

JUNE 1951

RADIO — ELECTRONICS

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HUGO GERNSBACH, Editor



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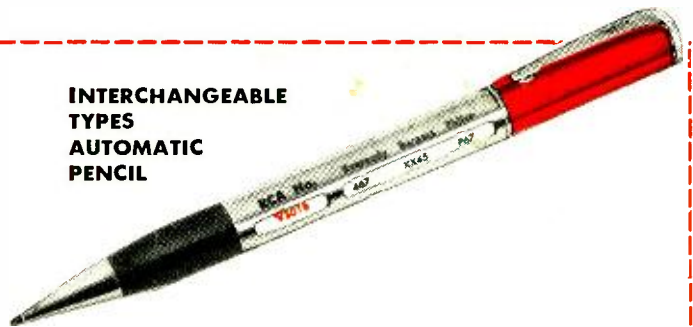
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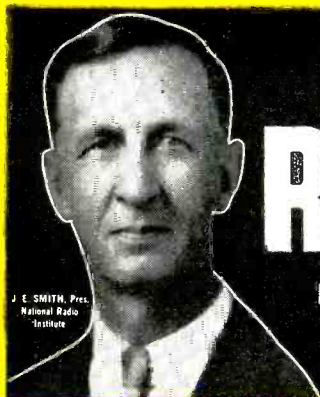
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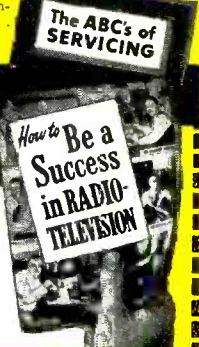
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ON THE COVER:

L. O. Schott of the Bell Telephone Laboratories operates the electric voice which is used by the Laboratories in speech research work.
Kodachrome by Avery Slack

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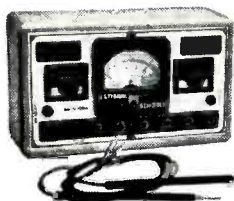
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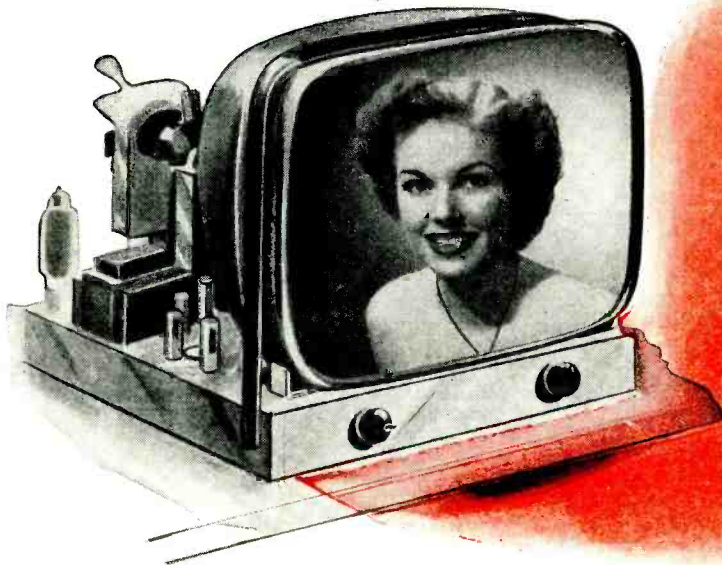
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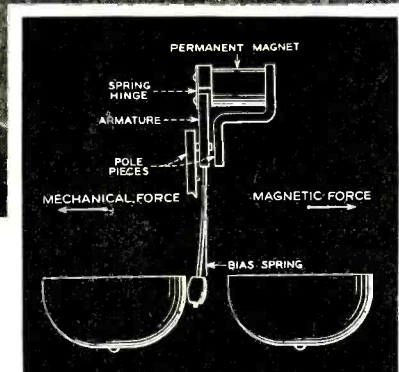
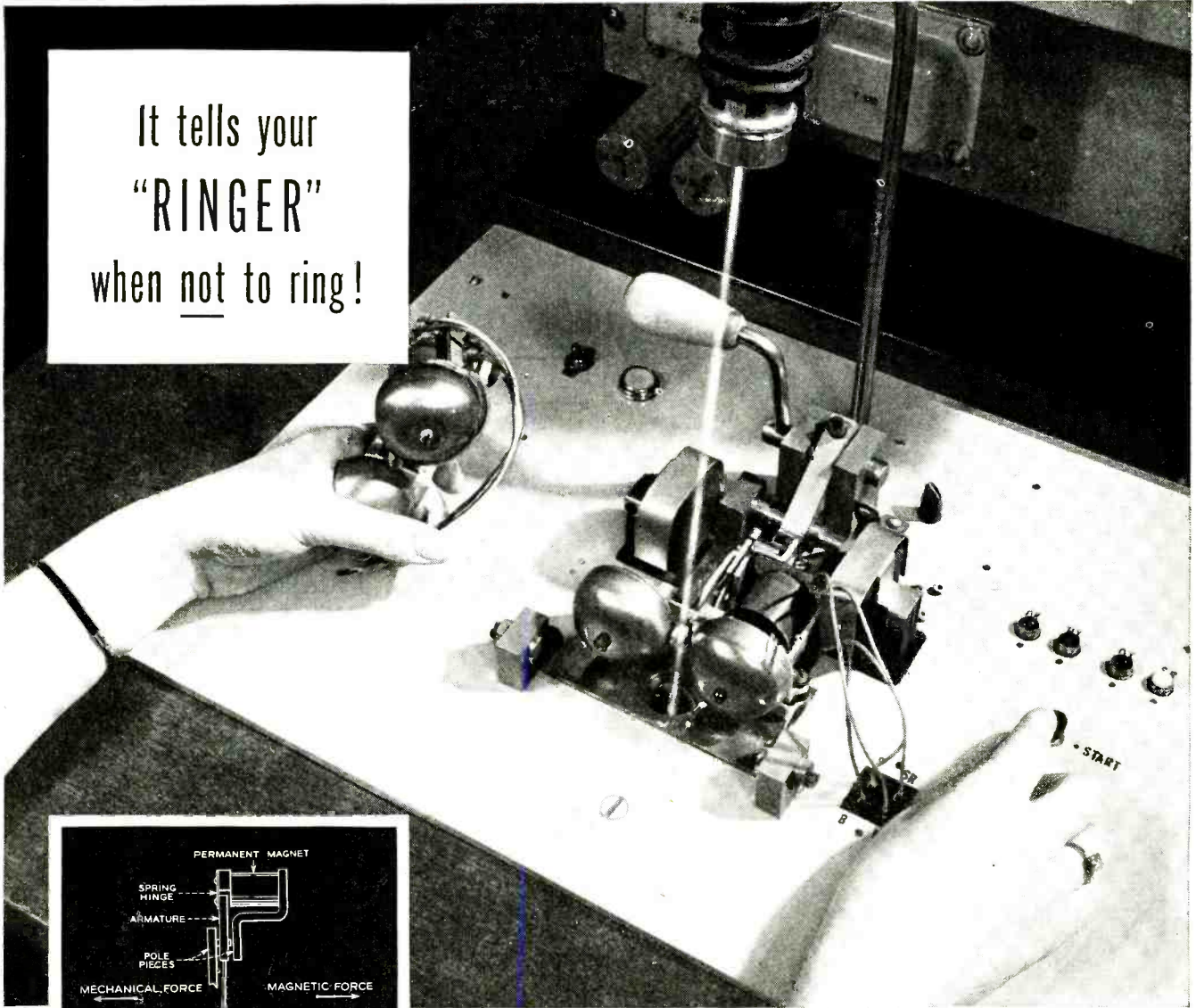
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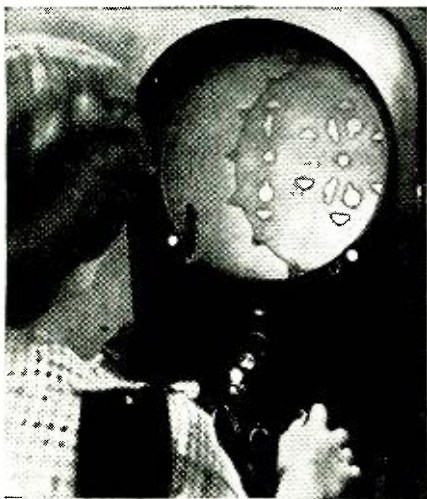


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PREDICTING THE FUTURE from the motion of the planets, long the basis of the ancient pseudo-science of astrology, has emerged from the realm of superstition into the field of modern science. RCA engineer John H. Nelson, writing in the *RCA Review*, reports evidence that the magnetic storms on the earth which disrupt radio communications are directly related to the positions of the planets.

Engineer Nelson, also an amateur astronomer, was assigned years ago to the task of studying the spots on the sun through a 6-inch telescope set up for him on the roof of a downtown office building in New York City. He failed to find enough correlation between the sunspots and the behavior of radio communications to be able to make predictions of more than a few days in advance, and in 1948 caused some comment in astronomical circles by reporting that the size of the sunspots is a "meaningless criterion" in predicting radio disturbances. The type of sunspots, their age and activity, and their position on the sun are the determining factors.

Engineer Nelson turned to the planets for his research inspired by suggestions from the late Ellsworth Huntington of Yale and Henry Helm Clayton. He studied hundreds of daily propagation reports compiled by technicians at RCA's receiving station at Riverhead, L. I., and from overseas stations of Radio France and Sweden's Telegraph Administration. These he tried to correlate with the positions of the planets.

From these studies Mr. Nelson concluded that the planets disturb the sun; and the sun in turn affects electromagnetic conditions on the earth. From daily plots of the courses of the six inner planets he observed that disturbances on the earth occur more frequently when two or more planets form a right angle (with the sun as apex), or form a straight line with the sun.

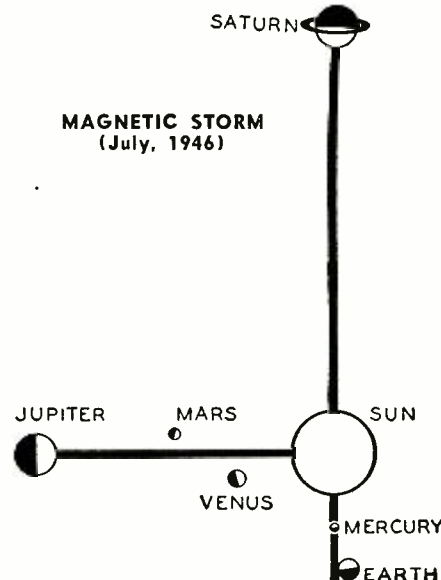
The most disturbed periods are the twelve months preceding and following the positioning of Saturn and Jupiter in such a configuration. The most severe

disturbances occur when Mars, Venus, Mercury, and Earth are in critical relationship near points of the Saturn-Jupiter configuration. When Saturn and Jupiter have moved away from their configuration, the earth's magnetic activity decreases, although the smaller planets cause storms of shorter duration. The quietest periods occur when Saturn, Jupiter, and Mars are equally spaced around the sun by 120°. The figure shows the positions of the planets during the great 1946 magnetic storm.

Not all planetary configurations coincide with magnetic storms, but studies of the Riverhead records show that storms are about ten times more frequent during a configuration than on ordinary days.

Major disturbances can be predicted as much as two years in advance. By combining planetary observations with daily inspection of the sun's surface, Mr. Nelson has been able to predict good and bad radio weather with 85% accuracy or better.

MEDAL OF HONOR of the Institute of Radio Engineers was awarded to Dr. Vladimir K. Zworykin, vice-president and technical consultant of RCA Laboratories, Princeton, N. J. In his acceptance speech at the Institute's annual banquet at New York's Waldorf-Astoria, Dr. Zworykin stressed the importance of the role of electronics in the future of medicine, both in therapy and diagnosis. Close co-operation between physician and engineer is needed to work out these problems, he said.



AUTO TV SETS will be banned in New York state after July 1. A bill, signed without comment by Governor Thomas E. Dewey, provides: "It shall be unlawful to operate upon any public highway in this state a motor vehicle which is equipped with a television receiving set."

SHIP OPERATOR RULES have been changed somewhat by the FCC in an effort to relieve a serious shortage of manpower resulting from the expansion of the nation's merchant fleet. For the duration of the emergency, examination is waived for operators having less than two years of satisfactory service under the license being renewed. Another change establishes a temporary limited second-class license allowing the holder to operate radiotelegraph aboard ships only.

RADIO-ELECTRONICS for

Which Do You Want?



Better Pay



A Nice Home



A New Car



Greater Security



Happy Vacations and Travel

Get Your FCC Ticket
Then Use Our
Amazingly Effective
Job-Finding Service
To Get a Better Job



EDW. H. GUILFORD
Vice President

I can train you to pass your FCC License Exams in a minimum of time if you've had any practical radio experience—amateur, Army, Navy, radio servicing, or other. My time-proven plan can help put you, too, on the road to success.

Just fill out the coupon and mail it. I will send you free of charge, a copy of "How to Pass FCC License Exams," plus a sample FCC-type Exam, and the amazing new booklet, "Money Making FCC License Information."

How to Pass FCC License Exams

Commercial
Radio Operator



FREE

Tells where to apply for and take FCC examinations, location of examining offices, scope of knowledge required, approved way to prepare for FCC examinations, positive method of checking your knowledge before taking the examinations.

Get this Amazing Booklet FREE

TELLS HOW — WE GUARANTEE

TO TRAIN AND COACH YOU AT HOME
IN SPARE TIME UNTIL YOU GET

YOUR FCC LICENSE

TELLS HOW — Employers make

JOB OFFERS Like These

to Our Graduates Every Month

Telegram, August 9, 1950, from Chief Engineer, Broadcast Station, Pennsylvania. "Have job opening for one transmitter operator to start immediately, contact me at once." Letter, August 12, 1950, from Dir. Radio Div. State Highway Patrol. "We have two vacancies in our Radio Communication Division. Starting pay \$200; \$250 after six months' satisfactory service. Will you recommend graduates of your school?" These are just a few examples of the job offers that come to our office periodically. Some licensed radioman filled each of these jobs . . . it might have been you!

HERE'S PROOF FCC LICENSES ARE OFTEN SECURED IN A FEW HOURS OF STUDY WITH OUR COACHING AT HOME IN SPARE TIME

Name and Address	License	Lessons
Lee Worthy 2210 1/2 Wilshire St., Bakersfield, Cal.	2nd Phone	16
Clifford E. Vogt Box 1016, Dania, Fla.	1st Phone	20
Francis X. Foerch 38 Baucier Pl., Bergenfield, N. J.	1st Phone	38
S/Sgt. Ben H. Davis 317 North Roosevelt, Lebanon, Ill.	1st Phone	28
Albert Schoell 110 West 11th St., Escondido, Cal.	2nd Phone	23

CLEVELAND INSTITUTE OF RADIO ELECTRONICS
Desk RE-30, 4900 Euclid Bldg., Cleveland 3, Ohio
(Approved for Veteran Training Under "GI Bill of Rights")

JUNE, 1951

TELLS HOW —

Our Amazing Effective
JOB-FINDING SERVICE

Gets Better Jobs for Graduates

Here is just one recent example of Job-Finding Results

OURS IS THE ONLY HOME STUDY COURSE WHICH SUPPLIES FCC-TYPE EXAMINATIONS WITH ALL LESSONS AND FINAL TESTS.

GETS FIVE JOB-OFFERS FROM BROADCAST STATIONS "Your 'Chief Engineer's Bulletin' is a grand way of obtaining employment for your graduates who have obtained their 1st class license. Since my name has been on the list I have received calls or letters from five stations in the southern states, and am now employed as Transmitter Engineer at WMMT." Elmer Powell, Box 274, Sparta, Tenn.

Your FCC Ticket is always recognized in all radio fields as proof of your technical ability.



Get All 3 FREE

MAIL COUPON NOW

CLEVELAND INSTITUTE OF RADIO ELECTRONICS
Desk RE-30, 4900 Euclid Bldg.,
Cleveland 3, Ohio
(Address to Desk No. to avoid delay.)

I want to know how I can get my FCC ticket in a minimum of time. Send me your FREE booklet, "How to Pass FCC License Examinations" (does not cover exams for Amateur License), as well as a sample FCC-type exam and the amazing new booklet, "Money-Making FCC License Information."

NAME
ADDRESS
CITY ZONE STATE

Paste on penny post card or send air mail

Watch
MERIT
for TV in '51

Merit is meeting the rapidly rising demand for TV replacements with a TV line as complete as current and advance information will permit

**TRY MERIT FIRST FOR
TV CONVERSION OR
REPLACEMENT!**



HV06—Universal Ferrite core "FLYBACK" permits widest coverage.



MDF70—70° high efficiency Ferrite yoke for tubes up to 19"



MWC-1—Width linearity control with AGC winding (Automatic Gain Control).



**FOCUS
COILS**

Free!

Write today for:

- MERIT TV REPL GUIDE AND CATALOG**
—Dec. 1950 issue. Up-to-date listing of all replacements.
- MERIT 1951 CATALOG No. 5111**
Show specs. on a complete line of TV, Radio, Amateur and Industrial Transformers.

REFER TO MERIT'S LISTING
in Howard Sam's Photofacts

**TAPE-MARKED
TO HELP YOU!**
Handy tape marking on every Merit Transformer shows permanent hook-up data for quick reference. **ORIGINALATED BY MERIT.**

MERIT
TRANSFORMER CORP.

4443 NORTH CLARK ST., CHICAGO 40, ILL.

FM BEEP SIGNALS, used by some FM broadcast stations to mute receivers during commercials and station announcements in restaurants and other public places, are not legal, according to a ruling by the FCC. A few FM stations have been using such signals to provide "functional music" programs to subscribers as a source of additional revenue. (See April, 1951 issue, p. 30.)

In a letter to four stations using the system, the FCC expressed sympathy with the aims of the broadcasters, but ruled that eliminating the station identification announcement violates the Communications Act. The commission further ruled that subscribers to such services must be logged as sponsors, and all such programs must be listed as commercial time periods. The stations involved—WRLD, Miami, Fla.; WACE-FM, Chicopee, Mass.; WFMF, Chicago, Ill.; and KDFC, Sausalito, Cal.—were ordered to show how they intend to comply with the order by April 30.

TELEVISION TRANSMITTER was presented as a gift to the Indiana Technical College, Fort Wayne, by the Zenith Radio Corporation, Chicago. The custom-designed unit first went into service in 1938 in Zenith's experimental station. Later it was used in Phonovision tests and has only recently been replaced by new equipment. The transmitter includes complete facilities for transmitting sound and picture on channel 2. An earlier gift by the Capehart-Farnsworth Corporation of the major portions of a TV transmitter gave the college's television engineering course its start.

WESTERN UNION is the latest comer to the television service ranks, it was announced in New York City recently. According to the announcement, a new subsidiary, Western Union Services, Inc., will open a pilot shop in East Orange, New Jersey, across the Hudson from New York City. The new company has an arrangement with Du Mont to install and service Du Mont receivers in three New Jersey counties, and at present will confine itself to the service of Du Mont telesets. Thomas F. McMains, president of the new company, explained that Western Union, backed by its 100 years of experience in the telegraph field, felt particularly capable of solving the problems likely to be encountered in the business of servicing electronic equipment such as television receivers.

The pilot plant is expected to have a staff of between 20 and 30 specially trained technicians and an adequate fleet of service vehicles. It will handle Du Mont installation and service work in Essex, Passaic, and Union Counties, at rates uniform with present Du Mont charges.

WILLIAM E. BEAKES, one of radio's pioneers and former president of the Tropical Radio Telegraph Company, died on March 30 at the age of 70. In 1941 Mr. Beakes was awarded the Marconi Wireless Pioneer Medal of the Veteran Wireless Operators Association for

his pioneering in radio in the North Atlantic and tropical zones. He took part in Marconi's first transatlantic radiotelegraph transmissions shortly after the turn of the century and later aided Professor Reginald Fessenden in wireless experiments. In 1912 he joined the United Fruit Company, which was then experimenting with radio in Central America. Mr. Beakes is credited with building up the Tropical Radio Telegraph Company, a subsidiary of United Fruit. Much of his work was devoted to the transition from long to short waves to overcome interference from tropical static.

ANTISUBMARINE TORPEDO that automatically "homes" on an enemy submarine either on the surface or at any depth to which it will submerge was disclosed by the Navy. The deadly high-speed missile operates on the same principle as similar homing torpedoes used successfully but to a limited extent during World War II, which were guided by the noise made by the enemy craft. The new weapon is at least twice as fast as the former one. A silent submarine trying to wait out an attack can be sought out by picking up reflections of sounds sent out by the torpedo itself. The torpedo would be equally effective against surface craft.

TELEVISION SCREENS may serve in place of windshields in supersonic planes of the future. The windshield is the only major projection from the surface of high-speed aircraft, and it creates objectionable friction and heat. Preliminary studies were made at the University of Illinois for the Navy to find out if it is feasible to use television. Dr. Stanley N. Roscoe, head of the project, said that a periscope was fitted to a Cessna plane for projection to an 8-inch screen in the pilot's compartment. The periscope allowed for various degrees of magnification. Pilots flew the plane with windows covered and uncovered, and found they could fly "just about as well" using the 8-inch screen with low magnification. Dr. Roscoe said he envisioned planes of the future with an optical system installed in the front of the craft, and a television screen in front of the pilot showing him what is ahead.

SECRET CONFERENCE was held by the FCC with more than 3,000 commercial broadcasters to give instructions on what to do and how to do it in the event of an air attack on the United States. Top experts of the air defense command outlined general instructions to the broadcasters, and it was assumed that this will be followed by top secret individual instructions to each owner of a broadcasting outlet. The part broadcasters will have in such a national emergency has not been announced, and probably will not be.

Some time ago the FCC said that it was issuing a series of unannounced permits for secret experiments involving the use of radio for national crisis. The nature of these tests has never been disclosed.

—end—

RADIO-ELECTRONICS for



HOME STUDY COURSE in TELEVISION SERVICING

... based on the experience of the RCA Service Company

Now available to the Industry

Here's *your* golden opportunity to take the time-tested RCA Service Company course on television receiver servicing... to earn a valuable RCA Institutes' certificate that can lead straight to a better job at higher pay.

Now, for the first time, *you* can take the same basic course that has already been given to the thousands of RCA's own servicemen... an easy-to-understand home-study course based on the actual experience of the RCA Service Company in servicing thousands of home television receivers.

Cost is *low*... only \$9 a unit for 10 units or \$90 total, on an easy pay-as-you-learn plan. And value is *high*... the certificate of completion issued by RCA Institutes is known and honored throughout the radio-electronics industry.

Never before available to anyone outside RCA. Now offered to *you* through RCA Institutes, one of America's oldest and most respected technical training schools. Course covers most major makes and types of TV receivers. Designed specially for men already in electronics; therefore no kits

or paraphernalia are required. Handled entirely by correspondence. Available *exclusively* to men in the radio-television-electronics field. Not offered to the general public, or under the G.I. Bill.

ENROLL NOW! Mail the coupon *today*. Don't miss your great opportunity to take this proven course. If you're just getting started in TV, it will make you a *good* serviceman. If you're already *good*, it can't help but make you *better!* Send the coupon... get on the reservation list... **NOW!**

LOWER RATES FOR GROUPS!

If any employer in the radio-electronic industry desires to enroll six or more of his employees for this course, lower rates will apply. A special group application form is available for employers desiring to take advantage of this offer.



RCA INSTITUTES, INC.
A SERVICE OF RADIO CORPORATION OF AMERICA
350 WEST FOURTH STREET, NEW YORK 14, N. Y.

MAIL COUPON TODAY!

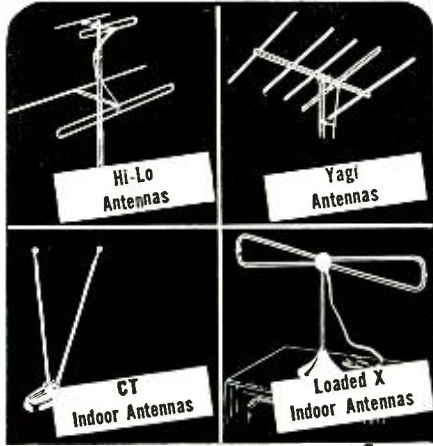
RCA INSTITUTES, INC.
Home Study Department, RE-651
350 West Fourth Street
New York 14, N. Y.

Without obligation on my part, please reserve a place for me in your *home study course on television servicing* and send me full details. No salesman will call. I understand I must be employed in the radio-TV-electronics field to qualify for the course.

Name _____
(Please Print)

Address _____
(Street)

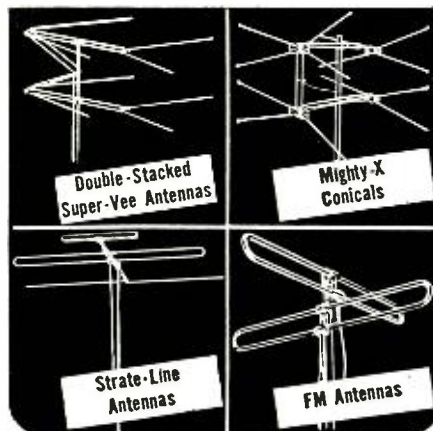
City _____ Zone _____ State _____



8 Good Reasons for you to CHOOSE CORNELL-DUBILIER Skyhawk TV ANTENNAS

One of the reasons for the splendid acceptance of C-D SKYHAWK antennas is the completeness of the line. Whatever the application... whatever the situation... THERE IS A CORRECT C-D ANTENNA FOR EVERY NEED. No need to accept inferior makes or substitute types when the C-D antenna line offers a full variety... each doing a specific job... BETTER!

CORNELL-DUBILIER ELECTRIC CORP.
SOUTH PLAINFIELD, NEW JERSEY

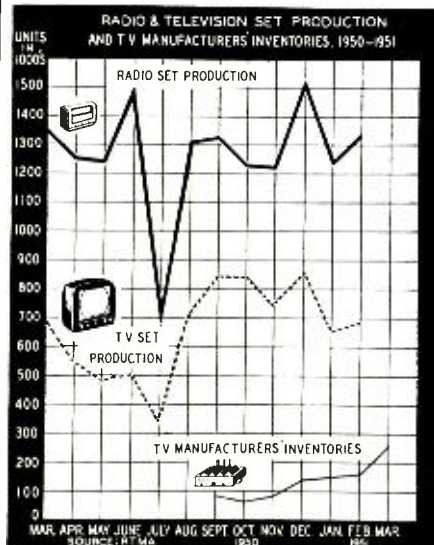


Merchandising & Promotion

RCA has launched a full-scale radio battery promotion stressing that RCA battery sales are made exclusively through radio trade channels. Timed for the opening of the spring-summer portable radio season but keyed to year-round selling, the drive features spot announcements on RCA radio and TV shows urging the purchase of radio bat-



teries from service technicians and dealers. Point-of-purchase displays will also be used extensively. Two unique sales and servicing aids have been developed for dealer use, the RCA battery "fact-finder" index and a mechanical pencil which shows interchangeable types of batteries. These selling aids are available free with the purchase of RCA batteries from distributors.



Walter L. Schott Co. is celebrating its twelfth anniversary with a gift offer of a kit containing five Walsco products for service technicians. The kit will be



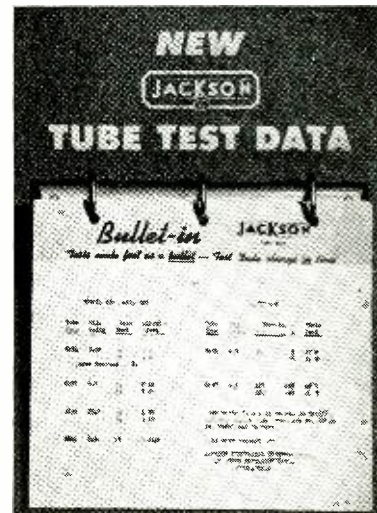
given away free with every \$2.00 purchase of Walsco hardware, chemicals, or accessories, or every \$10.00 purchase of Walsco antennas, during the months of June and July. The offer is available through distributors.

Television Supply Co. of New York City issued a new eight-page antenna and accessory folder which is suitable for mailing.

General Electric Tube Divisions' Advertising Manager, G. A. Bradford, announced a national TV picture tube promotion aimed at the 12-inch tube replacement market. National consumer magazines, radio and television and dealer helps are being used. An illustrated loose-leaf booklet, "Tele-Clues" which aids service technicians in localizing TV circuit defects is included in the promotion.

General Electric has issued a two-color catalog sheet describing its new civil defense receiver. The sheet gives complete specifications of the receiver, which is intended for two-way radio systems.

Jackson Electrical Instrument Co., Dayton, has issued a "Bulletin" holder free to distributors. The holder permits distributors to display data on new tubes in the interim period until a complete new roll chart on tube data is available.



National Union Radio Corp. is offering a new durable indoor fluorescent sign to service technicians and dealers. Steel



constructed with a gold-bronze finish, the sign may either be hung by chains or displayed on the counter. It is available from distributors at the non-profit price of \$8.95 plus shipping charges.

Sprague Products Co. introduced a new double-purpose package, holding five Telecap molded tubular capacitors of the same value. The new "Domepak"

RADIO-ELECTRONICS for

With every \$2.00 purchase of WALSCO products or \$10.00 worth of antennas.

it's

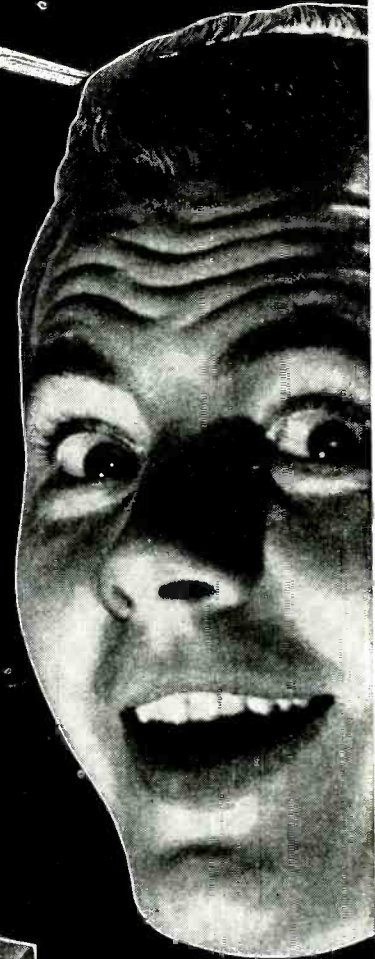
FREE!

WALSCO

12th

ANNIVERSARY

GIFT package



...all YOURS!

- WALSCO LUBRICATOR
- WALSCO CONTACTENE INJECTOR
- WALSCO TUNERLUB
- WALSCO NO-OX
- WALSCO CEMENT



A TERRIFIC FREE OFFER!

Each item in this attractive GIFT package will be useful to you. And it's yours at *no extra cost!* All 5 handy items in this package are from the famous line of WALSCO quality products. Every radio and TV service man will want one. Get yours today!



\$2.00 value FREE

with every \$2.00 purchase of WALSCO products... or \$10.00 worth of WALSCO antennas.

FREE GIFT PACKAGE available at your local parts jobber. *Get yours today!*

WALSCO

WALTER L. SCHOTT CO.
Los Angeles 18, Calif. • Chicago 6, Ill.

New Revolutionary Aid...

Superior's TELEVISION BAR GENERATOR



THROWS AN ACTUAL BAR PATTERN ON ANY TV RECEIVER SCREEN!!

Two Simple Steps

- 1.** Connect Bar Generator to Antenna Post of any TV Receiver.
- 2.** Plug Line Cord into A.C. Outlet and Throw Switch.

RESULT: A stable never-shifting vertical or horizontal pattern projected on the screen of the TV receiver under test.

Features:

1. Provides linear pattern to adjust VERTICAL linearity, height, centering.
2. Provides linear pattern to adjust HORIZONTAL drive, width, peaking, linearity, centering.
3. Provides vertical sweep signal for adjusting and synchronizing vertical oscillator discharge and output tubes.
4. Provides vertical signal to replace vertical oscillator to check vertical amplifier operation.
5. Provides horizontal sweep signal for adjusting and synchronizing horizontal oscillator A.F.C. and output tubes.
6. Provides horizontal sweep signal to check H.V. section of fly-back and pulse operating power supplies.
7. Provides signal for testing video amplifiers.
8. Can be used when no stations are on the air.

Specifications:

Power Supply: 105-125 Volt 60 Cycles
Power Consumption: 20 Watts
Channels: 2 - 5 on panel, 7 - 13 by harmonics
Horizontal lines: 4 to 12 (Variable)
Vertical lines: 12 (Fixed)
Vertical sweep output: 60 Cycles
Horizontal sweep output: 15,750 Cycles

TV BAR GENERATOR COMES COMPLETE WITH SHIELDED LEADS AND DETAILED OPERATING INSTRUCTIONS.

ONLY

39⁹⁵ NET

Manufactured by: SUPERIOR INSTRUMENTS CO. New York 7, N. Y.
DISTRIBUTED BY THESE LEADING JOBBERS:

ALABAMA
Steel City Supply Co., Inc., 600 North Seventh St., Birmingham 4, Ala.

ARKANSAS
Comerly Distributors, 1201 East 2nd St., Little Rock, Ark.
Martin Wholesale Radio Supply, 1207 West Kingshighway, Paragould, Ark.
Rye Wholesale Co., 117 W. Washington Ave., North Little Rock, Ark.

CALIFORNIA
Arrowhead Radio & TV Supply Co., 1216 "D" St., San Bernardino, Calif.
C. C. Brown Company, 61 Ninth St., San Francisco 3, Calif.
California Electronics Supply, Inc., 11801-03 West Pico Blvd., West Los Angeles 64, Calif.
Cass Altshuler Co., 6038 Telegraph Ave., Oakland 9, Calif.
Dealer's Wholesale Supply, 15 E. Simpson St., Ventura, Calif.
E. M. Kemp Company, 1115 B Street, Sacramento 14, Calif.
Fred S. Dean Co., 969 American Ave., Long Beach 13, Calif.

Henry Radio, 11240 West Olympic Blvd., Los Angeles 25, Calif.
Mac's Radio Supply, 8220-22 Long Beach Blvd., South Gate, Calif.
Market Radio Supply Co., 1240 Market St., San Francisco 2, Calif.
Offenbach-Reimus Co., 372 Ellis St., San Francisco 2, Calif.
Pacific Radio Exchange Inc., 1407 Caluena Blvd., Hollywood 28, Calif.
Pacific Wholesale Co., 116 Ninth St., San Francisco 3, Calif.
Radio Parts Sales Co., 5220 So. Vermont Ave., Los Angeles 37, Calif.
Radio Parts Supply Co., 281 Ninth St., San Francisco 3, Calif.
Radio Specialties Co., 1956 So. Figueroa St., Los Angeles 7, Calif.
San Francisco Radio & Supply Co., 1282 Market St., San Francisco, Calif.
Scott Radio Supply, 266 Alhambra Ave., Long Beach 2, Calif.
Silvergate Radio Supply, 2255 India St., San Diego 1, Calif.
Universal Radio Supply Co., 1727 So. Los Angeles St., Los Angeles 15, Calif.
Valley Electronic Supply Co., 1302 W. Magnolia Blvd., Burbank, Calif.
Jack Warren, 907 Yosemite Blvd., Modesto, Calif.

See following page for more distributors

INDISPENSABLE!
PHOTOFACT BOOKS



Photofact Television Course. Covers TV principles, operation and practice. 216 pages; profusely illustrated; 8 1/2 x 11". Order TV-1 Only \$3.00

Television Antennas. New 2nd edition. Describes all TV antenna types; tells how to select, install, solve troubles. Saves time; helps you earn more. 200 pages; illustrated. Order TAG-1 Only \$2.00

Television Tube Location Guide. Accurate diagrams show position and function of all tubes in hundreds of TV sets; helps you diagnose trouble without removing chassis. 200 pages; pocket-size. Order TGL-1 Only \$1.50

1949-1950 Record Changer Manual. Vol. 3. Covers 44 models made in 1949, including multi-speed changers and wire and tape recorders. Original data based on actual analysis of equipment. 286 pages; 8 1/2 x 11"; paper-bound. Order CM-3 Only \$3.00

1948-1949 Changer Manual. Vol. 2. Covers 45 models made in 1948-49. Paper bound. Order CM-2. Only \$4.95

1947-1948 Changer Manual. Vol. 1. Covers 40 post-war models up to 1948. Order CM-1 Only \$4.95

Recording & Reproduction of Sound. A complete authoritative treatment of all phases of recording and amplification. 6 x 9". Order RR-1 Only \$5.00



Post-War Audio Amplifiers. Vol. 2. A complete analysis of 104 well-known audio amplifiers and 12 well-known tuners made in 1949-50. 368 pages, 8 1/2 x 11". Order AA-2 Only \$3.95

Post-War Audio Amplifiers. Vol. 1. Covers 102 amplifiers and FM tuners made through 1948. 352 pages. Order AA-1 Only \$3.95

Auto Radio Manual. Complete service data on more than 100 post-war auto radio models. Covers over 24 mfgs. 350 pages, 8 1/2 x 11". Order AR-1 Only \$4.95

Communications Receiver Manual. Complete analysis of 50 popular communications models. 246 pages, 8 1/2 x 11". Order CR-1 Only \$3.00

Radio Receiver Tube Placement Guide. Accurate diagrams show where to replace each tube in 5500 radio models, covering 1938-1947 receivers. 192 pages, pocket-size. Order TP-1 Only \$1.25

Dial Cord Stringing Guide. Vol. 2. Covers receivers made from 1947 through 1949. Shows you the one right way to string a dial cord in thousands of models. Pocket-size. Order DC-2 Only \$1.00

Dial Cord Guide. Vol. 1. Covers sets produced 1938 through 1946. Order DC-1 Only \$1.00

Radio-TV Industry Red Book. 2nd Edition. Complete data on replacement parts for 22,000 sets made 1938-1950, including valuable TV information. Covers all major replacements. Over 600 pages. Only \$3.95



Making Money in TV Servicing. Tested, proved methods of operating a profitable TV service business. Written by Eugene Ecklund, B. E. E., former manager of the National Service Department, Allen B. DuMont Laboratories, Inc. Covers planning, financing, work control, purchasing, service charges, advertising—plus much more. Own this practical guide to success now. Over 130 pages. Order MM-1 Only \$1.25

Order from your Parts Jobber or write direct to
HOWARD W. SAMS & CO., INC., 2201 E. 46th St., Indianapolis 5, Indiana

HOWARD W. SAMS & CO., INC.



consists of a clear plastic dome mounted on a heavy cardboard backing. It is available through distributors.

Servicing Business

Allen B. Du Mont Laboratories, Teleset Service Control Department, has scheduled 450 television service clinics to be held on a national scale during the coming months. The clinics will be run by Du Mont regional service managers and field representatives in conjunction with the Receiver Sales Division's distributors. Meetings include lectures, a film on service and a question-and-answer period.

The Admiral Corporation has completed a series of servicing classes for independent and dealer service technicians. Factory specialists conducted the series, which was designed to train about 4,000 men.

Raytheon Manufacturing Co. announced that Main TV Supply Co., Akron, Ohio, was the latest parts distributor to be appointed as a sponsor of the Raytheon Bonded Dealer Program for the area covered by the company's Port Huron, Mich., branch.

Materials Conservation

General Electric is using an aluminum-clad material for the anodes of some of its receiving tubes to conserve scarce nickel. The company also is working on another conservation project to substitute specially processed terratex for mica spacers in these same tubes.

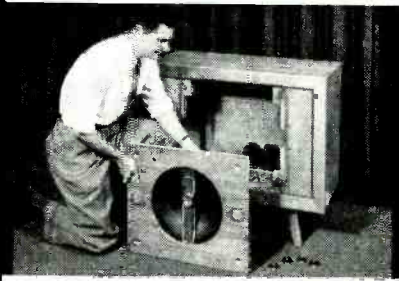
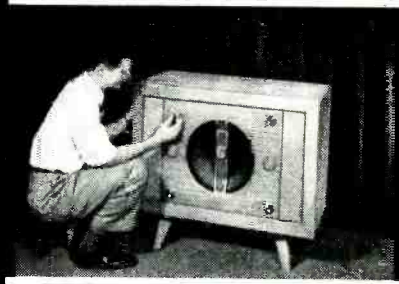
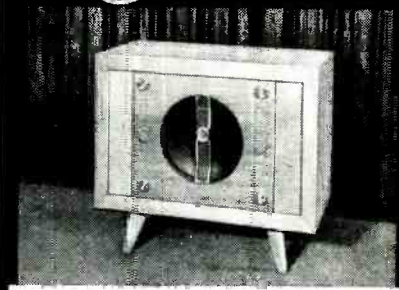
Dr. Burton Browne, president of the Burton Browne Advertising Agency, which handles the advertising of many companies in the electronics field, has designed a shield for inclusion in advertisements during the defense effort. The symbol which incorporates the slogan, "Conserve Critical Materials," is available without obligation to all advertisers.

New Plants & Expansions

National Union Radio Corp. purchased 50 acres of land in northeast Philadelphia as a site for a new electronics center. Construction has already begun on the first unit at a total investment of over six million dollars. It is expected to be completed around the end of 1951.

Radion Corp., maker of TV antennas, has purchased a new plant in Chicago to double its production capacity. The

FOR FINE SPEAKERS
World's Finest
Reproducer Cabinet
by **Jensen**



These new Customode Imperial Reproducer Cabinets combine fine acoustic performance with beautiful modern styling and new features for convenience. Speaker is easily, quickly installed or removed from the front. Adjustable Base Reflex port. Optional protective grille assembly furnished. Positive anchor nut attachment of speaker to baffle — no wood screws. Fine mahogany veneer, Blende or Cordovan finish. Ask for data sheet 161.

Jensen
MANUFACTURING CO.
Division of The Muter Company
6601 SO. LARAMIE, CHICAGO 38

RADIO-ELECTRONICS for

new plant adds 25,000 square feet to the company's present 23,000 square feet. Raytheon Manufacturing Co. will build a new plant in Quincy, Mass., to manufacture subminiature tubes for military use. The new plant will add 86,000 square feet to the company's factory space. Partial production is scheduled to begin in the fall of this year.

Tung-Sol Lamp Works has purchased a plant in Washington, N. J. It will add over 100,000 square feet to the company's present facilities in Newark, N. J.

Crest Television Laboratories, Inc., manufacturers of electronic test equipment, have opened new quarters in Far Rockaway, N. Y.

P. R. Mallory & Co. and Sharon Steel Corp. formed a jointly owned subsidiary, Mallory-Sharon Titanium Corp., to develop, produce, and market titanium and titanium alloys.

Sylvania Electric Products will build a new \$1,000,000 plant in Burlington, Iowa for the manufacture of radio receiving tubes. The plant, which will add 100,000 square feet of manufacturing space to the company's properties, is the third construction announced by Sylvania since the beginning of the year. W. A. Weiss, manager of Sylvania's Emporium, Pa., plant was named to head the new Burlington plant.

Jerrold Electronics Corp., manufacturer of multiple television antenna systems, has moved its production laboratory and office facilities to a new and larger plant in Philadelphia.

Workshop Associates, Inc., of Needham Heights, Mass., has become a subsidiary of The Gabriel Co. (parent company of Ward Products).

Technical Appliance Corp. completed an addition to its Sherburne, N. Y. plant which adds 65,000 square feet of factory space.

Associations

The Antenna Manufacturers Association was recently organized in New York City. M. S. Roth of Radiart was elected president, H. Harris, Channel Master, vice-president, and Ed Finkel, JFD Mfg. Co., treasurer.

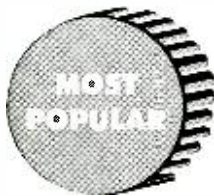
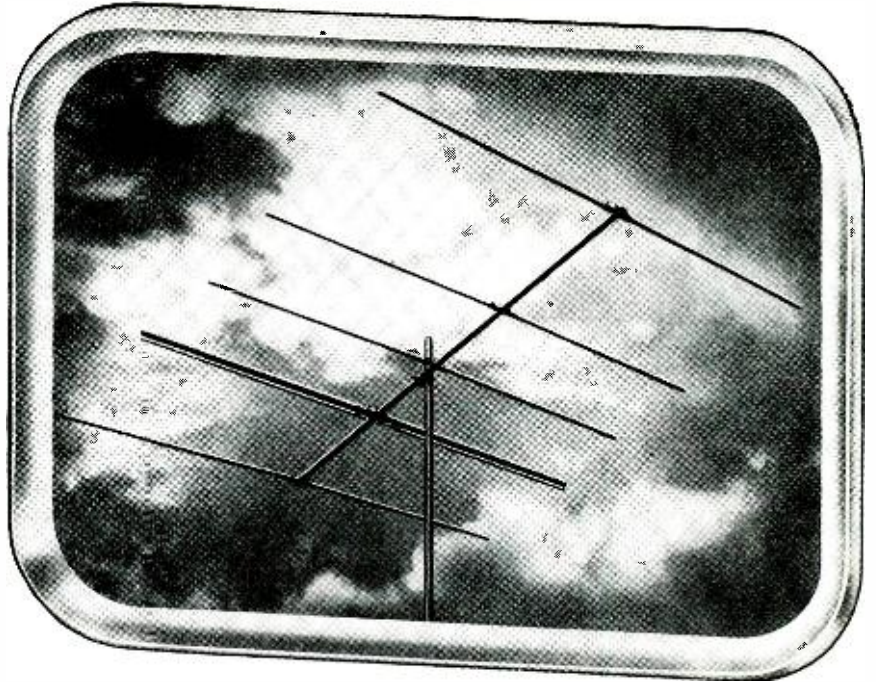
The National Association of Cathode-Ray Tube Manufacturers was formed recently in New York City. Charles E. Cohn, Arcturus Electronics, was elected president; Jacob J. Samuels, Sheldon Electric Co., vice-president; Lester A. Landeau, Television Tube Research Laboratories, secretary; and Thomas A. Stave, Eureka Television & Tube Corp., treasurer.

Business Briefs

... Hytron Radio & Electronics Corp. and the Columbia Broadcasting System, Inc. jointly announced that CBS will acquire the assets and business of Hytron and its subsidiary, Air King Products, subject to the approval of stockholders. Hytron and Air King will continue operations under present management and several top officers of both companies will become directors of CBS.

—end—

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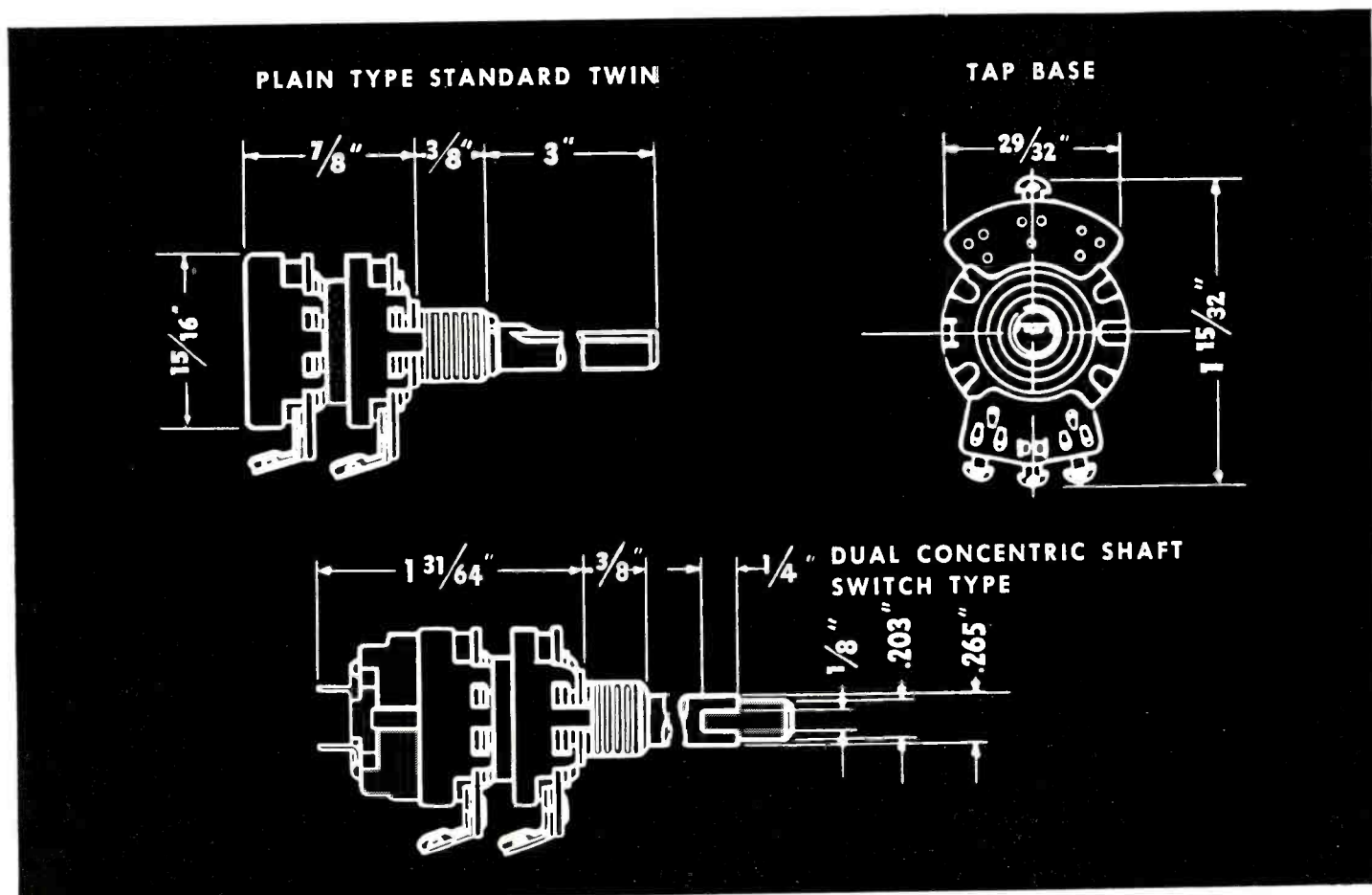
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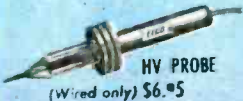
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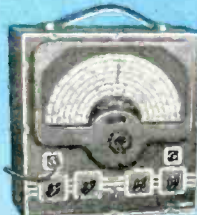
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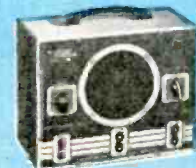
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BIO-ELECTRONICS

. . . *A vast field beckons the researcher* . . .

By HUGO GERNSBACK

BIOLOGICAL Electronics, one of the newer branches of the science, is also one of the fastest expanding ones. More and more we are coming to realize that most life processes are either linked with electronics or are electronic themselves. This is true of animal as well as of plant life.

Scientists all over the world are busy unraveling these processes, so that we may not only learn more about life and its secrets, but apply the new-found knowledge to man's progress.

Biological electronics is a fascinating science with an incredibly vast future. It pays rich dividends to all researchers who embark on its fast-moving stream. For its exploitation we require many new and refined tools; new and more sensitive electronic instruments; broader knowledge of atomic and nuclear forces as applied to biological processes. But all these will come in time to help us toward the progress for which we now grope.

Many years ago it was found that carrier pigeons lost their sense of direction when flying near broadcast stations. Evidently there is a direct relation between the sense of direction and radio waves. So far we have no conclusive answer to this puzzling phenomenon, though some encouraging results have been obtained by researchers.

The animal brain produces a pulsating electrical current. This can readily be recorded with the electroencephalograph. Tumors and brain injuries produce variations in these currents. Man's thoughts generate a different type of pulsating current. But we do not know exactly *how* these currents are produced.

The same is true of the electric eel, (*Electrophorus* [*Gymnotus*] *electricus*) and other electric fishes. From an anatomical point of view we know a great deal of the animal brain as well as of the "electrical battery" that generates the eel's current, but when we try to reproduce the eel's electric battery, we fail dismally. Nor do we know why one type of electric eel can stun and at times electrocute a horse that is standing in a river—yet the submerged eel is not even hurt by the deadly current it generates.

The researches conducted at Duke University by Professor J. B. Rhine have convinced many scientists that some people can communicate over

long distances by telepathy. It would seem that the human brain is capable of producing some type of wave motion or force capable of traversing hundreds and often thousands of miles. So far we have no instruments to intercept or record such waves or force. But the Duke scientists have been working on the problem. It is certain that they will find the answers in the years to come.

Professor H. W. Lissmann of Cambridge, England, recently investigated a "radar-guided" fish. He published his preliminary findings in the magazine *Nature*.

This incredible African fish, *Gymnarchus niloticus*, sent to him by a West African friend, swims forward and backward at will. Lissmann was puzzled as to how the fish always avoided all obstacles in the aquarium tank while swimming backward, no matter how fast its pace. This was the more mysterious since the fish has only one set of eyes—in front.

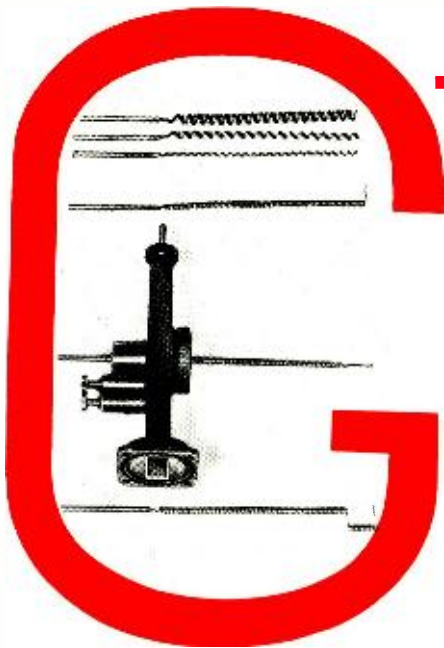
The scientist also had observed the fish's strange, finger-like tail that carries an unusual object. Lissmann concluded that this must be a radar-like biological organ—which indeed it proved to be. When two electrodes, placed in the aquarium were connected with an oscillograph, a series of regular electrical pulses registered on the oscillograph screen every time the fish swam near the electrodes.

When outside-generated electrical impulses were sent over two wires, immersed into the tank, the fish fled. He also fled in terror when a U-shaped loop of copper wire was inserted into the tank near him. When Professor Lissmann finally fed the fish's own electrical pulses back to the aquarium with a second set of electrodes, the little fish attacked them vigorously, evidently mistaking them for another fish of its own species.

At this point the fish died, either from excitement or from an overdose of misapplied electrical forces. We may hope that Professor Lissmann—with a new supply of *Gymnarchus niloticus*—may soon solve the mystery of the little fish's electronic equipment.

It is within the realm of possibility that some of our backward steering politicians could conceivably navigate the better—forward—with a biological radar!

—end—



G-String Transmission and Helical Wave Coils

Two new techniques
replace waveguides

By

SAMUEL FREEDMAN

in u.h.f. circuits

HELICAL coils and simple straight wires can be used as a substitute for waveguides to transmit electromagnetic waves at any frequency. For microwaves, the helical coils can be unwound at their termination to serve as either nondirectional or directional radiators.

The waveguides which these two devices replace are in many cases made to special dimensions and shapes and they are expensive. Waveguides are also narrow-band devices and are rather critical with regard to frequency.

Helical wave coils like those illustrated at the head of this article have been used to replace both rigid and flexible waveguides. They first came into prominence in the development of the broad-band traveling wave tube amplifier. Depending on their termination, they are capable of covering a wide range of frequencies.

More recently, the "G-string" has attracted wide attention because it is even simpler and more economical than either waveguides or helical wave coils, and it covers a wider frequency range with much less attenuation. The G-string makes possible much longer microwave transmission lines having far less attenuation than is now possible with current waveguide techniques.

The G-string, helical wave coil, and the waveguide each have their own advantages and disadvantages, depending on how they are used, so that in many systems all three are used. Neither the helical wave coil nor the G-string have been in use long enough and in a sufficient variety of circuits so that it is possible to tell the full extent of their usefulness. They will probably become most useful at those frequencies where waveguides will be too small (super-high frequencies) or too large (ultra-high or very-high frequencies) to be practical.

The G-string

A G-string (as used in electromagnetic transmission) is simply a long cylindrical conducting wire as illustrated in Fig. 1. Its theory dates back to 1899 when A. Sommerfeld described the possibilities of using such a line for wave propagation. It was put to practical use not long ago by George Goubau and associates of the Coles Signal Laboratory of the Signal Corps.

An enamel-coated copper wire serves admirably as a G-string (No. 12 or No. 8 will do). The dielectric layer of enamel reduces the radial extension of the electromagnetic field so the waves tend to hug the wire in a large number of nonradiating modes. Special launching horns are used to excite such waves in the arrangement shown in Fig. 1. Starting from a coaxial cable, the outer conductor of the cable is flared out as a horn and the central conductor becomes the G-string.

The launching horn acts like a transformer which converts the field of the coaxial cable or waveguide to the sur-

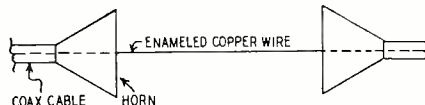


Fig. 1—Sketch of the G-string transmission line. The horns at each end keep the field pattern near the wire.

face wave field and vice versa at the termination. The larger the launching horn, the better will be the transition match. A new set of horns is needed each time the direction of the run is changed. Adding a new horn does not increase the energy at that point, but it does confine the field to the wire as it

extends into its new direction.

The most obvious advantage of the G-string is that it is exceedingly simple. While its full frequency range and attenuation characteristics are not yet fully known, the author was told that, in the study of a 120-foot and also a 600-foot length of G-string, the frequency range was from 200 to 30,000 megacycles and the transmission loss was one-tenth that of a waveguide. The author also had a report that it is possible to convey TV signals over such a line at the actual station frequency. This may mean that the underground coax or the microwave relay stations at vantage points on the horizon are no longer indispensable for network TV. The land-line may come back into its own because it is cheaper, more efficient, and is independent of FCC frequency allocations.

The helical wave coil

The helical wave coil is especially useful for microwaves because it can be used as both a transmission line and a radiator. Energy flows along both the inner and outer surfaces of the helical sheath. The field decreases to zero at the center axis of the helix, so that it can be supported by a rod at its center if necessary.

The circumference of the helix must be small compared to the wavelength if it is used as a transmission line. With the right termination, it will become a radiator. If the circumference of the helix is increased to the order of one wavelength, it becomes a radiator with maximum radiation in the direction of the helical axis, and the field is nearly circularly polarized. This is called the

axial or beam mode. Other modes also can be excited. For example, a helix with dimension not quite large enough for the axial mode will have a conical radiation pattern similar to those in dielectric rods in which the electrical

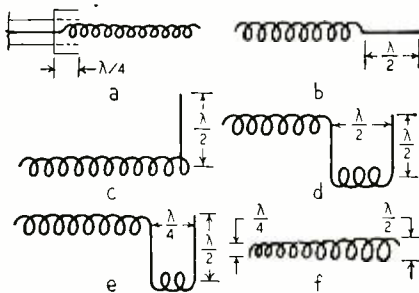


Fig. 2—Circuits using the helical wave coil to get various radiation patterns.

length of the radiator is either too long or too short compared to its physical length. For certain diameters the radiation pattern will be circularly polarized and normal to the helical axis. A linearly radiated field can be obtained by terminating the helix in straight sections. End-fire, broadside, and other multi-element arrays are easily made up by unwinding and winding helical sections.

Circuit *a* of Fig. 2 shows a section of coax terminated by a helical wave coil. The center conductor is wound into the helix and the outer conductor has an additional quarter-wave collar. The circuit is tuned by adjusting this collar to a critical length. If the end of the coil is dipped into aquadag or a graphite filler, it converts the coil to an r.f. load termination.

The circuit of Fig. 2-b may be fed in the same way as circuit *a*, but it terminates with a half-wave straight horizontal section which is a radiator. Circuit *c* is also the same, but it has a vertically polarized antenna termination. Circuit *d* is the same as *c* with a second half-wave element to produce a figure-8 pattern. A cardioid-type pat-

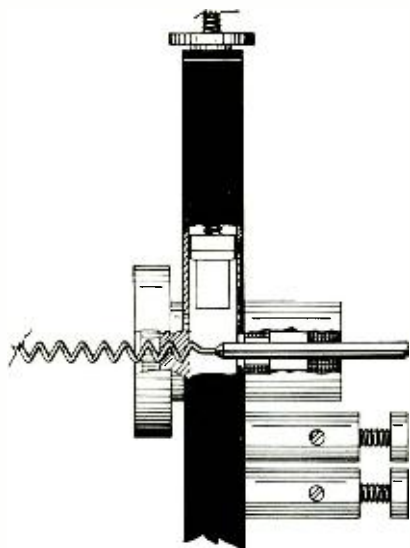


Fig. 3—Cutaway sketch showing how a waveguide connects to a helical coil.

tern is produced by *e*, which is the same as *d* except that the section between the two half-wave radiators is reduced to a quarter wavelength. The coil in *f* has a constantly increasing diameter which produces a circularly polarized pattern.

The helix can be excited by a coaxial cable by gradually winding the center conductor into a tapered helix, and at the same time terminating the outer conductor either by a flared section (similar to that used by the G-string) or by a quarter-wave coaxial choke. The latter is done by using a modified coaxial to waveguide transformer. Fig. 3 shows a typical waveguide coupler.

