Expanding Plastics Recycling Technologies: Chemical Aspects, Technology Status and Challenges

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Abstract

Less than 10% of the plastics generated globally are recycled, while the rest are incinerated, accumulated in landfills, or leak into the environment. New technologies are emerging to chemically recycle waste plastics that are receiving tremendous interest from academia and industry. Chemists and chemical engineers need to understand the fundamentals of these technologies to design improved systems for chemical recycling and upcycling of waste plastics. In this paper, we review the entire life cycle of plastics and options for the management of plastic waste to address barriers to industrial chemical recycling and further provide perceptions on possible opportunities with such materials. Knowledge and insights to enhance plastic recycling beyond its current scale are provided. Outstanding research problems and where researchers in the field should focus their efforts in the future are also discussed.

1.0 Introduction

Plastics have revolutionized our society, allowing us to inexpensively make a variety of materials that have a myriad of uses throughout industry. The first three synthetic plastics were polystyrene (PS) in 1839, polyvinyl chloride (PVC) in 1835 and Bakelite in 1907. Industrial plastic production really began to expand about 1950 when global plastic production reached 2 million tons/yr. Current global plastic production is around 380 million tons/yr and it is estimated that humankind will have produced more than 30,000 million tons plastics by the end of 2050. The growth in plastic production is occurring for three likely reasons²⁻⁴: 1) new plastic materials (made by both changing the structure and processing conditions of the plastics) allow for the use of plastics in new applications, 2) the developing world is using more plastics as their economy improves, and 3) the decreasing cost of plastic production due to cheap fossil feedstocks.

Figure 1 shows a Sankey diagram for the production, utilization and recycling of packaging plastics adapted from the Ellen McArthur Foundation.⁵ This shows that 32 percent of all plastics is mismanaged (littered or inadequately disposed).⁶ Between two to five percent of plastics are transported into the ocean through riverways.⁶ Any plastic waste on land has the potential to eventually reach the ocean as the ocean is the ultimate sink of the earth.⁷ In the environment, plastics will slowly degrade into microplastics which are plastic fragments less than 5 mm in diameter. Recently, microplastics were even found in the troposphere.⁸ Microplastics can also enter the environment from the degradation of plastic clothing into wastewater.⁹ Degradation mechanisms include weathering, leaching, fragmentation and potentially assimilation and mineralization. Plastic leaks into the environment through improper disposal, transport of plastics from collection sites to a central facility, and leakage from the solid waste facilities. Ocean plastics have two well-studied impacts on marine and freshwater animals: waste ingestion-egestion of plastics and entanglement in plastic waste.⁷

Forty percent of plastics is landfilled. Developed countries often have landfills with thick plastic covering which prevents leakage into the environment. However, less developed countries often have open landfills where plastic can easily leak into the environment. In the US, which has a modern solid waste disposal infrastructure, it has been estimated that 0.98-1.26 million metric tons of plastic (or 2.33-2.99% of plastic waste generated) leak into the environment. Large amounts of plastics wastes are also released into the environment during natural disasters. For example, in 2011 the Tohoku earthquake and tsunami in Japan deposited an estimated 5 million tons of debris into the ocean. By 2030, 58.4 million tons of plastics will be added to the oceans each year around the world.

Fourteen percent of plastics is burned for energy recovery. While this does not create a solid waste problem, it does generate greenhouse gases. Fourteen percent of plastics are "recycled" with 8% being "cascaded recycled" to lower quality materials and only 2% of plastics used in closed-loop recycling where virgin plastics can be used. The amount of plastics recycled varies by countries with the US recycling 10%, China 30%, and the EU 31% of plastics consumed. As will be discussed in this review, the low amount of recycled plastics is due to several reasons including: 1) plastics have a wide variety of compositions, 2) the high cost of collecting and sorting different types of plastics, especially the removal of contamination, and 3) the high capital costs and technological uncertainties of more "advanced recycling option". Recent changes in legislation along with the desire from consumers for more sustainable products has created a dramatic push by industry for more advanced plastic recycling technologies. IHS Markit has projected that \$300 billion of capital spending that is earmarked for new plastic production capacity should be redirected to plastic recycling technologies to meet circular economy goals. 12

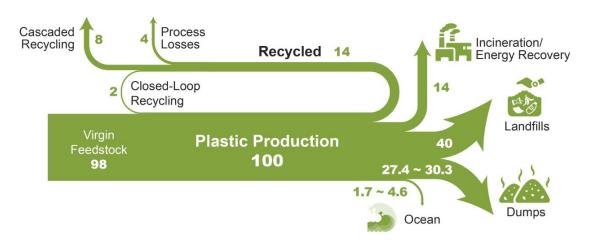


Figure 1. Sankey Diagram showing the life cycle of plastic packaging.⁵

Figure 2 shows the current and future infrastructure for plastic recycling technologies. The first step in plastic recycling is the sorting of plastic wastes into different streams through the material recovery facility (MRF). The MRF sorts out the glass, metals, carboard, and plastics, bails them, and then sells them to a downstream recycler. Plastic wastes can be divided up into four areas: post-industrial waste (PIW), post-consumer waste (PCW), plastics that are present in municipal solid wastes (MSW), and ocean plastics. PIW is typically of more uniform composition and lower in contaminants than the other types of plastic wastes. Oftentimes industry will recycle PIW in closed-loop recycling processes. However, PIW often contain multi-layer films which cannot be recycled by mechanical recycling due to material incompatibility. The current plastic recycling infrastructure is primarily focused on mechanical recycling of rigid #1 and #2 plastics. MRFs do not collect flexible films or textiles as this will clog the equipment. Ocean plastic waste is not currently collected at any large scale. MSW is primarily sent to landfills although some "dirty MRFs" can process these streams as well.

As shown in Figure 2, several technologies currently exist to chemically recycle plastics. Plastics can undergo thermal degradation to produce a liquid known as pyrolysis oil. Pyrolysis oil can be converted into aromatics and olefins by either steam cracking or using a form of catalytic upgrading as discussed in Section 5.0 and 6.0. This produces aromatics and olefins which can then be re-used to make new recycled plastics that have the same properties as the virgin plastics. Multilayer-plastics can be processed via dissolution-based recycling approaches generating pure plastic flakes which can then be re-extruded into recycled plastic resins. Polyesters and polycarbonates can be chemically or enzymatically (Section 9.0) converted into their monomers by methanolysis and other technologies. These monomers can then be re-used to remake the polymers. Plastics can also be gasified to synthesis gas which can be used to make methanol or transportation fuels as discussed in Section 7.0. Methanol can then be converted into aromatics and olefins.¹³ Other approaches to recycle plastics, primarily being studied in academia at present, include hydrogenolysis to produce lubricants and oils, functionalization of plastics, and the creation of plastic alloys as discussed in Section 10.0.

Sorting, recycling, disposal, and product redesign in the management of waste plastics have been reviewed. 14-22 The objective of this review is to first describe current plastic recycling infrastructure followed by a discussion of the chemistry, engineering, and technology of advanced

plastic recycling. We first review the manufacture of plastics (Section 2.0), landfilling of waste plastics and MSW sortation (Section 3.0), and mechanical recycling of waste plastics (Section 4.0). We then summarize the technologies that are being used or developed including pyrolysis (Section 5.0), liquefaction (Section 6.0), gasification (Section 7.0), dissolution-based approaches (Section 8.0), PET conversion to monomers (Section 9.0), followed by other catalytic processes for plastics conversion (Section 10.0). Conclusions and outlook are provided in Section 11.0.

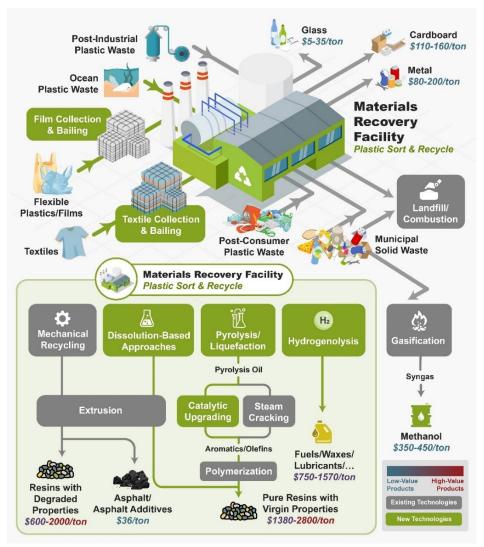


Figure 2. Summary of current management system of waste plastics.

2.0 Manufacture of Plastics and the Environmental Footprint of Plastics Disposal

2.1 Plastic Industry Supply Chain

2.1.1 Supply Chain of Plastics

Figure 3 depicts the current supply chain for production of virgin plastics. Natural gas and naphtha (a certain boiling fraction of crude oil) are the two main feedstocks. PET (#1) is formed from ethylene glycol (EG) and terephthalic acid (TPA) while both HDPE (#2) and low-density polyethylene (#4 LDPE) are produced from ethylene. Ethylene can also be used to produce vinyl

chloride monomer, which in turn is the key precursor to PVC (#3). Polypropylene (#5 PP) and PS (#6) are made from propylene and benzene with ethylene, respectively. #1-#6 plastics meet the majority of demands, and the rest is fulfilled by other plastics (#7 plastic). Typically, these resins are inexpensive and easy to process.

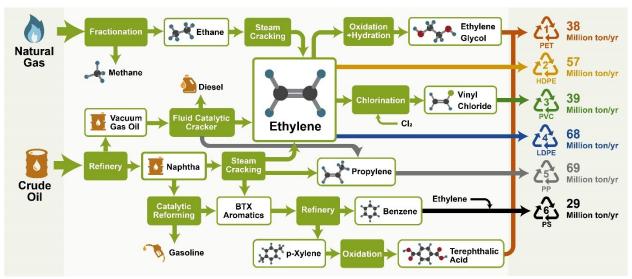


Figure 3. Supply chain of the manufacture of #1-#6 plastics and their volume of production in 2019. ¹⁹

The chemical process of polymerization is not the same for all plastics, since the reaction is dependent on monomer chemistry and controlled by several conditions such as temperature, pressure, monomer concentration, and desired end use well as by structure-controlling additives including catalysts, activators, accelerators, initiators and inhibitors.²³ There are two basic classifications that encompass most polymerization schemes: step growth (condensation) and chain growth (addition) polymerization. Linear and non-linear step growth polymerizations are processes in which the polymerization occurs through the reaction of more than one molecular species. On the other hand, chain polymerization processes occur with monomers that have an unsaturated group. For example, polyethylene (PE) is produced from the polymerization of ethylene (or ethene, olefin) monomers through polyaddition either from the radical polymerization of ethylene monomers or by using Ziegler-Natta or metallocene catalysts. Table 1 lists the various polymerization mechanisms and some examples of their polymer products.

PP, the most widely used thermoplastic globally, is exceptional due to its production cost-effectiveness and wide applications, such as flexible barrier film pouches, caps, closures, and containers. LDPE, the second most widely used resin, is typically used to make plastic films, and injection- or blow-molded products, such as wash bottles and computer hardware covers and packaging. HDPE is typically used as fibers for industrial plastics, pipes and tubing, and consumer products, such as containers. These polyolefins account for almost 48% of global plastic demand.²⁴

Copolymerization is used to manipulate the properties of manufactured plastics to meet specific requirements and industrial needs, allowing for the improvement of mechanical and chemical properties.²⁵ Through manipulation of monomer chemistry, more customized materials like copolymers have been formed and successfully introduced commercially, such as acrylonitrile-butadiene-styrene (ABS), styrene-butadiene copolymer (SBR), nitrile rubber (NR), styrene-acrylonitrile (SAN), styrene-isoprene-styrene (SIS), and ethylene-vinyl acetate (EVA), all

of which are formed through chain growth polymerization. Linear low-density polyethylene (LLDPE) is produced by polymerizing ethylene with 1-butene and smaller amounts of 1-hexene and 1-octene, leading to a product that is structurally similar to LDPE but with short, uniform branches, leading to improvements to the polymer's mechanical and chemical properties. Step growth polymerization has been used to produce the most polyamides, e.g., nylon-12 and 66 polymers, as well as the PET family. These polymers consist of at least two types of constituents (monomers, e.g., dicarboxylic acids and dialcohols) and can be classified depending on the repeat unit structure.

Table 1. Polymerization classification and inhibitors.²³

Classification	Polymerization	Examples		
		Polyamides (PA)		
	Polycondensation	Polycarbonate (PC)		
Step Linear		Polyesteramide (PEA) Polyetherimide (PEI)		
	Polyaddition	Polyethylene (PE)		
C N 1	N. 1 D 1	Epoxy resins (EP)		
Step Non-linear	Network Polymers	Melamine Formaldehyde (MF)		
		Polymethylmethacrylate (PMMA)		
	Free radical	Polyvinyl acetate (PVAC)		
		Polystyrene (PS)		
		Polyvinyl chloride (PVC)		
	Cationic	Polyisobutene (PIB)		
	Anionic	Butadiene Rubber (BR)		
Chain	Amonic	Polymethylmethacrylate (PMMA)		
		Polyamide from e-caprolactam (PA6)		
	Ring opening	Polycaprolactone (PCL)		
	King opening	Polyethylene oxide (PEO)		
		Polypropylene Oxide (PPO)		
	Ziegler-Natta	Polyethylene (PE)		
	Metallocene	Polypropylene (PP)		

2.1.2 Steam Cracking to Produce Plastic Feedstocks

As shown in Figure 3 the first step in the production of olefins is steam cracking of either ethane (for ethylene production) or naphtha. Figure 4 is a simplified flowsheet diagram of a steam cracking unit when naphtha is the feed, which we will describe since it can be used in chemically recycling of plastic pyrolysis oils. The feed is mixed with steam and heated by flue gas from the process in the convection zone. Before leaving the convection zone, the hydrocarbon stream is heated to 500-680 °C, which is the incipient cracking temperature range. After entering the tubular reactor of the radiant zone, the stream is heated to 750-875 °C in 0.1-0.5 s. During this short residence time, the feedstock is cracked into smaller molecules, including ethylene and propylene,

and other byproducts. In a steam cracker, the reaction follows a free radical chain mechanism. For this reaction scheme, there are hundreds of radical and molecular species and thousands of reactions between them. The chain reactions of ethane as the feedstock can be found in SI 2.0.

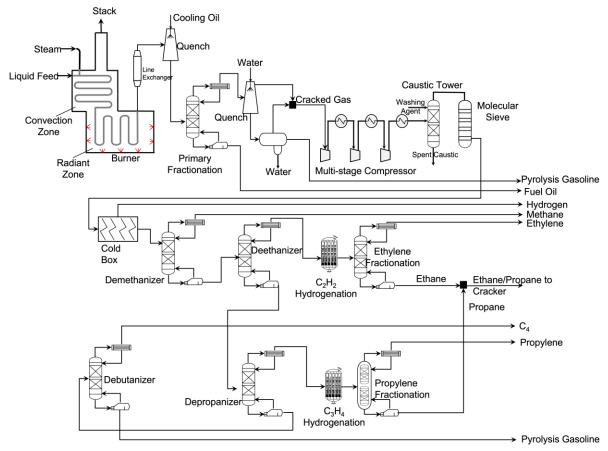


Figure 4. A simplified process flowsheet diagram of steam cracking. 27-29

When the feedstock is naphtha, a similar free radical reaction mechanism occurs. Adding steam to the steam cracker facilitates the control over residence time, prevents coke formation, and reduces hydrocarbon partial pressure. Steam does not participate in the free radical reaction mechanism. Its main role is to react with coke to form CO and CO₂. Since the cracking process is highly endothermic, energy is input from burners in the radiant zone.

The effluent stream from the cracking furnaces is cooled by a transfer line exchanger (TLE) where feed water is vaporized, and high-pressure steam is generated. Then the cracked gas is further cooled by contact with cooled oil in a quench tower. The resulting stream is sent to a primary fractionation column where fuel oil is obtained at the bottom. The stream on the top is further cooled down using a quench water tower. On the bottom of this quench tower, a three-phase separator splits water, liquid, and gas hydrocarbons. The liquid hydrocarbons are collected as gasoline-ranged products that is heavy in aromatics. These aromatics are also used to produce other types of plastics. On the top of the quench water tower, gas effluent is obtained and mixed

with gas effluent of the three-phase separator. This stream contains light hydrocarbons, including ethylene and propylene.

After compressing the cracked gas with a multi-stage compressor, the gas is sent to an acid-gas removal unit where CO₂ and H₂S are removed. After drying the purified gas with a molecular sieve dryer, the cracked gas is sent to the cold box where it is cooled down to -156°C. Under these conditions, hydrogen is recovered for use in hydrogenation of C₃H₄. The separation of hydrocarbons starts from a demethanizer where methane is removed. This methane stream is supplied to the cracker as fuel gas for providing the reaction heat. The bottom stream of the demethanizer is sent to a deethanizer where ethane or lighter components are obtained. To convert acetylene into ethylene, this C₂ stream is hydrogenated and fractionated cryogenically. The ethylene fractionator column splits ethylene and ethane. The ethane is mixed with propane and recycled back to the cracker. On the bottom of deethanizer, C₃ and heavier components are obtained and sent to a depropanizer where C₃ and C₄/heavy fractions are separated.

After hydrogenating methylacetylene and propadiene, the C₃ stream is split into propylene and propane. The propane is recycled back to the cracker. Meanwhile, the C₄ and heavier components stream is sent to a debutanizer where butylene/butane and gasoline-ranged products are obtained. When ethane/propane are fed, no primary fractionator is needed. The gas cleaning and separation processes are very similar to the above one when feeding the cracker with ethane only. Information related to steam cracking facilities in US can be found in SI 2.0.

2.2 Plastics Processing

The conversion of the raw or virgin plastics into finished products involves a series of plastic manufacturing processes. These manufacturing processes will vary depending on the type of plastic (thermoplastic, thermosetting, or elastomeric) and the final product desired. Plastic manufacturing can be commonly divided into three stages. The first stage is the compounding of the raw plastic with additives to achieve the desired material properties. For example, PE and PP films often stick together, which makes them difficult to separate, as when opening a PE bag. Anti-blocking agents (such as limestone and talc) can be added to lower the blocking force between the film layers. Table 2 lists the most common additives and their classifications. The compounding process is highly complex and involves taking into consideration the effect of all the additives utilized on the final properties of the plastic product. More often, a plastic will contain several additives to aid the processing of the material, modify color, and achieve the required mechanical properties. These formulations tend to be proprietary and will vary depending on the manufacturer.

Table 2. Plastic additive classifications and common examples.³⁰

Additive Classification	Common Agents		
Anti-blocking Agents	Limestone Synthetic Silica Gel Natural Silica Talc		
Slip Additives	Erucamide Oleamide Stearamide		
Plasticizers	Dioctylphthalate (DOP)		
Antioxidants	Hydrogen Donors – Phenols Hydroperoxide Decomposers – Phosphites and Phosphonites Alkyl Radical Scavengers – Hindered Amine Stabilizers and Hydroxyl Amines Metal Deactivators		
Flame Retardants	Aluminum Hydroxide/Oxalate Zinc Borate/Chloride/Sulfide Alumina Trihydrate		
UV Stabilizers	Sterically Hindered Amines (HALS) Carbon Black		
Antistatic Agents	Fatty Acid Esters Ethoxylated Alkylamines		
Antimicrobial Agents	10,10'-oxybisphenoxarsine (OBPA)		
Antifogging Agents	Glycerol Esters Polyglycerol Esters Alcohol Ethoxylates		
Chemical Blowing Agents	Azodicarbonamide Carbonates Semi-carbazides		
Colorants	White – Titanium Dioxide, Zinc Oxide Black – Spinel Black, Iron Oxide Black Yellow-Orange – Iron Oxide Yellow, Zinc Ferrite Brown – Chrome Iron Brown, Rutil Brown Red – Iron Oxide Red, Cadmium Orange Green – Chrome Oxide Green, Cobalt Spinel Green Blue – Cobalt Blue, Ultramarine Blue Metallic – Aluminum, Copper		
Fluorescent Whitening	Bis-benzoxazoles		
Agents	Phenylcoumarins		
Fillers	Glass Talc Ceramic Porcelain Clay		

The second stage, called forming, involves imparting the desired shape on the material. An inherent requirement of this step is that the material must be able to maintain this shape after the step is completed. Synthetic fibers, typically polymerized from petroleum-based chemicals, are formed through extruding a plastic solution or melt through a spinneret, a process known as spinning. This liquid-to-fiber formation process can be compared to the spinning of cotton candy. Depending on the type of spinneret used, either solid or hollow fibers can be formed. Synthetic fibers account for about half of all fiber usage, with applications in every field of fiber and textile technology. Nylon, polyester, acrylic, and polyolefin-based synthetic plastics dominate the market with these four accounting for approximately 98% of synthetic fiber production. Polyester alone accounts for around 60%. The final stage involves finishing the piece, which includes machining, decoration, and assembly. Plastics processing and manufacturing has greater opportunities for cost-savings through minimization of finishing processes as compared to the manufacture of more traditional materials. Table 3 lists common methods attributed to the three stages of plastics manufacturing.

Table 3. Typical stages in the plastics manufacturing processes.

Stage	Methods		
Compounding	Powder, Melt, Dispersion, Solution		
Forming	2-D: Extrusion, Calendering, Coating, Spinning		
	3-D: Thermoforming, Molding (Compression, Transfer, Injection, Blow)		
Finishing	Machining, Decoration, Assembly		

For polymeric materials, it is typical for a particular product to require multiple forming processes for ease of transfer and shipping (such as extruding a tube, then pelletizing for shipping and further use) or to carry out a specific chemical process (such as crosslinking or vulcanization). These forming processes typically involve the softened stage of the polymer, which is achieved by heating the polymer material. Each forming process will impact a thermal history and, in the case of reactive polymeric systems, will impact a degree of cure. These repeated forming processes will influence the properties of the material, either through the degradation of the material or unwanted side reactions. Setting the shape of the product is typically achieved either by cooling (which can cause crystallization, further impacting material properties) or a chemical process (crosslinking) to achieve dimensional stability. Table 4 demonstrates the most common plastics processing techniques used to form and set material shapes.

Table 4. Important plastics processing techniques.

Processing Method	Description			
Extrusion	Thermoplastic granules are forced through a heated barrel and the plastic melt is squeezed through a die with the desired profile for the extruded component. The extruded material is cooled as it leaves the die, then cut to the desired length.			
Spinning	A specialized form of extrusion that utilizes a spinneret to form multiple continuous filaments. Extruded liquid plastic filament is continuously drawn and simultaneously solidified to form a continuous synthetic fiber.			
Blow Molding	Compressed air is introduced underneath a warmed sheet of thermoplastic material, forcing the material into a cavity or allowing it to expand freely.			
Vacuum Forming	A sheet of plastic is set over a mold, where it is warmed and softened. Air drawn from under the softened plastic sheet, which forces it over or into mold by atmospheric pressure.			
Plastic material is first extruded as a tube shape into an open die. T Extrusion Blow Molding then closed to seal the ends of the tube and air is blown in, forcing the tube to take the shape of the die cavity.				
Injection Molding	Granulated plastic is heated until a melt is formed. The melt is then injected into a closed mold using high pressures and cooled inside the mold.			
Rotational Molding Plastic is placed in a closed mold that is heated and rotated slowly are vertical and horizontal axis. The plastic material melts and sticks to mold surface, building up the required thickness. The mold is gradually while rotating.				
Foaming	The base plastic is mixed with foaming/blowing agents. When heated, these agents release gas which form bubbles in the plastic. A separate method is to inject compressed nitrogen gas into molten plastics during the molding process.			
Calendering A thermoplastic melt is extruded onto heated rotating rollers whice the material into a continuous sheet or film.				
Compression Molding A thermosetting plastic charge is placed into a preheated low The mold is then closed and subjected to further heat and combined pressure and heat caused polymerization and the plasticized material within the mold.				

2.3 Mechanical and Thermal Properties

Most plastics produced are often specifically designed to serve very particular applications. Figure 5 demonstrates material properties and pricing of thermoplastics, aluminum, and ceramics compared to steel. During the forming of the product, it is standard for manufacturers to use additives to manipulate the properties of the raw material to achieve particular characteristics or homogenize the characteristics of their material batches as shown in Table 2. These additives influence the mechanical and thermal properties of the plastics, either by manipulating the glass transition temperature, imparting higher chemical resistance, increasing impact strength and elasticity, among other things.³¹ Figure 5 demonstrates average mechanical properties and pricing of common commercial plastics. Many commercial plastics will have different characteristics from those of the base plastic, even though they may have the same chemistry. In general, it is important to understand that many plastics are technically combinations of several materials. As a result,

mechanical and thermal properties are influenced by each component. Often, manufacturers change additives or blend ratios due to environmental concerns, to enhance specific properties, or simply for more economical processing. These subtle changes and introduction of new materials and compounding may drastically change one or more engineering properties; because of this, it is of utmost importance to continually test and evaluate commercial plastics and their specifications. Table 5 contains thermal and mechanical properties for common commercial plastics. It is of note that these properties are averages and specific material formulations can manipulate these properties for specific applications.

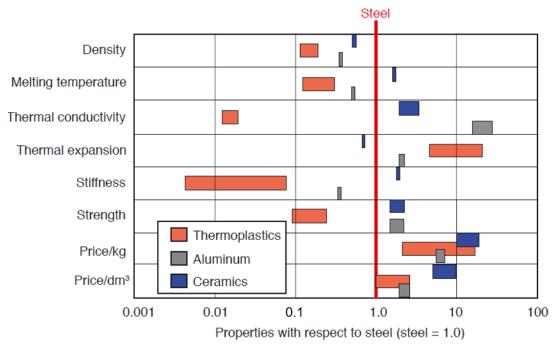


Figure 5. Properties of thermoplastics, aluminum, and ceramics with respect to steel. Published with permission from ref ³². Copyright Carl Hanser Verlag, Munich 2012.

Temperature can have varying effects on polymer products, from melting to degradation to morphological transitions.³³ Temperature can also affect mechanical properties due to enhanced polymer chain movement and free volume. Two key temperatures describe these effects: the glass transition temperature and melting temperature. The glass transition temperature is a property of the amorphous region of the plastic, whereas the melting point is property of the crystalline regions. At temperatures below the glass transition temperature, the molecules in the amorphous region exist in a frozen state where movement is minimized and the polymer chains can vibrate slightly. This is typically referred to as the plastic's glassy state. The rubbery state occurs when the plastic is heated above the glass transition temperature, allowing the polymer chains to move and shift around each other, which in turn allows the plastic to become soft and flexible. Glassy (amorphous) plastics exposed to heat eventually soften and flow into a viscous liquid.

Table 5. Morphological, thermal, and mechanical properties of common plastics.⁷⁻⁸

Material	Morphology	Density [g/cm³]	Glass Transition Temperature [°C]	Melting Temperature [°C]	Decomposition Temperature [°C]	Tensile Strength (MPa)	Tensile Modulus (Mpa)	Strain at Break (%)
ABS	Amorphous	1.03 – 1.07	-85/95 — 105/125	-	420 – 428	32 – 45	1300 – 2700	15 – 30
EVA	Semi- crystalline	0.92 – 0.95	-40 – 20	30 – 110	345 – 360/ 470 – 480	18 – 35	7 – 120	600 – 900
LDPE	Semi- crystalline (40% – 55%)	0.91 – 0.93	-130100/ -3010	100 – 115	487 – 498	8 – 23	200 – 500	300 – 1000
LLDPE	Semi- crystalline	0.91 – 0.94	-130100/ -7025	122 – 127	475 – 485	-	-	-
HDPE	Semi- crystalline (60% – 80%)	0.94 – 0.96	-130 – -100	125 – 135	480 – 498	18 – 35	700 – 1400	100 – 1000
UHMWPE	Semi- crystalline	0.93 – 0.94	-130 100	130 – 145	480 – 490	-	-	-
PLA	Semi- crystalline	1.21 – 1.43	45 – 65	150 – 160	350 – 375	-	-	-
PP	Semi- crystalline	0.90 – 0.91	-20 – 20	160 – 165	450 – 470	21 – 37	1100 – 1300	20 - 800
PS	Amorphous or Semi- crystalline	1.05	80 – 105	-	415 – 425	45 – 65	3200 - 3250	3 -4
PVAL	Semi- crystalline	1.21	70 – 100	220 – 260	260 – 320/ 420 – 450	-	-	-
PVC- Plasticized	Amorphous	1.16 – 1.35	-50 – 80	-	$\begin{array}{c} 290 - 315/ \\ 460 - 475 \end{array}$	10 – 25	-	170 – 400
PVC- Unplasticized	Amorphous	1.38 – 1.55	80 – 90	-	285 – 315/ 460 – 475	50 – 75	1000 – 3500	10 – 50
PA6	Semi- crystalline (30% – 40%)	1.12 – 1.15	45 – 80	225 – 235	445 – 460	70 – 85	1400	200 – 300
PA66	Semi- crystalline (35% – 45%)	1.13 – 1.16	65 – 90	225 – 265	430 – 473	77 – 84	2000	150 – 300
PC	Amorphous	1.20 – 1.24	140 – 150	-	480 – 535	56 – 67	2100 – 2400	100 – 130
PET	Semi- crystalline	1.33 – 1.45	70 – 85	245 – 260	425 – 445	47	3100	50 – 300
PUR	Thermoset	1.10 – 1.70	10 – 180	-	240 – 350	70 – 80	4000	3 – 6
SBR	Rubber with hard and soft segments	0.94	-55 – -35	-20	435 – 470	26 – 38	1800 - 2500	25 – 60

Melting transitions in some plastics refers to the transition between a crystalline solid and a liquid. When a semi-crystalline plastic is heated about the melting temperature, it forms a viscous liquid and flows. Amorphous plastics do not experience melting since there are no crystal regions

to melt. For semi-crystalline plastics, crystallinity is dependent on the type and structure of the plastic. Crystallinity is typically induced by cooling a melt, although strain-induced crystallization may occur due to the molecular chains disentangling, unfolding, and straightening above its yield point. Molecular weight plays a large role in crystallinity and most polymeric properties. A plastic's tacticity will also influence its crystallinity, with isotactic plastics demonstrating higher crystallinity than syndiotactic plastics, and atactic plastics being considered uncrystallizable due to the lack of chain regularity. Strong intermolecular forces and a stiff chain backbone favor the formation of crystals, while bulky side groups and branching have the opposite effect, due to the difficulty in folding and aligning the chains along the crystal growth direction. Crystallinity highly influences thermal, mechanical, and physical properties since it impacts strength, toughness, and opaqueness depending on the degree of crystallinity. These properties are further varied by the plastic's chemistry, composition, and compounding, which in turn influence the molecular weight of the plastic. Figure 6 demonstrates the key characteristics of various amorphous and semi-crystalline plastics based on their performance and applications.

The mechanical properties of plastics are highly varied, although there are specific relations between plastic structure and their properties. A plastic's strength (tensile, compressional, flexural, torsional, and so on) depends on the molecular weight, presence of crosslinking, crystallinity, and structure. In general, a linear plastic has less strength than a branched plastic, followed by crosslinked plastics having greater strength, and network plastics exhibiting the highest strength. Low molecular weight plastics exhibit low strength, regardless of crystallinity, due to weak van der Waals forces and the ease of movement between chains, while high molecular weight plastics exhibit a greater degree of entanglement, which greatly increases the plastic's strength. Crosslinking increases the strength of the plastic by restricting chain motion, while crystallinity increases strength due to the significant intermolecular bonding. These properties are highly influenced by environmental and application factors such as loading, temperature, humidity, weather conditions, exposure, and time.

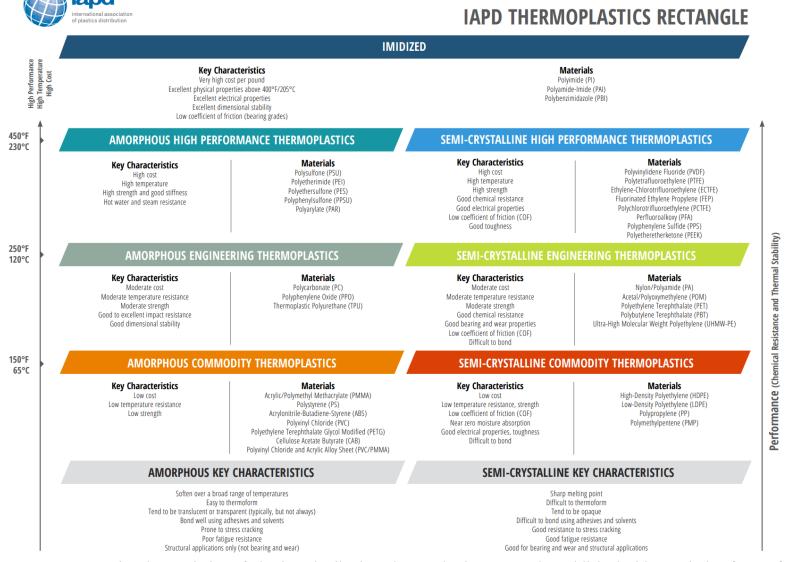


Figure 6. International Association of Plastics Distribution Thermoplastics Rectangle. Published with permission from ref ³⁴. Copyright 2021 International Association of Plastics Distribution.

2.4 Environmental Assessment on plastic production systems

Figure 7 presents the supply chain greenhouse gas emission arising in the production of major types of plastic. PET has the largest carbon footprint of these plastics. The equivalent GHG emissions for producing one kg of PET film is up to 4.5 kg, where 60% of the emissions result from the usage of processing fuel and 28% of emissions are from electricity usage. General-purpose (GP) HDPE has the lowest GHG emissions among the plastics listed. The production of injected molded (IM) LDPE tends to have a high emission associated with electricity usage (1.8kg eq CO₂/kg of plastic). In comparison with the GHG emissions of electricity and processing fuel, the emission associated with transportation is relatively low, and only corresponds to 9 to 18% of the emission of the plastic supply chain.

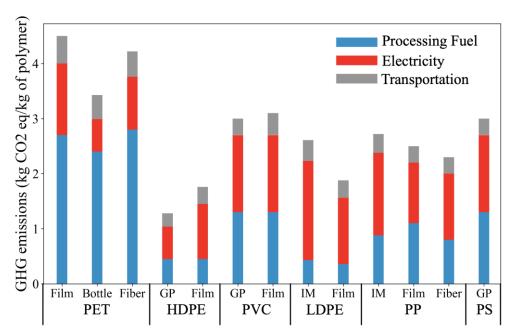


Figure 7. Supply chain GHG emissions arising in the production of different plastics. Published with permission from ref ¹⁴. Copyright Cell Press. LCA concepts were employed to estimate the cradle-to-gate energy requirement and GHG emissions. The GHG emissions associated with processing fuel and electricity correspond to the total energy consumption of the plastic supply chain. This includes emission associated with raw materials extraction, intermediate materials productions (e.g., monomer), and plastic production.

2.5 LCA on Plastic Recycling Technologies

In the past 17 years, 13 major life cycle assessment (LCA)/environmental assessment studies on recycling technologies and plastic waste disposal options have been conducted.³⁵⁻⁴⁷ These recycling/disposal options could be classified into four types: mechanical recycling, chemical recycling, incineration, and landfilling. These studies explored the environmental impact of each technology from greenhouse gas (GHG) emissions, water/air pollution, human health, and resource depletion perspectives. From these publications, some general conclusions can be made:

- (a) Climate change: Without considering the electricity credit, incineration of plastics has the highest greenhouse gas emission. The GHG emission of incineration ranges from 1.8~3 kg CO_{2,eq}/kg plastic wastes. ^{43, 48} However, accounting for the electricity credit lowers the GHGs of incineration to around 1.4 kg CO_{2,eq}/kg plastic wastes. Meanwhile, the chemical recycling technologies (e.g., pyrolysis, gasification) also have higher GHGs than the GHGs of mechanical recycling methods, due to the direct emission and electricity consumption. ⁴⁴
- (b) Acidification: Chemical recycling technologies tend to have high acidification potential. For example, gasifying one ton of plastic waste results in 0.49 kg emission of NO_x and 0.09 kg emission of SO_x.⁴⁸ However, after accounting for credit to avoid incineration of plastic waste, the acidification potential of chemical recycling options is lower than the acidification potential of producing virgin plastic from fossil fuel.⁴⁹
- (c) Air pollution: Incineration contributes to air pollution. The air emission of organic compounds is ten times higher than that of the air emission of pyrolysis (1.42 g emission of organic compounds per kg of plastic processed). Mechanical recycling has the lowest air emission among plastic disposal options.
- (d) Resource depletion: It is estimated that producing 1 kg of plastic requires 2 kg of crude oil, which is lost in cases where plastics are landfilled. Meanwhile, incineration also has high resource consumption, since the plastic is combusted for generating electricity. Among all the disposal options, mechanical recycling has the advantage in terms of natural recourse depletion. After accounting for the credit of avoided landfill or incineration, the amount of resource consumption of mechanical recycling (crude oil/gas) is even negative.

Incineration causes air pollution, CO₂ emission, and acidification of the disposal of plastic wastes. Although landfills tend to have low air pollution, they can cause soil and groundwater pollution. The available space for landfills is limited, even if parts of these areas can be reused in some cases.⁴⁹ Therefore, landfills are not a sustainable option. In comparison with chemical recycling, mechanical recycling has a lower energy consumption and a lower carbon emission. However, as will be discussed in Section 4.0, only a portion of plastic wastes can be mechanically recycled (e.g., PET and HDPE bottles). For plastics that cannot be mechanically recycled (e.g., plastic films), chemical methods are the most environmentally friendly approach.

