

SCALE: 1" = 2000

# **PROPERTY OWNERS LIST**

BLOCK & LOT	NAME	ADDRESS	CITY, STATE, ZIP
	NAVAL AIR	CODE CNI 01L	LAKEHURST NJ
	ENGINEERING		08733
	STATION -		
	COMMANDING		
	OFFICER COMCAST	830 RT 37 WEST	TOMS RIVER NJ
	COMCASI	050 KI 57 WEST	08755
	VERIZON ENG	PO BOX 152206	IRVING TX 75015
	DEPT		
	GPU	400 LINCOLN ST	PHILLIPSBURG NJ 08865
	MANCHESTER	1 COLONIAL DR	MANCHESTER NJ
	TWP CLERKS		08759
	OFFICE	C31.404	
	NJ DEP NJ DOT	CN 401 RT 79 & DANIELS	TRENTON NJ 08625 FREEHOLD NJ 0772
	INJ DOT	WAY	TREEHOLD NJ 0772
	NJ NATURAL GAS	PO BOX 1464	WALL NJ 07719
	CO	DO DOM D	DAMULE NI 0073
	OCEAN COUNTY MUA	PO BOX P	BAYVILLE NJ 0872
	OCEAN COUNTY	119 HOOPER AVE	TOMS RIVER NJ
B 64 – L 3.01	ROAD DEPT KIARI & EMBERLE	3808 RIDGE AVE	08753 MANCHESTER NJ
	PEARSON		08759
B 64 – L 6	PATRICIA GIORDANO	3134 HWY 547	MANCHESTER NJ 08759
B 64 – L 7	ROBERT J III & R J	224 EDGEMERE DR	TOMS RIVER NJ
	JR BLANK		08755
B 65 – L 1	RUSSELL DECKER	3163 RIDGEWAY AVE	MANCHESTER NJ
	& JOYCE H BLACKWELL		08759
B 65 – L 2	JAMES & FAITH	3153 RIDGEWAY AVE	MANCHESTER NJ
B 65 – L 4	JOHNS CYNTHIA S SEARS	3143 RIDGEWAY AVE	08759 MANCHESTER NJ
B 03 – L 4	CINIHIA 5 SEAKS	5145 KIDGEWATAVE	08759
B 65 – L 5	KARL E &	3133 RIDGEWAY AVE	MANCHESTER NJ
	VICTORIA		08759
B 65 – L 6	KOVACOFSKY CHARLES &	3099 RIDGEWAY AVE	MANCHESTER NJ
D 05 - L 0	MICHELE KOVACS		08759
B 65 – L 7.01	ORIETT S WTDV	3083 RIDGEWAY AVE	MANCHESTER NJ
B 65 – L 7.02	MARCUS	3087 RIDGEWAY AVE	08759 MANCHESTER NJ
B 03 – L 7.02	JOHN L JR & ERIKA M	5087 KIDGEWAY AVE	08759
B 65 – L 9	PROVEAUX GERARD R HEALY	3738 RIDGEWAY AVE	MANCHESTER NJ
			08759
B 65 – L 10	FRANK BARTH	3776 RIDGEWAY AVE	MANCHESTER NJ 08759
B 65 – L 11	PARKWOOD	305 MAIN ST	LAKEWOOD NJ
	SQUARE LP		08701
B 65 – L 12	PAKRWOOD	305 MAIN ST	LAKEWOOD NJ
B 65 – L 13	SQAURE LP PARKWOOD	305 MAIN ST	08701 LAKEWOOD NJ
	SQUARE LP		08701
B 65 – L 14	PARKWOOD	305 MAIN ST	LAKEWOOD NJ
	SQUARE LP &		08701
	PARKWOOD CTR B		
B 65 – L 15	D CARLOS &	3123 RIDGEWAY AVE	MANCHESTER NJ
	MONICA		08759
	ARTEAGA		
B 66 – L 2	LAKEWOOD	305 MAIN ST	LAKEWOOD NJ
	INVESTMENTS LLC		08701
B 67.01 – L 1.01	MANCHESTER	1 COLONIAL DR	MANCHESTER NJ
2 0 VI B I.VI	TWP		08759
B 67.06 – L 5	JAMES WALL	390 TOMS RIVER RD	JACKSON NJ 08527
B 67.07 – L 10	HARTMUT &	3857 RIDGE AVE	MANCHESTER NJ
	JOANN		08759
B 69 – L 4	HUEBSCHER TARANTINO	3875 RIDGEWAY AVE	MANCHESTER NJ
ש טא – ב 4	PROPERTIES LLC	JOIJ NIDUEWAYAVE	08759
B 71 – L 1.01	OCEAN COUNTY	101 HOOPER AVE	TOMS RIVER NJ
B 71 – L 1.02	OCEAN COUNTY	101 HOOPER AVE	08753 TOMS RIVER NJ
B71 - L 6.01			08753
	OCEAN COUNTY	101 HOOPER AVE	TOMS RIVER NJ

## APPROVED BY: THE MANCHESTER TOWNSHIP PLANNING BOARD

**BOARD CHAIRMAN** 

DATE

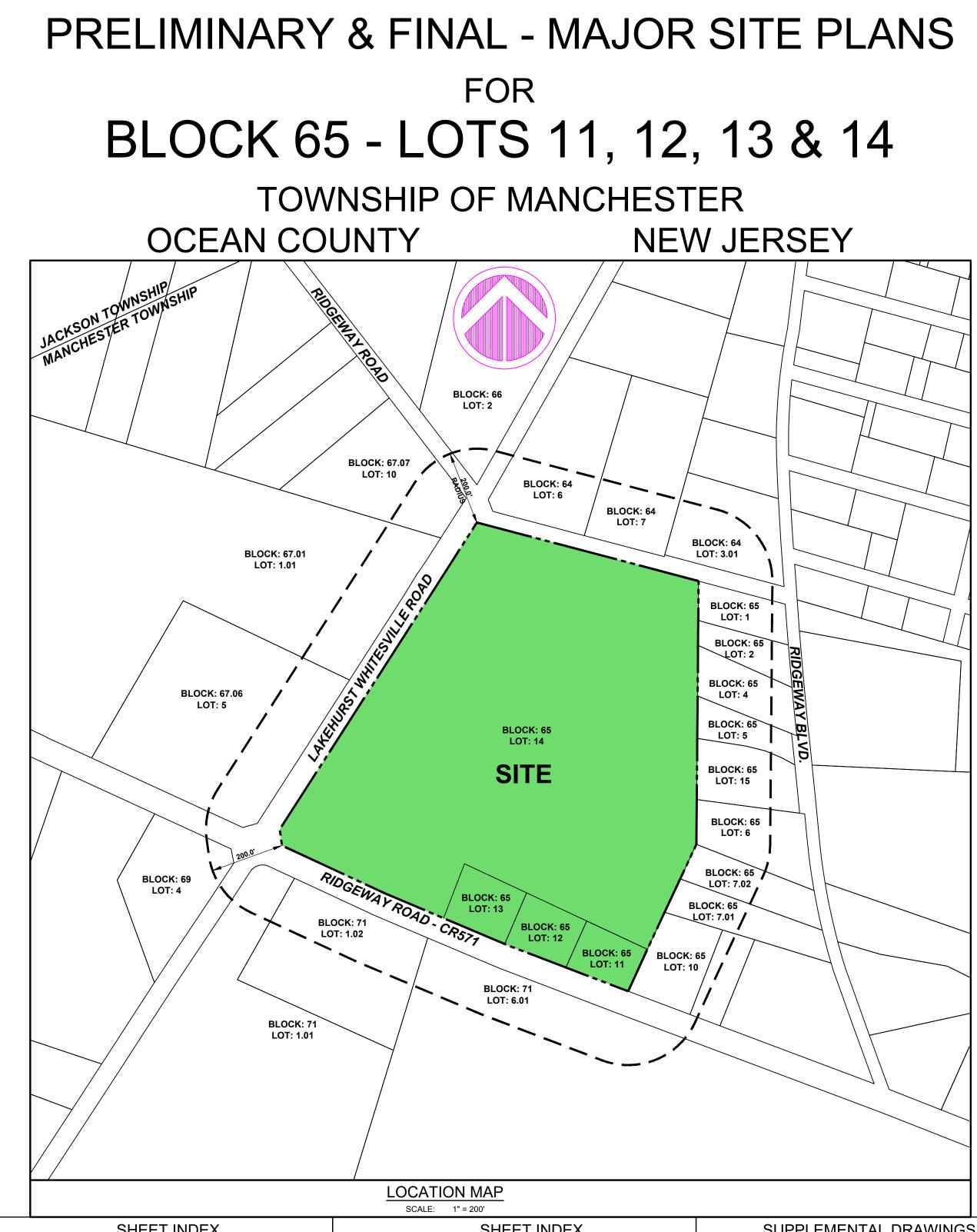
BOARD SECRETARY

BOARD ENGINEER

DATE

DATE

		-	SCALE: 1" = 200'				
	SHEET INDEX		SHEET INDEX			SUPPLEMENTAL DRAWING	s
No.	DESCRIPTION	No.	DESCRIPTION		TOTAL SHEET		
1	COVER SHEET	17	CONSTRUCTION DETAILS - STORMWATER DETA	AILS			
2	NOTES	18	CONSTRUCTION DETAILS - UTILITY DETAILS		1	BOUNDARY SURVEY	
3	SITE PLAN OVERALL	19	PRE-DEVELOPED DRAINAGE AREA MAP				
4	SITE PLAN "A"	20	POST DEVELOPED DRAINAGE AREA MAP				
5	SITE PLAN "B"	21	STORMWATER MAINTENANCE PLAN				
6	OVERALL GRADING & STORM DRAINAGE PLAN				•		
7	GRADING & STORM DRAINAGE PLAN "A"						
8	GRADING & STORM DRAINAGE PLAN "B"						
9	OVERALL UTILITY PLAN						
10	ROAD PROFILES			тні	NERSHIP OF DOC S DOCUMENT ANI	D THE IDEAS AND DESIGNS INCORPORATED HEREIN,	
11	ROAD PROFILES			PRC	OFESSIONAL DES	OF PROFESSIONAL SERVICE, IS THE PROPERTY OF IGN SERVICES, L.L.C., AND IS NOT TO BE USED IN FOR ANY OTHER PROJECT WITHOUT THE WRITTEN	
12	LANDSCAPE PLAN "A"		Г			PROFESSIONAL DESIGN SERVICES, L.L.C.	
13	LANDSCAPE PLAN "B"						
14	LANDSCAPE DETAILS						
15	LIGHTING PLAN						
16	CONSTRUCTION DETAILS - SITE DETAILS		-				
L	1	1		1 (	05/26/2023 GENER	RAL REVISIONS	KNL
			F	NO.	DATE	DESCRIPTION	BY





## **KEY MAP** 1"=2000'

## **GENERAL NOTES**

- PROPERTY IS KNOWN AS BLOCK 65 LOTS 11, 12, 13 & 14 AS SHOWN ON THE MANCHESTER TOWNSHIP TAX MAP SHEET 4.
- OUTBOUND & TOPOGRAPHIC INFORMATION TAKEN FROM A MAP ENTITLED "BOUNDARY & TOPOGRAPHIC SURVEY FOR TAX BLOCK 65 TAX LOTS 11, 12, 13 & 14 TOWNSHIP OF MANCHESTER, OCEAN COUNTY, NEW JERSEY," AS PREPARED BY PROFESSIONAL DESIGN SERVICES, LLC, DATED NOVEMBER 29, 2021.
- THE PROPERTY IS CURRENTLY LOCATED WITHIN THE PB ZONE AND CONTAINS APPROXIMATELY 20.86 ACRES.
- IT IS ASSUMED THAT THERE ARE NO FRESHWATER WETLANDS LOCATED ON OR WITHIN 300 FEET OF THE PROPERTY
- TOWNHOUSE DEVELOPMENTS ARE A CONDITIONAL USE IN THE PB-1 ZONE PURSUANT TO 245-74 AS SET FORTH IN ORDINANCE 17-025.
- IT IS PROPOSED TO CONSTRUCT 167 TOWN HOUSE UNITS.
- WATER SERVICE WILL BE PROVIDED BY PUBLIC WATER.
- SEWAGE SERVICE WILL BE PROVIDED PRIVATE SEPTIC SYSTEM
- ALL UTILITIES (ELECTRIC, TELEPHONE, ETC.) TO BE PROVIDED UNDERGROUND. THE CONTRACTOR MUST VERIFY LOCATION AND DEPTH OF ALL UTILITIES PRIOR TO CONSTRUCTION.
- 10. THE SIGHT TRIANGLE EASEMENTS ARE SUBJECT TO RESTRICTIONS CONTAINED WITHIN THE OCEAN COUNTY LAND USE REGULATIONS.
- 11. SOLID WASTE IS TO BE PICKED UP BY A PRIVATE GARBAGE HAULER. THE REFUSE AREA SHALL CONTAIN AN AREA FOR THE COLLECTION OF RECYCLABLE MATERIALS. 12. MAINTENANCE OF THE STORMWATER SYSTEM SHALL BE THE RESPONSIBILITY OF THE PROPERTY OWNER AND SUBJECT TO INSPECTION BY THE TOWNSHIP OF
- MANCHESTER.
- 13. ALL TRAFFIC CONTROL SIGNAGE INCLUDING PAVEMENT MARKINGS WILL BE PROVIDED IN ACCORDANCE WITH THE "MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES"
- 14. ALL DISTURBED AREAS WILL BE VEGETATIVELY STABILIZED IN ACCORDANCE WITH THE CERTIFIED SOIL EROSION AND SEDIMENT CONTROL PLAN UPON COMPLETION OF THE GRADING ACTIVITIES.
- 15. EXISTING CONDITIONS AND DIMENSIONS TO BE VERIFIED BY THE CONTRACTOR PRIOR TO CONSTRUCTION. CONTRACTOR SHALL VERIFY THE LOCATION AND DEPTH OF ALL UTILITIES PRIOR TO CONSTRUCTION.
- 16. ALL CONSTRUCTION TO BE IN CONFORMANCE WITH APPLICABLE CODES, ORDINANCES AND MANUFACTURER'S REQUIREMENTS.
- 17. TRAFFIC DIRECTION ARROWS, FIRE LANE MARKINGS, ETC. SHALL BE IN CONFORMANCE WITH MANCHESTER TOWNSHIP FIRE PREVENTION BUREAU AND TOWNSHIP ENGINEERING DEPARTMENT REQUIREMENTS.
- 18. THE OWNER OR HIS/HER REPRESENTATIVE. IS TO DESIGNATE AN INDIVIDUAL **RESPONSIBLE FOR CONSTRUCTION SITE SAFETY DURING THE COURSE OF SITE** IMPROVEMENTS PURSUANT TO NJAC 5:23-2:21(e) OF THE NJ UNIFORM CONSTRUCTION CODE AND CFR 1926.32(f) (OSHA COMPETENT PERSON). PROFESSIONAL DESIGN SERVICES, LLC ASSUMES NO RESPONSIBILITY FOR CONSTRUCTION SITE SAFETY.
- 19. ALL HANDICAPPED PARKING SPACES SHALL BE CONSTRUCTED TO MEET ADA REQUIREMENTS. 20. NO PHASING OF SITE IMPROVEMENTS IS PROPOSED.

- 21. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO REVIEW ALL OF THE DRAWINGS AND SPECIFICATIONS ASSOCIATED WITH THE PROJECT WORK SCOPE PRIOR TO THE INITIATION OF CONSTRUCTION. SHOULD THE CONTRACTOR FIND A CONFLICT WITH THE DOCUMENTS RELATIVE TO THE SPECIFICATION OR THE RELATIVE CODES, IT IS THE CONTRACTOR'S RESPONSIBILITY TO NOTIFY THE PROJECT ENGINEER OF RECORD IN WRITING PRIOR TO THE START OF CONSTRUCTION. FAILURE BY THE ACCORD IN WRITING PRIOR TO THE START OF CONSTRUCTION. FAILURE BY THE CONTRACTOR TO NOTIFY THE PROJECT ENGINEER SHALL CONSTITUTE ACCEPTANCE OF FULL RESPONSIBILITY BY THE CONTRACTOR TO COMPLETE THE SCOPE OF WORK AS DEFINED BY THE DRAWINGS AND IN FULL COMPLIANCE WITH LOCAL REGULATIONS AND CODES.
- CONTRACTOR IS RESPONSIBLE FOR COORDINATION OF SITE PLAN DOCUMENTS AND ARCHITECTURAL DESIGN FOR EXACT BUILDING UTILITY CONNECTION LOCATIONS, 22 GREASE TRAP REQUIREMENTS/ DETAILS, DOOR ACCESS AND EXTERIOR GRADING THE UTILITY SERVICE SIZES ARE TO BE DETERMINED BY THE ARCHITECT. THE CONTRACTOR SHALL COORDINATE INSTALLATION OF UTILITIES/SERVICES WITH THE INDIVIDUAL COMPANIES, TO AVOID CONFLICTS AND ENSURE PROPER DEPTHS ARE ACHIEVED. THE JURISDICTION UTILITY REQUIREMENTS SHALL ALSO BE MET, AS WELL AS COORDINATING THE UTILITY TIE-INS/CONNECTIONS PRIOR TO CONNECTING TO THE EXISTING UTILITY/SERVICE. WHERE CONFLICT EXISTS WITH THESE SITE PLANS, ENGINEER IS TO BE NOTIFIED PRIOR TO CONSTRUCTION TO RESOLVE SAME.
- 23. ALL FILL, COMPACTION AND BACKFILL MATERIALS REQUIRED FOR UTILITY INSTALLATION SHALL BE AS PER THE RECOMMENDATIONS PROVIDED IN THE GEOTECHNICAL REPORT AND SHALL BE COORDINATED WITH THE APPLICABLE UTILITY COMPANY SPECIFICATIONS.
- THE CONTRACTOR SHALL COMPLY TO THE FULLEST EXTENT WITH THE LATEST OSHA STANDARDS AND REGULATIONS, OR ANY OTHER AGENCY HAVING JURISDICTION FOR EXCAVATION AND TRENCHING PROCEDURES. THE CONTRACTOR IS RESPONSIBLE FOR DETERMINING "MEANS AND METHODS" REQUIRED TO MEET THE INTENT AND PERFORMANCE CRITERIA OF OSHA, AS WELL AS ANY OTHER ENTITY THAT HAS JURISDICTION FOR EXCAVATION AND/OR TRENCHING PROCEDURES.
- 25. PAVEMENT SHALL BE SAW CUT IN STRAIGHT LINES TO THE FULL DEPTH OF THE EXISTING PAVEMENT. ALL DEBRIS FROM REMOVAL OPERATIONS SHALL BE REMOVED FROM THE SITE AT THE TIME OF EXCAVATION. STOCKPILING OF DEBRIS WILL NOT BE PERMITTED.
- 26. IN CASE OF DISCREPANCIES BETWEEN PLANS OR RELATIVE TO OTHER PLANS, THE SITE PLAN WILL TAKE PRECEDENCE. IMMEDIATELY NOTIFY THE ENGINEER IN WRITING OF ANY CONFLICTS.
- 27. CONTRACTOR SHALL BE REQUIRED TO SECURE ALL NECESSARY PERMITS AND APPROVALS FOR ALL OFF-SITE MATERIAL SOURCES AND DISPOSAL FACILITIES. CONTRACTOR SHALL SUPPLY A COPY OF APPROVALS TO ENGINEER AND OWNER PRIOR TO INITIATING WORK.
- 28. THE DEVELOPER IS REQUIRED TO OBTAIN A PERMIT FROM THE OCEAN COUNTY ENGINEERING DEPARTMENT PRIOR TO THE START OF CONSTRUCTION OF ANY IMPROVEMENTS WITHIN THE RIGHT-OF-WAY OF LAKEHURST-WHITESVILLE ROAD (CR547) OR RIDGEWAY ROAD (CR571).
- 29. THE DEVELOPER SHALL OBTAIN A LETTER OF FINAL ACCEPTANCE FROM THE OCEAN COUNTY ENGINEER FOR THE ROAD IMPROVEMENTS ALONG LAKEHURST-WHITESVILLE ROAD (CR547) OR RIDGEWAY ROAD (CR571) PRIOR TO THE RELEASE OF ANY BOND OR FINANCIAL SURETY POSTED WITH THE MUNICIPALITY FOR THE COMPLETION OF SAID IMPROVEMENTS.
- 30. THERE IS NO NATURAL OR MAN-MADE WATERCOURSE TRAVERSING THE SITE.

## MANCHESTER LAND USE ZONE R-3 RURAL RESIDENTIAL R-20 SINGLE FAMILY RESIDENTIAL

(MEDIUM DENSITY)

## LAND USE

- (C) COMMERCIAL
- (I) INDUSTRIAL (R) RESIDENTIAL
- (V) VACANT

## **OWNER / APPLICANT**

**BELLEVUE ESTATES, LLC** 305 MAIN STREET

LAKEWOOD, NJ 08701

PRELIMINARY & FINAL MAJOR SITE PLAN

## **COVER SHEET**

FOR BLOCK 65 LOTS 11, 12, 13 & 14

) PP	TOWNSHIP OF MANCHESTER							
<b>1., 1.1.</b>		OCEAN CO	JNTY NE			EW JERSEN	/	
_	SCALE:	AS SHOWN	DATE: APRIL 2	5, 2022	JOB NUMBER:	18123	SHEET 1	
$\rightarrow$	DRAWN BY:	KNL	DESIGNED BY:	IMB	CHECKED BY:	WAS		21
							/	

/PDS
PROFESSIONAL DESIGN SERVICES, L.L.C
- FRUFESSIUNAL DESIGN SERVICES, L.L.C

CONSULTING ENGINEERS, LAND SURVEYORS, PLANNERS, ENVIRONMENTAL SCIENTISTS, CONSTRUCTION SERVICES

1245 AIRPORT ROAD, SUITE 1, LAKEWOOD, NEW JERSEY 08701

PHONE 732 363 0060 FAX 732 363 0073

ENGINEERING@PDS-NJ.COM WWW.PDS-NJ.COM

NEW JERSEY STATE BOARD OF P.E. & L.S.

CERTIFICATE OF AUTHORIZATION NO. 24GA28125400

§ 245-74 <b>Townhouse developments.</b>	PROVIDE
<u>A.</u> Permitted. subject to the conditions specified below: (1) Minimum lot size: 10 acres.	20 acres
(2) The maximum density for townhouses is eight units per gross acre.	7.05 /acre
(3) Minimum setback distance:	
(a) Minimum front yard: 75 feet from a collector road or arterial road as identified in the Master Plan;	75 ft.
(b) Minimum side yard setback: 50 feet;	N/A
(c) Minimum rear yard setback: 30 feet. (4) Minimum width of any townhouse shall be 20 feet.	30 ft. 22 ft.
(5) Minimum floor area per unit: 600 square feet.	1,760 sq. ft.
(6) Maximum building height: same as underlying zone.	Less than 40 f
(7) Maximum number of stories: same as underlying zone.	2 <sup>1</sup> / <sub>2</sub> stories
(8) Maximum number of units per structure: eight.	8
(9) Maximum number of eight-unit structures shall not be more than 20% of all residential structures included in the townhouse development.	16.0%
(10) Minimum distance between buildings shall be as follows:	
(a) For townhouse dwellings oriented essentially at 90° to each other, the minimum distance between same shall be 30 feet or one times the maximum height of the building, whichever is greater.	30 ft.
(b) For townhouse dwellings oriented essentially end-to-end to each other, the minimum distance between same shall be 30 feet minimum or 1.5 times the maximum height of the buildings, whichever is greater.	30 ft.
(c) For townhouse dwellings oriented essentially with parallel axis facing each other, the minimum distance between same shall be 50 feet or 2.5 times the maximum height of the buildings, whichever is greater.	50 ft.
(11) No portion of any dwelling unit shall be lower than the outside finished grade. No depressed siting shall be permitted.	Complies
<b>B.</b> Recreation requirement. (1)A playground area or areas shall be provided at the rate of 500 square feet per four dwelling units. A swimming pool of 1,500 square feet minimum size shall be provided, outdoor play equipment shall be installed in each outdoor playground in sufficient amount and variety to service the occupants of the project. At least one tennis court shall be provided for every 50 acres. No certificate of occupancy shall be issued until recreation areas are completed.	Complies
-	
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within the area of 20 feet inside the boundary line of the abutting a residential lot shall be cut, uprooted, destroye adequate trees, shrubs or planting exists in the twenty-for the premises before development, the area shall be provplanting plan to provide a belt of screening within the tw

**<u>F.</u>** Interior roads and driveway location.

(1)All roads and other accessways within the townhous roads constructed, paved and curbed to right-of-way wi such construction, paving and curbing shall be com subdivision regulations of Manchester Township.

(2)Driveways for ingress and egress for the project shall of an existing intersection or create any hazardous condudeceleration lanes shall be installed where a traffic hazar traffic congestion shall be created.

**<u>G.</u>** Accessory uses. Accessory uses usually incidental to below:

(1) Noncommercial garage for exclusive use of site reside
 (2) Noncommercial swimming pools for exclusive use of
 H. Association required. Any applicant requesting a tow provide for the creation of an association. Such documes shall specifically provide for the association to have respanded and shall provide for assurances that the be held responsible for and shall be held harmless for the common elements.

**I.** Affordable housing requirement. The applicant shall p inclusionary component or such other requirement that is court-approved housing plan or a housing plan approved Affordable Housing (COAH) at the time of final site plat construction and distribution of affordable housing units regulations in effect by COAH, by the Department of C state agency designated as the regulatory agency for affer housing construction in New Jersey at the time of the iss permit for the development.

<u>J.</u> Pinelands development credits. In the PB-1, POR-LI and PRC-1 Zoning Districts, Pinelands development credits shall be purchased and redeemed for 30% of all units, excluding up to 20% of the total project units that are made affordable for low- and moderate-income households in accordance with applicable state law. Units made affordable for low- and moderate-income households that account for more than 20% of the total project units shall purchase and redeem Pinelands development credits for 30% of all such units.

the townhouse development byed, or taken away. If no foot area in the natural state of ovided with an adequate approved twenty-foot area.	
ouse development shall be private width of not less than 26 feet. All ompleted in accordance with the	Complies
all not be located within 200 feet nditions. Acceleration and zard exists or where substantial	Complies
to the above uses, as specified	
esidents only. e of site residents only. ownhouse project approval shall nents creating the association esponsibility for maintenance for at the Township shall in no way the cost of maintenance of the	N/A Complies Complies
Il provide for a twenty-percent at is in effect in accordance with a ved by the New Jersey Council on plan approval. The type, hits shall conform to the Community Affairs or such other affordable housing and affordable issuance of the first building	28 Affordable Housing Units required, 28 Units Provided
LI and PRC-1 Zoning Districts, I redeemed for 30% of all units, made affordable for low- and licable state law. Units made that account for more than 20% inelands development credits for	8.5 PDCs are required

## ZONE REQUIREMNTS

# § 245-68 Garden Apartments <u>A.</u> Permitted. subject to the conditions specified below:

(1) Minimum lot size: 10 acres.

(2) The maximum density for garden apartments is six units per gross acre.

(3) Minimum setback distance: 75 feet from a collector road or arterial road as identified in

Master Plan;

(4) A swimming pool of 1,000 square feet minimum size shall be provided for all

developments of 90 units or more.(5) Minimum width of any garden apartment shall be 20 feet.

(6) Minimum floor area per unit: 600 square feet.

(7) Maximum floor area per unit: 1,200 square feet.

(8) Maximum building height: same as underlying zone.

(9) Maximum number of stories: same as underlying zone.

(10) Minimum number of units per structure: eight.

(11) Maximum number of units per structure: 24.

(12) Reserved

(13) Minimum distance between buildings shall be as follows:

(a) For garden apartment dwellings oriented essentially at 90° to each other, the minimum distance between same shall be 30 feet or one times the maximum height of the building, whichever is greater.

(b) For garden apartment dwellings oriented essentially end-to-end to each other, the minim distance between same shall be 30 feet minimum or 1.5 times the maximum height of the buildings, whichever is greater.

(c) For garden apartment dwellings oriented essentially with parallel axis facing each other, minimum distance between same shall be 50 feet or 2.5 times the maximum height of the buildings, whichever is greater.

(d) No portion of any dwelling unit shall be lower than the outside finished grade. No depressed siting shall be permitted.

## **<u>B.</u>** Recreation requirement.

(1)A playground area or areas shall be provided at the rate of 500 square feet per four dwelling units. A swimming pool of 1,500 square feet minimum size shall be provided, outdoor play equipment shall be installed in each outdoor playground in sufficient amount and variety to service the occupants of the project. At least one tennis court shall be provided for every 50 acres. No certificate of occupancy shall be issued until recreation areas are completed.

(2) All areas of a garden apartment development not used for the construction of buildings, roads, accessways, parking areas or sidewalks shall be fully landscaped or grassed.

#### **<u>C.</u>**Off-street parking requirements.

(1) There shall be two parking spaces for every dwelling unit.

(2) Garage facilities or off-street parking areas shall be provided on the lot sufficient to prov storage or parking for a number of vehicles equal to not less than twice the number of dwell units, and shall be developed and maintained in accordance with the following:

(a) Garages and parking area shall be used for automobile parking only with no sale of automobiles, dead storage of automobiles, repair work, dismantling or servicing of any kind

(b) Parking areas shall be paved and curbed and provided with an adequate system of stormwater drainage.

(c) No garages or off-street parking areas shall be located neared than five feet from any adjoining property line.

(d) No garages or off-street parking areas shall be located between the main building or buildings and the street line on which the building(s) fronts.

OWNERSHIP OF DOCUMENTS

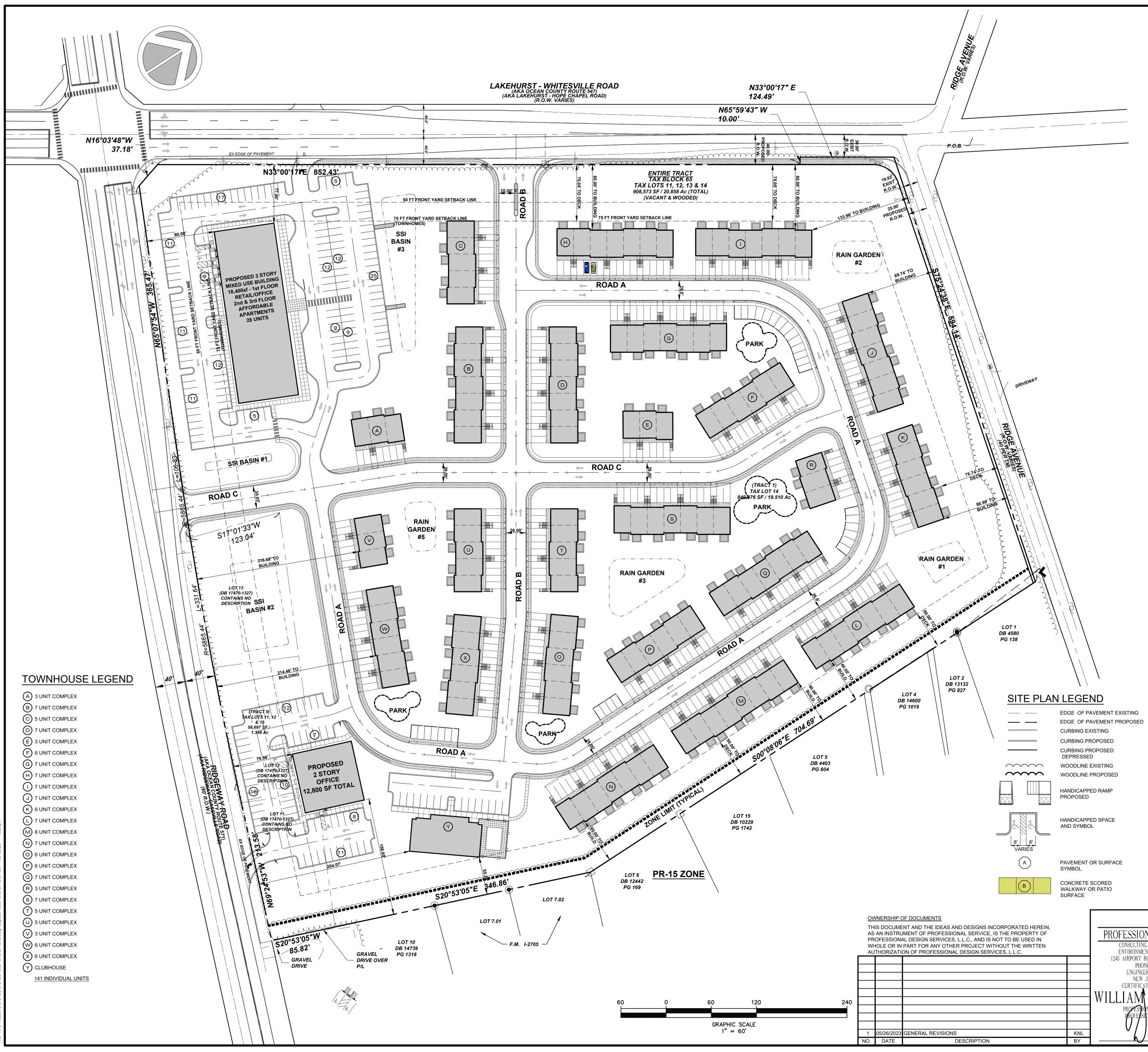
AS AN INSTRUMENT OF PROFESSIONAL SERVICE, IS THE PROPERTY OF PROFESSIONAL DESIGN SERVICES, L.L.C., AND IS NOT TO BE USED IN WHOLE OR IN PART FOR ANY OTHER PROJECT WITHOUT THE WRITTEN AUTHORIZATION OF PROFESSIONAL DESIGN SERVICES, L.L.C.								
NO.	DATE	DESCRIPTION						

THIS DOCUMENT AND THE IDEAS AND DESIGNS INCORPORATED HEREIN,

	PROVIDED		(e) Where the result of the shall be located
		_	(f) No parking a
	20 acres	_	permitted on an
	1.4 /acre		
n the	80 ft.		(g)All garage w planting or hedg
	N/A	-	(h) All off-stree foot-high wood
	20 ft.		shrub or hedge
	>600 sq. ft.		<b>D.</b> Utility requi
	<1,200 sq. ft.	-	(1)Utilities for a
	Less than 40 ft.		shall arrange wi supply lines and
	2 <sup>1</sup> / <sub>2</sub> stories	-	standard terms a Jersey Board of
	20 units		(2) All garden a
	20 units	-	requirements of [Amended 6-9-2
		_	<u><b>E.</b></u> Landscaping for the construc
			landscaped, and in a residential
		_	inside the bound cut, uprooted, d
	30 ft.		twenty-foot area
			provided with a twenty-foot area
mum	30 ft.		<b><u>F.</u></b> Interior roads
		_	(1)All roads an
r, the	50 ft.		roads construct
			regulations of N
	Complies	_	(2)Driveways fo
			existing intersects shall be installe
		-	created.
lling	Complies	-	<u>G.</u> Accessory u
у 0			(1) Noncommen
0			(2) Noncommer
			H. Pinelands de development cr
	Complies	-	20% of the total
''	-		households in a
			moderate-incon purchase and re
	3 / unit	-	
ovide	Complies		
elling			
	Complies	-	
nd.			
	Complies	-	
	Complies		

(e) Where the rear or side yard of a lot abuts on a street, no garage or off-street parking area shall be located nearer than 25 feet from such street line.	Complies
(f) No parking area may be place closer to a building than 12 feet. No parking shall be permitted on any access road within the garden apartment development.	Complies
(g)All garage walls facing any street shall be screened from street view by dense evergreen planting or hedge planting at least six feet in height, maintained in good condition.	Complies
(h) All off-street parking shall be efficiently screened along all side and rear lot lines, by a six- foot-high wood or wire fence landscaped with dense evergreen planting, or a dense evergreen shrub or hedge screening at least six feet in height maintained in good condition.	Complies
<b>D.</b> Utility requirements.	
(1)Utilities for all garden apartment developments. The applicant for the site plan approval shall arrange with the serving utility for the underground installation of the utilities distribution supply lines and service connections in accordance with the provisions of the applicable standard terms and conditions incorporated as part of its tariff on file with the State of New Jersey Board of Public Utility Commissioners.	Complies
(2) All garden apartment projects shall be served by public sewer in accordance with the requirements of the Manchester Township Division of Utilities. [Amended 6-9-2008 by Ord. No. 08-020]	Complies
<b>E.</b> Landscaping and buffer requirements. All areas of a garden apartment development not used for the construction of buildings, roads, accessways, parking areas or sidewalks shall be fully landscaped, and/or grassed. Where a garden apartment development boundary line abuts a lot in a residential zone, no existing trees, shrubbery or other planting within the area of 20 feet inside the boundary line of the garden apartment development abutting a residential lot shall be cut, uprooted, destroyed, or taken away. If no adequate trees, shrubs or planting exists in the twenty-foot area in the natural state of the premises before development, the area shall be provided with an adequate approved planting plan to provide a belt of screening within the twenty-foot area.	Complies
<b>F.</b> Interior roads and driveway location.	
(1)All roads and other accessways within the garden apartment development shall be private roads constructed, paved and curbed to right-of-way width of not less than 26 feet. All such construction, paving and curbing shall be completed in accordance with the subdivision regulations of Manchester Township.	Complies
(2)Driveways for ingress and egress for the project shall not be located within 200 feet of an existing intersection or create any hazardous conditions. Acceleration and deceleration lanes shall be installed where a traffic hazard exists or where substantial traffic congestion shall be created.	Complies
G. Accessory uses. Accessory uses usually incidental to the above uses, as specified below:	
(1) Noncommercial garage for exclusive use of site residents only.	N/A Complies
<ul> <li>(2) Noncommercial swimming pools for exclusive use of site residents only.</li> <li>H. Pinelands development credits. In the PB-1, POR-LI and PRC-1 Zoning Districts, Pinelands development credits shall be purchased and redeemed for 30% of all units, excluding up to 20% of the total project units that are made affordable for low- and moderate-income households in accordance with applicable state law. Units made affordable for low- and moderate-income households that account for more than 20% of the total project units shall purchase and redeem Pinelands development credits for 30% of all such units.</li> </ul>	None required for apartment units since all are affordable units

	$\underline{PDS}$	PRELIMINARY & FINAL MAJOR SITE PLAN				PLAN	
	PROFESSIONAL DESIGN SERVICES, L.L.C.			NO	TES		
	CONSULTING ENGINEERS, LAND SURVEYORS, PLANNERS, ENVIRONMENTAL SCIENTISTS, CONSTRUCTION SERVICES						
	1245 AIRPORT ROAD, SUITE 1, LAKEWOOD, NEW JERSEY 08701			FC	OR		
	PHONE 732 363 0060 FAX 732 363 0073 Engineering®PDS-nj.com www.pds-nj.com			BLOO	CK 65		
	NEW JERSEY STATE BOARD OF P.E. & L.S. CERTIFICATE OF AUTHORIZATION NO. 24GA28125400	LOTS 11, 12, 13 & 14					
	WILLIAM A. STEVENS, P.E., P.P.			TOWNSHIP OF	MANCHESTER		
	PROPESSIONAL ENGINEER, NEV JERSEY LIC. #39915	(	DCEAN CC	UNTY		NE	EW JERSEY
	PROFESSIONAL PLANNER, NEW JERSEY LIC. #5394	SCALE:	NTS	DATE: MAY 26, 2023	JOB NUMBER:	18123	SHEET
_	$\vee/$	DRAWN BY:		DESIGNED BY:	CHECKED BY:	10123	2
	$ N$ $M$ $'$ $N$ $\sim$ $\sim$		KNL	IMB		WAS	



## **PB-1 PINELANDS BUSINESS ZONE REQUIREMENTS**

	REQUIRED	PROVIDED
MINIMUM LOT AREA	20,000 SF	908,573 SF
MINIMUM LOT FRONTAGE	125 FT	594 FT
MINIMUM LOT WIDTH	125 FT	610 FT
MINIMUM IMPROVABLE LOT AREA	13,500 FT	9,600 FT
PRINCIPAL BUILDING		
MINIMUM FRONT YARD SETBACK	50 FT	77.80 FT
MINIMUM REAR YARD SETBACK	25 FT	N/A
MINIMUM SIDE YARD SETBACK	20 FT	50.38 FT
ACCESSORY BUILDING		
MINIMUM REAR YARD SETBACK	10 FT	N/A
MINIMUM SIDE YARD SETBACK	10 FT	N/A
SITE MAXIMUM IMPROVEMENT RATIO	0.2	<0.2%
MAXIMUM BUILDING COVERAGE	20%	13.7%
MAXIMUM LOT COVERAGE	65%	36.8%
MAXIMUM BUILDING HEIGHT	35 FT	<35 FT
MAXIMUM FLOOR AREA	1,500 SF	36,800 FT

NOTE: FOR TOWNHOUSE DEVELOPMENT ZONE REQUIREMENTS, SEE NOTES SHEET 2.

## PARKING REQUIREMENTS

	REQUIRED	PROVIDED
MIXED USE:		
RETAIL & OFFICE 1 SPACE PER 200 SF 18,400 SF	92 SPACES	98 SPACES
AFFORDABLE APARTMENTS 2 SPACES PER UNIT 28 UNITS	56 SPACES	56 SPACES
DWELLING UNIT 2 SPACES PER UNIT* 141 UNITS	282 SPACES	313 SPACES
*PER SECTION 245-74 C.(1)		
OFFICE 1 SPACE PER 200 SF 12,800 SF	64 SPACES	64 SPACES

## PROJECT YIELD

TOTAL NUMBER OF MARKET UNITS = 141

TOTAL AFFORDABLE UNITS = 28

TOTAL DWELLING UNITS = 169

(1) 30% OF ALL MARKET SINGLE FAMILY LOTS MUCH PURCHASE PINELANDS QUARTER CREDITS PER ORDINANCE 22-17

## COAH COMPLETION SCHEDULE

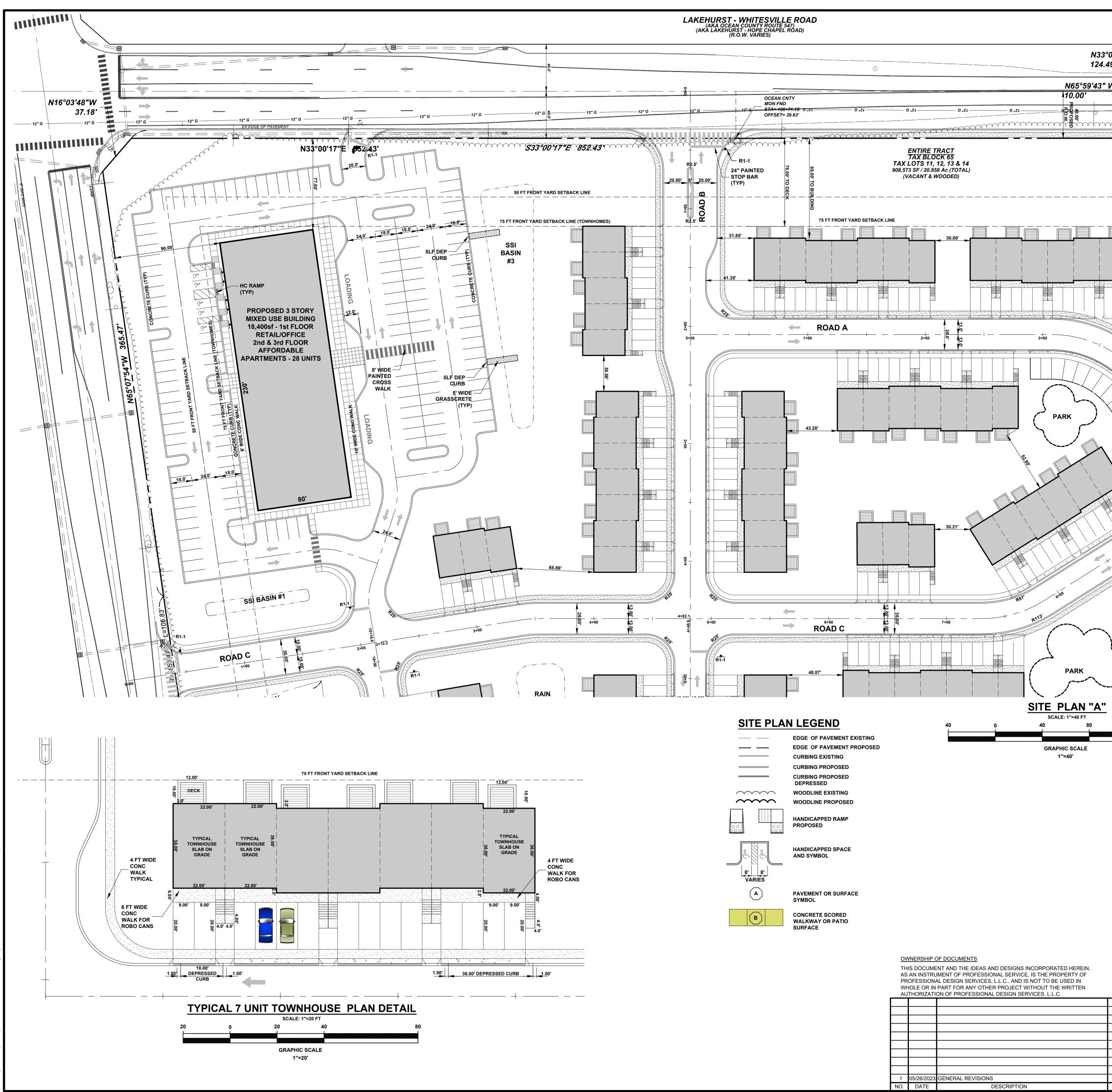
MINIMUM PERC LOW AND M NCOME UNITS	ODERATE	MINIMUM PERCENTAGE OF MARKET HOUSING UNITS COMPLETED		
0%		25%		
10%	3	25% PLUS 1	36	
50%	14	50%	71	
75%	21	75%	106	
100%	28	90%	127	

PAVEMENT OR SURFACE

CONCRETE SCORED

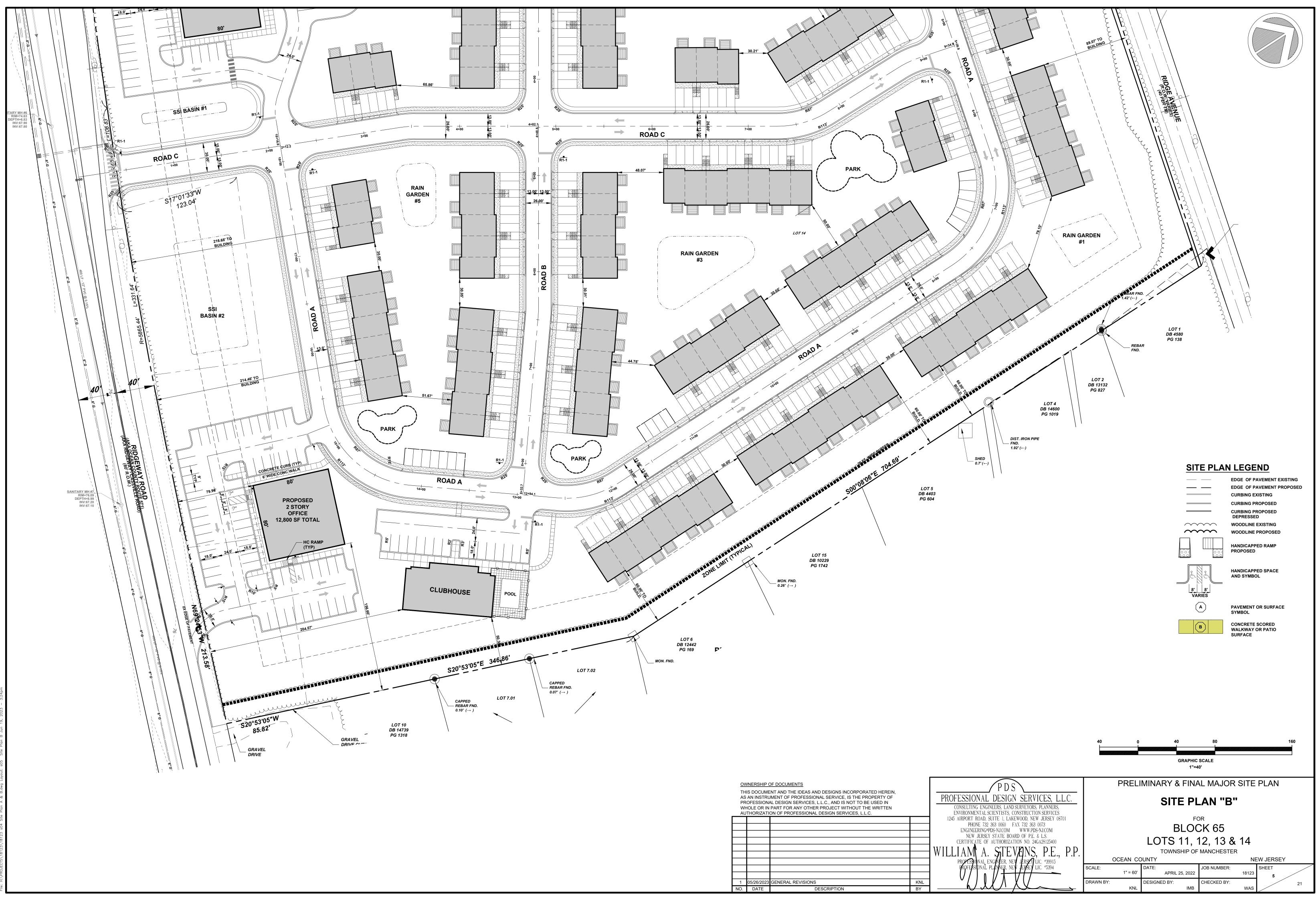
WALKWAY OR PATIO

FACE					
	P D S	PRELI	MINARY & FINA	AL MAJOR SITE	PLAN
	PROFESSIONAL DESIGN SERVICES, L.L.C.		OVERALL	SITE PLAN	
	ENVIRONMENTAL SCIENTISTS, CONSTRUCTION SERVICES 1245 AIRPORT ROAD, SUITE 1, LAKEWOOD, NEW JERSEY 08701 PHONE 732 363 0060 FAX 732 363 0073				
	ENGINEERING®PDS-NJ.COM WWW.PDS-NJ.COM NEW JERSEY STATE BOARD OF P.E. & L.S.			CK 65 12, 13 & 14	
	WILLIAM A. STEVENS, P.E., P.P.			MANCHESTER	
	PROPESSIONAL ENGINEER, NEV JERSEY LIC. #39915	OCEAN CO	DUNTY	N	EW JERSEY
	PROFESSIONAL PLANNER, NEW JERSEY LIC. #5394	SCALE: 1" = 60'	DATE: APRIL 25, 2022	JOB NUMBER: 18123	SHEET
KNL BV	$ \frac{1}{1111111111111111111111111111111111$	DRAWN BY: KNI	DESIGNED BY:	CHECKED BY: WAS	21

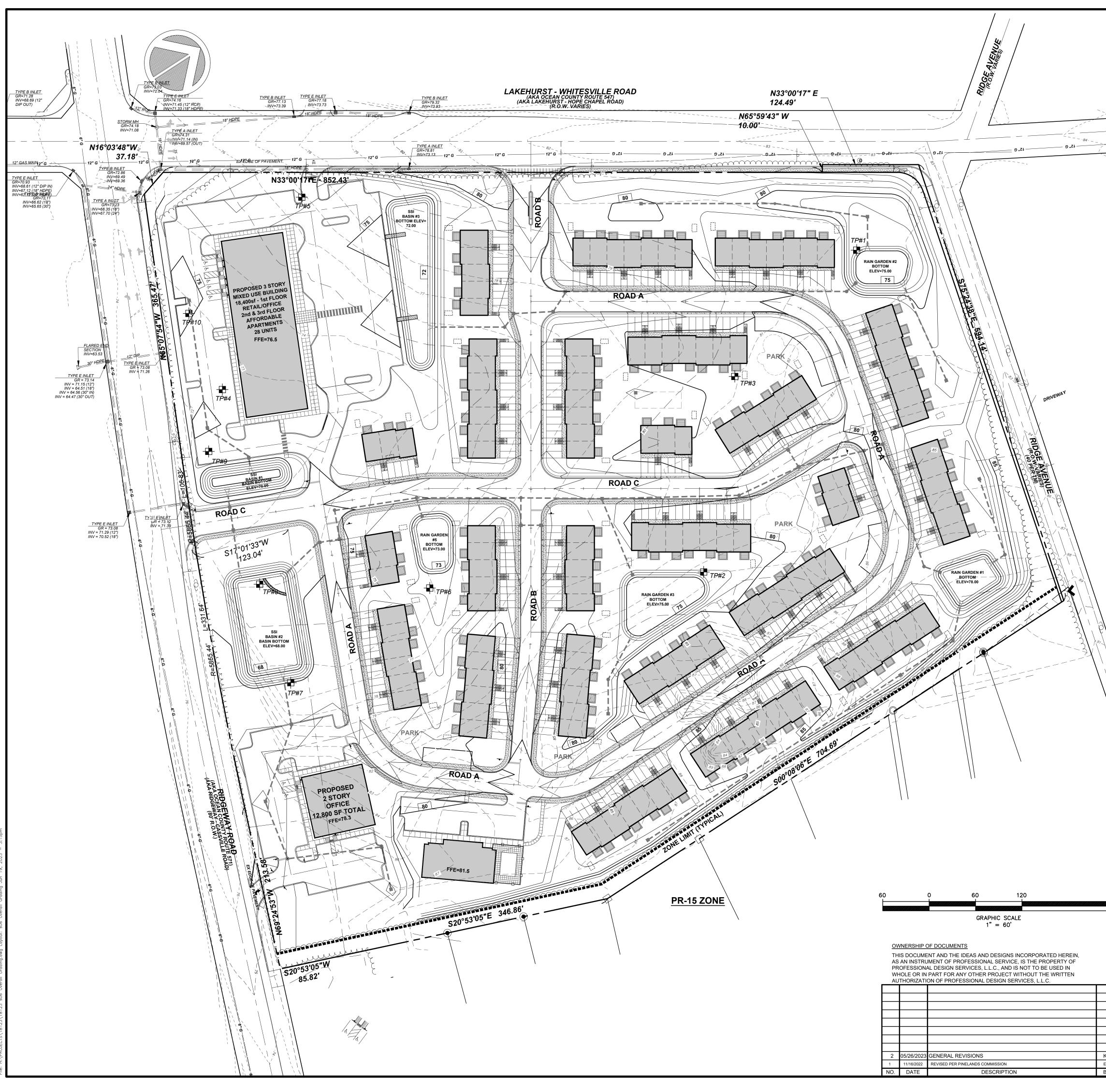


(PROJECTS\18123\18123 s04 Site Plan A & B.dwg Layout: s04 Site Plan A Jun 19, 2023 - 3:2

200'17" E 49' W	S	
	P.O.B. 9.21 9.21 9.21 9.21 9.21 9.21 9.21 9.21 9.21 9.21 9.21 1983 F.B.W P.O.B.	— 15. C
RAIN GARDEN #2	89.74' TO BUILDING	
<b>B</b>		
R1-1 P	RIDGE AMERICA PE OVERLAPE ADJOINING BK. 4580, BK. 4580,	
160		
PDS PROFESSIONAL DESIGN SER CONSULTING ENGINEERS, LAND SURVEYOF ENVIRONMENTAL SCIENTISTS, CONSTRUCT 1245 AIRPORT ROAD, SUITE 1, LAKEWOOD, N PHONE 732 363 0060 FAX 732 36 ENGINEERING®PDS-NJ.COM WWW.P	RS, PLANNERS, TION SERVICES VEW JERSEY 08701 FOR	N "A"
NEW JERSEY STATE BOARD OF P.E CERTIFICATE OF AUTHORIZATION NO. 2 WILLIAM A. STEVENS	E. & L.S. 24GA28125400 S, P.E., P.P. LIC. #39915 LIC. #5394 DATE: 1" = 40' APRIL 25, 2022 JOB	13 & 14



PR WH	OFESSION	IMENT OF PROFESSIONAL SERVICE, IS THE PROPERTY OF AL DESIGN SERVICES, L.L.C., AND IS NOT TO BE USED IN PART FOR ANY OTHER PROJECT WITHOUT THE WRITTEN ON OF PROFESSIONAL DESIGN SERVICES, L.L.C.
1	05/26/2023	GENERAL REVISIONS
NO.	DATE	DESCRIPTION