When used as a transmission line, the helix should be wound to have a pitch of 4 to 10 turns per wavelength, and its diameter should not be greater than 0.2 wavelength. How well the helix serves either as a transmission line or as a radiator depends entirely on how it is made. This is controlled mostly by the

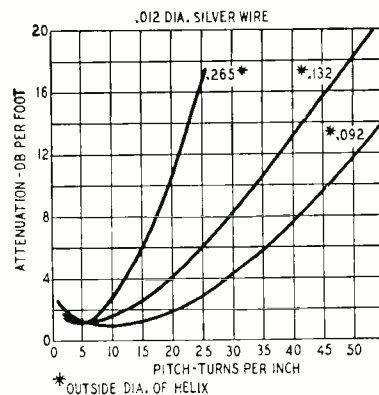


Fig. 4—Attenuation characteristics of a helical wave coil versus its pitch.

diameter of the turns in the helix, the spacing between turns, the length per turn, the total number of turns, the angle of pitch forming the turns, and the diameter of the wire which is used to wind the turns. These factors in turn determine the entire length of the helix.

Fig. 4 shows three curves which give an idea of the characteristics of the helical wave coil. They show how the attenuation losses increase as the pitch of the helix increases. Each curve is for a helix with different outer diameter, and they are calculated for a wavelength of 3.2 cm, which is a common wavelength for many radars.

By increasing the helix diameter to more than 0.2 wavelength, the coil radiates along or between its turns. Two such coils can be used as a coupling device to substitute for the rotating joints required in radar antennas. By selecting the correct diameter and pitch, the helical coil can be made to substitute for costly special waveguide configurations. Flexible helices can be used in place of flexible waveguides and waveguide elbows.

The G-string can be used only as a transmission line. It is not so adaptable as the helical coil, but it is much more efficient. Fig. 5 shows how the two can be used in combination. In this case the

G-string feeds the helical coil which is used as both a transmission line and radiator.

Both the G-string and the helical coil are easy to construct and they are especially useful where cut-and-try methods must be used to get the right circuit. Persons not too familiar with microwave techniques can use them more easily because they do not have the confusing frequency and cutoff characteristics of waveguides. The energy fields are easy to detect because they are not fully enclosed between the conducting surfaces. Further, the same setup can be used to cover a much larger part of the microwave spectrum than can waveguides.

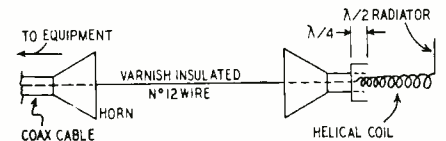


Fig. 5—A G-string transmission line used with a helical wave coil radiator.

The author wishes to acknowledge the work of Glenn Walters of Palo Alto, California, Professor John Kraus of Ohio State University, members of the Signal Corps, and others engaged in research and development of helical wave coils and G-string lines.

—end—

POLICE RADIO TRICK

With the help of handie-talkies, San Francisco police outwitted a "smart" ex-convict by trailing him for over 60 miles, not in one, but in *three* cars as he toured the city casing prospective places for stickups.

The ex-convict, Victor F. Witaschek, had kicked in a store window to get a shotgun which he planned to use for the stickups. Somebody got his license number, and police quickly got on his trail. This was their chance to test the new Motorola Handie-Talkies the department had. They operate at very high frequencies and have a range of about 30 blocks.

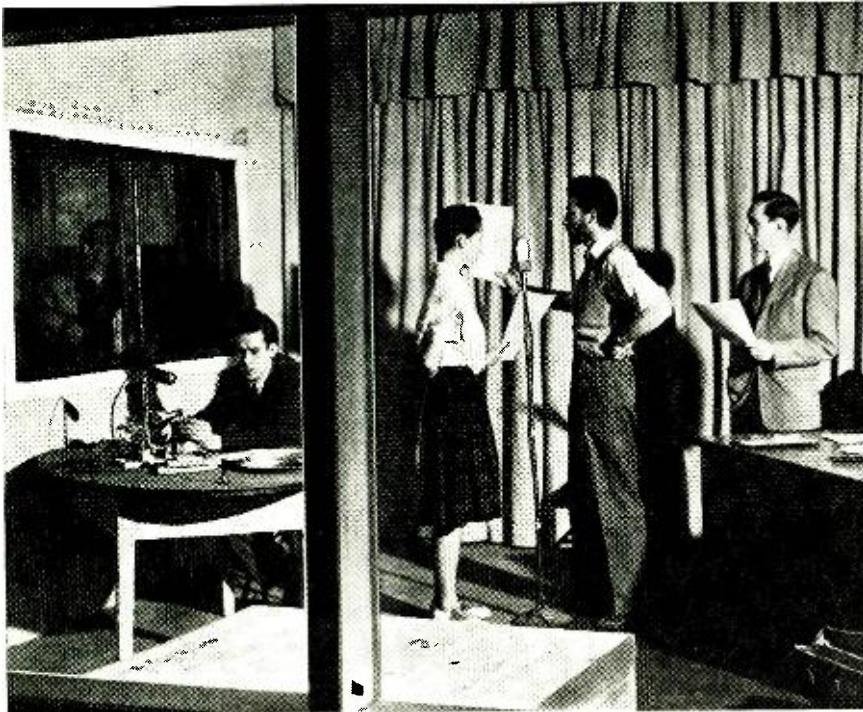
Witaschek drove off. Car No. 1 got on his tail, with Car No. 2 well behind and Car No. 3 running on a parallel street. Before Witaschek could get suspicious, Car No. 1 took a turn and Car No. 2 took over. Witaschek took the usual precautions. He made a sudden turn. The police car behind him kept going straight but passed the word to the car in the parallel street. For over two hours the chase went on like this—like hounds after a rabbit.

Nothing looked good to Witaschek, so he went home to try again another night. The police would have liked to nab him in the act, but rather than let him get a chance to shoot somebody with the shotgun, or to saw the barrel off the \$200 duck weapon, they picked him up when he got home. He was so astonished when they detailed his 60-mile tour that he did something a "smart" boy seldom does. He confessed.

—end—

Wired-Wireless Covers Campus

By R. H. VanHAAGEN



Student actors rehearse a radio show in the studios of Marietta College's campus radio station. Engineer and producer direct show from booth at left.

MANY schools, colleges, and even community housing centers have turned to a little-known phase of radio for inexpensive communication and entertainment. Although nonradiating radio-frequency carriers are well known to the electric power and telephone companies, automatic coin machine manufacturers, and other such groups, material has not been readily available to do any sort of a job in applying these principles to the fields of education and entertainment.

This was the problem which faced the Marietta (Ohio) College Radio Department when it decided to begin wired-wireless broadcasting. Careful analysis of the situation led to a successful program for student instruction in the technical aspects of engineering a broadcast, such as script writing and sound effects, and also provided experience in the electronic aspects, such as cueing of sound effects, fading of microphones and music, and placement of microphones.

Wired-wireless broadcasts have been aired daily, Tuesday through Saturday, from 6:30 to 9:00 pm. An interesting variety of programs is carried, including such campus shows as "Table-Hopping at the PX," a personal interview remote from the student center, and the very popular "Music to Study By." Daily programs are also broadcast from the local Mutual Network outlet, WMOA, over a leased telephone circuit, giving the students an opportunity to reach a greater audience than possible

by carrier-current transmission alone.

Carrier-current transmission, or wired-wireless, as it is more often called, is the transmission of a modulated radio-frequency carrier over a conductor (quite often a power circuit), so that only a specified point or area receives the signal. The wire acts as an antenna feeder, reaching to within a few inches of the receiving antenna, in the case of a power circuit. It differs from a telephone circuit in that no special line is needed, and in that the modulation must be removed from the carrying signal before it can be understood.

For home receivers, the transmitted carrier must lie within the broadcast band, where the signal may be received in the same way as any other broadcasting station. To regulate the number and types of stations on the air, the Federal Communications Commission permits no unlicensed radiation except at experimental frequencies. A well-designed carrier-current system avoids this radiation and still permits communication over a limited area. Usually the coverage is restricted to the power circuits serviced by the same transformer that supplies the transmitter.

Design points

The two main difficulties of carrier-current transmission are obtaining sufficient coverage and at the same time keeping the radiation level down to a legal maximum to avoid interfering with other services in the vicinity.

The first problem is easily solved by providing enough r.f. power to cover the desired territory or to reach the far end of the line. Now the second problem enters. The FCC regulations effectively limit the power an unlicensed carrier may use to 15 microvolts per meter at a distance (in feet) represented by 157,000 divided by the carrier frequency in kilocycles. Even within this limit, *no interference may be caused to any other service.*

As can be seen from the graph of Fig. 1, if we should use a higher frequency, transformer and other losses would be lower and the amount of power necessary to reach a given point would be less; at the same time, the radiation into space would increase at a greater rate as the frequency was increased. Thus the graph demonstrates that a lower frequency will allow us to use more power before exceeding the radiation limits. It shows purely relative values; it is impossible to calibrate the ordinates because conditions vary widely in each location.

According to agreement, all broadcast receivers are supposed to tune at least as low as 550 kilocycles. A canvass made of all radio shops in the author's community brought to light the surprising fact that nearly all home radios tune as low as 530 kc. Therefore, everyone would be able to receive a signal at 540 kc, which is below the standard broadcast band.

From this point the design of a transmitter for the radio department of Marietta College was finally started. We knew that we wanted a transmitter

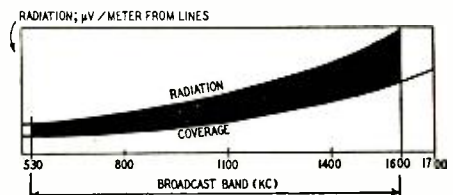


Fig. 1—Graph showing the increase in radiation and coverage with increase in frequency. These curves are relative only and were plotted experimentally.

delivering a maximum of 5 or 6 watts into our line feeders, at as low a frequency as was practical, at 100% modulation.

Planning the transmitter

The power-amplifier tube was chosen first. A beam pentode such as the 6V6-GT seemed best, and was readily available in surplus stocks. This tube requires very little grid drive, so that a buffer would not have been necessary. To maintain as much stability as possible, however, it was thought advisable to include the buffer, perhaps using a

dual-purpose tube for the oscillator and buffer, as is shown in Fig. 2. A 6SC7 high-mu duo-triode was used as a combined oscillator and untuned buffer, working into the 6V6-GT, which was modulated by paralleled 6V6-GT's. The buffer load L2 is an r.f. interstage coil with its primary removed.

The oscillator circuit in Fig. 2 is the tuned-grid plate-tickler oscillator, usually thought of as being inherently unstable. L1 is a standard broadcast band receiver oscillator coil tuned to 540 kc by a .0015- μ f fixed and a .0004- μ f variable padder in parallel. The frequency shift during line-voltage change and mechanical shock of all L-C tuned oscillator circuits known to the author were checked with the b.f.o. of a communications receiver, and the tickler circuit showed the least shift. An 0D3 regulated supply aided considerably in maintaining frequency.

The coil in the final tank circuit should be about 140 turns of No. 22 enamelled wire wound on a 1½-inch diameter polystyrene form. The secondary consists of about 10 turns wound over the center of the primary and is connected to the output terminals of the transmitter with a short length of twisted wire. C2 should be a transmitting type mica capacitor. C3 tunes the output over a small range. If the range does not cover the desired frequencies, the value of C1 can be changed accordingly.

The modulator section

The audio section in Fig. 2 does not seem exactly conventional at first glance, but there is nothing especially different about it. The dual triode serves to keep the 600-ohm audio line balanced. The output of one side is shunted to

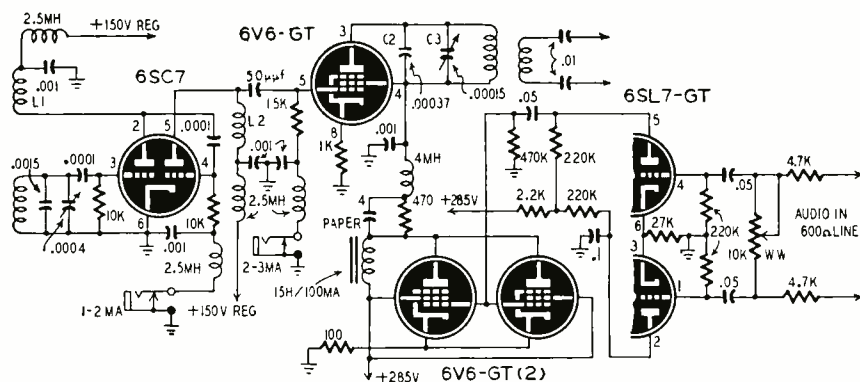


Fig. 2—The r.f. and audio circuits of the transmitter. The output is hooked directly to the a.c. line, or through a filter if harmonic radiation is strong.

ground, while the other side of it feeds into single-ended (parallel) 6V6's.¹

The 10,000-ohm potentiometer in the line is not for line balancing, but for control of the input speech level. The same output level from the monitoring amplifier as was used on the remote lines to the local network-affiliated station was correct for the input of the modulator without attenuation, so the control was set at zero attenuation and left in that position. It is mounted near the audio input socket to shorten the leads.

Transformer input would be quite permissible, but cost again enters the picture. Even if quality were to be sacrificed, the price would be several times that of a resistance-coupled stage.

Heising modulation, slightly modified, is used. An inexpensive replacement type 80-ma 15-henry filter choke is used as the plate load for the parallel 6V6-GT's, the audio voltage being applied through the 4- μ f paper capacitor (not

electrolytic), shunted by the 500-ohm resistor which provides the d.c. path.

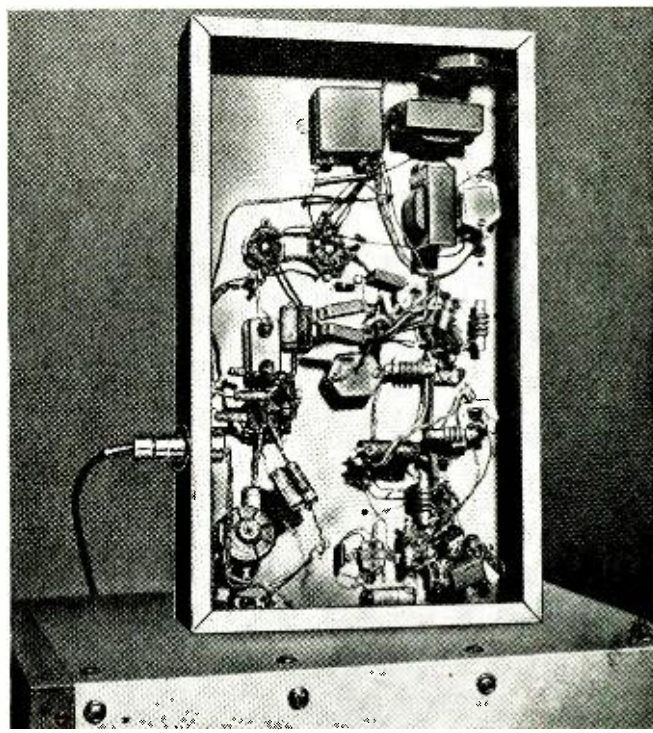
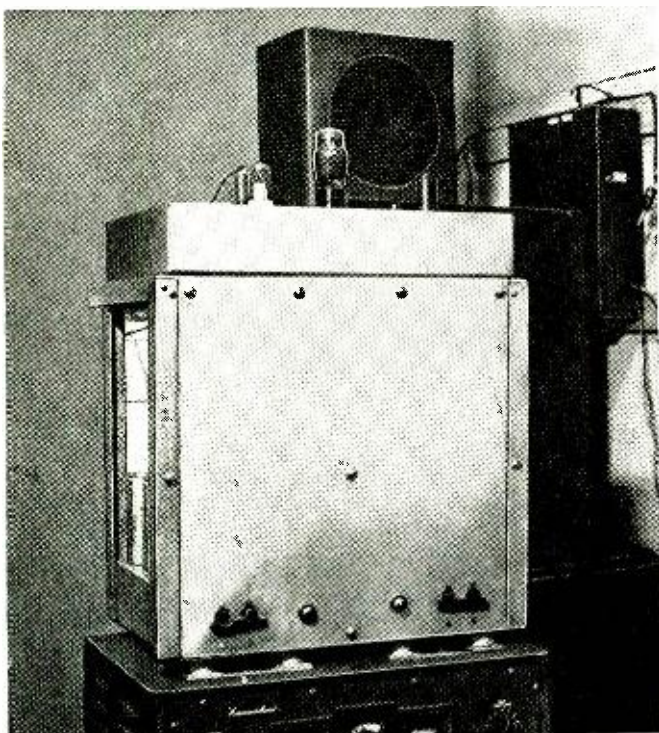
The power supply

The power supply (Fig. 3) is conventional except for the on-off switching, which is by push-button. The four buttons, on-off primary voltage, and on-off plate voltages, are the only controls on the transmitter. Metering is by means of a vacuum-tube voltmeter from the rear.

Tube substitution is simple. Each or all of the 6V6's can be replaced with 6L6's. Except for retuning, no changes are necessary. The 6SC7 oscillator-buffer was temporarily replaced with a 6SN7-GT and a 6SL7-GT, and, although socket changes and retuning were necessary, stability and performance were only slightly reduced.

Further hints and kinks

A receiver equipped with a b.f.o. provides a simple method of determining



The only controls on transmitter panel are push buttons. Bottom view of the transmitter's audio-r.f. chassis.

Television Service Clinic

Conducted By **WALTER H. BUCHSBAUM***

SHORTAGES continue to haunt the service industry and most of them will be with us for some time to come. The worst is probably the tube shortage, a large part of which is covered in this and other issues of **RADIO-ELECTRONICS**. Next to tubes, resistors, capacitors, and other TV parts are getting scarce.

While it is not possible to dream up replacements for every part, a great deal can be accomplished through com-

*Author of *Television Servicing*, Prentice-Hall, 1950

bining parts, modifying circuits, and similar means. For example, if you need a 1,000-ohm, 1-watt resistor, you can use two 2,000-ohm, 1/2-watt resistors in parallel instead. This is a very simple case. But suppose you need a value of resistance which you cannot obtain by substituting two equal ones? Then a

little calculation is required. $R = \frac{R_1 \times R_2}{R_1 + R_2}$

where R is the final resistance and R_1, R_2 are the two parallel resistances. In many instances resistances can be used

in series, in which case the final resistance is simply the sum of the series values.

The problem of correct wattage in unequal parallel or series arrangements may be too bothersome for many service technicians. You will get a safe value by simply using the wattage rating of the original resistor for each substitute. To calculate wattage, remember that it is the square of the current times the resistance, and that in a parallel arrangement of unequal resistors the current through each resistor depends in its resistance. Current equals the voltage divided by the resistance.

Like resistors, capacitors can be arranged in combinations to get certain values. When in parallel, their capacitances add. For example, paralleling a .05-, a .02- and a .03- μf capacitor will give a total capacitance of .1 μf , the sum of all three capacitors. When two equal capacitors are connected in series, their total value is one-half the value of each. Their voltage rating need be only half of the total since only half of the total voltage appears across each. When unequal capacitors are connected in series, the total capacitance is always less than that of the smallest. Their exact capacitance can be calculated from

$$C = \frac{C_1 \times C_2}{C_1 + C_2} \text{ where } C_1 \text{ and } C_2 \text{ are}$$

the series capacitors. Voltage ratings in the case of unequal series capacitors depend on their capacitance, but it will always be safe if each is rated at the total voltage across the series combination.

Coils usually cannot be replaced by combinations except in some cases in the video amplifier where peaking coil values are known. For example, if a 250-microhenry peaking coil is to be replaced, a series arrangement of a 120- and a 180-microhenry coil could be used as replacement. Inversely, to replace a 125-microhenry coil, two 250-microhenry coils in parallel could be used. Be careful to place the coils so there is little or no mutual inductance. One thing to look for in replacing peaking coils is the damping resistor which is often located inside the coil. If such damping resistors are used, a combination must be arranged so that the total of the damping resistors as well as the coils represent the proper replacement.

There are many other schemes for replacing defective parts with combinations of others. As shortages get worse, more and more "tricks of the trade" will become necessary to keep the service industry going. Your TV

WIRED WIRELESS COVERS CAMPUS (Continued from previous page)

the degree of modulation. Zero-beat the b.f.o. with the modulated signal and switch it on and off. At 100% modulation the audio level will be approximately the same for both positions. Although not a perfect check, it is usable. The chassis are standard 19-inch rack size and the cabinet was made from junk-yard aluminum. Remember, the more rigid the frame, the more stable the transmitter. Our unit was shock-mounted on rubber to further reduce shock and vibration.

The transmitter output can be fed directly to the line. If harmonics are too strong, it may be necessary to use a band-pass filter tuned to the carrier.

This transmitter would provide an inexpensive nucleus around which speech, drama, and music departments of the college could build a complete campus station, perhaps leading to the acquisition of an FM transmitter as permitted under the new educational institution regulations.

A word of warning! Many colleges using the carrier-current type of communication have received embarrassing letters from the FCC for exceeding radiation limits. Frequent and careful

field strength measurements should be made, with a good portable or car radio if a field strength meter is unavailable, especially if the conductors run above ground.

Materials for Transmitter

Resistors: 1—100; 1—470; 1—1,000; 1—2,200; 2—4,700; 2—10,000; 1—15,000; 1—27,000; 4—220,000; 1—470,000-ohm, 1/2-watt; 1—10,000-ohm potentiometer.

Capacitors: 1—50; 1—100- μf , mica; 1—370- μf , transmitting type mica; 5—.001; 2—.01; 3—.05; 1—0.1; 1—4- μf , 400-volt paper; 1—150- μf variable; 1—padding for oscillator coil.

Inductors: 1—broadcast receiver oscillator coil; 1—interstage r.f. coil with primary removed; 1—output coil (see text); 4—2.5-mh, 1—4-mh, r.f. chokes; 1—15-h, 150-ma audio choke.

Miscellaneous: 1—6SC7, 1—6SL7-GT, 3—6V6-GT tubes and sockets; 2—closed-circuit jacks; chassis, hookup wire, assorted hardware.

Materials for Power Supply

Resistors: 1—100,000-ohm, 2-watt, 1—3,200-ohm, 5-watt; 1—220,000-ohm, 1/2-watt.

Capacitors: 1—16- μf , 2—32- μf , 450-volt electrolytic.

Inductors: 1—300-0-300-volt, 200-ma power transformer with 6.3-volt, 2-amp, and 5-volt, 3-amp windings; 1—117-volt to 16-volt transformer for relays; 1—10-, 1—15-h, 200-ma chokes.

Miscellaneous: 2—break, 2—make, push-button switches; 1—s.p.s.t., 1—d.p.s.t. 64-ohm a.c. relays; 1—2-amp fuse and holder; 1—5Z3, 1—OD3, tube and socket; 1—NE51 neon lamp; chassis, hookup wire, assorted hardware.

¹ Credit for this circuit belongs to the engineering staff of WOUN at Ohio University, from whom the idea was obtained.

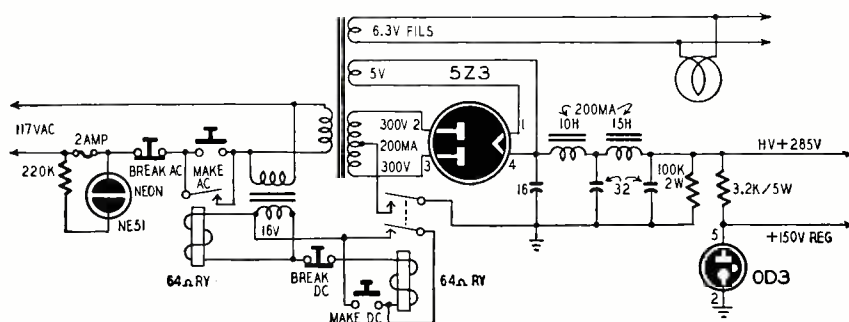


Fig. 3—The transmitter power supply. Push buttons make the circuit foolproof.

Clinic will bring up these substitutions as they come up.

When making any kind of a substitution, the service technician should be careful that the new parts are of at least the same quality as those replaced. If this is not possible, he should so inform the customer.

No brightness control

An Olympic Television model TV950 has a raster. Voltages, including the h.v., check O.K., but the brightness control has no effect, and the picture comes in with the contrast fully on.—Goldstein Radio, Brooklyn, N. Y.

Readjust the ion trap and try another ion trap, as the magnets may have weakened. Remove the rear cover of the cathode-ray tube socket and measure voltages between the green (grid) and yellow (cathode) leads. The grid should be slightly positive with the brightness control in one position and 90 volts negative at minimum brightness. Repeat these measurements with the socket off the kinescope.

If these tests do not show up the defect, you probably need a new picture tube.

Smearred image

Channel 4 comes in clear on an RCA model 6T65, channel 9 is sometimes clear, but channels 5 and 7 smear from left to right.—M. Woronka, Hammond, Ind.

Because the smear is observed only on two channels, it is probably due to the reception of these channels. Reorienting the antenna and checking the lead-in for standing waves may clear up the trouble. Take the 300-ohm line in one hand and slide the hand up and down for about 6 feet. If the picture changes during this manipulation, you may be able to improve reception. Wrap tinfoil around the antenna line at the point giving the best picture.

Intermittent narrowing

The picture on a G-E 810 receiver narrows intermittently. Several vertical bars are slightly noticeable on the raster when width is normal. This condition appeared when the horizontal output transformer was replaced.—Metz Radio Service, Hyattsville, Md.

Try replacing the damper and horizontal output tubes. An intermittent width coil or yoke connection may be at fault. Replace the 56- μ f capacitor inside the yoke, and check the horizontal drive trimmer for intermittent connections.

Rolled-up raster

After operating for about two hours, the bottom edge of the raster on an RCA 6T65 rolled up about $\frac{5}{8}$ inch to form a bright band. There it stays unchanged. We have replaced the vertical oscillator (6SN7-GT) and output (6K6-GT) tubes without result.—H. T. Bumpus, Indianapolis, Ind.

Since replacing the vertical-sweep tubes does not help, try replacing the 5U4-G. Another possibility is a faulty capacitor in the vertical section such as the cathode-bypass capacitor of the

6K6-GT, or the discharge capacitor in the plate circuit of the 6SN7-GT.

Tearing picture

The picture on an Emerson model 600 tears in the lower half, zigzagging back and forth as shown in the photo. When



the tear is severe, there is buzz in the audio. Tearing is most evident on "live" network shows. It is also difficult to get enough contrast without a distorted pic-

ture and a buzz in the audio. We contacted Emerson Radio, who told us that the trouble was severe video overload or a defective 6AL5 phase detector, or poor i.f. alignment. We have replaced the video amplifiers and the 6AL5 phase detector, and have tuned the set, but we still have the tear.—C. Hardin, Indianapolis, Ind.

From your description it appears that you get a very strong signal—so strong, in fact, that you get clipping in the last video i.f. amplifier. To overcome this, use an attenuator network in the antenna lead-in (see the TV Clinic in the March issue of RADIO-ELECTRONICS). Change the sync coupling capacitor or reduce it to a smaller value. Change the values of the video amplifier load resistor at the point of sync take-off. As a last resort, try signal-tracing the sync pulses from the second detector to the horizontal oscillator with a scope and watch for sync pulse compression.

—end—

TV DX—A Prediction of What to Expect during the month of June

The month of June is the most exciting period of the year for the TV dx enthusiast. It will also be a trying one for the technician. The conditions that make for long-distance TV reception can cause service technicians and TV station engineers no end of headaches. Our TV assignments are based on normal operating ranges, and the coverage of any v.h.f. station is likely to be anything but normal in June.

The summer sporadic-E skip¹ season, just getting under way in May, will reach its peak in the middle and latter part of June. Channel 2 reception should be possible over distances between 700 and 1,200 miles almost nightly during the month, and the higher channels, through 6, will be open only slightly less often. Though all parts of the country will see dx frequently, it will occur most often in the South and in the Middle West, the latter because of stations at the proper distances in several directions.

Sporadic-E ionization will be most dense and most widespread in two principal periods around June 12 to 14 and 24 to 27. The greater density will result in shorter skip, bringing in signals on occasion from as close as 300 miles, and simultaneous occurrence of ionization over many parts of the country will make possible multiple-hop effects, particularly during the latter period. Where there are no stations within single-hop range (normally 700 to 1,200 miles) to blanket them, signals from as far as 2,500 miles away may be observed.

The most likely time to try for dx via sporadic-E skip will be around noon or shortly before, and from 5 to 10 pm

local time, though it may be observed at any hour that stations are on the air. Low spots of the day will be mid-afternoon and the hours after midnight.

Tropospheric bending¹ will also be frequent and pronounced during June, though this is not the peak month for this type of propagation. Satisfactory reception range of low-band stations will be extended to as much as twice normal coverage when weather conditions are right, and high-band stations will be seen at distances of several hundred miles on a few occasions.

Best times for tropospheric dx will be the hours around sundown, and after 10 pm. All parts of the country will have tropospheric dx reception, but locations along the Atlantic Seaboard, the Gulf Coast, the West Coast, the Great Lakes areas, and the Lower Mississippi Valley will be especially favored.

Dates for best tropospheric bending are not readily predicted in advance by more than a few days, but a look at the daily weather map in your local newspaper will give you some good clues. A large stable high-pressure area coming over your part of the country will be one of the best warnings that some time spent in trying all channels may be rewarding.

To catch the best of the dx, you will have to do a lot of watching, because no amount of forecasting and weather-map watching will tell you exactly how the signals will hop around. Good dx'ing depends to no small extent on patience, persistence, and a lot of sheer good luck.

¹ "What's the Mystery Behind TV DX?" RADIO-ELECTRONICS, May, 1951.

—end—

HOME BUILT BOOSTER INCREASES TV RANGE

This a. c. powered circuit
produces amazing results

By "DOC" GAINES

OUT where the West really begins, some 235 air miles from Omaha, lies a place that I call home. Great was the amusement in this small community when it became known that I had foolishly purchased a television receiver. However, since that day I have had the last laugh many times, all due to my homemade signal booster. Not only did my booster bring television reception to this area, but it is adding greatly to the pleasure of TV reception in metropolitan Omaha and Lincoln.

The nearest TV stations are KMTV, channel 3, and WOW-TV, channel 6, both in Omaha. The useful audio and video signal input to my receiver was practically zero, indicating the need for a substantial boost in signal strength. For all-around performance, a tuned-grid, tuned-plate circuit using a 6J6 or similar tube seemed best. Such a booster, when used with a well-filtered a.c. power supply, will astound even the most skeptical.

Reception with this booster far surpassed the best results obtained with any commercial boosters. For the fringe-area viewer this booster supplies a signal of usable value and for the metropolitan owner in a weak-signal location its tendency to reduce ignition interference, in both audio and video, makes it a must in all but the best television areas.

The circuit

The power supply and booster can be built on the same chassis with no loss in efficiency. I constructed my boosters on two separate chassis measuring 3 inches wide, 5 inches long, and 2 inches deep. One is for channel 3 and the other for channel 6. Since the physical size of transformers and chokes vary great-

ly, the size of the power-supply chassis depends on the parts you use.

The power transformer must deliver 240 volts d.c. under load. The dropping resistor R1 is optional and is of such a value as to deliver 150 volts d.c. to the plate pins of the tube socket under load.

In my first experiments I used slug-tuned coils from a surplus Army tank transmitter. However, these forms are difficult to obtain, and I find that Mil-len 69045 forms are even better. These forms have a winding length of $1\frac{1}{16}$ inch and a winding diameter of $\frac{1}{2}$ inch. The iron slug is $\frac{3}{8}$ inch in diameter by $\frac{1}{2}$ inch in length. All coil data in this article refers to the Mil-len 69045, but any equivalent form may be used. In using forms other than the Mil-len 69045 make certain the form is long enough so that when the slug is turned completely out no part of it engages the coil windings. Coil windings L2 and L3 are space-wound for the desired channel. The winding is then insulated by a single layer of masking or Scotch tape before applying windings L1 and L4. See the table for coil data. If No. 19 wire is not available No. 18 or 20 may be used. Make certain that L1 is reverse-wound in regard to L2. The same applies to L3 and L4.

Adjustments

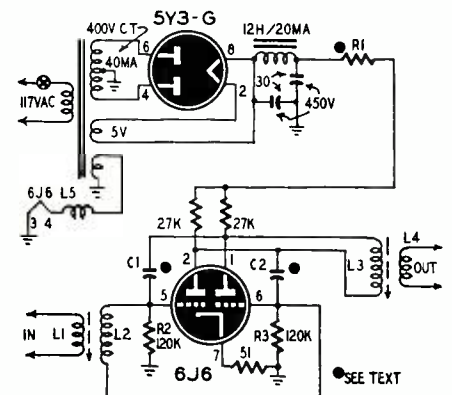
Very little capacitance need be added to prevent oscillation in this circuit. The neutralizing condensers C1 and C2 are constructed of $\frac{1}{8}$ -inch diameter copper tubing $\frac{3}{4}$ inch long with one end soldered to each grid pin at the tube socket. To each plate pin solder a piece of No. 22 well-insulated copper wire. Cross the wires from plate to opposite grid and insert them $\frac{1}{2}$ inch into the tubing to complete the neutralizers. Positive in-

sulation inside the tubing can be obtained by sliding spaghetti over each wire.

To neutralize this circuit, hook a signal generator to the input coil and a v.t.v.m. to the output coil. With the filament voltage removed and the generator supplying a signal of a frequency corresponding to the booster channel to be tuned, vary the distance that each wire extends into the tubing until minimum output is recorded. The null is very definite, although the tuning range is very broad.

By substituting 1.2-megohm resistors for the 120,000-ohm grid resistors R2 and R3 a total gain of 35.2 db is obtained. This is recommended only for extreme fringe areas, as the noise ratio increase exceeds that of the signal. The 23.8 db gain using 120,000-ohm resistors for R2 and R3 will give satisfactory reception up to a distance of 125 miles or more. This value of grid resistance furnishes the best signal-to-noise ratio.

Our next step is adjusting the coils. This is done with the same equipment hookup we used in neutralizing the booster. With the filaments on, we adjust the input coil L1 for maximum output at the video frequency and the output coil L2 for maximum output at the audio frequency. The final adjustments or fine tuning is made with the booster under actual operating conditions.



The circuit of the booster. A separate unit for each channel is recommended.

A separate booster for each channel is recommended, as it is slow work to adjust the slugs properly when changing channels. This is particularly true in fringe areas where any mismatch means a loss in gain.

Any type of switching arrangement that completely disconnects from the circuit when not in use will be found to be satisfactory.

Be sure that the switching arrangement includes provision for removing all plate voltage from the booster not in use. Failure to do so will cause the final adjustments to vary and make true alignment impossible. This is due to a field set up by the unloaded booster. No plate voltage means no field to cause trouble when making final adjustments.

—end—

TV Relay With PCM

By I. QUEEN

PCM or pulse code modulation may be the answer to long-distance relaying of TV programs. With PCM a signal may be relayed any number of times without adding appreciable noise or distortion.

In PCM the TV wave is sampled at twice its maximum signal frequency. For a TV bandwidth of 5 mc, this is 10 million times a second. At each sampling, the wave amplitude is noted. For example, the voltage of a wave may vary at successive intervals of .0000001 second as follows: 17, 18, 19, 19, 17, 15, 13, 12, 13 . . . If this information is transmitted as fast as it is determined, receiver circuits may be designed to re-create the wave.

A varying wave may have an infinite number of possible amplitude levels. However, the wave may be approximated quite closely if it is assumed that only certain standard levels may exist. Experience shows that with 32 standard steps or levels, good picture detail can be obtained. Therefore maximum amplitude is taken as 31 units. Any other amplitude is quantized to the nearest whole number. For example, a level of 12.4 units is taken as 12, while 12.6 becomes 13. This shows that the quantizing process does introduce a slight error (maximum of $\frac{1}{2}$ unit). The error is small, but it could be reduced by using even more units.

The PCM system uses pulses of equal amplitude and width. Any number (from 0 to 31) is represented by a 5-digit code group. A digit is a predetermined position (in its group) which may or may not be occupied by a pulse. The weightings of the pulses are, in their digit order: 16, 8, 4, 2, 1. Thus, if only the first, third, and fourth pulses occupy their assigned positions (and the other two are missing) the group indicates 22 units.

Noise is reduced because pulses can exist only at predetermined instants. The receiver can easily eliminate noise and interference which might arrive between pulses. Pulses occupy only a small fraction of the total time. Furthermore, each pulse has the same amplitude, so there is no problem if noise modulates them.

When a 5-digit code is transmitted through a single channel, a bandwidth of 50—100 mc is required. This can be handled by a microwave relay system. If the digits are transmitted along separate channels, the bandwidth is reduced proportionally and wire circuits may be used.

At present PCM for TV is in the experimental stage.¹ However, it promises to be an important factor in TV relaying in the future.

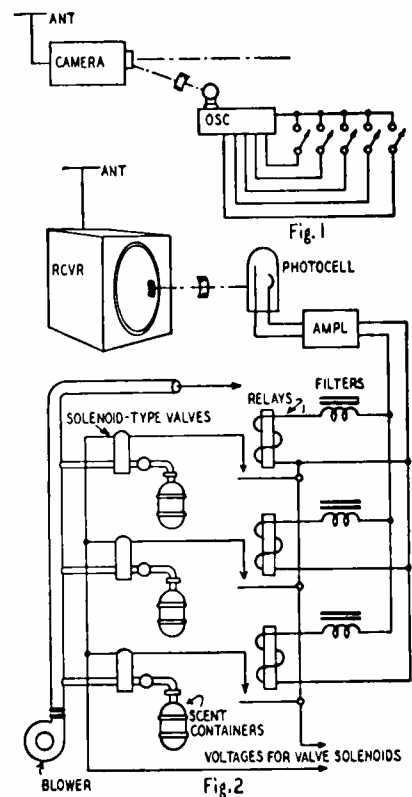
¹ Bell System Technical Journal, Jan. 1951.

SMELLEVISION NOW HERE!

Inventors have sought at different times and in various ways to add the illusion of scent to the arts of the theater. Scents actually have been released among the audience in experimentally produced plays, with some success, but apparently never enough to make scent effects a regular part of the theater. Patents have even been taken out for scent devices for use with motion pictures.

It remained to New York inventor Emery I. Stern to add scent effects to television. The idea no doubt was suggested by friends' remarks about some of the current programs. The theory of his invention is simple. As shown in Fig. 1, an oscillator supplies a lamp with current modulated at a frequency controlled by the switches connected to the oscillator. The lamp throws a beam on a corner of the iconoscope, making a modulated pattern there which is presented in the same corner of the receiving kinescope. It is a comparatively simple matter to detect the signal with a photocell (Fig. 2) and use each frequency to trip its own relay, releasing the appropriate odor into the blower system, which appears quite adequate to spread the smell through the average living room. The scents of course are kept under pressure so that as soon as each valve is opened by its relay the odor will gush out into the blower tube.

More elaborate methods for diffusing the scents would be used in auditoriums. The heating or cooling system of the auditorium might be used to cause air currents of the correct temperature and speed. The appropriate scent mixture would then be added to the air as it enters the room. It would also be very important that the scent be mixed with



the air in the proper proportions, so that it is strong enough for all in the auditorium to smell it, yet not too strong to spoil the desired effect.

How many of the containers will be necessary and what scents are considered the most useful on a television program are matters not mentioned in the patent, which is No. 2,540,144.

—end—

Orientation Wrinkles

The problem of orienting a TV antenna can be as full of surprises as a grab bag at a church bazaar, if the experience of Warren Werneke, of St. Paul, means anything.

He is a video enthusiast who lives in the Twin Cities area of Minnesota, where two TV stations serve the many listeners in St. Paul, Minneapolis and the surrounding territory. The stations are in the same general direction from his home but at a wide angle of separation.

His apartment building is cut off from line-of-sight to these stations by a towering hundred-foot bluff directly to the rear of his home.

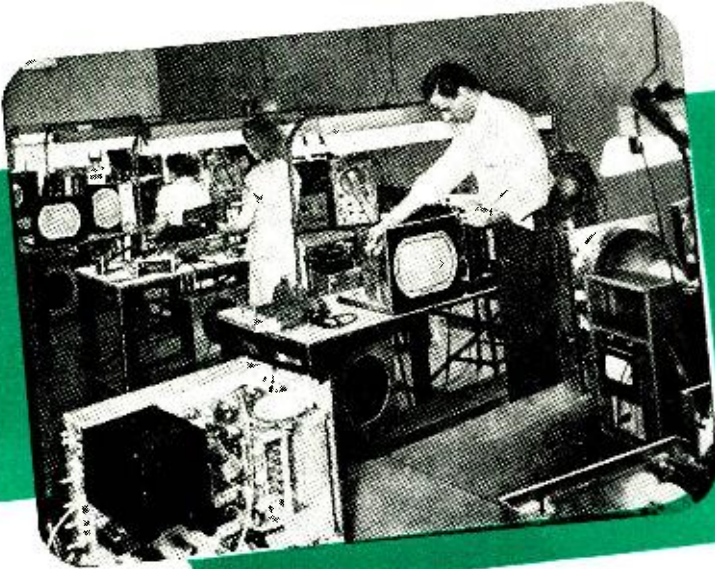
The antenna had been carefully oriented but he wasn't sure that the picture was all it should be. And being a dyed-in-the-wool electronics hobbyist he decided to do something about it. He picked a likely looking spot near the chimney and visualized a field of stand-

ing waves just waiting to be picked up. Tuning to the weaker of the two stations, he adjusted the set, assigned his wife to watch the screen, and told her to call him the instant there was an improvement in the picture. Then, with a fellow enthusiast, he climbed to the roof.

They loosened the guy wires and brackets and lifted the array out of its moorings. They carried it as far as the transmission line would reach, turning it in all directions. No improvement anywhere! Finally, tired and disappointed at the failure to locate a better signal area, they put the antenna flat on the roof, in disgust.

Right then they heard the enthusiastic voice of their TV observer. With all the enthusiasm she could muster she was shouting, "You've got it . . . leave it there . . . don't move it . . . it's a picture right out of this world . . . a perfect picture!"—James H. Bell

TV TROUBLE LEXICON



Continuing the quick-reference TV technote list of common faults

By

JOHN B. LEDBETTER*

Last month the operating peculiarities or typical symptoms of trouble in television receivers beginning with Admiral and continuing through Du Mont were covered. In this issue, we resume with Du Mont and include as many makes of receivers as space permits.

Du Mont

RA-103D. Collapsing of picture vertically (earlier models only). Arc between crossed plate and grid leads under socket of vertical deflection amplifier. Remedy: route one lead inside the socket and other lead outside.

Noise in audio. Arcing in base of 6SN7-GT vertical deflection amplifier (certain makes only). Du Mont would appreciate information on make of tube when this condition is encountered.

RA-104A, 110A. One or more black vertical lines on left side of raster. (Caused by Barkhausen oscillation). Improper adjustment of horizontal drive control. Defective 6BG6-G. Improper antenna lead-in (use coax line only). Transmission-line pickup from power supply. *Note:* Route lead-in as far away from power supply chassis as possible; ground power supply and main chassis together by anchoring to a common copper plate.

RA-105. A.g.c. drift (change of sensitivity as set is operating). Defective 6AT6 a.g.c. amplifier. When this tube is replaced, always readjust the a.g.c. setting.

Low Sensitivity (new set). Check a.g.c.

adjustment. This may have been jarred accidentally during shipment.

RA-105, -106. Loss of vertical sync (humid climates). Open primary in vertical blocking oscillator transformer. Impregnated units are available from manufacturer for use in high-humidity areas.

RA-105B, -108A. Filaments of 5U4-G rectifiers will not light. If 5U4-G's are good, check the .05- μ f cathode capacitor. If this shorts, the regulated voltage of the 5U4-G's will drop very low and give the appearance of no filament voltage. Also check capacitor C302 for possible short, or the wiring going to it for short or arc to chassis.

RA-105B, -108A. Hook (top portion of picture leans to left). Change .01- μ f capacitor C263 (in grid circuit of sync clipper V217) to .05 μ f or 0.1 μ f (0.1 μ f is preferable if heavy ignition noise is not encountered). Later models are modified to allow selection of .01 μ f or 0.1 μ f value as desired.

RA-105B, -108A. Vertical jitter (compression of sync in narrow-band sync amplifier. Where sync compression is cause of jitter, change the 6AU6 narrow-band sync amplifier (V225) to a 6BA6 and change resistor R363 from 22,000 to 15,000 ohms. Remove 100-ohm resistor R356 (connected from pin 7 to ground) and install a 68-ohm resistor in series with a 220-ohm resistor from pin 7 to ground. Bypass the 220-ohm resistor with a .01- μ f capacitor and realign narrow-band amplifier.

For increased gain, replace all 6AG5's with 6BC5's. (A 6BC5 has a higher gain than a 6AG5.)

Microphonic condition. Defective 6AB4 oscillator. Replace tube, or try reversing speaker leads.

Broken top slug in horizontal oscillator transformers. Replacing entire transformer is not necessary. Replacement slugs are available from manufacturer's spare parts department. Usually the top slug is broken and can be replaced simply by removing shield can and extracting slug. Broken bottom slug requires disconnection of transformer leads.

RA-108A. Thumping (with 19AP4 metal picture tube). Warning tag on h.v. lead striking side of tube. Re-position tag.

Hum in audio. Heater-cathode short in 6AL7-GT tuning indicator.

RA-109A, -111A. Low sensitivity on high channels (low oscillator injection voltage). Remedy: Remove Inputuner and dress 1- μ f capacitor C115 as far as possible from bottom of Inputuner chassis. Place close to standoff insulator between 6AK5 converter and 6AB4 oscillator. Do not disturb the position of other Inputuner components.

Weak picture (very snowy); weak sound. Defective 6SN7-GT a.g.c. clamp. If this tube is in a nonconducting condition, the effect may not be apparent immediately but may cause the 6J6 r.f. or 6AK5 mixer to become defective.

Horizontal wavering (top third of picture). Check with TV station. They may be operating with their sync generator on short a.f.c. sync time constant instead of long time constant.

No high voltage. Defective 1X2 h.v. rectifier. Defective 6AK6 horizontal oscillator or 6SN7-GT horizontal saw-

RADIO-ELECTRONICS for

* Engineer, WKRC-TV

maker. Blown ¼-amp fuse in damper plate circuit.

Replacement fuse blows. Check deflection yoke.

Insufficient picture size (horizontal and vertical). Focus control at extreme of range. Defective 5U4-G low-voltage rectifier.

Overloading with normal contrast (near station). Insufficient a.g.c.; signal is overdriving receiver. Check setting of a.g.c. control.

Tearing out (top of picture). Insufficient a.g.c. Check control setting.

Attenuation of weak stations. Excessive a.g.c. Reduce.

RA-111A. Beat interference (black horizontal streaks) on channel 7. Eighth harmonic (175.2 mc.) of sound i.f. (21.9 mc.) beating against video carrier (175.25 mc.) of channel 7 to produce a 50-kc beat. Remedy: Remove filament connection between 6T8 first sound amplifier and 6AQ5 second sound amplifier. Reconnect filament of 6AQ5 to filament tie-point of Inductuner (located near chassis front end, between band switch and contrast control). Connect a 5,000- μ f capacitor between 6T8 filament (pin 4) and ground. Note: Beat can also be eliminated by shifting i.f. from 21.9 to 21.75 mc.

Bright flashes on screen when tuning (most evident on high channels). Noisy Inputuner. Remedy: Lubricate with Lubriplate No. 105 (available from distributor of manufacturer). Apply only to contact rings of Inputuner.

Emerson

600, 639. Insufficient picture size. Defect in low-voltage supply (check for open or decreased value in filter capaci-

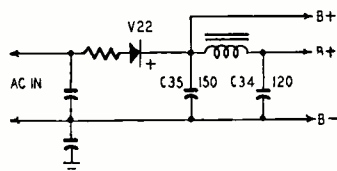


Fig. 1—An Emerson low-voltage circuit. tors C34 (120 μ f) and C35 (150 μ f). (See Fig. 1.)

609. Loss of brilliance (areas of severe dust accumulation). Dirt in projector unit. To clean mirrors, remove one side panel of projection unit. Do not wipe dust; remove with camel's-hair brush and polish with soft lens tissue. Use cleaning spray if discoloration is excessive. Clean top of corrector lens with soft lint-free cloth or tissue. Do not use alcohol or other solvents which might damage or loosen the lens cement.

No high voltage. Defective 6SR7 high-voltage oscillator. Defective 6BG6-G. Shorted h.v. capacitors (5,000- μ f or 2,500- μ f). Defective EY51 high-voltage rectifiers. (The h.v. power transformer,

filter capacitors and EY51 tubes are in a sealed can. A defective unit requires replacement of the entire can).

621, 622, 628, 630. TV operative, FM inoperative. Defective 12AU7 heterodyne oscillator. Defective band-switch contacts, leads, or soldered connections.

Fada

799. Horizontal jitter. Defective 6K6 horizontal oscillator or 6AC7 horizontal sync reactance tube. If replacing either of these tubes results only in temporary correction of trouble, look for leaky .005- μ f capacitor across synchrolock transformer.

Farnsworth

GV-260. Horizontal nonlinearity. Shorted turns in horizontal deflection coils. Shorted .008- μ f capacitor C58, 300- μ h coil L30, or 1,500-ohm resistor

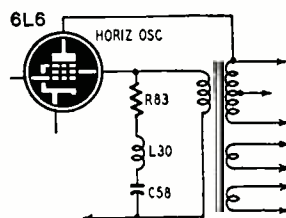


Fig. 2—A faulty part in the horizontal sweep oscillator may cause nonlinearity.

R83 in beam relaxor (6L6 horizontal oscillator) grid circuit. See Fig. 2.

Picture size changes or jumps when vertical centering control is moved. Defective vertical centering capacitor C105.

Picture jumps or moves only to one side when horizontal centering control is moved. Defective horizontal centering capacitor C107B or C107C.

Stationary bar in picture. Hum pickup in video chain. Defective filter capacitor in power supply.

Different shading in top and bottom portions of picture. Poor low-frequency response in video amplifiers. Open or partially open 10- μ f filter capacitors C102A or C102B, open 10- μ f cathode bypass, or open 0.1- μ f coupling capacitor (6AC7 video amplifier). Open .01- μ f cathode bypass capacitor (6SN7-GT d.c. restorer).

Garod

10TZ, 12TZ (Tele-Zoom). Failure of tele-zoom feature. Open connection or defective lead in 20-foot remote-control cord. Dirty switch or relay in receiver.

12TZ20. Intermittent distortion, drift in sound (high channels only). Defective 12AT7 oscillator.

1042G, 1043G series. Picture blooming (when brightness is increased). Increase in value of 470,000-ohm series anode resistor R88. (This applies to all receivers with series resistor in picture-tube anode lead.)

Parasitic oscillations in horizontal sweep oscillator. Change 5,600-ohm suppressor resistor R75 (plate of 6SN7-GT horizontal oscillator) to 4,700 ohms.

General Electric

12T3, 12T4. Audio buzz (on weak signals or with set adjusted for best picture on low contrast). Caused by 41.25-mc trap in second video i.f. Try shunting trap and tuning capacitor C281 with a 5,100-ohm resistor. (Later models eliminated trap entirely.)

800, 805, similar models. Sound bars in picture. Open or decreased capacitance in 5,000-mf capacitor between one end of focus coil and B-minus.

Audio Buzz. Open or decreased capacitance in capacitor C278 (connected between B1-minus and B2-minus).

Alternate light and dark bars, accompanied by foldover. Open 150- μ f filter capacitor C373, causing reduction of B-plus voltage to horizontal output and damper tubes.

White vertical bar in center of screen, wide black vertical bar on either side. Open in horizontal deflection coils (plate side of damper tube).

Raster normal for several seconds, narrows to vertical line, then blanks out. Open 6BG6-G grid resistor.

810. Horizontal stretching of left side of picture, slight foldover. Change in value of 0.1- μ f capacitor C55 in damping-tube cathode circuit.

Light vertical lines. Change in value of 47- μ f capacitor C56 in series with damping tube plate and horizontal deflection coils. Deflection yoke defective (check by substitution).

817, 821. Insufficient width, accompanied by black horizontal bars and decrease in brightness. Shorted 0.47- μ f bypass capacitor C324 in series with horizontal deflection coils. (C324 is paralleled with a 1,200-ohm resistor.)

Faint white vertical line in center of picture. Incorrect adjustment of horizontal linearity control. (This can also cause interference to broadcast sets.)

817, 825. Excessive brightness on left side of screen, suggesting form of foldover. (Left side stretched, faint white lines across rest of picture.) Defective 5V4-G damper.

835, similar models. Sound modulation of oscillator tube. Caused by feedback or mechanical vibration from speaker. Remedy: Shock-mount speaker on rubber grommets or spacers.

The foregoing notes were compiled from the service manuals and service bulletins graciously supplied by the various manufacturers named, and from field notes of the author.

(continued next month)

L-C COMPARATOR AIDS INDUSTRY

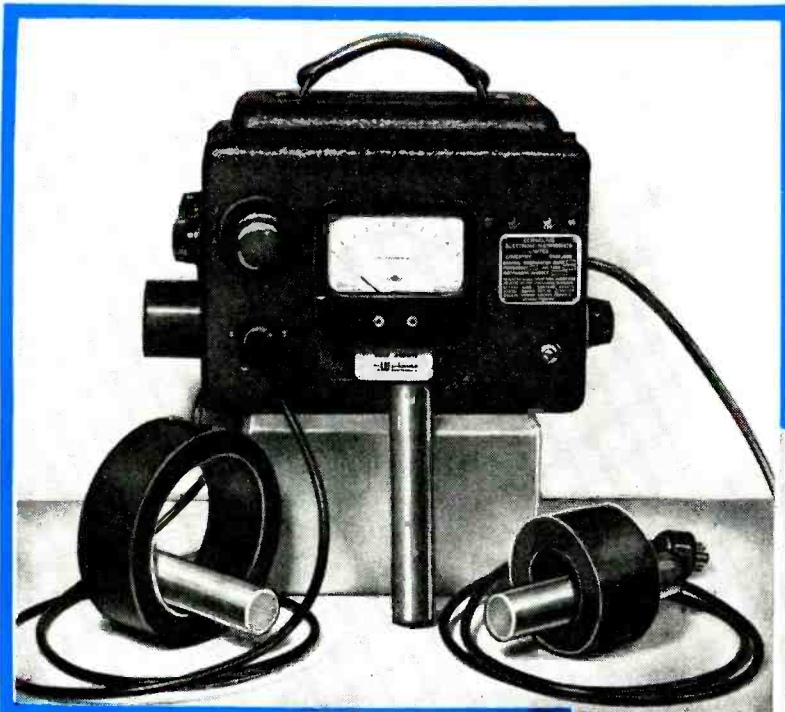


Photo A—The inductance comparator. A sample that is not passable produces a new reading.

PRACTICALLY all industrial measurements made with electronic equipment depend on the measurement of resistance, inductance, or capacitance. Resistance instruments are legion, but they have the great defect that they indicate movement in the subject being tested, and this movement must be transferred to some other device such as a strain gauge. These measurements can be very accurate, but the problem is that stress measurements cannot be made with strain gauges.

This leaves capacitance and inductance. In general, any movement of the subject to be tested can be detected by capacitance measurements, while variations in composition either as alloys or as defects can be found with inductance measurements. Variations in composition of many nonmetallic materials can be detected with the capacitance method, while in some cases variations in dimensions of nonmetallic materials can be detected by a combination of both methods.

The obvious conclusion is that only three instruments are needed for almost all industrial applications: one purely inductive, one purely capacitive, and one combined unit. These three instruments are shown in the accompanying photographs and diagrams. They are a product of Cornelius Elec-

*Cornelius Electronic Instruments, Ltd., Coventry, England

Stress and strain tests using electronic techniques

By

JAMES R. CORNELIUS*



Photo B—The combined inductance-capacitance instrument in a setup to show the stress-strain relation of a steel sample.

tronic Instruments, Ltd., of Coventry, England. They have been used for innumerable different tests from detecting strata variations in oil well borings to measuring the impact of an electron in a cloud chamber.

The inductance comparator

The instrument shown in Photo A and Fig. 1 is the inductance unit. It can be used as a low-frequency, high-frequency, or mixed-frequency unit, and the frequency is changed merely by changing a plug-in coil on the left side of the unit.

When operating at low frequencies, the unit requires a detector coil of suitable size (two such coils are shown in Photo A) to fit the work being tested. It need not match exactly the

dimensions of the work to be tested as long as the work will go into the detector coil easily. This coil plugs into the front of the unit.

Each detector coil has a matching oscillator coil plugged into the side of the instrument. The side coil connects the cathode of the 6J7 to ground, while the detector coil connects the grid of this tube to the cathode to form a very loosely coupled Hartley oscillator. The coupling is adjusted so the 6J7 just barely oscillates. The stronger the oscillation, the less sensitive the instrument becomes.

The detector coil is coupled to the grid of the oscillator tube through one of five capacitors selected by S2. This capacitor has some effect on the strength of oscillation but it also con-

RADIO-ELECTRONICS for

trols the harmonic content of the voltage induced in the test specimens.

The two coils are also coupled to each other through a large variable capacitor C1 in parallel with one of five others selected by switch S1. This gives a capacitance range sufficient to cover practically any frequency required between 500 and 25,000 c.p.s., which is the low frequency range of the instrument.

To use the instrument as a comparator, a known specimen of the material to be tested is inserted in the detector coil and the instrument is adjusted to an approximate frequency suitable for the work.

For either surface tests or for deep penetration tests, S1 being set to minimum capacitance and the potentiometer R1 for minimum screen voltage, the unit is not oscillating. R1 is then turned up until the unit just begins to oscillate as indicated by a deflection of the meter. C1 is then adjusted so the meter reads at about +4 (the meter is a zero-center instrument with five divisions either side of zero).

When another sample of the test material with somewhat different characteristics is inserted in the coil, the meter needle will fall either completely to the left or to the right. If the test specimen is very similar to the known specimen, the meter needle will float because the oscillator will hunt.

As an example, with a 2-inch coil for steel screws 10 mm in diameter and having a carbon content that is allowed to vary by only 0.2%, an operator can select the good from the bad at an average speed of 4,000 per hour without fatigue. After about ten days' training, an unskilled operator can use the instrument to select brasses, aluminum alloys, coppers, plated goods, etc. without supervision by skilled craftsmen.

To operate on high frequencies (25 to 100 kc), the side coil is removed and a single combined Hartley coil with near-center tapping is inserted in the front socket. This type of inspection is for surface defects and plating thickness or adhesion tests. It can also detect grinding or hardening cracks, flaws in wire rope, and numerous other types of fault. The testing need not be observed with the meter as plugs and sockets can be fitted to the instrument for connecting a cathode-ray oscilloscope or automatic recording equipment.

The combined unit

The combined inductance-capacitance unit shown in Photo B is a high-frequency unit extremely sensitive to slight variations in texture and surface conditions of materials.

The operation of this unit is somewhat different from that just described; the discriminating sections are frequency-tuned so the device is actually frequency-modulated. A series of tuned circuits in cascade feed a discriminator circuit and a vacuum-tube

voltmeter. A Hartley coil is plugged into the instrument in the same way as in the inductance unit. The known specimen is then inserted into this test coil and the oscillator is adjusted to the frequency of the tuned circuits or to a suitable harmonic. A variable capacitor in parallel with several fixed capacitors is fitted to give the oscillator a suitable frequency range for the testing to be done.

Variations in composition, position, strains, stresses, defects, cracks, fissures, hardness, and even size of the sample can be used to vary the meter reading. For many tests, such as surface defects in ball or roller bearings, injection pump needles, textile machine needles, etc., the specimens can be fed past the detector at a very high rate, and the results can be observed on a cathode-ray oscilloscope while simple relay circuits can be used to reject faulty parts.

Photo B shows the instrument being used to indicate the stress-strain relationship in a sample of steel under tension in the machine. This setup is actually a static test, but the instrument can also be used for high-speed dynamic testing for tension, torsion, or compression. A cathode-ray oscilloscope then shows the actual stress in the sample, not merely that which is imposed by the machine. Another feature of this electronic stress detection

is the instrument's ability to tell the difference between tension and compression and also reversing torsional stress.

The capacitance comparator

The capacitance unit is shown in Fig. 2 and Photo C. This instrument is pro-

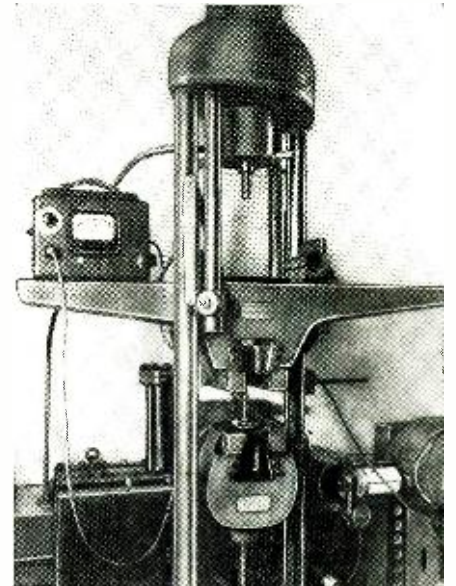


Photo C—The crystal-controlled capacitance unit in a setup for measuring thickness variations of .00001 inch.