3.0 Landfills, Disposal, and Sorting of Post-Consumer Waste Plastics

3.1 Landfill and Incineration

3.1.1 Municipal Solid Waste Overview

MSW is the aggregate of materials discarded from households, businesses, and institutions and consists primarily of readily degradable organic materials (food wastes, green wastes such as landscaping debris) and less readily degradable solid materials with potential for recycling (e.g., paper/cardboard, plastic, glass, wood and metal). Landfills also accept a variety of other materials specific to the locale, which are referred to as "special wastes." Wastewater treatment plant sludges, combustion wastes, and non-hazardous industrial wastes are examples of special wastes. Hazardous wastes and construction and demolition debris are not MSW, and are generally managed differently. The composition of MSW varies geographically and by income level (Figure 8), with the fraction of food and green waste decreasing as income level rises, replaced by a higher fraction of solid materials, particularly cardboard and plastics.

Plastics currently comprise 12% of all MSW generated globally.⁵⁰ In the US, only 9% of plastics are recovered through recycling, 16% incinerated, and 76% landfilled.⁵¹ The EU recycles 33% of plastics, with 43% incinerated, and 25% landfilled.⁵² Estimates for the cumulative global fate of plastics indicate 79% of plastics produced have landfilled or left in the open environment, whereas 12% have been incinerated, and 9% recovered for recycling.⁶

The UN Environment Programme and US EPA⁵³⁻⁵⁴ have established waste hierarchies focused on shifting from a philosophy of waste management to a philosophy of resource management in the context of a circular economy. The recommended hierarchy (highest to lowest priority) consists of waste prevention, waste minimization, reuse, recycling, energy recovery, and disposal (Figure 8). Most waste today, in the US and globally, is managed by disposal in landfills - the lowest priority in the hierarchy.

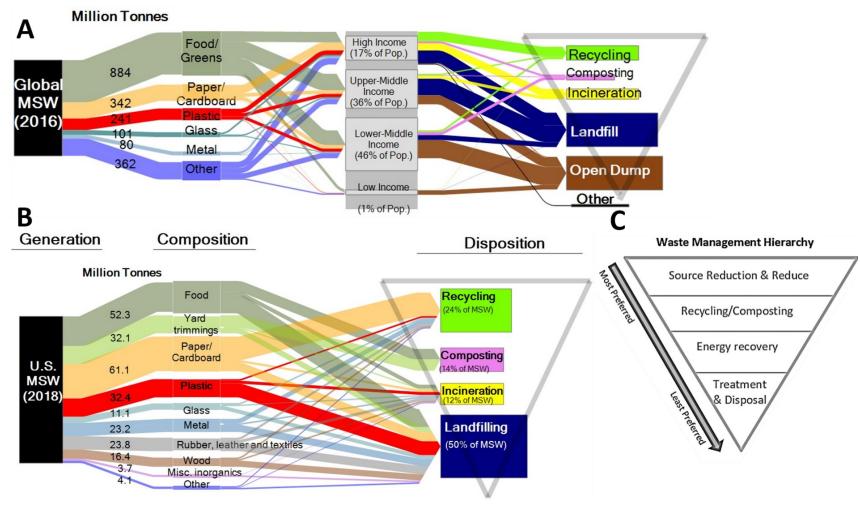


Figure 8. Municipal solid waste (MSW) generation and final disposition: (A) global generation in 2016 with fractions associated with national income, (B) US generation in 2018, and (C) waste management hierarchy. Inserted triangle illustrating how disposition pathways fit with preferred waste management hierarchy

3.1.2 Landfills

Landfills and dumps are the largest disposition pathway for MSW (Figure 8), primarily because this pathway is the least expensive and least cumbersome. Landfills and dumps have the common attribute of being a storage facility near the ground surface where waste is placed. However, a dump is an un-engineered facility with limited or no control on contaminated liquids or gases generated by the waste. In effect, waste is "dumped" and no longer managed. In contrast, landfills are engineered systems where liquids and gases are carefully managed so that impact on the environment remains within accepted norms. Dumps are more common in lower-income nations that lack the infrastructure and regulations for MSW management, although transitioning open dumps to engineered landfills has become a priority for some developing nations. ⁵⁵⁻⁵⁸ The remainder of this section focuses on landfills.

A modern engineered landfill consists of an engineered containment system situated in an earthen depression (Figure 9). The base is comprised of a multicomponent liner overlain by a leachate collection system. Waste is placed in layers approximately 3-4 m thick (called "lifts") that are compacted with heavy machinery. A gas collection system is installed in the waste to collect landfill gas (LFG) for treatment or production of renewable energy. Interim cover (soil or synthetic material) is placed over the waste during filling to reduce ingress of precipitation, control emissions and odors, and limit vectors. Once final elevations are met, a final cover is placed to limit the ingress of precipitation to *de minimis* amounts, facilitate gas collection, and provide separation from the surrounding environment for as long as the waste poses a threat. As with the liner, the final cover includes a multilayer hydraulic barrier overlain by a drainage layer. The surface is covered with vegetated cover soils for protection and aesthetics. descriptions of the surface is covered with vegetated cover soils for protection and aesthetics.

Leachate is generated when water percolating through the landfill contacts the waste. ⁵⁹ Leachate contains a variety of inorganic and organic contaminants, and therefore is treated before being discharged. Leachates are pumped from the leachate collection system, and generally are transported to a public wastewater treatment plant (a publicly owned treatment works, or POTW) where they are treated along with other wastewater (e.g., sewage from a community, etc.). In some cases, leachates are treated on site or are recirculated in the waste to stimulate waste decomposition to promote more rapid waste stabilization and greater gas production for renewable energy. ⁵⁵⁻⁵⁶

Landfills operate under anaerobic conditions where the microbial community decomposes the degradable organic fraction and generates gas comprised of approximately equal parts methane (CH₄) and carbon dioxide (CO₂).⁵⁶ MSW landfills are the third largest source of anthropogenic methane (CH₄) in the US⁵⁷ and contribute approximately 3% of global GHG emissions.⁶⁰ LFG also contains a variety of other contaminants in small quantities. Consequently, LFG must be treated before being released. Thermal treatment is most common, either through a flare or through combustion to create renewable energy (e.g., LFG to electricity). In recent years, landfills have also become a significant source of renewable natural gas (RNG), which is produced by treating and compressing LFG extracted from the landfill.⁵⁶

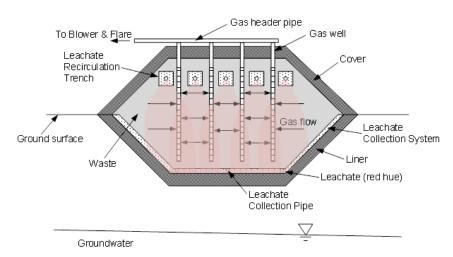


Figure 9. MSW landfill with liner, cover, leachate collection, leachate recirculation, and gas collection.

3.1.3 Incineration with Energy Recovery

Waste-to-energy (WtE) is the process of converting MSW into energy in the form of electricity, heat, or alternative fuels. Within a circular economy framework, WtE technologies have a crucial role in providing an alternative disposal option MSW that cannot be reused or recycled. The technical, economic, and environmental aspects of common WtE have been evaluated extensively. Astrup et al. Present a comprehensive review and comparison of WtE technologies. LCA methods were used to evaluate the environmental impacts of different technologies employed in WtE (e.g., plant type, energy recovery, type of energy output, flue gas cleaning, and residue types and management). Incineration is by far the most common technology for WtE, representing more than 88% of the global WtE market with a valuation of US\$ 50 billion predicted by 2027. The remainder of this section focuses on incineration.

Incineration is combustion of MSW at temperatures on the order of 750 – 1100 °C, with the heat being used to produce steam for generating electricity and/or heating. ⁷⁰⁻⁷¹ Plants producing steam for heating and electricity can have efficiencies on the order of 80%; whereas the efficiency is on the order of 20% for plants producing only electricity. 61 Most MSW incineration is conducted as mass burn (bulk MSW incinerated in a single chamber) or as refuse derived fuel (RDF) where screened and shredded MSW is combusted. 72 RDF is common in the Portland cement industry and can represent up to 80% of the thermal requirements in cement plants.⁶¹ Nearly 15% of all MSW is incinerated globally. Incineration rates vary significantly, with incineration more common in developed land-constrained countries and islands, 70 less common countries in developed countries without land constraints, and uncommon (<1%) in lower-middle and low-income countries. For example, Japan has significant land constraints and incinerates 74% of its MSW, 73 whereas the US has virtually no land constraints and incinerates only 12% of MSW. The effect of income is evident in the location of incinerators; 80% of MSW incinerators globally are located in North America, Europe, and Asia Pacific. 70 US incinerators manage 22% of discarded food and 16% of discarded plastics.⁷⁴ Most WtE incinerators in the US (77%) only generate electricity, 19% produce electricity and heat, and 4% export steam to local users.⁷⁵

Incineration reduces the mass and volume of MSW that is landfilled (70-85% by mass and 75-90% by volume 71 while generating energy for use or sale. Despite these advantages,

incinerators are difficult to implement, especially in the US. Emissions from MSW incinerators can contain dioxins and furans, which are toxic persistent organic pollutants and human carcinogens. These are pollutants are often of great concern to surrounding communities even when plants are in compliance with emissions criteria in the Clean Air Act. MSW incineration also generates ashes that need to be managed, generally through landfill disposal. Incinerator ashes tend to have higher levels of contaminants per unit mass than MSW, resulting in leachate with higher concentrations that requires more treatment. In some cases, ashes can be reactive, leading to heat generation that is problematic in landfills.

3.2 Material Recovery Facilities (MRFs)

Material recovery facilities, known as MRFs (pronounced "*murfs*"), receive waste material and separate (or bail) these materials. Their origin can be explained when terms such as municipal solid waste (MSW) and waste management began to be established in the 1950-60s, with the increased waste generation linked to economic growth and popularization of petrochemical derivatives. In the US, the first MRF was established in Groton, Connecticut in the early 1980s,⁷⁹ with the number of facilities multiplying in the following years. There were 40 MRFs in operation or under planning in 1991, 166 in 1993, and 307 in 1995.⁸⁰

MRFs are classified based on the input waste material they receive: single-stream, dual-stream, mixed-waste, or pre-sorted, with the first being a typical design in the US. Single and mixed-waste MRFs (containing more organic contaminants from MSW) have similar inbound composition, receiving a single stream with paper, plastic, glass, and metals, usually from automatic or semi-automatic vehicles. Dual-stream MRFs have a two-category stream line: fibers, composed of paper and cardboard, and containers, composed of plastic, metal, and glass, whereas pre-sorted MRFs receive source-separated material streams. Figure 10 is a block flow diagram for single-, mixed-, and dual-stream MRF frameworks (differences between operation modes are shown; otherwise, the process is the same for all) based on the work of Pressley, et al. who drew on common MRF designs around the US. The design of a MRF is unique to each location, with different specifications required and associated with inbound composition, investment capacity, and ownership and operation type.

Single and dual-stream frameworks have their advantages and disadvantages. Single-stream benefits from waste collection with larger volumes and lower costs but with increased difficulty and costs for processing at the MRF, in addition to an increased contamination rate. For example, during conversion from dual to single-stream, a MRF from Brookhaven (New York, US) observed a 25% increase in volume of input recycling streams, which led to a diversion of recyclable material from landfills from 50,000 to 35,000 tons, along with an increase in non-recyclables in the single-stream. Another study that investigated GHG emissions observed benefits from the conversion of three medium-size MRFs from dual-stream to single-stream systems, avoiding the emission of 711 kg-CO₂-equiv./metric ton. The advantages of switching from a dual to single stream were not observed on the economic side, as observed in a study conducted using data from 223 municipalities in the province of Ontario, Canada. For example, it was found that single-stream recycling incurs 48.7% higher processing costs and 9.6% lower values of a recyclable saleable stream compared to multi-stream recycling systems, with only a 3% reduction in the collection costs.

Specifications were determined in the US in an effort to standardize the inbound recycling streams at MRFs, such as those stipulated by the Institute of Scrap Recycling Industries (ISRI).⁸⁶ Table 6 describes the materials accepted, prohibited, and the possible contaminants in the majority

of US MRFs. It should be noted that plastic bags and films are considered contamination due to the possibility of issues during sorting and are removed early in the process. A pilot study conducted by Resource Recycling Systems (RRF) for the Materials Recovery for the Future (MRFF) on an existing MRF in Birdsboro (Pennsylvania, US) looked at how to modify an MRF design to accept flexible packaging from residential single-stream inbound waste. It demanded additional equipment for separation, with a processing cost of 2.41 USD/ton and a breakeven point compared with the sorted polypropylene market value.⁸⁷

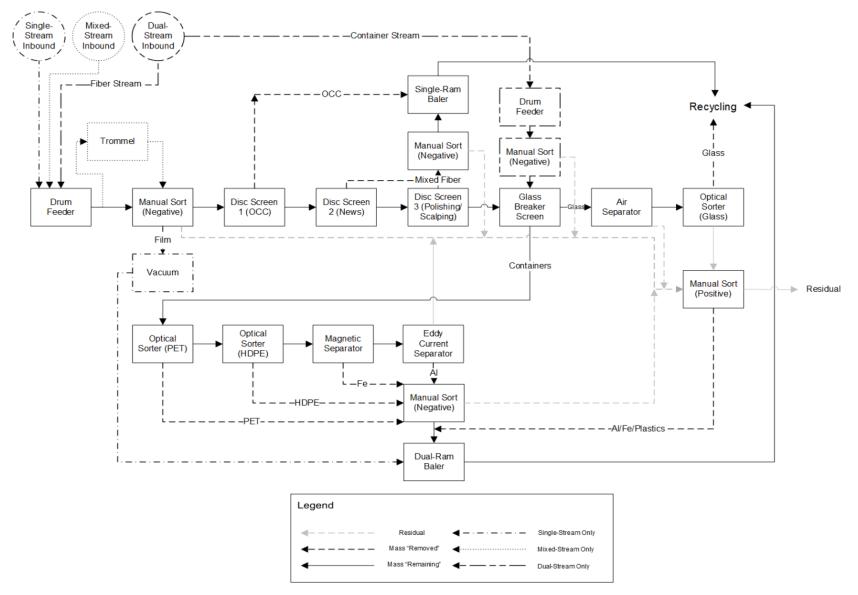


Figure 10. Block Flow Diagram of a single-, mixed-, and dual-stream MRF. Published with permission from ref ⁴². Copyright Elsevier.

Table 6. MRF inbound waste stream specification (ISRI).86

Allowed Materials Paper (Single Stream)	Plastic (Single Stream)	Metal (Single Stream)	Glass (Single Stream)	
Paper (Dual Stream – Separated)	Containers (Dual Stream – Not Mixed with Paper)			
Uncoated White Office, Printing, and Writing Paper Colored Paper	ng, and Writing (#2), PP (#5) Plastic Bottles, Jugs, Jars, and Containers Bulky Rigid Plastics such as Crates, Buckets, Totes, and Baskets Tubes and Lids bebooks and Junk Mail be boxes/rolls, paper and toilet paper rolls Cartons (#2), PP (#5) Plastic Bottles, Jugs, Jars, and Containers Bulky Rigid Plastics such as Crates, Buckets, Totes, and Baskets Cartons Aluminum, tin, steel beverage and product containers		Bottles and jars of any color	
Newspaper and Magazines Phonebooks and Junk Mail Tissue boxes/rolls, paper towel and toilet paper rolls Paperboard and Cardboard				
Brown or Kraft Paper Paper boxes/cartons, Pizza boxes (without food/liner)	rehish will be contate londfill			
Shredded Paper	which will be sent to landfill) Flexible Plastics (Plastic Bags and Plastic Film)	All metal except for those allowed	All glass except for those allowed	
Containers coated with wax, plastic or other materials	Expanded Polystyrene Foam (#6)		Drinking glasses, crystal, or tableware	
Wallpaper	Multi-layered juice pouches	Aerosol cans that are	Mirrors	
Material with excess food	Plastic form electronics	under pressure or partly filled	Non-container glass	
residue or other organic material	Plastic marked as biodegradable or compostable		Light Bulbs Windows	
Prohibited Materials				
pesticides, poisons, biohazar	s, radioactive materials, hazard rds, compressed gas cylinders, s, transformers, and ballast, asb	refrigerants, polychlorin	ated biphenyl	

3.2.1 Equipment Overview

Over the years, several new technologies have been applied to the equipment used in a MRF to increase sortation efficiency, maximize the recovery of marketable materials, and deal with the increased complexity and diversity of inbound waste streams. As a connector for the whole processing facility, conveyor belts transfer material between different equipment, sort stations, and storage areas, including infeed conveyors that receive the material from the tipping floor up to the conveyors carrying the final bales of material for shipping.

food waste, rock, dirt, asphalt, concrete, regulated materials, materials that can damage the equipment.

Two types of conveyors are usually used: rubber and chain belt conveyors. Rubber belts are divided into two categories: slider beds, where the belt moves through a flat or shaped trough

and is ideal for sorting with the material more spread-out, and idler conveyors, which have a belt over idler rollers perpendicular to the material movement, better suited for fine or gritty material. Chain belts conveyors are often employed when there is a need to move material through increased angles, such as feeding other equipment or weighty loads due to chain-link drive systems being more robust than rubber conveyors. The top speed for these conveyors is considerably slower.⁸⁸

After entering the MRF environment, the waste stream passes through multiple separation equipment and operations. The simplest method is known as manual sorting, a labor-intensive step in the MRF operation and a source of potential health and occupational hazards,⁸⁹ including physical, chemical, and biological concerns. The sorting can be divided into a negative sort when undesired materials are removed from the waste stream and a positive sort that looks for recyclables and placement into the correct bin.⁹⁰ For the separation involving multiple material sizes into a specific range, different types of screens are commonly employed, such as vibratory, disc, trommel, ballistic, and, more recently, auger screens, as described in Table 7.

Table 7. Common types of separation screens in MRFs. Published with permission from ref ^{88 91}. Copyright 2016 American Chemistry Council, CP Group Recycling Solutions.

Types	Description	Illustration
Vibratory (Shaking)	The screen can be horizontal or inclined, with the waste stream cascading through a series of finger elements, perforated plates, or meshes, promoting material separation. Presents better performance when operating with dry and cleaner waste, as it can be easily clogged.	
Disc	Rotating discs are positioned in shafts, moving the waste stream throughout the screen in horizontal or angled positions. The distance between discs (interface opening) is associated with the screened material size. Disc rolling might help by partially breaking the material on the screen. A specialized version of a disc screen that separates 2D (paper or film) from 3D materials (containers) can be called a polishing or planar screen.	
Trommel (Revolving)	Cylinder-mounted rollers in an inclined position contain holes in the sides and might have baffles. They are used for primary or final size screening. Factors that affect the input and separation efficiency include screen openings, trommel diameter, rotational speed, type and number of baffles, and cylinder inclination. Tumbling motion can be cascading, cataracting, or centrifuging.	
Ballistic	Combines parallel paddles that vibrate (similar to a vibratory screen) with a 2D/3D screen framework. Three flows are collected: a fines stream with material that passed through the paddles, a 2D stream with paper, cardboard, and films, and a 3D stream mainly consisting of containers.	
Auger	One of the newest types of equipment launched to the market consists of multiple cantilevered augers in corkscrewing motion, which prevents the wrap of plastic films and hoses. Mainly employed as a pre-sort step for removing large flat fractions such as (old corrugated containers) OCC from smaller objects.	

Air separation exploiting different densities of materials in mixed waste streams is another option at MRFs. A heavy fraction composed of metal, glass, and stones falls to the bottom of the equipment while a lighter fraction of paper, plastic, and dry organics is carried away by the air stream, requiring the use of a cyclone, for example, for the recycling of the air stream. ⁹⁰ Equipment in this category includes zig-zag classifiers, air-drum or rotary air, aspirator air or suction hood, cross-current air, and airbed classifiers. ^{88, 90}

Another crucial piece of equipment typically used for material sorting is the optical sorter. The use of this type of equipment can substitute for manual labor and lead to high sortation efficiencies; however, a significant capital cost is required for its installation, which hinders small and locally owned MRFs from selling bales in a market with low tolerance to contamination. An estimate using data from the United Kingdom by Eule showed that a MRF with a single operation shift could take up to 3.14 more years to break even after installing an optical sorter compared to manual labor.⁹²

Optical sorters use color-sensitive cameras and near-infrared (NIR) and ultraviolet (UV) spectroscopy sensors, or a combination of them, to identify different materials that pass through a conveyor belt. Once the material desired to be positively sorted is identified, air jets are activated to eject the piece to a different chute. 90,92 Spectrometric techniques exploit the unique wavelength signature of different kinds of materials. 88 NIR optical sorters are most commonly used for plastic separation as a non-destructive technique with high-speed measurement, penetration depth and signal-to-noise ratio. NIR optical sorter use has been growing for sorting fibers and cartons. Another advance in sorting technology is the use of hyperspectral imaging (HSI), which combines imaging from a digital camera with spectrometric analysis, to obtain a discrete spectrum for every pixel collected. This is then computationally analyzed using algorithms such as principal component analysis 94-95 for the sorting of more complex plastic streams containing low and high density polyethylene, for example. Machine learning algorithms are being studied to overcome some of the challenges associated with NIR sorters, 37 such as the difficulty of correctly sorting black plastics 80 or avoiding the still high costs of HSI technology.

For the sortation of ferrous materials, magnetic separators are used to sort materials such as steel from the remaining waste stream. Multiple factors are considered to determine the system's efficiency, including the distance between the conveyor carrying the waste stream and the magnet, the magnetic force employed, the conveyor speed, and the burden depth on the conveyor belt. Common types of setup include a drum holding magnet, a belt holding magnet, and a suspended type magnetic separator ¹⁰⁰. For non-ferrous materials, such as aluminum and copper, eddy current separators are used, often after the magnetic separator. The sorting is based on the eddy currents formed when conductive objects are close to a magnetic field (created using rotating magnets), with another magnetic field of opposite direction. According to Lenz's law, this creates a force that expels these objects from the initial magnetic field, giving them a different trajectory. Considering that less dense and conductive objects demand a lesser force, aluminum has the greatest potential for separation through this equipment since it has one of the highest conductivity/density ratios compared to other metals, such as lead, copper, zinc, and tin. ⁹⁰

At the end of the sorting process, each material stream is compacted or densified to reduce its volume to minimize storage space requirements and increase payload for recyclable material and residue transportation, significantly reducing costs. Balers are commonly used to reduce the bulk density of the material and can be divided into two different types: vertical balers, an option with reduced output but low costs, or horizontal balers, which are the most utilized in MRFs. Horizontal balers are usually single-ram or dual-ram (two-ram), with the first mainly used for fiber,

paper, and OCC output lines, while the latter is considered a multipurpose equipment utilized for plastic and aluminum outputs due to its capacity to produce more heavy and uniformly packed bales. ^{88, 102} Single-ram balers operate with the sorted material being pushed from a collection chamber into a narrow hopper, with the densified material moving continuously as more material is fed and tied with wires. On the other side, a dual-ram baler (Figure 11) has the main ram that loads the material into a chamber until the desired amount is achieved, while a secondary ram is responsible for moving the bale to a tying process. ⁸⁸

The Association of Plastic Recyclers (APR) has developed some specifications to standardize plastic bales and facilitate the sales between MRFs and recycled plastic reprocessors, brokers, or companies that can use them in their process. For rigid plastic containers bales, including natural and colored HDPE, PP, and #1-7 and #3-7 plastics, it is expected to have a bale density between 15 and 20 lb/ft³ (240 and 320 kg/m³), whereas, for a PET bottle bale, the targeted bale density is between 15 and 18 lb/ft³ (240 and 288 kg/m³), all using non-corrosive galvanized bale wires of 10-12 gauge (2.6-3.2 mm). The main products of a MRF are the bales of sorted material with the ultimate goal of producing saleable recycled material and the least amount of non-recyclable residues. In the optimal scenario, these residues can be used as fuel for waste-to-energy conversion, in anaerobic digestion or, in the worst case, be an expense for discard in a landfill. For plastic bales, the ISRI Scrap Specifications Circular defines standards for some of the most common types of bales from a MRF in terms of composition, contaminants, and prohibited items, as shown in Tables 8 and 9. The historical prices for some plastic bales are listed in Table 10.



Figure 11. Two-ram Baler from Machinex Recycling. Published with permission from ref ¹⁰⁴. Copyright Machinex Technologies.

Table 8. Outbound mixed plastic bale specifications (ISRI)⁸⁶

Bale Type	Material Description	Main Product	Allowed Contamination
#1-7 Bottles and	Rigid plastics, consisting of	Bottle and non-	5% wt. total, with less than 2% wt.
Small Rigid	at least 65% bottles, bulky	bottle	paper/cardboard and 1% wt. of
Plastic	rigid containers greater than	containers	metal/plastic bags/liquid/other
	5 gallons should be avoided		residues

#3-7 Bottles and Small Rigid Plastic	Rigid plastics without PET (#1) and (#2), bulky rigid containers greater than 5 gallons should be avoided	Bottle and non- bottle containers	5% wt. total, with less than 2% wt. paper/cardboard/metal and 1% wt. of liquid/other residues
Mixed Bulky Rigid (#2 and #5)	Large rigid plastics HDPE (#2) and PP (#5)	Bulky rigid plastic	15% wt. total, with less than 4% wt. for plastic/packaging items (#1, #3, #6, #7), 2% wt. of metals, glass, wood, liquid/other residues, paper/cardboard, plastic bags/sheets/films
Tubes and Lids (#2, #4, and #5)	Any whole container of HDPE (#2), LDPE (#4), and PP (#5)	Tubes and lids	10% wt. total, with less than 2% wt. of metals, liquid/other residues, paper/cardboard, injection-molded HDPE (#2), PET (#1) bottles and thermoforms, plastic/packaging items (#1, #3, #6, and #7)

Table 9. Outbound PET and HDPE plastic bale specifications by grade (ISRI).86

	Bale Grade	Grade A	Grade B	Grade C	Grade F
DET (#1)	Total Fraction (% wt.)	>94	93-83	82-73	<72
PET (#1)	Max. contamination (% wt.)	6	7-17	18-27	>28
HDDE (#3)	Total Fraction (% wt.)	>95	94-85	84-80	<79
HDPE (#2)	Max. contamination (% wt.)	5	6-15	16-20	21

Table 10. Historical prices for some plastic bales. 105

Materials		National Average Price (¢/lb)				
Year	2017	2018	2019	2020	2021	2022
Plastics PET (Baled)	11-16	14-17	9-15	6-11	7-26	18-25
Plastics Film (Grade A, sorted, 800+lb Bales)	8-11	8-12	9-12	8-11	11-21	21
Plastics Natural HDPE (Baled)	24-33	30-39	20-59	33-64	56-108	55
Plastics Colored HDPE (Baled)	13-17	14-17	10-16	4-14	17-58	20
Plastics Commingled (#1-7, Baled)	2-3	2-3	2	1-2	1	1
Plastics PP Post Consumer (Baled)	7-9	8-11	7-13	3-12	12-39	19-23
Plastics Polystyrene EPS (Baled)	2	2	2	2	2	2

3.2.2 MRFs in Europe vs the US (Typical size, numbers of MRFs in US)

According to the Environmental Protection Agency (EPA) there were 532 MRFs in the US in 2018 with an estimated daily throughput of 91,129 tons. ¹⁰⁶ The Recycling Partnership conducted another survey with data from Resource Recycling, initially finding 360 MRFs in the United States in 2019, a number that was updated in February 2020 to 367 after a verification conducted by The Last Beach Cleanup (a nonprofit 501(c)3 organization), with a spreadsheet available on their website ¹⁰⁷ and results published by Greenpeace. ¹⁰⁸ The distribution of MRFs across the U.S. is shown in Table 11. A list of the largest 75 MRFs in North America was published in 2019 by Recycling Today, with 65 located in the United States and 10 in Canada. The largest MRF was Sims Municipal Recycling's Sunset Park, located in New York, which shipped 241,884 tons in 2018. ¹⁰⁹ In England, data from the last quarter of 2019 totaled 85 regulated material facilities (>

1000 tonnes/year recyclables processed and required to submit their data to England's Environmental Agency), resulting in daily input of 9,237 tonnes. In Wales, there were 12 facilities in the same year, with daily input of 710.6 tonnes. ¹¹⁰ Ali and Courtenay ¹¹¹ observed from data that approximately 60% of United Kingdom MRFs have an annual capacity higher than 50,000 tonnes. Italy had 33 facilities for plastic sorting ("centri di selezione" - CSS) in 2020 associated with COREPLA (National Consortium for Collection and Recycling of Plastic Packaging) that receive a pre-sorted waste stream mainly composed of mixed plastics from 996 smaller and local sorting centers ("centri comprensoriali"). ¹¹²⁻¹¹³ Germany's federal statistics reported 987 waste sorting facilities in 2019, with a total input of 25,120,700 tonnes. ¹¹⁴ In France, it was reported that 399 waste sorting facilities ("centres de tri de déchets") were operating in 2016, receiving 11.1 million tons. ¹¹⁵

Table 11. Number of MRFs in the United States. 106-107

Dogion	Number of MRFs	
Region	EPA (2018)	The Last Beach Cleanup / Greenpeace (2020)
Northeast	128	66
South	142	107
Midwest	139	76
West	123	118
Total (U. S.)	532	367

3.2.3 Waste pickers in Latin America

In less economically developed countries, recycled material is typically manually removed from MSW by human "waste pickers". A key issue in MSW management and/or waste recycling in developing countries, is the role of waste pickers, who collect, haul, sort, and sell recyclable commodities from MSW. There are around 20 million people worldwide informally dedicated to waste recycling, which represents approximately 50% of the workers involved in waste management. In developing countries, this informal recycling sector recovers the largest fractions of recycled waste and in some cases, it is the only organized form of recycling. In Latin American waste pickers are recruited among vulnerable groups living under conditions of extreme poverty in communities that lack the educational, social, and psychological resources to prepare its citizens for more formal and remunerative employment. Another factor is the deficiency in MSW management systems in urban and rural areas. Under these conditions, waste collection and recycling offer waste pickers one of the few opportunities to support their families.

In this section we discuss waste pickers in PET recycling in Mexico to illustrate the challenges in Latin America. Mexico is the second largest PET bottle consumer in the world, mainly due to the high consumption of soft drinks and bottled water. The high consumption of PET bottles, many of them discarded in public places, roads and transport systems and rural areas, combined with a lack of recycling programs caused environmental and health problems, and the clogging of drainage systems in urban areas. Since the mid-1990s, the Mexican government has set voluntary PET recovery and recycling programs that were successful to some extent. PET recycling activities involve sorting, washing, re-granulating and pellet production by local enterprises. The pellets are then shipped to domestic Mexican plastic transformation industry (35%) or exported to other markets (65 %). In Mexico, recycled PET facilities produce textile fibers, bottles for non-food uses and industrial strapping.

In Mexico, recycling of the MSW is mostly in the hands of waste pickers, middlemen or brokers. ¹²²⁻¹²³ Waste pickers are self-employed, sometimes resorting to collecting plastics from neighborhood garbage containers before they are collected by contracted waste management services. Waste pickers often organize themselves into associations, cooperatives, unions or microenterprises, through which they feel empowered to carry out their activities. ^{116, 121} Often local authorities promote and recognize the formation of associations or cooperatives, which are able to negotiate agreements for waste collection and recycling services. However, even with these associations the waste pickers income is not fixed but based on the quantity and quality of recycled materials and the selling price in local markets.

Currently, recycled PET price depends on factors such as impurities (i.e., amount of other plastics or residues), quality (i.e., clear vs color PET), cleanliness, type of organization the waste pickers belong to, middleman or broker who buys the product, and even the geographical area (i.e., urban vs rural) where PET is collected and sold. An average price for recycled PET ranges is between 0.24 - 0.48 USD/kg, 105 although it is likely that most waste pickers receive the lowest price. Waste pickers who recycle PET must work long hours to obtain sufficient income to support their families. The official minimum daily wage set by the Mexican federal government was 8.25 USD/day in January 2022. If an average recycled PET price of 0.36 USD/kg is considered, a waste picker must collect around 23 kg of PET every day to receive the equivalent of the minimum daily wage. A number of studies highlight the low monthly income (120 - 360 USD per month) by waste pickers in Latin America. 124 There is an urgent need to propose business schemes that improve the income of waste pickers, in addition to providing them health, safety, labor and social benefits through formal employment. The development of business models in Latin America that formalize the inclusion of waste pickers in the recycling value chain and that limit the actions and profits of middlemen, will have social benefits for waste pickers and will bring favorable economic benefits for the Mexican recycled PET industry.

Some successful initiatives show that when waste pickers are organized by non-profit and for-profit organizations and they are formally included in the PET recycling value chain, a number of favorable social and economic benefits occurs. Social-oriented programs for waste pickers lead to their recognition and empowerment through the establishment of formal jobs, with fixed salaries and labor and health benefits with local government or private companies. Social-oriented programs may have a profound impact on the education and culture of waste piker's communities. Theses social-based initiatives are emerging in the MSW management value chain of Mexico, Brazil, Argentina, Colombia and Chile, but the benefits are still limited to a few communities. In the current socio-economic situation in Latin America, the development of technologies and industries that facilitate the processing of plastic waste into products with higher added value in the market, is a critical factor to facilitate the inclusion of waste pickers in the value chain of plastic recycling.

MSW from urban and rural areas is typically processed by public services run by local governments to avoid negative impacts on health and the environment. In countries such as Mexico and Brazil, the management of MSW is regulated by federal and local laws, which establish guidelines for the collection, separation, recycling and final disposal of waste, using strategies that, in principle, contribute to the preservation of the environment and take care of the health and safety of the employees. Various technological, economic, administrative, social and cultural factors prevent RSM management from being carried out properly, especially in rural areas. As a result, it is estimated that around 40 million people (6% of population) in Latin American communities lack trash service. Up to a third of MSW is disposed of in open dumps. 125-128

Consequently, the prevailing situation is that the MSW management in Latin America is a focus of concern in terms of public health, environmental risks, informal economy, security and social inequality, particularly for the communities where the MSW transfer units and final disposal sites are located.

A license is granted to private companies when MSW cannot be adequately collected by local governments. A growing number of companies in Latin America offer the following benefits in MSW management: a reduction in public spending, selective processing of domestic, commercial, and industrial waste, use of specialized technology and skilled workforce, generation of well-paying jobs, and management projects contributing to sustainable development. ¹²⁹⁻¹³⁰ This recycling strategy is very distinctive from the circular economy and it has been identified as a vector contributing to the fulfillment of Sustainable Development Objectives set by the United Nations. For this reason, federal and local governments in Latin American communities have established legal frameworks to trigger waste recycling, as in the case of Brazil, which in 2010 established the National Solid Waste Policy, and Mexico, which in 2003 approved the Law for the Prevention and Integrated Management of Waste, and very recently the General Law of Circular Economy with the aim of promoting efficiency in the use of waste through reuse and recycling. ^{119,} ¹³¹⁻¹³³

Poverty and the growing market value of recyclable products has induced many people in conditions of social and economic vulnerability to work as waste pickers. It is very common nowadays to find fixed human settlements around waste transfer and final disposal units. Entire families live in these settlements. It is common for waste picker's children to continue with the family tradition.

4.0 Mechanical Recycling

Mechanical recycling is defined by the U.S. Food and Drug Administration (FDA) as secondary recycling and is the most common approach for recycling plastic solid waste (PSW). This process has an established infrastructure in most countries. In secondary recycling, the postconsumer plastic waste is reprocessed and converted into new materials. 134 With the advancement and availability of mechanically recycled PSW, virgin plastics are substituted with post-consumer recycled materials or blends thereof in many industrial and consumer applications. 135-136 Mechanical recycling involves collection/segregation, cleaning and drying, chipping/sizing, coloring/agglomeration, pelletization/extrusion, and manufacturing the end product. Both primary and secondary recycling involve similar process steps. ¹³⁷ Primary recycling as defined by the FDA recovers the pre-consumer or post-industrial recycled (PIR) waste material and produces new products. Secondary recycling physically reprocesses post-consumer waste materials to produce new materials. 138 Primary recycling maintains the same quality as virgin material, whereas downcycling is common in secondary recycling due to some degradation of the plastic's properties. 135 Post-consumer materials, in particular polyolefins, can have unpredictable physical properties due to the large range of polymer structures, molecular weights, and additive packages. Such variation and lack of grading can make using these materials more difficult. The variation in color further complicates usage in new products due to the inability to control the final colors. For example, plastic materials having different colors produce undesirable grey color after reprocessing into pellets. 139

4.1 Processing Technologies in Mechanical Recycling

Mechanical recycling consists of a few general steps: shredding/granulation, contaminant removal, followed by flake segregation. The primary step involves the melting and re-extruding of the plastic into uniform pellets¹³⁵ which can then be utilized in cast/film extrusion, injection

molding, blow molding, etc.^{135, 140} The molecular weight of a plastic is highly influential to all the plastic's innate properties. ¹⁴¹⁻¹⁴³ In general, an increase in molecular weight increases the glass transition temperature, the melting temperature, plastic strength, elasticity, stiffness, toughness, and viscoelastic properties. The processing residence time and reprocessing of the material also influence the molecular weight of the polymeric materials.^{32, 144-146} Figure 12 demonstrates the change in melt-flow index (MFI) of various plastics subjected to extrusion and injection molding. The repeated exposure to high heat, time, and shear rates can cause degradation of the polymeric material, and in some cases, unwanted side reactions that can either increase or decrease the molecular weight of the final product. These structural modifications lead to changes on both flow and mechanical properties of the material. Manufacturers may be inclined to utilize additives to recover material properties or homogenize the recycled material, although this typically adds cost to the recycled plastic and may further complicate future recycling attempts of the material waste. Different variations of mechanical and thermal processing technologies (Figure 13) used in recycling are described below.

