

Rate of Uranium Release from Calcium Meta-Autunite: Effect of Bicarbonate Solutions on the Dissolution

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Overview

- Introduction
- Materials & Methods
 - Autunite Specimens
 - SPFT
 - Quantification of Dissolution Rate
 - Groundwater Modeling
- Results & Discussion
- Conclusions



Introduction

- DOE Hanford Site groundwater plume is contaminated with **uranium**
- A total of 58,967 kg of uranium was release due to leakages from underground storage tanks
- Injection of **soluble sodium polyphosphate** proved to be effective remediation solution
 - Polyphosphate forms insoluble uranyl-phosphate mineral, **autunite**, $X_{1-2}[(UO_2)(PO_4)]_{2-1} \cdot nH_2O$
 - In Ca- rich environments, Ca replaces Na and the exchange takes place rapidly into Ca-autunite



Introduction

- **Carbonate** is a major ion in the groundwater at Hanford Site (**1.2-2.71mM**)
- **Uranyl ion** (UO_2^{+2}) forms soluble uranyl-carbonate complexes, making uranium **mobile**
- Major uranyl-carbonate complexes are **$\text{UO}_2(\text{CO}_3)_2^{-2}$** and **$\text{UO}_2(\text{CO}_3)_3^{-4}$**
- Previous research on uranium release from the dissolution of autunite is **limited to pH and temperature**



Objective

- Quantify the rate of uranium release from autunite in following conditions
 - Bicarbonate: 0.5-3.0 mM
 - pH: 7-11
 - Temperature: 23 - 90°C



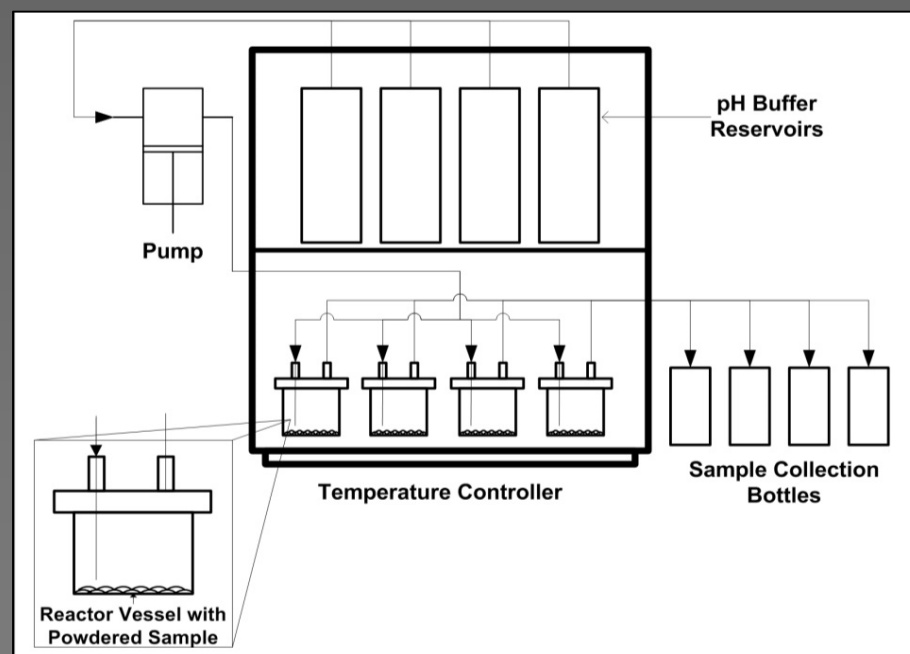
Materials and Methods

- **Natural Ca-autunite** was obtained from Excalibur Mineral Corporation
- Characterized via ICP-OES, ICP-MS, XRD, SEM-EDS and confirmed to be **99% pure** (Wellman et al., 2006)
- Sample size: **75 to 150 μm**
- Surface area: **0.88 $\text{m}^2 \text{g}^{-1}$**



Single-Pass Flow-Through (SPFT)

- SPFT experiments were designed to measure forward rate under tightly controlled conditions.
- 0.25 grams of autunite
- 0.5-3.0 mM of HCO_3^- and 0.01 M TRIS
- HNO_3 and LiOH
- KPA and ICP-OES