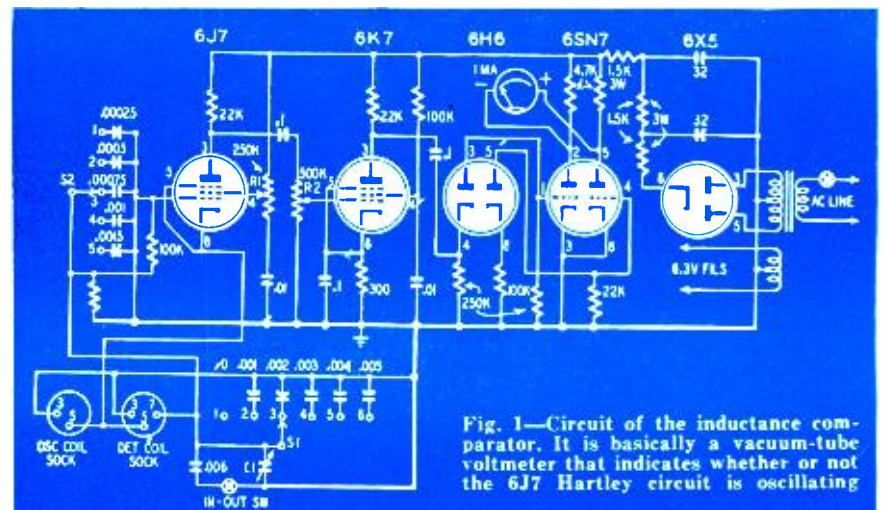


Fig. 1—Circuit of the inductance comparator. It is basically a vacuum-tube voltmeter that indicates whether or not the 6J7 Hartley circuit is oscillating.

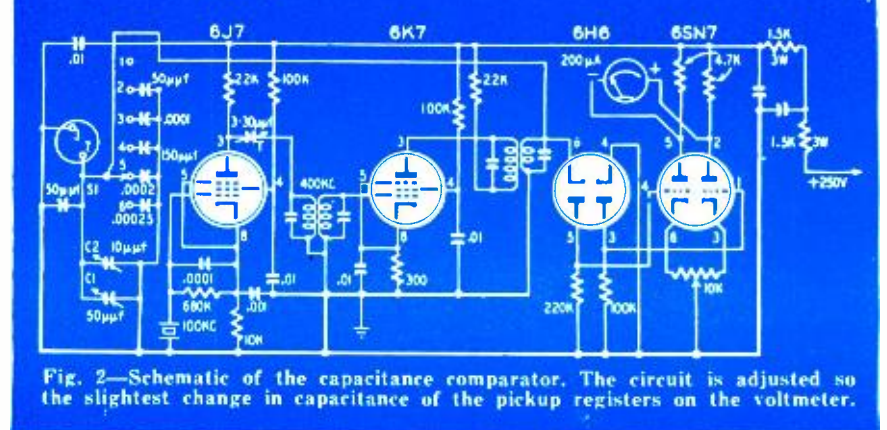


Fig. 2—Schematic of the capacitance comparator. The circuit is adjusted so the slightest change in capacitance of the pickup registers on the voltmeter.

Crystal Spots Radiation

Even in the simplest circuits the cadmium sulfide crystal is highly sensitive as a radiation detector

THE latest of the so-called semi-conductors to make the news is cadmium sulfide (CdS), which promises to become an important research and industrial tool because it can be made a very sensitive detector of various types of radiation. It will be especially useful for high-speed automatic X-ray inspection of industrial products.

These photo-sensitive CdS crystals are sensitive to both electromagnetic radiation (from the yellow region in the visible spectrum up to X-rays and gamma rays) as well as to high-energy particles (electrons, protons, and alpha particles). A polarizing voltage applied to the crystal makes it sensitive to ra-

diation, and, over a rather wide range, the photo-current is proportional to the applied voltage. (The electrical resistance of the crystal also varies with the intensity of applied radiation, but this is not always linear.)

Most important is the fact that the photo-current varies from crystal to crystal. In some crystals the photo-current corresponds to the number of free electrons produced in the crystal in a second (as in ionization chambers), while others the sensitivity may be as much as a million times greater.

The photo-current persists for a short time after the radiation is stopped. Generally the persistence is greater with greater sensitivity. In

some insensitive crystals the conductivity may decay within a microsecond after excitation stops, while in sensitive crystals the decay time may be measured in seconds or even minutes. In crystals where the photo-current is not proportional to the exciting radiation, the persistence still depends largely on the amount of excitation energy.

The CdS crystals also emit a reddish glow when irradiated. The amount of glow varies from crystal to crystal. The more sensitive crystals have a

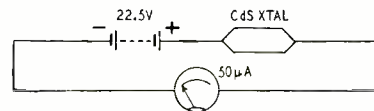


Fig. 1—Simple detector circuit using the crystal. When radiation hits the crystal, current through meter jumps.

greater output of light, while weakly luminous ones produce only a small change in conductivity. This fact is most important, because it means that crystals may be selected for any particular use before they are fitted with electrodes.

How it works

The reason for this unusual optical and electrical behavior of these crystals seems to depend on dislocations in the crystal lattice. In simplest terms, a crystal of any kind is different from other forms of matter because the atoms which make it up are arranged in orderly geometric patterns. Even extremely small dislocations in this structure seem to have a great effect on the luminescence and conductivity of these

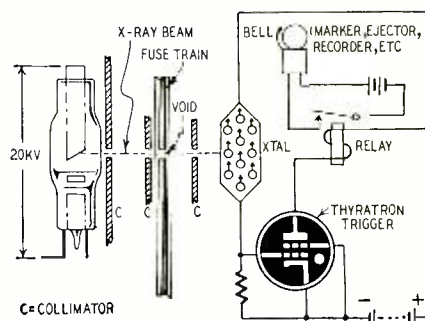


Fig. 2—Setup for testing powder continuity in a fuse train. Fuses can be checked as fast as 60 feet per minute.

L-C COMPARATOR AIDS INDUSTRY (Continued from page 35)

vided with a vertical bench comparator shown in the photo and used for reference checks with standard gauges. The operation of this unit is basically the same as that of the combined unit, except that it is much more sensitive and more carefully assembled. There is little difference in the circuit except for tube selection and voltage control.

As a detector of movement, this instrument has limitless uses. It has been used to detect movement in concrete dams, to detect vibration in machines, to control tool positions, to control machinery for boring mine shafts, and to inspect turbine blades both during manufacture and while assembled and rotating at high speeds. It has been used to measure the deflection of a 2-inch steel bar when a bee alighted on one end. In this case the deflection was $7 \frac{1}{2}$ gstrom units (100 million Angstrom units make 1 centimeter).

Its circuit is extremely simple and uses very old fundamental circuits. Even without voltage regulation its stability is very good.

The 6J7 crystal oscillator produces a 100-kc signal. This is multiplied to some suitable higher frequency by the tuned plate circuit. In the diagram this circuit is marked 400 kc (the frequency most often used in industry), but any other harmonic can be used to suit any particular purpose.

The 400-kc signal is amplified by the 6K7. The tuned circuit in the plate of this tube is unbalanced—its primary is tuned to 400 kc, but the secondary is

tuned externally by the operator by selecting an appropriate capacitor with switch S1 and varying C1 or C2. The capacitance pickup, which is designed to suit the particular test being made, is in parallel with these capacitors.

The 6H6 and the 6SN7 circuits make up a vacuum-tube voltmeter. The operator tunes the 6K7 plate circuit to produce a zero reading on the meter (the meter itself is not a zero-center instrument, but its scale is marked with a zero center). Any increase or decrease of the capacitance of the pickup then makes the meter needle move either to the right or left of the zero reading, depending on whether the change is an increase or decrease in capacitance.

The sensitivity of the instrument can be adjusted to any convenient value, but it is usually fixed so that a change of 2 μ f in the pickup will produce a deflection of 100 mm on the meter scale.

All of these instruments can be used for accurate quantitative measurements, but their greatest advantage is that they are easy to use for simple accept-reject tests for industrial quality control, even by unskilled operators with no knowledge of electronics. They are all housed in the same size cabinet, the heaviest weighs 16 pounds, and their power consumption is only 30 watts. They are built to withstand even the hardest abuse.

—end—

CdS crystals. To make crystals with specific properties, it is advantageous to produce these dislocations systematically.

When the crystal is not excited by radiation, the electrons are firmly bound to the atoms within the structure and there are no freely moving charged carriers to make up a current. When radiation is applied, some of the electrons absorb enough energy to be able to break away from the atoms and, if a polarizing voltage is applied to the crystal, a current flows. During this high-energy state, each electron that leaves the crystal at the anode is replaced by one that enters at the cathode, so that the amount of current depends on the number of electrons that are in the excited state. After a time (depending on the type and number of defects in the lattice) the excited electrons return to their normal state. In this process the energy which they picked up during radiation is emitted as luminescence. Luminescence and conductivity are thus closely related. The relation between sensitivity and persistence also becomes clear with this explanation.

Because it is highly sensitive even in the simplest of electrical circuits, the CdS crystal makes a good detector of all types of radiation. A CdS crystal hooked up to a single battery and an indicating meter can detect radiation intensities so weak that would otherwise require considerable apparatus.

Some useful circuits

Photo A shows a little pocket-size detector using a CdS crystal. Its circuit, which appears in Fig. 1, consists merely of the crystal, a 22½-volt hearing-aid battery and a microammeter. This device was built by Immanuel Broser and Ruth Warminsky at the Kaiser Wilhelm Institute in Germany. Credit is due them for much of the information which appears in this article. The smaller unit to the right of the meter case is a crystal holder. A small cylinder inside the holder takes several crystals, and any one may be selected for use by turning the cylinder so the crystal is in front of a small window. The crystal holder is separate so that instrument can be read at some distance from the actual point of measurement to protect the operator from harmful radiation.

In this detector the crystal can be selected for a variety of uses. For example, one is for measuring light, another is for measuring the intensity of X-rays, and a third is for detecting weak gamma rays. This gives even this little pocket instrument an extremely wide range.

The instrument could be made even more sensitive by using a higher-voltage battery. The only thing which limits the amount of voltage that can be applied to the crystal is that it begins to heat up when too much current flows through it.

Photo B shows a setup devised by the General Electric X-ray Corporation

using a CdS crystal and X-ray machine to check the product level in canned baby food. A fine beam of X-rays comes

speciation methods. In the case of the canned goods, as many as 600 units can be inspected per minute while the fuse

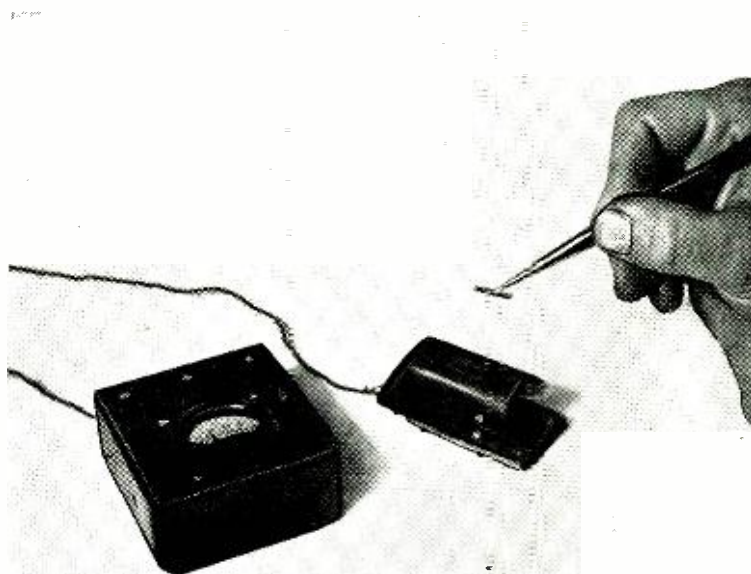


Photo A—This small portable radiation detector uses a CdS crystal. The meter and batteries are in the case at left, the unit at right houses the crystal.

from the generator on the left of the cans, and the crystal detector is at the right. This setup is only a pilot model, so the detector only operates the small neon lamp mounted on the crystal each time a bad can goes by. In actual production the detector would operate a reject lever or similar device. Fig. 2 shows the circuit of a similar setup used to check for defects a powder train of the type used in blasting fuses.

This crystal method will perform at much higher speeds than previous in-

goes by at the rate of 60 feet per minute. Because the crystals are so sensitive, very little if any amplification is needed, and fairly low-intensity X-rays can be used.

Another application which offers great promise is the control of the X-ray itself. In experiments at G-E X-ray, the output of the crystal has been used in a feedback arrangement to control the output of the X-ray generator and stabilize the beam.

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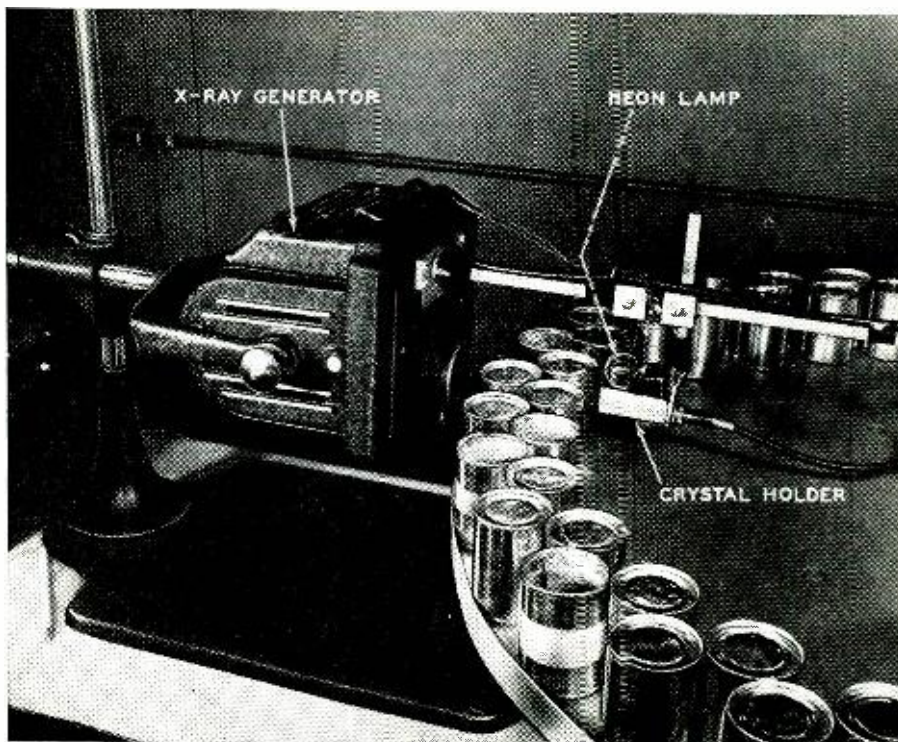


Photo B—A pilot setup for inspecting canned goods. X-rays are beamed through the cans to the crystal at right. Neon lamp indicates if a faulty can passes.

How an Electronic Brain Works

Part IX—Some electronic circuits for computers and how they are used for adding and subtracting

By EDMUND C. BERKELEY AND ROBERT A. JENSEN

IN THE previous article we began the discussion of an electric brain to be built around electronic tubes instead of relays. We discussed the storage information in the form of the state of a flip-flop, or pulses circulating in a delay line, or magnetized spots on a magnetic surface, or charges on the screen of an electrostatic storage tube.

But how do we compute? As soon as we have arranged to read, write, and erase information at electronic speeds, we need to consider how to compute with electronic elements.

For computing purposes, a unit of information is represented as a pulse, either a rise and fall of an otherwise constant voltage, or else a fall followed by a rise. We will call the first kind a positive pulse or a 1, the second kind a negative pulse or a -1, and the absence of a pulse a 0. See Fig. 1.

In a computer, the pulses are usually of a standard duration, and may be for example $\frac{1}{5}$ of a microsecond long and spaced $\frac{1}{5}$ of a microsecond apart. In this case the pulse repetition rate would

be 1 megacycle per second. In some computers, 1 and -1 pulses are both treated as the presence of information, the binary digit 1, the logical truth value 1, or "yes"; while 0 is treated as the absence of information, the binary digit 0, the logical truth value 0, or "no."

Phase inverter

The first computing element we need to consider is a *phase inverter*. In computer work, a phase inverter changes a positive pulse to a negative one, or a negative pulse to a positive one, that is, "inverts" the pulse. See Fig. 2. In this figure, and in Figs. 3 to 8, part *a* is the circuit diagram; *b* is its block diagram representation which we use for convenience; and *c* is a function table that indicates what the circuit does. Any grid-controlled electronic tube can act as a phase inverter.

Logical AND circuit

The next computing element we need to consider is called a "logical AND circuit." This is one of the meanings of

the electronic term "gate." See Fig. 3. In this circuit, a pulse appears on the output line if, and only if, two pulses come in simultaneously on two input lines.

A tube with two grids, normally cut off with either one or no pulses, is one of the forms which a logical AND circuit can take. The reason for the word "and" is that we have a pulse on output line C if and only if we have a pulse on input line A and on input line B. This (with emphasis on the idea "both") is the regular meaning for "and" in logic. This type of circuit may take many forms with and without electronic tubes.

Logical OR circuit

Another computing element is called a "logical OR circuit", sometimes called "buffer." It allows a pulse on the output line if a pulse comes in on either one or both of the two input lines. See Fig. 4.

A tube with two grids, which is normally conducting, is one of the forms which a logical OR circuit may have, although there are others. The reason for the word "or" is that a pulse is on output line C if a pulse is on input line A or if a pulse is on input line B, or both. This nonexclusive meaning of the word "or" is its regular meaning in logic.

Logical EXCEPT circuit

Another computing element is called a "logical EXCEPT circuit," or inhibitory gate. In this a pulse is allowed out on the output line if a pulse comes in on a specified one of the two input lines *except* if a pulse comes in at the same time on the other input line. See Fig. 5.

The circuit shown in Fig. 5 will act as a logical EXCEPT circuit. Its constants are chosen so that when A is not pulsed, whether or not B is pulsed, still there is no output on line C. If A is pulsed and B is pulsed, the two pulses coinciding in time and of opposite phase eliminate the pulse on line C. If A is pulsed and B is not pulsed, then the pulse goes on through. Other circuits besides that shown in Fig. 5 are of course possible.

Electrical delay lines

The computing section of an electronic computer also uses an electric delay line of very short delay, such as one pulse time, or a few pulse times. A circuit that does this appears in Fig. 6. These are different from the long sonic

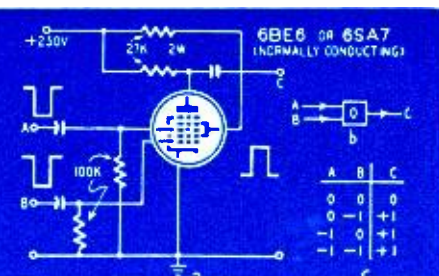


Fig. 3—A logical AND circuit, or gate. Output pulse appears at C only when inputs appear simultaneously at A and B.

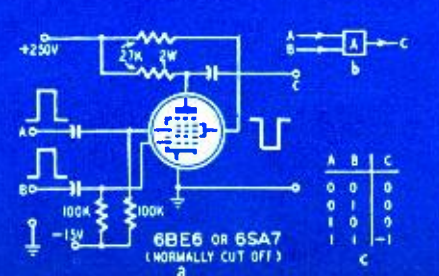


Fig. 4—Logical OR circuit, or buffer.

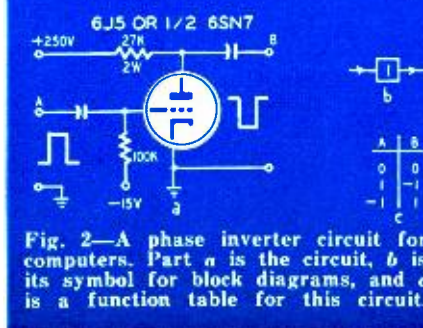


Fig. 2—A phase inverter circuit for computers. Part a is the circuit, b is its symbol for block diagrams, and c is a function table for this circuit.

delay lines such as the mercury tanks described in the previous article, because the purpose of the short delay line is not storage but computation. Short delay lines are important because pulses sent into the various parts of an electronic computer must arrive at the various points just when they are needed. For example, in the Bureau of Standards Eastern automatic computer,

of microseconds and pulses are timed to be safely within the planned intervals.

Half-adder

Now how do we take these various computing elements and begin to do computing with them?

The first thing is to assemble these elements so that we can add two binary digits. Suppose there are two input lines A and B, and either one may bring in a binary digit that may be 1 or 0. Suppose that we have two output lines, one of them S, that will give us the sum without carry, and the other C, that will give us the carry. The function that we want to express is the result of adding two binary digits: $A + B = C, S$, where $0 + 0 = 00, 0 + 1 = 01, 1 + 0 = 01,$ and $1 + 1 = 10$. See Fig. 7.

To make a half-adder circuit, one logical AND circuit, one logical OR circuit, and one logical EXCEPT circuit, combined as shown in Fig. 7-a, are sufficient.

Adder

But we are not finished, because a previous addition may have given a carry that has to be taken into account. The circuit which will perform complete binary addition is called an *adder*. See Fig. 8.

Now let us trace through the adder circuit with some numbers and see what actually happens in the sequences of pulses on the several lines in the circuit.

The digit 1 will represent a pulse (assumed to be positive or negative as the circuit requires), and the digit 0 will mean absence of a pulse at the proper time. At the same time the digits 1 and 0 will represent information that we desire to compute with.

Suppose we write a binary number (or more generally any set of binary digits) in the ordinary way (with the smallest ranking digit at the right) on any circuit line where the pulses are traveling from left to right. Then the binary number will be attended to as a pattern of pulses by the circuit in just the sequence from right to left that we ordinarily deal with in arithmetic. At the same time the number will show the sequence of pulses in the order that they are handled in the circuit.

As an example of using the adder, let us add 101 (one 4, no 2 and one 1 in binary, or 5 in decimal) and 1011 (one 8, no 4, one 2, and one 1 in binary, or 11 in decimal). We write the two numbers on the input lines A and B (See Fig. 9) and now we set out to see what happens.

At the first pulse-time, the pulse (the 1) on the A line and the 1 (another

pulse) on the B line go into half-adder No. 1, and give rise to no pulse on the S line (sum without carry) and a pulse on the C line (carry). The 0 on the S1 line goes into the second half-adder without delay; but the 1 on the C1 line goes into the one-pulse delay and so it is held back one pulse-time. As a result, at the first pulse-time, 0 and 0 go into the second half-adder; and so its output is 0 for the first digit of the true sum, and 0 for the carry. The 0 for the carry circles round the loop and comes up to the entrance of the one-pulse delay.

At the second pulse-time, 0 and 1 go into the first half-adder, and give rise to a 1 on the S1 line and a 0 on the C1 line. The 1 on the S1 line goes into the second half-adder without delay. Now the delayed previous carry (with no conflict from the absence of pulse that came around the loop) now issues from the one-pulse delay. So 1 and 1 now enter half-adder No. 2, and from it issues a 0 on the sum line S2 and a 1 on the carry line C2 which circulates around the loop, and enters the one-pulse delay so it will be ready for the next pulse time.

At the third, fourth, and fifth pulse-times, each of the proper operations takes place similarly, and so we get out of the second half-adder exactly the sum that we desire.

Subtractor

Now how do we manage to subtract? A circuit that will subtract is shown in Fig. 10, using the constituents of an adder, and a logical EXCEPT circuit. The word "minuend" means "the number to be diminished." The word "subtrahend" means "the number to be subtracted."

Let us test this circuit by subtracting five from eleven, or in binary subtracting 101 from 1011. The pulses appear in succession on each of the lines in the diagram, as shown. By following through the circuit, remembering what each stage does, we see that exactly the right answer, 0110 or six, appears on the output line marked "difference."

Acknowledgement is made to Henry W. Schrimpf for a number of the circuits and ideas in this article.

In the next article we shall take up the multiplication and division of binary numbers using electronic circuits and begin the discussion of the control of an electronic computer.

(continued next month)

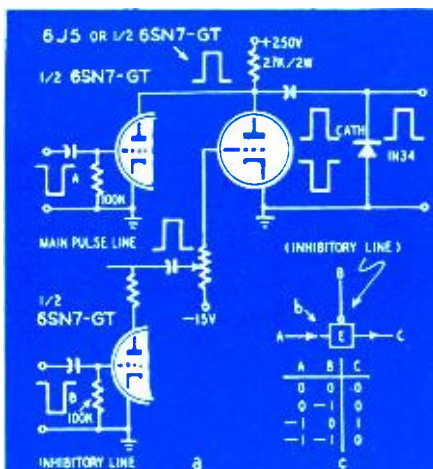


Fig. 5—A logical EXCEPT circuit. The pulse input at A appears at output C except if there is a pulse at input B.

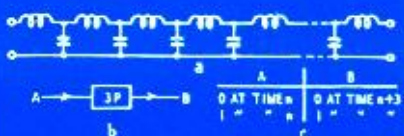


Fig. 6—Electrical delay line as used in computers. The 3 in the block symbol denotes a delay of three pulse times.

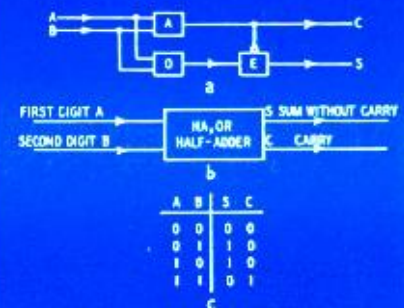


Fig. 7—This half-adder circuit gives the result of adding two binary digits.

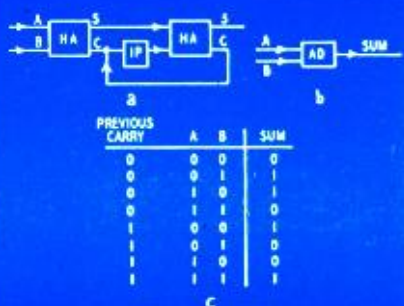


Fig. 8—An adder circuit is made up of two half-adders and a one-pulse delay.

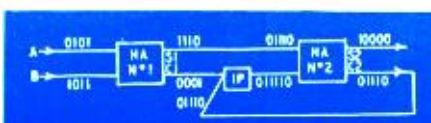


Fig. 9—The numbers on this adder show how 0101 is added to 1011 to get 10000.

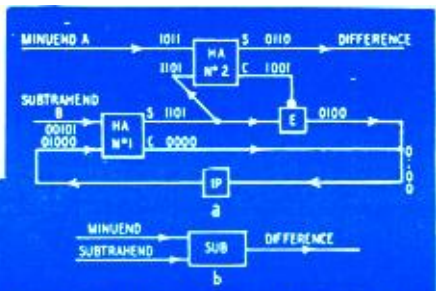


Fig. 10—Diagram of a subtracter. This one is taking 101 from 1011 to get 110.

Don't Touch Those Screws!

A fast method for diagnosis and alignment

By JOHN D. BURKE*

YOU can assume that one or more—or all—the screws on a radio set have been turned if you know that "Cousin Fred" tried to fix it before you came on the scene.

But how about you? Haven't you also an itch to twist a few?

Please—please—don't do it! Not until you are qualified to do the turning. And not even then, till you know for sure they need turning.

And don't kid yourself just because you ended up with the set playing that it is playing correctly. There is the little matter of the right i.f., for which the r.f. and oscillator of this set have been designed. If the i.f. is wrong, the set won't track properly. You will get some stations, but not others. You may end up with some weird whistles.

A repairman must understand alignment, for it plays a big part in the proper operation of the set.

If you must make a choice—shall you get a signal generator first, or a signal tracer—the generator is the most important for the beginner. The higher in frequency it goes, the better.

I happen to use a *tuned* signal tracer and have developed a different method of alignment from the conventional.

Instead of aligning i.f. stages with a generator, I let the broadcast signal of a local station beat against the local oscillator of the set (in other words, I tune in a station) and *check with the signal tracer* (tuned to the frequency that set is supposed to use for its i.f.), to see if the same signal, at proper strength, frequency, and quality, appears at each point of the i.f. circuit, and at the detector. This is easy to do, and may be done in the course of other tests with the tracer—and before needed repairs in the audio, for instance, have been completed.

In fact, this method makes it possible to align a dead set. Any other method of alignment usually requires that you hear and measure the final audio output of a radio; it presupposes that the set is in operating condition, and that you are just touching up the alignment as the last step before finishing the job.

However, if a set comes in with a defective loudspeaker or output transformer, for example, and the customer wants an estimate, there are likely to be other troubles in the set, and you want

to be sure. With this method you can test the set in every respect right up to the point of breakdown. And in some cases I inject a signal in some fashion into the rest of the set after the breakdown point. For instance, I test the customers' loudspeakers by hooking them to the output from my signal tracer, which, being tunable in the broadcast band, serves very well as a comparison receiver.

While we are discussing the price of the job, I can be adjusting his various trimmers so as to perfect the set's alignment.

I. f. alignment

Manufacturers' instructions for alignment (by signal generator) call for injecting the signal at the i.f. tube (second or third i.f. if the set has them), and working back toward the mixer.

My method calls for working from the mixer back. To put it another way, one listens in to the desired signal, and turns the screws that need turning to clear the road for that signal to reach the second detector.

Better yet, it is possible to tell whether a radio is in approximately correct alignment without making any connection of any instrument whatsoever to the set itself!

How is that?

Every radio, even the tiniest camera-type portable, produces such a strong i.f. signal as a result of the gain in the i.f. that it radiates.

A signal tracer of the tuned type is a tuned radio-frequency radio (with meters). It is tunable down to around 100 kc, and up through the broadcast band.

With one hand you sweep the tuning dial of the tracer across the i.f. that the set in question is supposed to use—above and below that point. With the other hand you probe with the lead connected to r.f.-i.f. test on your tracer, and *even outside the cabinet of the radio* you will be able to detect signal at i.f. (Of course you must be on a station with your radio.)

Generally I use an unshielded lead for r.f.-i.f. tracing to get better pickup than you get with a shielded lead.

Presto! By this method, when the customer walks in you can, in many cases, turn on his set and in a few minutes say to him: "The signal is going halfway through your set. There is probably no more than such and such wrong with it. The repair will be \$—, at the most."

Meantime the set has been sitting there not making a sound. You can even mystify your customer by letting him hear his own little set playing into a big speaker, often sounding much better than the original—and no wires! "Is that *my* set playing?" Time and again

* This article is based on a chapter in *Rapid Radio Repair*, a book recently published by the author.



A well equipped service bench. This one is at Radio Peeters, Amsterdam, Holland.

I hear that, and I explain as well as I can.

This situation requires that the set oscillator be working. If it is not working but the rest of the set is, then it can pick up your signal generator at its intermediate frequency, even from a distance. This is common practice in repair shops.

A tuned signal tracer eliminates search in the books for an unknown i.f. If you get nothing in the 450- to 470-ke region, you tune down to 262 ke, and in the case of some old-timers, still lower. Of course, if the set has been aligned on a wrong frequency, you may have difficulties, but wrong tracking will show up that trouble immediately.

You have no trouble with harmonics or images, as you do with a signal generator. You do not disable the oscillator to align an i.f. stage.

The greatest benefit of all is that you work with a broadcast signal, not the 400-cycle note. Thus you can check for distortion, rattles, loss of frequencies, etc., while doing the alignment.

The old-fashioned method of alignment calls for an output meter across the loudspeaker voice coil. That method is still good. However, for years I have relied either on a vacuum-tube voltmeter connected to a.v.c., or on the signal tracer or on my ears.

How about the last? I have satisfied myself that it is practically impossible to improve on an alignment done by ear. For one thing, if you peak a set (eliminate background noise) on a *weak* station, that set must be adjusted to its maximum gain. This done, all strong stations ride in perfectly.

The same goes for alignment by oscilloscope. You may object: What about high fidelity? How about wide bandpass sets (AM sets)? The answer is simple. A.v.c. action on any r.f., mixer or i.f. stage broadens the bandpass of that stage enough to pass the higher audio frequencies.

In television it is a different story. Very wide hands must be passed, and i.f.'s are stagger-tuned. As for FM, I note that even the manufacturers are calling for peaking their i.f.'s for maximum gain nowadays.

A few AM sets have wide bandpass built in; either by a switch to cut in and out another winding in an i.f. transformer, by a mechanically operated variable coupling device, or by using resistors in parallel or series. Generally speaking, the set is peaked to maximum in "sharp" position. Then high fidelity takes care of itself.

Checking sets with a.f.c.

For experience, and to prepare you for some models of television and FM sets, it will be a good thing if you get a chance to work on some sets with automatic frequency control. The service technician must study these circuits to understand how they take a voltage off a discriminator tube (which takes its signal off at the same point as the regular detector) and feed it to an auto-

matic frequency control tube, which has its plate, or cathode, circuit linked to the oscillator of the set.

Put simply, variations in tuning on the dial, away from dead center on a station, produce either a positive or a negative voltage (depending on whether the dial is set above or below the right frequency) from the discriminator. This tube works (at slow motion) just like the discriminator in FM sets—with the difference that it produces variable d.c., whereas the FM discriminator produces audio.

The d.c. voltage from the discriminator, applied to the grid of the a.f.c. tube, varies its plate current. Variations in current through a tube change its reactance. Result: the local oscillator shifts to approximately the right frequency to beat with the station which is *almost* tuned in.

The set will align normally when a.f.c. is turned off. Then you have to adjust the discriminator so that it will pull in stations an equal distance above or below on the dial.

Beginners spend a lot of time screwing series padders in and out. Here are a few tips. Assume that they are right all the time (provided the padder is down in its usual out of sight position on the chassis). Tamperers play around with screws on the i.f.'s and tuning gang mostly. Turn the series padder only *after* you have the right i.f., and *after* the oscillator parallel trimmer seems unable to correct the tracking within its normal adjustment range.

Any set on which you cannot peak the trimmers without the set breaking into regeneration (squealing, etc.) has something wrong with it. Exception: I often find that people have "aligned" the i.f.'s up near or on the frequency of

a station around 550 ke. Then anything is possible. If you have the right i.f., but cannot peak without regeneration, then the set has something wrong with it. Examine all the possibilities for undesired oscillation (shielding, lack of bypassing, bad tubes, loop too near i.f.'s, etc.). That set was capable of maximum gain without oscillation when it was built, and you are confronted by a repairable condition.

Powdered iron core coils (permeability tuned) sometimes develop shorted turns. Such a coil with shorted turns loses inductance, not to the tune of so many turns, but much more. So, you may come across broadcast band oscillators operating wildly way up in the amateur, police, and even high frequencies due to a shorted coil. Those are the times when the oscillator channel of a good tuned signal tracer will let you know what has happened and why.

Powdered iron tuning circuits, on the other hand, do not get out of adjustment frequently. As in the case of the screws on other sets, you will profit little by turning these core screws very much unless you know that they have been tampered with.

The problem of alignment includes many other things for which there is no space in this article. Like anything else, aligning becomes easier with practice. It is possible to go along in a rut year after year without seeing how to save time. I hope this article will come as something of a stimulus to old-timers as well as to the younger generation in our field.

In general: *If a radio set has not been tampered with, it probably needs no realignment. Smoke that in your pipe.*

—end—



"I guess they've signed off for the night"

Suggested by J. P. Sandlen, Hamilton, Ohio



With the Technician

TRENDS IN SERVICE LAWS

Legislation appears to be the early summer fashion in areas faced with television service problems. New York City, as usual, has a bill under consideration—at the time of writing there was actually a bill and a half in the offing.

The bill is a modified form of the earlier Keegan proposition, which would call for licensing all technicians and service organizations and would appoint a city czar to promulgate rules and enforce them. The near-bill is a proposition by A. B. Z. Silver, Brooklyn assistant district attorney, to set up a city agency to hold in escrow funds paid by television owners on television service contracts.

Complete records would be kept by the agency so that if a customer considered his service organization unsatisfactory, he could switch the remainder of his contract period to another one. Should the contractor go out of business (which would be less likely if his receipts were spread out over the 12-month period) his unexpired contracts would also be turned over to other companies. And if a service concern found it impossible to get along with a customer, it could also turn in the contract, to be finished by some other "lucky" service organization.

Rhode Island has actually passed a licensing ordinance—aimed purely and simply at the television service contractor. Its text appears elsewhere on this page.

Other license proposals have appeared at widely scattered points. The city council of Miami recently rejected a proposed ordinance which would cover the construction, installation, and maintenance of radio and television apparatus. It was submitted by a group called the Radio and Television Technicians Guild of Florida, and provided for a board of examiners, licenses based on technical qualifications, and inspections of outdoor antennas by the city's electrical inspectors. A licensing bill is being advocated for Wisconsin as well. Massachusetts proposes the following for antenna installers:

Any person installing an aerial or any device connected with the operation of a domestic or business television set shall pass an examination and shall be registered with the electrical board of the division of registration.

The board shall pass on all types of antenna and prices to be charged for the installation of same.

In New York State, television has become one of the chief subjects of legislative debate. After passing one bill to ban the use of televisers in motor cars, and another forbidding attachment of antennas "or any other wires"

to any fire escape or to any soil or vent line extending above the roof of a building, the Legislature sees the Levine Bill, which proposes state-wide licensing, looming up on the horizon. This follows the O'Connor Bill, described in our May issue, which was found unconstitutional in the form in which it was drawn.

The trend would seem to indicate that a number of acts designed to regulate or control radio and television servicing are likely to be passed. Some of these, like the Rhode Island law, may protect the television set owner and the honest technician. Others may increase the revenue of the municipality enforcing them. Still others, not aimed at the real problem, are no doubt destined to annoy authorities and service organizations alike till they are either repealed or die of nonenforcement.

OLD STORY, NEW REASON

New reason was given recently by a television contract service organization for going out of business. The Hano Television Maintenance Company of New York City suspended operations because of the failure of dealer clients to make payments to the company on the contracts held from them. Dealers have been protecting themselves against failure of the service contractor by paying him in installments, though the customer almost invariably pays the full amount at the beginning of the contract. Mr. Hano stated that back payments owed by dealers amounted to about \$75,000, and that the situation was further aggravated by the business failure of six retailers who had used his company as a servicing agency.

Television set owners would not be inconvenienced by the liquidation of his company, Mr. Hano said, as the dealers could simply transfer contracts and pay the new contractor some of the money that his firm was unable to obtain. He felt that dealers were willing to pay but were not able to because of being heavily overloaded with TV stocks.

NATIONAL RADIOMEN MEET

The second meeting of the new national radiomen's organization was held Sunday, March 4, at the Drake Hotel in Philadelphia. Some discussion as to the correct name of the body was closed by confirming the title: National Electronic Technicians and Service Dealers Associations (NETSDA).

Distinguished members of the industry, including the service department heads of two of the country's largest television set manufacturers as well as representatives of other

branches of the radio industry, were present to wish success to the new organization.

Considerable discussion on organization and membership took place and plans were laid down for carrying on educational and promotional work in that direction.

The third general meeting was held in New York City, April 1. A charter for the organization was discussed and a preliminary draft was referred to a committee for further development.

The treasurer, Vance Beachley of Harrisburg, Pa., reported that six organizations had forwarded membership dues since the last meeting. The publicity director, Mr. Marshall, pointed out that a recent report on a radio meeting in Philadelphia contained material which might be considered slanderous to the radio technician. The publicity committee was instructed to write to the reporting organization, pointing out the adverse effects of such publicity and urging them to try to hold down such publicity in the future. Dave Krantz, of Philadelphia, reported that the organization emblem was in the hands of the engraver, and that other pictorial publicity material for the organization was nearly ready to turn over to the publicity committee.

LETTER PROMOTES MEETINGS

The Long Beach Radio Technicians Association (California) has a system of keeping members up to date which might well be copied widely. We have received a copy of a letter, which is apparently manifolded and addressed personally to each of the absent members by the publicity director, Harry Ward. It gives the highlights of the two meetings of the month and points out that it would be better for the member to attend meetings, rather than stay away and then call other members by telephone to find out what transpired.

The Association, which believes itself to be the oldest and largest service technicians organization in the country, has elected Hal Meyers president. Other officers are: Fred Abrams, vice-president; Les Huckins, secretary; Clarence Spencer, treasurer; Harry E. Ward, head of public relations; and Joe Martin, technical adviser.

Long Beach is one of the organizations which issues its own certificates of qualification. It requires that all technicians undergo a four-year apprenticeship before being issued certificates as fully qualified technicians.

RHODE ISLAND LICENSE ACT

The State of Rhode Island has licensed all persons selling television service contracts. The Act also provides for a \$2,000 bond. The text follows:

State of Rhode Island and
Providence Plantations

JANUARY SESSION, A.D. 1951

AN ACT Providing for the Licensing of Sellers of Service Contracts for the Maintenance and Repair of Radios and Television Sets.

It is enacted by the General Assembly as follows:

SECTION 1. No person shall engage in the business of selling service contracts for the repair and maintenance of radios, and television sets within this state without having first obtained a license therefor from the department of business regulation in the manner hereinafter provided.

SEC. 2. The department of business regulation is hereby empowered to grant licenses to persons engaged in the business of selling service contracts for the maintenance and repair of radios and television sets. It shall be the duty of said department to provide such regulations and rules for the conduct of such business as shall be necessary to effect the intent and purposes of this act.

SEC. 3. The fee for such license shall be \$2.00 per year and shall be paid to the general treasurer for the use of the state; and each person so licensed shall give to the general treasurer and his successors in office a bond, with two sureties approved by said general treasurer in the sum of \$2,000.00 with condition for the proper discharge of the services which he may perform by virtue of such license.

SEC. 4. Every person who shall violate the provision of the foregoing section shall be fined not exceeding \$500.00.

SEC. 5. This act shall take effect upon its passage and all acts and parts of acts inconsistent herewith are hereby repealed.

PRMA PICKS NEW OFFICERS

The Philadelphia Radio Service Men's Association has elected James Daly, former secretary, to the presidency of their association, to fill out the unexpired term of Tom Middleton. Mr. Middleton plans to start a service business of his own in Miami, Florida. William Hume was elected to fill Mr. Daly's place as secretary.

NEW YORKERS JOIN NETSDA

Radio service technicians of New York voted their organization, the Empire State Federation of Electronic Technicians' Associations (ESFETA), into the new national radio service federation, the National Electronic Technicians and Service Dealers Associations (NETSDA), confirming a tentative decision made at an earlier meeting.

The decision to join the national federation was the most important business of the annual ESFETA meeting, which was held at the Arlington Hotel, Binghamton, New York. Twenty-five members were present, representing eight associations.

Other business included special measures to protect the rights of member associations of the State Federation who might not wish to join the new organization, a discussion of the licensing situation, financial measures, and notice of constitutional amendments.

Officers elected for the 1951 term were: President, Wayne Shaw, Binghamton; vice-president, Sid Gent, Endicott; recording secretary, Ed Fisk, Rochester; corresponding secretary, Don Lissow, Rochester; treasurer, Ben

de Young, Ithaca. Jack Wheaton, Sam Marshall, Ken Brunneman, and Sid Gent were appointed delegates to the national organization.

OHIOANS DISCUSS SAFETY

"Safety in Your Store" was the theme of the Columbus, Ohio, Associated Radio Service Dealers' March meeting.

The discussion was led by members Fred Oberle, Don Blazer, and George Dykes, each of whom had prepared an individual paper on the subject. In this manner subjects were brought out that many members admitted they had never thought of.

PROTESTS OPS APPOINTMENTS

Television Associates, Inc., of Washington, D. C., at a recent meeting protested the reported appointment by the Office of Price Stabilization of a group composed solely of distributors to represent the TV service industry on pricing problems. The organization is working individually and through the National Electronic Technicians and Service Dealers Associations to secure representation for the service industry at all governmental hearings where their interests are involved.

About 200 persons, representing some 60 firms, attended the meeting.

Tubeless Oscillator Covers Audio to 2 mc

By EDWIN BOHR AND HAL FRENCH

THIS wide-range tubeless test oscillator—a variation of one used in a telemetering circuit—generates signals from low audio frequencies to well above 2 mc. To appreciate its simplicity, you need only to look at the diagram and photograph. Its components are a transistor, two resistors, switch, a tuned circuit, and a 22.5-volt battery which delivers less than 1 ma to the circuit. The simplicity of the transistor oscillator is one of its best selling points. Just try to design a vacuum-tube oscillator which uses so few components and requires such low battery power.

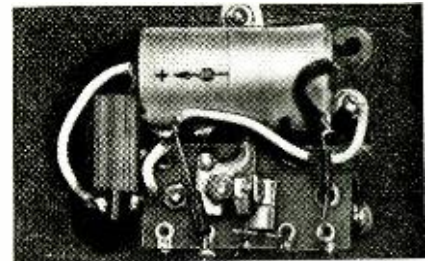
The absolute frequency range of the oscillator range depends upon the Q of the tuned circuit and certain other factors. The L-C circuit may be variable so that the output frequency may be tuned. For example, the secondary winding of an antenna coil and a 365-µf variable capacitor may be used to cover the broadcast frequencies, or one side of an i.f. transformer may be used to produce a fixed frequency at 456 kc. The oscillator is modulated by transistor noise or hiss. Its signal tunes broadly on a receiver because of the wide sidebands produced by the hiss.

A 2-terminal oscillator sustains oscillations because of its negative resistance characteristics. Because a transistor can be made to exhibit this characteristic, this tubeless 2-terminal oscillator is possible.

In a conventional or positive resistance, the voltage drop across a resistor varies directly as the current as shown by the familiar Ohm's law formula $E = IR$. Positive resistance absorbs power from an L-C circuit and damps oscillations. If it were not for this effect, an L-C circuit would oscillate in-

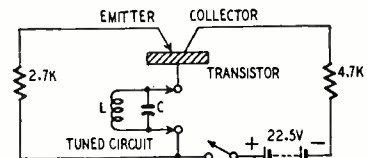
definitely after being excited.

In a negative resistance, the voltage drop decreases as the current increases. It contributes energy to the natural period of oscillation by causing heavier



A rear panel view of the oscillator.

current to flow through the tuned circuit as the voltage decays. Such circuits will sustain oscillations only as long as the value of negative resistance is greater than the positive resistance. Therefore, it is necessary that high-Q tuned circuits be used—particularly if one set of components is used to cover a wide range of frequencies.



Circuit of the wide-range oscillator.

Commercial sockets were not available for the Bell Laboratories transistor used in the circuit so we used the makeshift mounting shown in the photo.

1 "Transistor Oscillator for Telemetering," Frank Lehan, *Electronics*, August, 1949, page 90.

—end—

Handling Test Leads

Unimpressive but important, they can help you make better use of your test equipment

By H. LEEPER

Don't lose your time and risk your temper by neglecting your test leads and prods. They are the eyes and ears of your test equipment—its only means of making contact with the world outside. Yet how many technicians pay little or no attention to these essential accessories, and so lose time—and prestige in the eyes of their customers—by trying to do their work with ragged, tangled, unkempt-looking leads.

You can even have real trouble because of beat-up leads. I have seen a so-called service technician remove an output transformer—drilling and punching out two rivets to get it off the speaker—simply because his test lead was broken inside the insulation where it connected to the pin jack at the instrument end, and so indicated an open primary. Frayed braid on coaxial leads can short the lead, giving false short indications, and sometimes causing real damage in certain rectifier and other circuits.

System will help in handling your test prods. A single instrument may

have several of them for various applications.

You can save time by placing them so they can be reached easily without fumbling through a nest of cables for the correct lead. There will also be less chance of plugging in the wrong lead.

The photos below show some hints—gathered from the author's experience—on the care and handling of the humble test lead.

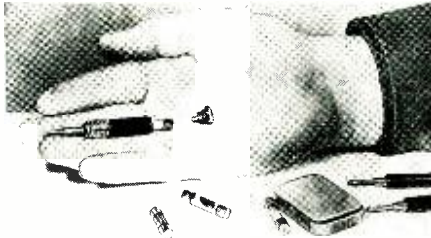


Photo C—Some types of test prods can be fitted with low-current fuses to protect the instrument. For some tests using leads only, protect the building fuses by using a 3-ampere fuse in the test prod.

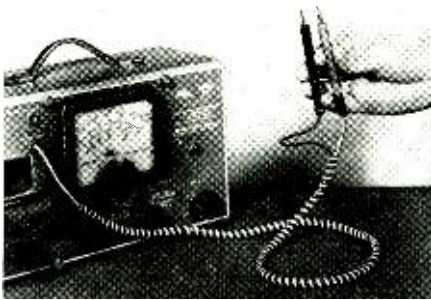


Photo D—A plastic telephone cord covering (obtainable at the dime store) will keep the test leads from twisting and getting tangled. Leave enough open wire at the ends for easy testing.



Photo E—If the meter is connected to the set under test for some time, as in checks for intermittents, a snap switch in one test lead may be convenient for starting or stopping the test at various times without disturbing the chassis.

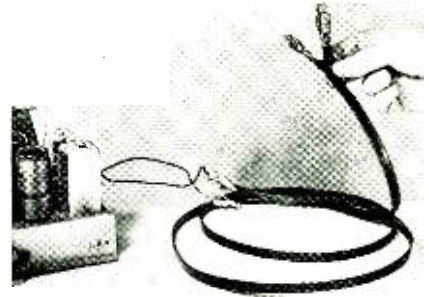


Photo F—A piece of TV ribbon line with clips on the ends is convenient for attaching a receiver output transformer to a PM speaker which is left in the cabinet. Do not use such leads in circuits carrying high voltages.

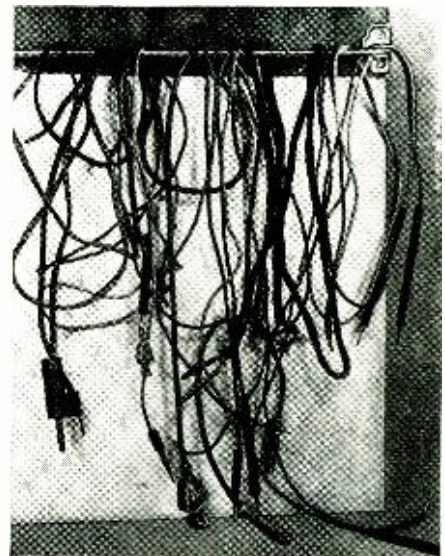


Photo G—A towel rack about 18 inches long mounted near the service bench will hold a number of test leads so they are easy to find, easy to get at, and do not get rubbed and dirty.



Photo H—Use a metal tooth brush holder to carry needle point prods and leads in the pocket or kit. The holder shown is about 7 inches long and an inch in diameter.



Photo A—Use a 6-inch length of No. 4 rubber covered wire to make a very simple test prod. Remove the insulation from both ends and grind one end to a point. Solder a piece of flexible wire to the other end and cover the joint with tape.

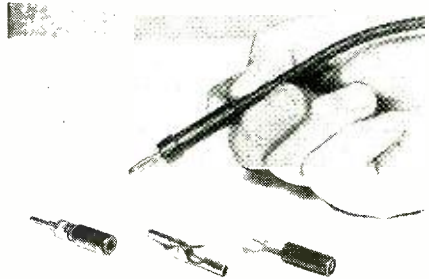


Photo B—Various types of commercial test leads are available. These have insulated handles and are fitted with banana plugs. These plugs will fit various types of jacks, such as pin jacks, spade jacks or alligator clips, which can be interchanged as required.

Electronics and Music

Part XII—Electrostatic mechanisms used in electronic tone generators

By

RICHARD H. DORF*

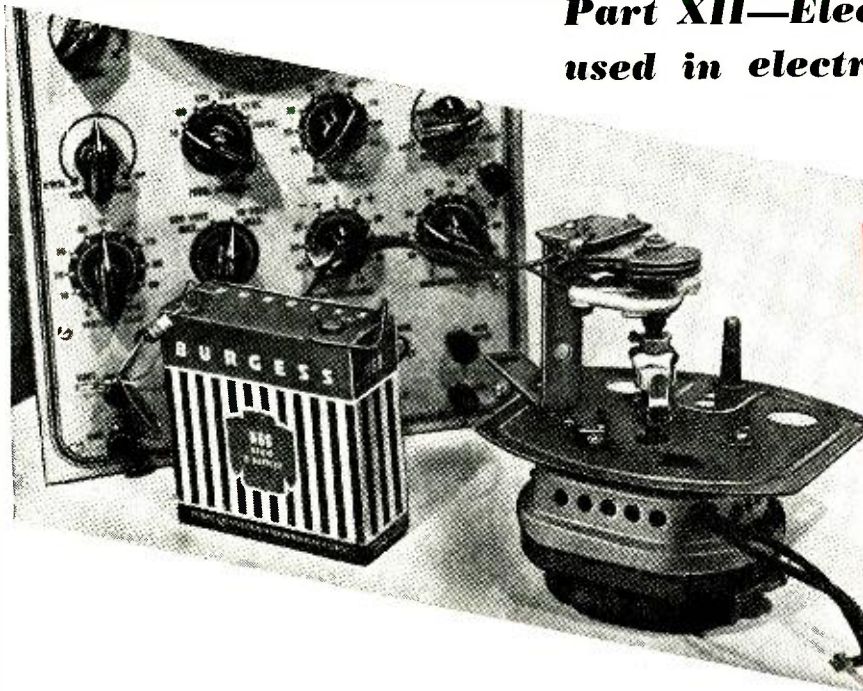


Photo A—This simple test setup shows how electrostatic organs work. An ordinary variable capacitor is connected to the shaft of an old phonograph motor. The electrical circuit appears in Fig. 1. Higher voltage or a larger-capacitance unit than the 10-30-muf the writer employed gives very much greater output.

IN THIS final article dealing with tone generators for electronic musical instruments, we shall take a brief look at a few more of the electro-mechanical methods. In general they are much more difficult for the individual constructor to make than the purely electronic product, but they tend to be more reliable once they are in working condition.

Electrostatic generators

The electrostatic system of tone generation is used in the Compton Elec-

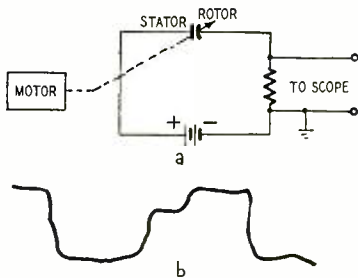


Fig. 1—Varying capacitance with a motor in the circuit of *a* produces the wave *b*.

trone, a British instrument which we hope to be able to describe in full in a future article. It is also the basis of most amplified reed systems, including the Wurlitzer, which we will explain fully at a later date.

Electrostatic pickups are based on the simplest principles of capacitance. A capacitor is a pair of conducting

surfaces in proximity to each other, separated by a nonconductor or dielectric. When a voltage is applied between the plates, there is a sudden rush of electrons from the positively charged plate to the negative one through the voltage source. Once all the electrons that can rush have rushed, the capacitor is charged—there is an excess of electrons on the negative plate and a scarcity on the positive.

The crucial point here is that the number of electrons that make the rush is determined by the magnitude of the applied voltage, the character (good or bad insulating properties) of the insulation between plates, the distance between the plates, and the area of the plates themselves. To distill things further, if the d.c. voltage and the dielectric remain the same, the area of the plates and the distance between them determine the magnitude of the initial current flow.

Now let us set up a laboratory experiment such as we have pictured in Photo A and diagrammed in Fig. 1. A variable capacitor with its plates fully meshed is connected to a resistor and battery in series. The moment we connect them there is an initial rush of current from the positive plate through the battery and the resistor to the negative plate. In a small fraction of a second the capacitor charges fully and the current flow comes to a gradual stop.

Now we give the capacitor shaft a half turn or so. The area of the rotor which is between the stator plates is now smaller—there is less capacitance, just as if we had lopped off a piece of the rotor plates. Some of the electrons on the effectively smaller rotor plates are now crowded off and return through the resistor and battery to the stators, creating a little rush of current through resistor and battery in the opposite direction to the original charging current.

We will find, in fact, that every time we rotate the rotors and change the capacitance, there will be this rush of current, its direction depending on whether we decrease the capacitance (discharge) or increase it (charge).

Now we haul a motor out of the stockpile and connect the shaft to the shaft of the capacitor. When we start the motor the capacitor's rotors begin whirling at the same speed as the motor. And with each revolution the capacitance reaches a minimum (plates unmeshed) and a maximum (plates fully meshed). As a result, current through the resistor and battery reaches a maximum, first in one direction, then in the other. In fact, the current takes the form of a.c. In the actual experiment shown in the photo the resistor was

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15 megohms, the d.c. supply 90 volts, and the capacitor a 10–30- μf unit. The current through the resistor created a very small a.c. voltage, too small to measure. Since the motor shaft drove the capacitor at about 900 r.p.m., the frequency of the a.c. was equal to the r.p.m. divided by 60 (to reduce it to revolutions per second), in this case 15 r.p.s. or cycles. It was fed to the vertical input of an oscilloscope and the waveform appears in Fig. 1-b.

It is obvious that the waveform in Fig. 1-b is not a sine, but since the a.c. was at an audio frequency it could easily be heard when a pair of headphones were placed across the output of the oscilloscope amplifier. The waveform depends only on the shape of the capacitor plates.

With that in mind we can design electrostatic generators to order, in at least two ways. The first involves varying the effective plate area. The specific method is taken from L. E. A. Bourn's Patent No. 2,522,923, though Bourn's method is presented here only in bare principle.

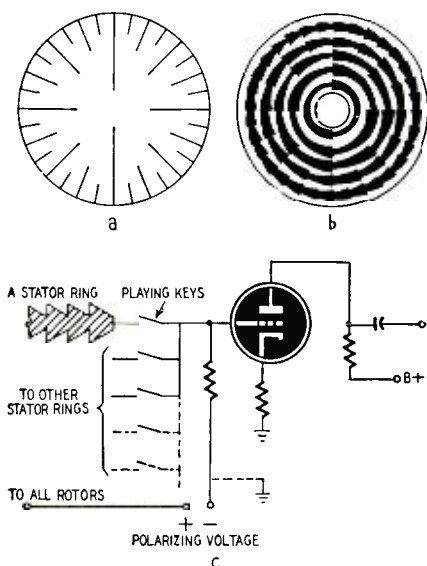


Fig. 2—Rotor *a* and stator *b* of one patented electrostatic instrument. The electronism at *c* is the input amplifier.

Fig. 2 shows the two necessary parts. A disc of insulating material at *b* has five annular rings of metal mounted on it. The rings are shown as the shaded push-pull sawtooth-shaped parts. This is the stator disc. Notice that the outer ring of the stator has 32 waveforms on it and each inner ring half the number of the next outer one. Each stator ring is electrically connected through a playing key to the grid of the first amplifier tube, as in *c* of Fig. 2.

The rotor appears in *a*. It is composed of a network of rigid wires mounted on a rim. The solid radial lines in the drawing represent the wires. All the wires are connected together and to the positive end of the polarizing potential, as shown in *c*. The rotor is placed parallel to the stator and very close to it.

Notice next that in the rotor there are radial wires of five different lengths.

The result is that the outer group numbers 32—the same number as the waveforms on the outer ring of the stator—and that their spacing is exactly the same as the stator's waveforms. The same holds true for each of the four inner rings.

Now let us set the mechanism in motion. When it is standing still, there is a constant capacitance between each wire of the rotor and the portion of an annular stator ring which faces it. As the rotor turns, each stator wire scans its wave pattern opposite. When a wire faces the wide portion of the waveform the capacitance is great; as it goes toward the narrow part the capacitance decreases. We thus have five continuously varying capacitors. Because of the 2-to-1 relationship in the number of waveform patterns and rotor wires between each ring and its neighbor, the outer ring's capacitance varies fastest, the next half as fast, and so on.

We thus have a mechanism and a circuit for refining the results obtained in our laboratory experiment. Because of the waveshapes on the stator, we can, by closing the appropriate playing switches, get from the output of the tube a note of the scale in sawtooth form over a range of five octaves. The speed of the disc determines what note it shall be. By providing twelve such discs, each rotating at an appropriate speed, we can make available five full octaves of notes. By placing six or seven annular rings on each rotor we can, with twelve discs, produce six or seven octaves.

The same trick can be attacked from another angle. In Fig. 3 we have a disc with a scalloped edge. Close to its edge and facing it edgewise is a small electrode. Connections are as shown in the figure. Now, as the disc rotates, its metal edge alternately approaches and draws away from the pickup electrode. The resulting capacitance between the two varies, and again an audio voltage appears across the resistor.

The electrostatic method has also been used extensively to make "electric pianos" and amplified reed organs. The method for a piano is illustrated in Fig. 4-a. A pickup screw is mounted close to the string and the polarizing voltage is connected. As the string vibrates, the capacitance between it and the string varies at an audio rate and there is output across the resistor. In an amplified reed organ the pickup screw is placed close to a selected portion of the vibrating reed as in Fig. 4-b.

FM organs

Electrostatic systems have the disadvantage that high voltages are used on more or less exposed parts of the mechanism, with consequent danger of shock. The high voltage is desirable even though a lower voltage will work because of a second disadvantage, the systems susceptibility to hum pickup due to the high impedances involved. Higher voltage means higher signal-to-noise ratio.