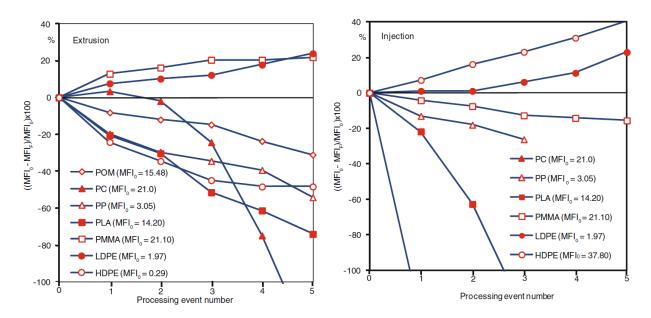


Figure 12. Change in MFI as a function of number of processing events for extrusion (left) and injection molding (right). Published with permission from ref ³². Copyright Carl Hanser Verlag, Munich 2012.

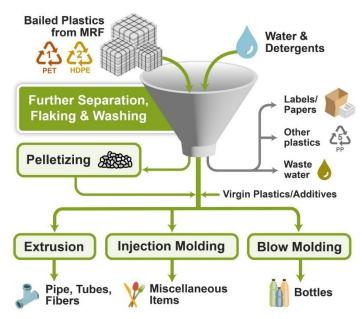


Figure 13. Various approaches for mechanical recycling of PSW (Plastic solid waste). 135

4.1 Extrusion Molding

In extrusion molding, plastic pellets enter the hopper into the barrel of the extruder in a continuous process. The plastic is fed into the barrel in the screw feed zone, and the screw forces raw material through the hot barrel and causes melting. The constant moving of the plastic through the barrel restricts overheating and limits resonance time, which may degrade the plastic. ¹⁴⁷ Because of the heating during extrusion, some alteration to the polymer chain occurs. The plastic melt in the barrel passes through screen packs to remove gross contaminants during the extrusion process. The screen pack and breaker plate are found in commercial plastic extrusion between the extruder and the die. Melted plastic is re-shaped using a die. ¹³⁵ The breaker plate ensures the proper mixing in the screw of the plastic by creating backpressure and reorients the plastic creating a stable linear flow before entering the die. The uneven flow of the molten plastic into the die can create undesirable residual stress that can cause warping during the cooling stage. ¹⁴⁷ The extrudate is cooled with a water bath or cooled air stream. This process is complicated as plastics are good thermal insulators. ¹⁴⁷ The extrusion process for recycling is similar to a new product manufacturing technique. Details of the extrusion molding, injection molding, blow molding, film molding, and fiber processing can be found in SI 4.0.

4.2 Mechanical Reprocessing of PET

Bailed PET often contains a large number of contaminants including adhesives, sugars, and other plastics. It is important to clean the PET and separate it from other materials before it is melt-processed through extrusion to produce recycled PET pellets (rPET). Figure 14 illustrates a typical PET bottle recycling process which is adapted from one of the PET bottle recycling companies in Europe. The delivered bottles are sorted depending on the type of material, color, processing method etc.. The bottles are then shredded into small flakes followed by washing processes. The flakes go to the extruder after cleaning and drying.

Melt extrusion of clean washed PET flake or granules is used to manufacture pellets of uniform shape for subsequent manufacturing processes (injection molding, extrusion, injection stretch blow molding, etc.). When PET reprocessing uses an established facility, processing

becomes more cost-effective, more straightforward, and possesses less environmental impact. Switching from virgin to recycled PET depends on material pricing, secure recycled material supply chains, and the ability to use existing facilities. Processing PET at high temperatures may cause chain degradation which influences crystallinity of the plastic. Plastic degradation from chain scission causes molar mass plastic decrease, which makes bottle-to-bottle recycling challenging. Legal 2019.

rPET can be used for most applications instead of virgin materials provided that the properties meet the quality criteria. Clarity and yellowing are major property challenges for rPET. ¹³⁶ Like other plastics, PET's quality is also affected by chain degradation because of thermo-oxidation. ¹⁵³⁻¹⁵⁴ Some contaminants (such as PVC and polyvinyl alcohol) accelerate chain scission in PET plastic during melt processing due to acidolysis. ¹⁵⁵⁻¹⁵⁶ Impurities in PET enhance chain scission reactions, and traces of PVC and poly-lactic acid (PLA) can accelerate acidolysis or hydrolysis. These reactions alters the plastic's microstructure and the mobile amorphous region is altered causing thickening of the crystalline domains. ¹⁵⁴ Crosslinking can also occur, resulting in increased viscosity in PET, hindering processability for applications such as injection molding. The multipole extrusion cycles of mechanical recycling increase the rates of chain scission because of thermo-oxidation.

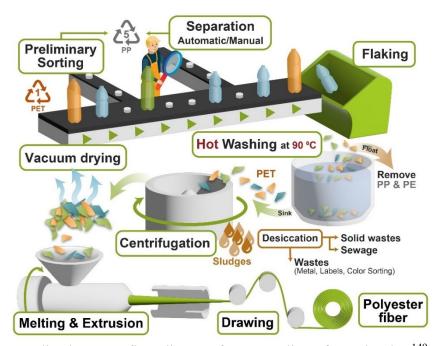


Figure 14: A generalized process flow diagram for a recycling of PET bottles. 149

Compounding additives into rPET during reprocessing can protect the plastic from chain scission and improve mechanical properties. To minimize thermo-oxidation of the plastic, metal-based stabilizers are often used.¹⁵³ The use of radical scavengers, such as organic phosphates, is another option to hinder radical induced oxidation of the terephthalate ring, which is a source of yellowing.^{154,157} The most common problem in PET reprocessing is viscosity reduction (molecular weight reduction) due to hydrolytic degradation and thermal oxidation. Color change in the post-consumer PET is another vital problem and normally the industry solves the problem by "open-

loop recycling "or "semi-closed-loop recycling". The concepts of "open-loop recycling" or "semi-closed-loop recycling" are described in Section 4.2.3.1.

If the molecular weight reduction is less severe, the plastic can be subjected to a process called solid state polymerization (SSP) to help rebuild the molecular weight. The plastic is heated to a temperature between the melting and glass transition temperatures to induce esterification and transesterification reactions. Is Industries are currently looking for a new stream of PET waste to reprocess, including colored PET. For example, in 2018 'Indorama Ventures' partnered with 'Unilever' to recycle fifty billion bottles per year by 2025, including colored PET. According to them, traditionally non-recyclable colored PET is subjected to a chemical recycling process. These colored PET are reduced to monomeric species, and then the contaminants removed before being used as raw material for polymerization. This technology produces transparent foodgrade PET plastic material from post-consumer PET. Recycling for food contact packaging requires a very demanding and clean plastic. No Objection Letters (NOLs) by the Food and Drug Administration are often sought by recyclers and manufacturers to demonstrate that their recycling process and materials are suitable for direct food contact applications.

Continuous improvements in plastic reprocessing is an ongoing effort with new technologies in degasser and filters to facilitate increased plastic melting quality. Degassing employs a vacuum vent on the extruder to enable volatile compound stripping from a plastic melt. This stage reduces hydrolysis by removing moisture and adds value by producing a high-quality plastic with maintained molecular weight and decreased contamination. The addition of a filter helps remove unwanted non-volatile contaminants from the plastic and increases the mechanical properties of the recycled plastic. When selecting recycling technologies in manufacturing processes, it is important to select the appropriate mechanism to minimize the degradation of the plastic for high-quality new parts. 154

4.2.3 Utilization of Recycled PET Waste

4.2.3.1 Closed-Loop and Open-Loop Recycling

The recycled raw material supply increases as plastic waste collection increases. These raw materials can be used to produce new material as 'open loop' or 'semi-closed loop' or 'closed loop' recycling. Closed-loop recycling means the recycled raw material is used for the same product and fully replaces the virgin material, e.g., PET bottle to bottle recycling. Open-loop recycling means the recycled material is used for a different product and fails to replace the virgin raw material in the original application, also referred to as downcycling. The inherent properties of raw materials for open-loop recycling are often too degraded by the service life and recycling process and the plastic cannot be used in the original application. Semi-closed recycling means the recycled raw materials are used to produce another type of product but cause no change in the inherent properties of the recycled materials. 166

4.2.3.2 Recycled PET Products

rPET is incorporated to form a wide range of new products, for example, shoes, bags, fibers, boards, mechanical parts, etc., as open-loop recycling. Most rPET is used for fibers. ¹⁶⁷ Consumers can currently purchase rPET food packaging containers. According to a 2020 NAPCOR (National Association for PET Container Resources) Report post-consumer rPET used in the US and Canada has continuously increased since 2004. It has been predicted that by 2026 the market will reach up to USD 12.5 billion, representing an ~8% Compound Annual Growth Rate (CAGR) from 2019 to 2026. ¹⁶⁷⁻¹⁶⁸ The NAPCOR Chairman mentioned that post-consumer rPET utilization is proceeding towards a circular economy. According to NAPCOR, fiber sectors made up more than 40% of the worldwide rPET market in 2019. ¹⁶⁹ The fiber market includes manufacturing mattresses, insulators,

car equipment, etc. Asia Pacific plastic industries are increasing their dependency on rPET. Colored rPET is used for food and non-food applications for its stability and strength. These have high popularity as they are light in weight and provide strength for a long period. 167

4.3 Mechanical Reprocessing of Polyolefins

Mechanical processing of polyolefins also induces degradation at the molecular level and the formation of aldehydes, ketones, short-chain hydrocarbons. The degradation mechanism is different in each type of polyolefin. The general degradation mechanisms begin with the generation of macroradicals within the molecular chain. This radical creates many shorter, branched, or cross-linked polymer chains. When these radicals react with oxygen centered radicals, further degradation occurs. The revious studies have demonstrated that HDPE is more prone to crosslinking whereas PP shows a large number of chain scission events. These degradation reactions mainly occur in the amorphous phase below the plastic's melting temperature because oxygen cannot diffuse into the crystalline phase.

As post-consumer plastic films are contaminated with various waste materials, an intensive pre-treatment is crucial before extrusion. The source of raw material in secondary recycling is MSW mixed with other plastics. This needs an initial separation step to separate the contaminants. The mechanical recycling process described here (Figure 15) is an example of a European processing facility. The process starts with comminution of large plastic parts and shredding/sieving to remove as much of the contaminants (metals, glass, paper, etc.) as possible. The contaminant-free plastics are sent for pre-washing then vigorous washing to avoid microphysical contamination. Afterward, the material enters the hydrocyclone to separate undesirable particles. A friction washer is used for washing to consistently remove contaminants from the plastic such as labels, glue, or organic dirt on the surface 175. After washing, the plastics are dried thermally to lower the moisture content before entering the extrusion and pelletizing stage. The function of extruder and blowing machines are discussed above. The quality of the recycled plastic film is degraded leading it to be used in applications such as products for constructions, public spaces, and traffic applications after injection molding or extrusion.



Figure 15: Mechanical recycling process of polyethylene plastic film at an industrial plant. 174

4.3.1 Mechanical Processing of HDPE

HDPE is a linear chain plastic with high molecular weight produced from carbon and hydrogen atoms. As this plastic has a straight chain, it has more strength than LDPE. It is an important component of MSW as this waste plastic has high recyclability potential. Commercially, two kinds of HDPE are often found in MSW depending on either the extrusion process or injection molding; each type differs in its viscosity. Like other plastics, chain scission and chain branching are also common in HDPE during the extrusion process. Generation of carbonyl groups in HDPE increases when the oxygen in the surrounding atmosphere is high. When oxygen is low, double bond formation is observed in the molecular backbone. Because of these reactions, the HDPE molecular weight is reduced. When the plastic chain length is lower the plastic becomes vulnerable to degradation by radical attack. This scenario worsens with each extrusion cycle. Studies have also shown that the viscosity in the plastic reaches a very high level (fivefold higher than the starting level) after sixty extrusion cycles due to crosslinking in chains. These degradation effects can partially be mitigated via controlling extruder parameters such as temperature, screw speed and screw design. These

Recycled HDPE and other recycled polyolefins have multiple applications in the food packaging sector and multilayer packaging applications. However, there is a concern with recycled raw material in direct food contact because potentially toxic small molecules (plasticizers, stabilizers, etc.) could diffuse and migrate into food products. As a result, recycled polyolefins are often utilized as the middle layer in multilayered packaging, and the surface layers are made of virgin plastics. Recycled HDPE has a large market as the processing cost can be relatively low. Post-consumer HDPE is a feasible option to produce plastic lumber which is a replacement for wooden lumber.

4.4 How legislation changes the scenario

The municipal waste management system and plastic recycling in most European countries has made remarkable advancement. EU countries with landfilling restrictions or bans have higher recycling and waste recovering percentages as shown in Figure 16. Recycling of HDPE, LDPE, PET, PP, and PS plastics are performed together. Post-consumer plastic waste collection was more than 32% in several EU countries which was mostly comprised of mechanical recycling techniques. The highest recycling rate was found in Norway at 45% in comparison to ~9% in the United States. 136, 181

The number of recycling companies is increasing. There are almost 115 PET recycling and 40 PE recycling facilities in the USA. For example, '77 recycling is a plastics (post-industrial plastic scrap) recycling company that accepts most materials (PET, PP, PS, PVC, HDPE, LDPE, etc.). China's ban on imports of plastic waste increased the recycling facilities across the USA. Good communication between product manufacturers and the recycling industries is needed to confirm the recycling of packaging materials. This communication can strengthen the use of recycled raw materials and create a new market for these recycled plastics. 184

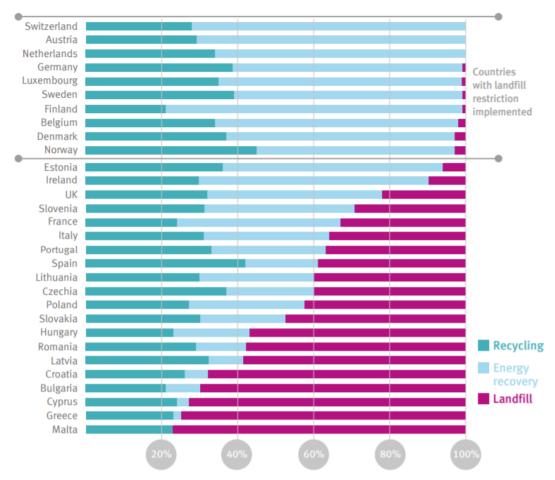


Figure 16: Post-consumer plastic waste recycling rate, energy recovery rate and landfilling rate per European country in 2018. Published with permission from ref ¹⁸⁵. Copyright Plastic Europe 2022.

4.4.1 Utilization of Mechanical Recycled Post-Consumer Materials as Food Contact Materials (FCM)

The most valueable type of recycled plastic is that plastic that can be used for food packaging application. In the US the Food and Drug Administration (FDA) employs regulations regarding the safety of the use of recycled plastic materials as food contact materials (FCM). The FDA expresses their concerns and regulations maintained for using recycled plastic:

- When recycled plastic/material is used as FCM, the chance of contaminants in the final product may increase.
- Post-consumer recycled plastic/materials are permissible to use as FCM material.
- The adjuvants (for example petroleum waxes, synthetic petroleum wax, colorants, plastic modifiers¹⁸⁷) coming from the post-consumer recycled plastic/material may not be suggested for use in FCMs as the contaminant present in the recycled material can pass on to the new product and migrate into the food matrix. ¹⁸⁸
- The FDA regulates the plastic recycling processes to ensure that the recycled materials are
 not contaminated and that the recycling process is suitable for direct food contact.¹⁶² For
 example, in secondary recycling, the physical reprocessing steps, grinding, melting, and

reforming, are documented and submitted for evaluation to obatain a favorable opinion letter through the No Objection Letter (NOL) program. For plastic depolymerization, it is necessary to confirm that the monomers are contamination-free and the produced plastic is the same as that from virgin monomers. 189

• In the case of multi-layered packaging, sometimes, when proper contamination removal is complex, the recycled layer is used as the most outer layer. For example, for recycled PET, FCM is used as the outer layer in multi-layered containers, and the inner layer in contact with food is made of virgin material. 154

Manufacturers of FCMs using post-consumer recycled materials often need special evaluation. He NOL determines the assessment of the plastic used for a FCM and whether the recycling process is physical or chemical. The earliest NOL was issued in 1990 for a physical recycling process of whole egg cartons. Many of the early NOLs that granted favorable opinions were for PET and PS plastics were, in recent years, much of the focus has been on polyolefin materials; utilization of post-consumer polyolefin streams for direct food contact applications is challenging due to a large number of different molecular structures, additive packages, and uses for which consumer abuse can lead to incidental contamination. Such challenges are overcome through careful source control of the post-consumer material and challenge surrogate chemical testing to determine if the recycling process can reduce the concentration of different types of compounds, which is often a requirement for the NOL process.

For the surrogate chemical challenge testing, the plastic is soaked in a chemical cocktail containing a volatile polar compound (e.g., chloroform, chlorobenzene, 1,1,1 trichloroethane, diethyl ketone, a volatile non-polar compound (toluene), a heavy metal compound (copper (II) 2-ethylhexanoate), non-volatile polar (benzophenone or methyl salicylate), and a non-volatile non-polar compound (tetracosane, lindane, methyl stearate, phenylcyclohexane, 1-phenyldecane, 2,4,6-trichloroanisole) using an isopropyl/hexane solvent delivery mixture to artificially contaminate the plastic. After the artificial contamination soaking of two weeks at 40 °C, the spiked plastic is subjected to recycling. The concentration of the artificial contaminants is quantified in the recovered, recycled plastic and the starting spiked plastic to demonstrate the ability of the recycling process to reduce contamination. These results, along with a description of the recycling procedure and post-consumer material feedstocks, are submitted to the FDA to evaluate suitability for manufacturing direct FCMs. Upon favorable review of the packet, a NOL is issued. As of the end of 2021, 254 NOLs have been issued by the FDA. 191

5.0 Thermal Decomposition of Plastics

5.1 Non-Catalytic Thermal Decomposition of Plastics

Pyrolysis is the thermal decomposition of organic compounds typically in an oxygen-deficient atmosphere. The decomposed products are then condensed and collected as oils, waxes, gases, and char, with distributions dependent on feedstock, reaction conditions, and reactor type. Temperatures in the range of 350-700 °C are typical for plastics pyrolysis, ¹⁹⁴ with the general trend of higher yields of gas at higher temperatures. Pyrolysis is generally classified according to heating rate (slow, fast, or ultra) and environment (catalytic pyrolysis, steam pyrolysis, vacuum pyrolysis, microwave pyrolysis, plasma pyrolysis, oxidative pyrolysis, etc.).

Pyrolysis is the most researched chemical recycling method for plastics.¹⁹⁴ The main advantage of plastic pyrolysis is the ability to convert plastic into lower molecular weight products to be used as fuels or feedstock for new chemicals or plastics.¹⁹⁶ Pyrolysis also produces less

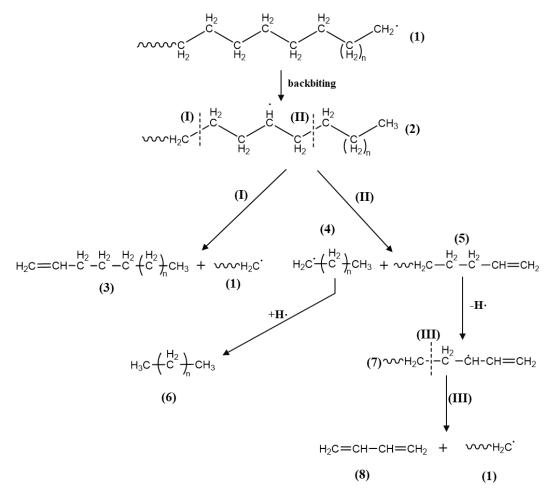
emission than plastics incineration.¹⁹⁷ Unlike mechanical recycling, pyrolysis can handle highly heterogeneous feedstocks with a higher degree of contamination.¹⁹⁶

5.1.1 Fundamental Chemical Processes during Thermal Pyrolysis of Plastics

5.1.1.1 Polyolefins

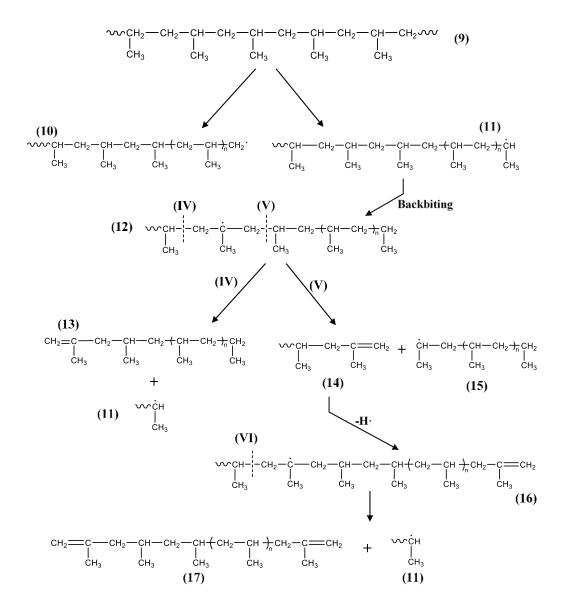
PE follows a free radical thermal decomposition that takes place through sequential random bond–scissions. The degradation begins in weak links (mainly peroxide groups formed during preparation and storage of PE) and proceeds in the pristine segments of the plastic. Peterson et al. employed thermogravimetric analysis to demonstrate that the activation energy depends on the extent of the decomposition reaction and assumes values between 150 kJ/mol and 240 kJ/mol. The latter number corresponds to the random scission process for pristine PE. Huber and coworkers reported a similar activation energy (234.8 kJ/mol), and argued that only models that include two random scission steps are capable of capturing the details of weight loss curves as obtained from thermogravimetric analysis. The complexity of the free radical thermal decomposition of PE is substantial, and this is reflected in the large variety of pyrolysis products. The main products are alkenes, alkanes and alkadienes, while Diels–Alder reactions may also lead to the formation of small amounts of cycloalkenes.

The initiation of PE pyrolysis involves a homolytic C–C cleavage reaction that happens at a random position along the PE chain, and gives two macroradicals (1) – (Scheme 1). Each of these radicals may undergo a β –scission to produce ethylene monomer and another primary radical. However, this unzipping process is not kinetically favorable at the early stage of PE decomposition (ca. 400 °C), and as a result no or little ethylene is produced in experiments (<1%). In contrast, radical (1) prefers to undergo a backbiting (often 1,5–backbiting through a six membered transition state) reaction, thereby generating a secondary internal radical (2) (Scheme 1). Subsequently, a β –scission at (I) gives rise to an alpha–olefin (3), whilst if the same process occurs at (II), a terminally unsaturated polymer residue (5) is produced, as well as a radical that transforms into an alkane (6) after abstracting a hydrogen atom. The formation of alkadienes (8) takes place either via a hydrogen abstraction reaction from (5) (Scheme 1) or via chain scission followed by a backbiting reaction. These processes give rise to (7) that, after a β –scission, is converted into an α , ω –alkadiene (8) (Scheme 1) and a new primary radical (1), which likely undergoes the processes of Scheme 1 anew.



Scheme 1. Fundamental reactions for the thermal decomposition of PE leading to alkanes (6), alkenes (5) and alkadienes (8). Arabic numerals indicate chemical species that form during the pyrolysis of PE, while Roman numerals indicate the occurrence and position of the scission of chemical bond.

Similar to PE, the thermal decomposition of PP (9), Scheme 2, proceeds via random scissions along the backbone of the polymer with an activation energy of about 250.0 kJ/mol.²¹¹ Each random scission produces a primary (10) and a secondary (11) radical (Scheme 2), which, in turn, are converted to alkanes, ²¹³ alkenes, ²¹⁶ and alkadienes. ²¹⁷ The major decomposition products are alkenes and alkadienes, and their formation takes place in a manner similar to what we described in Scheme 1.



Scheme 2. Fundamental reactions for the thermal decomposition of PP leading to alkenes and alkadienes. Arabic numerals indicate chemical species that form during the pyrolysis of PE, while Roman numerals indicate the occurrence and position of the scission of a chemical bond.

The highest products from PP pyrolysis (i.e., 2–methyl–1–pentene, 2,4-dimethyl–1–heptene) are produced via the decomposition of the secondary radical (11), while only minor quantities of products are derived from the primary radical (10).²¹⁰ On this basis, Scheme 2 focuses on the formation of alkenes and alkadienes via (11), which after a backbiting reaction and a β –scission at (IV) forms an alkene product (13) and another secondary radical (11). The new secondary radical is decomposed following the same sequence of steps. Alternatively, the β –scission may occur at (V), which results in a terminally unsaturated polymer (14). The latter species may undergo an atomic hydrogen abstraction reaction followed by a β –scission at (VI), thereby forming another secondary radical (11) and a series of alkadiene products (17).

5.1.1.2 Polyvinyl Chloride

The thermal decomposition of PVC (18), Scheme 3, follows a completely different mechanism compared to polyolefins. According to thermogravimetric analysis studies, PVC (18) starts decomposing at much lower temperatures (< 250 °C) than other common polymers, and its decomposition involves two distinct stages.²¹⁸

The dominant reaction in the first stage (250 °C – 350 °C) is the dehydrochlorination of the backbone that leads to a 60% weight loss. ²¹⁹ The activation energy for this process has been determined in several studies, and values in the range of 112.0 kJ/mol – 150.0 kJ/mol have been reported. ²²⁰⁻²²¹ It has been conjectured that the initiation occurs in thermally labile defects like butyl branches associated with tertiary chloride. ²²²⁻²²³ Once the reaction is initiated, its propagation proceeds via a quasi–ionic mechanism whereby HCl is removed in a concerted manner via a four–center transition state (19). ²²⁴ Subsequently, the propagation reaction is relatively fast owing to the continuous formation of internal allylic chloride structures [see (20) in Scheme 3], which are more thermally unstable and susceptible to C–Cl heterolysis via HCl catalysis [i.e., autocatalysis – transition state (21) in Scheme 3] than the pristine PVC polymer segments. ²²⁵⁻²²⁶ Remarkably, first–principles calculations by Yanborisov and Borisevich showed that the HCl–catalyzed dehydrochlorination of small chlorinated molecules (e.g., 2–chlorobutane) can be 60.0 kJ/mol more facile than the uncatalyzed process. ²²⁷

The main dehydrochlorination products are HCl gas and π -conjugated polyene sequences (22). The latter products are highly unstable under pyrolytic conditions and therefore undergo intramolecular and intermolecular reactions as soon as they form. The intermolecular reactions require the interaction between two polyene chains (22), and give rise to crosslinked polyene chains (23), which are the precursor of char (24). The intermolecular intermolecular electrocyclic reaction, thereby giving rise to π -conjugated 1,3-cyclohexadiene rings (25). The latter are converted to benzene (26), and subsequently polyaromatics (27), after two consecutive homolytic C—C cleavages that occur at temperatures beyond 350 °C having activation energies larger than 220.0 kJ/mol. C—C bond breaking also gives rise to small amounts of noncondensable gases (e.g., CH₄ and H₂). Importantly, we note that the formation of aromatics can be promoted by applying a high–temperature pyrolysis step in the presence of a solid catalyst (e.g., ZSM-5 zeolite).

$$(18) \qquad (19) \qquad (20)$$

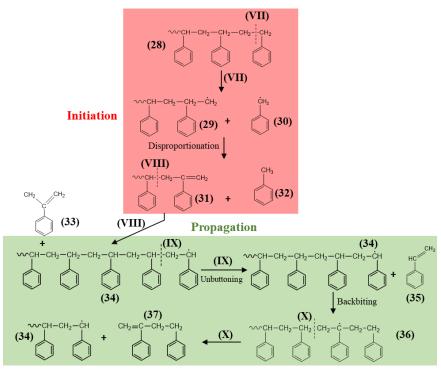
$$R_1, R_2 = -CH_2 - CHCIANN, -CH_2 - CH_2 - CH$$

Scheme 3. Fundamental reactions for the thermal decomposition of PVC leading to different products. The symbol [‡] indicates a transition state. Arabic numerals indicate chemical species and intermediates that form during the thermal degradation of PVC.

5.1.1.3 Polystyrene

The thermal degradation of PS (28) follows a radical chain mechanism (Scheme 4), with styrene (35) being the dominant product.²³³ By means of thermolysis experiments, Wall et al.²³⁴ demonstrated that the thermal stability of PS (28) depends on the polymerization method (i.e., anionic or radical polymerization) used in its synthesis. Preparation through a radical polymerization gives rise to polymer chains with randomly distributed "weak links", which perhaps are peroxidic in nature and are the sites where the thermal decomposition of PS starts.²³⁵ Yet, anionic polymerization yields PS of high thermal stability;²³³ the general thermal decomposition mechanism for this case is described in Scheme 4 and the following text.

The experimentally measured activation energy for the thermal degradation of PS is 200.0 kJ/mol and remains constant regardless of the extent of the reaction. This is indicative of a single rate-determine step during the reaction: the β -scission that forms styrene (35) (see Scheme 4). According to Guyot and coworkers, a likely initiation pathway for "anionically" prepared PS is via an end chain scission reaction that forms a benzyl radical (30) and a primary radical (29). The two radicals go through a disproportionation reaction and give toluene (32) and a chain with a thermally unstable unsaturated end (31). In turn, (31) decomposes into α -methylstyrene (33) and a secondary radical (34) that leads the degradation process thereafter. DFT work by Huang et al. revealed that the latter reaction is exothermic by 80.8 kJ/mol and its activation energy is 288.2 kJ/mol. α -methylstyrene (35) and α -methylstyrene (37) and α -methylstyrene (38) and α -methylstyrene (38) and α -methylstyrene (38) and α -methylstyrene (39) and α -methylstyrene (39) and α -methylstyrene (31) and α -methylstyrene (32) and α -methylstyrene (33) and α -methylstyrene (34) that leads the degradation process thereafter. DFT work by Huang et al.



Scheme 4. Fundamental reactions for the thermal decomposition of PS leading to different products. Arabic numerals indicate chemical species, while Roman numerals indicate the occurrence and position of the scission of a chemical bond.

The propagation occurs by a β -scission process at (**IX**), thereby generating styrene (**35**) and another secondary radical (**34**). According to DFT calculations on a PS trimer, this reaction has an activation energy of ca. 117.0 kJ/mol, but it is strongly endothermic (+105.4 kJ/mol) and therefore not favorable at temperatures below 250 °C.²³⁷ Interestingly, the computed activation energy for the unbuttoning reaction (i.e., 117.0 kJ/mol) is in stark contrast to the experimental value (200.0 kJ/mol) and this can, to some degree, be justified by the considerably smaller size of the simulated PS trimer as compared to actual PS chains. (**34**) can either undergo further unbuttoning to give extra monomer (**35**) or a backbiting reaction followed by another β -scission reaction at (**X**) and give a dimer (**37**) along with another secondary radical (**34**). Based on DFT, such backbiting and β -scission reactions require kinetic barriers of 174.0 kJ/mol and 134.5 kJ/mol, respectively, and the whole process that forms (**34**) and (**37**) is endothermic by 94 kJ/mol.²³⁷ We note that the formation of trimer or tetramer species takes place in an analogous manner to that for

dimer production (37) (Scheme 4) with the only difference that different tertiary hydrogen atoms are involved in the backbiting reaction.

5.1.1.4 Poly(ethylene terephthalate)

PET (38) is a thermally stable polymer thanks to the combination of short aliphatic chains and aromatic rings. Its thermal decomposition follows a molecular mechanism and the initiation reaction involves a scission at the ester linkage (Scheme 5).²³⁸⁻²⁴⁰ This reaction takes place through a six—membered transition state (39), and recent DFT studies predict activation and reaction energies of 184.0 and +48.0 kJ/mol, respectively.²⁴¹

The initiation reaction leads to the formation of an oligomer with an olefin end group (40) and another oligomer with a carboxylic end group (41). These two species decompose further to produce a wide spectrum of products with acetaldehyde (44) and CO₂ (43) being the most abundant at temperatures around 300 °C.²³⁹ The former can be produced directly from (40) and (41) or via the degradation of EG end groups as proposed by Holland and Hay,²⁴² while CO₂ is released by decarboxylation of (41). More than 45 wt% of the PET is degraded into CO₂ with trace of CO.²⁴³

Scheme 5. Fundamental reactions for the thermal decomposition of PET. The symbol ‡ indicates a transition state. Arabic numerals indicate chemical species and intermediates formed during the pyrolysis of PET.

5.1.2 Variables Affecting Product Distribution

Pyrolysis begins with free-radical initiation in the plastic melt, or condensed phase. Volatile products are released from the melt as depolymerization progresses, leaving behind ash, fillers and (sometimes) char. Secondary reactions occur in the vapor phase that cause further cracking. Gas, liquid, and wax are produced, with distributions dependent on reaction conditions. These products are usually categorized according to their carbon length and/or phase:²⁴⁴

• C1-5 = gas

- C6-20 = naphtha or oil, liquid at ambient conditions
- C21+ = wax, solid or highly viscous liquid at ambient conditions

Al-Salem et al.²⁴⁵ published an in-depth review addressing plastic pyrolysis variables and their influences on reaction and product distribution and asserted that the main decomposition behavior of the plastic is controlled by temperature. In PE pyrolysis, early studies showed that only liquid and gas – no wax – are produced above 600 °C.²⁴⁶ Increasing temperature leads to increased aromatic production, as gas is converted to aromatics through a Diels-Alder reaction and unimolecular cyclization reactions, ²⁴⁷⁻²⁴⁸ although a study by Kulas et al.²⁴⁹ showed that the reaction pathway from gas to aromatics has low temperature dependence.

The composition of naphtha is vastly different than the composition of plastic oil (Figure 17). The main products of naphtha are paraffin with around 10% aromatics, while the main products of plastic pyrolysis oil are olefins and cycloalkanes/alkadienes with a much wider range of carbon numbers.

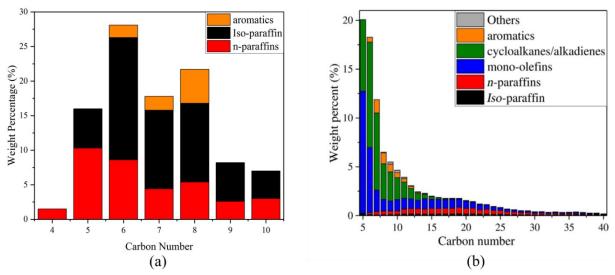


Figure 17. (a) A typical naphtha composition (made the graph based on the data obtained from ref ²⁵⁰, (b) A typical plastic pyrolysis oil composition obtained from PE pyrolysis. Published with permission from ref ²⁵¹. Copyright Wiley-VCH.