(PROJECTS\18123\18123 s06 Overall Grading.dwg Layout: s06 Overall Grading Jun 19, 2023 — 3:15

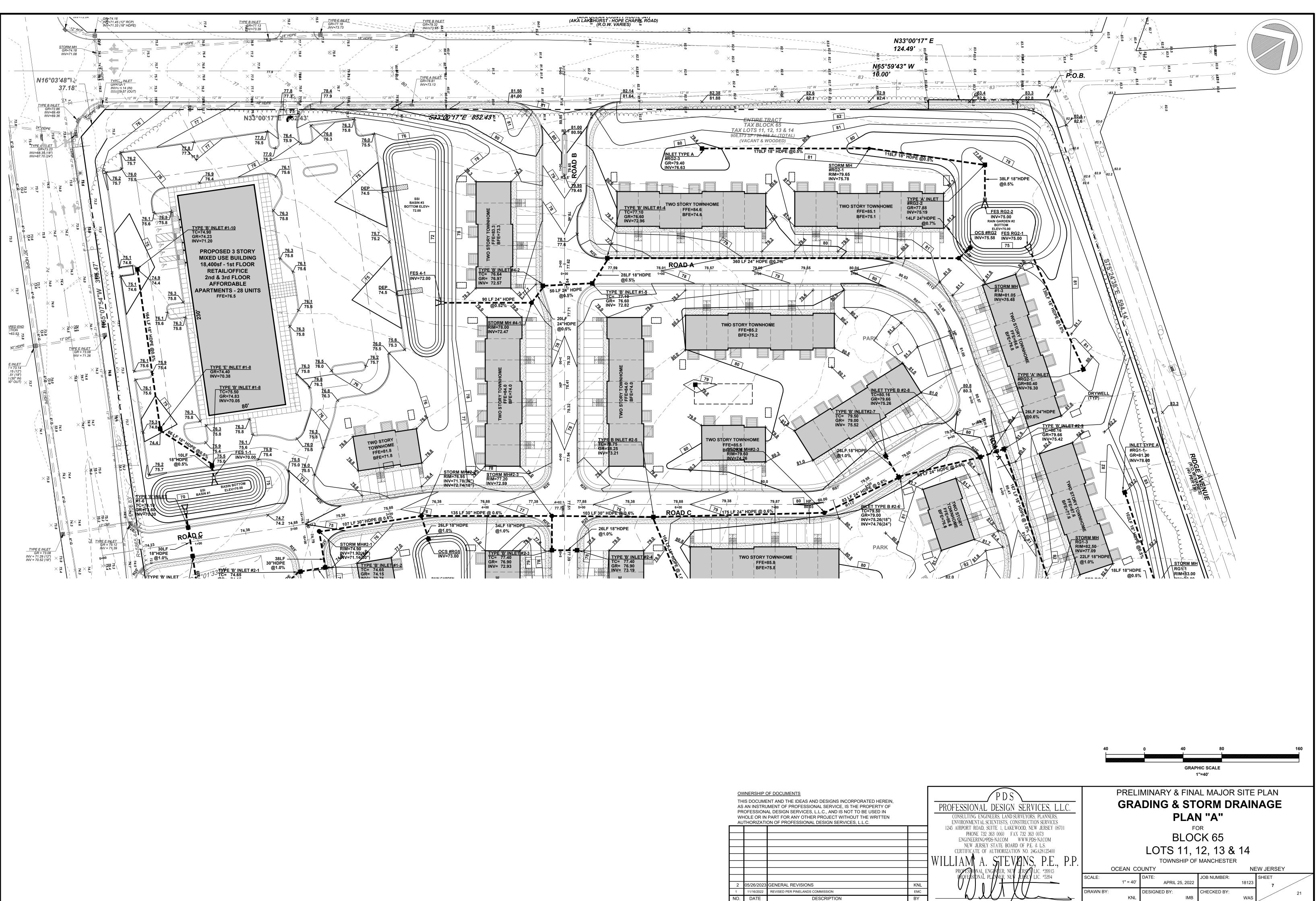
## TEST PIT LOGS

TD # 1	Elevation - 01.4	TD C	Elevation - 761
TP # 1	Elevation = 81.4	TP - 6	Elevation = 76.1
0 - 4"	10 YR 4/4 Loamy Sand	0 - 4"	10 YR 4/4 Loamy Sand
4-30"	10 YR 6/8 Sandy Loam	4 - 28"	10 YR 6/8 Sandy Loam
30-64"	10 YR 7/6 Loamy Sand	28 - 54"	10 YR 8/4 Loamy Sand
64 - 84"	10 YR 8/2 Loamy Sand	54 - 84"	10 YR 8/1 Loamy Sand
84 - 96"	10 YR 8/6 Sandy Loam	84 - 90"	10 YR 8/6 Sandy Loam
96 - 110"	10 YR 8/6 Sandy Loam 6/8 faint mottles	90 - 99"	10 YR 8/1 Sandy Loam
110 -120"	10 YR 8/2 Sandy Loam 6/8 distinct mottles	99 - 106"	10 YR 8/2 Loamy Sand
110-120	10 1 K 8/2 Sandy Loan 0/8 district motiles	106 - 130"	10 YR 8/8 Sandy Loam 6/8 distinct mottles
	SHWT @ 96 ", Elevation 73.4	130 - 144"	10 YR 7/2 Loamy Sand
	Permeability $(a)$ 66 " = 2.5 inches per hour	130 - 144	10 TK //2 Loanty Sand
	Fermeability $(u)$ 00 – 2.5 menes per noti		SINUT $@$ 106 " Elevation $= 67.2$
			SHWT @ 106 ", Elevation = 67.3
			Water encountered @ 140"
			Permeability 70" $@$ = 5.5 Inches per hour
TP # 2	Elevation = 83.2	TP - 7	Elevation = 76.3
0 - 3"	10 YR 4/4 Loamy Sand	0 - 6"	10 YR 4/4 Loamy Sand
3 - 34"	10 YR 6/8 Sandy Loam	6 - 28"	10 YR 6/8 Sandy Loam
34 - 56"	10 YR 6/8 Loamy Sand	28 - 64"	10 YR 7/8 Loamy Sand
56 - 73"	10 YR 8/6 Loamy Sand	64 - 88"	10 YR 8/6 Loamy Sand
73 - 85"	10 YR 6/8 Sandy Clay Loam	88 - 112"	10 YR 8/8 Sandy Loam
85 - 96"	7.5 YR 6/6 Sand	112 - 125"	10 YR 8/1 Sand
95 - 120"	5 YR 5/4 Loamy Sand 8/8 faint mottles @112"		
			SHWT @>125", Elevation = <66.0
	SHWT @ 112", Elevation 73.9		Permeability ( $\hat{a}$ ) 70" = 11.5 Inches per hour
	Permeability @ 60" = 7.5 Inches per hour		
TP # 3	Elevation = 81.0	TP - 8	Elevation = 74.0
0 - 4"	10 YR 4/4 Loamy Sand	0 - 4 "	10 YR 4/4 Loamy Sand
4 - 26"	10 YR 6/8 Sandy Loam	4 - 32"	10 YR 6/8 Sandy Loam
26 - 72"	10 YR 6/8 Loamy Sand	32 - 59"	10 YR 7/8 Loamy Sand
72 - 96"	10 YR 7/8 Loamy Sand	59 - 94"	10 YR 8/1 Loamy Sand
96 - 108"	10 YR 7/8 Loamy Sand	94 - 110"	10 YR 8/8 Sandy Loam
	10 2.5 YR 4/4 Sand 5/8 distinct mottles	110 - 130"	10 YR 8/1 Sand 8/8 distinct mottles
	SHWT @ 108", Elevation = 72.0		SHWT @ 110", Elevation = 64.9
	Permeability @ 55" = 9.0 Inches per hour		Permeability @ 90" = 2.5 Inches per hour
TP # 4	Elevation = 73.5	TP # 9	Elevation = 72.8
0-4"	10 Yr 4/4 Loamy Sand	0 - 4 "	10 YR 4/4 Loamy Sand
4 - 27"	10 YR 7/6 Sandy Loam	4 - 32"	10 YR 6/8 Sandy Loam
27 - 48"	10 YR 7/8 Loamy Sand	32 - 64"	10 YR 6/8 Loamy Sand
48 - 56	10 YR 7/8 Loamy Sand	64 - 96"	10 YR 7/8 Loamy Sand
56 - 67"	10 YR 7/8 Loamy Sand	96 - 106"	Gley 8/N Sandy Clay 8/8 distinct mottles
67 - 84"	10 YR 7/6 Loamy Sand	106 - 120"	10 YR 8/4 Loamy Sand
84 - 95"	10 YR 8/3 Loamy Sand 5/8 distinct mottles	100 120	To The of F Boundy Suite
95 - 104"	10 YR 8/1 Loamy Sand 8/8 distinct mottles		SHWT @ 96", Elevation = 64.8
95 - 104 104 - 109"	Gley 8/N Sandy Clay 8/8 distinct mottles		Permeability $(a)$ 70" = 6.5 Inches per hour
			f ermeability ( $w$ / 0 = 0.3 menes per nour
109 - 112" 112 - 132"	10 YR 8/4 Sandy Clay Loam8/8 distinct mottles10 YR 8/1 Loamy Sand8/8 distinct mottles		
	SHWT @ 84", Elevation = 66.5		
	Permeability $@ 60" = 15.5$ Inches per hour		
TP # 5	Elevation = 77.0	TP # 10	Elevation = 73.0
0 - 4"	10 YR 4/4 Loamy Sand	0 - 4"	10 YR 4/4 Loamy Sand
4 - 23"	10 YR 6/8 Sandy Loam	4 - 19"	10 YR 6/8 Sandy Loam
23 - 60"	10 YR 7/6 Loamy Sand	19 - 57"	10 YR 6/8 Loamy Sand
60 - 71"	10 YR 8/4 Loamy Sand	57 - 94"	10 YR 8/8 Loamy Sand
71 - 99"	2.5 Y 8/1 Loamy Sand	94 - 102"	10 YR 8/8 Loam / Silt Loam 5/8 distinct mottle
99 - 109"	10 YR 8/1 Loamy Sand 6/8 distinct mottles	102 - 120"	10 YR 8/1 Sand 8/8 distinct mottles
109 - 130"	10 YR 8/4 Sand 5/8 distinct mottles	102 120	
	SHWT @ 99", Elevation = 68.7		SHWT @ 102", Elevation = 64.5
	Permeability @ 64" = 13.0 Inches per hour		Permeability $(a)$ 60" = 3.5 Inches per hour
			formed by PDS February 5, 2022
		Dormonbility	results per Tube Permeameter Tests

## **STORMWATER BASN NOTES:**

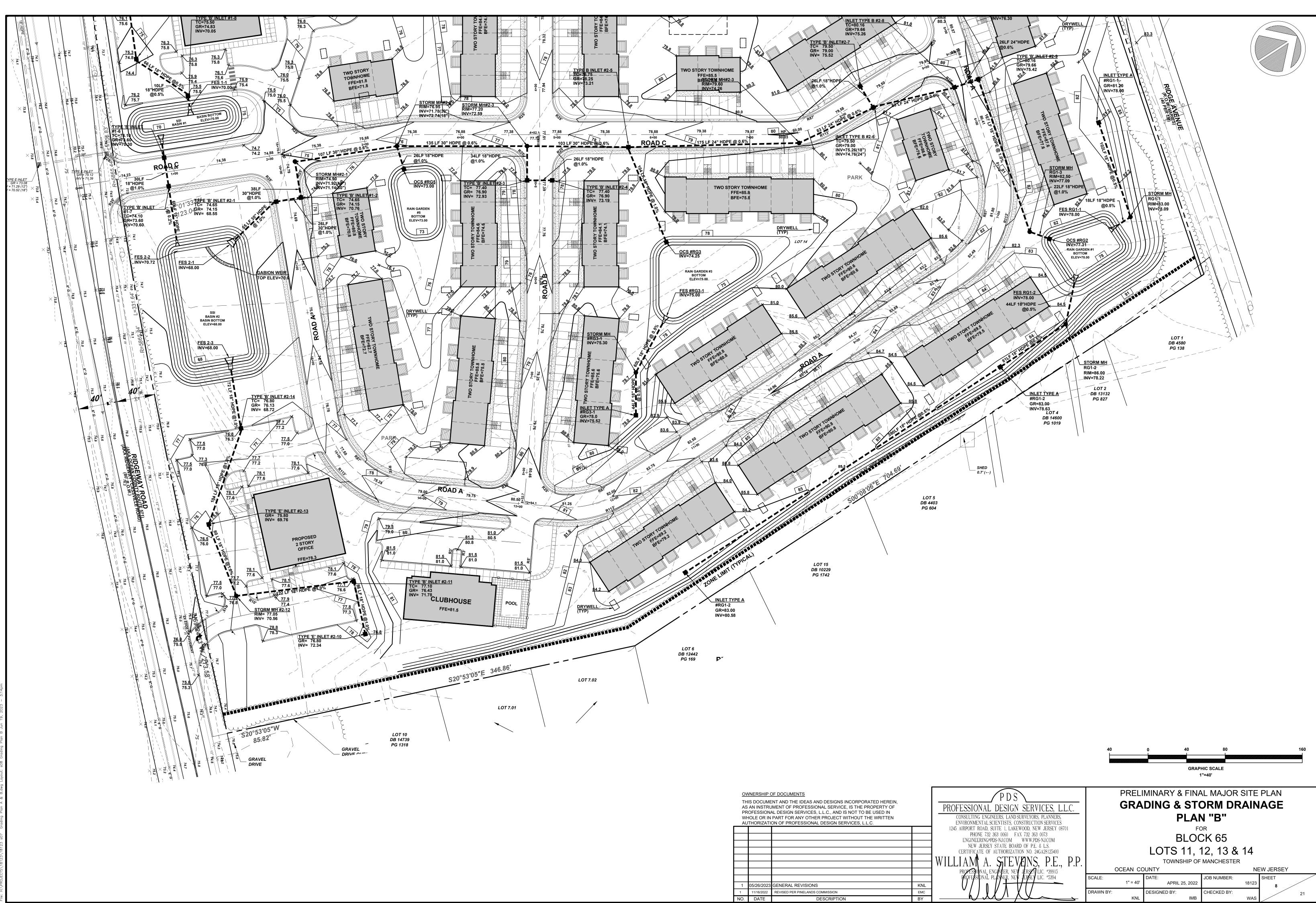
- 1. THE PROJECT DOES NOT CONTAIN ANY HIGH POLLUTANT LOADING AREAS (HPLA) AND SEGREGATION OR PRETREATMENT OF RUNOFF IS NOT REQUIRED.
- 2. THE STORMWATER BASIN HAS BEEN DESIGNED TO MAINTAIN A MINIMUM SEPARATION OF AT LEAST TWO (2) FEET FROM THE BASIN BOTTOM TO THE SEASONAL HIGH WATER TABLE.
- 3. THE SOIL PERMEABILITY BELOW THE BASIN DOES NOT PERMEATE IN EXCESS OF 20 INCHES PER HOUR AND NO BIORETENTION SYSTEM IS REQUIRED.
- 4. A GROUNDWATER MOUNDING ANALYSIS INDICATES NO ADVERSE IMPACT TO ADJACENT WATERBODIES, WETLANDS, STRUCTURES OR SEPTICS.
- 5. THE BASIN FOREBAY SHALL SERVE AS A TEMPORARY SEDIMENT BASIN UNTIL THE DRAINAGE AREA HAS BEEN COMPLETELY STABILIZED. WHEN THE DRAINAGE SYSTEM HAS BEEN COMPLETELY STABILIZED, TWO (2) FEET OF THE BOTTOM WITHIN THE FOREBAY MUST BE EXCAVATED AND REPLACED WITH CLEAN SAND HAVING A PERMEABILITY OF 6 TO 20 INCHES PER HOUR.
- 6. CARE MUST BE TAKEN DURING CONSTRUCTION TO MINIMIZE COMPACTION OF THE BASIN BOTTOM. THE BASIN AREA MUST BE RENOVATED AND TILLED AFTER CONSTRUCTION IS COMPLETED AND THE DRAINAGE AREA IS STABILIZED. NO EARTHWORK MAY BE PERFORMED WHEN SOIL MOISTURE CONTENT IS ABOVE THE LOWER PLASTIC LIMIT.
- 7. ONCE THE BASIN IS COMPLETED AND THE DRAINAGE AREA IS STABILIZED, FIELD PERMEABILITY TESTS MUST BE PERFORMED AND SUBMITTED TO THE TOWNSHIP ENGINEER TO ASSURE COMPLIANCE WITH THE DESIGN PERMEABILITY.
- 8. AS-BUILT PLANS MUST BE PERFORMED OF THE COMPLETED BASIN AND SUBMITTED TO THE TOWNSHIP ENGINEER TO ASSURE COMPLIANCE WITH THE DESIGN.
- 9. THE BASIN MUST BE DEED RESTRICTED TO PERMANENTLY PROTECT IT FROM FUTURE DEVELOPMENT.

	PDS		PRELI	MINARY & FINA	AL MAJOR S	ITE	PLAN
	PROFESSIONAL DESIGN SERVICES, L.L.C.			<b>OVERALL</b>	GRADING	<b>8</b> 6	•
	CONSULTING ENGINEERS, LAND SURVEYORS, PLANNERS, ENVIRONMENTAL SCIENTISTS, CONSTRUCTION SERVICES		S	TORM DRA	<b>INAGE P</b>	LA	N
	1245 AIRPORT ROAD, SUITE 1, LAKEWOOD, NEW JERSEY 08701			FG	OR		
	PHONE 732 363 0060 FAX 732 363 0073 Engineering®pds-nj.com www.pds-nj.com			BI O(	CK 65		
	NEW JERSEY STATE BOARD OF P.E. & L.S.						
	CERTIFICATE OF AUTHORIZATION NO. 24GA28125400			LOTS 11, <sup>2</sup>	12, 13 & 1	4	
	WILLIAM A STEVENS P.E. P.P.			TOWNSHIP OF	MANCHESTER		
	PROPESSIONAL ENGINEER, NEV JERSEY LIC. *39915		OCEAN CO	DUNTY		NE	EW JERSEY
	PROFESSIONAL PLANNER, NEW JEBSEY LIC. #5394	SCALE:	41 001	DATE:	JOB NUMBER:		SHEET
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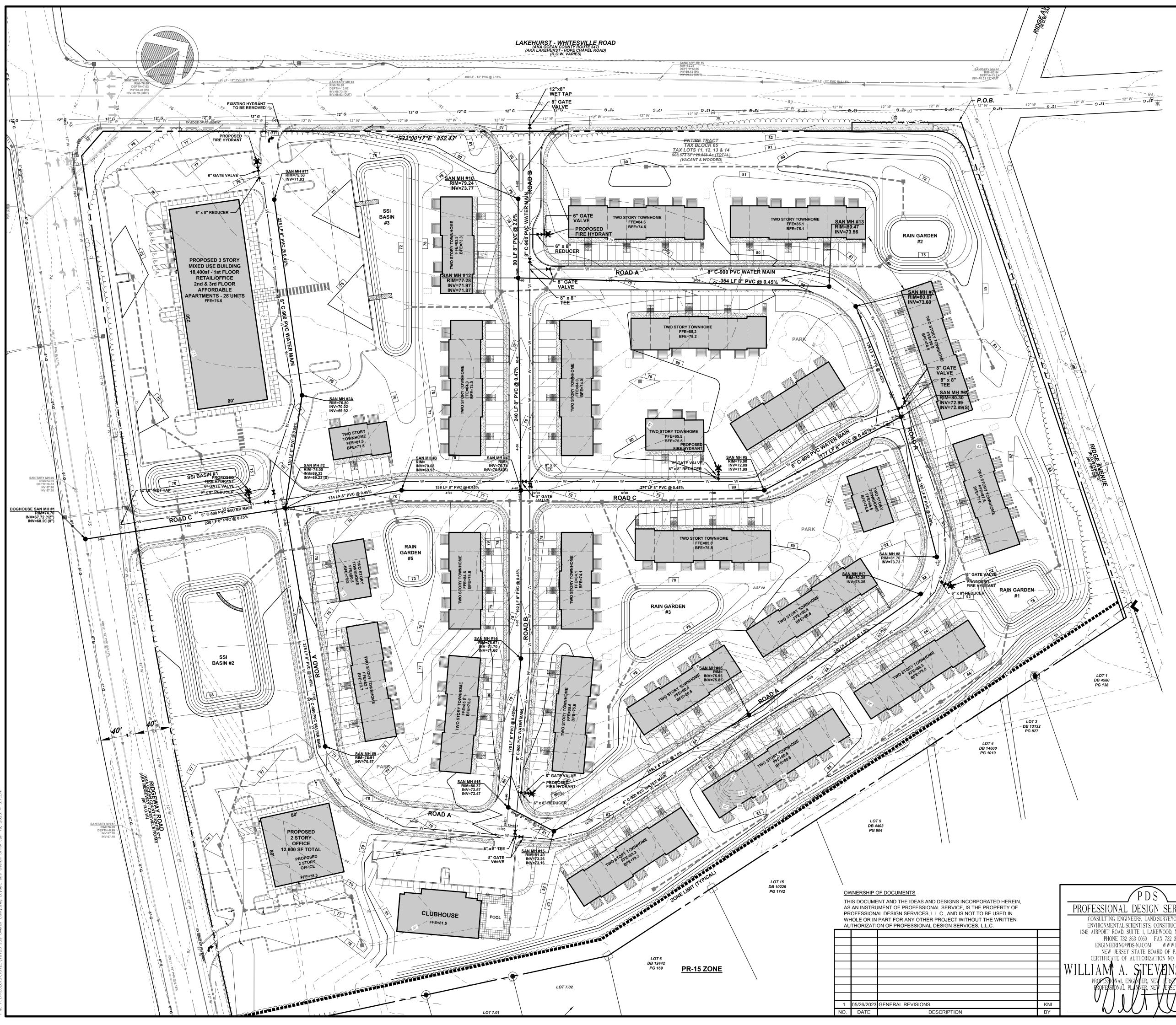




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1	11/16/2022	REVISED PER PINELANDS COMMISSION
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## **GENERAL UTILITY NOTES:**

- 1. THRUST BLOCKS ARE TO BE PROVIDED AT ALL WATER MAINS, BENDS AND FITTINGS.
- 2. FIRE HYDRANTS MUST BE SUPPLIED BY A MINIMUM OF 6" WATER LINES.
- 3. ALL SANITARY LATERALS SHALL BE INSTALLED WITH A MINIMUM SLOPE OF  $\frac{1}{4}$ " PER FOOT.
- 4. AT THE SANITARY LATERAL WYE OR TEE, MATCH THE CROWN OF THE SEWER MAINS AND THE LATERALS.
- 5. PROVIDE TEN FOOT (10') MINIMUM HORIZONTAL SEPARATION BETWEEN SEWER MAINS AND WATER MAINS. IF SUCH LATERAL SEPARATION IS NOT POSSIBLE, THE PIPES SHALL BE IN SEPARATE TRENCHES WITH THE SEWER AT LEAST 18 INCHES BELOW THE BOTTOM OF THE WATER MAIN. WHERE SEPARATION IS NOT MAINTAINED BETWEEN THE WATER AND SEWER MAINS INSTALL THE SEWER WITH DUCTILE IRON PIPE WITH WATER TIGHT JOINTS THAT ARE A DISTANCE OF AT LEAST 10 FEET ON EITHER SIDE OF THE WATER MAIN.
- 6. UTILITY CROSSING REQUIREMENTS:

A. IF A SEWER MAIN CROSSES LESS THAN 6 INCHES ABOVE THE WATER MAIN, SUPPORT THE SEWER MAIN WITH A CONCRETE CRADLE.

B. IF A WATER MAIN CROSSES LESS THAN 6 INCHES ABOVE THE SEWER MAIN SUPPORT THE WATER MAIN WITH A CONCRETE CRADLE.

C. IF OTHER PIPING OR UTILITIES CROSS LESS THAN 18 INCHES ABOVE THE SEWER, SUPPORT THE TOP PIPING OR UTILITIES WITH CONCRETE CRADLES.

D. IF OTHER PIPING OR UTILITIES CROSS LESS THAN 6 INCHES AVOVE THE WATER, SUPPORT THE TOP PIPING OR UTILITIES WITH CONCRETE CRADLES.

E. IF A WATER OR SEWER MAIN CROSSES LESS THAN 6 INCHE3S AVOVE OTHER PIPING OR UTILITIES, SUPPORT THE WATER OR SEWER MAIN WITH A CONCRETE CRADLE.

- 7. PROVIDE 3'-0" MINIMUM COVER OVER PVC SEWER MAINS PROVIDE 3'-0" MINIMUM COVER OVER SEWER LATERALS.
- 8. ALL SANITARY SEWER SHALL BE P.V.C. CONFORMING TO ASTM D-3034; SDR-35 WITH PUSH ON JOINTS, UNLESS OTHERWISE NOTED.
- 9. ALL WATER MAINS SHALL BE CLASS 52, CEMENT LINED DUCTILE IRON PIPE, RATED AT 150 PSI MINIMUM. PIPE JOINTS SHALL BE OF PUSH-ON TYPE OR MECHANICAL JOINT TYPE.
- 10. PROVIDE 4'-0" MINIMUM COVER OVER WATER MAINS. COVER MAY BE LESSENED TO 3'-9" WITH APPROVAL E OF M.T.D.O.U. TO CROSS OVER OTHER UTILITIES. WATER MAINS TO CROSS OVER STORM DRAINAGE PIPES EXCEPT WHERE INDICATED IN THE PROFILES TO CROSS UNDER, OR APPROVED BY M.T.D.O.U. WHERE THE WATER MAIN MUST CROSS UNDER THE STORM DRAINAGE, A MINIMUM CLEARANCE OF 6" MUST BE MAINTAINED.
- 11. ALL WATER SERVICES AND PLUMBING SHALL CONFORM WITH THE PLUMBING SUBCODE NJAC 5:23-3.15.
- 12. ALL WATER VALVES SHALL BE RESILIENT WEDGE TYPE IN ACCORDANCE WITH THE AMERICAN WATER WORKS ASSOCIATION STANDARD SPECIFICATION C-509.
- 13. VALVES SHALL BE PLACED ON WATER DISTRIBUTION MAINS NOT MORE THAN 1,000 FEET APART.
- 14. ALL DEAD END WATER MAINS SHALL BE TERMINATED WITH A FIRE HYDRANT.
- 15. WATER MAIN FITTINGS TO BE USED WHEREVER JOINT DEFLECTION EXCEEDS MANUFACTURERS SPECIFICATIONS.
- 16. CONNECTIONS TO EXISTING WATER MAINS AND THE ADDITION OF VALVES TO EXISTING WATER MAINS SHALL BE MADE WITHOUT THE LOSS OF WATER SERVICE TO MANCHESTER TOWNSHIP WATER UTILITY (MTWA) CUSTOMERS. WHERE A SECTION OF EXISTING WATER MAIN CANNOT BE ISOLATED WITHOUT DISRUPTING WATER SERVICE TO MTWA CUSTOMERS, CONNECTIONS TO THE EXISTING WATER MAINS WILL BE MADE BY WET TAPPING THE ACTIVE MAINS AND VALVES ADDED TO THE EXISTING MAINS WILL BE ADDED BY INSERTION INTO THE ACTIVE MAINS.
- 17. WATER MAINS SHALL BE CONSTRUCTED 5 FEET FROM CURBS. 4 FOOT OFFSETS WILL BE PERMITTED WHERE CURBS BEND AT ROADWAYS.
- 18. THE PROPOSED GAS MAINS SHALL BE LOCATED ON THE OPPOSITE SIDE OF THE ROADWAY FROM THE WATER MAINS. THE GAS MAINS SHOULD BE PARALLEL TO AND WITHIN 4 FEET OF THE CURBS TO PROVIDE ADEQUATE CLEARANCE FOR FUTURE EXCAVATIONS TO THE SANITARY SEWER MAINS, WHICH GENERALLY FOLLOW THE CENTERLINES OF THE ROADS.
- 19. THE PUBLIC WATER SUPPLY SHALL NOT BE UTILIZED FOR LAWN AND LANDSCAPE IRRIGATION. ALL LAWN AND LANDSCAPE IRRIGATION MUST BE SUPPLIED BY EACH PROPERTY OWNER'S PRIVATE WELL.

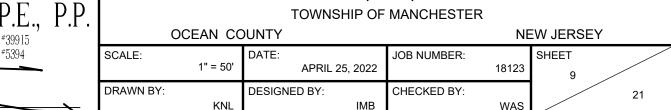
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PRELIMINARY & FINAL MAJOR SITE PLAN

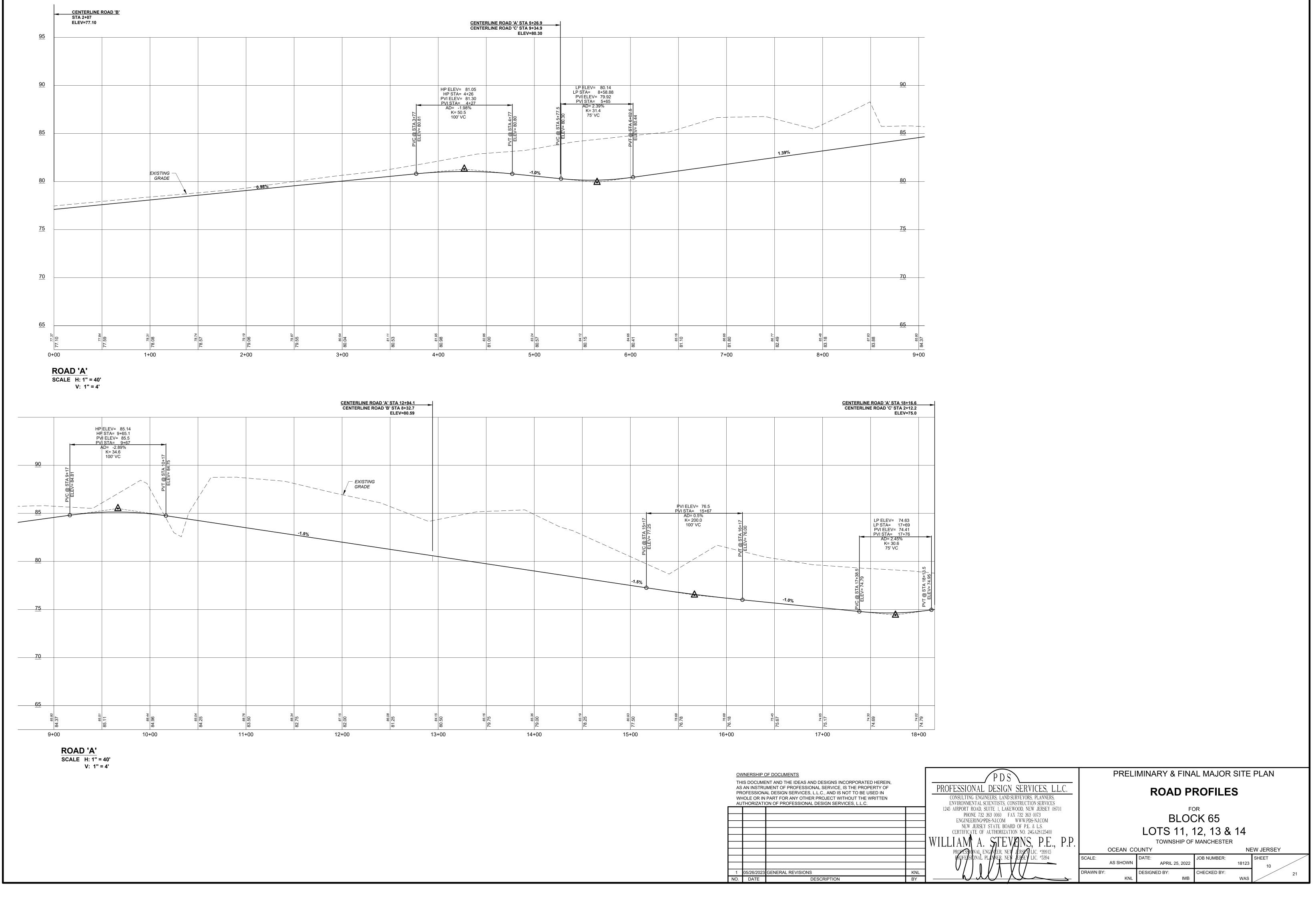
## OVERALL UTILITY PLAN

FOR **BLOCK 65** 

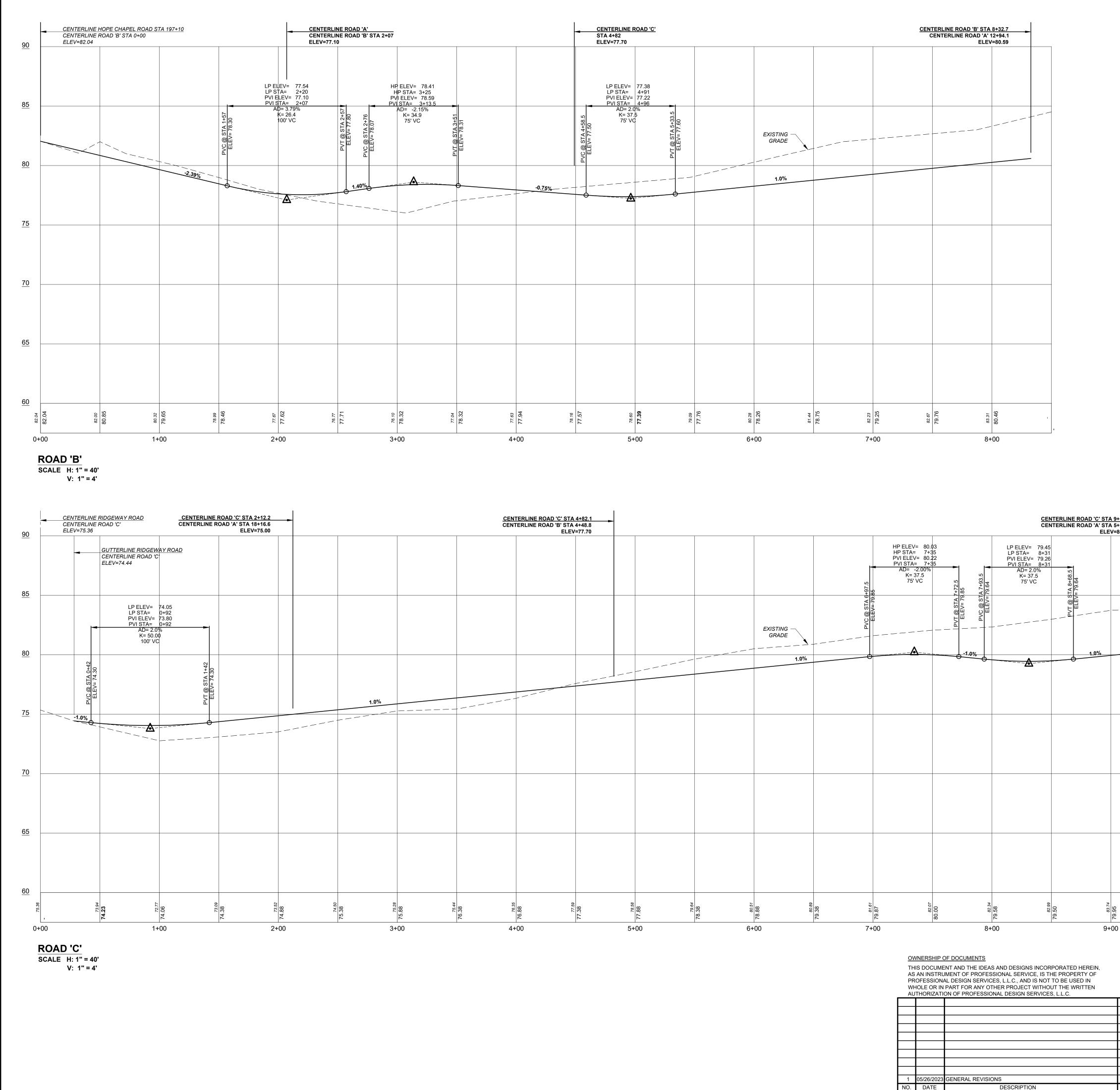
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	PROFESSIONAL DESIGN SERVICES, L.L.C.
	CONSULTING ENGINEERS, LAND SURVEYORS, PLANNERS, ENVIRONMENTAL SCIENTISTS, CONSTRUCTION SERVICES
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	PHONE 732 363 0060 FAX 732 363 0073 Engineering®pds-nj.com www.pds-nj.com
	NEW JERSEY STATE BOARD OF P.E. & L.S.
	CERTIFICATE OF AUTHORIZATION NO 24GA28125400

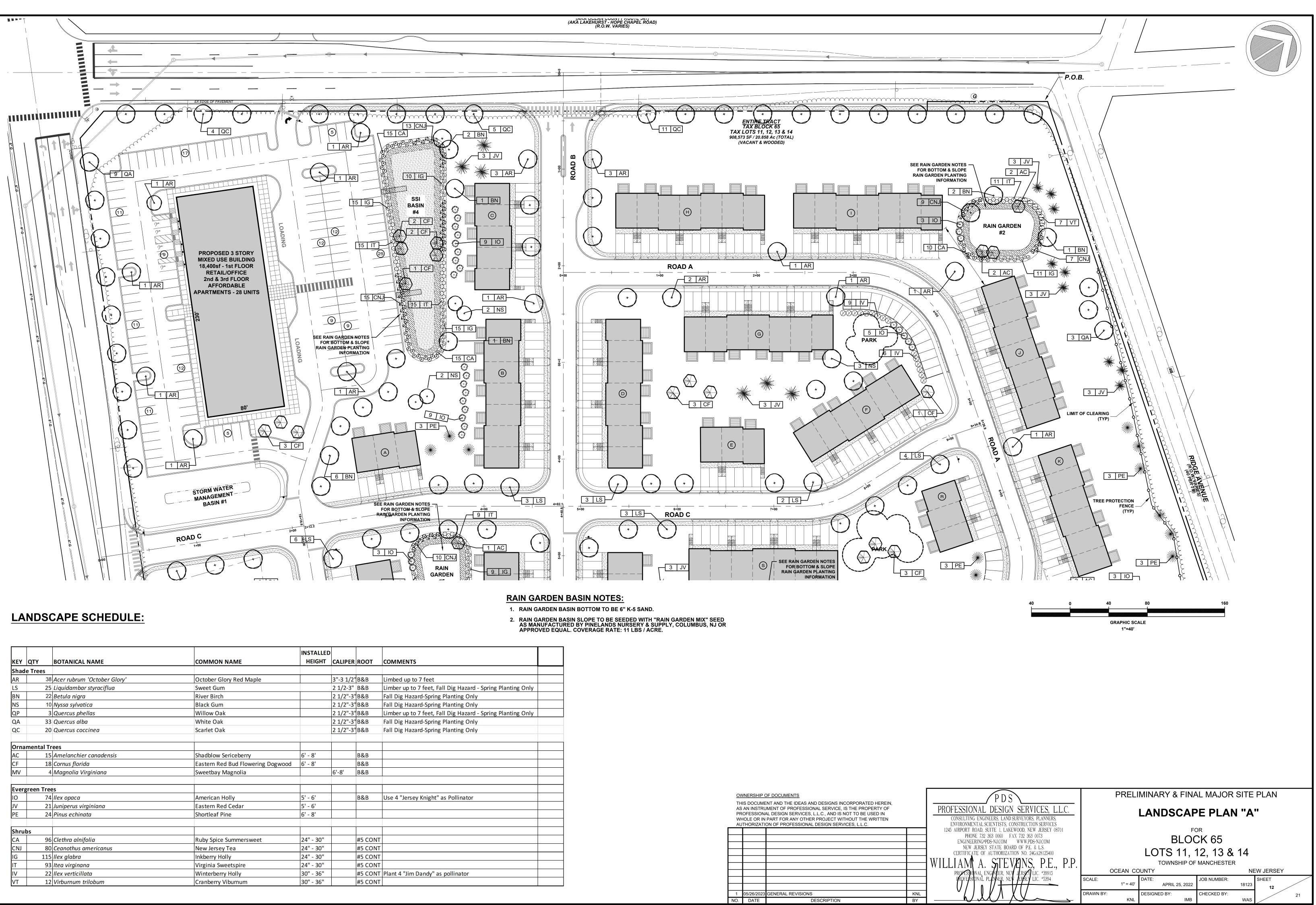


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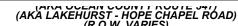


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KNL BY	WIL	CERTIFICATE OF AUTH	TEVENS, P.E., P.P.	LOTS 11, 12, 13 & 14         TOWNSHIP OF MANCHESTER         OCEAN COUNTY         NEW JERSEY         SCALE:         AS SHOWN         DATE:       APRIL 25, 2022         18123       11         DRAWN BY:       DESIGNED BY:         IMB       WAS

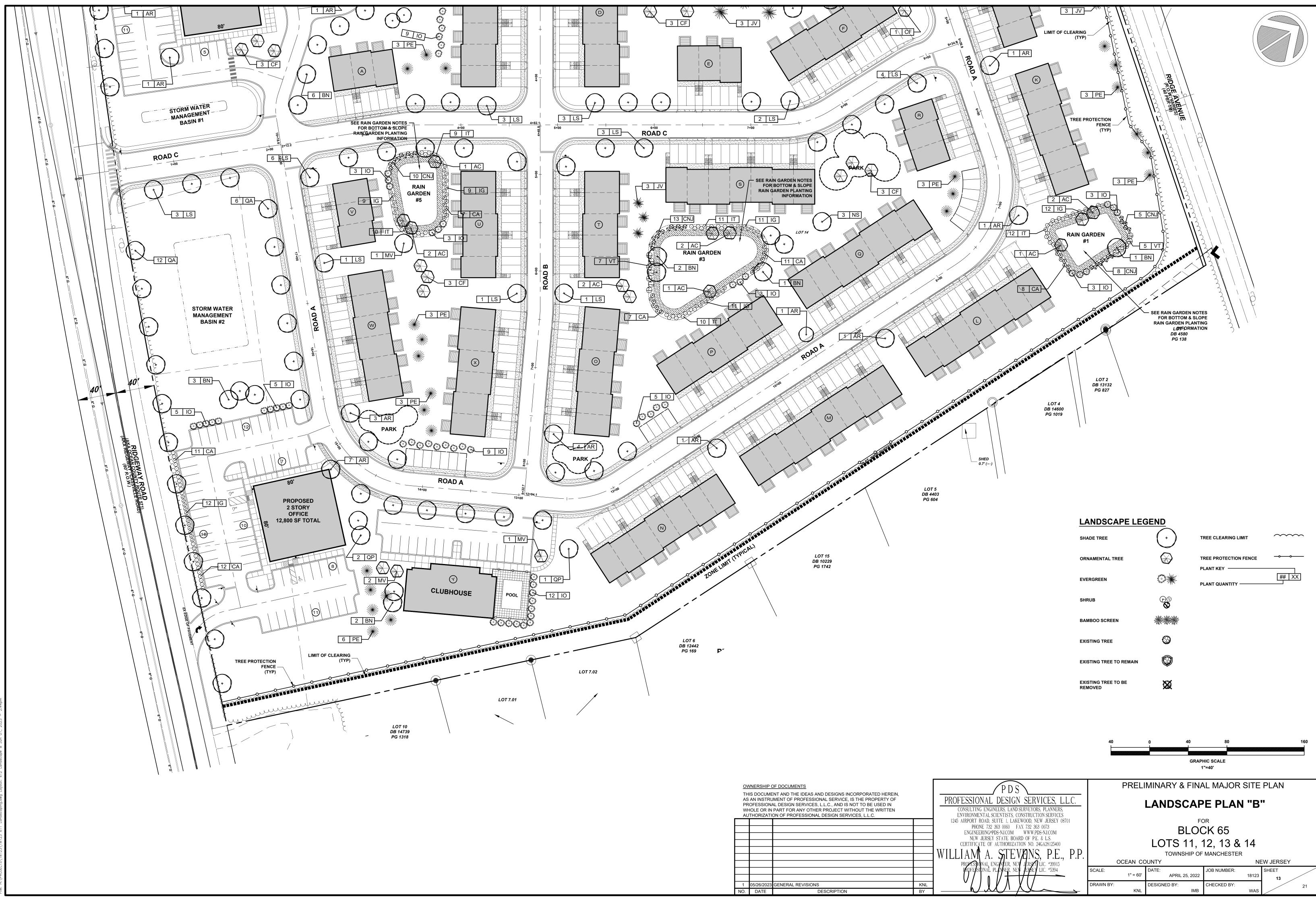


KEY	QTY	BOTANICAL NAME	COMMON NAME	INSTALLED HEIGHT	CALIPER	ROOT	COMMENTS
Shad	e Trees						
AR	38	Acer rubrum 'October Glory'	October Glory Red Maple		3"-3 1/2'	B&B	Limbed up to 7 fe
S	25	Liquidambar styraciflua	Sweet Gum		2 1/2-3"	B&B	Limber up to 7 fe
BN	22	Betula nigra	River Birch		2 1/2"-3'	B&B	Fall Dig Hazard-S
NS	10	Nyssa sylvatica	Black Gum		2 1/2"-3'	B&B	Fall Dig Hazard-S
QP	3	Quercus phellas	Willow Oak		2 1/2"-3'	B&B	Limber up to 7 fe
QA	33	Quercus alba	White Oak		2 1/2"-3'	B&B	Fall Dig Hazard-S
QC	20	Quercus coccinea	Scarlet Oak		2 1/2"-3'	B&B	Fall Dig Hazard-S
Orna	mental Ti	rees					
AC	15	Amelanchier canadensis	Shadblow Sericeberry	6' - 8'		B&B	
CF	18	Cornus florida	Eastern Red Bud Flowering Dogwood	6' - 8'		B&B	
MV	4	Magnolia Virginiana	Sweetbay Magnolia		6'-8'	B&B	
Ever	green Tre	es					
0	74	llex opaca	American Holly	5' - 6'		B&B	Use 4 "Jersey Kni
V	21	Juniperus virginiana	Eastern Red Cedar	5' - 6'			
PE	24	Pinus echinata	Shortleaf Pine	6' - 8'			
Shru	bs						
CA	96	Clethra alnifolia	Ruby Spice Summersweet	24" - 30"		#5 CONT	
CNJ	80	Ceanothus americanus	New Jersey Tea	24" - 30"		#5 CONT	
G	115	llex glabra	Inkberry Holly	24" - 30"		#5 CONT	
Т	93	ltea virginana	Virginia Sweetspire	24" - 30"		#5 CONT	
V	22	llex verticillata	Winterberry Holly	30" - 36"		#5 CONT	Plant 4 "Jim Danc
٧T	12	Virburnum trilobum	Cranberry Viburnum	30" - 36"		#5 CONT	



feet	
eet, Fall Dig Hazard - Spring Planting Only	
Spring Planting Only	
Spring Planting Only	
eet, Fall Dig Hazard - Spring Planting Only	
Spring Planting Only	
Spring Planting Only	
night" as Pollinator	
ndy" as pollinator	

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# LANDSCAPE NOTES

- 1. GENERAL NOTES
- A. THIS PLAN SHALL BE UTILIZED FOR LANDSCAPE AND TREE SAVE USES ONLY. PLEASE REFER TO SITE PLANS FOR CONSTRUCTION OF SITE IMPROVEMENTS.
- B. ALL TREES ARE DRAWN TO THEIR ANTICIPATED MATURE DRIPLINE.
- C. CONTRACTOR SHALL EXAMINE DRAWINGS AND REQUEST A MARKOUT OF FIELD CONDITIONS FOR SPECIFIC LOCATIONS OF UTILITIES, STRUCTURES, ETC. NOTIFY THE ENGINEER IN WRITING IMMEDIATELY, IN REFERENCE TO DISCREPANCIES OR LOCATION CONFLICTS.
- D. IN THE EVENT THAT PLANT QUANTITY DISCREPANCIES OR MATERIAL OMISSIONS OCCUR IN THE PLANTING SCHEDULE, THE PLAN SHALL SUPERSEDE.
- ALL PLANTING MATERIAL AND METHODS SHALL MEET OR EXCEED THE REQUIREMENTS OF THE MUNICIPAL ORDINANCES OF THE TOWNSHIP OF MANCHESTER AND ANSI Z-60.1 (CURRENT VERSION), "THE AMERICAN STANDARD FOR NURSERY STOCK," PUBLISHED BY THE AMERICAN ASSOCIATION OF NURSERYMEN. IN THE EVENT OF CONFLICT BETWEEN A.A.N. AND MUNICIPAL STANDARDS, THE MUNICIPAL REQUIREMENTS SHALL SUPERCEDE.
- ALL LANDSCAPING SHALL BE PLANTED SO AS TO NOT INTERFERE WITH UTILITY LINES, SIGHT TRIANGLES, UNDERGROUND UTILITIES, PUBLIC WALKWAYS OR OTHER EXISTING OR PROPOSED STRUCTURES. ALL PLANT MATERIAL PROPOSED WITHIN THE REQUIRED SIGHT DISTANCES OR SIGHT TRIANGLES ARE SELECTED SO AS TO NOT EXCEED A MATURE HEIGHT GREATER THAN 30" ABOVE THE ELEVATION OF THE ADJACENT ROADWAY. STREET TREES AND SHADE TREES PLANTED NEAR PEDESTRIAN OR VEHICULAR ACCESSES, OR WITHIN REQUIRED SIGHT DISTANCES / SIGHT TRIANGLE EASEMENTS SHALL NOT BE BRANCHED ANY LOWER THAN 7'-0" ABOVE GRADE, AND MUST BE APPROPRIATELY PRUNED. NO WOODY PLANTS, EXCEPT GROUND COVERS, ARE TO HAVE THEIR CENTERS CLOSER THAN 36" TO THE BACK OF THE CURB. NO STREET TREES ARE TO BE PLANTED IN SIGHT TRIANGLES IN ACCORDANCE WITH MANCHESTER TOWNSHIP ORDINANCE.
- 2. <u>PLANTING</u>
- A. SOIL MUST BE FROST-FREE, FRIABLE AND NOT MUDDY AT THE TIME OF PLANTING.
- B. BACKFILL MATERIAL FOR PLANTING PITS SHALL BE COMPOSED OF 70% TOPSOIL, 20% FULLY COMPOSTED COW OR HORSE MANURE AND 10% PEAT MOSS. TOPSOIL SHALL MEET NJDOT 2007 STANDARD SPECIFICATIONS SECTION 917.01, AND MAY BE FROM ON-SITE OR IMPORTED SOURCES. SOIL SHALL CONTAIN NO ACIDIC MARL, NOR ANY LARGE STONES.
- PLANTS SHALL BE SET TO ULTIMATE FINISHED GRADE SO THAT THEY WILL BE LEFT IN THE RELATIONSHIP TO THE SURROUNDING GROUND AS THEY HAD, PRIOR TO BEING DUG. IF EVIDENCE OF SATURATED SOILS IS ENCOUNTERED DURING EXCAVATION OF THE PLANTING PITS. UPON DIRECTION BY THE ENGINEER. PLANTS SHALL BE SET SO THAT THEIR ROOT CROWNS ARE APPROXIMATELY THREE INCHES ABOVE THE FINAL GRADE, WITH TOPSOIL AND MULCH GENTLY MOUNDED TO AVOID EXCESSIVE DRYING AT THE SURFACE. UNDER NO CIRCUMSTANCES SHALL PLANTINGS AT RELATIVELY DRY LOCATIONS BE PERFORMED IN A MOUNDED MANNER.
- THE CORD BINDING THE BALL OF ALL BALLED AND BURLAPPED (B&B) PLANTS SHALL BE CUT AND REMOVED, AND BURLAP ON THE UPPER ½ OF THE ROOT BALL SHALL BE REMOVED. PLANTS WITH SYNTHETIC NON-DEGRADEABLE ROOT BALL WRAPS SHALL NOT BE ACCEPTABLE.
- E. ALL WIRE BASKETS MUST BE REMOVED PRIOR TO PLANTING.
- F. ALL PROPOSED TREES SHALL BE SET IN BEDS MULCHED TO THE LIMIT OF THEIR PLANTING PITS. EXCEPT AS NOTED ALL OTHER TYPES OF PLANTINGS SHALL BE SET IN CONTINUOUS. MASSED PLANTING BEDS, RATHER THAN ISOLATED INDIVIDUALS, ALL TREE AND SHRUB BEDS SHALL RECEIVE A 3" THICK APPLICATION OF A THOROUGHLY COMPOSTED ORGANIC MULCH FREE FROM ANY OBJECTIONABLE OR FOREIGN MATERIALS.
- G. THE MULCH AT THE OUTER PERIMETER OF PLANTING PITS AND BEDS SHALL BE PREPARED SO THAT A 2" HIGH RIM TO RETAIN MOISTURE IS CONSTRUCTED. THE THICKNESS OF THE MULCH SHALL BE FEATHERED WITHIN 3" OF STEMS OR TRUNK . SO THAT NO MULCH IS IN DIRECT PHYSICAL CONTACT WITH THE PLANTS' BRANCHING OR TRUNKS. PLANTING OF GROUNDCOVERS MAY BE SUBSTITUTED FOR MULCH IN PARKING LOT ISLANDS.
- H. TREES SHALL NOT BE GUYED, EXCEPT IF AND WHERE REQUIRED BY THE MUNICIPALITY; WHEREIN TREES GREATER THAN FIVE FEET IN HEIGHT MAY BE STAKED AND GUYED PER THE DETAILS.
- 3. PLANT MATERIAL A. NO PLANT SUBSTITUTION SHALL BE ALLOWED WITH REGARD TO SIZE, SPECIES, NAMED VARIETY OR CULTIVAR. WITHOUT PRIOR PERMISSION FROM THE TOWNSHIP TREE SPECIALIST. ALL SUBSTITUTIONS SHALL BE SUBMITTED TO THE TOWNSHIP TREE
- SPECIALIST FOR REVIEW AND APPROVAL PRIOR TO INSTALLATION. ALL PLANTS SHALL BE DUG, PACKED, TRANSPORTED AND HANDLED WITH THE UTMOST CARE TO ENSURE ADEQUATE PROTECTION FROM INJURY DESICCATION.
- C. ALL PLANTS SHALL BE FREE FROM DISEASE AND INFESTATION, AND ALL LEGALLY REQUIRED AGRICULTURAL CERTIFICATIONS
- ALL PLANTS SHALL BE PRUNED TO ENHANCE VIGOR PRIOR TO, OR UPON INSTALLATION,

## **TREE REMOVAL AND LANDSCAPE NOTES**

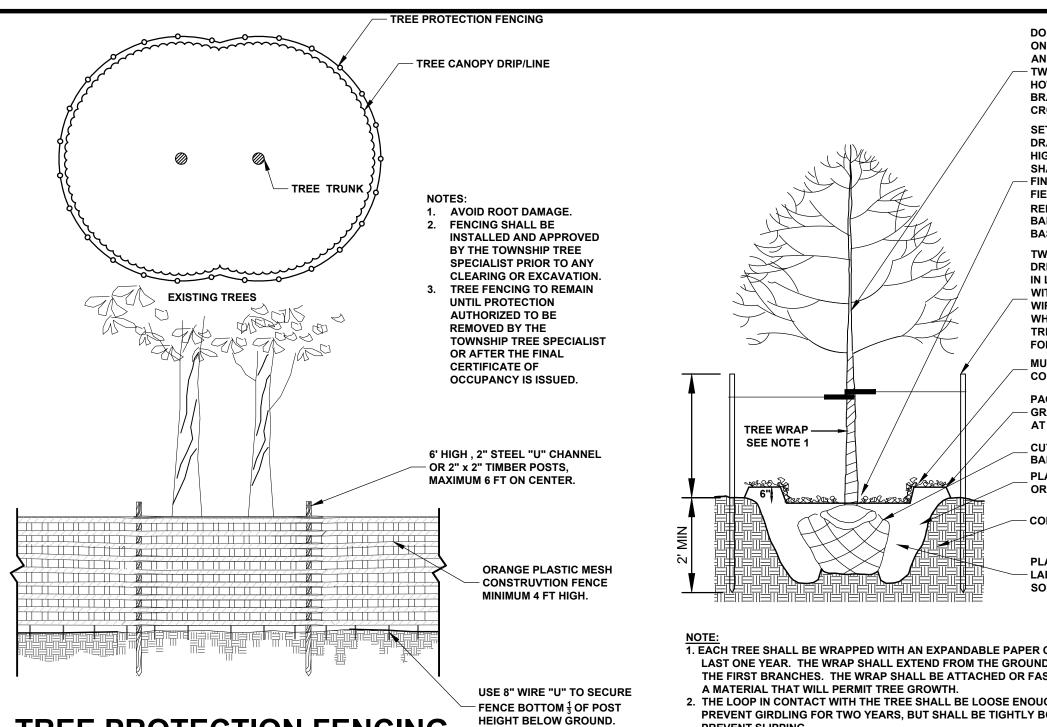
- 1. THE CONTRACTOR MUST PROVIDE WRITTEN NOTICE TO THE MANCHESTER TOWNSHIP FORESTER A MINIMUM OF 48 HOURS PRIOR TO COMMENCEMENT OF TREE REMOVAL OPERATIONS.
- 2. THE CONTRACTOR MUST COMPLY WITH ALL PROVISIONS OF MANCHESTER TOWNSHIP ORDINANCE 3. THE EXISTING TREES MUST BE PROTECTED BY INSTALLATION OF A 4 FOOT ORANGE CONSTRUCTION FENCING. THE FENCING MUST BE PLACED AT THE LIMIT OF CLEARING PRIOR TO COMMENCEMENT OF TREE REMOVAL OPERATIONS.
- 4. THE TREE PROTECTION FENCING SHALL BE INSTALLED AND APPROVED BY THE TOWNSHIP TREE SPECIALIST PRIOR TO ANY CLEARING OR EXCAVATION. TREE FENCING TO REMAIN UNTIL PROTECTION AUTHORIZED TO BE REMOVED BY THE TOWNSHIP TREE SPECIALIST OR AFTER THE FINAL CERTIFICATE OF OCCUPANCY IS ISSUED.
- . THE RETAINED TREES MUST BE IDENTIFIED BY FLAGGING EACH WITH RIBBON. THE CONTRACTOR MUST CONTACT THE MANCHESTER TOWNSHIP FORESTER TO SCHEDULE AN INSPECTION.
- 6. ALL REMAINING TREES ARE TO BE PRUNED AS NECESSARY IN ACCORDANCE WITH INDUSTRY STANDARDS BY A NJ CERTIFIED TREE EXPERT.
- 7. THE CONTRACTOR MUST COMPLY WITH ALL PROVISIONS OF MANCHESTER TOWNSHIP TREE REMOVAL ORDINANCE CHAPTER 403.
- 8. THE MANCHESTER TOWNSHIP FORESTER SHALL REQUIRE DEAD, BROKEN BRANCH AND SELECT RISK TREE REMOVAL ON REMAINING SPECIMEN TREES BEFORE PERFORMANCE BOND RELEASE.
- 9. THERE ARE NO SPECIMEN TREES LOCATED ON THIS SITE.
- 10. ALL TREE STUMPS AND OTHER TREE PARTS OR OTHER DEBRIS SHALL BE REMOVED FROM THE SITE AND DISPOSED OF IN ACCORDANCE WITH THE LAND. NO TREE STUMPS, PORTIONS OF A TREE TRUNK OR LIMBS SHALL BE BURIED ANYWHERE IN THE DEVELOPMENT.

