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CONTRACTOR REPORT ARLCD-CR-84020

GEMSS EXTENDED RANGE TRIPLINE SENSOR (ERTS) PRODUCT IMPROVEMENT PROGRAM (PIP)

M.B. WEIDENBACH B.J. AMUNDSON R.A. JOHNSON

HONEYWELL INC. DEFENSE SYSTEMS DIVISION 5640 SMETANA DRIVE MINNETONKA, MN 55343



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U.S. ARMY ARMAMENT RESEARCH AND DEVELOPMENT CENTER LARGE CALIBER WEAPON SYSTEMS LABORATORY

DOVER, NEW JERSEY

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Contractor Report <u>ARLCD-CR-84020</u>	ADA145030	
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GEMSS EXTENDED RANGE TRII PRODUCT IMPROVEMENT PROG	PLINE SENSOR (ERTS) RAM (PIP)	2 March 1983 30 December 198
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AUTHOR(S)		8. CONTRACT OR GRANT NUMBER(S)
M. B. Weidenbach B. J. Amundson		DAAK10-83-C-0049
R. A. Johnson		
PERFORMING ORGANIZATIONS NAM	ME/ADDRESS e Systems Division	10. PROGRAM ELEMENT PROJECT, TASK AREA & WORK UNIT NUMBERS
5640 Smetana Drive Minnetonka, MN 55343		PIP No. 1-82-09-7721
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Contents

		Page
Introduc	tion .	1
Technica	l Report	3
Chang	es Incorporated	3
Data F	leview	3
Bobbin	Analysis	8
Quality	Report .	10
First A	rticle Acceptance Tests	10
Lot Ac	ceptance Tests	11
Special 7	Cests	12
Leaka	ge Test	12
Langli	e Test	12
Appendi	xes .	
Α	First Article Test Summary Report and Lot Acceptance Test Results	13
В	Engineering Test Report OEXM 32211	31
Distribu	tion List	44



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iii

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INTRODUCTION

The extended range tripline sensor is used in the antipersonnel mines of the GEMSS, GATOR and MOPMS systems. The tripline is deployed when the bobbin on which it is wound is spring ejected from the sensor body. The bobbin is mechanically locked to the sensor body by a release mechanism which is designed to be activated by gas pressure above a threshold level. Activation of the release mechanism unlocks the bobbin. A pressure cartridge is used to supply the required threshold level of gas pressure. The deployed tripline is the mine's detection element; however, the sensitivity of this detection is dependent on how well the force of target/tripline interaction is transmitted through the tripline to a 0.0040-inch breakwire and the force needed to break this wire. The mine's electronic assembly monitors the continuity of this wire and initiates the self-destruct mode when wire continuity is lost.

In the subzero climate environments of the GEMSS DTII and OTII tests, the deployment of tripline from sensor was adequate but not 100 percent. Analysis of the hardware and data identified the reasons for this non-deployment as: the rigidity of the sensor's diaphragm and/or the lower output of the pressure cartridge at cold temperatures. The current material used for the diaphragm is Roylar E-82 and its flexibility is highly temperature dependent at cold temperatures; for example, its flexibility at the system's required low temperature operating limit of -35° F is approximately 52 percent of its flexibility at 0° F. Also, pressure cartridge closed bomb tests indicate that the average peak pressure at -35° F is approximately 65 percent of the average peak pressure at the system's high temperature operating limit of 125° F. The need for replacement is urgent because Roylar E-82 is no longer manufactured. It will be replaced by Estane 58880.

The detection sensitivity of the tripline/breakwire interface meets the requirements of the sensor specification; however, tactical field test data indicated that the strength of the tripline should be increased and that of the breakwire decreased. In the ideal detection situation, the minimum (1.8 lb) break strength of the tripline and the maximum (0.9 lb) break strength of the breakwire guarantee a detection if the tension force in the tripline exceeds 0.9 lb. In the tactical situation, it is often the case that between the source of the tension in the tripline and the breakwire, the tripline is in contact with other objects (vegetation, etc.). This means that the tension in the tripline at the source may exceed the minimum 1.8 lb needed to break the tripline before the tension force at the breakwire is sufficient to break the breakwire. An ideal tripline would be one that could not be broken. Another tactical situation that sometimes occurs is that the target detects the tension in the tripline before it induces a tension of 0.9 lb, the maximum breakwire strength. Detection sensitivity for this last case would be improved if the breakwire had a maximum break strength less than the current 0.9 lb.

