | 2   | -31.6  | -2.7        | 4.5  | -22.9  | 22.3               | 3.6  | 34.5   | -6.9        | 5.0  | -33.3  | 14.8               | 4.1  |
| TAN         275         1         74.3         2.1         10.5         81.7         -14.8         9.4         45.9         7.8         6.6         86.2         -9.3           TMN         275         1         91.0         7.6         12.9         132.4         8.4         15.1         118.8         25.5         17.1         113.9         9.1           TMN         275         2         91.0         7.6         12.9         132.4         8.4         15.1         118.8         25.5         17.1         113.9         9.1   | KEL  | MAG | 275 | 1   | 24.2   | 2.1         | 3.4  | 8.6    | -20.8              | 2.6  | -16.8  | 0.5         | 2.4  | -9.7   | -15.0              | 2.0  |
| TMN         275         1         91.0         7.6         12.9         132.4         8.4         15.1         118.8         25.5         17.1         113.9         9.1           TMN         275         2         91.0         7.6         12.9         132.4         8.4         15.1         118.8         25.5         17.1         113.9         9.1   | KPS  | TAN | 275 | 1   | 74.3   | 2.1         | 10.5 | 81.7   | -14.8              | 9.4  | 45.9   | 7.8         | 6.6  | 86.2   | -9.3               | 9.8  |
| TMN 275 2 91.0 7.6 12.9 132.4 8.4 15.1 118.8 25.5 17.1 113.9 9.1  | MAG  | TMN | 275 | 1   | 91.0   | 7.6         | 12.9 | 132.4  | 8.4                | 15.1 | 118.8  | 25.5        | 17.1 | 113.9  | 9.1                | 13.0 |
|   | MAG  | TMN | 275 | 2   | 91.0   | 7.6         | 12.9 | 132.4  | 8.4                | 15.1 | 118.8  | 25.5        | 17.1 | 113.9  | 9.1                | 13.0 |

|      |         |      |     |        |               | 00   | 0000   |             |      |        |               | 00   | 0202   |              |      |
|------|---------|------|-----|--------|---------------|------|--------|-------------|------|--------|---------------|------|--------|--------------|------|
|      | Ċ       | Line |     |        | II-Man mi     |      |        | Mintor Dool |      | Ŭ      | Hollow and    |      |        | Arinton Dool |      |
|      |         |      |     |        | Summer valley |      |        | winter Peak |      |        | Summer valley |      |        | WINTER PEAK  |      |
| From | To      | k۷   | No. | MM     | MVAR          | %    | MW     | MVAR        | %    | MW     | MVAR          | %    | MW     | MVAR         | %    |
| TAN  | TUR     | 275  | 1   |        | -             | '    | '      | '           |      | -76.4  | -18.8         | 11.1 | -145.7 | -26.5        | 16.8 |
| TAN  | TUR     | 275  | 2   | '      |               | '    | ,      |             |      | -76.4  | -18.8         | 11.1 | -145.7 | -26.5        | 16.8 |
| TMN  | TUR     | 275  | 1   |        | -             |      |        |             |      | 98.3   | 28.1          | 14.4 | 63.2   | 15.1         | 7.4  |
| TMN  | TUR     | 275  | 2   |        | -             | ,    |        |             |      | 98.3   | 28.1          | 14.4 | 63.2   | 15.1         | 7.4  |
| AD   | KRA     | 220  | 1   | 82.6   | -47.6         | 24.3 | 147.4  | 4.7         | 31.5 | 68.0   | -30.0         | 18.9 | 168.9  | 4.1          | 36.1 |
| AD   | RAF     | 220  | 1   | 110.9  | -54.8         | 28.5 | 117.6  | -12.7       | 23.1 | 55.1   | -47.2         | 16.7 | 128.7  | -12.0        | 25.2 |
| AD   | 660     | 220  | 1   | -85.0  | 89.7          | 21.6 | -96.0  | 6.9         | 16.8 | 80.5   | -71.3         | 18.8 | -125.7 | 10.9         | 22.0 |
| AD   | KRA     | 220  | 2   | 85.0   | -89.7         | 31.4 | 362.5  | 11.1        | 77.5 | 166.5  | -72.8         | 46.2 | 415.1  | 9.0          | 88.7 |
| ARK  | CKM     | 220  | 1   | 39.7   | 0.1           | 9.1  | 98.2   | -22.8       | 19.7 | 110.5  | -10.3         | 25.6 | 123.1  | -27.7        | 24.6 |
| ARK  | LWD     | 220  | 1   | -54.4  | -0.7          | 12.5 | -132.0 | 8.4         | 30.4 | -123.0 | 9.3           | 28.4 | -158.0 | 11.5         | 36.4 |
| BVK  | CLA     | 220  | 1   | -29.9  | 116.3         | 16.2 | -8.2   | 8.7         | 1.5  | -98.2  | 31.8          | 13.9 | -69.7  | 19.8         | 9.2  |
| BVK  | ВҮН     | 220  | 1   | 29.9   | -46.6         | 12.8 | 117.4  | -31.0       | 23.7 | 98.1   | -19.7         | 13.2 | 178.9  | -42.1        | 23.2 |
| BLC  | FIN (I) | 220  | 1   | -43.1  | -11.5         | 7.8  | -43.1  | -10.3       | 7.8  | -56.9  | 45.6          | 12.8 | -107.7 | -2.5         | 18.9 |
| BLC  | SHL     | 220  | 1   | '      |               | '    |        | ı           |      | -29.6  | -45.8         | 9.6  | -79.5  | -46.6        | 16.2 |
| CLE  | CDU     | 220  | 1   | 1.0    | -28.3         | 6.5  | -25.5  | -14.3       | 5.7  | 15.6   | -68.5         | 16.2 | 44.6   | -66.3        | 15.6 |
| CLE  | WOO     | 220  | 1   | -73.2  | 1.7           | 16.9 | -46.6  | -12.1       | 9.4  | -170.3 | 21.4          | 39.6 | -199.1 | 22.7         | 39.1 |
| CLE  | BTN     | 220  | 1   | ,      | -             | '    | ,      |             | '    | 0.0    | -8.3          | 1.5  | 0.0    | -9.6         | 1.7  |
| CLE  | BTN     | 220  | 7   |        |               | ı    |        | ·           |      | 0.0    | -8.3          | 1.5  | 0.0    | -9.6         | 1.7  |
| CLA  | KRA     | 220  | 1   | -61.0  | 99.2          | 18.0 | -73.4  | -11.6       | 9.9  | -95.2  | 38.7          | 15.9 | -117.9 | -4.4         | 15.7 |
| CSH  | FLA     | 220  | 1   | 55.2   | -20.5         | 16.8 | 120.6  | -4.9        | 27.7 | 51.3   | -20.4         | 15.8 | 77.6   | 1.9          | 17.8 |
| CSH  | PRO     | 220  | 1   | 3.8    | -38.5         | 9.9  | -69.9  | -13.4       | 15.2 | 13.1   | -25.5         | 7.3  | -49.4  | -8.1         | 10.7 |
| CSH  | TYN     | 220  | 1   | -151.4 | 110.3         | 24.6 | -215.9 | 9.8         | 27.3 | -124.3 | 94.1          | 20.5 | -157.0 | -2.7         | 19.8 |
| CKM  | DSN     | 220  | 1   | 8.4    | -37.1         | 8.8  | -3.7   | -2.6        | 0.9  | -45.7  | -24.7         | 12.0 | -110.7 | 35.7         | 22.7 |
| CKM  | ISH     | 220  | 1   | 37.0   | -35.1         | 8.6  | -23.2  | -180.2      | 30.6 | 186.3  | -72.5         | 33.7 | 99.0   | -218.5       | 40.4 |
| CUL  | GI      | 220  | 1   | -28.8  | 22.4          | 4.9  | 53.0   | -42.4       | 8.6  | -3.0   | 14.0          | 1.9  | 51.5   | -45.3        | 8.7  |
| CUL  | KRA     | 220  | 1   | -14.0  | -9.2          | 2.6  | -160.2 | 26.6        | 21.2 | -36.7  | -1.9          | 5.7  | -163.0 | 27.0         | 21.6 |

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|      | eak           | R %  | 4.3  | 4.3  | 3 28.7  | 1 77.2 | 3 28.7  | 32.6   | 18.3   | 30.5  | 30.5  | 53.6   | 13.6  | 4.5   | 38.6    | 19.9    | 37.6  | 38.1  | 0.2   | 6.2   | 206   |       |        |                |                       |                                 |  |   |
|------|---------------|------|------|------|---------|--------|---------|--------|--------|-------|-------|--------|-------|-------|---------|---------|-------|-------|-------|-------|-------|-------|--------|----------------|-----------------------|---------------------------------|--|---|
|      | Winter Peak   | MVAR | 3.3  | 3.3  | -15.3   | -200.1 | -15.3   | 35.5   | 21.2   | -7.1  | -7.1  | 25.5   | 4.4   | 0.0   | -1.3    | -62.9   | 20.4  | 1.5   | -1.3  | 13.1  | -29.8 | 1     | +·/-   | -1.4<br>-108.3 | -7.4<br>-108.<br>94.8 | -1.4<br>-108.3<br>94.8<br>-69.6 | -/.4<br>-108.3<br>-108.3<br>-108.3<br>-108.3<br>-69.6<br>-64.9 | -7.4<br>-108.3<br>-108.3<br>94.8<br>-69.6<br>-69.6<br>-32.6 |
| 2029 |               | MM   | 24.0 | 24.0 | 146.4   | -378.8 | 146.4   | -163.3 | -83.0  | 156.3 | 156.3 | -186.5 | 64.5  | -23.2 | -229.2  | -20.4   | 174.9 | 195.7 | 0.0   | -26.2 | -84.5 | 279.4 |        | -741.0         | -741.0<br>-10.6       | -741.0<br>-10.6<br>-250.7       | -741.0<br>-10.6<br>-250.7<br>-263.5                            | -741.0<br>-10.6<br>-250.7<br>-263.5<br>137.7                |
| 50   | ey            | %    | 4.3  | 4.3  | 30.9    | 36.4   | 30.9    | 31.8   | 30.3   | 19.4  | 19.4  | 11.3   | 9.2   | 3.4   | 0.7     | 21.4    | 31.2  | 32.4  | 14.5  | 15.7  | 6.4   | 17.7  |        | 65.6           | 65.6<br>7.1           | 65.6<br>7.1<br>0.7              | 65.6<br>7.1<br>0.7<br>16.3                                     | 65.6<br>7.1<br>0.7<br>16.3<br>6.0                           |
|      | Summer Valley | MVAR | 4.0  | 4.0  | -93.9   | 31.7   | -93.9   | 35.1   | 32.7   | 3.5   | 3.5   | -7.4   | 10.4  | -14.3 | -3.9    | -71.0   | -13.7 | -25.5 | 38.0  | -0.4  | 9.4   | -61.1 | 4 C C  | 7.11           | 45.2                  | 2/.1<br>45.2<br>-3.6            | -7.1<br>45.2<br>-3.6<br>70.9                                   | -7.1<br>45.2<br>-3.6<br>70.9<br>-24.2                       |
|      | S             | MM   | 24.0 | 24.0 | 95.5    | -199.7 | 95.5    | -133.4 | -114.3 | 84.1  | 84.1  | 38.9   | 33.7  | -3.0  | 0.0     | -1.9    | 121.8 | 138.3 | -77.0 | -68.0 | 20.5  | 80.5  | -367.7 |                | 30.0                  | 30.0                            | 30.0<br>0.0<br>-97.2   | 30.0<br>0.0<br>-97.2<br>36.7                                |
|      |               | %    |      | -    | 13.5    | 73.4   | 13.5    | 5.6    | 18.5   | 24.6  | 16.9  | 20.5   | 12.8  | 0.4   | 55.2    | 17.6    | 40.9  | 32.8  |       | 2.8   | 19.4  | 43.8  | ####   |                | 4.1                   | 4.1<br>52.0                     | 4.1<br>52.0<br>42.0  | 4.1<br>52.0<br>42.0<br>14.2                                 |
|      | Winter Peak   | MVAR |      | -    | -4.0    | -81.4  | -4.0    | -5.8   | 35.2   | -8.1  | -15.7 | -3.8   | -4.2  | -1.9  | 16.0    | -51.2   | 15.9  | -3.4  |       | 11.3  | -27.7 | -9.4  | -13.4  |                | 29.3                  | 29.3<br>45.1                    | 29.3<br>45.1<br>71.4   | 29.3<br>45.1<br>71.4<br>-26.5                               |
| 2020 |               | MW   |      | -    | 69.1    | -399.0 | 69.1    | -28.0  | -79.1  | 106.8 | 71.9  | 71.7   | 60.8  | -0.5  | -326.8  | -28.3   | 190.9 | 168.1 | -     | -7.0  | -79.8 | 249.4 | -650.2 |                | -14.0                 | -14.0<br>-281.6                 | -14.0<br>-281.6<br>-203.2                                      | -14.0<br>-281.6<br>-203.2<br>105.1                          |
| 20   | ey            | %    |      | -    | 20.1    | 38.4   | 20.1    | 13.0   | 11.2   | 10.1  | 11.6  | 7.4    | 4.7   | 7.3   | 0.7     | 12.0    | 20.9  | 17.7  |       | 10.6  | 3.0   | 15.0  | 59.7   |                | 1.5                   | 1.5<br>20.5                     | 1.5<br>20.5<br>8.0   | 1.5<br>20.5<br>8.0<br>7.1                                   |
|      | Summer Valley | MVAR | ı    |      | -59.0   | 75.1   | -59.0   | 8.7    | 14.9   | -5.7  | 10.6  | -6.6   | 14.5  | -17.1 | -3.9    | -27.1   | -20.0 | -25.5 | ı     | 3.0   | 10.3  | -82.0 | 127.2  | ,              | -8.1                  | -8.1<br>37.8                    | -8.1<br>37.8<br>-18.1  | -8.1<br>37.8<br>-18.1<br>42.7                               |
|      | S             | MM   | ı    |      | 64.2    | -199.7 | 64.2    | -55.6  | -41.2  | 35.0  | 39.2  | 25.1   | -10.7 | 26.5  | 0.0     | -29.0   | 79.8  | 72.3  |       | -46.1 | 1.1   | 23.7  | -310.4 |                | -8.2                  | -8.2<br>-105.9                  | -8.2<br>-105.9<br>-29.7  | -8.2<br>-105.9<br>-29.7<br>29.7                             |
|      |               | No.  | 1    | 2    | 1       | 1      | 2       | 2      | 1      | 1     | 2     | 1      | 1     | 1     | 1       | 1       | 1     | 1     | 1     | 1     | 1     | 1     | 1      |                | 7                     | 1                               | 1 1  | 0 -1 -1 -1  |
|      | LINE          | kV   | 220  | 220  | 220     | 220    | 220     | 220    | 220    | 220   | 220   | 220    | 220   | 220   | 220     | 220     | 220   | 220   | 220   | 220   | 220   | 220   | 220    |                | 220                   | 220<br>220                      | 220<br>220<br>220  | 220<br>220<br>220<br>220                                    |
| :    | 3             | To   | CRH  | CRH  | FIN (I) | NH     | (I) NIJ | MOO    | KLS    | MAY   | MAY   | ΗT     | ΓΟΠ   | SRA   | NH      | ΝM      | KLS   | LWD   | LWN   | LOU   | MAY   | RAF   | HSI    |                | CBT                   | CBT<br>SHL                      | CBT<br>SHL<br>BYH  | CBT<br>SHL<br>BYH<br>KPG                                    |
|      |               | From | CDU  | CDU  | CDU     | CDU    | CDU     | CDU    | DSN    | DSN   | DSN   | DSN    | FLA   | FLA   | FIN (I) | FIN (I) | GI    | GI    | GI    | GOR   | GOR   | GGO   | INC    |                | INC                   | INC                             | INC<br>ISH<br>KNR  | INC<br>ISH<br>KNR<br>KNR                                    |

|      | ak            | %    | 41.8  | 33.2   | 38.6  | 9.9   | 8.6   | 26.5   | 12.4  | 12.4  | 4.7   | 38.4   | 3.8   | 16.4   | 15.6  | 53.1   | 23.9  | 2.7  | 7.6   | 37.7   | 7.9    | 41.9  | 51.0   | 53.2   | 7.4   | 4.8   | 15.4  | 32.1  |
|------|---------------|------|-------|--------|-------|-------|-------|--------|-------|-------|-------|--------|-------|--------|-------|--------|-------|------|-------|--------|--------|-------|--------|--------|-------|-------|-------|-------|
|      | Winter Peak   | MVAR | -12.6 | -4.3   | -16.2 | -39.9 | 24.9  | -71.1  | -23.9 | -23.9 | -11.9 | 79.5   | 12.1  | -129.0 | -13.0 | 15.6   | 17.3  | -6.3 | 14.5  | -79.0  | 27.2   | -54.5 | 37.2   | 36.2   | -0.8  | 10.1  | 77.2  | -12.2 |
| 2029 |               | MM   | 235.4 | -150.5 | 135.6 | 31.5  | 59.3  | -184.5 | 78.3  | 78.3  | 16.6  | -294.1 | -27.6 | 14.3   | -79.2 | -185.7 | -82.7 | 15.0 | -20.4 | -176.6 | -38.2  | 97.7  | -131.0 | -183.1 | -34.7 | -18.1 | 16.9  | 36.0  |
| 20   | ey            | %    | 22.5  | 17.5   | 29.3  | 12.7  | 2.8   | 16.1   | 5.4   | 5.4   | 2.0   | 27.0   | 2.8   | 9.8    | 15.0  | 10.2   | 29.7  | 1.5  | 1.2   | 49.3   | 7.4    | 40.7  | 18.4   | 19.5   | 2.6   | 1.4   | 15.4  | 27.5  |
|      | Summer Valley | MVAR | -20.0 | 17.5   | -13.3 | -34.2 | -20.7 | -26.3  | -21.9 | -21.9 | -6.4  | -38.0  | 15.1  | -62.6  | 8.7   | -12.1  | -20.2 | 0.7  | -3.6  | 45.8   | -32.8  | -45.5 | 13.3   | 11.5   | -11.0 | 4.0   | -19.3 | -18.0 |
|      | Sı            | MM   | 104.0 | -59.3  | 77.8  | 43.0  | -5.9  | -119.4 | 28.3  | 28.3  | -2.4  | -201.7 | -15.1 | -40.5  | 64.4  | -31.0  | -77.3 | -8.1 | -1.9  | -209.1 | 29.6   | 98.7  | -47.3  | -67.3  | 5.0   | 2.7   | -64.0 | 20.4  |
|      |               | %    | 35.3  | 28.4   | 38.8  | 10.2  | -     |        | 16.7  | 16.7  | 5.9   | 8.4    | 11.8  | 5.8    | -     | 11.6   | 17.3  | 3.6  | 11.6  | 36.3   | 20.6   | 40.6  | 37.8   | 39.6   | 10.5  | 6.2   | -     | 32.7  |
|      | Winter Peak   | MVAR | -6.3  | -6.6   | -26.1 | -52.3 |       |        | -28.1 | -28.1 | -10.5 | 39.5   | 34.8  | -41.8  |       | -3.4   | 18.7  | -2.7 | 26.2  | -13.3  | 53.8   | -47.0 | 25.1   | 22.7   | -4.1  | 8.5   | -     | -13.8 |
| 2020 |               | MW   | 199.0 | -128.7 | 134.7 | -0.4  |       |        | 106.4 | 106.4 | 23.3  | 53.8   | -86.8 | 18.9   |       | -40.5  | -58.4 | 21.5 | -28.3 | -185.8 | -109.6 | 97.7  | -97.8  | -137.1 | -48.9 | -25.6 | -     | 37.1  |
| 20   | ey            | %    | 17.0  | 17.0   | 13.5  | 10.6  | -     | -      | 1.3   | 1.3   | 0.8   | 3.7    | 2.4   | 1.9    | -     | 4.4    | 12.1  | 1.0  | 14.9  | 31.6   | 8.5    | 39.7  | 16.9   | 18.1   | 4.3   | 0.3   | -     | 12.0  |
|      | Summer Valley | MVAR | -48.1 | 36.1   | -12.5 | -45.1 | -     | -      | -7.5  | -7.5  | -2.5  | -27.0  | 13.0  | 8.8    | -     | -6.5   | -31.1 | 4.9  | 40.1  | 68.3   | 31.4   | -38.2 | 0.4    | -5.9   | -19.9 | -0.4  | -     | -9.8  |
|      | Sı            | MW   | 72.6  | -47.8  | 34.1  | -9.9  | -     |        | 4.1   | 4.1   | -0.8  | -6.5   | -12.8 | 11.1   | -     | -12.6  | -9.6  | -2.1 | -29.0 | -118.9 | -39.6  | 98.9  | -45.1  | -63.3  | 1.6   | 0.8   | -     | 6.7   |
|      |               | No.  | 1     | 1      | 1     | 1     | 1     | 1      | 1     | 2     | 1     | 1      | 2     | 1      | 1     | 1      | 1     | 1    | 1     | 1      | 1      | 1     | 1      | 2      | 1     | 2     | 1     | 1     |
|      | e             | kV   | 220   | 220    | 220   | 220   | 220   | 220    | 220   | 220   | 220   | 220    | 220   | 220    | 220   | 220    | 220   | 220  | 220   | 220    | 220    | 220   | 220    | 220    | 220   | 220   | 220   | 110   |
| :    | LINE          | To   | KLN   | RAF    | SH    | KPG   | MAY   | 00M    | MP    | MP    | TB    | MAY    | MAY   | INC    | ORL   | TH     | SH    | PRO  | PB    | TYN    | SHL    | CKM   | INC    | INC    | TB    | KPG   | ORL   | DRU   |
|      |               | From | KRA   | KRA    | KLN   | KLN   | КYN   | КУN    | ВЧЯ   | KPG   | KPG   | CBT    | CBT   | CBT    | LOU   | MAY    | MAY   | MP   | MN    | 0ST    | PB     | PB    | PB     | BB     | PRO   | TB    | MOO   | AA    |