WHILE RETAINING NATURAL GROWTH HABIT OF THE PLANTS. THE CENTRAL LEADER SHALL NOT BE CUT; PLANTS PROVIDED IN THIS CONDITION SHALL NOT BE ACCEPTED. DAMAGED, BROKEN OR CONFLICTING BRANCHES SHALL BE PRUNED CLEANLY, FLUSH WITH THE MAIN FRUNK OR BRANCH.

E. ALL PLANTS SHALL BE NURSERY-GROWN AND TAGGED WITH A DURABLE LABEL INDICATING THE GENUS, SPECIES, SPECIFIED VARIETY OR CULTIVAR, PLANT PATENT NUMBER (IF A PATENTED TREE), AS WELL AS CULTURAL REQUIREMENTS, INCLUDING WATERING AND FERTILIZATION.

4. MAINTENANCE

- A. ALL PLANTING SHALL BE WATERED AS NECESSARY FOR SOUND HORTICULTURAL PRACTICE DURING THE FIRST GROWING SEASON, TO ENSURE THEIR PROPER ESTABLISHMENT ALL TREES IN A SCREENING AREA SHALL BE WATERED WEEKLY THROUGH THE FIRST GROWING SEASON
- B. IN GENERAL, SHRUBS ARE TO BE PLANTED AT INTERVALS WHICH WILL ALLOW THEM TO FULLY DEVELOP INTO CONTINUOUS MASSES OF THE INDIVIDUAL SPECIES. SHEARING OR SHAPING IS ONLY REQUIRED OR DESIRABLE WHERE DEAD OR CONFLICTING BRANCHING DEVELOPS.
- C. STAKING SHALL BE ATTACHED TO THE TREE WITH TWELVE GAUGE GALVANIZED WIRE COVERED WITH RUBBER OR PLASTIC HOSE, OR TREE TIES ESPECIALLY MANUFACTURED FOR THIS PURPOSE. THE LOOP IN CONTACT WITH THE TREE SHALL BE LOOSE ENOUGH TO PERMIT GROWTH AND PREVENT GIRDLING FOR TWO YEARS, BUT SHALL BE TIGHTLY BOUND TO THE STAKE TO PREVENT SLIPPING.
- D. EACH TREE SHALL BE WRAPPED WITH AN EXPANDABLE PAPER OR CLOTH TREATED TO LAST ONE YEAR. THIS WRAP SHALL EXTEND FROM THE GROUND LEVEL UP THE TRUNK TO THE FIRST BRANCHES. THIS WRAP SHOULD BE ATTACHED OR FASTENED AT EACH END WITH A MATERIAL THAT WILL PERMIT TREE GROWTH.
- E. A PERMANENT IRRIGATION SYSTEM SHALL BE INSTALLED TO ENSURE PROPER ESTABLISHMENT AND MAINTENANCE OF ALL PLANTINGS. THE APPLICANT SHOULD ADDRESS THE BOARD REGARDING THEIR PLANS TO INSTALL A PRIVATE WELL TO PROVIDE IRRIGATION WATER TO THE SITE.
- F. A PRIVATE WELL SHALL BE PROVIDED TO SUPPLY IRRIGATION WATER TO THE SITE. 5. MISCELLANEOUS
- D. NO TOPSOIL SHALL BE REMOVED FROM THE SITE OR USED AS SPOIL. TOPSOIL MOVED DURING THE COURSE OF CONSTRUCTION SHALL BE REDISTRIBUTED SO AS TO PROVIDE AT LEAST FOUR (4) INCHES OF SPREAD COVER TO ALL SEEDING AND PLANTING AREAS OF THE SITE AND SHALL BE STABILIZED BY SEEDING OR PLANTING. IN THE EVENT THAT THE QUANTITY OF TOPSOIL AT THE SITE IS INSUFFICIENT TO PROVIDE FOUR (4) INCHES OF COVER FOR ALL SEEDING AND PLANTING AREAS, THE DEVELOPER SHALL PROVIDE SUCH A COVER. TOPSOIL SHALL BE APPROVED BY THE TOWNSHIP ENGINEER.
- E. TOPSOIL SHALL BE PROVIDED ON ALL LAWN AND PLANTING AREAS. TOPSOIL SHALL EITHER BE EXISTING MATERIAL THAT HAS BEEN STRIPPED AND STOCKPILED FOR REUSE OR NEWLY FURNISHED MATERIAL.
- F. STREET AND PARKING LOT TREES SHALL HAVE NO BRANCHES LOWER THAN 7' ABOVE GRADE
- G. ALL DEAD OR SEVERELY DECLINING PLANTS SHALL BE REPLANTED WITHIN THE NEXT GROWING SEASON DURING PERFORMANCE AND MAINTENANCE BOND PERIODS.
- H. THE TREE PROTECTION FENCING SHALL BE INSTALLED AND APPROVED BY THE TOWNSHIP TREE SPECIALIST PRIOR TO ANY CLEARING OR EXCAVATION. TREE FENCING TO REMAIN UNTIL PROTECTION AUTHORIZED TO BE REMOVED BY THE TOWNSHIP TREE SPECIALIST OR AFTER THE FINAL CERTIFICATE OF OCCUPANCY IS ISSUED.



## **TREE PROTECTION FENCING** NOT TO SCALE

LEADER OR TRUNK. CONTACT WITH TREE TRUNK THE TREE TRUNK PURPOSE. SEE NOTE 1 5 8220 くちちょうしょう PERKERS PLANTING PIT MASS 

1. THE LOOP IN CONTACT WITH THE TREE SHALL BE LOOSE ENOUGH TO PERMIT GROWTH AND PREVENT GIRDLING FOR TWO YEARS, BUT SHALL BE TIGHTLY BOUND TO THE STAKE TO PREVENT SLIPPING.

**EVERGREEN TREE PLANTING** NO SCALE

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1	05/26/2023	GENERAL REVISIONS
NO.	DATE	DESCRIPTION

THIS DOCUMENT AND THE IDEAS AND DESIGNS INCORPORATED HEREIN,

DO NOT HEAVILY PRUNE TREE AT PLANTING. PRUNE ONLY CROSSOVER LIMBS, CO-DOMINANT LEADERS AND BROKEN OR DEAD BRANCHES. SOME INTERIOR TWIGS AND LATERAL BRANCHES MAY BE PRUNED; HOWEVER DO NOT REMOVE THE TERMINAL BUDS OF BRANCHES THAT EXTEND TO THE EDGE OF THE CROWN. NEVER CUT CENTRAL LEADER OR TRUNK. SET ROOT BALL FLUSH TO GRADE. IN POORLY

DRAINING SOILS, SET ROOT BALL SEVERAL INCHES HIGHER THAN GRADE. AFTER SETTLEMENT, TREE SHALL BE PLUMB AND BEAR SAME RELATIONSHIP TO - FINISHED GRADE AS IT DID TO ITS NURSERY AND FIELD GROWN GRADE. CAREFULLY CUT AND REMOVE BURLAP AND TWINE FROM TOP 1/3 OF ROOT BALL. AND/OR CAREFULLY CUT TOP BANDS OF WIRE BASKET FROM TOP 1/3 OF ROOT BALL. TWO 2"x2" MINIMUM STAKES PLACED OUTSIDE HOLE.

DRIVEN 2' MINIMUM INTO UNDISTURBED SOIL, PLACED IN LINE WITH PREVAILING WINDS. ATTACH TO TREE WITH A DOUBLE STRAND OF #12 GAUGE GALVANIZED WIRE COVERED BY RUBBER OR PLASTIC HOSE WHERE THE WIRE COMES INTO CONTACT WITH THE TREE, OR TREE TIES ESPECIALLY MANUFACTURED FOR THIS PURPOSE. SEE NOTE 2 MULCH 4" MINIMUM; DO NOT PLACE MULCH IN

**CONTACT WITH TREE TRUNK** PACKED SAUCER SHALL BE 4" HIGHER THAN FINISHED

- GRADE. SAUCERS ON SLOPES SHALL BE LEVEL AT THE TOP & PERPENDICULAR TO THE TREE TRUNK

\_ CUT & REMOVE BURLAP AND STRING FROM TOP  $rac{1}{3}$  OF ROO PLANTING MIXTURE INCORPORATING A MINIMUM 25%

ORGANIC MATTER BY VOLUME - COMPACTED SUBGRADE

PLANTING HOLE SHALL BE A MINIMUM OF 12" LARGER IN DIAMETER AND 6" DEEPER THAN THE SOIL BALL OR ROOT MASS

- 1. EACH TREE SHALL BE WRAPPED WITH AN EXPANDABLE PAPER OR CLOTH TREATED TO LAST ONE YEAR. THE WRAP SHALL EXTEND FROM THE GROUND LEVEL UP THE TRUNK TO
- THE FIRST BRANCHES. THE WRAP SHALL BE ATTACHED OR FASTENED AT EACH END WITH

TREE PLANTING

NOT TO SCALE

2. THE LOOP IN CONTACT WITH THE TREE SHALL BE LOOSE ENOUGH TO PERMIT GROWTH AND PREVENT GIRDLING FOR TWO YEARS, BUT SHALL BE TIGHTLY BOUND TO THE STAKE TO PREVENT SLIPPING.

DO NOT HEAVILY PRUNE TREE AT PLANTING. PRUNE ONLY CROSSOVER LIMBS, CO-DOMINANT LEADERS AND BROKEN OR DEAD BRANCHES. SOME INTERIOR TWIGS AND - LATERAL BRANCHES MAY BE PRUNED: HOWEVER DO NOT REMOVE THE TERMINAL **BUDS OF BRANCHES THAT EXTEND TO THE** EDGE OF THE CROWN. NEVER CUT CENTRAL

- FINISHED GRADE AT CROWN OF ROOT MULCH 4" MINIMUM; DO NOT PLACE MULCH IN

PACKED SAUCER SHALL BE 4" HIGHER THAN FINISHED GRADE. SAUCERS ON SLOPES SHALL BE LEVEL AT THE TOP AND PERPENDICULAR TO

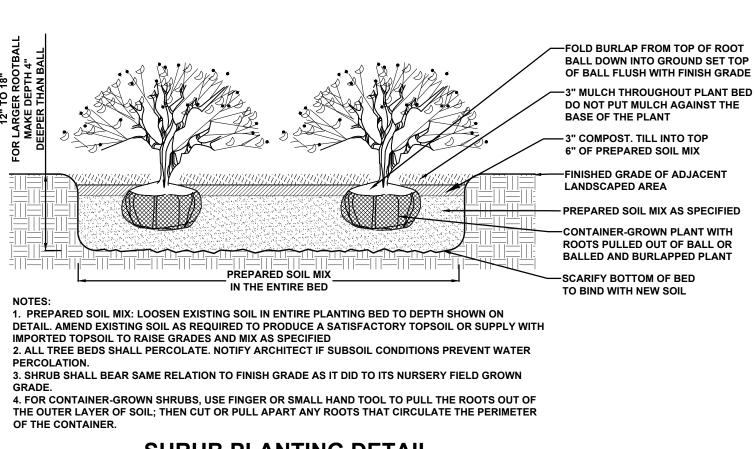
TWO 2"x2" MINIMUM STAKES PLACED OUTSIDE HOLE, DRIVEN 2' MINIMUM INTO UNDISTURBED SOIL, PLACED IN LINE WITH PREVAILING WINDS. ATTACH TO TREE WITH A DOUBLE STRAND OF - #12 GAUGE GALVANIZED WIRE COVERED BY RUBBER OR PLASTIC HOSE WHERE THE WIRE COMES INTO CONTACT WITH THE TREE, OR TREE TIES ESPECIALLY MANUFACTURED FOR THIS

CUT AND REMOVE BURLAP AND STRING FROM TOP ½ OF ROOT BALL; ALL WIRE BASKETS TO BE REMOVED PRIOR TO BACKFILLING OF THE

PLANTING MIXTURE INCORPORATING A MINIMUM **25% ORGANIC MATTER BY VOLUME** 

PLANTING HOLE SHALL BE A MINIMUM OF 12" LARGER IN DIAMETER AND 6" DEEPER THAN THE SOIL BALL OR ROOT

COMPACTED SUBGRADE

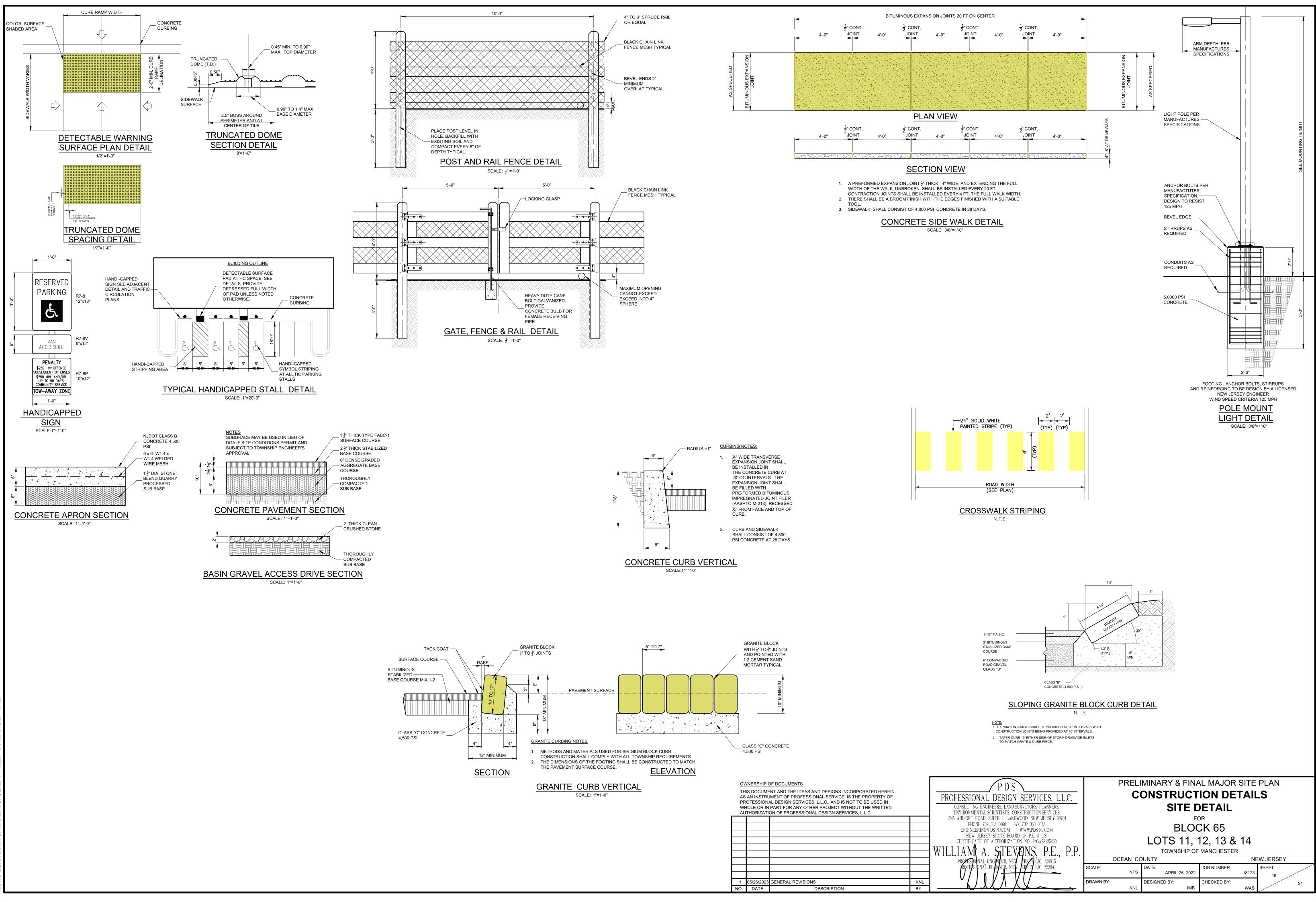


SHRUB PLANTING DETAIL NOT TO SCALE

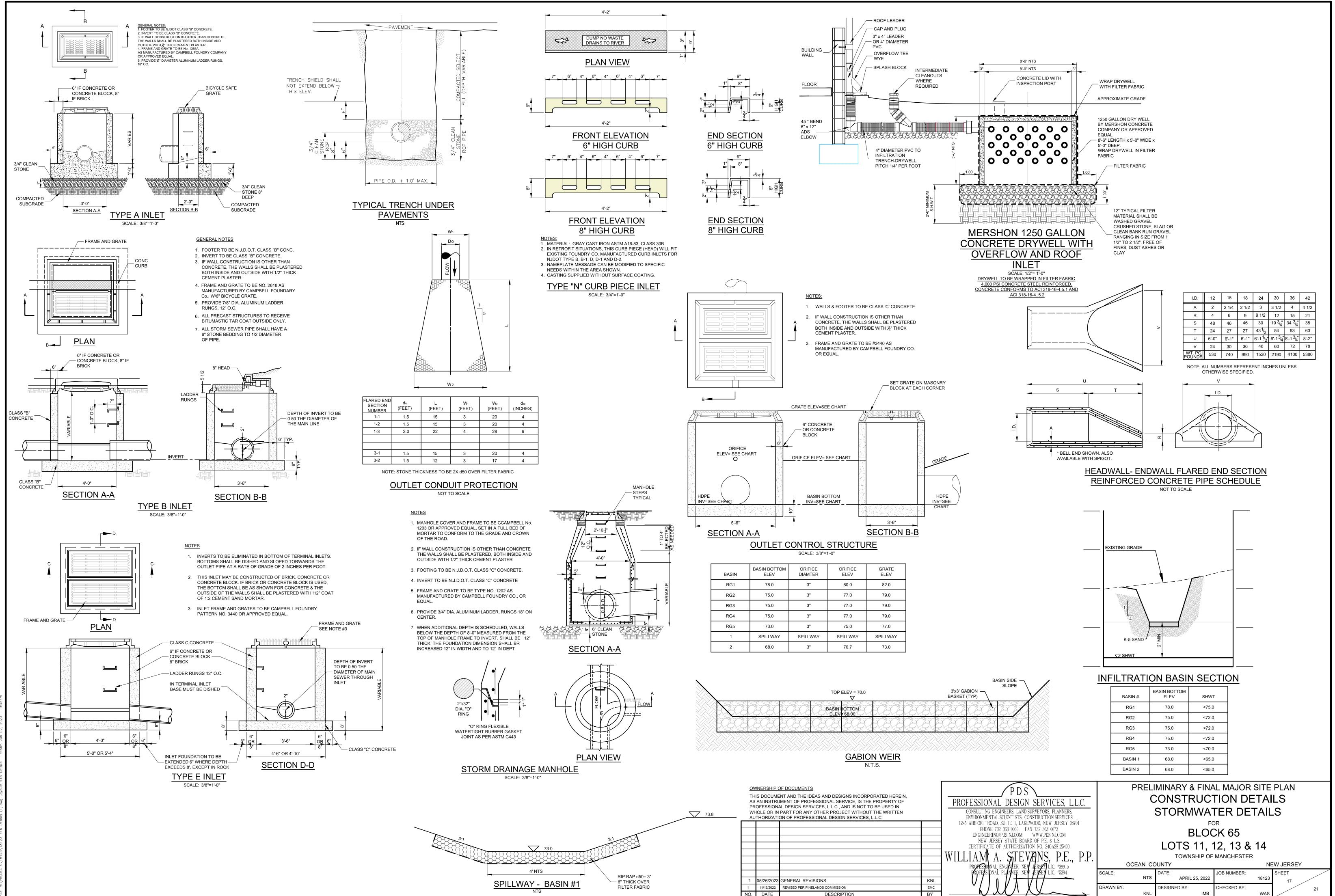
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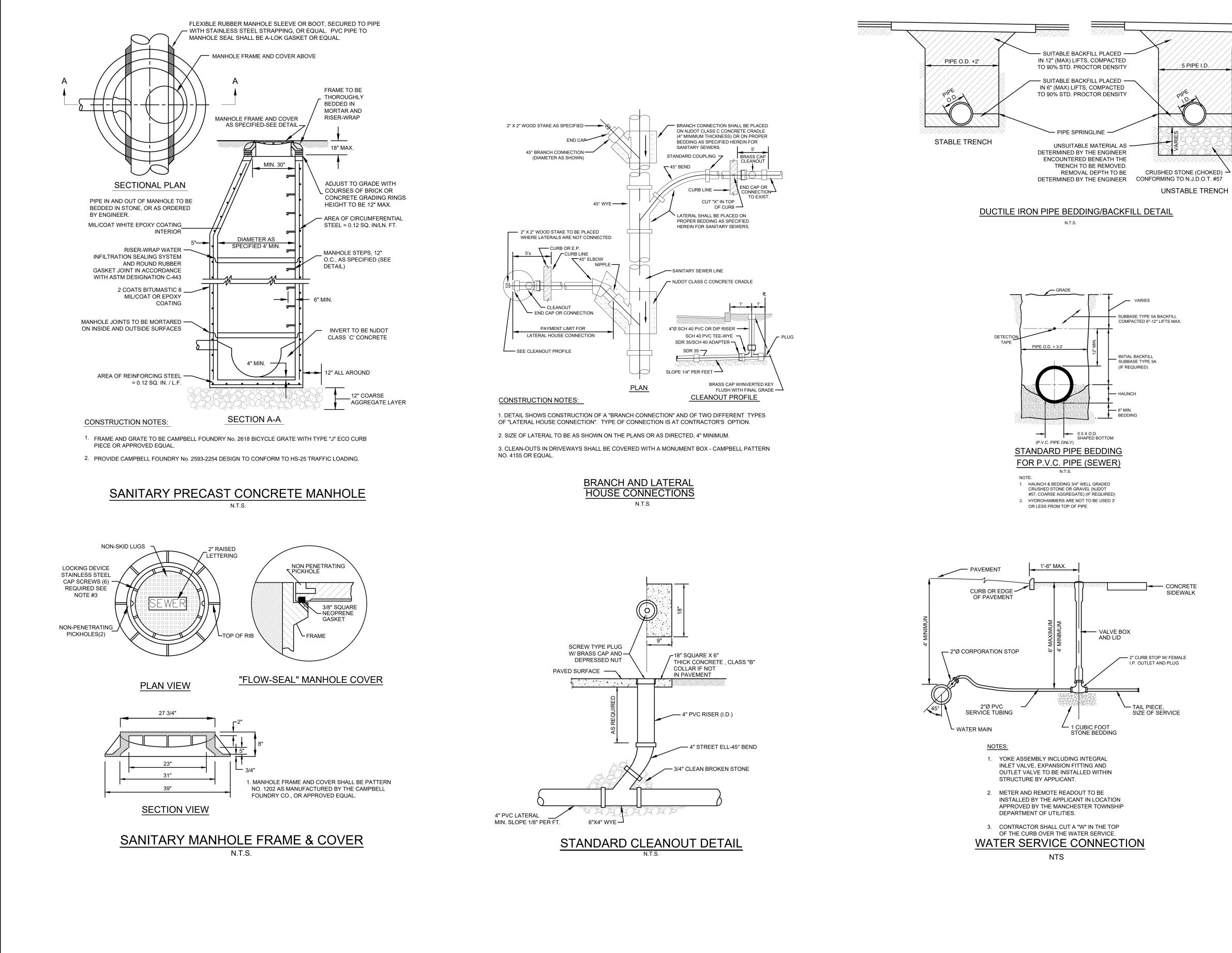


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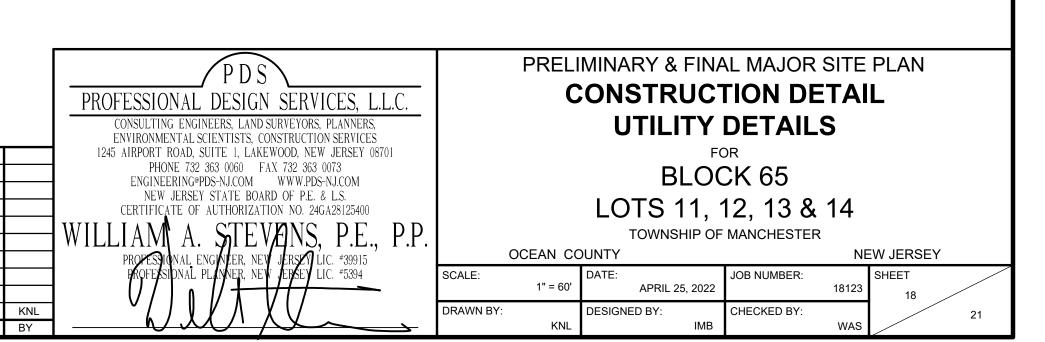


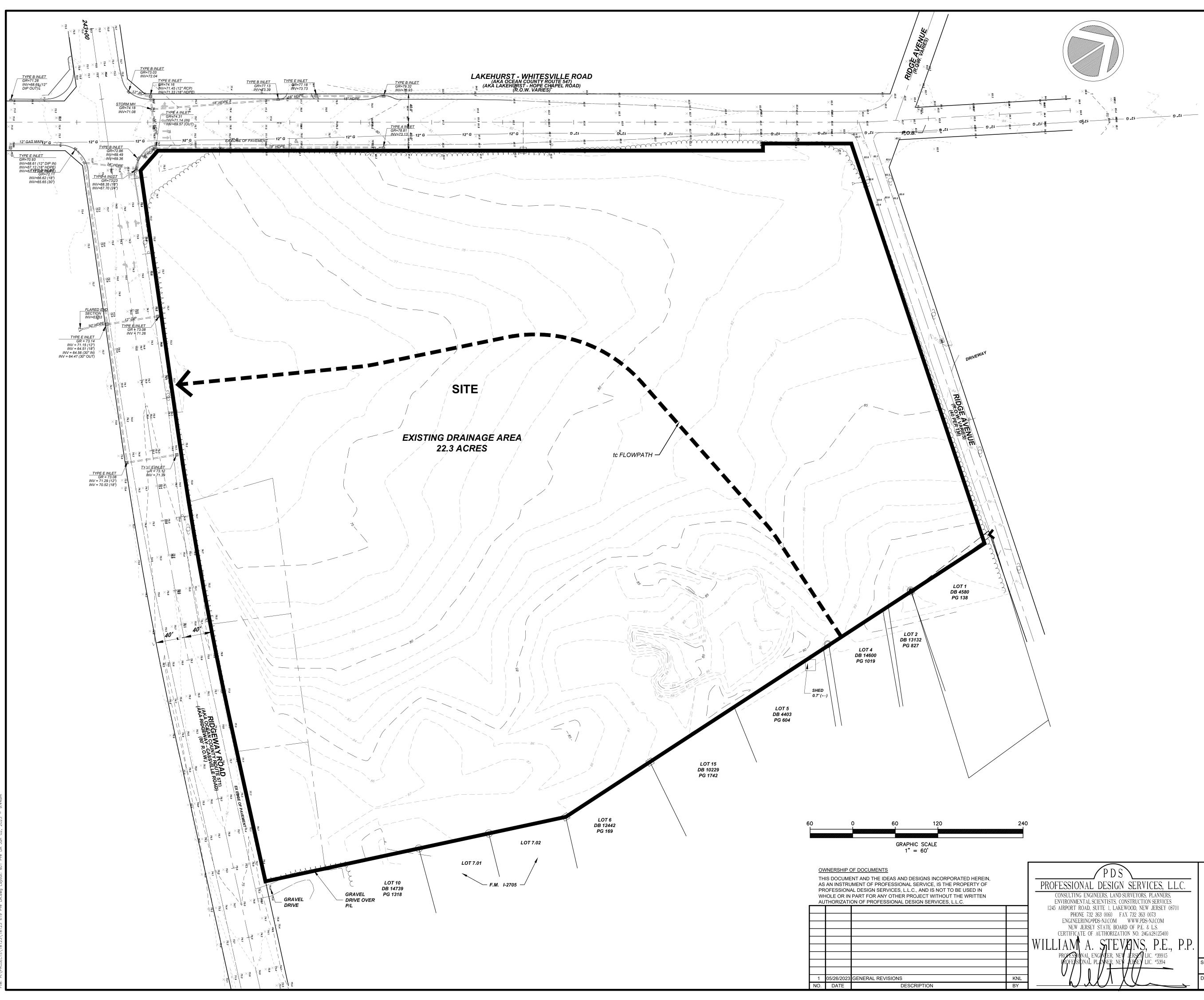


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TYLER PIPE, CAST -----IRON VALVE BOX, TWO EXISTING -PIECE, 6855 SERIES - FINISHED GRADE ROAD SURFACE LID MARKED "WATER" OR APPROVED EQUAL <sup>2</sup> SIDEWALK — 7 CUBIC FEET OF GRAVEL AROUND HYDRANT DRIP CONCRETE THRUST BLOCKING (SEE TABLE OF -OPENING FOR - 6"Ø GATE VALVE HYDRANT DRIP THRUST BLOCKS) DEPTH: 1'-3" WATER MAIN -- WIDTH: 1'-3" MIN. 12"x6" TEE (SEE UTILITY PLANS) CONC. BLOCK POURED AGAINST 4" MIN. UNDISTURBED EARTH. (SEE TABLE OF PUSH ON JOINT (TYP.) W/ THRUST THRUST BLOCKS) BLOCKS (RESTRAINT JOINTS ARE -1'-3" MIN ----ACCEPTABLE ALTERNATE SUBJECT TO REVIEW BY AUTHORITY ENGINEER) NOTES: 1. HYDRANT TO BE MUELLER COMPANY SUPER CENTURION 250, MODEL A-423. FIRE HYDRANT DETAIL N.T.S.



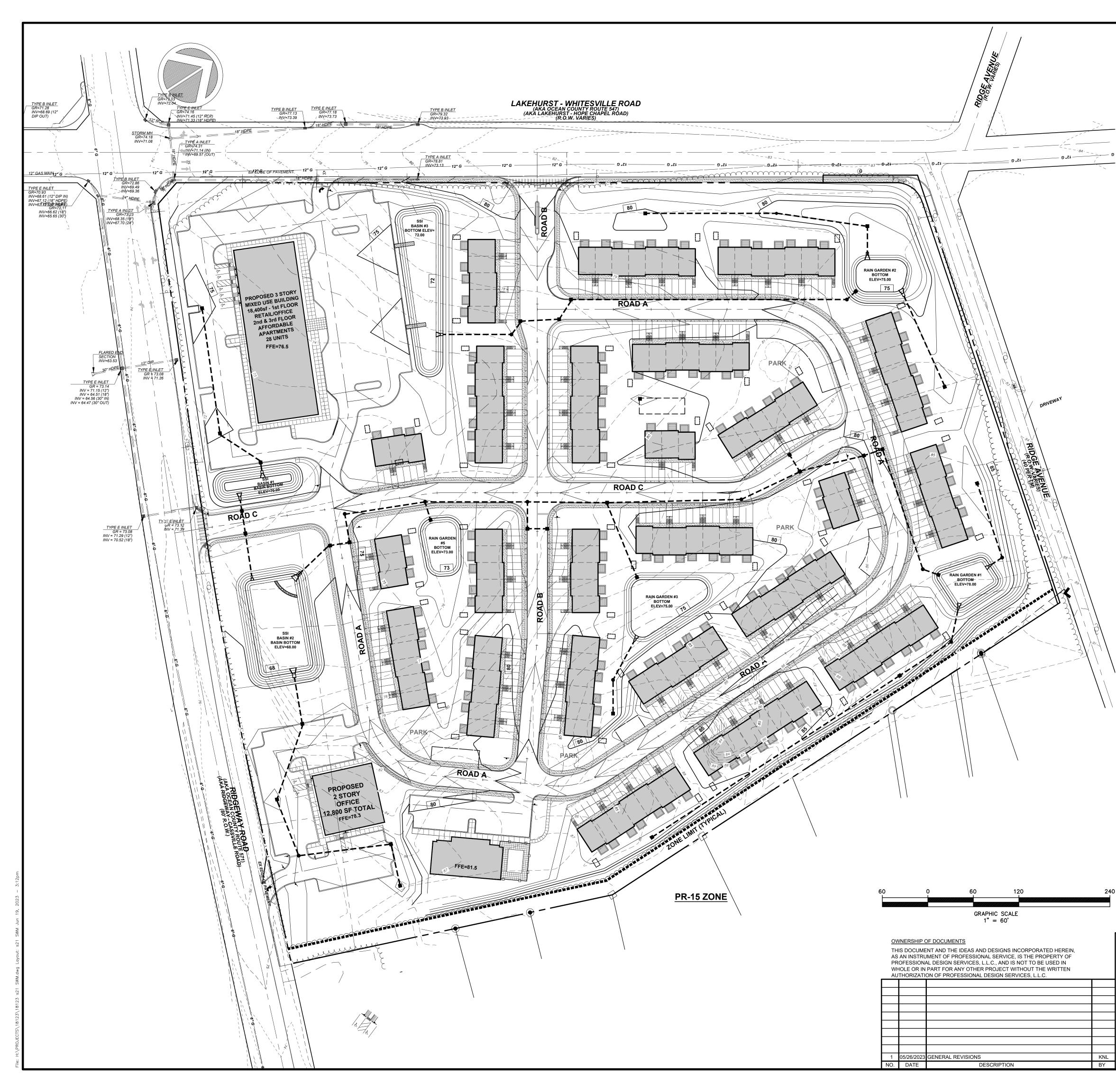


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	PROPESSIONAL ENGINEER, NEV JERSEY LIC. #39915		OCEAN CC	UNTY			NE	EW JERSEY
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	PROFESSIONAL PLANNER, NEW JEBSEY LIC. #5394	SCALE:	1" = 60'	DATE:		JOB NUMBER:	40400	SHEET
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## MAINTENANCE NOTES

- REQUIRED MAINTENANCE PLAN PROCEDURES:
- 1. COPIES OF THE MAINTENANCE PLAN MUST BE PROVIDED TO THE OWNER AND OPERATOR OF THE STORMWATER MANAGEMENT MEASURE AND TO ALL REVIEWING AGENCIES. A COPY SHOULD ALSO BE PROVIDED TO THE LOCAL MOSQUITO CONTROL OR EXTERMINATION COMMISSION UPON REQUEST.
- 2. THE TITLE AND DATE OF THE MAINTENANCE PLAN AND THE NAME AND/OR TITLE AND ADDRESS OF THE PERSON WITH OVERALL MAINTENANCE RESPONSIBILITY MUST BE RECORDED ON THE DEED OF THE PROPERTY ON WHICH THE STORMWATER MANAGEMENT MEASURE IS LOCATED. ANY CHANGE IN THE NAME OR TITLE MUST ALSO BE RECORDED ON THE DEED, PARTICULARLY IF THERE IS A CHANGE OF PROPERTY OWNERSHIP.
- 3. THE MAINTENANCE PLAN MUST BE EVALUATED FOR EFFECTIVENESS AT LEAST ANNUALLY AND MUST BE REVISE AS NEEDED. 4. A DETAILED, WRITTEN LOG OF ALL PREVENTATIVE AND CORRECTIVE MAINTENANCE PERFORMED AT THE STORMWATER MANAGEMENT MEASURE MUST BE KEPT, INCLUDING A RECORD
- OF ALL INSPECTIONS AND COPIES OF MAINTENANCE WORK ORDERS. 5. THE PERSON WITH OVERALL MAINTENANCE RESPONSIBILITY MUST MAKE THE MAINTENANCE PLAN, LOGS, AND OTHER RECORDS AVAILABLE FOR REVIEW UPON REQUEST FROM A PUBLIC ENTITY WITH JURISDICTION OVER ACTIVITIES AT THE SITE.

## **REQUIRED MAINTENANCE PLAN COMMENTS:**

1. ENTITY RESPONSIBLE FOR OVERALL MAINTENANCE OF THE STORMWATER MANAGEMENT MEASURE: HOMEOWNERS ASSOCIATION

#### 2. SCHEDULE OF MAINTENANCE INSPECTIONS AND MAINTENANCE TASKS: EXTENDED DETENTION BASIN

- A. GENERAL MAINTENANCE
- ALL EXTENDED DETENTION BASIN COMPONENTS EXPECTED TO RECEIVE AND/OR TRAP DEBRIS AND SEDIMENT MUST BE INSPECTED FOR CLOGGING AND EXCESSIVE DEBRIS AND SEDIMENT ACCUMULATION AT LEAST FOUR TIMES ANNUALLY AS WELL AS AFTER EVERY STORM EXCEEDING 1 INCH OF RAINFALL. SUCH COMPONENTS MAY INCLUDE BOTTOMS, TRASH RACKS, LOW FLOW CHANNELS, OUTLET STRUCTURES, RIPRAP OR GABION APRONS, AND INLETS, SEDIMENT REMOVAL SHOULD TAKE PLACE WHEN THE BASIN IS THOROUGHLY DRY. DISPOSAL OF DEBRIS AND TRASH SHOULD BE DONE AT SUITABLE DISPOSAL/RECYCLING SITES AND IN COMPLIANCE WITH ALL APPLICABLE LOCAL, STATE AND FEDERAL WASTE REGULATIONS.
- B. VEGETATED AREAS: Wowing and/or trimming of vegetation must be performed on a regular schedule based on specific site conditions. Grass should be mowed at least once a month during the growing season. Vegetate areas must also be inspected at least annually for erosion and scour. Vegetated areas should also be inspected at least annually for unwanted growth, which should be removed with minimum disruption to the bottom surface and remaining vegetation. When establishing or restoring vegetation, biweekly inspections of vegetation health should be performed during the first growing season or until the vegetation is established, inspections of vegetation health, density and diversity should be performed at least twice annually during BOTH THE GROWING AND NON-GROWING SEASONS. THE VEGETATIVE COVER SHOULD BE MAINTAINED AT 85%. IF VEGETATION HAS GREATER THE 50% DAMAGE, THE AREA SHOULD BE REESTABLISHED IN ACCORDANCE WITH THE ORIGINAL SPECIFICATIONS AND THE INSPECTION REQUIREMENTS PRESENTED ABOVE. ALL USE OF FERTILIZERS, MECHANICAL TREATMENTS, PESTICIDES AND OTHER MEANS TO ASSURE OPTIMUM VEGETATION HEALTH SHALL NOT COMPROMISE THE INTENDED PURPOSE OF THE EXTENDED DETENTION BASIN. ALL VEGETATION DEFICIENCIES SHOULD BE ADDRESSED WITHOUT THE USE OF FERTILIZERS AND PESTICIDES WHENEVER POSSIBLE.
- C. STRUCTURAL COMPONENTS: ALL STRUCTURAL COMPONENTS MUST BE INSPECTED FOR CRACKING, SUBSIDENCE, SPALLING, EROSION, AND DETERIORATION AT LEAST ANNUALLY.
- D. OTHER MAINTENANCE CRITERIA: THE OPERATION AND MAINTENANCE PLAN MUST INDICATE THE APPROXIMATE TIME THAT THE SYSTEM WOULD NORMALLY TAKE TO COMPLETELY DRAIN THE STORMWATER QUALITY DESIGN STORM RUNOFF VOLUME, THIS NORMAL DRAIN TIME SHOULD THEN BE USED TO EVALUATE THE SYSTEM'S ACTUAL PERFORMANCE. IF SIGNIFICANT INCREASES OR DECREASES IN THE DRAIN TIME ARE OBSERVED. THE SYSTEM'S OUTLET STRUCTURE, UNDERDRAIN SYSTEM, AND BOTH GROUNDWATER AND TAILWATER LEVELS MUST BE EVALUATED AND APPROPRIATE MEASURES TAKEN TO COMPLY WITH THE MAXIMUM DRAIN TIME REQUIREMENTS AND MAINTAIN THE PROPER FUNCTIONING OF THE BASIN.

#### INFILTRATION BASIN: A. GENERAL MAINTENANCE

ALL INFLITRATION BASIN COMPONENTS EXPECTED TO RECEIVE AND/OR TRAP DEBRIS AND SEDIMENT MUST BE INSPECTED FOR CLOGGING AND EXCESSIVE DEBRIS AND SEDIMENT ACCUMULATION AT LEAST FOUR TIMES ANNUALLY AS WELL AS AFTER EVERY STORM EXCEEDING 1 INCH OF RAINFALL. SUCH COMPONENTS MAY INCLUDE BOTTOMS, RIPRAP OR GABION APRONS, AND INFLOW POINTS. THIS APPLIES TO BOTH SURFACE AND SUBSURFACE INFILTRATION BASINS. SEDIMENT REMOVAL SHOULD TAKE PLACE WHEN THE BASIN IS THOROUGHLY DRY. DISPOSAL OF DEBRIS & TRASH SHOULD BE DONE AT SUITABLE DISPOSAL/RECYCLING SITES AND IN COMPLIANCE WITH ALL APPLICABLE LOCAL, STATE AND FEDERAL WASTE REGULATIONS. STUDIES HAVE SHOWN THAT READILY VISIBLE STORMWATER MANAGEMENT FACILITIES LIKE INFILTRATION BASINS RECEIVE MORE FREQUENT AND THOROUGH MAINTENANCE THAN THOSE IN LESS VISIBLE, MORE REMOTE LOCATIONS. READILY VISIBLE FACILITIES CAN ALSO BE INSPECTED FASTER AND MORE EASILY BY MAINTENANCE AND MOSQUITO CONTROL PERSONNEL.

## B. VEGETATED AREAS:

Wowing and/or trimming of vegetation must be performed on a regular schedule based on specific site conditions. Grass should be mowed at least once a month during the growing season. Vegetated areas must also be inspected at least annually for erosion and scour. The structure must be inspected for unwanted tree growth at least once a year. When establishing or restoring vegetation, biweekly inspections of vegetation health should be performed during the first growing season or until the vegetation is established. Once established, inspections of vegetation health, density and deversity should should be performed at least twice annually during both the growing and non-growing season. If vegetation has greater than 50% damage, the area should be reestablished in accordance with the original specifications and the inspection requirements presented by during the intervent properties and other and should be performed and the intervents of the intervent properties and other intervent properties and other properties the intervent properties and other properties and other properties of the intervent properties and other properties the intervent properties and other properties the intervent properties of the intervent properties and other properties of the properties of the properties of the properties of the intervent properties of the intervent properties of the pr TREATMENTS, PESTICIDES AND OTHER MEANS TO ASSURE OPTIMUM VEGETATION HEALTH MUST NOT COMPROMISE THE INTENDED PURPOSE OF THE BIORETENTION SYSTEM. ALL VEGETATION DEFICIENCIES SHOULD BE ADDRESSED WITHOUT THE USE OF FERTILIZERS AND PESTICIDES WHENEVER POSSIBLE. ALL VEGETATED AREAS SHOULD BE INSPECTED AT LEAST ANNUALLY FOR UNWANTED GROWTH. WHICH SHOULD BE REMOVED WITH MINIMUM DISTRUPTION TO THE REMAINING VEGETATION AND BASIN SUBSOIL.

#### C. STRUCTURAL COMPONENTS: ALL STRUCTURAL COMPONENTS MUST BE INSPECTED FOR CRACKING, SUBSIDENCE, SPALLING, EROSION AND DETERIORATION AT LEAST ANNUALLY.

- D. OTHER MAINTENANCE CRITERIA: THE OPERATION AND MAINTENANCE PLAN MUST INDICATE THE APPROXIMATE TIME THAT THE BASIN WOULD NORMALLY TAKE TO DRAIN THE STORMWATER QUALITY DESIGN STORM RUNOFF VOLUME BELOW THE GROUND SURFACE. THIS NORMAL DRAIN OR DRAWDOWN TIME SHOULD THEN BE USED TO EVALUATE THE BASIN'S ACTUAL PERFORMANCE. IF SIGNIFICANT INCREASES OR DECREASES IN THE DRAIN TIME ARE OBSERVED, THE BASIN'S BOTTOM SURFACE, SUBSOIL AND BOTH GROUNDWATER AND TAILWATER LEVELS MUST BE EVALUATED AND APPROPIATE MEASURES TAKEN TO COMPLY WITH THE MAXIMUM DRAIN TIME REQUIREMENTS AND MAINTAIN THE PROPER FUNCTIONING OF THE BASIN. THIS APPLIES TO BOTH SURFACE INFILTRATION BASINS. THE BOTTOM SAND LAYER IN A SURFACE INFILTRATION BASIN SHOULD BE INSPECTED AT LEAST MONTHLY AS WELL AS AFTER EVERY STORM EXCEEDING ONE INCH OF RAINFALL. THE PERMABILITY RATE OF THE SOIL BELOW THE BASIN MAY ALSO BE RETESTED PERIODICALY. IF THE WATER FAILS TO 72 HOURS AFTER THE END OF THE STORM, CORRECTIVE MEASURES MUST BE TAKEN. ANNUAL TILLING NY LIGHT EQUIPMENT CAN ASSIST IN MAINTAINING INFILTRATION CAPACITY AND DEPAK UP OF CONFECT. AND BREAK UP CLOGGED SURFACES.
- 3. PROBLEMS FOUND DURING MAINTENANCE INSPECTIONS SHALL BE CORRECTED. THESE INCLUDE THE RESTORATION OF ERODED AREAS, REPAIR OR REPLACEMENT OF STORMWATER MANAGEMENT MEASURE COMPONENTS, RESTORATION OF VEGETATION, AND REPAIR OR REPLACEMENT OF NON-VEGETATED LININGS.

4.	THE EQUIPMENT NECESSARY TO PERFORM THE MAIN	
	A. LAWN MOWING EQUIPMENT B. GAS POWERED TRIMMERS C. GAS POWERED BLOWERS D. RAKES E. SHOVELS F. PICKS	G. WHEEL BARROWS H. GAS POWERED HEDGE TRIMMERS I. CHAIN SAW J. FERTILIZER/PESTICIDE APPLICATION K. WASTER RECEPTACLES L. MAINTENANCE VEHICLES
5.	COST ESTIMATE OF THE INSPECTION AND MAINTENA	NCE TASKS:
	ITEM	EST. ANNUAL COST
1.	ITEM INSPECT BASIN, REMOVE AND DISPOSE OF SILT & DEBRIS 4 TIMES PER YEAR.	EST. ANNUAL COST \$800
1. 2.	INSPECT BASIN, REMOVE AND DISPOSE OF	

- INSPECT & MAINTAIN FENCE & BASIN ACCESS DRIVE 2 TIMES PER YEAR. \$300
- 5. DEEP TILL & RE-GRADE SAND BOTTOM ONCE EVERY 5 YEARS (\$1,000)

## TOTAL ANNUAL MAINTENANCE COST

MAINTENANCE PLAN CONSIDERATIONS ACCESS:

ALL STORMWATER MANAGEMENT MEASURES COMPONENTS MUST BE READILY ACCESSIBLE FOR INSPECTION AND MAINTENANCE. THEREFORE, ACCESS MUST BE PROVDED TO THE ENTRE STORMWATER MEASURE VIA ROADWAYS AND PATHS. TREES, SHRUBS, AND UNDERBRUSH MUST BE PRUNED OR TRIMMED AS NECESSARY TO MAINTAIN THIS ACCESS. THIS INCLUDES PATHWAYS THROUGH THE VEGETATION ALONG PERMANENT POOL PERIMETERS, INCLUDING AQUATIC BENCHES, TO ALLOW FOR THE INSPECTION AND CONTROL OF MOSQUITO BREEDING .:

\$200

\$2,450

INSPECTION AND MAINTENANCE EASEMENTS CONNECTED TO THE STREET OR RIGHT-OF-WAY SHOULD BE PROVIDED AROUND THE ENTIRE FACILITY. THE EXACT LIMITS OF THE EASEMENTS AND RIGHTS-OF-WAY SHOULD BE SPECIFIED ON THE PROJECT PLANS AND INCLUDED IN THE MAINTENANCE PLAN. ACCESS ROADS AND GATES SHOULD BE WIDE ENOUGH TO ALLOW PASSAGE OF NECESSARY MAINTENANCE VEHICLES AND EQUIPMENT, INCLUDING TRUCKS, BACKHOES, GRASS MOWERS, AND MOSQUITO CONTROL EQUIPMENT. IN GENERAL, A MINIMUM ACCESS ROADWAY WIDTH OF 12 FEET INSIDE A MINIMUM RIGHT-OF-WAY WIDTH OF 15 FEET IS RECOMMENDED. TO FACILITATE ENTRY, A CURB SHOULD BE PROVIDED WHERE AN ACCESS ROAD MEETS

A CURBED ROADWAY:

TO ALLOW SAFE MOVEMENT OF MAINTENANCE VEHICLES, ACCESS RAMPS SHOULD BE PROVIDED TO THE SHORELINE OR BOTTOM OF ALL FACILITIES WITH SIDE SLOPES GREATER THAN 3 FEET IN HEIGHT. ACCESS RAMPS SHOULD NOT EXCEED 10 PERCENT IN GRADE AND SHOULD BE SUITABLY STABILIZED TO PREVENT DAMAGE BY VEHICLES AND EQUIPMENT. TURNAROUNDS SHOULD BE PROVIDED WHERE BACKING UP IS DIFFICULT OR DANGEROUS. TO EXPEDITE OVERALL MAINTENANCE, VEHICLE AND EQUIPMENT STAGING AREAS SHOULD BE PROVIDED AT OR NEAR EACH FACILITY SITE.

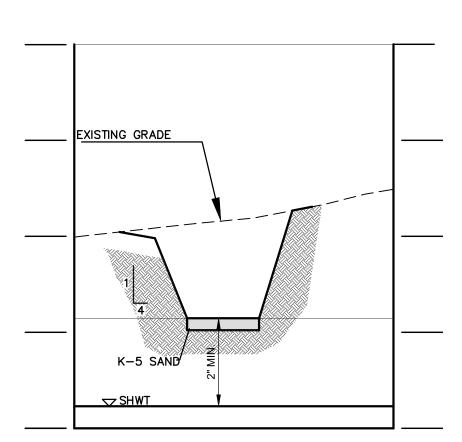
TRAINING OF MAINTENANCE PERSONNEL: DEPENDING ON THE SIZE, CHARACTER, COMPONENTS, AND LOCATION OF A STORMWATER MANAGEMENT MEASURE, MAINTENANCE PERSONNEL MAY REQUIRE SPECIALIZED TRAINING TO ENSURE THAT THE MEASURE IS MAINTAINED IN A MANNER CONSISTENT WITH ITS FUNCTION. SUCH TRAINING MAY ADDRESS SPECIALIZED INSPECTION OR MAINTENANCE TASKS AND/OR THE OPERATION OF SPECIALIZED MAINTENANCE EQUIPMENT.

DISPOSAL COLLECTION AND DISPOSAL OF SEDIMENT, DEBRIS, AND TRASH FROM STORMWATER MANAGEMENT MEASURES MUST COMPLY WITH LOCAL, STATE, AND FEDERAL WASTE HANDLING AND DISPOSAL REGULATIONS. ALL COLLECTED MATERIAL MUST BE SENT TO APPROPRIATE DISPOSAL/RECYCLING FACILITIES.

AESTHETICS: THE SAFETY, NEEDS AND AESTHETIC PREFERENCES OF THE ADJACENT COMMUNITY CAN HELP DETERMINE THE TYPE, AMOUNT, AND FREQUENCY OF NECESSARY MAINTENANCE.

EMERGENCY MAINTENANCE: EMERGENCY MAINTENANCE AND REPAIRS MUST BE PERFORMED IN A TIMELY MANNER.

DEVELOPMENT OF A STORMWATER MANAGEMENT MEASURE DESIGN AND THE INSPECTION AND MAINTENANCE TASKS NECESSARY TO KEEP IT FUNCTIONING RELIABLY MUST INCLUDE CONSIDERATIONS FOR THE SAFETY OF INSPECTION AND MAINTENANCE PERSONNEL WHO WILL BE WORKING IN OR NEAR THE MEASURE.



## INFILTRATION BASIN SECTION

	BASIN BOTTOM	01114/7
BASIN #	ELEV	SHWT
RG1	78.0	<75.0
RG2	75.0	<72.0
RG3	75.0	<72.0
RG4	75.0	<72.0
RG5	73.0	<70.0
BASIN 1	68.0	<65.0
BASIN 2	68.0	<65.0

PROFESSIONAL DESIGN SERVICES, L.L.C CONSULTING ENGINEERS, LAND SURVEYORS, PLANNERS, ENVIRONMENTAL SCIENTISTS, CONSTRUCTION SERVICES 1245 AIRPORT ROAD, SUITE 1, LAKEWOOD, NEW JERSEY 08701 PHONE 732 363 0060 FAX 732 363 0073 ENGINEERING@PDS-NJ.COM WWW.PDS-NJ.COM NEW JERSEY STATE BOARD OF P.E. & L.S. CERTIFICATE OF AUTHORIZATION NO. 24GA28125400 SCA

## PRELIMINARY & FINAL MAJOR SITE PLAN

## **STORMWATER MAINTENANCE PLAN**

FOR BLOCK 65 LOTS 11, 12, 13 & 14

TOWNSHIP OF MANCHESTER							
	OCEAN CC	DUNTY			NE	EW JERSEY	
ALE:	1" = 60'	DATE:	APRIL 25, 2022	JOB NUMBER:	18123	SHEET 21	
AWN BY:		DESIGNE	D BY:	CHECKED BY:		21	
	KNL		IMB		WAS		



## **PROFESSIONAL DESIGN SERVICES, L.L.C.**

1245 AIRPORT ROAD• SUITE 1 • LAKEWOOD • NEW JERSEY 08701• 732-363-0060 • FAX 732-363-0073 ENGINEERING@PDS-NJ.COM WWW.PDS-NJ.COM

WILLIAM A. STEVENS, P.E., P.P. VICE PRESIDENT SEAN D. COUGHLAN ASSOCIATE

IAN M. BORDEN, P.P. PRESIDENT GRAHAM J. MACFARLANE, P.E., P.P., C.M.E. ASSOCIATE STEVEN L. METELSKI, P.L.S. ASSOCIATE

June 21, 2023

Ms. Amanda Kisty Manchester Township Planning Board One Colonial Drive Lakehurst, NJ 08759

Re: Parkwood Square Preliminary & Final Major Site Plan Block: 65 – Lots: 11, 12, 13 & 14 Manchester Township, Ocean County *PDS Ref. #18123* 

Dear Ms. Kisty:

Per your request, enclosed please find the following plans and supporting data with respect to a site plan approval for the above referenced project:

1. Five (5) copies of Manchester Township Planning Board Application, revised consistent to the plans provided to your office on June 20, 2023.