One of the principal objectives of this product improvement program was to incorporate the following changes into the extended range tripline (ERTS) technical data package and to demonstrate/characterize each for adequacy:

a. Alternate diaphragm material which is more flexible at cold temperature. (Original material in TDP is also no longer available.)

b. Weaker breakwire for increased sensitivity.

c. Stronger tripline thread to increase probability of breakwire opening before tripline breaks when pulled.

A second objective was to manufacture and deliver 4,500 ERTS with above modifications to Aerojet Corp., who had a parallel PIP contract to include improved sensors plus other modifications in the M74 mine.

The third objective was to provide a quantity of lithium cells to both Aerojet Corp. and Burroughs Corp. as government furnished material (GFM) to be used on PIP contracts for the M74 and M75 mines, respectively. The lithium cell is the power source for the GEMSS M74 and M75 mines and will be required in many of the mines manufactured under the GEMSS PIP program. The technical data package (TDP) for the lithium cell is a proven TDP; therefore, with respect to the lithium cell, Contract DAAK10-83-C-0049 was simply the vehicle to procure lithium cells and deliver them as GFM to the appropriate PIP contractors.

TECHNICAL REPORT

The principal objectives of this contract were to incorporate three changes into the Extended Range Tripline Sensor (ERTS), to test the effectiveness of these changes, and to ship 4500 ERTS to a specified contractor. An additional objective was to ship 2250 standard lithium batteries to the same contractor.

Changes Incorporated

The three changes incorporated into the ERTS in this contract were:

1. A stronger tripline (2.5 lb minimum break strength versus the original 1.8 lb minimum break strength).

2. A smaller breakwire (0.0035-inch diameter versus the original 0.0040 inch diameter).

3. A different diaphragm material (B.F. Goodrich Estane 58880 versus the original Uniroyal E-82).

Data Review

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The initial effort on this contract consisted of a review of the technical data (drawings and specification) to determine changes necessary to make them compatible with the three changes specified above. Results of this review were submitted in a letter from J.H. Lundquist, dated 13 April 1983, Subject: Contract DAAK10-83-C-0049, GEMSS ERTS PIP, CRDL Requirements.

Drawing Changes

The drawing changes necessary to reflect the three changes and to correct minor errors are presented in Table 1.

All NEXT ASSEMBLY and USED ON boxes should be changed as necessary to assure that the drawings are identified with the proper mine.

Drawing	Change required	Comments
9298576 (Wire, Magnet, Electrical)	In Note 1B, "#38 AWG" should be "#39 AWG". In Note 1C, " 0.004 ± 0.0001 ROUND" should be " 0.0035 ± 0.0001 ROUND".	This is an ADAM drawing. If this change is made the drawing cannot be used for ADAM. The drawing can either be changed to a tabulated drawing or a new drawing can be made.
9292972 (Tripline Sensor Extended Range)	In Note 3, "LOCATED 32 FEET" should be "LOCATED 29 FEET" and "0.3 TO 0.9 LB" should be "0.22 TO 0.82 LB".	See paragraphs entitled "Deployment Barrier Distance" and "New Minimum and Maximum Limits on Breakwire Strength" on pages 8 and 9, respectively.
9292991 (Release Mechanism Assembly)	In Zone C5 change "RING, LOCK - 9298586" to "RING, BALL LOCK - 9298586".	
9292998 (Diaphragm Assembly)	In Zone CD-3 change "DIAPHRAGM - 9298598-2" to "DIAPHRAGM - 9298598-1".	
9298592 (Thread, Polyester)	In Note 1A, "234 \pm 8 DECITEX" should be "320 \pm 8 DECITEX". In Note 1B, "1.8 LB MIN" should be "2.5 LB MIN".	This is an ADAM drawing. If this change is made it cannot be used for ADAM. The drawing can either be changed to a tabulated drawing or a new drawing can be made.
9298598 (Diaphragm)	In the table at the bottom of the drawing add "9292998" in the NEXT ASSEMBLY box for 9298598-1.	
9292982 (Bobbin Assembly)	In Note 2, "46 \pm 3 FEET" should be "34 \pm 2 FEET". In Note 7, "750 REVOLUTIONS" should be "580 REVOLUTIONS". Delete Note 8. Change left view as shown in Figure 1. Add Note 10: "ADD A DROP OF ADHESIVE AT EXIT POINT OF THREAD JUST PRIOR TO ASSEMBLY OF THE BOBBIN WEIGHT INTO THE BOBBIN".	Permission to incorporate this change was granted by ARRADCOM approval of Deviation 0297-008 (Ref PAN A3N7705).
XXXXXXX (Adhesive)	Make a new drawing like Figure 2 for the adhesive.	