Increasing vapor residence time increases the yields of oil and non-condensable gases.^{247,} As primary products are exposed to heat for longer periods of time, secondary reactions and further cracking to smaller molecules are encouraged.²⁵³ Thus, the product distribution shifts from high molecular weight products to lower molecular weight hydrocarbons (MWHCs).²⁵⁴⁻²⁵⁶ For polyolefin feedstocks, longer reaction times decreased product olefin concentrations and increased polyaromatic hydrocarbon concentrations.²⁵⁷

Polyolefins have received the most attention in the field of plastics pyrolysis. PE and PP decompose into a distribution of hydrocarbons, with decreasing product molecular weights as reaction temperature and time increase. Waxes and heavy oil olefins dominate product distributions at low temperatures, while gases and light oils are the main products at high temperatures.²⁴⁹ Polyolefins such as HDPE, LDPE, and PP decompose into a distribution of hydrocarbon products that have high concentrations of olefins and dienes (>70%).²⁵⁸⁻²⁵⁹ Mixed plastic feedstock with high PE content will lead to higher paraffin concentrations.²⁶⁰ Pure PP yields

higher amounts of olefins, with lesser amounts of paraffins, naphthenes, and aromatics. ²⁶¹⁻²⁶² Due to the tertiary carbon present on the backbone of PP, multiple types of secondary radicals are formed, shifting liquid product composition towards branched olefins. ^{260, 263}

PS decomposes primarily into the monomer styrene and its oligomers²⁶⁴⁻²⁶⁵ with the polymer undergoing chain scission followed by random scission.²⁶⁵ PS pyrolysis produces liquid products at yields greater than 90 wt.% in both batch^{261, 266-267} and continuous^{246, 268-269} reactors. Liu et al.²⁶⁸ pyrolyzed PS in a fluidized bed reactor at 600°C and achieved 98.7 wt.% oil, of which 78.7 wt.% was styrene. Secondary reactions and increased reaction temperature decrease the concentration of styrene in the liquid product and increases the formation of coke and gas.²⁶⁸ PS accelerates the pyrolysis of polyolefins due to higher concentrations of free radicals.²⁷⁰ Green Mantra Technologies is commercializing PS pyrolysis to recover styrene.²⁷¹ A thorough review on the pyrolysis of PS can be found elsewhere.²⁶⁵

The pyrolysis of PET yields oxygenated compounds from the presence of oxygen in the backbone of the polymer chain. Fast pyrolysis of PET produces mostly mixtures of aromatics and the organic acids benzoic and phthalic acid, char, and gas.²⁷² Formation of TPA is particularly problematic due to its high boiling/sublimation temperatures, which clogs reactor and condenser internals.²⁷²⁻²⁷³ The presence of phthalic acids in product oils increases viscosity and acidity and lowers calorific value, resulting in low-quality oils.^{272,274-275} Pyrolysis temperature has little effect on calorific values of PET products.²⁵⁹ PET in mixed plastics, increases the CO and CO₂ concentrations in product gases from pyrolysis reactions.^{195, 276} While some investigators have concluded that PET is not suitable for plastic pyrolysis,^{254, 277} others advocate for it based on the valorization of product char to activated carbon and product oil to fuel.²⁷² US-based pyrolysis company Agilyx has undertaken pyrolysis of PET with some success,²⁷⁸ but PET is rarely used as a feedstock in commercial pyrolysis processes. Other possible chemical recycling processes of PET are detailed elsewhere and in Section 9.1.²⁷⁹⁻²⁸²

Many commercial pyrolysis processes have low tolerance to PVC, which produces significant concentrations of organic chlorine, HCl and a solid residue.^{274, 276} The HCl causes corrosion issues with downstream processing of the products. Thermal decomposition of PVC is initiated by a dechlorination reaction, resulting in the formation of hydrogen chloride and benzene.²⁸³⁻²⁸⁴ The polymer chain then undergoes cyclization, yielding aromatic and alkylaromatic compounds that are often chlorinated.²¹⁹ Pyrolysis oil containing chlorinated compounds has limited use.²⁸⁵ Most previously reported pyrolysis processes had a specification that the PVC content of the plastic feeds be less than 2 wt%.²⁸⁶

Plastics can also be co-processed with waste tires, ²⁸⁷⁻²⁸⁸ wastepaper, ²⁸⁹ and agricultural residues, ²⁹⁰⁻²⁹¹ which has been shown to enhance products for fuels and value-added chemicals. ²⁹² The majority of waste plastics will contain high levels of contaminants. Additives, heavy metals, and pigments are often added to plastic to enhance its physical appearance or performance. Specific problematic elements include nitrogen, oxygen, sulfur, chlorine, iron, sodium, and calcium. ²⁹³ In low-temperature pyrolysis, sulfur presents in the pyrolytic oil, which reduces its ability to be used as ultra-low sulfur diesel. ²⁹³ Produced liquid may also contain amines or alcohols if the feedstock contains N, O, or S. ²⁹⁴ Siloxanes can be present in the pyrolysis oil as well. ²⁹⁵ Dechlorination is possible through the use of sorbents ²⁸⁵, ²⁹⁶⁻³⁰⁰, absorption and neutralization ³⁰¹, subcritical water treatment ³⁰², catalysts ³⁰³, or stepwise pyrolysis ²⁸⁵, but the latter was shown to modify the composition of liquid products. ²⁸⁵ Untreated plastic waste pyrolysis oils with high levels of contaminants are not feasible feedstocks for steam cracking unless sufficiently diluted. ³⁰⁴ Contamination may lead to catalyst deactivation if catalytic upgrading of products is desired. For

example, a municipal plastic waste pyrolysis plant in Idaho, U.S.A. produced an oil only suitable for low-value applications due to severe contamination.³⁰⁵

Thermal oxo-degradation (TOD) involves adding small amounts of oxygen to the pyrolysis process to increase chain cleavage.³⁰⁶ Plastics subjected to TOD are decomposed to oxygenated products and hydrocarbons, with exothermic partial oxidation reactions releasing energy to provide heat back to the process. This process mirrors that of autothermal pyrolysis developed for the process intensification of biomass,³⁰⁷⁻³⁰⁸ with the possibility to achieve autothermal operation for plastics.³⁰⁹

5.1.3 Reactor Configurations

Various reactor configurations have been used for plastic pyrolysis, including fixed beds, fluidized beds, rotary kilns, auger reactors, conical spouted bed reactors, and melting vessels (Figure 18). Detailed information on reactor types for plastic pyrolysis can be found in recent review papers. 263, 274, 310-312313 Fluidized bed reactors have excellent heat and mass transfer characteristics for pyrolysis of plastics and are the reactors that are most typically used for continuous large-scale processing of solids. In a gas-solid system, fluidized bed rectors have vigorous solid contact with different gas flow rates. An increasing of flow rate in a bubbling fluidized bed (BFB) leads to larger instabilities and bubbling channels of gas with a more vigorous solid movement.³¹⁴ In turbulent fluidized bed, with a sufficiently high gas flow rate, the terminal velocity of the solids is exceeded and solids undergo a turbulent motion so that the upper surfaces of the solid disappear. ³¹⁴ Fluidized bed reactors were used extensively in the groundbreaking work in plastics pyrolysis by Walter Kaminsky at the University of Hamburg.^{287-288, 315-317} Both BFBs and circulating fluidized beds (CFB) have been commonly employed in both laboratory studies²⁵³, ^{255-256, 316, 318-321} and industrial deployment. ³²² Fluidized beds usually employ smaller feedstock particles than other reactors, which, along with their inherently high convection coefficients, enhances heat transfer rates. Feedstock injected into a fluidized bed is rapidly dispersed and efficiently contacted with gas, resulting in high mass transfer rates. 310, 312 The combination of high heat and mass transfer rates are responsible for significant yields of light hydrocarbons and noncondensable gas from the pyrolysis of plastics in fluidized beds. 304, 323 Disadvantages include comminution of plastics to achieve small feedstock particles, and complicated reactor setups.²⁷⁴ Additionally, the high gas velocities required for fluidization can cause entrainment of char particles, requiring particulate separation downstream of the reactor. 195 Fluidized beds may also see agglomeration of melted plastic that can lead to bed defluidization.³²⁴

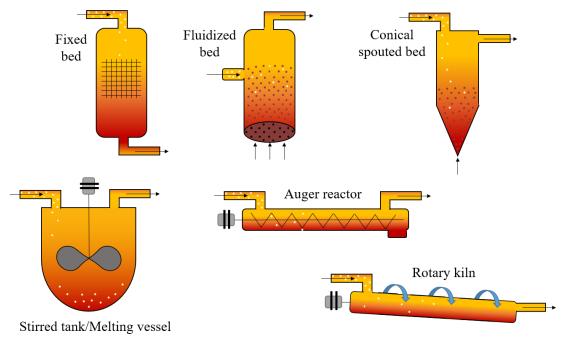


Figure 18. Schematics of various plastic pyrolysis reactors including fixed bed, fluidized bed, conical spouted bed, stirred tank, auger, and rotary kiln reactors.

Conical spouted bed reactors are a type of fluidized bed with a cylindrical geometry and a conical base. Cyclic and vigorous movements by sand particles in the bed prevent agglomeration upon melting and subsequent bed defluidization. ^{258, 325} Conical spouted beds have been employed in laboratory-scale pyrolysis studies of PS³²⁶ and polyolefins, ^{325, 327-328} which report high yields of wax. Orozco et al. ²⁵⁸ identified stable operating conditions for conical spouted bed reactors for individual plastic feedstocks.

Fixed bed reactors are inexpensive, simple to operate, and have low maintenance requirements. However, these types of reactors would be difficult to operate for solid feedstocks on the industrial scale due to large amounts of solid coke/char formation. Vertical fixed beds use gravity to force products through the reactor. Tubular reactors are very similar to fixed beds, but are usually horizontal with co-current flow of feedstock and carrier gas. ³²⁹⁻³³⁰ Due to the relatively long times required to devolatilize plastic, the entrance to the tubular reactor can become quickly blocked with melted plastic, limiting feed rates. While commonly used in laboratory settings, ³³¹⁻³³⁴ fixed beds are not suitable for industrial applications. ^{274, 312} BASF reported the use of a tubular pyrolysis reactor to crack plastic wastes at scale to produce oil and gas, but the feed rates achieved were not documented. ³¹¹

Auger reactors consist of a rotating screw inside a tubular reactor. The helical screw is used to convey feedstock while also discharging residual solid products. The auger reactor is a simple system that can be easily scaled and is feedstock flexible. Providing enthalpy for pyrolysis through the reactor wall is increasingly difficult as the reactor is made larger. This limitation can be substantially overcome by conveying heated metal shot or granular material into the reactor. As outlined by Campuzano et al., 535 potential disadvantages of auger reactors include the risk of blockage, mechanical wear, and higher vapor residence times, which can lead to sometimes undesirable secondary reactions. Auger reactors have been used to pyrolyze plastics to high yields of liquids for use as fuel 336 or wax, 337 or as the first stage in a multi-staged pyrolysis system to

activate molecules for further cracking.³²⁰ Brightmark, a US company, is using an auger reactor to process plastic pyrolysis, and the reactor has five heating zones in series to improve the heat transfer. The number of zones of a reactor can be varied depending on different feedstock.³³⁸

The rotary kiln is one of the most common reactors used in industrial pyrolysis processes. The kiln is a slightly inclined cylindrical vessel rotated slowly on its axis to allow feedstock and residual solids to move through the kiln. Because they can handle various feedstock sizes and shapes, rotary kilns have been used to process scrap tires³³⁹⁻³⁴⁰ and municipal wastes.³⁴¹⁻³⁴² Heat is supplied to the kiln by internally or externally heated walls,³¹⁰ although heating rates are so slow as to qualify as slow pyrolysis.³¹³ Residence times of solids and vapors in rotary kilns are highly controllable, depending upon rotational speed and carrier gas flow rates.³⁴³ Rotary kilns are considered robust and affordable however they are limited to certain scales due to heat transfer.³¹⁰

Stirred tank reactors, also known as melting vessels, have been used for pyrolysis of plastics in batch, ²⁶⁶, ³⁴⁴, ³⁴⁵ semi-batch, ²⁵⁷ and continuous operation. Commercial examples include the Smuda process, ³⁴⁶ the Hitachi Zosen process, ²⁷⁴ and the Plastic Energy process. ³⁴⁷ Stirred tank reactors are characterized by a simply-designed vessel heated through the reactor wall and a stirrer to promote uniform heat distribution and homogenous reactants. Heat gradients, large infrastructure requirements, and frequent maintenance limit the use of stirred tank reactors. ³¹¹ Stirred tank reactors are primarily used for batch reactions, which is not economical on a large continuous scale process.

Pyrolysis reactors can be heated by a heat carrier (Figure 19a) or with an external heat exchanger (Figure 19b). The heat balance when a heat carrier is used is shown in Eq.1, where \dot{M}_{cat} is the mass flow rate of catalyst (or heat carrier), C_p is the heat capacity of the gas, T is the temperature, \dot{M}_{feed} is the mass flow rate of reactant, and ΔH_{rxn} is the net energy of the heat of the pyrolysis reaction. When using a heat carier, the reactor can be scaled to larger industrial sizes without limitations to the heat transfer area by use of an external fluid. In constrast if an external fluid is used for heating the energy balance is dependent on the heat transfer area as shown in Eq.2 and 3.

$$\dot{M}_{cat}Cp(T_{out}-T_{in})=\dot{M}_{feed}(\Delta H_{rxn}+Cp(T_{out}-T_{in}))$$
 Eq.1

$$\dot{Q}_{in} = UA\Delta T = \dot{M}_{feed}(\Delta H_{rxn} + Cp(T_{out} - T_{in}))$$
Eq.2

$$A=2\pi rL$$
 Eq.3

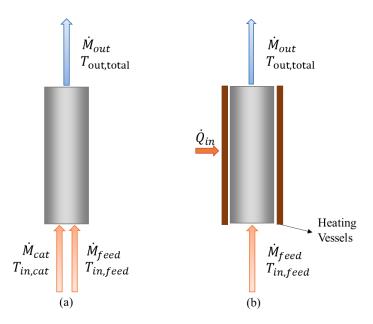


Figure 19. (a). Scheme of reactor with heat carrier (b) Scheme of reactor with external heating vessels

PE pyrolysis requires around 260 kJ/kg of heat.³⁴⁸ In a larger reactor, the heat transfer efficiency decreases due to the larger reactor diameter. Brown et al.³⁴⁹ reported that the maximum diameter of biomass fast pyrolizer is 9.4 mm, and an analogous calculation for a PE pyrolizer obtained a maximum diameter of 6.4 cm. The reaction rate of PE used for the calculation is obtained from Zhao et al.²⁵¹ In addition, the overall heat transfer will be affected by the bulky nature of the fed plastic, and the real diameter of the plastic pyrolyzer may be smaller than 6.4 cm. Autothermal pyrolysis can help to reduce the amount of heat required for pyrolysis by adding a certain amount of oxygen to partially oxidize the hydrocarbon feed, which makes the rate of energy release from the oxidation reaction equal the rate of energy consumed by the plastic pyrolysis.³⁴⁹ However, one main problem of the autothermal process is that it causes hot or cold spots due to the heat absorbed or released from the autothermal pyrolysis. The key to eliminating the hot and cold spots is again improving heat transfer within the reactor.

5.1.4 Economic Analysis

Hundreds of species of hydrocarbons may be present in the pyrolysis oil, including olefins, paraffins, aromatics, diolefins, iso-paraffins, and naphthenes. PE-derived oils have high concentrations of linear hydrocarbons, while PP-derived oils contain more branched components such as trimers, tetramers, and pentamers of propene. Many petroleum companies like Shell, BP, TotalEnergies, SABIC, and ExxonMobil, are planning to upgrade pyrolysis oil through steam cracking. Kusenberg et al. 404 has reported that the uncertainty and contaminants in the pyrolysis oil hampered industrialization.

Various studies have shown that the profitability of plastic pyrolysis refineries depends on several factors including feedstock cost, yield rate, product type to facility scale. Feedstock composition, pyrolysis yield, and product selectivity are critical drivers for process efficiency. Feedstock cost, capital investment, and market prices play a significant role in the profitability of

a plastic pyrolysis facility. Table 12 summarizes the key assumptions and findings from several studies on plastic pyrolysis. ^{277, 355-357} Fivga & Dimitriou investigated the pyrolysis of plastic waste to produce wax/oil products that can be used as a heavy fuel oil substitute or as raw materials by the petrochemical industry. The study evaluated a base case scenario of a 0.7 kton/year pyrolysis pilot plant built by a recycling company in the United Kingdom. The base case analysis resulted in a capital cost of 1.34 MM USD. The product cost from the base case scenario was 0.98 USD/kg of fuel produced, which was more than the market price of the heavy fuel oil product of ca.0.8 USD/kg. Increasing the pyrolysis scale from 70.1 kton/year to 701 kton/year decreased the product price from 29.4 cents to 3.39 cents per kg. ³⁵⁵ The pyrolysis plants can be designed as either closed-loop or open-loop where the former indicates recycled material can substitute the original virgin material further be used in the same type of products and the latter means the properties of the recycled material differ from those of the virgin material, so it is can substitute other materials in other product applications. ³⁵⁶ Larrain et al. also emphasized that to make an open-loop plastic pyrolysis plants should be scaled up to at least 70 kton/year and 115 kton/year, respectively. ³⁵⁶

Larrain et al. investigated the economic feasibility of open-loop and closed-loop pyrolysis of mixed polyolefins (mainly LDPE and residual PP) in a 120 kton/year facility in Belgium. In the open-loop system, the process only produces naphtha, while the closed-loop system produces naphtha and wax. The study recorded a base case net present value (NPV) per tonne of plastic waste processed of 32.5 USD/ton and 2.72 USD/ton for the open-loop and closed-loop systems, respectively. The market value of the products resulted in a significant difference of 24.75 USD/ton, thereby emphasizing that the type of products plays a vital role in the facility's profitability. The study went further to consider the uncertainties in oil prices that significantly affect the prices of wax and naphtha in the market and concluded that the open-loop system has about 98% probability of achieving positive returns compared to 58% recorded for closed-loop system ³⁵⁶.

Gracida-Alvarez et al. conducted the economic analysis of a multi-product 193 kton/year pyrolysis-based refinery for the conversion of HDPE to value-added chemicals (ethylene, propylene, and aromatic mixtures) and hydrocarbon mixtures via pyrolysis. In this study, the authors estimated the capital cost, operating cost, and NPVs for a base case where HDPE is converted to the products and a heat integrated case. The authors reported a capital cost of 118.5 MM USD for the base case and 120.5 MM USD for the heat integrated case. The NPV can range from 320 MM USD to 450 MM USD depending on the selling price of low MWHCs and the internal rate of return (IRR). The study showed that plastic pyrolysis targeting multiple products could be very profitable.

Table 12. Summary of waste plastic techno-economic analysis pyrolysis articles by feedstock, products, region, capacity, capital cost, and return on investment (ROI).

Technology	Feedstock	Major Products	Region	Capacity (kton/year)	Capital Cost (MM USD)	NPV (\$)	Ref
Pyrolysis	PS, PP, PE	Heavy oils Petrochemical feedstock	United Kingdom	0.7 - 701	1.36 – 77.2	-0.44 /kg – 0.71 /kg	355
Pyrolysis + upgrading	PS, PP, PE, PET	Hydrocarbon Fuel	Korea	260	\$ 118MM	0.062 /gal	277

Pyrolysis	PE, PP, PET	Diesel Power Char	Australia	14.6	3.76 MM	2.03 MM	359
Pyrolysis & Heat Integration	HDPE	Ethylene Propylene	United States	193	118.5MM - 120.5 MM	\$367.8MM - \$383MM	358
Fast Pyrolysis (Open-loop & closed- loop)	Mixed Polyolefins mainly LDPE and residual PP	Naphtha	Belgium	120	Not disclosed	open loop: 32.5/ton Closed loop: 2.72 /ton	356
Pyrolysis	Plastic waste (PP, PE, PS)	Light oil Heavy oil	Malaysia	120	58.6 MM	20.9 MM	357

5.1.5 Commercial Activities

Table 13 lists the publicly made announcements about major plastic pyrolysis technologies that are in operation, were previously planned or are currently planned. Western Europe began to study plastic pyrolysis in the late 1970s.²⁸⁶ The first of these plants was designed by BP in 1994. Using mixed waste packaging plastics, research on a laboratory scale was followed by demonstration on a continuous pilot plant scale (nominal 50 kg/hr) at BP's Grangemouth site. BP Chemicals, VALPAK, and Shanks & McEwan formed a collaborative initiative (POLSCO) in 1998 to study the viability of a 25 kton/year factory with a fluidized bed reactor, which would include logistical infrastructure for delivering mixed plastics from Scotland.³⁶⁰ This plant was never built because BP claimed it would require a tipping fee of 250 €/ton (225 \$/ton) to fulfill a 15 − 20 M£ (24.75 − 33M\$) total investment cost of this plant. ²⁸⁶

In Europe, there are 3 operating pyrolysis plants owned by Quantafuels and Plastic Energy. Quantafuel's first commercial production facility is in Skive, Denmark. The plant processes 20 kton/year. The liquid product is sent to BASF, who uses the liquid product to produce virgin plastic and other chemicals.³⁶¹ Plastic Energy currently has two plants in Almeria (started in 2014) and Seville (started in 2017) in Spain. The plant in Seville has the ability to treat 5 kton/year.³⁶²

Several companies have announced plans in the past few years to build plastic pyrolysis plants and convert the plastic oils into aromatics/olefins by steam cracking. In Germany, SABIC and BP announced in 2021 plans to build a plastic recycling plant in Gelsenkirche.³⁵⁴ BP will build plants to steam crack the plastic oil obtained from SABIC and forward the cracking materials to SABIC for making new plastics.³⁵⁴ One goal of BP is to achieve 30% of propylene and ethylene produced from recycled material by 2030.³⁶³ Shell plans to work with Pryme to build a plastic pyrolysis plant and produce circular chemicals in the Netherlands and Germany with the capacity of 60 kton/year in 2022.³⁶⁴ Plastic Energy announced a collaboration with ExxonMobil in early 2021. Starting in 2023, ExxonMobil will use the plastic oil from Plastic Energy and upgrade the plastic to a naphtha-quality petrochemical feedstock.³⁵³ The company has started to construct a recycling plant in France next to ExxonMobil's Notre Dame de Gravenchon petrochemical complex, which will have a capacity of 25 kton/year. ³⁶⁵ QuantaFuel plans to build a 100 kton/year plant in Sunderland UK and to work with VITOL and VITTO to build another 100 kton/year plant in Amsterdam. ³⁶⁶ Fuenix Ecogy raised €4 million (\$ 4.53 million USD) to scale up its technology to recycle mixed plastic waste, and in a collaboration with Dow to build a plant to

pyrolyze plastic in Weert, Netherlands in 2019.³⁶⁸⁻³⁶⁹ The pyrolysis plastic oil will be sent to Dow Terneuzen, Netherlands, for steam cracking and producing virgin quality plastics.³⁷⁰ The goal for both Dow and Fuenix is to generate 100 kton of the recycled plastics by 2025.³⁷¹

In the US, Brightmark is planning to build one of the largest plastic pyrolysis plants in the world, with a scale of 100 kton/year, in Ashley, Indiana.³⁷² Freepoint Eco-Systems plan to invest 60 million USD to construct a plastic pyrolysis plant in Obetz, Ohio, with a capacity of 90 kton/year. The company claims that the plant will be operating in 2023 and will be able to convert 300 tons of waste plastic into 1500 barrels of oil.³⁷³⁻³⁷⁴ TotalEnergies is also working with the Freepoint Eco-Systems to build a 33 kton/year plant in Houston, Texas in mid-2024. The products will be sent to TotalEnergies' steam cracker to produce monomer and manufacture high-quality plastics.^{351,375} Agilix and ExxonMobil created a joint venture together called Cyclyx International, which will be focused on creating novel ways to collect and pre-process massive amounts of plastic trash into feedstocks for higher-value products.³⁷³

There are also some plastic pyrolysis projects underway in Asia. Shell decided to start producing plastic oil with a capacity of 50 kton/year at Pulau Bukom, Singapore in 2023. ³⁷⁶ Plastic Energy collaborates with WWF-Indonesia and aims to help Indonesia to reduce 100 kton of plastic waste by 2025. ³⁷⁷ Insights provided by McKinsey showed that pyrolysis could be the most profitable process in the coming years. ³⁷⁸ Due to the large amounts of oil required to run the hydrocarbon economy, the use of blends of plastic pyrolysis products and petroleum-derived feedstocks is expected to expand. ³⁰⁴

Table 13. Commercial plastic pyrolysis plants that were previously planned, operational or shut down

Name	Plant location	Scale (kton/yr)	Status	Reactor type	Feedstocks	Product	Collaborators	
BP ³⁶⁰	Grange-mouth (Polit plant)	25	1998-2000 (Design only)	Fluidized bed reactor	PP, PE, PET, PS, PVC	Hydrocarbon liquid	VALPAK, and Shanks & McEwan	
BASF ³⁶⁰	Ludwig-shafen (Polit plant)	15	1994-1996	Not reported	Not reported	Not reported	Duales System Deutschland	
Agilyx ³⁷⁵	Tigard (Polit plant)	3	Operational since 2018	Stirred tank reactor	PS	Styrene monomer	Toyo, Exxon Mobil, Braskem, AmSty, Lucite, and NextChem	
Skive (Polit plant)		20	Operational since 2017					
QuantaFuel 366 338, 367	Amsterdam	100	Under construction and plan to operate in 2023-2024	Fluidized bed rector	HDPE, LDPE, PP, PS, and PET	Liquid oil, non-condensable gas, and carbon rich ash. The liquid oil will be used to	BASF, VITOL, and VITTI	
	Sunderland	100	Under construction and plan to operate in 2024	-	rs, and re1	produce virgin-quality plastic		
Pryme ^{352,} 379	Rotterdam	40-60	Under construction and plan to operate in 2022	Fluidized bed reactor	PS, PE, and PP	Kerosine, naphtha, and wax followed with steam cracking to obtain petroleum products	Shell	
Brightmark 338, 372, 380	Asheley	100	Partially Operational since 2021	Auger rector	PET, HDPE, PVC, LDPE, PP, and PS	Ultra-low sulfur diesel, naphtha, and wax	BP, Chevron, Clean fuel Partners, and Northeast Indiana Solid Waste Management District	
Plastic — Energy ³⁵³ ,	Seville (Pilot plant)	5	Operational since 2017	Ctime d	I DDE	Diesel and naphtha followed	SABIC, ExxonMobil,	
	Le Havre	25	Design phase planned to start up in 2023	- Stirred tank	LDPE, HDPE, PP, PS	with steam cracking to obtain raw materials to make new	and Freepoint Eco-	
	Almeria	Not reported	Operational since 2014	- reactor	13	plastic	Systems	

Table 13 (cont.)

Name	Plant location	Scale (kton/yr)	Status	Reactor type	Feedstocks	Product	Collaborators
Freepoint Eco-	Houston	33	Plan to operate in Mid-2024	Fluidized bed	LDPE, HDPE, PP,	Synthetic oil	Plastic Energy, and
Systems ³⁷³	Obetz	90	Plan to operate in 2023	reactor	PS	Synthetic on	TotalEnergies
Shell ³⁷⁶	Pulau Bukom	50	Under construction and plan to operate in 2022	Not reported	Not reported	Not reported	Pryme
ExxonMobil	Baytown	30	Under construction and plan to operate in End-2022	Fluidized bed reactor	Not reported	Not reported	Cyclyx, Agilyx, and Plastic Energy

5.2 Catalytic Thermal Decomposition of Plastics5.2.1 Catalysts

Numerous catalysts have been explored for catalytic pyrolysis with entire review papers written on this topic. 20, 381-383 A large number of catalytic pyrolysis studies focus on the use of aluminosilicate materials such as amorphous SiO₂-Al₂O₃, mesoporous SiO₂-Al₂O₃, and zeolites. Aluminosilicates offer the unique advantage of having tunable acidity which can be used to direct the product selectivity of catalytic pyrolysis transformations. ¹⁰ By increasing the alumina content - and thus acidity - within these materials, improved selectivities towards gas fractions can be achieved, while lower acidity can yield greater liquid fractions.³⁸⁴ Aluminosilicates can increase product quality, and reduce residue production as compared to thermal degradation. 382, 384-393 Amorphous SiO₂-Al₂O₃ lacks a pore network that could induce higher control over product selectivity.³⁸¹ Mesoporous catalysts have been explored for catalytic pyrolysis to increase masstransfer. 381 The presence of mesopores allow for improved diffusion of the plastic molecules, which accelerate the initial rate of degradation and thus enhance plastic cracking. Both pure silica (kanemite-derived folded silica, FSM, MCM-41) and aluminosilicate (Al-MCM-41 and SBA-15) mesoporous structures have been explored for the degradation of PSW with varying success.³⁸⁹, ^{391, 394-399} Pure silica mesoporous materials were found to yield higher quantities of liquid products - with higher selectivity towards kerosene and diesel fractions - during the catalytic pyrolysis of PE and PP as compared to thermal degradation. 389, 394 It was found that the siloxane oxygens lining the channels of the mesopores could interact with the hydrogen atoms of the polymers to induce cracking. 397 The interaction allows for liquid oil product selectivity to be increased at the expense of heavy oil and wax fractions.^{395, 398} Additionally, the mild acidic character of the pure silica materials was found to enhance the cracking rate of polymers as compared to thermal degradation while also inhibiting extensive secondary cracking. As such, the all-silica mesoporous catalysts were found to be coke-resistant throughout multiple runs.³⁸⁹

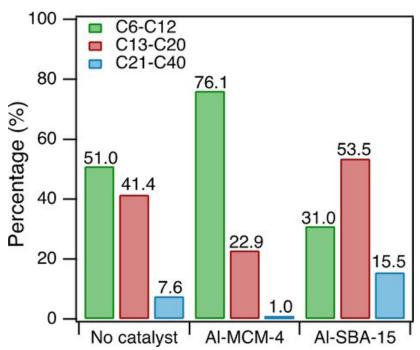


Figure 20. Distribution of liquid and wax products for thermal pyrolysis and mesoporous aluminosilicates in the conversion of PE/PP (ratio 6:5). Pyrolysis experiments were conducted at 500°C for 30 minutes using a batch reactor set up, where the catalyst-to-feedstock ratio was 0.03:1. Published with permission from ref ⁴⁰⁰. Copyright Wiley-VCH.

For mesoporous aluminosilicates, the plastic decomposition product distribution was dependent on the acidity of the material. Low-acidic materials (Al-MCM-41, Al-SBA-15) have high resistance to coking and increased cracking activity compared to all-silica materials. ^{391,399, 401-403} The additional acidity induced by the presence of alumina sites facilitates plastic cracking and can yield higher selectivity towards lighter hydrocarbons. For example, the product distribution for a PP/PE mixture was shifted towards C₆-C₁₂ products for Al-MCM-41, while Al-SBA-15 yielded high-quality diesel oil (high selectivity towards C₁₃-C₂₀ fraction, Figure 20). However, both Al-MCM-41 and Al-SBA-15 were found to degrade a mixed plastics feed (HDPE, LDPE, PP, PE, and PS) to a similar product distribution of near equal amounts of C₁-C₅, C₆-C₁₂, and C₁₃-C₄₀ hydrocarbons. ^{401, 404} The large pore size of mesoporous aluminosilicates allows for improved intercalation of polymer molecules to Brønsted acid sites but prevents the moderately cracked products from undergoing re-adsorption and secondary reactions that result in extensive cracking. ⁴⁰⁵ However, it was found that the promising cracking ability of mesoporous materials was only effective with polyolefin and polyaromatic PSW – polymers with other heteroatoms form coke which causes catalyst deactivation. ⁴⁰¹

While mesoporous aluminosilicates were found to be capable of producing favorable product distributions with limited amount of coke, zeolites have still been extensively explored for the catalytic pyrolysis of plastic waste. ^{20, 381} Zeolite Y was found to have high cracking ability due to its high accessibility to active sites, but the larger micropores and high acidity were found to facilitate condensation and secondary reactions leading to fast deactivation. ⁴⁰⁶⁻⁴¹⁴ Similarly, ZSM-5 has high cracking activity for polyolefins due to its strong acidity. ^{412, 415-424} The microporous

network within the ZSM-5 structure is ideal for the aromatization of cracked intermediates, however this precludes coke formation and fast deactivation. β-zeolite yields higher gas fractions at the expense of liquid products because it is highly active for secondary reactions. 388, 425-430 Additionally, β-zeolites were found to produce high quantities of residue and wax. Natural zeolites were found to have moderate cracking ability with higher selectivity towards the liquid fraction, but its efficiency was strongly correlated to the plastic/catalyst ratio. 392, 431-441 Given the uncontrolled structure of natural zeolites, the materials contain impurities and there is little consistency amongst the materials. As such, there is high variability in the effectiveness of natural zeolites. Lastly, doped zeolites have been explored to enhance the acidity of the material. 435, 442-451 Doped zeolites were found to yield high selectivity towards olefinic products and were active for the removal of heteroatoms such as Br. One great challenge of the catalytic pyrolysis of plastic waste with zeolites is catalyst deactivation due to secondary coking reactions and limited diffusion of polymeric molecules into the microporous network.

Clays are another form of aluminosilicate that are of interest due to their weaker acidity, wide availability, and ability to produce medium distillate products such as diesel fuel. 408, 452-455 Clays are composed of silica and alumina or magnesia (or both) and have a macroporous structure which induces high coke resistance and moderate polymer cracking to heavier products. Structured clays, such as pillared clays (PILC), can include heteromoieties like metal oxides (Al, Fe, Ti, and Zr) to improve the textural properties and increase catalyst acidity. 452-455 As such, PILCs have been found to have improved catalytic performance for HDPE and PE, as well as improved regeneration abilities. Clays, however, have lower activity due to the macroporous nature of the material, resulting in reduced contact of the feedstock with the weakly acidic sites within the structure.

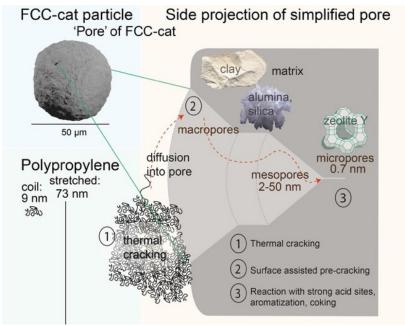


Figure 21. Structure of a spray dried FCC catalyst. Published with permission from ref ⁴⁵⁶. Copyright Wiley-VCH.

Spray dried catalysts (typically Geldart Particle size A) are used in fluidized bed reactors

because they are easier to flow in the fluidized bed. Spray dried catalysts (Figure 21) are a mixture of clays or binders, zeolites, and silica-alumina matrices. 456-462 Spray dried catalysts can have a bimodal pore structure with micropores in the zeolite framework and mesopore in the silicaalumina matrix. It was recently determined by Weckhuysen and coworkers that, in the conversion of PP, the fluidized catalytic cracking (FCC) matrix was responsible for aromatization of cracked products and the zeolite domain was responsible for coking. 456 Zeolite and silica alumina catalysts can undergo structural changes during the reaction due to water vapor (dealumination) and impurities from the feed building up on the catalyst surface. Thus, in a circulating fluidized bed reactor, such as in fluid catalytic cracking, it is important to study the "equilibrium catalyst." It is the equilibrium catalyst which is the actual catalyst in the reactor. Studies of the effect of the equilibrium FCC catalyst on PP conversion found the same aromatic content as fresh FCC catalysts with reduced coking. The zeolite domains in an equilibrium catalyst were found to be inaccessible - resulting in reduced coking - and the FCC matrix was found to have enhanced cracking activity due to leached metal deposits. This work by Weckhuysen and co-workers suggests that the strong acidity and microporous structure of the zeolite domain within an FCC catalyst is not necessary for the aromatization of polyolefin feedstocks. 456 Further, the presence of zeolite domains may even be detrimental to the effectiveness of FCC catalysts for the catalytic pyrolysis of plastic waste.

Like FCC catalysts, multi-catalyst systems are zeolites mixed with MCM-41, NiO, muds, clays, salts, or metal silicates. 395, 463-467 The systems are typically formed by either the mechanical mixing of the two separate catalysts via mortar and pestle or by layering the catalysts within the bed. As with other catalytic pyrolysis systems, the presence of the catalysts reduces the required temperature for polymeric degradation as compared to thermal pyrolysis. 463, 466 The use of muds and clays with zeolites - such as a combination system of zeolite Y, metakaolin, aluminum hydroxide, and sodium silicate – has been found to improve the selectivity toward liquid products for a mixed plastic waste feed stream as compared to thermal pyrolysis. 414, 468-469 Additionally, red mud and calcium hydroxide was found to reduce chlorine content in the products. The combination of zeolites and MCM-41 has been found to induce synergistic effects on plastic degradation, where the MCM-41 provides enhanced surface area, and the zeolite provides strong acidity. 463 For zeolite/MCM-41 systems, diffusional limitations were observed for the direct catalytic pyrolysis of HDPE. In two-stage pyrolytic-catalytic cracking with HZSM-5/MCM-41, a high yield of aromatic gasoline range products was formed. 463 Similarly, HY-zeolite/NiO was explored in a twostage reactor. 465 The addition of NiO was found to increase gas selectivity at the expense of liquid products and reduce coke formation as compared to HY-zeolite alone. NiO was speculated to promote primary degradation of larger polymer fragments into radicals preventing coke deposition. 465 In total, composite systems can induce favorable synergistic effects that can result in a narrowed carbon number distribution of products as compared to thermal pyrolysis, however the favorable effects are highly dependent on the catalyst mixture ratio. Further, diffusional limitations are increased in composite systems given the physical mixture of varying pore networks and may require two-stage pyrolysis-catalysis.

Like composite systems, hierarchical and core-shell catalysts combine the advantageous properties of various materials into one system. Unlike composite systems, hierarchical and coreshell catalysts are contained within one structure rather than in a heterogeneous mixture or across multiple reactors. Many of the studies to date of hierarchical or core-shell catalysts for plastic waste deconstruction combine the micropores of zeolites with secondary mesoporosity. 444-445, 448-

^{449, 470-480} The goal is to allow for enhanced accessibility where faster intra-crystalline diffusion and lower steric hindrances occur. Catalysts such as these have been found to have higher resistance to coking and deactivation compared to traditional microporous zeolites. ⁴⁷⁸ Further, the secondary porosity of such materials renders improved gas and aromatic hydrocarbon production than their microporous counterpart. Hierarchical and core-shell materials are capable of supporting metals to enhance acidity and therefore activity. ^{445, 448-449, 470-475, 477-478} However, these materials require refined and detailed synthesis – making scale up difficult – and the dual porosity must be well defined otherwise deactivation via coking will occur.

Silica and aluminosilicates have dominated catalytic pyrolysis because of their porous networks and acidity, however other metal oxides such as ZrO2, MgO, and CaO have shown interesting results. 481-493 In particular, sulfated zirconia – despite suffering from coke deactivation – has shown high cracking activity and isomerization, esterification, and hydrocracking ability. 484, ^{486, 491, 493} By sulfating the metal oxide, the acidity of the material is enhanced, resulting in improved reactivity. Further, studies have explored promoting sulfated ZrO₂ with platinum and found that the material – in a two-step pyrolysis-catalytic hydrocracking process – can enhance the hydrocracking of LDPE into liquid products as compared to the non-doped material. 482 Other metal oxides such as MgO and CaO, have been shown to reduce activation barriers and enhance selectivity toward phenolic compounds for PC catalytic pyrolysis, as well as reduce production of light gases (H₂, CO₂, CO, and methane) for PC and LDPE degradation. 481, 483, 487-488, 490 It was determined that the basicity of CaO allowed for the reaction of CO₂ in the pyrolysis vapors, resulting in the production of CaCO₃, while MgO was found to interact with H₂ and utilize the molecule for hydrogenation reactions. 487, 490 However, CaO and MgO produce significant amounts of solid residue, where the carbonaceous char inhibited the movement of free radicals during the cracking reaction, preventing propagation and degradation of the plastic molecule. 483

Outside of metal oxide catalysts, activated carbon has been tested for plastic catalytic pyrolysis but has been found to only minimally change product distribution. 395, 480, 494-496 Further, activated carbon has variable acidity – which can be modulated by the addition of different acid groups (-OH, -OOH, and -P—O) – that dictates the product distribution. 495, 496 Weakly acidic activated carbons have been found to have high selectivity towards jet-fuel range alkanes within the liquid fraction and strongly acidic carbons (with P functionality) have improved selectivity towards jet-fuel range aromatics. Additionally, metal-doped carbons have been utilized for PSW decomposition due to the high thermal stability of the material and the cracking ability of transition metals. For example, Pt/C and Pd/C were found to decompose PET into monocyclic compounds within the liquid fraction by improving decyclization activity and promoting thermal free radical cracking mechanisms. 497 Pt/C was also found to crack the carbonaceous compounds that formed during catalytic pyrolysis of PET, further inhibiting the production of undesirable products. 497

Like many of the catalysts described above, carbonates have been found to increase the rate, reduce operational temperature, and reduce residence time of plastic decomposition. However, carbonates are prone to decomposition under thermal treatment, resulting in the formation of oxide compounds and CO₂. MgCO₃, CoCO₃, and CuCO₃ were all found yield largely diesel fuel components in the liquid fraction for the catalytic pyrolysis of HDPE. ⁴⁹⁸⁻⁵⁰¹ At the same time, gas yields were increased by 10-15% due to the decomposition of the material under reaction conditions. ⁴⁹⁸ The basic carbonates were hypothesized to initiate the plastic cracking mechanism via a different step than the acidic catalysts previously described, where the carbonates will accept

a proton from a plastic defect site to create a carbocation chain rather than the catalyst donating the proton to form a carbonium molecule. The carbocation chain will undergo β -scission to form lower carbon number alkanes and alkenes, then further reaction will occur through carbonium ion attacks or interactions with the catalyst basic sites.