Should you have any questions or require additional information, please do not hesitate to contact this office.

Very truly yours,

Ian M. Borden, P.P., President Professional Design Services, L.L.C.

IMB/ma Enclosure Cc: Parkwood Center Sal Alfieri, Esq. w/ encl.

### 245 Attachment 7

### **Township of Manchester**

### Appendix 7 Application for Development Before Zoning Board of Adjustment and Planning Board (§ 245-12B)

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  - =**□**<sup>\*</sup> )5 ?43'\$: IB5@,**5**4?'<sup>\*</sup>Ä2234@A
  - <sup>1</sup><sup>1</sup><sup>1</sup>/<sub>2</sub> (3/A5C 5?63J") 6H43'\$: IB5@54?"Ä2234@6A
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### MANCHESTER CODE

13.	Location of Premises: Lakehurst Whitesville Road		
	Tax Map Block 65	and Lot 11, 12, 13 & 14	
	Tax Map Sheet	(Course Feet)	
	Size of Tract: (Acres) 20.86 Zoning District PB Zone	_ (Square Feet)	
14.	If there has been a previous appeal or applic None	ation involving these pre	emises, give details.
15.	Give a brief statement of facts in support of Commercial Use is permitted in PB-1 zone. Apartment conditional uses per Ordinance 17-025	this application. (245-68) and Townhouse (245-	.74) uses are permitted as conformin
16.	If Application involves a variance, what see No Variance is required	tion of the chapter is app	licant seeking relief from:
17.	If a variance is involved, state under what su	ubsection of N.J.S.A. 40:	55D-70:
	(a) (b) (c) (d)		
18	Names and Addresses of Persons Preparing	Submission:	
1.474			Fax:
	Architect: Engineer: Professional Design Services, LLC	Phone: 732-363-0060	Fax:
	Other - Designate:	Phone:	Fax:
	Names and addresses of all witnesses Appli number of witnesses the Applicant intends to Ian Borden P.P., Bill Stevens P.E., P.F. In the event the Applicant is a corporation corporation and individuals owning 10% or	o call. P., John Rea P.E. n, set forth names and a	addresses of officers of the
21.	Environmental Impact Statement: For all m cases as determined by the Approving Agen		ajor site plans and in special
	We) hereby depose and say that the foreg ewith are true and correct to the best of my (		ed in the papers submitted
	M. E.L		(Applicant)
Parl	wood Square LP and Parkwood Center B LLC - Mordecha	ii Eichorn	
Sw	orn and subscribed to before me on this	day of	20
sub	I (We) the Owners(s) hereby depose and say mitted herewith are true and correct to the b the Owner)		
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Sworn and subscribed to before me on this \_\_\_\_\_ day of \_\_\_\_\_ 20\_\_\_\_

Failure to complete this application in its entirety and submit the required documents will result in the determination that this application is incomplete, in which event the application will not be considered by the Board. The applicant is hereby informed that in addition to the documents set forth herein, he must present evidence that he has met the notification requirements as set forth in the municipal notice of application of development forms and Chapter 245 of the Manchester Township Code.

245 Attachment 7:2

## **ENVIRONMENTAL IMPACT STATEMENT**

For

## **MAJOR SITE PLAN**

Block 65 Lots 11, 12, 13 & 14 Manchester Township Ocean County, New Jersey

**Prepared By:** 

PROFESSIONAL DESIGN SERVICES, L.L.C. 1245 Airport Road, Suite 1 Lakewood, NJ 08701 PDS #18123

**MARCH 3, 2023** 

IAN M. BORDEN P.P., PRESIDENT

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## APPENDICES

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### **1.0 PROJECT DESCRIPTION**

#### 1.1 <u>Introduction</u>

Being known as Block 65, Lots 11 thru 14, the project site contains 20.9 acres and is located at the northeast corner of South Hope Chapel Road (OC Route 547) and Ridgeway Road (OC Route 571) in Manchester Township, Ocean County, New Jersey. Figure 1 is a location map for the project site. The surrounding area is developed with residential single family homes to the north and east. The intersection of South Hope Chapel Road and Ridgeway Road is signalized with dedicated left turn lanes at all approaches.

The property is zoned PB-1 (Pinelands Business). It is proposed to develop the site with commercial, residential apartment and townhouse units as permitted in the PB-1 zone consistent with the Township Master Plan and Fair Share Housing Plan. 31,200 square feet of commercial retail and office use, 28 residential apartments and 141 residential townhouse units are proposed. The 28 residential apartments are located above a portion of the commercial use will be affordable housing units.

The property does not contain any freshwater wetlands or wetlands transition area. There are no regulated flood hazard areas nor riparian buffers on site.

The project is located within the Pinelands National Reserve and, therefore, regulated by the NJ Pinelands Commission pursuant to the Comprehensive Management Plan (NJAC 7:50-1.1 et. seq.). The site is located within the Regional Growth Land Use Management area as defined by the Pinelands Comprehensive Management Plan (CMP). The Pinelands Commission has issued a Certificate of Filing for the project and a copy is included in the appendices.

The project will be serviced by public water and sewer.

The project is proposed to be developed consistent with the Manchester Township Land Use and Development Regulations and the Pinelands Comprehensive Management Plan.

The Environmental Impact Statement (EIS) and site design have been prepared in conformance with the Manchester Township Ordinance regarding preparation and content of an EIS (Section 109-169). Township and County Master Plans, the Manchester Township Natural Resources Inventory and various other pertinent planning documents were reviewed to assist in the preparation of this document. The EIS addresses specific elements of the proposed site design (i.e., stormwater runoff) and potential impacts and steps taken to minimize or avoid adverse environmental impacts (Environmental Performance Controls).

Site development plans have been prepared by Professional Design Services; these plans have been utilized in support of the preparation of this document.

### 1.2 Land Use and Zoning

The site is located within the Regional Growth Land Use Management area as defined by the Pinelands Comprehensive Management Plan (CMP); the Regional Growth area is defined by the CMP as areas of existing growth capable of accommodating regional growth influences while protecting the essential character and environment of the Pinelands. The subject properties are located within the Pinelands Business PB-1 zone which permits commercial use on a lot larger than 20,000 square feet as well as apartment and townhouse residential development on tracts larger than 10 acres. Manchester Township Ordinance 17-025, as certified by the Pinelands Commission in 2018, permits residential apartment and townhouse units on tracts larger than 10 acres. The ordinance, which was created to be consistent with the Township affordable housing settlement and updated Master Plan, also requires affordable housing residential units be provided of 20% of the number of units. The project fully conforms to the Apartment (245-68) and Townhouse zone requirements (245-74) and no variances are required.

The project is being developed consistent to the Residential Site Improvement Standards. All of the proposed streets contain 26' of pavement with curb and sidewalk on both sides. Parking is provided in a driveway for each unit as well as off-street spaces.

### 1.3 <u>Utility Plans</u>

The Manchester Township Municipal Utilities Authority owns and operates public potable water and sanitary sewer systems in Manchester Township. The site lies within the JTMUA's franchise area and also within the Central Sewer Service Area of the OCUA.

There is no public sewer in this portion of Manchester Township; An off-site extension will be constructed by the developer of the Jackson Trails project located in Jackson Township to allow for public sewer service to the project. The off-site extension will include extension of the Manchester Township System (MTDOU) from its nearest location in County Route 571, approximately 2 miles southeast of the site. An on-site collection system will be constructed to convey flows to the proposed extension of the MTDOU system. Similarly, public water main does not exist along the site frontage; however, an off-site extension of the water system will be constructed by the Jackson Trails project to provide for potable water and fire service to the project. Water main will be extended by Jackson Trails from the existing water main located within Ridgeway Road east of the site through the intersection of South Hope Chapel Road to the existing JTMUA water system at Whitesville Road (OC Route 527).

### 1.4 <u>Stormwater Management</u>

The stormwater management plan will provide green infrastructure and non-structural low impact measures with management practices to efficiently collect and control increased stormwater runoff. Design standards of the Pinelands Commission (NJAC 7:50-6.84) require the applicant manage stormwater runoff by recharging all increased runoff from impervious areas from the 10-year, 24 hour storm and controlling runoff peaks for the 2, 10 and 100 year storm events to less than pre-development runoff levels.

Multiple stormwater management facilities will be constructed to provide green infrastructure, in a decentralized system to reduce the nitrate loading of runoff while providing groundwater recharge and flood control attenuation.

The Stormwater Management Report prepared by PDS contains the description, design methodology and outlines the regulatory compliance of the proposed stormwater management system.

### 2.0 SITE DESCRIPTION AND INVENTORY

Investigations of the project site were conducted by the author and PDS staff from 2018 till 2023. The following inventory describes the existing environmental conditions onsite.

### 2.1 <u>Topography and Hydrology</u>

The project site lies within the outer coastal plain physiographic province. The project site is located within the Coastal Plain geomorphic province. The geologic framework of the Coastal Plain is one of underlying gently southeastward dipping unconsolidated clays, marls, silts and sands of the tertiary (65 to 1.75 million years ago) period.

The project lies within the Kirkwood Formation, which is overlain by the Cohansey Sand and underlain by the Shark River/Manasquan Marl. The Kirkwood Formation crops out along the northern part of Ocean County. The Kirkwood Formation ranges in thickness from a minimum of 50 feet in the outcrop area to a maximum reported thickness of about 800 feet in Atlantic City (Geology and Groundwater Resources of Ocean County, NJ 1969). The topography of the site slopes gradually from the southwest towards the northeast.

Figure 2 is a copy of the USGS Quadrangle Topography Map with the site located.

### 2.2 <u>Soils</u>

The project site is underlain by the following soils as depicted by the U.S. Department of Agriculture; Ocean County Soil Survey (issued April 1980 and reissued February 1989). Figure 3 is a copy of the Soil Survey with the site located.

Soil Type	% Slope	Depth to SHWT*
DoB- Downer Sand	0-5	>6.0'

### \*SHWT = Seasonal High Water Table

The permeability of the Downer soil series are typically rapid and the available water capacity is low. The depth to seasonal high water is typically greater than 6 feet. This soil series typically have an acidic reaction but are not acid-producing. The use of lime in landscaped areas is required to neutralize the soil to provide adequate growing conditions.

Soil borings were performed throughout the project site to assess soil conditions and seasonal high water table. The depth to seasonal high water occurs at a depth greater than five (5) feet. The soils are permeable and do not pose any significant limitations on the proposed development.

### 2.3 Surface Water

There is no surface waters located on the site.

### 2.4 <u>Subsurface Water</u>

The upper part of the Kirkwood Formation and the Cohansey Sand are hydraulically connected and together function as an aquifer system. Underlying the Kirkwood-Cohansey aquifer system is the composite confining unit, a complex series of geologic units that, depending on location, can include as many as nine distinct units. The part of the composite confining unit of interest in this area ranges in age from Palecene to early Miocene and is made up of the Vincentown Formation, Manasquan Formation, Shark River Formation, Piney Point Formation, and basal clay of the Kirkwood Formation. Two minor aquifers are present in this part of the composite confining unit. The Vincentown aquifer consists of the Vincentown Formation, which is comprised of moderately permeable Quartz sand. The Vincentown aquifer is used as a source of water only in and near the outcrop areas, in the northwestern part of the County. The other minor aquifer, Piney Point aquifer, is confined and is composed of fin to coarse grained glauconitic quartz sand and shell beds.

Based upon field observations, there are approximately 22 wells currently located with 500 feet of the project site. Such wells are typically screened in the unconfined portion of the Cohansey/Kirkwood Aquifer at depths between 40 and 120 feet in depth and are used to service existing single family homes located around the subject property on the northern and eastern sides.

The project will also recharge stormwater runoff to this aquifer by virtue of compliance with the Pinelands Stormwater Management Regulations. As a result, the runoff from all impervious surfaces during a 10 year, 24 hour storm (5.4 inches) event will be retained on the site and recharged to this aquifer.

### 2.5 <u>Topography and Existing Development Features</u>

Topographic contours and all existing feature onsite and within 50 feet of the site are depicted on the Subdivision Plans.

### 2.6 <u>Wetlands and State Open Waters</u>

Wetlands are areas where the substrate is inundated or saturated by surface or groundwater at a frequency and duration sufficient to support, and that under normal circumstances do support, a prevalence of vegetation typically adapted for life in saturated soil conditions. Wetlands include lands with poorly drained or very poorly drained soils, as designated by the National Cooperative Soil Survey of the Soil Conservation Service of the United States Department of Agriculture. All activities must comply the Pinelands Comprehensive Management Plan.

There are no freshwater wetlands located on or within 300 feet of the site. There is no disturbance proposed to the freshwater wetlands or wetland buffer area.

## 2.7 <u>Floodplains</u>

There is no floodplain or riparian buffer located on or within the property. No development is proposed within any regulated flood hazard areas or flood plain.

### 2.8 <u>Vegetation</u>

The subject property is forested with an oak/ pine forest. The portion of the property at

the intersection is a successional pine forest over a small area. Vegetation identified on the site include tree species such as White oak (Quercus alba), Eastern black oak (Quercus velutina), Eastern red cedar (Juniperus virginiana), and Pitch pine (Pinus rigida). The understory comprises of American holly (Ilex opaca), Green briar (Smilax rotundifolia), Mountain laurel (Kalmia latifolia), Late low-bush blueberry (Vaccinium angustifolium), and Numblewill (Muhlengergia schreberi).

## 2.9 <u>Wildlife</u>

The property does not contain critical habitat for threatened or endangered species based on the studies performed by Dubois Environmental.

## 2.10 <u>Noise</u>

Noise is defined as "any sound of such level to be injurious to human health or welfare, or which would unreasonably interfere with the enjoyment of life or property throughout the state or in any portion thereof, but excludes noise emanating from residential structures." Ambient noise levels are assumed to be well below the NJDEP standards, due to the nature of the area.

The existing noise characteristics within the area are representative of a residential setting and are influenced by auto traffic on South Hope Chapel Road. Typical daytime noise levels of residential communities range from 45 to 50 dBA (decibel). As the general project area is low-density residential and accounts for a low volume of traffic, noise levels are minimal. Local traffic in the site vicinity is the primary on-site noise contributor.

Lakehurst Naval Air Engineering Station (NAES) is located approximately 3 miles southwest of the project site. McGuire Air Force Base, Fort Dix and NAES have been combined to form a Joint Base in 2009. This consolidation has created an increase in the tempo of aviation operations at NAES by deployment of additional Air National Guard aircraft and adding Assault Landing Zone training for C-17 aircraft. An Air Installation Compatible Use Zone (AICUZ) Study completed in July 2013 determined the project site is not located within any noise zone areas.

## 2.11 <u>Cultural, Historical and Archaeological Resources</u>

Historic and archaeological resources may include objects, structures, shipwrecks, neighborhoods, districts, and manmade or man-modified features of the landscape and seascape, including archaeological sites, which either are on or are eligible for inclusion on the State or National Register of Historic Places. The property does not contain any cultural, historic or archaeological resources.

## 2.12 Land Use

The site is currently forested. The surrounding land uses to the north and east are existing residential lots.

The Manchester Township Land Use and Development Ordinance (Chapter 245) zones the property within the Regional Growth Zone as PB-1. The project complies with all of the zone requirements. Purchase of 10.5 Pinelands Development Quarter Credits is required as outlined in

the certified ordinance 17-025 as is the development of 28 affordable housing units.

The project proposes a total of 141 market rate townhouse units and 28 low/moderate apartment housing units. The resulting density for the 141 to townhouse residential units proposed is 6.7 units per gross acre, less than the maximum permitted density of 8.0 units per acre for townhouse development. The resulting density for the 28 apartment residential units proposed is 1.4 units per gross acre, less than the maximum permitted density of 6.0 units per acre for apartment development. The project is consistent with the Manchester Township Zoning Ordinance and Pinelands Comprehensive Management Plan.

## 2.13 <u>Air Quality</u>

The subject property lies within a rural residential setting of Manchester Township and is zone PB-1. There are no point sources of air pollution within or surrounding the subject property, including fossil-fueled electric power generating plants, industrial boilers or processing plants. The air quality within this setting is generally good.

The NJDEP, Bureau of Air Monitoring maintains two (2) air quality monitoring stations in Ocean County (the Colliers Mills Fish & Wildlife Management Area Station and the Toms River Elementary School Station) and a station in Burlington County (at the Lebanon State Forest). The Colliers Mills station is in close proximity to the site and is indicative of the ambient air quality in the "northern coastal region" of New Jersey.

The tables from the NJDEP, Bureau of Air Monitoring 2000 Air Quality Report describe the ambient air quality monitoring results of the monitoring stations. As indicated in the table, the air quality standards for the State are generally good at the three stations.

Due to the residential nature of the project proposed, the most significant potential air quality impact would arise from carbon monoxide vehicle emissions. Localized increases typically occur at places of vehicular concentration and delays, such as intersections. Based on the traffic impact study performed by McDonough, Rea & Associates the project will not create any air quality impacts from vehicular concentrations and delays.

## 3.0 ENVIRONMENTAL IMPACT STATEMENT

The Manchester Township Ordinance regarding preparation and content of an Environmental Impact Statement requires an assessment of both adverse and positive impacts of the proposed activity. These impacts have been previously addressed within the site description and inventory. The following brief list of impacts is provided in summary:

- a. <u>Soil Erosion and Sedimentation</u>
  - Run-off shall be directed to catch basins and a collection system for sedimentation control and direction to detention basins. No erosion is anticipated along the roadways since the project proposes curbing to stabilize the edge of pavement. The proposed development shall be reviewed by the Ocean County Soil Conservation District and complies with their standards. All disturbed areas not occupied by improvements such as roads and houses will be vegetatively stabilized as required by the certified plan.

b. <u>Floodplain</u>

No regulated floodplain areas are located on the project site. No development activities are proposed within any floodplain areas.

c. <u>Surface Water</u>

No surface waters are located on the project site.

d. <u>Ground Water</u>

Significant subsurface disruption will not occur and major impacts to groundwater resources are not anticipated. Potable water will be provided by the JTMUA. Estimated average demand will be approximately 57,000 GPD for the project, based upon the NJ Residential Site Improvement Standards, NJAC 5:21.

e. <u>Ground Water Capabilities</u>

Potable water will be provided by the Manchester Township public water supply system. The groundwater withdrawal will be regulated by the NJDEP under the Manchester Township's diversion and allocation permit. There will be no local impact from the project as there is no groundwater withdrawal proposed at the project site.

f. <u>Sewage Disposal</u>

Sewage will be conveyed to the MTDOU system, and ultimately to the OCUA for treatment. Estimated discharge of approximately 50,000 GPD will result from the project.

g. <u>Solid Waste Disposal</u>

1. <u>Construction</u> All solid waste generated during tree removal activities shall be recycled by creating mulch or firewood for reuse, as appropriate and market conditions dictate. All solid waste generated during construction such as lumber, paper, etc. will be collected in dumpsters located on the site and disposed of in a manner consistent with local ordinances and the Ocean County Recycling Plan. Care will be taken to ensure that all construction debris is collected frequently to prevent any temporary adverse impacts such as wind blown movement.

2. <u>Residences</u> Solid waste generated by the homes will be collected, recycled and disposed of in a manner consistent with local ordinances and the Ocean County Recycling Plan.

h. <u>Vegetation</u>

Approximately 20 acres of forest vegetation will be removed. The project will comply with the Manchester Township Land Use and Tree Ordinance.

i. <u>Wildlife Habitats</u>

Upland forested wildlife habitat will be cleared and developed by the project. No critical wildlife habitats for threatened or endangered species are located on this property.

- j. <u>Scenic and Historic Features</u> No scenic or historic features exist onsite.
- k. <u>Air Quality</u>

Decreased air quality because of air-borne dust associated with the proposed construction activities is a projected short-term impact. Methods to control soil erosion and sediment control will be implemented in order to minimize air quality degradation. Long-term degradation of air quality as a result of an increase in traffic is not expected. Levels of service at nearby intersections will not degrade as a result of the project. The proposed project by itself is not anticipated to result in a significant impact on ambient air quality since it will not generate traffic delays.

1. <u>Noise</u>

Projected noise levels, as a result of the proposed development, is not anticipated to increase ambient noise levels above NJDEP standards as described in Section 2.10. The noise levels during construction will be temporarily increased but are subject to regulatory constraints such as maximum noise levels and permissible construction times.

- m. <u>Energy Utilization</u>
   The proposed development is designed to include energy conservation fixtures and measures, as appropriate.
- n. <u>Wetland Impacts</u>

Freshwater wetlands on the project site will not be impacted since no development activities are proposed within freshwater wetlands or the wetland transition area. No irreversible or significant adverse impacts to any wetlands or wetland buffers will occur as a result of this proposed development.

## 4.0 ENVIRONMENTAL PERFORMANCE CONTROLS

As discussed in the previous sections, various measures have been utilized throughout the design process to avoid or minimize potential adverse environmental impacts. These measures are specifically addressed for individual resource item. In general, the following steps have been taken in order to avoid or minimize adverse environmental impacts:

- 1. Design of stormwater management system in accordance with current regulations, including green infrastructure and de-centralized stormwater management measures to promote nitrate attenuation, groundwater recharge and flood control.
- 2. Installation and maintenance of soil erosion control measures during construction.
- 3. A significant investment in off-site potable water and sanitary sewage systems to provide public water and sewer service to the project, and to minimize any local impacts.

#### 5.0 COMMITMENT OF RESOURCES AND UNAVOIDABLE IMPACTS

The applicant and its consultants have designed and planned this community in concert with the existing and surrounding natural resources. The project will require the following irreversible and irretrievable commitment of resources as well as produce the following unavoidable impacts:

- 1. Removal of 20 acres of forested vegetation.
- 2. Increased utilization of municipal services such as solid waste disposal, recycling and educational services by potential population increase.
- 3. Increased utilization of energy such as electricity and natural gas.
- 4. Decrease in air quality due to increased traffic.

Compliance with all state, local and municipal regulations shall be demonstrated by the necessity to obtain all required approvals prior to the commencement of construction.

#### 6.0 ALTERNATIVES AND MITIGATING MEASURES

The alternatives to the proposed project are "no-build" which would deny the property owner their lawful use of the land as permitted by Manchester Township Zoning Regulations and the Pinelands Comprehensive Management Plan. The current zoning regulations were established to comply with the affordable housing settlement agreement with Fair Share Housing Council and the Regional Growth requirements in the Pinelands Comprehensive Management Plan. The project serves to meet the goals and objectives of the Master Plan and Fair Share Plan.

The project serves to meet the objectives of the Pinelands Comprehensive Management Plan as residential development within a Regional Growth Zone that will construct affordable housing units and purchase Pineland Development Credits.

There are no environmental factors present on this site to limit the extent of development of the subject property. These factors include freshwater wetlands and wetlands buffers. Layout of the proposed development features is based upon Township Ordinances and setback requirements as well as the Pinelands Comprehensive Management Plan. The site development layout reflects best management practices regarding avoidance and/or minimization of adverse impacts on the environmental resources within the project area.

The stormwater management system meets the criteria for water quality and flood control in the Manchester Township, Ocean County and Pinelands Commission regulations. Alternative designs were investigated in consideration of the existing site limitations (i.e. depth to groundwater, topography). The proposed design provides for green infrastructure, groundwater recharge, water quality and flood control in accordance with applicable regulations.

The resulting design is consistent with applicable State and Local requirements. The proposed design, use of native species in the landscaping plan, adherence to the Soil Erosion and Sediment Control Plan, and utilization of the public water and sewer facilities are the primary mitigating measures incorporated into the project design.

After reviewing a variety of alternatives permitted under the Land Use Ordinances, it was determined that the project, as proposed, will not have any significant impact upon the environment. As proposed, the development is consistent with adopted regulations and standards of the Municipality, State and NJ Pinelands Commission. The mitigating measures included in the site design will offset any potential adverse impacts associated with the project.

#### **OTHER REQUIRED APPROVALS** 7.0

The following Table 7.0-5 lists all applicable licenses, permits and approvals required by Federal, State, County and Municipal law, to the best of our knowledge. Copies of each approval will be provided to Manchester Township when received.

TABLE 7.0-5
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#### LIST OF ALL APPLICABLE APPROVALS AND PERMITS

<u>Permit/App</u> Federal	roval	<u>Required</u> No	
i cuciui		110	
State -			
Pinelands Co	mmission	Yes	
NJDEP -	CAFRA	No	
	Wetlands	No	
	Stream Encroachment	No	
	Sewer Extension	Yes	
	Water Quality Certification	No	
	Water Extension	Yes	
	Well Permits		
			No
NJDOT -	Drainage	No	
	Access	No	
Ocean Coun	ty		
Preliminary A	-	Yes	
Final Approv		Yes	
	erage Authority)	Yes	
Soil Erosion		Yes	
	(Well & Septic)	No	
-	(Subdivision)		
			Yes
			105
Maaalaast	T		
Manchester	-	<b>V</b> 7	
	Site Plan and Subdivision Approval	Yes	
Final Site Pla	in and Subdivision Approval	Yes	

Manchester MUA - Preliminary

- Tentative

Yes

Yes

	- Fii	nal
	Yes	
Local Clearing Permit		
		Yes
Environmental Commission	Yes	
Bureau of Fire Prevention	Yes	

#### 8.0 **REFERENCES**

Kummel, H.B. The Geology of New Jersey, 1940 N.J. Dept. Conserv. Del. Bull. 50, 203 pp. McCormick, J. The Pine Barrens: A Preliminary Ecological Study (1970). Munsell, Munsell Soil Color Chart, Baltimore, MD, 1975. "New Jersey's Record Trees," New Jersey Outdoors, September/October 1984. National Wetland Inventory Map, Lakehurst, NJ Quadrangle. Shaw, Frank, 1990. Eastern Birds. W.H. Smith Publishers, Inc., New York. United States Department of Agriculture, Soil Conservation Service, Soil Survey of Ocean County, New Jersey, 1980. USGS Lakehurst, NJ Quadrangle. Wolfe, Peter E., The Geology and Landscapes of New Jersey, 1977. Crane, Russak & Company, Inc. New York. USGS Simulation of groundwater flow in the unconfined aquifer system of the Toms River, Metedeconk River, and Kettle Creek Basins, New Jersey; Water Resources Investigations Report 97-4066; 1997. Traffic Impact Study prepared by McDonough & Rea Associates Pinelands Comprehensive Management Plan, NJAC 7:50-1.1 et seq. Manchester Township Master Plan and Fair Share Housing Plan Joint Base McGuire-Dix-Lakehurst Joint Land Use Study for Counties of Ocean and Burlington, May, 2009.

**FIGURES** 

# **APPENDIX A**

## **CERTIFICATE OF FILING**



PHILIP D. MURPHY Governor SHEILA Y. OLIVER Lt. Governor

## State of New Jersey

THE PINELANDS COMMISSION PO Box 359 New Lisbon, NJ 08064 (609) 894-7300 www.nj.gov/pinelands



LAURA E. MATOS Chair SUSAN R. GROGAN Executive Director

General Information: Info@pinelands.nj.gov Application Specific Information: AppInfo@pinelands.nj.gov

March 1, 2023

Mordechai Eichorn (via email) Parkwood Square LP and Parkwood Center B, LLC 1500 River Ave. Lakewood NJ 08701

> Re: Application # 1985-1254.004 Block 65, Lots 11 - 14 Manchester Township

Dear Mr. Eichorn:

Pursuant to N.J.A.C. 7:50-4.34 of the Pinelands Comprehensive Management Plan, the completion of this application has resulted in the issuance of the enclosed *Inconsistent Certificate of Filing*. The reason(s) for the inconsistency is explained on Page 3 and must be resolved.

The Inconsistent Certificate of Filing is not an approval. It is the document necessary to allow any municipal or county agency to review and act on the proposed development application. All municipal and county permits and approvals granted for the proposed development are subject to review by the Pinelands Commission. No permit or approval shall take effect and no development may occur until the Commission issues a letter indicating that the municipal or county permit or approval may take effect.

Upon receipt of any municipal or county permit or approval, please submit a copy to the Commission's office with the additional items listed on the enclosed *Local Agency Approval Submission Checklist*.

If you have any questions, please contact Ernest M. Deman of our staff.

Sincerely,

*for* Charles M. Horner, P.P. Director of Regulatory Programs

Enc: Inconsistent Certificate of Filing <u>Local Agency Approval Submission Checklist</u> (Above form(s) may be found at <u>nj.gov/pinelands/appli/tools/</u>.)

c: Secretary, Manchester Township Planning Board (via email) Manchester Township Construction Code Official (via email) Manchester Township Environmental Commission (via email) Secretary, Ocean County Planning Board (via email) Ian M Borden, PP, AICP (via email)

•



#### **BACKGROUND**

Existing development:

Vacant land

**Relevant Information:** 

- The proposed development will be serviced by public sanitary sewer.
- The parcel is located in Manchester Township's PB-1 zoning district.
- The Manchester Township land use ordinance requires that Pinelands Development Credits (PDCs) must be acquired and redeemed for 30 percent of the proposed market rate units in any townhouse development located within the PB-1 zoning district. The applicant has indicated that 139 market rate units are proposed. A total of 10.50 PDCs are required.
- The Manchester Township land use ordinance permits townhouses at a maximum density of eight dwelling units per acre in the PB-1 zoning district. The "by-right" density on the 20.86 acre parcel is 166 dwelling units. The applicant proposes a total of 167 dwelling units. To maintain consistency with the density requirement of the Manchester Township land use ordinance, 0.25 PDCs must be acquired and redeemed.

#### **CONDITIONS**

- 1. Prior to Commission issuance of a letter advising that any submitted municipal construction permit may take effect, the Commission must receive documentation from the Pinelands Development Credit (PDC) Bank that the requisite 10.75 PDCs have been acquired and submitted to the PDC Bank for redemption.
- 2. Item(s) on the attached *inconsistencies* document must be resolved prior to Commission issuance of a letter indicating that any approvals or permits can take effect.

# NSIS1

#### NEXT STEPS

- This Certificate of Filing is not an approval.
- Submit a copy of this Certificate of Filing to all county and municipal agencies that are required to review and act on your application (municipal planning board, building department, county health department, etc.).
- Send a copy of all approvals/permits that are issued by the county or municipality to the Pinelands
  Commission for review. Please use the attached *Local Agency Approval Submission Checklist* to make sure you are submitting all required documentation related to the approval/permit.
- No local approval/permit takes effect and no development can occur until the Pinelands Commission has reviewed the approval. When we complete our review, we will issue you a letter stating that the approval/permit can take effect.

#### **INCONSISTENCIES**:

This application as currently proposed is inconsistent with the following standard(s) of the Manchester Township certified land use ordinance and the Pinelands Comprehensive Management Plan (CMP):

1. Stormwater (N.J.A.C. 7:50-6.84(a)6)

The Manchester Township land use ordinance and the CMP require that all development meet the stormwater standards. The application has not provided the information required to demonstrate that the proposed development will meet this standard.

2. Protection of threatened or endangered plants and wildlife (N.J.A.C. 7:50-6.27 & 6.33)

The Manchester Township land use ordinance and the CMP require that all development be designed to avoid irreversible adverse impacts on the survival of any local population of threatened or endangered plant species and on habitats that are critical to the survival of any local populations of threatened or endangered animal species. The applicant has not provided the information required to demonstrate that the proposed development will meet these standards.

Commission receipt of any county or municipal approval or permit for the development as currently proposed will likely result in the scheduling of a Commission staff public hearing to review the issues raised by the above-referenced inconsistency(ies).

### **PROFESSIONAL DESIGN SERVICES, L.L.C.**

1245 AIRPORT ROAD • SUITE 1 • LAKEWOOD • NEW JERSEY 08701 • 732-363-0060 • FAX 732-363-0073

ENGINEERING@PDS-NJ.COM

IAN M. BORDEN, P.P., PRESIDENT SEAN D. COUGHLAN ASSOCIATE

June 19, 2023

Ms. Amanda Kisty Manchester Township Planning Board One Colonial Drive Lakehurst, NJ 08759

Re: Parkwood Square Preliminary & Final Major Site Plan Manchester Township, Ocean County PDS Ref. #18123

Dear Ms. Kisty:

The above captioned application was deemed complete. The project has been revised to include commercial uses along Route 571 as well as the affordable housing units in apartment units located above a portion of the commercial uses as well as the townhouse residential units. Enclosed please find the following information:

- 1. Four (4) sets of Major Site Plans
- 2. Four (4) copies of Stormwater Management Report
- 3. Four (4) copies of Environmental Impact Statement
- Four (4) copies of Traffic Report prepared by McDonough Rea & Associates dated May 30, 2023

Should you have any questions or require additional information, please do not hesitate to contact this office.

Very truly yours,

Ian M. Borden, P.P., President Professional Design Services, L.L.C.

IMB/ec Enclosure Cc: Parkwood Square, LLC WILLIAM A. STEVENS, P.E., P.P. VICE PRESIDENT GRAHAM J. MACFARLANE, P.E., P.P., C.M.E. ASSOCIATE

JUN 2 n 2023



McDonough & Rea Associates, Inc.

#### Traffic and Transportation Consulting

Kevin P. McDonough (1953-1994) John H. Rea, P.E. Jay S. Troutman, Jr., P.E. Scott T. Kennel

*Revised* May 30, 2023 May 10, 2022

Manchester Township Planning Board 1 Colonial Drive Manchester, New Jersey 08759

Re: Townhouse Plan/Mixed-Use Plan Lots 11, 12, 13 and 14 in Block 65 Manchester Township, Ocean County MRA File No. 22-147

Dear Board Members:

McDonough & Rea Associates (MRA) has been asked to provide the Planning Board with a *Traffic Impact Analysis* for plans to construct 169 multi-family homes and office/retail space on the noted property. The subject property is on the northeast corner of Ridgeway Road (CR 571) and South Hope Chapel Road (CR 547), as shown on *Figure 1, Site location Map* in the *Appendix*.

Access is proposed to both CR 571 and CR 547 which are both under the jurisdiction of Ocean County.

#### **SCOPE OF STUDY**

In order to prepare a thorough *Traffic Impact Analysis* for the townhome project, MRA conducted the following tasks:

- 1. Made field visits to the site to inventory existing roadway and traffic conditions in the area.
- 2. Conducted peak hour traffic counts at the intersection of CR 571/CR 547 during the critical AM and PM peak hours when traffic flow on the adjacent roadway network and traffic generated by the townhomes will be at maximum levels
- 3. Prepared trip generation estimates based on the Institute of Transportation Engineers (ITE) data.
- 4. Distributed site generated traffic from the multi-family homes and office/retail space in accordance with anticipated origins and destinations.



 Traffic and Transportation Consulting

 1431 Lakewood Road, Suite C, Manasquan, NJ 08736 • (732) 528-7076 • Fax (732) 528-6673

 105 Elm Street, Lower Level, Westfield, NJ 07090 • (908) 789-7180 • Fax (908) 789-7181

Manchester Township Planning Board -2-

May 30, 2023

- 5. Prepared estimates of future traffic volume demand for a design year of 2033 in accordance with Ocean County Planning Board protocol including background traffic growth and traffic generated by other adjacent development projects.
- 6. Conducted level of service capacity analyses for the 2 site driveways to CR 571 and CR 547 as well as the off-site signalized intersection of CR 571/CR 547.
- 7. Reviewed the *Site Plan* with respect to availability and accessibility of the parking supply and conformance to New Jersey Residential Site Improvement Standards (RSIS).

The following report sets forth the database accumulated and the conclusions reached with respect to the Manchester townhomes.

#### EXISTING CONDITIONS

The subject property is located on the northeast corner of CR 571/CR 547 and contains approximately 20.86 acres and is located within the PB-1 Zone. South Hope Chapel Road, also known as CR 547, is a north/south Ocean County arterial roadway in the vicinity of the site. Ridgeway Road, also known as CR 571, is an east/west Ocean County arterial roadway in the vicinity of the site.

CR 547 intersects CR 571 at a signalized intersection. All 4 legs to the intersection provide for 3 approach lanes. The intersection has crosswalks across all 4 corners and also has pedestrian pushbuttons and pedestrian signals. All 4 approaches to the intersection have protected/permissive left turn arrows.

#### EXISTING TRAFFIC VOLUMES

Traffic volume data was collected at CR 571/CR 547 intersection by conducting manual turning movement counts in April 2022. The AM peak street hour counts were conducted on April 6, 2022 and the PM peak street hour counts on April 11, 2022. Design year 2033 no-build volues are shown on *Figure 2R* in the *Appendix* and include background traffic growth and traffic from other approved projects in the area.



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May 30, 2023

#### TRIP GENERATION/DISTRIBUTION

Estimates of traffic to be generated by the 169 multi-family homes and office/retail uses were made after consulting the  $11^{th}$  Edition of the Institute of Transportation Engineers (ITE) Trip Generation Manual. Table I illustrates the anticipated peak hour traffic generation from the project.

# TABLE I TRIP GENERATION 169 Multi-Family Homes & Office/Retail Space

		<u>AM P</u>	SH		<u>PM P</u>	<u>SH</u>
<u>USE</u>	In	<u>Out</u>	TOTAL	<u>In</u>	OUT	TOTAL
9,200 SF Retail	13	9	22	30	30	60
22,000 SF Office	30	4	34	6	26	32
169 Multi-Family Units	<u>18</u>	<u>58</u>	<u>    76</u>	<u>    59</u>	<u>34</u>	<u>_93</u>
Total	61	71	132	95	90	185

With respect to the distribution of site generated traffic, a review was made of existing traffic patterns in the area, locations of employment centers and access to higher order roadways. Based on this review, traffic was distributed as follows:

- ▶ 25 percent to/from the north on CR 547
- > 25 percent to/from the south on CR 547
- > 25 percent to/from the east on CR 571
- > 25 percent to/from the west on CR 571

Site generated and distributed traffic volumes are shown on *Figure 3R* in the *Appendix*.

#### ANALYSIS OF FUTURE TRAFFIC CONDITIONS

A design year of 2033 was assumed in accordance with Ocean County Planning Board protocol. Existing 2023 traffic volumes were expanded by 10 percent to include background traffic growth based on New Jersey Department of Transportation (NJDOT) historical growth rate data for the area. In addition to the foregoing, traffic from the following projects was included in a projection of future 2033 design year volumes.



#### McDonough & Rea Associates, Inc.

Traffic and Transportation Consulting 1431 Lakewood Road, Suite C, Manasquan, NJ 08736 • (732) 528-7076 • Fax (732) 528-6673 105 Elm Street, Lower Level, Westfield, NJ 07090 • (908) 789-7180 • Fax (908) 789-7181

Manchester Township Planning Board -4May 30, 2023

- > Jackson Trails residential project on CR 547 in Jackson Township north of the Manchester Township border (467 units).
- > Manchester Township office/retail project on CR 547 north of the subject property.
- ▶ Proposed Ocean County park on the southeast corner of CR 571/CR 547 (250 acres; scheduled for a passive/recreational park).

Figure 4R in the Appendix, illustrates design year 2033 build traffic volumes, including the aforementioned projects and other background traffic growth as described.

Traffic engineers calculate levels of service of unsignalized and signalized intersections which relate to the quality of traffic flow. Level of service is a measure of average control delay. Average control delay is the time lost due to deceleration and the amount of time from when a vehicle is stopped for a traffic control device (or at the end of the queue) to when the vehicle departs the intersection. Delay is a relative quantity of driver discomfort, frustration, fuel consumption, and loss in travel time.

Levels of service range from "A" to "F," with "A" being the highest, or best attainable level of service. Level of service "E" with average control delays of not more than 50 seconds per vehicle at an unsignalized intersection or 80 seconds per vehicle at a signalized intersection indicates near to at capacity conditions and is generally considered the limit of acceptable level of service and delay.

Full definitions of levels of service for unsignalized and signalized intersections and level of service summaries are included in the *Appendix*. The intersections studied by this report were analyzed according to the procedures set forth in the Highway Capacity Manual 2010, using the McTrans Highway Capacity Software (HCS7), release 7.9.5.

#### CR 571/CR 547

At the signalized CR 571/CR 547 intersection the signalized level of service protocol was followed with a finding that the intersection will operate at an overall level of service "C" for the AM peak street hour for both the *no-build* and *build* condition in the 2033 design year. The intersection will operate at an overall level of service "D" for the PM peak street hour for both the no-build and build condition. Incremental increases in delay at the intersection are minimal due to the project.



#### McDonough & Rea Associates, Inc.

 Traffic and Transportation Consulting

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Manchester Township Planning Board -5-

May 30, 2023

#### SITE ACCESS TO CR 571

At the site access to CR 571, findings were that exiting movements from the project to CR 571 will do so at level of service "C" for the AM peak street hour and level of service "D" for the PM peak street hour for the 2033 design year. Therefore, this intersection will operate within accepted traffic engineering parameters.

#### SITE ACCESS TO CR 547

At the site access to CR 547, findings were that exiting movements will do so at level of service "B" during the AM peak street hour and level of service "C" for the PM peak street hour. Therefore, this intersection will operate within accepted traffic engineering parameters.

#### **CONCLUSIONS**

It is concluded, based on MRA's analyses of the Manchester Township residential/office/retail project, that it can be approved and operate compatibly with future traffic conditions in the area. The site driveways to CR 571 and CR 547 will operate at acceptable levels of service for the 2033 design year as will the signalized offsite intersection of CR 571/CR 547.

A representative from MRA will attend an upcoming Manchester Township Planning Board meeting to provide expert testimony and answer questions Board members, Board experts or the public may have.

Very truly yours,

John H. Rea, PE Principal

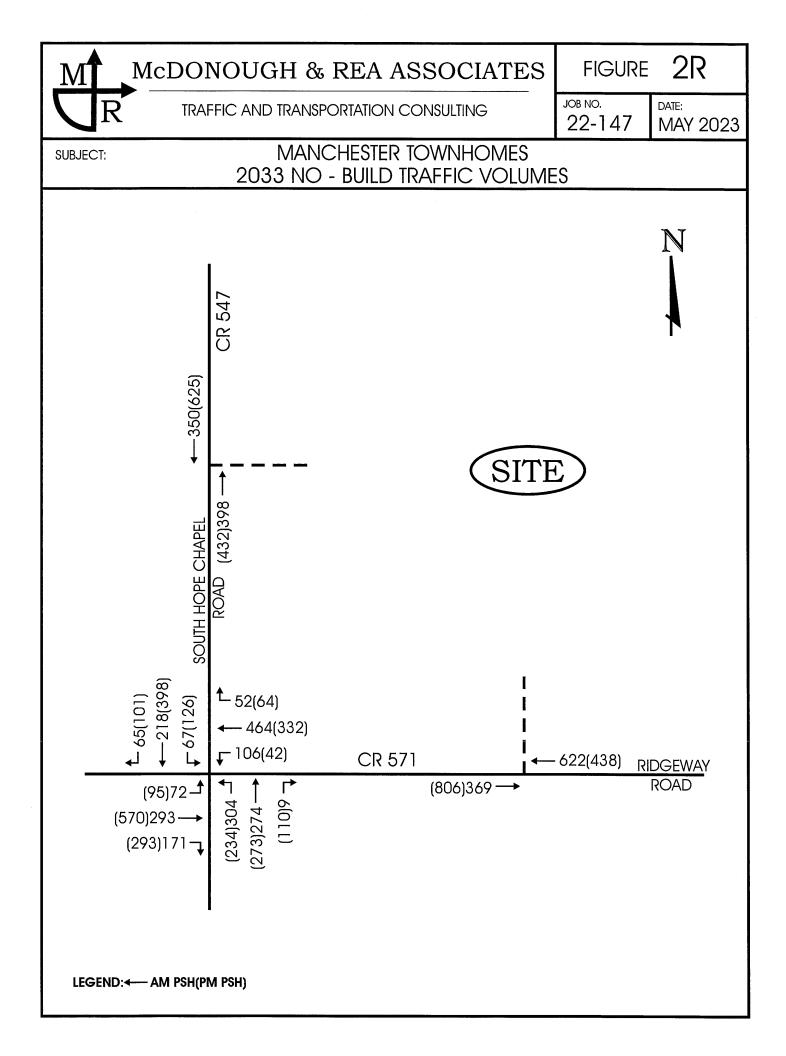
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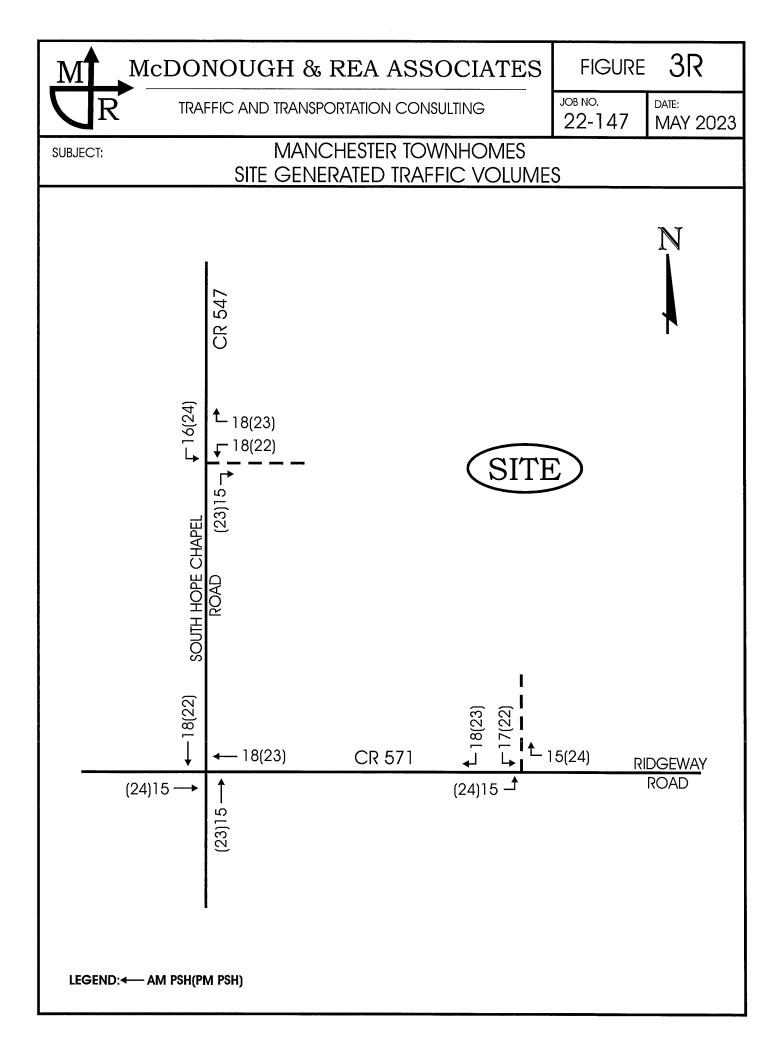
Mordechai Eichorn Ian Borden, PE

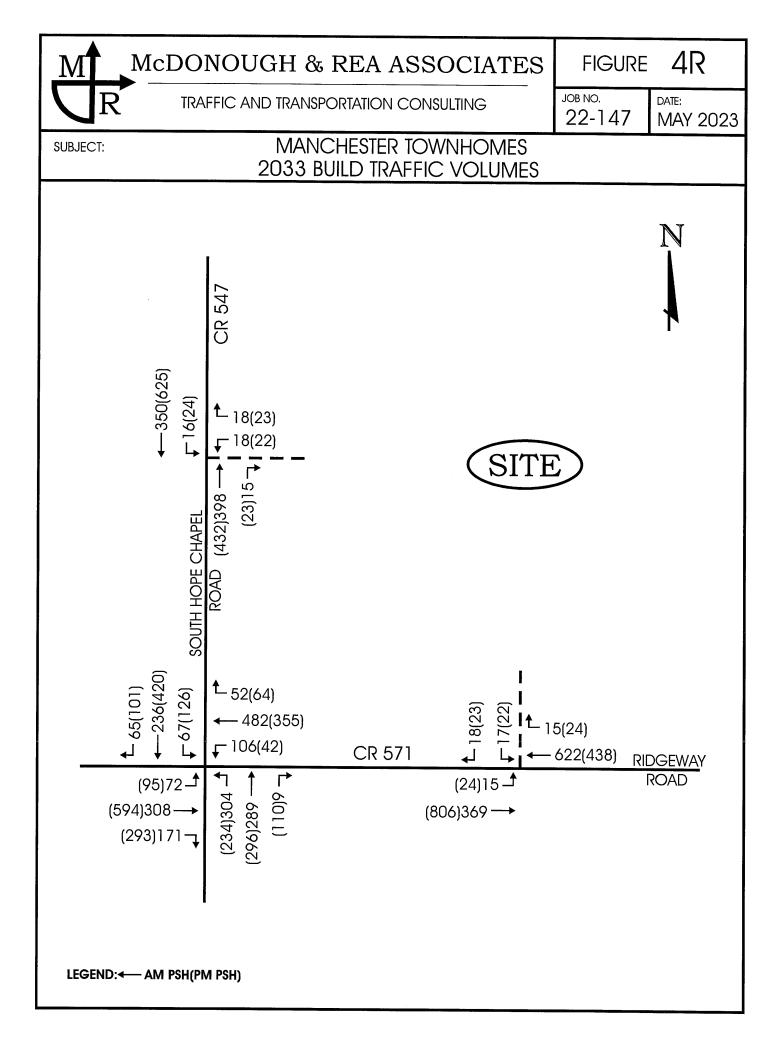
Scott T. Kennel Sr. Associate

# APPENDIX

MCDONOUGH & REA ASSOCIATES FIGURE	
TRAFFIC AND TRANSPORTATION CONSULTING	2022
SUBJECT: MANCHESTER TOWNHOMES SITE LOCATION MAP	
Condit On The LOCATION WAT	Club E







#### LEVEL OF SERVICE FOR SIGNALIZED INTERSECTIONS<sup>1</sup>

Level of Service	Description	Control (Signal) Delay <u>Per Vehicle (Seconds)</u>
А	Very short delay, good progression; most vehicles do not stop at intersection.	<u>&lt;</u> 10.0
В	Generally good progression and/or short cycle length; more vehicles stop at intersection than at Level of Service "A."	$> 10.0 \text{ and } \le 20.0$
С	Fair progression and/or longer cycle length; significant number of vehicles stop at intersection, though many still pass through without stopping.	$>$ 20.0 and $\leq$ 35.0
D	Congestion becomes noticeable; longer delays from unfavorable progression, long cycle lengths, or high volume/capacity ratios; many vehicles stop at intersection.	$>$ 35.0 and $\leq$ 55.0
Е	Considered to be the <u>limit of acceptable delay;</u> indicative of poor progression, long cycle lengths, or high volume/capacity ratios; frequent individual cycles failures.	$> 55.0$ and $\le 80.0$
F	Often an indication of over-saturation (i.e., arrival flow exceeds capacity); also caused by poor progression and long cycles lengths; capacity is not necessarily exceeded under this level of service.	> 80.0

<sup>&</sup>lt;sup>1</sup> Transportation Research Board, <u>Highway Capacity Manual 2010</u>, National Research Council, Washington, DC, 2010.