Dissolution Rate Quantification

$$R_i = (C_i - C_{ib}) \frac{q}{f_i S}$$

- R_i = normalized dissolution rate for element i ($\text{mol m}^{-2} \text{s}^{-1}$)
- q = flow rate (L d^{-1})
- C_i = concentration of component i in the effluent (g L^{-1})
- C_{ib} = mean background concentration of component i (g L^{-1})
- f_i = mass fraction of the element in the metal (dimensionless)
- S = surface area of the sample (m^2)



Groundwater Modeling

- Steady state concentrations were used to identify predominant uranium species
- **Visual MINTEQ 3.0** was used for speciation modeling
- Thermodynamic database was updated with
 - Nuclear Energy Agency's thermodynamic database for uranium (Guillaumont et al., 2003)
 - calcium-uranyl-carbonate complexes (Dong and Brooks, 2006)
 - becquerelite (Gorman-Lewis et al. 2008)



Results

- Influence of bicarbonate on the dissolution of Ca-autunite was experimentally determined using $\log (r) = \log (k) + \eta \log [\text{HCO}_3^-]$
 - r is dissolution rate, k is intrinsic rate constant and η is power law coefficient
- Non-linear regression was performed at each temperature, slope of rate vs concentration provided power law coefficient



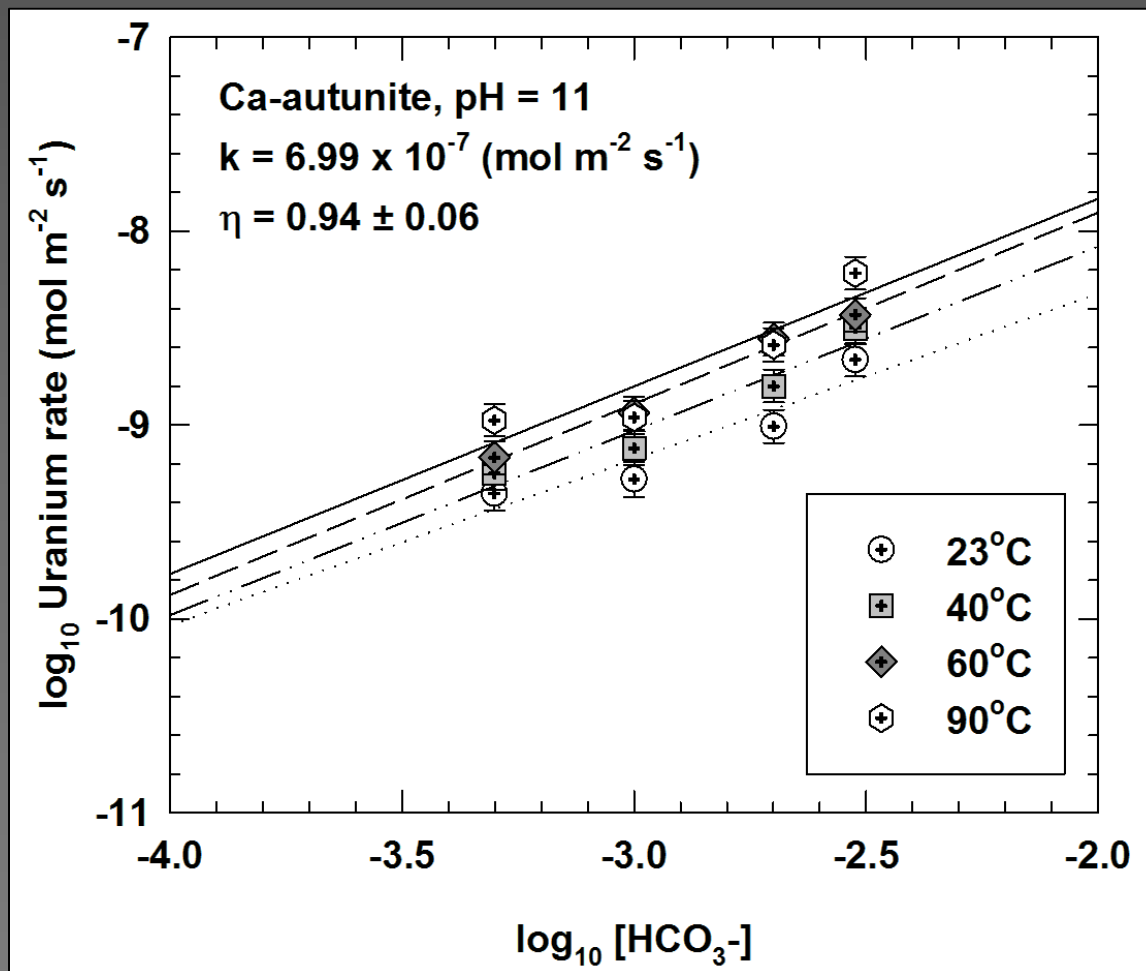
Results

- Dissolution showed strong influence on pH

pH	Ca-autunite		
	η	$k \text{ (mol m}^{-2} \text{ s}^{-1}\text{)}$	Increase compared to pH 7
7	0.50 ± 0.12	1.09×10^{-09}	-
8	0.52 ± 0.10	3.15×10^{-09}	17
9	0.79 ± 0.08	5.60×10^{-08}	65
10	1.09 ± 0.11	1.58×10^{-06}	392