The fact that electrostatic pickup depends on variations in capacitance immediately suggests another approach which eliminates the high voltage and can greatly reduce hum—using the variable capacitance to vary the frequency of an oscillator and produce frequency modulation.

Practical circuits for the purpose will quickly suggest themselves, especially for electric pianos and reed organs which need no electrical keying circuits. An article describing an FM reed organ and explaining the design methods can be found on page 32 of the October, 1948, issue of RADIO-ELECTRONICS.

Record reproductions

One of the grandest ideas in scope ever kept in mind by the writer—and undoubtedly by many readers—is to make an instrument with a series of sound recordings as tone sources. If we could make a record of several ordinary acoustic instruments, each record containing a single pitch played on a single instrument, then have all the records playing continuously, we could select the output of any record with playing keys and produce a precise replica of the sounds of each instrument.

Fascinating as the idea is, it is very difficult to make practical, although one fairly well-known kind of organ—the photoelectric—does, in a sense, use recordings. Obviously the idea is totally impractical with phonograph records, if for no other reason than that no record has yet been invented in which a single groove could be played over and over again without soon getting unusually worn. It is fairly practical with magnetic records, though the required equipment would probably be voluminous and expensive.

One inventor, Graydon F. Illsey, of Omaha, Nebraska, has worked on the idea in patent No. 2,533,961, using magnetic wire. In bare outline, he has a series of discs, each with a length of recorded wire mounted in a shallow groove around its edge. If the organ has five octaves, there are 61 discs for each instrument to be reproduced, and each disc has a recording of one tone. If there are 10 instruments to be reproduced, 610 discs are necessary—each with its own magnetic playback head. While there is no reason why the idea

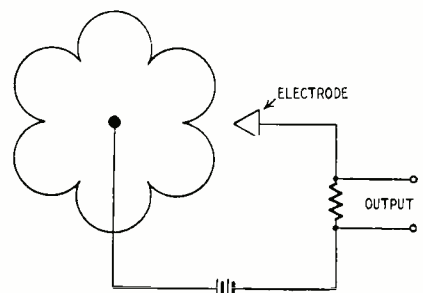


Fig. 3—Another way of varying capacitance. The shirred disc and the pointed pickup are the plates; distance between them is varied as the disc is rotated.

would not work, it would probably not be cheap to produce!

The same problem rears its head here as with other rotating-disc ideas—the fact that the waveforms must be re-entrant. That is, the joined ends of the circular recording must have waveforms in phase. To put it another way, each record must contain an integral number of waveforms. The problem is not difficult with photoelectric and electrostatic

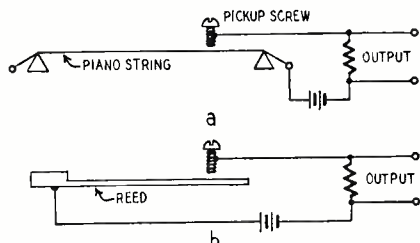


Fig. 4—Electrostatic pickup arrangements for amplified pianos *a* and reeds *b*.

discs, for they are usually provided with the necessary patterns by an artist or draftsman when the original models and the production dies are made. In any case the waveforms are visible.

In magnetic records the waveforms cannot be seen, so another method is necessary. John Hays Hammond, Jr., has given an excellent answer in his Patent No. 2,475,742. Fig. 5 shows how it works.

The note to be recorded is played into the microphone, amplified, mixed with supersonic bias, and sent to the recording head. The disc on which the endless recording is to be made is driven by a synchronous motor (through a mechani-

probably be placed so that signals could be erased after unsuccessful tries.) Naturally, the speed of the disc and the frequency of the signal have been calculated in advance.

Any incorrectness manifests itself as a single point on the disc where the phase of the monitored signal suddenly jumps—that is, the reproduced wave, if sine, might suddenly for one cycle take on an appearance like that shown in Fig. 6, and a portion of a cycle is skipped. In that case the signal contains a large component of a frequency equal to the rotational speed of the disc.

The invention has a way to check that. When the switch S1 is closed, the monitored signal is sent through a filter which selects one harmonic of the recorded sound (actually, of course, it is not a sine wave) and suppresses all others. This is followed by an amplifier and a tuned detector similar to that in any broadcast receiver. The frequency of the sound is, naturally, much higher than that caused by the rotational speed, so the selected harmonic is modulated by the once-per-revolution frequency. The detector demodulates the harmonic frequency, leaving only the rotation-frequency component, if any, and passes the latter on to an indicator. The finished record can then be judged by the indicator reading, optimum condition being no reading at all.

As the finishing touch to our discussion of tone generators, we shall give complete details next month about the Stroboconn, an electronic instrument used for tuning organs (both electronic and acoustic), pianos, and most other

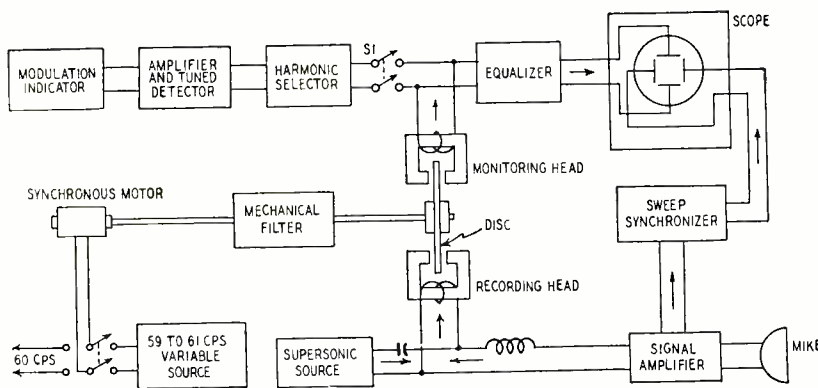


Fig. 5—Block diagram of a patented method of making reentrant magnetic recordings. The disc speed is varied to get an integral number of waveforms.

cal filter to remove transient speed variations) which may be powered either by the 60-cycle line or by a variable 59-61-cycle source.

At the other edge of the disc is a monitor head which picks up the recording just made and sends it through the necessary equalizer to one pair of plates of an oscilloscope. The other pair of plates is fed a sweep signal triggered by the same amplifier.

The waveform on the scope quickly shows whether the track is re-entrant. If not, the operator simply adjusts the speed of the motor by switching the motor to the variable-frequency power source until it is. (Although Hammond does not mention it, an erase head would

instruments, and which can also indicate roughly the harmonic structure of the notes of various instruments. It is portable, yet its accuracy is much less than the hundredth part of a semitone! (continued next month)

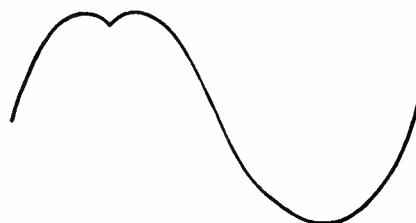
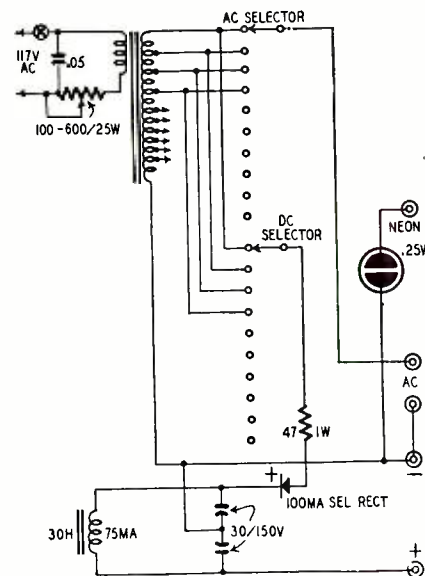


Fig. 6—A sine-wave signal on a non-reentrant endless record might look like this at one point on the record's output.

EXPERIMENTER'S POWER SUPPLY

The transformer from an old tube tester can be used to make a useful power supply for experimental work. With the transformer that I have, the supply delivers 1.5, 2.5, 5, 6, 12, 25, 35, 50, 70, and 120 volts a.c. and d.c. Any two a.c. and d.c. voltages can be selected and used simultaneously as long as the current drain does not exceed the rating of the transformer.



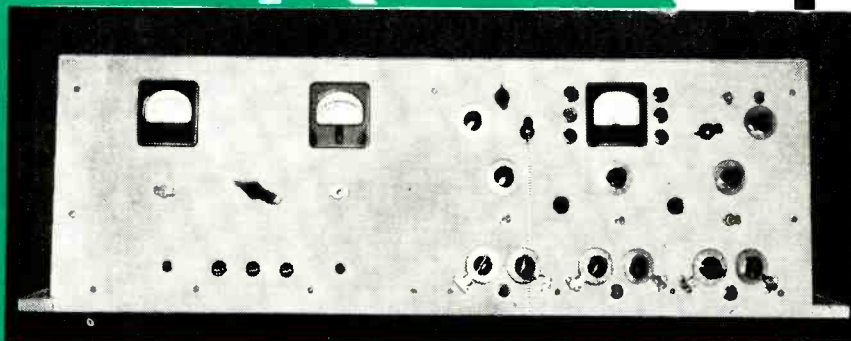
If the transformer you select has more or less than 10 taps, the selector switches can be changed accordingly. A 100-600-ohm, 25-watt potentiometer can be inserted in series with the primary winding to vary the output voltage between the taps.

A ¼-watt neon lamp is inserted in series between the common terminal on the transformer and a pin jack on the panel. This is used to check paper capacitors and large micas for shorts and open circuits. The usefulness of the supply can be increased by adding another switch in the a.c. circuit, and a switch, rectifier, and filters to the d.c. circuit. These will make it possible for the supply to deliver four different voltages simultaneously.

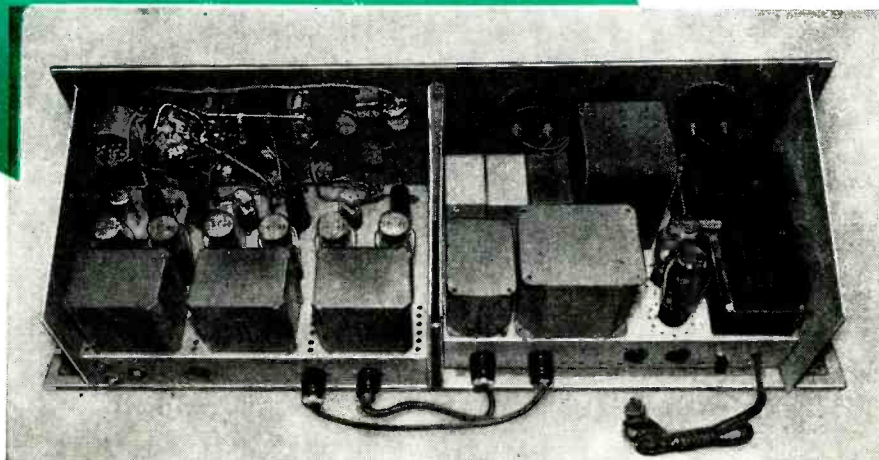
A variable supply such as this is inexpensive to build and has many uses. Surplus transformers, for example, often lack markings to indicate what windings it has. These are easily found by first checking continuity of the various leads, then applying a low a.c. voltage to any pair which show a low resistance. If the voltmeter does not read, the a.c. voltage can be increased until it does. This avoids the danger of applying a high voltage to a low-voltage winding.

A variable d. c. supply is also useful for determining the optimum operating conditions for a circuit. Once the circuit is hooked up, the voltages can be varied until the best conditions are found. The permanent power supply for the circuit can then be designed to provide this voltage.—Frank A. Graulich

Rico Amplifier



Front panel of the amplifier. Behind the left half is the power supply; the amplifier chassis is behind the right.



A top view of the amplifier shows its two chassis and general parts layout.

A new approach to realism in audio from Puerto Rico

By JACINTO SUGRAÑES

THE intense search by audio men to find a way to get realism into sound reproduction has led along many paths. One trend has been toward the use of multichannel amplifiers, in which each channel has control over a different part of the audio spectrum.

This system is such an amplifier. It is a 3-channel, all-triode circuit with each channel ending in a pair of 2A3's in push-pull. Each channel has its own roll-off frequency control, compensated phase inverter adjustment, individual power-tube bias adjustment, and volume control.

The three channels are fed by a pre-amplifier which also has a volume control as well as a variable equalizer for different types of records. Another pre-amplifier is used to boost the output of a variable-reluctance pickup. The power supply has a built-in line-voltage selector.

The question is, are all these controls necessary? "Yes!" is the answer. This is because there is little standardization in recordings and in loudspeaker and

pickup performance, and also because of the differences in room acoustics and personal tastes.

Usually the weakest link in a high-quality audio amplifier is in the speaker system. Even the costliest loudspeakers are far from ideal. It has so far been impossible to build a single cone loudspeaker that has a uniform frequency response over the full audio range. The impedance of a loudspeaker varies as the frequency applied to it is varied. Usually speaker impedances are given only for 400 cycles.

The greatest advantage of using three channels in an amplifier is that it is no longer necessary to use high-priced speakers. By dividing the amplifier output into three frequency ranges and using different speakers for each range, each speaker can be matched for best results over a relatively narrow band. This assures optimum speaker performance over the entire audio range.

In this amplifier the medium frequency channel is matched to the 400 to 1,000-cycle range, which is the same as that of most monochannel systems. The

treble channel is matched to about four to five times the 400-cycle impedance because the impedance increases with frequency. The bass channel is matched to the bass speaker at somewhat below 400 cycles to avoid the resonant peaks which are so common. This system permits matching at the most favorable conditions in three acoustic regions, providing what is perhaps the most important feature of this amplifier.

Obviously the correct taps to use on the output transformer will depend on the particular speakers used. The best way to determine this is to actually measure the impedance of each speaker over the range it must cover, and choose the taps accordingly.

The schematic of the amplifier is shown in Fig. 1. Each of the three channels is similar both in design and construction to the others, except for slight variations in the values of some of the components. Besides the 2A3 push-pull output stage, each channel has one 6N7 double triode which acts as a voltage amplifier and phase inverter, and one 12AH7 resistance-coupled amplifier.

The voltage outputs at the two plates of the 6N7's must be 180° out of phase to feed the 2A3 grids. The phase inversion is obtained by tapping a voltage-divider circuit connected in the plate of the first half of the 6N7. All three channels are similar in this respect. Potentiometer R6, in series with R5 and R7 and shunted by C8, acts as a tone equalizer for the phase-inverted voltage. Adjusting R6 balances the signal voltage on the grids of the two output tubes. Once the adjustment is made, the potentiometer is locked. The volume control for each channel is in the grid circuit of the first half of each 6N7 tube.

The input circuit

A 12AH7 voltage-amplifier stage precedes each of the 6N7 phase inverters. Each of these stages has a 100,000-ohm resistor in both the plate and cathode circuit to make up the total load of the tube. The resistance in the cathode gives the stage a large degree of negative current feedback. Further negative feedback is obtained through a plate-cathode network consisting of R3, R4, C5 and C6 in the treble channel and similar networks in the other two chan-

nels. In the treble and bass channels these serve also as frequency-discriminating circuits by the addition of C7 and C9. With R3 and R8 made variable, the low frequency turnover and the high-frequency roll-off may be preset at will. The diagram shows another feedback loop to the grid of this stage from the secondary of the output transformer. A 100,000-ohm resistor is indicated in this loop, but the actual value will depend on the impedance of the speakers used, and a little cut-and-try may be necessary.

The leftover half of the 12AH7 voltage amplifiers is used as a common stage to feed all three channels. The plate and cathode resistors of this stage have a relatively low value and the cathode is heavily bypassed. The output of this stage may contain voltages of higher than audio frequencies, and these must be filtered out. The choke-capacitor filter L1-C4 serves this purpose. L1 should not be less than about 80 mh and the capacitor should be about .001 μf.

The input circuit to this common pre-amplifier stage has the over-all volume control R1 as well as a record equalizer made up of R2, C1, C2, and C3. A loud-

ness control is used in series with the 2-megohm volume control R1. This is nothing more than a compensated control which keeps the balance between highs and lows regardless of volume level. R1 is then used to preset the volume level so that the amplifier will not be overdriven on loud signals. To design and construct a compensated control is rather tedious and we use a commercial product (Livingston) which has a good characteristic for this purpose. However, this control is a refinement that can be omitted, if not desired.

The magnetic pickup we use is a Pickering which is coupled to its pre-amplifier through an input transformer. The two primary coils of the transformer (in this case, a Shure microphone cable transformer model A86A) are connected in parallel, the low tones are too predominant. The secondary feeds directly to the grid of the G-E preamplifier, which is slightly modified to suit the pickup-transformer combination. These changes consist of simply removing the resistance-capacitance network in the input circuit of the amplifier, and establishing a feedback loop between the two plates of the 12SC7

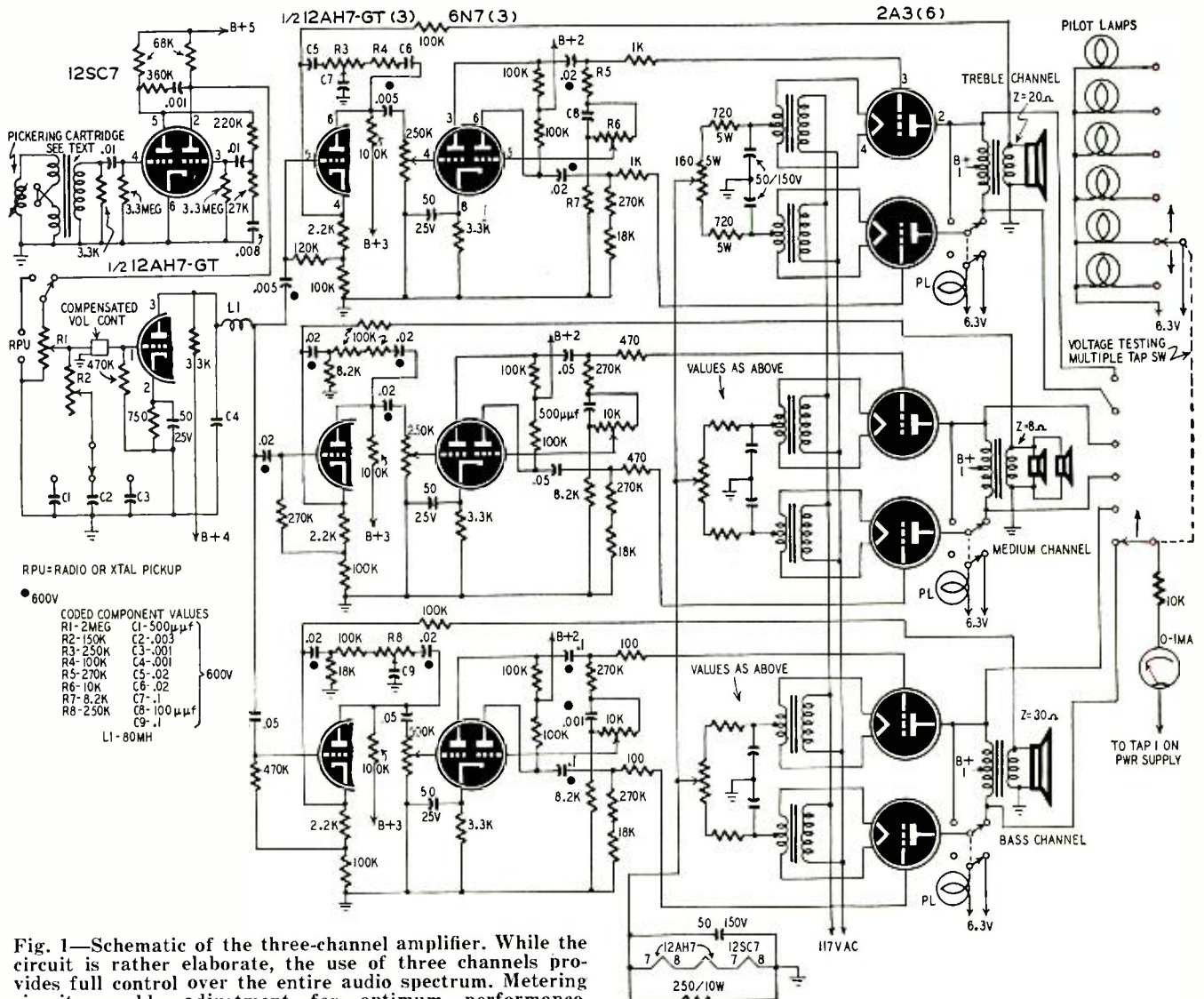


Fig. 1—Schematic of the three-channel amplifier. While the circuit is rather elaborate, the use of three channels provides full control over the entire audio spectrum. Metering circuits enable adjustment for optimum performance.

with the 360,000-ohm, .001- μ f combination.

Because 2A3's in push-pull must be carefully balanced for best results, the circuit is designed so that the bias is adjustable on each pair of output tubes and the plate voltages are metered for making the adjustment. The meter is connected to measure the d.c. voltage drop across both halves of each of the three output transformers. (This method assumes that the two halves of the output transformer primary have equal d.c. resistance. This is usually the case only with the more expensive types of output transformers. Measuring the plate current is more accurate because changes in the voltage drop will be small even for fairly large changes in plate current.—*Editor*)

The heater supply for the two 12AH7's and the 12SC7 is direct current. The heaters of these tubes are put in series and form part of the self-bias resistance for the 2A3's. By this simple expedient, one circuit does two jobs. Direct current for the heater is important in these early stages to keep hum at a low level.

Power supplies

The power supply for the amplifier is built on a separate chassis, as indicated by the photos. The two chassis for the amplifier and power supply are each 11 x 17 x 3 inches. These are mounted side by side on a steel frame and a single $\frac{1}{2}$ -inch metal panel, 12 x 37 inches, holds the meters, pilot lamps, and all controls.

The normal plate-current drain of the

amplifier is about 250 ma, so the power transformer should be capable of supplying at least this current with a little to spare. We had no such transformer available when building the supply, and used two 200-ma transformers in the hookup shown in Fig. 2. The rectifier filaments are in series with each other and with the 5-volt windings of the power transformer. This protects the power transformers in case one of the rectifier tubes should burn out. The 5-volt heater windings must be phased correctly when the circuit is wired up.

The rectified current is fed through a series of filter sections, and voltages are tapped off from these sections for appropriate stages of the amplifier. The plate-current load of the amplifier is metered with a 500-ma d.c. instrument, and the meter is protected by a $\frac{1}{2}$ -amp fuse. The input circuit to the power transformers includes a 350-watt line-voltage selector of the autotransformer type which permits variations from 80 to 150 volts a.c. This can be omitted if the line voltage variations are not large enough to affect the amplifier's operation. The a.c. input voltage is also metered, and two fuses protect the transformers.

The layout

The front panel photo shows the layout of meters, switches, and controls. The power supply is behind the left side of the panel. The a.c. voltmeter and the plate-load-current meter are at the top of this half of the panel. Three fuses and two pilot lights are in a row at the bottom, and halfway up are the ON-OFF

switch and the line-voltage selector switch.

The bottom row of controls on the amplifier side of the panel includes the phase-inverter-control and the bias-control potentiometers for each of the three channels. These six controls are all supplied with locking devices. Below these controls, at the very bottom of the panel, are three pilot lights. The one at left (green) indicates when the treble channel is on; the middle (amber) represents the medium channel; the one at right (red) is the bass channel lamp.

The three toggle switches in a row directly above the row of phase-inverter and bias controls are d.p.d.t. switches used to connect the plates of the output tubes in parallel for balancing and for switching in the pilot lamp of each channel. The two small knobs directly above the toggle switches are on the roll-off frequency setter in the treble channel (at left) and the bass turnover control.

The row of three controls just below the meter are the volume controls for the three channels. The meter on this half of the panel is the 1-ma unit used to check the voltage drop across the transformer windings. The three controls to the left of this meter, which are arranged in a triangle, are (from left to right) the general volume control, the record equalizer capacitor selector switch, and the record equalizer adjuster. To the right of the meter is its selector switch, the radio-phonograph selector toggle switch, and the compensated gain control. The three pilot lights on each side of the meter light up to show which output plate circuit is being metered. The meter selector switch also chooses the appropriate light.

The top chassis photo indicates the general layout of the amplifier. The power-supply layout is not at all critical and will depend largely on the size and shape of the transformers and chokes. The amplifier chassis layout is simplified by the fact that the three channels are nearly identical. Here it is important to use short leads and to shield the low-level signal carrying leads.

In the second part of this article we shall discuss the operation of this deluxe amplifier and how to adjust it to get the most from it.

Materials for amplifier

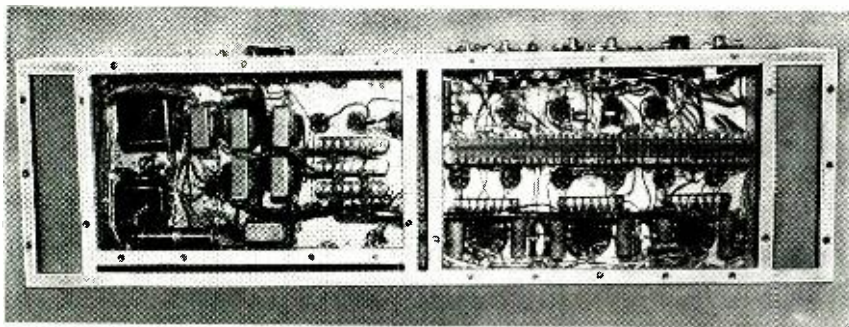
Resistors: 2—100, 1—750, 2—1,000, 2—2,200, 4—3,300, 4—8,200, 4—18,000, 1—33,000, 2—68,000, 20—100,000, 1—120,000, 1—150,000, 7—270,000, 1—360,000, 2—470,000 ohms, 2—3.3 megohms, $\frac{1}{2}$ watt; 1—27,000, 1—33,000, 1—220,000 ohms, 1 watt; 6—720, 1—30 ohms, 5 watts; 1—20,000 ohms, 20 watts; 3—10,000, 4—250,000, 1—500,000 ohms, 1—2 megohms, potentiometers; 3—160 ohms, 5 watts, potentiometers.

Capacitors: 1—.0001, 1—.0005, 4—.001, 2—.003, 2—.005, 10—.02, 4—.05, 1—0.1 μ f, 600 volts, paper; 4—50 μ f, 25 volts, 7—50 μ f, 150 volts, 6—8 μ f, 600 volts, electrolytic.

Inductors: 2—800 volts, c.t. power transformers with 5-volt and 6.3-volt windings; 6—2.5 volts, filament transformers; 1—15 h, 500 ma, 1—15 h, 120 ma, chokes; 1—80 mh, choke; 1—microphone transformer (Shure A-66-A or equivalent); 3—audio output transformers, push-pull 2A3's to voice coil; 1—line-voltage selector (optional).

Miscellaneous: 1—12SC7, 2—12AH7-GT, 3—6N7, 6—2A3, 2—5U4-G, tubes and sockets; 11—pilot lamps and assemblies; 1—1 ma, 1—500 ma, d.c. meters; 1—150-volt a.c. meter; 2—5-amp, 1—1-amp fuses and holders; 3—d.p.d.t., 3—s.p.s.t., 1—6 position, 2-gang switches; chassis, hookup wire, assorted hardware.

(concluded next month)



The wiring under the chassis is neat. The amplifier chassis has only three ground points, one for each channel. Terminal boards simplify the wiring.

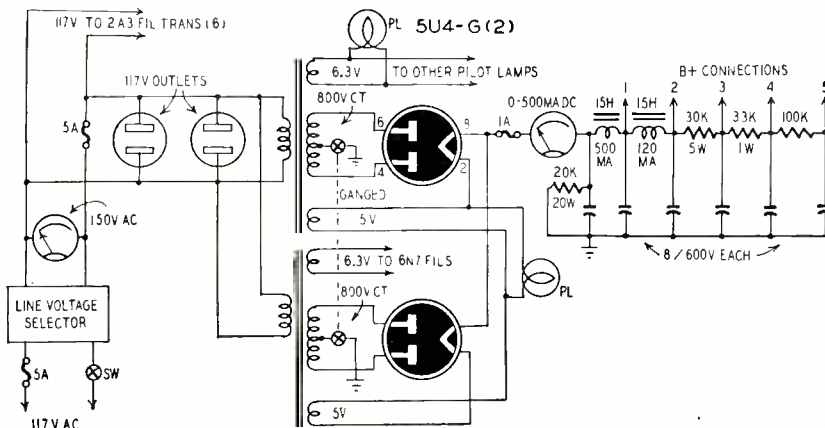


Fig. 2—Circuit of the power supply of the amplifier. One transformer may be used to replace the two shown if its current rating is sufficiently high.

Audio Feedback Design

By

GEORGE FLETCHER COOPER

Part VIII—Negative feedback as a regulator of both output and input impedance of an amplifier circuit

IN THE earlier articles of this series we have seen how the use of negative feedback makes the properties of an amplifier depend more on the behavior of a passive network than on the behavior of the amplifier itself. Since the "passive network" is usually just a couple of resistors, with no distortion and no frequency dependence, the overall circuit gives a flat distortion-free response. Very often, though, that in itself is not enough. For most readers, though not for most amplifiers, the probable load is a loudspeaker: If you get the cone vibrating nicely and then cut off the input you have a coil moving in a magnetic field and thus acting as a generator, so that the impedance seen by the coil looking back into the amplifier is important. I confess freely that I have never discovered just what musical instrument can produce the sounds which make this important to the hi-fi boys; but that idea is un-American, not cricket, or like ordering a certain soft drink in a Bordeaux bar.

Right or wrong, output impedance control is usually considered part of the job of a feedback amplifier. In quite a different connection, so is input impedance control. The commonest example of this is in voltmeter and oscilloscope amplifiers, when we wish to avoid loading down the circuit to which the amplifier is connected. Nine times out of ten a cathode follower, which is just a stage with a feedback β of 1, is used.

Before we consider the amplifier as a whole, it is rather instructive to see what happens to a single tube with feedback. For an example which is reasonably typical, I have drawn in Fig. 1 the characteristics of a 6AQ5 tube: a miniature which will give you 3-4 watts. It is a pentode, and at the standard working point, $E_b = E_c = 250$ volts, $E_g = -12.5$ volts, $I_b = 45$ ma, the transconductance is about 4,000 μ mhos and the impedance about 50,000 ohms. This last figure is the real problem: the optimum load is 5,000 ohms, so that if you transform down to use a 15-ohm loudspeaker, the speaker will be looking back at 150 ohms. It might as well be an open circuit, as far as damping down speaker resonances goes.

Let us see what happens to the tube characteristics if we apply negative feedback. To make the calculations easy, let us apply feedback of $1/10$ of

the plate voltage to the grid. Starting at the point $E_c = 10$, $E_b = 300$, let us reduce E_c to -5 volts; then if E_b drops by 50 volts we shall feed back $+5$ volts to the grid, and we shall be on the same E_c line as the starting point. Similarly, the point $E_c = -10$, $E_b = 300-100$ is on this $E_c = 0$ line.

The resulting characteristic is drawn in Fig. 1: I've drawn the feedback tube curves as broken lines. Forget that I said we had a pentode and you will see that the new characteristics are those of a triode, with an impedance of 2,100 ohms at the original working point. If you connect this plate-grid feedback around a pentode and put it in a black box, anyone measuring the characteristics will think they have a triode. There is only one difference: you can swing this triode down to a plate voltage of 50 without running into grid current; the corresponding limit when the screen and plate are joined together is about 170 volts.

The results of Fig. 1 are well worth a closer study. In the area below $E_c = 0$ there is no grid current, because the feedback circuit will be an a.c. coupling. A pentode with negative feedback of this kind has the same characteristics as a triode, including the triode positive grid region, but you can work over the whole set of characteristics without grid current trouble. I stress this because I have just had a letter from a British reader who doesn't believe that tetrodes can sound as good as triodes. Cast your eye over those curves, they are better than triode curves! Maybe we should call the feedback triode *Bit-ter Rice*.

We can, to some extent, reverse this effect. A typical triode characteristic is shown in Fig. 2. This triode has a μ of about 50, and an impedance of about 20,000 ohms. By putting in a cathode resistor of 2,000 ohms we can make a change of 1 ma in the plate current feed back 2 volts to the grid. The effect of this is shown in part by the broken lines on Fig. 2. These are part of the characteristics of a "black box" tube having an impedance of about 105,000 ohms, which is getting on toward the pentode class. If you need a pentode, and only have a triode handy, this is one way of making the circuit think it sees a pentode.

These two examples of modified tube characteristics have been considered

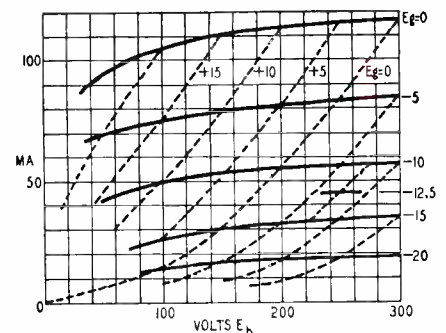


Fig. 1—Negative feedback from plate to grid makes the 6AQ5's characteristic (shown in solid lines) look like those of a triode tube (broken lines).

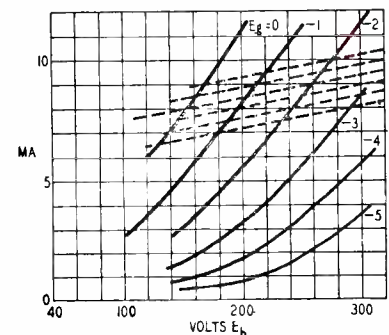


Fig. 2—Negative current feedback will alter the curves of a triode so they will take on the high-impedance characteristic of a pentode (broken line).

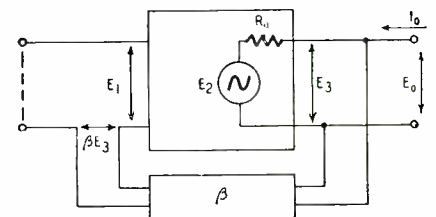


Fig. 3—Voltage feedback network used for calculating the output impedance.

because they provide a useful background to the general discussion of amplifier impedances. Ultimately any amplifier can be considered as a 4-terminal network in a box, and if you don't look inside you cannot be certain that it is not just one tube, with a transconductance of 1 amp/volt, perhaps! Now we can turn to the general amplifier circuit. Fig. 3 shows the general voltage

feedback amplifier, with input short-circuited and output connected to a generator. This generator produces a voltage E_o at the output terminals, and the current flowing into the amplifier is I_o . The amplifier itself has an impedance of R_o and an open-circuit gain, E_2/E_1 of K_o . Notice that we are using now the open-circuit gain, which will be quite a lot higher than the usual loaded gain. For a triode the difference is 6 db, but for a pentode or tetrode it may be much more. The feedback network β is assumed to be of such high impedance that it does not affect the impedances.

In the output mesh, we have this equation:

$$E_o - E_2 = I_o R_o$$

Now $E_2 = K E_1$, and since the only input is that provided by the feedback network $E_1 = \beta E_o$ or, indeed, $-\beta E_o$ since E_2 and E_o are the same here.

Thus $E_2 = -K_o \beta E_o$, and we can substitute in the previous equation:

$$E_o + K_o \beta E_o = I_o R_o$$

$$\frac{E_o}{I_o} = \frac{R_o}{1 + K_o \beta}$$

Of course E_o/I_o is the impedance seen by the generator connected to the output, and if the feedback were absent, $\beta = 0$, the impedance would be R_o . With negative feedback the impedance is reduced by the factor $(1 + K_o \beta)$.

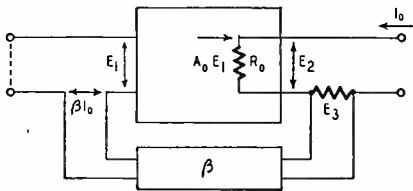


Fig. 4—Network using current feedback.

This feedback was voltage feedback. We could use a circuit like that of Fig. 4, in which the feedback voltage depends on the current in the output circuit. To keep the formulas very simple, the resistance across which the feedback is picked off will be assumed to be small, just as before we assumed that the β network was of infinite impedance. In calculating this circuit we work in terms of current: the amplifier is assumed to have a transconductance of A_o , under short-circuit conditions, so that it produces an output current of $A_o E_1$ for an input of E_1 . When we apply an additional current of I_o , we have a current of $(I_o + A_o E_1)$ through R_o , so that the voltage across the output terminals is:

$$E_2 = (I_o + A_o E_1) R_o$$

The feedback network (including the small resistor across which E_3 is produced) delivers a voltage βI_o to the input terminals, and since the input has no other supply $E_1 = \beta I_o$.

$$\text{Thus } E_2 = (I_o + A_o \beta I_o) R_o$$

The admittance seen at the output is I_o/E_2 and is

$$\frac{1}{R_o} \times \frac{1}{1 + A_o \beta}$$

If there were no feedback ($\beta = 0$) this would be just $1/R_o$. With current

negative feedback, therefore, the output admittance is reduced by the factor $(1 + A_o \beta)$. This means, of course, that the impedance is increased by this factor.

It must be noted that the factor A_o is not the same as the K_o we have discussed, and it is not the same as the factor K in the $(1 + K \beta)$ term we used in the distortion and gain effects in earlier articles. This means that we must make a separate calculation when determining the output impedance. When using voltage feedback we must use the equation

$$M = \frac{\mu R}{R + R_o}$$

for the gain of the last stage in determining the gain factor K , but $M_o = \mu$ for the impedance factor K_o . If, however, the feedback network uses resistors of normal value, we may find it more accurate to write

$$M_o = \frac{\mu R'}{R' + R_o}$$

where R' is the input impedance of the feedback network. We also ought to bring the output transformer losses into R' . Usually this means that K_o is about 3 times the usual value of K .

By using positive feedback, the term $(1 + K_o \beta)$ can be made less than unity. Thus, positive voltage feedback increases the output impedance and positive current feedback reduces the output impedance. We can mix positive voltage feedback and negative current feedback to give a very high impedance, for example, without losing too much gain. I should like to devote a lot more space to this, but it is of rather restricted interest. As examples of what can be done, I may say that I have one small amplifier, using a 12AT7, which has an impedance, at the high side of the output transformer, of something around 5 megohms. This is better than pentode performance. Another amplifier, using pentodes, gives an impedance of 0.1 ohm when designed to work into a 25-ohm load: this uses positive current and negative voltage feedbacks. There are good reasons for these designs: the pentode is needed to get power at low supply voltage, the 12AT7 to get gain from a single bottle, and the extreme impedances are "musts."

The circuits for giving voltage and current feedback are summarized in Fig. 5. F is the feedback voltage in each case, and a, b, c are voltage feedback, d, e, f are current feedback. The table is a summary showing whether the feedback should go to cathode (k) or grid (g) of an earlier stage to be negative or positive. The plus signs show positive feedback, the minus signs negative. Thus in a 3-stage circuit you must feed back from cathode to cathode (circuit d) or from anode to grid (circuit e) to get negative current feedback.

For the sake of completeness I must mention the bridge feedback circuit. In this the feedback does not affect the impedance, but having mentioned it I

should add that I have never seen it used. Tube impedances are not so constant that anyone wants to keep them unaffected.

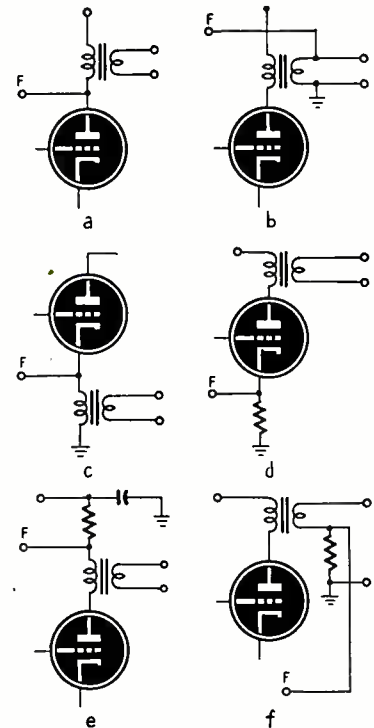


Fig. 5—Skeleton circuits showing six ways to pick off feedback F . The first three, $a, b,$ and c , are voltage feedback; the others are current feedback.

Now let us consider the input impedance. A typical input circuit is shown in Fig. 6, and although I have shown a resistor between grid and cathode, this could be a more complicated impedance. The biasing arrangements are also neglected. In this circuit, the input to the amplifier section K is V_1 , and the voltage developed by the feedback circuit is $V_2 = K \beta V_1$. We must have $E_o = E_1 + E_2 = (1 + K \beta) E_1$, and from this we could deduce that the gain would fall by a factor $(1 + K \beta)$ when feedback was added, because we now need an input of E_o to produce E_1 at the grid.

The current which flows through R is given by

$$I_o = E_o/R = E_o/R(1 + K \beta)$$

So far as any circuit connected to the input can tell, this current is produced by E_o , so that the input impedance is

$$\frac{E_o}{I_o} = R(1 + K \beta)$$

Table for Feedback Connections				
No. of stages	Circuit of Fig. 5			
	a	c	d	e
1	g-			g-
2	k- g+	g- k+	g- k+	k- g+
3	g- k+	k- g+	k- g+	g- k+
4	k- g+	g- k+	g- k+	k- g+

Circuits b and f depend on transformer sense.

The impedance therefore has been increased by a factor $(1 + K\beta)$. This may be 10 to 100, so that a resistance of 1 megohm, which is all we can normally use because of gas current in the tube, looks like 10-100 megohms to the external circuit. The input capacitance is reduced, too, which is important if you are using a crystal pickup. Notice, how-

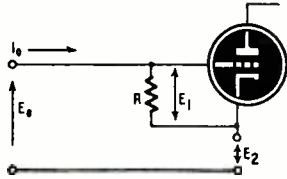


Fig. 6—Amplifier input circuit having series-connected feedback at cathode.

ever, that positive feedback in this connection will reduce the input impedance, since then $(1 + K\beta)$ is less than unity.

An alternate way of connecting the feedback is shown in Fig. 7. The current which flows into this circuit is

$$I_o = \frac{E_o - E_2}{R_1 + R_2}$$

Now

$$E_2 = -K\beta E_1$$

and

$$E_1 = E_o - I_o R_1$$

We therefore have

$$E_2 = -K\beta E_o + K\beta I_o R_1$$

and

which we rearrange

$$I_o (R_1 + R_2 + K\beta R_1) = E_o (1 + K\beta)$$

giving

$$\frac{E_o}{I_o} = R_1 + \frac{R_2}{1 + K\beta}$$

The R_1 term is the impedance of the external generator, so that the input impedance, R_2 without feedback, is reduced by the factor $(1 + K\beta)$ with negative feedback. As before, if the feedback is positive this is an increase in input impedance. I have seen no uses

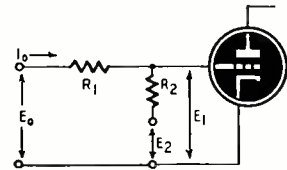


Fig. 7—A parallel hookup for feedback.

for this particular connection described anywhere, but it would seem to be quite possible to apply negative feedback to the cathode and positive to the grid to produce an extraordinarily high input impedance. The negative feedback would stabilize the gain so that the term $(1 - K\beta)$ in the positive feedback equation could be made quite small.

It has been claimed by Griffiths (*Wireless World*, March, 1950) that using Fig. 7 one can get more distortion reduction than loss of gain, mainly as a result of changes in the matching conditions at the input. I have not examined his results carefully, but I do not like using this circuit since the input impedance depends on the value of K .

In many applications it is necessary to provide a controlled value of input impedance, which involves the use of the circuit of Fig. 6 with an additional shunt resistor across the input. Often, too, we need a good 600-ohm output impedance, and then a high impedance shunted by 600 ohms is used.

This has only been a general survey of the problems of impedance control. If an amplifier is needed with some special impedance properties, a closer study may be required, but for almost all jobs the discussion here will be sufficient. Always the effect of feedback is to modify the apparent tube characteristics, and it is probably wise to

point out one important thing. If you turn a tetrode into a triode by means of feedback, the optimum load is unchanged: you should not try to match this "triode." I have checked this statement very carefully, both with modified characteristics and by actual experiment. This is specially important if you are using a high degree of feedback to get a low impedance for damping a loudspeaker, or to get a high impedance for some other purpose. And don't forget, if you want a low impedance, to allow for the resistance of the output transformer windings. This is also important.

(Continued next month)

Audio V.T.V.M. Measures Millivolts

Many audio enthusiasts who construct amplifiers and experiment with a.f. circuits have need for an audio millivoltmeter like the one described here through courtesy of Cornell-Dubilier Electric Corp.

Using a 1-ma d.c. meter, the full-scale ranges of the instrument are .01, 0.1, 1.0, 10 and 100 volts. The response is linear, so the standard 1-ma meter scale is used on all ranges. The 12AX7 is used as two high-gain, resistance-coupled triodes in cascade. The output of the second stage is rectified by four 1N34's in a bridge circuit and fed to the meter at a level of 10 volts r.m.s. for full-scale deflection on all ranges. The power and range switches are on the panel. Calibration controls R_1 and R_2 have slotted shafts and are mounted on the chassis.

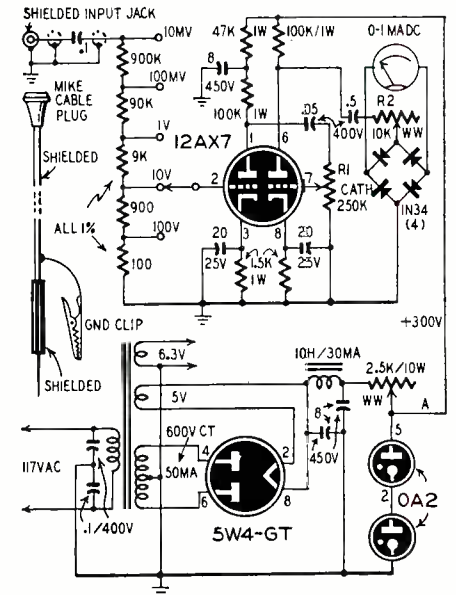
Take the following precautions when wiring the unit: (1) Return all grounds to one point on the chassis. (2) Use shielded leads at points shown on the diagram. (3) Use a shielded, cushioned socket for the 12AX7. (4) The range switch must have ceramic insulation. (5) Twist heater and a.c. power leads into pairs and clamp close to the chassis. Keep them away from the 12AX7 grid leads. (6) Ground the back cover of R_1 . (7) Use shielded cable and plug on the test prod. (8) All wiring should be point-to-point with solid, insulated hookup wire. (9) Do not leave out the voltage regulator tubes or filter choke to save space or cut cost. Without regulation, the accuracy of the meter varies with line voltage. When a resistor is substituted for the choke, the meter is unstable when the signal voltage is near the fundamental, harmonic, or subharmonic of the line frequency. (10) Mount the unit in a metal case.

To adjust the instrument, break the B-plus line at A, insert a 50- or 100-ma meter in series with the plate of the top 0A2 and the slider on the 2,500-ohm resistor. Set the slider for exactly 30 ma through the meter. Remove the meter and re-connect the B-plus lead.

Set the range switch to 100 volts. Adjust R_1 to approximately one-half scale and R_2 to one-quarter scale. Do not plug in the probe.

Let the unit warm up for about 5

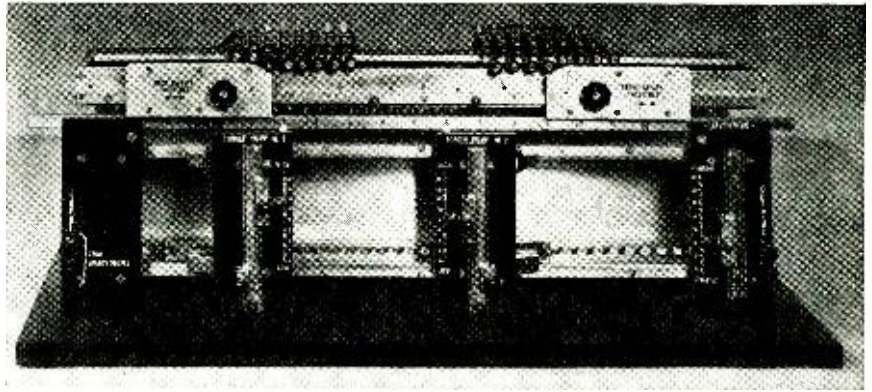
minutes. Turn the range switch through its ranges and watch the meter for any steady deflection which is an indication of oscillation, noise, or hum. If there is a steady deflection, replace the meter with headphones and identify the signal. If it is hum, ground the center terminal of the input jack. If the hum disappears, it is caused by a strong a.c. field near the unit. If it does not, it may be caused by failure to ground one heater lead, faulty shielding, excessive lead length between the range switch and the input grid, or by mounting the power supply too near the 12AX7.



Continuous crackling, hissing, or noise is probably caused by defective tubes, resistors, or capacitors.

To calibrate, set the range switch to 100 volts, R_1 to half scale, and R_2 to maximum resistance. Plug in the test lead and connect it to an accurate 10-volt a.c. source. A 60-cycle source will do, but 1,000 cycles will provide better accuracy. Throw the switch to 10 volts and adjust R_2 so the meter reads exactly full scale. Vary the input from 0 to 10 in 1-volt steps. If the readings cramp at higher voltages, the second triode is overloading. Decrease the setting of R_1 .

—end—



A closeup photo of the equipment. The tongue hump and lip opening sliders are in front, and the contacts for the sliding cavity shorteners project on top.

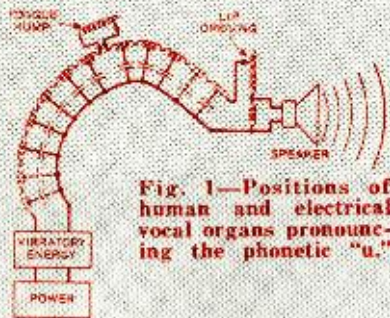
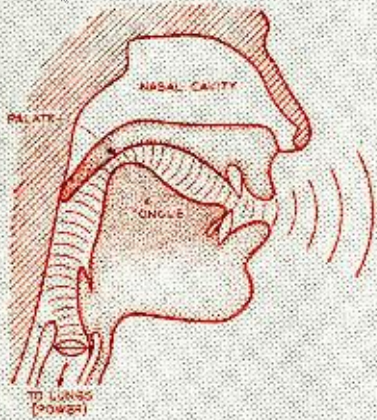


Fig. 1—Positions of human and electrical vocal organs pronouncing the phonetic "u."

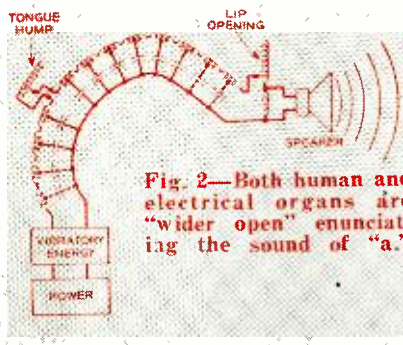
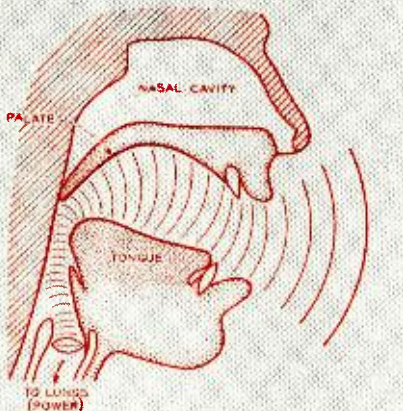


Fig. 2—Both human and electrical organs are "wider open" enunciating the sound of "a."

ELECTRIC VOICE

This electrical analog of the human vocal apparatus produces good vowel sounds

By ERIC LESLIE

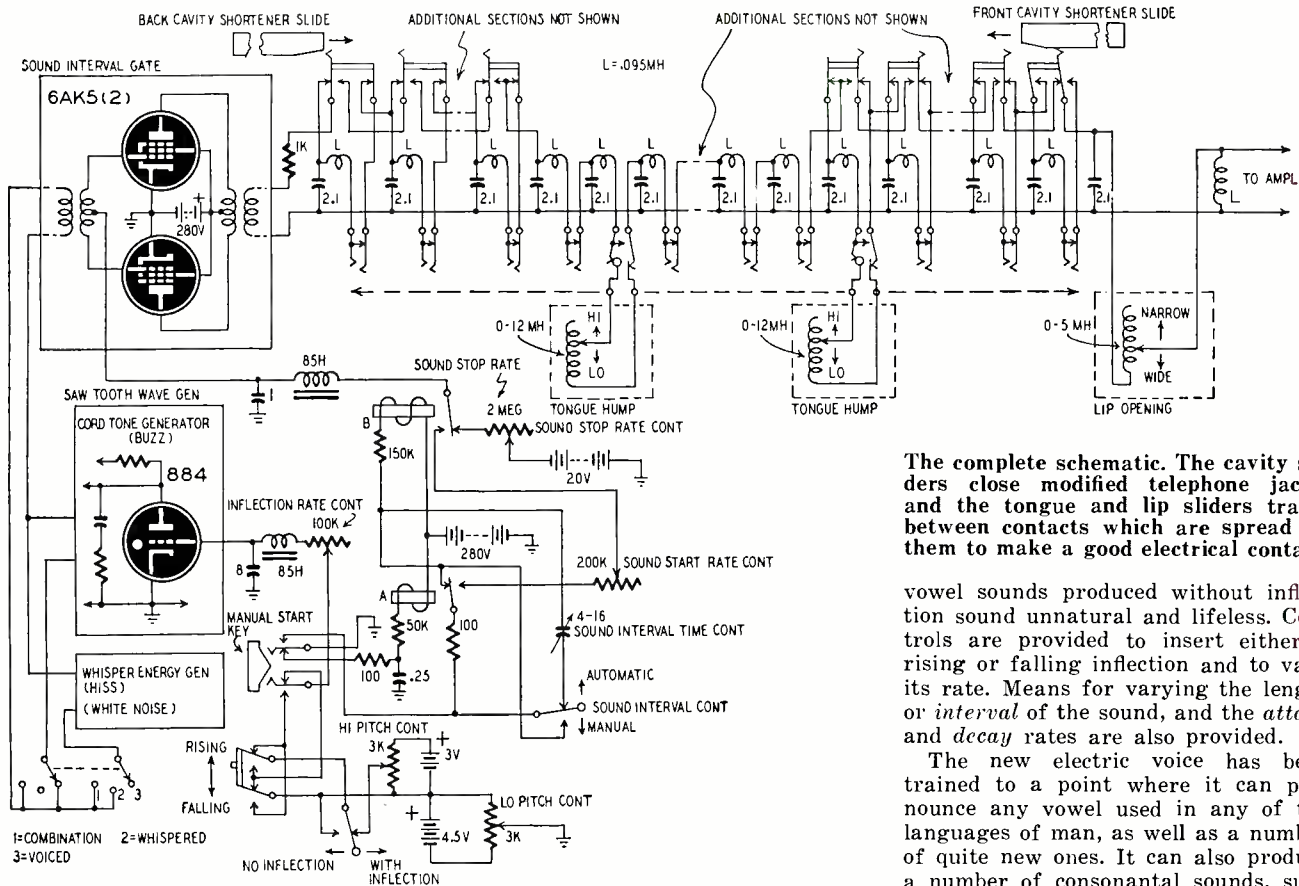
WE ALL used analogies when we learned radio. Current flow was illustrated by water flowing through a pipe. With a reciprocating pump added, alternating current was illustrated. Radio waves were (all too simply) represented by a stone thrown into water. Tesla even devised an "oscillator" with a weight for inductance and a spring for capacitance, with steam (from the building's heating circuit) as the source of power. So successful was the analogy that it not only oscillated furiously at a frequency set by the spring tension and the weight, but could also be "loaded," furnishing power for small workbench appliances. So we went through electricity and radio, getting acquainted with each new phenomenon with the help of familiar mechanical analogies.

As we learned more about electronics some of these phenomena turned out to be far more simple than the analogies used to explain them. It was by no means surprising that the analogies should reverse, and that engineers should study the action of a vibrating weight at the end of a spring with the help of an electrical circuit analogy. Radio engineers found it worthwhile to break down the mass, compliance, and friction of a loudspeaker into inductance, capacitance, and resistance, when

studying the action of the cone. Books have been written devoted to describing mechanical actions in terms of electrical circuits.

The reason that such analogies are possible is that we can describe the behavior of both electrical and mechanical circuits with mathematical equations that look exactly alike. Thus in one equation the symbol for voltage may take the place of the symbol for force in the other; inductance is analogous to mass, etc. The same applies also to the equations of thermodynamics, acoustics, and other systems so that a circuit in one of these systems can have an analogy in any of the others. Engineers make frequent use of this fact.

The electric voice equipment shown on our cover is a recent and daring example of the analog-in-reverse. It was designed and constructed by H. K. Dunn and L. O. Schott of the Bell Telephone Laboratories, an organization which makes study of the human voice and human speech one of its chief activities. Since the human vocal apparatus can be represented with an electrical analog, they decided to set up one and feed it from oscillators which produce signals electrically equivalent in frequency and composition to those produced by the vocal cords. Then if its output were turned into sound by a loudspeaker,



The complete schematic. The cavity sliders close modified telephone jacks, and the tongue and lip sliders travel between contacts which are spread by them to make a good electrical contact.

vowel sounds produced without inflection sound unnatural and lifeless. Controls are provided to insert either a rising or falling inflection and to vary its rate. Means for varying the length or interval of the sound, and the attack and decay rates are also provided.

The new electric voice has been trained to a point where it can pronounce any vowel used in any of the languages of man, as well as a number of quite new ones. It can also produce a number of consonantal sounds, such as the fricatives *f* and *v*, *s* and *z*, and the sounds of *l* and *r*, though some of these require certain additional apparatus not shown in the schematic. Work has been in progress to make it possible to pronounce more of the consonants, but has had to give way, for the moment at least, to projects considered more vital to the national interest. So the time when we will have an artificial voice which can recite "Mary's Little Lamb" is still far in the future. Meanwhile the equipment is a valuable device for studying human speech sounds and their formation in detail.

—end—

GUIDED MISSILE RECORDER

Magnetic recorders using a metal tape 6 inches wide and 150 feet long will be placed in the noses of guided missiles to record data that ordinarily is automatically sent out by radio. As the rockets penetrate the atmosphere above the earth, there is often difficulty with reception of the automatically transmitted signals. The magnetic recorder, announced recently, is manufactured by United Aircraft for the Navy's Bureau of Ordnance. Weighing only 46 pounds, the machine can record 200 pieces of information simultaneously and continuously. The tape is led into an armored cylinder that withstands the shock of dashing into the ground. The tape, played back through a transcriber, enables personnel to make graphs of air pressures, temperatures, and so on. The device was developed by the Armour Research Foundation.

sounds similar to those of the human voice should be produced.

Several attempts to synthesize speech sounds have been made (see "Manufactured Speech," RADIO-CRAFT, August, 1939, for a description of the voder, or vocoder). Voice sounds were analyzed into their frequency components with a series of bandpass filters, like those shown in the illustration of visible speech equipment on page 235, RADIO-CRAFT, January, 1946. Then the frequencies which appear in a given sound were picked out—usually from a bank of tone generators—and mixed in the correct proportions to produce the sound.

That method dealt with the disembodied sounds, without reference to the mechanism which produced them originally. Dunn and Schott started out with the opposite approach, to produce an electrical analog of just that speech-producing mechanism.

The human vocal apparatus, consisting of the throat, tongue, and lips, can be represented by a cylindrical cavity about a square inch in cross-section and about five inches in length. The area and length of this cavity can be varied to some extent by the speaker's throat muscles. Its size and shape is still further modified by the back and tip of the tongue, and by the lips, any or all of which may be moved to pronounce a given sound.

The most exact analog of the human vocal apparatus would be a section of transmission line, with inductance and capacitance distributed along its length. A section of waveguide might be even

more exact. But at voice frequencies such models would be too big to construct, so lumped constants (coils and capacitors) are used.

The vocal cavity is represented electrically by 24 sections of transmission line. The end sections of these are shown in the schematic. Sections can be cut off or added at either front or rear (or both) of the electrical cavity, varying the timbre from that of a baby to the voice of a bass singer.

Two variable inductors serve as the tongue hump (back of tongue) and tongue tip. The tongue hump divides the cavity into two parts, as the real tongue hump tends to do in speech. A similar inductor acts as the lip opening. High inductance in these circuits is equivalent to constricted throat passages and narrow lip opening; lower inductance represents wider vocal passages and a more open mouth. Fig. 1 is a representation of the human and electrical vocal tract while pronouncing the phonetic "u" (as in "rule"). Fig. 2 is the position while pronouncing the vowel "ah." (The drawings were made before the forward tongue hump had been added to the circuit.)

The "larynx" and control circuits appear at the left end of the schematic. A sawtooth oscillator and "white-noise" generator provide, respectively, the electrical equivalents of voiced and unvoiced sounds from the vocal cords. An important part of the circuit is the inflection control. The human voice does not maintain exact pitch while pronouncing even short vowel sounds, and

U. H. F. is The Keynote of Annual I. R. E. Show

RADIO engineers look to the annual I.R.E. conventions and exhibitions for a key to the future of electronic development. This year's meeting indicated plainly that the immediate future of electronics is in the higher frequencies. Equipment and discussions aimed at u.h.f. television broadcasting and at other commercial and military uses in the ultra-highs signalled that trend unmistakably.