|      | -       |     |     |       |               | 2020  | 20    |             |      |       |               | 20   | 2029  |             |      |
|------|---------|-----|-----|-------|---------------|-------|-------|-------------|------|-------|---------------|------|-------|-------------|------|
|      | LING    | Ð   |     | SL    | Summer Valley | ĥ     |       | Winter Peak |      | S     | Summer Valley | ey   |       | Winter Peak |      |
| From | To      | k۷  | No. | MM    | MVAR          | %     | MM    | MVAR        | %    | MW    | MVAR          | %    | MM    | MVAR        | %    |
| AA   | ENN (I) | 110 | 1   | 2.7   | -12.5         | 12.9  | 24.1  | -11.2       | 22.0 | 19.8  | -20.9         | 29.1 | 23.5  | -9.7        | 21.0 |
| AA   | (I) WIT | 110 | 1   | -11.4 | 17.4          | 11.7  | -11.3 | 12.0        | 7.9  | 12.9  | 6.1           | 8.0  | -9.6  | 21.5        | 11.3 |
| AD   | MHI     | 110 | 1   | 23.3  | 7.7-          | 24.8  | 56.5  | 4.3         | 46.8 | 19.0  | -5.6          | 20.0 | 60.8  | 4.0         | 50.3 |
| ARI  | ARI T   | 110 | 1   | -1.1  | -0.3          | 1.1   | 2.2   | -1.9        | 2.4  | -0.7  | -0.1          | 0.7  | 2.1   | -2.0        | 2.3  |
| AGL  | DYN     | 110 | 1   | 0.0   | -0.3          | 0.3   | -17.7 | 8.8         | 16.1 | 0.0   | -0.3          | 0.3  | -17.8 | 4.4         | 14.9 |
| AGL  | ENN (I) | 110 | 1   | -6.1  | -1.5          | 6.3   | -17.4 | 7.2         | 15.6 | -13.6 | 4.1           | 14.3 | -13.0 | 5.3         | 11.6 |
| AGL  | ΗS      | 110 | 1   | 6.1   | 1.8           | 6.1   | 35.2  | -16.0       | 32.5 | 13.6  | -3.8          | 13.6 | 30.7  | -9.7        | 27.1 |
| AHA  | KLN     | 110 | 1   | -0.8  | -0.3          | 1.2   | -5.2  | -0.8        | 7.7  | -0.5  | -0.2          | 0.7  | -5.5  | -0.9        | 8.1  |
| ADM  | GCA     | 110 | 1   | -     |               |       |       |             |      | -0.3  | 3.1           | 2.2  | -0.6  | 4.1         | 3.0  |
| ADM  | INC     | 110 | 1   | -24.0 | 2.4-7         | 23.8  | -32.7 | -6.8        | 24.9 | -10.2 | -7.1          | 12.1 | -16.4 | -11.4       | 14.9 |
| ANR  | D00     | 110 | 1   | -14.0 | 6.9-          | 2.4.5 | -14.0 | 6.9-        | 34.7 | -14.0 | -6.9          | 34.7 | -14.0 | -6.9        | 34.7 |
| ARK  | BEG     | 110 | 1   | 14.6  | 5.3           | 15.7  | 34.7  | 0.9         | 28.5 | 28.8  | 3.5           | 29.3 | 41.0  | 0.3         | 33.6 |
| ARK  | BOG     | 110 | 1   | -5.8  | -1.8          | 3.4   | -7.6  | 6.9         | 4.9  | -20.8 | 0.9           | 11.7 | -12.8 | 8.4         | 7.3  |
| ARK  | РНҮ     | 110 | 1   |       |               |       |       |             | 1    | 1.2   | 0.3           | 0.7  | 1.2   | 0.3         | 0.6  |
| ARK  | РНҮ     | 110 | 2   | -     |               |       |       |             | ,    | 1.1   | 0.3           | 0.6  | 1.1   | 0.3         | 0.5  |
| ATE  | DRO     | 110 | 1   | 0.0   | -6.9          | 5.7   | -13.8 | 5.7         | 10.7 | 0.0   | -6.6          | 5.5  | -13.8 | 5.9         | 10.7 |
| ATE  | KNR     | 110 | 1   | 0.0   | 6.9           | 3.9   | 25.1  | -18.4       | 14.8 | 0.0   | 6.6           | 3.7  | 46.7  | -28.0       | 25.9 |
| ATH  | LA      | 110 | 1   | 5.8   | 10.2          | 11.8  | 10.1  | 11.1        | 12.4 | 9.0   | 8.0           | 12.1 | 1.4   | 2.5         | 2.4  |
| ATH  | SH      | 110 | 1   | -24.3 | 24.4          | 19.4  | 2.67- | 37.2        | 46.3 | -20.5 | 26.9          | 19.0 | -75.3 | 8.0         | 39.8 |
| BKE  | AUG     | 110 | 1   | -     | -             | -     | -     | -           |      | -51.9 | 36.3          | 35.6 | -48.0 | 15.6        | 24.0 |
| BKE  | KPG     | 110 | 1   |       | -             | -     |       |             | •    | 51.9  | -36.3         | 35.6 | 48.0  | -15.6       | 24.0 |
| AUG  | CFM     | 110 | 1   | 25.4  | 14.1          | 30.3  | 25.4  | 14.1        | 30.3 | 25.4  | 14.2          | 30.3 | 25.4  | 14.1        | 30.3 |
| AUG  | MTN     | 110 | 1   | 41.8  | -35.1         | 30.7  | 64.3  | -4.0        | 30.7 | 37.1  | -22.2         | 24.3 | 63.0  | 2.0-        | 30.0 |
| AUG  | SK      | 110 | e   | -60.0 | 26.1          | 54.5  | 6.67- | -1.4        | 66.6 | -69.9 | 14.8          | 59.6 | 6.08- | -6.0        | 67.6 |
| AUG  | SK      | 110 | 4   | -60.0 | 26.1          | 54.5  | -79.9 | -1.4        | 66.6 | -69.9 | 14.8          | 59.6 | -80.9 | -6.0        | 67.6 |
| AUG  | CFM     | 110 | 2   | 25.4  | 14.1          | 30.3  | 25.4  | 14.1        | 30.3 | 25.4  | 14.2          | 30.3 | 25.4  | 14.1        | 30.3 |

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|      | -       |     |     |       |               | 2020 | 20    |             |      |       |               | 20   | 2029  |             |      |
|------|---------|-----|-----|-------|---------------|------|-------|-------------|------|-------|---------------|------|-------|-------------|------|
|      | LINE    | е   |     | SI    | Summer Valley | ĥ    |       | Winter Peak |      | SI    | Summer Valley | ey . |       | Winter Peak |      |
| From | To      | kv  | No. | MM    | MVAR          | %    | MW    | MVAR        | %    | MM    | MVAR          | %    | MW    | MVAR        | %    |
| ARV  | COS     | 110 | 1   | -10.5 | 6.4           | 11.8 | -33.9 | 9.6         | 28.6 | -21.8 | 11.1          | 23.5 | -40.6 | 13.9        | 34.9 |
| ARV  | GWE     | 110 | 1   | 22.5  | -0.4          | 12.6 | -10.0 | 1.8         | 4.8  | -4.9  | 5.4           | 4.1  | -27.2 | 5.7         | 13.3 |
| ARV  | NAV     | 110 | 1   | -4.3  | 9.0           | 5.6  | 11.9  | -0.7        | 5.7  | 15.8  | 6.9           | 9.7  | 24.3  | 1.1         | 11.6 |
| ARV  | SKL     | 110 | 1   | -4.3  | -8.3          | 6.8  | 17.8  | -5.8        | 13.7 | 6.1   | -13.0         | 10.5 | 24.4  | -11.4       | 19.6 |
| ARV  | SKL     | 110 | 2   | -3.4  | -6.8          | 4.2  | 14.1  | -4.8        | 7.1  | 4.8   | -10.5         | 6.5  | 19.2  | -9.3        | 10.2 |
| ART  | FIN (I) | 110 | 1   | -7.6  | 2.1           | 6.6  | -34.9 | -2.1        | 26.7 | -4.7  | 2.5           | 4.4  | -37.0 | -2.5        | 28.3 |
| ART  | MCD     | 110 | 1   | 5.1   | -2.2          | 9.4  | 18.9  | 0.3         | 14.4 | 3.1   | -2.5          | 3.3  | 20.1  | 0.6         | 15.3 |
| BVK  | GRO     | 110 | 1   | 0.0   | -25.1         | 12.9 | -56.4 | 15.7        | 26.6 | 0.0   | -23.4         | 12.0 | -56.4 | 15.7        | 26.6 |
| ATY  | CLW     | 110 | 1   | -22.5 | 3.4           | 23.0 | -51.5 | 2.2         | 42.6 | -25.1 | 8.5           | 26.8 | -24.0 | 0.1         | 19.8 |
| ATΥ  | CNB     | 110 | 1   | -     | -             |      |       |             | -    | 22.0  | -8.8          | 13.3 | 0.5   | -6.3        | 3.0  |
| BWR  | CRA     | 110 | 1   | 0.0   | -14.2         | 20.8 | 12.6  | -9.1        | 22.8 | 0.0   | -14.1         | 20.7 | 12.6  | -9.1        | 22.8 |
| BOL  | ENN (I) | 110 | 1   | 12.9  | 0.1           | 7.3  | 48.2  | 0.9         | 23.0 | -4.7  | 2.9           | 3.1  | 43.2  | -1.5        | 20.6 |
| BOL  | TBKT    | 110 | 1   | -12.9 | 2.3           | 7.4  | -17.4 | -9.6        | 9.5  | 4.7   | -0.5          | 2.7  | -6.1  | -8.6        | 5.0  |
| BAL  | CDU     | 110 | 1   | 7.2   | 12.8          | 8.2  | -38.6 | -9.2        | 19.0 | 23.6  | 7.7           | 13.9 | -22.4 | -15.6       | 13.1 |
| BAL  | DRY     | 110 | 1   | -10.5 | -13.5         | 9.6  | 25.0  | 5.7         | 12.2 | -25.6 | -8.1          | 15.1 | 8.0   | 11.9        | 6.8  |
| BLI  | DMY     | 110 | 1   | -3.4  | 1.6           | 5.5  | 2.8   | -4.9        | 8.3  | -2.1  | 1.9           | 4.2  | 1.9   | -5.1        | 8.0  |
| BEG  | CKM     | 110 | 1   | 11.5  | 5.6           | 9.4  | 19.9  | -0.7        | 12.5 | 26.8  | 3.4           | 19.9 | 25.3  | -1.8        | 16.0 |
| CDL  | ВҮН     | 110 | 1   | 0.0   | 0.7           | 0.3  | 49.3  | -43.9       | 30.0 | 0.0   | 0.7           | 0.3  | 49.3  | -44.2       | 30.1 |
| BLK  | BLKT    | 110 | 1   | -3.9  | 0.5           | 2.9  | -11.1 | -2.3        | 7.2  | -2.5  | 0.3           | 1.8  | -11.9 | -2.5        | 7.6  |
| BLU  | CDU     | 110 | 1   | -     |               | -    | -     | -           | -    | 17.4  | 1.4           | 13.4 | 0.5   | 0.3         | 0.5  |
| BLU  | MUL     | 110 | 1   | -     |               |      |       |             | -    | -17.4 | -1.4          | 16.6 | -0.5  | -0.3        | 0.5  |
| BIN  | CF      | 110 | 1   | -9.0  | 5.5           | 10.6 | -4.7  | -5.1        | 5.7  | -2.5  | 14.8          | 15.2 | 12.6  | -12.2       | 14.5 |
| BIN  | TIV     | 110 | 1   | 4.7   | -5.2          | 5.1  | 10.8  | -2.6        | 7.0  | 4.1   | -15.0         | 11.4 | 10.8  | -1.6        | 6.9  |
| BDA  | MON     | 110 | 1   | -3.0  | 3.6           | 4.8  | 4.0   | -13.2       | 11.4 | 4.6   | -0.6          | 4.7  | 14.9  | -10.1       | 14.9 |
| BDA  | NEW (I) | 110 | 1   | -2.2  | -4.5          | 4.1  | -9.3  | 12.4        | 12.7 | -9.9  | 6.0-          | 8.1  | -20.2 | 9.2         | 18.2 |
| BDN  | CUL     | 110 | 1   | -29.8 | 8.3           | 15.8 | -30.7 | -1.1        | 14.2 | -23.7 | 4.1           | 12.3 | -30.6 | 2.3         | 14.2 |

| -     |      |     |       |               | 20   | 2020  |             |      |       |               | 07     | 5029  |             |      |
|-------|------|-----|-------|---------------|------|-------|-------------|------|-------|---------------|--------|-------|-------------|------|
|       | LINE |     | S     | Summer Valley | ey   |       | Winter Peak |      | S     | Summer Valley | ey     |       | Winter Peak |      |
| To    | kv   | No. | MM    | MVAR          | %    | MW    | MVAR        | %    | MM    | MVAR          | %      | MM    | MVAR        | %    |
| D00   | 110  | 1   | 21.6  | -10.6         | 13.5 | 12.9  | -3.9        | 6.4  | 16.3  | -6.1          | 9.8    | 13.3  | -7.4        | 7.3  |
| CLG   | 110  | 1   | -     | -             | -    | -     | -           |      | 8.7   | 7.3           | 5.9    | 8.7   | 7.3         | 5.9  |
| SBH   | 110  | 1   |       |               |      |       |             |      | -26.7 | -13.3         | 15.5   | -26.7 | -13.3       | 15.5 |
| RAF   | 110  | 1   | -11.8 | -3.2          | 19.4 | -13.9 | -3.5        | 15.6 | -7.4  | -2.0          | 12.1   | -14.7 | -3.7        | 16.5 |
| RAF   | 110  | 2   | -5.4  | -0,2          | 5.5  | -16.7 | -2.3        | 14.0 | -3.4  | -0.1          | 3.4    | -17.7 | -2.5        | 14.8 |
| CBR   | 110  | 1   | 11.1  | -2.4          | 5.8  | 43.6  | -17.6       | 21.3 | 8.1   | -1.9          | 4.3    | 59.7  | -23.9       | 29.1 |
| моү   | 110  | 1   | -12.5 | 7.0           | 10.4 | 4.3   | -14.4       | 11.0 | -9.0  | 6.7           | 8.2    | 25.3  | -12.2       | 20.5 |
| INC   | 110  | 1   | -15.5 | 0'5-          | 11.6 | -15.5 | -5.0        | 11.6 | -28.0 | -9.2          | 21.1   | -28.0 | -9.2        | 21.1 |
| INC   | 110  | 2   | -15.5 | -5.0          | 11.6 | -15.5 | -5.0        | 11.6 | -28.0 | -9.2          | 21.1   | -28.0 | -9.2        | 21.1 |
| RE    | 110  | 1   | -16.6 | -2.4          | 14.1 | -67.3 | -11.6       | 57.4 | -10.3 | -1.4          | 8.8    | -71.3 | -12.8       | 60.9 |
| ККҮ   | 110  | 1   | -     | -             | -    |       | -           |      | -24.8 | 5.7           | 14.3   | -19.6 | -4.8        | 9.6  |
| CNB   | 110  | 1   | '     |               | ı    | ı     | ı           |      | 21.2  | -6.5          | 12.4   | -8.5  | -4.3        | 4.5  |
| BRI   | 110  | 1   | 2.0   | 0.4           | 4.5  | 2.0   | 0.4         | 4.5  | 2.0   | 0.4           | 4.5    | 2.0   | 0.4         | 4.5  |
| DMY   | 110  | 1   | -2.8  | -13.7         | 14.1 | -20.7 | 2.4         | 17.2 | 2.3   | -8.5          | 8.9    | -20.3 | 1.4         | 16.8 |
| RAF   | 110  | 1   | -18.1 | 9.2           | 20.5 | -30.5 | -2.8        | 25.3 | -17.5 | 5.2           | 18.5   | -32.2 | -2.8        | 26.7 |
| BRI   | 110  | 2   | 2.0   | 0.5           | 4.5  | 2.0   | 0.4         | 4.5  | 2.0   | 0.5           | 4.5    | 2.0   | 0.4         | 4.5  |
| CDU   | 110  | 1   | -66.1 | -22.9         | 37.4 | -68.4 | -23.0       | 32.9 | -75.5 | -23.8         | 42.4   | -75.5 | -23.8       | 36.2 |
| BAR T | 110  | 1   | -9.1  | -1.7          | 6.8  | -24.0 | -8.5        | 16.0 | -5.7  | 6.0-          | 4.3    | -26.0 | -9.1        | 17.3 |
| DRN   | 110  | 1   | 21.5  | 5.1           | 9.7  | 21.5  | 4.6         | 9.7  | 57.6  | 20.9          | 26.9   | 57.6  | 20.0        | 26.7 |
| DRN   | 110  | 2   | 21.5  | 5.1           | 9.7  | 21.5  | 4.6         | 9.7  | 57.6  | 20.9          | 26.9   | 57.6  | 20.0        | 26.7 |
| DTN   | 110  | 2   |       |               | -    |       |             |      | -7.9  | -12.8         | 10.7   | 9.8   | -4.2        | 7.5  |
| GRA   | 110  | 1   |       |               | -    |       |             |      | -11.6 | -16.5         | 14.4   | 36.0  | 2.8         | 25.8 |
| KLM   | 110  | 1   |       |               | -    | 1     | ı           |      | -9.3  | -14.9         | 12.5   | 26.0  | -0.2        | 18.5 |
| CUL   | 110  | 1   | -6.3  | -0.2          | 3.6  | -43.6 | -0.4        | 22.7 | -10.0 | 1.5           | 5.7    | -45.0 | -2.4        | 23.5 |
| KTN   | 110  | 1   | -2.5  | 0.0           | 1.3  | 3.0   | -7.3        | 3.7  | 4.5   | -1.2          | 2.3    | 3.2   | -5.8        | 3.1  |
| TRI   | 110  | 1   | 0.0   | 1.3           | 0    | 1 00  | -171        | 070  | c     | ,<br>,        | (<br>, |       | ļ           |      |