11	0.94 ± 0.06	6.99×10^{-07}	434



Results





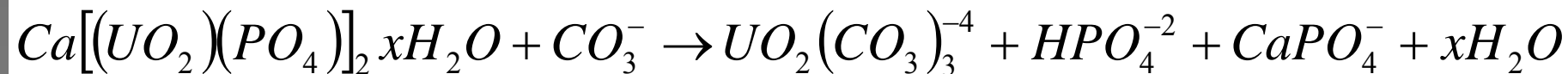
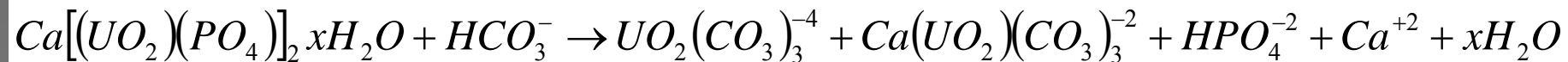
Results - Geochemical Modeling

pH	HCO ₃ ⁻ (M)	Schoepite	β- UO ₂ (OH) ₂	Hydroxyapatite	β- Ca ₃ (PO ₄) ₂	Ca ₃ (PO ₄) ₂ (am2)	Ca ₃ (PO ₄) ₂ (am1)	Ca ₄ H(PO ₄) ₃ ·3H ₂ O(s)	(UO ₂) ₃ (PO ₄) ₂ (s)
7	0.0005	0.057	-0.173						2.904
	0.001	-0.179	-0.409						2.275
	0.002	-0.528	-0.757						1.856
	0.003	-0.758	-0.988						1.587
8	0.0005	0.335	0.106	-0.942					0.98
	0.001	0.011	-0.219	0.575					0.5
	0.002	-0.471	-0.7	2.898					-0.232
	0.003	-0.741	-0.971	3.275					-0.378
9	0.0005	0.586	0.356	6.386	-0.69	-1.526	-4.285	-3.248	-1.078
	0.001	0.361	0.132	6.915	-0.323	-1.16	-3.918	-2.678	-1.261
	0.002	0.034	-0.196	8.487	0.669	-0.168	-2.926	-1.275	-1.757
	0.003	-0.584	-0.814	8.716	0.845	0.008	-2.75	-0.975	-3.227
10	0.0005	0.652	0.422	14.551	3.928	3.091	0.333	2.44	-3.695
	0.001	0.607	0.377	13.598	3.376	2.539	-0.219	1.737	-3.63
	0.002	0.344	0.114	12.11	2.512	1.675	-1.083	0.632	-4.136
	0.003	-0.991	-1.221	11.935	2.393	1.557	-1.202	0.453	-8.272
11	0.0005	0.265	0.035	15.229	3.923	3.087	0.328	1.749	-8.966
	0.001	0.215	-0.015	14.877	3.717	2.88	0.122	1.482	-9.068
	0.002	0.055	-0.175	14.381	3.431	2.594	-0.164	1.118	-9.437
	0.003	-0.333	-0.563	14.155	3.284	2.447	-0.311	0.903	-10.717



Results - Geochemical Modeling

- Predominant species
 - $UO_2(CO_3)_3^{-4}$
 - $H_2PO_4^{-2}$
 - Ca^{2+} (pH 7), $CaUO_2(CO_3)_3^{-2}$ (pH 8-10), $CaPO_4$ (pH 11)