Table 1. Drawing change summary

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Figure 1. Changes to end view on drawing 9292982



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Figure 2. Adhesive drawing

During this contract it was apparent that vendors were having difficulty manufacturing the booster spring (9292990). The drawing had ambiguities in it as evidenced by various interpretations of what it meant. In addition, it was obvious that the spring load test fixture was not conducive to providing repeatable load readings. In order to clear up the ambiguities and improve the load test fixture, ECP 83-0007-045 was submitted. It was submitted on ERTS GATOR Contract DAAK10-83-C-0007 running concurrently with the ERTS GEMSS PIP contract which this report covers; however, the changes requested in it apply to the GEMSS PIP sensor because the same booster spring is used in both sensors. The ECP requested the following changes to drawing 9292990:

- a. In Zone C4 change "0.395 + 0.010 SEE NOTE 8" to "0.395 + 0.010 SEE NOTES 8 & 9."
- b. In Zone C4 add "SEE NOTE B" with an arrow pointing to the left end of the spring.
- c. In Zone C3 change "SEE NOTE 5" to "SEE NOTE B."
- d. In Zone C2 change "0.385 + 0.010" to "0.385 MIN."
- e. In Zone D2 change "0.455 MAX DIA, 8 COILS REF SEE NOTE 9" to "0.455 MAX DIA, 9 COILS REF SEE NOTE 9."
- f. In Zone D2 make the extension lines defining the 0.455 MAX DIA refer to the OD of the 9 smaller coils rather than to the OD of the 2 larger coils.
- g. In Note 7 change 0.475 to 0.484 and change 0.340 to 0.384.

The ECP was approved with modifications and the final changes are described in NOR A3N5166. The drawing should be changed per this NOR.

Specification Changes

The changes to Specification MIL-S-48755 (AR) necessary to reflect the three . changes and to correct minor errors are:

- a. Delete paragraphs 3.3 and 4.5.1.1 and all further references to these paragraphs.
- b. In paragraph 3.5 change "thirty-two (32) feet" to "twenty-nine (29) feet."
- c. In paragraph 3.6 change "140 grams (0.3 pound) min and 410 grams (0.9 pound) max" to "100 grams (0.22 pound) min and 370 grams (0.82 pound) max."
- d. In agraph 3.11.a change "Assemble" to "Assembly."
- e. In paragraph 3.11.f change "Ball Lock Ring" to "Ring, Ball Lock."
- f. In paragraph 4.4.2.22 Major 104 change "140 grams (0.3 pound) to 410 grams (0.9 pound)" to "100 grams (0.22 pound) to 370 grams (0.82 pound)." Delete Major 101 and Note 2.

- g. In paragraph 4.5.1.3.a change "32 feet" to "29 feet."
- h. In paragraphs 6.1.a, 6.1.b, and 6.1.c revise to reflect whatever mines use the smaller breakwire, stronger thread and different diaphragm material.

Bobbin Analysis

An analysis of the bobbin assembly was made to determine the amount of stronger thread that can be wound on the bobbin, and to determine the effect of this stronger thread on deployment barrier distance and bobbin assembly CG location. Results of this analysis were submitted to ARRADCOM in a letter from J.H. Lundquist dated 11 May 1983, Subject: Contract DAAK10-83-C-0049, GEMSS ERTS PIP CRDL Requirements.

Thread Length

The stronger thread used on this contract has a larger diameter than the standard thread. Thus, when the standard length $(46 \pm 3 \text{ feet})$ of the stronger thread is wound on the Bobbin (9292985), the diameter over the wound thread is significantly larger than when the standard thread is used. This results in interference between the thread and the inside of the Sleeve (9292988), causing assembly difficulties when assembling the Bobbin Assembly (9292982) into the Sleeve. Cut and nicked thread and friction between the thread and Sleeve ID results.

In order to eliminate these problems, less of the stronger thread must be wound on the bobbin. It has been experimentally determined that a maximum of 36 feet of the stronger thread should be used to provide proper assembly and release and to maintain thread integrity. Using a realistic overall length tolerance of ± 2 feet results in the recommended thread length of 34 ± 2 feet for the stronger thread.

Deployment Barrier Distance

Because the stronger thread is thicker, less thread can be wound on the bobbin, making the deployment distance less. Deployment test (OEXM 31388) shows that at the standard barrier deployment distance of 32 feet the barrier could not be cleared consistently. When the barrier distance was moved closer at 29 feet, the barrier was cleared consistently. In additional deployment tests on 36 sensors, all cleared the barrier at 29 feet. The three-foot reduction in barrier distance is strictly a function of thread length and has nothing to do with the weight and CG characteristics of the bobbin. The bobbin wound with the stronger thread clears the barrier located at 29 feet just as well as the bobbin wound with the standard thread clears the barrier located at 32 feet.