|      |               | %    | 16.3  | 25.3  | 9.7   | 16.9  | 4.8  | 33.6  | 1.7 | 5.4  | 30.1 | 14.4  | 9.4  | 27.3  | 1.2   | 21.5 | 24.9 | 9.1  | 8.8     | 12.3 | 15.1  | 15.1  | 10.0 | 21.1 | 6.0  | 8.0  | 8.8  | 17.0 |
|------|---------------|------|-------|-------|-------|-------|------|-------|-----|------|------|-------|------|-------|-------|------|------|------|---------|------|-------|-------|------|------|------|------|------|------|
|      | Winter Peak   | MVAR | 1.6   | -22.9 | -5.9  | -3.8  | -0.7 | 2.1   | 1.6 | 2.3  | 0.2  | 4.2   | -6.9 | 4.2   | -1.3  | -7.8 | 10.2 | -0.6 | 11.8    | 7.4  | 9.2   | 9.2   | 2.1  | 1.3  | 0.1  | 5.4  | -5.2 | -1.0 |
| 2029 |               | MM   | -34.3 | 48.0  | -10.3 | -19.7 | 6.3  | 63.8  | 3.2 | 10.1 | 63.1 | -30.9 | 17.5 | -24.5 | 2.2   | 44.4 | 51.4 | 11.0 | -14.2   | 13.2 | 16.1  | 16.1  | 9.4  | 25.9 | 7.2  | 8.2  | 9.2  | 20.5 |
| 20   | y             | %    | 13.7  | 0.4   | 2.2   | 4.6   | 2.6  | 13.5  | 0.8 | 6.2  | 13.2 | 2.7   | 2.2  | 9.0   | 7.2   | 6.8  | 11.7 | 5.9  | 3.8     | 10.2 | 12.4  | 12.4  | 11.7 | 13.7 | 4.4  | 4.2  | 4.3  | 7.1  |
|      | Summer Valley | MVAR | 0.8   | 0.6   | -0.4  | 2.2   | -2.7 | -10.7 | 1.0 | 4.2  | -9.7 | -3.9  | 3.9  | 8.2   | -4.8  | -2.4 | -3.7 | -1.4 | -0.1    | -8.8 | -10.7 | -10.7 | 6.6- | -4.4 | 2.8  | -2.8 | -4.2 | -5.6 |
|      | SL            | MM   | -24.4 | 0.0   | -2.2  | -2.9  | 1.6  | 21.5  | 1.0 | -9.0 | 21.4 | -3.5  | 6.0  | 0.0   | -11.8 | 11.8 | 20.5 | 5.7  | -6.7    | 6.1  | 7.5   | 7.5   | 5.6  | 13.7 | 3.4  | -3.4 | 0.2  | 4.2  |
|      |               | %    |       | 23.7  | 8.9   | 15.9  | 4.6  | 29.9  | 3.9 | 7.8  | 26.8 | 14.9  | 10.4 | 29.0  | 5.0   | 18.6 | 28.6 | 13.3 | 11.1    | 17.7 | 21.6  | 21.6  | 15.6 |      | 4.7  | 9.0  | 5.4  | 16.0 |
|      | Winter Peak   | MVAR |       | -25.5 | -5.6  | -3.3  | -0.8 | 1.4   | 0.9 | 0.7  | 0.2  | 5.3   | -7.8 | 9.9   | -6.0  | -8.8 | 4.6  | -2.1 | 12.6    | 9.1  | 11.2  | 11.2  | 4.7  |      | -5.6 | -2.3 | -5.3 | -1.4 |
| 20   |               | MW   | ·     | 42.6  | -9.4  | -18.6 | 5.9  | 56.8  | 8.2 | 15.0 | 56.3 | -31.9 | 19.3 | -24.4 | 8.5   | 38.1 | 59.9 | 16.0 | -19.5   | 19.4 | 23.7  | 23.7  | 14.4 |      | 0.5  | 10.8 | 3.8  | 19.3 |
| 2020 | Ŋ             | %    |       | 0.4   | 3.5   | 6.1   | 2.9  | 9.4   | 4.1 | 6.6  | 9.1  | 7.6   | 8.5  | 10.6  | 9.5   | 0.5  | 12.6 | 8.6  | 6.3     | 13.2 | 16.0  | 16.0  | 12.8 |      | 4.5  | 4.2  | 6.1  | 8.6  |
|      | Summer Valley | MVAR |       | 0.6   | -0.7  | 1.7   | -2.4 | -7.0  | 4.6 | 10.1 | -5.7 | -14.8 | 14.7 | 9.7   | -9.4  | 0.7  | -1.9 | 0.1  | -8.9    | -8.4 | -10.1 | -10.1 | -9.2 |      | 4.3  | -4.3 | -5.6 | -5.2 |
|      | S             | MW   | ı     | 0.0   | -3.6  | -4.6  | 2.5  | 15.2  | 5.6 | 3.4  | 15.2 | -0.8  | -3.3 | 0.0   | 0.3   | -0.4 | 22.3 | 8.5  | 6.8     | 10.0 | 12.2  | 12.2  | 8.4  |      | -0.9 | 0.9  | -2.2 | 6.8  |
|      |               | No.  | 1     | 1     | 1     | 1     | 1    | 1     | 1   | 1    | 1    | 1     | 1    | 1     | 1     | 1    | 1    | 1    | 1       | 1    | 2     | 3     | 1    | 1    | 1    | 1    | 1    | 1    |
| 9    | U             | kv   | 110   | 110   | 110   | 110   | 110  | 110   | 110 | 110  | 110  | 110   | 110  | 110   | 110   | 110  | 110  | 110  | 110     | 110  | 110   | 110   | 110  | 110  | 110  | 110  | 110  | 110  |
|      | 3             | To   | TUL   | CLA   | TIV   | PTN   | MOL  | CKN   | DMY | MAC  | KER  | IA    | KBY  | GRV   | SRA   | ARIT | CLN  | DLT  | ENN (I) | GAL  | GAL   | GAL   | SAL  | SHN  | TRI  | TRL  | CLN  | CBG  |
|      |               | From | BOG   | BGH   | AGY   | CAB   | CAB  | CLA   | CLA | CLA  | CKN  | CRO   | CRO  | СДУ   | СDY   | СDY  | CSH  | CSH  | CSH     | CSH  | CSH   | CSH   | CSH  | CSH  | CLH  | CLH  | CBR  | CBR  |

|      |         |     |     |       |               | 2020    | 20    |             |      |       |               | 2029 | 29    |             |      |
|------|---------|-----|-----|-------|---------------|---------|-------|-------------|------|-------|---------------|------|-------|-------------|------|
|      | 5       | ע   |     | SI    | Summer Valley | ,<br>Ki |       | Winter Peak |      | S     | Summer Valley | ey   |       | Winter Peak |      |
| From | To      | kv  | No. | MM    | MVAR          | %       | MM    | MVAR        | %    | MW    | MVAR          | %    | MM    | MVAR        | %    |
| CBR  | DLT     | 110 | 1   | -2.1  | -4.3          | 4.8     | -1.9  | -7.2        | 6.2  | -1.7  | -3.0          | 3.5  | 4.6   | -8.4        | 7.9  |
| CD   | KВҮ     | 110 | 1   | -4.5  | 16.0          | 9.3     | 23.2  | 6.0-        | 11.0 | -9.4  | 5.6           | 6.1  | 18.9  | 0.5         | 9.0  |
| CD   | MAC     | 110 | 1   | 4.5   | -16.0         | 9.3     | -15.2 | -1.3        | 7.3  | 17.3  | -7.1          | 10.5 | -11.0 | -2.0        | 5.3  |
| СРК  | TNΥ     | 110 | 1   | 2.3   | -7.3          | 7.6     | 12.9  | -6.3        | 14.3 | 1.5   | -7.3          | 7.4  | 13.6  | -6.2        | 15.0 |
| CF   | CL      | 110 | 1   | 0.0   | -0.2          | 0.3     | -19.9 | 6.7         | 30.8 | -19.9 | 7.3           | 31.1 | -19.9 | 1.8         | 29.4 |
| CF   | COR     | 110 | 1   | 3.8   | 8.8           | 5.4     | 43.2  | -6.1        | 20.9 | 29.3  | 3.8           | 16.6 | 61.7  | -6.1        | 29.6 |
| CF   | SRA     | 110 | 1   | -14.1 | 15.3          | 10.6    | 7.9   | -5.8        | 4.2  | 10.1  | 4.1           | 5.6  | 27.7  | -10.4       | 12.7 |
| CF   | CLO     | 110 | 2   | 6.0   | -16.7         | 10.0    | -7.2  | 0.6         | 3.5  | 0.9   | -31.0         | 17.4 | -28.2 | 12.6        | 14.8 |
| CAH  | D00     | 110 | 1   | -0.8  | 16.3          | 9.2     | 33.3  | 2.6         | 15.9 | 1.9   | 11.3          | 6.5  | 28.5  | 6.8         | 14.0 |
| CAH  | ТНХ     | 110 | 1   | 12.7  | -11.1         | 9.5     | 15.8  | 8.0         | 8.4  | 19.0  | -12.1         | 12.7 | 18.6  | 13.4        | 10.9 |
| CAH  | dIT     | 110 | 1   | 6.0-  | -15.9         | 9.0     | -31.4 | 9.6         | 15.6 | -2.8  | -10.2         | 5.9  | -21.7 | 12.0        | 11.8 |
| CAH  | BAR T   | 110 | 1   | -17.1 | 10.5          | 19.1    | -45.4 | 23.8        | 41.7 | -22.0 | 10.9          | 23.4 | -46.5 | 26.7        | 43.6 |
| CKM  | CHE     | 110 | 1   | 19.0  | 4.1           | 18.5    | 19.0  | 3.7         | 15.8 | 19.0  | 4.1           | 18.6 | 19.0  | 3.6         | 15.8 |
| CKM  | POT     | 110 | 1   | 4.1   | -5.3          | 5.7     | 15.7  | -3.3        | 13.5 | 2.6   | -5.5          | 5.1  | 16.6  | -3.1        | 14.2 |
| CKM  | CPK     | 110 | 1   | 6.1   | -9.5          | 8.3     | 24.8  | -7.4        | 18.9 | 3.8   | -9.6          | 7.6  | 26.2  | -7.2        | 19.9 |
| BRA  | NEW (I) | 110 | 1   | 7.3   | 4.1           | 6.2     | 7.1   | -14.6       | 10.2 | 33.6  | -2.8          | 24.8 | 41.3  | -14.2       | 27.4 |
| BRA  | PLS     | 110 | 1   | -10.4 | -4.8          | 11.6    | -21.3 | 11.0        | 19.8 | -35.5 | 2.3           | 36.0 | -56.3 | 10.4        | 47.3 |
| C00  | BCT     | 110 | 1   | 2.0   | 1.7           | 2.0     | 0.4   | 1.2         | 1.0  | 2.4   | 1.9           | 2.3  | 0.5   | 1.3         | 1.1  |
| C00  | CKM     | 110 | 2   | -2.9  | -2.0          | 2.7     | -4.8  | -2.7        | 4.2  | -3.0  | -2.1          | 2.8  | -5.1  | -2.9        | 4.5  |
| CLU  | KUD     | 110 | 1   |       | 1             | ı       | ·     |             |      | -2.6  | 2.4           | 1.9  | -2.6  | 2.4         | 1.6  |
| CLU  | CBT     | 110 | 1   | '     | ı             | ı       |       |             |      | -34.4 | -15.0         | 20.1 | -34.4 | -14.9       | 16.8 |
| CLN  | LA      | 110 | 1   | 13.3  | -5.7          | 22.9    | 31.8  | -9.3        | 27.3 | 16.4  | -5.7          | 17.5 | 27.9  | -3.8        | 23.3 |
| SCR  | KNΥ     | 110 | 1   | -7.5  | -1.9          | 5.7     | -28.3 | -10.1       | 18.9 | -4.7  | -1.0          | 3.6  | -22.0 | -10.6       | 15.3 |
| CRA  | LWD     | 110 | 1   | -17.4 | 8.8           | 11.0    | -64.2 | 1.4         | 30.6 | -13.5 | 8.7           | 9.0  | -66.2 | -0.6        | 31.5 |
| CRA  | TUL     | 110 | 1   | -     | -             |         | -     |             |      | 24.5  | -1.4          | 13.8 | 34.5  | -1.9        | 16.4 |
| CRA  | WEX     | 110 | 1   | 1.6   | 4.1           | 4.4     | 12.7  | -5.9        | 12.4 | -13.8 | 6.7           | 15.5 | 8.6   | -4.6        | 8.6  |

|             |         |     |     |       |               | 20   | 2020  |             |      |       |               | 2020 | 20    |             |      |
|-------------|---------|-----|-----|-------|---------------|------|-------|-------------|------|-------|---------------|------|-------|-------------|------|
|             | Line    | Je  |     | S     | Summer Vallev |      |       | Winter Peak |      | S     | Summer Vallev |      |       | Winter Peak |      |
| From        | To      | k   | No. | MM    | MVAR          | %    | MW    | MVAR        | %    | MW    | MVAR          | %    | MM    | MVAR        | %    |
| COS         | FLA     | 110 | 1   | -9.2  | 4.3           | 10.3 | -12.0 | -3.2        | 10.2 | -7.5  | 5.2           | 9.2  | -12.1 | -1.9        | 10.2 |
| COS         | FLA     | 110 | 2   | -9.4  | 4.4           | 10.5 | -12.3 | -3.2        | 10.5 | -7.7  | 5.3           | 9.4  | -12.5 | -1.9        | 10.4 |
| COS         | ARI T   | 110 | 1   | 1.4   | -1.8          | 1.3  | -40.0 | 11.0        | 19.7 | -11.1 | 1.4           | 6.3  | -46.1 | 10.6        | 22.5 |
| (I) COL (I) | FIN (I) | 110 | 1   | 5.1   | -0.8          | 4.9  | 2.8   | -1.4        | 2.5  | 1.3   | -3.5          | 3.5  | 4.4   | -2.3        | 4.0  |
| (I) TOJ     | CDU     | 110 | 1   | -15.5 | -1.1          | 10.8 | -29.9 | -4.0        | 21.1 | -7.8  | 2.4           | 5.7  | -33.1 | -3.5        | 23.3 |
| CHA         | GLE     | 110 | 1   | 3.8   | 0.3           | 3.8  | 9.9   | 4.3         | 8.9  | 2.4   | -0.2          | 2.4  | 11.0  | 4.6         | 9.9  |
| CHA         | KLN     | 110 | 1   | 5.4   | -10.4         | 8.6  | 13.8  | -15.4       | 13.0 | 11.3  | -6.8          | 9.7  | 19.9  | -16.6       | 16.3 |
| CHA         | MAL     | 110 | 1   | -13.0 | 12.5          | 10.1 | -19.3 | 3.6         | 9.4  | -16.0 | 9.4           | 10.4 | -27.6 | 4.2         | 13.3 |
| CLW         | KLS     | 110 | 1   | -19.7 | 1.8           | 20.0 | -49.2 | -15.6       | 42.7 | -1.5  | -9.6          | 9.8  | -35.8 | -18.0       | 33.1 |
| CLW         | KLS     | 110 | 2   | -19.8 | 1.7           | 20.1 | -49.3 | -16.1       | 42.8 | -1.5  | -9.7          | 9.9  | -35.8 | -18.4       | 33.3 |
| CLW         | STR T   | 110 | 1   | 3.6   | -1.4          | 5.7  | -7.5  | 15.2        | 24.9 | -30.7 | 27.3          | 60.3 | -10.1 | 18.2        | 30.5 |
| COW         | CVW     | 110 | 1   | 6.5   | -5.7          | 8.8  | 22.8  | -1.3        | 18.9 | 6.9   | -5.0          | 8.7  | 24.5  | -1.9        | 20.3 |
| COW         | OLD     | 110 | 1   | 0.3   | 0.0           | 1.0  | 0.3   | 0.0         | 1.0  | 0.3   | 0.0           | 1.0  | 0.3   | 0.0         | 1.0  |
| COW         | RAF     | 110 | 1   | -4.4  | 0.0           | 4.4  | -22.9 | -2.1        | 19.0 | -6.4  | 0.6           | 6.5  | -23.7 | -1.8        | 19.7 |
| COW         | IHM     | 110 | 1   | -3.7  | 6.1           | 7.2  | -13.7 | 1.9         | 11.4 | -1.6  | 4.7           | 5.1  | -15.3 | 2.0         | 12.8 |
| CUN         | GLR     | 110 | 1   | -20.6 | 16.3          | 14.8 | -33.4 | 12.9        | 17.1 | -10.8 | 9.7           | 8.2  | -26.8 | 9.7         | 13.6 |
| CUN         | SLI     | 110 | 1   | 20.6  | -14.5         | 14.2 | 43.6  | -6.1        | 21.1 | 10.8  | -7.9          | 7.5  | 37.0  | -3.1        | 17.8 |
| CUS         | MLC     | 110 | 1   | 4.3   | 0.7           | 3.2  | 1.9   | -13.7       | 8.7  | 12.6  | -1.6          | 9.3  | 6.6   | -10.5       | 7.8  |
| CUS         | NEW (I) | 110 | 1   | 1.4   | 2.2           | 2.0  | 6.9   | 4.1         | 5.3  | 8.0   | 1.4           | 6.0  | 19.7  | 3.7         | 13.2 |
| CUS         | PLS     | 110 | 1   | -5.7  | -2.9          | 4.7  | -8.8  | 9.5         | 8.2  | -20.6 | 0.2           | 15.1 | -26.4 | 6.7         | 17.1 |
| CVW         | KRA     | 110 | 1   | -0.4  | -4.8          | 4.9  | -3.9  | -6.1        | 6.0  | 2.6   | -3.8          | 4.6  | -2.6  | -7.1        | 6.2  |
| CGL         | GAE     | 110 | 1   | 0.0   | -2.6          | 2.8  | -10.7 | 5.7         | 13.3 | 0.0   | -2.4          | 2.7  | -10.7 | 5.7         | 13.3 |
| CGL         | CKN     | 110 | 1   | 0.0   | 2.6           | 1.4  | 34.9  | -23.3       | 22.1 | 0.0   | 2.4           | 1.4  | 34.9  | -23.3       | 22.1 |
| COR         | GWE     | 110 | 1   | 3.8   | 10.9          | 6.5  | 41.5  | -5.8        | 19.9 | 29.2  | 4.5           | 16.6 | 59.7  | -8.2        | 28.7 |
| COR         | ENN (N) | 110 | 1   | 0.0   | 0.1           | 0.1  | 1.1   | -1.4        | 1.5  | -0.2  | 0.0           | 0.3  | 0.7   | -2.5        | 2.1  |
| CDK         | LWD     | 110 | 1   | 0.0   | -5.3          | 5.8  | 12.5  | -9.0        | 16.9 | 0.0   | -5.3          | 5.8  | 12.5  | -9.0        | 16.9 |

