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Modèle à densité constante

$$P(r) = \int_{r}^{R} \frac{Gm\rho}{r^{2}} dr \qquad m(r) = \frac{4\pi}{3}r^{3}\rho = M\frac{r^{3}}{R^{3}} \qquad \rho = \frac{3M}{4\pi R^{3}}$$

$$= \frac{3GM^{2}}{8\pi R^{6}}(R^{2} - r^{2})$$

$$T(r) = \frac{P}{\rho} \frac{\mu m_{u}}{k} = \frac{GM}{R^{3}} \frac{\mu m_{u}}{2k}(R^{2} - r^{2})$$

$$\frac{T}{P} = \frac{1}{\rho} \frac{\mu m_{u}}{k} = cst. \implies \frac{d\ln T}{d\ln P} = \frac{1}{2} \implies 2/5$$
Hyper instable vis-à-vis de la convection !
Un tel modèle n'est pas réaliste, la densité doit augmenter vers le centre pour
que dhT/dhP \constant 1 - dhp/dh P soit suffisamment petit.







Modeles de polytropesPoisson
$$\frac{1}{r^2} \frac{d}{dr} \left(r^2 \frac{d\phi}{dr} \right) = 4\pi G \rho = 4\pi G \left[\frac{-\phi}{K(n+1)} \right]^n$$
Changement de variables
te adimensionalisation $z = Ar$, $w = \frac{\phi}{\phi_c} = \left(\frac{\rho}{\rho_c}\right)^{1/n}$
 $A^2 = \frac{4\pi G}{(n+1)^n K^n} (-\phi_c)^{n-1} = \frac{4\pi G}{(n+1)K} \rho_c^{\frac{n-1}{n}}$ **Equation de**
Lane-Emden $\frac{1}{z^2} \frac{d}{dz} \left(z^2 \frac{dw}{dz}\right) + w^n = 0$
 $w(0) = 1$, $w'(0) = 0$























































$$\begin{aligned} \text{Les réactions nucléaires} \\ \text{Détermination de la section efficace } \sigma(E) \\ \sigma(E) &= (1/E) P_G S(E) = \frac{S(E)}{E} \exp(-b E^{-1/2}) \\ \sigma(v) &= \int_0^\infty \sigma(E) v(E) f(E) dE \\ &= \int_0^\infty \frac{S(E)}{E} \exp(-bE^{-\frac{1}{2}}) \sqrt{\frac{2E}{m_\mu}} \frac{2}{\sqrt{\pi}} \frac{E}{kT} \exp\left(-\frac{E}{kT}\right) \frac{dE}{(kTE)^{\frac{1}{2}}} \\ &= \left(\frac{8}{\mu\pi}\right)^{\frac{1}{2}} \frac{1}{(kT)^{\frac{3}{2}}} \int_0^\infty S(E) \exp\left(-\frac{E}{kT} - bE^{-\frac{1}{2}}\right) dE \end{aligned}$$





Les méactions nucléaires

$$\begin{aligned}
\langle \sigma v \rangle &= \left(\frac{8}{\mu\pi}\right)^{\frac{1}{2}} \frac{S_0}{(kT)^{\frac{3}{2}}} \int_0^{\infty} \exp\left(-\frac{E}{kT} - \frac{b}{\sqrt{E}}\right) dE \\
\end{aligned}$$
Approx, par une gaussienne

$$exp\left(-\frac{E}{kT} - \frac{b}{\sqrt{E}}\right) &= exp(-f(E)) \\
\approx exp(-f(E_0)) exp\left(-\left(\frac{E-E_0}{\Delta E/2}\right)^2\right) \\
\end{aligned}$$

$$\begin{aligned}
f'(E_0) &= 0 \Rightarrow E_0 = \left(\frac{bkT}{2}\right)^{2/3} \\
\tau &= f(E_0) = 3E_0/(kT) \propto T^{-1/3} \\
\Delta E &= \sqrt{8/f''} = 4\sqrt{E_0kT/3} \propto T^{5/6} \\
\end{aligned}$$

$$\begin{aligned}
exp\left(-\frac{T^{-3/2}}{2}\Delta E e^{-f(E_0)} \\
\approx T^{-3/2}T^{5/6}e^{-\tau} \\
\approx \tau^2 e^{-\tau}
\end{aligned}$$











































3. Process	us trois alphas (T > 100 10º K)	
	${}^{4}_{2}He + {}^{4}_{2}He \Leftrightarrow {}^{8}_{4}Be$	
	${}^{8}_{4}Be + {}^{4}_{2}He \rightarrow {}^{12}_{6}C + \gamma$	
	${}^{12}_{6}C + {}^{4}_{2}He \rightarrow {}^{16}_{8}O + \gamma$	
	${}^{16}_{8}O + {}^{4}_{2}He \rightarrow {}^{20}_{10}Ne + \gamma$	
	$^{20}_{10}Ne + {}^{4}_{2}He \rightarrow {}^{24}_{12}Mg + \gamma$	
	14_{M} 4_{M} 18_{O} 0_{O} 0_{O}	
	${}_{7}^{IV} + {}_{2}^{II} e \rightarrow {}_{8}^{O} + {}_{1}^{I} e + {}_{0}^{V}$	








































