		HCS	6 Sigr	nalize	d Int	ersect	ion R	esult	s Sun	mary	1				
General Inforn	nation							1	ntersec	tion Inf		4			
Agency		MRA						Ľ	Duration	h	0.250			×↓↓ ↓	2851
Analyst		STK		Analys	sis Dat	е	******	A	rea Typ	е	Other				
Jurisdiction				Time F	Period	AM			PHF		0.90				
Urban Street	andidi Mildia ana ani ini an	CR 571-CR 547	nan na san an a	Analys	sis Yea	r 2033	NOBUIL	DA	Analysis	Period	1> 7:0	00			
Intersection				File Na	ame	22-14	7ANB-1	.xus						ጘቀቱ	
Project Descrip	tion	22-147ANB-1												RIA HA	
Demand Inform	nation				EB			WB			NB			SB	
Approach Move	ement			L	Т	R	L	T	R	L	Т	R	L	Т	R
Demand (v), v	reh/h			72	293	171	106	464	52	304	274	9	67	218	65
Signal Informa	tion		2000 - 2000 APR - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000				ιĻ	1245							
Cycle, s	90.0	Reference Phase	2		۲.	r∰" ∛	R	R			Ľ		4	5	
Offset, s	0	Reference Point	End	Green	7.0	25.0	10.0	26.0		0.0					4.
Uncoordinated	No	Simult. Gap E/W	On	Yellow		5.0	5.0	5.0	0.0	0.0					
Force Mode	Fixed	Simult: Gap N/S	On	Red	0.0	2.0	0.0	2.0	0.0	0.0		ŝ	6	2	
			n an baile The Contract												
Timer Results	4. Y			EBI	dina dina Tanàna dia kaominina dia kao Tanàna dia kaominina dia kaomini	EBT	WB	L	WBT	NBI		NBT	SB		SBT
Assigned Phase	e			5		2	1		6	3		8	7		4
Case Number		<ul> <li>A BEAUX PROPERTY AND A DESCRIPTION OF A DESC</li></ul>		1.1		4.0	1.1	(1997) - 1997) - 1997	4.0	1.1	and the second	4.0	1.1		4.0
Phase Duration				10.0		32.0	10.0		32.0	15.0		33.0	15.0		33.0
Change Period				3.0		7.0	3.0	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	7.0	5.0		7.0	5.0		7.0
Max Allow Head				2.7		0.0	2.7		0.0	2.7		2.9	2.7		2.9
Queue Clearan	ce Time	( <i>g</i> s), s		4.7		382 () 	6.1			12.0	)	7.9	4.4	an a	8.3
Green Extensio	n Time	(ge), s		0.0		0.0	0.0		0.0	0.0		1.0	0.0		1.0
Phase Call Pro	bability			1.00	)	1997 - 1997 1997 - 1997 - 1997 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1	1.00	)		1.00	)	1.00	1.00	) - I	1.00
Max Out Proba	bility			1.00			1.00			1.00	)	0.00	0.01	1	0.00
Movement Group Results		. see 2942	din e se	ËB			WB			NB			SB		
Approach Movement			L	Т	R	L	T	R	L	Т	R	L	Т	R	
Assigned Movement			5	2	12	1	6	16	3	8	18	7	4	14	
Adjusted Flow I	Rate ( v	), veh/h		80	271	244	118	291	282	338	158	157	74	161	154
Adjusted Satura	ation Flo	w Rate ( <i>s</i> ), veh/h/l	n	1781	1870	1641	1781	1870	1804	1781	1870	1849	1781	1870	1725
Queue Service				2.7	11.0	11.4	4.1	12.0	12.1	10.0	5.9	5.9	2.4	6.0	6.3
Cycle Queue C		e Time ( <i>g c</i> ), s		2.7	11.0	11.4	4.1	12.0	12.1	10.0	5.9	5.9	2.4	6.0	6.3
Green Ratio ( g				0.36	0.28	0.28	0.36	0.28	0.28	0.40	0.29	0.29	0.40	0.29	0.29
Capacity ( c ), v		2010) <u>- 110 - 110 - 110 - 110 - 110 - 110</u>		321	520	456	333	520	501	488	540	534	492	540	498
Volume-to-Cap				0.250	0.522		0.354	0.560	0.563	0.692	0.292	0.293	0.151	0.297	0.309
	and the second se	t/In ( 85 th percentile	and the second se	54.6	188	172.4	81.9	202.6	195.6	208.7	109.1	106.8	43.8	111	106.4
		eh/ln ( 85 th percenti		2.1	7.4	6.9	3.2	8.0	7.8	8.2	4.3	4.3	1.7	4.4	4.3
		RQ) (85 th percent	ile)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Uniform Delay				20.8	27.5	27.6	21.2	27.8	27.8	22.2	24.9	24.9	17.3	24.9	25.0
Incremental De			en in statut. Satu tunga	1.9	3.7	4.5	2.9	4.3	4.5	7.9	1.4	1.4	0.7	1.4	1.6
Initial Queue De				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Control Delay (		əh		22.6	31.2	32.1	24.1	32.1	32.4	30.1	26.2	26.3	17.9	26.3	26.6
Level of Service		/1.00		C	C		C	C	C	C	C	C	В	C	C
Approach Delay				30.4		C	30.8	3	С	28.2	2	С	24.8	3	С
Intersection De	lay, s/ve	en / LOS				29	9.0				·		С		
Multimodal Re					EB			WB			NB			SB	
Pedestrian LOS	S Score	/LOS													
Bicycle LOS Sc	ore / LC	)S													

	НС	S Sigr	nalize	d Inte	ersect	ion R	esult	ts Sun	nmary	7				
											1997 - Alexandra 1997 - Alexandra III - Alexandr 1997 - Alexandra III - Alexandra		- S. 197	
General Information							•	Intersec	tion Inf	ormatio	on	Q.	<b></b>	
Agency	MRA							Duration	h	0.250				
Analyst S	STK		Analy	sis Date	÷		/	Area Typ	е	Other	•			
Jurisdiction			Time I	Period	AM			PHF		0.90	5.1 1 1 1 1 1 1 1 1 1 1		vi 🕂 E	<b>↓</b>
Urban Street C	CR 571-CR 547		Analy	sis Year	· 2033	BUILD	4	Analysis	Period	1> 7:(	00			
Intersection			File N	ame	22-14	7AFB-1	.xus						ጘቀቅ	
Project Description 2	22-147AFB-1											i i i i i i i i i i i i i i i i i i i	N THE	ein
Demand Information		an de la compañía de La compañía de la comp		EB			WE	3		NB			SB	
Approach Movement			L	Т	R	L	Т	R	L	Т	R	L	Т	R
Demand ( v ), veh/h			72	308	171	106	482	2 52	304	289	9	67	236	65
Signal Information					N N N N N N N N N N N N N N N N N N N	ЦĻ	1,11,							
Cycle, s 90.0	Reference Phase	2	1	<b>۲</b> «	╘╴					Ľ		3		QÈ .
Offset, s 0	Reference Point	End	Green	7.0	25.0	10.0	26.0	<b>17</b> 0.0	0.0					<u></u>
Uncoordinated No	Simult. Gap E/W	On	Yellow		5.0	5.0	5.0		0.0					ৰিছিল
Force Mode Fixed	Simult. Gap N/S	On	Red	0.0	2.0	0.0	2.0	0.0	0.0		5	6		
Timer Results		State and	EB	New Iss.	EBT	WB		WBT	NBI		NBT	SBI	120	SBT
Assigned Phase			5	<b>-</b> 1638 6.353	2	тур 1		о <b>м</b> ы 6	3	- yest (Arth)	1ND 1 8	<u>о</u> ві 7	-97.98 SOUC	<u>301</u> 4
Case Number		6,6283	1.1		4.0	1.1	્રે તેર કે દિવસ	4.0	1.1	802 (SA)	4.0	1.1	9.0635 (1986)	4.0
Phase Duration, s		an an stàitean an	10.0		32.0	10.0		32.0	15.0	A LEAST STOLEN AND A SHALLOOF	33.0	15.0		33.0
Change Period, (Y+R c)	) s		3.0		7.0	3.0		7.0	5.0		7.0	5.0		7.0
Max Allow Headway ( M		and an and an an an	2.7	100000	0.0	2.7		0.0	2.7	3226.71 (* 1666)	2.9	2.7	and the second second second	2.9
Queue Clearance Time (			4.7		0.0	6.1		0.0	12.0	<u>)</u>	8.3	4.4		8.7
Green Extension Time (			0.0	a la caracteria de la cara	0.0	0.0	w stratect scales	0.0	0.0	- 166 (A. 16)	1.0	0.0		1.0
Phase Call Probability	9 : ), 0		1.00	······		1.00		0.0	1.00		1.00	1.00		1.00
Max Out Probability		999 - 19 <b>19 19</b> 19	1.00		onese er de s	1.00		an brinn de ste skriederen.	1.00	and days waters	0.00	0.01	menterike disetine	0.00
Movement Group Resu	ilfs			EB			WB		154.14-14	NB	and the second		SB	
Approach Movement		and a strength of the	L	Т	R	L	Гт	R	L	Т	R		Гт	R
Assigned Movement			5	2	12	્યારક	6	16	- 3	8	18	- 7	4	14
Adjusted Flow Rate (v),	, veh/h		80	280	253	118	301	292	338	166	165	74	171	164
Adjusted Saturation Flow		n	1781	1870	1647	1781	1870		1781	1870	1850	1781	1870	1733
Queue Service Time (g			2.7	11.4	11.8	4.1	12.5		10.0	6.2	6.3	2.4	6.4	6.7
Cycle Queue Clearance			2.7	11.4	11.8	4.1	12.5		10.0	6.2	6.3	2.4	6.4	6.7
Green Ratio ( g/C )			0.36	0.28	0.28	0.36	0.28	0.28	0.40	0.29	0.29	0.40	0.29	0.29
Capacity ( c ), veh/h			314	520	458	327	520	502	479	540	535	485	540	501
Volume-to-Capacity Rati	o(X)		0.255		0.552	0.360	0.579	1 - 2 <sup>21</sup> - 2 <sup>2</sup> - 2 <sup>2</sup>	0.705	0.307	0.309	0.154	0.316	0.327
Back of Queue (Q), ft/l		e)	54.8	194.3	178.8	82.2	210.4		210.5	114.4	112	43.9	117.2	112.3
Back of Queue (Q), veh			2.2	7.7	7.2	3.2	8.3	8.1	8.3	4.5	4.5	1.7	4.6	4.5
Queue Storage Ratio ( R			0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Uniform Delay ( <i>d</i> 1), s/v			20.9	27.6	27.7	21.2	28.0		22.4	25.0	25.0	17.3	25.0	25.1
Incremental Delay ( d 2 )			1.9	4.0	4.7	3.1	4.7	4.9	8.4	1.5	1.5	0.7	1.5	1.7
Initial Queue Delay ( d 3			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Control Delay ( d ), s/veh			22.8	31.6	32.5	24.3	32.6	32.9	30.8	26.4	26.5	18.0	26.6	26.9
Level of Service (LOS)		21.76 L	С	С	С	С	С	С	С	С	С	В	С	С
Approach Delay, s/veh /	LOS		30.8	3	C	31.4	4	С	28.7		С	25.1		C
				<b>.</b>	29	9.4		1997 - 1995 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -				С		
Intersection Delay, s/veh	1/LOS													
Intersection Delay, s/veh	LOS			FR			\//P	1 19 A A	na ana ana ana ana ana ana ana ana ana	NR			QD	
				EB			WB			NB			SB	

#### **HCS Signalized Intersection Results Summary**

		HCS	S Sigr	nalize	d Inte	ersect	ion R	esul	ts Sun	nmary	1				
General Inform	nation							ľ	Intersec	tion Infe		424	£ L		
Agency		MRA	far en ser						Duration	, h	0.250			*+ + \	
Analyst		STK		Analys	sis Dat	е			Area Typ	e	Other	•			
Jurisdiction				Time F	Period	PM			PHF		0.90				↓
Urban Street		CR 571-CR 547		Analys	sis Yea	r 2033	NOBUIL	D	Analysis	Period	1> 7:0	00			
Intersection		la -		File N	ame	22-14	7PNB-1	.xus						为十体	
Project Descrip	otion	22-147PNB-1											5	3 1 5 1	
Demand Infor	mation				EB			W	3		NB			SB	
Approach Mov	ement			L	Τт	R	L	Τ		L	ГТ	R	L	Т	R
Demand (v), v				95	570		42	33		234	273		126	398	101
				,										In British and States	
Signal Informa	ation						L L	171							
Cycle, s	90.0	Reference Phase	2	1	<b>•</b>	TË '	۳ <b>א</b>		17						
Offset, s	0	Reference Point	End	Green	7.0	25.0	10.0	26.		0.0					
Uncoordinated		Simult. Gap E/W	On	Yellow	3.0	5.0	5.0	5.0	0.0	0.0		P			
Force Mode	Fixed	Simult. Gap N/S	On	Red	0.0	2.0	0.0	2.0	0.0	0.0		5	6		
Timer Results				EBI		EBT	WB		WBT	NBI	Suc 200	NBT	SBI		SBT
Assigned Phas				5		2	1		6	3		8	7	- 331 233	4
Case Number			ie cieren	1.1	25.0 S.S	4.0	1.1	239	4.0	1.1	NG 1 2020	4.0	1.1	525-55 MAG	4.0
Phase Duration	ı s			10.0		32.0	10.0		32.0	15.0		33.0	15.0	st the second	33.0
Change Period		<u>_)                                    </u>		3.0		7.0	3.0		7.0	5.0		7.0	5.0		7.0
Max Allow Hea			anterne i cato.	2.7		0.0	2.7	in the second second	0.0	2.7	- 10 July -	7.0 3.0	2.7		3.0
Queue Clearar			1998 - 199 1998 - 1999	5.7		0.0	3.6		0.0	11.2		10.9	6.6		13.7
Green Extensio				0.0	Manufasar (1986)	0.0	0.0		0.0	0.0	1403.52	10.9	0.0		1.5
Phase Call Pro		(90,70	1. 19 A.	1.00			1.00		0.0	1.00		1.00	1.00		1.00
Max Out Proba				1.00	a an		0.2			1.00		0.01	0.36	andere e de service	0.03
Movement Gr	ouro Peo	5110 S	N. S. S. S. Filmer and	1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	EB			WB		an a	NID	e in a start fil		OD	
Approach Mov		suits		<u> 1997</u>	с ср Гт	R		T	-	1 1	NB T			SB	
			a na sa	L Sare Said	। 		L		R	L		R	L	T	R
Assigned Move Adjusted Flow		· )		5	2	12	1	6	16	3	8	18	7	4	14
			12	106	509	450	47	224		260	220	205	140	285	269
	inni inni ini ini ini ini ini ini ini i	ow Rate (s), veh/h/l	<u>in a çes</u>	1781	1870	1655	1781	1870		1781	1870	1689	1781	1870	1740
Queue Service			an an taona an a	3.7	24.3	24.3	1.6	8.9		9.2	8.5	8.9	4.6	11.5	11.7
<u>antitutui, iliin kiin kuun kuun kuun kuun kuun kuun k</u>		e Time ( <i>g c</i> ), s	0.85.8860	3.7	24.3	24.3	1.6	8.9		9.2	8.5	8.9	4.6	11.5	11.7
Green Ratio ( g			aansi sekarit	0.36	0.28	0.28	0.36	0.28		0.40	0.29	0.29	0.40	0.29	0.29
Capacity (c),		atia (X)	eta, Stil	366	520	460	219	520		395	540	488	440	540	503
Volume-to-Cap			Ne. viziti	0.289	0.979		0.214	0.43		0.659	0.408	0.421	0.318	0.528	
		t/In (85 th percentile		72.2	482.3		33.1	154.8	11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	164.6	149.2	140.2	85.8	194	183.7
		eh/In (85 th percenti		2.8	19.0	17.4	1.3	6.1	5.9	6.5	5.9	5.6	3.4	7.6	7.3
		RQ) (85 th percent	uie)	0.00	0.00	0.00	0.00	0.00	and and and and a state of the	0.00	0.00	0.00	0.00	0.00	0.00
Uniform Delay				20.6	32.2	32.2	22.7	26.7		20.5	25.8	25.9	18.3	26.9	26.9
Incremental De				2.0	34.7	37.1	2.2	2.6		8.4	2.3	2.7	1.9	3.7	4.0
Initial Queue D				0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0
Control Delay (				22.6	66.9	69.4	24.9	29.3		28.8	28.1	28.6	20.2	30.5	31.0
Level of Servic				C	E	<u>E</u>	С		<u> </u>	С	С	<u> </u>	С	C	C
Approach Dela				63.6	<u>ن</u> ا	E	29.0	0	С	28.5	<u>)</u>	С	28.6	3	С
Intersection De	elay, s/ve	en / LOS				4	1.3						D		
Multimodal Re	esults			an an sta	EB			WB			NB			SB	
Pedestrian LO		/LOS			Í		ant an isi a	Ī					ľ	T	
													-	1	

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******	HCS	S Sigr	nalize	d Inte	ersect	ion R	esul	ts Sur	nmary	1				
General Information								Intersec	tion Inf	14403年1月1日				
Agency	MRA							Duration	, h	0.250			i4 ↓ ∫.	
Analyst	STK		Analy	sis Date	e			Area Ty	be	Other	•			
Jurisdiction			Time I	Period	PM			PHF		0.90				4
Urban Street	CR 571-CR 547		Analys	sis Yea	r 2033	BUILD	Γ	Analysis	Period	1> 7:(	00			*
Intersection			File N	ame	22-14	7PFB-1	.xus						ጘተቱ	
Project Description	22-147PFB-1											-2 04	an ara	an a
Demand Information		The second		EB			W	З		NB		a an	SB	
Approach Movement			L	Т	R	L	Т	R	L	Т	R	L	Т	R
Demand ( v ), veh/h			95	594	293	42	35	5 64	234	296	110	126	420	101
Signal Information		The second second			, in the second s	ιŢ	Į.Į							
Cycle, s 90.0	Reference Phase	2		₽.	∼⊟" ≗					Ľ				¢)
Offset, s 0	Reference Point	End	<u></u>	170								<u>Y – –</u>		<u>.</u>
Uncoordinated No	sdiction sdiction $(P \times P)$ (P + P + P + P + P + P + P + P + P + P		Green Yellow	000000000000000000000000000000000000000	25.0 5.0	10.0 5.0	26. 5.0		0.0				U J	ৰেছিয়
Force Mode Fixed		On On	Red	0.0	2.0	0.0	2.0		0.0		3	6		
							onocional live			n Europa				
Timer Results			EB	<b>-</b> 201	EBT	WB	Le	WBT	NBI	<u>1963</u> 863	NBT	SB	<u>-</u>	SBT
		en de Lines de	5	SAL 25 252	2	1	1.1.2.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1	6	3	A. Mari Manih	8	7		4
and the second state of the second stat			1.1	N. The State of the second	4.0	1.1	terre en e	4.0	1.1		4.0	1.1		4.0
		an a	10.0	1	32.0	10.0		32.0	15.0		33.0	15.0		33.0
			3.0		7.0	3.0		7.0	5.0		7.0	5.0		7.0
			2.7		0.0	2.7		0.0	2.7		3.0	2.7		3.0
			5.7	tanà amin'ny dia		3.6	Sacher and		11.2	CONSISTER OF STREET	11.4	6.6	21.000	14.3
	(ge), S		0.0		0.0	0.0		0.0	0.0		1.7	0.0		1.6
		n da serie da da Granda da serie da ser Serie da serie da ser	1.00	7 . 100 Dec . 1995 - 1		1.00	30 - 10 - 10 - 10 - 10 - 10 - 10 - 10 -		1.00		1.00	1.00		1.00
Max Out Probability			1.00	)		0.2	1		1.00	)	0.01	0.36	5	0.04
Movement Group Res	sults			EB			WB			NB			SB	
Approach Movement			L	Т	R	L	Т	R	L	Т	R	L	Т	R
Assigned Movement			5	2	12	-1	6	16	3	8	18	7	4	14
Adjusted Flow Rate (v	), veh/h		106	522	463	47	237	228	260	233	218	140	298	281
		1	1781	1870	1660	1781	1870	) 1771	1781	1870	1699	1781	1870	1745
Queue Service Time (	g s ), S		3.7	25.0	25.0	1.6	9.5	9.6	9.2	9.1	9.4	4.6	12.1	12.3
Cycle Queue Clearanc	e Time ( g c ), s		3.7	25.0	25.0	1.6	9.5	9.6	9.2	9.1	9.4	4.6	12.1	12.3
Green Ratio ( g/C )			0.36	0.28	0.28	0.36	0.28	0.28	0.40	0.29	0.29	0.40	0.29	0.29
Capacity ( c ), veh/h			356	520	461	219	520	492	387	540	491	430	540	504
Volume-to-Capacity Ra	itio(X)		0.296	1.005	- L	0.214	0.45	7 0.464	0.673	0.432	0.444	0.325	0.551	0.557
		and the second	72.6	517.1	466.3	33.1	163.0	3 157	166.2	157.6	148.3	86	203.5	192.3
· · · · · · · · · · · · · · · · · · ·			2.9	20.4	18.7	1.3	6.4	6.3	6.5	6.2	5.9	3.4	8.0	7.7
		ile)	0.00	0.00	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00
Uniform Delay ( <i>d</i> 1), s	/veh		20.7	32.5	32.5	22.7	26.9	26.9	20.6	26.0	26.1	18.4	27.1	27.1
			2.1	40.7	43.1	2.2	2.9	3.1	9.0	2.5	2.9	2.0	4.0	4.4
			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Control Delay ( d ), s/v	əh		22.8	73.2	75.6	24.9	29.8	30.1	29.6	28.5	29.0	20.4	31.1	31.5
Level of Service (LOS)			С	F	F	С	C	С	С	С	С	С	С	С
			69.3	3	E	29.5	5	С	29.1	1	С	29.2	2	С
Intersection Delay, s/ve	eh / LOS				4:	3.6						D		
Multimodal Results				EB	2. 1997 - 1997		WB	1992. Ng tao 1993 a	97 - S.	NB			SB	
Pedestrian LOS Score	/108				ng ta tang é.		, vo				vy střížek	<u>li terre e di</u>		
Bicycle LOS Score / LO		s	8 . S				04 9. V		N 8 1 1		a da ana ana			

#### LEVEL OF SERVICE CRITERIA FOR TWO-WAY STOP-CONTROLLED INTERSECTIONS<sup>1</sup>

Level of Service	<b>Average Control Delay</b>
А	$\leq 10.0$ Seconds Per Vehicle
В	$> 10.0$ and $\le 15.0$ Seconds Per Vehicle
С	$>$ 15.0 and $\leq$ 25.0 Seconds Per Vehicle
D	$>$ 25.0 and $\leq$ 35.0 Seconds Per Vehicle
E	$>$ 35.0 and $\leq$ 50.0 Seconds Per Vehicle
F	> 50.0 Seconds Per Vehicle

<sup>&</sup>lt;sup>1</sup> Transportation Research Board, <u>Highway Capacity Manual 2010</u>, National Research Council, Washington, DC, 2010.

		l sea	ICS	TWO-	way	διορ	D-COI	ntrol	керс	on						
General Information							Site	Inform	natio	n		and the			an a	
Analyst	STK			2.00.00.000			Inter	section			RT 57	1 & SITE	ACCESS		198703.1-57	
Agency/Co.	MRA						Juris	diction								
Date Performed	5/24,	/2023					East/	West Str	eet		RT 57	71		and in the sea		1946 - Yoshing A.
Analysis Year	2033						Nort	h/South	Street		SITE	ACCESS				
Time Analyzed	AM	ininitian di kinak	inega ang ang ang ang ang ang ang ang ang a				Peak	Hour Fa	ctor		0.90					
Intersection Orientation	East-	West					Analy	ysis Time	Period (	hrs)	0.25					
Project Description	22-14	47AFB-2	BUILD				<b>Barran</b> an Andrea		terint den det terintetet			initiitemines/hisk				
Lanes	No.2 years		and the second s								e Diger.					
						L or Street: Ea										
Vehicle Volumes and Adju	ıstme	ents												and the second	- (3.4 %)	
Approach	a luga ja 1980 menar	- Contractory	oound	1		West	bound	1	an a	and take week	bound	a nggalantan na		NO TRACTOR M	bound	and the second second
Movement	-U	L.	T.	R	J	L.L.	T :	, R	U	L J	ा	; R	: U	L.	T	R
Priority	10	1	2	3	4U	4	5	6		7	8	9		10	11	12
Number of Lanes	0	0	1	0	0	0	1	0		0	0	0		⊇ 0.÷;	1	0
Configuration		LT		a washer w				TR	a and a state						LR	No.41 Sec. 1994
Volume (veh/h)		-15	369				622	15			14 21 - 14			17		18
Percent Heavy Vehicles (%)	a 2 constator relation	3		- Carolina Science		NAMES / COLORADO	Strengt Stern					- 20700-00-00 - 2010		3		3
Proportion Time Blocked			1. 1. A.									a state				
Percent Grade (%)						THE SECOND									0	
Right Turn Channelized														÷		
Median Type   Storage				Und	ivided							2010-002010-0020-0020	and the second second second	March March 1997		
Critical and Follow-up He	adwa	ys						9 dini								
Base Critical Headway (sec)	ſ	4.1		I	T		Γ				I		I	7.1		6.2
Critical Headway (sec)		4.13												6.43		6.2
Base Follow-Up Headway (sec)		2.2		ľ		T	I	1			I	T	l	3.5	ľ	3.3
Follow-Up Headway (sec)		2.23												3.53		3.3
Delay, Queue Length, and	l Leve	l of S	ervice	<b>)</b>												90 M.
ciaj, daoac nongen, ana		17	neko seri je T				oanasio/d		<u></u>			n se			39	
		1 ''	<u> </u>			1.000	5.85 M								291	
Flow Rate, v (veh/h)		886		그는 것이 같은 것이야? 가			1.200.20	<b>_</b>	<b> </b>	11 12 19 19	13435		<b>F</b> errar	1387-833¥	L: 67 5 3	
Flow Rate, v (veh/h) Capacity, c (veh/h)		886 0.02				anger na fa	T							I	0.13	ľ
Flow Rate, v (veh/h) Capacity, c (veh/h) v/c Ratio		886 0.02 0.1											STAR STAR		0.13	203
Flow Rate, v (veh/h) Capacity, c (veh/h) v/c Ratio 95% Queue Length, Q <sub>95</sub> (veh)		0.02	0.2												0.5	
Flow Rate, v (veh/h) Capacity, c (veh/h) v/c Ratio 95% Queue Length, Q <sub>95</sub> (veh) Control Delay (s/veh)		0.02 0.1 9.1	0.2 A												0.5 19.3	
Flow Rate, v (veh/h) Capacity, c (veh/h) v/c Ratio 95% Queue Length, Q <sub>95</sub> (veh)		0.02 0.1 9.1 A												1	0.5	

			HCS	Two-	Way	Stop	o-Co	ntrol	Repo	ort										
General Information		19 1				2 m	Site	Infor	natio	n										
Analyst	STK						Inter	section			RT 57	1 & SITE	ACCES	5						
Agency/Co.	MRA						Juris	diction												
Date Performed	5/24/	/2023					East/	West Str	eet		<b>'1</b>									
Analysis Year	2033						Nort	h/South	Street		SITE ACCESS									
Time Analyzed	PM						Peak	Hour Fa	ctor		0.90	0.90								
Intersection Orientation	East-	West					Anal	ysis Time	Period	(hrs)	0.25									
Project Description	22-14	47PFB-2	BUILD								a and a second second				2	8 <u></u>				
Lanes								an Mana arta		- 24 - S. S		C.G. C.L.								
						ـــــــــــــــــــــــــــــــــــــ														
Vehicle Volumes and Adj	justme	nts			Maj	or Street: E	ast-West				n Lesser Poly									
Approach		Eastł	oound			West	tbound			North	bound		Contraction of the Contraction of Co	South	bound					
Movement	U.	L.S.	. T .:	R	U	L	T.	R	U .	L	T	R	U	L.	τ÷	R				
Priority	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12				
Number of Lanes	0	. 0	1	0	. 0	0	1	0		0	0	0		0	,1	0				
Configuration		LT						TR							ĻR	T				
Volume (veh/h)		24	806				438	24						22		23				
Percent Heavy Vehicles (%)		3									I		Ι	3		3				
Proportion Time Blocked	16												100							
Percent Grade (%)					Ι								l		0	allacione di science i				
Right Turn Channelized				Sing Ann Chi Martin Sing Martin Sing																
Median Type   Storage				Und	ivided				1					utition and a second						
<b>Critical and Follow-up H</b>	eadwa	ys		Cippedia	e file state	$p(a^2)$		See ada				estex.								
Base Critical Headway (sec)		4.1			1		I		<u> </u>					7.1		6.2				
Critical Headway (sec)		4.13								1. 1. set 1. s				6.43		6,23				
Base Follow-Up Headway (sec)		2.2		<u>e 2382,355</u>		1 (j. 14 (m. 64)) 1					지는 것을 많이 한다.	gel sindigette		3.5	: 2023 AUT	3.3				
Follow-Up Headway (sec)		2.23								1				3.53		3.33				
Delay, Queue Length, an	dlave			in de la compañía de	1			Line States		L	<b>I</b>	l Second	L Geografie	1	l Materia	<u></u>				
	u Leve			r T	2-12-16-1 T	1	ringer T	- 147 S	1				T							
Flow Rate, v (veh/h)	11 11 (11 (11 (11 (11 (11 (11 (11 (11 (1	27							Marian		an a		a Sata Aria	17-2-2	50					
Capacity, c (veh/h)	<u> 1993</u> 8	1047		174822	10000	123783		1						<u> Sasta</u>	223					
v/c Ratio		0.03		Ngangalaka				5 38422423	an ser an		n en generation		1989-1914 - 1		0.22	a de la constante				
95% Queue Length, Q <sub>95</sub> (veh)		0,1									1				0.8	18986				
Control Delay (s/veh)		8.5	0.4	 			2 200 S S S S	1		1	<u> </u>	<u> </u>		<u> </u>	25.7	<u> </u>				
Level of Service (LOS)	10000	A	A												D					
Approach Delay (s/veh)			.7		-				ļ					2	5.7					
Approach LOS			A												D					

	5		HCS	Two-	Way	Stop	-Cor	ntrol	Repo	ort									
General Information							Site	Inform	natio	n					a Caratan Santa				
Analyst	STK					40020-003	Inters	section			RT 54	7 & SITE	ACCESS						
Agency/Co.	MRA		19. 19.				Jurisc	liction	Area Gula										
Date Performed	5/24/	/2023					East/	West Str	eet		ACCESS								
Analysis Year	2033	÷					Nortł	n/South	Street		RT 54	RT 547							
Time Analyzed	AM	<u></u>					Peak	Hour Fa	ctor		, selection (Constraints)								
Intersection Orientation	North	n-South			1	144 ( 1	Analy	vsis Time	Period (	hrs)	0.25								
Project Description	22-14	47AFB-3	BUILD		deres seguration of the														
Lanes					V.						0.00								
					<u>na</u>	网级数	<b>FE IO</b> IIA	998999999999 	1.										
					- All	↓ ↓													
				Ď															
				_		1													
					Majo	r Street: Nor	th-South												
Vehicle Volumes and Adju	ıstme	nts																	
Approach	09203/079271	2010-000-000-000-000-000-000-000-000-000	bound			West	bound		a composite	North	ibound Southbound								
Movement	Ú	L.	Т	, R	Ū	L -	Т	R	U	Ŀ	т	R	. U	L.	т	R			
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6			
Number of Lanes		<u>, 0</u>	-0	.0		0	1	- 0	-0	0	1	0	0	0	1	0			
Configuration		-1.236-16-8257A	1				LR		anna ann an 1979. Tha ann an 1979 anns an 1979			TR	a sanaran	LT	ali de la composition de la composition La composition de la c				
Volume (veh/h)						18		18			398	15		16	350				
Percent Heavy Vehicles (%)		nong ti papah	1 10000 2000	0.000	e na Nerada	3		3						3	792.99%).	28.470			
Proportion Time Blocked	ni standar Alexandra																		
Percent Grade (%)	o a canadara a na c	10 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		an and an area of		an an chuir an ch	0	an i dhe internet						2 Mar 2 (1977)	1.111.24				
Right Turn Channelized				an search										5.4.5					
Median Type   Storage	De control de Marie			Undi	vided		<u>Reflecte de </u>			Constanting and a second			a bela n chu		energia (VE) dej	NG 196 1-23			
Critical and Follow-up He	adwa	vs	ak wa	- ang kapang sa		en Carlige		e dan kara		en server e		look attai			e des	100			
Base Critical Headway (sec)	200369293 	<b>-</b>	<u>1</u>			7.1		6.2	1	initeration T	Ī		1990 (1990) 	4.1	<u></u>	Ī			
Critical Headway (sec)	an a					6.43		6.23					<u> </u>	4.13		198.0			
Base Follow-Up Headway (sec)						3.5		3.3			06.03559			2.2					
Follow-Up Headway (sec)		ere egi servi Vetava filad				3.53		3.33						2.23					
				La sectore		L		1.5.55	and the second sec	a a desta		l Astronom			l Salat 18	1			
Delay, Queue Length, and	i Leve	1013	ei vice T			75875 1				n services I		T			T T	1			
Flow Rate, v (veh/h)							40			and the	a na sanaka	1		18		10,000			
Capacity, c (veh/h)	n ddaeldi	1999		133.68		esseries.	412							1097	Pressee				
v/c Ratio	1.5328	an a				ar sairar i	0.10	-	ing sing the	(Alternation		1.000 COR-1	化基门管路路	0.02	TANK SOUTH				
95% Queue Length, Q <sub>95</sub> (veh)			19353				0.3	말음을	0.550					0.0					
Control Delay (s/veh)	Darquiner.				an that the		14.7 P				2. 2. s. s. (1944)		્રે છે. સંસ્થાર	8.3	0.2				
Level of Service (LOS)	15 4 (ALE) 		- Second				B		prosition		196933			A	A				
Approach Delay (s/veh)				an a			4.7				1. 1	Antonia di Santa		international	).5				
Approach LOS					1323		B		L						A				

			HCS	Two-	Way	Stop	o-Cor	ntrol	Repo	ort									
General Information					and the		Site	Inforr	natio	n				1 12 - 22 - 13					
Analyst	STK				an is a subsidie		Inter	section	1.9		RT 54	7 & SITE	ACCES	5					
Agency/Co.	MRA	e de la composition de la comp			1976 - S		Juriso	diction		Not March									
Date Performed	5/24/	/2023					East/	West Stre	eet	and and a second	SITE ACCESS								
Analysis Year	2033						Nortl	n/South !	Street		RT 547								
Time Analyzed	PM		ng ing pangang ng pa					Hour Fac			0.90	en e							
Intersection Orientation	North	1-South				a Angel	Anal	/sis Time	Period (	hrs)	0.25				1947. AN				
Project Description	22-14	47PFB-3	BUILD			1992 - SAN S	1.1				a da ang ang ang ang ang ang ang ang ang an		n an						
Lanes										i internet									
			ang carbagi			nya	BE	1000-000-000 1				88 - 19 - 20 - 19 - 19 - 19 - 19 - 19 - 19 - 19 - 1							
						ł	ken i den konstandigen die best												
				S															
						4	EXECUTION	7											
					0010000 100000000 0	Street: No	The South												
Vehicle Volumes and Adju	stme	nts											194 OF						
Approach		Easth	bound			West	bound			North	bound			South	nbound				
Movement	U	Ľ		R	* U -	Ľ	T.	, R	Ú	L	Т	R	Ű	L.	T.	R			
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6			
Number of Lanes		0	0	0		0	1	0	··0 ·	0	1	0	0	Ú. Ó	8 14	0			
Configuration							LR	and a subject of				TR	CHARGE CONTRACTOR	LT					
Volume (veh/h)					843 S	22		23			432	23		24	625				
Percent Heavy Vehicles (%)	0-96403649	1996 W. K. 1998 H.	1 (27) - 20)			3	1999-1997 (No. 1975	3				1. 1997 - 1943 - 1944 1947 - 1947 - 1947 - 1947 - 1947 - 1947 - 1947 - 1947 - 1947 - 1947 - 1947 - 1947 - 1947		3	10.558N5.051				
Proportion Time Blocked	a Alayana Marina																		
Percent Grade (%)			1 Charles and				0	1997-00940											
Right Turn Channelized	a geografi						e Mary			1. Maria		1999. 1997	and a star	692.003		a an			
Median Type   Storage				Und	ivided					982 A. 279 (2.)					ing a find with the				
Critical and Follow-up He	adwa	vs						and the same											
Base Critical Headway (sec)	aleran in the		inana 2003) I	in staat		7.1		6.2		1688-0154 		(C2+)_3(4) 	a' 35.4.'		WARCEST!	<u>8</u> 1 - 2019 - 1			
Critical Headway (sec)	ang pang		r Belleview				3.00 Ma				1.42 A.A.A		1. <b>31</b> 16 13	4.1	1000				
Base Follow-Up Headway (sec)						6.43		6.23	22.192			120.404	3 C. 1997	4.13					
Follow-Up Headway (sec)						3.5 3.53	Naparaje	3.3			19/9(1993)	- 1903-045-114	6.19.354	2.2		1955-578-00			
and the second		1. 1	<u> </u>	1000		5.55		3.33				L. Statistics	NOT DO	2.23					
Delay, Queue Length, and	Leve	i ot So	ervice		<u></u>		5.3589 2.4 - 00.48 1			<u>г</u>		<u>.</u>		1					
Flow Rate, v (veh/h)						antes antes a	50	the second second	a da station e	National Second Second		a la secondada da seconda		27	a ada secura da secura	1 2012 100000			
Capacity, c (veh/h)				123			282							1054					
v/c Ratio						Sec. 1996	0.18	1		a selan in se		The second second		0.03		1			
95% Queue Length, Q <sub>95</sub> (veh)					194853		0.6							0.1					
Control Delay (s/veh)							20.5	1000-00-00						8.5	0.4				
Level of Service (LOS)					이는 같은 24 10명		С							Α	Α				
Approach Delay (s/veh)						20	0.5							(	).7				
Approach LOS							С							38 <u>77</u> 7	Α				

	apel am1			Int. Total	386	447	439	1746	394	408	379	3/0	ACCI	337	304 2040	0240			Int. Total		1754	474	0.920	
	22147 ridgeway & hope chapel am1 00022147 4/6/2022 1		App. Total	66	96	121	450	111	107	111	071	004	66	100	104	28.0		App. Total		462	130		130 0.888	
		Ridgeway Road (CR 571) Eastbound	RTOR	6	6 ¢	<u>~</u> ∞	43	9	2	ωı	0	7	41	- ¦	C 0	1.9	Ridgeway Road (CR 571) Eastbound	RTOR		40 7	17		17	
	22147 ridge 00022147 4/6/2022	7707	ay Road (C Eastbound	Right	26	34 8	- R	121	20	37	33	07	<u>901</u>	20	77	4/7 7/0	24.0 6.9	ay Road (C Eastbound	Right		115 24 9	31		31
-	•• •• ••		Ridgew	Thru	57	48	27	253	20	59	23		780	57	66	049	38.8 16.4	Ridgew	Thru		266 57.6	74	M	74
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			S. Hope Chapel Road (CR 547) Northbound	RTOR	-	რ ჯ	- 0	വ	0	0	<del>~</del> (	N .	Ċ,	4	ິ່ງ	2 7	1.0 4.7	S. Hope Chapel Road (CR 547) Northbound	RTOR		ο 4α			0
	McDonough & Rea Associates 1431 Lakewood Road Suite C Manasquan NJ 08736 (732) 528-7076 Printed- CARS - TRUCKS - SCHOOL BUS	hapel Road Northbound	Right	5	∩ <del>.</del>	- 0	2	~	2	4,	- 0	χ	2	- ;	<u>0</u> 1	0.1 0.4	hapel Road Northbound	Right	Right	4α			0	
ciates		SCHOOL	Hope Ch	Thru	60	53	20	242	37	00	58	<del>1</del>	201	45	37	070 1 07	49.5 13.3	Hope Ch N	Thru		219 13 5	62 62	Σ	67
a Asso Snad S	10873 -7076	ucks -	S.	Left	48	74	70 20	263	61	47	33	43	184	29	29-	202	47.6 12.8	S.	Left		276 54 9	62	07:45 AM	79
McDonough & Rea Associates	Manasquan NJ 08736 (732) 528-7076	Groups Printed- CARS - TRUCKS - SCHOOL BUS		App. Total	134	161	109	561	117	129	102	68	437	66	74	1711	29.7		App. Total		544	157		161 0.845
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130 Central Avenue, Island Heights, NJ 08732 P. O. Box 5232, Toms River, NJ 08754 732.270.9690 / Fax 732.270.9691

Engineers Surveyors Planners Flood Plain Managers

July 19, 2023

Ms. Amanda Kisty, Secretary Manchester Township Planning Board 1 Colonial Drive Manchester, NJ 08759

Application No. PB-2023-05 "Parkwood Square LP & Parkwood Center B LLC" Preliminary & Final Site Plan Submission Block 65, Lots: 11, 12, 13 and 14 Manchester Township, Ocean County, New Jersey Morgan Engineering, LLC - Project No MTPB23-011

Dear Ms. Kisty:

We have received a follow up response to the above referenced Application for Preliminary & Final Site Plan Submission for Completeness. The subject of the Application is to develop the existing four (4) lots for a 167 Townhouse Development. The properties have been designated as Zone District PB-1. **This project has been deemed complete.** 

#### These New/Revised comments are in BOLD.

The following additional documents were received:

1. List of property owners within 200 feet of the subject property (B.23.), Owner's List dated April 24, 2023.





- 2. Lighting Plan for Block 65, Lots 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P of Professional Design Services, dated April 25, 2022, last revised 5/26/23.
- 3. Map of Survey for Block 65, Lot 11, 12, 13 & 14, prepared by Steven Metelski, Jr., P.L.S. of Professional Design Services, dated, 11/29/21, revised 6/28/22.
- 4. Preliminary & Final Major Site Plan for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- 5. Overall Site Plan for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- 6. Site Plan "A" for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- 7. Site Plan "B" for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- 8. Overall Grading Plan & Storm Drainage Plan for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- 9. Grading & Storm Drainage Plan "A" for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- 10. Grading Plan & Storm Drainage Plan "B" for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- 11. Overall Utility Plan for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- 12. Road Profiles for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- 13. Landscape Plan "A" for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- 14. Landscape Plan "B" for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- 15. Landscape Details for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- Construction Details & Site Details for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- 17. Construction Details & Stormwater Details for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- 18. Construction Details & Utility Details for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022,





revised 5/26/23.

- 19. Pre Construction Drainage Area Map for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- 20. Post Construction Drainage Area Map for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- 21. Preconstruction Drainage Area Map for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.
- 22. Stormwater Maintenance Plan for Block 65, Lot 11, 12, 13 & 14, prepared by William A. Stevens, P.E., P.P. of Professional Design Services, dated April 25, 2022, revised 5/26/23.

## Completeness

The Applicant is deemed incomplete based on receipt of the following:

- 1. Metes and bounds descriptions with dimensions and bearing of the existing and proposed lots (B.14.). or request a waiver from providing same. The applicant has requested a waiver.
- 2. Metes and bounds descriptions with dimensions and bearing of all existing right-of-way centerlines (B.15.) or request a waiver from providing same. The applicant has requested a waiver.
- 3. List of property owners within 200 feet of the subject property (B.23.). This comment has been addressed.
- 4. Lighting plan (C.6) including location and height of proposed fixtures (C.6.1) and detail for construction of fixture (C.6.2.). **This comment has been addressed.**
- 5. Supplementary Documents (D). This comment has been addressed. The applicant shall provide testimony as to any existing or proposed deed restrictions or covenants.

Morgan Engineering, LLC has reviewed the completeness of the submitted documents for the Planning Board's consideration and has found this applicant to be **complete**.





Should you have any concerns or require any additional information please do not hesitate to contact me directly.

Respectfully submitted,



Frank Sadeghi, P.E., C.M.E. Morgan Engineering, LLC Manchester Township Planning Board Engineer <u>frank@morganenigneeringllc.com</u>

FS/bq

CC: Pasquale Popolizio, Township Zoning Board Official Joseph D. Coronato, Jr., Esq., Planning Board Attorney Gary T. Sylvester, CPWM, Twp. Director of Inspections & Land Use Ian M. Borden, P.P., Applicant's Engineer

# STORMWATER MANAGEMENT REPORT

For

Block 65 Lot 11, 12, 13 & 14 Manchester Township Ocean County, New Jersey

**Prepared By:** 

**P**ROFESSIONAL **D**ESIGN **S**ERVICES, LLC

1245 Airport Unit 1 Lakewood, New Jersey 08701 PDS Ref. No. 18123

WILLIAM A. STEVENS P.E., P.P. LICENSE No. 39915

April 25, 2022

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## 1.0 **PROJECT DESCRIPTION**

Being known as Block 65 Lots 11, 12, 13 & 14 10, the project site contains 22.3 acres and is located at the corner of Ridgeway Road (OC Route 547) and South Hope Chapel Road in Manchester Township, Ocean County, New Jersey. Figure 1 is a location map for the project site.

It is proposed to develop the property into townhouse residential unitsincluding affordable housing units as shown on Preliminary & Final Major Subdivision Plans prepared by Professional Design Services, in accordance with Manchester Township Land Use Regulations.

This report outlines the methodologies and results for management of the increased stormwater runoff created as a result of the development.

### 2.0 EXISTING SITE CONDITIONS

The following analysis describes the existing environmental conditions based upon literature review and field investigation.

### 2.1 Topography and Hydrology

The project site lies within the outer coastal plain physiographic province. The site is forested and the topography of the site slopes from the north towards the south. There are no freshwater wetlands or riparian areas on the property.

Figure 2 is a copy of the USGS Quadrangle Topography Map with the site located.

## 2.2 Soils

The upland portion of the project site is underlain by the following soils as depicted by the U.S. Department of Agriculture; Ocean County Soil Survey. Figure 3 is a copy of the Soil Survey with the site located.

Soil Type	% Slope	Depth to SHWT*
DoA – Downer Loamy Sand	0-5	>6.0'

#### \*SHWT = Seasonal High Water Table

The permeability of this soil is typically rapid and the available water capacity is low. The depth to seasonal high water is typically greater than 6 feet. Downer is hydrologic soil group A.

Soil test pits were performed at stormwater basin locations and other locations to assess soil conditions and seasonal high water table. The depth to seasonal high water occurs at a depth greater than five (5) feet. The location of each test pit and log are shown on the site plans.

## 3.0 <u>REGULATORY STANDARDS</u>

### 1. <u>REGULATIONS</u>

## A. <u>Applicable Regulations</u>

All increased stormwater runoff resulting from the proposed development must be managed both qualitatively and quantitatively in accordance with New Jersey Regulations.

On February 4, 2004, the New Jersey Department of Environmental Protection (DEP) adopted new Stormwater Management Rules (NJAC 7:8) which require all major developments to address storwmater-related water quality, groundwater recharge and water quantity impacts. The Pinelands Commission subsequently adopted amendments to the Comprehensive Management Plan (NJAC 7:50) which integrate the new DEP rules into the CMP stormwater runoff rules. These amendments became effective May 2007 and the project is required to comply with these standards as well as the DEP rules.

The Flood Hazard Area, Freshwater Wetland Regulations and Residential Site Improvement Standards (RSIS), as administered by the Pinelands Commission require the utilization of best available technology to minimize the amount of stormwater runoff, maintain existing onsite infiltration, simulate natural drainage systems and minimize the discharge of pollutants to ground or surface waters. The overall goal of the post-construction stormwater management system design shall be to meet the erosion control, groundwater recharge, stormwater runoff quantity and quality standards at N.J.A.C. 7:8-5.4 and 5.5.

The stormwater management must be design to:

- 1. Reduce flood damage, including damage to life and property;
- 2. Minimize, to the extent practical, any increase in stormwater runoff from any new development;
  - 3. Reduce soil erosion from any development or construction project;
  - 4. Assure the adequacy of exiting and proposed culverts and bridges, and other in-stream structures;
  - 5. Maintain groundwater recharge;
  - 6. Prevent, to the greatest extent feasible, an increase in nonpoint pollution;
  - 7. Maintain the integrity of stream channels for their biological functions, as well as for drainage;
  - 8. Minimize pollutants in stormwater runoff from new and existing development in order to restore, enhance and maintain the chemical, physical, and biological integrity of the waters of the State, to protect public health, to safeguard fish and aquatic life and scenic and ecological values and to enhance the domestic, municipal, recreational, industrial and other uses of water; and
  - 9. Protect public safety through the proper design and operation of stormwater management basins.

These standards shall be met by utilizing nonstructural stormwater management strategies (7:8-5.3) into the design. Structural measures (7:8-5.7) will be used as necessary where the nonstructural measures are not sufficient. Analysis of each strategy will utilize the New Jersey Stormwater Best Management Practices (BMP) Manual as guidance.

Nonstructural stormwater management strategies incorporated into site design shall:

- 1. Protect areas that provide water quality benefits or areas particularly susceptible to erosion and sediment loss;
- 2. Minimize impervious surfaces and break up or disconnect the flow of runoff over impervious surfaces;
- 3. Maximize the protection of natural drainage features and vegetation;
- 4. Minimize the decrease in the "time of concentration" from preconstruction to post-construction. "Time of Concentration" is defined as the time to takes for runoff to travel from the hydraulically most distant point of the drainage area to the point of interest within a watershed;
- 5. Minimize land disturbance including clearing and grading;

- 6. Minimize soil compaction;
- 7. Provide low-maintenance landscaping that encourages retention and planting of native vegetation and minimizes the use of lawns, fertilizers and pesticides;
- 8. Provide vegetated open-channel conveyance systems discharging into through stable vegetated areas; and
- 9. Provide other source controls to prevent or minimize the use or exposure of pollutants at the site in order to prevent or minimize the release of those pollutants into stormwater runoff.

## B. <u>Design and Performance Standards</u>

1. <u>Erosion Control</u>

The minimum design and performance standards for erosion control are those established under the Soil Erosion and Sediment Control Act, N.J.S.A. 4:24-39 et seq. and implementing rules.

# 2. <u>Groundwater Recharge</u>

The minimum design and performance standards for groundwater recharge require compliance with either of the following:

- a. Demonstrate through hydrologic and hydraulic analysis that the site and its stormwater management measures maintain 100 percent of the average annual pre-construction groundwater recharge volume for the site.
- b. Demonstrate through hydrologic and hydraulic analysis that the increase of stormwater runoff volume from pre-construction to post-construction for the two-year storm is infiltrated.

# 3. <u>Runoff Quantity</u>

In order to control stormwater runoff quantity impacts one of the following must be demonstrated:

- a. Demonstrate through hydrologic and hydraulic analysis that for stormwater leaving the site, post-construction runoff hydrographs for the two, 10 and 100-year storm events do not exceed, at any point in time, the pre-construction runoff hydrographs for the same storm events;
- b. Demonstrate through hydrologic and hydraulic analysis that there is no increase, as compared to the pre-construction condition, in the peak runoff rates of stormwater leaving the site for the two, 10 and 100-year storm events and that the increase volume or change in timing of stormwater runoff will not increase flood damage at or downstream of the site. This analysis shall include the analysis of impacts of existing land uses and projected land uses assuming full

development under existing zoning and land use ordinances in the drainage area;

- c. Design stormwater management measures so that the postconstruction peak runoff rates for the two, 10 and 100-year storm events are 50, 75 and 80 percent, respectively, of the pre-construction peak runoff rates. The percentages apply only to the postconstruction stormwater runoff that is attributable to the portion of the site on which the proposed development or project is to be constructed.
- 4. <u>Water Quality</u>

Stormwater management measures shall be designed to reduce the postconstruction load of total suspended solids (TSS) in stormwater runoff generated from the water quality design storm by 80 percent of the anticipated load from the development site expressed as an annual average.

In accordance with the definition of FW1 at N.J.A.C. 7:9B-1.4, stormwater management measures shall be designed to prevent any increase in stormwater runoff to waters classified as FW1.

5. <u>Mounding Analysis</u>

In order to ensure design performance, the newly adopted Pinelands Commission regulations require a groundwater mounding analysis for the detention/retention basins was performed by utilizing a commercially available computer model called MODRET. The model uses the modified Green and Ampt infiltration equation to calculate unsaturated infiltration and a modified USGS model "A Modular Three-Dimensional Finite Difference Ground Water Flow Model (MODFLOW)," McDonald and Harbaugh, 1984, to calculate saturated infiltration. MODRET stimulates the unsaturated and saturated infiltration which normally occurs within stormwater detention/retention ponds. In order to compute these infiltration losses and to estimate the overflow from a detention/retention pond, the following hydrologic and hydraulic characteristics are given as input to the model simulation:

### Hydraulic Conductivity

Hydraulic conductivity can be defined as the discharge rate through a unit area under a unit hydraulic gradient. The model requires unsaturated vertical hydraulic conductivity to analyze the infiltration through the unsaturated zone; and saturated horizontal hydraulic conductivity to simulate lateral dissipation of the groundwater mound through the saturated zone of the unconfined aquifer.

The average unsaturated vertical hydraulic conductivity was determined by multiplying the equivalent saturated vertical hydraulic conductivity as determined by permeability testing by a factor of 0.67. A safety factor of 2.0 was used to further reduce the hydraulic conductivity during the model applications. This safety factor is primarily to account for potential long-term clogging due to the effects of sediment accumulation.

As the infiltration process continues, the groundwater mound has to be dissipated laterally within the saturated zone of the groundwater aquifer. The process is dependent on the horizontal hydraulic conductivity that was also measured in the field through the piezometers tests and included in the geotechnical report in the

Appendix C. The average horizontal hydraulic conductivity used in the model after applying a safety factor of two was 10.1 ft/day for Basin 1 and 17.43 ft/day for Basin 2.

### **Effective Storage Coefficient of Soil**

The void space in which water is stored after passing of the wetting front during the stormwater infiltration process is the difference between the initial moisture content and the moisture content in the transmissive zone. These values depend on the soil types, in-situ moisture content of the soil, and the average groundwater mounding during the infiltration process. THE MODRET model requires the coefficient for both saturated and unsaturated analyses. For the present study, these values are estimated from Table A-1 (Stormwater Retention Pond Infiltration Analysis is Unconfined Aquifer, Nicolas E. Andreyev, PE, March 1989). As shown in this table, storage coefficient value increases with the effective depth to the groundwater table (measured from the pond bottom for unsaturated analysis and from the design high water level in the detention pond for saturated analysis).

### **Elevation of Effective Aquifer Base**

The effective aquifer base can be defined as the top of the first semiconfining soil layer or poorly permeable soil layer that occurs below the stormwater detention/retention pond. In other words, the model requires the thickness of the present study, the aquifer thickness is assumed to be 20 ft.

## **Basin Characteristics**

The MODRET program assumes a rectangular shape of pond bottom to simulate the stormwater infiltration. The design high water level (DHWL) is the maximum water surface elevation during a design storm event. The pond volume is the actual storage volume of the pond between the bottom of the pond and the DHWL. The MODRET program utilizes the pond bottom area in combination with pond volume, DHWL, and length-to-width ratio to calculate the average length and width of pond for subsequent sizing of the finite difference grid system for saturated infiltration simulation by MODFLOW. The average pond-bottom area and length-to-width ratio to calculate the average length and width of the pond for subsequent sizing of the finite difference grid system for saturated infiltration simulation by MODFLOW. The average pond-bottom area and length-to-width ratio for each basin are estimated from the actual geometric configuration of each particular basin. The specified values of pond volume and DHWL are adjusted by trial and error, as needed, to match the assumed DHWL and the actual simulated maximum water surface elevation in each basin.

### 2. <u>PINELANDS COMPREHENSIVE MANAGEMENT PLAN</u>

The Pinelands Comprehensive Management Plan (CMP) administered by the Pinelands Commission requires that the total runoff generated from impervious surfaces during a 10 year storm be retained and infiltrated on-site in a management system employing the green infrastructure standards for a decentralized The CMP also of stormwater runoff to any surface prohibits direct discharge waterbody. In addition, stormwater runoff shall not be directed in such a way as to increase the volume and rate of discharge into any surface waterbody from that which existed prior to development of the parcel. The CMP further provides standards for permanent stormwater facility maintenance, and address management of onsite soils resources including post construction soil and site assessments to field verify that as-built site conditions are consistent with stormwater design assumptions.

## 4.0 PROPOSED STORMWATER MANAGEMENT PLAN

As shown on the Subdivision Plans, the proposed stormwater management plan consists of a conventional storm sewer system to collect and convey onsite runoff to a number of de-centralized stormwater management systems which will contain sufficient volume to retain the increased runoff

from impervious surfaces for the 10 year 24 hour storm event and control any increased runoff from the proposed development for the 2, 10 and 100 year 24 hour storm events. A series of small scale infiltration basins are proposed to manage the additional runoff generated by the project.

### 5.0 <u>METHODOLOGY</u>

Low Impact Design techniques will be utilized to interact with the hydrologic process to control stormwater runoff and pollutants closer to their source while providing site design measures that can significantly reduce the overall impact of land development on stormwater runoff as required by the Stormwater Management Rules.

The methodology typically used to estimate the stormwater runoff peak flows and volumes for the required storm events is the 24-hour storm using the rainfall distribution recommended by the U.S. Department of Agriculture Soil Conservation Service as defined in Technical Release - 55 (TR-55) dated June 1986. The time of concentrations utilized will be calculated for each contributory area utilizing the TR-55 methodology.

For the purpose of calculating runoff coefficients and groundwater recharge, there is a presumption that the pre-construction condition of a site or portion thereof is a wooded land use with good hydrologic condition. A runoff coefficient or a groundwater recharge land cover for an existing condition may be used on all or a portion of the site if the hydrologic condition has existed on the site or portion of the site for at least five years without interruption prior to the time of application.

The runoff computations shall account for all significant land features and structures, such as ponds, wetlands, depressions, hedgerows, or culverts, that may reduce pre-construction stormwater runoff rates and volumes.

The management systems proposed contains a series of small scale infiltration basins. The system contains 2 types of outflows, the first being exfiltration from the various systems and the second being outflow from the system as controlled by the various outlet control structures. Based upon soil testing performed by PDS, we have confirmed a permeability rate of around 13 - 18 inches/hour for the natural material below both the basin. For design purposes, we have utilized 6 inches/hour for the recharge rate (0.00013 feet per second), allowing for adequate factor of safety. The recharge to groundwater is shown as "discarded" flows in the flood routings. The runoff calculations separately tabulate the impervious and pervious contributory drainage areas and sequentially route the inflow through the basin for each design storm to ensure that each of the design goals are met.

The water quality design storm is 1.25 inches of rainfall in two hours. Water quality calculations shall take into account the distribution of rain from the water quality design storm, as reflected in the New Jersey Stormwater Rules. The calculation of the volume of runoff may take into account the implementation of non-structural and structural stormwater management measures.

All hydrologic and flood routing computations will utilize the Haested Methods (1989) computer software. The stormwater drainage collection system will be designed in accordance with

RSIS standards. The Rational Formula was used to compute peak runoff rates for design of the proposed internal collection system. A 25 year frequency storm was used for design as required by RSIS and the rainfall intensities were obtained from the NJDEP Rainfall Intensity Curves. The subareas tributary to each inlet are shown on the Drainage Area Plans. Soil erosion and sediment controls will also be employed as required by the "Standards for Soil Erosion and Sediment Control in New Jersey."

Copies of the TR-55 hydrologic computations, detention basin routings, and Rational Formula computations are contained within the appendices of this report.

### 6.0 <u>SUMMARY</u>

The stormwater basins have been designed to provide a minimum separation of two (2) feet between the basin bottom and seasonal high water table. The existing soils have a permeability of less than 20 inches per hour. A forebay has been provided in the two (2) larger basins to provide temporary sediment storage during construction. The subdivision plans contain the performance and maintenance standards required to maintain maximum soil infiltration capacity.

#### Low Impact Design

The project complies with the low impact design criteria to the maximum extent practicable given the design limitations imposed by Municipal zoning and Residential Site Improvement Standard Regulations.

The project has implemented several low impact design techniques as follows:

A. Providing low maintenance landscaping by usage of native grasses.

B. De-centralized stormwater management systems

### Erosion Control

The project complies with the "New Jersey Standards for Soil Erosion and Sediment Control." Certification for the project must be granted by the Ocean County Soil Conservation District prior to commencement of construction.

## Groundwater Recharge

The increase in runoff volume from the pre-construction to post-construction for the 2 and 10 year storm will be retained in the retention basins as summarized below.

STORM EVENT	<b>RETENTION VOLUME</b>	RETENTION VOLUME
	REQUIRED	PROVIDED
2	1.9 acre feet (1)	
10	3.0 acre feet (2)	6.6 acre feet

(1) Increased volume from pre-developed to post developed condition per Stormwater Regulations.

(2) Runoff from impervious surfaces per Pinelands regulations, 0.43' per s.f. <u>Runoff Quantity</u>

C	Pre-Developed	Allowable	Post-Developed
Storm Event	Peak Flow	Peak Flow	Peak Flow
2	0	0	0
10	0	0	0
100	2.7	2.2	2.2

The following is a summary of the runoff from the project site for the flood storm events:

#### Water Quality

The system will perform water quality control by the utilization of an infiltration basin, which will retain runoff from the stormwater quality design storm thereby promoting pollutant removal through sedimentation and biological processing. The forebay of the basin will retain and infiltrate all of the water quality storm runoff volume thereby reducing the post-construction loading of TSS by 100%.