| MIRE Peak         Aumer Valley           MVAR         %         MVAR         %         MW           16.9         15.0         -8.7         -0.1         4.9         -22.2           -8.2         28.2         14.4         -6.1         8.8         57.5           -16.9         15.0         -8.7         -0.1         4.9         -22.2           -15.3         69.3         -12.5         -2.15         10.3         86.7           -15.3         69.3         -15.8         1.3         15.4         -88.9           -15.3         69.3         -15.8         1.3         15.4         -88.9           -15.3         69.3         -15.8         1.3         15.4         -88.9           -22.5         19.8         19.1         21.6         16.2         10.4           22.0         19.8         19.1         21.1         13.5         15.2           20.6         46.2         0.0         -4.3         86.7         -70.4           22.0         32.0         10.1         15.8         52.0         -70.4           -71.1         9.0         -11.8         8.5         15.2         -70.4           -5  | Line              |        |       |              |      | 2020  |             |      |       |             |      | 2029  |             |      |
|---|-------------------|--------|-------|--------------|------|-------|-------------|------|-------|-------------|------|-------|-------------|------|
| WMR%MWA%MW16.915.00 $-87$ $-0.11$ $4.9$ $-22.2$ $16.9$ 15.00 $-87$ $-0.11$ $4.9$ $-22.2$ $-8.2$ $28.2$ $14.4$ $-6.1$ $8.8$ $57.5$ $14.2$ $62.9$ $12.5$ $-2.5$ $10.3$ $86.7$ $14.2$ $62.9$ $12.5$ $-2.55$ $10.3$ $86.7$ $-15.3$ $69.3$ $-15.8$ $1.2$ $22.0$ $86.7$ $-15.3$ $69.3$ $-15.8$ $1.91$ $21.6$ $10.4$ $22.5$ $19.8$ $19.1$ $21.6$ $10.2$ $10.4$ $-20.6$ $25.4$ $0.0$ $-4.3$ $1.9$ $22.0$ $20.6$ $25.4$ $0.0$ $-4.12$ $1.9$ $22.7$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-7.1$ $9.0$ $-11.8$ $-11.8$ $8.5$ $15.2$ $-7.1$ $9.0$ $-11.8$ $3.8$ $-27.3$ $-7.1$ $9.0$ $-11.8$ $3.8$ $-29.7$ $-7.1$ $9.0$ $-11.8$ $-11.2$ $4.9$ $-7.1$ $9.0$ $-10.0$ $-10.6$ $-10.6$ $-7.1$ $-11.2$ $-11.2$ $-11.2$ $-11.2$ $-11.2$ $-11.2$ $-11.2$ $-11.2$  | Summer Valley     | Summer | Immei | <b>Valle</b> | y    | -     | Winter Peak |      | Su    | Immer Valle | şy   |       | Winter Peak |      |
| 16.915.0 $-8.7$ $-0.1$ $4.9$ $-22.2$ $-8.2$ $28.2$ $14.4$ $-6.1$ $8.8$ $57.5$ $57.5$ $14.2$ $62.9$ $12.5$ $12.5$ $10.3$ $86.7$ $57.5$ $14.2$ $62.9$ $12.5$ $12.5$ $10.3$ $86.7$ $57.5$ $-15.3$ $69.3$ $-15.8$ $1.2$ $1.2$ $86.7$ $10.3$ $-15.3$ $69.3$ $-15.8$ $1.2$ $1.2$ $86.7$ $10.4$ $-20.6$ $25.4$ $0.0$ $-4.3$ $21.2$ $52.0$ $10.4$ $220.6$ $25.3$ $0.0$ $-11.8$ $6.2$ $10.4$ $27.3$ $-20.6$ $46.2$ $0.0$ $-4.3$ $21.2$ $52.0$ $10.6$ $-20.6$ $46.2$ $0.0$ $-4.3$ $22.2$ $52.0$ $10.4$ $-20.6$ $46.2$ $0.0$ $-4.3$ $22.2$ $10.4$ $22.0$ $-20.6$ $5.3$ $0.0$ $-11.8$ $8.5$ $15.2$ $10.4$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $10.6$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $10.6$ $-7.1$ $9.0$ $-11.8$ $8.5$ $15.2$ $10.4$ $-7.1$ $9.0$ $-11.8$ $8.5$ $15.2$ $10.6$ $-7.1$ $9.0$ $1.4$ $1.2$ $8.3$ $70.4$ $-7.1$ $9.0$ $1.2$ $1.2$ $1.2$ $1.2$ $-7.1$ $9.0$ $1.2$ $1.2$ $1.2$ $1$   | kV No. MW MVAR    |        | MV    | AR           | %    | MM    | MVAR        | %    | MM    | MVAR        | %    | MM    | MVAR        | %    |
| -8.2 $28.2$ $14.4$ $-6.1$ $8.8$ $57.5$ $14.2$ $62.9$ $12.5$ $-2.5$ $10.3$ $86.7$ $-15.3$ $69.3$ $-15.8$ $1.3$ $15.4$ $88.9$ $-15.3$ $69.3$ $-15.8$ $1.3$ $15.4$ $-88.9$ $-7$ $-9.0$ $-19.9$ $5.9$ $11.7$ $13.5$ $22.5$ $19.8$ $19.1$ $21.6$ $10.4$ $28.9$ $22.6$ $25.4$ $0.0$ $-4.7$ $1.9$ $52.0$ $-20.6$ $25.4$ $0.0$ $-4.7$ $1.9$ $52.0$ $-20.6$ $25.3$ $0.0$ $-4.7$ $1.9$ $52.0$ $-20.6$ $25.3$ $0.0$ $-4.7$ $1.9$ $52.0$ $-7.1$ $9.0$ $-4.7$ $1.8$ $8.5$ $15.2$ $-7.1$ $9.0$ $-4.7$ $1.8$ $8.5$ $15.2$ $-7.1$ $9.0$ $-4.7$ $1.9$ $8.5$ $15.2$ $-7.1$ $9.0$ $-14.7$ $15.8$ $8.5$ $15.2$ $-7.1$ $9.0$ $-14.7$ $15.8$ $8.5$ $15.2$ $-7.1$ $9.0$ $-14.7$ $15.8$ $8.5$ $15.2$ $-7.1$ $9.0$ $-10.6$ $24.7$ $4.5$ $14.2$ $-5.8$ $25.9$ $10.6$ $24.7$ $4.5$ $14.2$ $-5.8$ $25.9$ $14.6$ $24.9$ $24.9$ $-5.3$ $-7.2$ $-7.2$ $-7.2$ $-7.2$ $-7.2$ $-7.2$ $-7.2$ $-7.2$ $-7.2$ $-7.2$ $-7.2$ </td <td>110 1 0.0 -1.4</td> <td></td> <td>-1.7</td> <td>t.</td> <td>0.8</td> <td>-23.3</td> <td>16.9</td> <td>15.0</td> <td>-8.7</td> <td>-0.1</td> <td>4.9</td> <td>-22.2</td> <td>16.8</td> <td>14.5</td>  | 110 1 0.0 -1.4    |        | -1.7  | t.           | 0.8  | -23.3 | 16.9        | 15.0 | -8.7  | -0.1        | 4.9  | -22.2 | 16.8        | 14.5 |
| 14.2 $62.9$ $12.5$ $-2.5$ $10.3$ $86.7$ $-15.3$ $69.3$ $-15.8$ $1.3$ $15.4$ $88.9$ $-5.5$ $-9.3$ $1.3$ $1.5.4$ $88.9$ $-88.9$ $22.5$ $19.8$ $19.1$ $21.6$ $10.4$ $23.5$ $20.6$ $25.4$ $0.0$ $-4.3$ $1.9$ $22.0$ $20.6$ $25.4$ $0.0$ $-4.3$ $1.9$ $22.0$ $-20.6$ $25.3$ $0.0$ $-4.3$ $1.9$ $52.0$ $-70.4$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $0.5$ $5.3$ $0.0$ $-4.7$ $1.9$ $52.0$ $-70.4$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-71$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-71$ $9.0$ $-11.8$ $8.5$ $15.7$ $15.7$ $-71$ $9.5$ $14.6$ $12.4$ <td>110 1 6.4 -3.7</td> <td></td> <td>-3.7</td> <td></td> <td>4.2</td> <td>55.8</td> <td>-8.2</td> <td>28.2</td> <td>14.4</td> <td>-6.1</td> <td>8.8</td> <td>57.5</td> <td>-4.9</td> <td>28.9</td>   | 110 1 6.4 -3.7    |        | -3.7  |              | 4.2  | 55.8  | -8.2        | 28.2 | 14.4  | -6.1        | 8.8  | 57.5  | -4.9        | 28.9 |
| $\cdot 15.3$ $69.3$ $\cdot 15.8$ $1.3$ $5.9$ $13.4$ $-88.9$ $\cdot$ $\cdot$ $\cdot$ $\cdot$ $\cdot$ $\cdot$ $19.0$ $\cdot 5.9$ $11.7$ $13.5$ $22.5$ $19.8$ $19.1$ $21.6$ $16.2$ $10.4$ $13.5$ $13.5$ $20.6$ $25.4$ $0.0$ $-4.3$ $2.2$ $-52.0$ $-52.0$ $-20.6$ $46.2$ $0.0$ $-4.3$ $2.2$ $-52.0$ $-70.4$ $-20.6$ $46.2$ $0.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-52.0$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-70.4$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-70.4$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-70.4$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-70.4$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-70.4$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-70.4$ $-5.8$ $29.3$ $14.6$ $-10.6$ $24.7$ $4.5$ $5.3$ $-5.8$ $55.6$ $14.6$ $-10.6$ $-25.0$ $-70.4$ $-5.8$ $55.7$ $-10.0$ $-17.7$ $-7.3$ $-70.4$ $-5.8$ $50.7$ $-10.6$ $-10.6$ $-10.7$ $-5.3$ $-7.7$ $-10.6$ $-10.6$ $-10.7$ $-20.4$ $-10.4$ $-7.7$ $-10.2$ $-10.7$ $-10.7$ $-17.7$ $-1$   | 110 1 20.1 -1.6   |        | -1.6  |              | 16.3 | 81.8  | 14.2        | 62.9 | 12.5  | -2.5        | 10.3 | 86.7  | 15.7        | 66.7 |
| $\cdot$ | 110 1 -25.3 -0.3  |        | -0.3  |              | 24.5 | -83.9 | -15.3       | 69.3 | -15.8 | 1.3         | 15.4 | -88.9 | -16.9       | 73.6 |
| 22.5 $19.8$ $19.1$ $21.6$ $16.2$ $10.4$ $10.4$ $20.6$ $25.4$ $0.0$ $-4.3$ $2.2$ $-52.0$ $10.4$ $-20.6$ $46.2$ $0.0$ $-4.3$ $2.2$ $-52.0$ $10.6$ $-7.1$ $9.0$ $4.6.7$ $10.8$ $6.2$ $-10.0$ $10.6$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $15.2$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $15.2$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $15.2$ $-13.8$ $29.3$ $1.8$ $-3.4$ $3.8$ $-27.3$ $15.2$ $-5.8$ $0.0$ $-10.6$ $7.2$ $12.4$ $-41.2$ $17.2$ $-6.7$ $32.0$ $-10.0$ $7.2$ $12.4$ $-41.2$ $17.2$ $-6.7$ $32.0$ $-10.0$ $7.2$ $12.4$ $-41.2$ $14.2$ $-6.7$ $32.0$ $-10.0$ $7.2$ $12.4$ $-41.2$ $14.2$ $-6.7$ $32.0$ $-10.0$ $7.2$ $12.4$ $-41.2$ $14.2$ $-6.7$ $32.0$ $-10.0$ $3.0$ $1.7$ $5.3$ $17.4$ $-7.8$ $6.3$ $32.9$ $-14.6$ $14.7$ $4.5$ $17.4$ $-7.8$ $6.3$ $32.9$ $-14.7$ $4.5$ $17.4$ $14.4$ $-7.7$ $14.7$ $11.7$ $11.7$ $5.3$ $11.4$ $-7.7$ $-7.8$ $12.4$ $-7.2$ $12.4$ $14.4$ $-7.8$  | 110 1             |        |       |              | ı    | ,     | ı           |      | -19.9 | -5.9        | 11.7 | 13.5  | 12.3        | 8.7  |
| 20.6 $25.4$ $0.0$ $-4.3$ $2.2$ $-52.0$ $-20.6$ $46.2$ $0.0$ $4.3$ $1.9$ $52.0$ $-10.0$ $0.5$ $5.3$ $0.0$ $-11.8$ $6.2$ $-10.0$ $-10.0$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-27.3$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-27.3$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-27.3$ $-7.1$ $9.0$ $-4.7$ $1.8$ $-3.4$ $3.8$ $-29.7$ $-13.8$ $29.3$ $1.8$ $-3.4$ $3.8$ $-29.7$ $-27.3$ $-13.8$ $29.3$ $1.8$ $-3.4$ $3.8$ $-29.7$ $-27.3$ $-5.8$ $6.5$ $14.6$ $-19.6$ $7.2$ $12.4$ $41.2$ $-5.8$ $6.5$ $14.6$ $-19.6$ $24.7$ $4.5$ $-5.3$ $-4.6$ $6.6$ $-23.0$ $-3.0$ $1.7$ $5.3$ $-70.4$ $-4.6$ $6.6$ $-24.7$ $4.6$ $-5.3$ $-70.4$ $-75.3$ $-4.6$ $6.6$ $-24.7$ $-10.6$ $-24.7$ $4.6$ $-5.3$ $-4.6$ $6.6$ $-24.7$ $-24.7$ $4.6$ $-5.3$ $-4.6$ $6.6$ $-10.6$ $-24.6$ $-10.6$ $-10.7$ $-7.7$ $-17.2$ $-17.2$ $-17.2$ $-17.2$ $-17.2$ $-17.2$ $24.7$ $-16.4$ $-17.2$ $-12.6$ $-17.2$ $-10.6$ $-10.6$ $-10.6$ <t< td=""><td>110 1 41.8 15.7</td><td></td><td>15.7</td><td></td><td>43.3</td><td>37.0</td><td>22.5</td><td>19.8</td><td>19.1</td><td>21.6</td><td>16.2</td><td>10.4</td><td>28.6</td><td>13.9</td></t<>   | 110 1 41.8 15.7   |        | 15.7  |              | 43.3 | 37.0  | 22.5        | 19.8 | 19.1  | 21.6        | 16.2 | 10.4  | 28.6        | 13.9 |
| -20.6 $46.2$ $0.0$ $4.3$ $1.9$ $52.0$ $7.0$ $0.5$ $5.3$ $0.0$ $-11.8$ $6.2$ $-10.0$ $15.2$ $10.0$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $15.2$ $15.2$ $-13.8$ $29.3$ $1.8$ $-3.4$ $3.8$ $-27.3$ $-77.3$ $-13.8$ $29.3$ $1.8$ $-3.4$ $3.8$ $-27.3$ $-77.3$ $-13.8$ $29.3$ $1.8$ $-70.4$ $3.8$ $-27.3$ $-77.3$ $-6.7$ $32.0$ $-10.0$ $7.2$ $12.4$ $-41.2$ $-77.3$ $-6.7$ $32.0$ $-10.0$ $7.2$ $12.4$ $-41.2$ $-70.4$ $-6.7$ $32.9$ $-14.7$ $1.7$ $8.3$ $-70.4$ $-70.4$ $-5.8$ $6.5$ $14.66$ $-19.6$ $24.7$ $4.5$ $-70.4$ $-7.8$ $32.9$ $-14.7$ $1.7$ $8.3$ $-70.4$ $-70.4$ $-7.8$ $32.9$ $-14.7$ $1.7$ $8.3$ $-70.4$ $-70.4$ $-7.8$ $32.9$ $-14.7$ $1.7$ $8.3$ $-70.4$ $-70.4$ $-7.9$ $-7.9$ $-7.9$ $-7.9$ $-7.9$ $-7.9$ $-7.9$ $-7.7$ $-7.9$ $-7.9$ $-7.9$ $-7.9$ $-7.9$ $-7.9$ $-7.7$ $-7.9$ $-7.9$ $-7.9$ $-7.9$ $-7.9$ $-7.9$ $-7.7$ $-7.9$ $-7.9$ $-7.9$ $-7.9$ $-7.9$ $-7.9$ $-7.7$ $-7.9$ $-7.9$ $-7.9$ <td>110 1 0.0 -4.4</td> <td></td> <td>-4.4</td> <td></td> <td>2.2</td> <td>-52.0</td> <td>20.6</td> <td>25.4</td> <td>0.0</td> <td>-4.3</td> <td>2.2</td> <td>-52.0</td> <td>24.5</td> <td>26.1</td>   | 110 1 0.0 -4.4    |        | -4.4  |              | 2.2  | -52.0 | 20.6        | 25.4 | 0.0   | -4.3        | 2.2  | -52.0 | 24.5        | 26.1 |
| 0.5 $5.3$ $0.0$ $-11.8$ $6.2$ $-10.0$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-7.1$ $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $-73.3$ $-13.8$ $29.3$ $1.8$ $-3.4$ $3.8$ $-27.3$ $-73.3$ $-13.8$ $29.3$ $1.8$ $-3.4$ $3.8$ $-29.7$ $-79.7$ $-5.5$ $32.0$ $10.0$ $7.2$ $12.4$ $-41.2$ $-79.7$ $-5.3$ $32.9$ $-10.0$ $7.2$ $12.4$ $-41.2$ $-70.4$ $-5.8$ $32.9$ $-14.6$ $14.6$ $10.7$ $8.3$ $-70.4$ $-5.8$ $32.9$ $-14.7$ $11.7$ $8.3$ $-70.4$ $-7.3$ $-17.2$ $24.7$ $4.6$ $-19.6$ $-27.3$ $-7.4$ $-7.4$ $-17.2$ $24.7$ $4.6.9$ $-7.4$ $-7.5$ $-7.4$ $-7.4$ $-7.4$ $-$   | 110 1 0.0 4.4     |        | 4.4   |              | 4.4  | 52.0  | -20.6       | 46.2 | 0.0   | 4.3         | 1.9  | 52.0  | -24.5       | 25.2 |
| -7.1 $9.0$ $-4.7$ $15.8$ $8.5$ $15.2$ $15.2$ $   0.0$ $-0.6$ $0.4$ $-27.3$ $-27.3$ $-13.8$ $29.3$ $1.8$ $-3.4$ $3.8$ $-29.7$ $-7.3$ $-6.7$ $32.0$ $-10.0$ $7.2$ $12.4$ $-41.2$ $-7.2$ $-5.8$ $6.5$ $14.6$ $-19.6$ $24.7$ $4.5$ $-70.4$ $-5.8$ $6.5$ $14.6$ $1.7$ $8.3$ $-70.4$ $-70.4$ $-5.8$ $6.5$ $14.6$ $14.6$ $1.7$ $5.3$ $-70.4$ $-5.8$ $0.5$ $-14.7$ $1.7$ $8.3$ $-70.4$ $-70.4$ $-5.8$ $0.5$ $-14.7$ $1.7$ $8.3$ $-70.4$ $-70.4$ $-7.8$ $32.9$ $-14.7$ $1.7$ $8.3$ $-70.4$ $-70.4$ $-5.8$ $0.2$ $0.0$ $-3.0$ $1.7$ $5.3$ $-70.4$ $-4.6$ $6.6$ $-2.3.0$ $-3.0$ $1.7$ $5.3$ $-70.4$ $-4.6$ $6.6$ $-2.9$ $-2.0$ $-1.7$ $-5.3$ $-70.4$ $-4.6$ $-2.6$ $-2.0$ $-2.6$ $-2.6$ $-2.6$ $-2.6$ $-4.6$ $-2.6$ $-2.6$ $-2.6$ $-1.7$ $-2.6$ $-2.6$ $-7.7$ $-2.6$ $-2.6$ $-2.6$ $-2.6$ $-2.6$ $-2.6$ $-7.7$ $-2.6$ $-2.6$ $-2.6$ $-2.6$ $-2.6$ $-2.6$ $-7.7$ $-2.6$ $-2.6$ $-2.6$ $-2.6$ $-2.6$   | 110 1 0.0 -11.9   |        | -11.9 |              | 6.3  | -10.0 | 0.5         | 5.3  | 0.0   | -11.8       | 6.2  | -10.0 | 0.1         | 5.3  |
| - $ 0.0$ $0.06$ $0.4$ $-27.3$ $-27.3$ $-27.3$ $-27.3$ $-29.7$ $-13.8$ $29.3$ $1.8$ $-3.4$ $3.8$ $-29.7$ $-29.7$ $-13.6$ $-13.6$ $29.3$ $1.8$ $-3.4$ $-29.7$ $-29.3$ $-70.4$ $-29.3$ $-70.4$ $-29.3$ $-29.7$ $-29.3$ $-29.1$ $-29.3$ $-29.1$ $-29.3$ $-29.1$ $-29.3$ $-29.1$ $-29.6$   | 110 1 -7.5 14.4   |        | 14.4  |              | 8.3  | -18.6 | -7.1        | 9.0  | -4.7  | 15.8        | 8.5  | 15.2  | 6.2         | 7.5  |
| -13.8         29.3         1.8         -3.4         3.8         -29.7         -           -6.7         32.0         -10.0         7.2         12.4         -41.2         -           -5.8         6.5         14.6         -19.6         7.2         12.4         -41.2         -           -5.8         6.5         14.6         17.6         8.3         -70.4         -           6.3         32.9         -14.7         1.7         8.3         -70.4         -           6.3         32.9         -14.7         1.7         8.3         -70.4         -           76.4         32.9         -14.7         1.7         8.3         -70.4         -           7         -5.3         32.9         -14.7         1.7         8.3         -70.4           7         -5.1         0.0         -3.0         1.7         5.3         -         -           7         -4.6         6.6         -23.0         -31.7         44.9         14.4         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -         - <td>110 1</td> <td></td> <td></td> <td></td> <td>-</td> <td></td> <td></td> <td></td> <td>0.0</td> <td>-0.6</td> <td>0.4</td> <td>-27.3</td> <td>-12.9</td> <td>21.6</td>   | 110 1             |        |       |              | -    |       |             |      | 0.0   | -0.6        | 0.4  | -27.3 | -12.9       | 21.6 |
| -6.7 $32.0$ $-10.0$ $7.2$ $12.4$ $-41.2$ $-5.8$ $6.5$ $14.6$ $-19.6$ $24.7$ $4.5$ $6.3$ $52.9$ $-14.7$ $1.7$ $8.3$ $-70.4$ $6.3$ $32.9$ $-14.7$ $1.7$ $8.3$ $-70.4$ $  0.0$ $3.0$ $1.7$ $5.3$ $  0.0$ $-3.0$ $1.7$ $5.3$ $-4.6$ $6.6$ $-23.0$ $-8.8$ $24.9$ $-5.3$ $-4.6$ $6.6$ $-23.0$ $-8.8$ $24.9$ $-29.1$ $-17.2$ $24.7$ $-40.4$ $-21.6$ $46.3$ $-51.2$ $-17.2$ $24.7$ $-40.4$ $-21.6$ $46.3$ $-51.2$ $-17.2$ $24.7$ $-40.4$ $-21.6$ $46.3$ $-51.2$ $-17.2$ $24.7$ $-40.4$ $-21.6$ $46.3$ $-51.2$ $-17.2$ $24.7$ $-40.4$ $-21.6$ $46.3$ $-51.2$ $-17.2$ $13.1$ $44.9$ $14.4$ $-21.6$ $-17.2$ $10.0$ $0.0$ $-1.2$ $11.7$ $-2.03$ $-12.3$ $10.0$ $0.0$ $-1.2$ $11.7$ $-2.03$ $-12.3$ $10.0$ $0.0$ $-1.2$ $10.1$ $-2.03$ $-12.3$ $10.0$ $-1.2$ $-1.2$ $10.1$ $-2.03$ $-12.3$ $10.0$ $-10.2$ $-10.2$ $-20.3$ $-12.3$ $-1.2$ $-1.2$ $-1.2$ $-20.3$ $-12.4$ $-10.2$ $-10.2$ $-10.2$ $-10.2$   | 110 1 -2.5 -4.5   |        | -4.5  |              | 5.2  | -32.7 | -13.8       | 29.3 | 1.8   | -3.4        | 3.8  | -29.7 | -20.3       | 29.7 |
| -5.8 $6.5$ $14.6$ $-19.6$ $24.7$ $4.5$ $6.3$ $32.9$ $-14.7$ $1.7$ $8.3$ $-70.4$ $   0.0$ $3.0$ $1.7$ $5.3$ $   0.0$ $3.0$ $1.7$ $5.3$ $  0.0$ $-3.0$ $1.7$ $5.3$ $  0.0$ $-3.0$ $1.7$ $5.3$ $-4.6$ $6.6$ $-23.0$ $-8.8$ $24.9$ $-29.1$ $-17.2$ $24.7$ $-40.4$ $-21.6$ $46.3$ $-51.2$ $-17.2$ $24.7$ $-40.4$ $-21.6$ $46.3$ $-51.2$ $-17.2$ $24.7$ $-40.4$ $-21.6$ $46.3$ $-51.2$ $-17.2$ $24.7$ $-10.7$ $-10.7$ $-20.3$ $-17.2$ $-17.2$ $-1.2$ $1.7$ $-2.8$ $-17.2$ $-10.2$ $-1.2$ $1.7$ $-2.03$ $-17.2$ $-17.2$ $-1.2$ $1.7$ $-2.8$ $-17.2$ $-10.2$ $-1.2$ $-1.7$ $-2.8$ $-17.2$ $-10.2$ $-1.2$ $-1.7$ $-2.8$ $-17.2$ $-10.2$ $-1.2$ $-1.7$ $-2.03$ $-12.3$ $-10.2$ $-1.2$ $-1.7$ $-2.03$ $-12.3$ $-10.2$ $-10.2$ $-20.3$ $-12.4$ $-10.8$ $-10.4$ $-10.4$ $-12.4$ $-10.4$ $-10.4$ $-10.4$ $-12.4$ $-10.4$ $-10.4$ $-10.4$ $-12.4$ $-10.2$ $-10.2$ $-10.4$  | 110 1 -10.5 8.2   |        | 8.2   |              | 13.5 | -38.1 | -6.7        | 32.0 | -10.0 | 7.2         | 12.4 | -41.2 | -2.9        | 34.1 |
| 6.3         32.9         -14.7         1.7         8.3         -70.4           -         -         -         0.0         3.0         1.7         5.3           -         -         -         0.0         3.0         1.7         5.3           -         -         -         0.0         -3.0         1.7         5.3           -         -         -         0.0         -3.0         1.7         5.3           -         -4.6         6.6         -23.0         -8.8         24.9         -29.1           -         -17.2         24.7         -40.4         -21.6         46.3         -51.2         -           -         -         -         45.3         13.1         44.9         14.4         -           -         -         -         -         45.3         13.1         44.9         14.4           -   | 110 1 -2.3 -12.2  |        | -12.2 |              | 12.5 | 5.4   | -5.8        | 6.5  | 14.6  | -19.6       | 24.7 | 4.5   | -4.7        | 5.4  |
| ·         ·         ·         0.0         3.0         1.7         ·5.3           ·         ·         ·         0.0         ·3.0         1.7         ·5.3           ·         ·         ·         0.0         ·3.0         1.7         ·5.3           ·         ·         ·         ·         ·         ·         ·         ·           ·         ·         ·         ·         ·         ·         ·         ·         ·           · <td< td=""><td>110 1 -9.6 0.3</td><td></td><td>0.3</td><td></td><td>5.4</td><td>-68.8</td><td>6.3</td><td>32.9</td><td>-14.7</td><td>1.7</td><td>8.3</td><td>-70.4</td><td>5.4</td><td>33.6</td></td<>   | 110 1 -9.6 0.3    |        | 0.3   |              | 5.4  | -68.8 | 6.3         | 32.9 | -14.7 | 1.7         | 8.3  | -70.4 | 5.4         | 33.6 |
|   | 110 1             |        |       |              | ı    | ı     | ı           | ·    | 0.0   | 3.0         | 1.7  | -5.3  | -6.4        | 4.0  |
| -4.6 $6.6$ $-23.0$ $-8.8$ $24.9$ $-29.1$ $-17.2$ $24.7$ $-40.4$ $-21.6$ $46.3$ $-51.2$ $ -17.2$ $24.7$ $-40.4$ $-21.6$ $46.3$ $-51.2$ $ -0.8$ $3.7$ $-3.2$ $13.1$ $44.9$ $14.4$ $ -0.8$ $3.7$ $-3.2$ $-1.2$ $1.7$ $-2.8$ $ 10.8$ $3.7$ $-3.2$ $-1.2$ $1.7$ $-2.8$ $-2.8$ $12.3$ $10.0$ $0.0$ $-0.4$ $0.2$ $-20.3$ $-2.0.3$ $12.3$ $10.0$ $0.0$ $-1.3.5$ $19.1$ $-2.0.3$ $-2.0.3$ $-8.4$ $19.8$ $-23.1$ $-13.5$ $19.1$ $-9.0$ $-0.03$ $-0.7$ $5.9$ $16.2$ $0.5$ $16.3$ $26.4$ $-26.4$  | 110 1             |        |       |              |      |       |             |      | 0.0   | -3.0        | 1.7  | 5.3   | 6.4         | 4.0  |
| -17.2         24.7         -40.4         -21.6         46.3         -51.2         -           -         -         -         45.3         13.1         44.9         14.4           -         -0.8         3.7         -3.2         -1.2         1.7         -2.8           10.8         3.7         -3.2         -1.2         1.7         -2.8         14.4           12.3         10.0         0.0         -0.4         0.2         -20.3         1           -8.4         19.8         -23.1         -13.5         19.1         -9.0         1           -6.2         12.4         5.1         3.5         4.4         8.8         1           -6.7         5.9         16.2         16.3         56.4         1         1   | 110 1 -6.8 -8.3   |        | -8.3  |              | 10.8 | -6.6  | -4.6        | 6.6  | -23.0 | -8.8        | 24.9 | -29.1 | -1.0        | 24.1 |
| ·         ·         ·         45.3         13.1         44.9         14.4           ·0.8         3.7         ·3.2         ·1.2         1.7         ·2.8           10.8         3.7         ·3.2         ·1.2         1.7         ·2.8           12.3         10.0         0.0         ·0.4         0.2         ·20.3           •8.4         19.8         ·23.1         ·13.5         19.1         ·9.0           6.2         12.4         5.1         3.5         4.4         8.8           ·0.7         5.9         16.2         0.5         26.4         56.4   | 110 1 -21.7 -20.2 |        | -20.2 |              | 29.9 | -24.4 | -17.2       | 24.7 | -40.4 | -21.6       | 46.3 | -51.2 | -24.1       | 46.7 |
| -0.8         3.7         -3.2         -1.2         1.7         -2.8           12.3         10.0         0.0         -0.4         0.2         -20.3           -8.4         19.8         -23.1         -13.5         19.1         -9.0           6.2         12.4         5.1         3.5         4.4         8.8           -0.7         5.9         16.2         0.5         16.4         8.8  | 110 1             |        | ı     |              | ı    | ·     | ı           |      | 45.3  | 13.1        | 44.9 | 14.4  | 4.3         | 12.2 |
| 12.3         10.0         0.0         -0.4         0.2         -20.3           -8.4         19.8         -23.1         -13.5         19.1         -9.0           6.2         12.4         5.1         3.5         4.4         8.8           -0.7         5.9         16.2         0.5         16.3         26.4   | 110 1 -7.5 -4.0   |        | -4.0  |              | 4.3  | -8.1  | -0.8        | 3.7  | -3.2  | -1.2        | 1.7  | -2.8  | -2.7        | 1.8  |
| -8.4         19.8         -23.1         -13.5         19.1         -9.0           6.2         12.4         5.1         3.5         4.4         8.8           -0.7         5.9         16.2         0.5         16.3         26.4  | 110 1 0.0 -0.4    |        | -0.4  |              | 0.2  | -17.9 | 12.3        | 10.0 | 0.0   | -0.4        | 0.2  | -20.3 | 10.5        | 10.5 |
| 6.2         12.4         5.1         3.5         4.4         8.8           -0.7         5.9         16.2         0.5         16.3         26.4  | 110 1 -17.4 -2.9  |        | -2.9  |              | 12.6 | -26.3 | -8.4        | 19.8 | -23.1 | -13.5       | 19.1 | -9.0  | -3.2        | 6.8  |
| -0.7 5.9 16.2 0.5 16.3 26.4   | 110 1 7.2 0.7     |        | 0.7   |              | 5.2  | 16.2  | 6.2         | 12.4 | 5.1   | 3.5         | 4.4  | 8.8   | 2.3         | 6.5  |
|   | 110 1 8.6 0.0     |        | 0.0   |              | 8.7  | -7.1  | -0.7        | 5.9  | 16.2  | 0.5         | 16.3 | 26.4  | -1.1        | 21.8 |
| 8.3 0.5 4.7 -29.6 -0  | 110 1             |        | '     |              | ı    | 1     | ı           |      | -8.3  | 0.5         | 4.7  | -29.6 | -0.3        | 14.1 |