Ashes from plastic incineration plants have also proven to be effective in reforming plastic pyrolysis vapor using a pyrolysis-reforming reactor. Incineration ashes contain ppm levels of metals due to metal evaporation and adsorption to the surface of ash particles during incineration. When used for in-line upgrading of plastic vapor, flying ash increased the BTX content of liquid product compared to non-catalytic upgrading. The Fe content of ash promoted the formation of monoaromatics while inhibiting the formation of polyaromatics. Although the use of ash as a catalyst is attractive as it is a waste, the catalytic performance of this material is still inferior compared ZSM-5. Furthermore, pretreatment of ashes is required to remove impurities that prevent access to active sites.

5.2.2 Reactor Design

Two main approaches for catalytic pyrolysis have been proposed for plastic conversion: a single-stage catalytic-pyrolysis (*in-situ*) process and a two-stage pyrolysis-catalysis (*ex-situ*) process. In the single-stage process, the plastic waste and catalyst are directly mixed in a reactor (usually a fluidized bed reactor, Figure 22) and heated to the degradation temperature. In the two-stage pyrolysis-catalysis process, the plastic waste is first thermally pyrolyzed and then the pyrolysis vapors are passed over a catalyst bed (which could potentially be a fixed bed reactor). ⁵⁰⁴ Fluidized beds are the most commonly used industrial reactors for processing solid materials. They have high rates of heat transfer and therefore can be scaled to larger industrial reactors. ⁵⁰⁶ Circulating fluidized bed reactors are commonly used in industry as they circulate the catalyst between a reaction and regeneration zone, where the coke on the catalyst can be continuously removed by oxidation. In contrast, fixed bed reactors must be shut down when the catalyst is regenerated leading to a decrease in capital efficiency. Fixed-bed catalytic reactors are preferred when no solids reactants or products are formed as they are simpler to design and operate than fluidized bed reactors. Plugging of the fixed-bed reactors is another major concern when operating with solids or having reactions that form larger amounts of coke.

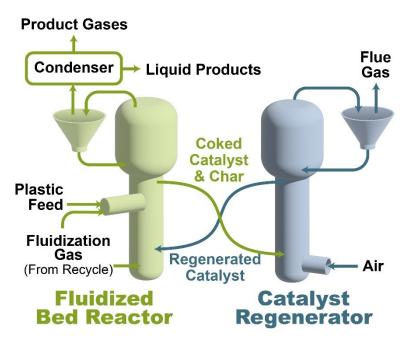


Figure 22. Fluidized bed reactor for plastic pyrolysis. 507

5.2.3 Commercial Activities

Anellotech, who originally developed a technology to catalytic convert biomass into aromatics called Bio-TCat, has developed a sister process that transforms plastic waste into virgin commodity chemicals using a circulating fluidized bed reactor. The process, Plas-TCat, converts mixed plastic waste into olefins and aromatics to be used as "drop in" raw materials to produce new plastics and work towards a plastic circular economy. ⁵⁰⁷ Plas-TCat uses a zeolite catalyst in a fluidized bed reactor to generate the desired products in a single catalytic step. ⁵⁰⁷⁻⁵⁰⁸ The technology can be used to either produce a high olefin or high aromatic product from mixed plastic wastes. It has several advantages compared to pyrolysis and steam cracking including lower capital cost, higher value of product, scalability of the fluidized bed reacotor system, feedstock flexibility, and a narrower product yield.

Braskem, the leading biopolymer producer of thermoplastic polyolefins in America, has formed several partnerships to develop new catalysts for plastic catalytic upgrading. ⁵⁰⁹⁻⁵¹¹ Braskem is working with FCC S.A., the leading catalysts supplier of fluid catalytic cracking in the South American market, to develop new catalysts for plastic upgrading. In addition, Braskem and Encina have formed a long-term partnership to produce recycled PP. Encina development group is focusing on developing a catalytic pyrolysis process to produce BTX from plastics #3 through 7, with the focus on PP.

6.0 Liquefaction of Plastics

Liquefaction typically operates at temperatures between 200-450 °C under high pressure to convert the plastic feedstock into a liquid oil in the liquid phase. Heterogenous or homogenous catalysts are sometimes added.⁵¹²⁻⁵¹³ When liquefaction occurs in a solvent, it is called solvent liquefaction. Fuel liquids or monomers can be obtained from the liquefaction of plastics.^{512, 514-522}

During liquefaction, pressurized nitrogen or other gases keep the pressure high, helping maintain the products in the liquid phase. Pressurized hydrogen enhances polymer chain cleavages, caps the chain ends with hydrogen, and produces liquids with higher H/C ratios and/or low boiling point products. Various organic solvents, including hydrocarbons, alcohols, and water, are used to enhance the reaction rate and lower the activation energy of plastic decomposition, in addition to reducing unfavored secondary reactions for repolymerization. Chemically-compatible solvents can facilitate product removal and dissolution, suppressing intermolecular coupling reactions. Hydrogen-donating solvents can enhance product dissolution and stabilize intermediate products.

When performed under supercritical states of solvents, solvent liquefaction also takes advantage of drastically increased reaction rates and enhanced solubilization capability of the polar and non-polar products. ^{517, 527} In the case of hydrothermal liquefaction (HTL), water is a low-cost green solvent. Table 14 summarizes some of the previous work on plastic liquefaction processes, which are grouped into liquefaction using pressurized gases, HTL, and liquefaction by organic solvents with the majority of this work in stirred-tank batch reactors.

6.1 Products

6.1.1 Liquefaction using Pressurized Gases

Direct liquefaction of plastics using pressurized gases has been investigated since the 1990s, mainly applied to producing synthetic fuel oils from individual non-polar polymers or co-mingled waste plastics. Increasing the reaction pressure during liquefaction enhances liquid production and reduces gas formation. Hydrogen can be added to the liquefaction process to increase product yields by hydrogenating the products in a single step. Williams et al. 522 reported an increase in the oil yields from 71% to 77% for PS and 15% to 27% for PET by switching from a nitrogen to a hydrogen atmosphere, which almost entirely contributed to the decreased solid yields. In comparison, there were no significant increases in the oil yields from PE and PP by switching from a nitrogen atmosphere to hydrogen, as shown in Table 14. Liquefaction under pressurized gases also promotes the formation of aromatics from PE and PP. While PE pyrolysis at atmospheric pressure nitrogen almost exclusively produced aliphatic hydrocarbons, the oil produced using pressurized nitrogen contained 16.4% aromatics. 522 The increased gas pressure promoted secondary reactions of PE decomposition, such as saturation, cyclization, and isomerization. 528 Cyclization reactions were also promoted during hydrogen liquefaction, albeit less so than in liquefaction under nitrogen gas.⁵²² The work of Williams et al. also showed that hydrogen liquefaction increased the selectivity of single-ring aromatics for PS, 522 because the hydrogen atmosphere enhanced both chain cleavage and secondary saturation reactions compared to nitrogen.

Solid acid catalysts are often used during the hydrogen liquefaction of plastics. In general, the addition of catalyst lowers reaction temperature, increases conversion, and produces oils with higher light fractions. Shabtai et al. reported that conversion of HDPE during hydrogen liquefaction at 350 °C increased from nearly zero without a catalyst to 30% with a 17 wt% of SO₄/ZrO₂ catalyst, and 64.7% using a 33% Pt/SO₄²⁻/ZrO₂ ctalyst.⁵¹⁹ Much lower metal loadings were used in other related studies. For example, Zmierczak et al.⁵¹⁶ found catalytic hydrogen liquefaction of PS at 375 °C increased the conversion from 59.4% without a catalyst to 70.5% with a 5 wt% Fe₂O₃/SO₄²⁻ catalyst and to 80.3% with a 5 wt% ZrO₂/SO₄ catalyst. Other catalysts were also evaluated for hydrogen liquefaction, as shown in Table 14. Shah et al. converted post-

consumer plastic waste using 1 wt% HZSM-5 zeolite, a ZrO₂/WO₃ catalyst, nanoscale ferrihydrite treated with citric acid, ferrihydrite containing 5% Mo, a SiO₂-Al₂O₃ binary oxide, and two TiO₂-SiO₂ binary oxides.⁵²¹ They reported that while there were no significant differences in the oil yields, the presence of ZSM-5 reduced the boiling point distribution of the oil products resulting in the most gasoline-like products. Similar results were also observed by Feng et al.⁵¹⁸

Chemically compatible or hydrogen donor solvents have been used to aid the hydrogen liquefaction of plastics. For example, adding n-octadecane during Pt/SO₄²⁻/ZrO₂ catalyzed hydrogen liquefaction of HDPE at 350 °C increased the conversion from 64.7% without solvent to 92.5% with the solvent.⁵¹⁹ The plastic conversion in the solvent without catalyst was only 2%.⁵¹⁹ Tetralin has been studied as a hydrogen donor for coal liquefaction. As shown in Table 14, Taghiei et al.⁵¹⁵ reported that tetralin-aid hydrogen liquefaction of PE and PP increased the oil yield from 11% without a catalyst to 83% with a catalyst.² In contrast, the oil yield only increased from 62% to 64% for PET. Since PE and PP-derived products are non-polar hydrocarbons whereas PET-derived products are oxygenated polar products, chemical compatibility between the solvent and plastic decomposition products seemed to play a critical role in their study. Murty et al.⁵¹⁷ reported that PVC absorbs tetralin and that this promoted PVC decomposition. Feng et al.⁵¹⁸ reported that liquefaction of co-mingled waste plastics in the absence of solvent resulted in higher oil yields than the liquefaction in tetralin or waste motor oil, regardless of whether catalyst was added or not.

Table 14. Literature reporting liquefaction of typical waste plastics (if not mentioned otherwise, assume stirred-tank batch reactors)

Type of Plastics	Temp.	Pressure (MPa)	Time (h)	Concentration (%)	Solvent/Gas/Catalyst	Products	Oil Yield (wt%)	Year	Ref.
				Liqu	efaction under pressuriz	ed gases			
PE, PP, PS (continuous reactor)	400	-	-	-	w/ or w/o ZSM-5	Majority aromatics, some aliphatic liquids and gases	85% (PE, PP); 90% (PS)	1992	514
MDPE, HDPE, PP, PET or mix	420-450	5	1	66% plastics in Tetralin/waste oil	H ₂ ; w/ or w/o 1 wt% HZSM-5/Ferrihydrite catalyst	Hydrocarbon oil and gases	w/o to with catalyst): 11 to 96% (HDPE); 83 to 98% (PP); 33 to 93% (MDPE)	1994	515
Mix of HDPE, LDPE, PET and PS	400-440	5.6	0.5-2	50% plastics in Tetralin, decalin, dodecane, C ₁₂ -C ₂₀ alkanes	H ₂ ; 10-20 wt% HZSM-5/FCC catalysts	Hydrocarbon oil and gases	56.2-75.8% conversion (mixture); 90-100% conversion (individual plastics)	1996	512
PS and SBR	350-450	3.45- 17.23	0.25-	1-5 wt% Fe ₂ O ₃ /\$	SO ₄ ²⁻ and ZrO ₂ /SO ₄ ²⁻	Aromatics (PS); Aromatics and C5-C9 paraffins/cycloparaffins.	80.3% (PS); 72% (SBR)	1996	516
LDPE, PET, PVC	420-440	5.5	0.25- 1	70% in Tetralin	Hydrogen	C9-C40 hydrocarbons and gases	59% (LDPE)	1996	517
MDPE, HDPE, PP	> 420	0.68-5.5	0.3-1		n; H ₂ or N ₂ ; HZSM-5 or D ₂ -ferrihydrite	Light, medium and heavy oils	> 90% (all plastics)	1996	518
HDPE, PP, PB	350-450	3.5-13.8	0.5-3		-2 wt% Fe ₂ O ₃ /SO ₄ ²⁻ and D ₂ /SO ₄ ²⁻	Gasoline range paraffins as major products	> 90%	1997	519
PE and PP	500	0.79	0.5	Ну	drogen	Light and heavy oils	up to 60%	1998	520
Post-consumer plastic (PCW) mixture	415-455	1.4	0.5-1	H ₂ , 1-5 wt% of	HZSM-5 and others	Higher gasoline range oil with catalysts	up to 85%	1999	521
PE, PP, PS, PVC, and PET (standalone and mixed)	500	1	1	Nitrogen	and Hydrogen	Hydrocarbon oil and gases with high concentrations of alkanes and single-ring aromatics	Calculated mix vs. PCW (DSD/Waste Fost Plus): 72.3% vs 32.5/64.1% (N ₂); 75.12% vs 48.2/70.6% (H ₂)	2007	522
					Hydrothermal Liquefact	ion			
HDPE	425	corresp.	0.16-		None	Light and medium oil	90.2% (120 min)	1999	523
SBR	450-686	<1000	0.022 -0.5		5/10% H ₂ O ₂	Light and medium HCs	25.9-66%	2002	529

Table 14 (cont.)

Type of Plastics	Temp.	Pressure (MPa)	Time (h)	Concentration (%)	Solvent/Gas/Catalyst	Products	Oil Yield (wt%)	Year	Ref.
				Н	ydrothermal Liquefa	ection			
HDPE	450-480	corresp. to T	0.016 -0.5	25-50	None	Light and medium oil	91.4% (460°C, 1 min)	2004	530
PVC	200-600	1.6-55.7	1	0.1-2	None	Low-molecular weight aromatic and aliphatic compounds	179ppm (300°C), 396ppm (400°C)	2004	531
HDPE (Continuous reactor)	530	25	0.02- 0.07	-	None	C7-C11, C12-C18, C19- C24, >C24	79%	2007	532
Model mix of PE, PP, PS and PVC	200-400	1-5		100-200	glass powder additive	Chlorine content after NaOH-based dechlorination	40-120 ppm in oil (negl.)	2011	533
PBT, PC, PLA, PMMA, POM, PPO, PVA, SB.	400	25	0.25	10	None	48/nil (PMMA), 13.7/8.1 (PO	T), 99.8/nil PC), /68.5 (PET), OM), 78.9/8.8 (PPO), 35.4/2.9 0.8/1.2 (SB)	2017	534
High Impact PS (HIPS)	350-550	30	0.12-	1-9	None	Ethylbenzene (51.3wt%), Toluene (14wt%) and other polyaromatics (490°C/1 h)	Maximum carbon Liquefaction rate of 77wt% (490°C, 1 h)	2019	535
PP	425-450	23	0.5-4	-	None	80% naphtha	91% (2 h/425 °C; 1 h/450 °C)	2019	536
ABS, PA6, PA66, PET, Epoxy, PC, PUR, HDPE, PVC, LDPE, PP, PS	350	corresp. to T	0.33	5.6	КОН	PA66), TE & EG (PET), TD	Epoxy), caprolactam + (PA6, A + (PUR) and no polyolefin- products	2020	537
PP, PS, PC and PET	350-450	25+	0.5-1	0.06-0.35	None		16% (PET, 450°C, 30 min), nd 60% (PC, 425°C, 30 min).	2020	527
PC	350-450	corresp.	0.03-	5	None	IPP, IPrP, phenol, BPA, and other alkylphenols	57.7	2020	538
HDPE	400-450	corresp. to T	0.5-4	57.1	None	Naphtha, heavy oil and heavy waxes	86-87% (425°C, 2.5 h or 450°C, 0.75 h)	2020	539
LDPE, HDPE	380-450	corresp. to T	0.25- 4	20	1% acetic acid	Alkanes, alkenes, cycloalkanes, aromatics, and negligible alcohols	85-90% (425-450°C, 1 h)	2020	513

Table 14 (cont.)

Type of Plastics	Temp.	Pressure (MPa)	Time (h)	Concentration (%)	Solvent/Gas/Catalyst	Products	Oil Yield (wt%)	Year	Ref.
					Hydrothermal Liquefact	ion			
Mix of LLDPE and PP	400	25	1	16.67	None	Paraffins, olefins, cyclics and aromatics	90.7% (mixture); 87.04% (LLDPE); 86.42% (PP)	2021	540
A waste mixture containing Polyolefins, PET, nylon, PVAc, and Cellulose	340	corresp. to T	5	10	2% NaOH	Aromatics, oxygenated compounds, benzoic acid, phenols, caprolactones, fatty acids, and no polyolefin-derived products.	w/o/with NaOH: Oil (7.7%/7.4%), Solid (75.1%/65.5%), Gas (11%/11%), Unreacted & aqueous-phase products (6.2%/16%)	2021	541
				Liquefacti	on with other supercr	ritical solvents			
HDPE, PP and HDPE/PP mix	450-470	corresp. to T	1	10%	Acetone	Aliphatic hydrocarbons	Oil yield: 88% (HDPE); 96% (PP); 90% (mix)	2021	524
PS	370	corresp. to T	1.5	7-10%	n-hexane	Styrene (primary); toluene and ethyl benzene (secondary)	90% conversion	2001	525
PS	340-420	corresp. to T	0.25-	-	Methanol	Styrene, toluene, ethylbenzene, dimer, and other 2-ringed aromatics.	92% conversion (380 °C/15 min)	2008	526
HDPE; HDPE + spirulina microalgae	340	corresp. to T	-	6-14%	Ethanol	Aliphatic hydrocarbons	7.55% (PE oil); ~50% (HDPE + spirulina)	2012	542
PS	350 (SC Ethanol); 370 (HTL)	corresp. to T	0.25- 1.25	25-400%	Ethanol; Water	Alkyls, alkenes, and aromatics (SC Ethanol)	Oil yield: 84.74% (SC Ethanol); 78.3% (HTL)	2020	543
HDPE + sugarcane bagasse mix	240-280	corresp. to T	1-1.5	5-10%	Ethanol	Aliphatic hydrocarbons	32.3% (bio-oil yield)	2020	544- 545

The liquefaction of plastics is highly sensitive to reaction temperature. Zmierczak et al. ⁵¹⁶ reported an increase in the distillable product yield from 71% at 350 °C to 93% at 450 °C during catalytic hydrogen liquefaction of PS. Increasing temperature also increased the formation of single-ring aromatics (i.e., benzene and alkylbenzenes) by further decomposing multi-ring products (e.g., diphenyl or triphenyl alkenes). ⁵¹⁶ However, increasing the temperature during catalytic liquefaction can also promote the cracking of liquid products to gases. Compared to catalytic liquefaction, reaction temperature seemed to have a greater effect on non-catalytic liquefaction. Feng et al. ⁵¹⁸ showed that the oil yield from mixed post-consumer plastics at 430 °C was only about 25% with no catalyst and 60-63 wt% with 1 wt% HZSM-5 or Al/Si as the catalyst. However, oil yields of over 90% were obtained at 460 °C both with and without catalysts. ⁵¹⁸ For all cases, gasoline and kerosine fractions increased with increasing temperature.

In general, increasing reaction time increased both conversion and secondary reactions. Shabtai et al.⁵¹⁹ reported that increasing reaction time during catalytic hydrogen liquefaction of HDPE at 450 °C improved the conversion from 82.5% to 100% but also reduced the oil yield from 92.8% to 60.2% due to increased cracking at prolonged reaction times. A similar trend was also observed with PP.⁵¹⁹ Increasing the reaction time also enabled the complete depolymerization of PS to single ring aromatics and promoted secondary cyclization of the primary monomers to form more naphthalene and indane as reported by Zmierczak et al.⁵¹⁶ While the effect of hydrogen pressure is usually less significant than reaction temperature or time, it can improve both conversion and oil quality.⁵¹⁸⁻⁵¹⁹ For example, Murty et al.⁵¹⁷ reported that the oil produced from LDPE at 440 °C using 800 psi hydrogen pressure was three times less viscous than the oil obtained using 100 psi hydrogen pressure because of the conversion from heavy oil to light oil at higher pressure. Increasing pressure also promoted single-ring aromatics and suppressed secondary cyclization during catalytic liquefaction of PS.⁵¹⁶

Feedstock heterogeneity is the most challenging problem in converting real-world plastic wastes. Williams and Slaney⁵²² evaluated the feedstock compositional variability under comparable liquefaction in this context. They conducted non-catalytic liquefaction of a mixture containing HDPE, PP, PET, and PVC. The product yields obtained from the mixture were then compared with the theoretical product yields calculated using those obtained when their constituent polymers were independently converted under the same condition. The oil yields produced from the mixed plastics were significantly lower than the calculated yields for nitrogen and hydrogen liquefaction. The effect of feedstock preparation methods showed that the PCW prepared in Belgium by Fost Plus via air blowing separation (obtaining a low density fraction of PCW) produced much higher oil yields and lower solid residues than the non-plastic removed PCW prepared by water washing (Waste DSD). 522 Plastic wastes from Waste Fost Plus were expected to contain a high fraction of low-density plastics (LDPE, PP, and PS) and a lower fraction of high-density plastics (HDPE, PVC, and PET). 522 Unfortunately, the authors investigated neither the product compositions nor the possible interactions among the compositions to elaborate on the crucial results. Contaminant content in mixed plastics also had a significant detrimental impact during hydrogen liquefaction. The catalytic effect was severely hindered during Shah et al.'s study when the dirtier PCW prepared by dry separation was converted.⁵²¹ The authors found no noticeable changes in either yields or boiling point distributions of the products before and after using 1 wt% of HZSM-5 or other catalysts. In contrast, adding identical amounts of catalysts to a cleaner PCW prepared by water washing significantly increased the gasoline fraction of the oil

products. 521 The dirtier PCW contained slightly more N and Cl elements than the cleaner PCW (0.67% vs. 0.65% for N, 1.26% vs. 0.03% for Cl), likely from PVC and polyurethane. 521 Thus, catalyst deactivation by the heteroatoms Cl and N can be considered among the reasons for the reduced catalyst performance.

6.1.2 Hydrothermal Liquefaction (HTL)

Water and other solvents behave differently beyond their critical points. Above the critical point, water exhibits two-phase behavior with characteristics of both liquids and gases. When the critical state temperature and pressure are reached (T=375 °C and P=22 MPa), the diffusivity, viscosity, and solubility parameters of water change, thereby inducing changes in its density, heat and mass transfer coefficients, and dielectric constant. Supercritical water (SCW), with its excellent heat transfer properties, can be leveraged to chemically recycle waste plastics by deconstructing the plastics into their constituent monomers or other value-added chemicals, as well as hydrocarbon fuels. This is made possible by the acid catalyst-like behavior exhibited by the SCW at high temperatures where an abundance of H*, H*, and OH* ions are produced. S15 HTL facilitates both ionic and free-radical reactions depending on the reaction conditions. S27, S37

Depending on their polymer structure, either monomers or fuel oil products are obtained during the HTL of plastics. Some step-growth polymers formed by condensation polymerization, such as PET, PC, polyamides, and polyurethane (PUR), have ether, ester, or acid amide linkages. 527, 534, 537-538 These functional groups can be hydrolyzed to rapidly depolymerize the plastics with high chemical selectivity and liquefaction efficiencies even under sub-critical conditions. 527, 537-538 There is pronounced support for hydrogen bonding and ion solvation due to the higher density of the sub-critical water medium. 527, 537 HTL of PUR mainly promotes monomer production. It was reported that the sub-critical liquefaction of PUR at only 250 °C for 30 min produced diaminotoluene (TDA) at 72% yield along with some other aromatics and polyols. 546 Passosa et al. 537 reported oligomers as the primary products when PUR was converted at 350 °C using fast heating rates and short residence times, suggesting partial depolymerization under such conditions. HTL of PUR produces NH₃. The solubilized NH₃ then acts as a base catalyst to promote PUR decomposition.⁵³⁷ As reported by Passosa et al.⁵³³ and Goto et al.⁵⁴³, polyamides (PA including PA6 and PA66) were hydrolyzed during HTL at temperatures above 300 °C to produce εaminocaproic acid, which further decomposed to form ε-caprolactam in nearly theoretical yield. When caprolactam was further hydrolyzed over extended reaction time, a range of water-soluble oxygenated platform chemicals were produced. 537, 547 Passosa et al. 537 showed that adding KOH catalyst to the HTL of PA could significantly increase oil yield and promote complete depolymerization in reduced residence times. The presence of the base catalyst also accelerated the production of oxygenated products soluble in water⁵⁴¹ and increased the selectivity of polyaromatics and oxygenated compounds derived from the plastics like PC and PURs. 537

HTL of non-polar plastics (Polyolefins and PS) usually requires supercritical or near supercritical conditions to be effective. According to Ciuffi et al.⁵⁴¹, compounds from PE, PP, and PS depolymerization were absent from the liquid products obtained for subcritical HTL of mixed plastic wastes. The lack of heteroatoms (i.e., polar reactive sites) in the polyolefins and PS prevents the plastics from depolymerizing under mild conditions.^{537, 541} As shown in Table 14, HTL of PS has been widely studied. Kwak et al.⁵⁴⁸ reported the complete and nearly instantaneous conversion of PS at 400 °C. Higher temperatures or prolonged reaction times at supercritical conditions will

further decompose liquefied products by promoting secondary reactions. Seshasayee et al. 527 reported a decrease in PS-derived oil yield from 86.2% at 350 °C to 38.3% at 450 °C after 30 minutes of treatment. HTP of PS usually produces styrene monomer, ethylbenzene, α -methylstyrene, styrene dimer, styrene trimer, and other dimer/trimer associated products. Toluene and ethylbenzene were the major liquid products under supercritical reaction conditions. Bai et al. 535 reported yields for toluene and ethylbenzene at 490 °C to reach 14% and 51.3%, respectively.

HTL of polyolefins was conducted under supercritical conditions to produce an oil similar to naphtha. Several articles have reported 85-90% oil yields from HDPE and LDPE in supercritical HTL. ^{513, 539-540} As given in Table 14, oil yields higher than 90% from HDPE were reported by Murty et al. ⁵¹⁹ and Su et al. ⁵²⁶ where HTL was performed in batch reactors. ^{523, 530} In comparison, the highest yield obtained using a continuous reactor system was 79% at 530 °C (Table 14). ⁵³² Supercritical HTL of polyolefins yields oils with a wide range of molecular weights. A narrower distributions can be obtained by increasing temperature and reaction time. ⁵³⁰ HTL of PE produces n-alkanes as the major products, followed by 1-alkenes and alkadienes. ^{513, 539}

Intramolecular β-scission and intermolecular hydrogen abstraction (H abstraction) are generally considered the primary mechanisms for polyolefins to degrade during HTL. When the PE backbone undergoes homolytic cleavage, the random scission produces free radicals with a random number of carbon atoms. These radical ends can be terminated by hydrogen abstraction from within the molecule (by β-scission) or from other molecules (by H abstraction).⁵⁴⁹ The ratio between 1-alkenes and n-alkanes in the product can indicate which reaction is prominent.⁵⁴⁹ During HTL, polymer fragments with radical ends immediately dissolve in SCW, where large amounts of excited H radicals are available. Thus, H abstraction becomes more prominent than βscission. 527 This is also why previous studies frequently report the 1-alkene-to-n-alkane ratio to be lower in HTL of PE than in thermal pyrolysis of PE. 523 At extended reaction times, n-alkanes can undergo isomerization, and alkenes can undergo secondary reactions like cyclization. 539 Gas production is also increased under these conditions due to increased cracking or recombination of short-chain free radicals. 539 Aromatization is suppressed under HTL, thus producing less char from plastics. 523 When HTL was conducted in a continuous or a semi-batch reactor system, the radicals were quickly removed from the reaction region. This led to a decreased opportunity for H abstraction, producing more alkenes than n-alkanes. 532,550 In addition to promoting chain cleavage, HTL can also oxidize the hydrocarbon products to form alcohols and ketones. Products such as 2propanol, 2-butanol, 2-propanone, and 2-butanone were found in the aqueous phase products obtained during HTP of polyolefins by Moriya et al.⁵²³

As shown in Table 14, oil yields up to 91% from supercritical HTL of PP were reported using reaction temperatures up to 450 °C. The oil fraction consisted of olefins, paraffins, and cyclic and aromatic compounds, with 80-90% of these compounds in the naphtha range. The authors also reported that the PP-derived oil is comparable to gasoline in terms of their H/C and O/C ratios, boiling point range, carbon numbers, density, viscosity, and surface tension. Similar product composition from HTL of PP was also reported by others, proposing an opportunity for PP-derived oil to be directly used as fuel feedstocks and blendstocks without further upgrading. Zhao et al. studied co-conversion of LLDPE and PP by HTL at 400 °C and reported the oil yield from the plastic mixture to be higher than the yield produced by converting LLDPE or PP alone, as shown in Table 14. In this study, PE produced more heavy oil than medium or light oils whereas PP produced equal amounts of naphtha (light oil), medium, and heavy oils. In comparison,

the mixtures of PP and PE produced more heavy oil than naphtha or light oil. HTL co-conversion also increased the formation of cyclic compounds while reducing paraffin production.⁵⁴⁰ Thus, relatively lower quality oil was obtained by co-conversion, although the oil yield synergistically increased.

Subcritical HTL of PVC was also investigated because hydrochloric acid, produced from the PVC, is water soluble. PVC was dechlorinated in subcritical water at 200 °C in Takeshita et al.'s work to yield polyenes as solid residue without producing any hazardous organochlorine compounds. When the reaction temperature increased to 250-350 °C, a mixture of low-molecular-weight aromatic and aliphatic compounds was produced. As the temperature further increased to 400 °C, the increased production of light alkanes and alkenes was also accompanied by the formation of the aliphatic ketones and oxygenated benzene compounds at higher yields. Inside the highly acidic solution created by the PVC-derived HCl, the PVC-derived polyene can undergo cyclization, hydrolysis, oxidation, and thermal degradation. As shown in Table 14, base catalysts, such as NaOH or KOH, were added during HTL of PVC to study their effect on dechlorination. Passosa et al. Showed that although adding KOH did not affect the oil and solid yields produced from PVC at 350 °C, it caused more chlorine to leave as Cl₂ gas rather than remaining in the solution as HCl.

Increasing temperature and treatment time during HTL often facilitated conversion to increase liquid and gas yields. 513, 523, 530, 538-539 However, it has been noted that high reaction temperatures and a prolonged residence time can reduce the desired product yield and increase coke formation due to over-cracking of the liquefied products. 529, 531, 535 The feedstock-to-solvent mass ratio also affected the HTL process. Increasing the feedstock mass loading caused the liquefaction reaction rate to increase first and then decrease. Increasing the solid mass loading to beyond the corresponding optimum led to increased heat transfer limitations and decreased mobility of the macromolecular free-radical fragments in the solution. 538 Such limitations favored undesired secondary reactions like repolymerization. Jin⁵³⁸ et al. also reported that increasing temperature and mass ratio would eventually result in decreased liquefaction efficiency for the same reaction time. When high mass ratios were employed at higher reaction temperatures, increased reaction rate and higher H⁺/H[•] concentration in the solution caused the monomers and oligomers of the liquified products to undergo further cracking to form gaseous products.⁵³⁸ The effect of pressure during HTL of plastics is generally considered less significant than reaction temperature and time, especially for continuous and semi-batch reactor systems. 532 Although the pressure effect was only observed in some studies, an increase in pressure increased the ion products of the water due to increased density, subsequently bolstering the cracking and hydrolysis process. 535 An increase in pressure also enables enhanced interaction among different reaction species, promoting cyclization, hydrolysis, oxidation, and thermal degradation all at the same time.⁵³¹ Depending on plastic types and the availability of reactive sites, any of these reactions may take precedence.

6.1.3 Liquefaction with Other Organic Solvents

Liquefaction of plastics in supercritical hydrocarbons and alcohol solvents has also been studied, as shown in Table 14. In general, the solvents were used to enhance product dissolution, increase reaction rates, and stabilize products. However, in these cases, the solvent is a co-reactant and the conversion of the solvent must be considered. Hwang et al.⁵²⁵ reported that at least 90% of

PS was converted in n-hexane at 370 °C, while there was almost no conversion when PS was pyrolyzed at the same temperature.

Ethanol achieves its critical states at relatively milder operating conditions, and its low dielectric constant increases the solubility of both polar and non-polar products. Furthermore, ethanol can also act as a hydrogen-donor solvent to stabilize the intermediate products and reduce repolymerization reactions. Breaking alcohol solvent at the critical state produces excessive hydrogen and hydroxyl ions, aiding the hydrogenation reactions. Ahmad et al. reported that the oil yield produced from PS conversion in ethanol at 350 °C was 84.74%, higher than 71% from pyrolysis at 500 °C, and 78.3% obtained using HTL at 370 °C.⁵⁴³ Rather than producing styrene as the primary monomer, the liquid produced using ethanol solvent consisted of alkyls, alkenes, and aromatics.⁵⁴³ Compared to PS, less liquid was produced when PE was converted in ethanol. According to Pei et al., the oil yield of HDPE in 340 °C ethanol was only 7.55%.⁵⁴² However, coliquefying PE with microalgae or lignocellulosic biomass in ethanol was found to synergistically increase the liquid yield because the oxygenated feedstock enhanced the thermal decomposition of PE in the solvent probably by hydrogen abstraction from PE by the oxygenated biopolymers.⁵⁴⁴⁻⁵⁴⁵

Methanol is also a hydrogen donor solvent with low critical conditions. Shin and Bae reported 92% conversion for PS by treating with 380 °C methanol for 15 min. ⁵²⁶ Their comparative study showed that the activation energy for degrading PS in supercritical methanol was 117.2 kJ/mol, lower than 132 kJ/mol in supercritical n-hexane, 157 kJ/mol with supercritical water, and 224 kJ/mol in pyrolysis. The authors reported the hydrogenation of unsaturated products to be the predominant reaction in methanol. Besides donating hydrogen, methanol also directly reacted with styrene monomer and α -methylstyrene to produce 3-phenyl propanol and 3-phenyl-1-butanol. ⁵²⁶

6.2 Reactor Designs

Lab-scale liquefaction studies have predominantly been carried out in batch reactors with few accounts of continuous reactor systems. Industrial-scale processes have incorporated both batch and continuous reactor designs. Stirred or agitated tank reactors are the most employed batch reactor designs at both lab and industry-scale. The different continuous reactor designs adopted for industrial-scale processes are continuous flow stirred tank, rotary kiln, fixed bed, and tubular reactors, with gravity or auger/extruder-based material feeding mechanisms⁵⁵¹⁻⁵⁵² Figure 23 shows an example of an industrial-scale continuous flow reactor design.

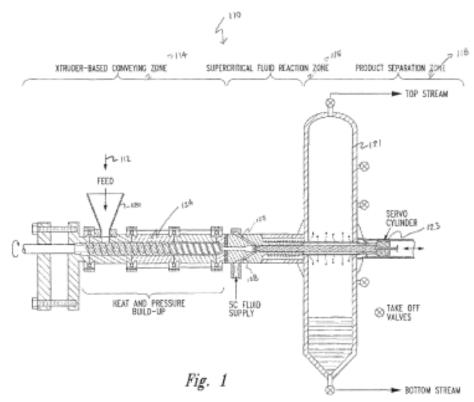


Figure 23. Example of a continuous tubular reactor design for hydrothermal liquefaction of plastics (Extracted from the US patent US 8,980,143 B2).⁵⁵³

6.3 Commercial Activities in Plastics Liquefaction

6.3.1 Hydrogenation Plants in Germany

The Vega process was initially developed to convert coal into naphtha and gas oil. This process was pioneered by Vega Oel GmbH of Germany and then later adopted to depolymerize waste plastics into syncrude, hydrogenated solid residue, and HCl if a dechlorination step was involved. Later, in 1999, the technology was discontinued due to the higher cost involved than in more economical feedstock recycling processes and mechanical recycling. Several other multi-stage upgrading and direct hydrogenation liquefaction projects of waste plastics were also established by German companies like RWE-Entsorgungs AG, Hiedrierwerke Zeitz GmbH and Bergakademie Freiberg, but later terminated.