Center of Gravity

The bobbin analysis shows that the CG shift of the bobbin assembly wound with the stronger thread is 0.002 inch. This is insignificant with respect to sensor deployment characteristics. The weight of the bobbin assembly wound with the stronger thread is 0.0218 gram more than that of the bobbin assembly wound with the standard thread. This weight increase can be eliminated by removing material from the bobbin weight, either by making it shorter or by increasing the diameter of the hole in it. Since the heavier bobbin assembly clears the barrier located at 29 feet just as well as the standard bobbin assembly clears the barrier located at 32 feet, a change to lighten it is unnecessary and is not recommended.

New Minimum and Maximum Limits on Breakwire Strength

The new minimum and maximum breakwire break strength limits were established from the data on 182 ERTS sensors tested on the GATOR PIP program (Contract DAAK10-82-M-0504) and reported in test report OEXM 31388. The former limits of 140 grams minimum and 410 grams maximum resulted in a spread of 270 grams. Based on statistical analysis of the data and past experience on the ADAM program, it is felt that this spread should be maintained. This is also the basis for selecting the new limits of 100 grams (0.22 lb) minimum and 370 grams (0.82 lb) maximum.

QUALITY REPORT

Quality tests conducted for the GEMSS PIP contract were the standard tests: (1) First Article Acceptance Test (FAAT) and, (2) Lot Acceptance Test (LAT). A total of four tests were actually run, consisting of two unsuccessful FAATs, a final successful FAAT, and a single successful LAT for the single delivery lot containing a quantity of 4,500 units. See Appendix A for attachments dealing with quality tests. Attachment 1 is the conditional approval of the FAAT, Attachment 2 is the raw data sheet for this FAAT, Attachments 3 and 4 are the raw data sheets for the first two FAATs and Attachment 5 is the raw data sheet for the LAT.

First Article Acceptance Tests

The first FAAT occurred on 27 July 1983. Failures to release the bobbin (three units) were traced to a machine assembly problem that was damaging the diaphragm. Appropriate corrective action was taken, which eliminated this problem. All existing hardware was scrapped and a new set of units was built.

The second FAAT on 30 August 1983 was unsuccessful due mainly to test errors as well as sample preparation problems. Improper calibration of the pressure system, used in conjunction with the test equipment during cold temperature testing, caused an overpressurization of the diaphragm assembly. When combined with inadequate sealing, it caused separation from the sensor case, resulting in release failures. Appropriate corrective action was taken and a third FAAT was scheduled.

The successful FAAT of 20 September 1983 had the following results:

- One of 82 units experienced post pullout below the 540-gram requirement (recorded for information only)
- One of 82 units failed breakwire force
- One of 32 units failed cold release (see Attachment 2 for test data).

The breakwire and release failures were caused by potting material intrusion under the post cover during sample preparation. The sample's post covers had not been sealed with epoxy prior to potting. This type of defect would not normally occur on shipped units since all sensors would be properly sealed with epoxy prior to shipment. These units were classed as "no tests" and spares were functioned in their place. All subsequent testing has been performed with epoxy sealed sensors. Following this FAAT, a conditional approval was given by ARDC (see Appendix A). Honeywell's action for achieving full Governmental approval for the first article test was to ensure that all future LATs would be conducted using sample units sealed with epoxy before potting. The production layout was changed to formalize this action. The corrective action was completed and locally approved by DCAS on 14 October 1983.

Lot Acceptance Test

The LAT was conducted on 16 November 1983. The results of this test were as follows:

- One of 80 units failed breakwire force
- Three of 80 units failed post retention and thread strength (see Attachment 5 for test data).

Analysis of the breakwire failure showed that the breakwire retaining ring was not assembled properly, allowing the post to be pulled out of the sensor without breaking the breakwire. Thus, this unit was also counted in the second category as well, for a total of three defective units (not four). No cause was discerned for the other two units that experienced thread breakage below the 540-gram minimum. No corrective action for the above defects has been taken since additional quantities are not being built. The lot was accepted as tested since the defects identified were below allowable defects per the sample plan and AQL's specified.

SPECIAL TESTS

Leakage Test

The leakage test was conducted to determine: (1) the leak rate through undeployed sensors at a sensor pressurization of 75 ± 5 psi, and (2) the leak rate through deployed sensors at their deployment pressure or, if the sensors did not deploy before being pressurized to 300 ± 10 psi, their leak rate at 300 ± 10 psi. All tests were conducted at ambient temperature $(75^{\circ} \pm 10^{\circ}F)$ and nitrogen gas was used as the pressure medium. Results are contained in test report OEXM 32211 (Appendix B). This test report was also submitted with a letter from J.H. Lundquist dated 6 January 1984, Subject: Contract DAAK10-83-C-0049 GEMSS ERTS PIP Test Report, Langlie Test.