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|      |               | %    | 2.9  | 29.4  | 22.1  | 7.7   | 12.1    | 14.0  | 20.3 | 34.4  | 34.4  | 28.1  | 23.3  | 17.3  | 12.0  | 34.7 | 18.8  | 11.2  | 5.1  | 10.0  | 59.8    | 31.6    | 59.8    | 20.2    | 19.8    | 25.1    | 3.8     | 57.8 |
|------|---------------|------|------|-------|-------|-------|---------|-------|------|-------|-------|-------|-------|-------|-------|------|-------|-------|------|-------|---------|---------|---------|---------|---------|---------|---------|------|
|      | Winter Peak   | MVAR | 1.4  | -11.2 | 8.4   | 2.8   | -15.3   | -0.6  | 5.7  | -29.0 | -29.0 | -13.1 | -10.9 | 9.7   | 6.8   | -3.5 | -9.0  | -6.5  | -0.2 | -2.6  | -5.0    | 4.9     | 22.4    | -16.0   | -4.6    | 6.4     | 1.7     | 14.0 |
| 2029 |               | MW   | 3.2  | 34.4  | -25.4 | 0.6-  | -21.6   | 29.3  | 31.7 | -71.0 | -71.0 | -31.9 | 11.5  | -18.6 | -24.3 | 42.6 | -18.0 | -14.3 | -7.1 | -10.3 | 71.0    | 37.3    | 70.1    | 18.0    | 25.5    | 28.1    | 4.4     | 75.1 |
| 20   | ey            | %    | 8.0  | 17.4  | 0.2   | 16.9  | 15.0    | 12.5  | 9.3  | 41.1  | 41.1  | 4.2   | 17.4  | 8.2   | 7.7   | 15.4 | 2.8   | 1.5   | 1.3  | 2.3   | 15.5    | 7.3     | 8.8     | 25.8    | 26.6    | 5.9     | 1.0     | 0.6  |
|      | Summer Valley | MVAR | -1.0 | -16.6 | -0.2  | 16.8  | -29.3   | -11.7 | -1.1 | -29.3 | -29.3 | -1.4  | 3.0   | 0.8   | 4.4   | -4.0 | -1.2  | 1.4   | -0.2 | -1.2  | -15.7   | -3.1    | -2.6    | -9.7    | -0.5    | -5.0    | 0.2     | -1.1 |
|      | Sı            | MM   | -7.9 | 4.6   | 0.0   | -4.6  | 0.0     | 19.0  | 12.6 | -71.1 | -71.1 | -4.1  | 11.4  | -8.0  | -13.0 | 14.7 | -2.8  | -1.7  | -1.8 | -2.2  | 9.7     | 4.9     | 8.9     | 29.1    | 31.9    | 3.7     | 1.3     | 11.0 |
|      |               | %    | 5.9  | 32.1  | 22.9  | 9.7   | 11.3    | 12.7  | 17.3 | 0.4   |       | 26.4  | 23.2  | 14.2  | 17.3  | 20.9 | 17.9  | 10.7  | 4.8  | 9.4   | 56.5    | 29.8    | 56.1    | 39.3    | 37.1    | 23.5    |         | 54.5 |
|      | Winter Peak   | MVAR | 0.7  | -13.4 | 11.2  | 2.2   | -12.3   | -1.8  | 5.7  | -1.0  |       | -12.1 | -10.9 | 8.4   | 2.8   | -4.2 | -8.8  | -6.4  | -0.1 | -2.5  | -6.1    | 4.2     | 20.3    | -12.8   | -3.6    | 5.4     |         | 12.7 |
| 20   |               | MM   | 7.1  | 37.1  | -25.4 | -11.8 | -21.6   | 26.5  | 27.0 | 0.0   |       | -30.1 | 11.5  | -15.0 | 12.9  | 25.3 | -17.0 | -13.5 | -6.7 | -9.7  | 67.0    | 35.2    | 66.0    | 45.0    | 48.5    | 26.5    | -       | 70.8 |
| 2020 | ey l          | %    | 4.0  | 8.5   | 0.2   | 8.2   | 15.5    | 9.3   | 3.3  | 0.5   |       | 6.7   | 17.4  | 2.6   | 5.8   | 4.4  | 4.4   | 2.1   | 2.1  | 3.6   | 17.9    | 10.2    | 13.6    | 25.3    | 21.9    | 6.9     | -       | 14.3 |
|      | Summer Valley | MVAR | -2.4 | 0.1   | -0.2  | 0.1   | -30.1   | -10.6 | 1.2  | -0.8  | -     | -2.3  | 3.0   | -2.6  | 0.0   | -0.4 | -1.4  | 1.2   | -0-5 | -1.7  | -14.6   | -2.4    | -0.9    | -21.8   | -11.3   | -4.3    | -       | -0-5 |
|      | Sı            | MM   | 3.1  | 8.4   | 0.0   | -8.4  | 0.0     | 12.6  | 4.3  | 0.0   | -     | -6.6  | 11.4  | 0.3   | 4.4   | 4.3  | -4.5  | -2.7  | -2.9 | -3.5  | 15.6    | 7.8     | 14.3    | 20.8    | 23.8    | 5.9     | -       | 17.7 |
|      |               | .oN  | T    | 1     | T     | T     | 1       | 1     | 1    | 1     | 2     | 1     | 1     | T     | 1     | 1    | T     | T     | 1    | T     | 1       | 1       | 1       | T       | 1       | 1       | 1       | 1    |
|      | LINE          | k٧   | 110  | 110   | 110   | 110   | 110     | 110   | 110  | 110   | 110   | 110   | 110   | 110   | 110   | 110  | 110   | 110   | 110  | 110   | 110     | 110     | 110     | 110     | 110     | 110     | 110     | 110  |
| :    |               | To   | TSB  | LET   | MEE   | CLO   | SLC     | THU   | TSB  | CBT   | CBT   | CKM   | GIL   | SLI   | TON   | SLB  | HAR   | TRN   | HEU  | INC   | MCD     | PTN     | GLA     | GRA     | POP     | SVN     | MCE     | CO 0 |
|      |               | From | DER  | DRM   | DRM   | DRM   | ENN (I) | KHL   | MLC  | CKG   | CKG   | FAS   | FLA   | FLA   | FLA   | FLA  | FRA   | FRA   | FRA  | FRA   | FIN (I) | FTT  |