One of the first signposts pointing toward the ultra-highs was the ceramic triode announced by General Electric, illustrated in Photo A. This tube, only

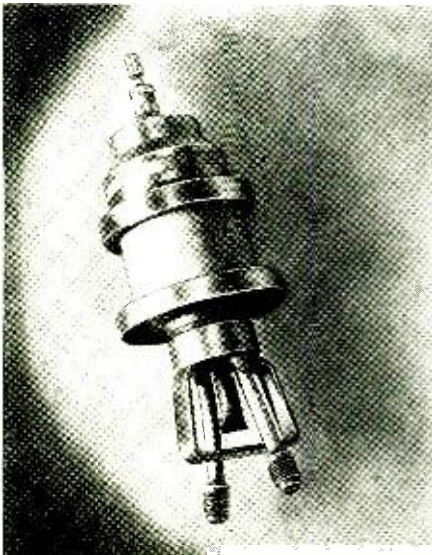


Photo A—The new ceramic tube by G-E which has an output of 1 kw at 900 mc.

8 inches long, will operate at 1 kilowatt output up to 900 mc. It is designed to be used, like the lighthouse type receiving tubes, in a special cavity built for it.

The same company, in co-operation with Varian Associates, approached the ultra-highs from the opposite direction, with a velocity-modulated tube. These tubes, best known under the Sperry trademark *Klystron*, are normally built for centimeter waves, and the spectrum between 500 and 1,000 mc looks like very low frequency to them. But, as it was possible to get up into the ultra-highs with conventional tubes by making them smaller and reducing element spacing, so by building bigger it was possible to get down into the u.h.f. television band with a velocity-modulated tube. The result is shown in Photo B, a picture of the big tube in place in an experimental transmitter. The two large cylinders that look like coiled wire are just that. They are focusing coils to control the beam of electrons as it "drifts" down the tube in regular velocity-modulation style.

On the receiving end, the little magnetron described in our January issue appeared with means for tuning it over a band comparatively wide for a magnetron. Acting as a receiver oscillator, it is expected to do for u.h.f. reception what the bigger tubes just described will do for transmission. A demonstration setup, with the tube, tuning equipment, and a meter to show output against frequency, appears in Photo C.

Still another possible future aid to u.h.f. television and other receiving circuits was a miniature traveling-wave

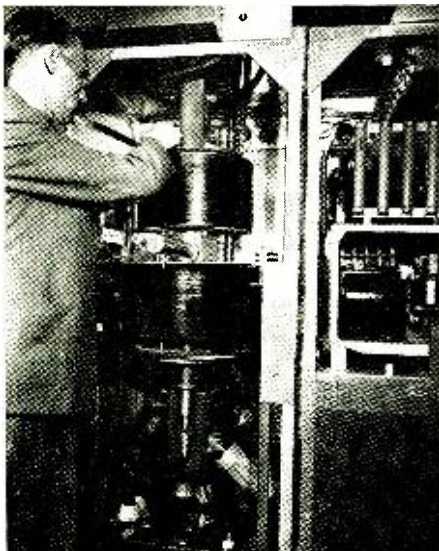


Photo B—G-E Engineer H. M. Crosby is adjusting the u.h.f. velocity modulated tube which operates at around 500 mc.



Photo C—Another G-E showpiece was the miniature magnetron for u.h.f. TV. Here H. W. A. Chalberg makes an adjustment on a demonstration circuit.

tube (Photo D) described by Robert Adler of Zenith. Means of adapting standard receivers to u.h.f. were also discussed. A paper on a u.h.f. converter for standard television receivers was read by B. F. Tyson of Sylvania. He described it as a low-cost design, giving adequate performance, which should serve a useful purpose in the early years of u.h.f. television broadcasting.

For the audio man?

Another component that may have revolutionary applications is the *Plasmatron*, described by E. O. Johnson of RCA Laboratories. The Plasmatron is a gas tube that will respond to audio or low-frequency radio signals. The secret of this tube is in its two cathodes. The regular cathode and anode have a relatively low voltage between them, as shown in Fig. 1. An auxiliary cathode



Photo D—Miniature traveling wave tube.

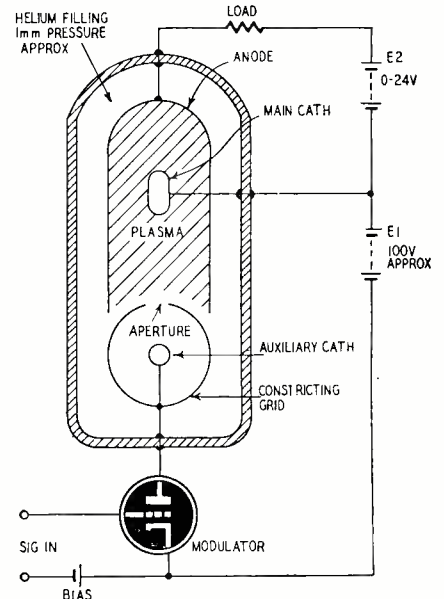


Fig. 1—Diagram of a Plasmatron in a series feed hookup. Note two cathodes.

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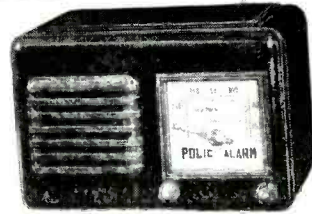
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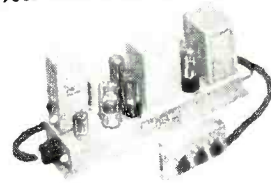
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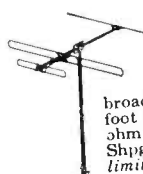
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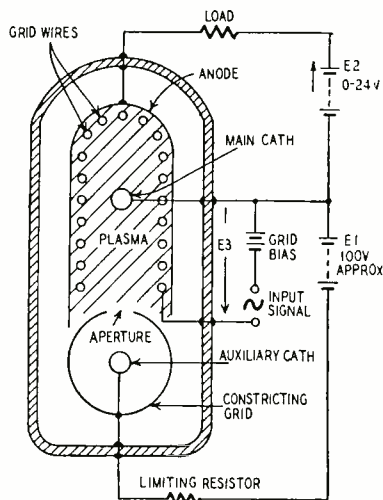


Fig. 2—Plasmatron circuit using grid.

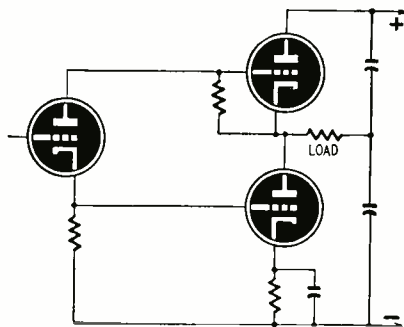


Fig. 3—Single-ended push-pull circuit.



Photo E—The G-string u.h.f. antenna.

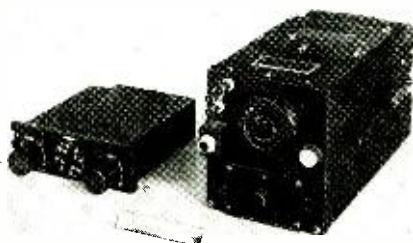


Photo F—Miniature aircraft receiver.

is operated at about 100 volts negative to the main cathode. Electrons from this cathode ionize the helium gas in the tube. Two modulation methods are possible. In Fig. 1 the signal is applied in series with the auxiliary cathode, and the varying electron stream from that cathode changes the conductivity of the ionized gas, or plasma, between main cathode and anode, thus varying the current in that circuit as well. Fig. 2 illustrates the second method. A grid is inserted between main cathode and anode, with the auxiliary cathode still ionizing the gas. Due to low plate voltage and the tube design, the grid does not lose control, but compels the main cathode-anode current to follow an input signal.

The new tube is still in the experimental stage, but very interesting applications suggest themselves. Most exciting is the possibility that it might match a loudspeaker without an output transformer, the Plasmatron working directly into a voice coil.

Single-ended push-pull

A single-ended push-pull amplifier was another paradoxical-sounding device. Described by Arnold Peterson and Donald B. Sinclair of General Radio Co., it is a true push-pull stage, as shown in the simplified diagram, Fig. 3. The two tubes are in series across the d.c. supply and the load is connected between the junction point of the two tubes to the plate supply. In practical circuits this is done with the help of a special output transformer, with separate windings through which the screens of pentode amplifiers may be fed. The grids of the two tubes are fed 180° out of phase, in true push-pull style.

The advantage of the circuit is that it has a very low output impedance—between 200 and 300 ohms with high-perveance tubes. It is conceivable that high-impedance voice coils might be designed which would permit this circuit to operate without an output transformer. The circuit maintains the advantage of push-pull cancellation of distortion, and in addition is able to supply a single-ended load.

Strangely enough for an organization whose members depend to no small extent on commercial broadcasting for their living, the paper which received the most lively reception was the *Practical Speech Silencer* described by R. Clark Jones. The paper was sponsored by the Polaroid Corporation, though the device is Mr. Jones' personal invention. No details were available pending application for patent, but the designer made it known that the equipment depends on the abruptness of the sounds in speech as opposed to the more continuous character of a musical program. A few clearly enunciated syllables sufficed to cut off the program, which started again after a few bars of music. Demonstrated with recorded segments of radio programs, the instrument brought howls of applause from the assembled engineers.

An interesting feature was the way

singing commercials were treated. The silencer cut them off like speech. Mr. Jones explained that since the advertiser was especially interested in getting his message across, the enunciation in a singing commercial was so clear and careful as to be more like speech than music, and was silenced, though ordinary songs were not cut off.

More was heard on the G-string, that fantastically wide-band and inexpensive high-frequency transmission line originally reported in *RADIO-ELECTRONICS*, May, 1950, and further described in Samuel Freedman's article, page 24 in this issue. Latest application is the G-string antenna mast shown in Photo E. The signals travel along the surface of the mast rather than inside a cable, then are reflected by the two flat plates, which, mounted at 45°, send the waves in a horizontal direction.

Miniaturization methods

More progress was shown in sub-miniaturization. The Bureau of Standards showed a 12-tube receiver for aircraft use which tunes from 190 to 550 kc and has a 135-kc i.f. Its size is shown graphically in Photo F, where it sits beside its well-known World War II equivalent, and the interior construction is shown in Photo G.

The Signal Corps exhibited an "auto-assembly" system of miniature construction which is almost the reverse of the printed circuit. The circuit is drawn on a copper-foil covered ceramic plate. Then the *undesired* parts are etched off.

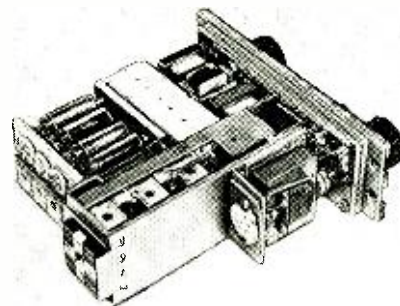
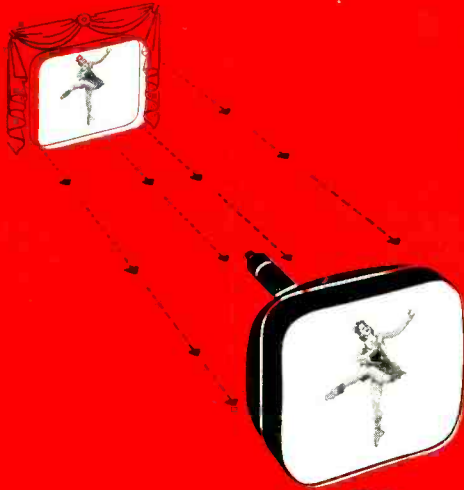


Photo G—The miniature set's insides.



Photo H—The miniature d.c. amplifier.

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leaving the circuit in copper lines. Components are attached along these lines by pushing their leads through pre-fabricated holes in the plates, and the whole dipped in solder, to produce a small, rugged unit of excellent conductivity and extreme ease of assembly.

The miniature high-frequency d.c. amplifier of Photo H is the result of normal miniaturization plus reducing the number of parts. The old-type conventional amplifier, beside it, uses at least 240 parts, whereas the new one requires only 35. The amplifier was described by E. L. Crosby, Jr., of Bendix Radio, who pointed out that the new circuit technique which made this amplifier possible, in addition to making the amplifier smaller, reduced the

chances of component failure, since the fewer the parts, the fewer the opportunities for component breakdown. Designed at present for radar, the amplifier may find wide application in the higher frequencies.

The most striking general impression that a visitor to the show got was that we are still only treading lightly around the obscure boundaries of a vast new era of electronics. The items described in this article and many other items at the show seem to be only the basic components that may become essential parts of entirely new systems, the likes of which we cannot yet fully imagine. We shall no doubt see our progress into this new era more clearly at next year's I.R.E. show.

—end—

New Tubes of the Month

As electrostatically focused kinescopes will soon be making their appearance in more and more new large-screen televisers, it would be well to review their characteristics briefly. Three models are now or will soon be in production by major tube manufacturers, the 14GP4, 17FP4, and 20FP4. These tubes do not use focusing magnets, but have a special gun design which allows the beam to be focused with a zero-current electrostatic potential.

The focusing voltage is about 25% of the second anode potential. It can be obtained from a bleeder across the high-voltage supply. This is generally unsatisfactory because the added drain on the h.v. rectifier will drop the picture tube voltage and the regulation is poor. A better method is to use a separate rectifier, fed from the horizontal output tube plate. Circuits for doing this appear in the May issue of RADIO-ELECTRONICS on page 27.

The Rauland company has announced another electrostatically focused picture tube type which uses from 150 to 350 volts for focusing, but technical data is not yet available.

A new secondary emission, wide-band amplifier tube having a transconductance of 25,000 micromhos and for use at frequencies up to 200 mc is announced by National Union. Designated as type 5857, the tube is contained in a miniature envelope with a 9-pin base. It is also useful as a square wave generator, providing rise times on the order of .005 microseconds.

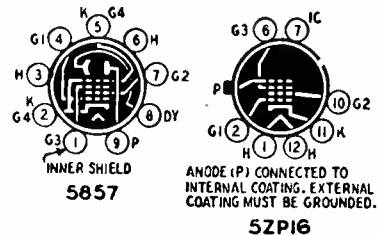
The construction of the 5857 is such that the electrons pass through the grids in the usual manner and then strike a dynode. Here, through secondary emission, the current is increased by a factor of four and proceeds to the plate. In a sample three-stage, stagger-tuned amplifier, 20 mc wide and centered at 100 mc, these tubes produce an overall gain of 1,200. The same circuit using 6AK5's has a gain of only 47. The tube is intended for radar use and other special applications, where its high cost is not important.

RCA has a new flying-spot cathode-ray tube, the 5ZP16. It is designed for high-quality video signal generators. A

flying spot generator produces still pictures, like a monoscope, but has the advantage that the picture may be



The 5ZP16 flying-spot cathode-ray tube.



Basing diagrams of the two new tubes.



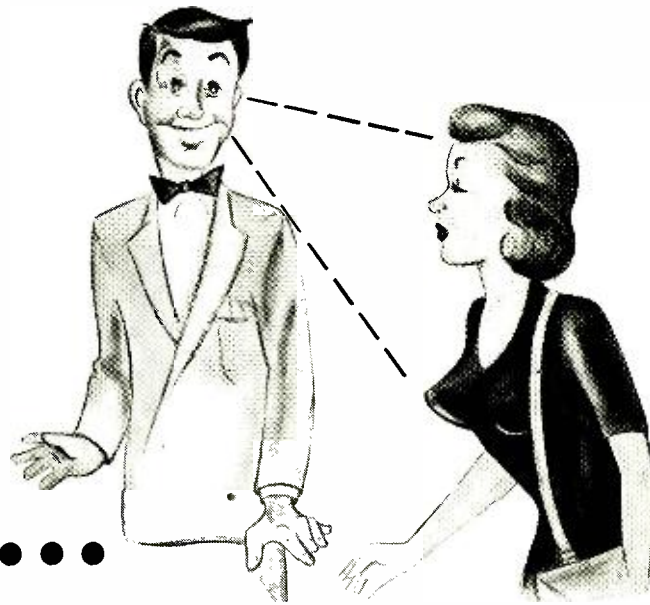
Photo of the secondary emission tube.

changed at will and has a halftone fidelity like that of photographic film. This tube supersedes the 5WP15 for new equipment design.

—end—

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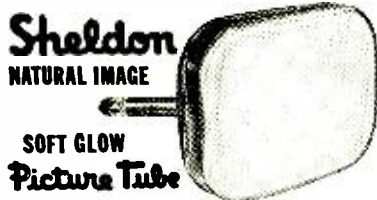
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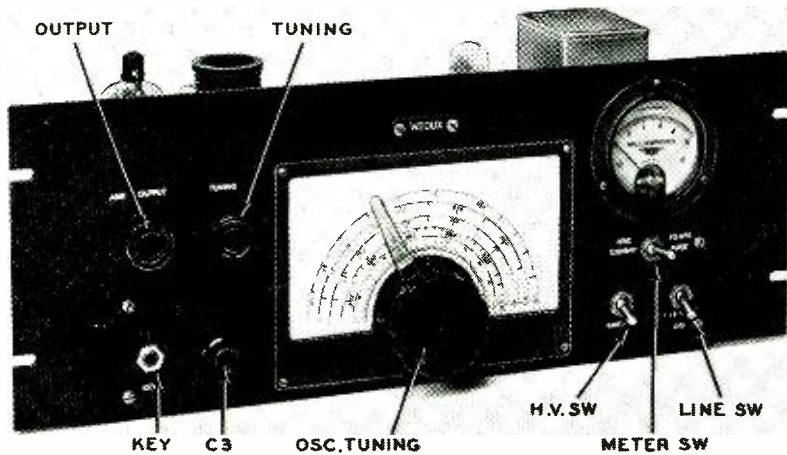
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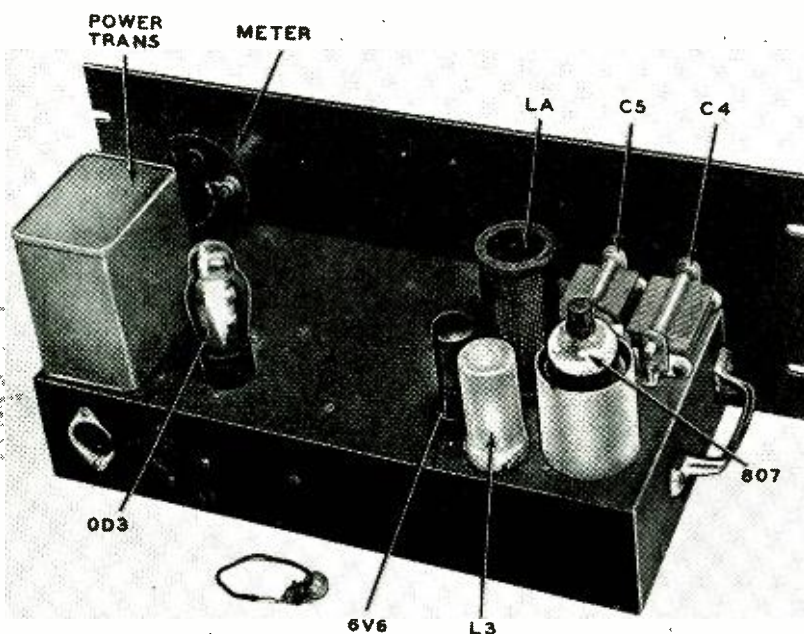
Four-Band C. W. Ham Transmitter

Plug-in coils in the final stage select ample output on 15, 20, 40, or 80 meter bands, eliminating complex bandswitching

By I. QUEEN



The transmitter panel. The meter reads the 807 grid current and power input.



The transmitter from the rear. The plug-in coil marked LA is the output coil L4.

THIS transmitter operates on several ham bands without complicated switching. It is based on the excellent Clapp or series-tuned oscillator. Except for the final high voltage, all grid, filament, and plate power supplies are self-contained. (See Fig. 1) The v.f.o. (6AK5) resonates in the 80-meter band. A screen-grid amplifier (6SJ7) follows, also on 80. Next is a broad-band stage (6V6) tuned to 40 meters. No neutralization is required and there is ample output on both 40 and 80 meters from this tube. The final (807) operates straight through on either 40 or 80, and it doubles or triples for 20 or 15. Although output is maximum on 40, there is only little tapering off at 15, 20, and 80. The output band is chosen by plug-in coils.

The oscillator is built within a 3 x 4 x 5-inch metal box without top and bottom covers. This box is screwed beneath the 15 x 7 x 3-inch transmitter chassis. When the chassis bottom cover is put in place, the oscillator is completely shielded. Only the 6AK5 extends outside the box and this is shielded also.

For best results L1, the oscillator coil, must have high Q and be ruggedly built. After trying several we came across the power amplifier coil (7-9 mc) for the BC-459. This proved excellent for the job and is available at very low cost as surplus. The coil is a variometer. The outer winding has heavy wire on a grooved ceramic form 1½ inches in diameter. It has 15 turns occupying about ¾ inch, then a ¼-inch space, then 5 more turns. The inner winding of 4 turns is arranged to rotate through 180° and the total inductance is variable over a considerable range. There is also a slug for fine adjustment.

When the BC-459 coil was wired in, the low-frequency end of the tuning range came just above 3.5 mc. Therefore we removed about ¼ turn from the outer winding. The variometer control is adjusted to reach 3.5 mc with the tuning capacitor at maximum. The high-frequency limit will then be above 3.75 mc, or a little more than half the band. The limited range is convenient for multiplying into the other bands. Incidentally, the fourth harmonic of 3.75 mc makes a good check point against WWV at 15.0 mc.

Subsequent minor retuning may be done with the slug at the top of the coil. It is reached by a long screwdriver through a hole drilled through the transmitter chassis.

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A.C. VOLTS: 0 to 15/30/150/300/1,500/3,000 Volts
OUTPUT VOLTS: 0 to 15/30/150/300/1,500/3,000 Volts
D.C. CURRENT: 0 to 1.5/15/150 Ma. 0 to 1.5 Amperes
RESISTANCE: 0 to 500/100,000 Ohms 0 to 10 Megohms
CAPACITY: .001 to .2 Mfd. .1 to 4 Mfd. (Quality test for electrolytics)
REACTANCE: 700 to 27,000 Ohms 13,000 Ohms to 3 Megohms
INDUCTANCE: 1.75 to 70 Henries 35 to 8,000 Henries
DECIBELS: -10 to +18 +10 to +38 +30 to +58

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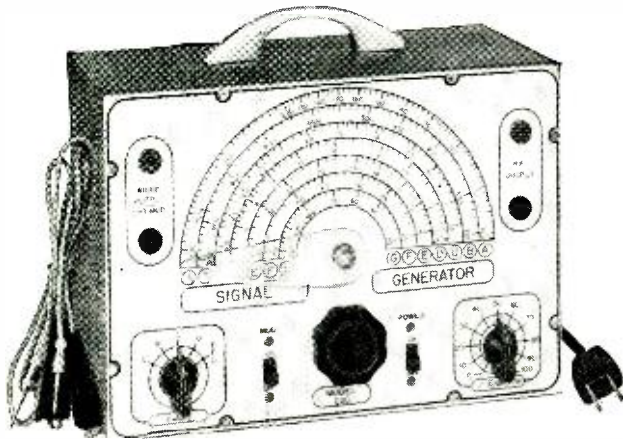
The Model 670 includes a special GOOD-BAD scale for checking the quality of electrolytic condensers at a test potential of 150 Volts.

The Model 670 comes housed in a rugged, crackle-finished steel cabinet complete with test leads and operating instructions. Size 5 1/2" x 7 1/2" x 3".

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The New Model 200

AM and FM SIGNAL GENERATOR



SPECIFICATIONS

- ★ **R.F. FREQUENCY RANGES:** 100 Kilocycles to 150 Megacycles.
- ★ **MODULATING FREQUENCY:** 400 Cycles. May be used for modulating the R.F. signal. Also available separately.
- ★ **ATTENUATION:** The constant impedance attenuator is isolated from the oscillating circuit by the buffer tube. Output impedance of this model is only 100 ohms. This low impedance reduces losses in the output cable.
- ★ **OSCILLATORY CIRCUIT:** Hartley oscillator with cathode follower buffer tube. Frequency stability is assured by modulating the buffer tube.
- ★ **ACCURACY:** Use of high-Q permeability tuned coils adjusted against 1/10th of 1% standards assures an accuracy of 1% on all ranges from 100 Kilocycles to 10 Megacycles and an accuracy of 2% on the higher frequencies.
- ★ **TUBES USED:** 12AU7—One section is used as oscillator and the second is modulated cathode follower. T-2 is used as modulator. 6C4 is used as rectifier.

The Model 200 operates on 110 Volts A.C. Comes complete with output cable and operating instructions.

\$21⁸⁵
NET

Superior's New Model TV-11

TUBE TESTER



Tests all tubes including 4, 5, 6, 7, Octal, Lock-in, Peanut, Bantam, Hearing-aid, Thyatron, Miniatures, Sub-miniatures, Novals, Sub-Minars, Proximity Fuse Types, etc. Tests for "shorts" and "leakages" up to 5 Megohms.

Uses the new self-cleaning Lever Action Switches for individual element testing. Because all elements are numbered according to pin-number in the RMA base numbering system, the user can instantly identify which element is under test.

The Model TV-11 does not use any combination type sockets. Instead individual sockets are used for each type of tube. Thus it is impossible to damage a tube by inserting it in the wrong socket.

Newly designed Line Voltage Control compensates for variation of any line voltage between 105 Volts and 130 Volts.

EXTRA SERVICE

The Model TV-11 may be used as an extremely sensitive Condenser Leakage Checker. A relaxation type oscillator incorporated in this model will detect leakage even when the frequency is one per minute.

The Model TV-11 operates on 105-130 Volt 60 Cycles A.C. Comes housed in a beautiful hand-rubbed oak cabinet complete with portable cover.

\$47⁵⁰
NET

*NOISE TEST

Phono Jack on front panel for plugging in either phones or external amplifier will detect microphonic tubes or noise due to faulty elements and loose external connections.

MONEY BACK GUARANTEE!!

GENERAL ELECTRONIC DISTRIBUTING CO.

DEPT. RC-6, 98 PARK PLACE, NEW YORK 7, N. Y.

GENTLEMEN: PLEASE RUSH THE MATERIAL LISTED BELOW:

Phone—REctor 2-1677

QUANTITY	MODEL	PRICE
	670 SUPER METER	
	200 SIGNAL GENERATOR	
	TV-11 TUBE TESTER	
	TOTAL	

Name _____

Address _____

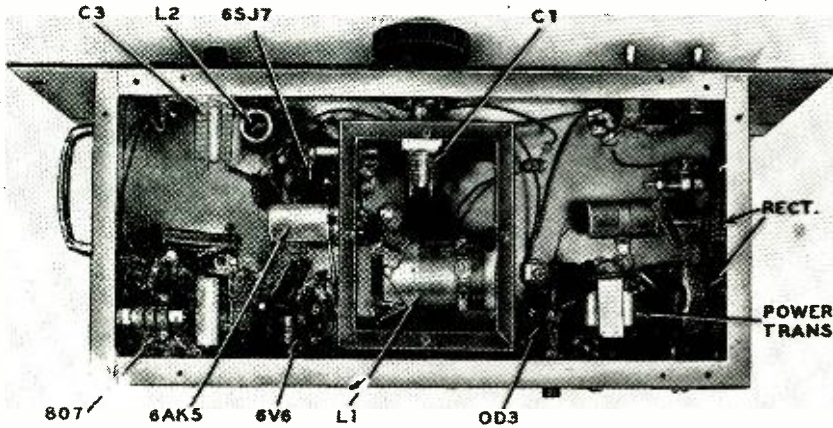
City _____ Zone _____ State _____

\$ _____

(Payment in Full Enclosed)

\$ _____

(Deposit Enclosed—Ship Balance C.O.D.)



A bottom view. The metal sub-chassis contains the Clapp oscillator circuit.

The 6SJ7 plate is tuned to the fundamental of the v.f.o. L2 is 30 turns of No. 22 wire wound on a 3/4-inch diameter form. C2 sets the band and C3 tunes it. One setting of C3 is enough to work any narrow band such as 3.5-3.6 mc (or harmonics thereof).

L3 is a Millen slug-tuned coil form (No. 74001). It is wound with 32 turns of No. 26 wire. The form plugs into an octal socket, and the slug should be adjusted for maximum output near 7 mc. This may be indicated by a wavemeter. Then screw down the shield over the coil form. Set the v.f.o. to 3.57 mc and note the grid current of the 807. Now the coil slug is tuned from the bottom (since the shield is in place over the

is equivalent to 50 watts input. It is more convenient to calibrate the meter in terms of POWER INPUT than merely plate ma. In any case R2 will depend upon the meter used as well as the plate supply voltage.

The power supply for the first three tubes is conventional. The transformer, a surplus device, has 150- and 85-volt windings. These are connected in series for a total of 235 volts, and the 85-volt winding is used to supply bias for the final. Two rectifiers are used in series because of the high voltage. Regulated voltage is applied to the 6AK5 and 6SJ7. All tubes run relatively cool, since they are operated well below maximum ratings.

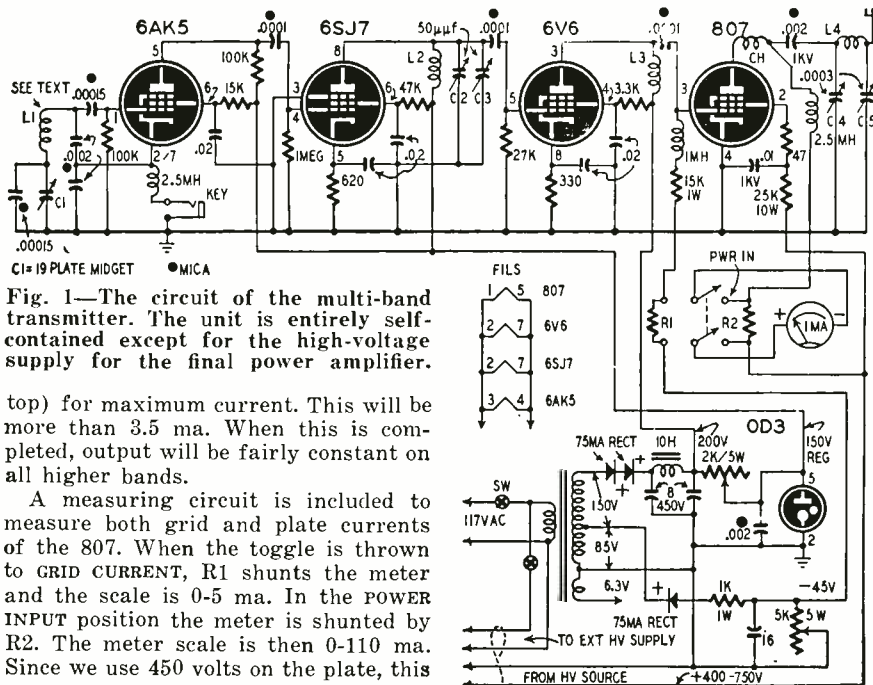


Fig. 1—The circuit of the multi-band transmitter. The unit is entirely self-contained except for the high-voltage supply for the final power amplifier.

top) for maximum current. This will be more than 3.5 ma. When this is completed, output will be fairly constant on all higher bands.

A measuring circuit is included to measure both grid and plate currents of the 807. When the toggle is thrown to GRID CURRENT, R1 shunts the meter and the scale is 0-5 ma. In the POWER INPUT position the meter is shunted by R2. The meter scale is then 0-110 ma. Since we use 450 volts on the plate, this

Tuning and adjustment

To put a signal on the air, plug in the desired coil L4. (See table.) Switch to GRID CURRENT. Tune the v.f.o. to the desired frequency. Adjust C3 for maximum meter reading. Now switch to POWER INPUT and turn on the high voltage to the final. With 450 volts the meter will show less than 15 watts input when the key is up. The reading will be almost 50 watts when the key is depressed. Tune C4 near maximum capacitance and resonate for a dip with C5. If more power is desired, reduce the C4 setting and retune with C5. With the antenna disconnected, the following dip values will be obtained:

3.5 mc	16 watts
7.0	5
14.0	17
21.0	19

These values show that ample output may be obtained on any of the bands but that maximum power can be radiated on the 7.0 mc band.

The pi antenna network will couple to any length antenna. We use a straight wire about 30 feet long and less than 20 feet above ground on all bands.

The oscillator should always be completely shielded before transmitting, especially on the 3.5 mc band. Oscillator blocking may result in poor signal quality or chirp. Also, C3 should never be left too far off resonance. No difficulty is being encountered here due to r.f. feedback. If this problem is met, chokes or 100-ohm resistors may be added in the power leads to the oscillator. We did, however, detect a v.h.f. parasitic in the final. A small choke of 20 turns of fine wire around a 1/2-watt resistor (25,000 ohms) cured this immediately. Keying the oscillator shows no ill effects on signal quality.

Winding Data for L4

Band (mc)	Turns	Dia. (inches)	Length (inches)	Wire size
3.5	30	1/2	2 1/4	20
7.0	16	1/2	1 1/4	20
14.0	7	1/4	1	20
21.0

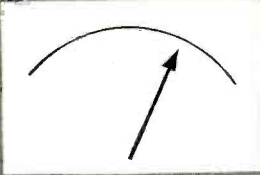
This transmitter is definitely superior to our early v.f.o. built in 1946 (see June-July, 1947, RADIO-CRAFT). It operates on more bands, is more efficient, and all tubes run much cooler.

Materials for Transmitter

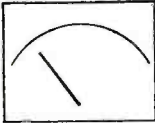
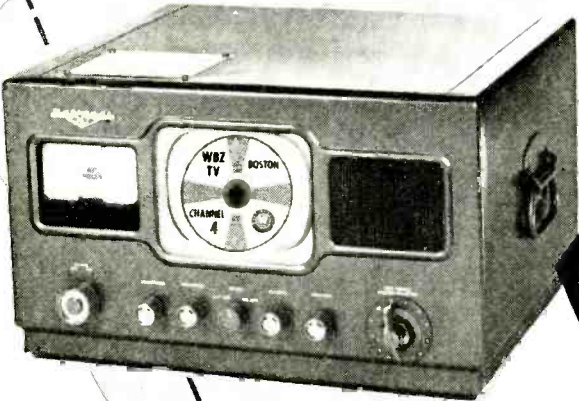
Resistors: 1—47; 1—330; 1—420; 1—3,300; 1—15,000; 1—27,000; 1—47,000; 2—100,000-ohm, 1—1 megohm, 1/2 watt; 1—1,000; 1—15,000-ohm, 1 watt; 1—25,000-ohm 10 watt; 1—2,000; 1—5,000-ohm, 5-watt, adjustable. Also 2 meter shunts (see text).
 Capacitors: 2—150; 3—100; 3—2,000-µmf, mica; 1—.002-µf, 1-kv, mica; 1—50-µmf variable (screw adj.); 1—50-µmf midget variable; 1—19-plate midget variable; 2—.003-µf variable transmitter; 5—.02-µf, 400-volt paper; 1—.01-µf, 1-kv, paper; 2—8-µf, 450-volt, electrolytic; 1—16-µf, 250-volt, electrolytic.
 Inductors: Power transformer, 235-volt with 85-volt tap and 6.3-volt, 3-amp winding (see text); 2—2.5-mh, 1—1-mh, 1—10-h, 60-ma, chokes; 1—parasitic choke (see text).
 Miscellaneous: 1—6AK5, 1—6SJ7, 1—6V6, 1—807, 1—OD3 tubes and sockets; 1—d.p.d.t., 2—s.p.s.t., switches; 3—75-ma selenium rectifiers; 1—0-1-milli-ammeter; key jack, knobs and dial, chassis, hookup wire, and assorted hardware.

—end—

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INTERFERENCE
and **GHOSTS** on
a meter...



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power companies
and TV servicemen
choose the
NATIONAL
VIDEOMETER



A. C. LINE ● SIG. STRENGTH

The National Videometer has proved an invaluable instrument to both power companies and TV servicemen in (1) locating the source of TV interference and (2) orienting TV antennas for ghost-free reception. For the National Videometer combines a sensitive TV receiver with an accurate meter for measuring field strength and A.C. line voltages. You see what you *measure . . . measure what you see!*

METER CHECK ON BOTH FIELD INTENSITY AND LINE VOLTAGE

Set the meter switch to A.C. LINE and read the line voltage at the receiver input terminal directly on the 0-150 volt scale. Set the switch to SIG. STR. and read the field intensity on the 0-10 scale. A table is provided to convert directly to microvolts. Reading is independent of contrast and brightness controls.

\$169.95
(Plus \$12.75 excise tax)



Cut QRM With Noise Limiters

Some noise limiter circuits that will make a marked improvement in your shortwave pickup

By ALVIN B. KAUFMAN, WØYOV

A GOOD noise limiter is important for shortwave reception, especially in the city. The lower frequency bands are troubled with static, and the higher frequency bands have QRM or man-made interference such as automobile ignition, street car noise, and random power-line corona.

A noise limiter simply removes any signal from the output whose level ex-

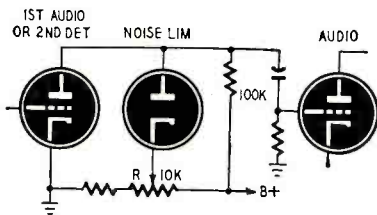


Fig. 1—A simple noise limiter hookup.

ceeds the average audio level of the transmitted signal. It must be adjusted so that it passes the audio signal level, but clips off any noise peaks or pulses extending above that level. It is apparent then that the limiter should be automatic in type, adjusting to the audio level.

Such limiters operate on the principle

that each individual noise pulse is of short duration, yet of high amplitude, and may produce noise peaks 10 to 20 times as great as the incoming radio signal. Because the duration of these noise peaks is short, the receiver can be cut off during the noise pulse and the human ear will not notice the loss of signal.

Limiters use one or more diodes either as clippers or gates in the a.f. system, the first being known as the *shunt* type and the latter as the *series* type. When the noise pulse exceeds a set value, the limiter diode acts either as a dead short or open circuit depending upon whether it clips or gates. These two most common type of limiters can be made automatic and much superior to any manually adjusted limiter.

A manually adjusted limiter is shown on Fig. 1 to indicate its simplicity. Potentiometer R is adjusted until the noise pulses cause the diode to conduct. When the diode conducts, it shunts the plate loading resistor with its low value of plate resistance until hardly any noise signal appears in this tube's plate circuit. The resistance of the potentiometer must not exceed about 10% of the plate resistor value or the noise diode could not effectively short out the plate resistor for its clipping action. Nor can

the potentiometer value be made too low or it will draw excessive bleeder current. The limiter control must be manually adjusted for each signal so as to not chop off any of the audio, which will vary in amplitude. Germanium crystals are not recommended for this circuit because chance high voltages may destroy them.

Two limiter circuits

A series-type noise limiter is shown in Fig. 2. Note that the addition of several resistors and the slight rewiring of one section of the 6H6 detector allows self-adjusting noise limiter action. The cathode of the limiter diode is maintained at a d.c. voltage developed by a.v.c. action, while its plate circuit voltage may fluctuate with any signal. The diode acts as a series gate, allowing audio to get to the grid of the a.f. tube only so long as the diode is conducting. Pulses which exceed the carrier level

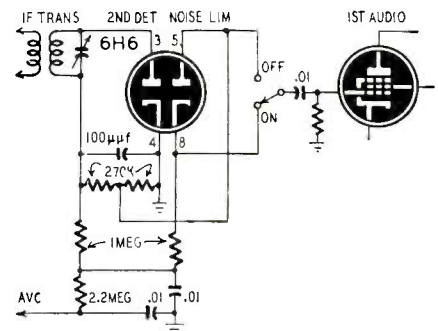
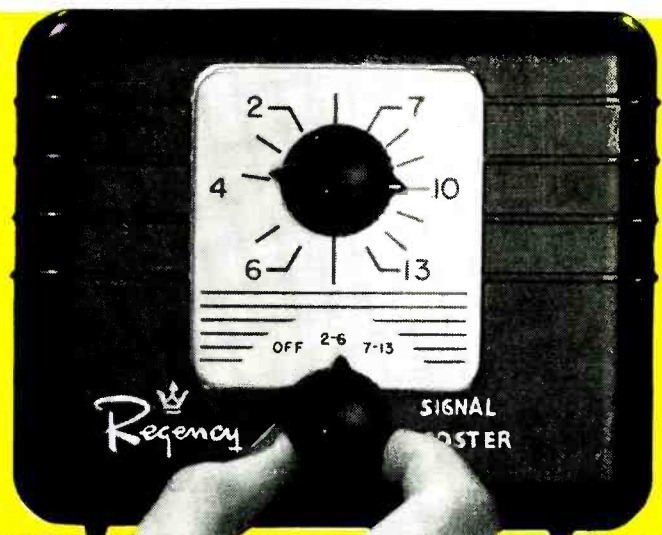


Fig. 2—This series noise limiter uses a.v.c. voltage for automatic control.

Largest Selling Booster

AT ANY PRICE !



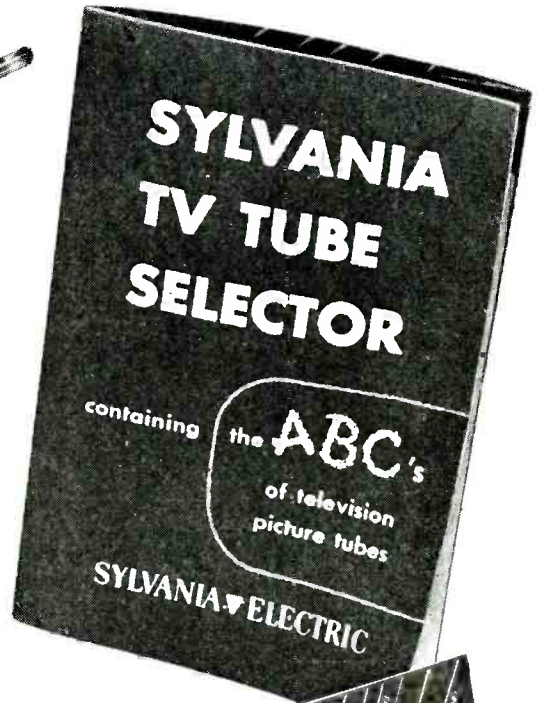
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19AP4?
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Type	TYPE	SHAPE	FACE PLATE	CONDUCTIVE COATING	TEMPERATURE RESISTANCE	NET PRICE	REMARKS
	14CP4	G	C	C			
	14DP4	G	C	C			
	14EP4	G	C	C			
	15CP4	G	C	C			
	15DP4	G	C	C			
	16AP4	A	C	C		58.50	
	16BP4	A	C	C			
	16CP4	A	C	C			
	16DP4	A	C	C			
	16EP4	A	C	C			
	16FP4	A	C	C			
	16GP4	A	C	C		51.00	
	16HP4	A	C	C			
	16IP4	A	C	C			
	16JP4	A	C	C			
	16KP4	A	C	C		51.00	
	16LP4	A	C	C			
	16MP4	A	C	C		51.00	
	16NP4	A	C	C		52.50	
	16OP4	A	C	C			
	16PP4	A	C	C			
	16SP4	A	C	C		51.00	
	16TP4	A	C	C			
	16UP4	A	C	C		52.50	
	16VP4	A	C	C			
	16WP4	A	C	C			
	16XP4	A	C	C			
	16YP4	A	C	C			
	16ZP4	A	C	C			

This Selector will save you lots of time and bother... eliminate errors. Get your FREE copy!

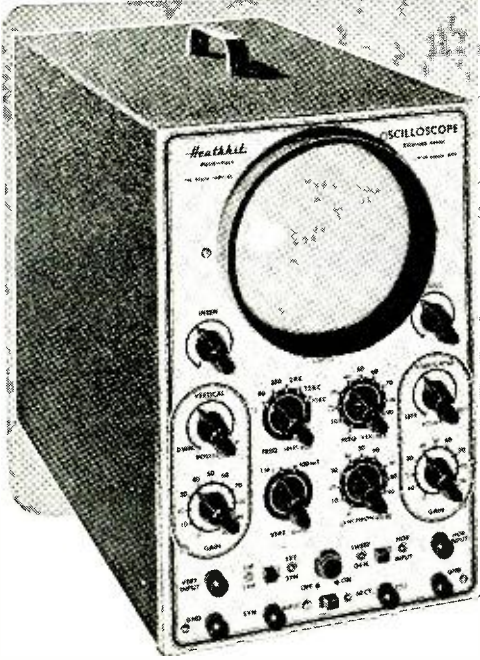


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Sylvania Electric Products Inc., Television Picture Tube Division, Emporium, Pa.

TELEVISION PICTURE TUBES; RADIO TUBES; ELECTRONIC PRODUCTS; ELECTRONIC TEST EQUIPMENT; FLUORESCENT TUBES, FIXTURES, SIGN TUBING, WIRING DEVICES; LIGHT BULBS; PHOTOLAMPS; TELEVISION SETS

JUNE, 1951



Heathkit MODEL 0-6... PUSH-PULL... 5" OSCILLOSCOPE KIT

The new Heathkit 5" Push-Pull Oscilloscope Kit is again the best buy. No other kit offers half the features — check them. Measure either AC or DC on this new scope — the first oscilloscope under \$100.00 with a DC amplifier.

The vertical amplifier has frequency compensated step attenuator input into a cathode follower stage. The gain control is of the non frequency discriminating type — accurate response at any setting. A push-pull pentode stage feeds the CR tube. New type positioning control has wide range for observing any portion of the trace. The horizontal amplifiers are direct coupled to the CR tube and may be used as either AC or DC amplifiers. Separate binding posts are provided for AC or DC.

The multivibrator type sweep generator has new frequency compensation for the wide range it covers: 15 cycles to over 100,000 cycles. The new model 0-6 scope uses 10 tubes in all, including 5" CR tube. Has improved amplifiers for better response useful to 2 megacycles. Tremendous sensitivity 64V RMS per inch horizontal — 99V RMS per inch vertical. Only Heathkit scopes have all the features.

New husky heavy duty power transformer has 30% more laminations. It runs cool and has the lowest possible magnetic field. A complete electrostatic shield covers primary and other necessary windings and has lead brought out for proper grounding.

The new filter condenser has separate sections for the vertical and horizontal screen grids and prevents interaction between them. An improved intensity circuit provides almost double previous brilliance and better intensity modulation.

A new synchronization circuit allows the trace to be synchronized with either the positive or negative pulse, an important feature in observing the complex pulses encountered in television servicing.

Model 0-6..... Shipping Wt. 24 lbs.

\$3950

The magnetic alloy shield supplied for the CR tube is of new design and uses a special metal developed by Allegheny Ludlum for such applications.

The kit is complete, all tubes, cabinet, transformer, controls, grid screen, tube shield, etc. The instruction manual has complete step-by-step assembly and pictorials of every section. Compare it with all others and you will buy a Heathkit.

NEW INEXPENSIVE Heathkit ELECTRONIC SWITCH KIT

The companion piece to a scope — Feed two different signals into the switch, connect its output to a scope, and you can observe both signals — each as an individual trace. Gain of each input is easily set (gain A and gain B controls), the switching frequency is simple to adjust (coarse and fine frequency controls) and the traces can be superimposed for comparison or separated for individual study (position control).



Model 5-2 Shipping Wt. 11 lbs.

\$1950

Use the switch to see distortion, phase shift, clipping due to improper bias, both the input and output traces of an amplifier, — as a square wave generator over limited range.

The kit is complete; all tubes, switches, cabinet, power transformer and all other parts, plus a clear detailed construction manual.

New MODEL V-4 A

Heathkit VTVM KIT

The new Heathkit Model V-4A VTVM Kit measures up to 30,000 Volts DC and 250 megacycles when used with accessory probes — think of it, all in one electronic instrument more useful than ever before. The AC Voltmeter is so flat and extended in its response (± 1 db from 20 cycles to 2 megacycles) that it eliminates the need for separate expensive AC VTVM's.

The new 200 microampere, $4\frac{1}{2}$ " streamline meter with quality Simpson movement (five times as sensitive as the commonly used 1 MA meter) has a shatter proof plastic meter face for maximum protection. Meter has all the desirable scales and indicates AC volts, DC volts, ohms, db (direct reading), and even has a special zero center marking for quick FM alignment.

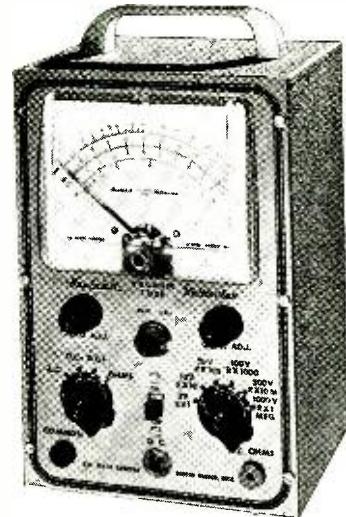
There are six complete ranges for each function. Four functions give total of 24 ranges. The 3 volt range allows 33 1/3% of the scale for reading 1 volt, as against only 20% of the scale on the 5 volt types.

New 1/2% ceramic precision resistors are the most accurate commercial type available — you find the same make and quality in the finest laboratory equipment selling for thousands of dollars. The entire voltage divider decade uses these 1/2% resistors.

Both AC and DC voltmeter measurements use a push-pull electronic voltmeter circuit, and the meter circuit makes the meter burn-out proof. Electronic ohmmeter circuit measures resistance over the amazing range of 1/10 ohm to one billion ohms, all with internal 3 volt battery. Ohmmeter batteries mount on the chassis in snap-in mounting for easy replacement.

Voltage ranges are full scale — 3 Volts, 10 Volts, 30 Volts, 100 Volts, 300 Volts, 1000 Volts. Complete decade coverage without gaps.

The DC probe is isolated for dynamic measurements. Negligible circuit loading. Gets the accurate reading without disturbing the operation of the equipment under test. Kit comes complete: cabinet, transformer, Simpson meter, test leads, complete assembly and instruction manual.



Model V-4A... Shipping Wt. 8 lbs.

Note New Low Price

\$2350



\$550

No. 336 High Voltage Probe Kit..... Shipping Wt. 2 lbs.

Heathkit 30,000V DC PROBE KIT

A new 30,000 V DC Probe Kit to handle high voltages with safety. For TV service work and all other high voltage applications. Sleek looking — Two color molded plastic — Red body and guard — jet black handle. Comes with connector, cable, and PL55 type plug. Plugs into Heathkit VTVM so that 300V scale is conveniently multiplied by 100. Can be used with any standard 11 megohm VTVM.

Heathkit RF PROBE KIT

This RF Probe Kit comes complete with probe housing, crystal diode detector, connector, lead and plug and all other parts plus clear assembly instructions. Extends range of Heathkit VTVM to 250 Mc. $\pm 10\%$. Works on any 11 megohm input VTVM. Specify No. 309 RF Probe Kit.



Shipping Wt. 1 lb.

\$550

ROCKE INTERNATIONAL CORP.
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CABLE: RELEA-H.F.

The HEATH COMPANY

... BENTON HARBOR 20, MICHIGAN

NEW Heathkit TV ALIGNMENT GENERATOR KIT

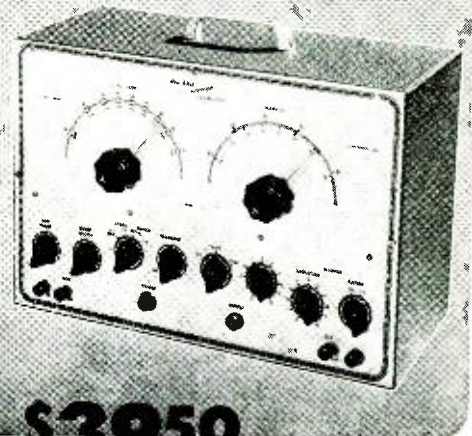
Here is an excellent TV Alignment Generator designed to do TV service work quickly, easily, and properly. The model TS-2 when used in conjunction with an oscilloscope provides a means of correctly aligning television receivers.

The instrument provides a frequency modulated signal covering, in two bands, the range of 10 to 90 Mc. and 150 to 230 Mc. — thus ALL ALLOCATED TV CHANNELS AS WELL AS IF FREQUENCIES ARE COVERED.

An absorption type frequency marker covers from 20 to 75 Mc. in two ranges — therefore, you have a simple, convenient means of frequency checking of IF's, independent of oscillator calibration.

Sweep width is controlled from the front panel and covers a sweep deviation of 0-12 Mc. — all the sweep you could possibly need or want.

And still other excellent features are: Horizontal sweep voltage available at the front panel (and controlled with a phasing control) — both step and continuously variable attenuation for setting the output signal to the desired level — a convenient instrument stand-by position — vernier drive of both oscillator and marker tuning condensers — and blanking for establishing a single trace with base reference level. Make your work easier, save time, and repair with confidence — order your Heathkit TV Alignment Generator now!



\$3950

Model TS-2
Shipping Wt. 20 lbs.

Heathkit SIGNAL GENERATOR KIT



Model SG-6
Shipping Wt. 7 lbs.

\$1950

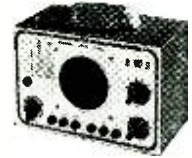
The new Heathkit Signal Generator Kit has dozens of improvements. Covers the extended range of 160 Kc to 50 megacycles on fundamentals and up to 150 megacycles on useful calibrated harmonics; makes this Heathkit ideal as a marker oscillator for TV. Output level can be conveniently set by means of both step attenuator and continuously variable output controls. Instrument has new miniature HF tubes to easily handle the high frequencies covered.

Uses 6C4 master oscillator and 6C4 sine wave audio oscillator. The kit is transformer operated and a husky selenium rectifier is used in the power supply. All coils are precision wound and checked for calibration making only one adjustment necessary for all bands.

New sine wave audio oscillator provides internal modulation and is also available for external audio testing. Switch provided allows the oscillator to be modulated by an external audio oscillator for fidelity testing of receivers. Comes complete, all tubes, cabinet, test leads, every part. The instruction manual has step-by-step instructions and pictorials. It's easy and fun to build a Heathkit Model SG-6 Signal Generator.

Heathkit SIGNAL TRACER and UNIVERSAL TEST SPEAKER KIT

The popular Heathkit Signal Tracer has now been combined with a universal test speaker at no increase in price. The same high quality tracer follows signal from antenna to speaker — locates intermittents — finds defective parts quicker — saves valuable service time — gives greater income per service hour. Works equally well on broadcast, FM, or TV receivers. The test speaker has an assortment of switching ranges to match either push-pull or single output impedances. Also tests microphones, pickups and PA systems. Comes complete: cabinet, 110V 60 cycle power transformer, tubes, test probe, all necessary parts, and detailed instructions for assembly and use.



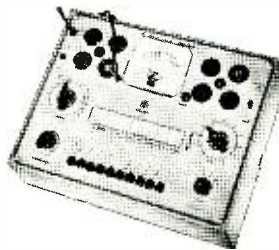
Model T-2
Shipping Wt. 7 lbs.

\$1950

Heathkit TUBE CHECKER KIT

Test your tubes the modern way — dynamically — the simplest, yet fastest and surest method — your Heathkit has a switch for each tube element and measures that element — no chance for open or shorted elements slipping by, all the advantages of the mutual conductance type without the slow cumbersome time consuming setups. Checks for opens, shorts, each element individually, filament and filament tap continuity, and emission.

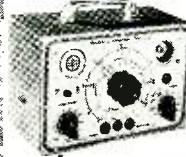
This Tube Checker has all the features — beautiful 3 color BAD-?-GOOD meter — complete selection of voltages — roller chart listing hundreds of tubes including the new 9 pin miniatures — finest quality Centralab lever switches — high grade birch, counter-type cabinet — continuously variable line adjust control — every feature you need to sell tubes properly. The most modern type tube checker with complete protection against obsolescence. Uses only the best of parts — rugged oversize 110V 60 cycle power transformer, finest of Mallory and Centralab switches and controls, complete set of sockets for all type tubes with blank spare for future types. Fast action, gear driven roller chart quickly locates the setting for any type tube. Simplified switching cuts necessary testing time to a minimum and saves valuable service time. Simple method allows instant setup of new tube types without waiting for factory data. No matter what the arrangement of tube elements is, the Heathkit flexible switching method easily handles it. Order your Heathkit Tube Checker Kit today and see for yourself that Heath again saves you two-thirds and yet retains all the quality. Complete with instructions, all parts, and cabinet.



Model TC-1
Shipping Wt. 12 lbs.

\$2950

Heathkit CONDENSER CHECKER KIT



\$1950

Checks all types of condensers — paper, mica, ceramic, electrolytic. All condenser scales are direct reading and require no charts or multipliers. Covers range of .00001 MFD to 1000 MFD. A Condenser Checker that anyone can read. A leakage test and polarizing voltage for 20 to 500 V provided. Measures power factor of electrolytics between 0% and 50% and reads resistance from 100 ohms to 5 megohms. The magic eye indicator makes testing easy.

The kit is 110V 60 cycle transformer operated and comes complete with rectifier tube, magic eye tube, cabinet, calibrated panel and all other parts. Has clear detailed instructions for assembly and use.

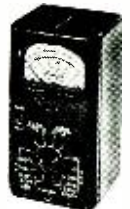
Model C-2 Shipping Wt. 6 lbs.

NEW Heathkit HANDITESTER KIT

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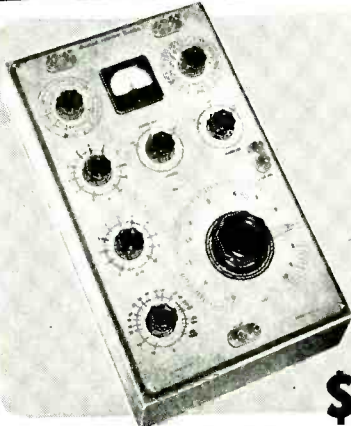
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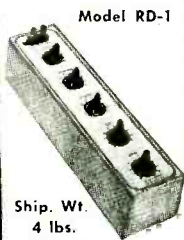
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(and a.v.c. bias voltage) by approximately 60% cause the diode to cut off.

This limiter action does not produce any apparent audio distortion with voice transmissions, but it does distort music noticeably. If the receiver is to be used strictly for voice communication the limiter may be wired in permanently. Where this audio distortion is not acceptable, an on-off switch may be installed, as indicated in the diagrams. This will allow normal reception, as in mobile service where the receiver is

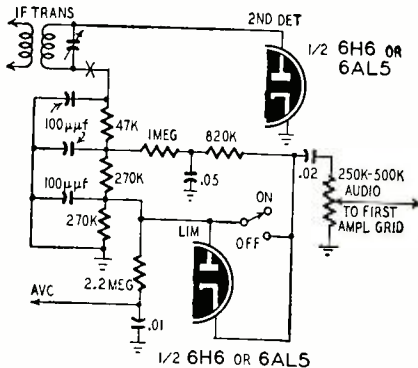


Fig. 3—The HQ-129X limiter circuit.

used both for shortwave and broadcast reception. Use short leads to connect the limiter switch because high stray capacitance will bypass the signal around the noise limiter diode and cause poor operation of the limiter.

The HQ-129X noise limiter is the favorite of many mobile amateurs. It does require a few more components, but it is excellent for removing high-level ignition noise. The circuit of this limiter appears in Fig. 3 while Fig. 4 indicates some common second detector circuits marked with an X to indicate where the limiter is inserted. The problem is simply to alter the connections between the second detector i.f. trans-

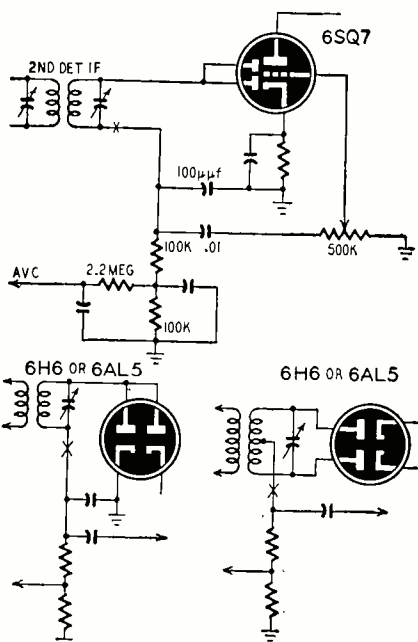


Fig. 4—Three common detector hookups. X marks the spot where the circuit is broken to connect the HQ-129X limiter.

former and the first audio grid. If this second detector uses a simple diode circuit then the chances are that only the ground-return lead of the i.f. transformer need be disconnected and re-wired. In any case, the a.v.c. return will have to be shifted to the new limiter resistance network. When the second detector i.f. transformer wiring is not otherwise changed, there is no need to realign this transformer. If the unused diode in the added tube is to be used for the second detector, then the second detector i.f. coil may require slight realignment, especially if long leads are used. The new tube should be mounted close to where the second detector is installed in the receiver.