Langlie Test

The Langlie test was conducted to determine sensor tripline deployment at three different square pressure pulse time durations at various pulse pressure levels. Results are also contained in test report OEXM 32211 (Appendix B).

APPENDIX A FIRST ARTICLE TEST SUMMARY REPORT AND LOT ACCEPTANCE TEST RESULTS

1. First Article Test Summary	Report
US Army Armament Research and Development Center Dover, MJ 07801	2. Date 3. Report No. 462-33 4. In reply refer to 5. Preliminary Supplemental Supplemental
	DRSHC-QAM-VF(D)/92 Finds EX
6. To Commander DCASPRO Honeywell 2701 Fourth Ave. So. Honeyvell Plaza Minneepelis, MI 55408	7. Date initial production sorple received at <u>See Reighton</u> 107 (insert location) Date <u>20 Sept. 1983</u> 8. Contract No. <u>DAAR10_83_C_0069</u> 9. Contractor
10 Complete sample 17 11. Item nor	Boographi, Inc.
Portial sample	
3rd Selmission Senaor Trip	line Extended Range
12: Quantity 12: Is inspection	I In accordance with
As per Contract MIL-S-4875	5(AR) w/mend. 5 dtd 5 May 82.
	13. Representing
16. Inspected by	17. Submitted by
R. Flageran	A. Signfriet/stb/201-724-2458
18. Anconstation des Conseine Antivity	
The contractor may proceed with production.	Corrective action cited on black 28 is required
The contractor may proceed with production provided the deviations cited under Remark of block 28 are corrected.	Conditionally Approved.
19. Distribution	20ICHARD W. PORTER
Cy Farm: Econoywell, Inc.	C. Mines & Sel Arm Br
R. Currie 1992-3553	
	CONCURS
5. AMUDISON MI29-3661 7. Rohumide MI20-3681	
S. Amindson M129-3681 V. Rehvuldt M129-3681 M. Weidenbech M129-3680	Signed: Gael C. Balter W. & Bran
J. Lundquist 19904-1200	Signed: Gael C. Baker W. F. BELET Contracting
B. Ammidson M129-3681 T. Rehvaldt M129-3681 M. Weidenbach M129-3680 J. Lundquist M104-1200 C. Files M104-1280 E. Ludge M428-3561	Signed: Gael C. Baker W. F. BELET Contracting Office GAEL C. BAKER ActC, Product Verification Errach

ATTACHMENT 1

ARRADCOM FORM S1 JUN 78 replaces SHI 1031-R AUG 66 which is obsolete

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Nomencloture	Part No.	Serial No.	Specification No.	Paragraph No.	Identification	Pass	Fail
Tripline, Sensor	9292972	N/A	HIL-5-48755(AR)	4.5.1.2.1	Release of Sensor		
Extended Range 82 each	70-61-0		S May 82		Temperature	×	
				4.5.1.2.2	Release of Sensor		
					Assy. at Cold		:
					Temperature		×
			-	4.5.13	Tripline Deploy-	;	
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TTC MIDE MOMMIN	JUN (D LEDIE	ICCE PUT TOTT-N	VIG OD ARTCH TE ODE	919T0	SHEE	-	- ¦;

28. Summary of failures encountered and required corrective action.

Tripline Sensor, Extended Range, Dwg. 9292972 -

1. One unit failed to release at cold temperature. Major Defect

2. One unit failed breakwire functioning at cold temperature. Breakwire broke at 800 grams in lieu of 100 to 378 grams. Major Defect

3. One unit failed post retention at cold temperature. Post released at 280 grams,min. requirement is 540 grams. Test performed for informational purposes only.

ACTION TO BE TAKEN:

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The contractor may proceed with production provided the defects noted above in paragraphs 1 and 2 are corrected to the satisfaction of the QAR.

ARRADCC.1 FORM 51b JUN 78 ruplaces SUJ 1031-R AUG SI - vhich is obsolete

SHEET _3 OF _3

ATTACHMENT 2

MN28-3861 MN28-3660 MN28-3680	MN29-3386	MN29-3668	
AMUNUSON HANSON	McCABE	STACHOUSKI	
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SENSOR ASSEMBLY LAT RESOLTS SUMMARY	E 7-40-85	(chio) ALA	
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MIL-S-48755 PARA. 4.4.2.22

	RESULTS	EQUIREMENT		REMARKS	
		 		BLU-82/8 ONLY	
LIGE ANHITENT RELEASE	5%	20			
102 COLD RELEASE	320 *	8			
103 AMRTENT DEPLOYMENT	5%				
tas caro nem nyment	32	32	· · · · · · · · · · · · · · · · · · ·		
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DEFECTIVES SHALL EXCEED 544 GRAMS.