6.3.2 Liquefaction Plants in Japan

The growth of feedstock recycling in Japan was spurred by the Plastic Containers and Packaging Recycling Law passed in 2000. This law promoted sorting at collection and recycling of plastic waste containers. Less of the waste plastic bale materials were made available to liquefaction plants and at a higher tender price when compared to other feedstock recycling. Due to this, liquefaction had a lower combined plant capacity than other feedstock recycling approaches. The Niigata liquefaction plant was established with a capacity of 6 kton/yr with support from the Plastic Waste Management Institute (PWMI) and the city of Niigata. The plant operated by Rekisei Koyu started commercial operation in April 1998 and demonstrated that unsegregated and contaminated household waste plastics could be converted to oil. Mixed

plastic bales comprising PE, PP, PS, PET, and PVC were allocated from the city of Niigata. The PWMI designed, and TOSHIBA-built plant has a pretreatment stage to remove PET and other contaminants followed by a dechlorination stage. The liquefaction process occurs at 420 °C in a stirred tank reactor where 65% of the oil produced was utilized as process fuel within the plant. ^{552, 555} Details for this process can be found in the 2019 PWMI annual report. ⁵⁵⁶

The Sapporo Plastic Recycle Co. Ltd (SPR) was established in 2000 with the support of PWMI and Sapporo city with an initial capacity of 13.5 kton/yr which later grew into 14.5 kton/yr.⁵⁵² The SPR plant treated mixed plastics at three stages. The first stage involved pretreatment, sorting and pelletizing, followed by dechlorination, which fed calcium hydroxide into the system. The third and final stage involved thermally decomposing the waste plastics in a rotary kiln reactor at 400 °C and 5 kPa overpressure to produce light, medium, and heavy fractions of oils. 552, 555 Approximately 65% of the total oil produced was utilized as a process fuel within the plant. 552 Due to the tender system governed by the Japan Container and Package Recycling Association (JCPRA), only half of the baled plastics were used in the SPR liquefaction plant. Additionally, the small operation scale of the SPR plant also raised the cost of waste plastics recycling.⁵⁵² In Mikasa city, another large scale (6 kton/yr. capacity) liquefaction plant started operation in 2000 but was shut down in early 2004 due to a lack of waste plastic feedstock to process. 555 By 2010, all major liquefaction plants in Japan ceased, with the advanced SPR plant being the last of them. A 2019 PWMI report suggested that the need for the crude oil product to be further cracked and refined meant that the process was not commercially viable at that time. 556 Furthermore, these facilities are prone to fire accidents due to the risk of an explosion associated with the liquefaction reactors. Since the 2000s, liquefaction research and development have improved direct liquefaction methods to convert waste feedstocks to naphtha and diesel and thus reduced the burden for further refining. Nevertheless, the issues related to the scale of the plants and businesses remain, and any new companies adopting this technology will face difficulties. 556

6.3.3 Plants with Hydrothermal Liquefaction

Licella Holdings, Australia, has carried out HTL research over the past two decades and has established the Cat-HTR technology. 557 The first-ever continuous-flow Cat-HTR liquefaction facility, with a capacity of 20 kton/yer, was established by Licella Holdings in Australia in 2007, now operated by iQRenew. 557 Cat-HTR technology is being commercialized internationally via MURA Technology Ltd., Licella's global joint-venture with Armstrong Energy based in the UK. 557 MURA technology has proposed a process called Hydro-PRS adopting the Cat-HTR technology. 558 In 2021, Renew-ELP, based in the UK, started construction of a similar plant in England after obtaining a license for the Hydro-PRS process from Mura Technology. 558 The companies claim that mixed plastic waste with a limited PVC content can be treated using this process. The Cat-HTR/Hydro-PRS process involved treating waste plastics or other carbonaceous feedstock at sub-critical or supercritical water to produce naphtha, distillate gas oil, heavy gas oil, and heavy wax residue. 558-559 Decontaminated waste plastic mixture is added to the hopper with an extruder (1), and the melted plastics exiting the hopper were pressurized (2). These molten plastics and SCW were mixed in a chamber (3) before the slurry was fed into the Cat-HTR reactors (4). Note that the Cat-HTR reactors are heated by both heat carrier (hot water in the chamber) and an external heat exchanger. Here, the waste plastics are treated for 20 – 25 min at 350-420 °C and above 220 bar to produce over 85% liquid. The post-conversion contents are depressurized (5) before feeding into the flash distillation chamber, where the products are separated (6). The condensable products are then stored (7), and the gases are used as process fuel. ⁵⁵⁷⁻⁵⁵⁹ The used water after the product separation was recycled in the same system. This process operated at a waste concentration of about 70%. ^{557, 560}

Another company called Aduro Clean Technologies from Canada has also developed an HTL-based commercial process. They call their process Hydrochemolytic Plastic Upcycling where the reactor operates at only 240-390 °C and takes about 25 min to completely convert the plastic mixtures. S61-562 According to their claim, their water-based process operates under less severe conditions and allows the manipulation of chemical reactions associated with different types of plastics to form a comprehensive approach for chemical conversion of plastics. S62

7.0 Gasification of Waste Plastics

7.1 Fundamentals of Gasification Reactions

Gasification (or partial oxidation) of MSW converts solid waste into synthesis gas or producer gas (CO, H₂, CH₄) by the reaction shown in Eq.4, where CH_qO_r represents the feedstock; q and r are the hydrogen and oxygen to carbon ratios, respectively; m and b are the input air and steam to MSW ratios; x_i is the mole number of molecular species i. Froducer gas (CO, H₂, N₂) is produced when air is used for the gasification while synthesis gas (CO, H₂) is produced when oxygen is used for gasification. Synthesis gas can be further processed to produce a range of chemicals and fuels. MSW and mixed plastic waste can be used as the feed for gasification. MSW gasification could be more profitable and environmentally sustainable than incineration. Soft-Soft A comparative study estimates that the global warming impacts of waste gasification with a combined cycle powerplant are over 50% lower than incineration.

$$CH_qO_r + m(O_2 + 3.76N_2) + bH_2O \rightarrow x_{H_2}H_2 + x_{CO}CO + x_{CO_2}CO_2 + x_{CH_4}CH_4 + x_{N_2}N_2 + x_{H_2O}H_2O$$
 Eq. 4

Gasification of MSW occurs above 550 °C.⁵⁶⁸ The main MSW gasification products are gases including CO, H₂, CO₂, and CH₄. Solid residues (i.e., ash) are also produced. The amount of ash depends on the equivalence ratio (i.e., the ratio of oxygen in the employed oxidant and the oxygen required for complete combustion). Ash can be minimized by applying equivalence ratios between 0.25 and 0.35. Accordingly, equivalence ratios within this range are usually used in commercial reactors. Chemical thermodynamics can be used to predict the gas phase products during gasification.⁵⁶⁹⁻⁵⁷⁰

As shown in Table 15, at lower gasification temperatures (i.e., around 600 °C) there is a significant amount of CO₂⁵⁷¹ formed from the highly exothermic CO oxidation (Eq. 5), the oxidation of carbon (Eq. 6) and the water–gas shift reaction (Eq. 7). These reactions are thermodynamically unfavorable at higher gasification temperatures (> 700 °C) leading to a decrease in the amount of CO₂ produced.^{570, 572} Conversely, more CO is formed at these higher temperatures by the steam reforming of CH₄ (Eq. 8), steam reforming of hydrocarbons, the steam gasification of char (Eq. 9) and the dry reforming of hydrocarbons (Eq. 11) all which are highly endothermic reactions. The Boudouard reaction (Eq. 10) is yet another highly endothermic reaction that yields CO.⁵⁷³ Material and operational constraints such as tar condensation and accumulation⁵⁷⁴ often require maintaining gas temperatures above 700 °C.

Table 15. Fundamental reactions that take place during the gasification of MSV	V along with the
heat of reaction at standard conditions.	

Reaction	ΔH (kJ/mol)	Name	Eq.
$CO + \frac{1}{2}O_2 \rightarrow CO_2$	-283.7 kJ/mol	CO oxidation	5
$C + O_2 \rightarrow CO_2$	-394.1 kJ/mol	Carbon partial oxidation	6
$CO + H_2O \leftrightarrow CO_2 + H_2$	-41.0 kJ/mol	Water-gas shift	7
$+ CH_4 H_2O \leftrightarrow CO + 3H_2$	+206.0 kJ/mol	Methane steam reforming	8
$C + H_2O \leftrightarrow CO + H_2$	+131.0 kJ/mol	Steam gasification of char	9
$C + CO_2 \leftrightarrow 2CO$	+172.0 kJ/mol	Boudouard reaction	10
$C_XH_Y + XCO_2 \leftrightarrow 2XCO + Y/2 H_2$	Endothermic	Dry reforming	11

7.2 Waste Plastic Gasification Process Flow Diagram

Figure 24 shows a general flow diagram for waste plastic gasification processes. The feedstock is fed into a gasifier where gasification takes place. The volatiles enter a combination of physical, thermal, or chemical gas cleaning technologies where char, slags, and ash are removed. The clean syngas is then cooled in a quench unit to the temperature required for a secondary gas cleaning step. The secondary gas cleaning step removes contaminants that can impact catalyst performance, such as sulfur, halides, HCN, NH₃, and tar, to levels of less than 0.1 parts per million by volume.⁵⁷⁵ The cleaned syngas can either go to a turbine for power generation or for catalytic upgrading to other products. Synthetic gas consisting mostly of CO and H₂ is the feedstock for many catalytic synthesis systems.⁵⁷⁶⁻⁵⁷⁷ The synthetic gas mixture can be catalytically converted to methanol and other alcohols. Platform chemicals such as ethylene, propylene, and other alkenes can be produced via the methanol-to-olefins process.⁵⁷⁸

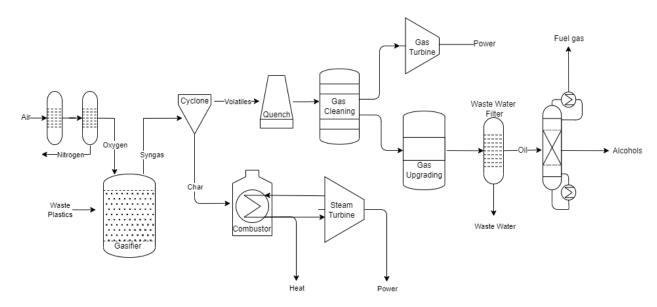


Figure 24. Gasification of waste plastics and upgrading to heat, power, olefins, alcohols, and other fuels.

The design and configuration of waste plastic gasification facilities depend on the facility scale and targeted products. Some gasification facilities combust the synthetic gas and solid by-product streams to produce combinations of heat and power. Other gasification facilities include steam generation, catalytic upgrading, and other product recovery units to improve energy efficiency and target higher-value markets.

7.3 Commercial Activities Scale

According to the Energy Information Administration (EIA), global waste gasification capacity is estimated to be less than 10,000 Megawatts thermal (MWth) compared to more than 200,000 MWth of coal gasification capacity. Despite the low total capacity, the number of global waste gasifiers in operation is estimated to be about 100 facilities which is similar to the number of biomass and natural gas gasifiers. These gasifiers primarily produce electricity and heat.

One of the leaders in gasification of MSW is Enerkem who is currently planning to build four commercial MSW recovery facilities. Enerkem's facility, in Québec, Canada, cost \$680 million and will convert 200 kton/yr of MSW and forest residues to 125 million liters of biofuels and chemicals starting in approximately 2023. In Alberta, Canada Enerkem recently commissioned \$50 million waste-to-biofuel facility with a capacity of 38 million liters per year. ⁵⁸⁰ In partnership with Shell and the Port of Rotterdam, Enerkem plans to convert about 360 kton/yr of MSW to 80 kton of renewable products including aviation fuels. Finally, Enerkem, Agbar, and Repsol plan to build a facilty processing 400 kton/yr to 220 million liters per year of fuels in Tarragona, Spain pending final investment decisions. ⁵⁸¹

7.4 Techno-Economic Analysis

The profitability of waste plastic gasification facilities depends on several process factors and market drivers. Feedstock composition, process yields, and energy efficiency are key drivers for process performance. Feedstock tipping fees, capital costs, and market prices have a significant impact on profitability. Several studies show that waste plastic gasification is more profitable than conventional waste management practices such as incineration and landfilling. 58, 582-583

There are numerous techno-economic analysis studies on MSW gasification, but only a small subset focuses on waste plastic upgrading. For this review, we identified three comparative analyses that investigate the costs of waste plastic gasification as a primary strategy. Table 16 shows a summary of the key assumptions and findings from these studies.

Table 16. Summary of techno-economic analysis estimates for waste plastic gasification

Technology	Feedstock	Major Products	Region	Feed Capacity (kton/yr)	Capital Cost (\$MM USD)	IRR (%)	Ref
Chemical Recycling + Gasification + Catalytic upgrading	MSW	Propylene, Ethylene, LPG, others	Germany	76	158.2 - 271.2	Not reported	582
Bubbling Fluidized Bed Gasifier	Package Derived Fuel	Syngas, Electricity	Italy	4	0.00549 - 0.00841/kWe	0.5-29.8	583
Gasification to Hydrocarbons	Waste Polypropylene	Propylene, Ethylene, Aromatics	United States	100	49.09 (annualized)	16.91	58

Voss et al. compared the economic performance of chemical recycling and gasification to incineration as municipal waste treatment options in Germany. 582 In their study, they assumed that their feedstock consists of "not differentiable mixed municipal waste" and "household waste, household-type commercial waste" as defined by the European Waste Classification Syste. 584 Their MSW stream contains 6.9 wt.% plastics. Most of Germany's waste streams are incinerated directly via combustion to produce heat and power or indirectly via anaerobic digestion of the organic fraction and the refuse-derived fuel (RDF) combustion. The chemical recycling scenario assumes that 1 tonne of MSW is initially mechanically separated into the organic fraction (750 kg) and RDF (250 kg). The organic fraction undergoes anaerobic digestion followed by a biogaspowered combined heat and power system. The RDF fraction is gasified to produce syngas, and the syngas is catalytically upgraded to methanol and subsequently to olefins using sodium hydroxide as the catalyst. Hydrocarbons including propylene (32 kg), ethylene (30 kg), butadiene (4.2 kg), LPG (4.0 kg), and butane (1.9 kg) are recovered in the recovery stage. The chemical recycling unit has a capital cost of 176.6 million USD for a 76 kton/yr facility. Under the basic scenario, this technology is not profitable. It yields a net present value of -180.8 million USD versus 8927 million USD for direct incineration. A combination of increasing the plant scale, environmental regulations, and favorable market conditions increases the net present value to 497.2 million USD.

Gregorio and Zaccariello investigated the economic performance of gasifying packaging-derived fuel (PDF) to produce power, heat and power, and district heating in Italy. PDF is a mixture of primarily plastic-derived materials. Their samples contained 53.9 wt. % carbon, 7.7 wt. % hydrogen, and 26.0 wt. % oxygen. The material contains 0.1 wt. % sulfur and 0.3 wt. % chlorine, among other contaminants. The nominal capacity (4 kton/year) for the plant was 500 kilowatt-electric (kWe). Total plant costs ranged from \$5.5 k (USD) for the power system to \$8.4 k t for the district heating scenario. The revenue generated from the three scenarios analyzed includes a tariff of \$0.07/kWe delivered to the grid and \$0.09/kWht for the sale of saturated or superheated steam production in the combined heat and power plant. Based on the revenues, the internal rate of return was estimated at 0.5% for power generation, 18.9% for district heating, and 29.8% for combined heat and power generation. 583

Bora, Wang, and You compared plastic gasification to other recycling strategies. In their study, the gasifier processes plastic waste containing 84.5 wt. % carbon, 13 wt. % hydrogen, and 2.5 wt.% oxygen. The gasification facility has a plant capacity of 100 kton/year, and an annualized capital cost of \$49.1 million. They estimated a 16.91% internal rate of return from the sale of synthetic gases. 58

8.0 Dissolution-Based Approaches for Plastics Recycling

Dissolution-based approaches are methods to use solvents to separate and recycle plastics without chemically modifying their structures. The basic workflow of a dissolution-based polymer recycling process can be described as follows: first, the target polymer is selectively dissolved in a suitable solvent or solvent mixture at a defined temperature; second, the mixture is filtered to separate the solid plastic and the liquid phase that contains the solvated polymer; last, the polymer precipitates from the solution by adding an antisolvent (*i.e.*, a solvent in which the polymer is

insoluble) and/or decreasing the temperature. Dissolution-based polymer recycling has several advantages over chemical or mechanical recycling methods: it produces high-quality polymers by removing impurities and additives, it can deal with multicomponent plastic mixtures by selectively dissolving a single target polymer; it does not require a high-purity input stream, and it is typically more environmentally friendly than chemical recycling. 585-587

8.1 Thermodynamics of Selective Dissolution and Solvent Screening

The key to a dissolution-based polymer recycling process is the selection of appropriate solvents. In a selective dissolution process, the solvent should dissolve the target polymer with a sufficient solubility without dissolving other unwanted components of the input stream. Since each polymer presents unique interactions that dictate solubility, and the composition of plastic waste is often complicated, theoretical approaches are valuable for systematically identifying suitable solvents. The thermodynamics of polymer-solvent mixing is governed by the free energy of mixing (Eq.12), 588 where ΔG_{mix} is the molar Gibbs free energy of mixing, ΔH_{mix} is the molar enthalpy of mixing, T is temperature, and ΔS_{mix} is the molar entropy of mixing. A polymer will favorably mix with a solvent if ΔG_{mix} is negative.

$$\Delta G_{\text{mix}} = \Delta H_{\text{mix}} - T \Delta S_{\text{mix}}$$
 Eq.12

Key contributions to the Gibbs free energy of mixing can be understood using Flory-Huggins theory, a mean-field model for polymer solutions (Eq.13),⁵⁸⁹ where k_B is the Boltzmann constant, ϕ is the volume fraction of the polymer, N is the degree of polymerization, and χ is the Flory interaction parameter that characterizes interactions in the mixture.

$$\Delta G_{\text{mix}} = k_B T \left[\frac{\phi}{N} \ln \phi + (1 - \phi) \ln(1 - \phi) + \chi \phi (1 - \phi) \right]$$
 Eq.13

The χ parameter is the critical parameter that governs how favorable a solvent system is for a selected polymer; smaller values promote mixing. The χ parameter can be estimated by Eq.14, where v_0 is the molar volume of a monomer and δ_i is the Hildebrand solubility parameter of compound i, which is defined as the square root of the cohesive energy density. A polymer is expected to interact more favorably – and exhibit a higher solubility – in a solvent with a similar solubility parameter, reflecting the general axiom of "like dissolves like." This conceptual framework thus highlights polymer- and solvent-specific solubility parameters as critical to the design of dissolution-based processes.

$$\chi = \frac{v_0}{k_B T} \left(\delta_{\text{polymer}} - \delta_{\text{solvent}} \right)^2$$
 Eq.14

8.2 Origin of Polymer Dissolution and Precipitation Processes

The simplicity and relevancy of dissolution/precipitation for the separation and purification of polymeric materials has been demonstrated experimentally and disclosed in patents since the 1930s. For example, the dissolution and purification of condensation products, mainly polyesters, in ethyl alcohol was disclosed in a 1936 patent by Sändig. ⁵⁹⁰ In 1949, Young and Sparks of the

Standard Oil Development Company patented a method to purify polyesters via the solvent-mediated separation of high-molecular weight compounds using paraffinic mineral oils.⁵⁹¹ These approaches showed the feasibility of using solvents to dissolve and purify polymerization products, giving way to the idea that this could be used to separate dissimilar polymers. In the 1970s, Seymour and Stahl demonstrated the separation of PE, PVC, PS, polyvinyl acetate (PVAC), and polymethyl methacrylate (PMMA) using a series of solvents that included toluene, methanol, and petroleum ether.⁵⁹² Around the same time, companies like Dupont filed patents for the recovery of solid scrap thermoplastic polymers like PET, pol(hexamethylene adipamide), poly(acrylonitrile), and poly(oxymethylene) by dissolving them in hexafluoroisopropanol.⁵⁹³ In 1977, Monsanto patented a process for recovering solid PET, poly(cyclohexanedimethanol terephthalate), and poly(butylene terephthalate) from fibers using naphthalene as a selective solvent and dimethylformamide (DMF), water, and acetone as quenching mediums (antisolvent).⁵⁹⁴

8.3 Applications of Dissolution-Based Plastic Recycling

Building upon these early materials recovery and purification processes, applications of dissolution and precipitation to plastic recycling has gained interest along the years. Nauman et al. proposed an approach to separate plastics in physically comingled solid mixtures by selective dissolution. Single solvents were used to dissolve plastics like PS, PVC, LDPE, HDPE, and PP, at different temperatures and pressures 595-596. The process consisted of shredding the comingled solids, dissolution of the plastic, filtration, flash devolatization, and pelletization of the separated plastic. Model experiments of plastic recycling with the dissolution/precipitation method were performed by Kampouris, Papaspyrides, and collaborators to recover PVC, LDPE, PP and PS. 597-601 In one study, Pappa et al. designed a pilot unit for the separation of LDPE/PP mixtures using the dissolution/precipitation method with xylene and 1-propanol as solvent and antisolvent, respectively. They claimed that the costs of the plastics produced from the process were comparable to those of the virgin plastics. 602 Regarding the impact of solvent treatment to the plastic properties, early recycling experiments with LDPE, HPDE, PET and PP showed that applying these processes once or twice did not affect the rheological, thermal, or mechanical properties of the final plastic. 586, 597, 601, 603 Many of these reports established solvent/antisolvent systems for common plastics, including solvent combinations, as summarized in Table 17.

Recent and ongoing research efforts have developed dissolution/precipitation methods for increasingly complex sources of plastic waste. Researchers at the Illinois Sustainable Technology Center have developed a nontoxic energy-efficient chemical solvent process to recover plastics from blends of electronic waste that are converted to fuel oil by pyrolysis. The process has been demonstrated at the lab scale and can produce plastics with properties similar to virgin resins and will begin a pilot-scale project depending on the performance of the recovered plastics. 604-606 Recently, Georgiopoulou et al. 607 demonstrated a process to recycle Tetra Pak® packaging materials composed of LDPE, paperboard, and aluminum. Their approach included a hydropulping process to recycle the paper component and a dissolution/precipitation process to recover LDPE, using xylene and i-propanol as the solvent/antisolvent pair. Researchers at the Center for the Chemical Upcycling of Waste Plastics at the University of Wisconsin-Madison have developed a solvent-based method called Solvent-Targeted Recovery and Precipitation (STRAP) that has been demonstrated for the recycling of different post-industrial multilayer films composed of PE, EVOH, PET and EVA. 608-609 STRAP combines experiments, computational modeling, and process

design tools to develop solvent systems to recycle multilayer plastics via selective dissolution. A technoeconomic analysis showed that STRAP can produce plastics at costs similar to virgin resins and can be more economically feasible when the use of antisolvents is reduced by instead inducing precipitation via temperature. 608

Table 17. Solvents/antisolvents used experimentally for the dissolution/precipitation of common plastics.

Polymer	Solvent	Antisolvent	Ref.
PVC	Cyclohexanone	n-hexane	600
PVC	Dichloromethane	Methanol	610
PVC	Toluene	Methanol	610
PVC	Tetrahydrofuran (THD), xylene	-	595
PS	Methyl ethyl ketone (MEK)	Methanol, n-hexane	598
PS	p-xylene	n-pentane	598
PS	Benzene, toluene	water	599
PS	Toluene	n-hexane	610
PS	Xylene	Methanol	610
PS	THF, toluene, xylene	-	595
PS	p-cymene		611
EPS	D-limonene	-	610
HDPE	Xylene	n-hexane, methanol	610
HDPE	THF, toluene, xylene	-	595
HDPE, LDPE, PP	Turpentine	n-hexane, petroleum ether (PetE)	612-
	•		613
HDPE, LDPE, PP	Turpentine/PetE	n-hexane, PetE	612-
			613
HDPE, LDPE, PP	Turpentine/benzene	n-hexane, PetE	612-
			613
LDPE	Xylene	n-hexane	610
LDPE	THF, toluene, xylene	-	595
PE, PP, PS	n-butane, propane	-	614
PP	Xylene	n-hexane	610
PP	Tetrachloroethylene	-	615
PP	THF, toluene, xylene	-	595
PET	THF	-	595
PET	γ-valerolactone (GVL)	-	616
PET	N-methyl-2-pyrrolidone (NMP)	n-octane, n-hexane	603
PET	diphenyl, diphenyl ether,	-	617
	naphthalene, methylnaphthalene,		
	benzophenone, diphenylmethane		
PET	Benzyl alcohol	Methanol	610
PC	Dichloromethane	Acetone	618
PA 6	Dimethyl sulfoxide (DMSO)	MEK	619
PA 6,6	Formic acid	MEK	619

Other than targeting specific plastic components in plastic waste, solvents can also be used to extract additives from plastics or to selectively dissolve or decompose adhesives in plastic structures to trigger delamination. While these topics are out of the scope of this discussion, they have been discussed at length in recent publications. 620-623

8.4 Industrial Demonstrations of Dissolution/Precipitation Processes

A handful of technologies are being commercialized for the recycling of different plastic waste feeds via dissolution methods. Here, we focus primarily on technologies that are currently in the process of commercialization. We omit discussion of past efforts; for example, the Solvay VinyLoop process was developed to separate PVC from a polymer coating using a selective dissolution step in a proprietary solvent, 624 but the process ceased operations in 2018.

APK AG's NewCycling process is being demonstrated in a 8,000 ton/year plant in Germany to produce polyamides (PA) and PE from PIW multilayer plastics. Their technology is based on dissolving a plastic using a solvent mixture from a group of alkanes, isooctane or cycloalkanes The plastics are recovered from solution and then pelletized by extrusion. Cest-626 Centrifuges separate the solids from the plastic solution and solvent APK AG claims that PP, PET, PS, polylactic acid (PLA) and aluminum could also be recovered with this process in the future.

The Fraunhofer Institute is developing a solvent-based process called CreaSolv that produces plastics with comparable properties to virgin materials, effectively removing contaminants and additives. The process is likely based on the dissolution of a target plastic, mainly polyolefins, using a solvent with a Hansen parameter δ_H between 0.0 to 3.0 MPa^{1/2}, selected from a group of aliphatic hydrocarbons. An antisolvent made out of mono/polyhydroxy hydrocarbons, like 1-propanol or 1,3-propanediol, with a δ_H between 4.0 and 38.0 MPa^{1/2} is then used to precipitate the polyolefin from the mixture. The institute has also studied the separation of PS⁶³² and are researching the recycling of multilayer food packaging that can consist of PET, PE, PP, EVOH, PA and metalized layers. Currently, Unilever is implementing the CreaSolv process in a 1,100 ton/year demonstration plant in Indonesia to recover PE from multilayer sachets. CreaSolv is also reported to have a demonstration plant in Holland to separate EPS from POP, a pilot plant for recycling packaging and automotive compounds, and a demonstration plant in Germany for multilayer films.

PureCycle Technologies is building a 54,000 ton/year facility that uses solvents to produce PP from PIW and PCW in collaboration with P&G. 637-638 The method consists of contacting the plastic waste with an alkane at elevated temperatures and pressures to obtain the purified PP. 639 The process removes impurities, undesired colors and odors and produces PP with comparable properties to the virgin resin. 638 P&G has recently filed patents with methods to separate and purify adhesives, PP, PE, PET, cellulose, and polyacrylic acid (PAA). 640 The company also has inventions in the purification of PE using a pressurized solvent consisting of hydrocarbons, primarily n-butane or pentane. 641 Additionally, they have a process for the separation of PS, PP, PE and poly(dimethylsiloxane) under similar conditions. 614

Polystyvert developed a dissolution process to recycle different types of PS, including expanded PS, extruded PS and high-impact PS. Polystyvert operates at 125 kg/hour with an output of 600 metric tons per year. 604 In their technology p-cymene is used as a selective solvent for PS and a non-polar solvent is used as an antisolvent to precipitate the plastic and remove p-cymene. 611

Through this approach they can separate and recover PS from other materials, as only PS dissolves in the solvent and other materials float or sink in the system.⁶⁴²

Dissolution-based recycling processes have also been applied to textile waste. For example, Worn Again Technologies has patented a technology to recycle PET into pellets. In their process, the polyesters are dissolved in a solvent system with either benzyl acetate, benzyl benzoate, benzaldehyde, or similar solvents, precipitated by cooling of the solvent system, and then separated via filtration. After the plastic is separated, it is washed and dried and then molded into pellets and/or converted into fibers. This process can be applied to cotton textiles, post-consumer PET bottles, and plastic packaging containing PET. Worn Again has also partnered with companies such as H&M and Kering to promote the reduction of textile waste. Another start-up company, Ambercycle, has developed a technology to purify and separate polyesters from different garments and is planning a demonstration plant to produce a metric ton of recycled material per day. 645-646

Other approaches are being used to recycle multilayer plastics using a combination of mechanical and solvent-mediated steps. For example, Saperatec has introduced a low-energy mechanical recycling process that involves shredding the multilayer film followed by use of surfactant-containing microemulsions to break up and separate the layers.⁶⁴⁷ The technology separates PE and aluminum film, PP from aluminum, and PE from PP. The technology was originally developed for rigid packaging and is being extended to flexible packaging and will be demonstrated at a 17,000 ton per year facility in Germany.⁶⁴⁸

8.5 Advanced Solvent Selection for Complicated Feedstocks

As presented above, several solvents and antisolvents have already been identified for many common plastics, enabling the development of dissolution/precipitation processes for single plastics by selecting solvents from past literature. S87, 649-650 However, an ongoing challenge is solvent selection for plastic mixtures which are ubiquitous in realistic plastic waste. Multicomponent polymeric materials are often made from two or more plastics, each of which is selected to contribute its own useful properties. For example, food packaging boxes are typically multilayer plastic films, which are extremely challenging to recycle because of their complex compositions and the incompatibility of different polymer layers. Dissolution-based methods are promising for recycling such materials because selective dissolution enables the separation of different plastics and is tolerant to the additives and impurities present in waste. However, due to the variety of possible plastic combinations, as well as the necessity for choosing appropriate operating temperatures for dissolution and precipitation, solvent selection for plastic mixtures is a difficult task.

Based on the thermodynamic framework described above, one method for solvent selection is to compute solubility parameters for target plastics and solvents to predict dissolution. Hildebrand solubility parameters can be applied with reasonable accuracy to predict solubility in systems dominated by non-polar interactions, but are inaccurate for mixtures with strong polar or specific interactions such as hydrogen bonds. S89, 652 Similar to the Hildebrand solubility parameter, other parameter sets have been applied to identify solvents and antisolvents for plastics; examples include Hansen Kamlet-Taft G54, Gutmann G55, and Swain G56 parameters. These parameter assess the chemical similarity between species to predict dissolution behaviors. Among them, Hansen solubility parameters (HSP) are the most widely used to select solvents for plastic dissolution. Among them, Hansen solubility parameters (HSP) are the most widely used to select solvents for plastic dissolution.

polar (δ_P) , and hydrogen-bonding (δ_H) interactions. Solvent-polymer interactions are measured by their distance R_a in the 3-dimensional HSP space $(2\delta_D - \delta_P - \delta_H)$ space) as shown in Eq.15.

$$R_a^2 = 4\left(\delta_D^{\text{solvent}} - \delta_D^{\text{polymer}}\right)^2 + \left(\delta_P^{\text{solvent}} - \delta_P^{\text{polymer}}\right)^2 + \left(\delta_H^{\text{solvent}} - \delta_H^{\text{polymer}}\right)^2$$
Eq.15

Each polymer has an additional radius parameter, R_0 , that defines a sphere in the HSP space. Solvents within this sphere ($R_a/R_0 < 1$) are expected to dissolve the polymer, whereas solvents outside of this sphere ($R_a/R_0 > 1$) are not expected to dissolve the polymer. Tabulated HSP and R_0 values are available for a large number of polymers and solvents based largely on empirical data and have been used in many successful applications of solvent screening. 657-658

Building upon the success of these solubility parameter methods, newer computational approaches for predicting polymer solubilities and screening solvents with minimal experimental effort have emerged in recent years. A recent example was the development of machine learning techniques for the large-scale binary classification of solvents and antisolvents for polymers, thus categorizing solvents into similar categories as HSPs. Specifically, Chandrasekaran et al⁶⁵⁹ developed a deep neural network to classify 24 common solvents for over 4500 homopolymers with an accuracy of 93.8%. This example demonstrates the feasibility of applying data-centric methods to rapidly screen potential polymer-solvent combinations for selective dissolution processes, although more data will be required to extend the solvent library.

The preceding techniques primarily focus on qualitatively classifying solvents and antisolvents for target polymers. However, the development of dissolution/precipitation processes requires quantitative analysis of solubilities as a function of temperature in order to assess the feasibility and economics of potential industrial-scale processes. To address this challenge, Zhou et al. developed a computational approach for quantitatively predicting temperature-dependent polymer solubilities using molecular-scale models. ⁶⁶⁰ This approach employs molecular dynamics simulations to sample polymer conformations in representative solvents. These conformations are used as input to the COnductor-like Screening MOdel for Real Solvents (COSMO-RS), a model that used quantum mechanical calculations and statistical thermodynamics methods to predict polymer solubilities through solid-liquid equilibrium calculations. ^{609, 660} After initial polymer conformations are available, temperature-dependent solubilities can be obtained rapidly (~minutes). This approach was applied to screen over 500 solvent combinations for the selective dissolution of PE and EVOH and extended to develop a STRAP process for a commercial multilayer film with four polymer components. ^{608-609, 660}

8.6 Techno-Economic Analysis of STRAP

A published techno-economic analysis of the STRAP process has demonstrated that plastics recovered via this technology can be sold at prices that are comparable to virgin resins. Due to STRAP being a new technology, the size of the process required to achieve a competitive sell price is important, as large capital costs can make scaling up to an industrial level difficult. At a feed rate of 3000 tonnes/yr, plastic recycled by the STRAP process can be sold at a minimum selling price (MSP) of \$2.18/kg, while delivering a discounted return on investment (DROI) of 10% to investors over a 20-yr lifetime. The MSP can be further reduced through optimization of STRAP design parameters, as shown in Figure 25.

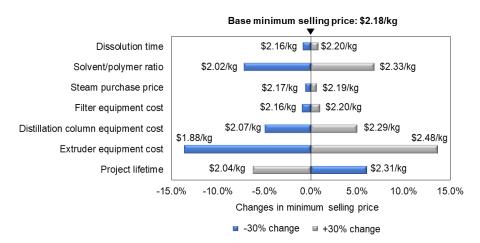


Figure 25. Sensitivity analysis of MSP for the STRAP process. Published with permission from ref ⁶⁰⁸. Copyright Wiley-VCH.

A key feature that drives economic performance is solvent selection. A solvent with a high affinity for a target polymer can decrease the dissolution time and solvent/polymer ratio which can in turn decrease the filter equipment cost by reducing its size. A low-boiling solvent/antisolvent pair with a high relative volatility or solvent that allows for temperature-controlled precipitation can reduce the size of or eliminate the need for distillation columns. Using less solvent, an easily separable solvent/antisolvent system, or eliminating the need for an antisolvent then reduces the quality and quantity of steam required. This illustrates that efficient solvent screening and selection is essential for establishing economic as well as technical feasibility of STRAP.

Figure 26 shows that STRAP is far from the point of diminishing returns at a processing capacity of 3000 tonnes/yr. These data indicate that there will be a significant economic incentive to scale STRAP up to larger sizes if the process is shown to be effective at smaller processing capacities. At a feed rate of 15,000 tonnes/yr, the recycled plastic could be sold for \$0.95/kg to achieve a DROI of 10% or deliver a DROI of approximately 30% if the selling price of \$2.18/kg is maintained while requiring about twice as much capital investment. This analysis demonstrates that the process has significant economic potential and can be made even more competitive via process optimization and solvent selection. More broadly, this analysis, along with the commercial demonstrations described previously, supports the economic viability of dissolution-based recycling techniques.

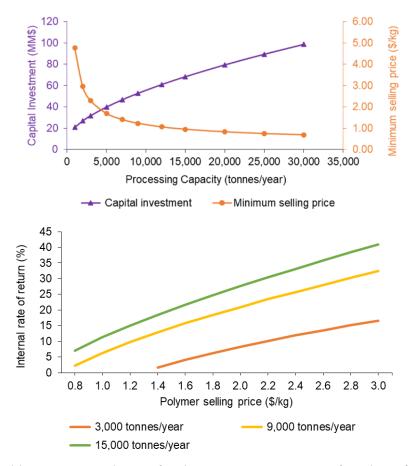


Figure 26. Capital investment and MSP for the STRAP process as a function of feed capacity(left) and DROI as a function of MSP at three different feed capacities (right). Published with permission from ref ⁶⁰⁸. Copyright Wiley-VCH.

9.0 Chemical Recycling of Polyester to Monomers9.1 Chemical Recycling of PET

The commercial uses of PET span a wide variety of industrial sectors, from fiber for textiles to resin for beverage bottles. In 2021, global PET consumption totaled 89.3 million metric tons (MMT) (Figure 27). It is the fourth most consumed plastic in the world after PE, PP, and PVC. 14, 661-662 There are many reviews in the literature summarizing recent progress in chemical plastics recycling, as well as several which focus solely on PET. 17, 280, 662-673 Chemical recycling of PET is an area of intense focus in the literature, and a comprehensive review of every report in this field is thus not attempted here. This section summarizes each strategy for PET depolymerization, with a focus on important and practical advances and their potential for industrial application. This review is organized into sections based on the approach to PET depolymerization: aerobic oxidation, hydrolysis, alcoholysis, glycolysis, aminolysis, hydrogenolysis, and enzymatic depolymerization (Figure 28). Current commercial activity in chemical PET depolymerization is included at the end of this section, along with comments on the economics of these processes.

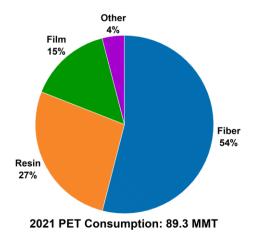


Figure 27. Global PET consumption in 2021.

9.1.1 Aerobic Oxidation

Aerobic oxidation of PET involves heating the polymer to high temperatures in the presence of oxygen, and sometimes a catalyst or promoter. In 1984, Jabarin and Lofgren⁶⁷⁴ studied the thermal oxidation of PET and showed that it was an exothermic reaction with an activation energy lower than the thermal decomposition of PET under vacuum. At all temperatures and drying conditions studied, increased decomposition of PET was observed under air as compared to under nitrogen. However, specific products of the reaction were not identified and PET degradation was measured only by the weight loss of the sample.

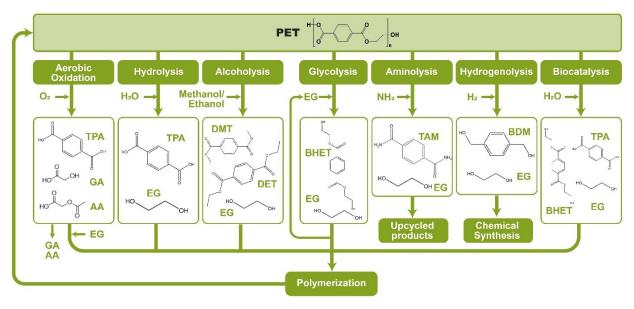


Figure 28. Strategies for PET chemical recycling discussed in this section, and their most common products. (TPA = terephthalic acid, EG = ethylene glycol, DMT = dimethylterephthalate, DET = diethylterephthalate, BHET = bis-2-hydroxyethylterephthalate, BDM = benzenedimethanol, MHET = mono-2-hydroxyethylterephthalate.)