|      |         |      |     |       |               | 20   | 2020  |             |      |       |               | 2029 | 29    |             |      |
|------|---------|------|-----|-------|---------------|------|-------|-------------|------|-------|---------------|------|-------|-------------|------|
|      |         | Line |     | S     | Summer Vallev | ∧ä   |       | Winter Peak |      | S     | Summer Vallev | ۸.   |       | Winter Peak |      |
| From | To      | ş    | No. | MM    | MVAR          | %    | MM    | MVAR        | %    | MM    | MVAR          | %    | MM    | MVAR        | %    |
| GLA  | SVN     | 110  | 1   | -1.6  | -5.5          | 4.2  | 2.7-  | -9.0        | 2.7  | -1.0  | -5.2          | 3.9  | -8.2  | -9.3        | 8.0  |
| GI   | ККҮ     | 110  | 1   | 14.8  | -12.0         | 19.2 | 60.4  | -13.6       | 51.2 | 29.3  | -8.8          | 17.2 | 62.6  | -5.2        | 29.9 |
| GI   | WAT     | 110  | 1   | 9.7   | -2.7          | 5.7  | 3.1   | 14.4        | 7.0  | -2.7  | -1.3          | 1.7  | 3.6   | 12.6        | 6.3  |
| GI   | WAT     | 110  | 2   | 8.8   | -2.5          | 5.2  | 2.8   | 13.0        | 6.3  | -2.4  | -1.2          | 1.5  | 3.3   | 11.4        | 5.6  |
| GI   | RSP     | 110  | 1   |       | -             | -    | -     | -           | -    | 22.8  | -7.4          | 13.5 | 40.2  | 0.7-        | 19.4 |
| GRA  | NBY     | 110  | 1   | 8.1   | 1.2           | 6.9  | -9.4  | -8.4        | 10.5 | 9.6   | -0.1          | 8.0  | -3.6  | -6.4        | 6.1  |
| GRO  | CKN     | 110  | 1   | 0.0   | -18.8         | 15.7 | -34.7 | 8.0         | 29.7 | 0.0   | -17.6         | 14.6 | -34.7 | 8.0         | 29.7 |
| GAL  | SAL     | 110  | 1   | 13.0  | -28.7         | 31.8 | 46.3  | -8.3        | 44.4 | 7.8   | -29.8         | 31.1 | 20.8  | -18.5       | 26.3 |
| GAN  | MUC     | 110  | 1   |       | '             |      |       | ·           |      | -20.0 | -5.7          | 11.7 | 13.5  | 12.7        | 8.8  |
| GOL  | GL T    | 110  | 1   | 0.0   | -0.2          | 0.1  | 4.5   | -3.2        | 4.5  | 0.0   | -0.2          | 0.1  | 4.5   | 0.2         | 3.7  |
| GOR  | MTH     | 110  | 1   | -12.0 | -1.1          | 12.1 | 2.1   | 7.3         | 6.3  | -21.0 | -1.1          | 21.3 | -11.9 | 9.7         | 12.7 |
| GOR  | NAV     | 110  | 1   | 12.8  | -10.7         | 16.8 | 25.1  | -1.6        | 20.8 | 4.7   | -9.4          | 10.6 | 21.9  | -1.0        | 18.1 |
| GOR  | NAV     | 110  | 2   | 11.2  | -9.1          | 14.6 | 21.7  | -1.2        | 18.0 | 4.2   | -8.1          | 9.2  | 19.0  | -0.7        | 15.7 |
| GOR  | NAV     | 110  | Э   | 15.6  | -11.0         | 19.2 | 28.5  | 0.6         | 23.5 | 6.3   | -10.4         | 12.3 | 24.8  | 0.9         | 20.6 |
| GOR  | PLA     | 110  | 1   | 10.6  | 9.5           | 14.4 | 2.8   | 2.8         | 3.3  | 30.2  | 10.5          | 32.2 | 27.5  | 0.3         | 22.7 |
| GOR  | GOR (I) | 110  | 1   |       | -             | -    |       |             |      | 0.0   | -0.6          | 0.3  | 0.0   | -0.6        | 0.3  |
| GCA  | INC     | 110  | 1   | -26.6 | -4.5          | 26.1 | -38.1 | -7.5        | 29.0 | -11.1 | -7.9          | 13.3 | -18.0 | -12.8       | 16.5 |
| GCA  | INC     | 110  | 7   | -26.6 | -4.5          | 26.1 | -38.1 | -7.5        | 29.0 | -11.1 | 6.7-          | 13.3 | -18.0 | -12.8       | 16.5 |
| GCA  | INC     | 110  | £   |       | ı             |      | ı     | ı           | ı    | -53.6 | -9.1          | 43.8 | -87.0 | -13.1       | 70.9 |
| GCA  | NAN     | 110  | 1   | 5.4   | 0.3           | 4.5  | 3.5   | 0.4         | 2.7  | 5.4   | 0.3           | 4.5  | 3.5   | 0.4         | 2.7  |
| GCA  | NAN     | 110  | 2   | 5.7   | 0.5           | 4.8  | 3.6   | 0.5         | 2.8  | 5.7   | 0.5           | 4.8  | 3.6   | 0.5         | 2.8  |
| CLO  | MRY     | 110  | 1   | 0.0   | -10.4         | 7.6  | -38.3 | 24.0        | 33.2 | 0.0   | -10.5         | 7.7  | -38.4 | 0.1         | 28.2 |
| CLO  | CF      | 110  | 1   | -10.1 | 14.8          | 10.1 | 7.8   | -0.2        | 3.7  | -8.2  | 31.5          | 18.3 | 32.9  | -6.8        | 16.1 |
| CLO  | GLT     | 110  | 1   | 7.5   | -1.6          | 4.1  | 11.4  | -2.4        | 5.4  | 4.1   | -16.3         | 9.0  | 8.9   | -5.8        | 4.9  |
| NWH  | KIN     | 110  | 1   | ·     |               | ı    | I     | ı           | ı    | -14.4 | -3.0          | 10.8 | -0.7  | -1.2        | 1.0  |
| NWH  | DFR     | 110  | 1   |       | -             |      |       |             |      | 14.4  | 3.0           | 14.2 | 0.7   | 1.2         | 0.9  |

| From To<br>HAR RE |        |     |       |               |      |       |             |      |       |               |      |       |             |      |
|-------------------|--------|-----|-------|---------------|------|-------|-------------|------|-------|---------------|------|-------|-------------|------|
|                   | LINE   |     | St    | Summer Valley | ĥ    |       | Winter Peak |      | S     | Summer Valley | ey   |       | Winter Peak |      |
|                   | kV     | No. | MW    | MVAR          | %    | MM    | MVAR        | %    | MW    | MVAR          | %    | MM    | MVAR        | %    |
|                   | 110    | 1   | -8.2  | 0.5           | 2.7  | -34.7 | -11.3       | 34.1 | -5.1  | 1.1           | 4.9  | -36.8 | -12.0       | 36.1 |
| HEU INC           | 110    | 1   | -4.3  | 1.5           | 3.2  | -12.9 | 0.5         | 9.2  | -2.6  | 2.0           | 2.4  | -13.7 | 0.3         | 9.8  |
| IA MAC            | 110    | 1   | -0.8  | -14.7         | 5.7  | -17.0 | 0.4         | 7.8  | 15.4  | -10.2         | 9.4  | -12.0 | -1.7        | 5.6  |
| INC MIL           | 110    | 1   | 9.2   | -5.1          | 8.8  | 39.3  | -1.1        | 30.0 | 5.8   | -5.1          | 6.4  | 41.7  | -0.5        | 31.8 |
| IKE IKE T         | Γ 110  | 1   | -5.7  | -0.1          | 7.1  | -20.9 | -12.7       | 20.6 | -3.6  | 0.1           | 4.4  | -22.8 | -13.6       | 22.3 |
| KNR KPG           | 110    | 1   | -11.4 | 2.6           | 8.6  | -17.3 | -14.9       | 14.3 | -3.2  | 2.2           | 2.9  | -12.0 | -9.7        | 9.7  |
| KNR TRI           | 110    | 2   | 11.4  | -2.6          | 11.8 | 17.3  | 14.9        | 18.8 | 3.2   | -2.2          | 3.9  | 12.0  | 9.7         | 12.8 |
| KNR TRI           | 110    | 1   | 0.0   | -17.0         | 9.6  | -41.7 | 5.5         | 20.1 | 0.0   | -16.6         | 9.3  | -43.7 | 8.4         | 21.3 |
| KRA MEN           | 110    | 1   |       | -             |      |       |             | -    | 0.0   | -3.5          | 2.8  | 0.0   | -3.8        | 3.1  |
| KRA KBY           | , 110  | 1   | 15.1  | -10.3         | 10.3 | 32.4  | 16.5        | 17.3 | 8.9   | -4.5          | 5.6  | 36.9  | 18.4        | 19.6 |
| KRA BAR T         | T 110  | 1   | 26.7  | -9.9          | 20.9 | 72.0  | -11.0       | 45.8 | 28.2  | -10.7         | 22.2 | 75.3  | -12.7       | 48.0 |
| KRA MID           | 110    | 1   | 4.0   | 8.5           | 9.5  | 9.1   | 9.4         | 10.8 | 0.8   | 6.3           | 6.4  | 6.7   | 10.4        | 10.8 |
| KRA WHO           | 0 110  | 1   | 9.6   | -2.0          | 5.5  | 53.5  | -2.3        | 25.5 | 14.8  | -4.7          | 8.7  | 55.2  | -1.5        | 26.3 |
| KRA KBY           | 110    | 2   | 10.7  | -11.2         | 15.7 | 29.8  | 7.9         | 25.5 | 6.6   | -5.4          | 8.6  | 33.9  | 8.6         | 28.9 |
| KTL MAY           | / 110  | 1   | -17.5 | 4.5           | 18.3 | -61.2 | 3.8         | 50.7 | -4.4  | 1.3           | 4.6  | -48.6 | 5.7         | 40.5 |
| KTL MON           | V 110  | 1   | 6.3   | -6.5          | 6.7  | 9.8   | 12.3        | 9.9  | -2.6  | -2.5          | 2.6  | -1.5  | 9.3         | 5.9  |
| REM TRL           | 110    | 1   | 0.0   | 3.0           | 2.4  | 17.3  | -0.3        | 12.3 | 0.0   | 3.0           | 2.4  | 28.9  | -2.3        | 20.5 |
| KKY KLS           | 110    | 1   | 1.7   | -11.7         | 11.9 | -9.6  | -9.7        | 11.3 | -2.3  | -2.4          | 3.3  | -17.3 | 6.0-        | 14.3 |
| KLN LIM (I)       | () 110 | 1   | 9.3   | 17.2          | 19.7 | 26.3  | 14.1        | 24.7 | -0.3  | 11.4          | 11.5 | 32.0  | 8.5         | 27.3 |
| KLN CUR           | 110    | 1   | 7.9   | -28.7         | 21.9 | -23.4 | 13.8        | 17.1 | 5.0   | -28.4         | 21.2 | -22.1 | 4.0         | 14.2 |
| KLN SNG           | 110    | 1   | 21.2  | -1.1          | 11.9 | 45.2  | 8.1         | 22.0 | -18.2 | 4.0           | 10.5 | 51.2  | -8.0        | 24.8 |
| KER OUG T         | T 110  | 1   | 5.0   | -5.6          | 4.2  | 18.4  | -10.1       | 10.0 | 15.1  | -9.4          | 10.0 | 22.6  | -11.4       | 12.1 |
| KUR NAV           | 110    | 1   | -23.7 | -13.0         | 27.3 | -23.7 | -12.9       | 21.9 | -23.7 | -13.0         | 27.3 | -23.7 | -12.9       | 21.9 |
| BYH GLE           | 110    | 1   | 0.1   | -41.0         | 33.0 | -38.9 | 1.8         | 31.4 | 0.1   | -35.6         | 28.7 | -38.9 | 1.1         | 31.4 |
| KIN MUL           | - 110  | 1   | -0.8  | -5.6          | 3.2  | 0.5   | -5.5        | 2.6  | -8.5  | -4.7          | 5.5  | 15.4  | -4.5        | 7.7  |
| KCR GLE           | 110    | 1   | 0.0   | -14.7         | 12.0 | 31.0  | -39.1       | 40.9 | 0.0   | -12.6         | 10.3 | 31.0  | -39.0       | 40.9 |

|      |               | %    | 10.7  | 1.1  | 1.1  | 32.3 | 3.8   | 25.7  | 12.8    | 7.0  | 0.5  | 16.2 | 16.2 | 32.7  | 14.7 | 18.4 | 48.1  | 34.0 | 7.6   | 20.9    | 3.2     | 23.5    | 46.3  | 10.3  | 12.9  | 7.4  | 7.4   | 2.5  |
|------|---------------|------|-------|------|------|------|-------|-------|---------|------|------|------|------|-------|------|------|-------|------|-------|---------|---------|---------|-------|-------|-------|------|-------|------|
|      | Winter Peak   | MVAR | -9.3  | -1.5 | -1.5 | 8.0  | 4.0   | -22.5 | 7.1     | 4.8  | -0.9 | 13.4 | 13.4 | -19.7 | 4.5  | 5.8  | 5.3   | 22.1 | 7.1   | 16.2    | -2.0    | -7.0    | -0.5  | 9.8   | 12.1  | -6.5 | 6.5   | 4.0  |
| 2029 | ^             | MM   | -9.0  | 0.0  | 0.0  | 37.6 | -2.9  | -52.8 | 19.0    | 6.9  | 0.0  | 33.6 | 33.6 | 34.3  | 17.5 | 21.8 | -58.9 | 34.6 | -4.8  | -40.8   | 3.3     | -24.9   | 97.2  | -8.1  | -10.3 | 14.2 | -14.2 | -0.4 |
| 20   | ey            | %    | 2.8   | 1.0  | 1.0  | 20.7 | 24.3  | 30.7  | 4.5     | 3.4  | 0.6  | 16.6 | 16.6 | 33.0  | 2.3  | 2.9  | 15.1  | 4.9  | 8.0   | 22.0    | 15.7    | 11.8    | 29.2  | 7.0   | 7.2   | 6.6  | 6.6   | 8.7  |
|      | Summer Valley | MVAR | -1.7  | -1.4 | -1.4 | 3.0  | -5.5  | -22.7 | 6.0     | -3.3 | -0.8 | 11.6 | 11.6 | 2.7   | -0.6 | -0.6 | 3.2   | 4.1  | -7.4  | 36.1    | -7.0    | -9.4    | -11.3 | -6.8  | 6.6   | 3.8  | -3.8  | 11.7 |
|      | Sı            | MW   | 2.2   | 0.0  | 0.0  | 24.4 | -28.7 | -52.8 | -1.6    | -0.6 | 0.0  | 28.8 | 28.8 | 32.6  | 2.2  | 2.8  | -14.6 | 2.7  | -2.0  | -15.2   | 13.9    | 0.3     | 50.8  | -1.6  | -2.7  | 11.0 | -11.0 | -1.8 |
|      |               | %    | 11.2  | 1.1  | 1.1  | 37.4 | 20.8  |       | 12.0    | 11.0 | ı    |      |      | 28.2  | 13.9 | 17.3 | 34.6  | 33.6 | 5.6   | 22.1    | 3.7     | 21.4    |       | 4.5   | 9.9   | 20.2 | 20.2  | 3.1  |
|      | Winter Peak   | MVAR | -10.6 | -1.5 | -1.5 | 10.1 | 2.7   | ı     | 7.4     | 5.6  | ı    |      |      | -15.4 | 4.2  | 5.4  | 4.6   | 15.4 | 6.2   | 19.7    | -2.7    | -11.5   |       | 2.6   | 2.6   | -0.5 | 0.5   | 4.8  |
| 2020 |               | MW   | -8.4  | 0.0  | 0.0  | 43.4 | -27.2 |       | 17.6    | 12.0 | -    | -    | -    | 30.4  | 16.6 | 20.6 | -42.3 | 37.6 | 1.3   | -42.0   | -3.6    | -20.5   | -     | -4.9  | -11.9 | 42.3 | -42.3 | -1.4 |
| 20   | ey            | %    | 6.3   | 1.0  | 1.0  | 21.8 | 16.2  |       | 12.2    | 7.3  |      |      |      | 14.6  | 3.7  | 4.5  | 4.4   | 8.8  | 18.7  | 30.4    | 3.3     | 19.7    |       | 12.1  | 16.1  |      |       | 1.7  |
|      | Summer Valley | MVAR | -0.8  | -1.4 | -1.4 | 1.5  | 5.3   |       | 1.6     | -4.8 |      |      |      | 8.3   | -0.5 | -0.4 | -0.7  | 5.2  | -11.3 | 50.4    | -1.3    | -14.0   |       | -10.4 | 9.5   |      |       | 1.9  |
|      | S             | MM   | -6.2  | 0.0  | 0.0  | 25.9 | -18.6 |       | 16.5    | 5.4  |      |      |      | 11.8  | 3.6  | 4.5  | -4.3  | 7.0  | 13.7  | -19.6   | 3.0     | -7.3    |       | 5.9   | -12.8 |      |       | -1.1 |
|      |               | No.  | 1     | 2    | 1    | 1    | 1     | 1     | 1       | 1    | 1    | 1    | 2    | 1     | 1    | 2    | 1     | 1    | 1     | 1       | 1       | 2       | 1     | 1     | 1     | 1    | 1     | 1    |
|      | ы             | kV   | 110   | 110  | 110  | 110  | 110   | 110   | 110     | 110  | 110  | 110  | 110  | 110   | 110  | 110  | 110   | 110  | 110   | 110     | 110     | 110     | 110   | 110   | 110   | 110  | 110   | 110  |
| -    | 2             | To   | WAT   | CRM  | CRM  | NBY  | РОР   | CBT   | RAT (I) | TRL  | СН   | ВКҮ  | ВКҮ  | MUL   | RIC  | RIC  | SLB   | MLN  | RRU   | MTN     | RAT (I) | KLN     | PLS   | SKL   | LOU   | PLS  | DAL   | TIV  |
|      |               | From | KTN   | KLM  | KLM  | KLM  | KLM   | KUD   | KPG     | KPG  | KPG  | CBT  | CBT  | ΓA    | ΓA   | ΓA   | LA    | LOU  | LOU   | (I) WIT | (I) WIT | (I) WIT | CNB   | LIS   | LIS   | LUM  | LUM   | LET  |