#### Mounding

The mounding analysis was performed by utilizing one of the MODRET simulation schemes identified as the recovery of pollution abatement volume of a dry retention pond. It was assumed that (i) runoff would occur in a relatively short period of time, (ii) the entire runoff would occur instantaneously, and (iii) the basin was completely full up to the retention storage volume.

The mounding that will occur beneath and adjacent to the basin will only be temporary after large storm events and will not alter groundwater levels. As a result, the basins will not adversely impact wetlands, surface water bodies, septic systems or man-made structures.

### 7.0 <u>MAINTENANCE</u>

All maintenance activities for the stormwater collection system and retention basins will be the responsibility of the property owner.

# APPENDIX A

# **EXISTING CONDITION CALCULATIONS**

	Pre Developed.
Pre Developed N	OAA 24-hr D 2 year Rainfall=3.40"
Prepared by {enter your company name here}	Printed 4/25/2022
HydroCAD® 10.00-22 s/n 09416 © 2018 HydroCAD Software Solutions L	LC Page 1

Time span=0.00-28.00 hrs, dt=0.05 hrs, 561 points Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment Site: Site

Runoff Area=22.300 ac 0.00% Impervious Runoff Depth=0.00" Flow Length=1,175' Tc=42.3 min CN=30 Runoff=0.00 cfs 0.000 af

Total Runoff Area = 22.300 ac Runoff Volume = 0.000 af Average Runoff Depth = 0.00" 100.00% Pervious = 22.300 ac 0.00% Impervious = 0.000 ac

# Summary for Subcatchment Site: Site

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Area	(ac) C	N Dese	cription					
22	22.300 30 Woods, Good, HSG A							
22	.300	100.	00% Pervi	ous Area				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
12.4	75	0.0400	0.10		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.50"			
29.9	1,100	0.0150	0.61		Shallow Concentrated Flow, Woodland Kv= 5.0 fps			
42.3	1,175	Total						

		Pre Developed.
Pre Developed	NOAA 24-hr D	10 year Rainfall=5.40"
Prepared by {enter your company name here}		Printed 4/25/2022
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Time span=0.00-28.00 hrs, dt=0.05 hrs, 561 points Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment Site: Site

Runoff Area=22.300 ac 0.00% Impervious Runoff Depth>0.02" Flow Length=1,175' Tc=42.3 min CN=30 Runoff=0.08 cfs 0.042 af

Total Runoff Area = 22.300 acRunoff Volume = 0.042 afAverage Runoff Depth = 0.02"100.00% Pervious = 22.300 ac0.00% Impervious = 0.000 ac

# Summary for Subcatchment Site: Site

Runoff = 0.08 cfs @ 24.05 hrs, Volume= 0.042 af, Depth> 0.02"

Area	(ac) C	N Des	cription					
22	22.300 30 Woods, Good, HSG A							
22	.300	100.	00% Pervi	ous Area				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
12.4	75	0.0400	0.10		Sheet Flow,			
29.9	1,100	0.0150	0.61		Woods: Light underbrush n= 0.400 P2= 3.50" Shallow Concentrated Flow, Woodland Kv= 5.0 fps			
42.3	1,175	Total						

		Pre Developed.
Pre Developed NO.	AA 24-hr D	100 year Rainfall=9.20"
Prepared by {enter your company name here}		Printed 4/25/2022
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Time span=0.00-28.00 hrs, dt=0.05 hrs, 561 points Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment Site: Site

Runoff Area=22.300 ac 0.00% Impervious Runoff Depth>0.74" Flow Length=1,175' Tc=42.3 min CN=30 Runoff=2.73 cfs 1.370 af

Total Runoff Area = 22.300 ac Runoff Volume = 1.370 af Average Runoff Depth = 0.74" 100.00% Pervious = 22.300 ac 0.00% Impervious = 0.000 ac

# Summary for Subcatchment Site: Site

Runoff = 2.73 cfs @ 13.47 hrs, Volume= 1.370 af, Depth> 0.74"

Area	(ac) C	N Des	cription					
22	22.300 30 Woods, Good, HSG A							
22	.300	100.	00% Pervi	ous Area				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
12.4	75	0.0400	0.10		Sheet Flow,			
29.9	1,100	0.0150	0.61		Woods: Light underbrush n= 0.400 P2= 3.50" Shallow Concentrated Flow, Woodland Kv= 5.0 fps			
42.3	1,175	Total						

# **APPENDIX B**

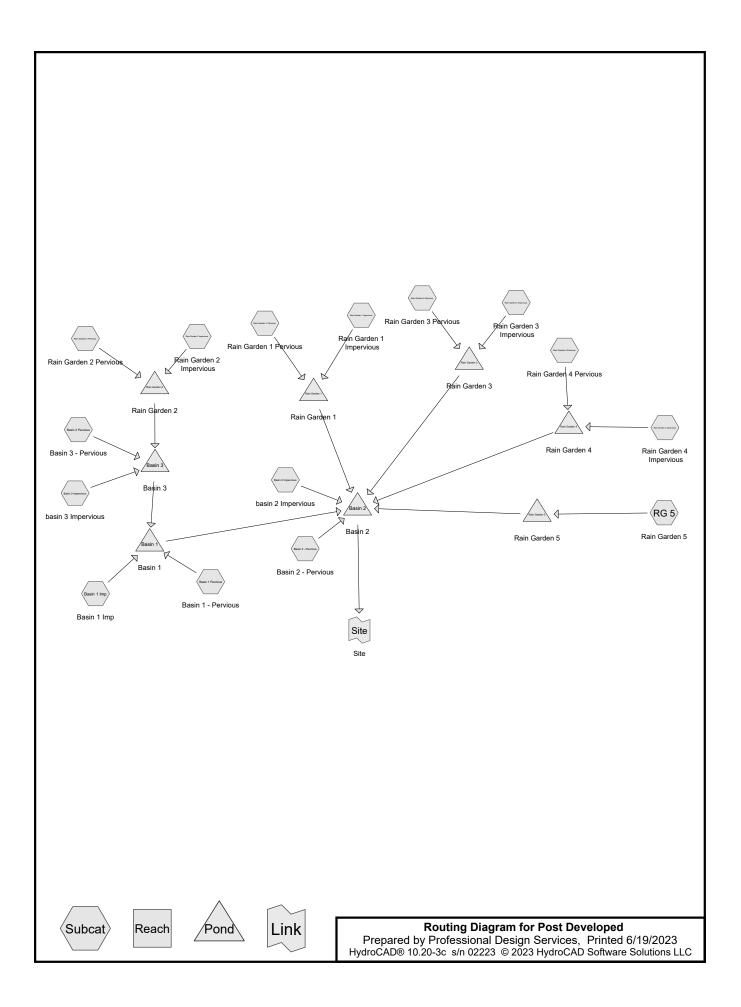
# **PROPOSED CONDITION CALCULATIONS**

# **B1 - WATER QUALITY CALCULATIONS**

# **B2 - RETENTION BASIN CALCULATIONS**

BASIN VOLUME BASIN OUTFLOW BASIN ROUTINGS CUMULATIVE BASIN OUTFLOW HYDROGRAPH

# **B3. MOUNDING CERTIFICATION**



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Ever	nt#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
	1	2 year	NRCC 24-hr	D	Default	24.00	1	3.40	2
	2	10 year	NRCC 24-hr	D	Default	24.00	1	5.40	2
	3	25 year	NRCC 24-hr	D	Default	24.00	1	6.70	2
	4	100 year	NRCC 24-hr	D	Default	24.00	1	9.20	2
	5	WQ storm	NRCC 24-hr	D	Default	24.00	1	1.25	2

# **Rainfall Events Listing**

Post DevelopedPost Developed.Post DevelopedNRCC 24-hr D2 year Rainfall=3.40"Prepared by Professional Design ServicesPrinted 6/19/2023HydroCAD® 10.20-3c s/n 02223 © 2023 HydroCAD Software Solutions LLCPage 3
Time span=5.00-30.00 hrs, dt=0.05 hrs, 501 points Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method
Subcatchment Basin 1 Imp: Basin 1 Imp Runoff Area=0.900 ac 100.00% Impervious Runoff Depth>3.05" Tc=10.0 min CN=98 Runoff=1.77 cfs 0.229 af
Subcatchment Basin 1 Pervious: Basin 1 - Runoff Area=0.500 ac 0.00% Impervious Runoff Depth=0.00" Tc=15.0 min CN=39 Runoff=0.00 cfs 0.000 af
Subcatchment Basin 2 - Pervious: Basin 2 - Runoff Area=4.050 ac 0.00% Impervious Runoff Depth=0.00" Tc=15.0 min CN=39 Runoff=0.01 cfs 0.002 af
Subcatchment Basin 2 Impervious: basin Runoff Area=2.750 ac 100.00% Impervious Runoff Depth>3.05" Tc=10.0 min CN=98 Runoff=5.41 cfs 0.699 af
Subcatchment Basin 3 Impervious: basin Runoff Area=2.400 ac 100.00% Impervious Runoff Depth>3.05" Tc=10.0 min CN=98 Runoff=4.72 cfs 0.610 af
Subcatchment Basin 3 Pervious: Basin 3 - Runoff Area=1.600 ac 0.00% Impervious Runoff Depth=0.00" Tc=15.0 min CN=39 Runoff=0.00 cfs 0.001 af
Subcatchment Rain Garden 1 Impervious: Runoff Area=0.350 ac 100.00% Impervious Runoff Depth>3.05" Tc=10.0 min CN=98 Runoff=0.69 cfs 0.089 af
Subcatchment Rain Garden 1 Pervious: Rain Runoff Area=1.150 ac 0.00% Impervious Runoff Depth=0.00" Tc=15.0 min CN=39 Runoff=0.00 cfs 0.000 af
Subcatchment Rain Garden 2 Impervious: Runoff Area=0.350 ac 100.00% Impervious Runoff Depth>3.05" Tc=10.0 min CN=98 Runoff=0.69 cfs 0.089 af
Subcatchment Rain Garden 2 Pervious: Rain Runoff Area=1.650 ac 0.00% Impervious Runoff Depth=0.00" Tc=15.0 min CN=39 Runoff=0.00 cfs 0.001 af
Subcatchment Rain Garden 3 Impervious: Runoff Area=1.450 ac 100.00% Impervious Runoff Depth>3.05" Tc=10.0 min CN=98 Runoff=2.85 cfs 0.369 af
Subcatchment Rain Garden 3 Pervious: Rain Runoff Area=1.350 ac 0.00% Impervious Runoff Depth=0.00" Tc=15.0 min CN=39 Runoff=0.00 cfs 0.001 af
Subcatchment Rain Garden 4 Impervious: Runoff Area=0.400 ac 100.00% Impervious Runoff Depth>3.05" Tc=10.0 min CN=98 Runoff=0.79 cfs 0.102 af
Subcatchment Rain Garden 4 Pervious: Rain Runoff Area=0.600 ac 0.00% Impervious Runoff Depth=0.00" Tc=15.0 min CN=39 Runoff=0.00 cfs 0.000 af
Subcatchment RG 5: Rain Garden 5 Runoff Area=1.100 ac 36.36% Impervious Runoff Depth=0.49" Tc=10.0 min CN=60 Runoff=0.23 cfs 0.045 af
Pond Basin 1: Basin 1Peak Elev=71.95'Storage=0.078 afInflow=1.77 cfs0.229 afDiscarded=0.20 cfs0.229 afPrimary=0.00 cfs0.000 afOutflow=0.20 cfs0.229 af

Post Developed Prepared by Profession HydroCAD® 10.20-3c s/n 0.	al Design Services 2223 © 2023 HydroCAD Software Solu	Post Developed. NRCC 24-hr D 2 year Rainfall=3.40" Printed 6/19/2023 utions LLC Page 4
Pond Basin 2: Basin 2		.77' Storage=0.231 af Inflow=6.09 cfs 0.790 af ry=0.00 cfs 0.000 af Outflow=1.00 cfs 0.790 af
Pond Basin 3: Basin 3		.29' Storage=0.287 af Inflow=4.72 cfs 0.611 af ry=0.00 cfs 0.000 af Outflow=0.30 cfs 0.565 af
Pond Rain Garden 1: Rai		.00' Storage=0.000 af Inflow=0.69 cfs 0.089 af ry=0.69 cfs 0.089 af Outflow=0.69 cfs 0.089 af
Pond Rain Garden 2: Rai		.20' Storage=0.011 af Inflow=0.69 cfs 0.090 af ry=0.00 cfs 0.000 af Outflow=0.30 cfs 0.090 af
Pond Rain Garden 3: Rai		.72' Storage=0.135 af Inflow=2.85 cfs 0.369 af ry=0.00 cfs 0.000 af Outflow=0.30 cfs 0.369 af
Pond Rain Garden 4: Rai		.19' Storage=0.016 af Inflow=0.79 cfs 0.102 af ry=0.00 cfs 0.000 af Outflow=0.30 cfs 0.102 af
Pond Rain Garden 5: Rai		.03' Storage=0.003 af Inflow=0.23 cfs 0.045 af ry=0.00 cfs 0.000 af Outflow=0.18 cfs 0.045 af
Link Site: Site		Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af
Total Runo	ff Area = 20.600 ac Runoff Volun = 56.31% Pervious	<b>U I</b>

## Summary for Subcatchment Basin 1 Imp: Basin 1 Imp

Runoff = 1.77 cfs @ 12.19 hrs, Volume= 0.229 af, Depth> 3.05" Routed to Pond Basin 1 : Basin 1

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 2 year Rainfall=3.40"

	Area	(ac)	CN	Desc	cription		
*	0.	500	98	Pave	ement		
*	0.	400	98	Root	-		
	0.	900	98	Weig	ghted Aver		
	0.900 100.00% Impervious Area					rvious Area	
	Тс	Leng	th	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	10.0						Direct Entry, pavement and pipe

## Summary for Subcatchment Basin 1 Pervious: Basin 1 - Pervious

Runoff = 0.00 cfs @ 24.03 hrs, Volume= Routed to Pond Basin 1 : Basin 1

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 2 year Rainfall=3.40"

_	Area	(ac)	CN	Desc	cription		
*	0.	500	39	lawn	, A soils		
	0.	500		100.	00% Pervi	ous Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0						Direct Entry,

### Summary for Subcatchment Basin 2 - Pervious: Basin 2 - Pervious

Runoff = 0.01 cfs @ 24.03 hrs, Volume= Routed to Pond Basin 2 : Basin 2 0.002 af, Depth= 0.00"

0.000 af, Depth= 0.00"

	Area (ac)	CN	Description
*	4.050	39	lawn, A soils
	4.050		100.00% Pervious Area

<b>Post Developed</b> Prepared by Professional Design Services	NRCC 24-hr D 2 year Rainfall=3.40" Printed 6/19/2023								
HydroCAD® 10.20-3c s/n 02223 © 2023 HydroCAD Software Solution	s LLC Page 6								
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)									
15.0 Direct Entry,									
Summary for Subcatchment Basin 2 Impervious: basin 2 Impervious									
Runoff = 5.41 cfs @ 12.19 hrs, Volume= 0.69 Routed to Pond Basin 2 : Basin 2	99 af, Depth> 3.05"								
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Tim NRCC 24-hr D 2 year Rainfall=3.40"	e Span= 5.00-30.00 hrs, dt= 0.05 hrs								
Area (ac) CN Description									
* 0.600 98 Parking									
* 0.450 98 Roof									
* 0.700 98 Driveways * 1.000 98 Boad & Sidowalk									
2.750 98 Weighted Average									
2.750 100.00% Impervious Area									
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)									
10.0 Direct Entry, pa	avement								
Summary for Subcatchment Basin 3 Impervious: basin 3 Impervious									
Runoff = 4.72 cfs @ 12.19 hrs, Volume= 0.61	10 af, Depth> 3.05"								

Routed to Pond Basin 3 : Basin 3

Post Developed.

	Area	(ac)	CN	Desc	ription					
*	0.	900	98	Park	Parking					
*	0.	300	98	Roof						
*	0.	500	98	Drive	eways					
*	0.	700								
	2.	400	98	Weig	hted Aver	age				
	2.	2.400 100.00% Impervious Area			00% Impe	vious Area				
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	10.0		- /	(, (.)	(12,500)	(0.0)	Direct Entry, pavement			

## Summary for Subcatchment Basin 3 Pervious: Basin 3 - Pervious

Runoff = 0.00 cfs @ 24.03 hrs, Volume= 0.001 af, Depth= 0.00" Routed to Pond Basin 3 : Basin 3

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 2 year Rainfall=3.40"

_	Area	(ac)	CN	Desc	cription		
*	1.	600	39	lawn	, A soils		
	1.	600		100.	00% Pervi	ous Area	
	Tc (min)	Lengt (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0						Direct Entry,

## Summary for Subcatchment Rain Garden 1 Impervious: Rain Garden 1 Impervious

0.089 af, Depth> 3.05"

Runoff	=	0.69 cfs @	12.19 hrs,	Volume=	
Routed	to Pond	Rain Garder	n 1 : Rain G	arden 1	

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 2 year Rainfall=3.40"

	Area	(ac)	CN	Desc	cription						
*	0.	350	98	Roof	f						
	0.	350		100.	00% Impe	rvious Area	3				
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
	10.0						Direct Entry, pavement and pipe				
	Summary for Subcatchment Rain Garden 1 Pervious: Rain Garden 1 Pervious										

Runoff = 0.00 cfs @ 24.03 hrs, Volume= 0.000 af, Depth= 0.00" Routed to Pond Rain Garden 1 : Rain Garden 1

	Area	(ac)	CN	Desc	ription		
*	1.	150	39	lawn	, A soils		
	1.	150		100.0	00% Pervi	ous Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	15.0						Direct Entry,

## Summary for Subcatchment Rain Garden 2 Impervious: Rain Garden 2 Impervious

Runoff	=	0.69 cfs @	12.19 hrs,	Volume=	0.089 af,	Depth>	3.05"
Routed	to Pond	l Rain Garde	n 2 : Rain Ga	arden 2		-	

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 2 year Rainfall=3.40"

	Area	(ac)	CN	Desc	cription		
*	0.	350	98	Root	-		
	0.	350		100.	00% Impe	rvious Area	
	Tc (min)	Lengt (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	10.0			/			Direct Entry, pavement and pipe

## Summary for Subcatchment Rain Garden 2 Pervious: Rain Garden 2 Pervious

Runoff	=	0.00 cfs @	24.03 hrs,	Volume=	0.001 af,	Depth= 0.00"
Routed	to Pond	l Rain Garder	n 2 : Rain G	arden 2		

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 2 year Rainfall=3.40"

_	Area	(ac)	CN	Desc	cription		
*	1.	650	39	lawn	, A soils		
1.650 100.00% Pervious Area							
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0						Direct Entry,

## Summary for Subcatchment Rain Garden 3 Impervious: Rain Garden 3 Impervious

Runoff = 2.85 cfs @ 12.19 hrs, Volume= 0.369 af, Depth> 3.05" Routed to Pond Rain Garden 3 : Rain Garden 3

	Area (ac)	CN	Description
*	0.450	98	Pavement
*	0.600	98	Roof
*	0.400	98	Driveway
	1.450	98	Weighted Average
	1.450		100.00% Impervious Area

Post Developed	Post Developed. NRCC 24-hr D 2 year Rainfall=3.40"
Prepared by Professional Design Services HydroCAD® 10.20-3c s/n 02223 © 2023 HydroCAD Software So	Printed 6/19/2023 utions LLC Page 9
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)	
10.0 Direct Entr	y, pavement and pipe
Summary for Subcatchment Rain Garden 3	Pervious: Rain Garden 3 Pervious
Runoff = 0.00 cfs @ 24.03 hrs, Volume= Routed to Pond Rain Garden 3 : Rain Garden 3	0.001 af, Depth= 0.00"
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN NRCC 24-hr D 2 year Rainfall=3.40"	Time Span= 5.00-30.00 hrs, dt= 0.05 hrs
Area (ac) CN Description	
<u>* 1.350 39 Iawn, A soils</u> 1.350 100.00% Pervious Area	
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)	
15.0 <b>Direct Ent</b>	у,
Summary for Subcatchment Rain Garden 4 Im	nonvious: Pain Gardon 4 Imponvious
Summary for Subcatchment Ram Garden 4 mi	pervious. Rain Garden 4 impervious
Runoff = 0.79 cfs @ 12.19 hrs, Volume= Routed to Pond Rain Garden 4 : Rain Garden 4	0.102 af, Depth> 3.05"
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN NRCC 24-hr D 2 year Rainfall=3.40"	Time Span= 5.00-30.00 hrs, dt= 0.05 hrs
Area (ac) CN Description	
* 0.400 98 Roof	
0.400 100.00% Impervious Area	
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)	
10.0 Direct Entr	y, pavement and pipe
Summary for Subcatchment Rain Garden 4	Pervious: Rain Garden 4 Pervious
Runoff = 0.00 cfs @ 24.03 hrs, Volume= Routed to Pond Rain Garden 4 : Rain Garden 4	0.000 af, Depth= 0.00"
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN NRCC 24-hr D 2 year Rainfall=3.40"	Time Span= 5.00-30.00 hrs, dt= 0.05 hrs
Area (ac) CN Description	
* 0.600 .39 Jawn A soils	

	/ 100 (u0)		Description
1	* 0.600	39	lawn, A soils
_	0.600		100.00% Pervious Area

HydroCAD® 10.20-3c     s/n 02223     © 2023     HydroCAD     Software Solutions     LLC     Page 10							
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)							
15.0 Direct Entry,							
Summary for Subcatchment RG 5: Rain Garden 5							
Runoff = 0.23 cfs @ 12.25 hrs, Volume= 0.045 af, Depth= 0.49" Routed to Pond Rain Garden 5 : Rain Garden 5							
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D_2 year Rainfall=3.40"							
Area (ac) CN Description							
* 0.400 98 Roof * 0.700 39 Lawn A soils							
1.100 60 Weighted Average							
0.700 63.64% Pervious Area 0.400 36.36% Impervious Area							
0.400 30.30 % Impervious Area							
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)							
10.0 Direct Entry, pavement and pipe							
Summary for Pond Basin 1: Basin 1							
Inflow Area = 7.400 ac, 49.32% Impervious, Inflow Depth > 0.37" for 2 year event							
Inflow = 1.77 cfs @ 12.19 hrs, Volume= 0.229 af							
Outflow         =         0.20 cfs @         11.10 hrs, Volume=         0.229 af, Atten= 89%, Lag= 0.0 min           Discarded         =         0.20 cfs @         11.10 hrs, Volume=         0.229 af							
Primary = $0.20 \text{ cfs}$ @ $5.00 \text{ hrs}$ , Volume= $0.229 \text{ ar}$							
Routed to Pond Basin 2 : Basin 2							
Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 71.95' @ 13.58 hrs Surf.Area= 0.049 ac Storage= 0.078 af							
Plug-Flow detention time= 123.8 min calculated for 0.229 af (100% of inflow) Center-of-Mass det. time= 123.3 min ( 913.9 - 790.6 )							
Volume Invert Avail.Storage Storage Description							

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NRCC 24-hr D 2 year Rainfall=3.40"

Volume	Invent A	van.otorage	olorage Description	
#1	70.00'	0.200 af	retention basin (P	rismatic)Listed below
Elevation (feet)	Surf.Area (acres)	Inc.Sto (acre-fee		
70.00	0.030	0.00	0.000	
71.00	0.040	0.03	35 0.035	
72.00	0.050	0.04	45 0.080	
73.00	0.060	0.05	55 0.135	
74.00	0.070	0.06	65 0.200	

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Post Developed. NRCC 24-hr D 2 year Rainfall=3.40" Printed 6/19/2023

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Device	Routing	Invert	Outlet Devices
#1	Discarded	70.00'	0.20 cfs Exfiltration when above 70.00'
#2	Primary	72.00'	<b>4.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Primary	74.00'	48.0" x 48.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

**Discarded OutFlow** Max=0.20 cfs @ 11.10 hrs HW=70.04' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.20 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=70.00' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs) 3=Orifice/Grate (Controls 0.00 cfs)

# Summary for Pond Basin 2: Basin 2

Inflow Area =	20.600 ac, 43.69°	% Impervious, Inflow D	epth > 0.46"	for 2 year event
Inflow =	6.09 cfs @ 12.1	9 hrs, Volume=	0.790 af	-
Outflow =	1.00 cfs @ 11.7	0 hrs, Volume=	0.790 af, Atte	en= 84%, Lag= 0.0 min
Discarded =	1.00 cfs @ 11.7	0 hrs, Volume=	0.790 af	
Primary =	0.00 cfs @ 5.0	0 hrs, Volume=	0.000 af	
Routed to Link	Site : Site			

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 68.77' @ 13.13 hrs Surf.Area= 0.332 ac Storage= 0.231 af

Plug-Flow detention time= 72.0 min calculated for 0.789 af (100% of inflow) Center-of-Mass det. time= 71.2 min ( 862.8 - 791.6 )

Volume	Invert	Avail.Storag	e Sto	orage Description
#1	68.00'	3.600 a	af Cu	ustom Stage Data (Prismatic)Listed below x 1.2
Elevatio (fee 68.0	t) (acres	s) (acre	Store -feet) 0.000	(acre-feet)
69.0	• • • • • • • • • • • • • • • • • • • •	-	0.000	
70.0		-	0.350	
71.0	0 0.50	0	0.450	1.050
72.0	0.60	0	0.550	1.600
73.0	0 0.70	0	0.650	2.250
74.0	0.80	0	0.750	3.000
<u>Device</u> #1 #2	Routing Discarded Primary	68.00' 70.70'	1.00 cfs 3.0" Ve	Devices fs Exfiltration when above 68.00' ert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Primary		-	<b>W x 42.0" H Vert. Orifice/Grate</b> C= 0.600 d to weir flow at low heads

**Discarded OutFlow** Max=1.00 cfs @ 11.70 hrs HW=68.09' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 1.00 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=68.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs) -3=Orifice/Grate (Controls 0.00 cfs)

### Summary for Pond Basin 3: Basin 3

Inflow Area =	6.000 ac, 45.83% Impervious, Inflow De	epth > 1.22" for 2 year event				
Inflow =	4.72 cfs @ 12.19 hrs, Volume=	0.611 af				
Outflow =	0.30 cfs @ 10.10 hrs, Volume=	0.565 af, Atten= 94%, Lag= 0.0 min				
Discarded =	0.30 cfs @ 10.10 hrs, Volume=	0.565 af				
Primary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af				
Routed to Pond Basin 1 : Basin 1						

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 73.29' @ 15.04 hrs Surf.Area= 0.257 ac Storage= 0.287 af

Plug-Flow detention time= 366.7 min calculated for 0.563 af (92% of inflow	w)
Center-of-Mass det. time= 323.3 min (1,113.9 - 790.7)	

Volume	Invert	Avail.Storage	Storage Description
#1	72.00'	1.200 af	Custom Stage Data (Prismatic)Listed below x 1.2
Elevatio (fee 72.0 73.0 74.0 75.0 76.0	et) (acres 00 0.15 00 0.20 00 0.25 00 0.30	s)     (acre-f       0     0       0     0       0     0       0     0       0     0       0     0	
DeviceRouting#1Discarded#2Primary#3Primary		72.00' <b>0.</b> 74.00' <b>3.</b> 75.00' <b>42</b>	utlet Devices <b>30 cfs Exfiltration when above 72.00'</b> <b>0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads <b>2.0" W x 42.0" H Vert. Orifice/Grate</b> C= 0.600 mited to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 10.10 hrs HW=72.07' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=72.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs) -3=Orifice/Grate (Controls 0.00 cfs)

## Summary for Pond Rain Garden 1: Rain Garden 1

Inflow Area =	1.500 ac, 23.33% Impervious, Inflow De	epth > 0.72" for 2 year event			
Inflow =	0.69 cfs @ 12.19 hrs, Volume=	0.089 af			
Outflow =	0.69 cfs @ 12.19 hrs, Volume=	0.089 af, Atten= 0%, Lag= 0.0 min			
Discarded =	0.00 cfs @ 12.19 hrs, Volume=	0.000 af			
Primary =	0.69 cfs @ 12.19 hrs, Volume=	0.089 af			
Routed to Pond Basin 2 : Basin 2					

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 78.00' @ 12.19 hrs Surf.Area= 0.060 ac Storage= 0.000 af

Plug-Flow detention time= 0.0 min calculated for 0.089 af (100% of inflow) Center-of-Mass det. time= 0.0 min (792.9 - 792.9)

Volume	Invert A	vail.Storage	e Storage Description			
#1	78.00'	0.400 af	f Custom Stage Data (Prismatic)Listed below (Recalc)			
Elevatio (fee			Store Cum.Store -feet) (acre-feet)			
78.0	0.060	0	0.000 0.000			
79.0	0.080	0	0.070 0.070			
80.0	0.100	0	0.090 0.160			
81.0	0.120	0	0.110 0.270			
82.0	0.140	0	0.130 0.400			
Device	Routing	Invert O	Dutlet Devices			
#1	Discarded	78.00' <b>0.</b>	0.30 cfs Exfiltration when above 75.00'			
#2	Primary	80.00' <b>3.</b>	<b>3.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads			
#3	Primary	58.00' <b>42</b>	12.0" x 48.0" Horiz. Orifice/Grate C= 0.600			
	-	Li	imited to weir flow at low heads			
Discarded OutElow Max-0.20 of @ 12.10 hrs. HW/=78.00' (Erec Discharge)						

**Discarded OutFlow** Max=0.30 cfs @ 12.19 hrs HW=78.00' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=301.47 cfs @ 12.19 hrs HW=78.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs)

-3=Orifice/Grate (Orifice Controls 301.47 cfs @ 21.53 fps)

# Summary for Pond Rain Garden 2: Rain Garden 2

Inflow Area =	2.000 ac, 1	17.50% Impervious, Inflo	w Depth > 0.54" for 2 year event		
Inflow =	0.69 cfs @	12.19 hrs, Volume=	0.090 af		
Outflow =	0.30 cfs @	12.05 hrs, Volume=	0.090 af, Atten= 56%, Lag= 0.0 min		
Discarded =	0.30 cfs @	12.05 hrs, Volume=	0.090 af		
Primary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af		
Routed to Pond Basin 3 : Basin 3					

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs

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Peak Elev= 75.20' @ 12.56 hrs Surf.Area= 0.057 ac Storage= 0.011 af

Plug-Flow detention time= 10.3 min calculated for 0.089 af (100% of inflow) Center-of-Mass det. time= 9.9 min (804.0 - 794.2)

Volume	Invert /	Avail.Storage	e Storage Description
#1	75.00'	0.300 af	f Custom Stage Data (Prismatic)Listed below (Recalc)
Elevatio (fee 75.0 76.0 77.0 78.0 79.0	(acres)           00         0.055           00         0.065           00         0.065           00         0.075           00         0.075           00         0.075           00         0.085	) (acre- 5 0 5 0 5 0 5 0	Store         Cum.Store           .feet)         (acre-feet)           0.000         0.000           0.060         0.060           0.070         0.130           0.080         0.210           0.090         0.300
Device #1 #2 #3	Routing Discarded Primary Primary	75.00' <b>0</b> 77.00' <b>3</b> 79.00' <b>4</b>	Outlet Devices.30 cfs Exfiltration when above 75.00'.0" Vert. Orifice/GrateC= 0.600Limited to weir flow at low heads2.0" x 48.0" Horiz. Orifice/GrateC= 0.600imited to weir flow at low heads

Discarded OutFlow Max=0.30 cfs @ 12.05 hrs HW=75.04' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=75.00' (Free Discharge)

-2=Orifice/Grate (Controls 0.00 cfs)

-3=Orifice/Grate (Controls 0.00 cfs)

# Summary for Pond Rain Garden 3: Rain Garden 3

Inflow Area =	2.800 ac, 51.	.79% Impervious,	Inflow Depth > 1.	58" for 2 year event
Inflow =	2.85 cfs @ 1	2.19 hrs, Volume	= 0.369 af	-
Outflow =	0.30 cfs @ 1	1.15 hrs, Volume	= 0.369 af,	Atten= 89%, Lag= 0.0 min
Discarded =	0.30 cfs @ 1	1.15 hrs, Volume	= 0.369 af	-
Primary =	0.00 cfs @	5.00 hrs, Volume	= 0.000 af	
Routed to Pond	Basin 2 : Basir	n 2		

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 75.72' @ 13.68 hrs Surf.Area= 0.222 ac Storage= 0.135 af

Plug-Flow detention time= 155.0 min calculated for 0.369 af (100% of inflow) Center-of-Mass det. time= 154.2 min (945.1 - 790.9)

Volume	Invert	Avail.Storage	Storage Description
#1	75.00'	2.000 af	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation

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Inc.Store

			0.01010	Call.Coloro	
(fee	et) (acres)	(ac	re-feet)	(acre-feet)	
75.0	0.150		0.000	0.000	
76.0	0.250		0.200	0.200	
77.0	0.350		0.300	0.500	
78.0	0.450		0.400	0.900	
79.0	0.550		0.500	1.400	
80.0	0.650		0.600	2.000	
Device	Routing	Invert	Outlet De	evices	
#1	Discarded	75.00'	0.30 cfs	Exfiltration wh	en above 75.00'
#2	Primary	77.00'	3.0" Ver	t. Orifice/Grate	C= 0.600 Limited to weir flow at low heads
#3	Primary	79.00'	42.0" x 4	8.0" Horiz. Ori	fice/Grate C= 0.600
	-		Limited t	o weir flow at lov	w heads

Cum.Store

**Discarded OutFlow** Max=0.30 cfs @ 11.15 hrs HW=75.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=75.00' (Free Discharge) **2=Orifice/Grate** (Controls 0.00 cfs)

**3=Orifice/Grate** (Controls 0.00 cfs)

Surf.Area

-3=Orifice/Grate (Controls 0.00 cis)

# Summary for Pond Rain Garden 4: Rain Garden 4

Inflow Area =	1.000 ac, 4	0.00% Impervious, Inflow	Depth > 1.22" for 2 year event
Inflow =	0.79 cfs @	12.19 hrs, Volume=	0.102 af
Outflow =	0.30 cfs @	12.10 hrs, Volume=	0.102 af, Atten= 62%, Lag= 0.0 min
Discarded =	0.30 cfs @	12.10 hrs, Volume=	0.102 af
Primary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af
Routed to Pond	l Basin 2 : Bas	sin 2	

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 75.19' @ 12.61 hrs Surf.Area= 0.087 ac Storage= 0.016 af

Plug-Flow detention time= 17.4 min calculated for 0.102 af (100% of inflow) Center-of-Mass det. time= 16.8 min ( 808.2 - 791.4 )

Invert A	Avail.Storage	Storag	e Description	
75.00'	0.550 af	Custo	m Stage Data	(Prismatic)Listed below (Recalc)
			Cum.Store (acre-feet)	
0.085	5         0.0	00	0.000	
0.095	5 0.0	90	0.090	
0.105	5 0.1	00	0.190	
0.115	5	10	0.300	
0.125	5 0.1	20	0.420	
0.135	5	30	0.550	
	75.00' Surf.Area (acres) 0.085 0.095 0.105 0.115 0.125	75.00'         0.550 af           Surf.Area         Inc.Sto           (acres)         (acre-fe           0.085         0.0           0.095         0.0           0.105         0.1           0.115         0.1           0.125         0.1	75.00'         0.550 af         Custo           Surf.Area (acres)         Inc.Store (acre-feet)           0.085         0.000           0.095         0.090           0.105         0.100           0.115         0.110           0.125         0.120	75.00'         0.550 af         Custom Stage Data           Surf.Area (acres)         Inc.Store (acre-feet)         Cum.Store (acre-feet)           0.085         0.000         0.000           0.095         0.090         0.090           0.105         0.100         0.190           0.115         0.110         0.300           0.125         0.120         0.420

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Device	Routing	Invert	Outlet Devices
#1	Discarded	75.00'	0.30 cfs Exfiltration when above 75.00'
#2	Primary	77.00'	<b>3.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Primary	79.00'	<b>42.0" x 48.0" Horiz. Grate</b> C= 0.600 Limited to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 12.10 hrs HW=75.06' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=75.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs) -3=Grate (Controls 0.00 cfs)

# Summary for Pond Rain Garden 5: Rain Garden 5

Inflow Area =	1.100 ac, 36.36% Impervious, Inflow	Depth = 0.49" for 2 year event
Inflow =	0.23 cfs @ 12.25 hrs, Volume=	0.045 af
Outflow =	0.18 cfs @ 12.47 hrs, Volume=	0.045 af, Atten= 21%, Lag= 13.3 min
Discarded =	0.18 cfs @_ 12.47 hrs, Volume=	0.045 af
Primary =	0.00 cfs $\overline{@}$ 5.00 hrs, Volume=	0.000 af
Routed to Pond	d Basin 2 : Basin 2	

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 73.03' @ 12.47 hrs Surf.Area= 0.085 ac Storage= 0.003 af

Plug-Flow detention time= 10.3 min calculated for 0.045 af (100% of inflow) Center-of-Mass det. time= 10.3 min (976.4 - 966.1)

Volume	Invert A	vail.Storage	e Storage Description
#1	73.00'	0.550 a	f Custom Stage Data (Prismatic)Listed below (Recalc)
Elevatio (fee		,	Store Cum.Store -feet) (acre-feet)
73.0	0.085	(	0.000 0.000
74.0	0.095 0.095	(	0.090 0.090
75.0	0.105	0	0.100 0.190
76.0	0.115	(	0.110 0.300
77.0	0.125	(	0.120 0.420
78.0	0.135	(	0.130 0.550
Device	Routing	Invert C	Dutlet Devices
#1	Discarded		.30 cfs Exfiltration when above 73.00'
#2	Primary	-	<b>.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Primary		<b>2.0" x 48.0" Horiz. Grate</b> C= 0.600 imited to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 12.47 hrs HW=73.03' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=73.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs) -3=Grate (Controls 0.00 cfs)

# Summary for Link Site: Site

Inflow Are	a =	20.600 ac, 43	3.69% Impervious, Ir	flow Depth = $0.00"$	for 2 year event
Inflow	=	0.00 cfs @	5.00 hrs, Volume=	0.000 af	
Primary	=	0.00 cfs @	5.00 hrs, Volume=	0.000 af, Att	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs

Post DevelopedPost DevelopedPost DevelopedNRCC 24-hr D10 year Rainfall=5.40Prepared by Professional Design ServicesPrinted 6/19/202HydroCAD® 10.20-3c s/n 02223 © 2023 HydroCAD Software Solutions LLCPage 1
Time span=5.00-30.00 hrs, dt=0.05 hrs, 501 points Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method
Subcatchment Basin 1 Imp: Basin 1 Imp Runoff Area=0.900 ac 100.00% Impervious Runoff Depth>4.92 Tc=10.0 min CN=98 Runoff=2.83 cfs 0.369 a
Subcatchment Basin 1 Pervious: Basin 1 - Runoff Area=0.500 ac 0.00% Impervious Runoff Depth=0.29 Tc=15.0 min CN=39 Runoff=0.02 cfs 0.012 a
Subcatchment Basin 2 - Pervious: Basin 2 - Runoff Area=4.050 ac 0.00% Impervious Runoff Depth=0.29 Tc=15.0 min CN=39 Runoff=0.16 cfs 0.097 ac
Subcatchment Basin 2 Impervious: basin Runoff Area=2.750 ac 100.00% Impervious Runoff Depth>4.92 Tc=10.0 min CN=98 Runoff=8.65 cfs 1.127 a
Subcatchment Basin 3 Impervious: basin Runoff Area=2.400 ac 100.00% Impervious Runoff Depth>4.92 Tc=10.0 min CN=98 Runoff=7.55 cfs 0.983 a
Subcatchment Basin 3 Pervious: Basin 3 - Runoff Area=1.600 ac 0.00% Impervious Runoff Depth=0.29 Tc=15.0 min CN=39 Runoff=0.06 cfs 0.038 a
Subcatchment Rain Garden 1 Impervious: Runoff Area=0.350 ac 100.00% Impervious Runoff Depth>4.92 Tc=10.0 min CN=98 Runoff=1.10 cfs 0.143 a
Subcatchment Rain Garden 1 Pervious: Rain Runoff Area=1.150 ac 0.00% Impervious Runoff Depth=0.29 Tc=15.0 min CN=39 Runoff=0.04 cfs 0.028 a
Subcatchment Rain Garden 2 Impervious: Runoff Area=0.350 ac 100.00% Impervious Runoff Depth>4.92 Tc=10.0 min CN=98 Runoff=1.10 cfs 0.143 a
Subcatchment Rain Garden 2 Pervious: Rain Runoff Area=1.650 ac 0.00% Impervious Runoff Depth=0.29 Tc=15.0 min CN=39 Runoff=0.06 cfs 0.040 a
Subcatchment Rain Garden 3 Impervious: Runoff Area=1.450 ac 100.00% Impervious Runoff Depth>4.92 Tc=10.0 min CN=98 Runoff=4.56 cfs 0.594 a
Subcatchment Rain Garden 3 Pervious: Rain Runoff Area=1.350 ac 0.00% Impervious Runoff Depth=0.29
Tc=15.0 min CN=39 Runoff=0.05 cfs 0.032 a Subcatchment Rain Garden 4 Impervious: Runoff Area=0.400 ac 100.00% Impervious Runoff Depth>4.92
Tc=10.0 min CN=98 Runoff=1.26 cfs 0.164 a Subcatchment Rain Garden 4 Pervious: Rain Runoff Area=0.600 ac 0.00% Impervious Runoff Depth=0.29
Tc=15.0 minCN=39Runoff=0.02 cfs0.014 aSubcatchment RG 5: Rain Garden 5Runoff Area=1.100 ac36.36% ImperviousRunoff Depth=1.54
Tc=10.0 min         CN=60         Runoff=1.07 cfs         0.141 a           Pond Basin 1: Basin 1         Peak Elev=72.86'         Storage=0.127 af         Inflow=2.83 cfs         0.435 a           Discarded=0.20 cfs         0.343 af         Primary=0.35 cfs         0.092 af         Outflow=0.55 cfs         0.435 a

Post Developed Prepared by Professiona HydroCAD® 10.20-3c s/n 02	al Design Services 2223 © 2023 HydroCAD Softw		Post Developed. 10 year Rainfall=5.40" Printed 6/19/2023 Page 19
Pond Basin 2: Basin 2		Elev=69.59' Storage=0.547 a f Primary=0.00 cfs 0.000 af	
Pond Basin 3: Basin 3		Elev=74.25' Storage=0.563 a f  Primary=0.08 cfs  0.054 af	
Pond Rain Garden 1: Rai		Elev=78.00' Storage=0.000 a f  Primary=1.10 cfs  0.171 af	
Pond Rain Garden 2: Rai		Elev=75.51' Storage=0.029 a f  Primary=0.00 cfs  0.000 af	
Pond Rain Garden 3: Rai		Elev=76.30' Storage=0.279 a f Primary=0.00 cfs 0.000 af	
Pond Rain Garden 4: Rai		Elev=75.43' Storage=0.037 a f Primary=0.00 cfs 0.000 af	
Pond Rain Garden 5: Rai		Elev=73.34' Storage=0.029 a f Primary=0.00 cfs 0.000 af	
Link Site: Site			Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af
Total Runol			rage Runoff Depth = 2.29" 9% Impervious = 9.000 ac

#### Summary for Subcatchment Basin 1 Imp: Basin 1 Imp

Runoff = 2.83 cfs @ 12.19 hrs, Volume= 0.369 af, Depth> 4.92" Routed to Pond Basin 1 : Basin 1

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 10 year Rainfall=5.40"

	Area	(ac)	CN	Desc	cription		
*	0.	500	98	Pave	ement		
*	0.	400	98	Root	-		
	0.900 98 Weighted Average						
	0.	900		100.	00% Impe	rvious Area	
	Тс	Leng	th	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	10.0						Direct Entry, pavement and pipe

# Summary for Subcatchment Basin 1 Pervious: Basin 1 - Pervious

Runoff = 0.02 cfs @ 13.21 hrs, Volume= Routed to Pond Basin 1 : Basin 1

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 10 year Rainfall=5.40"

	Area	(ac)	CN	Desc	cription		
*	0.	500	39	lawn	, A soils		
	0.500 100.00% Pervious Area					ous Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0	(166		(1011)	(11/360)	(03)	Direct Entry,

#### Summary for Subcatchment Basin 2 - Pervious: Basin 2 - Pervious

Runoff = 0.16 cfs @ 13.21 hrs, Volume= Routed to Pond Basin 2 : Basin 2 0.097 af, Depth= 0.29"

0.012 af, Depth= 0.29"

	Area (ac)	CN	Description
*	4.050	39	lawn, A soils
	4.050		100.00% Pervious Area

Post Developed	NRCC 24-hr D 10 year Rainfall=5.40" Printed 6/19/2023									
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Trydrocade 10.20-50 Sin 02223 e 2023 Hydrocad Soliware Sold										
Tc Length Slope Velocity Capacity Description										
(min) (feet) (ft/ft) (ft/sec) (cfs)										
15.0 Direct Entry	/,									
Summary for Subcatchment Basin 2 Imp	Summary for Subcatchment Basin 2 Impervious: basin 2 Impervious									
	•									
	1.127 af, Depth> 4.92"									
Routed to Pond Basin 2 : Basin 2										
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN,	Time Span= 5.00-30.00 hrs, dt= 0.05 hrs									
NRCC 24-hr D 10 year Rainfall=5.40"										
Area (ac) CN Description										
* 0.600 98 Parking										
* 0.450 98 Roof										
* 0.700 98 Driveways										
* 1.000 98 Road & Sidewalk										
2.750 98 Weighted Average										
2.750 100.00% Impervious Area										
Tc Length Slope Velocity Capacity Description										
(min) (feet) (ft/ft) (ft/sec) (cfs)										
10.0 Direct Entry	/, pavement									
Summary for Subcatchmont Pasin 2 Imp	orvious: basin 3 Imporvious									
Summary for Subcatchment Basin 3 Imp	ervious. Dasili s illipervious									

7.55 cfs @ 12.19 hrs, Volume= 0.983 af, Depth> 4.92" Runoff = Routed to Pond Basin 3 : Basin 3

Post Developed.

	Area	(ac)	CN	Desc	cription		
*	0.	900	98	Park	ing		
*	0.	300	98	Roof			
*	0.	500	98	Drive	eways		
*	0.	700	98	Road	d & Sidewa	alk	
	2.	2.400 98 Weighted Average					
	2.	2.400 100.00% Impervious Area				rvious Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	10.0	•	-			\$ F	Direct Entry, pavement

#### Summary for Subcatchment Basin 3 Pervious: Basin 3 - Pervious

Runoff = 0.06 cfs @ 13.21 hrs, Volume= 0.038 af, Depth= 0.29" Routed to Pond Basin 3 : Basin 3

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 10 year Rainfall=5.40"

	Area	(ac)	CN	Desc	cription		
*	1.	600	39	lawn	, A soils		
	1.	1.600 100.00% Pervious Area					
	Tc (min)	Lengt (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0						Direct Entry,

# Summary for Subcatchment Rain Garden 1 Impervious: Rain Garden 1 Impervious

Runoff	=	1.10 cfs @	12.19 hrs,	Volume=	0.143 af,	Depth> 4.92"
Routed	to Pond	Rain Garder	n 1 : Rain G	arden 1		-

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 10 year Rainfall=5.40"

	Area	(ac)	CN Des	cription					
*	0.	350	98 Roo	f					
	0.350 100.00% Impervious Area								
	Тс	Length	n Slope	Velocity	Capacity	Description			
	(min)	(feet	) (ft/ft)	(ft/sec)	(cfs)				
	10.0					Direct Entry, pavement and pipe			
	Summary for Subcatchment Rain Garden 1 Pervious: Rain Garden 1 Pervious								
	Su	immai	y for Sul	ocatchm	ent Rain	Garden 1 Pervious: Rain Garden 1 Pervious			

	Area	(ac)	CN	Desc	cription		
*	1.	150	39	lawn	, A soils		
	1.	150		100.	00% Pervi	ous Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	15.0						Direct Entry,

# Summary for Subcatchment Rain Garden 2 Impervious: Rain Garden 2 Impervious

Runoff	=	1.10 cfs @	12.19 hrs,	Volume=	0.143 af,	Depth> 4.92"
Routed	to Pond	Rain Garder	n 2 : Rain Ga	arden 2		

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 10 year Rainfall=5.40"

_	Area	(ac)	CN	Desc	cription		
*	0.	350	98	Roof			
	0.	350		100.	00% Impe	rvious Area	l
	Tc (min)	Lengt (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	10.0		-,	(	()	()	Direct Entry, pavement and pipe

# Summary for Subcatchment Rain Garden 2 Pervious: Rain Garden 2 Pervious

Runoff	=	0.06 cfs @	13.21 hrs,	Volume=	0.040 af,	Depth= 0.29"
Routed	to Pond	Rain Garder	n 2 : Rain G	arden 2		

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 10 year Rainfall=5.40"

	Area	(ac)	CN	Desc	cription		
*	1.	650	39	lawn	, A soils		
	1.	650		100.	00% Pervi	ous Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0						Direct Entry,

#### Summary for Subcatchment Rain Garden 3 Impervious: Rain Garden 3 Impervious

Runoff = 4.56 cfs @ 12.19 hrs, Volume= 0.594 af, Depth> 4.92" Routed to Pond Rain Garden 3 : Rain Garden 3

	Area (ac)	CN	Description
*	0.450	98	Pavement
*	0.600	98	Roof
*	0.400	98	Driveway
	1.450	98	Weighted Average
	1.450		100.00% Impervious Area

Post Developed	Post Developed. NRCC 24-hr D 10 year Rainfall=5.40"
Prepared by Professional Design Services HydroCAD® 10.20-3c s/n 02223 © 2023 HydroCAD Software	Printed 6/19/2023
Tc Length Slope Velocity Capacity Descrip (min) (feet) (ft/ft) (ft/sec) (cfs)	tion
10.0 <b>Direct</b>	Entry, pavement and pipe
Summary for Subcatchment Rain Garder	3 Pervious: Rain Garden 3 Pervious
Runoff = 0.05 cfs @ 13.21 hrs, Volume= Routed to Pond Rain Garden 3 : Rain Garden 3	0.032 af, Depth= 0.29"
Runoff by SCS TR-20 method, UH=Delmarva, Weighted NRCC 24-hr D 10 year Rainfall=5.40"	CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs
Area (ac) CN Description	
* 1.350 39 lawn, A soils	
1.350 100.00% Pervious Area	
Tc Length Slope Velocity Capacity Descrip (min) (feet) (ft/ft) (ft/sec) (cfs)	
15.0 <b>Direct</b>	Entry,
Summary for Subcatchment Rain Garden 4	Impervious: Rain Garden 4 Impervious
Runoff = 1.26 cfs @ 12.19 hrs, Volume= Routed to Pond Rain Garden 4 : Rain Garden 4	0.164 af, Depth> 4.92"
Runoff by SCS TR-20 method, UH=Delmarva, Weighted- NRCC 24-hr D 10 year Rainfall=5.40"	CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs
Area (ac) CN Description	
* 0.400 98 Roof	
0.400 100.00% Impervious Area	
Tc Length Slope Velocity Capacity Descrip (min) (feet) (ft/ft) (ft/sec) (cfs)	
10.0 Direct	Entry, pavement and pipe
Summary for Subcatchment Rain Garder	4 Pervious: Rain Garden 4 Pervious
Runoff = 0.02 cfs @ 13.21 hrs, Volume= Routed to Pond Rain Garden 4 : Rain Garden 4	0.014 af, Depth= 0.29"
Runoff by SCS TR-20 method, UH=Delmarva, Weighted- NRCC 24-hr D 10 year Rainfall=5.40"	CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs
Area (ac) CN Description	
* 0.600 39 lawn, A soils	

_	/	0.1	Beechpitch
*	0.600	39	lawn, A soils
	0.600		100.00% Pervious Area

Post Developed Prepared by Professional Design Services	NRCC 24-hr D 10 year Rainfall=5.40" Printed 6/19/2023
<u>HydroCAD® 10.20-3c s/n 02223 © 2023 HydroCAD Software Solu</u> Tc Length Slope Velocity Capacity Description	utions LLC Page 25
(min) (feet) (ft/ft) (ft/sec) (cfs)	
15.0 Direct Entry	<b>y</b> ,
Summary for Subcatchment R	G 5: Rain Garden 5
Runoff = 1.07 cfs @ 12.21 hrs, Volume= Routed to Pond Rain Garden 5 : Rain Garden 5	0.141 af, Depth= 1.54"
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, NRCC 24-hr D 10 year Rainfall=5.40"	Time Span= 5.00-30.00 hrs, dt= 0.05 hrs
Area (ac) CN Description	
* 0.400 98 Roof * 0.700 30 Lown A soils	
0.700 39 Lawit A solis	
1.10060Weighted Average0.70063.64% Pervious Area	
0.400 36.36% Impervious Area	
· ·	
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)	
	y, pavement and pipe
Summary for Pond Basi	n 1: Basin 1
Inflow Area = 7.400 ac, 49.32% Impervious, Inflow De Inflow = 2.83 cfs @ 12.19 hrs, Volume=	pth > 0.71" for 10 year event 0.435 af
	0.435  af, Atten = 81%,  Lag = 49.6  min
Discarded = $0.20 \text{ cfs} (\overline{a}) = 9.95 \text{ hrs}, \text{ Volume} = 0.20 \text{ cfs} (\overline{a}) = 0.2$	0.343 af
Primary = 0.35 cfs @ 13.02 hrs, Volume= Routed to Pond Basin 2 : Basin 2	0.092 af
Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt=	0.05 hrs
Peak Elev= 72.86' @ 13.02 hrs Surf.Area= $0.059$ ac Storage	
Plug-Flow detention time= 166.0 min calculated for 0.434 af (	100% of inflow)

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Plug-Flow detention time= 166.0 min calculated for 0.434 af (100% of inflow) Center-of-Mass det. time= 165.6 min ( 999.0 - 833.4 )

Volume	Invert	Avail.Storage	Stor	age Description	
#1	70.00'	0.200 af	rete	ntion basin (Pris	smatic)Listed below
Elevation (feet)	Surf.Are (acres			Cum.Store (acre-feet)	
70.00 71.00 72.00 73.00 74.00	0.03 0.04 0.05 0.06 0.07	0 0.0 0 0.0 0 0.0	)00 )35 )45 )55 )65	0.000 0.035 0.080 0.135 0.200	

Post DevelopedPost Developed.Prepared by Professional Design ServicesNRCC 24-hr D10 year Rainfall=5.40"HydroCAD® 10.20-3cs/n 02223© 2023 HydroCAD Software Solutions LLCPrinted6/19/2023Page 26

Device	Routing	Invert	Outlet Devices
#1	Discarded	70.00'	0.20 cfs Exfiltration when above 70.00'
#2	Primary	72.00'	<b>4.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Primary	74.00'	<b>48.0" x 48.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Discarded OutFlow** Max=0.20 cfs @ 9.95 hrs HW=70.04' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.20 cfs)

Primary OutFlow Max=0.35 cfs @ 13.02 hrs HW=72.86' (Free Discharge) 2=Orifice/Grate (Orifice Controls 0.35 cfs @ 4.01 fps) 3=Orifice/Grate (Controls 0.00 cfs)

# Summary for Pond Basin 2: Basin 2

Inflow Area =	20.600 ac, 43.69%	Impervious, Inflow D	Depth > 0.87"	for 10 year event
Inflow =	9.75 cfs @ 12.19 l	nrs, Volume=	1.486 af	-
Outflow =	1.00 cfs @ 11.10 l	nrs, Volume=	1.486 af, Atte	en= 90%, Lag= 0.0 min
Discarded =	1.00 cfs @ 11.10 l	nrs, Volume=	1.486 af	
Primary =	0.00 cfs @ 5.00 l	nrs, Volume=	0.000 af	
Routed to Link	Site : Site			

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 69.59' @ 14.97 hrs Surf.Area= 0.431 ac Storage= 0.547 af

Plug-Flow detention time= 213.5 min calculated for 1.486 af (100% of inflow) Center-of-Mass det. time= 212.8 min (1,027.3 - 814.5)

Volume	Invert	Avail.Storag	e Stor	brage Description
#1	68.00'	3.600 a	af Cus	stom Stage Data (Prismatic)Listed below x 1.2
Elevatio (fee 68.0	et) (acre	s) (acre	Store -feet) 0.000	Cum.Store (acre-feet) 0.000
69.0		-	0.250	0.250
70.0		-	0.350	0.600
71.0	0.50	00	0.450	1.050
72.0	0.60	00	0.550	1.600
73.0	0.70	0	0.650	2.250
74.0	0.80	00	0.750	3.000
Device #1 #2 #3	Routing Discarded Primary Primary	68.00' 70.70' 73.00'	1.00 cfs 3.0" Vei 12.0" W	Devices <b>S Exfiltration when above 68.00'</b> <b>ert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads <b>V x 42.0" H Vert. Orifice/Grate</b> C= 0.600 I to weir flow at low heads