Results - Activation Energy

- Describes the nature of the reaction, < 20 kJ/mol

surface dif

pH	[HCO ₃ ⁻] (mM)			
	0.5	1.0	2.0	3.0
7	21.87	26.39	27.72	26.00
8	22.41	20.72	15.57	13.95
9	2.63	13.07	8.95	7.32
10	8.17	16.68	15.05	15.17
11	11.39	10.19	12.23	11.78

on

- pH has not

- Modified T

$$\ln r = \ln I$$

- Average ac

- Rate contr

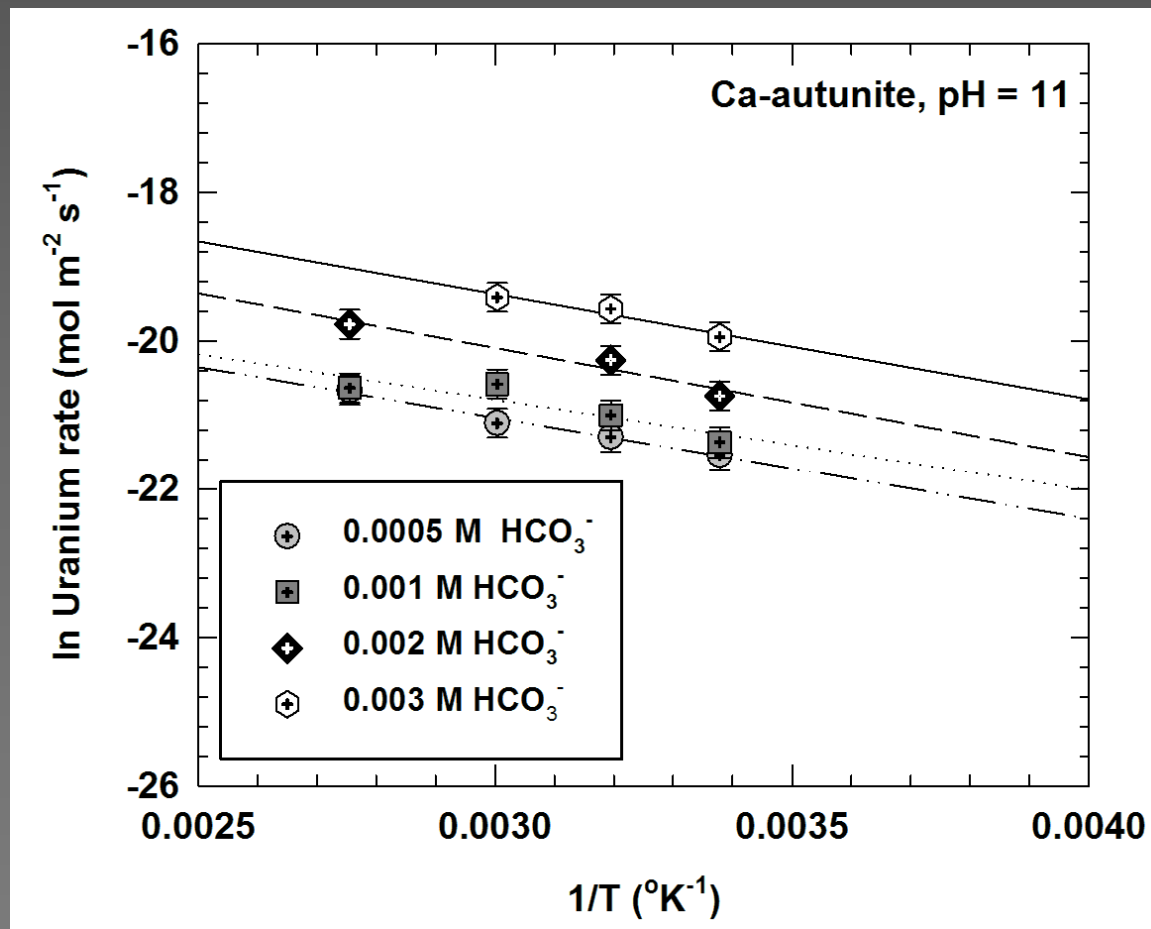
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– Surface bond-breaking @ pH 7