|      | line    | a   |     |       |               | 2020 | 20    |             |      |       |               | 2029 | 29    |             |      |
|------|---------|-----|-----|-------|---------------|------|-------|-------------|------|-------|---------------|------|-------|-------------|------|
|      |         | ,   |     | S     | Summer Valley | ٨i   |       | Winter Peak |      | S     | Summer Valley | ey   |       | Winter Peak |      |
| From | To      | kv  | No. | MM    | MVAR          | %    | MW    | MVAR        | %    | MM    | MVAR          | %    | MM    | MVAR        | %    |
| LET  | TLK     | 110 | 1   | 4.3   | -2.1          | 4.6  | -10.8 | 4.7         | 9.6  | 2.7   | -2.9          | 3.7  | -11.0 | 4.3         | 9.6  |
| LET  | GLT     | 110 | 1   | -7.5  | -0.1          | 7.6  | -15.8 | 4.2         | 13.5 | -4.0  | 14.8          | 15.4 | -13.3 | 4.2         | 11.5 |
| LET  | STR (N) | 110 | 1   | 0.1   | -1.5          | 1.5  | 1.6   | -1.0        | 1.6  | £•0-  | -4.7          | 4.7  | 1.2   | -0.1        | 0.9  |
| LIB  | MR      | 110 | 1   | -3.8  | -0.8          | 5.7  | -14.5 | -5.0        | 22.6 | -2.4  | -0-5          | 3.5  | -15.4 | -5.3        | 23.9 |
| LIB  | MR      | 110 | 2   | -1.9  | -0.5          | 2.0  | -7.0  | 0.4         | 5.9  | -1.2  | -0.3          | 1.2  | -7.5  | 0.3         | 6.3  |
| LSN  | THU     | 110 | 1   | 0.0   | -0.4          | 0.4  | 29.8  | -6.6        | 25.0 | 0.0   | -0.4          | 0.4  | 29.8  | -3.5        | 24.6 |
| CUR  | NEN     | 110 | 1   | 7.8   | 6.0           | 7.5  | 18.4  | 8.3         | 16.4 | 4.9   | 6.0           | 4.7  | 19.8  | 8.9         | 17.6 |
| CUR  | BKM     | 110 | 1   | 0.0   | -29.4         | 15.5 | -42.0 | 5.8         | 22.3 | 0.0   | -28.5         | 15.0 | -42.0 | -4.5        | 22.2 |
| MHL  | RE      | 110 | 1   | -15.3 | 3.9           | 11.3 | -60.6 | -12.9       | 44.3 | -9.6  | 4.8           | 7.6  | -64.3 | -14.2       | 47.0 |
| MHL  | TRN     | 110 | 1   | 7.7   | -4.6          | 6.4  | 36.3  | 7.5         | 26.5 | 4.8   | -5.1          | 5.0  | 38.5  | 8.2         | 28.1 |
| MCE  | CDU     | 110 | 1   | -8.7  | -0٠           | 8.9  | -22.6 | -6.4        | 19.0 | -8.2  | 0.7           | 8.4  | -31.4 | -7.4        | 26.0 |
| MCD  | MOL     | 110 | 1   | 5.7   | 1.4           | 4.9  | 25.0  | 7.5         | 20.0 | 3.5   | 0.6           | 2.9  | 26.5  | 8.1         | 21.2 |
| MID  | MHI     | 110 | 1   | -10.4 | 6.1           | 12.2 | -33.3 | -1.0        | 27.5 | -8.3  | 5.2           | 9.9  | -35.9 | -0.6        | 29.7 |
| MTH  | LOU     | 110 | 1   | -24.2 | -2.3          | 24.5 | -41.8 | -14.1       | 36.5 | -28.7 | -1.5          | 29.1 | -49.8 | -15.2       | 43.0 |
| MAY  | MIT     | 110 | 1   |       |               |      |       | 1           |      | 8.3   | -2.2          | 7.7  | 9.1   | £•0-        | 8.1  |
| MAY  | GRI     | 110 | 1   | 6.3   | 2.1           | 6.7  | 29.1  | 2.8         | 24.7 | 2.0   | 0.5           | 2.0  | 28.8  | 9.9         | 24.6 |
| MAY  | GRI     | 110 | 1   | 6.3   | 2.1           | 6.7  | 29.1  | 5.8         | 24.7 | 2.0   | 0.5           | 2.0  | 29.1  | 6.3         | 24.2 |
| MAY  | RYB     | 110 | 1   | 63.4  | 32.4          | 40.0 | 68.2  | 28.7        | 33.8 | 86.4  | 30.4          | 51.4 | 95.0  | 23.4        | 44.7 |
| MAY  | RNW     | 110 | 1   | 12.2  | -3.7          | 15.9 | 37.6  | -0.6        | 36.5 | -3.9  | -2.7          | 5.9  | 18.3  | 0.4         | 17.8 |
| MAY  | BLKT    | 110 | 1   | 1.5   | -7.3          | 7.5  | 35.8  | 1.2         | 29.6 | -26.2 | -2.4          | 26.6 | 0.8   | 4.2         | 3.5  |
| MIL  | RE      | 110 | 1   | -4.3  | 7.0-          | 4.4  | -19.5 | -5.5        | 20.3 | -2.7  | -0.7          | 2.7  | -20.7 | -5.9        | 21.5 |
| MIL  | RE      | 110 | 2   | -3.5  | 0.5           | 3.0  | -15.2 | -3.9        | 12.0 | -2.2  | 0.5           | 1.9  | -16.1 | -4.3        | 12.7 |
| MAC  | CLA     | 110 | 2   | -6.6  | -24.0         | 15.5 | -27.7 | -6.4        | 14.8 | 16.6  | -13.4         | 13.2 | -18.7 | -9.6        | 11.0 |
| MTN  | MUN     | 110 | 1   | 10.8  | 6.6           | 28.0 | 10.8  | 6.6         | 28.0 | 10.8  | 6.6           | 28.0 | 10.8  | 6.6         | 28.0 |
| MTN  | MUN     | 110 | 2   | 10.8  | 6.6           | 28.0 | 10.8  | 6.6         | 28.0 | 10.8  | 6.6           | 28.1 | 10.8  | 6.6         | 28.0 |
| MP   | TBKT    | 110 | 1   | 16.1  | -3.2          | 9.2  | 14.9  | 12.8        | 9.4  | -2.8  | -0.8          | 1.6  | 9.2   | 11.4        | 7.0  |

| From     To       MR     TBG       MR     TBG       MR     TBG       MR     KBY |     |     |       |               |      |        |             |      |       |               |             |       |             |      |
|---|-----|-----|-------|---------------|------|--------|-------------|------|-------|---------------|-------------|-------|-------------|------|
|   | ۴۸  |     | Su    | Summer Valley | Ń    | 1      | Winter Peak |      | SI    | Summer Valley | ey          |       | Winter Peak |      |
|   | AN  | No. | MW    | MVAR          | %    | MM     | MVAR        | %    | MM    | MVAR          | %           | MM    | MVAR        | %    |
|   | 110 | 1   | -10.5 | 11.5          | 8.8  | -33.2  | -4.8        | 15.3 | -12.2 | 6.4           | 7.7         | -38.4 | -4.2        | 17.6 |
|   | 110 | 2   | -12.2 | 13.9          | 10.4 | -38.6  | -5.0        | 17.8 | -14.1 | 8.0           | 9.1         | -44.5 | -4.3        | 20.4 |
|   | 110 | 1   | 6.8   | -11.6         | 12.4 | 17.2   | 3.5         | 14.6 | 10.9  | -5.5          | 10.2        | 22.1  | 3.8         | 18.7 |
|   | 110 | 2   | 6.8   | -11.6         | 13.1 | 17.2   | 3.5         | 13.5 | 9.8   | -6.3          | 11.3        | 21.2  | 1.4         | 16.3 |
| MAL KBY   | 110 | 1   | -18.4 | 12.3          | 16.5 | -42.5  | -1.5        | 26.7 | -19.4 | 9.5           | 16.1        | -49.5 | -1.4        | 31.1 |
| MOY GLR   | 110 | 1   | 21.1  | -17.3         | 25.9 | 23.0   | -11.6       | 20.9 | 10.9  | -11.3         | 15.0        | 4.0   | -7.0        | 6.6  |
| MOY TAW   | 110 | 1   | 0.0   | -0.4          | 0.7  | -5.8   | 0.3         | 8.5  | 0.0   | <b>†</b> .0-  | <i>2</i> .0 | -5.8  | 6.0         | 8.5  |
| MOY TAW   | 110 | 2   | -39.6 | 25.5          | 69.3 | 2.962- | 25.6        | 69.4 | -39.6 | 25.4          | 69.3        | -39.7 | 25.3        | 69.2 |
| MOY TON   | 110 | 1   |       |               |      |        |             | -    | 16.0  | -6.1          | 9.6         | 38.2  | -3.3        | 18.2 |
| BCT CKM   | 110 | 1   | -45.1 | -14.0         | 33.7 | -46.7  | -14.1       | 34.8 | -49.0 | -16.3         | 36.9        | -50.8 | -16.5       | 38.1 |
| NEW (I) BLKT  | 110 | 1   | 2.4   | 5.4           | 4.3  | -24.3  | 0.9         | 15.3 | 29.0  | 1.7           | 21.4        | 11.1  | -3.3        | 7.3  |
| NQS RE  | 110 | 1   | -6.5  | -0.6          | 5.5  | -18.6  | -2.9        | 15.9 | -4.0  | -0.3          | 3.4         | -19.8 | -3.2        | 16.8 |
| OUG OUG T   | 110 | 1   | -7.2  | -0.8          | 6.9  | -24.2  | -5.9        | 20.3 | -4.5  | -0.4          | 4.3         | -24.6 | -6.2        | 20.6 |
| PA STR T  | 110 | 1   | 0.0   | -0.8          | 1.1  | 30.0   | -11.0       | 47.0 | 34.0  | -26.2         | 63.2        | 34.0  | -13.3       | 53.7 |
| PHY SHE   | 110 | 1   |       |               |      | ı      |             | ı    | 2.3   | 0.7           | 1.4         | 2.3   | 0.7         | 1.1  |
| PB RE   | 110 | 3   | 10.2  | -11.5         | 5.7  | 110.8  | -6.5        | 41.3 | -7.9  | -12.7         | 5.6         | 118.7 | -8.1        | 44.2 |
| PB RE   | 110 | 4   | 9.9   | -11.1         | 5.5  | 107.4  | -6.2        | 40.0 | -7.7  | -12.3         | 5.4         | 115.2 | -7.8        | 42.9 |
| PLA RMN   | 110 | 1   |       |               |      |        |             | ı    | -8.2  | -1.3          | 7.9         | 22.7  | 7.3         | 19.3 |
| PLA MUC   | 110 | 1   |       |               |      |        |             |      | 20.0  | 5.1           | 11.6        | -13.4 | -13.4       | 9.0  |
| RE WBK  | 110 | 1   | -50.9 | 28.0          | 46.5 | -59.9  | -30.9       | 47.8 | -59.9 | 28.9          | 53.2        | -60.9 | -40.0       | 51.7 |
| RE PB   | 110 | 1   | 0.0   | -1.6          | 3.6  | 0.0    | -1.8        | 4.0  | 0.0   | -1.6          | 3.6         | 0.0   | -1.8        | 4.0  |
| RAF TBG   | 110 | 1   | 21.6  | -18.3         | 14.5 | 71.5   | 4.8         | 3.3  | 19.7  | -12.3         | 11.9        | 78.5  | 4.9         | 3.6  |
| RAF RSY   | 110 | 1   | 0.7   | 0.0           | 1.2  | 4.1    | 0.4         | 4.5  | 0.5   | 0.0           | 0.7         | 4.4   | 0.5         | 4.8  |
| RAF TBG   | 110 | 2   | 24.4  | -10.6         | 14.9 | 77.5   | 14.7        | 37.8 | 21.2  | -7.4          | 12.6        | 84.9  | 15.3        | 41.3 |
| RNW DFR   | 110 | 1   | 3.1   | -5.2          | 6.1  | 28.3   | -2.3        | 23.5 | -13.0 | -4.1          | 13.8        | 9.1   | -1.0        | 7.6  |
| RRU SKL   | 110 | 1   | 13.5  | -10.2         | 17.8 | 25.0   | -5.8        | 22.9 | -2.0  | -5.9          | 6.5         | 19.0  | -1.0        | 16.9 |

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|        |       |     |     |       |               | 20   | 2020  |             |      |       |               | 20   | 2029  |             |       |
|--------|-------|-----|-----|-------|---------------|------|-------|-------------|------|-------|---------------|------|-------|-------------|-------|
|        | ГША   | IJ  |     | SI    | Summer Valley | ey . |       | Winter Peak |      | S     | Summer Valley | ey   |       | Winter Peak | 2     |
|        | To    | kV  | No. | MM    | MVAR          | %    | MM    | MVAR        | %    | MM    | MVAR          | %    | MM    | MVAR        | %     |
|        | DAL   | 110 | 1   | 13.7  | 4.7           | 8.1  | 54.7  | 2.9         | 26.1 | 13.3  | 2.5           | 7.6  | 27.4  | -3.9        | 13.2  |
| =      | IKE T | 110 | 1   | 0.7   | 2.8           | 1.6  | -17.5 | 9.6         | 9.5  | -10.5 | 4.0           | 6.3  | -16.7 | 6.8         | 8.6   |
| S(     | SOMT  | 110 | 1   | -8.6  | 2.7           | 8.6  | -10.4 | 7.2         | 10.3 | -11.4 | 1.6           | 11.0 | -7.3  | 2.7         | 6.4   |
|        | SRA   | 110 | 1   | 3.7   | -8.0          | 8.9  | -13.4 | 2.6         | 11.3 | -3.0  | -2.6          | 4.0  | -20.5 | 4.2         | 17.3  |
|        | SRA   | 110 | 2   | 3.5   | -7.4          | 8.3  | -12.4 | 2.4         | 10.4 | -2.8  | -2.4          | 3.7  | -18.9 | 3.9         | 16.0  |
|        | TLK   | 110 | 1   | 0.0   | -0.2          | 0.2  | 18.9  | 1.7         | 15.5 | 0.0   | -0.2          | 0.2  | 20.4  | 2.4         | 16.7  |
| SOM SC | SOM T | 110 | 1   | -3.4  | 0.6           | 3.3  | -16.8 | -5.2        | 14.3 | -2.1  | 0.7           | 2.1  | -18.1 | -5.5        | 15.4  |
|        | CF    | 110 | 2   | 19.5  | -16.5         | 14.3 | -10.0 | 3.1         | 2.0  | -10.6 | -8.6          | 7.7  | -33.3 | 6.3         | 16.2  |
| S      | STR T | 110 | 1   | -3.6  | -0.1          | 8.0  | -22.1 | -4.8        | 50.2 | -2.3  | 0.0           | 5.0  | -23.4 | -5.2        | 53.3  |
| SNG    | AA    | 110 | 1   | 18.5  | -1.6          | 12.8 | 33.5  | 4.8         | 19.1 | -19.9 | 3.8           | 14.0 | 38.8  | -11.6       | 22.9  |
| SBH C  | CDU   | 110 | 1   | -11.6 | -2.3          | 8.7  | -19.4 | -5.5        | 14.7 | -59.7 | -23.7         | 46.9 | -59.7 | -23.6       | 46.9  |
| SHN S( | SOM T | 110 | 1   |       |               |      |       | -           |      | 13.7  | -4.2          | 13.6 | 25.9  | 1.4         | 21.1  |
| CNN C  | CLO   | 110 | 1   | 0.0   | 16.2          | 9.1  | 0.0   | 15.5        | 7.4  | 0.0   | 16.4          | 9.2  | 41.3  | -29.1       | 24.1  |
| _      | CAG   | 110 | 1   | 0.0   | -9.1          | 6.5  | 0.0   | -8.7        | 6.2  | 0.0   | -9.2          | 6.6  | -21.5 | 12.6        | 17.8  |
| )      | CDF   | 110 | 1   | 0.0   | -7.1          | 5.1  | 0.0   | -6.8        | 4.9  | 0.0   | -7.2          | 5.2  | -19.7 | 16.6        | 18.4  |
| Ē      | TBK T | 110 | 1   | -3.1  | -0.1          | 3.0  | 2.6   | -4.1        | 3.9  | -2.0  | 0.2           | 1.9  | -3.1  | -3.8        | 4.0   |
| ×      | KLN   | 110 | 1   | -6.3  | -5.8          | 4.8  | 0.1   | 3.0         | 1.4  | -6.2  | 0.1           | 3.5  | 9.7   | 5.1         | 5.2   |
|        | TIP   | 110 | 1   | 6.3   | 15.7          | 9.5  | 52.8  | -2.7        | 25.2 | 6.1   | 9.6           | 6.4  | 44.3  | -5.2        | 21.3  |
| Ŭ<br>O | OUG T | 110 | 1   | 2.2   | 4.7           | 2.9  | 6.0   | 14.9        | 7.6  | -10.5 | 8.4           | 7.6  | 2.2   | 16.7        | 8.0   |
| THU    | IKE T | 110 | 1   | 5.0   | -5.6          | 4.2  | 38.8  | 1.9         | 18.5 | 14.1  | -6.7          | 8.8  | 39.8  | 5.5         | 19.1  |
| RSP V  | WEX   | 110 | 1   | '     | ı             | ı    | I     | ·           |      | 22.8  | 0'2-          | 13.4 | 39.9  | -7.2        | 19.3  |
| E      | BVK   | 110 | 1   | 0.0   | 1.0           | 0.4  | 53.0  | -45.0       | 30.5 | 0.0   | 1.0           | 0.4  | 53.0  | -45.0       | 30.5  |
| WHO K  | KMA   | 110 | 1   | -     |               |      | -10.2 | 0.8         | 8.2  | 0.0   | -1.6          | 1.3  | -10.2 | 0.8         | 8.2   |
| 57     | SKY   | 110 | 1   | 0.0   | -4.7          | 2.5  | -51.1 | 30.3        | 26.6 | 0.0   | -4.7          | 2.5  | -51.3 | -1.0        | 23.0  |
|        | CRN   | 110 | 1   | 0.0   | -0.1          | 0.1  | 0.0   | -0.1        | 0.1  | 0.0   | -0.1          | 0.1  | -14.9 | 30.1        | 16.0  |
|        | FAS   | 110 | 1   | 6.6   | 2.0           | 6.6  | 30.1  | 12.0        | 26.4 | 4.1   | 1.1           | 1 1  | 0 00  | 0,00        | 0 0 0 |

|         | rine |     | ľ     |               |      |       | Winter Peak |      |       |               |      |       |             |      |
|---------|------|-----|-------|---------------|------|-------|-------------|------|-------|---------------|------|-------|-------------|------|
|         |      |     | nc    | Summer Valley | Ŋ    |       |             |      | Ā     | Summer Valley | ey   |       | Winter Peak |      |
| To      | kV   | No. | MW    | MVAR          | %    | MW    | MVAR        | %    | MM    | MVAR          | %    | MM    | MVAR        | %    |
| CUR     | 110  | 1   | 0.0   | -8.1          | 6.7  | -28.1 | 15.1        | 26.6 | 0.0   | -7.8          | 6.5  | -28.1 | 8.3         | 24.5 |
| ENN (N) | 110  | 1   | -2.8  | 4.7           | 5.0  | 3.3   | 9.7         | 8.2  | -4.1  | 5.7           | 6.5  | 0.9   | 10.4        | 8.4  |
| ROS     | 110  | 1   |       |               |      |       |             |      | -5.5  | 6.0-          | 6.8  | -18.9 | -3.6        | 18.7 |
| ROS     | 110  | 1   | -     |               |      |       |             |      | -5.5  | 6.0-          | 6.8  | -18.9 | -3.6        | 18.7 |
| KEL     | 110  | 1   | -4.5  | 4.4           | 7.6  | -17.3 | 1.8         | 16.9 | -4.9  | 4.4           | 8.0  | -18.5 | 1.2         | 18.0 |
| KEL     | 110  | 2   | -5.2  | -6.1          | 9.8  | -18.4 | -9.1        | 19.9 | -5.6  | -6.2          | 10.2 | -19.8 | -9.2        | 21.2 |
| BPS BVG | 110  | 1   | 12.0  | 2.6           | 15.0 | 24.2  | 2.0         | 23.6 | 9.3   | 3.9           | 12.3 | 8.7   | 5.7         | 10.1 |
| BPS BVG | 110  | 2   | 12.0  | 2.6           | 15.0 | 24.2  | 2.0         | 23.6 | 9.3   | 3.9           | 12.3 | 8.7   | 5.7         | 10.1 |
| BPS EDE | 110  | 1   | 18.8  | -16.0         | 35.8 | 60.9  | -11.2       | 72.0 | 16.0  | -12.3         | 14.1 | 55.1  | -16.6       | 34.7 |
| BPS EDE | 110  | 2   | 18.8  | -16.1         | 35.4 | 61.2  | -11.3       | 71.5 | 16.1  | -12.4         | 14.2 | 55.3  | -16.8       | 34.8 |
| BMA KEL | 110  | 1   | -11.1 | -1.7          | 10.3 | -32.3 | -6.1        | 26.5 | -11.9 | -1.9          | 11.1 | -35.0 | -6.9        | 28.8 |
| BMA KEL | 110  | 2   | -10.8 | -1.6          | 10.0 | -31.3 | -5.6        | 25.7 | -11.6 | -1.8          | 10.8 | -34.0 | -6.4        | 27.9 |
| BAN TAN | 110  | 1   | -5.6  | -1.6          | 7.1  | -19.1 | -4.6        | 19.1 | -6.0  | -1.8          | 2.7  | -20.6 | -6.0        | 20.9 |
| BAN TAN | 110  | 2   | -5.9  | -1.7          | 7.4  | -20.0 | -5.1        | 20.0 | -6.2  | -1.8          | 7.8  | -21.1 | -6.3        | 21.4 |
| BVG KEL | 110  | 1   | 5.4   | -0.1          | 5.0  | 4.2   | -3.2        | 4.3  | 2.4   | 0.9           | 2.3  | -12.1 | 0.2         | 9.8  |
| BVG KEL | 110  | 2   | 5.7   | -0.1          | 5.2  | 4.4   | -3.3        | 4.5  | 2.5   | 1.0           | 2.5  | -12.7 | 0.3         | 10.2 |
| BVG LAR | 110  | 1   | 6.4   | 3.3           | 9.1  | 19.7  | 5.6         | 18.1 | 6.8   | 3.5           | 9.7  | 21.1  | 6.1         | 19.4 |
| BVG LAR | 110  | 2   | 6.4   | 3.3           | 9.1  | 19.8  | 5.6         | 18.2 | 6.8   | 3.5           | 9.7  | 21.1  | 6.1         | 19.5 |
| BNH CAS | 110  | 1   | -8.3  | -1.0          | 10.2 | -28.4 | -5.8        | 28.1 | -8.8  | -1.1          | 10.8 | -30.1 | -6.2        | 29.9 |
| BNH CAS | 110  | 2   | -8.3  | -1.0          | 10.2 | -28.4 | -5.8        | 28.2 | -8.8  | -1.1          | 10.9 | -30.2 | -6.2        | 29.9 |
| BNM DON | 110  | 1   | -7.3  | -0.3          | 9.7  | -24.9 | -4.2        | 30.8 | -7.8  | -0.3          | 10.4 | -26.6 | -4.7        | 33.0 |
| BNM DON | 110  | 2   | -7.3  | -0.4          | 9.8  | -25.1 | -4.4        | 31.1 | -7.8  | -0.5          | 10.4 | -26.6 | -4.8        | 33.0 |
| BRO AGI | 110  | 1   |       |               |      |       |             | ı    | 0.0   | -0-5          | 0.4  | 14.2  | -12.7       | 13.2 |
| RSK     | 110  | 1   |       |               |      |       |             |      | 0.0   | 0.5           | 0.3  | 41.2  | -13.0       | 21.6 |
| CAR CAS | 110  | 1   | 8.6   | -17.2         | 27.8 | 28.0  | -18.2       | 38.9 | 7.0   | -13.3         | 21.8 | 22.9  | -23.4       | 38.0 |
| CAR EDE | 110  | 1   | -13.5 | 17.0          | 31.5 | -42.8 | 16.8        | 53.5 | -10.5 | 13.2          | 24.5 | -36.1 | 22.2        | 49.2 |