**Discarded OutFlow** Max=1.00 cfs @ 11.10 hrs HW=68.09' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 1.00 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=68.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs) -3=Orifice/Grate (Controls 0.00 cfs)

#### Summary for Pond Basin 3: Basin 3

Inflow Area =	6.000 ac, 45.83% Impervious, Inflow D	epth > 2.04" for 10 year event				
Inflow =	7.55 cfs @ 12.19 hrs, Volume=	1.022 af				
Outflow =	0.38 cfs @ 16.87 hrs, Volume=	0.653 af, Atten= 95%, Lag= 281.0 min				
Discarded =	0.30 cfs @     7.75 hrs,  Volume=	0.599 af				
Primary =	0.08 cfs @ 16.87 hrs, Volume=	0.054 af				
Routed to Pond Basin 1 : Basin 1						

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 74.25' @ 16.87 hrs Surf.Area= 0.315 ac Storage= 0.563 af

Plug-Flow detention time= 410.1 min calculated for 0.651 af (64% of inflow)	
Center-of-Mass det. time= 280.8 min ( 1,078.0 - 797.2 )	

	ge Description	Storage Description	Storage S	Avail.S	Invert	Volume
x 1.2	om Stage Data (Prismatic)Listed below x 1.2	<b>Custom Stage Data</b>	1.200 af <b>(</b>	1	72.00'	#1
	Cum.Store (acre-feet)		Inc.Stor (acre-fee		Surf.Area (acres	Elevation (feet)
	0.000	00.00 0.000	0.00	150	0.15	72.00
	0.175	75 0.175	0.17	200	0.20	73.00
	0.400	25 0.400	0.22	250	0.25	74.00
	0.675	75 0.675	0.27	300	0.30	75.00
	1.000	25 1.000	0.32	350	0.35	76.00
	vices	et Devices	vert Outle	Inv	Routing	Device F
	Exfiltration when above 72.00'	) cfs Exfiltration whe	.00' <b>0.30</b>	72.0	Discarded	#1 E
ir flow at low heads	. Orifice/Grate C= 0.600 Limited to weir flow a	Vert. Orifice/Grate	.00' <b>3.0''</b>	74.(	Primary	#2 F
	<b>42.0" H Vert. Orifice/Grate</b> C= 0.600 weir flow at low heads			75.0	Primary	#3 F
ir flow at low he	(acre-feet) 0.000 0.175 0.400 0.675 1.000 vices Exfiltration when above 72.00' . Orifice/Grate C= 0.600 Limited to weir flow a x 42.0" H Vert. Orifice/Grate C= 0.600	et)         (acre-feet)           00         0.000           75         0.175           25         0.400           75         0.675           25         1.000           let Devices         0           O cfs Exfiltration where         0           'Vert. Orifice/Grate         0           ''W x 42.0" H Vert.         0           ited to weir flow at low         0	(acre-fee 0.00 0.17 0.22 0.27 0.32 <u>vert Outle</u> 00' 0.30 .00' 3.0" .00' 42.0' Limit	res) 150 200 250 300 350 <u>Inv</u> 72.0 74.0	(acres 0.15) 0.20) 0.25) 0.30) 0.35) Routing Discarded Primary	(feet) 72.00 73.00 74.00 75.00 76.00 <u>Device F</u> #1 [ #2 F

**Discarded OutFlow** Max=0.30 cfs @ 7.75 hrs HW=72.07' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.08 cfs @ 16.87 hrs HW=74.25' (Free Discharge) -2=Orifice/Grate (Orifice Controls 0.08 cfs @ 1.72 fps) -3=Orifice/Grate (Controls 0.00 cfs)

Inflow Area =	1.500 ac, 23.33% Impervious, Inflow I	Depth > 1.37" for 10 year event
Inflow =	1.10 cfs @ 12.19 hrs, Volume=	0.171 af
Outflow =	1.10 cfs @ 12.19 hrs, Volume=	0.171 af, Atten= 0%, Lag= 0.0 min
Discarded =	0.00 cfs @ 12.19 hrs, Volume=	0.000 af
Primary =	1.10 cfs @ 12.19 hrs, Volume=	0.171 af
Routed to Pond	l Basin 2 : Basin 2	

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 78.00' @ 12.19 hrs Surf.Area= 0.060 ac Storage= 0.000 af

Plug-Flow detention time= 0.0 min calculated for 0.171 af (100% of inflow) Center-of-Mass det. time= 0.0 min (831.1 - 831.1)

Volume	Invert A	vail.Storage	e Storage Description			
#1	78.00'	0.400 af	f Custom Stage Data (Prismatic)Listed below (Recalc)			
Elevatio (fee	t) (acres)	(acre-				
78.0	0.060	0	0.000 0.000			
79.0	0.080	0	0.070 0.070			
80.0	0.100	0	0.090 0.160			
81.0	0 0.120	0	0.110 0.270			
82.0	0 0.140	0	0.130 0.400			
Device	Routing	Invert O	Dutlet Devices			
#1	Discarded	78.00' <b>0</b> .	0.30 cfs Exfiltration when above 75.00'			
#2	Primary	80.00' <b>3</b> .	<b>3.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads			
#3	Primary		<b>2.0" x 48.0" Horiz. Orifice/Grate</b> C= 0.600 imited to weir flow at low heads			
Discorded OutElow May-0.20 of a 2.10 bra LIW-78.00' (Erea Discharge)						

Discarded OutFlow Max=0.30 cfs @ 12.19 hrs HW=78.00' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=301.47 cfs @ 12.19 hrs HW=78.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs) -3=Orifice/Grate (Orifice Controls 301.47 cfs @ 21.53 fps)

# Summary for Pond Rain Garden 2: Rain Garden 2

Inflow Area =	2.000 ac, 17.50% Impervious, Inf	flow Depth > 1.10" for 10 year event
Inflow =	1.10 cfs @ 12.19 hrs, Volume=	0.183 af
Outflow =	0.30 cfs @ 11.90 hrs, Volume=	0.183 af, Atten= 73%, Lag= 0.0 min
Discarded =	0.30 cfs @ 11.90 hrs, Volume=	0.183 af
Primary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af
Routed to Pond	l Basin 3 : Basin 3	

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs

Peak Elev= 75.51' @ 12.90 hrs Surf.Area= 0.060 ac Storage= 0.029 af

Plug-Flow detention time= 23.9 min calculated for 0.183 af (100% of inflow) Center-of-Mass det. time= 23.5 min ( 869.7 - 846.1 )

Volume	Invert A	Avail.Storage	Storage Description
#1	75.00'	0.300 af	Custom Stage Data (Prismatic)Listed below (Recalc)
Elevatio (fee 75.0 76.0 77.0 78.0 79.0	et) (acres) 00 0.055 00 0.065 00 0.065 00 0.075	(acre- 0 0 0 0 0 0	Store         Cum.Store           feet)         (acre-feet)           0.000         0.000           0.060         0.060           0.070         0.130           0.080         0.210           0.090         0.300
Device #1 #2 #3	Routing Discarded Primary Primary	75.00' <b>0</b> . 77.00' <b>3</b> . 79.00' <b>4</b> 2	outlet Devices.30 cfs Exfiltration when above 75.00'.0" Vert. Orifice/GrateC= 0.600Limited to weir flow at low heads2.0" x 48.0" Horiz. Orifice/GrateC= 0.600imited to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 11.90 hrs HW=75.04' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=75.00' (Free Discharge)

**2=Orifice/Grate** (Controls 0.00 cfs)

-3=Orifice/Grate (Controls 0.00 cfs)

# Summary for Pond Rain Garden 3: Rain Garden 3

Inflow Area =	2.800 ac, 5	1.79% Impervious, Inflow	Depth > $2.68"$ for	10 year event
Inflow =	4.56 cfs @	12.19 hrs, Volume=	0.626 af	-
Outflow =	0.30 cfs @	9.95 hrs, Volume=	0.572 af, Atten=	93%, Lag= 0.0 min
Discarded =	0.30 cfs @	9.95 hrs, Volume=	0.572 af	-
Primary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af	
Routed to Pond	l Basin 2 : Bas	sin 2		

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 76.30' @ 15.34 hrs Surf.Area= 0.280 ac Storage= 0.279 af

Plug-Flow detention time= 354.3 min calculated for 0.570 af (91% of inflow) Center-of-Mass det. time= 304.4 min (1,105.5 - 801.0)

Volume	Invert	Avail.Storage	Storage Description
#1	75.00'	2.000 af	Custom Stage Data (Prismatic)Listed below (Recalc)

# **Post Developed**

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Elevatio (fee			c.Store re-feet)	Cum.Store (acre-feet)	
75.0	0.150		0.000	0.000	
76.0	0.250		0.200	0.200	
77.0	0.350		0.300	0.500	
78.0	0.450		0.400	0.900	
79.0	0.550		0.500	1.400	
80.0	0.650		0.600	2.000	
Device	Routing	Invert	Outlet De	vices	
#1	Discarded	75.00'	0.30 cfs I	Exfiltration wh	en above 75.00'
#2	Primary	77.00'	3.0" Vert	. Orifice/Grate	C= 0.600 Limited to weir flow at low heads
#3	Primary	79.00'	42.0" x 4	8.0" Horiz. Ori	fice/Grate C= 0.600
			Limited to	weir flow at lo	w heads

**Discarded OutFlow** Max=0.30 cfs @ 9.95 hrs HW=75.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=75.00' (Free Discharge) **2=Orifice/Grate** (Controls 0.00 cfs)

-3=Orifice/Grate (Controls 0.00 cfs)

# Summary for Pond Rain Garden 4: Rain Garden 4

Inflow Area =	1.000 ac, 40.00% Impervious, Inflow De	epth > 2.14" for 10 year event
Inflow =	1.26 cfs @ 12.19 hrs, Volume=	0.178 af
Outflow =	0.30 cfs @ 11.90 hrs, Volume=	0.178 af, Atten= 76%, Lag= 0.0 min
Discarded =	0.30 cfs @ 11.90 hrs, Volume=	0.178 af
Primary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af
Routed to Pond	d Basin 2 : Basin 2	

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 75.43' @ 12.89 hrs Surf.Area= 0.089 ac Storage= 0.037 af

Plug-Flow detention time= 34.2 min calculated for 0.178 af (100% of inflow) Center-of-Mass det. time= 33.7 min ( 842.7 - 809.0 )

Volume	Invert	Avail.Storage	Storage	e Description	
#1	75.00'	0.550 af	Custor	n Stage Data	(Prismatic)Listed below (Recalc)
Elevation (feet)	Surf.Ar (acre			Cum.Store (acre-feet)	
75.00	0.0	85 0.	000	0.000	
76.00	0.0	95 0.	090	0.090	
77.00	0.1	05 0.	100	0.190	
78.00	0.1	15 0.	110	0.300	
79.00	0.1	25 0.	120	0.420	
80.00	0.1	35 0.	130	0.550	

		Post Developed.
Post Developed	NRCC 24-hr D	10 year Rainfall=5.40"
Prepared by Professional Design Services		Printed 6/19/2023
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		1 490 01

Device	Routing	Invert	Outlet Devices
#1	Discarded	75.00'	0.30 cfs Exfiltration when above 75.00'
#2	Primary	77.00'	<b>3.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Primary	79.00'	<b>42.0" x 48.0" Horiz. Grate</b> C= 0.600 Limited to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 11.90 hrs HW=75.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=75.00' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs) 3=Grate (Controls 0.00 cfs)

# Summary for Pond Rain Garden 5: Rain Garden 5

Inflow Area =	1.100 ac, 36.36% Impervious, Inflow	/ Depth = 1.54" for 10 year event
Inflow =	1.07 cfs @ 12.21 hrs, Volume=	0.141 af
Outflow =	0.30 cfs @ 12.10 hrs, Volume=	0.141 af, Atten= 72%, Lag= 0.0 min
Discarded =	0.30 cfs @ 12.10 hrs, Volume=	0.141 af
Primary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af
Routed to Pond	d Basin 2 : Basin 2	

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 73.34' @ 12.99 hrs Surf.Area= 0.088 ac Storage= 0.029 af

Plug-Flow detention time= 31.5 min calculated for 0.141 af (100% of inflow) Center-of-Mass det. time= 31.3 min (945.6 - 914.4)

Volume	Invert A	Avail.Storage	e Storage Description				
#1	73.00'	0.550 a	af Custom Stage Data (Prismatic)Listed below (Recalc)				
Elevatio (fee			.Store Cum.Store e-feet) (acre-feet)				
73.0	0.085	; (	0.000 0.000				
74.0	0.095	; (	0.090 0.090				
75.0	0.105	; (	0.100 0.190				
76.0	0.115	; (	0.110 0.300				
77.0	0.125	; (	0.120 0.420				
78.0	0.135	; (	0.130 0.550				
Device	Device Routing		Outlet Devices				
#1	Discarded		0.30 cfs Exfiltration when above 73.00'				
		77.00' <b>4</b>	<b>3.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads <b>42.0" x 48.0" Horiz. Grate</b> C= 0.600 Limited to weir flow at low heads				
		L					

**Discarded OutFlow** Max=0.30 cfs @ 12.10 hrs HW=73.06' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=73.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs) -3=Grate (Controls 0.00 cfs)

# Summary for Link Site: Site

Inflow Area	a =	20.600 ac, 43	3.69% Impervious, I	nflow Depth = 0.00	)" for 10 year event
Inflow	=	0.00 cfs @	5.00 hrs, Volume=	0.000 af	
Primary	=	0.00 cfs @	5.00 hrs, Volume=	0.000 af, A	Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs

Post DevelopedPost Developed.Post DevelopedNRCC 24-hr D25 year Rainfall=6.70"Prepared by Professional Design ServicesPrinted6/19/2023HydroCAD® 10.20-3c s/n 02223 © 2023 HydroCAD Software Solutions LLCPage 33
Time span=5.00-30.00 hrs, dt=0.05 hrs, 501 points Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method
Subcatchment Basin 1 Imp: Basin 1 Imp Runoff Area=0.900 ac 100.00% Impervious Runoff Depth>6.12" Tc=10.0 min CN=98 Runoff=3.52 cfs 0.459 af
Subcatchment Basin 1 Pervious: Basin 1 - Runoff Area=0.500 ac 0.00% Impervious Runoff Depth=0.66" Tc=15.0 min CN=39 Runoff=0.08 cfs 0.028 af
Subcatchment Basin 2 - Pervious: Basin 2 - Runoff Area=4.050 ac 0.00% Impervious Runoff Depth=0.66" Tc=15.0 min CN=39 Runoff=0.62 cfs 0.224 af
Subcatchment Basin 2 Impervious: basin Runoff Area=2.750 ac 100.00% Impervious Runoff Depth>6.12" Tc=10.0 min CN=98 Runoff=10.75 cfs 1.403 af
Subcatchment Basin 3 Impervious: basin Runoff Area=2.400 ac 100.00% Impervious Runoff Depth>6.12" Tc=10.0 min CN=98 Runoff=9.38 cfs 1.225 af
Subcatchment Basin 3 Pervious: Basin 3 - Runoff Area=1.600 ac 0.00% Impervious Runoff Depth=0.66" Tc=15.0 min CN=39 Runoff=0.24 cfs 0.089 af
Subcatchment Rain Garden 1 Impervious: Runoff Area=0.350 ac 100.00% Impervious Runoff Depth>6.12" Tc=10.0 min CN=98 Runoff=1.37 cfs 0.179 af
Subcatchment Rain Garden 1 Pervious: Rain Runoff Area=1.150 ac 0.00% Impervious Runoff Depth=0.66" Tc=15.0 min CN=39 Runoff=0.18 cfs 0.064 af
Subcatchment Rain Garden 2 Impervious: Runoff Area=0.350 ac 100.00% Impervious Runoff Depth>6.12" Tc=10.0 min CN=98 Runoff=1.37 cfs 0.179 af
Subcatchment Rain Garden 2 Pervious: Rain Runoff Area=1.650 ac 0.00% Impervious Runoff Depth=0.66" Tc=15.0 min CN=39 Runoff=0.25 cfs 0.091 af
Subcatchment Rain Garden 3 Impervious: Runoff Area=1.450 ac 100.00% Impervious Runoff Depth>6.12" Tc=10.0 min CN=98 Runoff=5.67 cfs 0.740 af
Subcatchment Rain Garden 3 Pervious: Rain Runoff Area=1.350 ac 0.00% Impervious Runoff Depth=0.66" Tc=15.0 min CN=39 Runoff=0.21 cfs 0.075 af
Subcatchment Rain Garden 4 Impervious: Runoff Area=0.400 ac 100.00% Impervious Runoff Depth>6.12" Tc=10.0 min CN=98 Runoff=1.56 cfs 0.204 af
Subcatchment Rain Garden 4 Pervious: Rain Runoff Area=0.600 ac 0.00% Impervious Runoff Depth=0.66" Tc=15.0 min CN=39 Runoff=0.09 cfs 0.033 af
Subcatchment RG 5: Rain Garden 5       Runoff Area=1.100 ac 36.36% Impervious Runoff Depth=2.39"         Tc=10.0 min CN=60 Runoff=1.75 cfs 0.219 af
Pond Basin 1: Basin 1Peak Elev=73.61'Storage=0.175 afInflow=3.55 cfs0.702 afDiscarded=0.20 cfs0.393 afPrimary=0.51 cfs0.277 afOutflow=0.71 cfs0.669 af

Post Developed Prepared by Professiona HydroCAD® 10.20-3c_s/n 02		) Software :		?4-hr D	Post Dev 25 year Rainfa Printed 6/	nll=6.70"
Pond Basin 2: Basin 2	F Discarded=1.00 cfs 1.		•		Inflow=12.67 cfs Outflow=1.00 cfs	
Pond Basin 3: Basin 3	Discarded=0.30 cfs 0.				Inflow=9.50 cfs Outflow=0.50 cfs	
Pond Rain Garden 1: Rair	<b>Garden 1</b> Discarded=0.00 cfs 0.		•		Inflow=1.46 cfs Outflow=1.46 cfs	
Pond Rain Garden 2: Rair	<b>Garden 2</b> Discarded=0.30 cfs 0.				Inflow=1.50 cfs Outflow=0.30 cfs	
Pond Rain Garden 3: Rair	<b>Garden 3</b> Discarded=0.30 cfs 0.				Inflow=5.77 cfs Outflow=0.30 cfs	
Pond Rain Garden 4: Rair	<b>Garden 4</b> Discarded=0.30 cfs 0.		0		Inflow=1.61 cfs Outflow=0.30 cfs	
Pond Rain Garden 5: Rair	<b>Garden 5</b> Discarded=0.30 cfs 0.				Inflow=1.75 cfs Outflow=0.30 cfs	
Link Site: Site					Inflow=0.00 cfs Primary=0.00 cfs	
Total Runof	f Area = 20.600 ac   F 56.31	Runoff Vo % Pervioເ			age Runoff Dep % Impervious =	

#### Summary for Subcatchment Basin 1 Imp: Basin 1 Imp

Runoff = 3.52 cfs @ 12.19 hrs, Volume= 0.459 af, Depth> 6.12" Routed to Pond Basin 1 : Basin 1

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 25 year Rainfall=6.70"

	Area	(ac)	CN	Desc	cription		
*	0.	500	98	Pave	ement		
*	0.	400	98	Root	-		
	0.	900	98	Weig	ghted Aver	age	
	0.	0.900 100.00% Impervious Area					
	Тс	Leng	th	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	10.0						Direct Entry, pavement and pipe

# Summary for Subcatchment Basin 1 Pervious: Basin 1 - Pervious

Runoff = 0.08 cfs @ 12.50 hrs, Volume= Routed to Pond Basin 1 : Basin 1

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 25 year Rainfall=6.70"

_	Area	(ac)	CN	Desc	cription		
*	0.	500	39	lawn	, A soils		
	0.	500		100.	00% Pervi	ous Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0						Direct Entry,

#### Summary for Subcatchment Basin 2 - Pervious: Basin 2 - Pervious

Runoff = 0.62 cfs @ 12.50 hrs, Volume= Routed to Pond Basin 2 : Basin 2 0.224 af, Depth= 0.66"

0.028 af, Depth= 0.66"

	Area (ac)	CN	Description
*	4.050	39	lawn, A soils
	4.050		100.00% Pervious Area

	evelope			<b>_</b>		NRCC 24-hr	D 25 year Rainfall=6.70"			
	d by Prof						Printed 6/19/2023			
<u>HydroCA</u>	D® 10.20-3	<u>c s/n 02</u>	223 © 202	3 HydroCAE	) Software Solu	itions LLC	Page 36			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
15.0					Direct Entry	/,				
Summary for Subcatchment Basin 2 Impervious: basin 2 Impervious										
Runoff Route	= ed to Pond			9 hrs, Volu	ime=	1.403 af, Depth	> 6.12"			
NRCC 2	4-hr D 25	year Ra	infall=6.70		Veighted-CN,	Time Span= 5.00	0-30.00 hrs, dt= 0.05 hrs			
Area			cription							
0.	.600 98									
	.450 98									
	.700 98 .000 98		eways d & Sidewa							
	.750 98 .750		phted Aver							
Ζ.	.750	100.	00% impe	rvious Area	1					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
10.0					Direct Entry	/, pavement				
	Summ	nary fo	r Subcat	chment I	Basin 3 Imp	ervious: basi	n 3 Impervious			

9.38 cfs @ 12.19 hrs, Volume= 1.225 af, Depth> 6.12" Runoff = Routed to Pond Basin 3 : Basin 3

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	Area	(ac)	CN	Desc	ription		
*	0.	900	98	Park	ing		
*	0.	300	98	Roof			
*	0.	500	98	Drive	eways		
*	0.	700	98	Road	d & Sidewa	alk	
	2.	400	98	Weig	hted Aver	age	
	2.	2.400 100.00% Impervious Area					
	Тс	Leng	th	Slope	Velocity	Capacity	Description
	(min)	(fee		(ft/ft)	(ft/sec)	(cfs)	•
	10.0						Direct Entry, pavement

#### Summary for Subcatchment Basin 3 Pervious: Basin 3 - Pervious

Runoff = 0.24 cfs @ 12.50 hrs, Volume= 0.089 af, Depth= 0.66" Routed to Pond Basin 3 : Basin 3

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 25 year Rainfall=6.70"

_	Area	(ac)	CN	Desc	cription		
*	1.	.600	39	lawn	, A soils		
	1.	600		100.	00% Pervi	ous Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0						Direct Entry,

# Summary for Subcatchment Rain Garden 1 Impervious: Rain Garden 1 Impervious

0.179 af, Depth> 6.12"

Runoff	=	1.37 cfs @ 12.19	hrs, Volume=
Routed	l to Por	nd Rain Garden 1 : Ra	in Garden 1

Routed to Pond Rain Garden 1 : Rain Garden 1

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 25 year Rainfall=6.70"

Area	(ac) C	N Des	cription								
<u>*</u> 0	.350 9	98 Root	F								
0	.350	100.	00% Impe	rvious Area							
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description						
10.0					Direct Entr	y, pavement and pipe					
S	Summary for Subcatchment Rain Garden 1 Pervious: Rain Garden 1 Pervious										
Runoff	=	0.18 cfs	s@ 12.5	0 hrs, Volu	me=	0.064 af, Depth= 0.66"					

	Area	(ac)	CN	Desc	cription		
*	1.	150	39	lawn	, A soils		
	1.	150		100.	00% Pervi	ous Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0	(	-,	(1411)	()	()	Direct Entry,

# Summary for Subcatchment Rain Garden 2 Impervious: Rain Garden 2 Impervious

Runoff	=	1.37 cfs @	12.19 hrs, Volum	e=	0.179 af,	Depth>	6.12"
Routed	to Pond	l Rain Garde	n 2 : Rain Garden 2	2		•	

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 25 year Rainfall=6.70"

	Area	(ac)	CN	Desc	cription		
*	0.	350	98	Roof	-		
0.350 100.00% Impervious Area						rvious Area	
	Tc (min)	Lengt (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	10.0	(100	<u>()</u>		(1000)	(003)	Direct Entry, pavement and pipe

# Summary for Subcatchment Rain Garden 2 Pervious: Rain Garden 2 Pervious

Depth= 0.66"

Runoff	=	0.25 cfs @	12.50 hrs, Volume=	0.091 af,
Routed	to Pond	Rain Garder	n 2 : Rain Garden 2	

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 25 year Rainfall=6.70"

	Area	(ac)	CN	Desc	cription		
*	1.	650	39	lawn	, A soils		
1.650 100.00% Pervious Area					00% Pervi	ous Area	
	Tc (min)	Lengt (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0						Direct Entry,

#### Summary for Subcatchment Rain Garden 3 Impervious: Rain Garden 3 Impervious

Runoff = 5.67 cfs @ 12.19 hrs, Volume= 0.740 af, Depth> 6.12" Routed to Pond Rain Garden 3 : Rain Garden 3

	Area (ac)	CN	Description
*	0.450	98	Pavement
*	0.600	98	Roof
*	0.400	98	Driveway
	1.450	98	Weighted Average
	1.450		100.00% Impervious Area

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Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)
10.0 Direct Entry, pavement and pipe
Summary for Subcatchment Rain Garden 3 Pervious: Rain Garden 3 Pervious
Runoff = 0.21 cfs @ 12.50 hrs, Volume= 0.075 af, Depth= 0.66" Routed to Pond Rain Garden 3 : Rain Garden 3
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D_25 year Rainfall=6.70"
Area (ac) CN Description
<u>* 1.350 39 lawn, A soils</u>
1.350 100.00% Pervious Area
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)
15.0 Direct Entry,
Summary for Subcatchment Rain Garden 4 Impervious: Rain Garden 4 Impervious
Runoff = 1.56 cfs @ 12.19 hrs, Volume= 0.204 af, Depth> 6.12" Routed to Pond Rain Garden 4 : Rain Garden 4
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D_25 year Rainfall=6.70"
Area (ac) CN Description
* 0.400 98 Roof
0.400 100.00% Impervious Area
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)
10.0 Direct Entry, pavement and pipe
Summary for Subcatchment Rain Garden 4 Pervious: Rain Garden 4 Pervious
Runoff = 0.09 cfs @ 12.50 hrs, Volume= 0.033 af, Depth= 0.66" Routed to Pond Rain Garden 4 : Rain Garden 4
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D_25 year Rainfall=6.70"
Area (ac) CN Description

	Area (ac)	CN	Description
*	0.600	39	lawn, A soils
	0.600		100.00% Pervious Area

	d by Drof		l Design S	Sonvisoos		MACO	24-11020	Printed 6/19/2023			
					) Software So	lutions I I C		Printed 0/19/2023 Page 40			
	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)				<u> </u>			
15.0					Direct Ent	ry,					
	Summary for Subcatchment RG 5: Rain Garden 5										
Runoff Route	= ed to Ponc			0 hrs, Volu Rain Garde		0.219 af,	Depth= 2.39"				
	Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 25 year Rainfall=6.70"										
Area			cription								
	400 9	-									
-	700 <u>3</u> 100 6		<u>n A soils</u> hted Aver								
	700 0		4% Pervio								
	400			/ious Area							
Tc (min) 10.0	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		ent and pipe				
10.0					Direct Litt	y, paveine	and pipe				
			Sum	mary for	Pond Bas	in 1: Basi	in 1				
Inflow Ar Inflow Outflow Discarde Primary Route	= =	3.55 cfs 0.71 cfs 0.20 cfs 0.51 cfs	s@ 12.1 s@ 13.3 s@ 9.3 s@ 13.3	% Impervio 9 hrs, Volu 0 hrs, Volu 0 hrs, Volu 0 hrs, Volu 0 hrs, Volu	ume= ume= ume=	0.702 af	4" for 25 ye Atten= 80%,	ar event Lag= 66.2 min			
				<b>5</b> 00 0		0.051					

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NRCC 24-hr D 25 year Rainfall=6.70"

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 73.61' @ 13.30 hrs Surf.Area= 0.066 ac Storage= 0.175 af

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Plug-Flow detention time= 160.3 min calculated for 0.669 af (95% of inflow) Center-of-Mass det. time= 126.8 min (1,046.2 - 919.4)

Volume	Invert	Avail.Storage	Stor	age Description	
#1	70.00'	0.200 af	rete	ntion basin (Pr	ismatic)Listed below
Elevation (feet)	Surf.Are (acres			Cum.Store (acre-feet)	
70.00 71.00	0.03 0.04		000 035	0.000 0.035	
72.00 73.00 74.00	0.05 0.06 0.07	0.0	045 055 065	0.080 0.135 0.200	

Post DevelopedPost Developed.Prepared by Professional Design ServicesNRCC 24-hr D25 year Rainfall=6.70"HydroCAD® 10.20-3cs/n 02223© 2023 HydroCAD Software Solutions LLCPrinted6/19/2023Printed 6/19/2023Printed 6/19/2023Printed6/19/2023

Device	Routing	Invert	Outlet Devices
#1	Discarded	70.00'	0.20 cfs Exfiltration when above 70.00'
#2	Primary	72.00'	<b>4.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Primary	74.00'	<b>48.0" x 48.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Discarded OutFlow** Max=0.20 cfs @ 9.30 hrs HW=70.04' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.20 cfs)

Primary OutFlow Max=0.51 cfs @ 13.30 hrs HW=73.61' (Free Discharge) 2=Orifice/Grate (Orifice Controls 0.51 cfs @ 5.79 fps) 3=Orifice/Grate (Controls 0.00 cfs)

#### Summary for Pond Basin 2: Basin 2

Inflow Area =	20.600 ac, 43.69	% Impervious, Inflow E	Depth > 1.25" for  25 year e	vent
Inflow =	12.67 cfs @ 12.2	20 hrs, Volume=	2.146 af	
Outflow =	1.00 cfs @ 10.6	65 hrs, Volume=	1.854 af, Atten= 92%, Lag	= 0.0 min
Discarded =	1.00 cfs @ 10.6	35 hrs, Volume=	1.854 af	
Primary =	0.00 cfs @ 5.0	00 hrs, Volume=	0.000 af	
Routed to Link	Site : Site			

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 70.37' @ 17.68 hrs Surf.Area= 0.525 ac Storage= 0.921 af

Plug-Flow detention time= 351.9 min calculated for 1.849 af (86% of inflow) Center-of-Mass det. time= 281.2 min (1,122.8 - 841.5)

Volume	Invert	Avail.Stora	ge Sto	orage Description
#1	68.00'	3.600	af Cu	ustom Stage Data (Prismatic)Listed below x 1.2
Elevatic (fee 68.0	et) (acre	s) (acr	c.Store <u>e-feet)</u> 0.000	Cum.Store (acre-feet) 0.000
69.0		-	0.000	0.250
70.0		-	0.250	0.600
71.0	0.50	00	0.450	1.050
72.0	0.60	00	0.550	1.600
73.0	0.70	00	0.650	2.250
74.0	0.80	00	0.750	3.000
Device #1 #2 #3	Routing Discarded Primary Primary	Invert 68.00' 70.70' 73.00'	1.00 cfs 3.0" Ve 42.0" W	Devices fs Exfiltration when above 68.00' ert. Orifice/Grate C= 0.600 Limited to weir flow at low heads W x 42.0" H Vert. Orifice/Grate C= 0.600
			Limited	d to weir flow at low heads

**Discarded OutFlow** Max=1.00 cfs @ 10.65 hrs HW=68.09' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 1.00 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=68.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs) -3=Orifice/Grate (Controls 0.00 cfs)

#### Summary for Pond Basin 3: Basin 3

Inflow Area =	6.000 ac, 45.83% Impervious, Inflow D	Depth > 2.63" for 25 year event			
Inflow =	9.50 cfs @ 12.19 hrs, Volume=	1.313 af			
Outflow =	0.50 cfs @ 16.98 hrs, Volume=	0.823 af, Atten= 95%, Lag= 287.4 min			
Discarded =	0.30 cfs @ 6.65 hrs, Volume=	0.608 af			
Primary =	0.20 cfs @ 16.98 hrs, Volume=	0.215 af			
Routed to Pond Basin 1 : Basin 1					

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 74.82' @ 16.98 hrs Surf.Area= 0.349 ac Storage= 0.749 af

Plug-Flow detention time= 431.3 min calculated for 0.821 af (63% of inflow)	
Center-of-Mass det. time= 298.4 min ( 1,099.1 - 800.7 )	

Volume	Invert A	vail.Storag	e Stora	age Description
#1	72.00'	1.200 a	af Cus	stom Stage Data (Prismatic)Listed below x 1.2
Elevatio (fee			.Store e-feet)	Cum.Store (acre-feet)
72.0	0.150		0.000	0.000
73.0	0.200		0.175	0.175
74.(	0.250		0.225	0.400
75.0	0.300		0.275	0.675
76.0	0.350		0.325	1.000
<u>Device</u> #1 #2	Routing Discarded Primary	72.00'		evices Exfiltration when above 72.00' t. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#2 #3	Primary			<b>x 42.0" H Vert. Orifice/Grate</b> C= 0.600
			Limited t	to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 6.65 hrs HW=72.07' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.20 cfs @ 16.98 hrs HW=74.82' (Free Discharge) -2=Orifice/Grate (Orifice Controls 0.20 cfs @ 4.00 fps) -3=Orifice/Grate (Controls 0.00 cfs)

# Summary for Pond Rain Garden 1: Rain Garden 1

Inflow Area =	1.500 ac, 23.33% Impervious, Inflow [	Depth > 1.94" for 25 year event				
Inflow =	1.46 cfs @ 12.20 hrs, Volume=	0.242 af				
Outflow =	1.46 cfs @ 12.20 hrs, Volume=	0.242 af, Atten= 0%, Lag= 0.0 min				
Discarded =	0.00 cfs @ 12.20 hrs, Volume=	0.000 af				
Primary =	1.45 cfs @12.20 hrs, Volume=	0.242 af				
Routed to Pond Basin 2 Basin 2						

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 78.00' @ 12.20 hrs Surf.Area= 0.060 ac Storage= 0.000 af

Plug-Flow detention time= 0.0 min calculated for 0.242 af (100% of inflow) Center-of-Mass det. time= 0.0 min (843.3 - 843.3)

Volume	Invert A	vail.Storage	storag	e Description		
#1	78.00'	0.400 a	Custo	m Stage Data	(Prismation	<b>c)</b> Listed below (Recalc)
Elevatio	et) (acres)	(acre	Store feet)	Cum.Store (acre-feet)		
78.0			0.000	0.000		
79.0			0.070	0.070		
80.0	0.100	(	0.090	0.160		
81.0	0.120	(	).110	0.270		
82.0	0.140	(	).130	0.400		
Device	Routing	Invert C	outlet Dev	ices		
#1	Discarded	78.00' <b>0</b>	.30 cfs E	xfiltration whe	en above 7	/5.00'
#2	Primary	80.00' <b>3</b>	.0" Vert.	Orifice/Grate	C= 0.600	Limited to weir flow at low heads
#3	Primary			.0" Horiz. Orif weir flow at low		C= 0.600
Discoud		-0.00 -f- (				

Discarded OutFlow Max=0.30 cfs @ 12.20 hrs HW=78.00' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=301.47 cfs @ 12.20 hrs HW=78.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs)

-3=Orifice/Grate (Orifice Controls 301.47 cfs @ 21.53 fps)

# Summary for Pond Rain Garden 2: Rain Garden 2

Inflow Area =	2.000 ac, 17.50% Impe	ervious, Inflow Depth >	> 1.62" for 25 year event			
Inflow =	1.50 cfs @ 12.21 hrs,	Volume= 0.27	'0 af			
Outflow =	0.30 cfs @ 11.80 hrs,	Volume= 0.27	'0 af, Atten= 80%, Lag= 0.0 min			
Discarded =	0.30 cfs @ 11.80 hrs,	Volume= 0.27	'0 af			
Primary =	0.00 cfs @ 5.00 hrs,	Volume= 0.00	00 af			
Routed to Pond Basin 3 : Basin 3						

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs

Peak Elev= 75.99' @ 13.62 hrs Surf.Area= 0.065 ac Storage= 0.059 af

Plug-Flow detention time= 60.5 min calculated for 0.269 af (100% of inflow) Center-of-Mass det. time= 60.1 min ( 920.0 - 859.8 )

Volume	Invert	Avail.Storag	e Sto	orage Description
#1	75.00'	0.300 a	af Cus	ustom Stage Data (Prismatic)Listed below (Recalc)
Elevatio (fee 75.0 76.0 77.0 78.0 79.0	(acre           00         0.09           00         0.09           00         0.09           00         0.09           00         0.09           00         0.09           00         0.09           00         0.09	s) (acre 55 65 75 85	Store <u>-feet)</u> 0.000 0.060 0.070 0.080 0.090	Cum.Store (acre-feet) 0.000 0.060 0.130 0.210 0.300
Device #1 #2 #3	Routing Discarded Primary Primary	75.00' 77.00' 79.00'	).30 cfs 3.0" Vei 12.0" x	Devices fs Exfiltration when above 75.00' ert. Orifice/Grate C= 0.600 Limited to weir flow at low heads x 48.0" Horiz. Orifice/Grate C= 0.600 d to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 11.80 hrs HW=75.04' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=75.00' (Free Discharge)

**2=Orifice/Grate** (Controls 0.00 cfs)

-3=Orifice/Grate (Controls 0.00 cfs)

# Summary for Pond Rain Garden 3: Rain Garden 3

Inflow Area =	2.800 ac, 5	1.79% Impervious, Inflo	ow Depth > 3.49"	for 25 year event		
Inflow =	5.77 cfs @	12.19 hrs, Volume=	0.815 af	-		
Outflow =	0.30 cfs @	9.15 hrs, Volume=	0.589 af, Atte	en= 95%, Lag= 0.0 min		
Discarded =	0.30 cfs @	9.15 hrs, Volume=	0.589 af	-		
Primary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af			
Routed to Pond Basin 2 : Basin 2						

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 76.74' @ 17.36 hrs Surf.Area= 0.324 ac Storage= 0.411 af

Plug-Flow detention time= 397.3 min calculated for 0.589 af (72% of inflow) Center-of-Mass det. time= 280.6 min (1,086.6 - 806.0)

Volume	Invert	Avail.Storage	Storage Description
#1	75.00'	2.000 af	Custom Stage Data (Prismatic)Listed below (Recalc)

# Post Developed

Elevation

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Inc.Store

(fee	et) (acres	) (ad	re-feet)	(acre-feet)			
75.0	0.15	C	0.000	0.000			
76.0	0.25	C	0.200	0.200			
77.0	0.35 0.35	C	0.300	0.500			
78.0	0.45	C	0.400	0.900			
79.0	0.55	C	0.500	1.400			
80.0	0.65 0.65	C	0.600	2.000			
Device	Routing	Invert	Outlet D	evices			
#1	Discarded	75.00'	0.30 cfs	<b>Exfiltration whe</b>	en above 75.00'		
#2	Primary	77.00'	<b>3.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads				
#3	Primary	79.00'	42.0" x 48.0" Horiz. Orifice/Grate C= 0.600				

Cum.Store

Limited to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 9.15 hrs HW=75.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=75.00' (Free Discharge) **2=Orifice/Grate** (Controls 0.00 cfs)

-3=Orifice/Grate (Controls 0.00 cfs)

Surf.Area

# Summary for Pond Rain Garden 4: Rain Garden 4

Inflow Area =	1.000 ac, 40.00	)% Impervious, Inflow De	epth > 2.85" for 25	year event			
Inflow =	1.61 cfs @ 12.2	20 hrs, Volume=	0.237 af	-			
Outflow =	0.30 cfs @ 11.7	75 hrs, Volume=	0.237 af, Atten= 81%	6, Lag= 0.0 min			
Discarded =	0.30 cfs @ 11.7	75 hrs, Volume=	0.237 af	-			
Primary =	0.00 cfs @ 5.0	00 hrs, Volume=	0.000 af				
Routed to Pond Basin 2 Basin 2							

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 75.66' @ 13.23 hrs Surf.Area= 0.092 ac Storage= 0.058 af

Plug-Flow detention time= 57.1 min calculated for 0.237 af (100% of inflow) Center-of-Mass det. time= 56.6 min ( 873.1 - 816.5 )

Invert A	Avail.Storage	Storag	e Description	
75.00'	0.550 af	Custo	m Stage Data	(Prismatic)Listed below (Recalc)
			Cum.Store (acre-feet)	
0.085	5          0.0	00	0.000	
0.095	5 0.0	90	0.090	
0.105	5 0.1	00	0.190	
0.115	5 0.1	10	0.300	
0.125	5 0.1	20	0.420	
0.135	5	30	0.550	
	75.00' Surf.Area (acres) 0.085 0.095 0.105 0.115 0.125	75.00'         0.550 af           Surf.Area         Inc.Sto           (acres)         (acre-fe           0.085         0.0           0.095         0.0           0.105         0.1           0.115         0.1           0.125         0.1	75.00'         0.550 af         Custo           Surf.Area (acres)         Inc.Store (acre-feet)           0.085         0.000           0.095         0.090           0.105         0.100           0.115         0.110           0.125         0.120	75.00'         0.550 af         Custom Stage Data           Surf.Area (acres)         Inc.Store (acre-feet)         Cum.Store (acre-feet)           0.085         0.000         0.000           0.095         0.090         0.090           0.105         0.100         0.190           0.115         0.110         0.300           0.125         0.120         0.420

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Device	Routing	Invert	Outlet Devices
#1	Discarded	75.00'	0.30 cfs Exfiltration when above 75.00'
#2	Primary	77.00'	<b>3.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Primary	79.00'	42.0" x 48.0" Horiz. Grate C= 0.600
			Limited to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 11.75 hrs HW=75.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=75.00' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs) 3=Grate (Controls 0.00 cfs)

# Summary for Pond Rain Garden 5: Rain Garden 5

Inflow Area =	1.100 ac, 36.36% Impervious, Inflow D	Depth = 2.39" for 25 year event					
Inflow =	1.75 cfs @ 12.20 hrs, Volume=	0.219 af					
Outflow =	0.30 cfs @ 11.95 hrs, Volume=	0.219 af, Atten= 83%, Lag= 0.0 min					
Discarded =	0.30 cfs @ 11.95 hrs, Volume=	0.219 af					
Primary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af					
Routed to Pond Basin 2 : Basin 2							

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 73.73' @ 13.49 hrs Surf.Area= 0.092 ac Storage= 0.064 af

Plug-Flow detention time= 77.2 min calculated for 0.219 af (100% of inflow) Center-of-Mass det. time= 77.1 min (974.3 - 897.2)

Volume	Invert A	vail.Storage	Storage Description
#1	73.00'	0.550 af	Custom Stage Data (Prismatic)Listed below (Recalc)
Elevatio (fee		Inc.S (acre-	Store Cum.Store feet) (acre-feet)
73.0	0.085	0	.000 0.000
74.0	0.095	0	.090 0.090
75.0	0.105	0	.100 0.190
76.0	0.115	0	.110 0.300
77.0	0.125	0	.120 0.420
78.0	0.135	0	.130 0.550
Device	Routing	Invert O	utlet Devices
#1	Discarded		.30 cfs Exfiltration when above 73.00'
#2	Primary	•••••	<b>.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Primary		<b>2.0" x 48.0" Horiz. Grate</b> C= 0.600 mited to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 11.95 hrs HW=73.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=73.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs) -3=Grate (Controls 0.00 cfs)

# Summary for Link Site: Site

Inflow Area	a =	20.600 ac, 43	3.69% Impervious, I	nflow Depth = 0.00	)" for 25 year event
Inflow	=	0.00 cfs @	5.00 hrs, Volume=	0.000 af	
Primary	=	0.00 cfs @	5.00 hrs, Volume=	0.000 af, <i>I</i>	Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs

Post DevelopedNRCC 24-hr D100 year Rainfall=9.20"Prepared by Professional Design ServicesPrinted 6/19/2023HydroCAD® 10.20-3c s/n 02223 © 2023 HydroCAD Software Solutions LLCPage 48							
Time span=5.00-30.00 hrs, dt=0.05 hrs, 501 points Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN Reach routing by Stor-Ind+Trans method . Pond routing by Stor-Ind method							
SubcatchmentBasin 1 Imp: Basin 1 Imp Runoff Area=0.900 ac 100.00% Impervious Runoff Depth>8.44" Tc=10.0 min CN=98 Runoff=4.84 cfs 0.633 af							
Subcatchment Basin 1 Pervious: Basin 1 - Runoff Area=0.500 ac 0.00% Impervious Runoff Depth=1.70" Tc=15.0 min CN=39 Runoff=0.35 cfs 0.071 af							
Subcatchment Basin 2 - Pervious: Basin 2 - Runoff Area=4.050 ac 0.00% Impervious Runoff Depth=1.70" Tc=15.0 min CN=39 Runoff=2.83 cfs 0.573 af							
Subcatchment Basin 2 Impervious: basin Runoff Area=2.750 ac 100.00% Impervious Runoff Depth>8.44" Tc=10.0 min CN=98 Runoff=14.79 cfs 1.934 af							
Subcatchment Basin 3 Impervious: basin Runoff Area=2.400 ac 100.00% Impervious Runoff Depth>8.44" Tc=10.0 min CN=98 Runoff=12.90 cfs 1.688 af							
Subcatchment Basin 3 Pervious: Basin 3 - Runoff Area=1.600 ac 0.00% Impervious Runoff Depth=1.70" Tc=15.0 min CN=39 Runoff=1.12 cfs 0.226 af							
SubcatchmentRain Garden 1 Impervious: Runoff Area=0.350 ac 100.00% Impervious Runoff Depth>8.44" Tc=10.0 min CN=98 Runoff=1.88 cfs 0.246 af							
Subcatchment Rain Garden 1 Pervious: Rain Runoff Area=1.150 ac 0.00% Impervious Runoff Depth=1.70" Tc=15.0 min CN=39 Runoff=0.80 cfs 0.163 af							
Subcatchment Rain Garden 2 Impervious: Runoff Area=0.350 ac 100.00% Impervious Runoff Depth>8.44" Tc=10.0 min CN=98 Runoff=1.88 cfs 0.246 af							
Subcatchment Rain Garden 2 Pervious: Rain Runoff Area=1.650 ac 0.00% Impervious Runoff Depth=1.70" Tc=15.0 min CN=39 Runoff=1.15 cfs 0.233 af							
Subcatchment Rain Garden 3 Impervious: Runoff Area=1.450 ac 100.00% Impervious Runoff Depth>8.44" Tc=10.0 min CN=98 Runoff=7.80 cfs 1.020 af							
Subcatchment Rain Garden 3 Pervious: Rain Runoff Area=1.350 ac 0.00% Impervious Runoff Depth=1.70" Tc=15.0 min CN=39 Runoff=0.94 cfs 0.191 af							
Subcatchment Rain Garden 4 Impervious: Runoff Area=0.400 ac 100.00% Impervious Runoff Depth>8.44" Tc=10.0 min CN=98 Runoff=2.15 cfs 0.281 af							
Subcatchment Rain Garden 4 Pervious: Rain Runoff Area=0.600 ac 0.00% Impervious Runoff Depth=1.70" Tc=15.0 min CN=39 Runoff=0.42 cfs 0.085 af							
Subcatchment RG 5: Rain Garden 5 Runoff Area=1.100 ac 36.36% Impervious Runoff Depth=4.26" Tc=10.0 min CN=60 Runoff=3.22 cfs 0.390 af							
Pond Basin 1: Basin 1Peak Elev=74.17' Storage=0.200 af Inflow=5.20 cfs 1.459 af Discarded=0.20 cfs 0.407 af Primary=4.25 cfs 0.984 af Outflow=4.45 cfs 1.391 af							

Post Developed Prepared by Professiona HydroCAD® 10.20-3c s/n 02		<u>D Softwa</u>			4-hr D	Post Dev 100 year Rainfa Printed 6	all=9.20"
Pond Basin 2: Basin 2	Discarded=1.00 cfs 1			•		Inflow=20.16 cfs Outflow=1.30 cfs	
Pond Basin 3: Basin 3	Discarded=0.30 cfs 0			•		Inflow=13.82 cfs Outflow=2.58 cfs	
Pond Rain Garden 1: Rai	<b>Garden 1</b> Discarded=0.00 cfs 0					f Inflow=2.57 cfs Outflow=2.57 cfs	
Pond Rain Garden 2: Rai	<b>Garden 2</b> Discarded=0.30 cfs 0			•		f Inflow=2.89 cfs Outflow=0.42 cfs	
Pond Rain Garden 3: Rai	<b>Garden 3</b> Discarded=0.30 cfs 0					f Inflow=8.57 cfs Outflow=0.44 cfs	
Pond Rain Garden 4: Rai	<b>Garden 4</b> Discarded=0.30 cfs 0					f Inflow=2.50 cfs Outflow=0.30 cfs	
Pond Rain Garden 5: Rai	<b>Garden 5</b> Discarded=0.30 cfs 0					f Inflow=3.22 cfs Outflow=0.30 cfs	
Link Site: Site						Inflow=0.30 cfs Primary=0.30 cfs	
Total Runof	f Area = 20.600 ac 56.31		Volume = ⁄ious = 11			age Runoff Dep 9% Impervious =	

# Summary for Subcatchment Basin 1 Imp: Basin 1 Imp

Runoff = 4.84 cfs @ 12.19 hrs, Volume= 0.633 af, Depth> 8.44" Routed to Pond Basin 1 : Basin 1

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100 year Rainfall=9.20"

	Area	(ac)	CN	Desc	cription		
*	0.	500	98	Pave	ement		
*	0.	400	98	Root	F		
	0.	900	98	Weig	ghted Aver	age	
	0.900 100.00% Impervious Area						l de la construcción de la constru
	Тс	Leng	th	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	10.0						Direct Entry, pavement and pipe

# Summary for Subcatchment Basin 1 Pervious: Basin 1 - Pervious

Runoff = 0.35 cfs @ 12.31 hrs, Volume= Routed to Pond Basin 1 : Basin 1

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100 year Rainfall=9.20"

_	Area	(ac)	CN	Desc	cription		
*	0.	500	39	lawn	, A soils		
	0.	500		100.	00% Pervi	ous Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0						Direct Entry,

### Summary for Subcatchment Basin 2 - Pervious: Basin 2 - Pervious

Runoff = 2.83 cfs @ 12.31 hrs, Volume= Routed to Pond Basin 2 : Basin 2 0.573 af, Depth= 1.70"

0.071 af, Depth= 1.70"

	Area (ac)	CN	Description
*	4.050	39	lawn, A soils
	4.050		100.00% Pervious Area

	evelope					NRCC 24-hr D	0 100 year Rainfall=9.20"					
	d by Prof						Printed 6/19/2023					
HydroCA	D® 10.20-3	c s/n 02	<u>223 © 202</u>	<u>3 HydroCAE</u>	) Software Solu	itions LLC	Page 51					
Тс	Length	Slope	Velocity	Capacity	Description							
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)								
15.0					Direct Entry	/,						
	Summary for Subcatchment Basin 2 Impervious: basin 2 Impervious											
Runoff Route	Runoff = 14.79 cfs @ 12.19 hrs, Volume= 1.934 af, Depth> 8.44" Routed to Pond Basin 2 : Basin 2											
	y SCS TR 4-hr D 10				Veighted-CN,	Time Span= 5.00	-30.00 hrs, dt= 0.05 hrs					
Area	(ac) CN	Desc	cription									
* 0.	.600 98	8 Park	ing									
* 0.	.450 98	B Roof										
* 0.	.700 98	3 Drive	eways									
<u>* 1</u> .	.000 98	B Road	d & Sidewa	alk								
2	.750 98	3 Weig	ghted Aver	age								
2	.750	100.	00% Impe	rvious Area	1							
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description							
10.0		(11/11)		(015)	Direct Entr	, pavement						
10.0						, pavement						
	Summary for Subcatchment Basin 3 Impervious: basin 3 Impervious											

12.90 cfs @ 12.19 hrs, Volume= 1.688 af, Depth> 8.44" Runoff = Routed to Pond Basin 3 : Basin 3

Post Developed.