– Rate limiting mass transfer @ pH >=8



Results - Activation Energy





Results - Pseudo Equilibrium and Enthalpy

$$r = K_g [HCO_3^-]$$

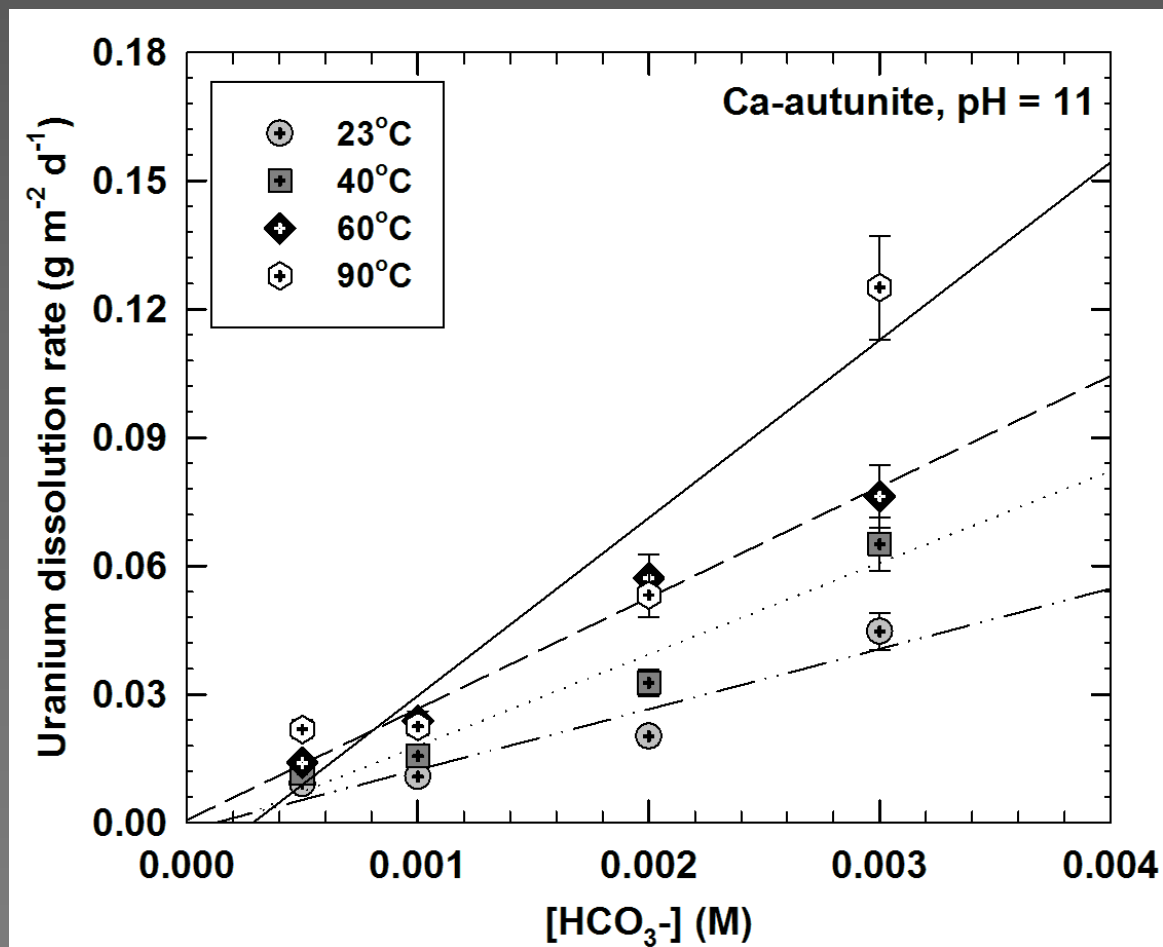
$$\Delta H = -RT \ln K_g$$

pH	Ca-autunite	
	K_g	ΔH
7	0.65	28.58
8	0.79	11.83
9	4.20	11.90
10	25.97	15.88
11	27.75	13.84

- Reaction is **slow at low pH** and significantly **fast at high pH**
- Enthalpy data is not significant to justify the uranium release mechanism but **correlates to the intrinsic rate (k)**