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NOTE: NO MORE THAN ONE OF THE FIVE ALLONABI Defectives shall exceed 544 grams.

ATTACHMENT 3

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B. AMINDSON	6. HANSON	N. NcCABE	U. SHEEHAN	
SENSOR ASSEMBLY	IT RESULTS SUMMARY	7/21/83	card 3-1 FAT	
	2	DATE	LOT •	LOT SIZE

MK29-3681 MK29-3096 MK29-3096 MK29-3306 MK20-3300 MK20-3690

DANKIO- 83-C-OOY9

Genss ERTS PIP

MIL-5-48755 PARA. 4.4.2.22

			RESULTS	REQU	DEDET	REWARKS
	162	ABIDIT RELEASE	1 /50	3	+1-2	
	ä	COLD RELEASE	2/32	32	-1-2	
21	8	ABIDI DEPLOMENT	1/50	3	H-3-4	
l	163	COLD DEPLOMENT	C/32	ž	-2-3	
	Đ	BREAKUTIOE	0/82	5 6	9 -S-1	
	Ä	Post retention and	C/ 67			DECONATION ONLY
		THREAD STRENGTH				

NOTES :

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280	270	270	ol 30	210	2 ZC	250	منغن	210	230	290	230	230	260	300	290	270	330	240	230	- 70	220	<u>1</u> 240	280
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NOTE: NO HORE THAN ONE OF THE FIVE ALLOWABLE DEFECTIVES SHALL EXCEED 544 GRAMS. ē

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ATTACHMENT 4

MN29-3681	MN29-3680	MN29-3680	MN29-3300	MN29-3690	MN29-3680
AMUNDSON	HANSON	NOSNHOD	McCABE	SHEEHAN	STACHOUSKI
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ERTS SENSOR ASSEMBLY	AT RESOLTS'SUMMARY	58-02-0		FARTEX	82
		1110	DAIE	LOT +	LOT SIZE

MIL-S-40755 PARA. 4.4.2.22

		RESULTS		REOUIREMENT	KEN	IARKS	
					BLU-92	2/B ONLY	
<u>8</u>	ANDIENT RELEASE	0/50		20			
162	COLD RELEASE	0/32		32			
 183	ANBIENT DEPLOYMENT	1/50					
69 1	COLD DEPLOYNENT	0/32		32			
191	BHEAKWINE	9/82		62			
16	POST RETENTION AND THREAD STRENGTH	2/82		81	INFORMA	TION ONLY	
NOT	ES :						
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ATTACHMENT 5

NN28-3661	MN29-3680 MN20-3660	NN29-3300	MN29-3698	0905-77NU
NOSONNA	HANSON	McCABE	SHEEHAN	SIACHUNGKI
				2
SENSOR ASSEMBLY	LAT RESOLTS SUMMARY	11-16-83	3-1	4621
	_	DATE	+ T01	LOT SIZE

HIL-S-48755 PARA. 4.4.2.22

	RESULTS	REQUIREMENT	REMARKS
181 NON-RELEASE	N/A	86- 2-3	BULL-82/B ONLY
182 AMBIENT RELEASE	0/50	54-1-2	
182 COLD RELEASE	. %50	36-1-2	
103 AMBIENT DEPLOYMENT	0/50	58-3-4 58-3-4	
103 COLD DEPLOYNENT	0/50	36-2-3	
104 DREAKUTRE	1/80	86-5-6	
POST RETENTION	3/6	88	INFORMATION ONLY
THREAD STRENGTH NOTES :			
		11- 21.83	
		11-21-83	

11-21-23 11-21-83 11-22-83 NOTES :

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NOTE: NO MORE THAN ONE OF THE FIVE ALLOWABLE DEFECTIVES SHALL EXCEED 544 GRAMS. ī

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APPENDIX B ENGINEERING TEST REPORT OEXM 32211