	Area	(ac)	CN	Desc	ription					
*	0.	900	98	Park	arking					
*	0.	300	98	Roof						
*	0.	500	98	Drive	eways					
*	0.	700	98	Road	& Sidewa	alk				
	2.	400	98	Weig	hted Aver	age				
	2.	2.400 100.00% Impervious Area				rvious Area				
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	10.0						Direct Entry, pavement			

# Summary for Subcatchment Basin 3 Pervious: Basin 3 - Pervious

1.12 cfs @ 12.31 hrs, Volume= 0.226 af, Depth= 1.70" Runoff = Routed to Pond Basin 3 : Basin 3

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100 year Rainfall=9.20"

_	Area	(ac)	CN	Desc	cription		
*	1.	600	39	lawn	, A soils		
	1.	600		100.	00% Pervi	ous Area	
	Tc (min)	Lengt (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0						Direct Entry,

# Summary for Subcatchment Rain Garden 1 Impervious: Rain Garden 1 Impervious

0.246 af, Depth> 8.44"

Runoff	=	1.88 cfs @	12.19 hrs,	Volume=
Routed	to Pond	Rain Garder	n 1 : Rain G	arden 1

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100 year Rainfall=9.20"

Ar	ea (ac)	CN	Desc	cription						
*	0.350	98	Root	-						
	0.350		100.	00% Impe	rvious Area	l				
- (mi	ີc Len າ) (fe	gth eet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
10	0					Direct Entry	y, pavement and pipe			
	Summ	ary fo	or Sul	ocatchm	ent Rain	Garden 1 F	Pervious: Rain Garden 1 Pervious			
	Runoff = 0.80 cfs @ 12.31 hrs, Volume= 0.163 af, Depth= 1.70" Routed to Pond Rain Garden 1 : Rain Garden 1									
	Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs									

NRCC 24-hr D 100 year Rainfall=9.20"

	Area	(ac)	CN	Desc	cription		
*	1.	150	39	lawn	, A soils		
	1.	150		100.	00% Pervi	ous Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	15.0	(100	-,	(	(12,000)	(0.0)	Direct Entry,

# Summary for Subcatchment Rain Garden 2 Impervious: Rain Garden 2 Impervious

Runoff	=	1.88 cfs @	12.19 hrs,	Volume=	0.246 af,	Depth>	8.44"
Routed	to Pond	l Rain Garder	n 2 : Rain G	arden 2		•	

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100 year Rainfall=9.20"

	Area	(ac)	CN	Desc	cription		
*	0.	350	98	Root	•		
	0.350 100.00% Impervious Area						1
	Tc (min)	Lengt (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	10.0						Direct Entry, pavement and pipe

# Summary for Subcatchment Rain Garden 2 Pervious: Rain Garden 2 Pervious

Runoff	=	1.15 cfs @	12.31 hrs,	Volume=	0.233 af,	Depth= 1.70"
Routed	to Pond	Rain Garde	n 2 : Rain G	arden 2		-

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100 year Rainfall=9.20"

	Area	(ac)	CN	Desc	cription		
*	1.	650	39	lawn	, A soils		
	1.	650		100.	00% Pervi	ous Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0						Direct Entry,

### Summary for Subcatchment Rain Garden 3 Impervious: Rain Garden 3 Impervious

Runoff = 7.80 cfs @ 12.19 hrs, Volume= 1.020 af, Depth> 8.44" Routed to Pond Rain Garden 3 : Rain Garden 3

	Area (ac)	CN	Description
*	0.450	98	Pavement
*	0.600	98	Roof
*	0.400	98	Driveway
	1.450	98	Weighted Average
	1.450		100.00% Impervious Area

Post DevelopedPost DevelopePrepared by Professional Design ServicesNRCC 24-hr D100 year Rainfall=9.2HydroCAD® 10.20-3c s/n 02223 © 2023 HydroCAD Software Solutions LLCPrinted 6/19/20	0" 23
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)	
10.0 Direct Entry, pavement and pipe	
Summary for Subcatchment Rain Garden 3 Pervious: Rain Garden 3 Pervious	
Runoff = 0.94 cfs @ 12.31 hrs, Volume= 0.191 af, Depth= 1.70" Routed to Pond Rain Garden 3 : Rain Garden 3	
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100 year Rainfall=9.20"	
Area (ac) CN Description	
* 1.350 39 lawn, A soils	_
1.350 100.00% Pervious Area	
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)	
15.0 Direct Entry,	
Summary for Subcatchment Rain Garden 4 Impervious: Rain Garden 4 Imperviou	IS
Runoff = 2.15 cfs @ 12.19 hrs, Volume= 0.281 af, Depth> 8.44" Routed to Pond Rain Garden 4 : Rain Garden 4	
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100 year Rainfall=9.20"	
Area (ac) CN Description	
* 0.400 98 Roof	
0.400 100.00% Impervious Area	
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)	
10.0 Direct Entry, pavement and pipe	
Summary for Subcatchment Rain Garden 4 Pervious: Rain Garden 4 Pervious	
Runoff = 0.42 cfs @ 12.31 hrs, Volume= 0.085 af, Depth= 1.70" Routed to Pond Rain Garden 4 : Rain Garden 4	
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100 year Rainfall=9.20"	
Area (ac) CN Description	
* 0.600 39 lawn, A soils	

			,	
0.600 100.00% Pervious Area	0.600	100.	00% Pervious Area	

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Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)							
15.0 Direct Entry,	15.0 Direct Entry,						
Summary for Subcatchment RG 5: Rain Garden 5	Summary for Subcatchment RG 5: Rain Garden 5						
Runoff = 3.22 cfs @ 12.20 hrs, Volume= 0.390 af, Depth= 4.26" Routed to Pond Rain Garden 5 : Rain Garden 5							
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hr NRCC 24-hr D 100 year Rainfall=9.20"	rs, dt= 0.05 hrs						
Area (ac) CN Description							
* 0.400 98 Roof * 0.700 39 Lawn A soils							
1.100         60         Weighted Average           0.700         63.64% Pervious Area           0.400         36.36% Impervious Area							
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)							
10.0 Direct Entry, pavement and pipe							
Summary for Pond Basin 1: Basin 1							
Inflow Area =7.400 ac, 49.32% Impervious, Inflow Depth > $2.37"$ for 100 year eventInflow = $5.20 \text{ cfs} @$ $12.20 \text{ hrs}$ , Volume= $1.459 \text{ af}$ Outflow = $4.45 \text{ cfs} @$ $12.39 \text{ hrs}$ , Volume= $1.391 \text{ af}$ , Atten= 14%, Lag= 11.7 minDiscourded = $0.20 \text{ cfs} @$ $7.20 \text{ hrs}$ , Volume= $0.407 \text{ cf}$							

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NRCC 24-hr D 100 year Rainfall=9.20"

 Discarded =
 0.20 cfs @
 7.30 hrs, Volume=
 0.407 af

 Primary =
 4.25 cfs @
 12.39 hrs, Volume=
 0.984 af

 Routed to Pond Basin 2 : Basin 2
 0.984 af
 0.984 af

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Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 74.17' @ 12.39 hrs Surf.Area= 0.070 ac Storage= 0.200 af

Plug-Flow detention time= 109.4 min calculated for 1.388 af (95% of inflow) Center-of-Mass det. time= 75.0 min ( 990.5 - 915.5 )

Volume	Invert	Avail.Storage	Stor	rage Description	
#1	70.00'	0.200 af	rete	ention basin (Pr	ismatic)Listed below
Elevation (feet)	Surf.Are (acres			Cum.Store (acre-feet)	
70.00	0.03	0.0	000	0.000	
71.00	0.04	0.0	)35	0.035	
72.00	0.05	0.0	)45	0.080	
73.00	0.06	0.0	)55	0.135	
74.00	0.07	0.0	065	0.200	

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Device	Routing	Invert	Outlet Devices
#1	Discarded	70.00'	0.20 cfs Exfiltration when above 70.00'
#2	Primary	72.00'	<b>4.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Primary	74.00'	<b>48.0" x 48.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Discarded OutFlow** Max=0.20 cfs @ 7.30 hrs HW=70.04' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.20 cfs)

Primary OutFlow Max=4.06 cfs @ 12.39 hrs HW=74.16' (Free Discharge) 2=Orifice/Grate (Orifice Controls 0.59 cfs @ 6.80 fps) 3=Orifice/Grate (Weir Controls 3.47 cfs @ 1.32 fps)

### Summary for Pond Basin 2: Basin 2

Inflow Area =	20.600 ac, 4	3.69% Impervious,	, Inflow Depth > 2.35" for 100 year event
Inflow =	20.16 cfs @	12.21 hrs, Volume	e= 4.036 af
Outflow =	1.30 cfs @	22.54 hrs, Volume	e= 2.324 af, Atten= 94%, Lag= 620.2 min
Discarded =	1.00 cfs @	9.65 hrs, Volume	e= 1.937 af
Primary =	0.30 cfs @	22.54 hrs, Volume	e= 0.387 af
Routed to Link	Site : Site		

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 72.46' @ 22.54 hrs Surf.Area= 0.776 ac Storage= 2.281 af

Plug-Flow detention time= 418.2 min calculated for 2.318 af (57% of inflow) Center-of-Mass det. time= 256.3 min (1,128.3 - 872.0)

Volume	Invert	Avail.Storage	e Stora	ge Description	
#1	68.00'	3.600 a	f Custo	om Stage Data	(Prismatic)Listed below x 1.2
Elevatio (fee 68.0	et) (acres	s) (acre	Store feet) ).000	Cum.Store (acre-feet) 0.000	
69.0		-	).000 ).250	0.000	
70.0		-	).350	0.600	
71.0	0.50	0 0	).450	1.050	
72.0	0.60 0.60	0 0	).550	1.600	
73.0	0.70	0 0	).650	2.250	
74.0	0.80 0.80	0 (	).750	3.000	
Device #1 #2 #3	Routing Discarded Primary Primary	68.00' 1 70.70' 3 73.00' 4	.0" Vert. 2.0" W x	Exfiltration whe Orifice/Grate	en above 68.00' C= 0.600 Limited to weir flow at low heads Drifice/Grate C= 0.600

**Discarded OutFlow** Max=1.00 cfs @ 9.65 hrs HW=68.09' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 1.00 cfs)

Primary OutFlow Max=0.30 cfs @ 22.54 hrs HW=72.46' (Free Discharge) -2=Orifice/Grate (Orifice Controls 0.30 cfs @ 6.16 fps) -3=Orifice/Grate (Controls 0.00 cfs)

### Summary for Pond Basin 3: Basin 3

Inflow Area =	6.000 ac, 4	5.83% Impervious, Inflo	ow Depth > 3.89" for 100 year event	
Inflow =	13.82 cfs @	12.20 hrs, Volume=	1.947 af	
Outflow =	2.58 cfs @	13.17 hrs, Volume=	1.369 af, Atten= 81%, Lag= 58.5 m	nin
Discarded =	0.30 cfs @	5.70 hrs, Volume=	0.614 af	
Primary =	2.28 cfs @	13.17 hrs, Volume=	0.755 af	
Routed to Pon	d Basin 1 : Ba	sin 1		

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 75.32' @ 13.17 hrs Surf.Area= 0.379 ac Storage= 0.934 af

Plug-Flow detention time= 350.1 min calculated for 1.368 af (70% of inflow) Center-of-Mass det. time= 231.3 min (1,038.0 - 806.7)

Volume	Invert	Avail.Storage	Storage	Description	
#1	72.00'	1.200 af	Custom	Stage Data	(Prismatic)Listed below x 1.2
Elevatio (fee				Cum.Store (acre-feet)	
72.0	0.150	0 C	.000	0.000	
73.0	0.200	0 C	.175	0.175	
74.0	0.250	0 C	.225	0.400	
75.0	0.300	0 C	.275	0.675	
76.0	0.350	0 C	.325	1.000	
Device	Routing	Invert O	utlet Device	es	
#1	Discarded	72.00' <b>0</b> .	30 cfs Exfi	iltration whe	en above 72.00'
#2	Primary	74.00' <b>3</b> .	0" Vert. Or	rifice/Grate	C= 0.600 Limited to weir flow at low heads
#3	Primary		-	2.0" H Vert. ( eir flow at lov	<b>Orifice/Grate</b> C= 0.600 w heads

**Discarded OutFlow** Max=0.30 cfs @ 5.70 hrs HW=72.07' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=2.28 cfs @ 13.17 hrs HW=75.32' (Free Discharge) 2=Orifice/Grate (Orifice Controls 0.26 cfs @ 5.26 fps) 2=Orifice/Grate (Orifice Controls 2.02 cfs @ 1.81 fps)

-3=Orifice/Grate (Orifice Controls 2.02 cfs @ 1.81 fps)

# Summary for Pond Rain Garden 1: Rain Garden 1

Inflow Area = 1.500 ac, 23.33% Impervious, Inflow Depth > 3.27" for 100 year event Inflow 2.57 cfs @ 12.22 hrs, Volume= = 0.409 af 2.57 cfs @ 12.22 hrs, Volume= 0.409 af, Atten= 0%, Lag= 0.0 min Outflow = Discarded = 0.00 cfs @ 12.22 hrs, Volume= 0.000 af Primary = 2.57 cfs @ 12.22 hrs, Volume= 0.409 af Routed to Pond Basin 2 : Basin 2

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 78.00' @ 12.22 hrs Surf.Area= 0.060 ac Storage= 0.000 af

Plug-Flow detention time= 0.0 min calculated for 0.408 af (100% of inflow) Center-of-Mass det. time= 0.0 min (852.5 - 852.5)

#3 Primary 58.00' 42.0" x 48.0" Horiz. Orifice/Grate C= 0.600	Volume	Invert A	vail.Storage	e Storage Description
(feet)         (acres)         (acre-feet)         (acre-feet)           78.00         0.060         0.000         0.000           79.00         0.080         0.070         0.070           80.00         0.100         0.090         0.160           81.00         0.120         0.110         0.270           82.00         0.140         0.130         0.400           Device         Routing         Invert         Outlet Devices           #1         Discarded         78.00'         0.30 cfs Exfiltration when above 75.00'           #2         Primary         80.00'         3.0" Vert. Orifice/Grate         C= 0.600           #3         Primary         58.00'         42.0" x 48.0" Horiz. Orifice/Grate         C= 0.600	#1	78.00'	0.400 af	f Custom Stage Data (Prismatic)Listed below (Recalc)
DeviceRoutingInvertOutlet Devices#1Discarded78.00'0.30 cfs Exfiltration when above 75.00'#2Primary80.00'3.0" Vert. Orifice/GrateC= 0.600#3Primary58.00'42.0" x 48.0" Horiz. Orifice/GrateC= 0.600	(fee 78.0 79.0 80.0	t) (acres) 00 0.060 00 0.080 00 0.100	(acre-f 0.0. 0.0. 0.0.	efeet)         (acre-feet)           0.000         0.000           0.070         0.070           0.090         0.160
#1Discarded78.00'0.30 cfs Exfiltration when above 75.00'#2Primary80.00'3.0" Vert. Orifice/GrateC= 0.600Limited to weir flow at low head#3Primary58.00'42.0" x 48.0" Horiz. Orifice/GrateC= 0.600	82.0	00 0.140	0.	0.130 0.400
#2Primary80.00'3.0" Vert. Orifice/GrateC= 0.600Limited to weir flow at low head#3Primary58.00'42.0" x 48.0" Horiz. Orifice/GrateC= 0.600	Device	Routing	Invert O	Outlet Devices
Limited to well flow at low heads	#2 Primary		80.00' <b>3.</b> 58.00' <b>42</b>	.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads

Discarded OutFlow Max=0.30 cfs @ 12.22 hrs HW=78.00' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=301.47 cfs @ 12.22 hrs HW=78.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs) -3=Orifice/Grate (Orifice Controls 301.47 cfs @ 21.53 fps)

Summary for Pond Rain Garden 2: Rain Garden 2

#### 2.000 ac, 17.50% Impervious, Inflow Depth > 2.88" for 100 year event Inflow Area = Inflow = 2.89 cfs @ 12.22 hrs, Volume= 0.480 af Outflow = 0.42 cfs @ 14.38 hrs, Volume= 0.480 af, Atten= 86%, Lag= 129.6 min Discarded = 0.30 cfs @ 11.50 hrs, Volume= 0.447 af 0.12 cfs @ 14.38 hrs, Volume= 0.033 af Primary = Routed to Pond Basin 3 : Basin 3

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs

Peak Elev= 77.38' @ 14.38 hrs Surf.Area= 0.079 ac Storage= 0.159 af

Plug-Flow detention time= 200.6 min calculated for 0.479 af (100% of inflow) Center-of-Mass det. time= 200.2 min (1,067.7 - 867.5)

Volume	Invert	Avail.Storage	e Storage Description
#1	75.00'	0.300 a	f Custom Stage Data (Prismatic)Listed below (Recalc)
Elevatio (fee 75.0 76.0 77.0 78.0 79.0	et) (acres 00 0.05 00 0.06 00 0.07 00 0.08	5 (acre- 5 ( 5 ( 5 ( 5 ( 5 (	Store         Cum.Store           -feet)         (acre-feet)           0.000         0.000           0.060         0.060           0.070         0.130           0.080         0.210           0.090         0.300
Device #1 #2 #3	Routing Discarded Primary Primary	75.00' <b>0</b> 77.00' <b>3</b> 79.00' <b>4</b>	Dutlet Devices         0.30 cfs Exfiltration when above 75.00'         8.0" Vert. Orifice/Grate       C= 0.600         Limited to weir flow at low heads         2.0" x 48.0" Horiz. Orifice/Grate       C= 0.600         Limited to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 11.50 hrs HW=75.04' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

**Primary OutFlow** Max=0.12 cfs @ 14.38 hrs HW=77.38' (Free Discharge)

2=Orifice/Grate (Orifice Controls 0.12 cfs @ 2.41 fps)

**3=Orifice/Grate** (Controls 0.00 cfs)

# Summary for Pond Rain Garden 3: Rain Garden 3

Inflow Area =	2.800 ac, 51.79% Impervious, Inflow De	epth > 5.19" for 100 year event
Inflow =	8.57 cfs @ 12.20 hrs, Volume=	1.211 af
Outflow =	0.44 cfs @ 17.59 hrs, Volume=	0.743 af, Atten= 95%, Lag= 323.7 min
Discarded =	0.30 cfs @ 7.15 hrs, Volume=	0.608 af
Primary =	0.14 cfs @ 17.59 hrs, Volume=	0.136 af
Routed to Pond	l Basin 2 : Basin 2	

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 77.48' @ 17.59 hrs Surf.Area= 0.398 ac Storage= 0.678 af

Plug-Flow detention time= 412.1 min calculated for 0.742 af (61% of inflow) Center-of-Mass det. time= 274.3 min (1,086.1 - 811.8)

Volume	Invert	Avail.Storage	Storage Description
#1	75.00'	2.000 af	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevatio (fee		ırf.Area (acres)		c.Store re-feet)	Cum.Store (acre-feet)	
75.0	00	0.150		0.000	0.000	
76.0	00	0.250		0.200	0.200	
77.0	00	0.350		0.300	0.500	
78.0	00	0.450		0.400	0.900	
79.0	00	0.550		0.500	1.400	
80.0	00	0.650		0.600	2.000	
Device	Routing		Invert	Outlet D	Devices	
#1	Discarde		75 00'	0 30 cf	Exfiltration w	hon abovo 75 00'

75.00' 0.30 cfs Exfiltration when above 75.00' #1 Discarded 77.00' **3.0" Vert. Orifice/Grate** C= 0.600 Limited to weir flow at low heads 79.00' **42.0" x 48.0" Horiz. Orifice/Grate** C= 0.600 #2 Primary #3 Primary Limited to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 7.15 hrs HW=75.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.14 cfs @ 17.59 hrs HW=77.48' (Free Discharge) -2=Orifice/Grate (Orifice Controls 0.14 cfs @ 2.85 fps) -3=Orifice/Grate (Controls 0.00 cfs)

# Summary for Pond Rain Garden 4: Rain Garden 4

Inflow Area =	1.000 ac, 40.00% Impervious, Inflow D	Depth > 4.40" for 100 year event
Inflow =	2.50 cfs @ 12.20 hrs, Volume=	0.366 af
Outflow =	0.30 cfs @ 11.40 hrs, Volume=	0.366 af, Atten= 88%, Lag= 0.0 min
Discarded =	0.30 cfs @ 11.40 hrs, Volume=	0.366 af
Primary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af
Routed to Pond	d Basin 2 : Basin 2	

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 76.31' @ 14.02 hrs Surf.Area= 0.098 ac Storage= 0.120 af

Plug-Flow detention time= 142.5 min calculated for 0.365 af (100% of inflow) Center-of-Mass det. time= 141.8 min (966.1 - 824.3)

Volume	Invert Av	vail.Storage	Storage Description	
#1	75.00'	0.550 af	Custom Stage Data (Prismatic)Listed below (Recalc)	
Elevation (feet)	Surf.Area (acres)	Inc.Sto (acre-fee		
75.00 76.00	0.085 0.095	0.09	000 0.000 090 0.090	
77.00 78.00	0.105 0.115	0.1	100         0.190           110         0.300	
79.00 80.00	0.125 0.135	-	120         0.420           130         0.550	

		Post Developed.
Post Developed NRC	C 24-hr D	100 year Rainfall=9.20"
Prepared by Professional Design Services		Printed 6/19/2023
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Device	Routing	Invert	Outlet Devices
#1	Discarded	75.00'	0.30 cfs Exfiltration when above 75.00'
#2	Primary	77.00'	<b>3.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Primary	79.00'	<b>42.0" x 48.0" Horiz. Grate</b> C= 0.600 Limited to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 11.40 hrs HW=75.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=75.00' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs) 3=Grate (Controls 0.00 cfs)

# Summary for Pond Rain Garden 5: Rain Garden 5

Inflow Area =	1.100 ac, 36.36% Impervious, Inflow I	Depth = 4.26" for 100 year event
Inflow =	3.22 cfs @ 12.20 hrs, Volume=	0.390 af
Outflow =	0.30 cfs @ 11.55 hrs, Volume=	0.390 af, Atten= 91%, Lag= 0.0 min
Discarded =	0.30 cfs @11.55 hrs, Volume=	0.390 af
Primary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af
Routed to Pond	d Basin 2 : Basin 2	

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 74.70' @ 14.76 hrs Surf.Area= 0.102 ac Storage= 0.159 af

Plug-Flow detention time= 234.2 min calculated for 0.390 af (100% of inflow) Center-of-Mass det. time= 234.1 min (1,109.6 - 875.5)

Volume	Invert	Avail.Storag	e Sto	brage Description
#1	73.00'	0.550	af Cus	stom Stage Data (Prismatic)Listed below (Recalc)
Elevatio (fee			.Store e-feet)	Cum.Store (acre-feet)
73.0	0.08	5	0.000	0.000
74.0	0.09	5	0.090	0.090
75.0	0.10	5	0.100	0.190
76.0	0.11	5	0.110	0.300
77.0	0.12	5	0.120	0.420
78.0	0.13	5	0.130	0.550
Device #1	Routing Discarded	73.00'	0.30 cfs	Devices s Exfiltration when above 73.00'
#2 #3	Primary Primary	77.00'	42.0" x	ert. Orifice/Grate C= 0.600 Limited to weir flow at low heads <b>48.0" Horiz. Grate</b> C= 0.600 I to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 11.55 hrs HW=73.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=73.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs) -3=Grate (Controls 0.00 cfs)

# Summary for Link Site: Site

Inflow Area	a =	20.600 ac, 4	3.69% Impe	ervious,	Inflow De	epth >	0.23'	' for 10	0 year event
Inflow	=	0.30 cfs @	22.54 hrs,	Volume	=	0.387	af		
Primary	=	0.30 cfs @	22.54 hrs,	Volume	=	0.387	af, A	tten= 0%	,Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs

Post DevelopedPost Developed.Post DevelopedNRCC 24-hr DWQ storm Rainfall=1.25"Prepared by Professional Design ServicesPrinted 6/19/2023HydroCAD® 10.20-3c s/n 02223 © 2023 HydroCAD Software Solutions LLCPage 63
Time span=5.00-30.00 hrs, dt=0.05 hrs, 501 points Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method
Subcatchment Basin 1 Imp: Basin 1 Imp Runoff Area=0.900 ac 100.00% Impervious Runoff Depth>1.02" Tc=10.0 min CN=98 Runoff=0.61 cfs 0.077 af
SubcatchmentBasin 1 Pervious: Basin 1 - Runoff Area=0.500 ac 0.00% Impervious Runoff Depth=0.00" Tc=15.0 min CN=39 Runoff=0.00 cfs 0.000 af
Subcatchment Basin 2 - Pervious: Basin 2 - Runoff Area=4.050 ac 0.00% Impervious Runoff Depth=0.00" Tc=15.0 min CN=39 Runoff=0.00 cfs 0.000 af
Subcatchment Basin 2 Impervious: basin Runoff Area=2.750 ac 100.00% Impervious Runoff Depth>1.02" Tc=10.0 min CN=98 Runoff=1.87 cfs 0.234 af
Subcatchment Basin 3 Impervious: basin Runoff Area=2.400 ac 100.00% Impervious Runoff Depth>1.02" Tc=10.0 min CN=98 Runoff=1.63 cfs 0.204 af
Subcatchment Basin 3 Pervious: Basin 3 - Runoff Area=1.600 ac 0.00% Impervious Runoff Depth=0.00" Tc=15.0 min CN=39 Runoff=0.00 cfs 0.000 af
Subcatchment Rain Garden 1 Impervious: Runoff Area=0.350 ac 100.00% Impervious Runoff Depth>1.02" Tc=10.0 min CN=98 Runoff=0.24 cfs 0.030 af
Subcatchment Rain Garden 1 Pervious: Rain Runoff Area=1.150 ac 0.00% Impervious Runoff Depth=0.00" Tc=15.0 min CN=39 Runoff=0.00 cfs 0.000 af
Subcatchment Rain Garden 2 Impervious: Runoff Area=0.350 ac 100.00% Impervious Runoff Depth>1.02" Tc=10.0 min CN=98 Runoff=0.24 cfs 0.030 af
Subcatchment Rain Garden 2 Pervious: Rain Runoff Area=1.650 ac 0.00% Impervious Runoff Depth=0.00" Tc=15.0 min CN=39 Runoff=0.00 cfs 0.000 af
Subcatchment Rain Garden 3 Impervious: Runoff Area=1.450 ac 100.00% Impervious Runoff Depth>1.02" Tc=10.0 min CN=98 Runoff=0.99 cfs 0.124 af
Subcatchment Rain Garden 3 Pervious: Rain Runoff Area=1.350 ac 0.00% Impervious Runoff Depth=0.00" Tc=15.0 min CN=39 Runoff=0.00 cfs 0.000 af
Subcatchment Rain Garden 4 Impervious: Runoff Area=0.400 ac 100.00% Impervious Runoff Depth>1.02" Tc=10.0 min CN=98 Runoff=0.27 cfs 0.034 af
Subcatchment Rain Garden 4 Pervious: Rain Runoff Area=0.600 ac 0.00% Impervious Runoff Depth=0.00" Tc=15.0 min CN=39 Runoff=0.00 cfs 0.000 af
Subcatchment RG 5: Rain Garden 5 Runoff Area=1.100 ac 36.36% Impervious Runoff Depth=0.00" Tc=10.0 min CN=60 Runoff=0.00 cfs 0.000 af
Pond Basin 1: Basin 1Peak Elev=70.37'Storage=0.013 afInflow=0.61 cfs0.077 afDiscarded=0.20 cfs0.077 afPrimary=0.00 cfs0.000 afOutflow=0.20 cfs0.077 af

<b>Post Developed</b> Prepared by Professional <u>HydroCAD® 10.20-3c s/n 022</u>		Post Developed. WQ storm Rainfall=1.25" Printed 6/19/2023 Page 64
Pond Basin 2: Basin 2	•	2 af Inflow=2.11 cfs 0.264 af af Outflow=1.00 cfs 0.264 af
Pond Basin 3: Basin 3		2 af Inflow=1.63 cfs 0.204 af af Outflow=0.30 cfs 0.204 af
Pond Rain Garden 1: Rain		) af Inflow=0.24 cfs 0.030 af af Outflow=0.24 cfs 0.030 af
Pond Rain Garden 2: Rain		2 af Inflow=0.24 cfs 0.030 af af Outflow=0.21 cfs 0.030 af
Pond Rain Garden 3: Rain		6 af Inflow=0.99 cfs 0.124 af af Outflow=0.30 cfs 0.124 af
Pond Rain Garden 4: Rain	 5	3 af Inflow=0.27 cfs 0.034 af af Outflow=0.21 cfs 0.034 af
Pond Rain Garden 5: Rain		0 af Inflow=0.00 cfs 0.000 af af Outflow=0.00 cfs 0.000 af
Link Site: Site		Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af
Total Runoff		verage Runoff Depth = 0.43" .69% Impervious = 9.000 ac

### Summary for Subcatchment Basin 1 Imp: Basin 1 Imp

Runoff = 0.61 cfs @ 12.19 hrs, Volume= 0.077 af, Depth> 1.02" Routed to Pond Basin 1 : Basin 1

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D WQ storm Rainfall=1.25"

	Area	(ac)	CN	Desc	cription		
*	0.	500	98	Pave	ement		
*	0.	400	98	Root	-		
	0.	900	98	Weig	ghted Aver	age	
	0.	0.900 100.00% Impervious A				rvious Area	
	Тс	Leng	th	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	10.0						Direct Entry, pavement and pipe

# Summary for Subcatchment Basin 1 Pervious: Basin 1 - Pervious

Runoff = 0.00 cfs @ 5.00 hrs, Volume= Routed to Pond Basin 1 : Basin 1

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D WQ storm Rainfall=1.25"

	Area	(ac)	CN	Desc	cription		
*	0.	500	39	lawn	, A soils		
	0.500 100.00% Pervious Area						
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0						Direct Entry,

### Summary for Subcatchment Basin 2 - Pervious: Basin 2 - Pervious

Runoff = 0.00 cfs @ 5.00 hrs, Volume= Routed to Pond Basin 2 : Basin 2 0.000 af, Depth= 0.00"

0.000 af, Depth= 0.00"

	Area (ac)	CN	Description
*	4.050	39	lawn, A soils
	4.050		100.00% Pervious Area

Prepare		essiona	I Design S				WQ storm Rainfall=1.25" Printed 6/19/2023		
HydroCA	D® 10.20-3	5C S/N U2	223 © 202	3 HydroCAL	) Software Sol	utions LLC	Page 66		
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
15.0					Direct Entr	у,			
	Sumn	nary fo	r Subcat	chment I	Basin 2 Imj	pervious: basi	in 2 Impervious		
Runoff Route	Runoff = 1.87 cfs @ 12.19 hrs, Volume= 0.234 af, Depth> 1.02" Routed to Pond Basin 2 : Basin 2								
	Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D_WQ storm Rainfall=1.25"								
Area	(ac) CN	Deso	cription						
	600 98								
	450 98		•						
* 0.	700 98	B Drive	eways						
<u>* 1</u> .	000 98	B Roa	d & Sidewa	alk					
	750 98		ghted Aver						
2.	750	100.	00% Impe	rvious Area	a				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
10.0					Direct Entr	y, pavement			
	Summ	nary fo	r Subcat	chment I	Basin 3 Imj	pervious: basi	in 3 Impervious		

1.63 cfs @ 12.19 hrs, Volume= 0.204 af, Depth> 1.02" Runoff = Routed to Pond Basin 3 : Basin 3

Post Developed.

	Area	(ac)	CN	Desc	ription		
*	0.	900	98	Park	ing		
*	0.	300	98	Roof			
*	0.	500	98	Drive	ways		
*	0.	700	98	Road	& Sidewa	alk	
	2.	400	98	Weig	hted Aver	age	
	2.	2.400 100.00% Impervious Area			00% Impe	rvious Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	10.0						Direct Entry, pavement

# Summary for Subcatchment Basin 3 Pervious: Basin 3 - Pervious

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00" Routed to Pond Basin 3 : Basin 3

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D WQ storm Rainfall=1.25"

_	Area	(ac)	CN	Desc	cription		
*	1.	600	39	lawn	, A soils		
	1.	1.600 100.00% Pervious Area					
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0						Direct Entry,

# Summary for Subcatchment Rain Garden 1 Impervious: Rain Garden 1 Impervious

0.030 af, Depth> 1.02"

Runoff	=	0.24 cfs @	12.19 hrs,	Volume=
Routed	to Pond	Rain Garder	า 1 : Rain G	arden 1

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D WQ storm Rainfall=1.25"

Area	(ac) Cl	N Desc	cription				
<u>*</u> 0.	.350 9	8 Roof	f				
0.	.350	100.	00% Impe	rvious Area	а		
Tc	Length	Slope	Velocity	Capacity			
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)			
10.0					Direct Entry, pavement and pipe		
Sı	ummary	for Sul	ocatchm	ent Rain	Garden 1 Pervious: Rain Garden 1 Pervious		
Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00" Routed to Pond Rain Garden 1 : Rain Garden 1							

_	Area	(ac)	CN	Desc	cription		
*	1.	150	39	lawn	, A soils		
	1.150 100.00% Pervious Area				00% Pervi	ous Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0			(13,11)	(10,000)	(010)	Direct Entry,

# Summary for Subcatchment Rain Garden 2 Impervious: Rain Garden 2 Impervious

Runoff	=	0.24 cfs @	12.19 hrs,	Volume=	0.030	af, Depth>	1.02"
Routed	to Pond	l Rain Garde	n 2 : Rain G	arden 2		-	

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D WQ storm Rainfall=1.25"

	Area	(ac)	CN	Desc	cription		
*	0.	350	98	Roof	-		
	0.350 100.00% Impervious Area					rvious Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	10.0	(100		(1610)	(10000)	(010)	Direct Entry, pavement and pipe

# Summary for Subcatchment Rain Garden 2 Pervious: Rain Garden 2 Pervious

Runoff	=	0.00 cfs @	5.00 hrs,	Volume=	0.000 af,	Depth= 0.00"
Routed	to Pond	l Rain Garder	12 : Rain G	arden 2		

Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D WQ storm Rainfall=1.25"

	Area	(ac)	CN	Desc	cription		
*	1.	650	39	lawn	, A soils		
	1.	650		100.	00% Pervi	ous Area	
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	15.0						Direct Entry,

### Summary for Subcatchment Rain Garden 3 Impervious: Rain Garden 3 Impervious

Runoff = 0.99 cfs @ 12.19 hrs, Volume= 0.124 af, Depth> 1.02" Routed to Pond Rain Garden 3 : Rain Garden 3

	Area (ac)	CN	Description
*	0.450	98	Pavement
*	0.600	98	Roof
*	0.400	98	Driveway
	1.450	98	Weighted Average
	1.450		100.00% Impervious Area

Post DevelopedNAPrepared by Professional Design ServicesHydroCAD® 10.20-3c s/n 02223 © 2023 HydroCAD Software Solution	Post Developed. RCC 24-hr D WQ storm Rainfall=1.25" Printed 6/19/2023 ns LLC Page 69
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)	
10.0 Direct Entry, p	pavement and pipe
Summary for Subcatchment Rain Garden 3 Per	rvious: Rain Garden 3 Pervious
Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.0 Routed to Pond Rain Garden 3 : Rain Garden 3	000 af, Depth= 0.00"
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Tir NRCC 24-hr D WQ storm Rainfall=1.25"	ne Span= 5.00-30.00 hrs, dt= 0.05 hrs
Area (ac) CN Description	
* 1.350 39 lawn, A soils	
1.350 100.00% Pervious Area	
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)	
15.0 Direct Entry,	
Summary for Subcatchment Rain Garden 4 Imper	rvious: Rain Garden 4 Impervious
Runoff = 0.27 cfs @ 12.19 hrs, Volume= 0.0 Routed to Pond Rain Garden 4 : Rain Garden 4	034 af, Depth> 1.02"
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Tir NRCC 24-hr D WQ storm Rainfall=1.25"	ne Span= 5.00-30.00 hrs, dt= 0.05 hrs
Area (ac) CN Description	
* 0.400 98 Roof	
0.400 100.00% Impervious Area	
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)	
10.0 Direct Entry, p	pavement and pipe
Summary for Subcatchment Rain Garden 4 Per	rvious: Rain Garden 4 Pervious
Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.0 Routed to Pond Rain Garden 4 : Rain Garden 4	000 af, Depth= 0.00"
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Tin NRCC 24-hr D_WQ storm Rainfall=1.25"	
	ne Span= 5.00-30.00 hrs, dt= 0.05 hrs
Area (ac) CN Description	ne Span= 5.00-30.00 hrs, dt= 0.05 hrs
Area (ac)         CN         Description           *         0.600         39         lawn, A soils           0.600         100.00% Pervious Area	ne Span= 5.00-30.00 hrs, dt= 0.05 hrs

<b>Post Developed</b> Prepared by Professional Design Services HydroCAD® 10.20-3c s/n 02223 © 2023 HydroCAD Software Sol	NRCC 24-hr D WQ storm Rainfall=1.25" Printed 6/19/2023 Iutions LLC Page 70								
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)									
15.0 Direct Entr	ry,								
Summary for Subcatchment RG 5: Rain Garden 5									
Runoff = 0.00 cfs @ 5.00 hrs, Volume= Routed to Pond Rain Garden 5 : Rain Garden 5	0.000 af, Depth= 0.00"								
Runoff by SCS TR-20 method, UH=Delmarva, Weighted-CN, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs NRCC 24-hr D_WQ storm Rainfall=1.25"									
Area (ac) CN Description									
* 0.400 98 Roof									
<u>* 0.700 39 Lawn A soils</u> 1.100 60 Weighted Average									
0.700 63.64% Pervious Area									
0.400 36.36% Impervious Area									
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)	1								
10.0 Direct Entr	ry, pavement and pipe								
Summary for Pond Basin 1: Basin 1									
Inflow Area =7.400 ac, 49.32% Impervious, Inflow DeInflow =0.61 cfs @12.19 hrs, Volume=Outflow =0.20 cfs @12.00 hrs, Volume=Discarded =0.20 cfs @12.00 hrs, Volume=Primary =0.00 cfs @5.00 hrs, Volume=Routed to Pond Basin 2 : Basin 2	epth > 0.12" for WQ storm event 0.077 af 0.077 af, Atten= 67%, Lag= 0.0 min 0.077 af 0.000 af								

Post Developed.

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 70.37' @ 12.69 hrs Surf.Area= 0.034 ac Storage= 0.013 af

Routed to Pond Basin 2 : Basin 2

Plug-Flow detention time= 16.6 min calculated for 0.077 af (100% of inflow) Center-of-Mass det. time= 16.4 min (823.4 - 807.0)

Volume	Invert	Avail.Storage	Sto	rage Description	
#1	70.00'	0.200 af	rete	ention basin (Pri	ismatic)Listed below
Elevation (feet)	Surf.Are (acre			Cum.Store (acre-feet)	
70.00 71.00	0.03 0.04	0.0	)00 )35	0.000 0.035	
72.00 73.00 74.00	0.05 0.06 0.07	0.0	)45 )55 )65	0.080 0.135 0.200	

		Post Developed.
Post Developed	NRCC 24-hr D	WQ storm Rainfall=1.25"
Prepared by Professional Design Services		Printed 6/19/2023
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Device	Routing	Invert	Outlet Devices
#1	Discarded		0.20 cfs Exfiltration when above 70.00'
#2	Primary	72.00'	<b>4.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Primary	74.00'	<b>48.0" x 48.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Discarded OutFlow** Max=0.20 cfs @ 12.00 hrs HW=70.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.20 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=70.00' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs) 3=Orifice/Grate (Controls 0.00 cfs)

# Summary for Pond Basin 2: Basin 2

Inflow Area =	20.600 ac, 4	3.69% Impervious,	Inflow Depth > 0	.15" for WQ storm event
Inflow =	2.11 cfs @	12.19 hrs, Volume	e= 0.264 af	
Outflow =	1.00 cfs @	12.20 hrs, Volume	e= 0.264 af	, Atten= 53%, Lag= 0.5 min
Discarded =	1.00 cfs @	12.20 hrs, Volume	e= 0.264 af	
Primary =	0.00 cfs @	5.00 hrs, Volume	e= 0.000 af	
Routed to Link	Site : Site			

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 68.14' @ 12.52 hrs Surf.Area= 0.257 ac Storage= 0.042 af

Plug-Flow detention time= 20.8 min calculated for 0.263 af (100% of inflow) Center-of-Mass det. time= 20.6 min ( 827.6 - 807.0 )

Volume	Invert	Avail.Storag	e Sto	orage Description
#1	68.00'	3.600 a	af Cu	ustom Stage Data (Prismatic)Listed below x 1.2
Elevatio (fee 68.0	t) (acres	s) (acre	Store -feet) 0.000	(acre-feet)
69.0	• • • • • • • • • • • • • • • • • • • •	-	0.000	
70.0		-	0.350	
71.0	0 0.50	0	0.450	1.050
72.0	0.60	0	0.550	1.600
73.0	0 0.70	0	0.650	2.250
74.0	0.80	0	0.750	3.000
<u>Device</u> #1 #2	Routing Discarded Primary	68.00' 70.70'	1.00 cfs 3.0" Ve	Devices <b>fs Exfiltration when above 68.00'</b> <b>ert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Primary		-	<b>W x 42.0" H Vert. Orifice/Grate</b> C= 0.600 d to weir flow at low heads

**Discarded OutFlow** Max=1.00 cfs @ 12.20 hrs HW=68.09' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 1.00 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=68.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs) -3=Orifice/Grate (Controls 0.00 cfs)

# Summary for Pond Basin 3: Basin 3

Inflow Area =	6.000 ac, 45.83% Impervious, Inflow D	Depth > 0.41" for WQ storm event				
Inflow =	1.63 cfs @ 12.19 hrs, Volume=	0.204 af				
Outflow =	0.30 cfs @11.95 hrs, Volume=	0.204 af, Atten= 82%, Lag= 0.0 min				
Discarded =	0.30 cfs @11.95 hrs, Volume=	0.204 af				
Primary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af				
Routed to Pond Basin 1 : Basin 1						

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 72.30' @ 13.06 hrs Surf.Area= 0.198 ac Storage= 0.062 af

Plug-Flow detention time= 73.6 min calculated for 0.204 af (100% of inflow)	
Center-of-Mass det. time= 73.1 min ( 880.2 - 807.0 )	

Volume	Invert /	Avail.Storage	Storage Description
#1	72.00'	1.200 af	Custom Stage Data (Prismatic)Listed below x 1.2
Elevatio (fee 72.0 73.0 74.0 75.0 76.0	et) (acres 00 0.150 00 0.200 00 0.250 00 0.300	) (acre-fi ) 0. ) 0. ) 0.	
Device #1 #2 #3	Routing Discarded Primary Primary	Invert Ou 72.00' <b>0.3</b> 74.00' <b>3.0</b> 75.00' <b>42</b>	utlet Devices         30 cfs Exfiltration when above 72.00'         0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads         .0" W x 42.0" H Vert. Orifice/Grate C= 0.600         mited to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 11.95 hrs HW=72.07' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=72.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs) -3=Orifice/Grate (Controls 0.00 cfs)

# Summary for Pond Rain Garden 1: Rain Garden 1

Inflow Area =	1.500 ac, 23.33% Impervious, Inflow De	epth > 0.24" for WQ storm event
Inflow =	0.24 cfs @ 12.19 hrs, Volume=	0.030 af
Outflow =	0.24 cfs $\overline{@}$ 12.19 hrs, Volume=	0.030 af, Atten= 0%, Lag= 0.0 min
Discarded =	0.00 cfs @ 12.19 hrs, Volume=	0.000 af
Primary =	0.24 cfs @ 12.19 hrs, Volume=	0.030 af
Routed to Pond	Basin 2 : Basin 2	

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 78.00' @ 12.19 hrs Surf.Area= 0.060 ac Storage= 0.000 af

Plug-Flow detention time= 0.0 min calculated for 0.030 af (100% of inflow) Center-of-Mass det. time= 0.0 min ( 807.0 - 807.0 )

#1       78.00'       0.400 af       Custom Stage Data (Prismatic)Listed below (Recalc)         Elevation       Surf.Area       Inc.Store       Cum.Store         (feet)       (acres)       (acre-feet)       (acre-feet)         78.00       0.060       0.000       0.000         79.00       0.080       0.070       0.070	Volume	Invert Av	vail.Storage	e Storage Description
(feet)         (acres)         (acre-feet)           78.00         0.060         0.000	#1	78.00'	0.400 af	af Custom Stage Data (Prismatic)Listed below (Recalc)
80.000.1000.0900.16081.000.1200.1100.27082.000.1400.1300.400	(feet) 78.00 79.00 80.00 81.00	(acres) 0.060 0.080 0.100 0.120	(acre-fe 0.0 0.0 0.0	e-feet) (acre-feet) 0.000 0.000 0.070 0.070 0.090 0.160 0.110 0.270
Device Routing Invert Outlet Devices	Device R	Routing	Invert Ou	Outlet Devices
#1Discarded78.00'0.30 cfs Exfiltration when above 75.00'#2Primary80.00'3.0" Vert. Orifice/GrateC= 0.600Limited to weir flow at low head#3Primary58.00'42.0" x 48.0" Horiz. Orifice/GrateC= 0.600Limited to weir flow at low heads	#2 P	Primary	80.00' <b>3.0</b> 58.00' <b>42</b>	<b>3.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low head <b>42.0" x 48.0" Horiz. Orifice/Grate</b> C= 0.600

Discarded OutFlow Max=0.30 cfs @ 12.19 hrs HW=78.00' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=301.47 cfs @ 12.19 hrs HW=78.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs) -3=Orifice/Grate (Orifice Controls 301.47 cfs @ 21.53 fps)

# Summary for Pond Rain Garden 2: Rain Garden 2

Inflow Area =	2.000 ac, 17	7.50% Impervious	Inflow Depth >	0.18" 1	for WQ storm event		
Inflow =	0.24 cfs @	12.19 hrs, Volume	e= 0.030	af			
Outflow =	0.21 cfs @	12.27 hrs, Volume	e= 0.030	af, Atten	n= 12%, Lag= 4.8 min		
Discarded =	0.21 cfs @	12.27 hrs, Volume	e= 0.030	af			
Primary =	0.00 cfs @	5.00 hrs, Volum	e= 0.000	af			
Routed to Pond Basin 3 : Basin 3							

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs

Peak Elev= 75.03' @ 12.27 hrs Surf.Area= 0.055 ac Storage= 0.002 af

Plug-Flow detention time= 5.7 min calculated for 0.030 af (100% of inflow) Center-of-Mass det. time= 5.3 min (812.4 - 807.0)

Volume	Invert	Avail.Storage	e Storage Description
#1	75.00'	0.300 at	af Custom Stage Data (Prismatic)Listed below (Recalc)
Elevatio (fee 75.0 76.0 77.0 78.0 79.0	et) (acres 00 0.055 00 0.065 00 0.065 00 0.075 00 0.075 00 0.085	) (acre- 5 C 5 C 5 C 5 C	Store         Cum.Store           -feet)         (acre-feet)           0.000         0.000           0.060         0.060           0.070         0.130           0.080         0.210           0.090         0.300
<u>Device</u> #1 #2 #3	Routing Discarded Primary Primary	75.00' <b>0</b> 77.00' <b>3</b> 79.00' <b>4</b>	Outlet Devices         0.30 cfs Exfiltration when above 75.00'         3.0" Vert. Orifice/Grate       C= 0.600         Limited to weir flow at low heads         Limited to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 12.27 hrs HW=75.03' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=75.00' (Free Discharge)

**2=Orifice/Grate** (Controls 0.00 cfs)

-3=Orifice/Grate (Controls 0.00 cfs)

# Summary for Pond Rain Garden 3: Rain Garden 3

Inflow Area =	2.800 ac, 51.79% Impervious, Inflow D	Depth > 0.53" for WQ storm event
Inflow =	0.99 cfs @ 12.19 hrs, Volume=	0.124 af
Outflow =	0.30 cfs @ 12.10 hrs, Volume=	0.124 af, Atten= 70%, Lag= 0.0 min
Discarded =	0.30 cfs @ 12.10 hrs, Volume=	0.124 af
Primary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af
Routed to Pond	d Basin 2 : Basin 2	

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 75.17' @ 12.72 hrs Surf.Area= 0.167 ac Storage= 0.026 af

Plug-Flow detention time= 30.9 min calculated for 0.124 af (100% of inflow) Center-of-Mass det. time= 30.4 min (837.4 - 807.0)

Volume	Invert	Avail.Storage	Storage Description
#1	75.00'	2.000 af	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevatio (fee		urf.Area (acres)		c.Store re-feet)		n.Store re-feet)
75.0	00	0.150		0.000		0.000
76.0	00	0.250		0.200		0.200
77.0	00	0.350		0.300		0.500
78.0	00	0.450		0.400		0.900
79.0	00	0.550		0.500		1.400
80.0	00	0.650		0.600		2.000
Device	Routing		Invert	Outlet D	evices	
	<b>D</b> <sup>1</sup>		75 001			

#1	Discarded	75.00'	0.30 cfs Exfiltration when above 75.00'
#2	Primary	77.00'	<b>3.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Primary	79.00'	42.0" x 48.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 12.10 hrs HW=75.06' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=75.00' (Free Discharge) **2=Orifice/Grate** (Controls 0.00 cfs)

-3=Orifice/Grate (Controls 0.00 cfs)

# Summary for Pond Rain Garden 4: Rain Garden 4

Inflow Area =	1.000 ac, 4	0.00% Impervious,	Inflow Depth >	0.41"	for WQ storm event
Inflow =	0.27 cfs @	12.19 hrs, Volume	= 0.034	af	
Outflow =	0.21 cfs @	12.33 hrs, Volume	= 0.034	af, Atte	n= 23%, Lag= 8.1 min
Discarded =	0.21 cfs @	12.33 hrs, Volume	= 0.034	af	-
Primary =	0.00 cfs @	5.00 hrs, Volume	e= 0.000	af	
Routed to Pond	l Basin 2 : Bas	sin 2			

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 75.04' @ 12.33 hrs Surf.Area= 0.085 ac Storage= 0.003 af

Plug-Flow detention time= 10.8 min calculated for 0.034 af (100% of inflow) Center-of-Mass det. time= 10.3 min (817.4 - 807.0)

Volume	Invert	Avail.Storage	Storage	e Description	
#1	75.00'	0.550 af	Custor	m Stage Data	(Prismatic)Listed below (Recalc)
Elevation (feet)	Surf.Are (acre			Cum.Store (acre-feet)	
75.00	0.08	85 0.0	000	0.000	
76.00	0.09	95 0.0	090	0.090	
77.00	0.10	0.1	100	0.190	
78.00	0.1	15 0. <sup>-</sup>	110	0.300	
79.00	0.12	25 0.1	120	0.420	
80.00	0.13	35 0. <sup>-</sup>	130	0.550	

		Post Developed.
Post Developed	NRCC 24-hr D	WQ storm Rainfall=1.25"
Prepared by Professional Design Services		Printed 6/19/2023
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Device	Routing	Invert	Outlet Devices
#1	Discarded	75.00'	0.30 cfs Exfiltration when above 75.00'
#2	Primary	77.00'	<b>3.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads
#3	Primary	79.00'	42.0" x 48.0" Horiz. Grate C= 0.600
			Limited to weir flow at low heads

**Discarded OutFlow** Max=0.30 cfs @ 12.33 hrs HW=75.03' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.30 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=75.00' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs) 3=Grate (Controls 0.00 cfs)

# Summary for Pond Rain Garden 5: Rain Garden 5

Inflow Area =	1.100 ac, 30	6.36% Impervious, Inflow	Depth = 0.00"	for WQ storm event
Inflow =	0.00 cfs @	5.00 hrs, Volume=	0.000 af	
Outflow =	0.00 cfs @	5.00 hrs, Volume=	0.000 af, Atte	en= 0%, Lag= 0.0 min
Discarded =	0.00 cfs @	5.00 hrs, Volume=	0.000 af	
Primary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af	
Routed to Pond	l Basin 2 : Bas	in 2		

Routing by Stor-Ind method, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs Peak Elev= 73.00' @ 5.00 hrs Surf.Area= 0.085 ac Storage= 0.000 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= (not calculated: no inflow)

Volume	Invert /	Avail.Storage	e Stora	ge Description	
#1	73.00'	0.550 a	f Cust	om Stage Data	(Prismatic)Listed below (Recalc)
Elevatio (fee			Store feet)	Cum.Store (acre-feet)	
73.0	0.085	5 (	000.	0.000	
74.0	0.095	5 (	.090	0.090	
75.0	0.105	5 (	.100	0.190	
76.0	0.115	5 (	).110	0.300	
77.0	0.125	5 (	.120	0.420	
78.0	0 0.135	5 (	.130	0.550	
Device	Routing	Invert (	utlet De	vices	
#1	Discarded			Exfiltration whe	
#2	Primary	-			C=0.600 Limited to weir flow at low heads
#3	Primary			8.0" Horiz. Grat weir flow at low	

**Discarded OutFlow** Max=0.00 cfs @ 5.00 hrs HW=73.00' (Free Discharge) **1=Exfiltration** (Controls 0.00 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=73.00' (Free Discharge) -2=Orifice/Grate (Controls 0.00 cfs) -3=Grate (Controls 0.00 cfs)

# Summary for Link Site: Site

Inflow Area	a =	20.600 ac, 43	3.69% Impervious,	Inflow Depth = 0.	00" for WQ storm event
Inflow	=	0.00 cfs @	5.00 hrs, Volume	= 0.000 af	
Primary	=	0.00 cfs @	5.00 hrs, Volume	= 0.000 af,	, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-30.00 hrs, dt= 0.05 hrs

# **Post Developed**

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### PROFESSIONAL ENGINEER'S GROUNDWATER MOUNDING ANALYSIS CERTIFICATION Submitted to STATE OF NEW JERSEY PINELANDS COMMISSION PO BOX 7 NEW LISBON, NJ 08064

#### Part A. General Information

Pinelands Application Number:					
Project Location	n: Ridgeway Road				
Municipality:	Manchester Township				
Block(s): 6	55	Lot(s):	11, 12, 13 & 14		

1. Facility Location: Either latitude and longitude for the approximate canter each stormwater Infiltration facility, or electronic map or site plan.

Facility a.	Basin
Facility b.	
Facility c.	
Facility d.	
Facility e.	

#### Part B. Professional Engineer's Certification

I hereby certify that, pursuant to the requirements of the Pinelands Comprehensive Management Plan (N.J.A.C. 7:50-6.84(a)6.iv.(3)), I have performed a groundwater mounding analysis for each of the stormwater infiltration facilities identified in Part A, above, for the purpose of assessing the hydraulic impacts on the water table from infiltrating stormwater runoff from the maximum design storm. I further certify the infiltration of stormwater or groundwater to breakout to the land surface of cause any changes to the hydrology of adjacent water bodies, wetlands or cause adverse impacts to subsurface structures, including, but not limited to basements and septic systems. In performing this analysis, I utilized the following methods:

MODRET

[Specify mounding analysis method(s)]

(Signature and seal)

39915

(License Number) April 25, 2022

William Stevens

(Name - Type or Print)

(Date)

# **TIME TO DRAIN CALCULATIONS**

Basin 1: Exfiltration Area

: Bottom area

Exfiltration rate at 3 in/hour

= 0.00007 ft/sec

Basin #	Bottom Area(af)	Rate (cfs)	Volume(af)	Time (hrs)
RG1	0.06	0.19	0.16	9
RG2	0.055	0.17	0.13	9
RG3	0.15	0.45	0.50	13
RG4	0.085	0.26	0.19	8.8
1	0.30	0.91	0.80	11
2	0.30	0.91	2.4	32

**APPENDIX C** 

**COLLECTION SYSTEM COMPUTATIONS** 

# **APPENDIX D**

# SOIL EROSION CALCULATION

# OUTLET PROTECTION CALCULATIONS OFSITE STABILITY CALCULATIONS SEDIMENT BASIN CALCULATIONS

### **CONDUIT OUTLET DESIGN**

Use 25 Year storm, Q (cfs)

#### Level Apron

Tw(ft) calculated from:

- (1) 2 Year flood routing for outlets into stormwater management basins
- (2) outlets from basins use 0.2 \* D

q = Q/Wo

Calculate length & width of rip rap apron: For  $Tw < \frac{1}{2}$  Pipe Size

- Length = (1.8 q/Do1/2) + 7Do
- Width = 3 Wo + L

For  $Tw > \frac{1}{2}$  Pipe Size

- Length = 3 q/Do1/2
- Width = 3 Do + 0.4 L

Calculate D50 stone size (in):

 $= \frac{0.02}{Tw} (q)^{1.33}$ 

# **Scour Hole**

Depth = 0.5(Do)

Width = 2 Wo Length = 3 Do

 $D50 = \frac{0.0125}{TW} q^{1.33}$ 

Outlet #	<u>Do</u>	<u>Wo</u>	<u>Q</u>	<u>Tw</u>	<u>q</u>	<u>L</u>	W	<u>D50</u>
1-1	18	18	7	0.8 (1)	4.7	12	10	3"
1-2	18	18	7	0.8 (1)	4.7	12	10	3"
2-1	18	18	7	0.8 (1)	4.7	12	10	3"
2-2	18	18	7	0.8 (1)	4.7	12	10	3"
3-1	18	18	7	0.8 (1)	4.7	12	10	3"
3-2	18	18	7	0.8 (1)	4.7	12	10	3"

# **OFF-SITE STABILTY**

The basins have been designed to comply with the off-site stability standard. The discharge from the system is basin 2 having an outlet towards Ridgeway Road. There is no discharge to an undeveloped or unpaved surface so the project meets the requirements for off-site stability.

# **SEDIMENT BASIN DESIGN**

-

### 1.0 **DESCRIPTION**

It is necessary to control and prevent off-site sedimentation from the project site during construction. It is proposed to utilize the basin as a sediment basin during construction.

#### 2.0 <u>REGULATORY STANDARDS</u>

### A. <u>Applicable Regulations</u>

The Standards for Soil Erosion and Sediment Control contains standards for the design and construction of sediment basins (chapter 26). Sediment basins are permitted where failure of the basin will not result in loss of life or damage to homes, buildings, highways, railroads or public utilities. The maximum drainage area is 320 acres and the maximum height of the dam is 20 feet. The basin must be designed in accordance with the standards contained in Chapter 26.

The sediment basin will outlet into the existing natural drainage system by the outlet structure. This report demonstrates off-site stability at the point of discharge and downstream of the discharge point.

### 3.0 PROPOSED SEDIMENT BASIN PLAN

The contributory drainage area to the basin is less than 320 acres and the dam height is less than 20 feet (5 feet).

Each basin will be designed assuming the entire contributory drainage area is disturbed and non-vegetated. Sediment will be removed from the basin quarterly.

#### 4.0 **METHODOLOGY and DESIGN**

Drainage Area = 12 Acres Disturbed Area = 1240 Acres
Time for Development = one year with quarterly removal of sediment
Determine Minimum Basin Volume
I Determine Trap Efficiency
Set trap efficiency at 75%
From curve 26-1 find C/I = $0.025$ (coarse sediment)
Average surface runoff for Toms River = $25$ inches
I = (25  in.)(1  ft./12  in.)(12  ac.)
I = 18  ac. ft.
C = 18  ac. ft. (0.025)
C = 0.44 ac. ft. minimum Sediment Basin Volume
II. 1. Determine Volume for Sediment Storage Capacity
Construction Area
(DA)(A) = 12  ac.  x 60  tons/ac./yr = 720  tons /yr.
Determine DR, Delivery Ratio
12/640 = 0.018 sq. mi
From curve 26-2 $DR = 20\%$ for sand
Determine the density of aerated sand
From Table 26-1 use 90 lbs./cf.
Determine the volume for the sediment storage for the life of the basin.
V = (DA)(A)(DR)(TE)(1/S)(2000 lbs./ton)(1/43560 sf./ac.)
V = (720)(0.20)(0.75)(1/90)(2000)(1/43560)
V = 0.03 ac. ft.
2. Determine the volume for the temporary floodwater storage
The required floodwater storage volume below the principal spillway is 0.5 ac ft
based upon a drainage area of 12 acres, CN of 86 and a discharge from the principal spillway of
5 cfs. The required storage volume is provided at the principal spillway peak elevation

principal spillway of 5 cfs. The required storage volume is provided at the principal spillway peak elevation.

Total required volume is 0.5 ac. ft. + 0.03 ac. ft. = 0.53 ac. Ft.

Use the larger of two values: I = 0.44 ac. ft. II = 0.53 ac. ft

Required basin volume to provide temporary floodwater storage governs, 0.53 ac. ft. is required. The basin provides 1.0 ac. ft. of storage volume below the principal spillway. The basin has adequate storage volume. Flood routing of the 2 year, 24 hour storm event through the sediment basin assuming the basin is full to the primary outlet is included in the report.