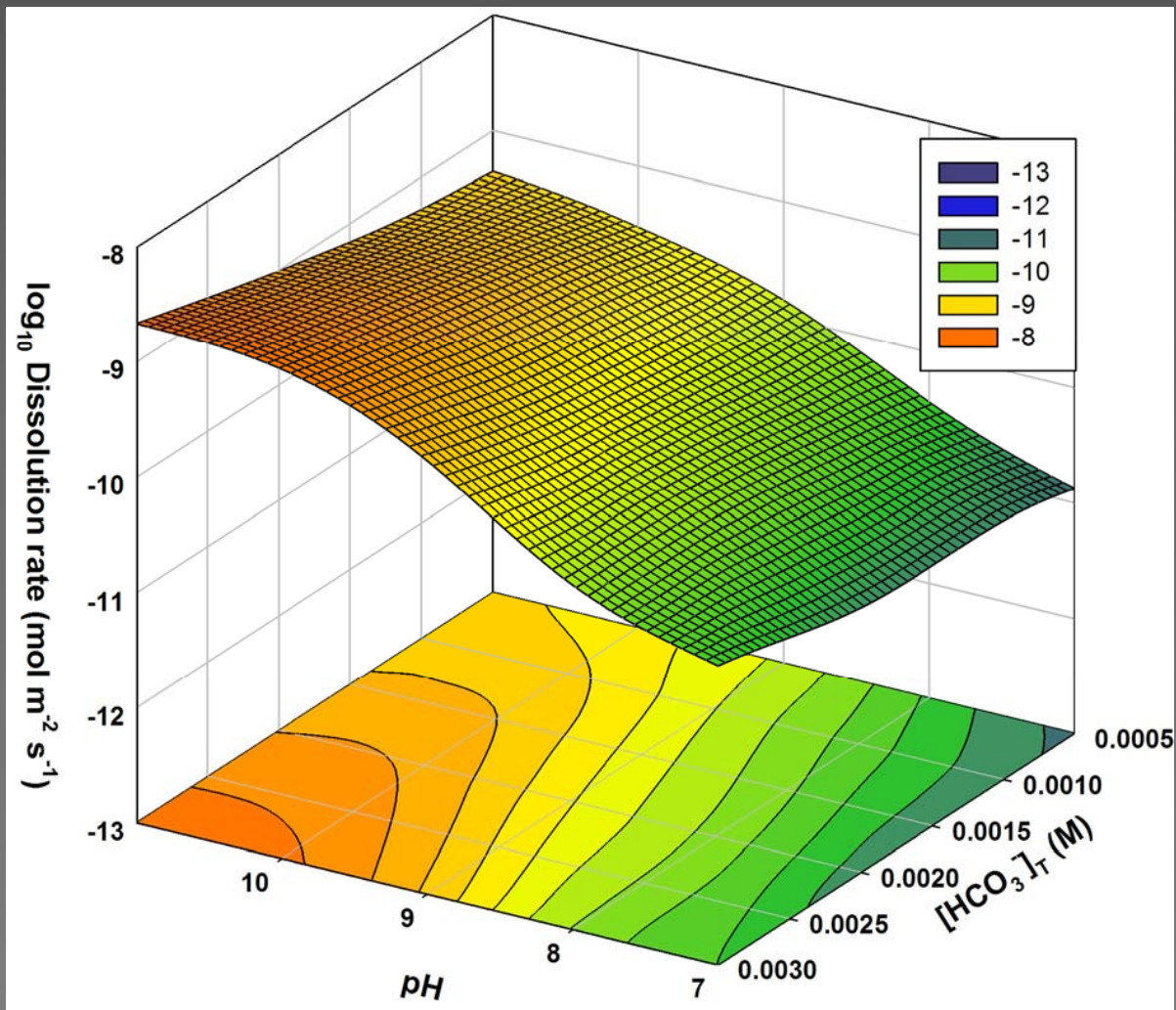


Results - Pseudo Equilibrium and Enthalpy





Results - 3D





Conclusions

- Power law coefficient is 0.5-1.0, no finite dependency on temperature
- Dissolution is slower at pH 7 and faster at pH 8 and beyond
- Dissolution data indicate **low concentration** of bicarbonate can **impact the stability** of autunite
- Data is being incorporated into modeling at Hanford Site



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