Honeywell

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ENGINEERING TEST REPORT

COPYLIST:		AVIONICS	12-29-83	OEXM 3	2211					
B. Amundson	MN29-3681	DEFENSE SYSTEMS	S4594-AA-	6000-2759	1 OF 7					
R. Currie	MN29-3553	N8103 - D & E Lab	c	DAAK 10-83-C-0049	_					
J. Funk	MN29-3682	UNITS TESTED.								
J. Haley	MN29-3553	One hundred thinty	five Extended	Dance Trinling Sensor	e /0202072					
J.Lundquist(3)	MN04-1200	Modified). Modific 0.0035 + .0001 diame	ations consis	t of the $9298598-1$ and $320 + 8$ Decitres	diaphragm, Thread					
T. Martorano	MN29-3682		our breakwing		THE COUL					
D. Stachowski	MN29-3680	OBJECT OF TEST:								
D. Swanson	MN11-1430	Conduct Leakage Rat	e and Langlie	One-Shot Release Test	ts as out-					
M. Weidenbach	MN29-3680	The The Commence								
L. Wilder	MN11-1430	DOCUMENTATION:								
D & E File	MN11-1430	See attached data sh	neets.							
Uniterm File	MN11-1430	PROCEDURE AND RESULT	<u>rs</u> :							
		Leakage Rate:								
KEYWORDS: GEMSS, XM74 Sensor, Extend	ed	Each unit was tested as shown on the attached Test Plan except the Nicolet Oscilloscope was set on a slow trace and started before applying pressure to the sensor. The starting pressure (supply pressure cut-off) and the fixture pressure at 30 second intervals as shown in the data sheets were read from the scope trace.								
Leakage Rate		Langlie Test:								
	·	Each test was con Initial "no relea psi and 350 psi re	nducted as sho set and tall a espectively.	wn on the attached release" limits were	Test Plan. set at 50					
ATTACHMENTS:										
I Leakage Te II Langlie Te	st Plan (2) st Plan (2)									
		1								

DATA BOOK NUMBER PAR	GE		TEST STARTED	TEST COMPLETED
0-2431	112-117		12-5-83	12-16-83
REQUESTED BY	DA'	TE	WRITTEN BY	
M. Weidenbad	ch l	12-1-83	J. Funk/T. Mart	torano
DEPARTMENT			APPROVED BY	
Production i	Engineering		L. D. Wilder	
HE-448 REV 12/78				

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2	25.1	21.2	6t. P	64.8	6.13	3.1	56.1	5.2	51.2	49.7	48.3	47.1	416.0	11.17
'n	50.0	75.1	63.3	63.0	56.1	53.7	•.مح	127	45.2	43.1	42.0	40.6	393	3 6
1	Se. e	77.4	61.9	54.4	47.9	424	35. /	35.7	1.52	30.8	23.5	75.4	28.0	1.10
5	22.0	65.8	5.2.8	50.6	44.2	3F. C	34.0	28.7	26.3	23.1	2.8	15.2	15. 9	2 71
٩	80.0	20.2	52.1	4.12	42.1	41.5	38.0	8.4	32.4	30.6	+ 60	25.6	229	12.5
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8	75.1	24.1	61.3	62.3	54.8	5.1.2	48.4	1,1, 2	42.1	39.6	32. 1	35.0	33.0	31.0
•	2.25	10.1	45.8	36.8	30.6	4.26	22.3	1.1	17.9	16.6	15.6	1.21	14.4	0.41
10	25.8	5.2	42.0	32.9	31.0	26.1	2.50	/2.3	16.7	15.5	14.3	12,5	12.7	11. 15
	2.2	1.1	47.9	37.2	32.5	23.4	6:50	3.46	376	20.4	1.1	15.2	12.5	120
27	2.5	1.12	45.4	35.6	25.6	24.0	که. تر	12.9	1.2	14.8	13.7	13.1	12.7	2.8
ζ,	72.6	43.6	53.6	4.24	39.0	33.7	21.4	2.16	-5.66	21.7	19.9	15.3	16.1	13.6
41	25.8	615	42.5	35.8	32.4	26.7	1.12	15.6	1.1	15.9	11.7	10.8	2.8	8.4
21	78.1	14.1	544	46.6	40.5	35.1	2.1	1.96	35.6	23.4	21.6	20.2	19.2	12.4
) (2.5	4.1	63.1	523	52.0	47.8	44.1	40.7	39.3	36.2	34.5	372	30.7	29.4
?	25.3	64.1	222	43.7	36.9	31.0	2.4	22.0	20.1	127	16.0	14.0	C.8/	13.4
15	22 2	6.2	25.5	33.4	24.4	18.4	14.5	• -//	10,1	2.4	9.0	0	۱	۱
•	74.4	71.6	24.6	1.5	54.7	46.6	124	36.1	1.72	32.7	20.3	25.6	27.1	35.6
90	255	62.4	59.1	51.7	404	40.2	35.8	22.5	21.5	26.9	2:56	28.4	526	21.4
ir	74.6	(1)	1.12	54.2	48.6	43.6	2.5	36.1	23,5	31.4	21.6	27.7	2.26	
22	141	69.5	65.2	61. 2	57.2	53.6	51.0	40.1	45.7	47.6	41.8	40.4	35.5	27.7
2	2:4	52.9	41:4	36.6	30.0	5:52	2.2	1.4	12.5	1.1	15.4	-2 .7/	1.1.1	11
22	25.2	596	35.3	26.1	20.4	16.6	14.1	1.3	11.2	10.7	10.1	8.8	9.3	• 3
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36	25.0	12.5	59.7	2.02	4.4	41. >	26.92	2.5	30.5	28.4	26.0	74.2	1.00	12. 5
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	128.0	o her	1225	112.0	116.0	112.5	110.0	107.5	105.0	102.0	10.0	97.5	74 1	32.1
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CEXM 32211 Page 6 of 7