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|      |               | %    | 37.9  | 49.5  | 42.3 | 42.2 | 40.3 | 40.3 | 20.2 | 19.8 | 29.6    | 31.0    | 20.7 | 20.8 | 19.9  | 19.9  | 22.3    | 12.2    | 19.6    | 19.2    | 9.0     | 2.5   | 27.7    | 14.7 | 14.8 | 24.7 | 24.7 | 23.0    |
|------|---------------|------|-------|-------|------|------|------|------|------|------|---------|---------|------|------|-------|-------|---------|---------|---------|---------|---------|-------|---------|------|------|------|------|---------|
|      | Winter Peak   | MVAR | -23.6 | 22.4  | 1.1  | 1.0  | 1.7  | 1.8  | -5.7 | -5.7 | 4.2     | 4.7     | 6.5  | 6.6  | -3.2  | -3.2  | -5.1    | -1.3    | 4.8     | 4.7     | -2.4    | 0.7   | 6.5     | 3.3  | 3.3  | 3.2  | 3.1  | -6.0    |
|      | Wi            | MW   | 23.1  | -36.2 | 61.3 | 61.1 | 29.3 | 29.3 | 24.4 | 23.9 | 30.2    | 31.6    | 30.7 | 30.9 | -28.5 | -28.5 | -22.4   | -12.5   | 19.6    | 19.2    | -17.1   | 4.1   | 27.8    | 14.8 | 14.9 | 25.2 | 25.2 | 27.9    |
| 2029 |               | %    | 21.6  | 24.6  | 14.6 | 14.6 | 13.9 | 13.9 | 8.2  | 8.0  | 10.7    | 11.3    | 5.0  | 5.1  | 5.8   | 5.8   | 22.5    | 16.0    | 7.5     | 7.3     | 3.5     | 18.6  | 25.5    | 6.3  | 6.3  | 9.0  | 9.0  | 35.4    |
|      | Summer Valley | MVAR | -13.4 | 13.3  | -7.1 | -7.1 | -3.3 | -3.3 | -5.4 | -5.3 | 0.4     | 0.5     | 1.3  | 1.4  | -0.6  | -0.6  | -2.1    | -1.5    | 0.1     | 0.1     | 2.6     | -9.5  | 1.3     | 0.6  | 0.6  | -0.4 | -0-5 | -7.0    |
|      | Sum           | MW   | 7.0   | -10.6 | 17.9 | 17.9 | 8.6  | 8.6  | 7.1  | 7.0  | 8.8     | 9.2     | 7.1  | 7.2  | -8.3  | -8.3  | -18.3   | -13.0   | 6.1     | 6.0     | 5.9     | 24.8  | 20.9    | 5.1  | 5.1  | 7.4  | 7.4  | 37.9    |
|      |               | %    | 38.7  | 53.8  | 44.0 | 43.9 | 43.2 | 43.2 | 19.1 | 18.7 | 27.8    | 29.2    | 8.5  | 8.6  | 18.5  | 18.5  | 20.0    | 10.9    | 18.3    | 17.9    | 8.3     | 3.2   | 24.9    | 13.7 | 13.7 | 23.3 | 23.2 | 24.6    |
|      | Winter Peak   | MVAR | -18.4 | 17.0  | 2.5  | 2.4  | 2.5  | 2.6  | -5.7 | -5.8 | 3.7     | 4.2     | 3.4  | 3.5  | -2.8  | -2.8  | -5.8    | -2.2    | 4.4     | 4.3     | 0.4     | -0.3  | 6.9     | 3.0  | 3.0  | 2.9  | 2.7  | -6.6    |
|      | W             | MW   | 28.2  | -43.0 | 63.8 | 63.6 | 31.4 | 31.5 | 22.9 | 22.5 | 28.4    | 29.7    | 12.4 | 12.6 | -26.4 | -26.5 | -19.8   | -11.0   | 18.3    | 18.0    | -16.0   | 5.3   | 24.7    | 13.8 | 13.8 | 23.8 | 23.8 | 29.7    |
| 2020 |               | %    | 27.6  | 31.6  | 15.1 | 15.1 | 14.8 | 14.8 | 8.2  | 8.0  | 10.1    | 10.6    | 3.1  | 3.1  | 5.4   | 5.4   | 20.0    | 14.0    | 7.0     | 6.9     | 2.2     | 19.3  | 23.0    | 5.9  | 5.9  | 8.5  | 8.5  | 35.3    |
|      | Summer Valley | MVAR | -17.3 | 17.1  | -7.1 | -7.2 | -3.4 | -3.3 | -5.9 | -5.8 | 0.3     | 0.4     | -0.6 | -0.6 | -0.5  | -0.5  | -0.1    | 0.4     | 0.1     | 0.1     | -1.1    | -13.9 | -0.9    | 0.6  | 0.6  | -0.4 | -0.6 | -13.9   |
|      | Sun           | MM   | 8.7   | -13.6 | 18.7 | 18.6 | 9.2  | 9.2  | 6.7  | 6.6  | 8.3     | 8.7     | 4.4  | 4.5  | -7.7  | -7.8  | -16.4   | -11.5   | 5.8     | 5.6     | 4.0     | 23.9  | 18.9    | 4.8  | 4.8  | 7.0  | 6.9  | 35.8    |
|      |               | No.  | 2     | 2     | 1    | 2    | 1    | 2    | 1    | 2    | 1       | 2       | 1    | 2    | 1     | 2     | 1       | 1       | 1       | 2       | 1       | 1     | 1       | 1    | 2    | 1    | 2    | 1       |
|      |               | kV   | 110   | 110   | 110  | 110  | 110  | 110  | 110  | 110  | 110     | 110     | 110  | 110  | 110   | 110   | 110     | 110     | 110     | 110     | 110     | 110   | 110     | 110  | 110  | 110  | 110  | 110     |
| -    |               | To   | CAS   | EDE   | CRE  | CRE  | KNO  | KNO  | NAR  | NAR  | RAT (N) | RAT (N) | ROS  | ROS  | CRE   | CRE   | CPS     | LIM (N) | DOJ     | DOJ     | RSK     | KMT   | LIM (N) | LMR  | LMR  | SPR  | SPR  | STR (N) |
|      |               | From | CAR   | CAR   | CAS     | CAS     | CAS  | CAS  | CEN   | CEN   | COL (N) | CPS   | CPS     | CPS  | CPS  | CPS  | CPS  | CPS     |

|      |               | %    | 18.6  | 7.9   | 32.4  | 31.3  | 23.6    | 26.5    | 17.9    | 21.3    | 21.3    | 1.9     | 1.9     | 18.4    | 18.4    | 17.3    | 36.0    | 37.5    | 12.5  | 16.6  | 14.3         | 14.8  | 13.6  | 27.0    | 25.1    | 27.9    | 1.2     | 12.9    |
|------|---------------|------|-------|-------|-------|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|-------|--------------|-------|-------|---------|---------|---------|---------|---------|
|      | Winter Peak   | MVAR | 4.2   | -7.7  | -4.3  | 2.3   | 4.9     | -8.9    | -2.6    | 0.4     | 0.4     | 0.9     | 0.9     | -20.4   | -20.4   | -21.2   | 17.7    | 18.0    | -1.4  | -14.2 | -7.5         | -1.3  | -14.5 | -10.6   | 3.1     | -7.6    | 1.8     | 4.5     |
| 2029 | ^             | MM   | -18.7 | -6.1  | -51.0 | -49.4 | -19.7   | -21.0   | -35.7   | 21.9    | 21.9    | -4.1    | -4.1    | -4.0    | -4.0    | -5.1    | -41.1   | -42.9   | -15.5 | -25.8 | -19.2        | -28.6 | -21.9 | -37.5   | -36.1   | -24.0   | 1.6     | 25.3    |
| 20   | ey            | %    | 12.9  | 6.1   | 10.4  | 11.4  | 11.9    | 14.9    | 1.9     | 15.2    | 15.2    | 6.6     | 6.6     | 6.5     | 6.5     | 5.0     | 10.6    | 11.0    | 2.1   | 6.0   | 4.6          | 3.9   | 4.5   | 9.6     | 8.2     | 8.9     | 0.7     | 2.5     |
|      | Summer Valley | MVAR | 4.4   | -6.4  | 0.6   | 7.6   | 6.0     | -8.1    | -3.5    | -4.2    | -4.2    | 5.9     | 5.9     | -4.5    | -4.5    | -4.6    | 5.7     | 5.7     | -2.6  | -0.6  | 0.5          | -6.3  | -1.8  | -8.1    | 5.9     | -1.9    | -1.2    | 4.9     |
|      | Sı            | MW   | -9.6  | 1.9   | -14.9 | -14.5 | -5.5    | -6.4    | 0.0     | 11.7    | 11.7    | -11.7   | -11.7   | -2.6    | -2.6    | -2.9    | -10.1   | -10.5   | 0.0   | -9.4  | -6.6         | -3.4  | -8.2  | -11.2   | -10.3   | -7.0    | -0.8    | 0.8     |
|      |               | %    | 18.5  | 8.4   | 33.7  | 27.2  | 26.9    | 30.1    | 10.1    | 18.5    | 18.5    | 8.9     | 8.9     | 19.4    | 19.4    | 18.3    | 31.8    | 33.0    |       | 15.6  | 13.5         | 12.9  | 12.9  | 28.6    | 26.6    | 26.1    | 0.5     | 10.5    |
|      | Winter Peak   | MVAR | 5.8   | -9.1  | -3.8  | 2.4   | 4.4     | -9.5    | -1.5    | -1.6    | -1.6    | 2.3     | 2.3     | -21.0   | -21.0   | -21.7   | 19.5    | 19.9    |       | -12.4 | -6.4         | -2.8  | -12.9 | -10.9   | 2.8     | -7.0    | 0.9     | 4.8     |
| 2020 |               | MM   | -18.1 | -5.2  | -53.1 | -42.9 | -22.7   | -24.1   | -20.2   | 19.0    | 19.0    | -8.8    | -8.8    | -6.5    | -6.5    | -7.7    | -34.3   | -35.8   | -     | -24.9 | -18.4        | -24.7 | -21.2 | -39.6   | -38.2   | -22.4   | 6.0-    | 20.4    |
| 20   | ey            | %    | 15.0  | 9.8   | 10.9  | 10.1  | 12.6    | 15.9    | 0.5     | 14.3    | 14.3    | 14.5    | 14.5    | 6.6     | 6.6     | 5.1     | -       | 16.4    |       | 5.5   | 4.2          | 2.7   | 4.2   | 10.0    | 8.6     | 8.3     | 1.1     | 1.5     |
|      | Summer Valley | MVAR | 8.7   | -10.5 | 1.6   | 7.3   | 5.8     | -8.2    | -0.9    | -4.5    | -4.5    | 5.0     | 5.0     | 2.5-    | -3.7    | -3.7    | -       | 5.2     |       | -1.7  | <b>†</b> .0- | -2.7  | -2.7  | -8.1    | 5.8     | -1.8    | 1.2     | 2.4     |
|      | Sı            | MW   | -8.7  | 1.4   | -15.6 | -12.5 | -6.4    | -7.3    | 0.0     | 10.8    | 10.8    | -10.8   | -10.8   | -3.7    | -3.7    | -4.1    |         | -15.3   | -     | -8.4  | -6.0         | -4.2  | -7.3  | -11.8   | -10.9   | -6.6    | -1.8    | 1.8     |
|      |               | No.  | 1     | 1     | 1     | 2     | 1       | 2       | 1       | 1       | 2       | 1       | 2       | 1       | 2       | 3       | 1       | 2       | 1     | 1     | 2            | 1     | 3     | 1       | 2       | 1       | 1       | 1       |
|      | rine          | kV   | 110   | 110   | 110   | 110   | 110     | 110     | 110     | 110     | 110     | 110     | 110     | 110     | 110     | 110     | 110     | 110     | 110   | 110   | 110          | 110   | 110   | 110     | 110     | 110     | 110     | 110     |
| -    |               | To   | KEL   | TMN   | HAN   | HAN   | FIN (N) | FIN (N) | DRQ     | ENN (N) | ENN (N) | OMA     | OMA     | TAN     | TAN     | TAN     | TMN     | TMN     | ΡТ    | TMN   | TMN          | OMA   | TMN   | HAN     | HAN     | KEL     | OMA     | TMN     |
|      |               | From | CRG   | CRG   | DON   | DON   | DON     | DON     | DRO (N) | DRU (N) | DRQ   | DUN   | DUN          | DUN   | DUN   | FIN (N) | FIN (N) | GLE (N) | GOR (N) | GOR (N) |

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|         | LINE    | Ð   |     | SI    | Summer Valley | , Ke |       | Winter Peak |      | S     | Summer Valley | ey ( |       | Winter Peak |      |
| From    | To      | k۷  | No. | MW    | MVAR          | %    | MM    | MVAR        | %    | MM    | MVAR          | %    | MM    | MVAR        | %    |
| HAN     | (N) SIJ | 110 | 1   | 6.2   | -15.0         | 19.8 | 12.9  | -7.9        | 14.7 | 6.4   | -12.2         | 16.8 | 18.3  | -2.6        | 17.9 |
| HAN     | (N) SIT | 110 | 2   | 6.6   | -15.6         | 21.2 | 12.2  | -8.9        | 15.1 | 6.8   | -12.6         | 17.9 | 17.2  | -3.4        | 17.5 |
| KEL     | GLE (N) | 110 | 2   | 0.0   | -2.9          | 3.6  | 0.0   | -2.9        | 3.2  | 0.0   | -2.9          | 3.5  | 0.0   | -2.9        | 3.3  |
| KEL     | RSK     | 110 | 1   | -9.4  | -6.5          | 6.2  | -25.6 | 4.3         | 13.4 | -6.2  | -5.4          | 4.4  | -23.6 | 5.8         | 12.6 |
| KEL     | RSK     | 110 | 2   | -     |               |      |       |             | -    | -5.7  | -6.2          | 4.5  | -24.7 | 2.9         | 11.7 |
| KMT     | SLK     | 110 | 1   | 0.0   | -17.8         | 16.3 | -21.8 | 4.6         | 18.0 | 0.0   | -18.1         | 16.6 | -21.8 | 6.3         | 18.3 |
| KMT     | STR (N) | 110 | 1   | 23.8  | 4.1           | 16.9 | 37.8  | -3.8        | 22.9 | 24.7  | 8.8           | 18.3 | 36.6  | -4.5        | 22.2 |
| LIS (N) | TAN     | 110 | 1   | -2.6  | -13.5         | 16.8 | -16.4 | -12.1       | 19.8 | 0.9   | -10.8         | 13.2 | -21.3 | -8.8        | 22.4 |
| LIS (N) | TAN     | 110 | 2   | -2.1  | -14.3         | 18.0 | -16.8 | -13.2       | 21.4 | 1.4   | -11.3         | 14.2 | -22.1 | -9.8        | 24.1 |
| MKL     | OMA     | 110 | 1   | 0.0   | 0.9           | 0.7  | 35.7  | 6.3         | 23.1 | 0.0   | 1.0           | 0.7  | 41.3  | 6.9         | 26.7 |
| NEW (N) | TAN     | 110 | 1   | -11.7 | -2.0          | 14.4 | -37.5 | -9.3        | 37.6 | -12.4 | -2.2          | 15.4 | -40.1 | -10.1       | 40.2 |
| NEW (N) | TAN     | 110 | 2   | -11.7 | -2.0          | 14.5 | -37.6 | -9.3        | 37.6 | -12.4 | -2.2          | 15.4 | -40.2 | -10.1       | 40.3 |
| OMA     | STR (N) | 110 | 1   | -23.5 | 6.4           | 22.3 | -17.5 | 8.4         | 15.7 | -24.3 | 2.5           | 22.4 | -14.4 | 8.4         | 13.4 |
| OMA     | STR (N) | 110 | 2   | -23.1 | 6.3           | 29.2 | -17.2 | 8.3         | 18.5 | -23.9 | 2.4           | 29.3 | -14.2 | 8.3         | 15.9 |
| OMA     | TRE     | 110 | 1   | 1.1   | -1.9          | 1.2  | 3.7   | -1.7        | 2.1  | 1.7   | 1.4           | 1.2  | 6.8   | -2.9        | 3.8  |
| TAN     | WAR     | 110 | 1   | 9.2   | 1.7           | 11.9 | 31.8  | 8.0         | 29.0 | 10.0  | 1.9           | 12.9 | 34.0  | 8.8         | 31.1 |
| TAN     | WAR     | 110 | 2   | 9.2   | 1.7           | 11.8 | 31.7  | 8.0         | 28.9 | 10.0  | 1.9           | 12.9 | 33.9  | 8.8         | 31.0 |
| TRE     | TMN     | 110 | 1   | 3.6   | 3.0           | 2.5  | 29.2  | 2.6         | 15.2 | 1.6   | 5.9           | 3.3  | 32.3  | 1.4         | 16.7 |



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