Partenheimer⁶⁷⁵ received a patent in 2005 for the oxidation of a wide variety of polymers using a range of simple metal salt promoters. PET sourced from blue film, recycled resin, and shirts were depolymerized as 4-20 wt% solutions in acetic acid under 1,000 psia air pressure at 150-205 °C. A combination of Co/Mn/Br/Zr in varying ratios was used as a catalyst, and the effect of adding co-oxidants such as toluene and *p*-xylene was also investigated (Figure 29). TPA yields of up to 100% were reached, and more efficient conversion was observed at higher temperatures, longer reaction times, higher initial PET concentrations, and in the presence of either co-oxidant. Partenheimer further published that a 56% yield of TPA could be isolated from the oxidation of PET at 190 °C in a water/acetic acid mixture using a similar Co/Mn/Br/Zr catalyst. The TPA yield increased to 100% in the presence of toluene as a co-oxidant. This chemistry was based on an extensive review published by Partenheimer about a decade earlier on metal/bromide autoxidation of hydrocarbons.

Figure 29. Typical reaction conditions and products for PET aerobic oxidation.

9.1.2 Hydrolysis

Hydrolytic PET depolymerization involves the reaction of the polymer in either a basic, neutral, or acidic aqueous solution. The products of PET hydrolysis are TPA and EG. One major disadvantage of hydrolysis is the large volumes of inorganic salt and aqueous waste that are generated, along with the high corrosivity of the basic and acidic systems. It has been estimated that, on an industrial scale, 20-50 L of aqueous solution would be required to hydrolyze 1 kg of post-consumer PET, generating 5 kg of inorganic salt waste. However, it is also more tolerant of post-consumer waste contaminants and other polymers than many chemical recycling strategies. Several studies are included in this section that utilize post-consumer PET sources. However, it is also more tolerant of post-consumer waste contaminants and other polymers than many chemical recycling strategies.

9.1.2.1 Basic Hydrolysis

Basic hydrolysis is typically carried out in a 4-20 wt% solution of NaOH or KOH in water. Reaction temperatures average around 200 °C and pressures are usually 15-20 bar (Figure 30a). The disodium or dipotassium terephthalate product must be protonated with acid after the reaction, generating stoichiometric inorganic salt waste. LCA performed on this reaction demonstrated that decreasing the volume of water required for product purification is critical to achieve lower GHG emissions for this recycling process compared to PET incineration. Yoshioka and coworkers evaluated a system in which PET was hydrolyzed in concentrated NaOH at 250 °C and 5 MPa O₂ pressure for 5 hours. The disodium terephthalate was not oxidized under these conditions and was obtained in quantitative yields. However, EG was oxidized to oxalic acid in roughly 70% yield, generating a value-added product that could be sold to further improve the economics of this recycling strategy. 81

b) Neutral Hydrolysis

$$H_2O, 200-300^{\circ}C, \quad n_{HO}OH \rightarrow n_{HO}OH$$
 $\Delta_r H^o(473 \ K) = +8.5 \ kJ/mol \quad \Delta_r G^o(473 \ K) = +11.5 \ kJ/mol$

c) Acidic Hydrolysis
$$\begin{array}{c} O \\ O \\ O \\ O \\ O \end{array}$$
 OH
$$\begin{array}{c} >50 \text{ wt\% H}_2\text{SO}_4 \text{ (aq)} \\ \hline 60\text{-}90^{\circ}\text{C, 1 bar} \end{array}$$
 $\begin{array}{c} O \\ O \\ \text{TPA} \end{array}$
$$\begin{array}{c} O \\ + \\ \text{n}_{\text{HO}} O \\ \hline C \\ O \\ \text{HO} \end{array}$$

$$\begin{array}{c} O \\ + \\ \text{HO} \\ \hline C \\ \text{HO} \end{array}$$

$$\begin{array}{c} O \\ + \\ \text{HO} \\ \hline C \\ \text{HO} \end{array}$$

$$\begin{array}{c} O \\ + \\ \text{HO} \\ \hline C \\ \text{HO} \end{array}$$

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$$\begin{array}{c} O \\ + \\ \text{HO} \\ \hline C \\ \text{HO} \end{array}$$

Figure 30. Typical reaction conditions and products for uncatalyzed PET a) basic, b) neutral, and c) acidic hydrolysis. Calculations of enthalpy and Gibbs free energy were performed in the presence of solvent [Polarizable Continuum Model (PCM)]. Exchange-correlation functional: B3LYP. Basis set: 6-31++g(d,p). Neutral and basic environments H₂O is the solvent – at small concentration of NaOH/KOH reactant and product species will mainly interact with H₂O molecules. Acidic environment was simulated by setting the refractive index equal to 1.3945, which corresponds to 50 wt% sulfuric acid; the result is not very sensitive to the value of dielectric constant and the one for H₂O was used (i.e., 78).

A phase transfer catalyst such as a quaternary ammonium salt can be used to lower the temperatures and pressures required for alkaline hydrolysis. Kosmidis and coworkers⁶⁸² used this strategy to isolate TPA at high purity using aqueous NaOH and catalytic trioctylmethylammonium bromide to depolymerize post-consumer PET soda bottles under atmospheric pressure and at temperatures as low as 70 °C. Similarly, microwave irradiation has been used to lower the required temperature of basic PET hydrolysis.⁶⁸³ Khalaf and Hasan⁶⁸⁴ isolated TPA from post-consumer soda bottles in almost quantitative yields after only 1 hour of irradiation in the presence of tetrabutylammonium iodide as a phase transfer catalyst. The catalyst could be recovered from the reaction mixture after product extraction, which improves the potential practicality of this method.

Hu et al.⁶⁸⁵ found that using a mixed solvent system of an ether and an alcohol enabled complete depolymerization of PET with NaOH in 40 minutes at only 60 °C. Pure TPA and EG were easily isolated from the reaction mixture. In 2017, Essaddam⁶⁸⁶ received a patent for the room temperature hydrolysis of PET. The system consisted of a nonpolar solvent such as CH₂Cl₂, which

swelled the polymer, and an alcoholic solution of NaOH to hydrolyze the PET. High purity TPA could be isolated using this method in up to quantitative yields. Ügdüler and coworkers⁶⁷⁸ used ethanol as a cosolvent in the alkaline hydrolysis of PET to achieve 95% TPA yield in only 20 minutes at 80 °C. When post-consumer multilayer PET/PE trays were used as a substrate, yields were lower but still reached 45%.

9.1.2.2 Neutral Hydrolysis

Neutral hydrolysis is in many ways preferable to basic or acidic strategies, as the solution will not require specialized reactor materials to prevent corrosion and stoichiometric salts are not required or formed in the reaction. However, this also means that impurities and additives present in the PET remain in the recycled monomer, which is not the case in TPA generated from acidic and basic hydrolysis. Additionally, high temperatures and pressures are required for the reaction to run at an appreciable rate. The temperatures used are 200-300 °C, and often in the upper half of this range so the reaction runs in the melt phase of PET. Pressures of 10-40 bar are typically used, along with a large excess of water or steam (Figure 30b). The large volume of water required leads to very dilute solutions of EG in the product mixture, which makes isolation more difficult and costly. The reaction proceeds in about 1 hour at 275°C, and it has been proposed that the TPA formed in the reaction can catalyze the hydrolysis, rendering the reaction autocatalytic. 680, 687

Campanelli and coworkers⁶⁸⁸ investigated possible catalytic effects in the neutral hydrolysis of PET but found that zinc salts exhibit only a minute accelerating effect on the reaction. Full conversions were only reached at temperatures above 250 °C. Xylene was utilized as a cosolvent in neutral hydrolysis, which reduced the required temperature, pressure, and volume of water in the reaction. Additionally, this strategy enabled the efficient isolation of EG as a concentrated solution in the organic layer.⁶⁸⁹

Zhang et al. 690 used a dual phase-transfer catalyst [(CH₃)₃N(C₁₆H₃₃)]₃[PW₁₂O₄₀] in the neutral hydrolysis of post-consumer bottle PET at 145°C for 3 hours to obtain TPA yields of up to 93%. The catalyst allowed the reaction to be run at much lower temperatures and could be separated from the products and recycled at least three times without any observed decrease in efficiency. Stanica-Ezeanu and Matei⁶⁹¹ found marine water to be an excellent solvent for neutral PET hydrolysis due to the presence of various metal ions that can act as catalysts. They used simple salts commonly found in the ocean, including NaCl, KHCO₃, and CaCl₂, as catalysts in the depolymerization of PET at 200°C and 40 bar to obtain TPA in up to 85% isolated yield. Yields were increased at milder conditions when more than one salt was added or when marine water was used as a catalyst.

9.1.2.3 Acidic hydrolysis

Several systems have been described for the acidic hydrolysis of PET in concentrated (>50 wt%) H₂SO₄ solutions to generate high purity TPA in high yields at ambient pressures and relatively low temperatures (Figure 30c). However, these reactions are highly impractical at scale due to the corrosivity of the solution, the need to recycle large volumes of acid, the generation of stoichiometric salt waste, and the difficulty in isolating EG from the reaction. ^{671, 680, 692} Yoshioka and coworkers discovered that they could decrease the H₂SO₄ concentration by about half and still achieve complete hydrolysis of PET to TPA in 5 hours at 150°C. The acid was subsequently recovered by dialysis. The same group also reported that 7-13 M HNO₃ completely hydrolyzed PET over about 2 days at temperatures below 100°C. The EG was simultaneously oxidized to oxalic acid, a value-added product. ⁶⁹⁴

Liu et al.⁶⁹⁵ studied the hydrolysis of PET using the ionic liquid (IL) 1-butyl-3-methylimidazolium (Bmim) chloride as the solvent and an acid-functionalized IL (1-methyl-3-(3-methylimidazolium)).

sulfopropyl)-imidazolium hydrogen sulfate) as a catalyst. After 4.5 hours at 170°C, they isolated TPA in 88% yield, and were able to recycle the ILs at least 8 times with no decrease in yield. Yang and coworkers found that TPA itself was an effective catalyst for acidic PET hydrolysis. They achieved a 95.5% yield of high purity TPA after 3 hours at 220°C. The only workup required was a simple filtration, and the hydrolysis efficiency was maintained over 8 consecutive reaction cycles. 696

9.1.3 Alcoholysis

Alcoholysis depolymerizes PET in the presence of alcohols to form an ester and EG (Figure 31). Methanol and ethanol are the most common alcohols utilized in this reaction, but other alcohols can also be used.

9.1.3.1 Methanolysis

Methanolysis of PET produces dimethylterephthalate (DMT) and EG. DMT can be used directly in transesterification polymerization to form PET or further hydrolyzed to TPA. ^{671, 679, 697} However, methanolysis of post-consumer PET leads to high separation and purification costs due to the mixture of glycols, alcohols, and phthalate derivatives produced in the reaction. ⁶⁶² Methanolysis typically operates at temperatures of 180-280°C and pressures of 20-40 bar. The high pressures ensure that the methanol remains a liquid during the reaction. Transesterification catalysts such as zinc acetate, magnesium acetate, cobalt acetate, or lead dioxide are typically used, and yields of DMT average 80-85%. This reaction can be run in continuous flow, but complex reactors are required to add feedstocks while maintaining the required high reaction pressures. In a typical continuous method, melted PET and preheated methanol are fed into an autoclave with a set residence time to complete the depolymerization, then the mixture is flowed to the bottom of a second pressurized reactor at a lower temperature so that high density impurities can be removed. After leaving the second autoclave the reaction pressure is reduced, the product mixture is further cooled in a mixer, and finally DMT is isolated by precipitation. ^{671, 679, 698}

Figure 31. Typical reaction conditions and products for PET alcoholysis.

Sako and coworkers⁶⁹⁹ reported in 1997 that PET could be completely depolymerized to DMT, EG, and some oligomers with no catalyst in only 30 minutes in supercritical methanol. This was achieved at temperatures above 300 °C and pressures of 110 bar. Above supercritical conditions, the pressure of the reaction was not found to have a significant effect on DMT yield, however the severe conditions make this process too cost intensive for large scale use and too difficult to adapt to continuous flow.⁶⁷⁹

Kurokawa et al.⁶⁹⁷ used the transesterification catalyst Al(OⁱPr)₃ to promote the methanolysis of PET from soda bottles under more mild conditions. They achieved 88% DMT and 87% EG yields in 4:1 methanol:toluene at 200 °C and no added pressure. Improved yields in this solvent mixture compared to pure methanol indicate that the rate of methanolysis strongly depends on PET solubility. Hofmann and coworkers⁷⁰⁰ found that microwave irradiation facilitated the methanolysis of PET under even milder conditions using zinc acetate as a catalyst and CH₂Cl₂ as

a cosolvent to improve solubility. In only 20 minutes at 160 °C, moderate to high yields of DMT were isolated from a variety of post-consumer PET sources, including a dish detergent bottle (46% yield), a soap dispenser with a label (70% yield), and a transparent food container (98% yield).

Phan and Cho⁷⁰¹ reported that the inexpensive salt K₂CO₂ catalyzes PET methanolysis at room temperature. A 93% yield of DMT was obtained after 24 hours in a mixed solvent system of 1:1 methanol:CH₂Cl₂. Tanaka and coworkers⁷⁰² developed a new strategy wherein they trapped the EG formed in the reaction as ethylene carbonate. This biased the depolymerization equilibrium towards the monomers and enabled the reaction to run in only 5 hours at ambient temperature. Various simple alkali salts were used as catalysts, and optimized yields of DMT exceeded 90% using 5 mol% LiOMe.

9.1.3.2 Ethanolysis

PET ethanolysis yields diethylterephthalate (DET) and EG. The strategy is similar to methanolysis in many ways but could be particularly advantageous in countries such as Brazil where ethanol from sugarcane is cheap and abundant.⁷⁰³

In 2006, it was reported that PET could be completely depolymerized to its monomers in 5 hours in supercritical ethanol. At 528 °C and pressures of 76-116 bar, DET yields of 65-98% were obtained using post-consumer PET from a variety of sources including green bottles, mechanically recycled fiber, and polyester string. Favaro and coworkers studied the ethanolysis of multilayer food packaging containing PET, PE, and aluminum. The material was depolymerized over 2 hours in supercritical ethanol at 255 °C and 116 bar. High purity DET was obtained in 80% yield after precipitation, and metallic aluminum could also be isolated from the reaction. Lozano-Martinez and coworkers found that the product distribution from PET ethanolysis could be changed by altering the reaction conditions. Long reaction times in supercritical ethanol generated DET as the only product, while shorter reaction times at lower temperatures and pressures led to the formation of TPA.

Nunes et al. 706 reported that the addition of catalytic [Bmim][BF4] reduced the required reaction time for PET depolymerization in supercritical ethanol from 6 hours to only 45 minutes. Cobalt and nickel oxides have also been found to be effective catalysts for PET ethanolysis under supercritical conditions, and provide almost quantitative yields of DET. The required reaction time was only 90 minutes with low catalyst loadings. 707

9.1.4 Glycolysis

Glycolysis is one of the most intensely studied routes for chemical PET depolymerization, and several systems have been commercially adopted. Glycolysis involves the transesterification of PET with excess glycol, most commonly EG, to generate the corresponding ester (bis-2-hydroxyethylterephthalate, BHET, when EG is used) and EG as products (Figure 32). Many different classes of catalysts have been studied in this reaction. G62, G69, 708 Without a catalyst, PET glycolysis requires temperatures of 200-240 °C and pressures of 2-6 bar, and high monomer yields are not obtained. In 1991, Chen and coworkers 9 studied the relationship between reaction pressure and EG:PET ratio on depolymerization kinetics. Higher pressures were reported to enable faster reactions, and at higher EG concentrations BHET was in equilibrium with PET oligomers. At lower EG concentrations, no monomer was observed.

Figure 32. Typical reaction conditions and products for PET glycolysis with EG.

Metal acetates were first reported as PET glycolysis catalysts in 1989 and have been widely studied. ^{708,710-711} Güçlü and coworkers ⁷¹² used xylene to form a multiphase reaction in zinc acetate-catalyzed PET glycolysis with EG at temperatures of 170-245 °C. BHET was pulled into the xylene layer to bias the equilibrium of the depolymerization and prevent oligomer formation, providing monomer in up to 80% yield. Other diols such as butanediol and triethylene glycol have also been used in PET glycolysis with zinc acetate to generate monomers and dimers. ⁷¹³ Chen found that the optimal PET glycolysis temperature was 190 °C when using manganese acetate as a catalyst. Conversion of PET to BHET and dimer reached ~100% after 1.5 hours. ⁷¹⁴ Ghaemy and Mossaddegh ⁷¹⁵ used various metal acetate catalysts in the glycolysis of PET in refluxing EG. Yields of BHET reached up to 85% from both fiber and flake PET.

Troev and coworkers⁷¹⁶ demonstrated that light metal salts could also be used as glycolysis catalysts. They reported that titanium(IV) phosphate catalyzes the depolymerization of PET to BHET in up to 97% selectivity at 190 °C with a reaction time of 2.5 hours. Fang et al.⁷¹⁷ utilized polyoxometalates as catalysts for PET glycolysis under mild conditions. BHET was isolated in 85% yield after only 40 minutes at 190 °C and 0.018 mol% catalyst loading, with no loss in activity observed after the catalyst was recycled four times.

ILs have gained interest in the literature as catalysts for PET glycolysis due to the ease of separating the products from the reaction mixture, enabling facile catalyst recycling. ⁷¹⁸⁻⁷²⁰ H. Wang et al. ⁷¹⁸ first published the use of ILs as catalysts for PET glycolysis in 2009. They synthesized and tested several different ILs as catalysts and were able to achieve full conversion of PET to primarily BHET and some oligomers at 180 °C in 8 hours at atmospheric pressure. Higher reaction temperatures led to improved BHET selectivity. A subsequent study found that the IL could be recycled with no loss in activity. ⁷²¹ They then found that an iron-containing IL could catalyze the depolymerization at temperatures as low as 140 °C. ⁷²² Q. Wang ⁷¹⁹ and coworkers studied different metal-containing ILs as PET glycolysis catalysts. They achieved isolated yields of up to 80% high purity BHET after 75 minutes at 175 °C and atmospheric pressure. Other metallic ILs have been shown to be effective catalysts for this reaction under a variety of conditions. ⁷²³ Yue et al. ⁷²⁴ used basic ILs at catalysts in PET glycolysis to isolate BHET in yields of up to 71% after 2 hours at 190 °C.

Deep eutectic solvents (DESs) have also garnered recent interest as catalysts for PET glycolysis due to their low cost, simple synthesis, low toxicity, and other characteristics shared with ILs such as thermostability and tunability. PET Q. Wang and coworkers first used DESs as catalysts for PET glycolysis in 2015. Under optimized conditions of 170 °C and only 30 minutes, BHET was obtained in 83% yield. These results are similar to those obtained under supercritical conditions. The high activity is attributed to a synergistic effect between H-bonds and coordination bonds between the DES and EG. Sert et al. PET glycolysis catalysts. The best catalyst tested was formed from potassium carbonate and EG, and reached isolated BHET yields of up to 88% after 2 hours at 180 °C.

A variety of different heterogeneous catalysts have also been used in the glycolysis of PET. Shukla and coworkers⁷²⁸ used β - and γ -zeolites as catalysts for PET glycolysis in 2008. BHET yields of over 60% were reached after 8 hours in refluxing EG. Al-Sabagh et al. 729 used multiwalled carbon nanotubes doped with Fe₃O₄ as catalysts for PET glycolysis, and reported quantitative BHET yields after 2 hours at 190 °C. The catalyst was successfully recycled 8 times with no loss in activity. Veregue et al. 730 used 3 nm cobalt nanoparticles as catalysts, and isolated pure BHET without additional water in 77% yield after 3 hours at 180 °C. The catalyst could be reused at least 5 times with no drop in activity. Laldinpuii and coworkers⁷³¹ used bamboo leaf ash as a bio-waste derived catalyst for PET glycolysis. Several metal oxides and other salts were identified in the catalyst, which provided BHET in up to 83% yield after 3 hours at 190 °C. The catalyst could be reused four times with only a slight decrease in yield, and EG was also recovered from the reactions for reuse. Z. Wang et al. 732 developed a colloidal catalyst based on graphitic carbon nitride for this reaction. 80% BHET yield was achieved in 30 minutes at 196 °C for five consecutive catalyst cycles. Several different post-consumer PET sources were successfully depolymerized to give BHET in ~80% yield, including green bottle flake, noise deadening foam, and bottle flake contaminated with PP.

IL catalysts have been tethered to heterogenous supports to enable even more facile catalyst recovery and product isolation. Najafi-Shoa⁷³³ and coworkers used a cobalt-containing IL supported on graphene to reach 95% isolated BHET yields after 3 hours at 190 °C and ambient pressure. The catalytic activity was maintained over five cycles. Al-Sabagh et al. ⁷³⁴ supported iron-containing ILs on bentonite to reach a maximum 44% BHET yield. Similarly, Cano et al. supported iron-containing ILs on silica-coated, magnetic Fe₃O₄ nanoparticles. The recoverable catalyst gave quantitative BHET yields for an impressive twelve consecutive 24 hour cycles at 190 °C, and the magnetic particles greatly simplified reaction workup. ⁷³⁵

Organocatalytic PET glycolysis was first reported in 2011 by Fukushima et al. ⁷³⁶ using the amine base 1,5,7-triazabicyclo[4.4.0]dec-5-ene (TBD). Isolated BHET yields of up to 78% were reached after 3.5 hours at 190 °C and atmospheric pressure, comparable to some of the most efficient metal-catalyzed reactions. A study of several other nitrogen-based catalysts led to the discovery that 1,8-diazabicyclo[5.4.0]undec-7-ene (DBU) was an even more efficient catalyst when EG was used as the glycol. Mechanistic studies revealed that EG and other short chain diols can act as cocatalysts to activate the PET ester group and assist in depolymerization (Figure 33). ⁷³⁷ Jehanno and coworkers ⁷³⁸ used a salt derived from TBD and methanesulfonic acid as a catalyst in PET glycolysis. 91% BHET was isolated after 2 hours at 180 °C. The catalyst could be recycled at least five times, and the monomer isolated from these reactions was used to synthesize new PET with similar thermal properties as commercial material.

Figure 33. Proposed mechanism of PET activation by the organic bases TBD or DBU and short chain alcohols. Longer chain alcohols cannot participate in this reaction.

Microwave irradiation is another growing strategy for facilitating PET glycolysis at milder conditions than conventional heating. Pingale and Shukla⁷³⁹ first published in 2008 that, under otherwise identical zinc acetate-catalyzed glycolysis conditions, microwave irradiation provided the same yield of BHET in 35 minutes that conventional heating did in 8 hours. This increased efficiency was confirmed by Chaudhary et al.⁷⁴⁰ Achilias et al.⁷⁴¹ studied the microwave glycolysis of PET to oligomers using diethylene glycol. They found that complete degradation was achieved in only 5 minutes at 180 °C, compared to more than 4 hours using conventional heating. Saravari et al.⁷⁴² glycolyzed PET bottles with propylene glycol under microwave irradiation with zinc acetate as a catalyst. Oligomers obtained from the reaction were reacted with linseed oil and toluene diisocyanate to obtain urethane oil with similar properties to commercially purchased material, showing the potential of this strategy for PET upcycling. Parrott⁷⁴³ received a patent for microwave-assisted PET glycolysis in 2020. BHET yields of up to 94% were achieved in only 5 minutes of irradiation at 250 °C with 0.1 wt% zinc acetate as a catalyst. A variety of simple salt catalysts were investigated, and zinc salts were generally the most effective.

9.1.5 Aminolysis

Aminolysis depolymerizes PET in the presence of amines to form terephthalamides and EG. This process is more thermodynamically favored than alcoholysis or glycolysis due to the stronger amide bonds formed in the products, and so less forcing conditions can be used (Figure 34).⁷⁴⁴ The terephthalamide monomers can be used in a variety of upcycling applications, including antibacterial drugs, adhesion promoters, and as components for rigid polyurethane foams.⁶⁶⁷ Aminolysis was first reported in the 1960s using a variety of primary and secondary amines.⁷⁴⁵ In 2010, Soni and coworkers⁷⁴⁶ depolymerized PET to terephthalamide using hydrazine in an uncatalyzed reaction at ambient temperature and pressure. After 12 hours, the product was isolated and reacted with acryloyl chloride to provide a UV curable acrylic oligomer, demonstrating a potential application of this depolymerization technique to generate upcycled products. In 2013, Bhatnagar and coworkers⁷⁴⁷ working for the Indian Oil Corporation received a patent for aminolysis of virgin or post-consumer PET using (poly)amines to generate diamino diamido mixtures with excellent bitumen anti-stripping properties. Reactions with quantitative product yield were run in xylene at 110-160 °C for 4 hours without a catalyst.

HOO OH HNRR'
$$R$$
 AND R AND

Figure 34. Typical reaction conditions and products for PET aminolysis.

Soni and Singh reported the aminolysis of PET in the presence of aqueous methylamine or ammonia using cetyl ammonium bromide as a catalyst in 2005. They found that the catalyst reduced the required time for complete degradation to N,N'-dimethylterephthalamide to 45 days at 40 °C, while large PET flakes were still visible in the uncatalyzed reaction after the same time.

Ammonolysis of PET was much slower, and full depolymerization was not achieved under any tested conditions.⁷⁴⁸ In 2006, Shukla and Harad⁷⁴⁹ reported the aminolysis of PET using excess ethanolamine and simple catalysts including acetic acid, sodium acetate, and potassium sulfate.

The product bis(2-hydroxy ethylene)terephthalamide (BHETA) was obtained in yields of up to 91% from post-consumer PET and 83% from bottle PET after 8 hours at reflux. Sodium acetate was found to give the highest yields in all reactions.

Tawfik and Eskander⁷⁵⁰ used dibutyltin oxide as a catalyst in the aminolysis of PET with ethanolamine at 190 °C and ambient pressure. Pure BHETA was obtained in yields of 49-62% after 1-4 hours. Chan and coworkers⁷⁵¹ used zinc acetate as a catalyst to depolymerize post-consumer bottle PET in the presence of tri- and tetraamines. The reactions were complete in 30 minutes at 190 °C, and no purification of the polyamine products was necessary before the authors used them in crosslinking reactions with ethylene glycol diglycidyl ether to form hydrogels with potential uses in removing industrial dyes from water and other environmental and agricultural applications (Figure 35).

Figure 35. Aminolysis of PET using a polyamine, followed by a crosslinking reaction to form a PET hydrogel.

Fukushima and coworkers⁷⁴⁴ used TBD as a catalyst in PET aminolysis with a variety of primary amines. The terephthalamide products were obtained in moderate to high yields at reaction temperatures of 110-190 °C in less than 24 hours. The monomers have potential applications as building blocks for high performance materials with desirable thermal and mechanical properties. The same group used this catalytic system to depolymerize PET with *o*-phenylenediamine and 2-aminophenol to generate bis-benzamidazole and bis-benzoxazole, which can be used in the synthesis of medicines and high-performance polymers .⁷⁵²

Microwave irradiation has also been studied in PET aminolysis. Pingale and Shukla⁷⁵³ reported the microwave-assisted aminolysis of PET using simple sodium salt catalysts and excess ethanolamine in 2009. BHETA yields of up to 90% were obtained in only 5 minutes under microwave irradiation, whereas similar yields required 8 hours using conventional heating. Cleaned post-consumer PET bottles and pristine PET fibers were both effectively depolymerized using this system. Achilias and coworkers⁷⁵⁴ utilized microwave heating to quantitatively depolymerize PET to BHETA in only 5 minutes at 260 °C without the addition of a catalyst.⁷⁵⁵

Hoang and Dang reported the uncatalyzed aminolysis of PET to bis(2-aminoethyl)terephthalamide and its oligomers α , ω -aminoligo(ethylene terephthalamide), but Sharma et al. ⁷⁵⁶ found that the same reaction could be carried out in only 10 minutes at 250 °C using microwave irradiation. They then used the obtained amides to synthesize bis-benzoxazines, which can be used as advanced performance thermosets.

The ammonolysis of PET involves the reaction of the monomer with excess ammonia to generate terephthalamide and EG as products. Terephthalamide can be further converted into platform chemicals *p*-xylenediamine or 1,4-bis(aminoethyl)cyclohexane.¹⁷ A patent from 1988 describes the ammonolysis of PET under 20 bar NH₃ pressure at temperatures of 120-180 °C for 1-7 hours. A simple filtration and drying workup provided the product in >99% purity and >90% yield. The same patent describes the use of zinc acetate as a catalyst to facilitate the transformation at only 70 °C and provide terephthalamide in 87% yield.¹⁷

9.1.6 Hydrogenolysis

Hydrogenolysis reductively depolymerizes PET under H₂ pressure, typically forming 1,4-benzenedimethanol (BDM) and EG, and sometimes providing deoxygenated products. BDM is a platform chemical that can be used to prepare polylactide-based thermoplastic elastomers, highly cross-linked polymers, and sulfonated aromatic resins.⁷⁵⁷⁻⁷⁵⁹ Organometallic catalysts have typically been used for these depolymerizations (Figure 36).

$$\begin{array}{c}
A \\
H
\end{array}$$

$$\begin{array}{c}
H_{2} \text{ (55-100 bar), cat.} \\
140-160^{\circ}\text{C}
\end{array}$$

$$\begin{array}{c}
\text{Cat. = organometallic catalyst}
\end{array}$$

$$\begin{array}{c}
\text{III)}
\end{array}$$

$$\begin{array}{c}
A_{1} \\
A_{1} \\
A_{2} \\
A_{2} \\
A_{1} \\
A_{2} \\
A_{2} \\
A_{3} \\
A_{4} \\
A_{5} \\
A_{$$

Figure 36. (A) Typical reaction conditions and products for PET hydrogenolysis and (B) Organometallic catalysts used for PET hydrogenolysis by I) Krall et al., II) Fuentes et al., and III) Westhues et al.

In 2014, Krall and coworkers⁷⁶⁰ found that a ruthenium pincer complex developed by Milstein could be used as a catalyst in the hydrogenolysis of PET (Figure 36B I). At 2 mol% catalyst loading, 55 bar H₂, and 160 °C in anisole/THF, quantitative conversion to BDM and EG was observed after 48 hours. Post-consumer PET soda bottles were used in these experiments without pretreatment. Fuentes et al.⁷⁶¹ found that a novel PNN pincer complex (Figure 36B II) catalyzed PET hydrogenolysis with moderate BDM yields, but the catalyst was poisoned by the EG formed in the reaction. This precluded monomer yields higher than 73%. Westhues et al.⁷⁶²

used a ruthenium triphos catalyst (Figure 36B III) to depolymerize PET from a variety of sources, including water bottles, pillow filling, and a sports jersey. Reaction selectivity for BDM and EG were over 98% with most substrates, but relatively forcing conditions of 100 bar H₂ and 140 °C were required. An entire PET water bottles with PP cap and PE label was depolymerized without pretreatment. Quantitative conversion to BDM was observed, with no conversion of PP or PE. The other polymers could be filtered off and subsequently depolymerized.

Supported metal catalysts have also been used in PET hydrogenolysis. In 2020, Kratish et al. ⁷⁶³ selectively depolymerized PET to TPA and ethylene using a carbon-supported molybdenum-dioxo catalyst under only 1 bar H₂. No solvent was required for the reaction, and TPA was obtained in 85% yield after 24 hours at 260 °C. The air and moisture stable catalyst could be recycled four times with no loss in activity, and the yield of TPA did not change when PET from a post-consumer beverage bottle was used as the substrate. Jing and coworkers ⁷⁶⁴ used a Ru/Nb₂O₅ catalyst to convert PET to benzene, toluene, and *p*-xylene in 84% total yield. The reactions were run in octane at 280 °C and 5 bar H₂ for 8 hours. The catalyst also successfully depolymerized a mixture of PET, polycarbonate (PC), PS, and polyphenylene oxide to a variety of aromatic monomers in 79% overall yields, showing the viability of this system in mixed waste streams. However, a 1:1 mass ratio of polymer to catalyst was required in this system. Wu et al. ⁷⁶⁵ prepared an N-doped carbon-supported bimetallic catalyst for the conversion of PET to TPA in 91% yield in 10 hours at 260 °C and 1 bar H₂. No solvent was used in the reaction, and the catalyst could be reused at least six times with no observed decrease in activity. Almost the same yield of TPA was achieved with PET from bottles and with a mixture of PET and PP from bottles.

9.1.7 Biocatalysis

Given the ubiquity of natural ester-linked compounds in nature, including polymers such as cutin and suberin, enzyme catalysts have been pursued as another means to hydrolyze PET. These biocatalytic reactions have the advantage of enabling PET hydrolysis under mild conditions (30-75 °C and ambient pressure) in aqueous solutions to provide BHET, mono-2-hydroxyethylterephthalate (MHET), TPA, and EG with varying selectivity as products (Figure 37). Many reviews have been written on this topic^{21, 662, 766-771} and it is a highly active area of research, thus we only discuss highlights here.

Figure 37. Typical reaction conditions and products for enzymatic PET depolymerization.

The first report of enzymatic hydrolysis of PET was in 2005 from Müller et al. 772 wherein they showed appreciable extents of PET conversion over 3 weeks at 55 °C using a cutinase enzyme from the thermophilic bacterium *Thermobifida fusca*. This study prompted a search in genome and metagenome databases for additional cutinases capable of PET hydrolysis. In addition to the

discovery and characterization of homologous enzymes from the genus *Thermobifida* and closely related bacteria, 773-781 Sulaiman et al. reported the discovery of a leaf-branch compost cutinase (LCC) that has been subsequently engineered by Tournier et al. for greater thermal stability and activity, enabling quantitative conversion of amorphous micronized PET substrates in 10 hours at 72 °C and enzyme loadings concomitant with industrial performance. Re2-784 Shirke et al. Red demonstrated that the addition of glycosylation to the LCC enzyme via expression in Pichia pastoris results in greater stabilization of the enzyme, thus highlighting the potential for post-translational modifications as another means of enzyme stabilization and engineering for industrial applicability. A similar enzyme to LCC was recently reported by Sonnendecker et al. Ref that is able to achieve similarly high PET conversion with no substrate pretreatment. Additional studies to diversify the known PET hydrolytic enzyme suite will likely be enabled by computational methods and the massive number of genome and metagenome sequences that are continuously being reported.

The seminal discovery of *Ideonella sakaiensis* by Yoshida and coworkers⁷⁸⁹ in 2016 highlighted that natural microbial systems are seemingly responding to the presence of PET in the natural environment. In particular, *I. sakaiensis* secretes a two-enzyme system, comprising the enzymes PETase and MHETase, to fully depolymerize PET into TPA and EG via the intermediates BHET and MHET. This two-enzyme system has been extremely well studied to date, with structural biology techniques⁷⁹⁰⁻⁷⁹⁶ and many types of protein engineering and evolution approaches used to improve the stability and performance particularly of the PETase enzyme.^{795,797-798} The *I. sakaiensis* system also points to the potential utility of an enzyme cocktail for industrial application of an enzymatic recycling approach, as is common in industrial cellulose deconstruction, especially in this case to overcome product inhibition due to the buildup of MHET during enzymatic hydrolysis.^{782,799}

Singh et al. recently conducted a detailed techno-economic, energy, and GHG emissions analysis of enzymatic PET recycling using the patent literature and the work from Tournier et al. 784,799 Therein, they estimated that with low-cost PET feedstocks, enzymatic recycling processes could achieve cost parity with virgin PET manufacturing at substantially reduced energy inputs and GHG emissions. This work directly highlighted two areas of prominence that merit further attention in process development for enzymatic PET recycling, which also may translate to other PET chemical recycling approaches discussed herein. Namely, it was estimated that approximately half of the energy input and GHG emissions arise from substrate pretreatment, which was modeled as thermal extrusion and cryo-grinding to yield micronized, amorphous PET. The development of enzymatic systems that can deconstruct crystalline substrates, which has been highlighted by studies as a major need for the field, 786, 798, 800-801 would thus be a major step forward for this approach. Secondly, EG recovery from water was estimated to roughly equate to the other half of energy use and GHG emissions. Advanced approaches to separations for EG that operate in the condensed phase or employ reactive distillation may be of use to further improve this process and will likely be relevant for EG recovery in chemical solvolysis reactions as well.

9.2 Chemical Recycling of Polycarbonates and Other Polyester Feedstocks **9.2.1** Polycarbonates

PC resins are generally distinguished by whether they have aliphatic or aromatic backbones. Aliphatic PC resins are not used as thermoplastics, while aromatic PCs are commonly used as engineering thermoplastics in electric and electronic equipment. Poly(BPA carbonate) (PBPAC) is the most commonly used PC and is the only PC resin that we will discuss in this section, though many chemical recycling strategies applied to PBPAC could also likely be applied

to other PCs. 802-803 PBPAC has many desirable properties including high impact resistance and ductility, good optical clarity, flame retardancy, and relatively low production costs. Its global production has risen to 5 million tons per year. 804 Though commercial PC chemical recycling has not yet been realized, 805 many of the chemical recycling techniques discussed previously for PET have been investigated on a laboratory scale for PBPAC, including pyrolysis, hydrolysis, alcoholysis, aminolysis, and hydrogenolysis (Figure 38).