LEARAGE TEST - BREAK WIPE & TRIP HINE FORCE

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/0	220	/340
//	240	//3•
12	+10	1200
/3	240	/150
14	710	/330
/5	180	1040
/6	240	//20
/7	250	1200
18	240	/330
/7	220	1140
J 0	230	1440
21	240	,300
22	230	/3/0
33	240	/230.
14	220	1140
25-	260	/3,0
36	270	//20
27	200	/040
28	260	/230
2 7	230	1350
30	250	//.0
31	230	/ 330
32	260	1410
33	230	1240
34	280	//80
35-	220	650

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ATTACHMENT I

OEXM 32211

Page 1 of 2

TEST PLAN

GEMMS/ERTS LEAKAGE TEST

1.0 Purpose

The purpose of the test is to determine the rate of pressure leakdown through the sensor.

- 2.0 Test Procedure
 - 2.1 Initial leakage.

2.1.1 Install sensor in release socket of pressure chamber.

- 2.1.2 Pressurize chamber with nitrogen gas to 75+5 psi.
- 2.1.3 Close shut off valve to chamber and start Nicolet Oscilloscope trace.
- 2.1.4 Record pressure trace on Floppy Disc.
- 2.2 Function and leakage
 - 2.2.1 Attach continuity meter to breakwire leads for continuous monitoring.
 - 2.2.2 Increase pressure in the chamber at a steady rate until tripline deploys or to 300+10 psi.
 - 2.2.3 Close shutoff valve to chamber and start Nicolet Oscilloscope trace.
 - 2.2.4 Record pressure trace on Floppy Disc.
 - 2.2.5 Pull trip line along longitudinal axis of sensor and record the force to break the break wire and the force to break the trip line.
- 2.3 Repeat (2.1) and (2.2) on 35 sensors at ambient temperature $(75\pm10^{\circ}F)$.
- 3.0 Fixture Design

The fixture design is shown on the attached drawing.

4.0 Pass/Fail Criteria.

There is no pass/fail criteria.

Submitted by: J. E. Funk Principal Engineer ١.



ATTACHMENT II

OEXM 32211 Page 1 of 2

TEST PLAN

GEMMS/ERTS LANGLIE TEST

1.0 Purpose

The purpose of the test is to determine the pressure level/pulse time characteristics to produce trip line deployment.

- 2.0 Test Procedure
 - 2.1 Test A
 - 2.1.1 Adjust pressure input solenoid to produce a square wave pulse of 50+5ms duration. Check that pressure rise and fall rates are 50 psi/ms minimum.
 - 2.1.2 Adjust pressure input level desired. (Estimate expected release level from results of leakage test for first trial).
 - 2.1.3 Install sensor in release fixture, pressurize and record result.
 - 2.1.4 Repeat 2.1.2 and 2.1.3 (for a total of 30 units) using the Langlie test procedure per MIL-STD-331A and a new sensor for each trial.
 - 2.2 Test B
 - 2.2.1 Repeat 2.1 except the pulse duration will be adjusted to 75+5 ms duration.
 - 2.3 Test C
 - 2.3.1 Repeat 2.1 except the pulse duration will be adjusted to 100+5 ms duration.
- 3.0 Fixture Design

The fixture design is shown on the attached drawing.

4.0 Pass/Fail Criteria

There is no pass/fail criteria.

Submitted by: J. E. Funk Principal Engineer



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Notion Senser

Distribution List

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Commander Armament Research and Development Center U.S. Army Armament, Munitions and Chemical Command ATTN: DRSMC-TSS(D) (5) DRSMC-LCU-CM(D) (2) Dover, NJ 07801

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