The procedure for adding these noise limiters depends on the receiver. Most commercial receivers use diode detection with either a 6H6 or 6S7 tube or equivalent. Where a 6H6 is used for the second detector, the modifications for noise limiter action are few and simple. A 6S7 second detector which has cathode bias presents more of a problem. Usually another diode must be added to the circuit. If a dual diode tube, such as the 6AL5, is added, one-half may be used for the limiter and the other for the detector. The bias network in the cathode of the 6S7 may not be removed, as it supplies bias for the triode section of the tube.

The noise-limiter rectifier is across approximately 1 to 2 megohms of resistance, so its inverse resistance characteristic must be high. The 1N34 inverse resistance, compared with that of a vacuum tube, is too low for these circuits. We tried a 1N34 in the HQ-129X circuit. Limiting action did occur, but not enough to be useful.

Other noise problems

Limiters will not eliminate power-line hum, corona, or other sinusoidal QRM. Luckily, much interference is pulse-like and may be removed from the signal intelligence by a limiter. For non-mobile operation, antenna noise balancing circuits may be used to eliminate this noise. Such a circuit is shown by Fig. 5. The antenna coil has a balanced center-tapped ground, which effectively introduces two inputs into the receiver 180° out of phase. C1 is tuned for maximum radio signal, while C2, which connects to a noise pickup antenna, is tuned to lower the noise. When properly balanced, power-line buzz can be reduced nearly to zero without attenuating the desired signal excessively. In some cases an incorrect adjustment can result in balancing out the signal as well as the noise. The use of a good high antenna for signal reception will prevent this. This method of noise balancing requires readjustment of C2 for different signals and should be used only if a shielded coaxial lead and a high dipole antenna will not eliminate the noise condition.

Although a limiter does reduce noise, precautions to prevent radio noise from being generated are better. The lower

the noise into the receiver, the better the signal intelligence, even with the limiter in operation. In the home, a .01 to 0.1-µf, 600-volt capacitor will suppress noise from your electric razor and the wife's cake mixer. This capacitor can be of the paper variety and may be fused with a 1-ampere fuse for safety. Install the capacitor across the line in the outlet box at the noise-producing device; it is useless at the receiver.

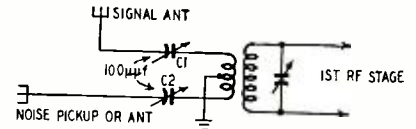


Fig. 5—A noise balancing antenna circuit such as this is useful for eliminating certain types of interference.

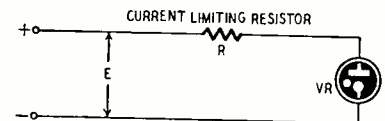
When a converter is added to an auto radio for short-wave reception, ignition noise will appear. Use of Auto-Lite resistor-type spark plugs will reduce the high levels of ignition noise in your receiver. These, plus your limiter, will eliminate ignition interference on short-wave bands. These spark plugs alone will not cure your own interference, but the improvement will be noticeable.

—end—

PUZZLING OSCILLATIONS IN VR TUBES

When a VR-type voltage regulator tube goes into oscillation, the technician usually looks for a capacitor (commonly about 0.1 µf) in the circuit to which regulated voltage is supplied. This capacitor, in parallel with the VR tube, and the limiting resistor R set up a relaxation oscillator circuit. Removing the capacitor, or sometimes lowering its value, cures the oscillation.

The gas tube voltage regulator can, and often does, oscillate without benefit of the capacitor. When the tube has not fired, it is passing no current through resistor R, and there is no voltage drop across this resistor. The tube therefore "sees" the full d.c. voltage (E) delivered by the power supply. If this voltage increases (or if resistance R is decreased), so that the tube just barely receives its full striking voltage, the tube will fire. Tube current (I) now

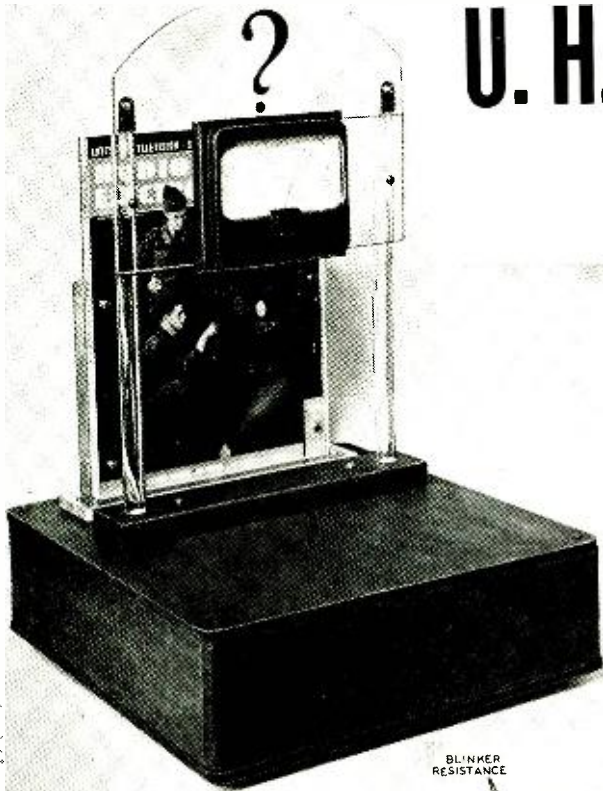


flows through R and produces a voltage drop across R equal to IR. The voltage across the tube itself quickly becomes E minus IR, which may be less than the extinguishing potential and the tube stops conducting. Once again, there is no drop across R, and the tube receives its full striking voltage and fires. The cycle then repeats itself.

This type of oscillation is most common when resistor R is varied or when the d.c. input voltage is varied. It always indicates that the resistance is incorrect for a given d.c. input voltage. —Rufus P. Turner, K6AI

U. H. F. Mystery Meter

By H. W. SECOR



The mystery meter as it was used on display appears in the photo at left. Below is a photo that shows the arrangement of parts under the wooden platform.

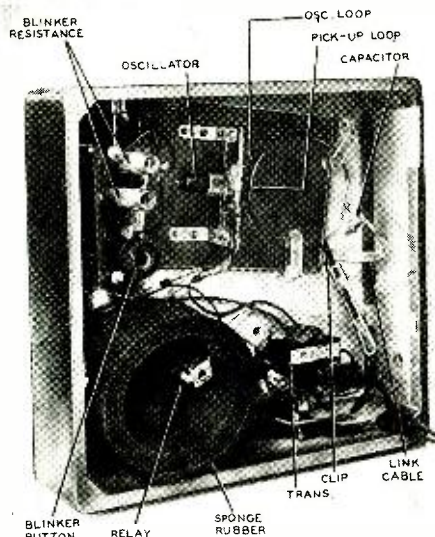
THIS u.h.f. mystery meter display is an attention-getter developed by the author at the suggestion of the editor of this magazine for exhibition at the I.R.E. Radio Show this spring. It has a meter mounted in a clear plexiglas panel in front of a copy of RADIO-ELECTRONICS. The meter needle swings back and forth, but there is no apparent energizing source of connection to the meter.

Besides being interesting as a "stopper" for customers passing a shop window, it could have applications as a remote-control device, and could be made into a small 420-mc transmitter by increasing the plate voltage and providing a suitable antenna.

The meter (a 0-to-50 d.c. microammeter) operates because of the electromagnetic field set up by a loop or coil hidden in the magazine. A germanium diode concealed in the meter rectifies the r.f. Two plexiglas plates rigidly mounted on top of the cabinet support the magazine. The 4-inch diameter single-turn loop of No. 10 wire is mounted in a space cut out of the centers of the pages of the magazine. The loop is fed high-frequency current from an oscillator hidden in the cabinet, through a piece of 300-ohm ribbon line (television lead-in) about 1 foot long. Any short length of this twin conductor may be used for different designs of the display. The ribbon passes through a slot cut in the top of the wood cabinet and the piece of plexiglas on which the magazine is supported. This is not visible to the observer.

The oscillator

The exciter for this display is a self-rectifying u.h.f. oscillator, using a 6J6



tube. As Fig. 1 shows, a transformer supplies the heater current to the tube, and the cathode (B-minus) lead is taken from the secondary center tap. The B-plus lead goes to the opposite side of the a.c. line.

The heater circuit and also the B-plus feed wire are supplied with r.f. chokes.

The heater-leads chokes have 8 turns of No. 26 enameled copper wire, wound closely on 1/4-inch diameter paraffined wood rods. Connect these r.f. chokes close to the tube socket terminals. The r.f. choke in the B-plus feed wire has 35 turns of No. 26 enameled wire, wound closely on a 1/4-inch diameter waxed wood rod. (Polystyrene is preferable.) The choke connects to a clip which fastens to the 1-turn plate coil. Since this is an a.c.-d.c. circuit, with one side attached to the electric-light line, it should be boxed carefully as shown in the photo, for safety. This is especially important in a window dis-

play—which may be handled by unskilled persons in close proximity to grounded objects such as steel frames of plate-glass windows. Such precaution should not be neglected in any case.

Keep all connections between the terminals on the base of the socket and the oscillator loop and tuning capacitor *very short*. Use No. 14 or 16 copper wire, with all joints soldered.

The oscillator loop is bent to a 4-inch diameter from a piece of No. 10 copper wire. The 3-30- μ f tuning capacitor (ceramic) is connected close to one end of the loop, as is the 4,700-ohm grid-leak resistor. If the tube refuses to oscillate (check with pilot-lamp test loop) try other resistor values. Also try adjusting the B-plus clip at different positions around the loop.

With the adjustable 3-30- μ f capacitor in the loop circuit adjusted about halfway in, the circuit oscillates at about 400 mc, as checked on Lecher wires.

The link circuit

Because the oscillator and its loop and capacitor would not fit inside the magazine, we used a link circuit as shown in Fig. 1. The two 4-inch diameter loops of No. 10 copper wire at each end of the link circuit are connected by a piece of 300-ohm ribbon about one foot long. A 3-30- μ f tuning capacitor tunes the *pickup loop* which is directly over the oscillator loop and separated from it by a piece of 1/2-inch plexiglas.

A neon lamp does not work well at these high frequencies, so a 4-inch diameter test loop was made with a 60-ma, 2-volt (pink bead) pilot lamp connected in series with the loop and a 3-30- μ f adjustable capacitor. Once the oscillator is set up and operating, the test lamp loop is brought close to it and the lamp will glow if the oscillator is working.

A lamp indicator could be used in place of a meter, where cost is an item, but the meter is much more interesting to watch. A 1N34 germanium crystal rectifier is connected across the meter terminals, together with a 50- μ f bypass capacitor, as Fig. 2 shows. A 3-30- μ f ceramic tuning capacitor is connected in the loop circuit. The meter pickup loop is 4 inches in diameter, made of No. 10 copper wire. Solder all connections in the meter unit. Use an insulated tuning rod to adjust the capacitors in these u.h.f. circuits. Adjust the meter loop capacitor for maximum deflection at a given distance.

The loop for the meter circuit, with its capacitor and rectifier, etc., are hidden in a wafer made of 3/8-inch thick bakelite, cut slightly larger than the

base of the meter. (See Fig. 2.) A piece of $\frac{1}{32}$ -inch black fiber is placed at the rear of the wafer to hide the "works." The meter screws hold the whole assembly against the plexiglass panel, a hole being cut in the panel to admit the

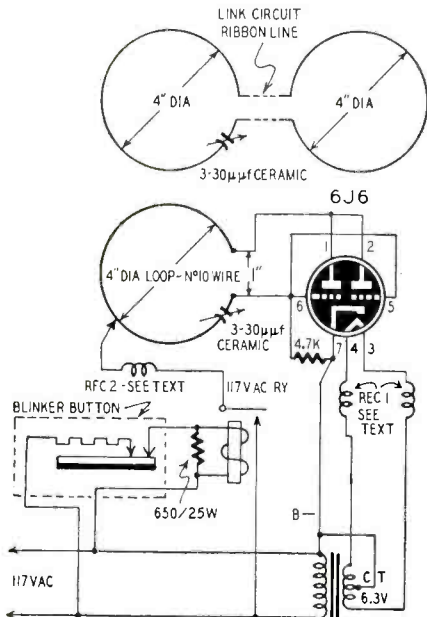


Fig. 1—Circuit of the mystery meter.

barrel of the meter. A false cover of thin bakelite fits over the barrel of the meter, to hide the wire connections to the posts of the meter.

A relay interrupter

The meter needle is made to swing back and forth at intervals of about one-half second, by means of a blinker-button. The button is in series with a 117-volt a.c. relay. (See Fig. 1.) The secondary terminals of the relay interrupt the B-plus feed to the oscillator loop, as Fig. 1 shows. The blinker-button was tried at first with a 15-watt, 117-volt lamp, but in the final model the light bulb was replaced by a 650-ohm, 25-watt resistor. We used three resistors in series for lack of a single unit of the right value. The relay is mounted in a sound-deadening rubber chamber.

Materials for Mystery Meter

Resistors: 1—4,700 ohms, $\frac{1}{2}$ watt; 1—650 ohms, 25 watts.

Capacitors: 3—3-30 μ f, variable, ceramic; 1—50 μ f, ceramic.

Miscellaneous: 1—6J6 tube and socket; 1—117-volt a. c. relay; 1—blinker-button; 1—6.3-volt filament transformer; 1—0-50- μ a meter; hookup wire, assorted hardware, plexiglass.

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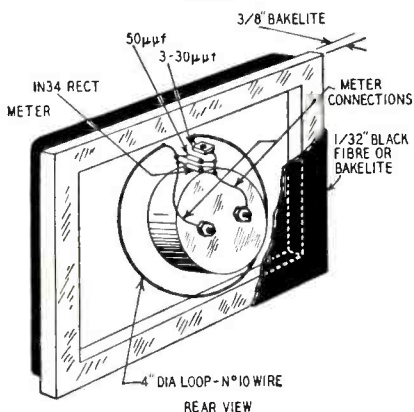


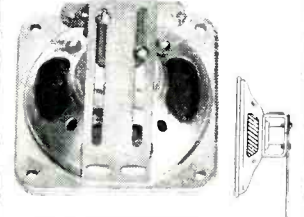
Fig. 2—The meter and pickup circuit.

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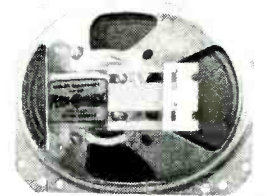
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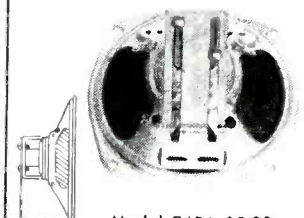
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ONE night last winter we answered our doorbell, and an insane man walked in. Before we could summon the police, the 200-pound stranger had torn a heavily bound book to pieces, kicked a glass-topped coffee table into a console radio, and, in general, scared all of us half out of our wits.

Inspired by the vivid memory of two husky officers wrestling the poor demented fellow all over our living room while trying to place handcuffs on him, we worked out a device to prevent a recurrence of this hair-raising experience. In brief, it is an electrically operated switch that turns on the porch light the instant the doorbell button is pushed and holds it on for a predetermined length of time. At the expiration of that time, the light is automatically turned off.

The gadget is shown in the photo and drawing. The portion of the diagram to the left of points A and B is an ordinary doorbell circuit, consisting of a step-down transformer, a pushbutton switch, and a doorbell, or chimes. The control circuit is inside the dashed lines; it consists of a 100-ma selenium rectifier, a 1,000- μ f, 25-volt electrolytic capacitor, and a sensitive, high-resistance, d.c. relay.

The rectifier develops a d.c. voltage which charges the capacitor during the time that the push-button is closed. This charge cannot flow backward through the rectifier after the push-button has been released, so the capacitor discharges through the winding of the relay. This discharge current closes the contacts of the relay. These contacts are connected in parallel with the usual porch light switch so the light is turned on. The contacts remain closed until the slowly diminishing discharge current reaches the drop-out point of the relay—a point considerably below the current level required to close the contacts. When the current falls to this drop-out value, the points open and the light is extinguished.

The actual time that the points remain closed depends upon the rectified voltage, value of the capacitor, the pull-in and drop-out current requirements of the relay, and the resistance of the relay winding. When the components shown in the diagram are connected across the 18-volt winding of a standard bell transformer, the points remain closed for almost exactly a minute.

The capacitor shown is a dual 500-

μ f, 25-volt unit with the two sections in parallel. The relay shown is a sensitive type manufactured by the RBM Company of Logansport, Indiana, and carries their part number 98341-9022. It has a 15,000-ohm coil and is designed to pull in at 0.98 ma and to drop out at 0.35 ma. However, any sensitive high-resistance relay can be used. For example, a relay with a 750-ohm winding would stay closed for only 15 seconds when connected directly across the capacitor; but when a 5,000-ohm resistor was connected in series with the relay coil across the capacitor the contacts were closed for 45 seconds.

Any relay that has a very low current requirement can be used with a series resistor to lengthen the time that the points will remain closed. If you were dealing with precisely known and stable voltage, capacitance, and resistance, this actual time could be calculated by employing the time-constant formula; but since these elements are subject to considerable variation in this case, it is quicker and simpler just to experiment with various resistance values until you have the particular time-delay you want.

To guard the sensitive relay against moisture and to make sure the device cannot become a fire hazard, it is constructed on the lid of a paint can 5 inches tall and 4 1/2 inches in diameter. The two leads that go to the bell transformer and the two that come from the relay contacts are all brought out

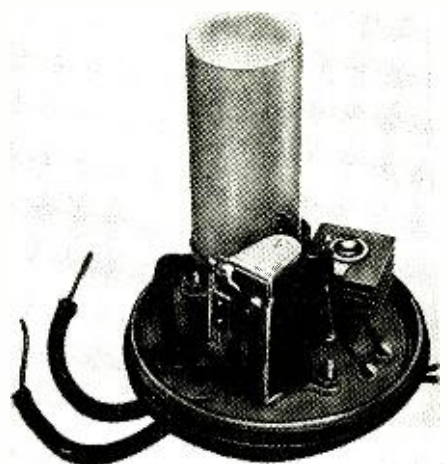
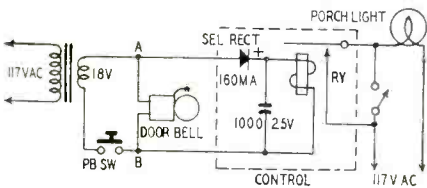


Photo of the porch light control. It is assembled on the lid of a paint can, then inserted into the can and sealed.

RADIO-ELECTRONICS for

through rubber grommets in the lid. Rubber-to-metal cement is used to seal these openings tightly against moisture. When the lid bearing the gadget is pressed tightly into its can for an airtight seal. Two brass angle pieces soldered to the sides of the can provide a means of mounting it.

This courtesy porch light may startle your guests the first time it flashes on as soon as they touch the push-button, but you will find they like the idea.



Circuit of the automatic porch light.

You will find yourself using the light, too. When you and the family come home late at night, you do not have to fumble around with your key on a dark porch. You simply punch the doorbell button and flood your porch with light.

Materials for Automatic Porch Light

1—selenium rectifier, 100 ma; 1—electrolytic capacitor, 1,000 uf, 25 volts; 1—relay, s.p.s.t. normally open contacts.

—end—

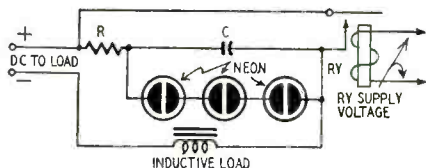
ARC SUPPRESSOR

Special precautions must be taken to suppress arcing at the contacts of small relays which handle direct current into a highly inductive load. The arcing, caused by a high induced voltage which

is developed when the circuit is broken, pits the contacts and shortens the useful life of the relay. The usual suppressor circuit consists of a resistor and capacitor in series across the contacts. The capacitor absorbs the induced e.m.f. and the resistor retards the flow of discharge current from the capacitor when the contacts close.

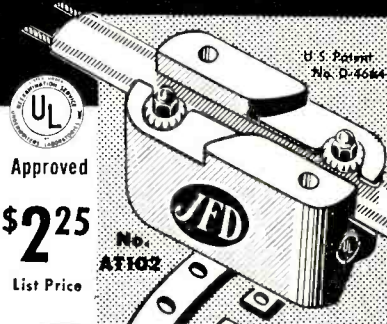
In many cases, the inductive load stores up more energy than can be absorbed by the capacitor, so there is sufficient energy left to arc across the contacts. Increasing the size of the capacitor may cause the contacts to weld together.

We find that these difficulties can be overcome by connecting several neon lamps in series across the capacitor as shown in the drawing. R and C are components of the standard arc suppressor. The sum of the ignition voltages of the individual lamps—without any external resistance—should be greater than the load voltage.



With this circuit, the lamps ignite and shunt the high self-induced voltage around the capacitor and contacts. The capacitor absorbs the surge energy until the voltage builds up enough to break down the lamps.—Harry Peach

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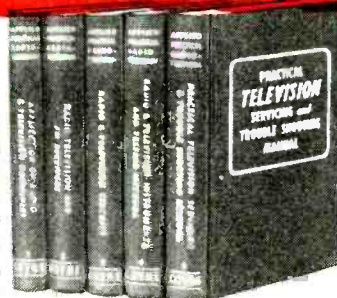
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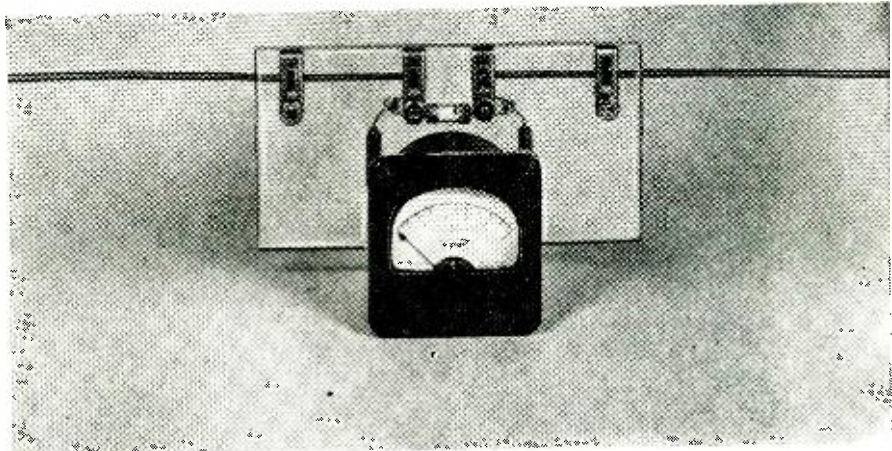
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(See advertising index for other advertisement of Progressive Electronics Co.)



The panel of the v.h.f. field-strength meter. The panel is clear polystyrene.

Field Strength Meter Covers V.H.F. Ranges

By HARDIN G. STRATMAN

TUNING in the final stage of many high-frequency transmitters is often so sluggish and broad that it is almost impossible to check antenna tuning and loading by reading a meter in the plate or grid circuit. The same thing occasionally occurs in low-frequency transmitters because of mismatch or overcoupling. Considerable time can be saved and much better results obtained if tuning and loading adjustments are based on readings taken with some sort of field-strength meter.

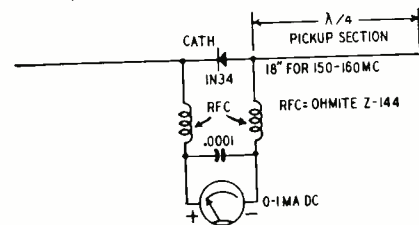
The construction of a simple field-strength meter for use in the 150-160-mc police and taxi bands is shown in the diagram and photo. All components are mounted on a 3 x 6 x 1/8-inch panel cut from polystyrene or similar insulating material. Two 1/4-inch holes—spaced to fit over the meter terminals—were drilled approximately 1/2 inch in from one of the long sides of the panel. Four holes large enough to pass 6-32 screws were drilled on a line parallel to and 1 inch in from the opposite side. The holes are 1/2 and 2 1/2 inches in from each end.

Mount four Fahnestock clips on the rear of the panel with soldering lugs under the screws holding the innermost clips. The meter mounts in front of the panel with its terminals projecting at the rear. A soldering lug should be placed over each terminal before screwing down the nuts which hold it to the panel.

Solder a 1N34 crystal diode between the innermost clips and an Ohmite Z-144 r.f. choke between these clips and the meter terminals. Bypass the meter with a 100-μf ceramic capacitor.

To complete the unit, cut two pieces of heavy bus bar approximately 1/4 wavelength long at the operating frequency. Pass these through the clips from the opposite ends. Make sure that they do not touch in the center.

When in use, the instrument may be held by a helper or suspended parallel to and approximately 3 feet from the transmitting antenna. Adjust the final tuning and antenna controls for maximum reading on the meter. With this setup, a 5-watt transmitter in the 150-160-mc band will deflect a 1-ma meter to full scale. After tuning up a 3-5 watt mobile transmitter by this method, reliable reception was obtained over a distance of 7 to 10 miles from the transmitter, even over hilly terrain.



A diagram of a field-strength meter suitable for police and taxi bands.

The meter can be used to make comparative measurements on the strengths of two or more transmitters, in the same band, and to plot directivity patterns of antennas. The antenna sections should be approximately 1/4 wavelength at the operating frequency. If the frequency is far removed from 155 mc, the Z-144 r.f. chokes should be replaced with chokes suitable for use at the operating frequency.

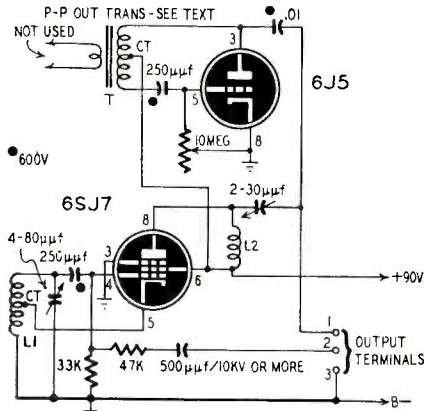
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RADIO-ELECTRONICS for

TV LINEARITY CHECKER

This low-cost TV linearity checker produces a grid of horizontal and vertical lines on a screen of a TV set. The service technician adjusts the set's linearity controls so the lines are evenly spaced across the face of the tube.

The 6J5 is a blocking oscillator operating at 540 c.p.s. to produce 9 horizontal lines on the screen. Its frequency is determined by the characteristics of transformer T and the setting of the 10-megohm variable grid resistor. Transformer T is a push-pull audio output transformer (Stancor A-3857) having a plate-to-plate impedance of 25,000 ohms. The secondary is not used.



The 12 vertical lines are generated by the 6SJ7—an electron-coupled oscillator operating at 189 kc. L1 and L2 are 10-mh r.f. chokes (National R-100). The former is tapped between the second and third pies.

To operate, connect terminal 1 to the signal lead of the picture tube and terminal 3 to the chassis of the TV set. Adjust the 80-µF trimmer and 10-megohm resistor for 12 vertical and 9 horizontal lines, respectively. If the set and generator do not stay in sync, connect terminal 2 to the high-voltage terminal on the picture tube. Use standard high-voltage cable for this connection. Adjust the 30-µF trimmer for uniform brightness of the bars. Replace the 6J5 with one having lower gas content if the horizontal bars are weak or do not appear.

The designers of this circuit, Precision Apparatus Co., state that the instrument can be constructed for approximately \$7.00. They suggest that the constructor try using this unit to modulate a high-frequency r.f. generator by using a vacuum-tube or crystal diode mixer. Some constructors may elaborate on this basic circuit by connecting cathode followers in series with the output leads of each oscillator. These will minimize pulling, by isolating the oscillators from each other and from the external load.

A linearity checker such as this is practically an essential to the service technician these days because test pattern broadcasts are becoming extremely rare. With this instrument an accurate linearity adjustment can be made at any time.

—end—



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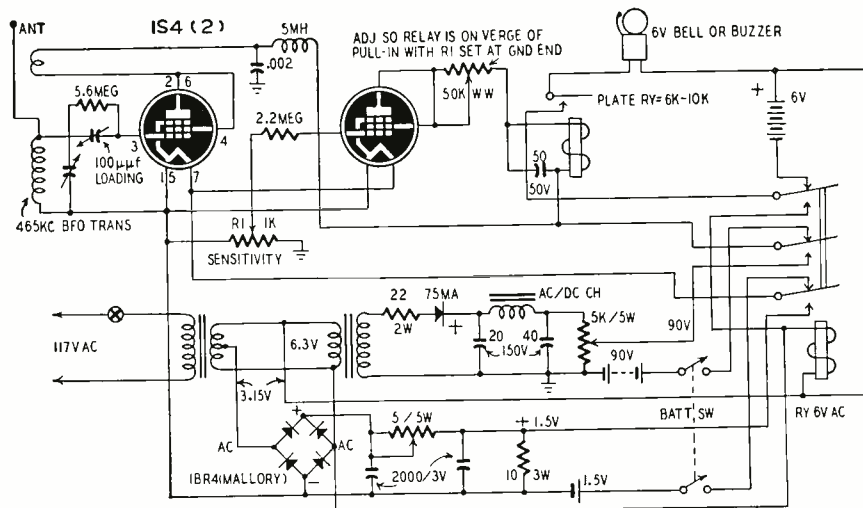
? Please print a diagram of an a.c.-operated capacitance relay which changes over immediately to battery operation in the event of failure of the a.c. power source.—E. J. R., San Diego, Cal.

A. The circuit is designed around a pair of 1S4 battery-type tubes which are used as the control oscillator and relay tube. The 5-ohm, 5-watt, and 5,000-ohm, 5-watt resistors are adjusted to give 1.5 volts and 90 volts respectively when the unit is operated from a 117-volt a.c. line. These voltages should be adjusted to the point where the alarm will not trigger when the unit

automatically changes over from a.c. to d.c. operation.

To adjust the unit, set the arm of R1 so that a further reduction in its resistance will trip the relay. Connect an antenna to the unit and vary the loading and sensitivity controls so the relay pulis in when anyone is within 4 or 5 feet of the antenna. Check for interference on nearby radio sets. If there is interference, vary the frequency of the oscillator circuit.

If the a.c. source should fail, the 6-volt a.c. relay releases and connects 1.5-, 90-, and 6-volt batteries to the filaments, plates, and alarm circuits.



POOR SELECTIVITY ON SMALL BROADCAST SETS

? Many of my customers who own 5- or 6-tube broadcast sets—usually a.c.-d.c. models—complain that stations at the high-frequency end of the dial interfere with each other so that from about 1300 kc up is just a jumble of whistles and distorted signals. What causes this and what can be done to remedy it?—D. B., Rison, Ark.

A. Much of this trouble can be traced directly to poor selectivity. The selectivity of a set is its ability to discriminate against unwanted signals close to the frequency of the desired one. The over-all selectivity is determined by the number of tuned stages and the selectivity of each.

In any capacitance-tuned circuit, the Q—the factor which determines selectivity—decreases as the resonant frequency increases. The average small receiver has only one tuned circuit between the antenna and converter grid and a pair of 455-kc i.f. transformers between the converter plate and the second detector. A single i.f. stage at this frequency does not have sufficient selectivity to reject adjacent-channel signals which ride through because of decreased front-end selectivity at the high-frequency end of the band. This effect is most noticeable at night when the range of broadcast stations is greater.

Co-channel interference is another source of trouble. As a rule, broadcast stations at the high end of the band operate with relatively low power on

channels shared by similar stations only a few hundred miles away. When the receiver is within the night-time range of two or more such stations, annoying heterodynes result. If the desired station is reasonably strong, the trouble can be minimized by using a shorter antenna or by rotating the set for minimum interference if it has a loop antenna.

If the interference is from adjacent-channel rather than co-channel stations, then a 10-kc "tweet" or whistle filter may be tried. It may be J. W. Miller Co.'s type EL-58 or EL-60. Installation instructions are supplied with each unit. Before installing one of these filters, be sure that the set is carefully aligned for maximum selectivity.

RADIO SERVICE



Suggested by
Morley Burteen, Chicago, Ill.

"Nope. Condenser is OKay!"

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TUBES

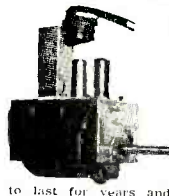
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IB7GT	1.60	6AF6G	1.33	6S7GT	1.00	12BN6	1.45	39 44	1.10
IC3GT	1.10	6AG5	1.33	6S7GT	1.00	12BT6	.75	40	1.10
IC6	.75	6AG7	1.33	6S7GT	1.00	12BU6	.75	41	1.00
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IG4GT	.75	6AT8 6V6GT	1.33	6S7GT	1.00	12SF5GT	1.00	50C5	1.00
IG5G	.75	6AU6	1.00	6S7GT	1.00	12S7GT	1.00	50C6G	1.45
IG6GT	.75	6AV5GT	1.33	6S7GT	1.00	12S7GT	.75	50L6GT	.90
IH4G	1.10	6AV6	.75	6S7GT	1.00	12S7GT	.75	50X6	1.00
IH5GT	.90	6AW6	1.33	6S7GT	1.00	12S7GT	.75	50YGT	.90
IH6GT	.90	6AX5GT	1.33	6S7GT	1.00	12S7GT	.75	50Y7GT	1.00
IJ5G	1.60	6B4G	1.60	6S7GT	1.00	12S7GT	1.00	50Z7G	.90
IJ6GT	1.60	6B5	1.60	6S7GT	1.00	12S7GT	1.00	52	1.95
IL4	.75	6B6G	1.10	6S7GT	1.00	12S7GT	1.00	53	1.33
IL6	1.33	6B7	1.60	6S7GT	1.00	12S7GT	1.00	55	1.10
IL4A	1.33	6B8G	1.60	6S7GT	1.00	12S7GT	1.00	57	.90
ILB4	1.33	6BA6	.90	6S7GT	1.00	12S7GT	1.00	58	1.00
ILC5	1.33	6BA7	1.20	6S7GT	1.00	12S7GT	1.00	59	1.78
ILC6	1.33	6BA8	1.20	6S7GT	1.00	12S7GT	1.00	70A7GT	1.95
ILD5	1.33	6BC5	1.00	6S7GT	1.00	12S7GT	1.00	70L7GT	1.60
ILE3	1.33	6BC7	1.33	6S7GT	1.00	12S7GT	1.00	71A	1.20
ILG5	1.33	6BD5	1.60	6S7GT	1.00	12S7GT	1.00	75	1.00
ILH4	1.33	6BD6	1.00	6S7GT	1.00	12S7GT	1.00	76	.45
ILN5	1.33	6BE5	.83	6S7GT	1.00	12S7GT	1.00	77	1.00
IN5GT	1.00	6BG6G	2.40	6S7GT	1.00	12S7GT	1.00	78	1.00
IP5GT	1.33	6BH6	1.00	6S7GT	1.00	12S7GT	1.00	79	1.33
IQ5GT	.75	6BJ6	1.00	6S7GT	1.00	12S7GT	1.00	80	.68
IQ6	1.10	6BK6	.75	6S7GT	1.00	12S7GT	1.00	81	2.40
IR4	.75	6BL7	1.45	6S7GT	1.00	12S7GT	1.00	82	1.33
IRS	1.00	6BN6	1.60	6S7GT	1.00	12S7GT	1.00	83	1.60
IS4	.75	6BQ6GT	1.60	6S7GT	1.00	12S7GT	1.00	84	.90
IS5	.90	6BT6	.75	6S7GT	1.00	12S7GT	1.00	85	1.10
IS6	1.10	6BU6	.83	6S7GT	1.00	12S7GT	1.00	89	.25
IT4	1.00	6BY5	1.33	6S7GT	1.00	12S7GT	1.00	90	1.60
IT5GT	.75	6C5	.83	6S7GT	1.00	12S7GT	1.00	91	1.60
IT6	.75	6C6GT	.83	6S7GT	1.00	12S7GT	1.00	99X	1.60
IU4	1.00	6C6	1.10	6S7GT	1.00	12S7GT	1.00	117L7GT	1.95
IU5	.90	6C8G	1.60	6S7GT	1.00	12S7GT	1.00	117N7GT	1.95
IU6	1.10	6C8B	1.00	6S7GT	1.00	12S7GT	1.00	117P7GT	1.95
IU7	.75	6C8B	3.00	6S7GT	1.00	12S7GT	1.00	117Z3	.75
IU5	1.10	6D1	1.10	6S7GT	1.00	12S7GT	1.00	117Z4GT	1.45
IW4	1.33	6D8	1.60	6S7GT	1.00	12S7GT	1.00	117Z6GT	1.20
IW5	1.10	6E5	1.10	6S7GT	1.00	12S7GT	1.00	FM-1000	1.60
IX2	1.33	6E6	1.33	6S7GT	1.00	12S7GT	1.00	XXD	1.20
IX2A	1.33	6E7	1.95	6S7GT	1.00	12S7GT	1.00	XXFM	1.33
2A3	.75	6F5GT	.83	6S7GT	1.00	12S7GT	1.00		
2A4G	.85	6F6	1.00	6S7GT	1.00	12S7GT	1.00		
2A5	.85	6F6GT	.83	6S7GT	1.00	12S7GT	1.00		
2A6	.45	6F7	1.60	6S7GT	1.00	12S7GT	1.00		
2A7	.45	6F8	1.60	6S7GT	1.00	12S7GT	1.00		
2B7	.40	6G6	1.33	6S7GT	1.00	12S7GT	1.00		
2E5	.45	6H4GT	1.33	6S7GT	1.00	12S7GT	1.00		
2X2	.75	6H8GT	1.33	6S7GT	1.00	12S7GT	1.00		
2X2A	2.18	6J5GT	.83	6S7GT	1.00	12S7GT	1.00		
222	1.95	6J6	1.45	6S7GT	1.00	12S7GT	1.00		
3A8GT	2.40	6J7GT	.85	6S7GT	1.00	12S7GT	1.00		
3B7	.45	6J8	1.60	6S7GT	1.00	12S7GT	1.00		
3C6/XXB	1.60	6K5GT	1.20	6S7GT	1.00	12S7GT	1.00		
3D6	1.60	6K6GT	.83	6S7GT	1.00	12S7GT	1.00		
3E6	.45	6K7GT	.83	6S7GT	1.00	12S7GT	1.00		
3FL4	1.33	6K8GT	.75	6S7GT	1.00	12S7GT	1.00		
3Q4	1.10	6L5	1.33	6S7GT	1.00	12S7GT	1.00		
3Q5GT	1.20	6L6G	1.78	6S7GT	1.00	12S7GT	1.00		
3S4	1.00	6L6GA	1.20	6S7GT	1.00	12S7GT	1.00		
3V4	1.00	6L7	1.20	6S7GT	1.00	12S7GT	1.00		
5A2A	.73	6N5	1.33	6S7GT	1.00	12S7GT	1.00		



A STANDARD TYPE TV TUNER

Exceptional value in a 12 channel turret tuner or front end. This high gain, low noise tuner is designed for receivers with 21.25 or 21.9 MC I.F. Drum type turret has replaceable channel coil and contact strips. Fine tuning is provided with stop at each extreme. Guaranteed to last for years and years. Will replace any tuner. **DOUBLE YOUR MONEY BACK** if replacement detent is ever required.

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PM Speaker Alnico #5 10 or more Each, List \$1.75, Our Price \$1.69, 5" 1.89, 1.79, 8" 3.49, 12" 6.89, 6.59

PM Speaker with 50L6 Output 4" 2.10, 2.00, 5" 3.40, 3.30, 8" Dynamic Speaker—50 OHM Field with 50L6 Output Trans. \$2.99

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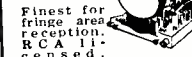
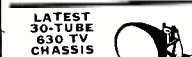
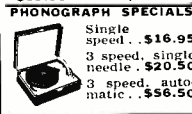
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COIL FRAME DATA FOR MODERN METAL LOCATOR

No information was given on the size of the cases and frames for coils used in the "Modern Metal Locator" described on page 16 of the 1948 RADIO-CRAFT REFERENCE ANNUAL. Please supply this information.—M. S. R., Waco, Texas

A. The cases for receiver and transmitter are 15 1/4 inches wide, 13 1/4

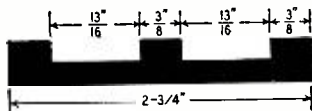


Fig. 1—Dimensions for the coil frame.

inches high, and 3 7/8 inches deep. The loop frames are built for a snug fit inside them. Frames are constructed from material approximately 3/8 inches thick and 2 1/16 inches wide. This material

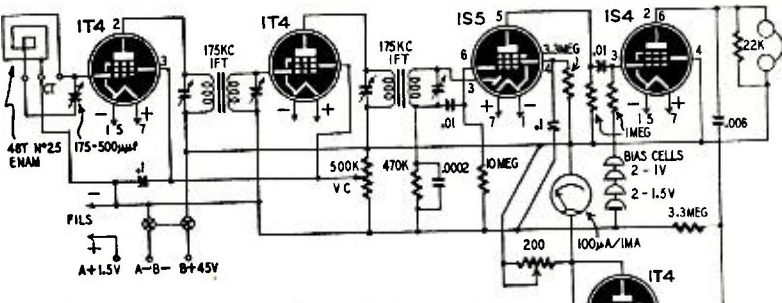


Fig. 2—Circuit of the receiver section of the device used for the location of metals by radio.

must be grooved with two 1/16-inch grooves as shown in Fig. 1.

HEADPHONE CONNECTION TO A.C.-D.C. RECEIVER

I want to connect a phone jack to a small a.c.-d.c. type receiver. The circuit must be wired so the speaker cuts out when the phones are plugged in. Please print a suitable circuit.—Wm. C., Miami Beach, Fla.

A. This circuit will do the job for you. The jack, a Mallory type A2A or equivalent, must be well insulated from the chassis and connected to it through a .01-µf, 600-volt blocking capacitor. Check the output transformer and speaker assembly and make sure that neither side of the voice-coil circuit is grounded before connecting the jack.

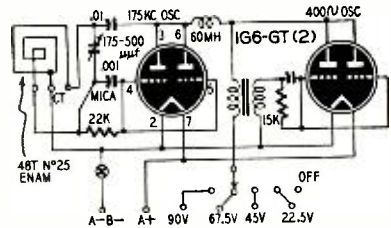


Fig. 3—The locator transmitter hookup.

The coils are laid in the grooves to prevent damage when the frames are inserted in the cases. Shelves for the transmitter and receiver are fastened inside the frames.

Diagrams of the receiver and transmitter are reprinted in Figs. 2 and 3, respectively, for the benefit of readers who have not access to the April, 1943

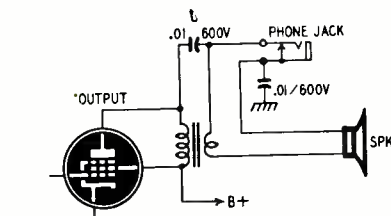
issue or the 1948 RADIO-CRAFT REFERENCE ANNUAL.

STROBOSCOPE USED FOR HIGH-SPEED ROTOR CHECK

I plan to construct the stroboscope described in the October, 1950, issue. I will increase the oscillator's frequency range to 240 c.p.s. and substitute a 1D21 Strobotron tube to provide direct calibration up to 14,000 revolutions per minute. How can I use this to check the speed of a small air turbine which I believe to be turning over at speeds between 50,000 and 75,000 r. p. m.—C. E., Flint, Mich.

A. Set the stroboscope control for maximum speed, then slowly reduce its speed until the rotor appears to stand still. Note the speed in r.p.m. on the dial. Make a chart showing speeds 2, 3, 4, and 5 times the indicated speed. Reduce the speed of the oscillator until the rotor again appears to stand still. Note the dial setting and prepare another chart.

If this circuit is used on an a.c. set, the frame of the jack can be fastened directly to the chassis, and the blocking capacitor from the jack to the chassis need not be used.



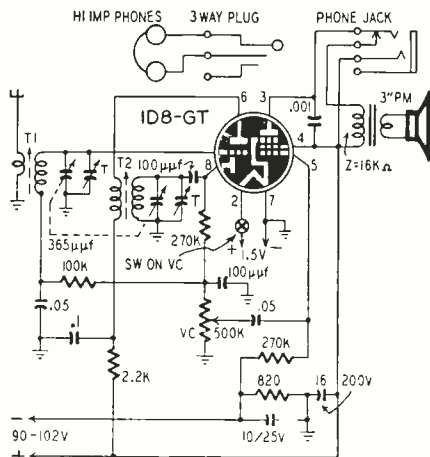
One number will appear on both charts. This number is the true speed of the rotor in r.p.m. For example: If the first reading is 12,300 r.p.m., 2, 3, and 4 times the indicated speed will be 24,600, 36,900, and 49,200 r.p.m. respectively. The second reading will be 9,840 r.p.m. Five times this speed is 49,200. This number appears on both charts so this is the true speed of the turbine.

In actual practice, there may be a slight difference between the two figures on the chart because in most cases, it is not possible to read the dial to one part in several thousand. Therefore, you can make the measurement several times and take an average of the readings. In this way you should be able to find the correct rotor speed.

ONE-TUBE RECEIVER

? Please publish a diagram of a portable broadcast receiver using a single 1D8-GT type tube. It should operate from batteries and drive a small loud-speaker on strong local stations. I would like to be able to use phones for the weaker stations.—A. E. S., Cambridge, Mass.

A. This circuit should perform as well as that of many 3-tube t.r.f. sets. High-gain antenna and r.f. coils having



powdered-iron cores should be used for T1 and T2 respectively, to insure maximum gain and selectivity. The triode section of the tube is the r.f. amplifier, the diode is the detector and a.v.c. rectifier and the pentode is the power output stage. The heater current used by the 1D8-GT is 0.1 amp., and the total B-supply drain in this circuit will be about 7 ma.

A 3-way phone jack and matching plug are used for the phones. The jack is wired so the speaker is silenced when the phones are plugged in.

18-TUBE RECEIVER QUERY

? I am planning to build the 18-tube communications receiver described in the June, 1950, issue, but before I begin, I would like to have data for winding coils for the 160-meter and broadcast bands. I will install these coils in place of those for the 6- and 10-meter bands.—G. H. R., Akron, Ohio

A. This set uses an oscillator which tunes from approximately 5 to 7 mc on all bands. To use this set on the broadcast band (550 to approximately 1350 kc—you cannot tune much higher without getting i.f. feed-through on 1425 kc) the oscillator will have to tune from 1975 to 2825 kc. The maximum capacitance across the oscillator coil would be approximately 1,200 µf. To cover the 160-meter band, the oscillator must tune from 3175 to 3425 kc, and the total oscillator capacitance will be about 500 µf.

We do not think it wise to attempt to pad the oscillator coil so it will cover these bands. This set is engineered for optimum performance over five narrow sectors in the radio-frequency spectrum. We suggest that you use converters to cover the 160-meter and broadcast bands.

JUNE, 1951

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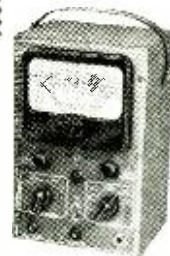
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3" square D'Arsonval meter. DC Voltmeter: 0-5-50-250-2500 Volts at 1000 Ohm per Volt. AC Voltmeter: 0-10-100-500-1000 Volts. Output Voltmeter: 0-10-100-500-1000 Volts. DC Milliammeter: 0-1-10-1000 MA. DC Ammeter: 0-1-10 Amperes. Ohmmeter: 0-10,000 Ohms—1 Megohm—10 Megohms Ext. Decibel Meter: -8 to +55 decibels. Complete with batteries.

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New Model Signal Tracer—Ultra Modern—Circuit design provides exceptionally high amplification so that actual gain measurements may be made. Accurate meter gives calibrated indications. Provides the speediest type of trouble shooting tool for tracing any type of disturbance or circuit defect from the antenna to the speaker. Indicates noise pickup at the aerial—checks AVC—APC, link and filter circuits. Tube Complement 6AU6—6AV6—6AQ5 and 6X4. Crystal Rectifier IN34. Speaker employs Alnico 5 magnet. Beautiful hammer-tone grey steel panel and case with new slenderized probe. Kit supplied complete, 105-130 volts, 50-60 cycles. Size 6 5/8" x 8 1/4" x 11". Weight 9 1/2 lbs.

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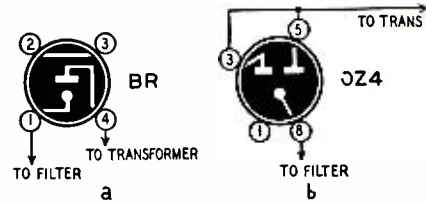
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REPLACING A BR RECTIFIER

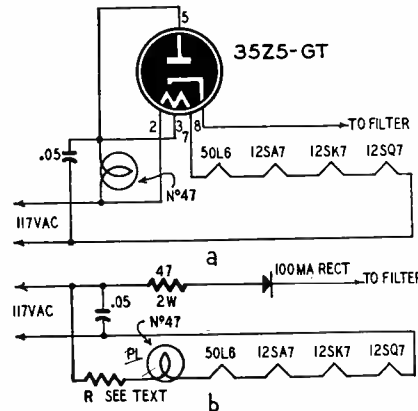
? I have a prewar Motorola auto radio which has a BR tube in its power supply. The tube is bad and I cannot find a replacement. Is there a substitute?—N. J., Dallas, Texas



A. Replace the socket with an octal unit and rewire it for an 0Z4. A base diagram of the BR is shown at a and wiring connections for the 0Z4 are at b.

SUBSTITUTE FOR 35Z5-GT

? Can I use a selenium rectifier to replace a 35Z5-GT in a 5-tube a.c.-d.c. set? If so, kindly prepare a diagram showing the changes. I am enclosing a drawing of the rectifier and heater string in the set.—H. L., Harvey, La.

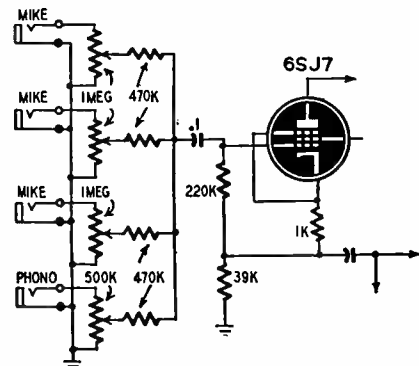


A. The original circuit is shown at a and the revision at b. Resistor R may be a Globar or Keystone type having a resistance of 1,400 ohms when cold and 200 ohms when hot.

MICROPHONE INPUT CIRCUIT

? I am planning to construct the high-gain amplifier described on page 45 of the September, 1950, issue. Please draw a diagram of the input circuit showing how I can use high-impedance microphones.—E. McD., Roselle, N. J.

A. The diagram shows how the input transformer is eliminated and the val-



ues of the gain controls and decoupling resistors changed to adapt the amplifier to use high-impedance microphones.

—end—

MEDIUM-VOLTAGE RECTIFIERS

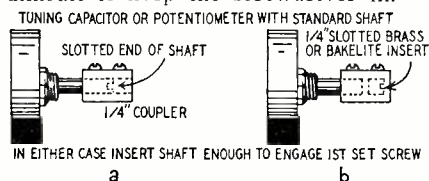
Amateurs and experimenters often use 83's, 83-V's, and 5Z3's in power supplies delivering up to 225 ma at 600 volts. These tubes do not last long under such operating conditions and are likely to arc or short between plate and filament. The resulting short circuit will blow fuses, or cause the primary of the transformer to burn out. A pair of 866's, 866-Jr.'s (2B26's), or 816's may be used if there is room for an additional tube, and if the filament winding is heavy enough to supply the required power.

I use a surplus 1641 RK-60 in all my supplies where the rectifier plate voltage is not more than 750 per plate. The maximum ratings for the 1641/RK60 are: 750 volts r.m.s. per plate, peak inverse voltage 2500, and output current 250 ma d.c. The internal voltage drop varies from 35 volts at 100 ma to 61 volts at 250 ma. The filament voltage is 5 volts and current is 3 amperes.

The 1641/RK-60 fits in a medium, 4-prong base with filament connections to pins 1 and 4. Plate connections are made to 0.36-inch caps on top of the tube. The envelope is 2 1/4 inches at the widest point and 5 1/8 inches from base to tip.—*Gerald Samkofsky*

SETTING SLOTTED CONTROLS

Transmitters, amplifiers, TV receivers, and numerous other electronic devices often have potentiometers or variable capacitors with slotted shafts for screwdriver adjustments. These controls are frequently under the chassis or behind a panel where the slots are difficult to find and even more difficult to keep the screwdriver in.



Adjusting slotted controls is simpler when a 1/4-inch metal or insulated coupler is placed over the end of the shaft as at *a* in the drawing. The drawing at *b* shows how a standard shaft can be converted for screwdriver adjustments. The shaft is fitted with a coupler and a short piece of 1/4-inch shaft which has been slotted for a screwdriver. If the control shaft is hot and must be insulated for safety, use an insulated coupler and a fiber insert.—*O. C. Vidden.*

SAFETY WITH A.C.-D.C. SETS

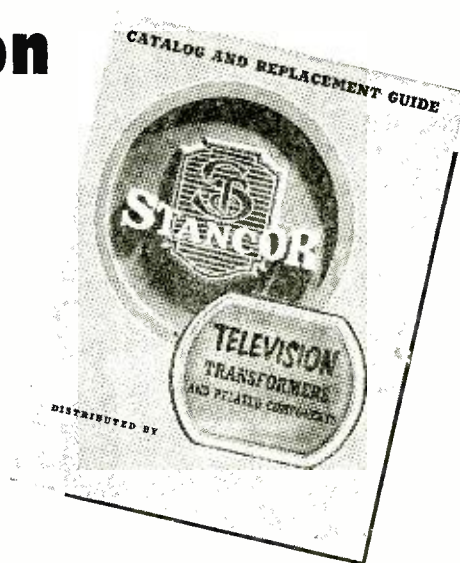
I have a sure-fire method of making certain that I do not get a shock while servicing a.c.-d.c. equipment. I covered one end of my workbench with sheet metal and connected it to ground through a large neon lamp. All transformerless equipment is serviced on this section of the bench. The neon lamp lights immediately when the line cord is inserted so the chassis is hot. Do not touch the chassis until you have reversed the plug. It is a good idea to mount the indicator lamp close to the power outlet where you will be sure to see it when you plug in the set.—*N. H. Kent*

JUNE, 1951

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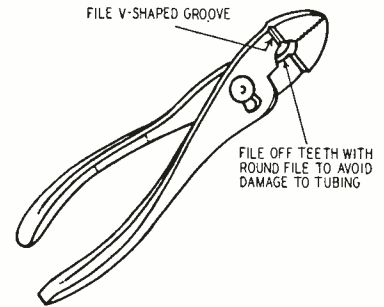
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3336-38-40 Frankford Ave., Phila. 34, Pa.

PLATING SOLDERING IRONS

Several months ago, a reader recommended using a solution of silver cyanide (a deadly poison) for plating soldering iron tips to prevent corrosion. A much simpler method is to plate the tip of the iron with Cool-Amp, a silver plating powder which can be applied to any clean copper surface with a damp cloth. This powder is also useful in improving the contact between heavy copper conductors which are clamped or bolted together.—*R. P. Balin*

DRILLING THIN-WALL TUBING

It is difficult to start a drill into soft thin-wall tubing without using a center punch which is very likely to deform the tubing. I have solved this problem by modifying a cheap pair of gas pliers to serve as a guide for the drill. The serrations are filed or ground off the inside of the jaws and a V-groove is filed down one side as shown



To use the tool, grip the tubing lightly with the groove centered over the spot where the hole is to be drilled. The groove is a guide for starting the drill. Remove the tool as soon as the hole is started.—*O. C. Vidden*

SIMPLE AUDIO PICKUP

Radio programs may be piped from a receiver to any recorder, amplifier, or public address system through inductive coupling between the output transformer of the set and a magnetic contact microphone connected to the amplifier. Tests have shown the strongest field to be at the top of the transformer. The mike may be suspended within 3 inches of the top of the transformer or mounted directly atop the transformer if it is cushioned with a thin layer of rubber or cork.—*Orren Reynolds*

OLD RECEIVERS MOTORBOAT

A number of old receivers have push-pull 45's and a 27 in the a.f. amplifier. Because most of these sets do not have a.v.c., tuning across a strong station will cause the set to blast and overload the 45's. Consequently these tubes soon go gassy and motorboat at the slightest provocation. Raising the bias to 60 volts helps in some cases. In others, I connect a .001- μ f capacitor from the grid of the 27 to the grid of one of the 45's. This connection forms a negative-feedback loop.

It may be necessary to connect the feedback capacitor to grid of first one 45 and then the other to determine which gives the best results.—*George F. Cutress*

—end—

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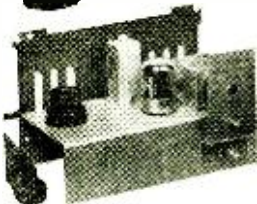


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MULTIPLE-BAND PANORAMIC RECEIVER

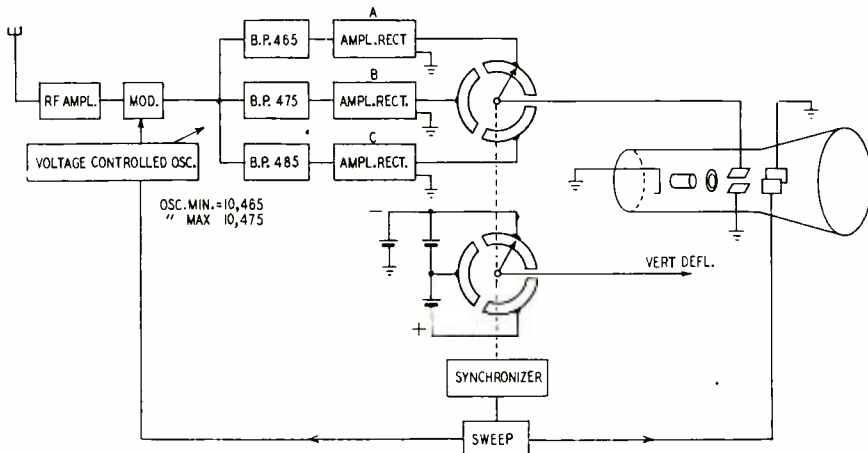
Patent No. 2,530,693

Estil I. Green, Millburn, N. J.

(Assigned to Bell Telephone Laboratories, Inc.)

This panoramic receiver can cover an unusually wide frequency range. All signals intercepted by it are displayed on an oscilloscope. The horizontal sweep of the scope is synchronized with the sweep of the local oscillator frequency. The demodulated receiver output feeds the vertical plates of the scope.

This i.f. can pass through channel A. If the r.f. is in the range 9990-10000 kc the beat will be 475 kc, which is the frequency of channel B. Frequencies between 9980-9990 kc create a beat of 485 kc and pass through channel C. If there were 10 channels, the receiver could cover a range of 100 kc although the oscillator is swept through



As the oscillator sweeps through its band it may heterodyne r.f. signals. Each beat appears as a vertical line on the screen. The height of each line indicates signal intensity. The position of each line (along the time-baseline) shows the frequency of the signal. The baseline may be calibrated in mc if desired.

No bandswitching is used in the local oscillator or r.f. circuits. The oscillator is swept over a range of 10 kc. The r.f. stages are untuned, wide-band amplifiers. Several sharply tuned i.f. channels are used, one at a time being connected to the scope through a rotating switch.

As the oscillator sweeps through its band (see figure) it creates a 465-kc beat whenever it heterodynes an r.f. signal between 10000-10010 kc.

only 10 kc.

The output of each channel is connected in turn to the scope. The lower pole of the ganged switch controls a d.c. supply. This may be fed to the vertical plates to control the height of the oscilloscope baseline. For example, with the switch as shown, channel A is in the circuit. At this time the d.c. supply is negative so the baseline is below center. When channel B is connected, the d.c. is zero and the horizontal baseline runs through the center of the screen. For channel C, the d.c. is positive, so the baseline is above center. The switch rotates rapidly so 3 baselines appear simultaneously, each displaying signals within the corresponding band. As many base lines are used as there are channels in the system.

SAWTOOTH GENERATOR FOR ELECTROSTATIC TUBES

Patent No. 2,509,761

Robert M. Crooker, Chicago, Ill.

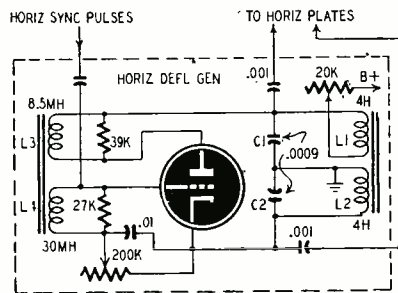
(Assigned to Motorola, Inc.)

This is an efficient circuit for horizontal deflection of an oscilloscope or small kinescope using electrostatic deflectors. It provides a sawtooth with an amplitude of about 450 volts from a B-supply of only 235 volts. The linear sweep is built up by charging a pair of capacitors in series. A blocking oscillator discharges them quickly to end the wave.

When the circuit is first turned on, C1 charges uniformly from the B-supply through L1. Because L1 is tightly coupled to L2, an equal but opposite current flows through L2 to charge C2. The upper plate of C1 becomes positive, the lower plate of C2 negative. This arrangement doubles the available output for the deflector plates.

The triode plate supply is equal to the total potential across C1, C2. As the charge increases the triode begins to conduct. Current through L3 induces a voltage across L4, which is phased to make the grid positive. Therefore conduction increases rapidly and the tube impedance is greatly reduced. Now C1, C2, L3 form an oscillator circuit through the tube. The capacitors discharge, then recharge in the opposite direction so that the upper plate of C1 becomes negative and the lower plate of C2 positive. By this time grid current is sufficient to block the tube again and the next charging cycle begins.