PBPAC pyrolysis produces a large amount of char due to the flame retardancy of the polymer. Uncatalyzed pyrolysis at 300-500 °C leads to the generation of BPA and phenolic compounds as the primary liquid products, leaving behind a residue which accounts for 20-30 wt% of the starting material. Rolling Metal chloride or oxide catalysts such as CuCl₂, FeCl₃, ZnCl₂, SnCl₂, CaO, and MgO have been shown to lower the temperatures required for pyrolysis, narrow the product distribution, and decrease the amount of char waste formed in the reaction. Rolling Papace and Co₂ are the primary products of PBPAC hydrolysis. Rolling At temperatures above 240 °C, BPA and CO₂ are the primary products of PBPAC hydrolysis. Rolling Alkaline earth metal oxides and hydroxides, alkali hydroxides and carbonates, and rare earth triflates all catalyze PBPAC hydrolysis, enabling milder reaction conditions and higher BPA yields especially when an organic cosolvent such as 1,4-dioxane is used. Rolling Fall Similar to hydrolysis of PET, ionic liquid catalysts and microwave heating Rolling Rolling facilitate this reaction.

Figure 38. Methods for the chemical depolymerization of PBPAC and their primary monomeric products.

To our knowledge, PBPAC alcoholysis was first reported with methanol, NaOH catalyst, and toluene cosolvent to swell the polymer and obtain BPA and methylene carbonate as products.⁸²³ The reaction has since been adapted to continuous flow,⁸²⁴ accelerated using

microwave heating, 822 and run under supercritical conditions. 825-827 Alkali halide, heterogeneous, ionic liquid, and organic base catalysts have also been employed to increase yield and selectivity for BPA under milder conditions. 828-836 The aminolysis of PCs provides value-added ureas and BPA as products. The yield of monomeric products is increased when a diamine is used to form a stable cyclic urea. 837-838 An ionic liquid/ZnO nanoparticle catalyst system provides excellent BPA and urea yields with a variety of mono- and diamines. 839 Ammonolysis of PBPAC in an aqueous ammonia solution provides BPA and urea in high yields. 840-841 Finally, many of the catalysts studied in PET hydrogenolysis also successfully depolymerize PCs under similar conditions to generate the corresponding alcohol monomer and methanol in high yields. 760, 762, 764

9.2.2 Other Polyesters

Poly(butylene terephthalate) (PBT) (Figure 39) can be used in similar applications as PET and also as an engineering thermoplastic in rigorous mechanical profile applications such as car bumpers.¹⁴ PBT resins have high strength and rigidity, low moisture absorption, and excellent electrical properties and chemical resistance.⁸⁴² Due to their similar chemical structures, many of the PET depolymerization strategies discussed above also successfully depolymerize PBT.

Figure 39. Chemical structure of PBT.

Poly(lactic acid) (PLA) is a widely used, industrially compostable bioplastic derived from the fermentation of renewable feedstocks. PLA has good mechanical properties but a low glass transition temperature, narrow temperature-processing window, and undesirable brittleness. Depolymerization of PLA to the lactide monomer is not possible due to side reactions including elimination to acrylic acid and epimerization. He primary method used for the deconstruction of PLA on the lab scale is hydrolysis to lactic acid (Figure 40). Additionally, some catalysts used in the hydrogenolysis of PET are capable of reductively depolymerizing PLA to form propylene glycol in high yields. PLA

HO
$$\xrightarrow{\text{Hydrogenolysis}}$$
 $\xrightarrow{\text{Hydrolysis}}$ $\xrightarrow{\text{Hydrolysis}}$ $\xrightarrow{\text{HO}}$ OH

Figure 40. Hydrolysis and hydrogenolysis of PLA to form lactic acid and propylene glycol, respectively.

9.3 Commercial Activity and Economics

Much of the current commercial progress in PET chemical recycling is not captured in scientific publications, with patents and press announcements typically constituting the public information in this field. A recent review of advanced PET chemical recycling focuses primarily on the development of commercial processes. 665 At the time of publication, commercial chemical

PET recycling has not yet been realized. However, many commercialization projects exist using different depolymerization chemistries and subsequent downstream purification processes.

Mechanical recycling of PET is complementary to chemical recycling processes, and both are needed to achieve a high degree of circularity in PET applications. Chemical recycling feedstocks will comprise primarily colored and/or opaque plastic bottles and polyester-based textiles that are unsuitable for the high purity standards required in mechanical recycling. 661, 663 The availability of a high volume, low cost feedstock is critical for commercial process viability, which will require processing highly impure PET feedstocks to produce high purity, polymerization-grade monomers at scale. The quality of the output of rPET from chemical recycling is higher than that from mechanically recycled PET. This allows the rPET from chemical recycling facilities to be infinitely recyclable, whereas the rPET produced from mechanical recycling degrades during each cycle.

The commercial activity described below is in the research and development-to-pilot stage unless otherwise indicated. To our knowledge, hydrolysis, methanolysis, glycolysis, and enzymatic depolymerization are the current primary areas of commercial focus, but it is likely that additional technologies will soon emerge on the commercial landscape. The intention of the processes described here is the transformation of waste PET plastic and textiles to monomers for subsequent repolymerization to rPET with physical and mechanical properties identical to those of pristine material.

9.3.1 Hydrolysis

DePoly is a Swiss start-up that uses a room temperature basic hydrolysis process with TiO₂ or another metal oxide absorber in the presence of UV light.⁸⁴⁵ The technology was originally developed at the Swiss Federal Institute of Technology Lausanne (EPFL).⁸⁴⁶ Tyton BioSciences, recently renamed Circ, is a start-up based in the US which uses alkaline water at high pressure and temperature, called hydrothermal processing, to hydrolyze PET fiber to TPA, EG, and products formed from the reaction of other materials such as cotton present in the textile waste stream.⁸⁴⁷ Gr3n, a Swiss-based start-up, announced the building of a demonstration plant in Italy in 2021. Their process features microwave-assisted hydrolysis that will be used to recycle both PET fiber and resin.⁸⁴⁹

9.3.2 Methanolysis

Loop Industries, a publicly traded Canadian company, has signed multiple partnerships for a global rollout of their methanolysis technology. Using a patented process, the PET resin or fiber input is mixed with methanol, an organic swelling solvent, and an inorganic alkoxide catalyst. The reaction proceeds at a temperature below the boiling point of methanol and does not require added pressure. At the time of writing this review, a timeline on their website states that Loop Industries has raised over \$116 million but as of yet does not have a commercial facility for their technology. Eastman Chemical has recently announced plans to build a \$250 million (USD), 100 kton/year PET methanolysis plant in Tennessee. They have been researching PET methanolysis for several decades, with patents in this field dating back to the early 1990s.

9.3.3 Glycolysis

There are many companies working to commercialize glycolysis processes with unique process concepts. JEPLAN, a Japanese start-up, uses a metal hydroxide catalyst and EG for PET glycolysis in a pilot plant in Japan. They utilize a two-step purification process involving crystallization and distillation to produce polymerization-quality BHET. Start Ioniqa, a spin-off from Eindoven University, developed a process which features an imidazole base tethered to a magnetic

iron oxide nanoparticle.⁸⁵⁴ The magnetic nature of the anchored catalyst facilitates simplified catalyst removal and recovery for reuse. Ioniqa has agreements with large consumer packaged goods companies in addition to PET producers and has recently announced a 10 kton/year facility.⁸⁵⁵ Researchers at IBM have taken a different path to enable the facile separation and reuse of a PET glycolysis catalyst. Their process is catalyzed by a volatile organic base that can be recovered by distillation after PET depolymerization is complete.⁸⁵⁶ This technology, known as VolCat (Volatile Catalyst), is being scaled up in a recently announced joint venture with several commercial partners.⁸⁵⁷

9.3.4 Biocatalysis

Commercial activity in biocatalytic PET depolymerization is highlighted by the publicly traded enzyme-catalyzed process from Carbios in France, who launched a demonstration plant in 2021. Carbios has announced partnerships including investors, end customers, enzyme producers, and process and plant designers to accelerate commercialization. Cabios has raised over \$126 million to develop their technology, and they currently operate a 1.2 kton/year demonstration facility with goals to build a 40 kton/year facility by 2025.

10.0 Other Catalytic Approaches for Plastics Conversion 10.1 Hydrogenolysis with Noble Metals

Hydrogenolysis of plastics cleaves the carbon-carbon bonds in the presence of hydrogen converting the polymers into hydrocarbons (ranging from C1 to C50) typically with noble metal (e.g., Ru, Pt etc.) catalysts. In such process, heterogeneous catalysts are used which enables simple separation and recycling from the reactants and products.

Table 18 summarizes different technologies utilized in hydrogenolysis of waste plastics where plastics were converted in batch reactors. Ruthenium supported on metal oxides or carbon has been reported to catalyze the production of alkanes, aromatics, and liquid fuels from polyolefins (i.e., LDPE, HDPE, PP), PS, and PC. 862-868 LDPE, HDPE, and PP can be converted to liquid fuel (C5-C21) and lubricants/waxes (C22-C45) at low temperature and low H₂ pressure (i.e., 200-250 °C, 20-30 bar) on metal oxides-supported Ru (e.g., Ru/TiO₂, Ru/CeO₂). 862, 868 Over multifunctional Ru/Nb₂O₅, monocyclic aromatics can be selectively produced from single or mixed aromatic plastics (i.e., PET, PC, PS, polyphenylene oxide) at 200-320 °C in the presence of hydrogen and solvent (e.g., water, octane etc.). 863 Ru hydrogenation sites with low coordination numbers (i.e., 5-6) prevent the over-hydrogenating of the aromatics, while the surface Lewis acid and Brønsted acid sites on NbO_x species act in concert to selectively adsorb, activate C-O bonds, and cleave C-C bonds of the plastics. The support can be adjusted to treat different plastics and obtain varied products. 864-867 Over Ru/WO₃/ZrO₂, LDPE can be converted into higher molecular weight fuels and wax/lubricant base-oils at 250 °C and 50 bar H₂. 867 While on Ru/FAU, methane (>97%) can be produced from PE, PP, and PS under 50 bar H₂ at 300-350 °C. 866 Ru nanoparticles can also be supported on carbon (Ru/C) to catalyze the hydrogenolysis of LDPE, HDPE, and PP towards liquid *n*-alkanes and alkane gases (C1-C6) under mild conditions (200–250 °C, 20–50 bar H₂). 864-865 In the liquid phase (water, n-hexane etc.), around 90 wt% of HDPE can be converted to liquid hydrocarbons (C8-C38) within 1 h on Ru/C catalysts at 220 °C in the presence of H₂ (30 bar).869

Table 18. Hydrogenolysis of Plastics into Various Hydrocarbons in Batch Reactors.

Catalyst	Polymer	Temperature (°C)	Pressur e (Bar)	Time (h)	Polymer/ Catalyst (Mass)	Products	Ref
Ru/CeO ₂	LDPE, HDPE, PP	200-240	20-60	5-24	34	Liquid fuels, waxes (C5-C45)	862
Ru/TiO ₂	PP	250	30	8-16	20-40	Lubricants (C20-C60), C1-C2 gases	868
Ru/Nb ₂ O ₅	PET, PS, PC	200-320	3-5	12-16	1-2	Aromatic hydrocarbons	863
5Ru/C	PE, LDPE	200-225	20	16	25	Liquid alkanes (C3-C13), light gases (C1-C6)	864
5Ru/C	PP	250	35	8-24	14	Liquid alkanes (C5- C32), light gases(C1-C5)	865
Ru/FAU	LDPE, PP	300-350	50	3	50	Methane, light paraffins (C2-C11)	866
Ru/WO ₃ / ZrO ₂	LDPE	250	30	2	40	Lubricants, waxes, diesel (C4-C35)	867
Ru/C	HDPE	220	30	1	2	Lubricants, liquid fuels (C6-C38)	869
Pt/WO ₃ / ZrO ₂ +Zeolite	LDPE	250	30	2	10	Liquid fuels (C5-C22)	870
Pt/SrTiO ₃	PE	300	12	96	5	Lubricants, waxes (Mw 200- 1000 Da)	871
SiO ₂ /Pt/SiO ₂	HDPE	300	14	24	88	Fuels, lubricants (C8-C32)	872
Pt/C	PP	300	15	24	10	Lubricants (C5-C45)	873

Pt-based catalysts are another class of materials utilized in the hydrogenolysis of plastics. R70-R73 Sadow and coworkers reported that PE can be converted into lubricants and waxes (M_w 200-1000 Da) over platinum supported on strontium titanate or mesoporous shell/Pt/silica at

250-300 °C in the presence of H_2 (10-17 bar). ⁸⁷¹⁻⁸⁷² Moreover, platinum can be supported on carbon which catalyzes the conversion of PP into liquid hydrocarbons (C5-C45)⁸⁷³, or on WO₃/ZrO₂ and mixed with zeolites which catalyzes the production of liquid fuels and short-chain hydrocarbons from PE, PP or PS. ⁸⁷⁰ The synergistic effects between platinum and supports (carbon/metal oxides) or co-catalysts (zeolites) are vital in these processes. Additionally, the hydrogenolysis of plastics can also be carried out over Al_2O_3 or SiO_2 supported transition metals (Cr, Ni, Mo, Co, or Fe)⁸⁷⁴, micro-mesoporous zeolites⁸⁷⁵, and other catalysts⁸⁷⁶ which are not discussed here.

10.2 Functionalization and Reactive Extrusion

Another strategy to valorize plastics is the addition of other chemical groups (e.g., aromatic ring, halogen, carboxylate, carbon-carbon unsaturated bond etc.) to these polymers via chemical methods (e.g., oxidation, halogenation, esterification, metathesis) ⁸⁷⁷⁻⁸⁷⁸ as shown in Figure 41. This approach is typically performed by reactive extrusion in an extruder. The products include polymers with new properties, ⁸⁷⁹ liquid fuels, ⁸⁸⁰ waxes, ⁸⁸¹ and platform molecules. ⁸⁸²

The C-H bonds in PE (HDPE, LDPE, LLDPE) can be oxidized to ketone or hydroxyl groups, which generates functionalized polymers with unique physical properties (e.g., strong adhesion, ability to be painted with common paint etc.). 879 A high-valent ruthenium-oxo catalyst (polyfluorinated ruthenium porphyrin) can be added with 2,6-dichloropyridine N-oxide to form esters from PE at 120 °C. The same complex can catalyze the oxidation of polyisobutene to oxopolyisobutene (Figure 41B) where the catalysts, reaction conditions, and oxidants are vital in selectively oxidizing the methylene positions and avoiding chain cleavage.⁸⁸³ Reactions besides oxidation can be utilized to functionalize the plastics. Kanbur et al. reported that the conversion of polyolefins (PE, PP) to shorter aliphatic alkylaluminium species can be achieved via β-alkyl elimination and heterobimetallic alkyl metathesis using organozirconium catalysts and aluminum reagents at 200 °C.884 The obtained shorter aliphatic alkylaluminium species can be further converted into alkyl alcohols, acids, halides, and hydrocarbons with a quenching process. Crossalkane metathesis can convert PE into liquid fuels and waxes (short-chain linear alkanes) at 175 °C.880 This process consists of three steps: (1) the dehydrogenation of PE and cofed light alkane; (2) the metathesis of olefins; (3) the hydrogenation of the obtained olefins. An iridium complex can catalyze Steps 1 and 3 while Re₂O₇/γ-Al₂O₃ catalyzes the olefin metathesis. The catalysts are compatible with various polymer additives and product distribution can be manipulated by the catalyst structure and reaction time.

Functionalized polymers can also be produced by dehydrogenation, sulfonylation, and amination. Zinc sulfide is active in PP dehydrogenation which enables simultaneous C-C cleavage, ring closure, and dehydrogenation of PE via controlled by produced by chlorosulfonic acid, further produced by this process can be sulfonated by chlorosulfonic acid, fuming/concentrated sulfuric acid, sulfur trioxide, and acetyl sulfate $^{887-890}$. Tian et al. reported that Ru/TiO2 can catalyze the amination of ether groups in PLA in ammonia solution at 140 °C (Figure 41C). 882 Alanine can be produced by this process with high selectivity in the absence of hydrogen. In most of the cases, other chemicals (e.g., light alkanes, water, halogens) need to be cofed for the functionalization of the waste plastics. However, the cofed species is not necessary if the carbon and hydrogen in the polymers can be utilized. One approach is to partially depolymerize the plastics. Long-chain alkylaromatics (ca. C30) can be produced from PE via controlled depolymerization on Pt/γ -Al2O3 without solvent or H2 at 280 °C 881 . This process couples exothermic hydrogenolysis and endothermic aromatization which enables simultaneous C-C cleavage, ring closure, and dehydrogenation under mild conditions (280 °C).

Reactive extrusion is a commercially practiced approach to install functionality of plastics. ⁸⁹¹ One example is the radical-mediated addition of maleic anhydride to PE and PP. ⁸⁹² One key step in reactive extrusion is the production of a pair of radicals which can be achieved through heating or photolysis of the reagent. One of the radicals cleaves a C-H bond in plastics and chain transfer step can functionalize plastics (Figure 41D). Thiocarbonyl amide reagent has been utilized to functionalize branched polyolefins. ⁸⁹³ The authors demonstrated that this metal-free C-H functionalization of isotactic PP can be performed on a decagram scale forming polymers with improved adhesion to polar substrates. Recently, another study demonstrated that an ideal reagent (e.g., O-alkenylhydroxamate) enables slow chain transfer kinetics which provides various functionality to the backbone of plastics by other radical sources. ⁸⁹⁴

The functionalization of waste polymers is being commercialized (e.g., Novoloop⁸⁹⁵). The company can recycle waste LDPE, HDPE, and LLDPE. Those PE wastes are shredded, cleaned, and fed into a patented, accelerated thermal oxidative decomposition (ATOD), reactor (Figure 42).⁸⁹⁵⁻⁸⁹⁶ The treated PE is then heated to a temperature range from 60 to 200 °C, and oxidized into dicarboxylic acid monomers by a group of oxidation agents including oxygen, nitrous oxide, nitric oxide, and aqueous nitric acid.⁸⁹⁷ The oxidized monomers are used to produce thermoplastic polyurethane (TPU).

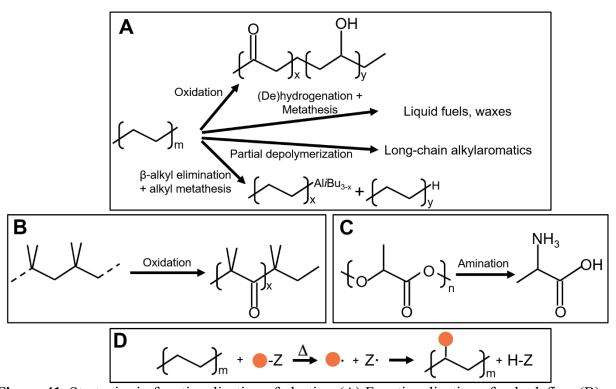


Figure 41. Strategies in functionalization of plastics: (A) Functionalization of polyolefins; (B) oxidation of polyisobutene; (C) PLA amination; (D) reactive extrusion.

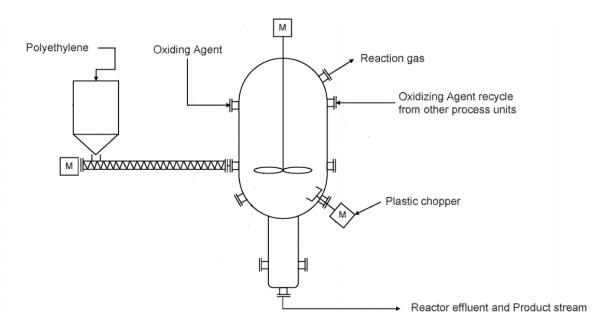


Figure 42. The scheme of the ATOD reactor. Published with permission from ref ⁸⁹⁷.

Plastic alloys are a type of functionalize plastic where different plastic materials are functionalized to create a single plastic phase. The properties of the plastic alloy can be tuned by adding other materials (e.g., waste fibers) which enables applications of plastic alloys in automotive, electrical & electronics, construction, home appliances, and healthcare equipment. The advantages of plastic alloying are short reaction times, no need for solvents, and low operating/capital costs compared with other plastic technologies like gasification. The solvents are functionally depicted by the solvents are solvents.

Plastic alloying can introduce long chain branching of the polymer backbone to improve the properties (e.g. melt strength) of plastics. This approach has been used for functionalization of PP, 904 PE, 905 and polyhydroxybutyrate (PHB). 901 Long chain branching can be added using peroxides, which can result in increases in melt elasticity. 903 Long chain branching can alter physical properties such as the crystallinity and transition temperatures. 906 The thermophysical properties including crystallinity, melting behavior and tensile properties of HDPE were shown to be influenced by di-tert butyl cumyl peroxide induced cross-linking. 905 Dicumyl peroxide (DCP)-induced cross-linking in PE improves the melt strength and is dependent on peroxide concentration. 907 The lifetime of the peroxide formed from DCP is relatively close to the residence time of extrusion. The generally accepted process of peroxide induced cross-linking of polymers follows three key steps 908:

(1) the primary radical formation from the thermal decomposition of peroxide,

 $RO - OR \rightarrow 2RO \bullet (Primary Radicals)$

(2) H abstraction from polymer backbone by free radicals of peroxide generated in step (1),

 $RO \bullet + P \text{ (polymer)} \rightarrow P \bullet \text{ (polymer radical)} + ROH$

(3) the bimolecular radical recombination of polymer radicals from step (2) to generate C-C crosslinks.

$2P \bullet \rightarrow P - P \text{ (crosslinking)}$

There is limited information on the chemical position(s) associated with cross-linked molecular chains to form a gel network structure. Long chain branching increases the plastic molar mass,

polydispersity, melt strength and strain hardening in PP. 904 One key step in plastic alloying is C-H activation which can be achieved by different routes. 2

Plastic alloying has been explained by inter-linking and interfacial adhesion between different polymers. Wigotsky pointed out the importance of plastic alloying to the plastic industry because of the improved physical properties of the alloys. 899 The compatibilizing agents in plastics acts as polymeric surfactants which lowers surface tension and promotes interfacial adhesion between polymer phases in plastic alloys. 909 In addition to this, PP functionalization (i.e., carboxylation) generates compatibilizers which can be used to produce plastic alloys. 910 Sakai reported a processing technology which can improve compatibility of plastic and produce plastic alloys using twin-screw extruders. 911 Asay et al. reported that PVC can be utilized to produce plastic alloys because of the varied degree of miscibility between PVC and a wide range of polymers. 912-913 Composite materials with improved properties can be obtained via addition of other materials. Kimura showed significant improvement in tensile strength by adding fillers to polyolefins.⁹¹⁴ Amor et al. studied the improvements of properties of PLA with biomass, demonstrating synergetic effect of small addition of PLA on the thermo-mechanical properties.⁹¹⁵ The above studies portray the importance of plastic alloying for the production of plastic and composite material products. However, these studies were all conducted with pure polymers by mixing two or three components. Aumnate et al. were the first to recognize that plastic waste could be also alloyed.⁸⁹⁸ In their fundamental study, they simulated plastic wastes by mixing pure components of LDPE and HDPE with PP and showed the effects of the branching of PEs on mechanical properties and crystallization behavior.

Another plastic alloying approach is the "grafting onto" method which grafts the PHB polymer onto cellulose fibers through plastic alloying processing with the use of a small amount of DCP. 901, 903 LDPE has also been shown to graft onto cellulose fibers, retaining the stiffness of cellulose and the flexibility of polymer matrix. 916 When the peroxide is exposed to heat during extrusion, it will decompose into strong free radicals which tend to abstract H's from the polymer and cellulose molecular chains and initiate the grafting between the two phases in composites.

10.3 Microwave-Assisted Conversion

Microwave radiation can be applied during catalysis to heat the reaction system, shorten reaction times, and enhance the kinetics of some chemical reactions. In conventional thermal heating processes, the whole reaction system (catalysts, reactor, diluent, feedstock etc.) are heated while microwave radiation enables the electromagnetic energy to be absorbed evenly and efficiently at the microwave-adsorbing points (e.g., catalyst surface) Furthermore, other researchers propose that the microwaves likely have intrinsic catalytic effects or assist in lowering the activation energy of the reactions.

Microwave-assisted depolymerization and catalytic upgrading can be separated by the reactor system. ^{490, 921} In microwave-assisted pyrolysis, LDPE is depolymerized into pyrolysis vapor and the microwave absorbent (e.g., SiC) enables even heating of the feedstock which promotes the formation of light olefins. ⁴⁹⁰ The products are then catalyzed by MgO to produce more valuable chemicals (i.e., aromatics, C₁₂₊ hydrocarbons) in a subsequent reactor. This process can be modified by changing the microwave absorbent to NiO and the catalyst in the separated reactor to HY zeolite which enhances the production of olefins in the pyrolysis zone and produces gasoline fuel with high yield as well as appropriate carbon number. ⁹²¹ Microwave-assisted conversion can also be performed with catalysts in the liquid phase. ⁹²²⁻⁹²³ LDPE powder can be completely degraded in 1 h of microwave irradiation at 180 °C in the presence of dilute nitric acid solution (0.1 g/mL). ⁹²² In this process, water is used to absorb microwave energy and nitric acid

catalyzes the oxidation of LDPE towards dicarboxylic acids (e.g., malonic acid, succinic acid, glutaric acid etc.). Bäckström et al. 923 pointed out that HDPE can be converted to dicarboxylic acids with a similar approach and the obtained products can then be utilized to synthesize plasticizers. Addition of the plasticizer to PLA improves the physical properties of the polymers. Much faster degradation can be achieved via microwave-assisted conversion combined with appropriate catalysts. Jie and coworkers 18 reported that pulverized plastics (HDPE, LDPE, PP, PS) can be deconstructed into hydrogen and high-value carbon materials (e.g., carbon nanotubes) in 30-90 s. FeAlO_x plays a significant role in this process by both efficiently absorbing microwave energy, which initiates the physical heating process and by catalyzing the depolymerization of the plastics.

Additionally, continuous processing and cofeeding of biomass can be applied to microwave-assisted conversion of plastics. Zhou et al. 924 reported a continuous microwave-assisted pyrolysis system which can convert HDPE and PP to gasoline-range hydrocarbons rich in aromatic hydrocarbons. The system consists of microwave heating with a SiC mixing-ball-bed and a secondary catalyst bed with ZSM-5 and can process up to 10 kg of plastics an hour with 89.6% energy efficiency. Considering the oxygen deficiency of polyolefins, it can be used as a hydrogen source to be co-processed with hydrogen-deficient biomass via microwave heating, thus improving the quality of the bio-oil. 925-926 Zeolites and metal oxides as well as the combination of these two materials have been reported to catalyze the production of hydrocarbons from the mixture of LDPE and lignin where microwave-assisted heating is vital in achieving even and efficient internal heating.

11.0 Conclusions and Outlook

Compared to other engineered materials (i.e., glass, metal, paper etc.), plastics are lightweight and can be easily manufactured into products for a variety of applications. Generation of plastic waste and the ratio of waste plastics in MSW have increased due to the growth of plastic production. Recycling of plastics is still far behind where it needs to be for a circular plastics economy, but improved technology is continuously being developed to efficiently increase the lifetime of plastics.

11.1 Collecting and Sorting of Waste Plastics

The first step in any plastic recycling involves collecting and separating the plastics. There is an opportunity to divert more material from landfills through an upgrade in the recycling infrastructure. This can be achieved by an increase in the number of facilities, such as MRFs, or by improving process efficiency along the recycling process, such as improved sorting by adding more optical sorters. However, this will result in additional capital costs for MRFs. Education and outreach regarding recycling is also critical, as consumers need to learn the environmental, social, and economic benefits of recycling.

The operation of a MRF presents multiple challenges. One is the difficulty in finding personnel. The lack of predictability of the inbound stream, as each week, the received material can fluctuate according to holidays. For example, in the period of the year close to the Thanksgiving and Christmas holidays, there is an increase in food containers (from dinner parties) and fibers (ads from the shopping season). In terms of the materials collected, some MRFs view the presence of full-body shrink sleeve labels on PET bottles and aluminum cans as a challenge, as it affects the recyclability of two significant sources of income (PET and aluminum). Other challenges include the presence of films and flexible packaging, shredded paper, and packaging with mixed types of material (e.g., plastic bottles with metal closures)⁹²⁷.

Increased contamination of the waste material stream is also an issue, especially with material collected from areas not used to having recycling programs, which often have less awareness of the waste sorting procedures. For example, lithium batteries are a growing concern due to the danger of starting fires, with 68 incidents reported in MRFs between 2013 and 2020. 928-929 The challenges associated with the presence of contaminants in the bales could result in lower yields per bale, showing an opportunity to improve bale quality. Such measures would include an increase in sortation efficiency by adding more optical sorters, expansion of recycling education to reduce contamination in inbound streams, or even construction of new MRFs.

In developing countries, the waste pickers also need support. The main needs of waste pickers include improving their working conditions, learning to manage their family needs, receiving education and training, preventing violence and guidance to reduce teenage pregnancies, alcoholism and drug addiction, and training to "produce something" from the waste that gives them more income. Some actions that would lead to fair living wage waste picking jobs include: a) develop strategies for precise censuses of waste picker communities and to have dynamic updates of this information; b) integrate waste pickers in the recycling value chain; c) harmonize recycling strategies with frontier technologies and train the waste pickers; d) develop innovative business models for MSW management with a social perspective, e) update and enforce the legal and regulatory framework of recycling value chains in compliance with human rights of waste pickers, f) integrate and establish social programs for waste pickers, from public, private, local, and international organizations.

11.2 Mechanical Recycling of Waste Plastics

Mechanical recycling works well for a very homogeneous plastic stream like HDPE milk bottles. However, contamination and other plastics decrease the quality of the plastics produced during mechanical recycling. Some plastics cannot undergo mechanical recycling or do not flow upon heating after cure (thermosets) as they cannot tolerate thermal treatment. Multi-layered plastic products (i.e., juice bottles) cannot be mechanically recycled. These multi-layered packaging materials are more challenging to recycle as each plastic in a different layer has a different melting temperature, and different plastics are often immiscible which makes them practically non-recyclable. Colored plastic products, for example, PET containers with carbon black in them, are not detected by the sensors during the sorting stage of recycling and complicate the recycling process. Films produce a low quality product during mechanical recycling.

11.3 Pyrolysis, Liquefaction, and Gasification of Waste Plastics

Pyrolysis, liquefaction and gasification have the advantage of being able to process mixtures of plastics and more easily dealing with contamination than mechanical recycling. Several plastic pyrolysis approaches are being commercialized. Catalytic pyrolysis is used to increase the product selectivity. 933

Despite continuing advancement of the technology, commercialization of plastics pyrolysis faces significant challenges which can be addressed by further research. Better understanding of the complex reaction mechanisms controlling depolymerization of plastics could improve selectivity to desired produce molecules. Novel approaches to process intensification will be important to overcome the combination of relatively modest chemical reaction rates and heat and mass transfer limitations that characterize many pyrolysis processes. Using process intensification to achieve economies of scale, determining optimal reactor and process conditions, and securing consistent feedstock streams will increase the profitability of pyrolysis plants. In addition to this, the reactors used in pyrolysis need to be well designed to enable efficient mass and heat transfer.

Liquefaction is another technology currently being commercialized. The major challenges of liquefaction are high costs related to the equipment and operation conditions. Supercritical HTL also increases reactor corrosion. Enabling a high feedstock mass loading in the solvent without significantly affecting liquefaction efficiency is also critical, as it is less efficient to heat a large amount of solvent and convert only a small amount of plastic waste. According to Licella, feedstock loading must be sufficiently high (i.e., 70%) for their Cat-HTR process to be economical. Developing an improved conversion strategy to produce higher quality products with minimal required upgrading is also essential. While lab studies indicate that feedstock compositions and reaction conditions strongly impact liquefaction product yield and quality, fewer studies discuss cross-interactions among different plastics. There is also a lack of information about the fate of contaminants and pollutants during liquefaction. HTL of polymers also promotes oxidative reactions, which become more noticeable under supercritical conditions. The effect of oxygenated compounds on the direct use of the crude oil or during subsequent upgrading should be addressed in future studies.

Gasification of MSW shares similar challenges and opportunities as other fossil-based gasification technologies, primarily associated with the high capital cost of gasification. Converting synthetic gas to heat and power produces energy that competes with the declining costs of solar and wind power generation which are now less than \$0.04/kWh.⁹³⁴ Pursuing higher-value chemicals such as ethylene which is valued at more than \$1000 per metric ton⁹³⁵ is possible but requires several catalytic steps (methanol synthesis and methanol to olefins). The varying composition of waste plastic streams presents an additional operational and management challenge for recycling facilities. An incentive program tailored to reduce the risk of economic losses due to market price volatility could serve as a complement or alternative to environmental regulations. Waste reduction policies and incentive programs will likely spur the development of waste gasification facilities.⁹³⁶

11.4 Dissolution-Based Approaches for Waste Plastics

Dissolution-based plastic recycling approaches can have advantages over other recycling technologies as they produce the virgin resins. Proper solvent selection for specific types of plastic waste is the key to the feasibility of dissolution-based plastic recycling. Many solvent systems for common polymers have been disclosed in the literature and in patents by different companies. However, when considering more complicated plastic waste feedstocks, advanced thermodynamic computational tools are a means to expedite the development and design of these processes. The recycled materials obtained via dissolution/precipitation methods could be economically competitive with virgin resins, showing the capability of these approaches to reduce plastic waste. These techniques can also be applied to complex multicomponent input streams (e.g., multilayer films) which are challenging for current mechanical recycling technologies.

Several challenges remain in the design of dissolution-based recycling techniques that merit future study. The use of large amounts of solvent in these processes poses potential challenges associated with toxicity and energy consumption. To address these concerns, methods for solvent selection based on polymer solubility can be combined with technoeconomic and life cycle analysis techniques to assess tradeoffs in solvent selection. Another challenge is the removal of potential contaminants (e.g., residual inks or retained solvent) from the recovered polymers. The kinetics of dissolution also could hinder dissolution-based recycling for large

amounts of plastic waste. 608, 650 These challenges could be addressed through additional processing steps for contaminant removal or mechanical shredding prior to dissolution; such steps will require further investigation. Finally, there are opportunities to explore the integration of dissolution-based techniques with liquid-phase chemical recycling techniques. 668, 940 For example, selective dissolution could be used to separate target polymers from mixed plastic waste prior to their chemical depolymerization, thereby mimicking pretreatment methods utilized in biomass conversion. In this context, solvents could be selected to promote both polymer solubility and desired reaction outcomes.

11.5 Chemical Recycling Approaches for Polyesters and Other Plastics

New chemical recycling processes centered around catalysis are emerging. PET can be depolymerized via many different routes generating chemicals to produce rPET or other commodities (Figure 28). For the hydrogenolysis of waste plastics, the product distribution can be tuned by adjusting the residence time, catalyst to polymer mass ratio, temperature, and H₂ pressure etc. Detailed reaction mechanisms for the hydrogenolysis of plastics should be elucidated to provide structure-function relationships at the molecular/atomic level which will provide insights in the rational design of new catalysts with improved efficiency or cheaper metal centers. The products from hydrogenolysis are mainly paraffins and light gases. Converting these back into plastics would involve dehydrogenation followed by steam cracking or another type of processing. The cost of H₂ and safety issues related to its use are major concerns in the industrialization of such processes. Continuous flow of feedstocks with uniform properties might be challenging due to the solid state of waste plastics. It would be ideal to design techniques which enable continuous feedstock flow with high polymer/catalyst ratio and short reaction times. Furthermore, noble metal centers are likely to be poisoned by the impurities in the feedstock, which also needs to be considered in the development of catalytic materials and processes for waste plastics hydrogenolysis.

In the functionalization of plastics, product selectivity and atom efficiency are two challenges since side reactions (e.g., undesired chain cleavage, over-functionalized etc.) easily occur under reaction conditions and an excess of reactant is often required to provide the functional groups. The impurities in waste plastics likely lead to contaminated products or poison the catalysts, which should also be considered in developing these techniques. The removal of impurities in feedstocks needs significant effort in the sortation and pretreatment of waste plastics. Instead, virgin plastic resin can be utilized to manufacture some of the functionalized polymers. Besides, some of the processes need long reaction times (i.e., up to 4 days), which needs to be addressed in scaling up the techniques. Plastic alloying has several advantages compared to other recycling technologies. The key advantages include: (1) little sorting is needed prior to forming the plastic alloys; (2) every type of plastics (#1-#7) can be recycled via this approach; (3) less manpower is needed to operate a plastic alloy facility compared to a MRF and the secondary recycling facility. Compared to pyrolysis of waste plastics, the advantages are: (1) higher ratio of the mixed plastic waste stream can be recycled; (2) fewer numbers of steps are required which results in lower capital/operating costs; and (3) higher value materials than a plastic oil can be produced. More work on this technology is needed to understand if it can be applied to real plastic waste feedstocks, understand the relationships between the catalysts/additives and identify the properties of the plastic alloys, as well as the desirable properties of the plastic alloys.

The removal of impurities in the feedstock is also one of the challenges in microwave-assisted conversion. The impurities that can absorb microwave energy likely lead to varied local temperature, which then results in wide product distribution. Accurate parameters (i.e., microwave

power, radiation intensity, magnetic permeability etc.) need to be standardized for the development of this technique. The capital cost and energy efficiency should also be considered in scaling up microwave-assisted techniques for plastic recycling. As for the biocatalytic processes, it is important to standardize and improve the efficiency of the isolation procedure for microbial species which contain plastic degrading enzymes so that pure breeding colonies of these microorganisms can be quickly screened. Enzyme production from pure colonies can be boosted by standardizing the initial step, which enhances the overall performance of biocatalytic plastic degradation.

Overall, enhancing plastic recycling requires focused efforts, particularly in chemical recycling technologies. Efficient approaches to process waste plastics need to be developed to decrease plastic waste and pollution.

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Conflict of interests

The authors declare conflict of interest.

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