The sweep voltage is large for two reasons. C2 doubles the sawtooth that can be obtained by charging one capacitor (C1). Also, after the first cycle, C1 can charge uniformly over a wide



range. As described above, C1 is negative when it begins to take current from the B supply. Therefore the charging range is the same as if C1 were discharged and the B supply doubled.

As in any charging circuit, to preserve linearity, C1 can be charged to only a fraction of the power-supply voltage.

CONTROL OF HALL EFFECT IN GERMANIUM CRYSTALS

Patent No. 2,536,806

Albert Hansen, Jr., Nahant, Mass.

(Assigned to General Electric Co.)

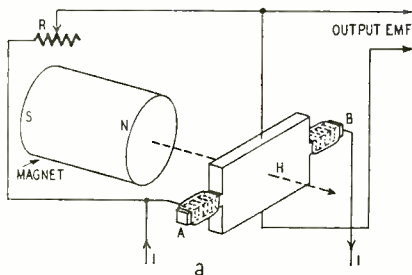
Certain materials like bismuth and germanium exhibit the "Hall effect." This effect is illustrated at a in the figure. A small plate of germanium is shown at H. A magnetic field passes through H at right angles to a current I. Due to the Hall

effect, an e.m.f. is generated through H at right angles both to the field and to the current. In this case the output e.m.f. would be in a vertical direction through H.

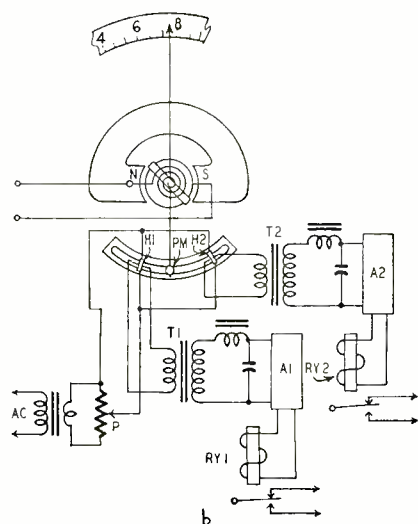
Points A and B must be at exactly opposite

ends of H. Otherwise a component of voltage drop (due to I) is present across the output terminals. R is added to compensate for this possible error.

A control circuit based on the Hall effect is shown at b. The pointer of the d.c. meter is counterbalanced with a small magnet which



rides along the curved slot. H1 and H2 are Hall plates fed with a.c. from potentiometer P. When the pointer is near 10 on the dial, P.M. passes near H1. Due to Hall effect, an a.c. is fed to transformer T1 and amplifier A1. Relay RY1 is operated to control the desired function. P.M. excites H2 when the pointer drops to about 4. Then



a.c. passes through T2 and feeds A2. This operates RY2 and some other function is controlled.

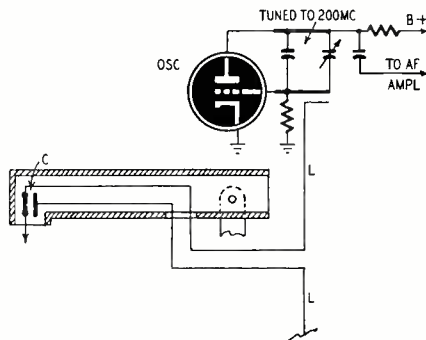
As an example, the meter may indicate the output of a thermocouple. When the low point is reached, RY2 can turn on the heat. At the other end of the scale too much heat is registered and RY1 may be used to disconnect the heater.

ABSORPTION-TYPE PICKUP

Patent No. 2,530,087

Chester M. Sinnett, Westmont, N. J.
(Assigned to Radio Corp. of America)

This variable capacitance pickup feeds a conventional a.f. amplifier. The stylus has negligible mass and reproduces a wide frequency range.



A metallic electrode is fixed adjacent to the stylus. As the stylus vibrates it changes capacitance C between itself and the electrode. The pickup is connected to a half-wave line L coupled to an oscillator. As C varies, it controls the power which L absorbs from the oscillator.

The tube plate current is modulated at an audio rate by the absorption of the line.

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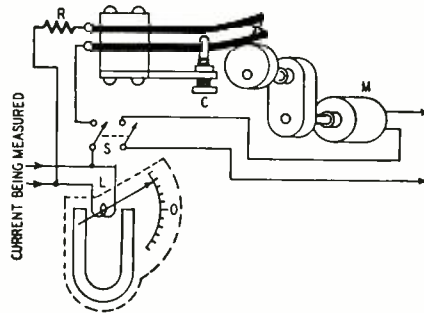
City and State

PERIODIC METER DAMPING

Patent No. 2,526,006

Ralph V. Cress, Syracuse, Ind.
(Assigned to Penn Electric Switch Co., Goshen, Ind.)

This invention provides meter damping without reducing sensitivity. Motor M operates a cam



which opens and closes a circuit shunting meter coil L. While the circuit is closed, R damps the meter movement by absorbing power from it. During open-circuit intervals, damping is removed and the needle is deflected normally. Knob C controls the ratio of time during which damping exists to the time when it is absent.

An optimum value of R may be chosen by experiment for the particular galvanometer to be damped. Then C is adjusted until the needle deflects in minimum time without overshooting or oscillation.

After the needle has come to rest, S may be opened. This disconnects both M and R, to assure accuracy of the final reading.

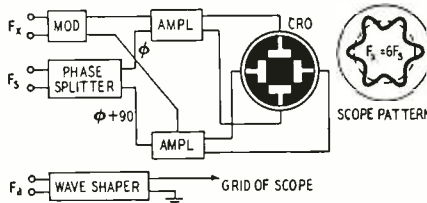
FREQUENCY MEASUREMENT

Patent No. 2,537,104

Albert H. Taylor,
Prince George's County, Md.
(May be used by the U. S. Government without royalty payment)

This is an improvement over the usual method of Lissajou figure measurement. A standard frequency F_s (preferably fixed for high accuracy) is compared with an unknown F_x by means of an oscilloscope. When F_x/F_s is a small integer or fraction, the oscilloscope pattern remains stationary and the unknown is easily calculated. The new invention permits accurate measurement even when the pattern is not stationary.

F_s is fed to a phase splitter and amplifiers. The outputs of the two amplifiers have equal amplitude but their phases differ by 90° . Therefore the CRO sweep is a circle (shown by dotted lines in the figure). When F_x modulates this sweep, a wavy pattern appears. If F_x/F_s is an exact integer N, the pattern remains stationary and there are N cycles. The figure shows a pattern which results when $F_x=6 F_s$.



When F_x/F_s is not an exact integer the wavy pattern appears to rotate in one direction or the other. This rotation can be "stopped" by stroboscopic methods. This is done by F_a and the wave shaper which frequency-modulates the oscilloscope grid and periodically blanks out the pattern. To calculate F_x , the stroboscopic frequency F_a is adjusted to a high frequency and gradually reduced until the rotating pattern appears to stop. Then the unknown equals $F_x = NF_s \pm F_a$.

F_a need not have the high accuracy of the standard frequency. As an illustration, assume that F_s is 102 cycles and F_x is 1,000. The pattern will contain 10 cycles and will appear to rotate. Motion will appear to stop when F_a is 20 cycles. If F_a has an accuracy of 5% it will be in error by 1 cycle so F_x will be known accurately to within 0.1% or 1 part in 1,000.

As in any stroboscope, F_a can stop the motion at more than one frequency. Use the highest value. Note also that F_a is added or subtracted from NF_s to find F_x . The correct sign depends upon whether the pattern rotates in one direction or the other. It may be determined experimentally for a given circuit and oscilloscope.

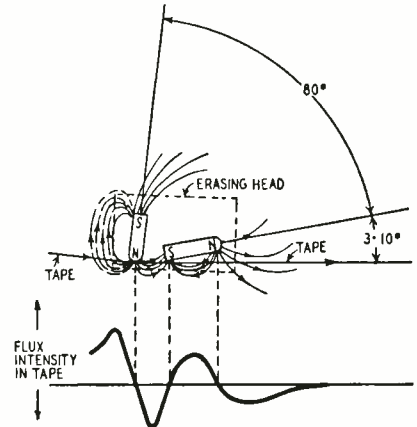
PM ERASING HEAD

Patent No. 2,535,498

Otto Kornei, Cleveland Heights, Ohio.
(Assigned to Brush Development Co.)

This erasing head is of the PM type. The magnetized tape travels past two bar magnets fixed in position. These magnets produce an alternating, decaying field which demagnetizes the tape and erases the sound recorded on it.

As the figure shows, the tape approaches the first magnet nearly perpendicularly (from the left in the figure). It recedes from the second magnet at an angle between 3° and 10° . The magnets themselves make an angle of about 80° with each other.



The field created by the first magnet is stronger than any recorded on the tape. This obliterates all residual recordings. As the tape moves adjacent to the N pole of the first magnet it enters a neutral field because of the divided flux from this pole. The field reverses between the magnets. The second magnet produces another magnetic cycle which tapers off to zero.

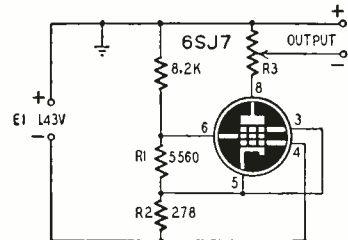
POWER SUPPLY FOR BIAS

Patent No. 2,536,830

Garet F. Ziffer, Syracuse, N. Y.
(Assigned to General Electric Co.)

This is a single-tube circuit which provides voltage for bias purposes. Its output is constant and its ripple low.

The plate current of a pentode is determined mainly by the voltages on the screen and control grids. In this circuit the two elements are



connected to have opposite effects. For example, when E_1 rises, there is an increase in screen voltage while the control grid goes more negative. By properly selecting R_1 and R_2 these effects become equal as well as opposite. Therefore the plate current remains constant when E_1 varies. Output voltage is taken from potentiometer R_3 .

Component values are shown for a 6SJ7. According to the inventor, this circuit shows less than 0.1% ripple for an E_1 ripple of 20%. The output voltage remains constant to better than 0.5% even when the input is varied as much as 50%.

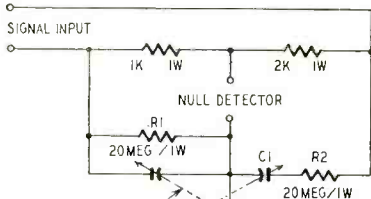
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CAPACITANCE-TUNED FREQUENCY BRIDGE

The Wien bridge is a perennial favorite with experimenters as an inexpensive, tunable frequency-selective network. It is especially useful for identifying unknown audio frequencies by the null method, as a selective feedback network in tuned amplifiers, and as a heterodyne eliminator ("heterofil") in radio receivers. The single practical drawback of this circuit has been the difficulty in obtaining inexpensive ganged potentiometers with satisfactory tracking between sections.

This difficulty is overcome in the accompanying circuit by varying the dual capacitors of the bridge, instead of the resistors. It is, of course, much easier to obtain good tracking between tuning capacitor sections than between dual volume controls. A common 365- μ f-per-section unit is used.

This circuit is not a true Wien bridge in the strictest sense, since the normal positions of C1 and R2 have been interchanged. This was done to use a standard tuning capacitor with common rotors. The null response is very good, however, when using headphones or v.t.v.m.



DUAL 365 μ f B C TUNING CAP

Circuit of the capacitance-tuned bridge.

Tuning range of the circuit shown is 18 to 370 cycles. This rather extended range may be restricted, if desired, by using a padder in parallel with each tuning capacitor section. The basic range may be multiplied in suitable steps by changing simultaneously the values of R1 and R2. When R1 and R2 each are 2 megohms, the range is 180 to 3,700 cycles; and when they are each 200,000 ohms, the range is 1,800 to 37,000 cycles. Because of unavoidable stray capacitances, there may be some difficulty in obtaining clean, sharp nulls at frequencies above 20,000 cycles.

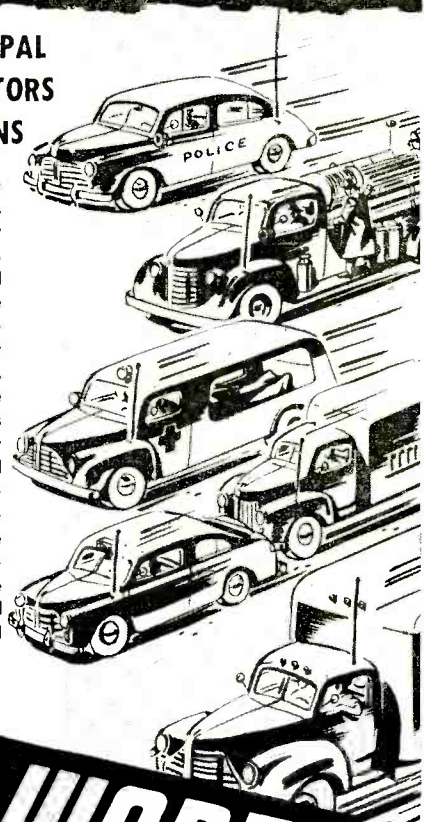
By using a ganged switch to change R1 and R2, the bridge can be made to cover the full audio range from 18 to 37,000 cycles in only three steps. If stray capacitance is kept low, only one dial scale need be used to cover all three ranges.

To eliminate body capacitance effects, a ceramic coupling *must* be placed between the tuning capacitor shaft and a bakelite shaft attached to the tuning knob. Also, the tuning capacitor must be mounted at least 3 inches back of the fingers. If the rotors of the tuning capacitor are grounded, as shown in the diagram, the signal input source must not be. However, the null detector can be. If, on the other hand, the signal source is grounded, the rotors and null detector cannot be.—Rufus P. Turner, K6AI

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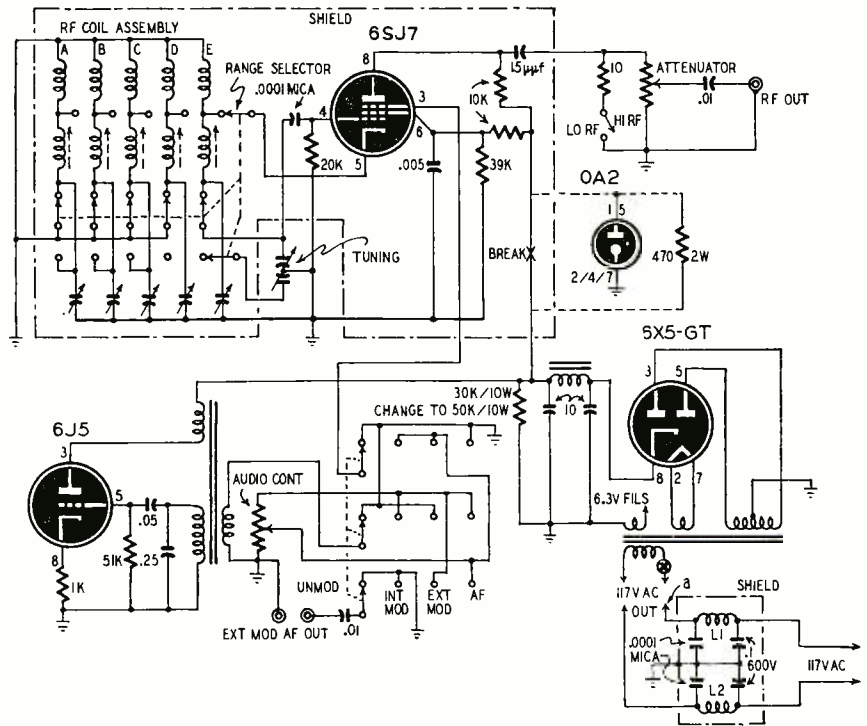
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1Q5GT	1.09	7A5	1.08
1R5	1.59	7A8	1.47
1S4	1.07	7B4	1.08
1S5	1.04	7B5	1.08
1T4	1.12	7B6	1.08
1T5GT	1.24	7B7	1.47
1U4	.98	7C5	1.08
1U5	.98	7C6	1.08
1X2	1.68	7F7	1.69
3A8GT	2.97	7F8	1.36
3Q4	1.38	7Q7	1.08
3Q5GT	1.44	7V7	1.47
3S4	.98	7Y4	.89
3V4	1.19	12AH7GT	1.64
5T4	2.17	12AL5	1.26
5U4G	1.08	12AT6	1.08
5V4G	1.87	12AT7	1.89
5W4	1.14	12AU6	.97
5Y3GT	.79	12AU7	1.98
5Y4G	.98	12AV6	1.17
5Z3	1.07	12AX7	1.63
5Z4	1.28	12BA6	1.08
6A7	1.06	12BE6	1.08
6AB7	1.89	12J5GT	.97
6A8GT	1.29	12K7GT	1.04
6AC7	2.29	12Q7GT	1.04
6AF6G	1.44	12SA7GT	.98
6AG5	1.74	12SF5	.98
6AG7	1.92	12SF7	1.08
6AH6	2.29	12SG7	1.08
6AK5	2.34	12SJ7GT	1.08
6AK6	1.47	12SK7GT	.98
6AL5	1.69	12SL7GT	1.49
6AL7GT	1.88	12SN7GT	1.39
6AQ5	1.49	12SQ7GT	.98
6AQ6	1.24	12SR7	.98
6AQ7GT	1.67	14A4	1.08
6AS7G	5.76	14A7	1.08
6AT6	1.08	14B6	1.08
6AU5GT	1.89	14Q7	1.08
6AU6	1.69	14R7	1.08
6AV6	1.37	19BG6G	3.64
6AX5GT	.97	19T8	1.49
6B6G	.84	24A	1.17
6BA6	1.08	25A6	1.49
6BE6	1.08	25L6GT	1.14
6BG6G	2.89	25W4GT	1.36
6BC5	1.74	25Z5	.98
6BH6	1.45	25Z6GT	1.08
6BJ6	1.37	27	.97
6BQ6GT	1.87	35A5	1.28
6C4	1.49	35B5	1.32
6C5GT	.98	35L6GT	1.24
6C6	.74	35W4	1.08
6CB6	1.74	35Y4	1.36
6CD6G	3.45	35Z3	1.34
6D6	.74	35Z5GT	.98
6E5	1.46	36	1.62
6F5GT	.99	41	1.19
6F6GT	1.07	42	1.32
6G6G	1.22	43	1.32
6H6GT	1.08	45	1.29
6J5GT	.87	45Z5	1.08
6J6	1.97	47	1.38
6J7GT	.98	50A5	1.54
6K5GT	1.62	50B5	1.24
6K6GT	1.08	50C5	1.24
6K7GT	1.08	50L6GT	1.24
6L6G	1.85	70L7GT	1.87
6N7GT	1.47	75	1.08
6P5GT	1.47	76	.98
6Q7GT	1.08	77	.98
6SA7GT	1.08	78	.98
6SC7	.89	80	.79
6SF5GT	.89	117L7GT	1.98
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REVAMPING A TRIPLETT SIGNAL GENERATOR

The Triplett Model 3432 AM signal generator has two characteristics which can limit its usefulness in a service shop. Although its power transformer has an electrostatic shield, enough r.f. is radiated through the

Change the bleeder resistor from 30,000 to 50,000 ohms. Break the B-plus lead to the r.f. oscillator and insert a 470-ohm, 2-watt resistor. Connect an 0A2 between ground and the junction of the 470- and 10,000-ohm resistors.



power line to cause interference to nearby radio and TV receivers and make alignment difficult if not impossible. Frequency shift with line-voltage variations also does its share to make servicing difficult.

The drawing shows the diagram of the 3432 and changes which reduce radiation and insure against frequency shift with line voltage fluctuations.

The 0A2 stabilizes the oscillator supply voltage at 150 and helps to keep the frequency constant.

To reduce radiation, insert the line filter shown at *a* between the switch and the line cord. L1 and L2 are 20 turns of No. 28 enamelled wire close-wound on a 1½-inch form. This filter should be enclosed in a well-grounded shield.—Wilbur J. Huntz

TESTER CHECKS FOR DEFECTIVE SELENIUM RECTIFIERS

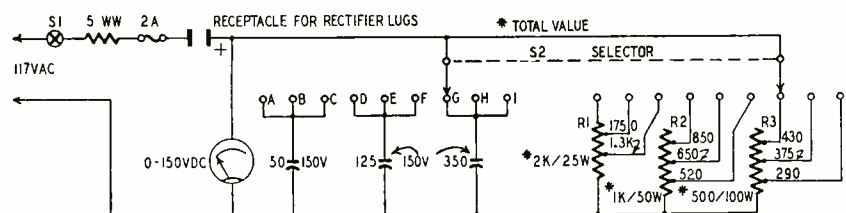
Defective selenium rectifiers which develop less than normal output voltage often cause loss of sensitivity in broadcast sets and many other types of troubles in TV sets. To assist the service technician in making qualitative measurements on these units, the Rectifier Division of Sarkes Tarzian has released a circuit of a tester for their selenium rectifiers.

Rectifiers are rated by the d.c. voltage which they develop across a large filter capacitor when delivering approximately full-load current. Load resistor R1 is an adjustable, 2,000-ohm, 25-watt unit tapped at 1,750 and 1,300 ohms; R2 is 1,000 ohms, 50 watts, tapped at

850, 650, and 520 ohms; and R3 is 500 ohms, 100 watts, tapped at 430, 375, and 290 ohms. A 2-circuit, 9-position, non-shortening switch selects the required load resistor and filter capacitor.

To operate the tester:

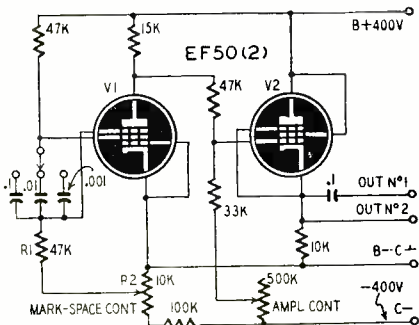
1. Make sure that S1 is OFF, then plug the rectifier into the receptacle. Be sure that polarity is correct.
2. Set the selector (S2) to the correct position for the rectifier being tested.
3. Throw S1 to ON.
4. Reject all rectifiers which, within 5 minutes from the time the voltage is applied, do not deliver the approximate voltages listed in the following table:



Rectifier Model No.	Selector Setting	D.C. Volts (Approximate)
65 (65 ma)	A	130
75 (75 ma)	B	130
100 (100 ma)	C	125
150 (150 ma)	D	130
200 (200 ma)	E	130
250 (250 ma)	F	130
300 (300 ma)	G	125
350 (350 ma)	H	125
450 (450 ma)	I	120

SQUARE-WAVE GENERATOR

When time is an important factor, use a square-wave generator and scope instead of a variable-frequency oscillator and voltmeter for checking the response of audio and video amplifiers. The latter method gives the true response curve which is more easily interpreted, but it takes too long to plot curves when comparative checks are made on several amplifiers or when cut-and-try methods are used to select components which give the desired response curve. A square-wave generator and oscilloscope are the ideal tools for making rapid measurements.



Described in *Wireless World* (London) is a simple generator which provides square waves at 80, 800, and 8,000 cycles with output variable from zero to 50 volts peak-to-peak. The circuit shown in the diagram is simpler than the usual multivibrator-type square-wave generator or the clipping and clamping circuits used to convert sine-wave voltages into square waves.

The negative half-cycles at the plate of the triode oscillator V1 are distorted, so a combined triode limiter and cathode-follower V2 is used to clip the negative half-cycle and provide a low-impedance output of approximately 150 ohms. The 10,000-ohm control varies the mark-space ratio from approximately 5 to 1 at one extreme to about 1 to 3 at the other. This control affects the repetition rate so the frequencies of 80, 800, and 8,000 cycles are correct only when the mark-space control is set for producing a perfect square wave. The frequency is continuously variable within each range when R1 is replaced with a variable control. When R1 is variable it interacts with R2 so calibrations do not hold.

The original constructor used EF50's. These are readily available on the surplus market but the special 9-pin lock-in sockets they require are hard to find. You can substitute a 6AB7, 7V7, 7W7, or any similar pentode for V1 and one



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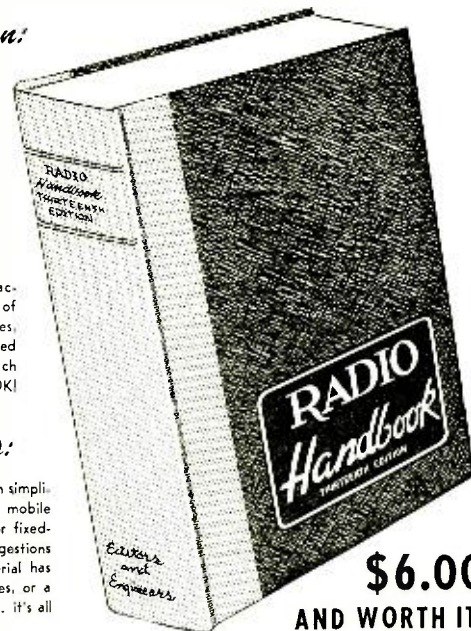
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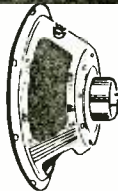
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section of a 6SN7 or a similar triode for V2.

The unit requires 400 volts of bias and 400 volts on the plates for 50 volts peak-to-peak output. The output is somewhat lower when operating voltages are halved.

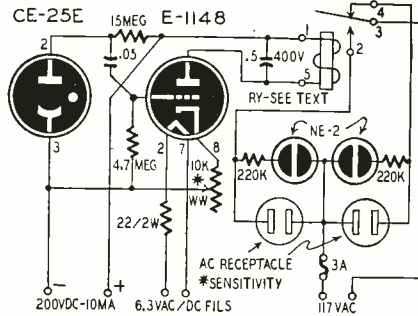
PHOTOELECTRIC RELAY

The photoelectric relay shown in the diagram has unusual characteristics which make it useful for many applications. It can be made to perform as follows:

1. Open or close an external circuit and hold it in that position until the relay is reset by the operator.
2. Operate as a high-speed photoelectric relay for counting, signaling, or control purposes.
3. Open or close an external circuit for a predetermined interval which is not controlled by the light source.

To operate the unit as a locking-type relay as in No. 1 above, advance the sensitivity control until the relay just closes, then back off the control just a hair.

For normal high-speed operation, advance the control slightly beyond the point where the relay pulls in. Touch-up the adjustment and vary the



strength of the light source for reliable operation at high speeds.

To operate the unit as a light-triggered time-delay relay, advance the sensitivity control well beyond the point where the relay pulls in. When light strikes the phototube, the relay opens for a few seconds and then closes again. The cycle repeats when the light is momentarily interrupted. The duration of the timed cycle depends on the setting of the sensitivity control and the intensity of the light beam which strikes the photo tube.

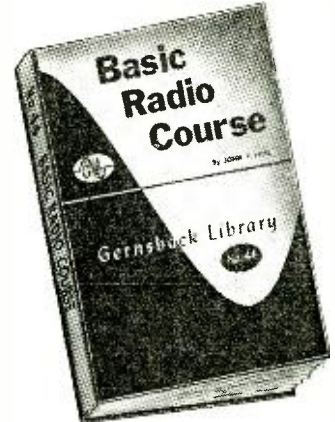
All components in the relay unit are available on the surplus market. The photo-tube is a CE-25E which is electrically equivalent to the 927 and 1P32. The control tube is a surplus E-1148 which is equivalent to the HY615. Any s.p.d.t. d.c. relay having a coil of 6,000 ohms or more can be used. Tiny neon lamps are connected across the a.c. outlets to serve as indicators showing whether the relay is in an energised or unenergised state.

A special socket is required for the CE-25E. You can make one from a miniature 7-pin socket. Remove the metal pin inserts and ream holes 1, 4, and 7 for a snug fit on the pins of the CE-25E. Solder the circuit wires directly to the base pins on the tube.—*O. C. Vidden*

—end—

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TV BALLAST TUBE

Clarostat Mfg. Co., Inc., Dover, N. H., announces a new TV ballast replacement for Pilot Radio, Type 35-37. This is one of the Clarostat plug-in tube-type wire-wound resistors which are avail-



able in some 75 standard numbers for exact-duplicate replacements, and in 10 Universal numbers representing a minimum inventory that can take care of upward of 85% of replacement coils.

PA MICROPHONE

Electro-Voice, Inc., Buchanan, Mich., introduces the model 636 Slimair microphone for PA work. It is 1-1/16 inch in diameter and 10 inches long. The



grille head is acoustically designed to prevent wind and breath blasts, and outdoor pickup is free from wind rumble. Bass response extends to 60 cycles and treble goes up to 13 kc.

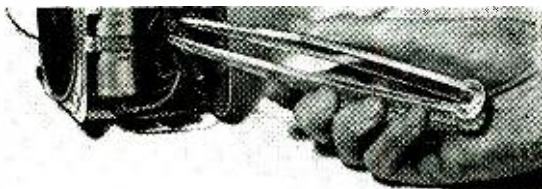
The omnidirectional polar pattern becomes somewhat directional at high frequencies. A swivel head permits vertical tilt for aiming at sound source. Stand coupler has a standard 3/8 inch 27 thread, and the case is made of brass and finished in satin chrome or ebony black. On off switch is optional.

PROBING TWEEZERS

Hytron Radio & Electronics Corp., Salem, Mass., is distributing plastic probing tweezers to the radio service trade.

With the set turned on, these probing tweezers probe, grasp, and manipulate suspected wiring and components to make it easier to ferret out intermittents, shorts, opens, feedback from adjacent wiring, etc. The operator is free from the danger of shocks and shorts.

The jaws of the tweezers have coarse and fine serrations for grasping different sizes of wire, resistors, etc. They are made of high-dielectric polystyrene to minimize capacitive detuning.



H. V. CAPACITOR

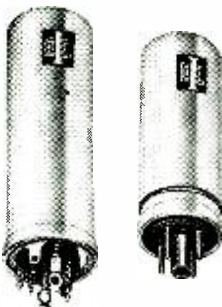
Sprague Electric Products Co., North Adams, Mass., has developed a new 500- μ mf, 15,000-volt ceramic capacitor consisting of a ceramic slug encased in a sturdy molded rubber jacket. Known as the type 510C1, the capacitor is rated for continuous operation at 85° C. and will withstand a 22,500-volt dielectric test. Its minimum insulation resistance is 10,000 megohms.

The composition of the special rubber jacket is such that it will withstand a corona atmosphere without physical deterioration. In addition, the rubber compound used is equal or superior to neoprene in its resistance to combustion. A self-grammet permits easy mounting in chassis. Capacitance and voltage rating markings are molded into the black rubber body.



ELECTROLYTICS

Illinois Condenser Co., 1616 North Throop St., Chicago, Ill., offers an improved line of plug-in and twist-prong electrolytic capacitors to meet JAN and commercial specifications. They feature a phenolic molded cap structure



that hermetically seals the container so that these units can be used under the most difficult conditions, from marine operations to stratosphere use. They are not affected by sudden temperature or pressure changes, and can withstand wide temperature ranges. Available with both high- and low-voltage ratings, they meet all Navy, Army and Air Force requirements.

V.H.F. TRANSMITTER TUBE



General Electric Co., Tube Division, Schenectady, N. Y., offers a new power tube for TV and FM transmitters. De-

signed for use as a grounded-grid class B or class C r.f. amplifier or as an oscillator, the GL-6039 has a water-cooled anode and a cathode with a thoriated tungsten filament, and can dissipate 7 kw. A pair of these tubes will put out 10 kw in TV service and 25 kw in FM. Neutralization is not necessary in a properly designed circuit, and the tube features low lead inductance, large terminal contact area, and silver-plated metal parts to reduce r.f. losses.

CRYSTAL MICROPHONE

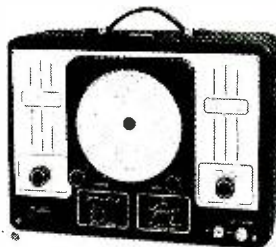
Turner Co., 900 17th Street, N.E., Cedar Rapids, Ia., announces model 60X crystal microphone for hand, desk, or stand use. Response is 70 to 7,000 cycles and sensitivity is 52 db below 1 volt/dyne/sq. cm. The case is finished with a baked-on beige wrinkle-finish enamel, and the microphone is furnished com-



plete with 6-foot cable and stand adapter. Available with on-off slide switch.

TEST OSCILLATOR

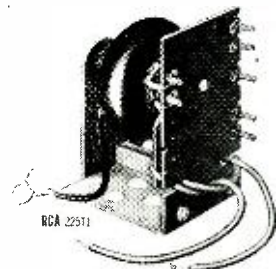
Triplet Electrical Instrument Co., Bluffton, Ohio, is marketing a new wide-range test oscillator, model 3432. Five fundamental ranges cover from 165 kc to 40 mc, and two harmonic ranges cover from 36 to 120 mc. Each range has its own easily read scale. An r.f. selector provides high and low output, and an output attenuator provides fine control of the output. Internal modulation is variable from 0 to 100% at 400 cycles. External modulation may



be applied. All audio and r.f. circuits are doubly shielded with copper-plated steel shields. The black enamel metal case measures 15 11/32 x 11 1/32 x 6 1/4 inches and has a strap for carrying.

H. V. TRANSFORMER

Radio Corp. of America, Tube Dept., Harrison, N. J., has a new horizontal-deflection-outout and high-voltage transformer, 225T1, for use with picture tubes having a deflection angle of about 66°. It provides omni-deflection with a single driver tube and requires only a single high-voltage rectifier tube. In properly designed circuits, the transformer can supply up to 16 kv at



no load, has good regulation, and provides good deflection linearity. The 225T1 uses a ferrite core for high efficiency and compactness. It is designed to match a 209D1 yoke.

MULTIMETER

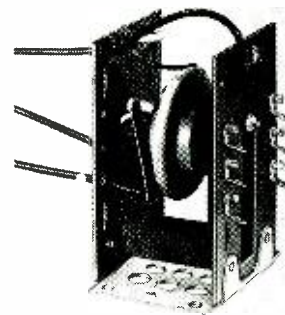
Electronic Instrument Co., 276 Newport St., Brooklyn, N. Y., is releasing its new 20,000 ohms/volt multimeter EICO model 555. Available either in kit form or factory wired, the instrument has 31 ranges. The 4 1/2 inch meter has a 50- μ a movement. All resistors have 1% or better accuracy. The case is high-impact bakelite with all figures and symbols imbedded for long wear.

Ranges: d.c. voltage: 0-2.5, 10, 50, 250, 1,000, 5,000, at 20,000 ohms/volt. A.c. voltage: same ranges, at 1,000 ohms/volt. Output voltage: some ranges, with 0.1- μ f internal series capacitor. Decibels: -12 db to +55 db, in 5 ranges. D.c. resistance: R x 1, R x 100, R x 10,000. D.c. current: 0-100 μ a, 10 ma, 100 ma, 500 ma, 10 amp. (250 millivolts). D.c. accuracy: 3% of full scale. A.c. accuracy: 5% of full scale on all ranges.



FLYBACK TRANSFORMER

RAM Electronics, Inc., Irvington-on-Hudson, N. Y., announces a new high-efficiency flyback transformer for replacement and conversion purposes. The XO45 is designed for all receivers originally using 1B3-G or 6BG6-G tubes. It generates 12.5 to 14 kv for 16- to 20-inch round or rectangular tubes, with horizontal sweep more than ample for 20-inch picture tubes. Both regulation and linearity are good.



DEFLECTION YOKE

Allen B. Du Mont Laboratories, Inc., Electronic Parts Division, East Paterson, N. J., presents the series Y2A distributed winding deflection yoke—designed for edge-to-edge sharp focus—for 60 to 70-degree deflection picture tubes.

The Y2A deflection yoke is available for use with transformer or auto-transformer output circuits and with different networks and lead lengths, or without networks and leads. In several standard stock types, it covers the needs of service technicians and set owners for improving existing equipment. For the service trade, the yokes come packed in the individual boxes with installation instructions.

Rugged in mechanical design, the yoke can withstand continuous operating temperatures up to 90° C., and voltages up to 4 kv between any windings or between windings and frame. Standard horizontal inductance is 10.5 millihenries, and vertical inductance 42 millihenries.

SCOPE CALIBRATOR

Tensor Electric Development Co., 343 Classon Ave., Brooklyn, N. Y., introduces its model A-42F oscilloscope calibrator. It permits monitoring the amplitude of a signal or any part of a signal on an oscilloscope screen. Voltages as low as 0.5 mv and as high as



100 v r.m.s. can be measured. The signal to be measured is connected to the input of the calibrator, and the calibrator output feeds the scope. The calibrator is set to give an image that is just larger than that of the test signal, and the amplitude is read on the calibrator meter. The meter scale is calibrated in r.m.s., peak-to-peak, and voltage db above 1 volt. The calibrator output is a 60-cycle sine wave with an accuracy of 5% from .0005 to 100 volts r.m.s.

TV ANTENNA

Technical Appliance Corp., Sherburne, N. Y., is marketing a new antenna called the Taco Special Twin-Driven Yagi which is designed to cut out most co-channel interference. Average front-to-back ratio over the 6-mc bandwidth of the channel for which it is tuned is 30 db. Terminal impedance is 300 ohms. Mechanically the new antenna is similar to the regular Taco twin-driven Yagi. Available for any of the low bands, the Special may be used as a single antenna, or as a stacked array. Elements are a director, two driven elements, and a reflector.

CALIBRATED POT

Chicago Industrial Instrument Co., 536 W. Elm St., Chicago, Ill., is offering a new precision potentiometer.

The Selectohm is a new accurately calibrated 0-to-100,000-ohm linear potentiometer for use as a resistance substitute for service or laboratory



work. It provides a fast means for determining the values of blackened burned-out resistors when it is substituted in radio, television, and other electronic circuits.

The new units is also useful for laboratory work and may be used to replace a decade box. The Selectohm serves as a precision rheostat, shunt, or multiplier. It is rated at 25 watts.

TV INSTALLATION KITS

Insuline Corp. of America, Long Island City, N. Y., is distributing a series of eight television antenna installation kits, designed to meet practically all receiving requirements in either primary service or fringe areas. The simplest kit contains a single conical aerial, a 5-foot steel mast, and 50 feet of lead-in wire. The others are progressively more elaborate, the largest kit containing a stacked conical aerial, 10-foot mast, base mount, guy wire, 100 feet of lead-in, lightning arrester, clamps, insulators, etc.

R-C OSCILLATOR

Southwestern Industrial Electronics Co., 2831 Post Oak Road, Houston, Tex., announces a new precision oscillator.

The model M-2 oscillator covers a range of 1 to 120,000 cycles in five bands. The circuit is an improved version of a bridge stabilized type oscillator which affords a means of reducing to a minimum the influence of amplifier parameters on the frequency of oscillation. The dial is calibrated to within 1 1/2% plus 0.1 c.p.s. One of the two output circuits provides from 0 to 20 volts r.m.s. to a 1,000-ohm load, and the other provides from 0 to 1 volts into a 300-ohm load.

Harmonic distortion is less than 2% within the audio range.

An electronically regulated power supply provides plate current for all stages, and deposited-carbon resistors



are used in the frequency-determining networks. Power consumption is 125 watts at 115 volts, 60 cycles. Dimensions are 9 3/4 inches high, 18 1/2 inches long, and 12 inches deep. Weight is 43.5 pounds.

VIDEO AMPLIFIER

Ripley Co., P.O. Box 31, Middletown, Conn., presents a new video amplifier.

Having a gain of 1000, the frequency response of this amplifier is flat from 15 c.p.s. to 4 mc within 1.5 db of the 10-kc response point. A cathode-follower input stage is used for circuit isolation and includes an input attenuator providing 1:1, 1:10 and 1:100 attenuation ratios as indicated by a control knob on the front panel. The input impedance, without probe, is approximately 2.2 megohms and 40 μ mf on all attenuator ranges.

A gain control is provided for adjusting the output from 0 to 50 volts r.m.s. A signal-polarity switch on the front panel varies the cathode bias so that the amplifier unit may be adjusted for



optimum performance regardless of the polarity of the input signal. Phase shift is minimized to provide satisfactory reproduction of pulses on the order of .1 microsecond and of square waves at repetition rates as low as 100 per second.

TUBE TESTER

Triplet Electrical Instrument Co., Bluffton, Ohio, announces a new tester.

Model 3413-A has flexible 3-position lever switches for complete coverage of present and future tube connections. RMA pin numbering of tube element levers makes for quick reference of tube base connections. Illuminated, easy-to-read roll type chart is built into the tester. Simplified test procedure makes it possible for the user to add new tube data to the chart when desired.

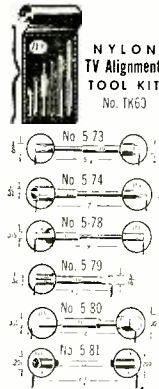
Line-voltage indication on center of meter dial permits observation and adjustment for line fluctuations. Filament voltage: 0.63 volts to 110 volts in 14 steps.

The large 6-inch meter has a 3-color easy-to-read good-bad scale.

Portable metal case, 15-11/32 x 11-1/32 x 6-1/8 inches, is of black satin wrinkle finish, and has removable, hinged cover and leather handle.

ALIGNMENT TOOL KIT

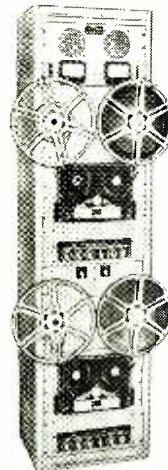
JFD Manufacturing Co., 6101-23 Sixteenth Ave., Brooklyn, N. Y., introduces a new alignment tool kit No. TK60. It contains six alignment tools made of molded nylon. Each tool has two different tuning tips, one on each end. Made in contrasting colors for quick identification, the tools are packed in a handy plastic case.



Service adjustments provided by the tools are: No. 5-73 for tuners, trimmers, and i.f. transformers; No. 5-74, for midjet transformers; No. 5-78, for nested iron cores; No. 5-79, for close trimmer and i.f. transformers; No. 5-80, for K-tron and i.f. transformers; No. 5-81, tuning rod for changing coil inductance.

24-HOUR TAPE RECORDER

Amplifier Corp. of America, 398 Broadway, New York, N. Y., is introducing the Magmaster model 550-B, a 24-hour recording recorder designed for continuous recording of airport plane-to-control tower conversations, continuous telephone monitoring, and all other applications requiring unattended, continuous, round-the-clock recording and playback.

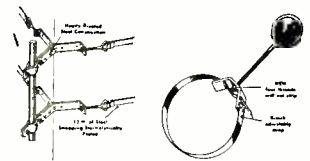


The instrument has two complete recording-playback systems, each of which operates continuously for 12 hours at a tape speed of 3 inches per second using a 15-inch diameter reel containing 6,000 feet of standard 1/4-inch recording tape. After two tracks have been recorded or played on one reel, a relay sets the other reel into operation. By changing the reel at any time during the 12-hour interval, continuous play for extended periods is attained.

Frequency response of the over-all system is 50 to 4,500 cycles \pm 3 db. Dynamic range is 40 db. Input impedances are 500 ohms for recording off telephone lines, and 200 and 50 ohms for microphone line recording. Output impedances are 3.2 and 500 ohms for playback through external speakers or into a telephone line. Amplitude variation at 1,000 cycles is less than 0.75 db. Power output through the built-in playback amplifier is 5 watts, with facilities provided for higher power using external amplification.

ANTENNA HARDWARE

Industrial Precision Products Co., 315 N. Hoyne Ave., Chicago, Ill., announces a new line of antenna hardware which features some heavy riveted construc-



tion for chimney and wall mounts, and mast standoffs made with a deep extrusion to accommodate four or more threads to prevent stripping.

SOLDERING GUN

Phillips Manufacturing Co., Inc., Minneapolis, Minn., offers a new soldering gun. The Versa-Tool combines heating element, transformer, light, two-position switch and fuse into a single unit. Its four interchangeable tips of rigid construction enable the operator to unsolder old work by exerting tip pres-



sure with the heating element on. The two-position, trigger-actuated switch in the first position closes the circuit to a concentrated light beam, set at an angle to eliminate shadows. This position enables the operator to use the tool as a flashlight. The second position maintains the light circuit and closes the heating element circuit. Both transformer and basic circuit are protected by a fuse, and the carbon element is replaceable.

WEATHERPROOF DRIVER UNIT

Racon Electric Co., 52 East 19th St., New York, N. Y., announces a new driver unit. The model PM-708TR features a built-in 25-watt, vacuum impregnated, line-matching transformer with available impedances of 15, 500, 1,000, 1,500, and 2,000 ohms.



The voice coil is wound of aluminum wire and the coil terminals are welded. The voice-coil lead is a strip of fatigue-resistant beryllium copper, and the voice-coil suspension is Bakelized linen cemented to the phenolic diaphragm with thermosetting plastic.

This driver unit has a 75-100% overload capacity, is completely waterproof and tropicalized, and has combined solder lug and binding post terminals.

TEST EQUIPMENT LINE

Precision Apparatus Co., 92-27 Horace Harding Blvd., Elmhurst, L.I., announces to the service trade a new moderately priced, matched-panel-mounting test instrument combination, available complete or in separate units. This new combination includes the series E-200C-PM signal and marker generator, the series 10-12-PM Electronic tube master and battery tester, series E-400-PM sweep signal generator—all three mounted in standard matching panels. Also included in this set are the new Precision EV-20 zero-center vacuum-tube voltmeter, and multirange test set, and the series ES-500 5-inch wide-range, high-sensitivity portable oscilloscope.

—end—

The Radioman's Wife Puts in A Good Word

By MRS. ROBERT E. ALTOMARE

Every time I try to dun my husband for money for a new hat, or a coat, or any similar necessary appurtenances to feminine happiness, I'm always met with, "If you need extra money why don't you write an article?"

"Why not?" quoth I, and add with some ascerbity, "On what?"

To which said husband, being a radioman, replies in great surprise at my stupidity, "On radio, of course."

Whether this will net me a new bonnet or not, it looks like a good way to air my many and uncomplimentary views on the subject.

LET'S get one little matter straight for the record right now. I do not now, nor from the looks of things, will I ever, "see" radio.

Little facts such as expecting a new rug from carefully nurtured savings and having hubby gleefully exhibit a "bridge" purchased from same are just the sort of things that could have curdled my enthusiasm, but I doubt it. It had to be much more than that.

For instance: At a gay gathering where husbands and beaus are do-si-do'ing and swinging their ladies with great good will, if I happen to spy some wistful creature sitting alone with her hands clasped quietly in her lap, I can usually start out on the right conversational foot by asking, "And what branch of radio is your husband's hobby?"

When I see some frail female up on a housetop battling a stiff wind while

she nails down the flapping shingles, I just look beyond her for the short-wave antenna that's sure to be in the back yard.

One girl I know spends her evenings sitting on the basement stairs talking to her husband and knitting, and, incidentally, accumulating callouses since there is never room for a chair among the radio paraphernalia. Hers is an extreme case, of course. The only reason her husband can still talk is that he is only a *student* radioman. Not full-fledged, you see!

Whenever I hear a woman speak of her "two lovely children" and then, laughing resignedly add, "But of course, I really expected a larger family." I can get a reputation for being psychic simply by asking whether her husband does experimental radio work or transmitting.

Now this observation may seem a



"One girl spends her evenings sitting on the basement stairs . . . and knitting."



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backhanded slight of radio's manhood but you'll have to admit that the real "ham" generally gets up at 5:30 am to talk to Timbuctoo, recognizes his

a certain amount of patriotic excur-sioning toward increasing the popula-tion that dwindled due to the war, the enticing things we girls heard around



"All those boxes you have to climb over before you can open up the studio couch."

status as pater familias by putting in eight grudging hours at some job, then rushes from the supper table to spend the rest of the evening talking to Ootcutbit, which is Timbuctoo spelled backward and pretty much the way that shortwave sounds to me.

If, however, the husband is only interested in experimental radio work, then he sleeps to the last possible moment—any morning—so that he will have long, reasonably fresh evening

the lockers during the second year of high was not the type of activity that would engage the interest of the real radioman and we radiowives would simply have dismissed such ideas along with those about the Easter bunny and the birds and bees.

Where to find the shack

"Shack" is a word of many strange and varied meanings. If you live in a one-room affair with your radio



"I've learned to swing a pretty neat hacksaw, but even there I get stymied."

hours to "try" things in his shop.

Except for the weaker mind and backsliding of the radio novice and

husband, then it is all those boxes of stuff you have to climb over before you can open up the studio couch.

If you live in two rooms, "shack" is the three-fourths of the dining table that you can no longer eat off.

If you live in a house, the shack is the space designated on the plans or by the real estate agent as "laundry" or "lovely recreation room."

In my own case "shack" brings back bitter memories.

My husband always used to refer to me with a certain kindly affection, "My wife? Yeah, she's a pretty nice girl." But one day a girl friend and I were having a heart-to-heart talk about how many times you should rinse the clothes when I mentioned that it was pretty darned hard for me to get any laundry done at all because of all the junk in the basement. Wouldn't you just know that he would hear me? JUNK! His most precious precious!

Well, they say it is the little things in life that really count. Upon such loose name-calling on my part my husband was ready for the divorce courts then and there, when I reminded him of the baby. Nevertheless, he watches his words and thinks twice before he cautiously refers to me as "My wife? Yeah."

But I'm not the type to let these things get me down. Having been the girl voted "most likely to—," I put my thinking cap on and decided that the way to dethrone that radio usurper of my rightful place in the American Home would be to study radio. Yes, I would study radio, and hubby and I would go hand in hand down Life's Lane in Happy Companionship.

If I could persuade my husband to take cooking lessons written in Sanskrit, he'd get an approximate idea of what I went through.

Who in tunket would know that Xmfr was a transformer?

"Measure the c.m. area of the conductors," the experiment read.

"Conductors?" I cried wildly, "There's nothing here but a bunch of wires!"

"Plug in the jack," the instructions said.

"Oh, my gosh, what is a jack?" My experience led me to think of a boy or one of those things you use when you get a flat. Nothing like that here.

"Why is damping necessary?" read the question sheet. Having raised a baby or two, I had a ready answer for that one but it wasn't the answer they wanted.

"And these calipers," said the instructor matter-of-factly, "are hermaphrodites."

"Oh," I gasped, shocked, "not really!"

My lessons are all well surrounded by marginal notes mostly concerned with translating the jargon into standard usage. Actually, I have become so word conscious that I'm a better proof-reader than the school ever had.

A lady is limited

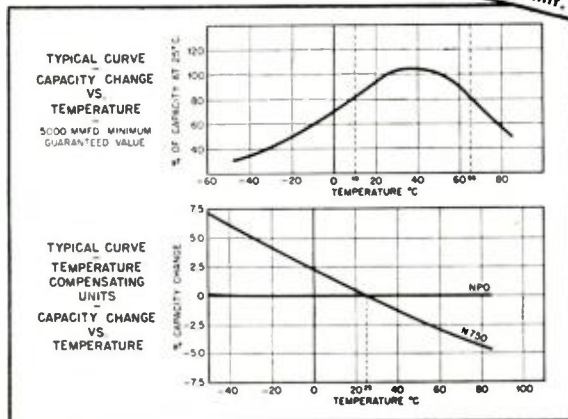
It hasn't all been in vain, though. I've learned to swing a pretty neat hacksaw but even there I get stymied. The comfortable "go to H—" with

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2x2000 mmf.	6TMSDD2C
2x2500 mmf.	6TMSDD25C
2x3000 mmf.	6TMSDD3C
2x4000 mmf.	8TMSDD4C
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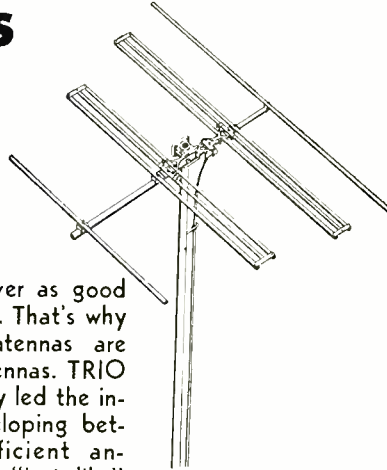
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A copy is never as good as the original. That's why TRIO TV Antennas are "wanted" antennas. TRIO has consistently led the industry in developing better, more efficient antennas. Never "just like" another, every new TRIO model is original and represents an improvement over any existing TV antenna.



*MODEL 445, the famous Single-bay TRIO Yagi for TV channels 4 & 5. Supplied less mast and transmission line.

*Patent Pending — No licensing arrangements granted for duplicating principle of this antenna.

TRIO YAGI SETS THE PACE

An example of TRIO's original design is the amazing dual channel TRIO Yagi — a single-bay 4 element yagi that provides full 10 DB gain on two channels! Available for channels 4-5 and 7-9, this revolutionary antenna makes bulky stacked arrays obsolete by providing excellent fringe area TV reception where other antennas fail!

HOW IT WORKS

Antenna consists of 4 elements whose function is different on the two channels. For example: in Model 445, the elements, on channel 4, act as reflector, dipole, director, director, in that order; while on channel 5, the same elements act as reflector, reflector, dipole and director. Careful design insures proper impedance match with standard 300 ohm lead.

COMPARE THESE ADVANTAGES

- Provides gain on both channels 4 and 5 (or 7 and 9) Equal to Any Two conventional 4-element yagis!
- One bay replaces bulky stacked array!
- One lead replaces old-style 2-lead systems!
- Less weight-per-gain than any other TV antenna!
- Greatly reduced installation costs for complete TV coverage!
- Can be stacked for additional gain.

Model 445. Single or stacked Yagi for Channels 4 & 5.

Model 479. Single or stacked Yagi for Channels 7 & 9.

Model 645. "Controlled Pattern" System consisting of 2 bays offset stacked and "Phasitron." Eliminates co-channel interference. For Channels 4 & 5.

Model 679. "Controlled Pattern" System for Channels 7 & 9.

Model 304. Single Channel Yagi with Double Dipole for Channels 2 to 13.

Model 604. Same as Model 645 except for single channel operation.



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which my husband addresses the material when it slips out of the vise—as it is bound to do in a crucial moment—is denied to me, a woman.

When a woman makes a dress or a cake, she gets all the essentials together in front of her and proceeds from one step to the next to its completion. But not radio!

Take a transformer replacement for instance. You take the old one out and get the new one spaghetted and soldered ready to put in. Since it is the same thing going into the same place with the same parts you'd think you'd be all set for a nice neat job. Are you? Hah! In the first place the lugs are too darned high for the holes so you replace them. Then they don't clear the transformer properly so you have to get the hacksaw and file and do a job on that. Now you find that the screws from the old one are too big for the new transformer. You've got 8-32 and you need 6-40. All the ones in the jar are just a little too short. So off you trot for the electric drill to make the holes in the transformer bigger. Finally you get to mounting the blithering Xmfr and, bless my soul, if the screws aren't too short because of the extra washers you had to use to line it up right! So—to the jar of 6-32's. Now *they're* all too short or too long and have to be filed, *dammit!* And right here I'd like to say that *dammit* is *not* profanity on my part. It is an absolutely necessary part of every full-fledged radioman's equipment. Or his helper's.

Well, it has been an interesting experience, I must say. But I'm afraid that if my husband goes down Radio Lane hand in hand with someone it shall have to be a hand other than mine. I'm quitting while I'm still ignorant instead of insane so—Farewell, dear old radio; Farewell, disheartening struggle with obscure word meanings; Farewell, dull pity in the eyes of lab instructors; Farewell, math formula taken with two aspirins and a glass of water.

Yes, I say, farewell, dear radio, farewell to you!

And after this I guess I'd better. Just wait until His Nibs sees it!

—end—

SIMPLIFIED TV INSTALLATION

When installing a TV antenna on my home, I found it impossible to anchor the lead-in at the correct points on the outside wall. The antenna being mounted on an unused chimney, I decided to bring the transmission line down by the most direct route—straight down the chimney. The lead-in came out through a flue in the basement and was then run along the floor joists and passed through a hole directly under the TV set.

In other installations, the lead-in can be brought out of any convenient fireplace or flue not in use. This method not only simplifies installations, but it also protects the lead-in from damage by heavy ice and snow.—Geo. H. Fieldhouse

RADIO-ELECTRONICS for



THE FUND GOES OVER \$7,900.00

HELP-FREDDIE-WALK FUND

We are happy and proud to announce that the Help-Freddie-Walk Fund this month tops \$7,900.00.

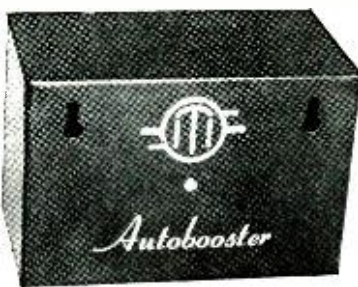
Freddie, as most of our readers know by this time, is the three-year-old son of Herschel Thomason, Arkansas radio technician, who unfortunately was born completely without the vestige of arms or legs.

We are also happy to announce that one of the large circulation magazines—*The Family Circle*—with a total circulation of over 2,500,000 copies a month—became interested in Freddie's misfortune through a reader who had seen articles in *RADIO-ELECTRONICS*. The editor of *Family Circle* magazine in turn ran a story on Freddie and asked readers to send in contributions to *RADIO-ELECTRONICS*. These contributions are now coming in in volume and during this month the total collection from this source was \$253.95. We are pleased to list these contributions here:

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A Family Circle Reader—Tacoma, Wash. ..	1.00
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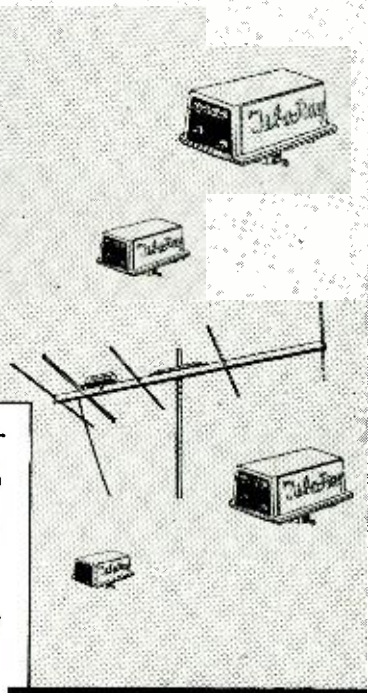
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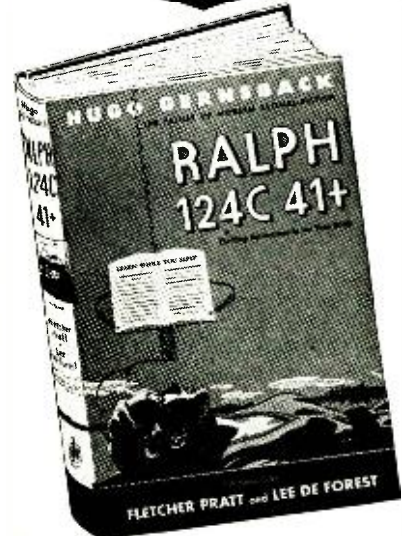
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RADIO-ELECTRONICS contributions	\$7,691.83
FAMILY CIRCLE contributions	253.95

Total received to April 19, 1951.....\$7,945.78

Please keep up your efforts in behalf of Freddie, who, when he grows up will, we all hope, become a radioman once he has been equipped with his final legs and mechanical arms.

Please send your contributions from time to time—even the smallest donation will be greatly welcome.

Make all checks, money orders, etc., payable to Herschel Thomason. Please address all letters to:

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TELEVISION ABROAD

While the TV controversies rage at home, other countries are making progress more slowly, but perhaps also more surely. In the Western Hemisphere, Cuba now has two stations on the air in Havana, and a third is expected to begin broadcasting soon. Mexico City has two stations on the air and one other is due to be in the near future. One of these is supposed to be experimenting with a color system similar to that of CBS. Mexico will also have a station soon in Tijuana and a number of other stations along the U.S. border are now in the planning stages.

Brazil has one station in Sao Paulo and another in Rio de Janeiro. Argentina, Uruguay, and several other South American countries are making plans, but have done nothing definite as yet.

Of the European countries, England is the most advanced in TV, having two stations now operating (one said to be the world's most powerful) and two others to be completed sometime this year. France has a station in Paris and another in Lille, and a third being assembled at Lyon.

The Russians are said to have two stations, one each in Moscow and Leningrad, and others on the way in other cities. Countries which are not yet on the air officially but which have been conducting experimental broadcasts are West Germany, the Netherlands, Sweden, and Italy.

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024G	.66	5Z3	.72	6HG6T	.66	7A7	.72	12SC7	.88	35L6GT	.72
1A5GT	.72	5Z4S	1.06	6J5GT	.80	7A8	.72	12SF5GT	.80	35W4	.72
1A6	1.28	6A3	1.28	6J6	1.93	7A77	1.28	12SW7GT	.80	35Z4	.72
1A7GT	.80	6A4	1.28	6J7G	.60	7A7F	.72	12SG7	.80	35Z3	.72
1B3GT	1.06	6A5G	1.56	6J8G	1.24	7A7G	.88	12SH7	.88	35Z4GT	.60
1C5GT	.88	6A7	.88	6K9GT	.66	7A77	.88	12S7GT	.72	35Z5GT	.60
1C6	1.28	6A8GT	.80	6K6GT	.65	7B4	.72	12S7GT	.72	35Z6G	1.06
1C7G	1.28	6A8	1.16	6K7G	.66	7B5	.72	12S7GT	.72	36	1.06
1D5GT	1.56	6A8S 6N5	1.06	6K7G	.66	7B7	.72	12SK7GT	.80	39/44	1.05
1D7G	1.28	6A8T	1.28	6K8	.88	7B7	.72	12SK7GT	.72	36	1.06
1D8GT	1.56	6A8SGT	1.16	6K8GT	.88	7B8	.72	12SL7GT	.96	41	.66
1F5G	1.06	6A7G	1.16	6L5G	1.06	7C4	1.28	12SN7GT	.80	42	.66
1F8	1.06	6AD7G	1.28	6L6	1.41	7C5	.72	12SO7GT	.60	43	.66
1G4GT	1.06	6AF6G	1.06	6L6G	1.41	7C6	.72	12SO7GT	.66	43	.66
1G5GT	1.06	6A5	1.06	6L6GA	1.41	7C7	1.06	12SR7GT	.88	46	1.06
1M5GT	.66	6A7	1.28	6L7	.96	7E5	.88	1223	1.06	47	.96
1M6G	1.28	6A6H	1.56	6N6G	1.16	7E6	.88	14A4	1.06	50	1.56
1J5G	1.06	6AKS	1.56	6N7GT	.96	7E7	.88	14A5	1.06	50A5	.96
1J6G	1.28	6AK6	.96	6P5GT	.96	7F7	1.06	14A7	.96	50B5	.80
1J6GT	1.28	6AL5	.80	6Q7	.80	7F8	1.06	14A7	.96	50C5	.80
1L4G	1.06	6AL7GT	1.06	6Q7GT	1.06	7G7	1.06	14AF7	.88	50C6G	1.16
1L4A	1.06	6A25	.80	6R7GT	1.06	7H7	1.06	14B8	.88	50L6GT	.66
1L4E	1.06	6A26	.72	6S4	1.28	7J7	1.06	14C5	1.06	50S5	.80
1L4F	1.06	6A27GT	.96	6S4GT	1.28	7K7	1.06	14C5	1.06	50Y6GT	.72
1L4G	1.06	6A28	.72	6S4	1.28	7L7	1.06	14E6	.88	50Y7GT	.80
1L4H	1.06	6A29	.72	6S4GT	1.28	7M7	1.06	14E7	.88	50Z6	.72
1L4I	1.06	6A30	.72	6S4GT	1.28	7N7	1.06	14E8	.88	50Z7GT	.80
1L4J	1.06	6A31	.72	6S4GT	1.28	7P7	1.06	14F7	.88	51	.72
1L4K	1.06	6A32	.72	6S4GT	1.28	7Q7	1.06	14F8	.88	51	.80
1L4L	1.06	6A33	.72	6S4GT	1.28	7R7	1.06	14F9	.88	51	.80
1L4M	1.06	6A34	.72	6S4GT	1.28	7S7	1.06	14G7	.88	51	.80
1L4N	1.06	6A35	.72	6S4GT	1.28	7T7	1.06	14H7	.88	51	.80
1L4O	1.06	6A36	.72	6S4GT	1.28	7U7	1.06	14I7	.88	51	.80
1L4P	1.06	6A37	.72	6S4GT	1.28	7V7	1.06	14J7	.88	51	.80
1L4Q	1.06	6A38	.72	6S4GT	1.28	7W7	1.06	14K7	.88	51	.80
1L4R	1.06	6A39	.72	6S4GT	1.28	7X6	1.06	14L7	.88	51	.80
1L4S	1.06	6A40	.72	6S4GT	1.28	7X7	1.06	14M7	.88	51	.80
1L4T	1.06	6A41	.72	6S4GT	1.28	7Y7	1.06	14N7	.88	51	.80
1L4U	1.06	6A42	.72	6S4GT	1.28	7Z6	1.06	14O7	.88	51	.80
1L4V	1.06	6A43	.72	6S4GT	1.28	7Z7	1.06	14P7	.88	51	.80
1L4W	1.06	6A44	.72	6S4GT	1.28	7Z8	1.06	14Q7	.88	51	.80
1L4X	1.06	6A45	.72	6S4GT	1.28	7Z9	1.06	14R7	.88	51	.80
1L4Y	1.06	6A46	.72	6S4GT	1.28	7Z0	1.06	14S7	.88	51	.80
1L4Z	1.06	6A47	.72	6S4GT	1.28	7Z1	1.06	14T7	.88	51	.80
1L5A	1.06	6A48	.72	6S4GT	1.28	7Z2	1.06	14U7	.88	51	.80
1L5B	1.06	6A49	.72	6S4GT	1.28	7Z3	1.06	14V7	.88	51	.80
1L5C	1.06	6A50	.72	6S4GT	1.28	7Z4	1.06	14W7	.88	51	.80
1L5D	1.06	6A51	.72	6S4GT	1.28	7Z5	1.06	14X7	.88	51	.80
1L5E	1.06	6A52	.72	6S4GT	1.28	7Z6	1.06	14Y7	.88	51	.80
1L5F	1.06	6A53	.72	6S4GT	1.28	7Z7	1.06	14Z7	.88	51	.80
1L5G	1.06	6A54	.72	6S4GT	1.28	7Z8	1.06	15A7	.88	51	.80
1L5H	1.06	6A55	.72	6S4GT	1.28	7Z9	1.06	15B7	.88	51	.80
1L5I	1.06	6A56	.72	6S4GT	1.28	7Z0	1.06	15C7	.88	51	.80
1L5J	1.06	6A57	.72	6S4GT	1.28	7Z1	1.06	15D7	.88	51	.80
1L5K	1.06	6A58	.72	6S4GT	1.28	7Z2	1.06	15E7	.88	51	.80
1L5L	1.06	6A59	.72	6S4GT	1.28	7Z3	1.06	15F7	.88	51	.80
1L5M	1.06	6A60	.72	6S4GT	1.28	7Z4	1.06	15G7	.88	51	.80
1L5N	1.06	6A61	.72	6S4GT	1.28	7Z5	1.06	15H7	.88	51	.80
1L5O	1.06	6A62	.72	6S4GT	1.28	7Z6	1.06	15I7	.88	51	.80
1L5P	1.06	6A63	.72	6S4GT	1.28	7Z7	1.06	15J7	.88	51	.80
1L5Q	1.06	6A64	.72	6S4GT	1.28	7Z8	1.06	15K7	.88	51	.80
1L5R	1.06	6A65	.72	6S4GT	1.28	7Z9	1.06	15L7	.88	51	.80
1L5S	1.06	6A66	.72	6S4GT	1.28	7Z0	1.06	15M7	.88	51	.80
1L5T	1.06	6A67	.72	6S4GT	1.28	7Z1	1.06	15N7	.88	51	.80
1L5U	1.06	6A68	.72	6S4GT	1.28	7Z2	1.06	15O7	.88	51	.80
1L5V	1.06	6A69	.72	6S4GT	1.28	7Z3	1.06	15P7	.88	51	.80
1L5W	1.06	6A70	.72	6S4GT	1.28	7Z4	1.06	15Q7	.88	51	.80
1L5X	1.06	6A71	.72	6S4GT	1.28	7Z5	1.06	15R7	.88	51	.80
1L5Y	1.06	6A72	.72	6S4GT	1.28	7Z6	1.06	15S7	.88	51	.80
1L5Z	1.06	6A73	.72	6S4GT	1.28	7Z7	1.06	15T7	.88	51	.80
1L6A	1.06	6A74	.72	6S4GT	1.28	7Z8	1.06	15U7	.88	51	.80
1L6B	1.06	6A75	.72	6S4GT	1.28	7Z9	1.06	15V7	.88	51	.80
1L6C	1.06	6A76	.72	6S4GT	1.28	7Z0	1.06	15W7	.88	51	.80
1L6D	1.06	6A77	.72	6S4GT	1.28	7Z1	1.06	15X7	.88	51	.80
1L6E	1.06	6A78	.72	6S4GT	1.28	7Z2	1.06	15Y7	.88	51	.80
1L6F	1.06	6A79	.72	6S4GT	1.28	7Z3	1.06	15Z7	.88	51	.80
1L6G	1.06	6A80	.72	6S4GT	1.28	7Z4	1.06	16A7	.88	51	.80
1L6H	1.06	6A81	.72	6S4GT	1.28	7Z5	1.06	16B7	.88	51	.80
1L6I	1.06	6A82	.72	6S4GT	1.28	7Z6	1.06	16C7	.88	51	.80
1L6J	1.06	6A83	.72	6S4GT	1.28	7Z7	1.06	16D7	.88	51	.80
1L6K	1.06	6A84	.72	6S4GT	1.28	7Z8	1.06	16E7	.88	51	.80
1L6L	1.06	6A85	.72	6S4GT	1.28	7Z9	1.06	16F7	.88	51	.80
1L6M	1.06	6A86	.72	6S4GT	1.28	7Z0	1.06	16G7	.88	51	.80
1L6N	1.06	6A87	.72	6S4GT	1.28	7Z1	1.06	16H7	.88	51	.80
1L6O	1.06	6A88	.72	6S4GT	1.28	7Z2	1.06	16I7	.88	51	.80
1L6P	1.06	6A89	.72	6S4GT	1.28	7Z3	1.06	16J7	.88	51	.80
1L6Q	1.06	6A90	.72	6S4GT	1.28	7Z4	1.06	16K7	.88	51	.80
1L6R	1.06	6A91	.72	6S4GT	1.28	7Z5	1.06	16L7	.88	51	.80
1L6S	1.06	6A92	.72	6S4GT	1.28	7Z6	1.06	16M7	.88	51	.80
1L6T	1.06	6A93	.72	6S4GT	1.28	7Z7	1.06	16N7	.88	51	.80
1L6U	1.06	6A94	.72	6S4GT	1.28	7Z8	1.06	16O7	.88	51	.80
1L6V	1.06	6A95	.72	6S4GT	1.28	7Z9	1.06	16P7	.88	51	.80
1L6W	1.06	6A96	.72	6S4GT	1.28	7Z0	1.06				

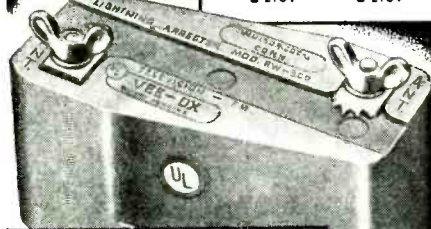
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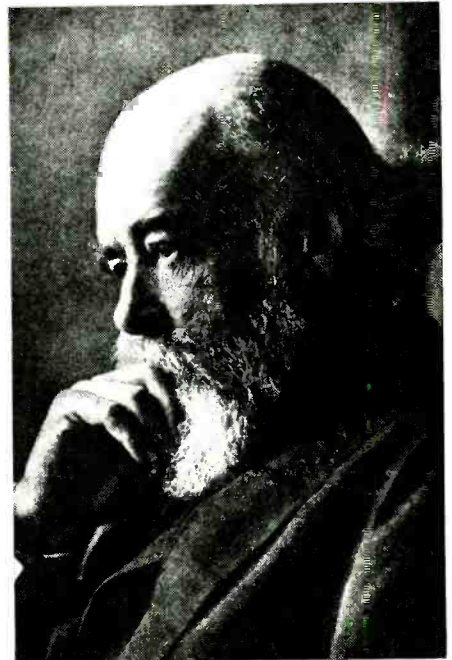
June 12, 1951 is the 100th anniversary of the birth of that great figure of wireless, Sir Oliver Lodge.

Not of a wealthy family, he received only a grammar-school education, but he continued his education by dint of night study, first in chemistry, then in general physics, and finally as a matriculated student in the University of London, and in 1875 obtained a Bachelor of Science degree, with honors in physics. Appointed demonstrator of physics at University College, Liverpool, he immediately began to publish papers on the flow of electricity and to devise apparatus to explain conductors, dielectrics, and insulators in mechanical terms.

His most important work was in connection with tuning. As early as 1894 he demonstrated that some electrical circuits when excited would continue in electrical vibration a long time, while others would be "rapidly damped," and declared that circuits which vibrated persistently would receive only radio waves whose frequencies were near their own natural periods. In 1898 he applied for a patent on a "syntonic" or tuned receiving circuit. Although both Tesla and Marconi devised tuned circuits during the same period—possibly independently of Lodge—it was Lodge's authority and influence that established the value of tuning.

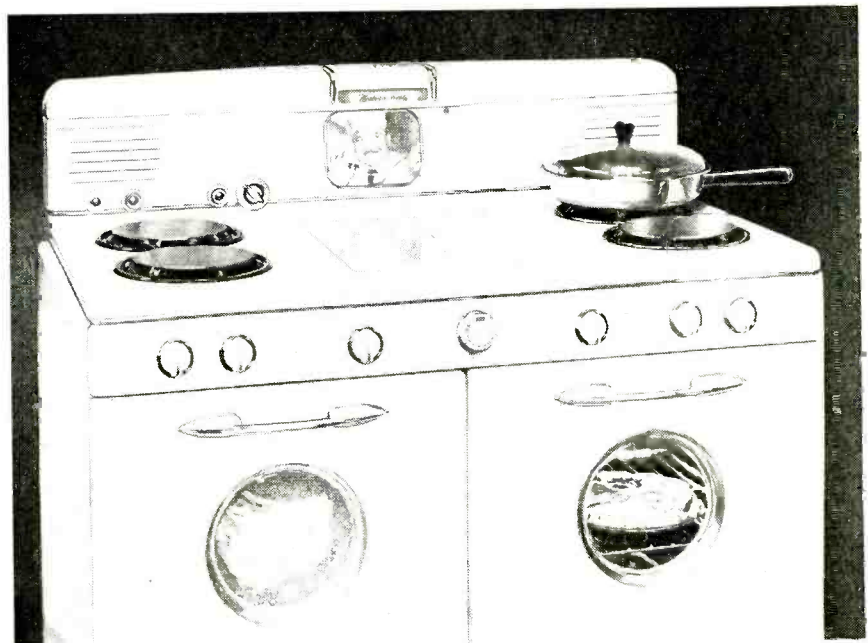
Although Lodge constructed many pieces of equipment to demonstrate radio waves and "syntony," he never became interested in wireless as a means of communication. However, his work was well known, and many scientists of the period considered him the real father of wireless. Foremost among

them was Professor Sylvanus Thompson, who in letters to the press denounced the young Marconi bitterly as a usurper attempting to steal the credit rightfully due to Lodge.



In later years Sir Oliver turned to other interests—including exploration of the occult—but maintained close connections with radio till after the beginning of broadcasting. He contributed several articles on the design of tuning inductors to the American magazine *Popular Radio* as late as the mid-20's. He died in 1940.

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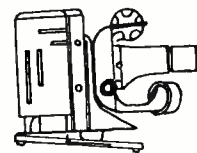
Any person about to enter military service who has experience in communications, electronics, or photography is advised by the Army to bring with him all available credentials such as radio amateur licenses and union cards, to demonstrate his skill in these fields. Technically trained inductees are being assigned to Army jobs in keeping with their skills wherever possible, particularly in the electronics and communications fields where there is a critical shortage of trained personnel. Inductees should also obtain statements of experience from their employers or unions. Forms for such statements may be obtained from the Signal Corps.

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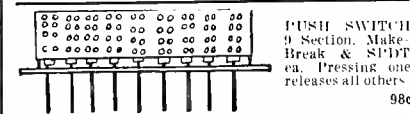
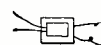
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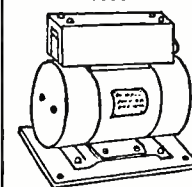


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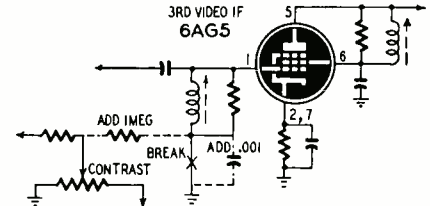
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61

CROSLY LD MODELS

The LD models such as the 9-419-M1LD, 9-409M3LD, and others are designed especially for fringe-area reception. When these sets are operated in areas where one or more stations are exceptionally strong, the contrast and vertical sync controls may be critical and the sound output weak. These conditions may be corrected by adding variable bias to the third video i.f. stage. With this added circuit, the gain of the video i.f. stage can be adjusted for best results with either a strong or a weak signal.

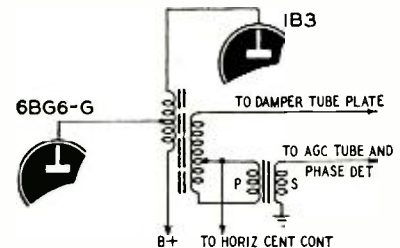


Disconnect the third i.f. grid coil from ground. Connect a .001- μ f capacitor (part No. 160034) between the low side of the grid coil and ground. Connect a 1-megohm resistor (part No. 39374-61) between the low side of the third i.f. grid coil and the arm of the contrast control. The pertinent parts of the circuit are shown in the diagram. The resistor and capacitor which are added are shown in dashed lines.

If the picture brightness fluctuates with line-voltage changes, disconnect the 470,000-ohm picture-tube grid resistor from the cathode of the 6AL5 d.c. restorer and connect it to the chassis.—Crosley Service Dept.

STROMBERG-CARLSON TV SETS

Loss of horizontal sync in the TC-19, TC-125, and similar models is most often caused by an open primary on the a.g.c. pulse coil. This coil is connected



across a section of the secondary of the flyback transformer as shown in the diagram. Disconnect one side of this coil from the flyback transformer before checking continuity.—W. R. Worrell

BUICK RADIO 980798

We have received numerous complaints stating that the fuses blow when operating this and similar models. Since thorough investigations have not revealed a specific cause, we have replaced the original 15-ampere fuses with 20- or 30-ampere units.

We mention this because we know that some technicians will not violate manufacturers' recommendations. In this instance the trouble cannot be cured to the customers' satisfaction without a heavier fuse.—Adams Radio Service

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CROSLY 10-102E, 10-103, 10-104W
In later sets, capacitor C7 is connected between pins 1 and 7 of the 50C5 output tube instead of across the primary of the output transformer. This change improves the stability of the receiver noticeably. — *Crosley Service Department*

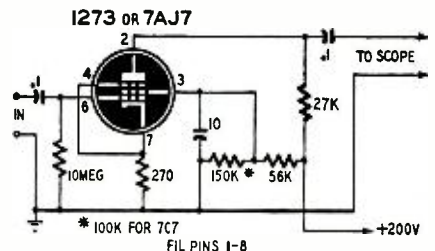
STRIPPED SCREW HOLES

Some sets have backs fastened to the cabinet with wood screws. The screw holes are usually stripped after the back has been removed and replaced a few times. A good remedy for stripped wood-screw holes is to slip a piece of small-diameter rosin-core solder into the hole and replace the original screw in the ordinary manner.

This will in most cases hold more securely than the original hole and will eliminate the possibility of splitting the wood with a larger screw. — *Westinghouse Service Hints*

SCOPE PREAMPLIFIER

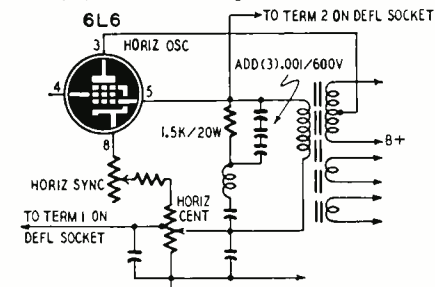
Although it was designed for use with Sylvania 131 and 132 oscilloscopes, experimenters and service technicians will find this preamplifier a useful addition to conventional scopes of almost any make. Having a gain of approximately 30, it makes many traces viewable which do not show up well on



the scope alone. The frequency response is $\pm 10\%$ from 10 cycles to 70 kc (1,000 cycles reference), down not more than 15% at 90 kc or 25% at 145 kc. The 1273 is a nonmicrophonic pentode having physical and electrical characteristics of the 7AJ7. A 7AJ7 or 7C7 may be used. The 150,000-ohm resistor must be changed to 100,000 ohms when the 7C7 is used. — *Sylvania News*

FARNSWORTH GV-260

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across the 1,500-ohm, 20-watt resistor connected to the grid of the 6L6 horizontal oscillator tube. This change increases the width enough to spread both sides beyond the edges of the mask. — *Frank Jusaites*

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Starting with the 50-T1400 series, code 125 TV receivers, a blocking-type horizontal oscillator with a stabilizing section is used in all sets. When this oscillator is improperly adjusted a shrill sound of approximately 1,000 cycles may be heard and the picture will lose sync. This condition—called gunboating—is the result of double firing of the horizontal oscillator. It usually occurs when the horizontal hold control is in the extreme clockwise or counterclockwise position.



To prevent this trouble, turn the horizontal hold control *fully clockwise*, then adjust the horizontal frequency control (in the core of the transformer) to obtain five blanking bars sloping to the right. If gunboating is still apparent, rotate the *hold control* in the opposite direction then return it to the extreme clockwise position. Try resetting the frequency control on the blocking transformer.

In areas having moderately strong noise-free signals, the tendency to gunboat is reduced by adjusting the stabilizing core in the horizontal blocking transformer so the top of the rounded portion of the oscillator waveform is below the narrow pointed peak as shown at *a* in the diagram. The drawing at *b* shows the waveform which should be obtained when the oscillator circuit is adjusted for reception in weak- or noisy-signal areas. These waveforms are viewed by connecting a scope to pin No. 3 of the horizontal test jack (J600 on most diagrams).—Philco Serviceman

CROSLEY MODEL 10-421MU

An 18,000-ohm, 1/2-watt resistor R210 has been connected in parallel with the 18,000-ohm resistor R197 to increase the horizontal drive in some sets. This may produce excessive horizontal drive when the sets are used in some areas. When this condition is experienced, remove R210.—Crosley Service Instructions

PHILCO 925, 926

Sets which are intermittent or dead on FM sometimes can be repaired with little or no trouble. Check the bottom lug on the oscillator stator plates. In several of these sets, the lug was found to be shorted to the frame of the capacitor by a small blob of solder. This can be cleared up by bending the lug or by removing the excess solder with a hot iron.—Milton Margolis

EMERSON 600 AND 639

Hum in the audio is usually caused by misalignment of the sound trap in the second video amplifier circuit. Adjust this trap to remedy the trouble.—William Porter

—end—

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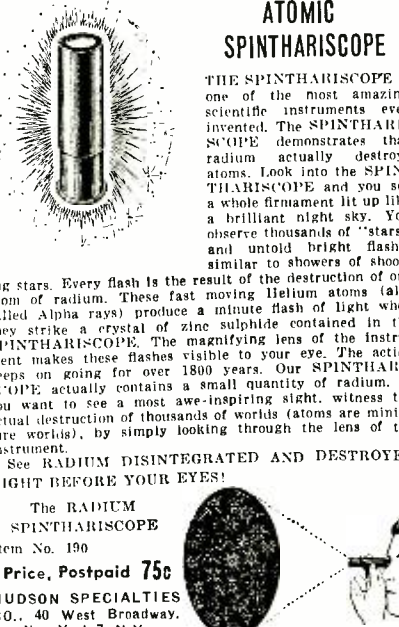
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Charles E. Krampf was elected executive vice-president of the AEROVOX CORPORATION. He succeeds Bert Conway, who resigned as executive vice-president, but will remain as a consultant and as a member of the board of directors. Mr. Krampf will continue as president of the Electrical Reactance Corporation, ceramic division of Aerovox.



C. E. KRAMPF

W. Myron Owen was re-elected president and treasurer, and J. Fraser Cocks as comptroller and clerk. The company also announced the re-election of W. Myron Owen, Herbert W. Marache, Donald E. Nichols, John Cronin, and H. Lynn Pierson as directors. Charles L. Cade joined SARKES TARZIAN, Inc. as director of distributor sales. His appointment marks the availability of the entire Tarzian line to the replacement market. Previously all the company's products except selenium rectifiers were sold only to television set manufacturers.

Stanley F. Patten, U. S. N. (Ret.), was named director of mobilization

planning for the Government Department of ALLEN B. DU MONT LABORATORIES. He has been assistant to Dr. Du Mont since July, 1947. The company also assigned Ernest A. Marx, manager of the TV Receiver Sales Division, to additional duties as manager of the Government Department. Other appointments to the Du Mont Government Department include H. B. Graham, head of negotiations and bids; Z. Soucek, manager of the Washington office; B. V. K. French, manager of the Dayton office; Edgar H. Felix and William C. Lupfer, contract administrators, and T. G. Rogers, administrative assistant to Mr. Cramer, vice-president.



S. F. PATTEN

Frank J. Stroempel was named executive assistant to M. S. (Mike) Roth, jobber sales manager of the RADIART CORPORATION. D. W. Gunn and G. V. Bureau were named equipment sales manager and government sales manager, respectively, of the Radio and TV Tube Divisions of PENNSYLVANIA ELECTRIC PRODUCTS, INC. George F. Sandore, formerly district manager of the Atlanta area, was named manager of the newly created Sales and Merchandising Section of the Technical Products Division of the RCA SERVICE CO. Carl E. Johnson, former manager of the Theater Service Section, was named manager of District Operations. Adolph Goodman, former manager of the District Sales Section, became manager of the Commercial Operations, and C. L. Swinney, former supervisor of the Atlanta district, was appointed manager of the district.

—end—

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377	425	461	491	518	396	454
379	425	462	492	519	397	455
380	427	468	493	520	398	456
381	429	469	494	522	400	457
383	430	470	495	523	401	463
384	431	472	496	525	402	465
385	433	473	497	526	403	488
386	434	474	498	527	404	500
387	435	475	503	529	405	501
388	436	476	504	530	406	538
412	437	477	505	531	407	540
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CONTAMINATED GRID

Dear Editor:

On page 92 of your March issue, S. W. Hou describes a very ancient trouble with multigrad output tubes. I first ran into this some 20 years ago with a few type 47 tubes, and since then have seen it in nearly every type of screen-grid output tube. The 50L6-GT is perhaps the worst offender.

This trouble is not leakage in the usual sense between grid and screen. The grid has become contaminated with some of the emitting material from the cathode, and after a thorough warmup emits electrons. Since the control grid is the most negative element in the tube, this emission will go to any of the other electrodes. As the screen is positive and very close to the control grid, most of the emission goes there and appears the same as leakage. This is only one-way leakage and gives no indication if the d.c. test voltage is polarized so that the control grid is positive and the screen negative.

The distortion noticed by Mr. Hou is due to this emission current flowing through the grid resistor in such a direction as to reduce the negative bias between grid and cathode. The higher the grid resistance, the greater this effect; thus shunting the grid resistor with 50,000 ohms reduces distortion.

Do not throw away such 50L6-GT's. Though they cannot be used again as output tubes, except perhaps in transformer-coupled amplifiers, I used them during the last war as a substitute for 35Z5-GT's and other rectifiers. The 35Z5-GT usually has pins 3 and 5 connected on the socket. One side of the a.c. line connects to pin 2 and the dial light is between pins 2 and 3. The 50L6-GT can be used here by connecting pins 2, 3, 4, and 5, either on the socket or on the pins at the base of the tube. Be sure that pin 4 on the socket does not have other connections; if it does, remove them. If jumpers are put on the tube base, a 35Z5-GT can be put back in the socket when available without any wiring changes.

I cannot bring this letter to a close without telling you that for a great many years I have been a reader of your magazines and in that time have gotten a great deal of pleasure and good from them.

W. L. JOHNSTON

Arlington, Texas

5-TUBE POCKET SUPER

It was necessary to withdraw the article "5-Tube Pocket Super" from the May issue at the last moment, due to a problem which had to be solved by correspondence with the author. The story is again being readied for an early issue, and will probably appear in July or August. Our sincere apologies to those miniature fans whose hopes were aroused by the announcement on our May cover.

—end—

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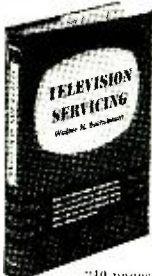
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F-M SIMPLIFIED (Second Edition), by Milton S. Kiver. Published by D. Van Nostrand Co., New York, N. Y. 5 3/4 x 8 1/2 inches, 458 pages. Price \$6.50.

This latest edition is a complete revision of a popular work which has been widely used as an elementary textbook on FM theory and practice. It has been rewritten, 111 additional pages of text and illustrations have been added, and the material has been rearranged so the various discussions fall into a more logical sequence.

Like the first edition, this book serves to bridge the gap between AM and FM techniques. It explains fully and in simple language the theory of FM propagation and FM receiver and transmitter circuits. Several chapters are devoted to detailed descriptions of circuits in commercial FM receivers and methods of servicing them.—RFS

TELEVISION AND FM ANTENNA GUIDE, by Edward M. Noll and Matthew Mandl. Published by The Macmillan Co., 60 Fifth Avenue, New York, N. Y. 6 1/2 x 9 1/2 inches, 311 pages. Price \$5.50.

The performance of many TV and FM sets—particularly in weak-signal and fringe areas—depends directly on the type of antenna and its installation and orientation. If the installation crew lacks a thorough understanding of v.h.f. antenna theory, the performance of the set is likely to be unsatisfactory.

Messrs. Noll and Mandl, authors of a series of articles on TV antennas in RADIO-ELECTRONICS, have prepared this book to enable the TV and FM installation man to get the most out of any set in a given location.

After devoting the opening chapter to discussions of radio propagation, the authors get down to cases and devote the balance of the book to practical design data, specifications, and characteristics of basic antenna types. Drawings and photographs are used to illustrate the antenna under discussion. In round-

ing out the book into a guide or handbook on antennas for TV and FM reception, the authors cover transmission lines, interference elimination, commercial boosters, and general installation hints.—RFS

RADIO AND TELEVISION RECEIVER CIRCUITRY AND OPERATION, by Alfred A. Ghirardi and J. Richard Johnson. Published by Rinehart Books, Inc., New York, N. Y. 6 1/2 x 9 inches, 669 pages. Price \$6.00.

The modern service technician must be thoroughly familiar with the basic circuits of both aural and visual receivers if he wants to stay in business long. This book is intended to provide just that familiarity. It is a text for technical schools or for the practicing technician who needs a home refresher course.

It differs from most textbooks by being clear and concise. What is perhaps more important, it covers those many little practical details (such as how to check for filament continuity in a.c.-d.c. sets and how push-button tuning mechanisms operate) so often omitted in textbooks.

All types of home receiving equipment are covered. Each chapter concludes with a summary of the high points, a set of questions, and problems.

SURVEY OF MODERN ELECTRONICS, by Paul G. Andres. Published by John Wiley & Sons, Inc., New York, N. Y. 5 1/2 x 8 1/2 inches, 522 pages. Price \$5.75.

A one-volume treatment of the vast field of modern electronics naturally can cover only the highlights. But that is exactly what Professor Andres intends with this book, which was written for a short course in electronics to show beginning engineering students what they are getting into. It demonstrates the vital importance of electronics to nearly all branches of science and engineering.

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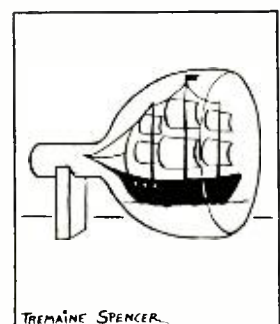
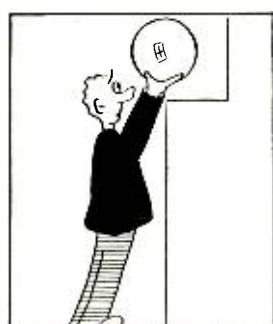
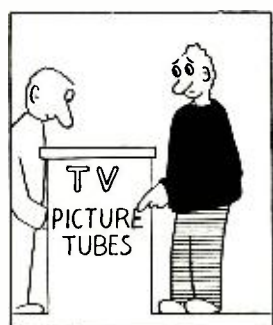
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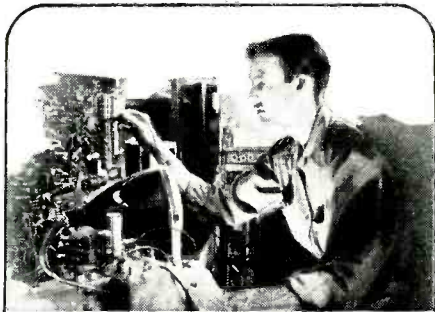
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SERVICING RADIO AND TELEVISION WITH A VACUUM TUBE VOLTMETER, Published by Sylvania Electric Products Inc., 1740 Broadway, New York 19, N. Y. 8 1/2 x 11 inches, 48 pages. Price \$1.00.

The text of this booklet was prepared by Rufus P. Turner, a writer well known to readers of this magazine. He discusses the various types of v.t.v.m.'s, and—in a chapter each—their use in radio receiver tests, audio amplifier measurements, television receiver tests, and miscellaneous applications. The booklet is attractively printed and well illustrated.

UNDERSTANDING RADIO (Second Edition), by Herbert M. Watson, Herbert L. Welch, and George S. Eby. Published by McGraw-Hill Book Co., New York, N. Y. 6 1/2 x 9 1/4 inches, 716 pages. Price \$5.50.

Understanding Radio is a simple but thorough home-study type text and workbook for those with little or no knowledge of radio. Fundamentals of radio receiver and transmitter theory are introduced one-by-one in a logical sequence. New technical terms and theories are introduced gradually so there is no sharp transition from one thought to another. Over 500 drawings, diagrams, and photographs are used to illustrate the text.

A number of simple radio and electrical experiments which enable the

reader to learn by doing are described. The experimental setups which can be used to study vacuum-tube circuits and to construct amplifiers, receivers and transmitters are described in detail. The more advanced experiments are performed by combining circuits constructed in earlier lessons.

MAKING MONEY IN TELEVISION SERVICING, by Eugene Ecklund. Published by Howard W. Sams & Co., 2201 East 46th St., Indianapolis, Indiana. 5 1/2 x 8 1/2 inches, 136 pages. Price \$1.25.

The author, himself successful in the television service business, points out that the problems of the new industry had to be answered largely by guesswork, but that a previous grounding in business methods helped in guessing right. Having learned many of the answers through three years of actual experience, he now shares them with the rest of the television servicing fraternity.

The book begins with planning and establishing the new business, and while covering such standard subjects as location, overhead, collections, and advertising, brings in a few subjects not always covered in such a book. Thus, expansion, work control, and the problems of busy and slack seasons are discussed in the light of the special features of the television service business. Obviously, actual installation and service problems

do not belong in such a book, but forms for installation and servicing and hints on reporting trouble are included.

DUNLAP'S RADIO AND TELEVISION ALMANAC, by Orrin E. Dunlap, Jr. Published by Harper & Brothers, 49 East 53rd St., New York 16, N. Y. 5 1/4 x 8 1/2 inches, 211 pages. Price \$4.00.

A complete chronology of radio from 640 B.C. to November, 1950 A.D., this book is a handy reference for student, writer, or any person who may have to know who did what, and when, in the radio field. Divided into sections, or eras, with a short introduction to each, it becomes an interesting work for the general radio reader as well.

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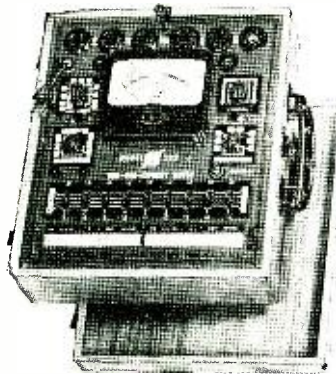
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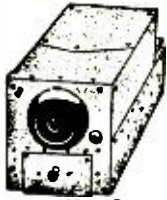
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The electronic equipment that saved many lives in the war. Set can be modified to use for 2-way communication, voice or code, on following bands: ham band 420-450 mc, citizens radio 460-470 mc, fixed and mobile 450-460 mc, television experimental 470-500 mc. 15 tubes (tubes alone worth more than sale price!) : 4—7F7, 4—7H7, 2—7E6, 2—6F6, 2—955 and 1—WE316A. Now covers 460 to 490 mc. Brand new BC-645 with tubes, less power supply in factory carton. Shipping weight 25 lbs.

PE-101C DYNAMOTOR for above BC-645 \$3.95

UHF ANTENNA ASSY. for above BC-645 \$2.45

**SETCHEL-CARLSON
Beacon Radio Receiver
BC-1206-C**

Receives A-N beam signals, operates on 21-28 V DC, 5 Tubes; 3—11H7, 1-1R7, 2-8D7. Tubes 195 to 120 Kc. Size 4"x4"x6" wide, 4 lbs. In original carton.



New \$9.95

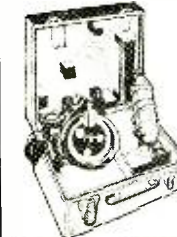
Used \$7.95



**11-TUBE SUPERHET RECEIVER
Model BC-652-A—2000 to 6000 KC
(75-80 Meters) BRAND NEW IN ORIGINAL CRATE
SMASHING LOW PRICE**

Complete with Crystal Tubes and Dynamotor. For those of you "salties" in need of a good radio receiver aboard ship, the Model BC-652-A made by General Electric Co., will fill your needs! It is a rugged, good performing receiver which will give fine service for a long long time. This set is designed for 12/24 volt DC operation, which is ideal for shipboard use. It needs absolutely no conversion, just connect it into your batteries. Technically this set is an 11-tube superhet receiver with a freq range of 2000 to 6000 Kc (75-80 meter ham bands), a crystal freq standard, and a 12/24 volt dynamotor, on two chassis combined into one case. The sensitivity is one microvolt or greater.

\$49.50



**TERRIFIC VALUE
BUBBLE SEXTANT**

Actually worth \$100 or more! Has illuminated averaging disc for nighttime use. Complete with carrying case, recording discs, flash light with rheostat for using sextant at night, 2X telescope for faint stars, and Allen **\$15.45** wrench. Only **\$15.45** Complete

OIL FILLED CONDENSERS

2-mfd.—1000V	99c
4-mfd.—800V	1.25
4 x 4 mfd.—400V	1.05
3 x 3 mfd.—600V	1.10
2.5 mfd.—300V	89c

TRANSMITTING COND.

02 mfd.—10,000V	3.25
-----------------	------

FULL WAVE SELENIUM RECTIFIER

110V at 150 mil's **\$1.19**

- JK-26 and 11-541 JAK & PLG combination, for headset extension, etc. Pair **35c**
- PL-50—Standard 2-circ. phone plug, fits all phone jacks. Each **29c**
- PL-68—Standard 3-circ. mike plug, fits all 3-way mike jacks. Each **22c**

GE THYRATRON FG-105



Brand New MERCURY RECTIFIER
Individually boxed in factory sealed cartons. 1st Price \$60.00. Your cost **\$18.95** each
While They Last!
For continuous rectifier and welder control service. Tetrode type, indirectly heated cathode; 10000 V peak, 10000 V peak inverse. Av. Max. current 6.1 amps continuous, 2.4 to 4 amps welder control service.

SAVE ON THESE STANDARD TUBES

1HSGT	1.12	6L6G	1.65	12S17	.95
1LA4	1.45	6Q7	.75	12SK7	1.35
1LB4	1.45	6S17	1.25	12SL7	1.10
1LC5	1.45	6SC7	1.20	12SN7	1.75
1LD5	1.45	6SF5GT	1.10	12SQ7	1.25
1LE3	1.45	6SK7	.95	12SR7	.90
1LH4	1.45	6SG7	.95	12Z3	.85
1LN5	1.35	6SJ7	1.20	14A7	1.05
1LQ5	1.55	6SK7	.95	14E7	1.05
1LH4	1.45	6SL7GT	1.35	14F8	1.35
1LN5	1.35	6SN7GT	1.65	14F7	1.20
1LQ5	1.20	6S7	.95	14J7	1.35
1RS	1.20	6T8	2.20	14N7	1.10
1LQ5	1.20	6V6GT	.95	14N7	1.35
1S5	1.00	6W4	1.50	14R7	1.25
1T4	1.10	6X5GT	1.30	19	.49
1S4GT	1.25	6Y6G	1.25	2A4	.80
1U4	1.10	7A4	2.20	25L6	.90
1V	.90	7A5	1.20	25Z6	.85
1A3	1.45	7A6	1.20	25Z6GT	1.10
2A5	1.15	7A6	1.20	26	.59
2A6	.95	7A7	1.20	27	.65
2A7	.95	7A8	1.20	28D7	1.35
2B7	.95	7B4	1.20	30	.75
2X2A	.88	7B5	1.20	31	.55
30SGT	1.10	7B6	1.20	32	.55
3A4	1.05	7C7	1.20	33	.59
3V4	1.05	7B8	1.20	34	1.20
5T4	1.70	7C4	1.20	35	51
6AG	1.20	7C5	1.25	35A5	.90
5V4G	1.85	7C6	1.25	35B5	1.25
5W4	.95	7C7	1.10	35C5	1.25
5X4G	1.10	7E6	1.10	35L6GT	1.25
5Y3GT	1.00	7F7	1.10	35W4	1.05
5Y4G	.85	7F7	1.00	35Z4	.88
5Z4	.95	7H7	1.10	35Z4	.75
5Z4	1.20	7H7	1.75	35Z5	1.20
6A3	1.35	7K7	1.30	35Z5	.65
6A6	1.25	7L7	1.30	35Z5	.65
6A7	1.15	7M7	1.65	37	.65
6A8	1.10	7N7	1.10	38	.65
6A8	1.10	7P7	1.10	38	.44
6A8SGT	1.30	7P7	1.10	40	.44
6A7	1.90	7Y4	.90	41	.75
6AG5	1.90	117L7 M7	.70	42	.82
6A6	2.50	117L7	1.70	43	.82
6A15	1.65	117N7	1.70	45	.75
6A15	2.60	117P7	1.70	46	.75
6A16	1.90	12A6	1.25	56	.70
6A15	1.65	117Z6	1.40	48	2.75
6A17	1.95	12A	.85	49	1.25
6A6	1.75	12A6	1.30	50A5	1.40
6A7E	1.30	12ARGT	.95	50B5	1.40
6A6	1.70	12AH7GT	.95	50C5	.95
6A6	1.30	12A7G	1.30	50L6GT	1.25
6B4E	1.50	12A76	1.30	50Y6	1.05
6B6E	1.50	12A77	2.25	53	1.25
6BG6	2.20	12A86	1.25	56	.70
6BH6	1.75	12A97	1.95	57	.85
6C4	1.10	12AV6	1.30	58	.85
6C6	1.85	12AW6	1.30	59	1.75
6D6	.85	12BA6	1.45	70L7	1.65
6E5	1.00	12BE6	1.55	71A	.90
6F5	.80	12J7	.80	75	.75
6F6	1.20	12K7	1.05	76	.75
6F6GT	1.00	12K8	1.60	77	.75
6J5	.75	12L7	.85	78	.75
6J6	1.85	12O7	.85	80	1.05
6J7GT	1.25	12S7	1.10	82	1.25
6K7	.85	12S7	1.00	83	1.35
6K8	1.15	12SC7	.90	84	1.35
6L6	1.95	12S7	.95	85	1.05

183 1.40

**DC AMMETER
0-15 Amps**

A terrific buy! 3 1/2" easy reading scale, 15 divisions. Black plastic case. 1 1/2" x 5 1/4" x 2 3/8". Rubber covered test clip leads plus black metal carrying case with hinged cover. Brand new. Wonderful for automotive, battery charging, general test work. Value \$25. All yours for **\$5.25** only



SELSYN 2J1G1
Operates from 5 1/2 V 100 cycles. Suggested wiring for 110 V 60 cycle included. New, tested. Price per pair **\$4.50**



BC 605 INTERPHONE AMPLIFIER
Easily converted to an ideal intercommunications set for office—home—or factory. Complete w/conversion diagram for 110V operation. BRAND NEW **\$4.95**

Please include 25% Deposit with order—Balance C.O.D. MINIMUM ORDER \$3.00. All Shipments F.O.B. Our Warehouse N.Y.C.

G&G RADIO PARTS SERVICE
53 WESEY STREET · NEW YORK 7, N.Y.

**TERRIFIC VALUE
24-VOLT STORAGE
BATTERY, BRAND NEW
17 AMP. HRS.**

Made by Delco. 12 cells heavy duty, very rugged. Shipped dry, uses standard sulphuric acid electrolyte.



VERY SPECIAL \$17.95



6-VOLT STORAGE BATTERY
Navy Standard BRAND NEW. 15 ampere-hour rating **\$7.95**

ASTATIC R-3 CRYSTAL HANDMIKE
with 6-ft. R. C. Mike Cable **\$5.95**

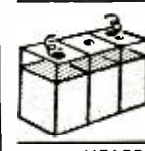


ONE-QUART BOTTLE BATTERY ELECTROLYTE
Made by Willard, for above storage batteries. 1 quart sufficient for 2-volt cells. Hermetically sealed. SPECIAL. Hermetically sealed. per qt. bottle **\$1.45**

7-PRONG 2-VOLT RADIO VIBRATOR
for Portable and Farm Sets Replacement for GE LB 530 **\$1.95**



WILLARD 2-VOLT STORAGE BATTERY
20 Ampere-Hours
Exact replacement for GE portables for LB-500—BRAND NEW. Each **\$2.69**

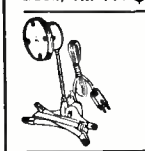


WILLARD MIDGET 6-V STORAGE BATTERY
3 amp hour rating. Transparent plastic case. Brand new. 3 3/8" x 1 3/16" x 2 3/8" high. Uses standard electrolyte. Each **\$2.65**

HEADPHONES—All Brand New!
Individually packed, complete with phone plug.
HS-33 600 ohms, in lots of 3 **3.95** each
HS-23 2000 ohms, in lots of 3 **3.25** each
HS-30 With earplugs, LOTS OF 12 **1.65** each

**U. S. Army
Field Phone Set
EE-8**

Leather case, with handset, generator, ringer, etc. Requires 2 flashlight cells. Wonderful value! Good Used, ea. ... **\$14.95**

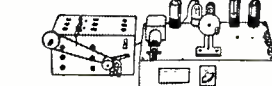


W.E. BREAST MIKE
Single button carbon mike, with breastplate. Very sensitive, complete with 6-ft. cord and W.E. plug. SPECIAL. New **\$1.29**



HANDSET
Cradle-type handset with battery switch, unbreakable black plastic, 4-ft. 3 wire cable. BRAND NEW, individually packed. each **\$7.50**

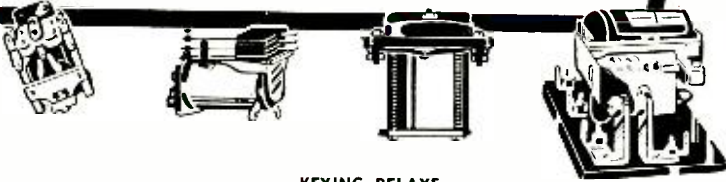
**McElroy
Automatic
KEYER**



Suitable for keying transmitter, or for code practice. Has photocell and sensitive relay. Variable speed motor. 110V AC or DC. Complete with 2-117Z6 and 1-117L6 tubes. **\$21.00** your cost

**We Have Available
CODE PRACTICE TAPE \$12.75**
which was used for code practice work by the Signal Corps—from slow to fast practice. 15 rolls on 16MM metal reels in heavy wooden slotted case, to be used with McElroy TG10 Keyers. Tone Keyers or any code practice.

RELAYS FOR EVERY PURPOSE Over a Million in Stock!



Whether you require large quantities of relays for production runs or single units for laboratory or amateur work, Wells can make immediate delivery and save you a substantial part of the cost.

Our capable engineering staff is prepared to offer assistance in the selection of correct types to suit your exact requirements.

Each relay is brand new, standard make, inspected, individually boxed and fully guaranteed.

The following list represents only a tiny portion of our relay stock. Write or wire us for information on types not shown.

KEYING RELAYS

STK. NO.	VOLT-AGE	OHM-AGE	CONTACTS	UNIT PRICE
R-714	9/14 VDC.	65	2C 5 Amps.	\$1.55
R-653	12 VDC.	14	2C	1.55
R-721	18/21 VDC.	290	2C 5 Amps.	1.55
R-773	24 VDC.	280	3C 10 Amps.	1.60
R-694	24 VDC.	300	1A 5 Amps.	1.50
R-704	2/6 VDC.	.25	2B 5 Amps.	1.35
R-297	115 VAC.	...	2C	2.80
R-173	2 6 VDC.	7	1A	1.55
R-280	6 8 VDC.	22	1A Double Break	2.45
R-647	6 12 VDC.	15	1B 20 Amps.	1.45
R-273	20 VDC.	160	2A 15 Amps. Dbl-Bk	3.55
R-168	24 VDC.	200	1A	2.45
R-570	24 VDC.	230	1B Double Break	2.70
R-171	24 VDC.	230	2C 10 Amps.	2.70
R-529	24 48 VDC.	1020	2C Ceramic	3.10
R-715	24 VAC.	...	2C	3.70
R-584	6 VDC.	20	1A Double Break	1.30
R-192	12 VDC.	44	3C 10 Amps.	1.70
R-204	12 VDC.	66	2A	1.45
R-224	12 VDC.	85	1A	1.45
R-221	18 24 VDC.	5000	1A	1.45
R-205	24 VDC.	260	2C	1.55
R-536	27 VDC.	230	2C	1.55
R-220	75 VDC.	5000	1C	1.51
R-627	115 VAC.	...	1A Double Break	3.10
R-608	12 VDC.	75	1A	1.55
R-734	24 VDC.	150	3C 10 Amps.	1.20
R-598	28 VDC.	185	2C	1.30
R-622	20 30 VDC.	200	3A & 2C 10 Amps.	1.45
R-274	24 VAC.	...	2A	1.55
R-273	24 VAC.	...	1A	1.55
R-269	24 VAC.	...	1A 15 Amps.	1.55
R-277	12 VDC.	30	2C Dbl-Bk. Cera.	2.20
R-594	12 VDC.	50	2C	2.00
R-668	12 VDC.	50	1C 10 Amps.	1.30
R-613	12 VDC.	50	1C	1.30
R-772	12 VDC.	70	1A 15 Amps.	1.45
R-293	12 VDC.	150	1C Double Break	3.10
R-607	12 24 VDC.	100	1A 10 Amps.	1.45
R-580	12 24 VDC.	150	1C Double Break	2.45
R-276	24 VDC.	100	2C Dbl-Bk. Mica.	3.10
R-752	24 VDC.	150	2C 3 Amps.	1.45
R-768	24 VDC.	175	2A 5 Amps.	1.45
R-699	24 VDC.	200	3C 5 Amps.	1.55
R-700	24 VDC.	200	2C 8 Amps.	1.55
R-282	24 VDC.	325	1A Double Break	1.55
R-286	115 VAC.	950	2C	2.80
R-612	2 6 VDC.	1	1A	1.55
R-815	2 6 VDC.	1.5	1A 10 Amps.	1.55
R-263	6 VDC.	12	2C 15 Amps.	1.55
R-279	14 VDC.	250	1A 15 Amps. Dbl-Bk	1.45
R-278	18 24 VDC.	260	2C 1A 1B	1.55
R-706	24 VDC.	150	4C 10 Amps.	2.45
R-177	24 VDC.	250	4C	2.05
R-609	250 VDC.	5000	1A Double Break	2.45
R-779	12 VAC.	...	1B 10 Amps.	1.70
R-272	24 VAC.	...	1A 1B 5 Amps.	1.55
R-271	24 VAC.	...	2A 1B 3 Amps.	1.55
R-685	115 VAC.	600	1A 6 Amps.	2.50
R-663	12 VDC.	40	2C 10 Amps.	1.30
R-757	12 VDC.	44	2C 1A Ceramic	1.45
R-152	12 VDC.	50	2C 1B Ceramic	1.35
R-624	12 VDC.	50	1C	1.45
R-268	12 24 VDC.	260	3A 1B	1.55
R-805	18 VDC.	200	1A 10 Amps.	1.30
R-644	18 24 VDC.	275	1A 25 Amps. & 1A 5A	1.45
R-687	26.5 VDC.	125	2C 15 Amps. & 3A 10A	2.45
R-674	24 VDC.	250	1C 5 Amps.	1.45
R-593	28 VDC.	125	2C 10 Amps.	1.45
R-191	28 VDC.	125	2C 10 Amps. Ceramic	1.50
R-248	28 VDC.	150	1A 20 Amps.	1.30
R-615	32 40 VAC.	...	3A 15 Amps.	1.55

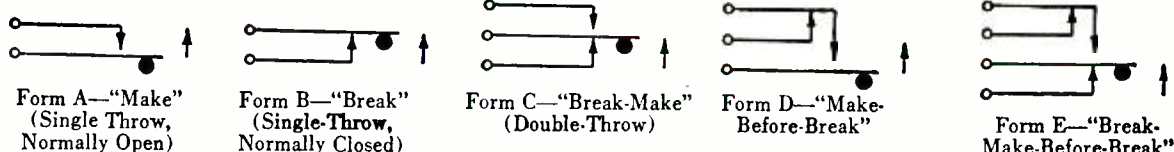
STK. NO.	VOLT-AGE	OHM-AGE	CONTACTS	UNIT PRICE
R-592	120 VAC.	...	1A	2.45
R-812	115 VAC.	...	1A Dbl-Bk. 15A	2.45
R-260	115 VAC.	500	3A 15 Amps.	2.45
R-249	100 135 VAC.	600	2A Ceramic	2.80
R-665	115 VAC.	500	2B 10 Amps.	2.80
R-693	2 6 VDC.	125	1C 3 Amps.	1.10
R-597	4 12 VDC.	16	1A 25 Amps.	2.45
R-193	5 8 VDC.	11	2C 1A 10 Amps.	1.30
R-595	5 8 VDC.	18.5	3C	1.35
R-692	6 24 VDC.	1280	1C 3 Amps.	1.35
R-793	12 VDC.	42	2C 10 Amps.	1.55
R-599	12 VDC.	67	3A 15 Amps.	1.45
R-599	24 VDC.	95	1A 10 Amps. & 1A 20A's.	1.30
R-560	24 VDC.	160	1A	2.80
R-795	24 VDC.	160	2A 15 Amps.	1.55
R-796	24 VDC.	160	2A 15 Amps.	1.60
R-562	24 VDC.	160	4A 10 Amps.	1.60
R-797	24 VDC.	160	8A 8 Amps.	2.80
R-549	24 VDC.	160	1C 10 Amps.	1.55
R-758	24 VDC.	160	2C 10 Amps.	1.55
R-742	24 VDC.	170	1C 20 Amps.	1.55
R-242	24 VDC.	180	2A 10 Amps.	1.30
R-675	24 VDC.	180	2A 10 Amps.	1.30
R-649	24 VDC.	265	1A	1.30
R-744	24 VDC.	265	1A 20 Amps.	1.50
R-530	24 VDC.	265	2A 10 Amps.	1.45
R-574	24 VDC.	265	2B	1.30
R-791	24 VDC.	375	2C 10 Amps.	1.55
R-775	28 VDC.	180	2C Ceramic	1.55
R-776	28 VDC.	265	2A	1.70
R-731	22 28 VDC.	425	2B 10 Amps.	1.70
R-802	24 VDC.	160	3A Dbl-Bk. 15 Amps.	2.80
R-792	24 VDC.	200	1A 15 Amps.	1.30
R-798	24 VDC.	500	1C 5 Amps.	2.40
R-695	12 VDC.	70	2C 3 Amps.	1.30
R-288	18 24 VDC.	175	2A Ceramic	2.25
R-558	24 VDC.	280	2C 3 Amps.	1.55
R-299	6 VDC.	24	2A	1.55
R-267	12 VDC.	65	2C 5 Amps.	1.55
R-206	24 VDC.	150	3C	1.50
R-207	24 VDC.	210	1C	1.35
R-219	50 VDC.	1500	2A 15 Amps.	1.50
R-531	12 24 VDC.	80	2A 10 Amps.	1.20
R-506	24 VDC.	300	2A 6 Amps.	1.20
R-581	24 VDC.	4500	1A 5 Amps.	2.45
R-825	115 VAC.	...	1A 6 Amps.	2.45
R-819	115 VAC.	...	2A 6 Amps.	2.45
R-652	115 VAC.	...	1A Dbl-Bk 20 Amps.	2.80
R-217	115 VAC.	...	1C	2.25
R-824	2 VDC.	.75	1C	2.80
R-609	8 12 VDC.	5000	1C	2.80
R-820	10 VDC.	20	1B Dbl-Bk 6 Amps	2.45
R-821	18 VDC.	160	1A 1B 2 Amps.	1.55
R-567	24 VDC.	200	1A 10 Amps.	1.35
R-739	24 VDC.	200	1A	1.35
R-724	75 VDC.	2200	2B 3 Amps.	2.40
R-823	110 VDC.	5000	1B	2.45
R-617	12 VDC.	600	1C Double Break	1.30
R-729	12 VDC.	80	1A 10 Amps.	1.25
R-722	24 VDC.	300	1A 10 Amps.	1.30
R-577	48 VDC.	220	2C	2.45

STK. NO.	VOLT-AGE	OHM-AGE	CONTACTS	UNIT PRICE
R-137	24 VDC.	300	1C	1.45
R-142	24 VDC.	400	2C	1.50
R-785	24 VDC.	200	2C/10 Amps.	2.00
R-607	24 VAC.	...	1A	1.20
R-606	24 VAC.	...	1A & 1B	1.20
R-605	24 VAC.	...	3A	1.20
R-728	6 VDC.	30	1A	1.25
R-907	6 VDC.	30	2C	1.25
R-625	6 VDC.	45	1C/3 Amps.	1.35
R-732	12 VDC.	120	1A	1.45
R-733	12 VDC.	120	2C	1.50
R-281	12 VDC.	126	2A	1.25
R-818	18 24 VDC.	300	1B	1.25
R-139	24 VDC.	200	4C	1.45
R-135	24 VDC.	250	1B	1.45
R-133	24 VDC.	300	None	1.45
R-138	24 VDC.	300	4A	1.45
R-132	24 VDC.	300	2C	1.53
R-731	24 VDC.	300	2C	1.55
R-730	24 VDC.	500	2C & 1A	1.55
R-292	24 VDC.	400	1C	1.25
R-626	24 VDC.	400	1A 5 Amps.	1.55
R-786	60 VDC.	1300	2C	2.00
R-588	90 125 VDC.	6500	4C	2.70
R-755	24 VDC.	300	1A	1.45
R-150	6 VDC.	30	1A	1.20
R-640	24 VDC.	330	1C/3 Amps.	1.50
R-148	12 VDC.	100	2C & 1B	1.35
R-285	12 VDC.	75	2A	1.35
R-222	12 VDC.	100	2C	1.21
R-639	6 VDC.	20	3C 3 Amps.	1.45
R-696	24 VDC.	230	1A 8 Amps.	2.00
R-143	24 VDC.	280	1A	1.45
R-141	24 VDC.	280	3A	1.45
R-140	24 VDC.	280	1C	1.45
R-590	24 VDC.	300	2B	1.45
R-540	24 32 VDC.	300	2C	1.25
R-543	24 32 VDC.	300	4C	1.50
R-743	110 VDC.	5000	3B & 1A	2.05
R-783	100 VDC.	6500	1C Micalex.	2.40
R-782	100 VDC.	6500	4C & 1A.	2.45

SPECIAL RELAYS

R-503	12 32 VDC.	100	3A, 2C	2.80
R-748	600 VDC.	...	Max. 28 Amps.	7.45
R-804	550 VAC.	...	1B 38 Amps.	4.35
R-250	115 VAC.	...	Adj. Cir. Br.-.04-.16A	17.50
R-579	220 VAC.	...	1B	8.70
R-294	27.5 VDC.	200	1B	5.35
R-686	115 VAC.	...	2C	6.10
R-246	115 VAC.	...	1B	11.20
R-246A	115 VAC.	...	1A	11.20
R-611	24 VAC.	...	1A 30 Amps.	5.35
R-283	12 VDC.	125	1C/15 Amps.	1.25
R-614	18 24 VDC.	60	1A 15 Amps.	4.35
R-262	12 VDC.	200	1C	4.70
R-245	12 VDC.	25	4" Micalex Lever	1.20
R-527	6 12 VDC.	50 50	In Series	1.20
R-544	12 24 VDC.	60 60	1C	2.05
R-255	1A	1.20
R-669	75 VAC.	400 Cy.	1B, 1A	1.20
R-660	6 VDC.	...	3/8" Stroke	1.20
R-651	24 VDC.	100	Solenoid Valve	3.10
R-295	12 VDC.	275	Annunciator Drop	2.70
R-230	5 8 VDC.	2	2A, 1C	2.70
R-813	12 VDC.	12	Wafer	5.35
R-275	12 VDC.	750	1A, 1B, 1C	3.45
R-716	24 VDC.	70	2A 5 Amps.	1.63
R-820	6 12 VDC.	35	2C, 1A	1.30
R-629	9 14 VDC.	40	1C/10 Amps.	1.55
R-720	24 VDC.	50	2C Ceramic	1.70
R-500	12 VDC.	10/10	2C/6 Amps.	3.55
R-816	12 VDC.	10/15	2C/6 Amps.	3.55
R-524	24 VAC DC.	1.20
R-566	115 VAC.	...	Coil only	1.00
R-710	150 VAC.	...	Coil only	1.75
R-811	48 VDC.	8000	1C	2.05

BASIC CONTACT ASSEMBLIES SHOWN IN UNOPERATED NORMAL POSITION



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